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3000-HP ROLLER GEAR TRANSMISSION DEVELOPMENT PROGRAM. VOLUME IV. LABORATORY BENCH TEST

G. F. Gardner, et al

United Aircraft Corporation

Prepared for:

Army Air Mobility Research and Development Laboratory

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3000-HP ROLLER GEAR TRANSMISSION DEVELOPMENT PROGRAM

Volume IV - Laboratory Bench Test

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Sikorsky Aircraft
Division of United Aircraft Corporation
Stratford, Connecticut 06602



Final Report

Approved for public release; distribution unlimited.

Prepared for

EUSTIS DIRECTORATE

U. S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY Fort Eustis, Va. 23604

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EUSTIS DIRECTORATE POSITION STATEMENT

This report is one of six volumes of the final report under this contract. The objective of this program is to conduct research on the feasibility of a high-reduction ratio roller gear transmission of 3000 horsepower through experimental flight test. This report covers the 200-hour laboratory or bench test phase of the overall program. The roller gear unit is the 20:1 output stage of a growth S-61 type main transmission.

Laboratory back-to-back testing results indicated that the roller gear unit proved that it would perform for extended periods of time in the fatigue environment of a helicopter transmission. The major problems encountered in the earlier phases of testing were related to electron beam welding rather than to the roller gear concept. Specific details on the approach to solutions of the manufacturing problems with electron beam welding are presented in a separate final report of this contract.

The technical monitors for this contract were Messrs.

James Gomez and Leonard M. Bartone, Technology Applications Division.

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This report presents the results of dynamic load tests performed on a helicopter transmission which incorporates a roller gear drive unit as the main reduction stage. The primary purpose of this program was to conduct a 200-hour endurance test at 100 percent design speed and at a load spectrum equivalent to military helicopter usage.

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The transmission speed reduction from dual inputs operating at 18,966 rpm to the main rotor shaft speed of 203 rpm is via an input bevel mesh, combining spur gear reduction mesh and a 20:1 roller gear reduction output stage. Maximum operational input power is 1870 hp per input with the roller gear unit rated for 3000 hp.

The 200-hour endurance test was successfully completed after some design modifications to the roller gear assembly components. The changes, resulting from fractures originating at electron beam welded joints, were incorporated during initial development tests which preceded the 200-hour endurance test. Included in the transmission test program was a no-load lubrication test, a gear pattern development test, and an efficiency test.

Testing was primarily conducted in a regenerative test stand wherein two identical transmissions are coupled in a closed power path. An instrumentation system continuously monitored loads, speed, temperatures, oil flows and pressures. A chip detection system integral within the transmission provided warning of incipient failure.

The tests showed that the efficiency of the roller gear transmission is comparable to that of high reduction two-stage planetary transmissions of conventional design, and that the roller gear unit could perform for extended periods of time in the fatigue environment of a helicopter transmission.

The tests performed showed that the roller gear drive is a feasible reduction unit for helicopter main transmissions.

PREFACE

This report presents the results of a bench test development program to determine the feasibility of utilizing a high reduction ratio roller gear drive in a turbine-powered helicopter transmission system. The program was conducted at Sikorsky Aircraft for the Eustis Directorate of the U. S. Army Air Mobility Research and Development Laboratory, under Contract DAAJ02-69-C-0042 (Task 1G162203D14414). This contract resulted from a proposal submitted in March 1969 by Sikorsky Aircraft to conduct a two-phase program to design, fabricate and bench test a roller gear unit in a helicopter transmission (Phase I), and to ground test and flight test this transmission on an S-61 helicopter (Phase II). The bench test portion of this program was conducted under the cognizance of Mr. J. Gomez and Mr. L. Bartone, USAAMRDL representatives.

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INTRODUCTION

With the advent of the improved turbine power plants and with the demand for better performance, it has become necessary to provide helicopters with lighter, more efficient, and more reliable transmissions. One of the more interesting results of this search for improved transmissions has been the development of the roller gear drive transmission.

The roller gear drive is, basically, the combination of a planetary gear train with a roller traction drive. The rollers, besides contributing to the transmission of torque through rolling friction, provide the sole support for the planetary components. The only bearings needed for this type of gearbox are in the last row of pinions to react the torque through the system. If the roller gear drive is properly designed, these bearings react only tangential loads, not radial loads.

Development of the roller gear drive began in 1963 with a parametric study of the concept at TRV, Inc. This study examined the applicability of the roller gear drive principle to helicopter power trains. Various basic designs were examined to assure that no obstacles would preclude the use of the roller gear drive in helicopter transmissions. The possible effects on helicopter drive trains were also examined considering only state-of-the-art design methods and materials. The conclusion of this study was that the roller gear drive appeared to be superior to conventional planetaries with respect to weight, reliability, vibration life and efficiency.

Development work at TRII, Inc., continued in 1964 and 1965 with the design, fabrication, and testing of a roller gear power transmission capable of accepting 200 horsepower loads at 28,000 rpm. This transmission was tested for over 1000 hours in a regenerative test stand at TRU under the direction of Dr. Nasvytis. The successful completion of this test, with gearbox efficiencies running 98 percent and better, indicated that the roller gear drive was indeed a potentially valuable addition to helicopter transmission technology. It remained, however, to test a roller gear drive transmission at powers more representative of actual aircraft conditions.

In 1968 and 1969, the Bell Helicopter Company of Fort Worth, Texas, conducted an engineering design study to determine the feasibility of employing the roller gear concept in a transmission for the UH-1 helicopter. This study, which compared the roller gear drive to the existing UH-1 transmission and a new three-stage planetary design, showed that in the areas of efficiency and reliability the roller gear drive was the potentially superior design. The roller gear drive ranked last only in fabricability/cost of the areas examined, while

ranking second to the new three-stage planetary in weight. Meanwhile, TRW had proceeded to design and fabricate an 1100 hp roller gear drive unit for the U.S. Army Aviation Materiel Laboratories. This transmission, which converted an input speed of 21,000 rpm to an output speed of 325 rpm, was then tested in a regenerative test facility. The transmission logged 76.5 hours of testing before failures due to design deficiencies in roller gear components caused cessation of the test short of the 200-hour target. While this program was not an unqualified success, certain results, particularly efficiency, were especially encouraging, and the program did serve to delineate some of the difficult problems associated with the design and manufacture of a roller gear unit.

Sikorsky Aircraft became involved with the roller gear drive with a feasibility study, in 1966. This study examined the potential application of a roller gear drive to the CH-54 helicopter main transmission. While this study concluded that the roller gear drive was not feasibly applicable to this particular aircraft, it was this study and subsequent independent research and development studies into the roller gear drive by Sikorsky Aircraft which led to the present roller gear program for the S-61 aircraft.

Sikorsky Aircraft under contract with the Eustis Directorate of the U. S. Army Air Mobility Research and Development Laboratory is conducting a program involving the design, fabrication, and testing of a roller gear transmission for use with the Sikorsky Aircraft S-61 helicopter. This report covers the bench test segment of that program.

Under the bench test program, a total of five tests were performed:

- 1. No-Load Lubrication Test
- 2. Gear Pattern Development Test
- 3. Initial Development Test
- 4. 200-Hour Endurance Test
- 5. Efficiency Test

Inspections of the roller gear transmission were performed at the conclusion of each of these tests except the efficiency test which was performed coincidentally with the 200-hour endurance test. A complete teardown and inspection of the roller gear transmission was performed at the conclusion of the 200-hour endurance test. Included in this report are discussions of the procedures and facilities used for these tests as well as the results of inspections. The results of the tests and conclusions drawn from them are also presented. Brief discussions of the design and manufacture of the roller gear transmission are also included.

TRANSMISSION DESIGN

The roller gear drive consists of a roller friction drive compounded with a gear drive in a planetary or epicyclic arrangement. Earlier studies of feasibility and performance parameters by TRW, Bell, and Sikorsky (References 1, 2, 3 and 4) indicated that numerous advantages could be gained through the use of a roller gear drive in a helicopter transmission. Among these are improved efficiency, improved reliability, reduced height, reduced weight, and reduced gear noise.

Of primary importance to the operation of a roller gear drive unit such as that designed for the S-61 transmission shown in Figure 1 is the integration of rollers with the gears of the planetary gear train. These rollers, located on either side of the gear, have outside diameters coincident with the pitch diameters of the gears. Besides contributing to the transmission of torque through friction, these rollers support the gears in the optimum mesh position, i.e., parallel to each other at the pitch diameters. Parallel operation of gears at their pitch diameters is always desirable because in that position sliding friction is minimized, load is most evenly distributed, and contact is made across the greatest percentage of face width. With conventional means of support, positioning gears parallel to each other for operation at their pitch diameters is often difficult because of differential thermal expansion, manufacturing tolerances, and shaft deflections. These factors are eliminated or minimized with the roller gear drive.

Because of the use of rollers for support, conventional bearings are eliminated in all but the last row pinions where they are necessary to react the torque through the planetary system. A twofold saving of weight results from the elimination of the bearings. First, the total weight of the extra rolling surfaces on the gear cylinders is less than the corresponding bearing and bearing shaft weight. Second, the elimination of the bearings permits the use of the smallest gears compatible with load carrying ability. In conventional planetaries, the use of larger gearshafts is sometimes necessary to accommodate larger bearings needed to react shaft loads. In addition, the roller gear drive eliminates the centrifugal forces induced on bearing rollers or balls, making the roller gear design one of inherently longer life.

For the roller gear transmission development program, Sikorsky Aircraft chose its S-61 helicopter as the vehicle for which this advanced transmission was to be designed. This helicopter, which is in service commercially and with the Navy, Air Force, Coast Guard, Foreign Military, and U. S. Presidential Squadrons, is shown configured for the roller gear transmission in Figure 2. The design requirements for the roller gear transmission,

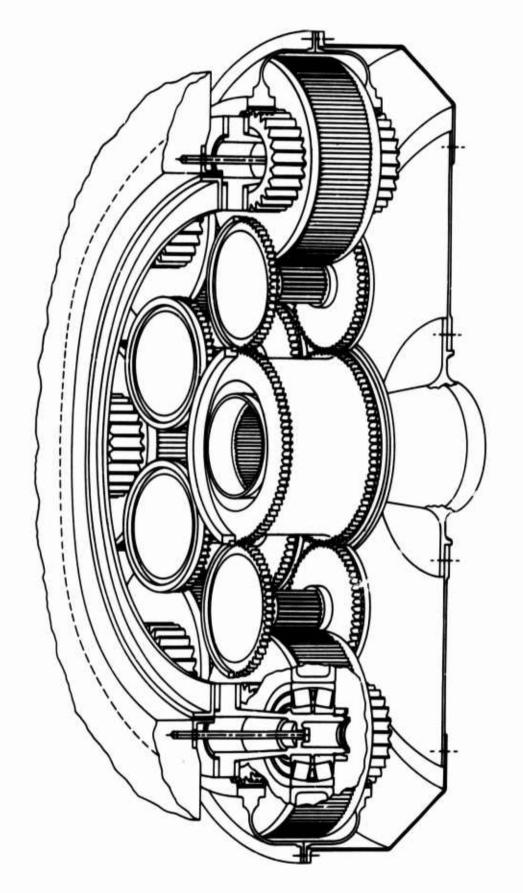
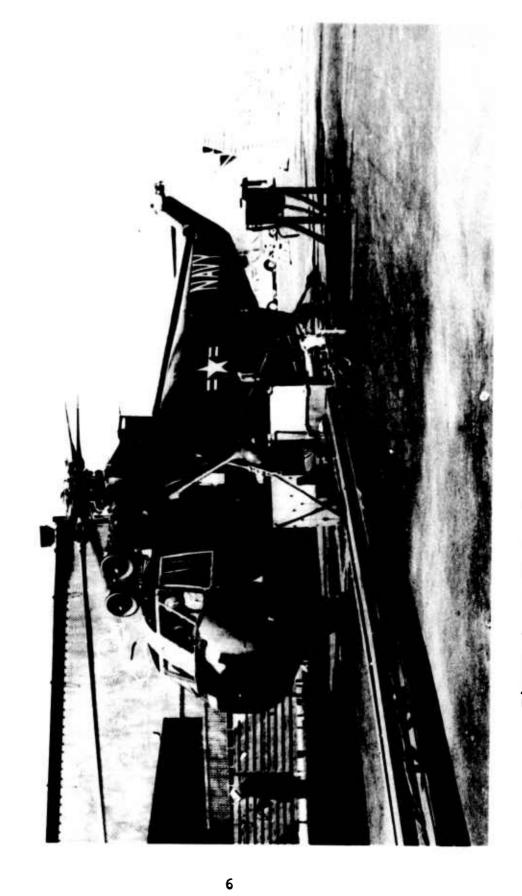


Figure 1. Roller Gear Drive Schematic.



S-61 Configured for Roller Gear Transmission. Figure 2.

outlined in Table I, are for a 27,000-pound gross weight growth version of the S-61. Design parameters for the roller gear unit are presented in Table II.

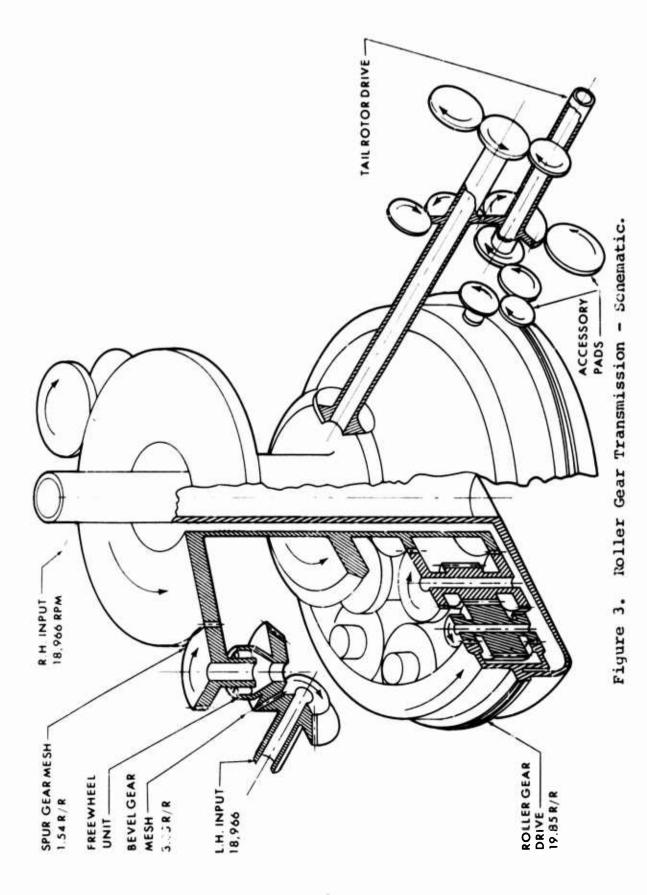
The main transmission, shown schematically in Figure 3, is divided into three reduction stages: input bevel mesh, combining spur mesh, and roller gear drive. The aft portion of the gearbox contains a bevel gear takeoff mesh and mounting pads for all accessories.

The gearbox cross-sectional drawing of Figure 4 shows the actual arrangement of the components. Input power is fed to the transmission from two T58-GE-16 engines rated at 1870 hp each. From each engine, power is transmitted to a spiral bevel gear mesh of 3.05 to 1 reduction, located on each side of the gearbox. The spiral bevel pinion of this mesh is mounted on a quadruple set of ball bearings lubricated centrifugally from an oil distribution tube inside the shaft. The centerline of the driven gear of the first-stage spiral bevel mesh is parallel to the main rotor shaft. This arrangement permits power from both engines to be transmitted through a spur gear combining mesh to the outer shaft, which has its centerline common with the main rotor shaft centerline. This second mesh, which has a 1.54 to 1 reduction ratio, provides a 32-inch spread between inputs to accommodate the side-by-side installation of the T53-GE-16 engines. Located between the first and second reduction stages on each engine drive train is a ramp roller type overrunning clutch. This clutch is designed with outer housing driving and can overrunning, to assure good lubrication to rollers, cam, and housing during freewheeling.

A spiral bevel gear attached to the lower portion of the outer shaft provides power for the tail and accessories through a speed increasing mesh. Power from the outer shaft is fed by means of a quill shaft to the 19.85 to 1 reduction ratio roller gear unit shown in Figure 5. This is a two-row roller gear drive with ring gear output, fixed carrier, and driving sun The sun gear, Figure 6, splits the power to the firstrow pinions into two paths to provide load equilibrium and to eliminate overturning moments about the axes of the pinions. The spline connection on the sun gear is centrally located to assure equal torsional deflection and therefore equal load on the gear teeth between both upper and lower paths. Two rollers, located on the ends of the sun gear, are concentric with the gear pitch diameters and are designed to equal the sun gear pitch diameter at full power when deflected by the induced roller radial loads. The sun gear is constrained in the axial direction by flanges on the ends of the rollers.

TABLE I. S-61 ROLLER GEA	R TRANSMISSION	DESIGN REQUIREMENTS
Location	Speed (rpm)	Power (hp max)
Input Drives		
Dual engine	18966	3700
Single engine	18966	1870
Main Rotor		
Roller Gear Output	203	3000
rail Takeoff Total	7031	700
Tail Rotor Takeoff	3025	565
Accessory Drives		
Generator (Left)	3100	54
Generator (Right)	8100	54
Tachometer	3900	1
Servo Hyd. Pump	4197	6.5
Aux Servo Hyd. Pump	4005	6.5
Utility Hyd. Pump	4005	13
Lubrication Pump	5149	4

TABLE II. ROLLER GEAR DRIVE DESIGN	PARAMETERS
Minimum Sun Gear Diameter	8.00 in.
Maximum Ring Gear Diameter	31.00 in.
Output rpm	203
Input rpm	4029
Reduction Ratio	19.84888:1
Gear Allowable Compressive Stress*	130,000 psi
Gear Allowable Bending Stress (one way)*	55,000 psi
Minimum Bearing Life	3,000 hr
Roller Allowable Compressive Stress	150,000 psi
* Using ACMA calculation method.	



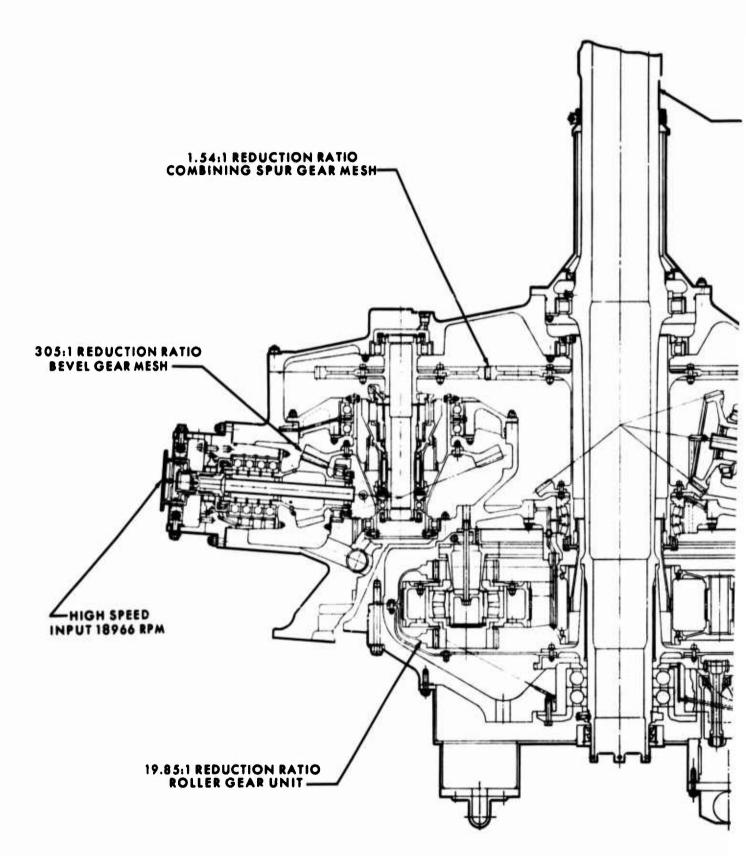
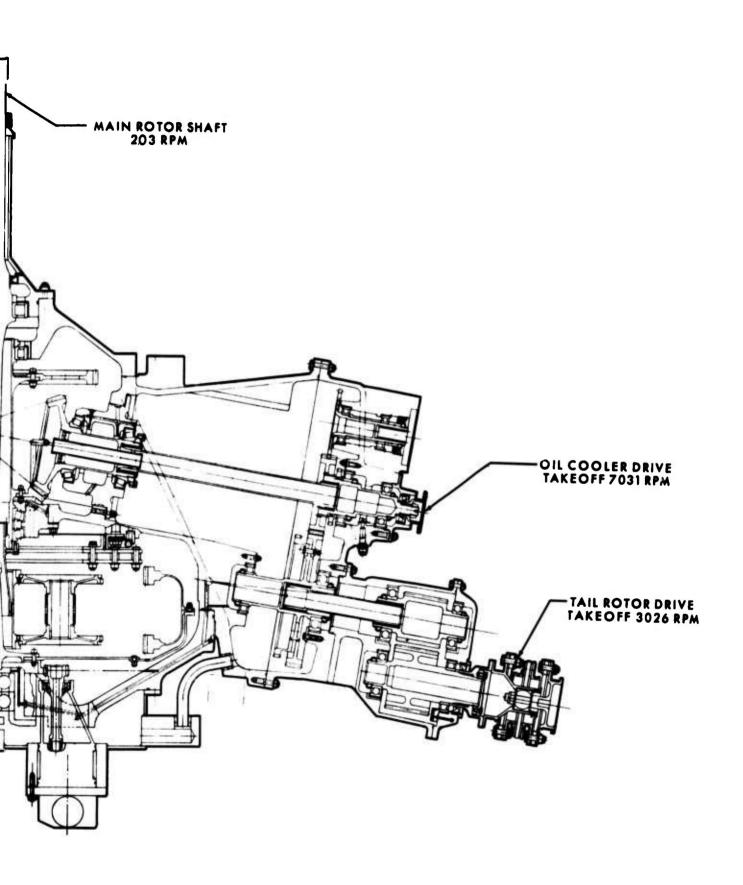


Figure 4. Roller Gear Transmission - Assembly.



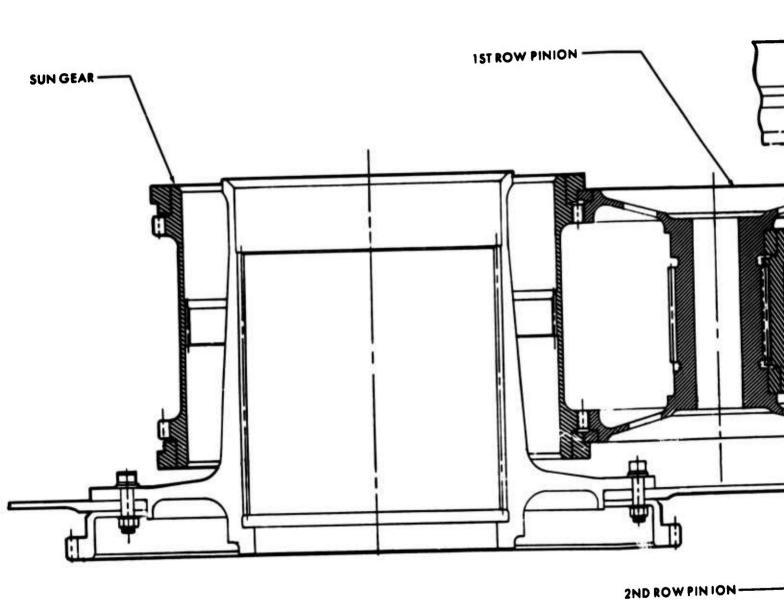
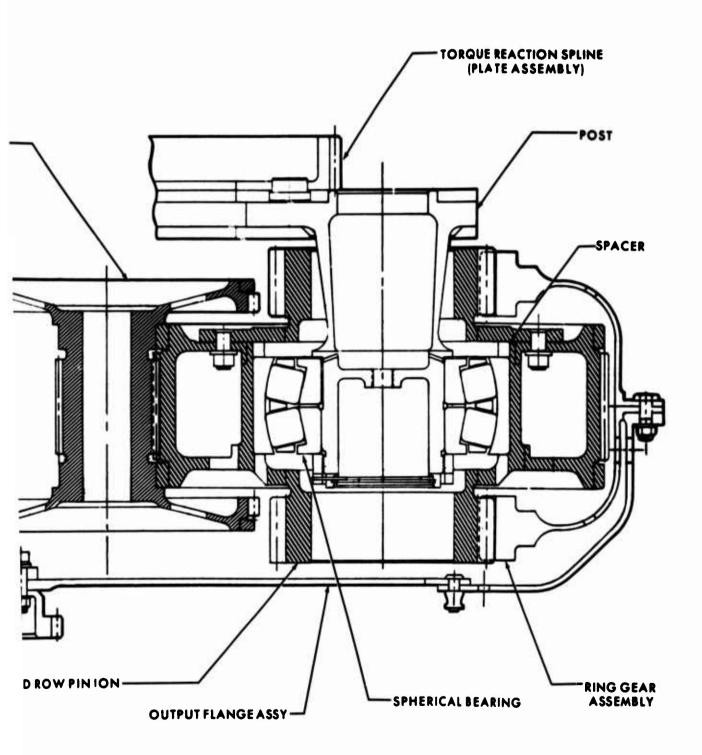


Figure 5. Roller Gear Drive.







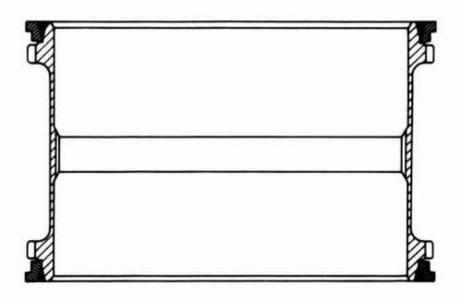


Figure 6. Sun Gear.



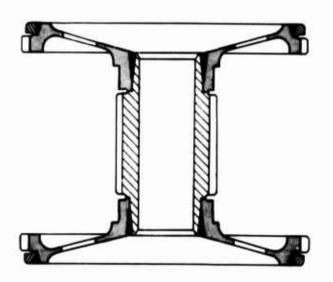
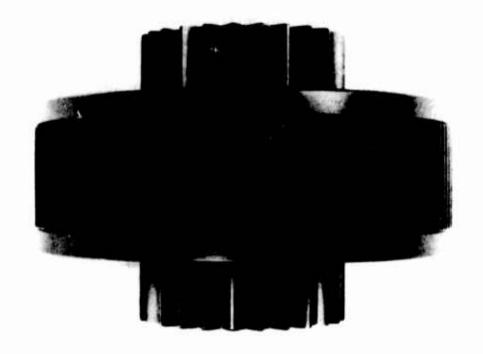


Figure 7. First-Row Pinion.



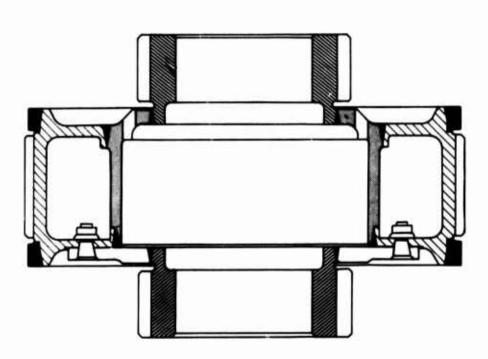


Figure 8. Second-Row Pinion.

The first-row pinion, Figure 7, contains two outer spur gears and rollers which mate with the sun gear, and an inner spur gear which mates with the two adjacent second-row pinions. The first-row pinion is accurately positioned at one point on the inside by the sun gear and at two points on the outside by the second-row pinions. This three-point support is inherently stable and obviates the need for bearing support. The inner rollers of the first-row pinions contain end flanges which constrain these pinions in the axial direction.

The second-row pinions, Figure 8, are supported at two inner points by the first-row pinions, and at one outer point by the ring gear. Spherical bearings are used to hold these pinions in place to react the torque. The internal clearances of the carrier plate reaction bearings are such that under the worst case of roller tolerances plus deflections, the bearings cannot react loads in the radial direction. These bearings react only loads in the tangential direction resulting from the reaction torque of the roller gear unit. The split ring gear, Figure 9, has no rollers since the resultant load on the second-row pinion is radially inward.

Figure 10 shows the arrangement of sun gear, first-row pinions, and second-row pinions, and Figure 11 shows the assembled roller gear unit. The basic data for the roller gear unit is presented in Table III.

	TABLE III. ROLLER	GLAR BASIC	DATA	
Location	Diametral Pitch	No. of Teeth	Pitch Diameter (in.)	Pressure Angle (deg)
Sun - a	9.448	84	8.89077	22.5
lst Row - X1	9.448	58	6.13387	22.5
lst Row - Y1	13.217	27	2.04282	25.0
2nd Row - X ₂	13.217	126	9.53318	25.0
2nd Row - Y2	5.583	25	4.47788	30.0
Ring - C	5.583	154	27.58374	30.0

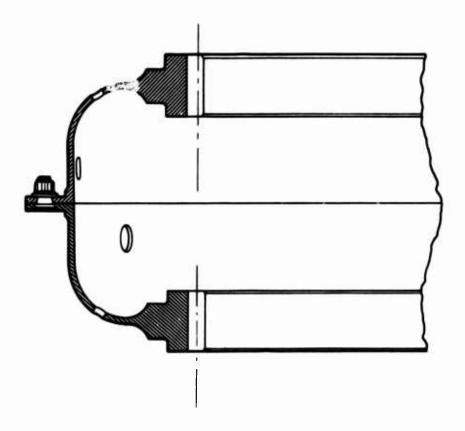


Figure 9. Ring Gear.

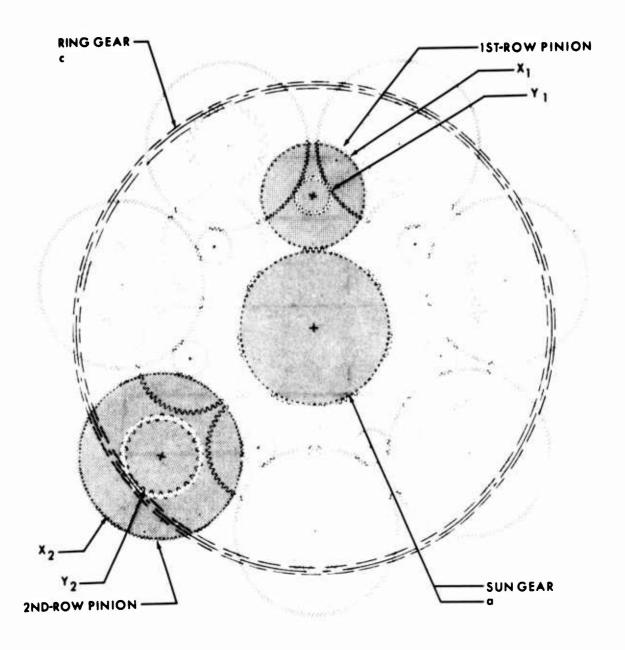


Figure 10. Roller Gear Component Arrangement.

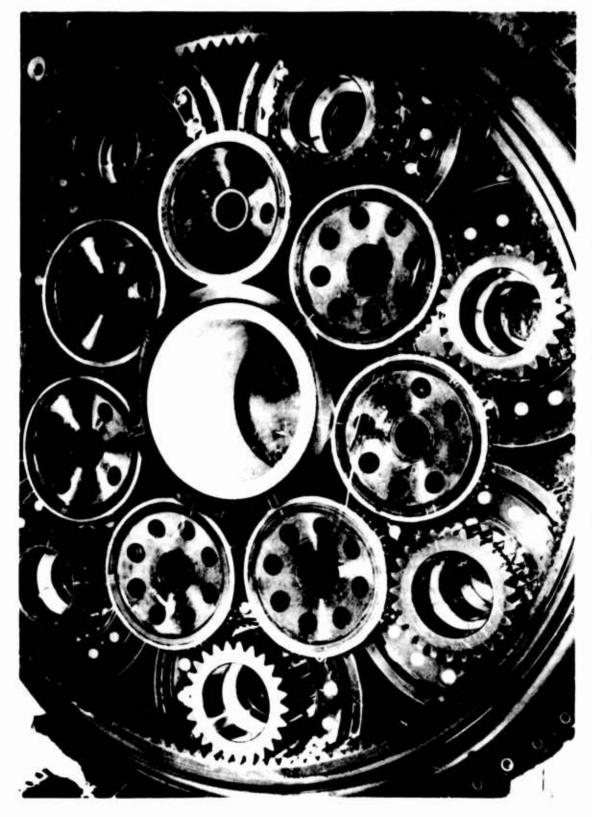


Figure 11. Roller Gear Unit - Assembly.

To ensure contact and proper location of "free" pinions such as the first-row pinions, earlier roller gear units used loading mechanisms that preloaded the first- and second-row pinions, holding them against one another and the sun gear. In these designs, the initial preload had to be sufficient to overcome the resultant gear loads at the maximum power to be transmitted.

The roller loads in the roller gear drive are a function of gear loads and roller gear geometry. Whenever torque is transmitted in the roller gear drive unit, tangential and radial gear tooth loads are induced. The rollers, which transmit loads normal to the rolling surface, must react the resultant loads from the gear teeth. Depending on the geometry and the gear tooth loads induced, the resultant roller loads may be either positive or negative and are directly proportional to horsepower. A negative roller load has no physical interpretation and indicates that the roller gear unit is unstable and tends to roll out of mesh. In this case, external preloading devices are required. However, by careful choice of roller gear design parameters, the roller reactive loads can be made to be always positive, thereby ensuring stability of the threepoint support. When the roller gear unit is designed so that all the roller loads are positive, the unit is said to be "self-preloading". This is achieved by using successively higher gear pressure angles for each gear mesh from sun gear to ring gear. The S-61 roller gear unit is a self-preloading unit and has no roller loads when at rest. As soon as power is applied, however, positive roller loads are generated, and all the roller gear members move radially inward to contact each other, thus forming a preloaded assembly. A summary of the preload forces is presented in Figure 12.

The S-61 roller gear drive also features a cantilever mounted cage post with double plate. The double plate effectively expands the cross section to obtain a higher moment of inertia for less weight. The carrier plate attachment to the main housing is accomplished with a splined connection. The male portion of the spline is attached to the carrier plate, while the female member is bolted to the main casting. During operation, the expansion of the magnesium housing with increasing operating temperature has no effect on the carrier plate since the splined connection simply repositions itself. The carrier to housing connection is therefore temperature compensated.

Figure 12. Roller Preload Forces.

The compound planetary arrangement of the roller gear drive pinions requires precise timing of the teeth. Tooth timing is achieved during manufacture and assembly and is best explained by the first-row pinion of Figure 13. In Figure 13, the two large outer gears are timed to each other during manufacture by holding the angular position of the teeth of the gear on one end to within +0.0002 inch of the angular position of the teeth on the other end. These outer gears can be imagined as one complete gear with the center portion removed.

The angular positions of the teeth of the inner gear are also precisely positioned during manufacture relative to the angular position of the teeth of the outer gears. A tooth is chosen on the outer gear and is marked as the index tooth. The angular positions of the teeth on the inner gear are then held to the master index tooth on the outer gear as shown by the dimension "X" in Figure 13. This dimension "X" may be any value, but is to be the same within ± 0.0002 inch for all gears in any one assembly.

