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Technical Report No.107

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THREE-LINE ANALYSIS OF BATHYTHERMOGRAPHS

by

J. CAPERON, B. SCHIPMOLDER and W. HARWOOD

1 MARCH 1968



TECHNICAL REPORT NO. 107

SACLANT ASW RESEARCH CENTRE Viale San Bartolomeo 400 I 19026 - La Spezia, Italy

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APPROVED FOR DISTRIBUTION FOR THE DIRECTOR

R. WELLER Deputy Director

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ABSTRACT

A method of BT analysis that fits three straight-line segments to each set of digital BT data is described. These segments are identified, in descending order, with the mixed layer, the thermocline, and the deep layer. The associated slopes, temperature ranges, and depth ranges provide statistical abstractions that can be useful in ASWEPS procedures. The results of using this method for sampling the MILOC-64 data are discussed.

INTRODUCTION

The method of analysis of digital BT data to be described is completely automatic and objective after certain initial decisions have been made. It abstracts parameters that are considered relevant to sonar range prediction and amenable to prediction in an ASWEPS programme.

The method approximates the BT data with three contiguous straightline segments to give statistical representation of the gradients and depth ranges of the mixed layer, the thermocline, and the top section of the deep layer.

It is an attempt to explore ASWEPS techniques that lies somewhere between prediction of the total temperature profile (Ref. 1) and those techniques that rely only on layer depth and sea surface temperature (Ref. 2). Limitations in fundamental understanding of the air-sea interaction process, and limitations in the amount of current oceanographic and meteorological data available, circumscribe the accuracy of prediction of the complete profile. This should certainly be the ultimate aim of any ASWEPS programme, but such an attempt at present may well be premature. The essentially empirical approach based on sea surface temperature and layer depth seems perhaps too entirely empirical and fails to include parameters that are frequently critical to sonar range

predictions (Ref. 3). It is hoped that the present method of BT-data analysis will give results useful in evaluating possibilities for a compromise ASWEPS programme and that, if this method is successful, it will be an essential part of such a programme.

1. METHOD

The method used considers representations of the points of a single BT record by three connected straight lines. A best least-squares straight line is determined for each segment. The program selects that set of lines which results in a minimum sum of squares of temperature residuals.

For a given partition the number of points associated with the first, second, and third line segment are designated i1, i2, and i3. The sum of squares for i1 is calculated by

$$\sum_{k=1}^{i1} \left[t_k - \left(a + bd_k \right) \right]^2,$$

where t_k and d_k are respectively the temperature and the depth of the point k, and where

$$a = \left[\frac{\sum_{k=1}^{i_1} \left(t_k - bd_k \right) \right] / i_1,$$

and

$$\mathbf{b} = \left(\mathbf{i}_{1} * \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{d}_{k} \mathbf{t}_{k} - \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{d}_{k} \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{t}_{k}\right) / \left(\mathbf{i}_{1} * \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{d}_{k}^{\mathbf{i}_{2}} - \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{d}_{k} * \sum_{k=1}^{\mathbf{i}_{1}} \mathbf{d}_{k}\right),$$

The terms $\sum d_k$ and $\sum d_k^*$ are directly determined for equallyspaced depth values. The same calculations are made using similar formula for i2 and i3.

Each partition is examined, retaining the identification for only that partition which has so far resulted in a minimum sum of residuals over all three lines. Thus, at the end, the best-fit three-line segments have been found.

In practice it is found that some additional criteria improve the result by eliminating an occasionally anomalous solution that bears little relation to a correct oceanographic interpretation.⁴ The criteria **are**:

a. Parallel lines are excluded.

b. The depth of intersection of 1st and 2nd line segments, INT1D, must be equal to or less than the depth of intersection of the 2nd and 3rd line segments.

c. INT1D must be less than the depth of the first point of the second subset.

d. INT1D must be equal to or greater than the depth of the third from last point of the first subset.

e. The depth of intersection of the 2nd and 3rd line segment, INT2D, must be greater than the depth of the third from last point of the second subset.

f. INT2D must be equal to or less than the depth of the first point on the third line.