The teeth of the gears on the second-row pinions are timed in a similar manner to the teeth of the first-row pinions.

The need for holding the timing of these gears all the same becomes obvious when examining the plan view of the roller gear unit, Figure 14. If for example, the teeth of any one of the gears were rotated to another angular position without rotation of the corresponding teeth of the other pinions, it is seen that the mating gear will not mesh properly; i.e., the tooth will no longer line up with a space on the mating gear.

During assembly of the roller gear unit, the master index teeth of all pinions must be aligned in the same angular relationship to their mating gears. If they are not, the ring gear, which is the last gear to be assembled, will not mesh with the teeth of the second-row pinions, since the teeth of one or more pinions will be rotated to an incorrect position. A final assembly check is made by examination of the alignment of the timing marks as shown in Figure 14.

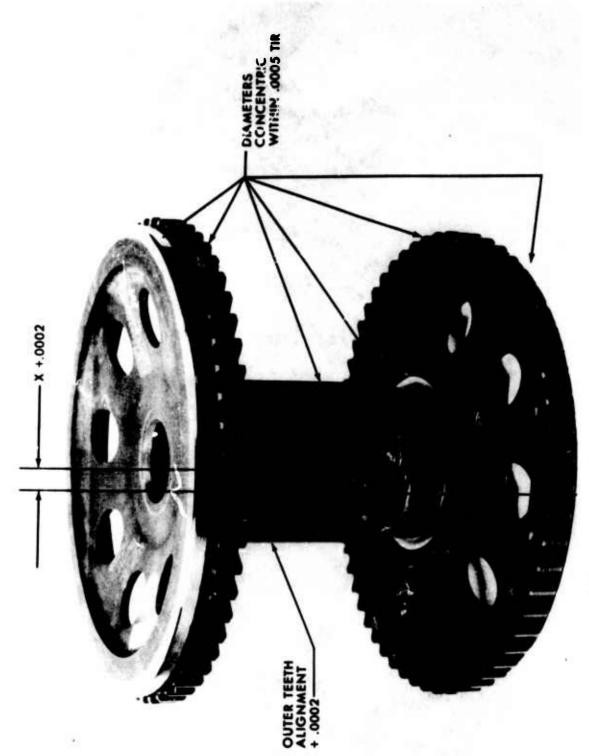


Figure 13. First-Row Pinion - Timing.

Figure 14. Roller Gear Unit.

TRANSMISSION MAMUFACTURE

Four complete roller gear transmission assemblies plus two sets of spare dynamic parts were manufactured.

All primary power gearing of the transmission was manufactured from AMS 6265, a consumable vacuum melt (CVM) case carburizing steel. All other dynamic components were fabricated from AMK 6260 or AMS 6415 steel. Ball and cylindrical roller bearings were made from 52100 CVM steel. The smaller gearbox housings were made from AZ91C magnesium castings. The main housing, however, was machined from a ZE41A magnesium casting. This material, a heat treatable magnesium-zinc-zirconium-cerium alloy, combines good castability and weldability with high strength and pressure tightness at ambient and moderately elevated temperatures. This program marked the first time this alloy was used for a Sikorsky transmssion housing.

The roller gear hardware presented unique manufacturing problems. Because of the complexity of the roller gear drive, where one gear assembly may have as many as three geared surfaces and four roller surfaces, electron beam welding was used extensively in the manufacturing proces. Gear members are joined by electron beam welding as are the rollers to the pinion assemblies. There are 72 electron beam welds in the roller gear transmission: 2 in the sun gear, 4 in each of the 7 first-row pinions, and 6 in each of the 7 second-row pinions. Exploded views of these gears are shown in Figures 15, 16, 17, and 18.

The manufacture of the sun, first-row pinion and second row pinions required the individual processing of the separate elements through blanking, gear hobbing, case carburizing, and heat treatment. From this point, each gear assembly had a separate and distinct manufacturing cycle.

The gear teeth of the sun gear are finish ground before the end rollers are welded on. The rollers' outside diameters are then ground concentric with the pitch diameter of the gears to within 0.0005 inch T.I.R. (total indicated reading).

The manufacture of the first-row pinion requires the finish machining of the small diameter gear before the machined and case-hardened two outer gears are welded on. These outer gears are then timed to the small gear during their finish grinding operation. The case-hardened outer rollers are then welded on and ground concentric to the outer gear pitch diameter.

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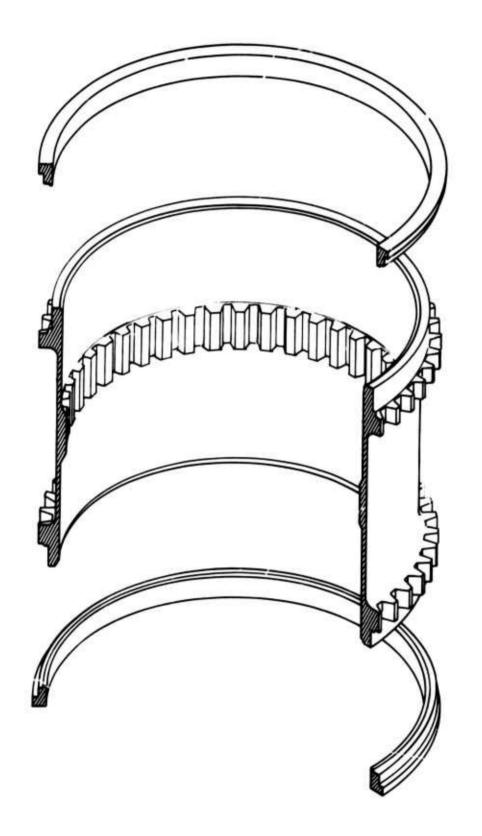
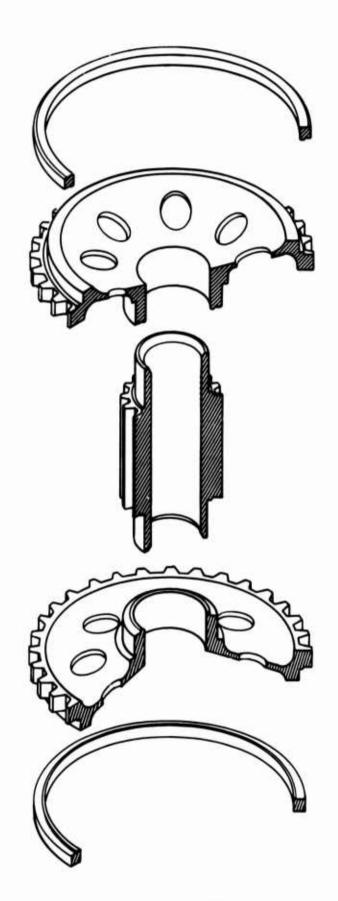
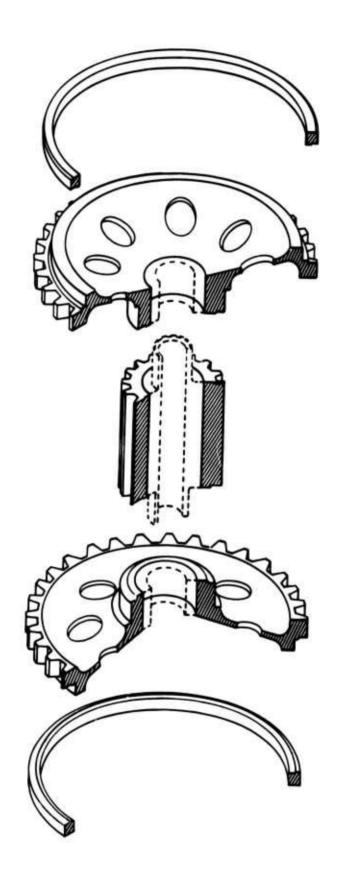


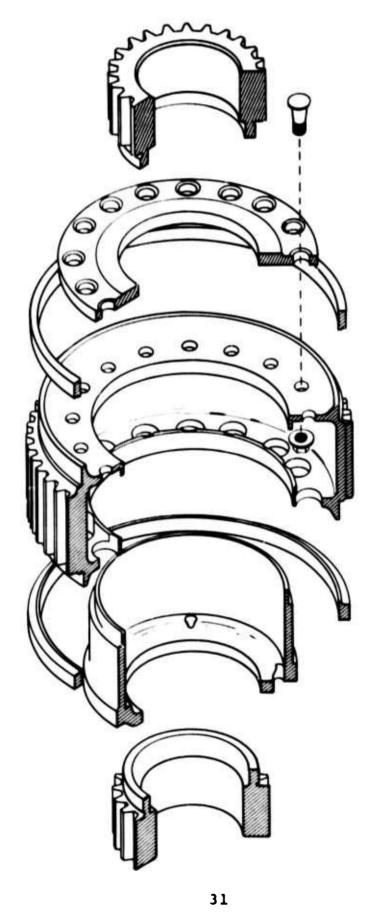
Figure 15. Sun Gear - Exploded View.



First-Row Pinion - Initial Configuration - Exploded View. Figure 16.



First-Row Pinion - Redesigned - Exploded View. Figure 17.



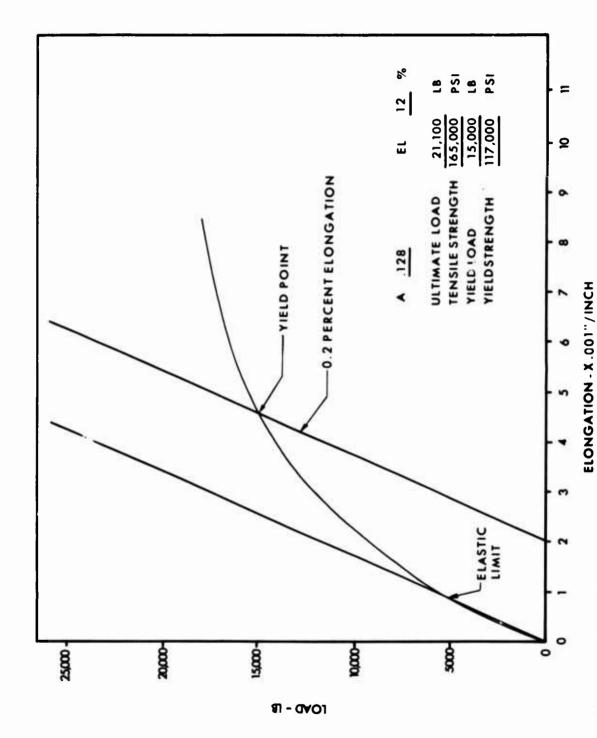
Second-Row Pinion - Exploded View. Figure 18.

Manufacture of the second-row pinion necessitated the assembly and welding of the finished ground and case-hardened small diameter end gears onto the machined and heat-treated center gear assembly. The case-hardened center gear teeth are then finished ground with relation to the end gears, thereby timing the assembly. The carburized and heat-treated rollers are then welded onto the assembly and finished ground concentric to the pitch diameter of the center gear.

The manufacture of the first- and second-row pinions presented several manufacturing problems and extremely close tolerances were demanded. The timing between gear members in these "stepped" roller gear pinions is held extremely close, as is the concentricity of the rollers to one another and to the pitch diameter of each gear. Tooth timing is best explained by the first-row pinion of Figure 13. In Figure 13, the two larger outer gears are timed to the center gear to within ± 0.0002 inch. Also, the two outer gears are aligned to each other within +0.0002 inch. A tooth is chosen on the inner gear and is marked The angular positions of the teeth on the as the index tooth. outer gears are then held to the master index tooth on the inner gear as shown by the dimension "X" in Figure 13. dimension "X" may be any value, but is to be the same within +0.0002 inch for all seven gears in any one assembly. When elelctron beam welding the first-row pinion assemblies, the gear members tended to "walk" as much as 0.002 inch relative to the center gear. This "walking" had to be accommodated for in the finish grinding of the outer gears.

The teeth of the gears on the second-row pinions are timed in a similar manner to the teeth of the first-row pinions.

Electron beam weld parameters were developed, prior to the manufacture of the roller gear components by subjecting sample welds to proof tests. Samples of various cross sections were made up and subjected to increasing tensile loads. Load versus strain curves were then plotted from the data of these tests to determine strength characteristics of the welds. Figure 19 shows one of these curves.



Electron Beam Weld Joint Strength - Load Versus Elongation. Figure 19.

TEST PROCEDURE

The roller gear transmission development program encompassed a series of bench tests, the objectives of which are described in this section. Other than the no-load lubrication test, all testing was conducted in the Sikorsky Aircraft S-61 regenerative bench test facility.

NO-LOAD LUBRICATION TEST

The first test to be performed on the roller gear transmission was the no-load lubrication test. The primary objective of this test was the determination of optimum lubrication parameters for the roller gear transmission. The factors under evaluation were the amount of lubricant and jet sizes required to provide adequate transfer of heat from the dynamic components of the gearbox while minimizing frictional losses caused by oil churning. In addition, the test was intended to locate and eliminate any lubricant flow problems which might be encountered such as restrictive oil paths, improper drainage, etc. Ancillary objectives included checks on the mechanical functioning of the roller drive gearbox, test instrumentation and compatibility of gearbox with S-61 bench test facility.

GEAR PATTERN DEVELOPMENT TEST

The second phase of bench testing to be performed in this program was the gear pattern development test. The primary objective of this test was the evaluation of gear patterns generated when the gearbox was operated under load. Examination of these gear patterns provided verification of the manufacture of the gears and the proper loading and alignment of gears and bearings. This test also provided a check on the functionality of the regenerative test stand with both test and dummy (slave) gearboxes installed. In addition, the gear pattern development test was used to evaluate the performance of special hollow ended roller bearings in the roller gear transmission. These bearings were being tested as a possible alternative to the spherical roller bearings used to support the second-row pinions of the roller gear drive.

INITIAL DEVELOPMENT TEST

Initial development testing was included in the bench tests to provide data for evaluation of the manufacturing methods of the sun gear and first—and second—row pinions of the roller gear drive. These gears were manufactured with the use of electron beam welds in certain operations of fabrication. Electron beam welding is a relatively recently developed method which employs a highly concentrated beam of electrons to melt and thereby fuse components together. Electron beam welding produces a relatively narrow joint (up to 20:1 depth

to width ratio) with a strength comparable to the annealed parent material. Since this program marks the first time electron beam welded gears have been used extensively in a helicopter main transmission, the initial development testing was necessary to check the endurance capabilities of these gears before the start of the 200-hour endurance test. Modifications necessary to ensure failure-free performance of the electron beam welded gears for extended periods of time were made as a result of this phase of testing.

200-HOUR ENDURANCE TEST

The 200-hour endurance test was designed to evaluate the effects on the roller gear transmission of long-term operation in a fatigue environment. The test was divided into two parts. After 110 hours were completed, as per the test schedule of Table IV, the test stand was shut down and both test and dummy gearboxes were removed from the test stand. Strainers and chip detectors were visibly inspected for any signs of failure and the roller gear unit was visually Upon completion of inspection, both gearboxes were inspected. then replaced in the test stand and the test continued for an additional 90 hours as per Table V. Throughout the 200-hour endurance test, transmission temperatures, oil pressures, and oil flows were continuously monitored. In addition, chip detectors were inspected at 10-hour intervals. Following completion of the 90 hours of testing, both gearboxes were removed from the test stand and completely disassembled. All gearbox components were subjected to magnaglow inspection. Those components containing electron beam welds were also subjected to pulse-echo ultrasonic inspection as a check on the integrity of the welds.

EFFICIENCY TEST

Coincident with the 200-hour endurance test, an efficiency test was conducted. The objective of this test was the accurate determination of the efficiency of the roller gear drive transmssion by means of heat loss calculation. to accomplish this, the test gearbox was insulated with a thickness of fiberglass insulation on all nonrotating The lube oil was plumbed through a water-oil heat exchanger, and both oil lines and heat exchanger were insulated. During the test, input power, tail takeoff power, main shaft power, water-in temperature, water-out temperature, and water mass flow rate were continuously recorded. From the data gathered, the heat loss (a measure of the inefficiency of the system) was calculated from the mass flow rate and the enthalpy of the heat exchanger water. A plot of heat loss expressed in friction horsepower versus input power was constructed by fitting data points by the least squares method.

TABLE IV.	ENDURANCE TEST SPECTRUM - 11	0 HOURS
Time (hr:min)	Total Input Power (hp)	Tail Power (hp)
15:00	1100	250
50:00	1950	250
25:00	2400	250
10:00	2700	250
6:30	3000	425
1:30	1950	425
1:30	3560	425
:30	3700	425

TABLE V.	ENDURANCE TEST SPECTRUM - 9	0 HOURS
Time (hr:min)	Total Input Power (hp)	Tail Power (hp)
0:45	400	40
7:30	1100	250
32:00	1950	250
12:30	2400	250
7:00	2700	250
19:30	3000	425
4:30	1950	425
4:30	3560	425
1:45	3700	425

TEST FACILITY

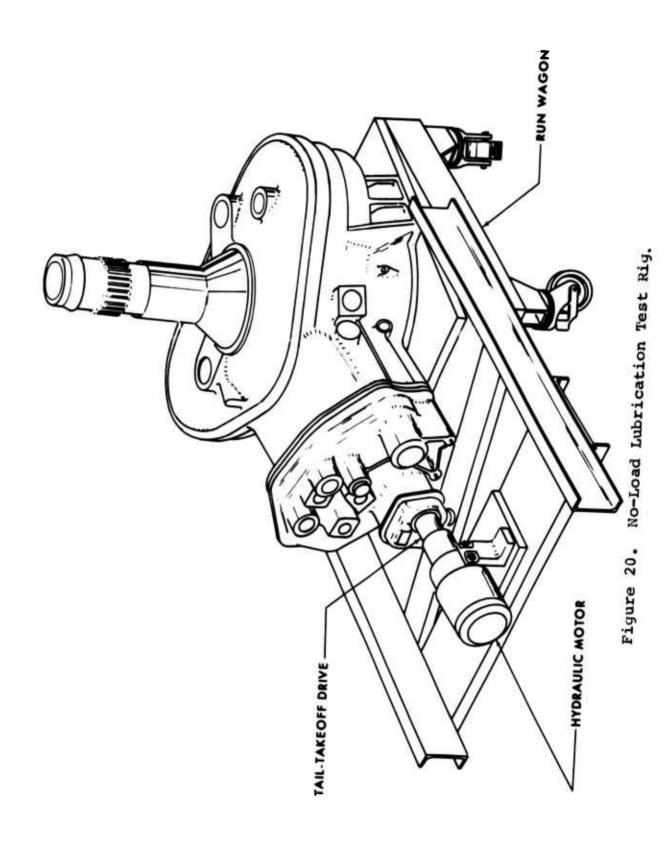
For the testing discussed in this report, a test facility was required in which the roller gear drive gearboxes could be mounted and tested under conditions duplicating as closely as possible actual aircraft conditions. This section discusses in detail the facilities used during the testing described herein. The first section is a short discussion of the no-load lubrication test rig which allowed for the testing of one gearbox to which no external torque is applied. The balance of this chapter discusses the setup of the regenerative test stand which was used for the majority of the testing.

NO-LOAD LUBRICATION TEST RIG

Testing of the roller gear transmission for the no-load lubrication test basically consists of applying a driving force that rotates the gearbox at a variable speed up to 100 percent speed. The driving force is required to rotate the gearbox only against internal friction. Instrumentation to monitor oil temperature, flow, and pressure is incorporated so that accurate determination of optimum lubrication parameters is possible. Although full-load testing may eventually determine additional lubrication requirements, the no-load lubrication test generally establishes the correct lubrication system besides initially checking the dynamic components in the gearbox.

To fulfill the requirement of variable speed in the no-load lubrication test of the roller gearbox, a hydraulic motor was selected to supply the driving force. The tail takeoff flange was selected as the most advantageous location to rotate the gearbox at 100 percent speed due to the speed limitation on hydraulic motors. Driving of the inputs which would have more closely approached aircraft conditions was unacceptable because of the high speed (18,966 rpm) required. The main rotor shaft was unacceptable because of its low speed (203 rpm). Tail takeoff flange rotational speed is 3025 rpm at 100 percent speed and is compatible with most hydraulic drive motors. The estimated no-load 100 percent speed power requirement was 50 hp. A hydraulic motor was selected that would meet these requirements.

The next consideration in the design of the no-load lubrication test rig was the support of the gearbox and drive motor. To expedite testing and reduce cost, the run wagon that is used to support and align the gearbox when installed in the regenerative test stand was selected as the test frame. A removable structural steel framework was added at the rear of the test wagon to support the hydraulic motor drive as shown in Figure 20. This configuration permits the gearbox to be installed directly in the regenerative test stand upon completion of the



no-load lubrication test. The only hardware to be removed then would be the hydraulic motor and framework. Most of the basic instrumentation used in the no-load lubrication test is required for the bench test and could remain intact during the transfer from one test facility to the other.

The structural steel framework to support the hydraulic motor was fabricated prior to assembly of the gearbox. Final installation of the framework and alignment of the hydraulic motor was completed after installation of the gearbox on the test wagon. A triple Thomas coupling assembly was installed between the flange of the hydraulic motor and the tail takeoff flange of the aircraft gearbox to allow for small angular shaft misalignments that could occur during the testing.

A 125-hp pumping unit was used to supply power to the hydraulic motor. A thermostatically controlled water-oil heat exchanger permitted operation of the pumping unit for extended periods of time without danger of overheating. An additional water-oil heat exchanger was employed to maintain gearbox lubricating oil temperature at normal operating conditions.

REGENERATIVE TEST STAND

Sikorsky Aircraft employs regenerative type (back-to-back) test stands in the testing of fully assembled transmissions. These facilities permit the testing of transmissions under laboratory controlled conditions. Loads similar to flight aircraft loads are applied to the transmission undergoing tests. Accelerated testing with loads in excess of those obtainable on the flight aircraft may be applied also. Testing is not restricted to environmental conditions and can be conducted on a 24-hour/7-day-a-week schedule.

The basic concept of a regenerative test facility for the testing of transmissions is the incorporation of torque loops. A transmission is essentially a device to transmit torque from point A to point B. Usually associated with this transmission of torque is a change in speed, and a change in angle. The roller gearbox is designed to transmit torque from two General Electric T58-GE-16 engines at 18,966 rpm to the aircraft main rotor head which rotates at 203 rpm and at an angle of 86 degrees to the input. In addition, the roller gearbox supplies torque to a tail takeoff flange which is used to rotate the tail rotor assembly. Additional torque takeoffs are provided to power generators and hydraulic pumps at various speeds.

The S-61 main transmission regenerative test stand at Sikorsky Aircraft, Figure 21, employs two basic torque loops in the testing of aircraft transmissions. In the main loop, Figure 22, torque is applied at the main rotor shaft of the dummy gearbox. It is transmitted through the dummy gearbox and into the test gearbox by means of the input shafts. The torque is then transmitted through the test gearbox up through the main rotor shaft of the test gearbox and back to the main rotor shaft of the dummy by means of spur gears. The second torque loop incorporates a pair of commercial gearboxes connected by a long shaft. The commercial gearboxes are connected to the tail takeoff outputs of the test and dummy gearboxes.

Electric motors, which are connected to the main torque loop, but not in series with the main torque loop, are used to overcome system friction and operate the transmissions at 50-percent and 100-percent speed.

It should be noted that although the "test" gearbox is rotated and loaded to simulate flight conditions, the dummy gearbox is not. In the S-61 test stand, the "aummy" gearbox is rotated in a reverse direction with the loads in the correct direction. In addition, the transmitted load in the dummy is from the main rotor shaft to the inputs, and is of a higher magnitude to compensate for losses in power flow. In most areas of the dummy box, particularly in the roller gear unit, the effect of opposite rotation and the small differences in magnitude of load are negligible. In effect then, the dummy gearbox roller gear unit is a second test sample.

To apply torque to the main "torque loop" in the S-61 main transmission test stand for testing of the standard production S-61 type transmissions, the dummy gearbox ring gear is rotated by means of hydraulic cylinders. The ring gear in the S-61 main transmission, being a fixed nonrotating member of the planetary gear train, transmits torque to the main housing of the gearbox through shear bolts. In the dummy gearbox, the shear bolts are eliminated and the ring gear is allowed to float. To react system torque, the ring gear is secured to the test stand by a pair of hydraulic cylinders which are employed not only to react system torque but also to apply system torque by rotating the ring gear in a direction opposite to that of the system torque.

The roller gearbox design incorporates a rotating ring gear that drives the main rotor shaft. The roller posts which react system torque to the gearbox housing are buried within the gearbox and could not be isolated from the rest of the gearbox in an acceptable manner for applying system torque.

Figure 21. S-61 Regenerative Test Stand.

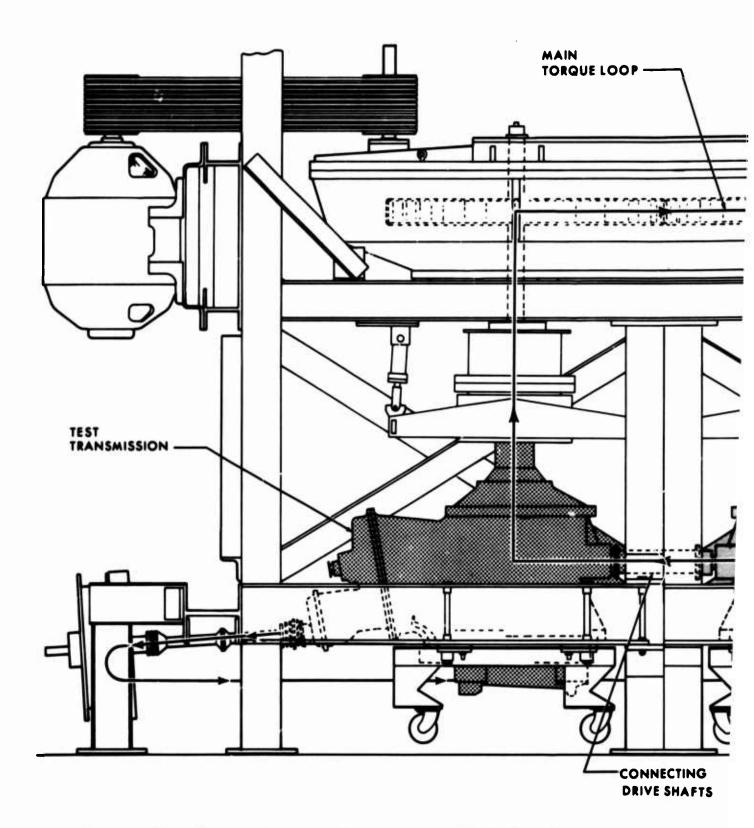
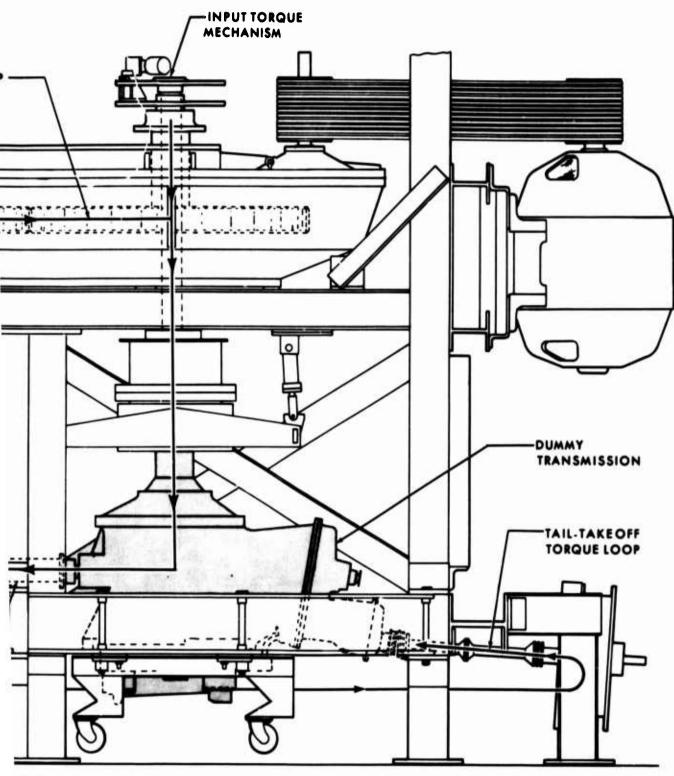


Figure 22. Torque Loops - Regenerative Test Stand.





NECTING E SHAFTS A modification to the basic S-61 main "torque loop" at the commercial gearbox was designed which would eliminate any rework to the aircraft gearbox for applying torque. The "torque loop" was severed and then reconnected through an arrangement of coaxial shafts and rotating torque plates (Figure 23). Electric jacks are used to connect the torque plate of the inner shaft, attached to the dummy gearbox main rotor shaft, to the torque plate of the outer shaft, attached to the commercial gearbox dummy bull gear. Actuation of these jacks rotates the inner shaft torque plate relative to the outer torque plate and thus applies torque to the system. Power to the torque jacks is through an electrical slip ring mounted on the axis of rotation. Control of the torque jacks is accomplished at the operator's console.

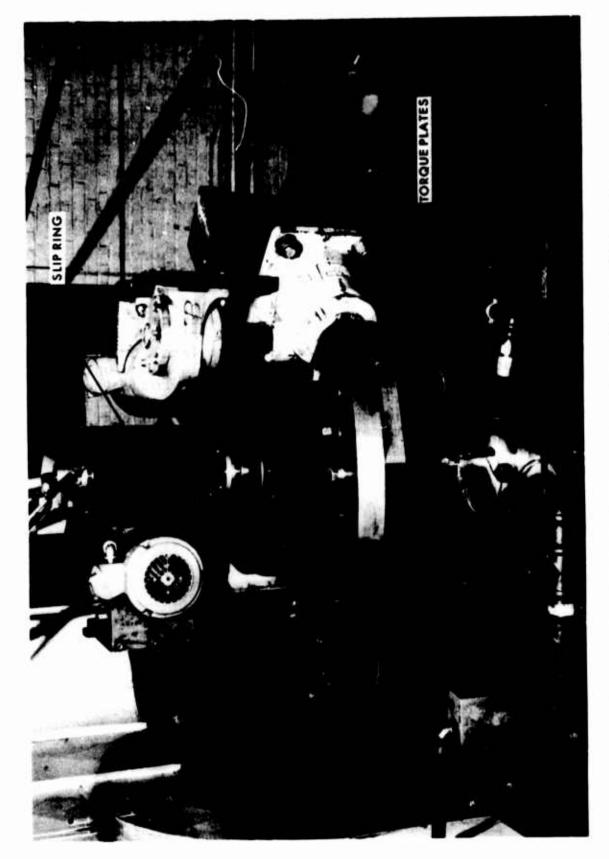
No rework of the secondary or tail drive shaft "torque loop" was required for this test, since the roller gearbox tail drive shaft system is identical to that of the standard S-61.

The overall envelope of the roller gearbox when compared to a production S-61 gearbox is lower and wider. Extensive rework to the structural steel supports of the test facility was required to accommodate the roller gearbox. In addition, the rework had to permit both roller gearboxes and production S-61 gearboxes to be tested in the same facility. Maintaining alignment between test and dummy inputs and between test and dummy outputs with the commercial gearbox incurred installation of additional supports before any of the existing structural steel was modified.

GEARBOX INSTRUMENTATION

Instrumentation requirements for the bench test of the roller gearbox were as follows:

Thermocouples	48
Strain gage measurements	13
Chip detectors	4
Pressures	7
Flow	1
Speed	1



Torque Mechanism - Regenerative Test Stand. Figure 23.

Thermocouples were installed in each gearbox at all primary bearings. The thermocouple locations are tabulated in Table VI and shown in Figure 24. These thermocouples are basically washer types, installed at or near the load zone of the non-rotating member of the bearing. Lead wires from the thermocouples were extended through holes in the outer housing to strip chart recorders. To eliminate oil leakage at these holes, packing gland fittings were installed, which compressed a rubber grommet around the lead wire. The strip chart recorders were of a sequential type that continually printed each temperature at 2.5-second intervals. In addition to measuring bearing temperatures, thermocouples were also installed to measure oil and ambient air temperature.

Strain gages were used to measure torque through both the main and tail drive shafts. All roller posts were also strain gaged using a full wheatstone bridge configuration in both the radial and tangential directions as shown in Figure 25. Outputs of all strain measurements were recorded on light beam oscillographs.

Pressure measurements were made at the two lubrication oil pumps, all manifolds, the two input extentions of the dummy gearbox, the input lines to roller gear units, and the jets furthest along the oil lines from the pump. Each pressure was monitored on direct reading pressure gages at the operator's console.

The oil lubrication systems of both the test and dummy gearboxes are connected to the test facility system. Each gearbox is serviced by separate filters and heat exchangers. The gearbox lubrication pumps supply the pressure for the system as shown in the schematic of Figure 26. A facility auxiliary pump which operates only when pressure from the gearbox pump drops below 40 psi is plumbed into the system.

Oil flow to each gearbox was monitored using a flow turbine installed in the lube oil pump discharge line. Readout of flows was on a frequency convertor installed in the operator's console.

Chip detectors were connected to a panel mounted light/alarm system. Each gearbox was equipped with four separate chip detector/strainer combinations. One chip detector was installed in both the l.h. and r.h. input drains. Others were located in the rear section drain and in the main lube oil sump, as shown in Figure 27.

TABLE VI.	THERMOCOUPLE LOCATIONS, ROLLER GEAR TRANSMISSION
Number	Location
1	L.H. dummy gearbox extension ball bearing
2	R.H. dummy gearbox extension ball bearing
3	L.H. input bevel pinion stack ball bearings
4	R.H. input bevel pinion stack ball bearings
5 6 7	L.H. input bevel pinion roller bearing
6	R.H. input bevel pinion roller bearing
	L.H. input bevel gear lower roller bearing
8	R.H. input bevel gear lower roller bearing
9	L.H. input bevel gear duplex bearings
10	R.H. input bevel gear duplex bearings
11	L.H. input spur gear upper roller bearing
12	R.H. input spur gear upper roller bearing
13	Main rotor shaft roller bearing
14	Outer shaft roller bearing
15	Outer shaft tapered roller bearings
16	Bevel pinion T.T.O. forward tapered roller brg.
17	Bevel pinion T.T.O. aft tapered roller bearing
18	Spur gear T.T.O. roller bearing
19	Main rotor shaft duplex hall bearings
20	Second-row pinion spherical bearing
21	Second-row pinion spherical bearing
22	Second-row pinion spherical bearing
23	Second-row pinion spherical bearing
24	Second-row pinion spherical bearing
25	Second-row pinion spherical bearing
26	Second-row pinion spherical bearing
27	Spur gear T.T.O. ball bearing
28	Adaptor gearbox input forward ball bearing
29	Adaptor gearbox output ball bearing
30	Adaptor gearbox idler ball bearing
31	Adaptor gearbox output roller bearing
32	Adaptor gearbox idler roller gearing
33	Adaptor gearbox input aft ball bearing
34	Spur gear input T.T.O. roller bearing
35	Spur gear output T.T.O. ball bearing
36	Rotor brake forward hall bearing
37	Rotor brake aft ball bearing
38	Lubrication 'oil out' temperature
39	Lubrication pump roller bearing
40	R.H. generator ball bearing
41	Lubrication 'oil in' temperature
42	L.H. generator ball bearing
43	L.H. generator roller bearing
44	Utility pump roller bearing
45	Auxiliary pump roller bearing
46	Primary pump ball bearing
47	Tachometer ball bearings
48	Ambient air temperature

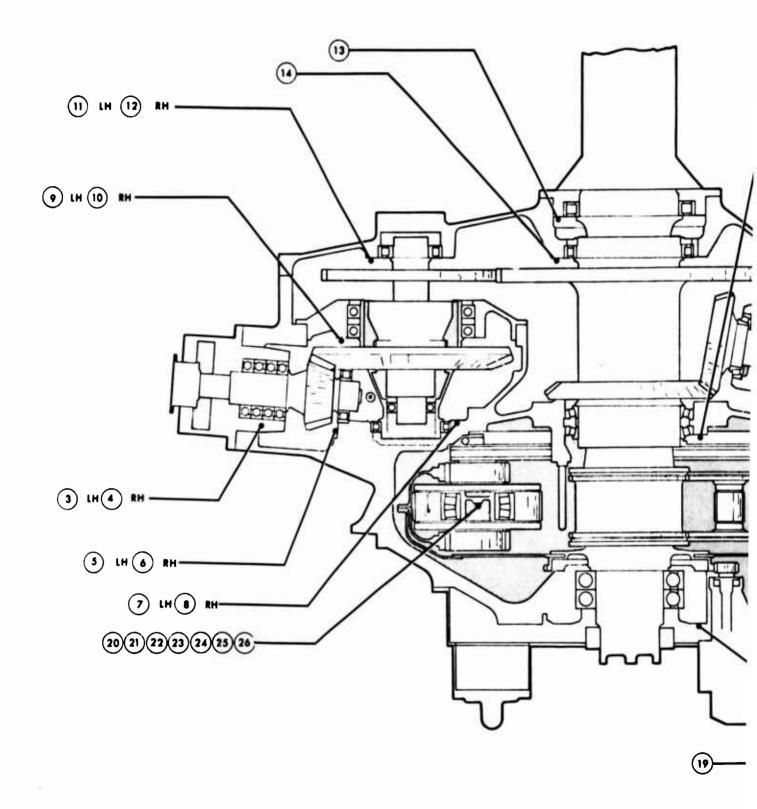
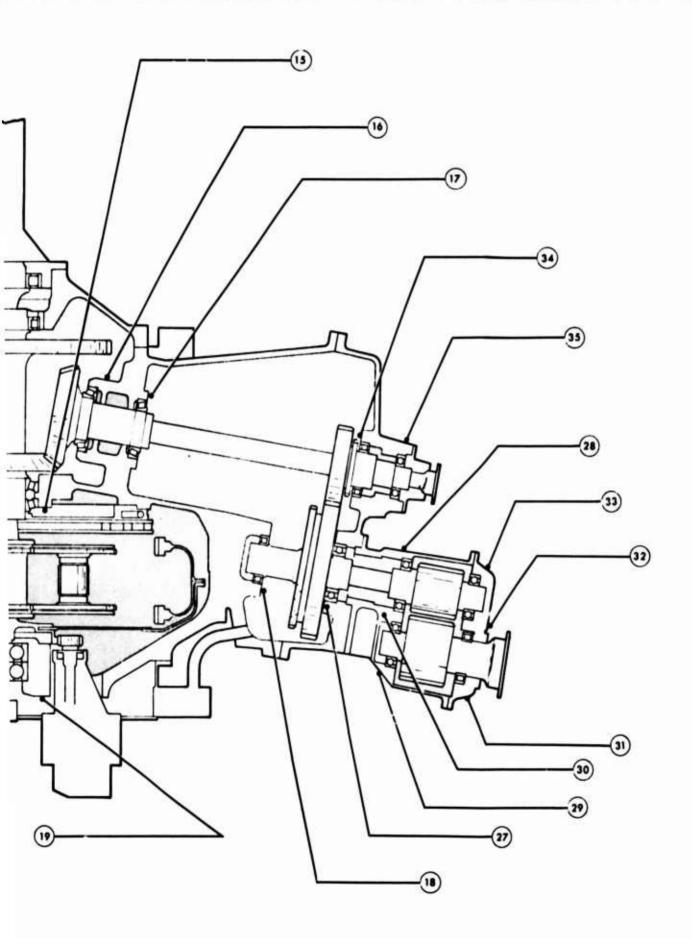


Figure 24. Thermocouple Locations - Roller Gear Transmission.







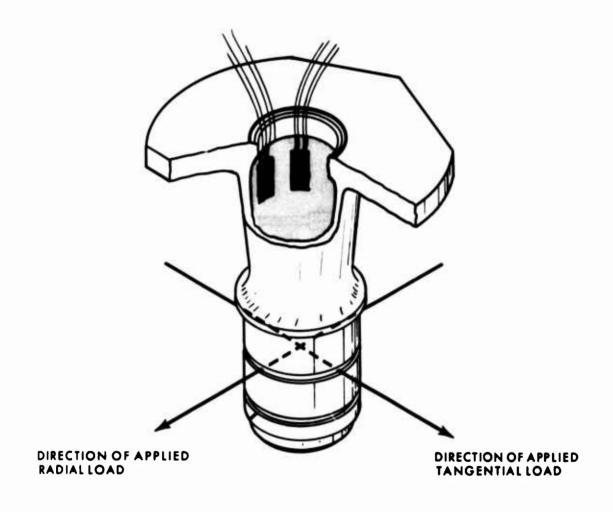
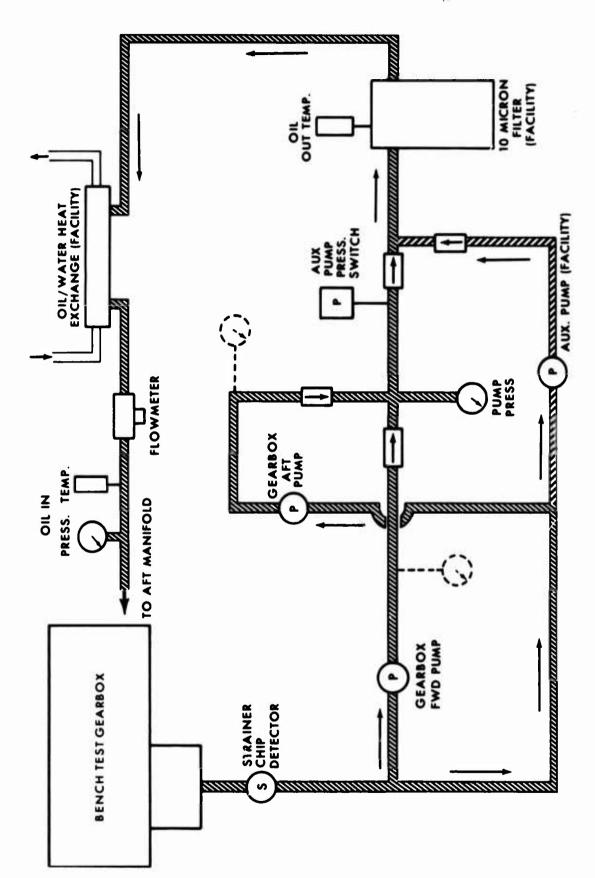


Figure 25. Strain Gage Locations - Post, Second-Row Pinion.



Lubrication System - Roller Gear Transmission. Figure 26.

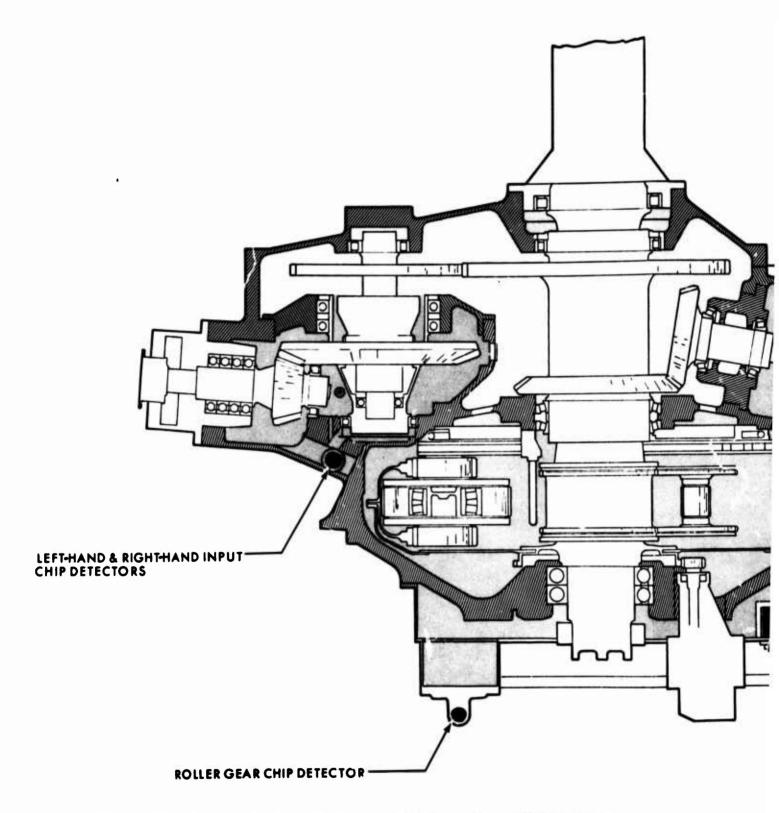
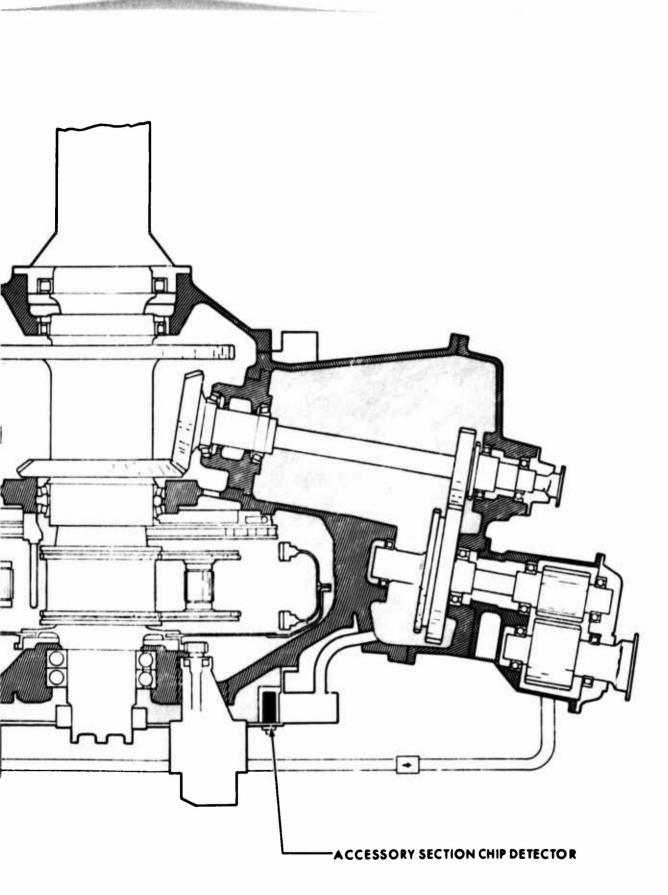


Figure 27. Chip Detector Locations - Roller Gear Transmission.





Transmission.

BEHCH TEST RESULTS

This chapter discusses the four phases of bench testing to which the roller gear drive transmission was subjected. During these tests, a total of 264 hours of testing was logged. Figure 28 shows a breakdown of the total test time into the four phases of bench testing including important shutdowns. The efficiency test, which is also included in this discussion, is not shown in the figure since it was conducted as part of the 200-hour endurance test.

NO-LOAD LUBRICATION TEST

The no-load lubrication test was conducted to evaluate the functional performance of the roller gear transmission and to ascertain the optimum lubrication system for the gearbox. The test was conducted to verify jet size, amount of oil required in the gearbox, and modifications to the gearbox necessary to ensure satisfactory lubrication and temperature levels. The initial lubrication system was based on analysis conducted during the design of the transmission.

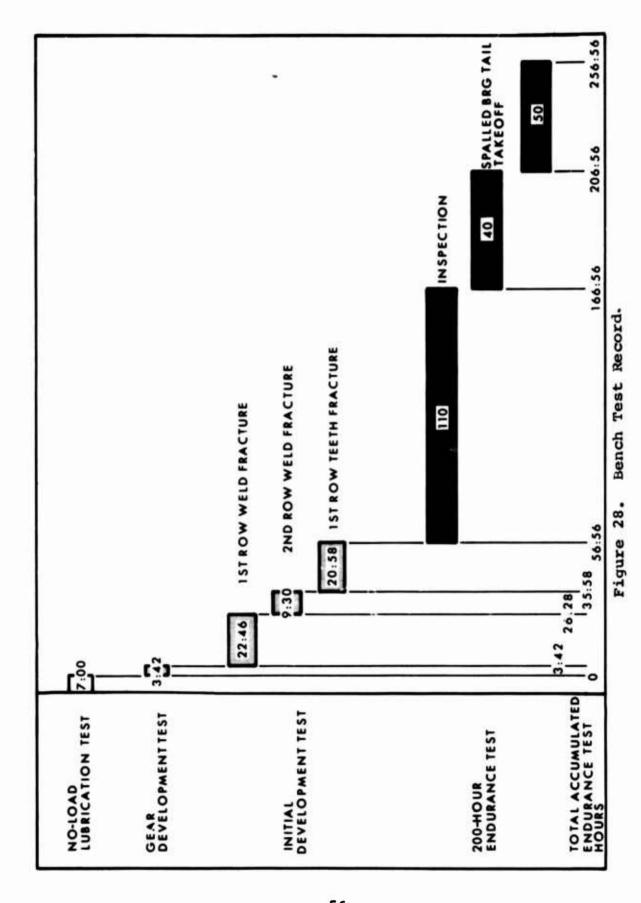
Test Wagon, No-Load Test

The assembled dummy (slave) gearbox was installed on the test wagon in preparation for the no-load lubrication test. The dummy gearbox was selected as the test article for this series of tests as it did not contain freewheel units.

Figure 29 shows the input section of the dummy gearbox. The freewheel units, normally installed inside the vertical bevel gear shafts, are replaced by single-piece shafts. This ensures rotation of the input pinions when power is applied at any output shaft. Also shown in Figure 29 is an extension/adaptor on the input bevel pinion housing. This enables aircraft type drive shafts to be used to drive the test gearbox during subsequent testing to be conducted in the regenerative test stand.

The hydraulic motor was installed on the no-load lubrication rig and aligned with the tail takeoff flange, as shown in Figure 20 (test facility, no-load lubrication rig). All instrumentation was connected and checked out. The gearbox was serviced with 15 gallons of SATO 35 oil.

Testing was initiated at 20 percent operating speed, and incremental speed changes of 10 percent were conducted after partial temperature stabilization was reached. At 48 percent speed (100 percent speed = 3025 rpm), testing was discontinued because of drive motor flow limitations which prevented higher speeds. A hydraulic motor of greater flow capacity was installed. Testing was continued until a speed of 70 percent was attained, at which point testing again was discontinued



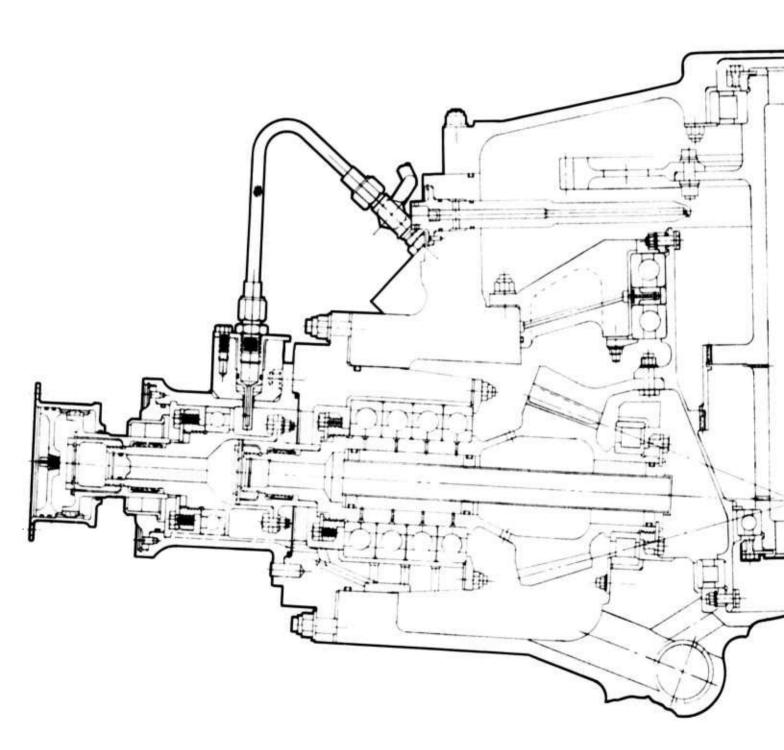
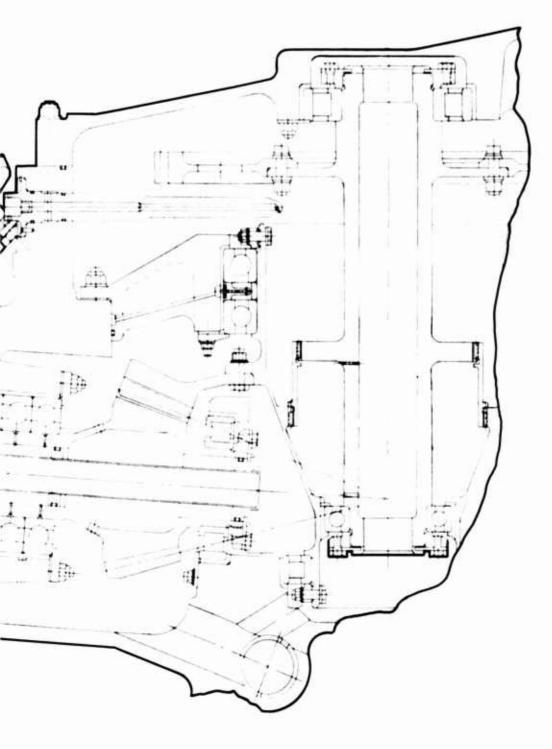


Figure 29. Input Section - Dummy Gearbox.





ny Gearbox.

because of drive motor flow limitations.

It was noted during this series of tests that the inputs were operating at temperatures approximately 20½°C higher than the remainder of the gearbox. No major problem was felt to exist at this time. This conclusion was based on the fact that all input temperatures stabilized and were identical at both the left-hand and right-hand sides.

Regenerative Test Facility, No-Load Test

Having attained a speed of 70 percent on the no-load lubrication test rig without experiencing any major problems, the decision was made to complete the test at 100 percent speed in the regenerative test facility. Initial testing in the regenerative stand was conducted at 50 percent speed to verify previous data and to check out compatibility of the gearbox with the stand. During this series of tests, drive power to the aircraft gearbox was transmitted through the main rotor shaft. The input drive shafts and the tail drive shaft were not installed. compatibility difficulties with the gearbox instrumentation and the lubrication system plumbing with the regenerative test stand facility were resolved and the gearbox speed was increased to 100 percent. After obtaining stabilized readings of temperature, the effects of varying the amount of lubricant in the gearbox were evaluated under stabilized conditions. This permitted the selection of the oil level for the gearbox which achieved the best compromise between oil volume and stabilized gearbox temperatures. Testing was discontinued and the gearbox removed from the test stand when several small magnetic particles were found in the chip detector at the end of day inspection, Figure 30. There were insufficient particles to activate the warning light. Testing was resumed after a The source of the magnetic partial teardown and inspection. particles could not be determined, and it was concluded that they may have entered during the final assembly of the gearbox.

The input stack bearings, operating at a rotational speed of 18,966 rpm with a DN of 1,043,000, ran hotter than expected with a mean operating temperature of 118½°C. Increasing the quantity of oil supplied to the bearings from 1.75 to 3.0 gallons per minute resulted in a temperature drop of only 3 degrees. Restricting the amount of oil conversely caused an increase in bearing temperature. Incorporating a shield around the input bevel pinion reduced the temperature of the stack bearings by 5½°C and the bevel pinion roller bearing by 12½°C. This shield, wrapped around the lower half of the gear and following the contour with 0.12 inch clearance as shown in Figure 31, allows the oil to drain freely from the stack bearings and the input housing.

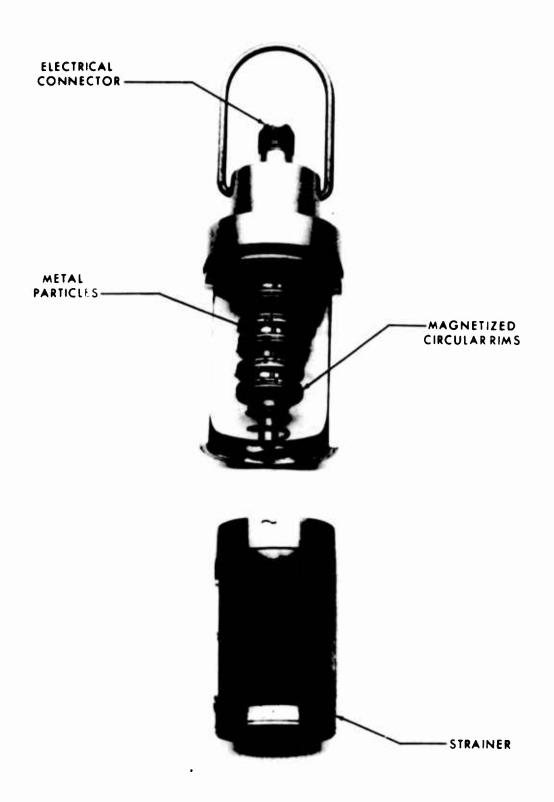


Figure 30. Chip Detector, No-Load Lubrication Test.

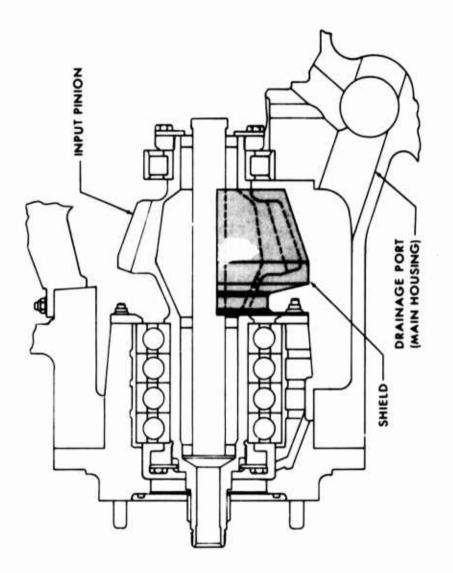


Figure 31. Input Bevel Pinion Shield.

The duplex bearings on the bevel gear shaft operate at a DN of 1,180,000, the highest in the gearbox. Lubrication to these bearings is supplied from a probe jet located between the bearings which directs oil to the inner raceways of each bearing. These bearings also ran hotter than anticipated at a temperature of 125° C. It was theorized that oil was accumulating around the bearing housing, thereby causing excessive heat as a result of churning. Oil lubricating the bevel gear mesh is forced outward by the rotation of the gear, thus creating a wall of oil which prevents the oil supplied to the bearings from draining. To alleviate this problem, drainage holes were machined in the main housing to allow the oil to escape, Figure 32.

Testing with 17 gallons of oil was terminated after 50 minutes when, after stabilization of temperatures, the temperatures of the spherical bearings in the roller gear unit output gears suddenly rose 20 degrees to a mean of 102° C. Accompanying this rise was an increase in friction horsepower. It was theorized that insufficient oil drainage in the roller gear unit caused a high dynamic oil level which extended into the roller gear assembly. The output ring gear of this unit acts as a collector for the oil and allows a head of oil to build up before it can bleed out. Within the head of oil, the second-row pinion gears operate, continuously churning the oil and thereby generating heat. It was apparent that better drainage of the oil collected by the ring gear was required. Holes in the vertical portion of the ring gear web were drilled to allow the oil to drain.

The rear cover casing containing the tail takeoff spur gears and accessory drive spur gears, whose bearings are gravity fed by oil collected in scuppers, experienced no problems; nor was there any excessive heat generated in the adaptor gearbox by the 3.37-inch-wide spur gears.

The final inspection included a complete disassembly of all the gearbox subassemblies. No sign of any malfunction was detected.

Test Results

The tests revealed that 14.5 gallons was the optimum amount of oil for the gearbox. This quantity of oil prevented cavitation in the two-vane type lubrication pumps, yet did not create excessive churning losses within the gearbox. The oil temperature increase for the gearbox with this quantity of oil is 27° C for an oil-in temperature of 70° C and oil-out temperature of 97° C. Pump cavitation occurred at oil levels less than 13 gallons. Various tests were conducted to determine if oil flow fluctuations were being caused by an insufficient oil recovering rate. However, tests conducted by-passing

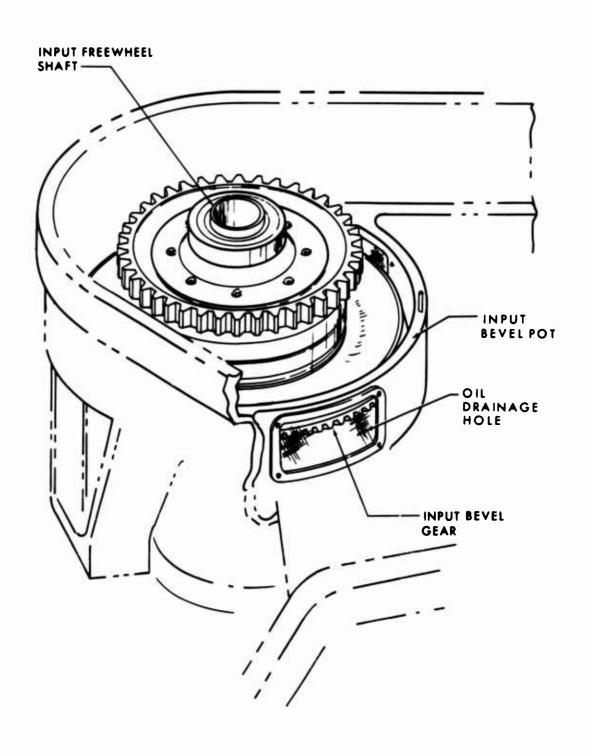


Figure 32. Drainage Ports - Input Bevel Gear Housing.

restrictive areas of the oil path had no effect.

Figure 33 shows both static and operating levels of 14.5 gallons of oil in the gearbox. With an initial 14.5 gallons of oil in the gearbox, the quantity that remains trapped after drainage is 2.5 gallons.

Gearbox Modifications

As a result of the tests, the following modifications were incorporated in both the dummy gearbox, on which the no-load test was conducted, and the test gearbox, which was in the process of being assembled:

Main housing - drainage holes machined in the input bevel pots and screens incorporated as shown in Figure 33. Mesh type screens with chip detectors incorporated in the center membrane of the main housing.

Ring gear output flange assembly - 0.5-inch-diameter holes machined in the ring gear and output flange as shown in Figure 34.

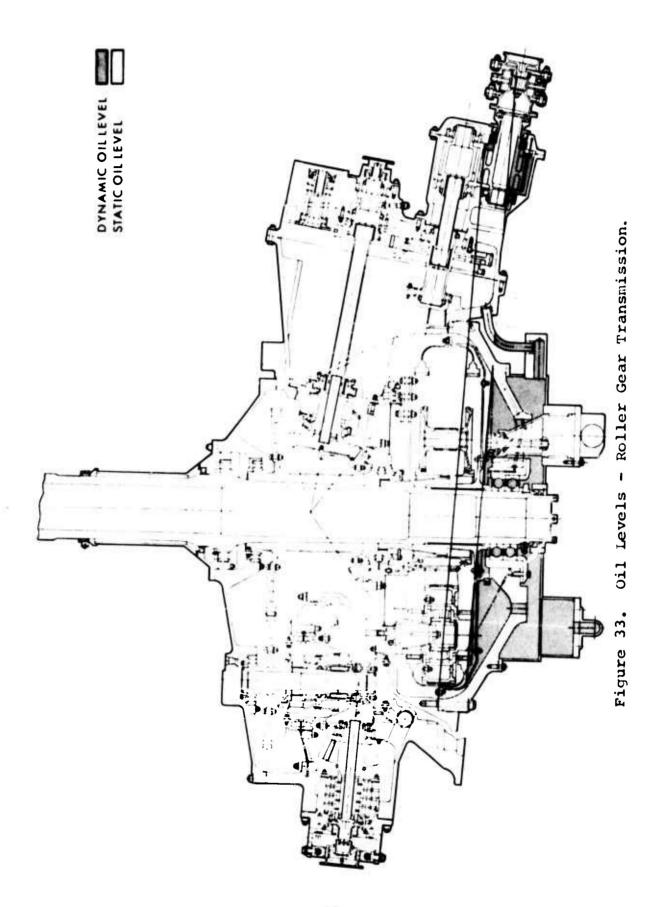
Lower housing sump - four drain back lines incorporated (Figure 34).

Input pinions - shields incorporated (Figure 31).

The inclusion of screens in the input bevel pots and center membrane compartmentalizes the gearbox into six units as shown in Figure 35. These incorporate the following gear meshes:

- 1 & 2 The left-hand and right-hand input bevel pinion and gear assemblies.
 - 3 The combining spur gears and tail takeoff bevel gears.
 - 4 The roller gear unit and sump pump drive gears.
 - 5 The accessory section.
 - 6 The adaptor gearbox.

The gearboxes now incorporating four magnetic chip detectors and eight plug type detectors (incorporated in the center membrane screen baskets) enable the location of any failure to be accurately determined.



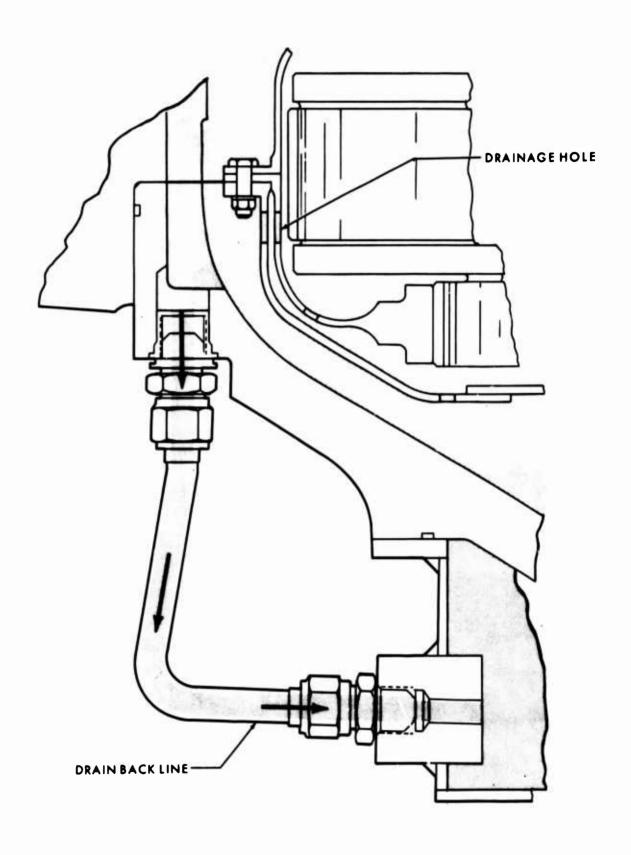


Figure 34. Oil Drainage - Ring Gear/Lower Housing.

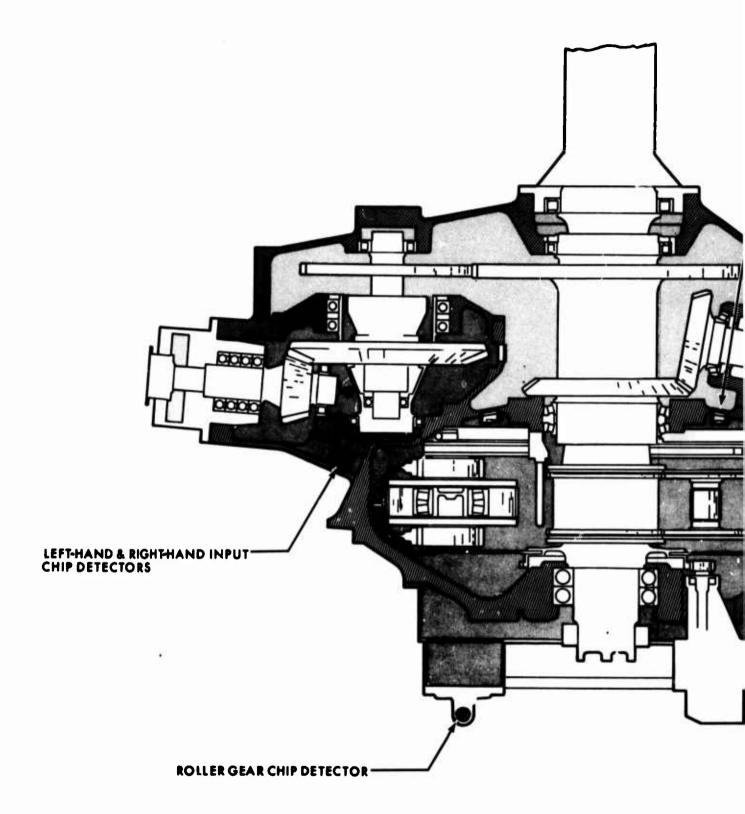
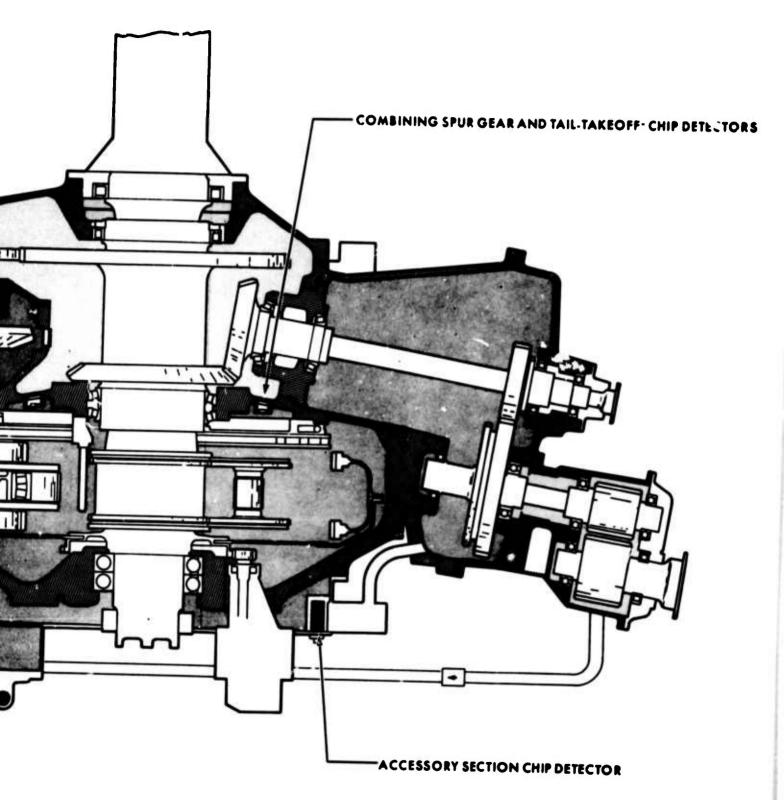


Figure 35. Compartmentalization - Roller Gear Transmission.





ar Transmission.