An optional feature of the analysis provides for separate treatment of surface transients superimposed on the mixed layer. The temperature gradient in the first 10 m and that between 10 and 25 m are calculated. If the difference between these two gradients is equal to or greater than 0.03°C per metre and this option is requested, then the points in the first 10 m are omitted from the three-line approximation. If the option is not called for, or the gradients differ by less than 0.03°C per metre, then all points are considered.

For many sets of BT data, large numbers of points are used in the third segment. In these cases it is possible to specify a minimum number of points to be included in the third segment without excluding the optimum partition. Specification of this number can be made by visual scanning of the analogue BT records. Selecting a value as large as possible will substantially reduce the computer processing time.

2. INPUT DATA

All information concerning the BT's is stored on magnetic tape (Ref. 4). For each BT there is a master block, a name block, and up to five data blocks. Each block corresponds to an 80-column punched card with one word per column and an extra word containing a sequential block number.

A punched paper tape specifies the BT's to be processed by listing the ship number, the starting BT number, and the ending BT number. The minimum number of points to be included in the third line segment, and whether or not the surface transient option is to be used, are also specified.

3. OUTPUT

An output magnetic tape contains

a. The number of points in each of the three subsets of the partition.

b. The slopes of the three lines and the temperature and depth coordinates of each of the end points of the three segments.

c. The sum, sum of squares, and sum of cross products for temperature and depth.

The original BT data is included on this output tape.

This output tape is a source tape for a program that generates a plot (e.g. Fig. 1) of the three lines and the original BT data. It is the source data for the output listing of the three-line data given in Table 1. Finally it forms the source data for statistical studies on the goodness-of-fit of the line segments and for general oceanographic interpretation of the BT data.



FIG. 1 EXAMPLE OF OUTPUT PLOT SHOWING ORIGINAL BT DATA AND THE THREE-LINE APPROXIMATIONS

TABLE 1

EXAMPLE OF PRINTED OUTPUT (see opposite)

SHIP	-	Ship's identification number
da moyr	=	Date, month, year
вт		BT number
TIME		
VAR	=	Standard error of estimate of first line segment
ம	-	Layer depth (metres)
ТО	=	Depth of bottom of thermocline (metres)
TRAN	IR	Temperature gradient in first 10 m
SL1	=	Temperature gradient of first line segment
SL2	=	Temperature gradient of second line segment
SL3	=	Temperature gradient of third line segment

SHIP	DA	MO	YR	BT	TIME	VAR	LD	TD	TRAN	SL1	SL2	SL3
6387	- 28	06	65	0009	0001	0.512	036	059	.000	004	190	006
€387	28	06	65	0010	0030	0.000	032	054	.000	.000	184	009
6387	28	06	65	0011	0100	0.305	042	082	.000	007	108	005
6387	28	06	65	0012	01 30	0,305	041	083	.000	013	089	007
6387	28	06	65	0013	0200	0.510	042	071	000	012	115	006
6387	28	06	65	0014	0300	-0.000	034	062	.000	000	124	005
6387	28	06	65	001 5	0330	0.067	047	072	000	001	140	004
6387	28	06	65	0016	0400	0.000	031	064	000	.000	102	005
6387	28	06	65	0017	0500	0.000	042	071	000	.000	106	007
6387	28	06	65	0018	0530	0.000	038	063	000	.000	124	006
					•							
6387	28	06	65	0019	0600	-0.000	026	058	.000	000	094	007
6387	28	06	65	0020	0700	0.031	033	053	000	.004	152	006
6387	28	06	65	0021	0730	0.039	028	057	000	002	112	004
6387	28	06	65	0022	0800	0.026	028	057	.000	.005	109	-,005
6387	28	06	65	0023	0900	0.000	032	053	.000	.000	154	005
6387	28	06	65	0024	0930	0.000	034	053	.000	.000	180	003
6387	28	06	65	0025	1000	0.604	037	052	000	008	210	004
6387	28	06	65	0026	1100	0.048	038	068	000	002	111	005
6387	28	06	65	0027	1130	0.053	033	062	010	007	116	005
6387	28	06	65	0028	1200	0,305	043	062	000	007	175	005
6387	28	06	65	0029	1300	0.165	033	063	010	011	102	005
6387	28	06	65	0030	1 3 3 0	0,122	045	073	.000	007	108	005
6387	28	06	65	0031	1400	0,968	047	067	000	013	138	007
6387	28	06	65	0032	1 500	0.178	037	072	010	005	098	006
6387	28	06	65	0033	1530	0.044	031	052	010	010	138	008
6387	28	06	65	0034	1600	0.026	027	062	010	005	087	008
6387	28	06	65	0035	1700	0.094	038	057	.000	007	162	007
6387	28	06	65	0036	1730	C.103	034	053	020	014	152	007
6387	28	06	65	0037	1800	0.450	037	067	010	035	082	006
6387	28	06	65	0038	1900	0.148	040	067	010	022	092	006
6387	28	06	65	0039	1930	0.224	038	062	020	028	094	005
6387	28	06	65	0040	2000	0.128	027	052	010	028	098	005
6387	28	06	65	0041	2100	0.053	035	061	.000	007	104	006
6387	28	06	65	0042	21 30	0.459	041	053	.000	025	180	008
6387	28	06	65	0043	2200	0.325	042	068	010	024	093	007
6387	28	06	65	0044	2300	1.100	057	083	010	008	110	-,010
6387	28	06	65	0045	2330	0.267	033	052	030	020	152	011
6387	28	06	65	0046	2400	0.768	043	072	040	022	110	008
6387	29	06	55	0047	0100	0.610	052	074	050	022	118	011
6387	29	06	65	0048	0130	1.857	052	067	010	020	-,160	008