GEAR PATTERN DEVELOPMENT TEST

The purpose of the gear pattern development test was to establish satisfactory gear patterns on the tail takeoff and input bevel gear sets and to determine the dynamic characteristics of the roller gear transmission.

Included in the preparation for the gear pattern development test was the calibration of the second-row pinion bearing posts and the main rotor shaft. The posts (seven per gearbox) were calibrated with the use of Wheatstone bridge strain gages bonded on the inside bore of the posts, as shown in Figure 25. A tangential load of 10,000 pounds and a radial load of 500 pounds were applied to each of the posts by means of a hydraulic cylinder as shown in Figure 36. By measuring the change in voltage across the strain gages, a relationship between voltage change and load was determined, thereby enabling loading characteristics of the posts to be monitored.

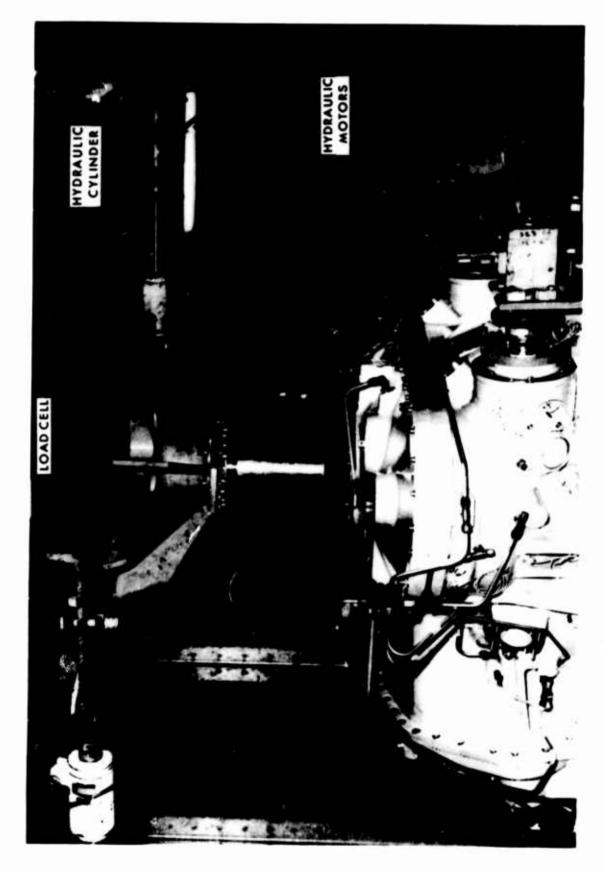
Calibration of the strain gages of the main rotor shaft was performed in a similar manner. A torque of 950,000 in.—1b was applied to the main rotor shaft by two hydraulic rams, as shown in Figure 37, and reacted by restraining the input shafts. Voltage changes across strain gages mounted on the inside of the rotor shaft were monitored and related to the applied torque. This enabled the torque through the main rotor shaft to be determined at any time by examination of the strain gage output voltage.

The roller gear units for the test and dummy transmissions were assembled with those components listed in Tables VII and VIII, respectively. These tables show the status and total number of test hours accrued for each part. Figures 38 and 39 show the location of the gears in the test and dummy roller gear units. Thermocouples attached to the posts as shown in Figure 40 and numbered T21 through T26 were used to measure the temperatures of the bearings in the second-row pinions. These temperatures are recorded on the run sheets given in Appendix I. These sheets are records of the data listed in the instrumentation section of this report for this test and subsequent tests.

Figure 41 shows the partially assembled roller gear unit with the top half of the double plate removed, exposing the flanges of the second-row pinion posts.



Figure 36. Static Calibration - Second-Row Pinion Posts.



Static Calibration - Roller Gear Transmission. Figure 37.

	TABLE VII. TEST #1 TEST GEA	#1 - ROLLER GEA GEARBOX	ROLLER GEAR COMPONENTS - OX	
Part Number	Nomenclature	Serial Number	Status	Test (hours:minutes)
RG351-11183-041	Sun Gear	0.4	Hew	0
-11182-04	1st-Row Pinion	0.5);ew	0
1-11182-0	C,	11	New	0
51-11182-04	st-Row	12	::ew	0
351-11182-04	st-Row	13	New	c
351-11182-04	st-Row	14	::ew	0
351-11182-04	st-Row P	15	Hew	0
-11182-04	1st-Row Pinion	17	lew	0
-11181-04	2nd-Row Pinion	03	New	C
1-11181	2nd-Row Pinion	04	::ew	0
351-11181-04		0.5	liew	C
51-11181-04	2nd-Row Pinion	90	New	0
351-11181-04		80	New	0
351-11181-04	Д	60	New	C
RG351-11181-042	2nd-Row Pinion	20	New	0
RG351-11184-041	Ring Gear	02	New	0
-131	iant	7	New	0
-131	iant	13	New	0
-131	iant	14	New	0
-131	iant	52	:Jew	0
-131	iant	58	New	0
LP-1313-UHAR-3906	iant	59	New	0
LP-1313-UHAR-3906	Compliant Bearing	09	New	0

	TABLE VIII. TEST #1 DUMMY GE	1 - ROLLER GEAR COMPONENTS GEARDOX	COMPONENTS -	
Part Number	Nomenclature	Serial Number	Status	Test (hours:minutes)
RG351-11183-041	Sun Gear	90	::ew	0
51-11182-04	D.	01	.:ew	0
351-11182-04		04	::cw	0
51-11182-04	r4	90	No.	0
351-11182-04	Ω,	07	::ew	0
351-11182-0	Δ,	96	::ew	0
351-11182-04	Ω,	60	: ew	0
1-11182-04	1st-Row Pinion	10	New	0
1-11181-04	2nd-Bow Pinion	[0		c
351-11181-04		10	7. C.	· c
51-11181-0	2nd-Row Pinion	15	i.ew	0
351-11181-04		16	.iew	0
351-11181-04	Д	17	ew	0
351-11181-04	C	19	::ew	0
1-04	2nd-Row Pinion	23	New	0
RG351-11184-041	Ring Gear	04	No.	0
22313VAG	ical	112	::ew	0
22313VAG	ical	1110	l:ew	0
22313VAG	Spherical Bearing	1.15	New	O
22313VAG	ical	1125	30%	0
22313VAG	cal	1126	No.	0
22313VAG	ical	131]:ew	0
22313VAG	ical	145	New	0

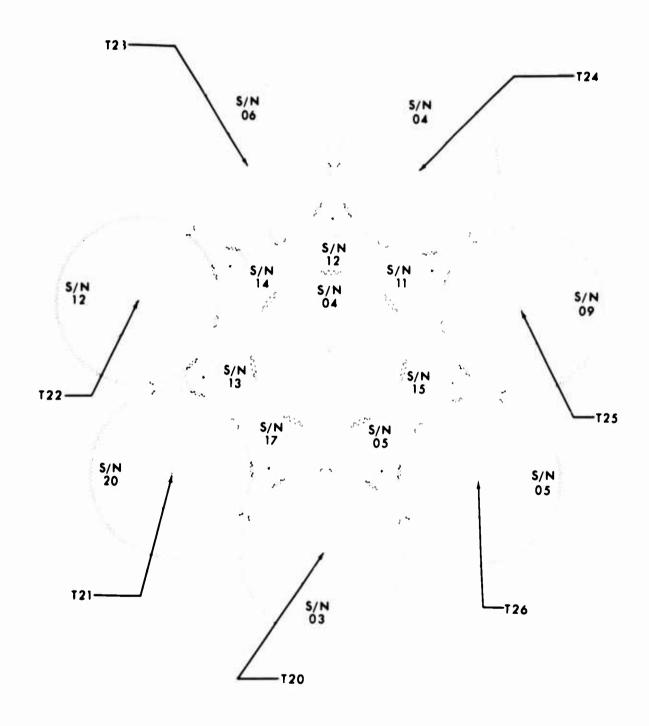


Figure 38. Component Location - Test Roller Gear Unit.

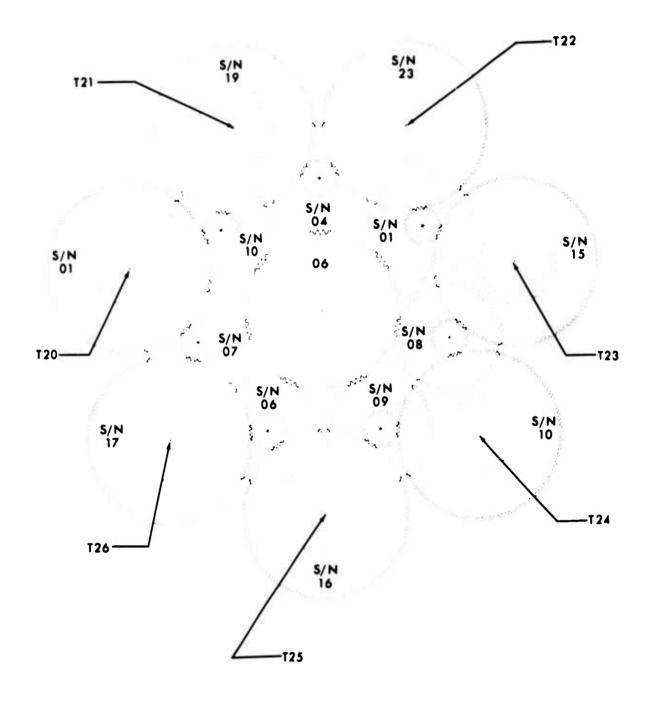


Figure 39. Component Location - Dummy Roller Gear Unit.

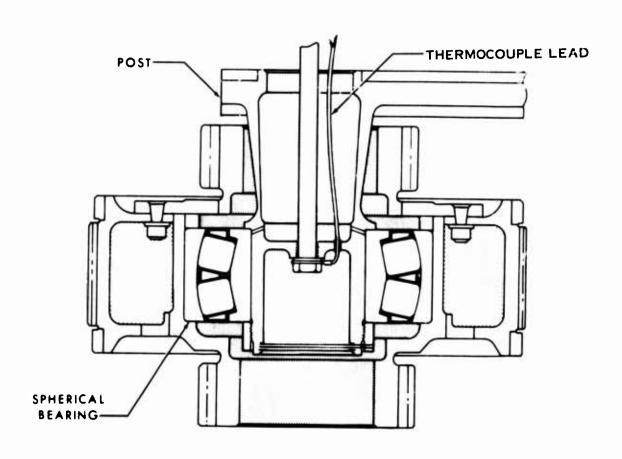


Figure 40. Thermocouple Installation - Second-Row Pinion Post.

Figure 41. Roller Gear Drive Assembly - Test Gearbox.

The test gearbox was installed in the regenerative test stand and checked out in a manner similar to the tests conducted on the dummy gearbox during the no-load lubrication test. The dummy gearbox, upon completion of the internal modifications performed after the no-load lubrication test and the calibration of the main rotor shaft, was installed in the test stand with the test gearbox as shown in Figure 22. An input drive shaft was installed between the test and dummy gearboxes as shown in Figure 42. The input drive shaft contains pole pieces (see Figure 42) that are used in measuring the torque transmitted through the rotating shaft when under load. When the shaft is subjected to torque, one end of the shaft is deflected relative to the other end. This difference in torsional deflection is measured by means of a magnetic pickup which detects the relative displacement of the pole pieces. To accomplish this with a single pickup, the pole pieces are cantilevered from each end of the shaft and are free floating. The pole pieces are of ferrous material to induce a signal in the pickup. signal from the pickup is then conditioned into an analog output proportional to shaft twist and displayed on an indicating system.

The natural frequency of the installed interconnect shaft (Figure 42) was determined by conducting a "rap" test. This test consisted of installing a small crystal accelerometer to the mid-span of the shaft, the output of which was recorded with a light beam oscillegraph. A 60 Hertz reference trace is used as a time base. The shaft was "rapped" and the resulting output of the accelerometer was a trace of the natural frequency in a decaying curve. The frequency of the accelerometer was compared with the 60 Hertz reference trace to determine the frequency of the first shaft critical mode. Operation of this shaft was determined to be unacceptable at 100 percent speed because the shaft critical mode was found to be within 3 percent of the operating speed. However, to expedite the bevel gear pattern development tests, testing with this shaft was permitted to a maximum of 50 percent speed.

In order to check out the test stand, both gcarboxes were run for 1 hour and 18 minutes (0 - 1:18 total test time) with no input shafts. After the installation of the drive shafts, as described above, the gearboxes were run for 47 minutes at 50 percent speed. At 2:05 test hours, the test stand was shut down for visual inspection of the input bevel gear patterns through the ports. However, shields incorporated as a result of the no-load lubrication test hindered inspection. The test stand was immediately restarted and run at 50 percent speed; at 2:26 test hours the test stand was then shut down.

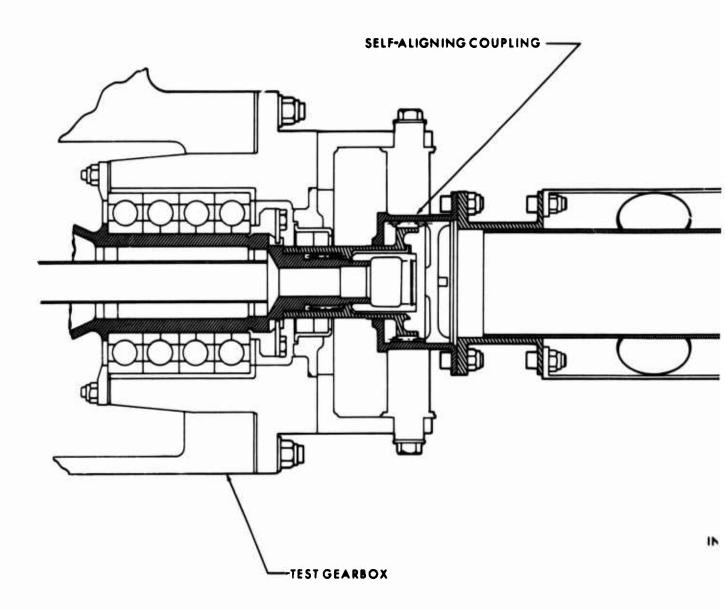
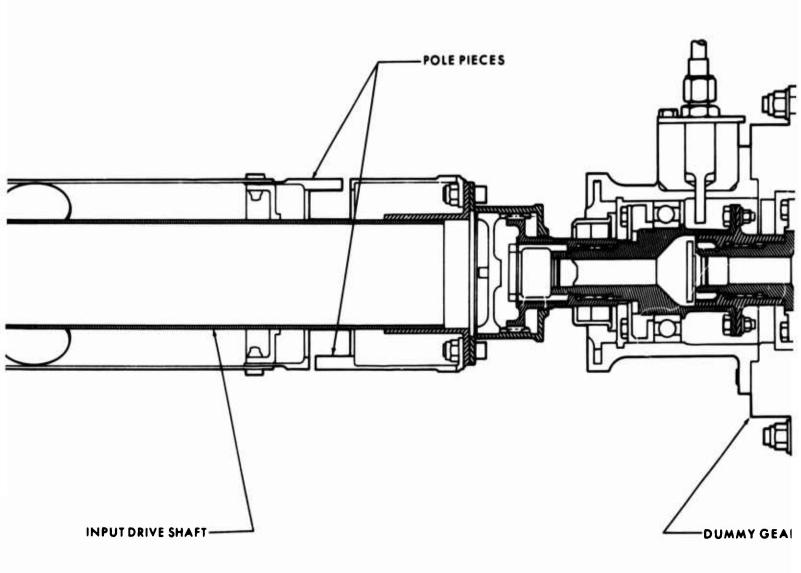
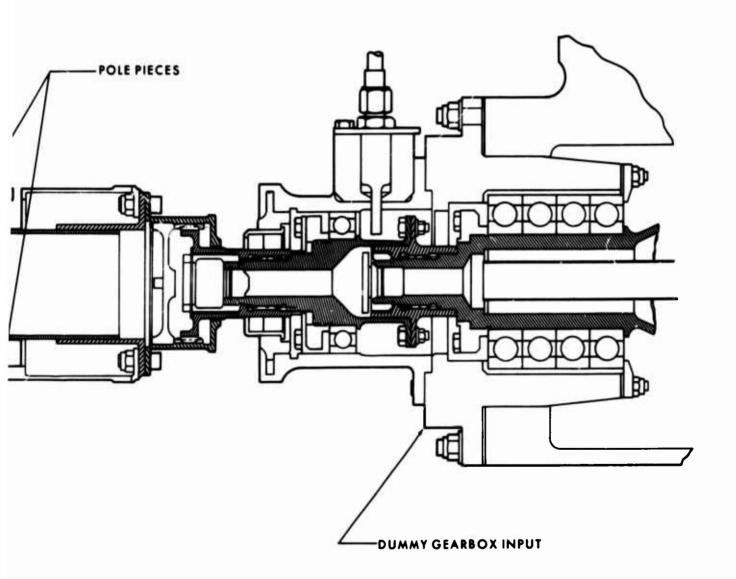


Figure 42. Drive Shaft Installation - Regenerative Test Stand.









To overcome the 50-percent speed limitation, a redesigned input drive shaft was fabricated. This new shaft, Figure 43, eliminates the cantilevered pole pieces, thereby reducing the weight of the shaft. A "rap" test of this configuration indicated critical speed to be acceptably high at 130 percent operating speed. In order to adjust the test facility for an equal torque split between the two input shafts, a new torque measuring system had to be devised for the drive shafts because of the removal of the pole pieces. This was accomplished by the bonding of Wheatstone bridge strain gages on the inside diameter of the drive shafts. Torque was applied to the system and measured statically. It was adjusted by "slipping" the proper coupling until a satisfactory torque balance was achieved.

With both redesigned shafts installed and an equal torque split established between the input shafts, gear pattern development testing was continued. In a series of incremental steps, load was increased up to a total input power of 3000 hp at the test main rotor shaft while operating at 100 percent speed (2:26 - 2:32 test hours).

The tail drive shaft torque loop was connected, and a series of incremental load changes up to 500 hp was conducted to establish tail takeoff bevel gear patterns and to check out the tail loop of the facility (2:32 - 3:42 test hours). At the completion of this series of tests both gearboxes were removed from the test stand for disassembly and inspection.

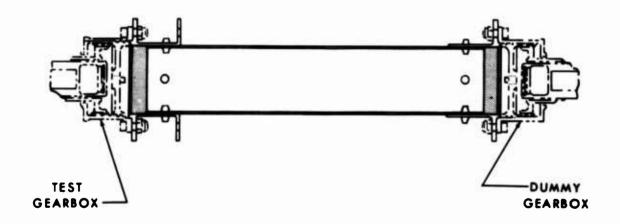


Figure 43. Strain Gaged Drive Shaft,

Test Results

The input bevel pinions exhibited a hard line in the root of the gear teeth, the result of insufficient chamfer on the edge of the bevel gear teeth. These teeth were dressed with 0.010/0.015 inch chamfer, thereby alleviating this problem. Apart from this, the gear patterns were excellent with contact patterns extending across the pinion face as shown in Figure 44. The tail takeoff bevels were also excellent, showing patterns very similar to those shown on tapes of the master gears. The combining spur gears and roller gear patterns were hardly visible. Evidence could be seen of very slight sliding on either side of the pitch line.

On the basis of these inspections, authorization to manufacture the gears for the third and fourth gearboxes and all spares was given.

Compliant Bearings

During the gear pattern development test runs, extremely high temperatures were recorded under high load conditions in the test gearbox at the second-row pinion bearings. This gearbox was assembled with compliant bearings, an advanced state-of-the-art bearing involving modifications to a cylindrical roller wherein both ends of the roller are recessed as shown in Figure 45. These hollow ended rollers were developed with the objective of increasing the range of misalignment which a cylindrical roller bearing could endure. Redistribution of the load due to misalignment is achieved by elastic deformation of the roller ends which produces a contact area without end effects (i.e., high stresses). These bearings were designed for this application to accommodate a slope of 0.0018 inch/inch at a load of 10,950 pounds.

The temperature of these bearings, which approached 150° C after a few minutes of operation at 3000 hp, never stabilized and limited high power test runs to 3 to 4 minutes duration. In contrast, the dummy gearbox second-row pinion spherical bearings operated at 85° C. Inspection revealed that the compliant bearings experienced overheating due to interference of the roller end faces with the inner and outer race bearing shoulders. The shoulder of the inner race and the inside face of the spacer, Figure 46, were heavily scored and discolored from contact with the end faces of the rollers. The reaction torque on the second-row pinion posts is 76,000 ft/lb when transmitting 3000 hp. This resolves to a tangential load on each cantilevered post of 10,950 pounds. The forces on the second-row gear meshes induce it to remain parallel; therefore, any slope of the pinion post has to be accommodated by the bearing. Detailed inspection of the bearings revealed 0.003 inch axial play with the rollers and outer race and 0.002 inch



Figure 44. Dynamic Gear Pattern - Input Bevel Pinion.

with the rollers and inner race. This was insufficient axial clearance to accommodate the slope of 0.0018 inch/inch induced on the shaft when transmitting full torque. Since the bearing could not absorb all the slope induced on the shaft, some was reacted by the gear. Inspection of the second-row gear assemblies revealed a slight burr on the top roller caused by the canted second-row assembly being reacted on the first-row pinion roller shoulder. This resulted in slight burrs on the first-row pinion shoulders. These and the second-row pinions were reworked to remove the burrs.

The compliant bearings of the dummy gearbox discussed above were replaced by spherical roller bearings. Also at this time, the main drive electric motors for the S-61 test facility were removed and rewound to increase their individual capacities from 150 hp to 225 hp. This requirement was to prevent motor overheating when running the roller gear transmissions. If the motors were not rewound, it would have necessitated operating in an overload condition. The overload condition would have generated excessive heat in the windings and possibly induced a breakdown in the wire insulation.

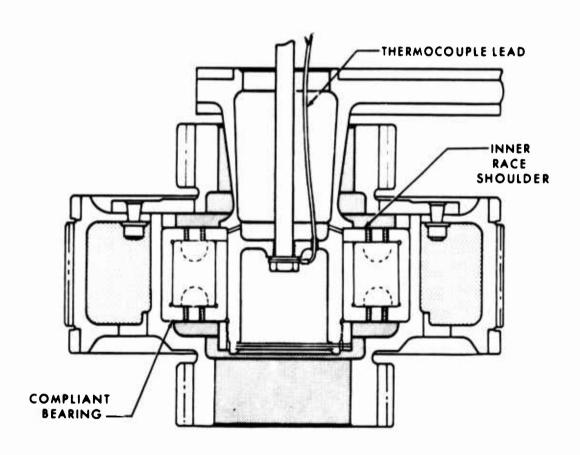
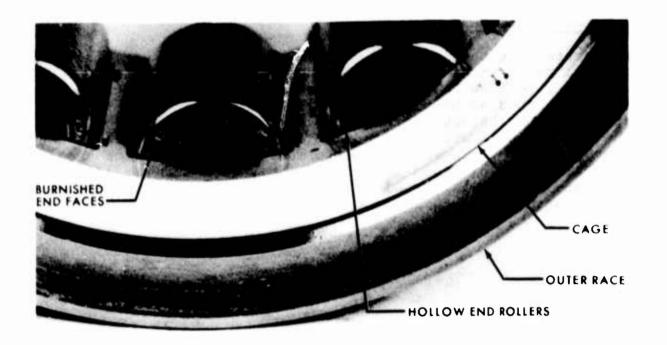


Figure 45. Compliant Bearing Installation - Second-Row Pinion Post,



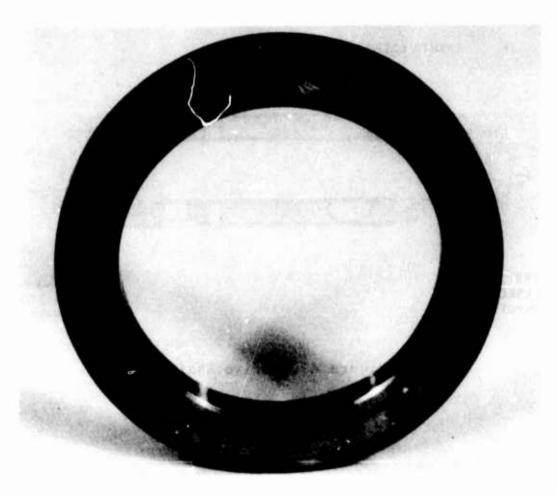


Figure 46. Compliant Bearing Damage.

INITIAL DEVELOPMENT TESTS

Preparatory to the 200-hour endurance tests, a series of initial development tests were conducted. In these test runs powers up to 3700 hp total input were imposed on the transmission with 3000 hp being transmitted through the roller gear drive and the balance through the tail rotor takeoff section. The purpose of these tests was to evaluate the S-61 roller gear transmission, to assess its performance characteristics under high loads for extended periods of time, to determine if there were any fundamental problems with the roller gear concept, and to evaluate manufacturing and assembly procedures.

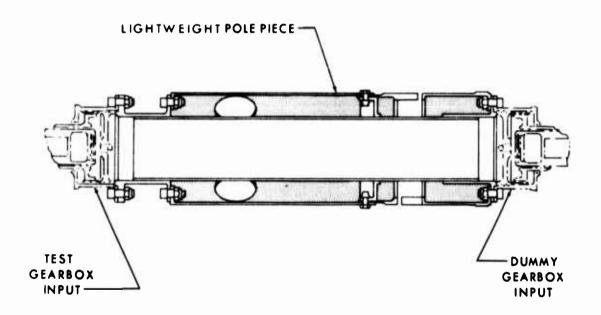


Figure 47. Drive Shaft.

Both test and dummy gearboxes were reinstalled in the regenerative test stand with a new input shaft assembly, Figure 47. This shaft was fabricated with lighter weight pole pieces than were used on the shaft for the gear pattern development test. The lighter pole pieces were designed to raise the critical speed of the shaft sufficiently to permit operation at 100 percent speed. A natural frequency test, similar to the one described for the gear pattern development test, indicated a natural frequency at 110 percent operating speed. Recognizing that with the limitations of this type of test a critical speed problem could be encountered, it was nevertheless decided to begin the initial testing with this shaft because of the desirability of having a dynamic torque measuring system.

The first segment of testing began at 3:42 total test time. Upon completing a warm-up period at 50 percent speed, facility speed was accelerated toward 100 percent speed. At approximately 95 percent speed, the long input shaft pole piece made contact with the protective shaft guard in the facility, and the test stand was immediately shut down (4:17 test hours).

The subsequent inspection revealed damage to the input shaft pole pieces and damage to the dummy gearbox input extension. Removal of the dummy left-hand input chip detector revealed numerous metallic particles, Figure 48. The input shafts and the dummy gearbox inputs were then removed for detail inspection. Teardown inspection of the left-hand dummy input revealed a complete breakdown of the ball bearing with extension housing, Figure 49. Severe spalling of the raceways had occurred from the high inertia loads of the whirling shaft. The balls had started to nelt from the heat caused by the spalling of the raceways. Inspection of the left-hand input bevel pinion stack bearing assembly revealed an uneven wear path in the preload bearing of the four ball bearing stack caused by a raised nick on the split inner race. In addition, debris had passed through the preload bearing and scored the balls. This bearing assembly was deemed unusable and replaced. The input bevel pinion roller bearing was inspected, found satisfactory, and reinstalled. The carbon graphite face seal was damaged as was the crowned spline coupling shaft where the O-ring had scored the chrone plate 0-ring seat, Figure 50. The seal and spline coupling were also replaced. Inspection of the right-hand dummy extension and input section showed minor damage to the stack bearings, roller bearing, and extension housing ball bearing. These bearings were replaced. The carbon seal and coupling were also damaged, resulting in their replacement.

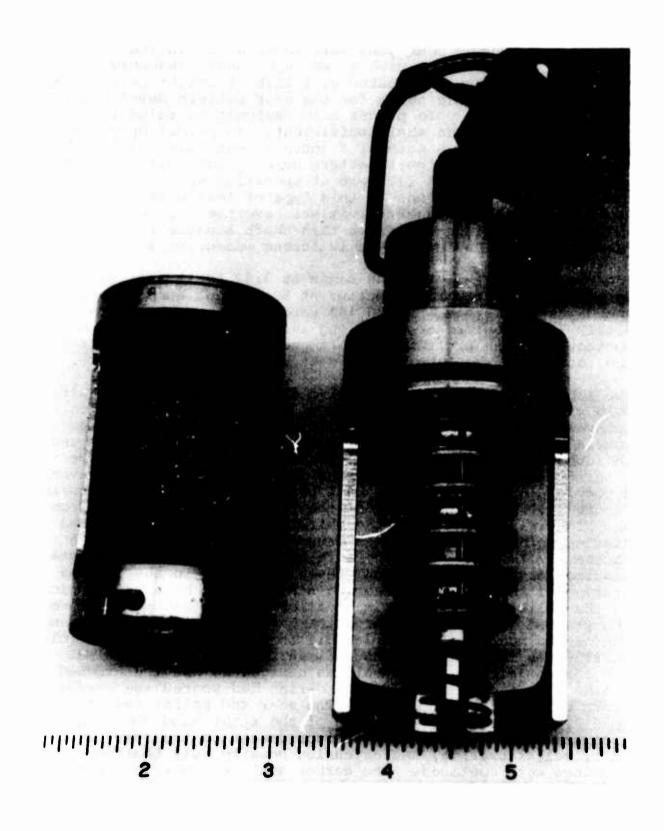


Figure 48. Chip Detector - Dunday Gearbox.

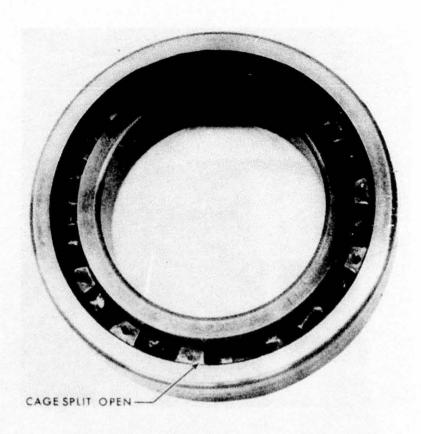


Figure 49. Ball Bearing - Dummy Gearbox Input.

Inspection showed that the test gearbox inputs were in good condition; however, the grease in the right-hand coupling had discolored. This coupling was repacked and reassembled. The left-hand coupling was in satisfactory condition.

Prior to reinstallation of the dummy gearbox input bevel pinion assemblies, blank covers were installed as seals over the dummy input bores, and the test stand was operated with no load at 50 percent and 100 percent speed to check out the gearboxes. The dummy inputs were then reinstalled. The input drive shafts were modified by removing the pole pieces, thereby reverting to the shaft configuration of Figure 43. The right-hand input shaft was strain gaged and calibrated.

The test stand with only the left-hand drive shaft installed was run for one hour at 1850 hp. This drive shaft was then removed to be strain gaged and calibrated. The right-hand drive shaft, which had been strain gaged and calibrated, was then installed and the test stand operated with only this drive shaft for one hour at 1850 hp. Testing was continued at 6:17 hours total test time with both shafts installed. Testing was halted at 17:28 total test time for a facility problem in the main rotor shaft coupling.

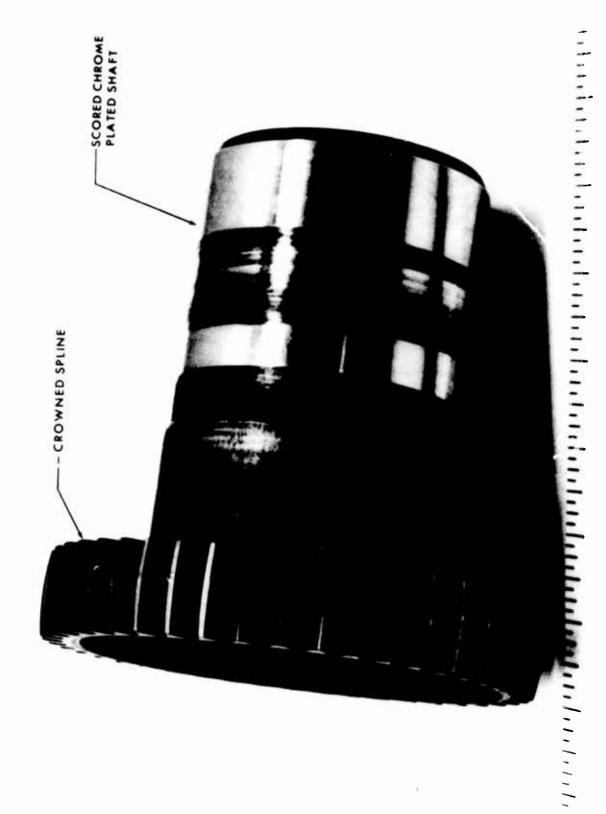


Figure 50. Splined Shaft - Input Coupling.

At this time both test and dummy gearboxes were partially disassembled. The roller gear units were removed from their respective gearboxes, disassembled and inspected. The roller gears from both gearboxes showed excellent gear tooth patterns on the sun/first row pinion and second row pinion/ring gear meshes. The first/second row gear pattern mesh was barely discernible. Visible on the shoulder of the first/second row lower rollers were signs of scuffing. Figure 51 shows gear serial number 12 which is the worse case. Lubrication to this area by gravity from the residue of the first/second row gear mesh was apparently insufficient. In order to ensure adequate lubrication to the first/second row lower rollers, orifices were drilled into the seven probe jets which directed oil onto the input side of the sliding contact surfaces of the rollers.



Figure 51. Scuffed Roller Shoulder - First-Row Pinion.

Upon completion of the above modification, testing was continued. At 18:28 total test time, the chip detector of the dummy gearbox roller gear unit was activated, and the test stand was immediately shut down. Inspection revealed that activation of the chip detector had been caused by an oil sealing washer which had come loose because of incorrect installation. No gearbox damage was sustained and a new washer was installed. While the gearbox was partially disassembled, it was noted that the main rotor thrust bearing was burred and had a debris pit in the outer race. This necessitated its replacement.

The gearbox was reassembled and installed in the test stand. Testing was continued at 18:28 test time.

At a total test time of 26:28 hours, chips were found in the forward sump chip detector of the test gearbox, Figure 52. Because of the compartmentalization of the gearbox, the chips could have originated only from the roller gear unit. The test and dummy gearboxes were removed from the test stand for disassembly and inspection.

Visual Inspection

Visual inspection of the test gearbox first-row pinions revealed spalling of the small roller diameters of pinion serial number 05 located as shown in Figure 53. This pinion shows a spalled area approximately 2.5 inches in length around the lower roller in Figure 54. Spalling of the top roller was less severe, extending for approximately 0.5 inch, Figure 55. Visual inspection of the remaining first-row pinions revealed some evidence of edge loading but no surface breakdown. The roller surfaces of the second-row pinions showed no wear. The sun gear rollers, although showing slight pitting due to debris, displayed no signs of fatigue damage. Inspection of the dummy transmission first-row pinions indicated burnishing of several small roller diameters, Figure 56. Magnetic particle inspection of all roller gear components from the test and dummy gearboxes did not reveal any surface orientated cracks.

Dimensional Inspection

A dimensional inspection of the sun, first-row pinions and second-row pinions indicated all critical dimensions including gear spacing and timing, roller diameters, and concentricity to be within the required drawing dimensions. Figures 57 and 58 show the inspection equipment used for measuring the 'X' dimensions between the master index teeth on the outer and inner gears of the first-row pinions.

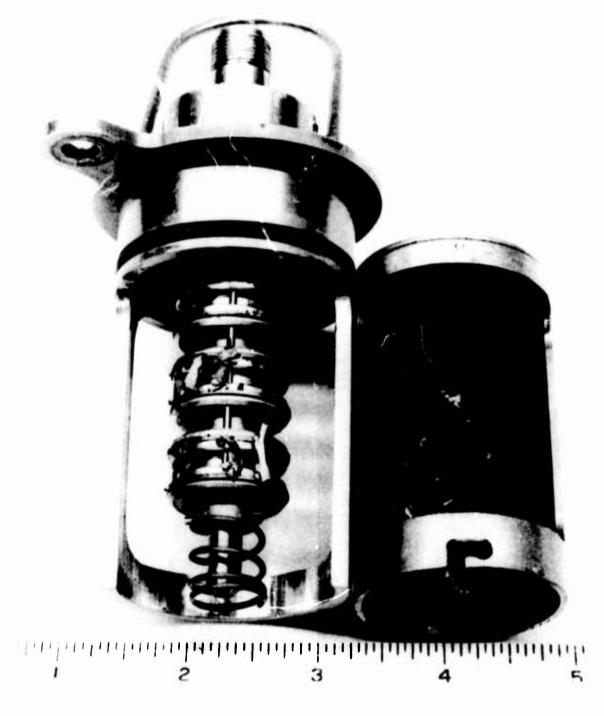


Figure 52. Chip Detector - Test Gearbox.

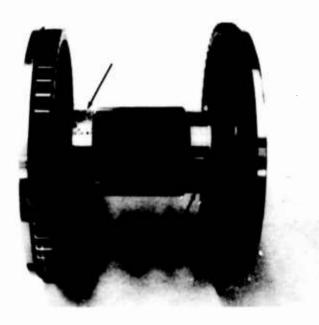


Figure 53. Spalled Rollers - First-Row Pinion Test Gearbox.



Figure 54. Spalled Lower Roller.



Figure 55. Spalled Top Roller.

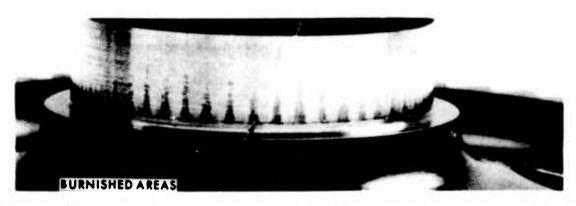


Figure 56. Burnished Roller - First-Row Pinion Dummy Gearbox.

Metallurgical Inspection, First-Row Pinion Roller Weld Fracture

Microscopic examination of first-row pinion serial number 05 revealed that spalling of the lower roller was caused by fatigue cracking originating below the surface and propagating to the surface. A cross-sectional sample, Figure 59, taken in an unspalled area immediately adjacent to the spalling revealed a subsurface crack extending through the electron beam weld zone as shown in Figure 60. There was no evidence of this crack at the surface. Metallographic examination revealed a series of voids along the weld line as shown in Figure 61. Cracks were evident extending from one of these voids, as indicated by the arrow in Figure 61 and shown in Figure 62. Examination revealed a desired case microstructure of martensite and tempered austenite with no evidence of carbide network.

Microscopic examination of the spalling on the roller from the top side of the assembly revealed fatigue cracking of the surface with no evidence of subsurface origins. A metallurgical specimen taken adjacent to the spalling did not exhibit subsurface cracking in this area. Voids in the weld zone, similar to those evident in the weld in the opposite roller, were evident. Spalling of this surface may have been a result of load transfer occurring from a loss of contact area when the lower roller spalled.

A microhardness traverse through the case-hardened surface of the small diameter rollers, in a direction normal to the surface, showed a slight reduction in hardness and effective case depth on both top and lower rollers. This plot is shown in Figure 63. This reduction is explained by the removal of stock during the final roller grinding operation and is probably the result of high temperatures generated during electron beam welding. The microhardness survey reveals a smooth transition from case to core with effective case depth measured at $R_{\rm C}$ 50. The low case hardness and depth were not considered factors in the spalling, since the cracking originated subsurface at voids in the weld.



Figure 57. Inspection - First-Row Pinion Small Gear.

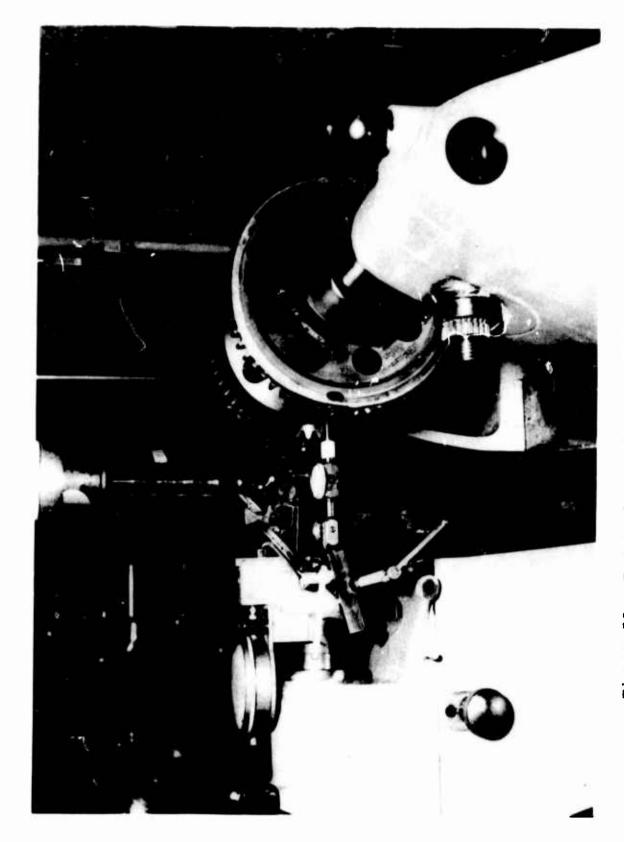


Figure 58. Inspection - First-Row Pinion Large Gear.



Figure 59. Sectional View - First-Row Pinion.

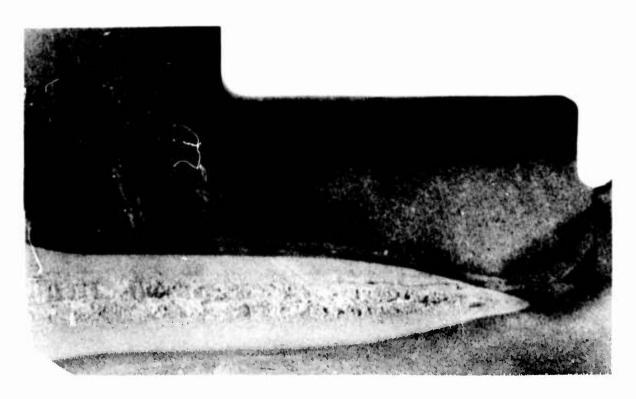


Figure 60. Electron Beam Weld - First-Row Pinion.

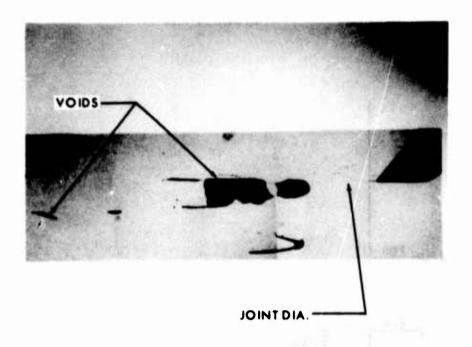


Figure 61. Voids - Electron Beam Weld.

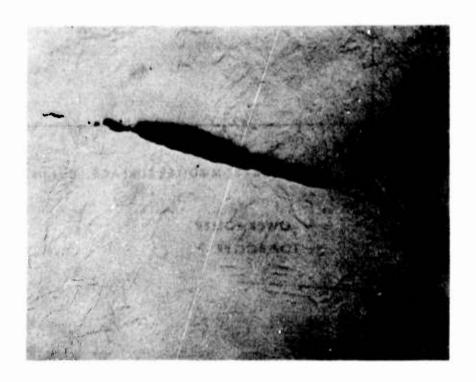


Figure 62. Cracks Extending From Electron Beam Weld Voids.

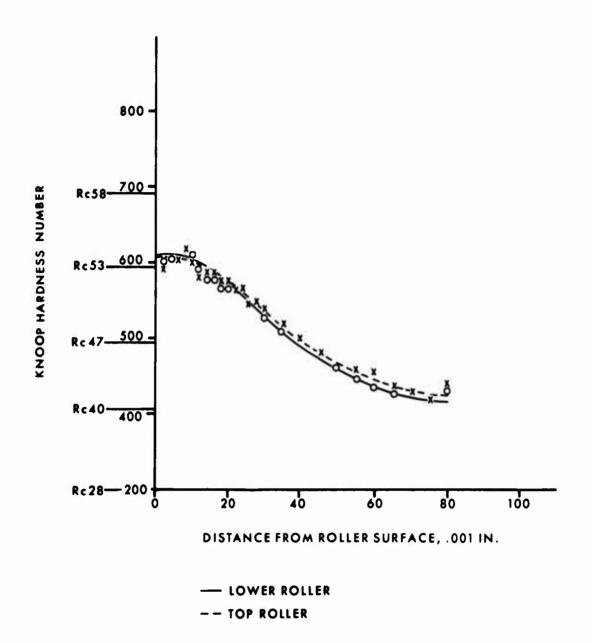


Figure 63. Roller Microhardness Versus Depth - First-Row Pinion.

It was concluded that the fracture initiated in the area of the electron beam weld. Subsurface stresses produced by roller contact forces caused cracking in areas of porosity of the electron beam weld. The weld porosity was most likely caused by the depth of the weld and the speed at which the part had to be welded in order to avoid affecting the hardness of the roller contact surfaces.

Ultrasonic Inspection, First-Row Pinion

Ultrasonic testing was conducted on the small diameter rollers of the first-row pinions to determine if detection of subsurface cracking was possible. A direct contact Krautkramer ultrasonic flaw detector was used in conjunction with a dual transducer utilizing longitudinal waves. Acoustic contact between the transducer and the roller surface was by glycerine. A 0.25-inch-thick steel reference block was used for calibration of the ultrasonic equipment, this being representative of the distance from the roller surface to the weld. Gear assembly serial number 14 from the test gearbox exhibited a sonic indication of an abnormality. Laboratory sectioning through the groove between the small gear and adjacent roller revealed subsurface cracking extending for approximately half the circumference, as shown in Figure 64. series of voids was apparent around the entire circumference, as shown in Figure 65. Separation of the crack interface revealed multiple fatigue zones originating at voids in the weld zone, shown typically in Figures 66 and 67. The cracking in this gear is similar to the cracking evident in gear assembly serial number 05.

First-Row Pinion Burnishing

It was concluded that the burnish markings which occurred only on the rollers in the dummy roller gear unit were the result of applying the lubricant into mesh. The probe jets were designed to lubricate the test gears and rollers out of mesh. Since the dummy transmission rotates in the opposite direction, lubrication for this box was applied into mesh, resulting in localized overheating.

On the basis of the findings, a two-phase course of action was decided upon. In the first phase, an ultrasonic inspection technique would be developed to ensure the integrity of the electron beam welds. The initial development test would continue with first-row pinions already manufactured provided they passed the ultrasonic inspection. The roller surface finish on all rollers would be improved. The second phase, to be incorporated should cracking occur in testing of these first-row pinions, would be a redesign of the first-row pinion assembly, which incorporates an electron beam butt welded joint as shown in Figure 68.

Average Control

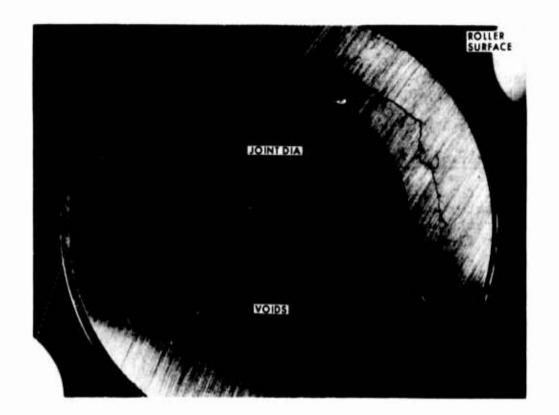


Figure 64. Circumferential Crack - Roller/Gear Interface.

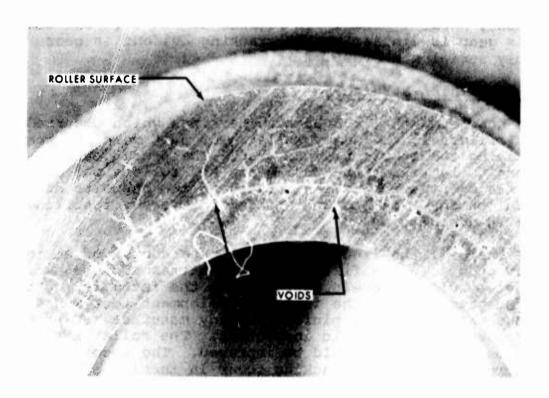


Figure 65. Circumferential Crack - First-Row Pinion.



Figure 66. Roller Separation - First-Row Pinion.

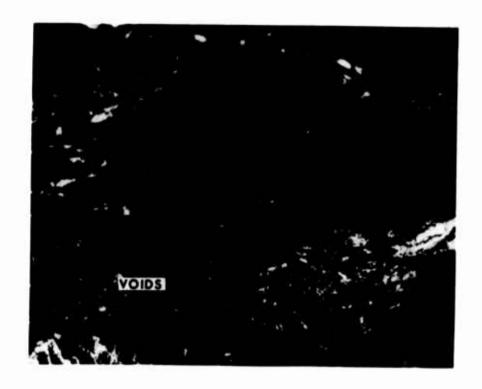


Figure 67. Voids - First-Row Pinion Roller.

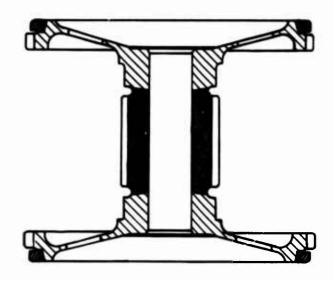


Figure 68. First-Row Pinion - Butt Weld Configuration.

Gearbox Modifications

Lubrication oil to the roller gear unit is supplied from the manifold via a cored line in the main housing to a reservoir in the outer shaft housing. Seven probe jets tap into this reservoir and direct oil to each roller/gear mesh. A restrictor aft of the manifold is used to regulate the amount of oil supplied to the roller gear unit. Figure 69 shows the oil path to the probe jet. At this time the size of the feed hole to the reservoir was increased from 0.18 to 0.37 inch diameter and the outer shaft housing was machined to increase the volume of the reservoir.

Inspection of the roller bearings on the input bevel pinions of the dummy gearbox revealed track marks in the outer race and glazing of the inner race, Figure 70, which necessitated their replacement.

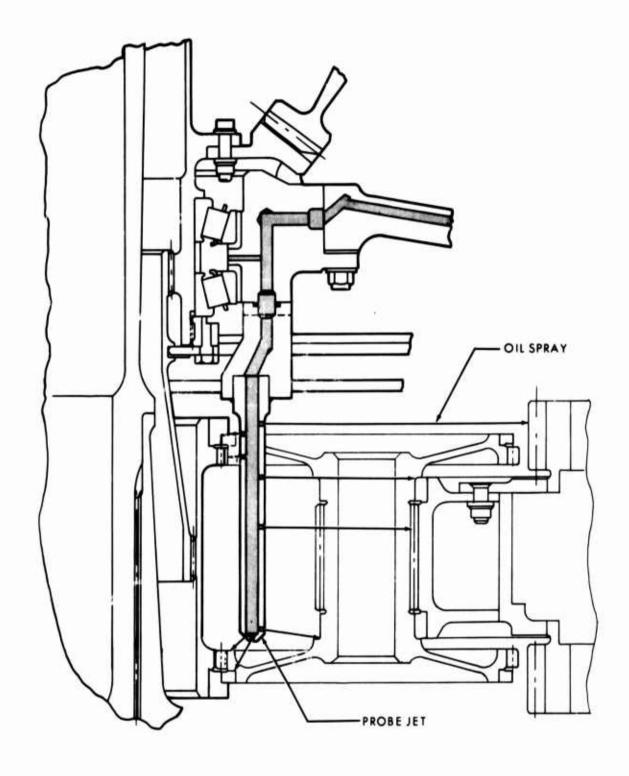
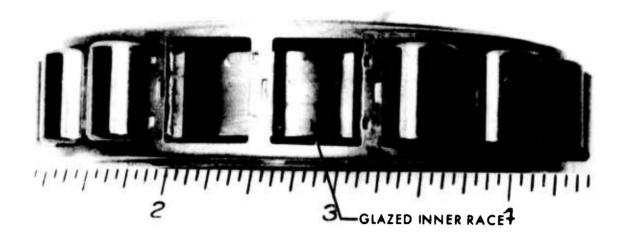


Figure 69. Probe Jet - Roller Gear Unit.



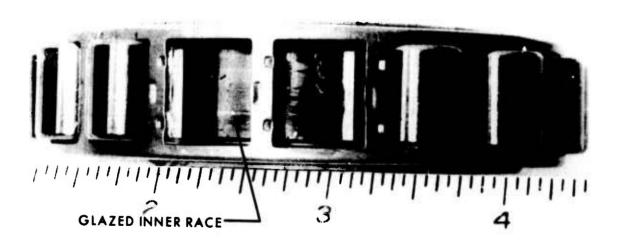


Figure 70. Roller Bearings - Input Bevel Pinions.

With the completion of the internal modifications to the transmission housings, and the assembly of both test and dummy roller gear units with new sun gears and first- and second-row pinions, as listed on Tables IX and X and located as shown in Figures 71 and 72, the gearboxes were reassembled and reinstalled in the test stand for continuation of the initial testing. A torque split at the inputs was obtained using strain gaged drive shafts. Testing was then continued for an additional 9.5 hours (total test time 35:58 hours), at which time testing was terminated when a large quantity of metallic particles were found on the dummy gearbox sump chip detector, as shown in Figure 73. Inspection of all other chip detectors in the test and dummy gearboxes showed them to be free of metallic particles. The gearboxes were removed from the test facility for teardown inspection. The power spectrum the gearboxes were subjected to during the 9.5 hours of testing is given in Appendix I. Review of the data sheets revealed no indication that a malfunction had or was occurring.

Removal of the dummy gearbox sump showed more chips similar to those in the chip detector. Removal of the roller gear drive and the disassembly of the output flange at the ring gear displayed the unit and parts located as shown in Figure 72. An assembly check using the timing marks on the first— and second—stage pinions revealed that all gears aligned correctly and the unit rotated freely. Further examination of the roller gear unit revealed separation of the second—row pinion, top, output ring gear meshing gear, serial number 32 at the 4.061—inch—diameter weld, Figure 74.

Visual Inspection

Inspection of the fractured second-row pinion revealed a machined surface approximately 0.090 inch wide and extending for approximately 50 percent of the circumference in the fractured area as indicated in Figure 75. This machined diameter is the electron beam weld joint face between the flange and the gear.

The remaining second-row pinions in the roller gear unit incurred damage on the large diameter gears from debris. Figure 76 is typical of the damage sustained by these gears. Figure 77 shows a similar type of damage sustained by the first-row pinions. The ring and sun gears from the dummy gearbox roller gear unit sustained slight superficial damage. It is interesting to note that the rolling surfaces on all pinions were in excellent condition.

	TABLE IX. TEST #2 - RO TEST GEARBOX	OLLER GEAR	ROLLER GEAR UNIT COMPONENTS-OX	
Part Number	Nomenclature	Serial Number	Status	Test Hours:Minutes
RG351-11183-041	Sun Gear	80	New	0
51-11182-04	-Row	19	New	0
51-111	1st-Row Pinion	21	New	0
51-11182-04	-Row	23	New	0
51-11182-04	-Row	5 6	New	0
51-11182-04	-ROW	27	New	0
-11182-04	-ROW	29	New	0
1-11182-04	1st-Row Pinion	30	New	0
		•		•
51-11182-04	-ROW	12	New	0
51-11182-04	-ROW	25	New	0
-11182-04	2nd-Row Pinion	27	New	0
	-ROW	34	New	0
51-11182-04	2nd-Row Pinion	36	New	0
-11182-04	2nd-Row Pinion	40	New	0
1-11182-04	2nd-Row Pinion	41	New	0
RG351-11184-041	Ring Gear	02 Us	Used in Test #1	26:30
231	rical	N	New	0
231	rical	NS N	New	0
231	rical	N14	New	0
2313	rical	N28	New	0
2313	rical	N33	New	0
22313 VAG	rical Bear	N34	New	0
231	Spherical Bearing	N37	New	0

	TABLE X. TEST #2 - ROL DUMMY GEARBOX	OLLER GEAR UN OX	ROLLER GEAR UNIT COMPONENTS- BOX	
Part Number	Nomenclature	Serial Number	Status	Test Hours:Minutes
RG351-11183-041	Sun Gear	03	New	0
1-11182-04	1st-Row Pinion	18	New	0
51-11182	st-Row	20	New	0
351-11182-04	st-Row	22	New	0
351-11182-04	1st-Row Pinion	24	New	0
351-11182-04	st-Row	25	New	0
351-11182-04	-ROW	28	New	0
-11182-04	1st-Row Pinion	31	New	0
RG351-11181-042	2nd-Row Pinion	28	Mew	c
51-11		32	New	. 0
-04	-Row	33	New	0
RG351-11181-042	2nd-Row Pinion	39	New	0
51-11181-04	-Row	42	New	0
51-11181-04	-ROW P	43	New	0
-04	-Row	47	New	0
RG351-11184-041	Ring Gear	04 Used	d in Test #1	26:30
m		N2 Used	in Test #	26:30
-		N10 Used	in Test #	26:30
13		N15 Used	d in Test #1	26:30
13		N25 Used	in Test #	26:30
13		N26 Used	in Test #	26:30
22313 VAG		N31 Used	in Test #	26:30
_	Spherical Bearing	N45 Used	d in Test #1	26:30

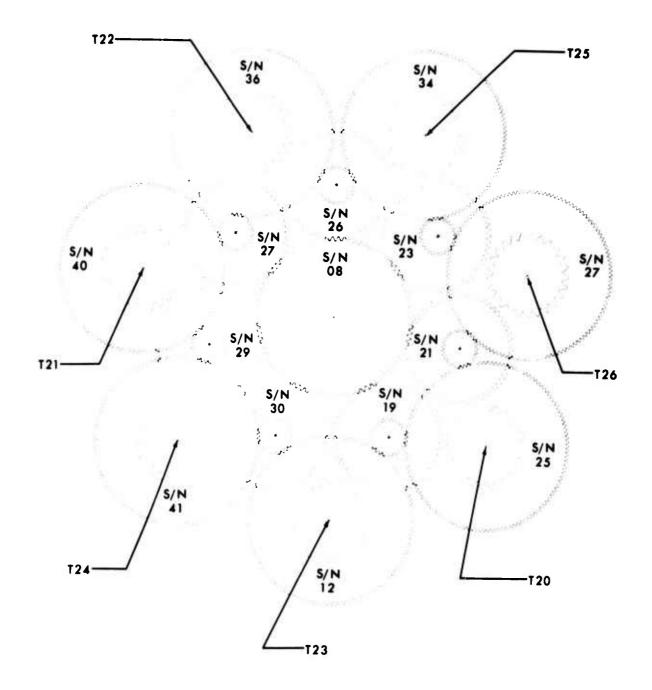


Figure 71. Component Location - Test Roller Gear Unit.

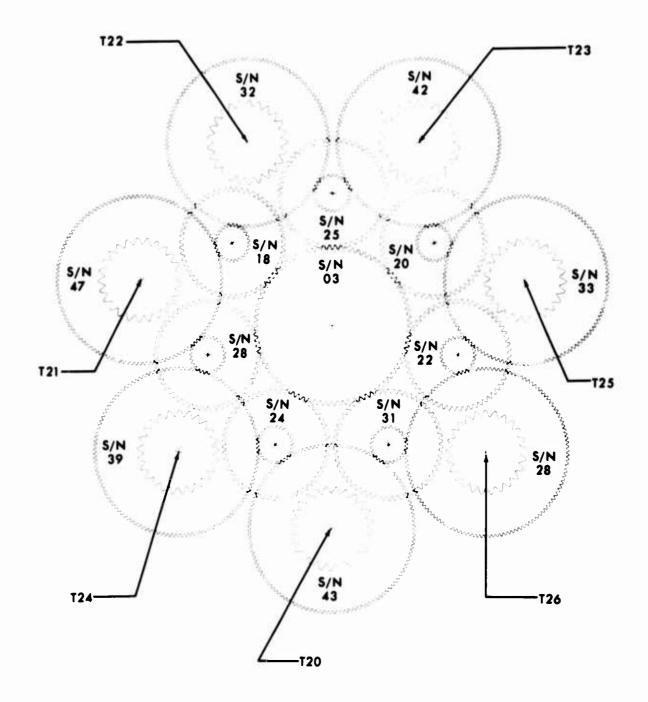


Figure 72. Component Location - Dummy Roller Gear Unit.



Figure 73. Chip Detector - Dummy Gearbox.



Figure 74. Gear Separation - Second-Row Pinion Dummy Gearbox.

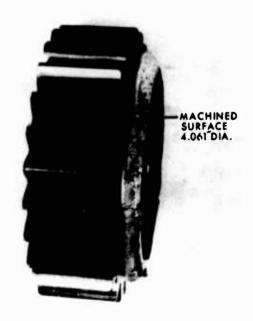


Figure 75. Separated Second-Row Pinion Gear,

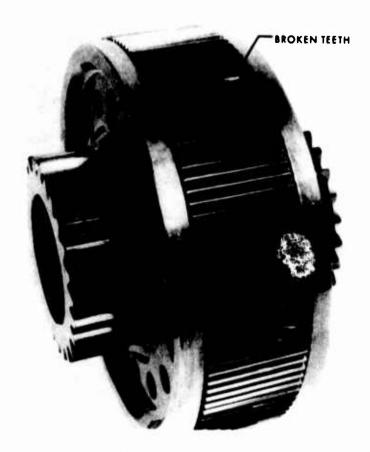


Figure 76. Gear Teeth Damage - Second-Row Pinion.



Figure 77. Gear Teeth Damage - First-Row Pinion.

Visual inspection of the test roller gear unit showed all parts to be in excellent condition. Magnetic particle inspection of the sun and first-row pinions failed to reveal any surface orientated cracks; it did, however, reveal cracks in the gear/flange assemblies of second-row pinions serial numbers 34 and 40 in the same area where the fracture of serial number 32 occurred. Subsequent examination of second-row gear/flange assemblies used during the initial test revealed similar cracks in serial numbers 12 and 15. Figure 78 shows the crack found in serial number 12 which is typical. The 0.25-inch-wide wear band on the 5.20-inch diameter is caused by the spacer which clamps the outer race of the spherical bearing.

Dimensional Inspection

To check if any undue wear had occurred in the dummy gearbox roller gear unit, a dimensional inspection of the rollers was conducted which revealed no wear of the surface.

Metallurgical Inspection

Metallurgical examination of the second-row gear assembly, serial number 32, revealed a fracture in the weld area between the gear and flange extending for the entire circumference of the gear. Fracture examination revealed fatigue cracking originating at the end of the weld zone as indicated in Figure 79. Evident in the fracture is a machined surface, Figure 80. A cross-sectional sample through the weld revealed that the weld beam had missed the joint between the mating components, as indicated in Figure 81 and Figure 82. Examination revealed that while complete weld beam penetration had been accomplished, fusion had not occurred where the center of the weld beam missed the mating surfaces. Metallographic examination of the microstructure in this area revealed an as-cast weld zone of typical core structure in the mating components. Hardness of the flange, gear and weld zone measured Rc 40, 38 and 40, respectively. Examination of gear/flange assembly serial number 40 shows a crack propagating from the end of the weld through the weld heat affect zone as seen in Figures 83 and 84.

It was concluded that fracture occurred because of incomplete fusion on the exit side of the weld.

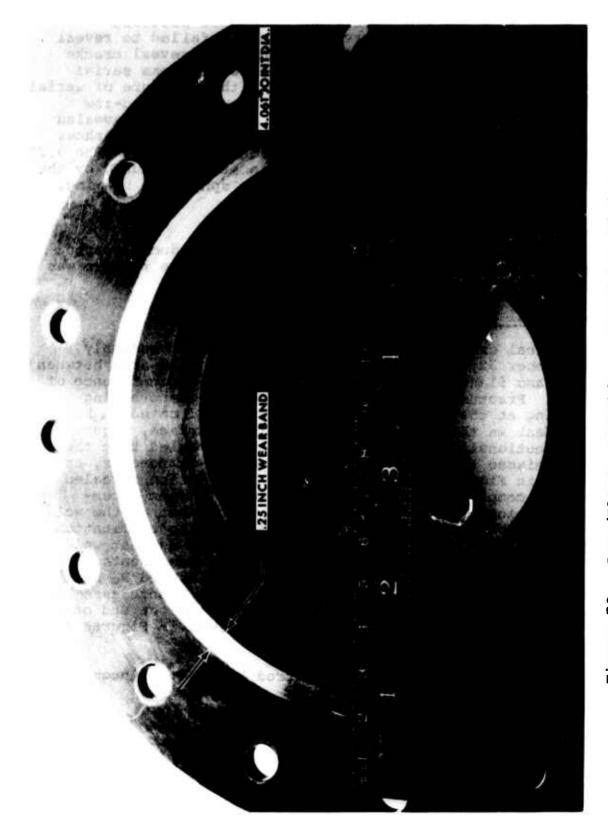


Figure 78. Gear/Flange Assembly - Second-Row Pinion.



Figure 79. Fatigue Crack Origin - Second-Row Pinion.

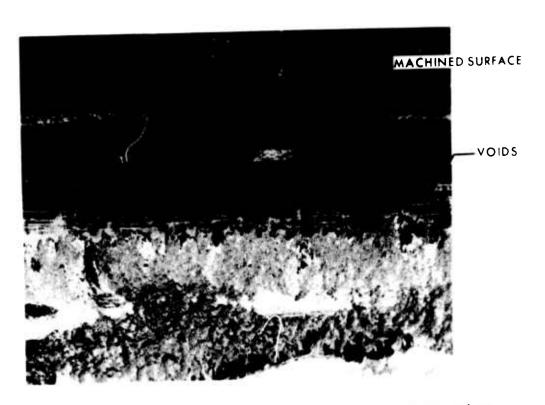


Figure 80. Machined Diameter - Fractured Section - Second-Row Pinion.

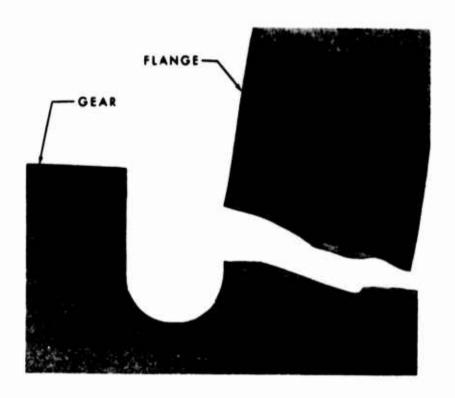


Figure 81. Gear/Flange Separation - Second-Row Pinion.

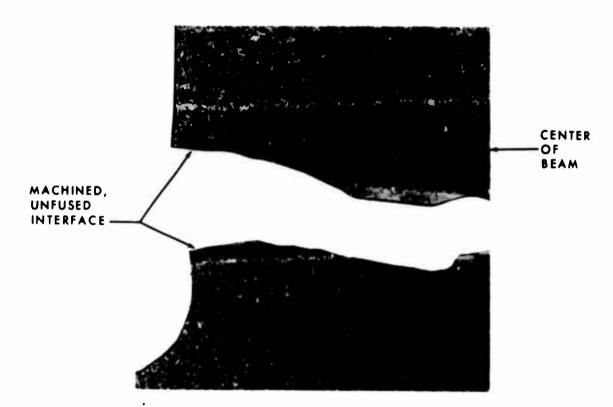


Figure 82. Electron Beam Weld - Gear/Flange, Second-Row Pinion.

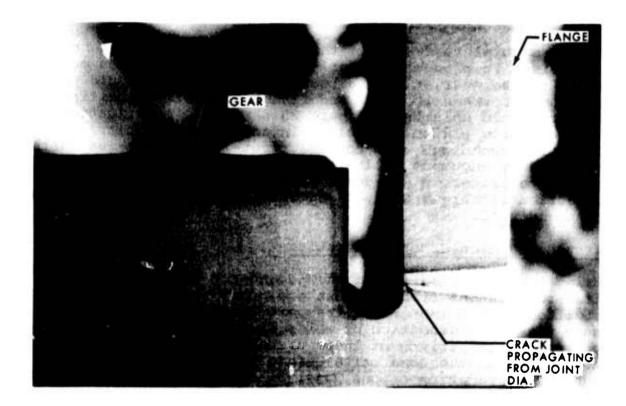


Figure 83. Crack - Gear/Flange Assembly, Second-Row Pinion.

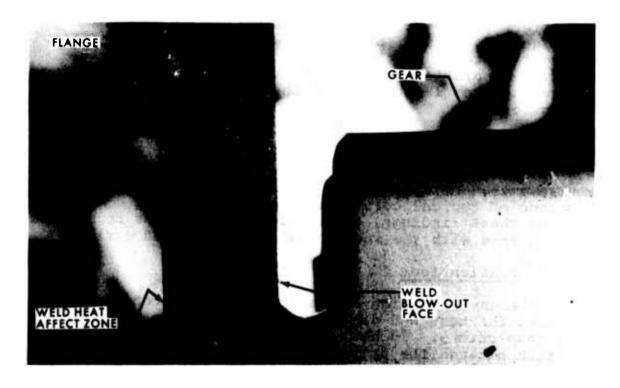


Figure 84. Crack Propagation - Gear/Flange Assembly, Second-Row Pinion.

Modification, Second-Row Pinion

To ensure complete fusion of this joint, the welding schedule was revised to produce a wider joint. This required a modification to the gear so that a heavier blast shield could be positioned between the gear and flange to protect the finish gear from weld splatter. Figure 85 shows the modification to the second-row pinion assembly. In addition, the ultrasonic inspection technique used for the first-row pinions was further developed to encompass all electron beam welded joints, and an acceptance criterion was developed. The resulting ultrasonic inspection technique and weld acceptance criterion are presented in Appendix II.