4. TEST WITH MILOC 64 DATA

A test of the program was made on twenty randomly-selected BT's from the MILOC 64 Phase A data. The mean standard error for these BT's is given in Table 2. The depth of intersection of the first and second line segment can be identified with "layer depth" and is the point of separation between the first (mixed) layer and the thermocline.

Table 2 contains a comparison between the layer depth, so defined, and layer depths computed by an earlier program used to determine layer depth based on a consideration of curvature of the BT trace. The difference exceeds 2 metres in four cases. Results more consistent with a subjective determination are provided by the present method in three of these cases and by the older method in the fourth case. It is clear that whenever the concept of layer depth has real meaning the present method will nearly always give a good result unaffected by small thermocline superimposed on the mixed layer.

The mean standard error of estimate for the twenty cases is 0.145 °C. The success of the program for the MILOC 64 data is surprisingly good. These BT records were taken in September — during the cooling season. The mixed layer was uniformly evident and well represented by a straight line. It could be expected that this

condition would continue during the remainder of autumn and winter. Experience with the MILOC 65 data from June shows equally good fits in only 60 to 70% of the cases. The remaining cases show a strong transient in the first 5 to 15 metres due to heating. The analysis is of less value in these cases and, indeed, the concept of "layer depth" itself is of questionable importance here.

A copy of the computer program and data handling procedures are available from SACLANTCEN.

TABLE 2

		l	Standard Error		
BT No.	Ship	Old Method	Present Method	Absolute Diff.	for three lines (°C)
57		26	27	r 1	0.24
121	JOÃO DE LITSBOA	48	49	1	0.11
169	(06353)	43	41	2	0.17
164	(00000)	48	49	1	0.066
227		43	42	1	0.24
139		50	49	1	0,13
152		45	45	0	0.089
271	DALRYMPLE	48	24	4	0.15
587	(06354)	57	57	0	0.12
612		51	49	2	0.16
14		35	33	2	0.18
22		39	41	2	0.130
32	SVERDRUP	54	29	25	0.080
41	(06356)	31	29	2	0.14
48		53	44	9	0.14
8		33	30	3	0,28
130		54	55	1	0.12
147	MAHIA PAOLINA	54	54	O	0.099
175	(06357)	36	34	2	0.14
219		33	34	1	0.12

REFERENCES

- U.S. Naval Weather Service Computer Products Manual. NAVAIR 50-IG-522.
- 2. ASWEPS Concept, ASWEPS Manual Series, Vol. 1, SP 105, USN Hydrographic Office.
- 3. National Oceanographic Data Center, Manual Series Pub. M-3 (Provisional). Manual for processing Bathythermograph Data. Part 1, "Instructions for Manually Digitizing Bathythermograph Data".

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