First-Row Pinion Crack Propagation

During the investigation of the second-row pinion fracture, first-row pinions from the test and dummy gearboxes were submitted to a pulse-echo ultrasonic inspection to determine if there was any degradation of welds during the 9.5 hours of testing. A comparison of these ultrasonic recordings with those taken on the same parts before testing was initiated revealed degradation of one small diameter roller of first-row pinion serial number 28, as shown in Figures 86 and 87. atory sectioning to remove the roller to determine the cause for the change in the ultrasonic output revealed a 1.5-inch crack in the area of the weld. The crack extended the width of the roller. Figure 88 shows the crack at a section through the roller/gear interface, and Figure 89 shows the crack extending to a section taken at the shoulder of the small diameter Separation of the crack revealed fatique cracking roller. propagating from large voids in the weld, as shown in Figure 90 and Figure 91.

These are the voids which had been recorded by the ultrasonic inspection. Hardnesses of the gear, component, and weld zone were $R_{\rm C}$ 38, 40 and 36, respectively, which conforms to core requirements. Metallographic examination revealed an as-cast weld zone of typical core structure in the mating components. Based on these findings, the first-row pinion was redesigned in accordance with the recommendations specified earlier.

Gearbox Modifications

During the investigation of the roller gear second-row pinion fracture, the test and dummy transmissions were subjected to split inspections. In both gearboxes fatigue fretting was occurring between the splines of the outer shaft and quill shaft. To arrest this condition, an oil dam was installed in the outer shaft, which forced oil to flow out through the spline instead of over the top of the outer shaft.

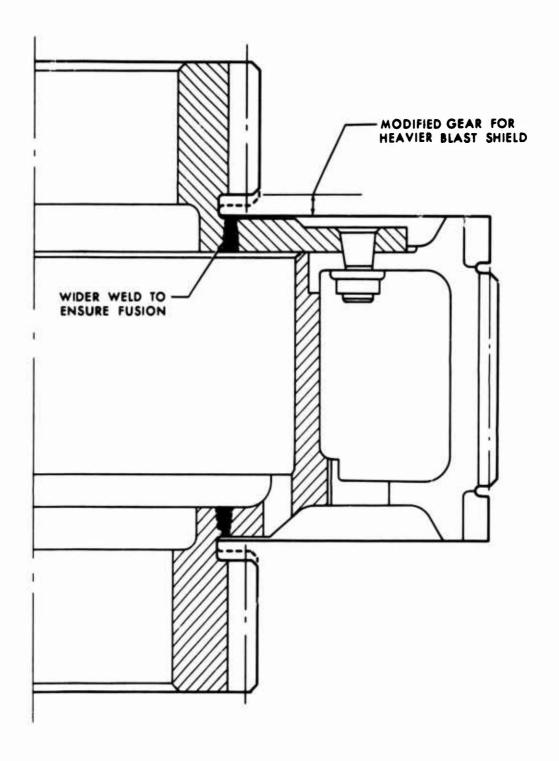


Figure 85. Second-Row Pinion Modification.



Figure 86. Ultrasonic Recording - First-Row Pinion Roller Weld, Small Diameter Roller.



Figure 87. Weld Degeneration - Ultrasonic Recording,
First-Row Pinion Roller Weld, Small
Diameter Roller.

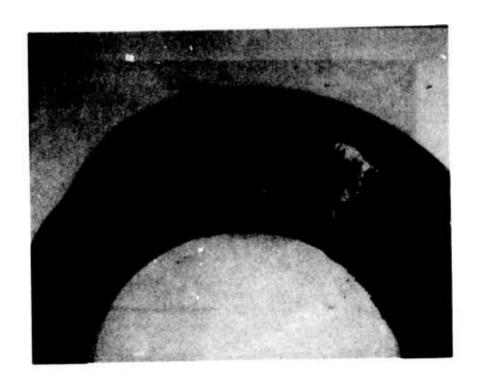


Figure 88. Crack - Roller/Gear Interface, First-Row Pinion.



Figure 89. Crack - Roller Shoulder Section, First-Row Pinion.



Figure 90. Crack Interface - First-Row Pinion Roller.



Figure 91. Void, Electron Beam Weld - First-Row Pinion.

Inspection of the test gearbox freewheel units revealed 0.060-inch-wide wear paths on both ends of the rollers, Figure 92. These marks were caused by "chucking" of the rollers in the cage slots due to insufficient load on the cage during free-wheeling operations. Stronger springs were installed which increased the load on the cage in the freewheel position from 4 pounds to 6 pounds.

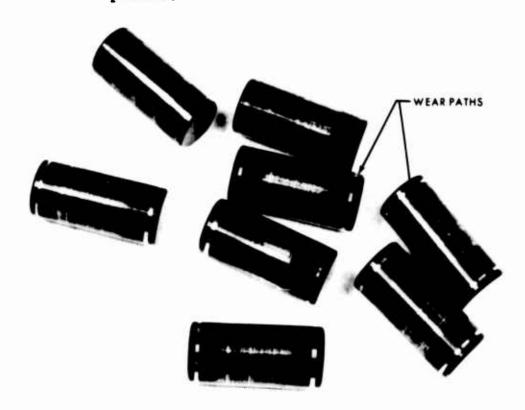


Figure 92. Rollers - Input Freewheel Unit.

Ultrasonic Inspection, Second-Row Pinion

Ultrasonic inspection of new second-row pinions revealed the presence of an unwelded section in the lower roller weld of pinion serial number 56. The ultrasonic recording shows an unfused arc 2.0 inches long. Removal of roller material from both sides of the unwelded area and machining 0.050 inch off the face of the roller allowed the unwelded portion to fall off. A cosmetic weld which had penetrated 0.045 inch had prevented detection of the subsurface crack by magnetic particle inspection. It was concluded that during welding, the electron beam was withdrawn prior to completion of the 360-degree weld. A cosmetic weld then covered all trace of the previous weld. This gear assembly was replaced by a second-row pinion assembly which had been manufactured as a spare.

Magnetic Particle Inspection, Second-Row Pinion

Prior to installation of these gears in the roller gear transmission, they were subjected to magnetic particle inspection which revealed longitudinal cracking on the inside diameter of the bearing bore, Figure 93. Examination of other second-row pinions which were in the process of rework revealed similarly located indications of cracking.

Metaliurgical examination revealed that the cracks were multiple in nature, as shown in Figure 94, and typical of cracks associated with grinding stresses. Several assemblies evidenced a series of deeper circumferential cracks extending for approximately 1.5 inches as shown in Figure 95. Examination of cross sectional metallurgical specimens revealed the longitudinal cracks to be between 0.0007 - 0.001 inch deep. The circumferential cracks measured approximately 0.025 -0.030 inch deep. All of the cracking was confined to a band 0.44 inch wide, which coincided with the weld zone which is located below this area, Figure 96. There was no cracking evident on the remaining surface area. Hardness of this surface measured uniformly Rc 56 across the width to within 0.25 inch of the edge where a hardness loss to Rc 50 was evident. The time span between the completion of manufacture, when magnetic particle inspection had last been performed, and detection of the cracking was approximately six months. It was concluded that cracking of these second-row gear assemblies was caused by residual stresses induced during manufacture, probably during the finish grinding operation.

Since the indications occurred in an area of redundant load support structure, removal of the cracked metal by machining would not be detrimental to the life or function of the part. On this basis the magnaglow indications were removed by machining 0.040 inch off the bore diameter for a depth of 0.50 inch. An extended stress relieving cycle, in which the parts were subjected to a 23-hour bake at 325° F, was conducted to alleviate any residual stresses that could have formed during the rework.

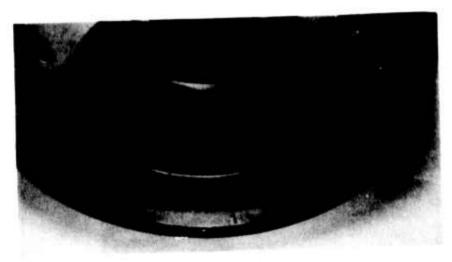


Figure 93. Bearing Bore Cracks - Second-Row Pinion.



Figure 94. Longitudinal Cracks - Bearing Bore.

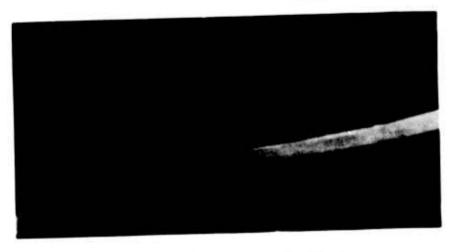


Figure 95. Circumferential Cracks - Bearing Bore.

Figure 96. Crack Location - Second-Row Pinion.

Testing was continued with the redesigned first-row pinion gears installed in both gearboxes. A list of the replacement roller gear parts is presented in Tables XI and XII. Their locations in the test and dummy roller gear units are shown in Figures 97 and 98. The test was stopped after 20.9 hours of testing (56:56 total test time) when the oil pressure in the dummy gearbox manifold dropped below an acceptable level. At this time all chip detectors were examined. Metallic particles were found in the dummy transmission forward sump chip detector, but were insufficient in number to trigger the detector. After investigation of the steel particles, it was decided to run at full speed low power to determine which pump was not delivering and to see if more chips would be generated. It was found that neither pump could generate enough output to take over from the test stand auxiliary pump which supplies lubrication oil until 40 psi is developed by the gearbox pumps, and the test was stopped after 2 minutes. Removal of the detectors showed an accumulation of more metallic particles in the sump chip detector. Consequently, the test was terminated and the gearboxes were removed from the test facility.

Visual Inspection

A review of the assembly procedure and inspection of the dummy roller gear unit, Figure 99, revealed that all timing marks on the gears were correctly oriented. Inspection of the partially disassembled unit, Figure 100, showed that first-row pinions serial numbers 14 and 15 had fractured teeth on the second-row mesh. Examination of each part showed the rollers to be in excellent condition, while gear patterns on the first-row pinions indicated load was distributed evenly across the face of the teeth.

	TABLE XI. TEST #3 - RO TEST GEARBOX	LLER	GEAR UNIT COMPONENTS -	
Part Number	Nomenclature	Serial Number	Status	Test Hours:Minutes
RG351-11183-041	Sun Gear	60	New	0
51-11182-05	-Row	02	weld	0
51-11182-05	-Row	90	weld	0 0
51-11182-05	-Row	60	weld	-
51-11182-05	-Row	o F	Weld	
KG351-11182-052	lst-kow Finion lst-Row Pinion	12	New weld config.	- C
51-11182-05	-Row	16	weld	0
51-11181-05	2nd-Row Pinion	01	Used in dummy box	26:30
51-11181-05	-Row	10	ij	26:30
RG351-11181-052		16	in	26:30
51-11181-05	-Row	17	in dummy	26:30
51-11181-05	-ROW	19		26:30
51-11181-05	2nd-Row Pinion	23	Used in dummy box	26:30
RG351-11181-041	2nd-Row Pinion	07	Replacement for s/n 15	0
EG351-11184-041	Ring Gear	02	Used in Tests #1 & #1	2 36:0
231	Spherical Bearing	90	New	0
22313 VAG	rical	117	New	0
2313	rical	N13	New	0
2313	rical	N21	New	0
231	rical	1132	New	0
2313	rical	1139	New	0
231	Spherical Bearing	N40	New	0

E	TABLE XII. TEST #3 - ROL DUMMY GEARBOX	ROLLER GEAR UNIT BOX	R UNIT COMPONENTS -	
Part Number	Nomenclature	Serial	Status	Test Hours:Minutes
RG351-11183-041	Sun Gear	03	Used in Test #2	9:30
351-11182-05	st-Row	03	weld	00
-11182- -11182-	<pre>lst-Kow Pinion lst-Row Pinion</pre>	0 4 5	New weld config.	00
51-11182-05	st-Row P	80	weld	0
51-11182-05	st-Row	13	weld	0 0
82-05	1st-Row Finion 1st-Row Pinion	15	New weld config.	00
	í	ć	E	
-TTT8T-02	2nd-Row Finion	5 0		26:30
51 - 11181	ROW	0 0	ij	26:30
351-11181-05	-Row	90	in Test	26:30
351-11181-05	-Row	60	in Test #	26:30
1-11181-05	-Row P	20	in Test #	26:30
-11181-05	2nd-Row Pinion	22	Replacement for s/n 12	0
RG351-11184-041	Ring Gear	04	Used in Tests #1 & #2	36:00
22313 VAG	Spherical Bearing	N4	New	0
	rical	N12	New	0
2313		N17	New	0
2313		N 20	New	c
2313		N29	New	0
2313	Bear	N35	New	0
231	Spherical Bearing	N36	New	0

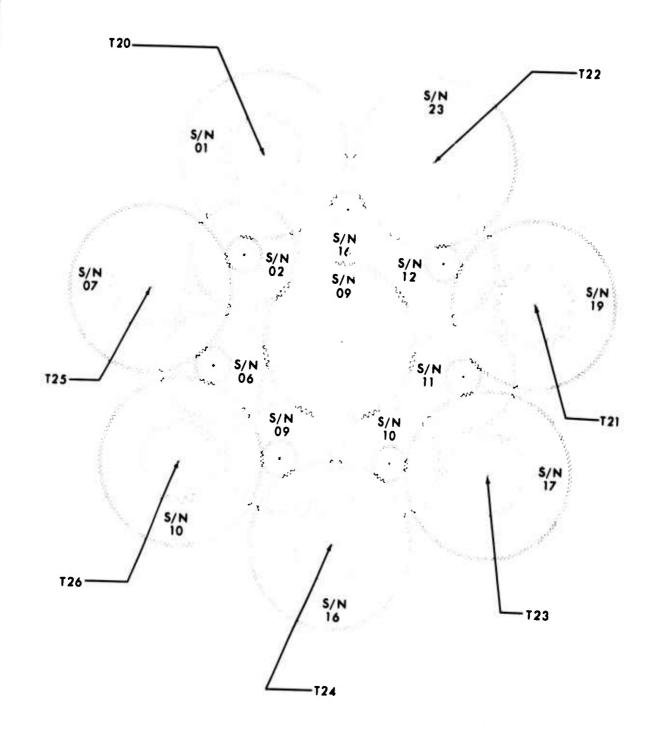


Figure 97. Component Location - Test Roller Gear Unit,

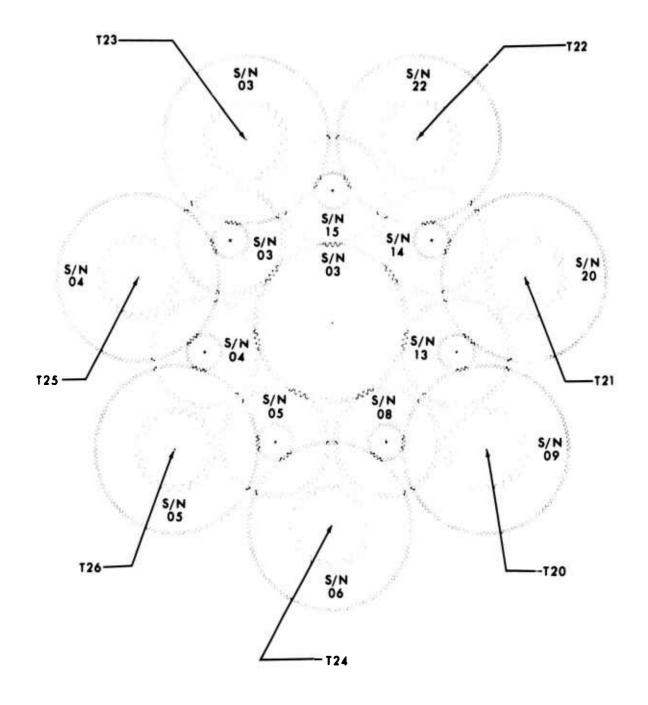


Figure 98. Component Location - Dummy Roller Gear Unit.

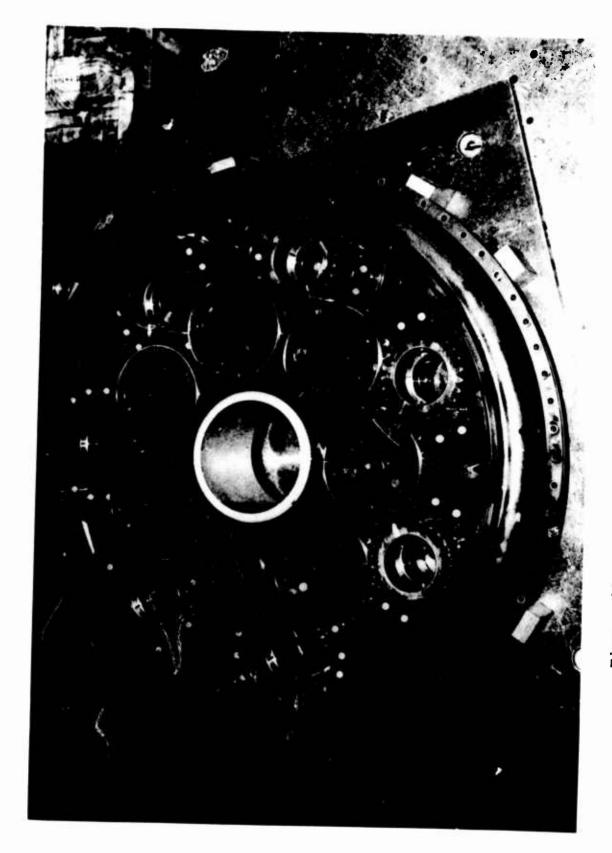


Figure 99. Roller Gear Unit - Dummy Gearbox.

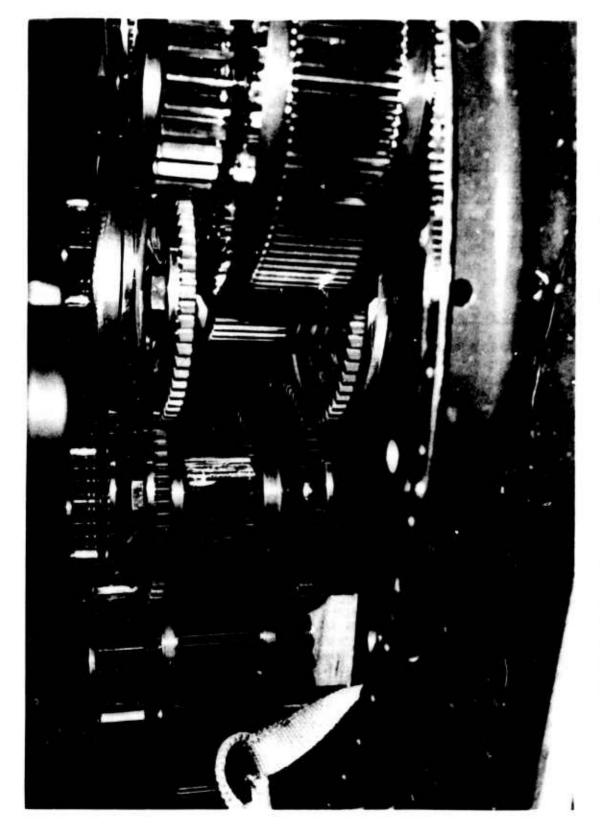


Figure 100. First-Row Pinion Damage - Roller Gear Unit.

Metallurgical Examination

Inspection of the fractured first-row pinion teeth revealed that the cracking had originated near the roots of the teeth where the heat affected zone adjacent to the weld had extended into the gear root, Figure 101. A plot of hardness readings, taken in the vicinity of the fracture origin, is shown in Figure 102.

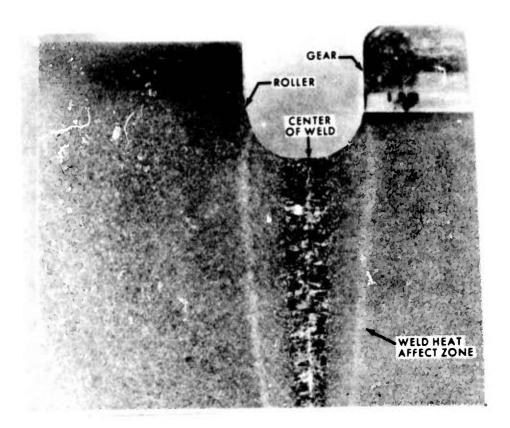
Metallurgical analysis of the heat affected zone showed that transformation changes occurring during the welding process had resulted in an area of residual tensile stress. This created a transition interface where an area of compressive stress (carburized layer) bordered an area of tensile stress. This transition in the material, from a state of tension to a state of compression, led to a stress concentration at the edge of the heat affected zone which, in turn, led to the failure of the gear teeth.

Fracture Analysis

An analysis of tooth bending stress was performed to determine whether or not the allowable stress could have been exceeded at the point of failure in the heat affected zone. This analysis showed that while the allowable stress in this area had been decreased from 55,000 psi to 48,000 psi by heat from the weld, existing tooth bending stresses in the area were still below the allowable stress for a 3-sigma incidence of tooth failure. Torsional stress in this area was calculated to be 4000 psi, a value judged low enough to have had a negligible effect on the teeth. Bending stress due to overall loading of the gear was calculated to be 3,110 psi, also of negligible effect when resolved into the plane of tooth bending stress.

Modification of First-Row Pinion

Since the heat affected area is inherent in the welding process, design modifications of the first-row pinions were selected to reduce bending stresses in the heat affected area. To accomplish this, 0.032 inch was removed from the edge of the teeth, Figure 103. Secondly, the teeth were crowned to 0.0002 - 0.0005 inch across the face width. This was done to concentrate stresses in the center of the tooth, thus reducing stress at the ends of the teeth. In addition, the heat affected zone was shot-peened to put the surface in compression.



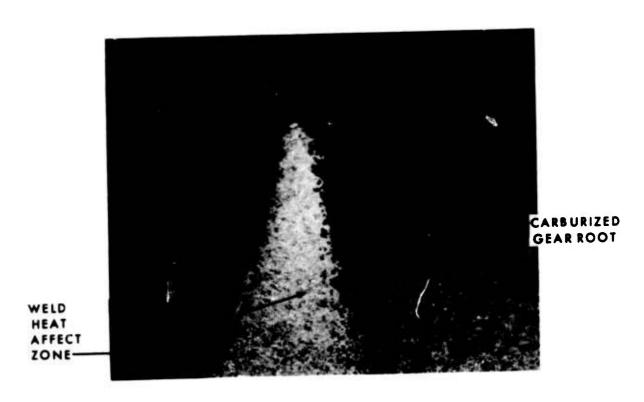
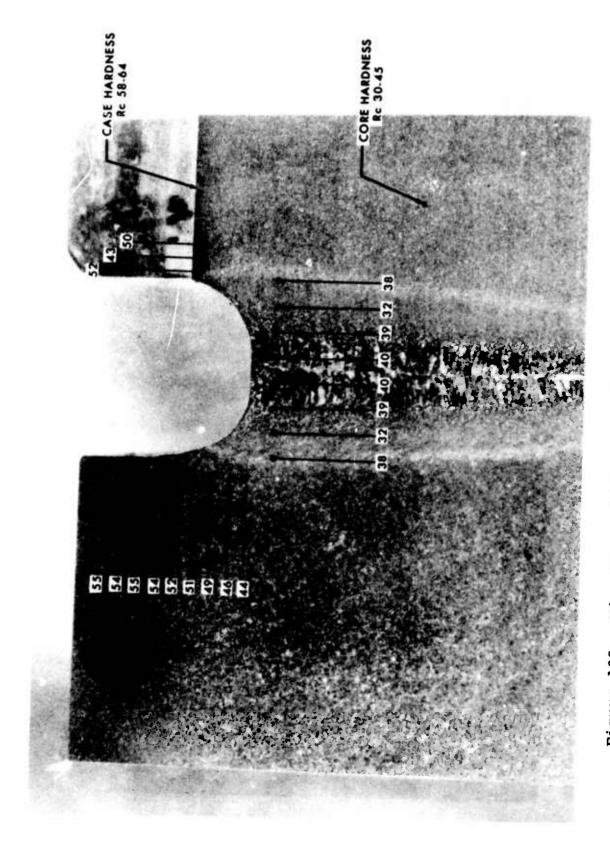


Figure 101. Butt Weld - First-Row Pinion.

west of the state of the



Microhardness Survey - Butt Weld, First-Row Pinion. Figure 102.

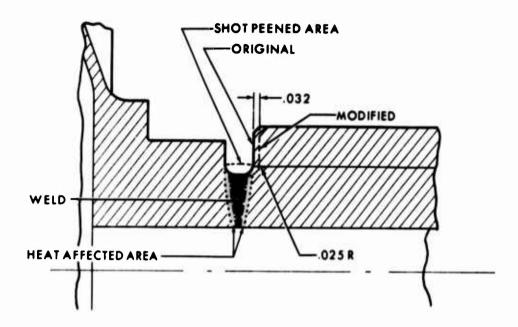


Figure 103. First-Row Pinion Modification.

Oil Pump Malfunction

Further inspection showed that the loss of lubrication was due to the fracture of the quill shaft driving the aft lubrication pump. This pump had seized when metal fragments from the fractured first-row pinion teeth entered the operating area of the vanes. The metallic particles were cold welded to the cam ring, thereby preventing rotation of the vanes, Figure 104, and sheared the quill shaft. It was discovered that the pump chip detector had been incorrectly installed, allowing the metallic fragments to enter the pump itself. On reassembly this problem was corrected.

With the implementation of these modifications, the initial testing was completed. Test time accumulated during initial test and the gear development test totaled 56:56.

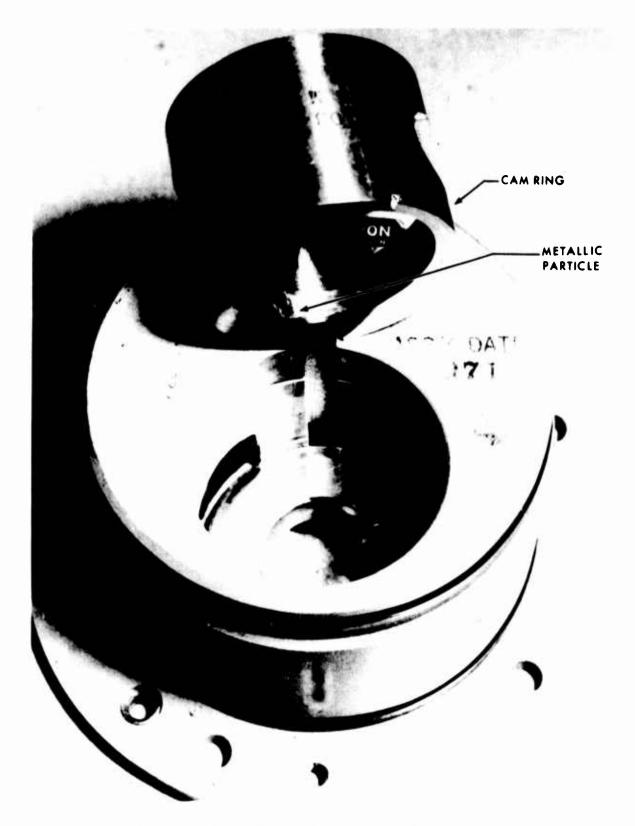


Figure 104. Disassembled Lubrication Pump - Roller Gear Transmission.

200-HOUR ENDURANCE TEST

The 200-hour endurance test was initiated upon the completion of modifications resulting from the earlier development testing. The components assembled into the test and dummy roller gear units, Tables XIII and XIV, contained first— and second—row pinions to the latest design configuration. These were located within the test and dummy roller gear units as shown in Figures 105 and 106. After 110 hours of trouble—free endurance test operation, during which the gearboxes were subjected to the test spectrum of Table XV, the test stand was shut down at 166:56 total test time for scheduled inspection of the gearboxes. Both gearboxes were removed from the test stand and partially disassembled. The roller gear units were removed and examination revealed no signs of distress. The gearboxes were reassembled and the endurance test was continued.

After an additional 40 hours of testing as per Table XVI, testing was stopped at 206:56 total test time for a problem in the tail takeoff adaptor gearbox of the dummy transmission. Inspection of this gearbox revealed a severely spalled idler shaft bearing, Figure 107. The bearing was replaced after a check showed the bearing was receiving adequate lubrication. The rest of the 200-hour endurance test, in accordance with the spectrum of Table XVII, was completed without incident.

Included as part of the 200-hour endurance test was a survey of the post loads of the second-row pinions in the test gearbox. Strain gages were installed in the pinion posts as shown in Figure 25, and the signals from these fed into an oscillograph. The results of the survey are shown in the graph of Figure 108 which plots post tangential load versus transmitted power. The tangential loads closely agreed with the loads obtained through analysis. While accurate radial load readings were difficult to obtain because of interference between the strain gages, the measurements indicated them to be approximately 5 percent of the tangential loads. Load distribution among the seven posts was excellent, with a maximum deviation from the mean of 5 percent.

Upon completion of the 200-hour endurance test at 256:56 total test time, both gearboxes were disassembled for detailed inspection. This encompassed visual, magnaglow, and ultrasonic inspection of welded components. The results of these inspections are presented in Tables XVIII and XIX for the test and dummy gearboxes, respectively.

Part Number	TABLE XIII.	200-HOUR ENDURANCE TEST GEARBOX	TEST - R	ROLLER GEAR UNIT COMPONENTS	NENTS -
51-11183-061 Sun Gear 09 Used in Test #3 20:55 51-11182-062 Ist-Row Pinion 35 New 0 51-11182-062 Ist-Row Pinion 35 New 0 51-11182-062 Ist-Row Pinion 42 New 0 51-11182-062 Ist-Row Pinion 43 New 0 51-11182-062 Ist-Row Pinion 43 New 0 51-11182-062 Ist-Row Pinion 49 New 0 51-11181-062 Ist-Row Pinion 49 New 0 51-11181-062 Ist-Row Pinion 48 New 0 51-11181-062 Ist-Row Pinion 49 New 0 51-11181-062 Ist-Row Pinion 49 New 0 51-11181-062 Ist-Row Pinion 57 New 0 51-11181-062 Ist-Row Pinion 58 New 0 51-11181-062 Ist-Row Pinion 100 Ist-Row	art	Nomenclature	Serial	Status	Test Hours:Minutes
St-Row Pinion 33 New New New St-11182-062 St-Row Pinion 35 New New New St-11182-062 St-Row Pinion 39 New N	51-11183-04		60	in Test #	ואו
State	351-11182-06	t-Row	33	New	0
State	351-11182-06	-Row	35	New	0
St-11182-062	51-11132-06	-Row	39	New	0
- 82-062 st-Row Pinion	51-11182-06	-Row	42	ilew	0
- 82-062	51-11182-06	-Row P		New	0
-	51-11182-06	-Row P	48	New	0
- 18 -062	351-11182-06	-Row P	49	New	0
	1-11181-06	-Row	29	New	0
51-11181-062 2nd-Row Pinion 48 New 0 51-11181-062 2nd-Row Pinion 53 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 Spherical Bearing N12 Used in Test #3 20:55 13 VAG Spherical Bearing N20 Used in Test #3 20:55 13 VAG Spherical Bearing N29 Used in Test #3 20:55 13 VAG Spherical Bearing N36 Used in Test #3 20:55 13 VAG Spherical Bearing	1-11181-06	-Row	38	New	0
51-11181-062 2nd-Row Pinion 49 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 Ring Gear 02 Used in Test #3 56:55 13 VAG Spherical Bearing N12 Used in Test #3 20:55 13 VAG Spherical Bearing N20 Used in Test #3 20:55 13 VAG Spherical Bearing N35 Used in Test #3 20:55 13 VAG Spherical Bearing N36 Used in Test #3 20:55 13 VAG Spherical Bearing N36 Used in Test #3 20:55 13 VAG Spherical Bearing N36 Used in Test #3	51-11181-06	-Row P	48	New	0
51-11181-062 2nd-Row Pinion 53 New 0 51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 Ring Gear 02 Used in Tests #1,2,3 56:5- 13 VAG Spherical Bearing N12 N2 Used in Test #3 20:5- 13 VAG Spherical Bearing N20 Used in Test #3 20:5- 13 VAG Spherical Bearing N35 Used in Test #3 20:5- 13 VAG Spherical Bearing N36 Used in Test #3 20:5- 13 VAG Spherical Bearing N36 Used in Test #3 20:5- 13 VAG Spherical Bearing N36 Used in Test #3 20:5- 13 VAG Spherical Bearing N36 Used in Test #3 20:5-	51-11181-06	-ROW P	49	New	0
51-11181-062 2nd-Row Pinion 57 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11181-062 2nd-Row Pinion 58 New 0 51-11184-041 Ring Gear 02 Used in Test #3 20:5 13 VAG Spherical Bearing N12 Used in Test #3 20:5 13 VAG Spherical Bearing N20 Used in Test #3 20:5 13 VAG Spherical Bearing N20 Used in Test #3 20:5 13 VAG Spherical Bearing N35 Used in Test #3 20:5 13 VAG Spherical Bearing N35 Used in Test #3 20:5 13 VAG Spherical Bearing N36 Used in Test #3 20:5 13 VAG Spherical Bearing N36 Used in Test #3 20:5 13 VAG Spherical Bearing N36 Used in Test #3 20:5 13 VAG Used in Test #3 20:5	51-11181-06	-Row P	53	New	0
-11181-062 2nd-Row Pinion 58 New 0 -11184-041 Ring Gear 02 Used in Tests #1,2,3 56:55 VAG Spherical Bearing N12 Used in Test #3 20:55 VAG Spherical Bearing N17 Used in Test #3 20:55 VAG Spherical Bearing N20 Used in Test #3 20:55 VAG Spherical Bearing N20 Used in Test #3 20:55 VAG Spherical Bearing N30 Used in Test #3 20:55 VAG Spherical Bearing N35 Used in Test #3 20:55 VAG Spherical Bearing N36 Used in Test #3 20:55	51-11181-06	-Row P	57	New	0
VAG Spherical Bearing N12 Used in Tests #1,2,3 56:55 VAG Spherical Bearing N12 Used in Test #3 20:55 VAG Spherical Bearing N17 Used in Test #3 20:55 VAG Spherical Bearing N20 Used in Test #3 20:55 VAG Spherical Bearing N20 Used in Test #3 20:55 VAG Spherical Bearing N35 Used in Test #3 20:55 VAG Spherical Bearing N36 Used in Test #3 20:55 VAG Spherical Bearing N36 Used in Test #3 20:55	351-11181-06	-Row P	28	New	0
2313 VAG Spherical Bearing N4 Used in Test #3 20:552313 VAG Spherical Bearing N12 Used in Test #3 20:552313 VAG Spherical Bearing N20 Used in Test #3 20:552313 VAG Spherical Bearing N29 Used in Test #3 20:52313 VAG Spherical Bearing N35 Used in Test #3 20:52313 VAG Spherical Bearing N36 Used in Test #3 20:52313 VAG Spherical Bearing N36 Used in Test #3 20:52313 VAG Spherical Bearing N36 Used in Test #3 20:552313 VAG Spherical Bearing N36 Used In Test #3 20:552313 VAG Spherical Bearing N36 Used In Test #3 20:552313 VAG Spherical Bearing N36 Used In Test #3 20:552313 VAG Spherical Bearing N36 Used In Test #3 20:552313 VAG Spherical Bearing N36 Used In Test #3 20:552313 VAG Spherical Bear	-11184-04		02	in Tests #1	6:5
2313 VAG Spherical Bearing N12 Used in Test #3 20:5 2313 VAG Spherical Bearing N20 Used in Test #3 20:5 2313 VAG Spherical Bearing N29 Used in Test #3 20:5 2313 VAG Spherical Bearing N35 Used in Test #3 20:5 2313 VAG Spherical Bearing N35 Used in Test #3 20:5 2313 VAG Spherical Bearing N36 Used in Test #3 20:5	2313		N 4	in Test #	LO
2313 VAG Spherical Bearing N17 Used in Test #3 20:5-2313 VAG Spherical Bearing N20 Used in Test #3 20:5-2313 VAG Spherical Bearing N35 Used in Test #3 20:5-2313 VAG Spherical Bearing N35 Used in Test #3 20:5-2313 VAG Spherical Bearing N36 Used in Test #3 20:5-2313 VAG	2313		N12	in Test #	S
2313 VAG Spherical Bearing N20 Used in Test #3 20:52313 VAG Spherical Bearing N35 Used in Test #3 20:52313 VAG Spherical Bearing N35 Used in Test #3 20:52313 VAG Spherical Bearing N36 Used in Test #3 20:52313 VAG	2313		N17	in Test #	S
2313 VAG Spherical Bearing N29 Used in Test #3 20:52313 VAG Spherical Bearing N35 Used in Test #3 20:52313 VAG Spherical Bearing N36 Used in Test #3 20:5	2313		N20	in Test #	Ď
2313 VAG Spherical Bearing N35 Used in Test #3 20:5 2313 VAG Spherical Bearing N36 Used in Test #3 20:5	2313		N29	in Test #	S
2313 VAG Spherical Bearing N36 Used in Test #3 20:5	2313		N35	in Test #	S
	2313	rical	N36	in Test #	'n

TABLE XIV.	200-HOUR ENDURANCE DUMMY GEARBOX	TEST - RO	ROLLER GEAR UNIT	UNIT COMPONENTS	ENTS -
Part Number	Nomenclature	Serial	St	Status	Test Hours:Minutes
RG351-11183-041	Sun Gear	03	Used in T	Tests #2, 3	30:24
1-11182	1st-Row Pinion	36	New	Ą	0
S	1st-Row Pinion	37	New	3	0
51-11182	-Row	38	New	3	0
51-11182	1st-Row Pinion	41	New	3	0
51-11182	-ROW P	44	New	3:	0
351-11182	-ROW P	45	New	A:	0
RG351-11182-062	1st-Row Pinion	46	New	Ŋ.	0
RG351-11181-062	2nd-Row Pinion	01	Used in I	Tests #1. 3	47:24
1-11181	-Row	07		Test #3	20:54
1-11181	-Row	10	in	s #1,	7:
1-11181	-Row	16	in	Tests #1, 3	47:24
351-1118	-Row	17		Tests #1, 3	47:24
1-11181	-Row P	19	in	#1,	47:24
RG351-11181-062	2nd-Row Pinion	23	Used in T	ests #1,	47:24
RG351-11184-041	Ring Gear	04	Used in T	Tests #1,2,3	56:54
22313 VAG	rical	9N		Test #3	20:54
m	rical	N7		Test #3	20:54
m	rical	N13		Test #3	
m	rical	N21		*	••
m	rical	N32	in	Test #3	Š
m	rical	N39	in	**	Š
22313 VAG	rical	N40	Used in I	Test #3	20:54

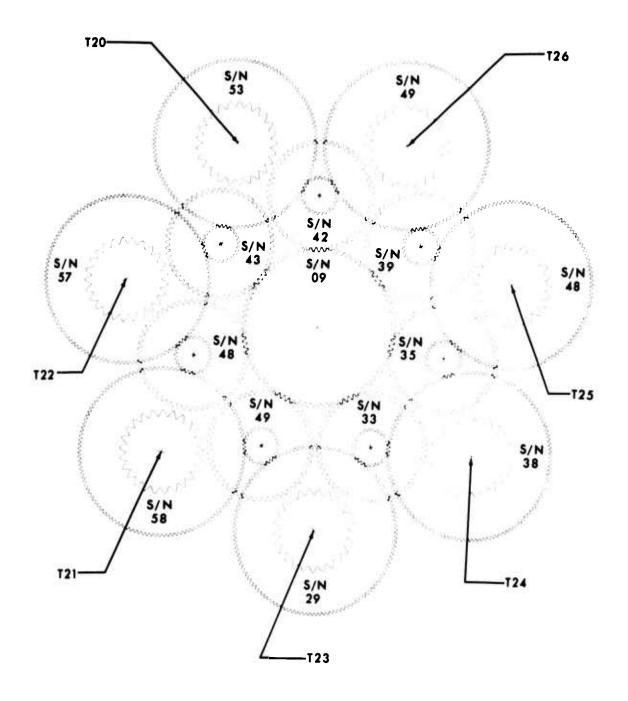


Figure 105. Component Location - Test Roller Gear Unit.

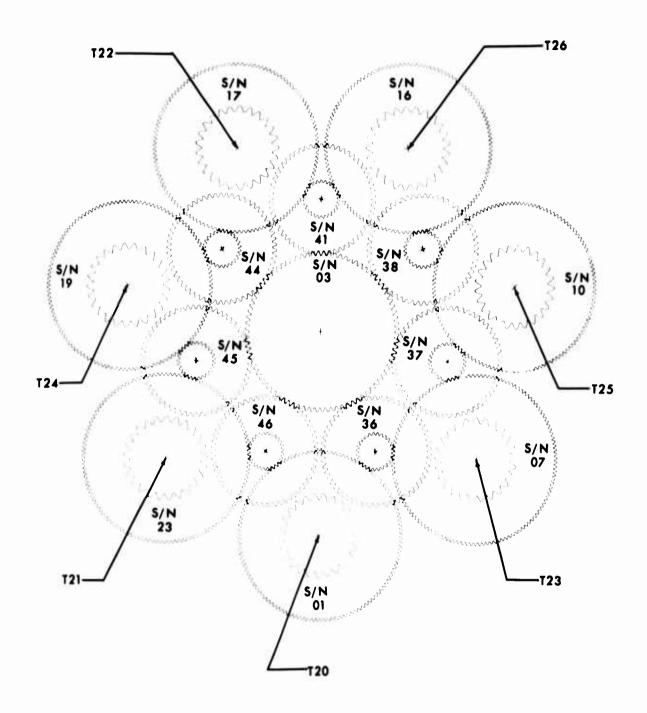


Figure 106. Component Location - Dummy Roller Gear Unit.

TABLE XV.	ENDURANCE TEST - 110-HOUR	SPECTRUM
Time (hr:min)	Total Input Power (hp)	Tail Power (hp)
15:00	1100	250
50:00	1950	250
25:00	2400	250
10:00	2700	250
6:30	3000	425
1:30	1950	425
1:30	3560	425
:30	3700	425

TABLE XVI.	ENDURANCE	TEST - 40-HOUR	SPECTRUM
Time (hr:min)	Total	Input Power (hp)	Tail Power (hp)
4:00		1100	250
10:15		1950	250
4:45		1950	425
4:00		2400	250
2:30		2700	250
11:45		3000	425
1:45		3560	425
1:00		3700	425

TABLE XVII.	ENDURANCE TEST - 50-HOUR	SPECTRUM
Time (hr:min)	Total Input Power (hp)	Tail Power (hp)
0:45	400	40
3:30	1100	250
21:30	1950	250
8:30	2400	250
4:30	2700	250
7 45	3000	425
2:45	3560	425
0:45	3700	425



Figure 107. Spalled Hall Bearing - Adaptor Gearbox.

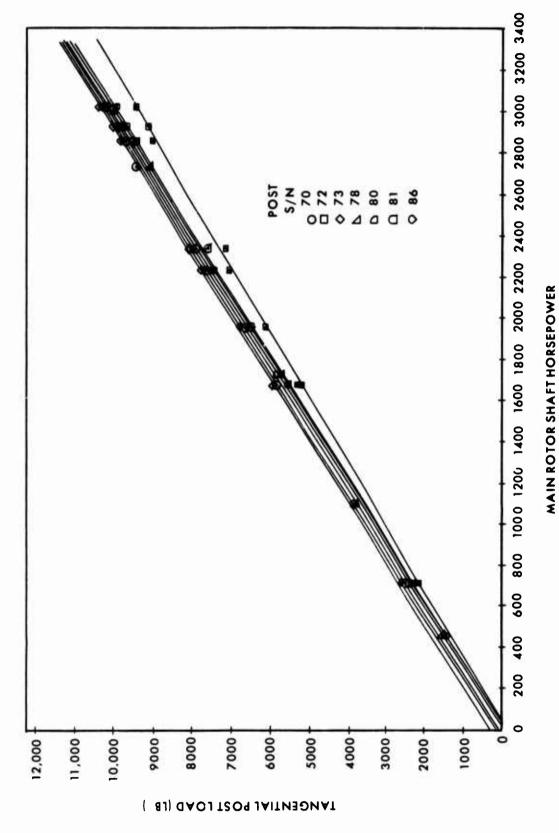


Figure 108. Tangential Post Load Versus Main Rotor Shaft Horsepower.

TABLE XVIII. 200-HOUR INSPECTION, TEST GEARS MAIN TRANSMISSION

				MAIN IRANSMISSION	
PART NUMBER	NOMENCLATURE	SER. NO.	TOTAL TEST TIME	VISUAL INSPECTION	Magnagl Inspe
RG351-11183-041	Sun Gear	09	220.9	Rollers excellent (Parco finish is on rollers and shoulders). Gear teeth excellent. Internal spline shows slight fretting.	No indi
RG351-11182-062	lst-Row Pinion	33	200.0	Gear teeth excellent. Lower inner roller exhibits surface flaking 1/8" from edge.	No indi
RG351-11182-062	lst-Row Pinion	35	200.0	Rollers and gear teeth excellent.	No indi
RG351-11182-062	lst-Row Pinion	39	200.0	Rollers and gear teeth excellent.	No indi
RG351-11182-062	lst-Row Pinion	42	200.0	Rollers and gear teeth excellent.	No indi
RG351-11182-062	lst-Row Pinion	43	200.0	Rollers and gear teeth excellent.	No indi
RG351-11182-062	lst-Row Pinion	48	200.0	Rollers and gear teeth excellent. Upper roller surface is not polished.	No indi
RG351-11182-062	1st-Row Pinion	49	200.0	Gear teeth excellent. Slight line on upper roller edge.	No indi
RG351-11181-062	2nd-Row Pinion	29	200.0	Gear teeth and rollers excellent. Parco finish on upper roller slightly removed.	around inside

XVIII. 200-HOUR INSPECTION, TEST GEARBOX MAIN TRANSMISSION

TAL ST ME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
0.9	Rollers excellent (Parco finish is on rollers and shoulders). Gear teeth excellent. Internal spline shows slight fretting.	No indications	-
).0	Gear teeth excellent. Lower inner roller exhibits surface flaking 1/8" from edge.	No indications	Spalling of roller surface .00015 deep, caused by insufficient crown blending on mating roller.
1.0	Rollers and gear teeth excellent.	No indications	t -
1.0	Rollers and gear teeth excellent.	No indications	-
• 0	Rollers and gear teeth excellent.	No indications	-
.0	Rollers and gear teeth excellent.	No indications	•
.0	Rollers and gear teeth excellent. Upper roller surface is not polished.	No indications	Indication of pure rolling.
.0	Gear teeth excellent. Slight line on upper roller edge.	No indications	Insufficient crown blending on mating roller.
.0	Gear teeth and rollers excellent. Parco finish on upper roller slightly removed.	around inside bearing	Crack originating from EB weld voids.

TABLE XVIII - Continued

<u> </u>						
	PART NUMBER	NOMENCLATURE		TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/Z INSPECTIO
	RG351-11181-062	2nd-Row Pinion	38	200.0	Rollers and gear teeth excellent.	Crack indication around inside be bore.
	RG351-11181-062	2nd-Row Pinion	48	200.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	Crack indication around inside be bore.
	RG351-11181-062	2nd-Row Pinion	49	200.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	Crack indications around inside bestore and on top
	RG351-11181-062	2nd-Row Pinion	53	200.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indication
1	RG351-11181-062	2nd-Row Pinion	57	200.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indication
	RG351-11181-062	2nd-Row Pinion	58	200.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indicatio
	RG351-11185-103	Hub	04	256.9	Internal spline in excellent condition.	No indicatio
	RG351-11185-041	Plate Ass'y	06	256.9	Excellent	No indicatio
	RG351-11176-041	Plate Ass'y	06	256.9	Light fretting about post interface.	No indicatio

TABLE XVIII - Continued

OTAL EST IME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
00.0	Rollers and gear teeth excellent.	Crack indication around inside bearing bore.	Crack originating from EB weld voids.
0.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	Crack indication around inside bearing bore.	Crack originating from EB weld voids.
)0.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	Crack indications around inside bearing bore and on top roller.	Crack originating from EB weld voids.
10.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indications	-
0.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indications	-
0.0	Rollers and gear teeth excellent. Slight fretting at flange interface holes.	No indications	, -
6.9	Internal spline in excellent condition.	No indications	-
6.9	Excellent	No indications	-
6.9	Light fretting about post interface.	No indications	-

TABLE XVIII - Continued

					TABLE XVIII - Continued		
	PART NUMBER	NOMENCLATURE	SER. NO.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZYG INSPECTION
	RG351-11187-101	Splined Plate	03	256.9	7 teeth located symmetrically exhibit full face loading.	No	indication
	RG351-11173-101	Nut	-	-	Excellent	No	indication
	RG351-11173-101	Nut	-	-	Excellent	No	indication
	RG351-11173-101	Nut	-	-	Excellent	ИО	indication
	RG351-11173-101	Nut	-	-	Excellent	No	indicamion
	RG351-11173-101	Nut	-	-	Excellent	No	indication
	RG351-11173-101	Nut	-	-	Excellent	No	indication
	RG351-11173-101	Nut	-	-	Excellent	No	indication
	RG351-11189-101	Oil Pump Gear	04	256.9	Gear pattern excellent.	No	indicatio
	RG351-11186-041	Plate Ass'y	06	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	70	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	72	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	73	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	78	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	80	256.9	Excellent	No	indicatio
:	RG351-11177-101	Post	81	256.9	Excellent	No	indicatio
	RG351-11177-101	Post	86	256.9	Excellent	No	indicatio

TABLE XVIII - Continued

TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
256.9	7 teeth located symmetrically exhibit full face loading.	No indications	Reaction torque deflections. No significant wear.
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
=	Excellent	No indications	-
256.9	Gear pattern excellent.	No indications	-
256.9	Excellent	No indications	-
256.9	Excellent	No indications	-
256.9	Excellent	No indications	-
26.9	Excellent	No indications	-
256.9	Excellent	No indications	-
256.9	Excellent	No indications	-
256.9	Excellent	No indications	-
256.9	Excellent	No indications	-

TABLE XVIII - Continued

· · · · · · · · · · · · · · · · · · ·					
PART NUMBER	NOMENCLATURE	SER. NO.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGI INSPECTION
RG351-11184-041	. Ring Gear	02	256.9	Gear teeth excellent	No indication:
22313 VAG	Spherical Brg.	N4	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N12	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N17	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N20	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N29	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N35	220.9	Excellent	No indications
22313 VAG	Spherical Brg.	N36	220.9	Excellent	No indications
RG351-11179-101	. Spacer	-	200.0	Face worn .002007	No indications
RG351-11179-101	. Sp acer	-	200.0	Face worn .002007	No indications
RG351-11179-101	. Spacer	-	200.0	Face worn .002007	No indications
RG351-11179-101	Spacer	-	200.0	Face worn .002007	No indications
RG351-11179-101	. Spacer	-	200.0	Face worn .002007	No indications

TABLE	XVIII	- Con	tinued

VISUAL INSPECTION	Magnaglow/zyglo inspection	COMMENTS
Gear teeth excellent	No indications	Excellent gear teeth patterns.
Excellent	No indications	-
Excellent	No indications	•
Excellent	No indications	•
Excellent	No indications	
Excellent	No indications	-
Excellent	No indications	- ,
Excellent	No indications	-
Face worn .002007	No indications	Wear due to working of 2nd row gear/flange assembly.
Face worn .002007	No indications	Wear due to working of 2nd row gear/flange assembly.
Face worn .002007	No indications	Wear due to working of 2nd row gear/flange assembly.
Face worn .002007	No indications	Wear due to working of 2nd row gear/flange assembly.
Face worn .002007	No indications	Wear due to working of 2nd row gear/flange assembly.
	Excellent Excellent Excellent Excellent Excellent Excellent Excellent Excellent Face worn .002007 Face worn .002007 Face worn .002007	Gear teeth excellent Excellent No indications Face worn .002007 No indications

TABLE XVIII - Continued

╘										
	PART N	NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME		Inspect	ION		enaglow, Inspect:
	RG351-111	179-101	Spacer	-	200.0	Face worn	.002 -	.007	No	indica
	RG351-111	179-101	Spacer	-	200.0	Face worn	.002 -	.007	No	indica
	RG351-111	L60 - 042	Main Rotor Shaft	-	-	Exc	cellent		No	indica ·
:	525519		Seal	-	-		-			-
	R1838-C-4	100	Roller Brg	-	-		-			-
	RG351-111	54-101	Spur Gear	06	-	Exc	cellent		No	indica
	CB63-4		Seal	-	-		-			-
	SB1357-2		Ball Brg.	-	-		-			•
	RG351-111	.94-101	Quill Shaft	03	1-	Fretting a	t both	ends	No	indica
	RG351-112	05-101	Quill Shaft	03	-	Fretting a external s			No	indica
	S6135-207	13-1	Nut	61	-	Exc	ellent		No	indica
	S6135-207	13-1	Nut	62		Exc	ellent		No	indica
	RG351-112	56-101	Gear	06	-	Slight pit teeth.	ting on	gear	No	indica

	TABLE	KVIII - Continued			
OTAL EST IME		INSPECTION		GNAGLOW/ZYGLO INSPECTION	COMMENTS
00.0	Face worn	.002007	No	indications	Wear due to working of 2nd row gear/flange assembly.
00.0	Face worn .	.002007	No	indications	Wear due to working of 2nd row gear/flange assembly.
-	Exce	ellent	No	indications	-
-		-,		-	-
-		-		-	-
-	Exce	ellent	No	indications	-
-		-		-	-
-		-		-	-
-	Fretting at	both ends	No	indications	More lubricant required
-	Fretting at external sp		No	indications	Lubrication needs adjusting.
-	Exce	llent	No	indications	-
_	Exce	llent	No	indications	-

No indications

Slight pitting on gear teeth.

TABLE XVIII - Continued

 				TABLE XVIII - Continued		
PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		Gnaglow/zy Inspection
RG351-11113-101	Input Bevel	06	256.9	Excellent	No	indicatio
MM212VM9-SMBR-A 1584	Stack Brgs	108	256.9	Excellent		-
SB2154-1	Roller Brg.	121	256.9	Slightly ratchety.		-
RG351-11117-102	Nut	-	-	Excellent	No	indicatio
RG351-11117-101	Nut	-	-	Excellent	No	indicatio
RG351-11113-101	Input Bevel	04	256.9	Slight score marks on teeth. Pattern excellent.	No	indicatio
MM212VM9-SMBR- A1584	Stack Brgs.	100	256. 9	Excellent		-
SB2154-1	Roller Brg.	131	256.9	Slightly ratchety.		-
RG351-11117-102	Nut	-	-	Excellent	No	indicatio
RG351-11117-101	Nut	-	-	Excellent	No	indicatio
RG351-11117-103	Nut	-	-	Excellent	No	indicatio
111-KS-400	Bearing	-	256.9	Excellent		-

TABLE	XVIII	- Continue	be

	TABLE XVIII - Continue	ed	
TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
256.9	Excellent	No indications	Dynamic gear teeth patterns excellent.
256.9	Excellent	-	-
256.9	Slightly ratchety.	-	Ultrasonically cleansed .
-	Excellent	No indications	-
-	Excellent	No indications	-
256.9	Slight score marks on teeth. Pattern excellent.	No indications	Dynamic gear teeth patterns excellent.
256.9	Excellent	-	-
256.9	Slightly ratchety.	-	Ultrasonically cleansed
-	Excellent	No indications	-
-	Excellent	No indications	-
. -	Excellent	No indications	-
256.9	Excellent	-	-

TABLE XVIII - Continued

				TABLE AVIII CONCINCE	
PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ INSPECTI
NAS 1493-14	Nut	-		Excellent	No indicat
RG351-11146-101	Quill Shaft	01	-	Int. spline shows slight fretting.	No indicat
RG351-11139-102	Bushing	•	-	Excellent	ı
1838-JD-400-B	Ball Brg.	E12	256.9	Excellent	-
RG351-11109-102	Nut	-	-	Excellent	No indicat
RG351-11136-101	Pin (2 pcs)	-	-	Excellent	-
RG351-11135-101	Cage	09	256.9	Slight wear at slot edges.	No indicat
RG351-11133-041	Cam	10	_	Non-uniform Parco removal on flats.	No indicat
RG351-11117-104	Nut	-	-	Excellent	No indica
SB2157-2	Roller Brg.	386B	-	Excellent	-
RG351-11131-101	Spur Shaft	14	256.9	Slight fretting about holes in mounting flange.	No indica
RG351-11132-101	Spur Gear	02	256.9	Slight fretting about mounting holes in flange.	No indica

	TABLE	XVIII	- Continued
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	TABLE XVIII - Continued		····	
OTAL EST IME	VISUAL INSPECTION		GNAGLOW/ZYGLO INSPECTION	COMMENTS
-	Excellent	No	indications	-
-	Int. spline shows slight fretting.	No	indications	Requires improved lubrication.
-	Excellent		-	-
6.9	Excellent		-	-
-	Excellent	No	indications	-
-	Excellent		-	-
6.9	Slight wear at slot edges.	No	indications	Normal wearing-in
-	Non-uniform Parco removal on flats.	No	indications	No surface indentations
•	Excellent	No	indications	-
	Excellent		-	-
; . 9	Slight fretting about holes in mounting flange.	No	indications	-
.9	Slight fretting about mounting holes in flange.	No	indications	Gear pattern excellent

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TABLT XVIII - Continued

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	PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZY INSPECTION
	RG351-11139-101	Bushing	•	-	Excellent		•
	X3762	Roller (14 pcs)	-	221.0	Excellent	No	indicatio
	RG351-11128-101	Bevel Gear	10	256.9	Excellent	110	indicatio
	RG351-11129-101	Bevel Shaft	01	256.9	Int. spline shows slight fretting.	НО	indicatio
	SB 1056-2	Duplex Ball Bearing	1842	-	Excellent	No	indicatio
	RG351-11134-101	Cam Housing	89	256.9	Slight fretting on ext. spline.	No	indication
	RG351-11143-101	Nut	-	-	Excellent	No	indication
	MR-1922-C-400	Roller Brg.	19	256.9	Excellent		-
	RG351-11126-041	Housing	006	-	Excellent		-
	RG351-11109-101	Nut	· -	-	Excellent	No	indication
	RG351-11117-103	Nut	-	-	Excellent	No	indication
	111-KS-400	Bearing	-	256.9	Excellent		-
1							

TABLE XVIII - Continued

上		Magnaglow/zyglo	
	VISUAL INSPECTION	INSPECTION	COMMENTS
	Excellent	-	-
, 0	Excellent	No indications	Excellent condition
, 9	Excellent	No indications	Excellent gear teeth patterns.
, 9	Int. spline shows slight fretting.	No indications	Requires improved lubrication.
	Excellent	No indications	-
, 9	Slight fretting on ext. spline.	No indications	Requires improved lubrication.
	Excellent	No indications	-
, 9	Excellent	-	-
	Excellent	-	<u>-</u>
	Excellent	No indications	-
	Excellent	No indications	-
, 9	Excellent	-7	-

TABLE XVIII - Continued

PART NUMBER	NOMENCLATURE	-	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZYG
NAS 1493-14	Nut	-	-	Excellent	Мо	indication
RG351-11146-101	Quill Shaft	05	256.9	Ext. spline excessive fretting. Int. spline has slight fretting.	No	indication
RG351-11139-101	Bushing	-	-	Excellent		-
1838-JD-400-B	Ball Brg.	E12	256.9	Outer race edge has pit marks.	No	indication
RG351-11109-102	Nut	-	_	Excellent	No	indications
RG351-11136-101	Pin (2 pcs)	-	-	Excellent		-
RG351-11135-101	Cage	06	-	Slight wear at slot end	No	indications
RG351-11133-041	Cam	03	-	Parco finish removed on flats.	No	indications
RG351-11117-104	Nut	-	-	Excellent	No	indications
SB2157-2	Roller Brg.	429B	256.9	Slight fretting on O.D.		-
RG351-11131-101	Spur Shaft	10	-	Fretting around flange holes.	No	indications

·	TABLE XVIII - Continued		
TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
•	Excellent	No indications	•
256.9	Ext. spline excessive fretting. Int. spline has slight fretting.	No indications	Requires improved lubrication.
-	Excellent	-	-
256.9	Outer race edge has pit marks.	No indications	Possibly insufficient clamp up pressure.
-	Excellent	No indications	-
-	Excellent	.	-
-	Slight wear at slot end	No indications	=
-	Parco finish removed on flats.	No indications	No surface indentation
-	Excellent	No indications	-
256.9	Slight fretting on O.D.	-	Localized fretting in area of oil drainage slot in housing.
-	Fretting around flange holes.	No indications	-

TABLE XVIII - Continued

_					TABLE AVEL CONCENSOR		
	PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		SNAGLOW/ INSPECTI
	RG351-11132-101	Spur Gear	10	256.9	Fretting around mounting holes. Gear teeth excellent.		-
	RG351-11139-101	Bushing	-	-	Excellent		-
	X3762	Roller (14 pcs)	-	-	Excellent	No	indicat
	RG351-11128-101	Bevel Gear	07	256.9	Excellent	No	indicat
	RG351-11129-101	Bevel Shaft	03	•	Int. spline fretted with excessive oxidation residue.	No	indicat
	SB1056-2	Duplex Brg.	1822	256.9	Excellent		-
	RG351-11134-101	Cam Hsg	82	••	Excellent	No	indica
	RG351-11143-101	Nut	-	-	Excellent	No	indica
	MR-1922-C-400	Roller Brg.	21	256.9	Excellent		-
	RG351-11126-041	Housing	01	-	Excellent	No	indica
	RG351-11109-101	Nut	-	-	Excellent	No	indica

TABLE XVIII - Continued

	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
	256.9	Fretting around mounting holes. Gear teeth excellent.	-	=
	-	Excellent	-	-
	-	Excellent	No indications	-
	256.9	Excellent	No indications	Dynamic teeth patterns excellent.
	-	Int. spline fretted with excessive oxidation residue.	No indications	Requires improved lubrication
2	256.9	Excellent	-	_
	-	Excellent	No indications	-
	-	Excellent	No indications	-
	256.9	Excellent	-	-
	-	Excellent	No indications	-
	-	Excellent	No indications	-

TABLE XVIII - Continued

				TABLE XVIII - Continued	
PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZY INSPECTION
RG351-11193-101	Bevel Gear	1	•	Small nick 2/3 along face (one tooth).	No indication
34306 34478	Timken Brg. Timken Brg.	-	-	Excellent	-
RG351-11266-041		-	-	Excellent	-
RG351-11191-041	Housing	05	-	Excellent	No indication
SB3253A-1 SB3253B-1	Timken Brg. Timken Brg.	-	-	Excellent	;-
RG351-11117-105	Nut	-	-	Excellent	No indication
RG351-11248-101	Spacer	-	-	Excellent	No indicatio
RG351-11157-101	Quill Shaft	03	-	Slight fretting at both external splines.	No indicatio
RG351-11156-102	Clip	-	-	Excellent	No indicatio
RG351-11178-101	Nut	-	ī .	Excellent	No indicatio
RG351-11151-041	Hag. Ass'y	04	-	Excellent	No indicatio

TABLE	XVIII	- Co	ntinued

		TABLE XVIII - Continued		
l.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
	-	Small nick 2/3 along face (one tooth).	No indications	This nick caused a slight impression in the mating gear RG351-11155-101. Nick was probably caused by mishandling.
	-	Excellent	-	-
	-	Excellent	-	-
	-	Excellent	No indications	-
	-	Excellent	-	-
	-	Excellent	No indications	-
	-	Excellent	No indications	-
	-	Slight fretting at both external splines.	No indications	Requires more lubricant.
	-	Excellent	No indications	-
	-	Excellent	No indications	-
	-	Excellent	No indications	-

TABLE XVIII - Continued

				TABLE XVIII - Continued		
PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		Gnaglow/z Inspectio
RG351-11155-101	Bevel Gear	04	•	Gear pattern has an impression 1/3 from O.D. on each tooth.	No	indicati
SB3602B-1 SB3602A-1	Timken Brg. LL639210	•	-	Excellent		-
RG351-11137-101	Spacer	-	-	-	No	indicati
RG351-11153-101	Outer Shaft	02	-	Internal spline fretting	No	indicati
MR-1840-C-400	Roller Brg.	Е9	-	Outer race O.D. shows slight fretting in one place.		-
RG351-11109-103	Nut	-	-	Excellent	No	indicati
RG351-11212-101	Spur Gear	01	-	Excellent	No	indicati
SB2102-1	Roller Brg.	3350	-	Excellent		-
SB1106-1	Ball Brg.	-		Excellent		_
B-107716	Seal	-	-	Excellent		-
S6135-20053-3	Nut	•	-	Excellent	No	indicat
RG351-11211-101	Spur Gear	02	-	Excellent	No	indicat

TABLE	XVIII	- Cor	ntinued

	TABLE XVIII - Continued		
TOTAL TEST TIME	VISUAL INSPECTION	Magnaglow/zyglo Inspection	COMMENTS
-	Gear pattern has an impression 1/3 from O.D. on each tooth.	No indications	This was caused by a nick in the mating pinion RG351-11193-101.
-	Excellent	-	-
-	-	No indications	-
-	Internal spline fretting	No indications	Requires improved lubrication.
-	Outer race O.D. shows slight fretting in one place.	-	Localized fretting in area of oil drainage slot in housing.
-	Excellent	No indications	-
=	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	-	-
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	No indications	-

TABLE XVIII - Continued

PART NUMBER NOMENCLATURE NO. TIME VISUAL INSPECTION INSPE SB2102-1 Roller Brg. 3283 - Excellent - SB1106-1 Ball Brg. - Excellent - B-107716 Seal - - Excellent No indi RG351-20053-3 Nut - - Excellent No indi RG351-11223-101 Gear Shaft 05 - Excellent No indi SB2100-2 Roller Brg 121 - Excellent No indi RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi SB1157-1 Ball Brg. - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi					TABLE AVIII - CONTINUED		
SB1106-1 Ball Brg. - - Excellent - B-107716 Seal - - Excellent - S6135-20053-3 Nut - - Excellent No indi RG351-11223-101 Gear Shaft 05 - Excellent No indi SB2100-2 Roller Brg 121 - Excellent No indi RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	PART NUMBE	R NOMENCLATURE		TEST	VISUAL INSPECTION		GNAGLOW/ZY INSPECTION
B-107716 Seal - - Excellent - S6135-20053-3 Nut - - Excellent No indi RG351-11223-101 Gear Shaft 05 - Excellent No indi SB2100-2 Roller Brg 121 - Excellent No indi RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg. - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	SB2102-1	Roller Brg.	3283	-	Excellent		-
S6135-20053-3 Nut - - Excellent No indi RG351-11223-101 Gear Shaft 05 - Excellent No indi SB2100-2 Roller Brg 121 - Excellent No indi RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	SB1106-1	Ball Brg.	-	-	Excellent		-
RG351-11223-101 Gear Shaft 05 - Excellent No indi SB2100-2 Roller Brg 121 - Excellent - RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg. - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	B-107716	Seal	-	-	Excellent		-
SB2100-2 Roller Brg 121 - Excellent - RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg - Excellent - NAS 1493-13 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	S6135-20053-3	Nut	-	-	Excellent	No	indicatio
RG351-11222-101 Gear 07 - Excellent No indi RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg - Excellent - NAS 1493-13 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	RG351-11223-1	01 Gear Shaft	05	-	Excellent	No	indicatio
RG351-11197-101 Gear 01 - Excellent No indi NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg - Excellent - - NAS 1493-13 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	SB2100-2	Roller Brg	121	-	Excellent		_
NAS 1493-12 Nut - - Excellent No indi SB1157-1 Ball Brg. - - Excellent - NAS 1493-13 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	RG351-11222-1	01 Gear	07	-	Excellent	No	indicatio
SB1157-1 Ball Brg. - - Excellent - NAS 1493-13 Nut - - Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	RG351-11197-1	01 Gear	01	-	Excellent	No	indication
NAS 1493-13 Nut Excellent No indi RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	NAS 1493-12	Nut	-	-	Excellent	No	indication
RG351-11196-101 Gear 02 - Excellent No indi RG351-11209-101 Gear 01 - Excellent No indi	SB1157-1	Ball Brg.	-	-	Excellent		-
RG351-11209-101 Gear 01 - Excellent No indi	NAS 1493-13	Nut	-	-	Excellent	No	indication
	RG351-11196-1	01 Gear	02	-	Excellent	No	indication
	RG351-11209-1	01 Gear	01	-	Excellent	No	indication
HU1013EAR5612 Roller Br. 12 - Excellent No indi	HU1013EAR5612	Roller Br.	12	-	Excellent	No	indication

TABLE XVIII - Continued

	TABLE XVIII - Continue	ed	
TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
-	Excellent	-	-
-	Excellent	-	-
-	Excellent	_	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-

TABLE XVIII - Continued

PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZY INSPECTION
NAS 1493-14	Nut	-	•	Excellent	No	indication
208-S-400	Ball Brg.	-	-	Excellent		-
515836	Seal	-	-	Excellent		-
65351-11231-102	Flange	_	-	Excellent	No	indicati
RG351-11220-101	Gear	05	-	Excellent	No	indicati
SB1131-102	Duplex Ball Brgs.	19	-	Excellent		-
508863	Seal	-	-	Excellent		-
S6135-20348-0	Flange	71	-	Excellent	No	indicat:
S6135-20031-1	Nut	-	-	Excellent	No	indicat:
RG351-11219-101	Gear	01	-	Excellent	No	indicat
SB1100-3(2)	Ball Brg.	-	-	Excellent		-
s6135-20075-0	Shaft Quill	-	-	Excellent	No	indicat
CB67-4	Seal	-	-	Excellent		-

TABLE XVIII - Continued

TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
-	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	-	-
_	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	-	<u>-</u>

TABLE XVIII - Continued

L					TABLE AVIII - CONCINGE		
	PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZY INSPECTION
	6435-20047-100	Nut	-	•	Excellent	No	indicatio
	SS5075-15	-	-	=	Tangs broke off.		-
	RC351-11213-101	Gear	05	-	Excellent	No	indication
	SB2102-1	Roller Brg.	3340	-	Excellent		-
ļ	SB1105-1	Ball Brg.	-	=	Excellent		-
	CB66-4	Seal	-	-	Excellent		-
	S6135-20053-2	Nut	-	-	Excellent	No	indication
	S6135-20181-2	Gear	703	-	Excellent	Ио	indication
	SB2102-1	Roller Brg.	-	-	Excellent		-
	SB1105-1	Ball Brg.	-	-	Excellent		-
	CB66-4	Seal	-	-	Excellent		-
	S6135-20053-2	Nut	-	-	Excellent	No	indication
	S6135-20181-2	Gear	699	-	Slight debris damage	No	indication
1							

TABLE XVIII - Continued

VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
Excellent	No indications	This nut was used in place of NAS1493-9
Tangs broke off.	-	SS5075-15 was used in place of NAS1443-9.
Excellent	No indications	-
Excellent	-	-
Excellent	-	-
Excellent	-	-
Excellent	No indications	-
Excellent	No indications	-
Excellent	-	-
Excellent	-	-
Excellent	-	-
Excellent	No indications	-
Slight debris damage	No indications	- ·

TABLE XVIII - Continued

<u> </u>						
	PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYG INSPECTION
	SB2102-1	Roller Brg.	3352	-	Excellent	•
	SB1105-1	Ball Brg	-	-	Excellent	-
	CB66-4	Seal	-	-	Excellent	-
	S6135-20053-2	Nut	-	-	Excellent	No indication
	RG351-1:.233-101	Oil Pump	B 1174	-	Excessive fretting at internal square drive.	-
	RG351-11218-041	Elbow Ass'y	007	-	Excellent	-
	S6135-20053-5	Nut	-	-	Excellent	No indication
	SB1104-3	Ball Brg.	-	-	Excellent	-
	RG351-11216-101	Spacer	13	-	Excellent	No indication
	SB2102-1	Roller Brg.	3301	-	Excellent	-
	RG351-11214-101	Gear	05	-	Slight debris damage on drive side of gear.	No indication
	RG351-11215-101	Quill Shaft	-	-	Fretting on external square drive.	No indication
	NAS1493-12	Nut	_	-	Excellent	No indication

TABLE XVIII - Continued

	TABLE XVIII - CONTINUED		
TAL ST ME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
_	Excellent	•	-
-	Excellent	-	-
-	Excellent	-	-
*	Excellent	No indications	-
-	Excessive fretting at internal square drive.	-	Insufficient lubrication.
-	Excellent	-	-
-	Excellent	No indications	-
-	Excellent	-	•
_	Excellent	No indications	-
-	Excellent	-	-
-	Slight debris damage on drive side of year.	No indications	-
•	Fretting on external square drive.	No indications	Insufficient lubrication.
-	Excellent	No indications	•

					TABLE XVIII - Continued		
	PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ INSPECTI
	M211KMBRA1590	Ball Brg.	-	-	Excellent		-
	RG351-11251-101	Gear	02	-	Slight pitting on gear teeth.	No	indicat
	SB1159-1	Ball Brg.	-	-	Excellent		-
:	NAS1493-10	Nut	-	-	Excellent	No	indicat
	NAS1493-12	Nut	-	-	Excellent	No	indicat
	M211KMBRA1590	Ball Brg	-	-	Excellent		-
	NAS1493-12	Nut	-	-	Excellent	No	indica
	NAS1493-10	Nut	-	-	Excellent	No	indica
	SB1159-1	Ball Brg.	-	-	Excellent		-
	RG351-11257-101	Gear	06	-	Slight pitting on gear teeth; external spline shows slight wear pattern.	No	indica
	HU-1012-LAR- 3514	Roller Brg	3	-	Excellent		-
	CB81-23	Seal	-	-	Excellent		-
	S6137-23067-1	Flange	-	-	Excellent	No	indica

MADIE	VITTT	- Continued
TABLE	XVIII	

		TABLE XVIII - Continued			
SER.	TOTAL TEST TIME	VISUAL INSPECTION		GNAGLOW/ZYGLO INSPECTION	COMMENTS
-	-	Excellent		-	-
02	•	Slight pitting on gear teeth.	No	indications	-
-	-	Excellent		-	-
-	-	Excellent	ИО	indications	-
-	-	Excellent	No	indications	-
-	-	Excellent		-	_*
-	-	Excellent	No	indications	-
-	-	Excellent	No	indications	-
-	-	Excellent		-	-
06	-	Slight pitting on gear teeth; external spline shows slight wear pattern.	No	indications	-
3		Excellent		-	-
-	-	Excellent		-	-
-	-	Excellent	No	indications	-

PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZY(INSPECTION
S6137-23047-3	Nut	•	•	Excellent	No indication
s6135-22072-1	Coupling	-	-	Excellent	No indication
s6135-22072-1	Coupling	•	•	Excellent	No indication

	TABLE XVIII - Continu	ed	
TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
	Excellent	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	-

TABLE XIX. 200-HOUR INSPECTION DUMMY GEARBOX ROLLER GEAR UNIT

_					NODIER GERK CHII	
	PART NUMBER	NOMENCLATURE	SER. NO.	TOTAL TEST TIME	VISUAL INSPECTION	Magnaglow/2 Inspectio
	RG351-11183-041	Sun Gear	03	230.4	Slight debris damage in both rollers and gear teeth.	No indicati
	RG351-11182-062	lst-Row Pinion	36	200.0	Rollers and gear teeth excellent.	No indicati
	RG351-11182-062	1st-Row Pinion	37	200.0	Rollers and gear teeth excellent.	No indicati
	RG351-11182-062	lst-Row Pinion	38	200.0	Small lower roller not polished. Other rollers and gears excellent.	No indicati
	RG351-11182-062	lst-Row Pinion	41	200.0	Small rollers are not polished. Other rollers and gears excellent.	No indicati
	RG351-11182-062	lst-Row Pinion	44	200.0	Stain on upper small roller. Rollers and gear teeth excellent.	No indicati
	RG351-11182-062	1st-Row Pinion	45	200.0	Rollers and gear teeth excellent.	No indicati
	RG351-11182-062	1st-Row Pinion	46	200.0	Small rollers are not polished. Small gear has pit marks on gear flank near root.	No indicati
	RG351-11181-062	2nd-Row Pinion	01	247.4	Rollers and gear teeth excellent.	No indicati
	RG351-11181-062	2nd-Row Pinion	07	220.9	Rollers and gear teeth excellent.	No indicati
	RG351-11181-062	2nd-Row Pinion	10	247.4	Rollers and gear teeth excellent.	Upper gear fland an indication.

TABLE XIX.	200-HOUR	INSPECTION	DUMMY	GEARBOX
	ROLLER GEA	AR UNIT		

R.	TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
13	230.4	Slight debris damage in both rollers and gear teeth.	No indications	-
6	200.0	Rollers and gear teeth excellent.	No indications	-
7	200.0	Rollers and gear teeth excellent.	No indications	-
3	200.0	Small lower roller not polished. Other rollers and gears excellent.	No indications	-
1	200.0	Small rollers are not polished. Other rollers and gears excellent.	No indications	-
١	200.0	Stain on upper small roller. Rollers and gear teeth excellent.	No indications	-
	200.0	Rollers and gear teeth excellent.	No indications	-
	200.0	Small rollers are not polished. Small gear has pit marks on gear flank near root.	No indications	•
	247.4	Rollers and gear teeth excellent.	No indications	-
	220.9	Rollers and gear teeth excellent.	No indications	-
	247.4	Rollers and gear teeth excellent.	Upper gear flange shows an indication.	Radial crack originating from EB weld.

TABLE XIX - Continued

PART NUMBER	NOMENCLATURE	SER.	TOTAL TEST TIME	VISUAL INSPECTION	Magnaglow/zyo inspection
RG351-11181-062	2nd-Row Pinion	16	247.4	Rollers and gear teeth excellent. Metallic particles inside bore.	Upper gear flange shows an indication
RG351-11181-062	2nd-Row Pinion	17	247.4	Rollers and gear teeth excellent.	No indication
RG351-11181-062	2nd-Row Pinion	19	247.4	Rollers and gear teeth excellent.	Upper gear flange shows an indication
RG351-11181-062	2nd-Row pinion	23	247.4	Large gear shows pitting 6 teeth. Rollers and small gear excellent.	No indication
RG351-11585-103	Hub	05	-	Excellent	No indication
RG351-11585-041	Plate Ass'y	04	-	Excellent	No indication
RG351-11176-041	Plate Ass'y	-	-	Excellent	No indication
RG351-11187-101	Splined Plate	01	-	7 groups of 7 teeth located symmetrically exhibit full face loading. Location midway between posts.	No indication
RG351-11173-101	Nut	-	-	Excellent	No indication
RG351-11173-101	Nut	-	-	Excellent	No indication
RG351-11173-101	Nut	-	-	Excellent	No indication
RG351-11173-101	Nut	-	-	Excellent	No indication

TABLE XIX - Continued

TOTAL TEST TIME	VISUAL INSPECTION	MAGNAGLOW/ZYGLO INSPECTION	COMMENTS
247.4	Rollers and gear teeth excellent. Metallic particles inside bore.	Upper gear flange shows an indication.	Radial crack originating from EB weld.
247.4	Rollers and gear teeth excellent.	No indications	-
247.4	Rollers and gear teeth excellent.	Upper gear flange shows an indication.	Radial crack originating from EB weld.
247.4	Large gear shows pitting 6 teeth. Rollers and small gear excellent.	No indications	-
-	Excellent	No indications	-
-	Excellent	No indications	=
-	Excellent	No indications	-
-	7 groups of 7 teeth located symmetrically exhibit full face loading. Location midway between posts.	No indications	Reaction torque deflections. No significant wear.
-	Excellent	No indications	-
-	Excellent	No indications	-
47	Excellent	No indications	-
-	Excellent	No indications	-

TABLE XIX - Continued

\vdash									
	PART I	NUMBER	NOMENCLATURE		TOTAL TEST TIME		UAL INSPECTION		Gnaglow/zy(Inspection
	RG351-11	173-101	Nut	_	-		Excellent	No	indication
İ	RG351-11	173-101	Nut	-	-		Excellent	No	indication
	RG351-11	173-101	Nut	-	-		Excellent	No	indication
	RG351-111	189-101	Oil Pump Gear	-	-		Excellent	No	indication
	RG351-111	186-041	Plate Ass'y	-	-		Excellent		-
	RG351-111	177-101	Post	74	256.9		Excellent	No	indication
	RG351-111	177-101	Post	75	256.9		Excellent	No	indication
	RG351-111	177-101	Post	76	256.9		Excellent	No	indication
	RG351-111	177-101	Post	83	256.9		Excellent	No	indication
	RG351-111	177-101	Post	85	256.9		Excellent	No	indication
	RG351-111	177-101	Post	87	256.9		Excellent	No	indication
	RG351-111	177-101	Post	89	256.9		Excellent	No	indication
	RG351-111	184-041	Ring Gear	04	-		Excellent	No	indication
	22313 VA	3	Spherical Brg	. N6	200.9	Slight face.	fretting on end		-
	22313 VA	3	Spherical Brg	. N7	220.9		Excellent		-
	22313 VA	3	Spherical Brg	. N13	220.9	Slight face.	fretting on end		-
	22313 VA	3	Spherical Brg	. N21	220.9		Excellent		-

TABLE XIX - Continued

TOTAL TEST TIME	VISUAL INSP	ECTION		GNAGLOW/ZYGLO INSPECTION			COMME	NTS
-	Excelle	nt	No	indications			-	
-	Excelle	nt	No	indications			-	
-	Excelle	nt	No	indications			-	
-	Excelle	nt	No	indications			-	
-	Excelle	nt		-			-	
256.9	Excelle	nt	No	indications			_	
256.9	Excelle	nt	No	indications			-	
256.9	Excelle	nt	No	indications			-	
256.9	Excelle	nt	No	indications			-	
256.9	Excelle	nt	No	indications			į .=	
256.9	Excelle	nt	No	indications			-	
156.9	Excelle	nt	No	indications			-	
-	Excelle	nt	No	indications			-	
	Slight fretting	g on end		-	Due	to	spacer	working
20.9	Excelle	nt		-			-	
20.9	Slight fretting face.	g on end		-	Due	to	spacer	working
10.9	Excelle	nt		-			-	

TABLE XIX - Continued

PART NUMBER	NOMENCLATURE		TOTAL TEST TIME	VISUAL INSPECTION	Magnaglow/2 Inspectio
22313 VAG	Spherical Brg.	N32	220.9	Excellent	-
22313 VAG	Spherical Brg.	Р ЕИ	220.9	Excellent	-
22313 VAG	Spherical Brg.	N40	220.9	Excellent	-
RG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati
RG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati
RG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati
RG351-11179-101	Spacer	- 1	200.0	Faces worn .002007	No indicati
FG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati
RG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati
RG351-11179-101	Spacer	-	200.0	Faces worn .002007	No indicati

TABLE XIX - Continued

VISUAL INSPECTION	Magnaglow/zyglo Inspection	COMMENTS
Excellent	-	-
Excellent	-	-
Excellent	-	-
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
Faces worn .002007	No indications	Wear due to working of 2nd row gear flange assembly.
	Excellent Excellent Excellent Faces worn .002007	Excellent - Excellent - Excellent - Excellent - Excellent - Faces worn .002007 No indications

Visual Inspection Results

Visual inspection of the roller gear units from the test and dummy gearboxes revealed slight surface flaking on one small roller of first-row pinion, serial number 33, from the test gearbox. This flaking, visible in Figure 109, is approximately 0.00015 inch deep and is caused by incorrect blending of the crown radius on the roller of second-row pinion serial number 29. First-row pinion, serial number 49, also exhibits similar signs of distress though not as pronounced as serial number 33. All other rollers are in excellent condition. Some second-row rollers still retain the phosphate (Parco-Lubrizing) finish, indicating pure rolling contact. The gear teeth on all roller gear components are in excellent condition as are the spherical bearings. The spacers, which clamp the outer races of the second-row spherical bearings, experienced working as a result of the deflections induced on the gear/flange assembly by the ring gear teeth loads. Further evidence of the fatigue loads imposed on this gear/flange assembly is shown in Figure 110 by the fretting around the taper-lock bolt holes.

Both roller gear reaction splined plate assemblies exhibited similar loadings and deflections with full face contact of the mating splines located midway between the second-row pinion posts.

Except for the splined connections on the quill shafts, the remaining components in both gearboxes are in excellent condition. The input and tail takeoff bevel gear patterns are excellent, and the stronger springs installed in the freewheel units successfully presented chucking of the rollers. The quill shaft splines require better lubrication to prevent the fretting oxidation which was occurring. The quill shaft driving the left-hand freewheel unit outer housing, Figure 111, generated excessive amounts of metallic particles as seen in the bevel gear shaft, Figure 112.

Ultrasonic Inspection

The sun gear and first- and second-row pinions from both gearboxes were subjected to the pulse-echo ultrasonic inspection of Appendix II. The ultrasonic recordings obtained were compared to the recordings received when the parts were accepted to determine if there was any degradation of the weld; none could be found.

Figure 109. Roller Surface Flaking - First-Row Pinion.



Figure 110. Fretting - Second-Row Pinion, Gear/Flange.



Figure 111. Bevel Gear/Freewheel Housing - Drive Arrangement.



Figure 112. Fretting - Bevel Gear Shaft.

Magnetic Particle Inspection (Magnaglow)

All ferrous components were subjected to fluorescent magnetic particle inspection by the wet continuous method. Indications appeared in the second-row pinions from both gearboxes. The test gearbox second-row pinions, serial numbers 29, 38, 48 and 49, showed circumferential cracks around the bearing bore; also, the roller on serial number 49 witnessed a crack radiating from the roller-gear butt face. The dummy second-row gear/flange assemblies, serial numbers 10, 16 and 19, all showed a single crack radiating from the radius between the gear and flange.

All other ferrous components successfully passed inspection.

Metallurgical Inspection

Sectioning of the second-row pinion, serial number 49, revealed the circumferential crack, indicated by the arrow A in Figure 113, was caused by fatigue cracking originating from multiple voids in the weld root. Figure 114 shows a weld root void penetrating past the butt faces of the gear vertical web and bearing bore shoulder.

The roller crack, indicated by the arrow B in Figure 113, is shown in the black light photograph of Figure 115 and in relation to the weld in Figure 116. Again, this fatigue crack originated from voids in the weld root.

Figure 117 is a view of the radius between the gear and flange of second-row pinion, gear/flange assembly, serial number 16. The crack indicated by the arrow is typical of those witnessed in serial numbers 10 and 19. Visible in Figure 117 is a weld splatter line caused by blow-out of the weld. Metallographic examination revealed a series of voids along the weld line as shown in Figure 118. Separation of the cracked part revealed a fatigue crack, as indicated by the beach marks visible in Figure 119. Microscopic examination revealed the crack originated from a weld void, Figure 120.

It was concluded that these fractures initiated from the voids in the electron beam welds.

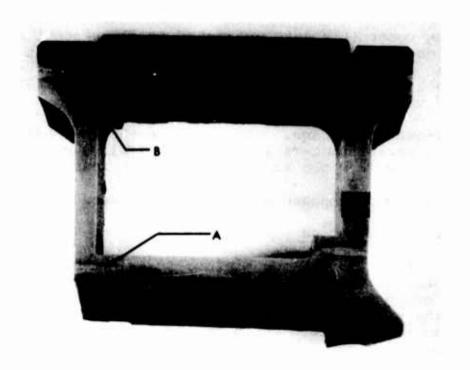


Figure 113. Cross-Section - Second-Row Pinion.

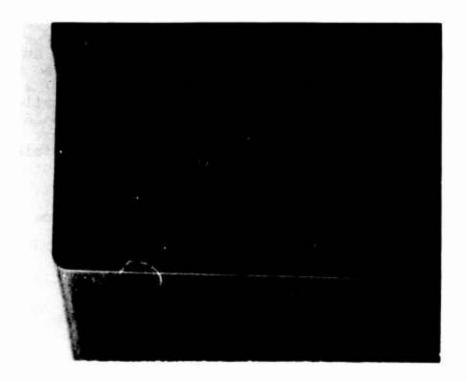


Figure 114. Crack - Bearing Bore.

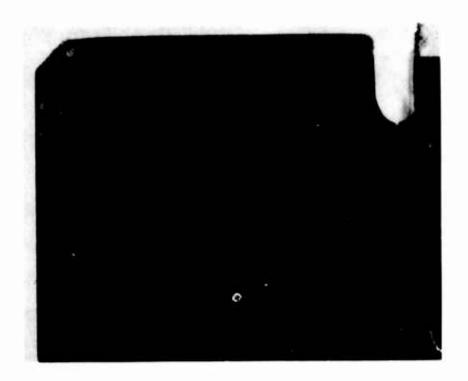


Figure 115. Roller Weld Crack - Second-Row Pinion.

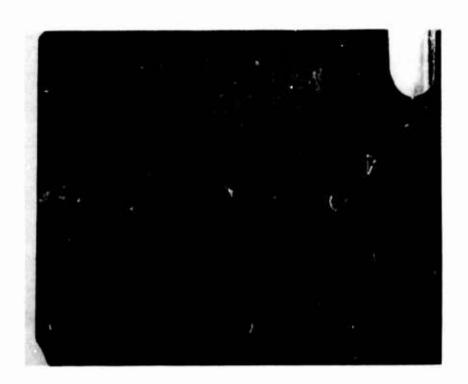


Figure 116. Roller Crack - Electron Beam Weld.



Figure 117. Gear/Flange Radius - Second-Row Pinion.

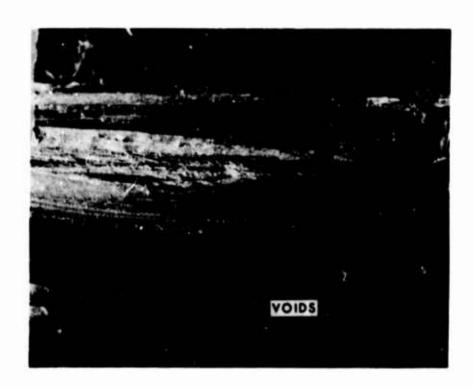


Figure 118. Weld Splatter - Gear/Flange Weld.



Figure 119. Fatigue Crack - Gear/Flange, Second-Row Pinion.



Figure 120. Crack Origin - Electron Beam Weld Void.

EFFICIENCY TEST

Coincident with the 200-hour endurance test, an efficiency test was performed on the roller gear drive test gearbox. After the first 110 hours of the 200-hour endurance test had been completed, layers of fiberglass insulation were installed around the test gearbox and the oil line between the test gearbox and the water-oil heat exchanger. Water temperature into and out of the heat exchanger was then monitored for a series of operating conditions.

Efficiency Test Results

Assuming no heat losses from the gearbox or oil line, the friction horsepower of the gearbox was calculated by assuming it to be equal to the heat absorbed by the water in the heat exchanger.

Then:

FHP = $0.02356 Q (h_2 - h_1)$

where

FHP = friction horsepower of test gearbox

0.02356 = conversion factor, Btu/min into horsepower

Q = water mass flow rate, lb/min

 h_2 = enthalpy of water at exit temperature (T_2)

 h_1 = enthalpy of water at inlet temperature (T_1)

The data resulting from this test is presented in Table XX and a sample calculation appears below.

			TABLE XX.	GEARBOX EFFICIENCY,		TEST RESULTS	
Input Power (hp)	Tail Power (hp)	T1 (°F)	T2 (°F)	h] (Btu/lb)	h2 (Btu/lb)	Q Water Mass Flow Rate (lb/min)	Frictional Power (hp)
1100	250		109.4	3.02	77.34	48.78	85.4
1950	250	32	113.0	3.02	80.94	2	
2400	250		91.4	3.02	59,39	7.7	0.06
2700	250		86.0	5.04	4.0	8.4	2.06 2.06
3000	425	36	86.0	4.03	54.00		•
3560	425	36	95.0	4.03	•		2 86
3700	425	36	91.4	4.03	•	75.97	ν ασ
1950	250	37	93.2	4.05	7	•	
2400	250	36	8.96	4.03	4.7		200
2700	250	37	93.2	5.04		. L	, <
3000	425	36	87.8	4.03	5.8	78.74	7.40
3560	425	36	95.0	4.03	2	72.11	
3700	425	36	93.2	4.03	61.18	76.73	103.3

Sample Test Point Data

For an input horsepower of 1950 and a tail horsepower of 250:

Q = 48.59 lb/min

 $T1 = 35^{\circ}F$

 $T_2 = 113$ °F

 $h_1 = 3.02 Btu/lb$

 $h_2 = 80.94 \text{ Btu/lb}$

FHP = (0.2356) (48.59) (80.94 - 3.02)

FHP = 89.2

A plot of friction horsepower versus total input power is presented in Figure 121, while Figure 122 shows a plot of test gearbox efficiency versus total input power.

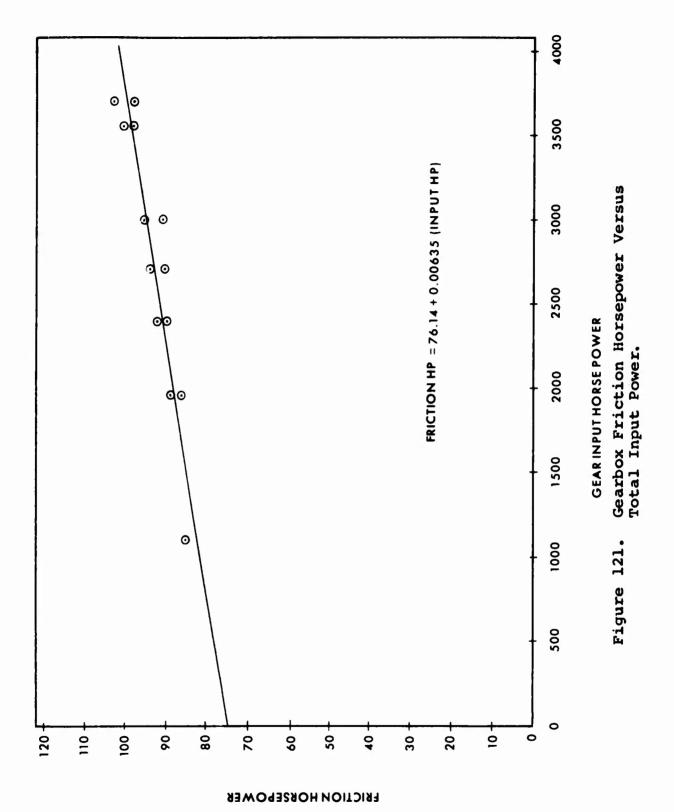
The efficiency of the gearbox at any input power is found from knowing the frictional horsepower at that particular input horsepower.

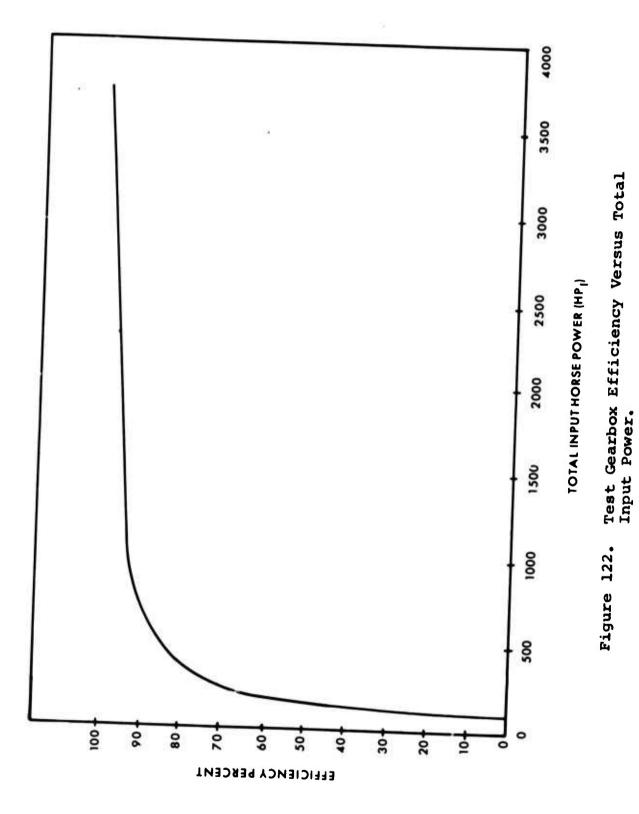
Thus:

Friction hp = 76.14 + 0.0065 (input hp)

And

Gearbox Efficiency, % = input hp - friction hp x 100 input hp





CONCLUSIONS

As a result of more than 250 hours of endurance testing, the following conclusions have been reached.

- 1. The roller gear unit proved it could perform for extended periods of time in the fatigue environment of a helicopter transmission.
- 2. Nearly all the major problems encountered in the earlier phases of testing were electron beam weld related problems. The majority of these problems have been resolved.
- 3. The ramp roller clutch type freewheel unit incorporated in the roller gear transmission performed exceedingly well, requiring only one slight adjustment of spring stiffness during the entire period of testing.
- 4. The roller gear unit exhibited excellent loading characteristics with very uniform loading of both first-and second-row pinions.
- 5. The roller surfaces supporting the roller gear unit completed the 200-hour endurance test in nearly perfect condition.
- 6. The compliant bearings tested in the gear development phase of testing require some design modification to permit greater shaft misalignment, perhaps by increased end play.
- 7. The chip detection system employed during testing performed exceedingly well in providing indications of failure within the roller gear transmission. The compartmentalization feature of this system also permitted rapid pinpointing of the failed component.
- 8. Lubrication of the quill shaft splines within the transmission during these tests was deemed inadequate, and further work is necessary to provide these splines with a greater supply of lubricant.
- 9. Spherical bearing spacers used within the second-row pinions exhibited excessive wear and should be modified to alleviate this problem.
- 10. The efficiency of the roller gear transmission at the maximum design power of 3,700 hp is 97.3%. This efficiency compares favorably to transmissions of conventional design. Efficiency tests for the roller gear drive unit alone were not conducted. This task will be accomplished during subsequent testing of the roller gear drive unit.

11. Ultrasonic inspection methods and acceptance criteria for electron beam welds were developed during this program and proved to be excellent tools in the evaluation of electron beam welded components.

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APPENDIX I

ROLLER GEAR TRANSMISSION - TEST DATA

Table XXI contains the data monitored on the test and dummy gearboxes during the bench tests. The total test time accumulated by both gearboxes during the gear pattern development, initial, and 200-hour endurance tests totaled 256 hours 56 minutes. Testing was initiated on 7/6/71 and concluded 1/19/73.

The total input horsepower is the power to the dual inputs of the test gearbox. It is computed from the power measured in the test main rotor shaft less the tail power and gearbox friction power. Wheatstone bridge signals are transmitted from the strain gaged main rotor and tail drive shafts through silver graphite bushes to a light beam oscillograph.

The test and dummy gearboxes are each equipped with 48 thermocouples to record bearing, oil-in, oil-out, and ambient temperatures. Two 24-channel 2-bank recorders identify, indicate and print out the thermocouple temperature.

The total oil flow to each gearbox and oil flow to each roller gear unit was monitored using a flow turbine. Oil pressure at the gearbox lubrication pumps, manifolds and two input extensions to the dummy gearbox was monitored on direct reading pressure gages.

						T,
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1 2 3 4 5 6 7 8 9
7/6/71	10:05	00:00	0	0	DUMMY TEST	Start on power at 10:05 Test stand check out both test and du
7/6	11:23	01:18	0	0	DUMMY TEST	83 109 114 119 105 100 99 110 110 1 59 67 71 70 73 73 74 74 87
7/9	13:26	01:18	0	0	DUMMY TEST	Start on power at 13:26 1/2 speed 00:35 at zero load, 00:06 at 25% lo
7/9	14:13	02:05	50%	0	DUMMY TEST	Stop inspect gear patterns
7/9	14:15	02:05	75%	0	DUMMY TEST	Start on power at 14:15 1/2 spec 00:06 at 75% load and 00:15 at 100%
7/9	14:36	02:26	100%	0	DUMMY TEST	75 85 94 93 92 78 90 86 94 9 55 63 66 83 65 80 67 86 73 8
7/12	14:36	02:26	0	0	DUMMY TEST	Start on power at 15:05 Dual shaft
7/12	15:00	02:29	100%	0	DUMMY TEST	Stop check temperatures
7/12	16:10	02:29	0	0	DUMMY TEST	Start on power at 16:10 Dual shaft fo
7/12	16:13	02:32	100%	0	DUMMY TEST	78 106 100 111 92 94 91 99 99 11 83 85 104 105 102 100 100 95 105 10
7/13	13:40	03:42	0	0	DUMMY TEST	Start on power at 9:50 tail loop check 00:25 at zero load, 00:15 at 100 H.P.



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY

TEMPERATURE (°C)

10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28

th test and dummy installed (No input shafts)

80 103 101 106 96 92 92 88 93 96 87 85 90 86 76 73 63 99 110 110 122 100 104 80 74 73 90 80 80 77 80 71 74 90 89 92 99 83 79 74 74 87 88 90 90 79

1/2 speed gear pattern test (R/H Test - L/H Dummy only) :06 at 25% load and 00:06 at 50% load (50% Load = 925 S.H.P.)

erns

1/2 speed gear pattern test (R/H Test - L/H Dummy only) 0:15 at 100% load (100% Load = 1850 S.H.P.)

83 83 86 94 97 76 84 87 84 79 81 80 85 85 84 84 85 84 85 90 72 130 131 131 117 121 124 116 68 62 72 86 73 71 71 67 73 82 72 73

Dual shaft full speed

es

Dual shaft full speed

78 72 76 75 65 70 76 71 69 75 79 94 88 93 81 88 93 99 99 116 91 70 52 94 95 86 82 81 145 148 137 131 122 129 121 70 68 92 100 95 105 105 95 95 70 66

tail loop check out

15 at 100 H.P., 00:15 at 250 H.P. and 00:15 at 425 S.H.P.



T	OR'	Y B	ACI	(-T	O-B	AC	KT	EST	(SH	EET	1	1									
																					PUM FLOW
3_	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL ROLLE
3	63 71	71 67	62 65	60 65	60 65	82 79	7 2 67	83 84	78 84	95 77	82 82	74 70	67 68	75 68	73 67	76 76	75 80	75 80	73 74	36	19.8 23.5
)	59 69	69 68	85 62	57 62	58 60	77 63	69 59	75 69	60 68	85 62	78 60	64 60	68 59	72 60	66 60	82 70	67 70	66 71	63 65		17.4 19.8
	52 66	57 65	60 65	50 53	49 62	65 74	58 63	68 80	68 80	84 90	67 77	61 68	67 62	62 60	61 60	58 70	56 75	66 73	61 69	34	18.0 22.8
						<u>. </u>							-								

3H	EET	1	}																
													PUMP			NIFC			AMY
		•	40	4.	46	4.6	14.4			4=	46		low			RES		PRI	:55
7	38	39	40	41	42	43	44	45	40	47	48	IOIAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
8 4	95 77	82 82	74 70	67 68	75 68	73 67	76 76	75 80	75 80	73 74	36	19.8 23.5		58 70	34 42	32 39	32 39	18	16
1	85 62	78 60	6 4 60	68 59	72 60	66 60	82 70	67 70	66 71	63 65	34	17.4 19.8		48 56	29 36	25 31	2 ¹ 4 31	15	15
	84 90	67 77	61 68	67 62	62 60	61 60	58 70	56 75	66 73	61 69	34	18.0 22.8		60 70	35 43	31 41	30 41	15	15



						TABL
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1 2 3 4 5 6 7 8 9 10
8/17/71	16:40	03:42				Start on power at 16:40
8/17	17:15	04:17		1		Stop input shaft problem
8/19						Start single shaft L/H on power at 13:10
8/19	13:10	04:17	1850	100	DUMMY TEST	98 112 114 124 103 109 100 117 115 133 60 87 115 112 113 75 110 78 114 97
8/19	14:10	05:17	1850	100	DUMMY TEST	97 111 114 124 103 108 99 116 114 132 62 89 114 112 113 74 110 78 114 97 Start single shaft R/H on power at 15:00
8/19	15:00	05:17	1850	100	DUMMY TEST	102 96 127 126 105 98 94 105 115 118 71 64 66 69 71 104 71 102 93 108
8/19	16:00	06:17	1850	100	DUMMY TEST	102 100 119 118 107 101 105 107 117 120 69 71 70 73 72 105 72 103 95 111
8/20	09:56	06:23	2200	200	DUMMY TEST	Start dual shaft on power at 09:50 Stop to check torque split
8/21	12:50	06:35	2200	250	DUMMY TEST	Start on power at 12:38 86 92 111 114 97 98 96 105 109 121 85 87 105 105 100 94 95 92 96 98
8/21	13:20	07:05	2200	250	DUMMY TEST	93 100 116 120 104 105 103 112 116 128 96 99 115 115 112 107 109 105 113 113 Start on power at 13:40
8/21	14:10	07:35	2200	250	DUMMY TEST	92 99 115 118 102 103 101 110 114 126 70 100 114 114 110 105 107 102 111 111



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABO

TEMPERATURE (

4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26

ver at 16:40

shaft problem

e shaft L/H on power at 13:10

		103 113	_		117 78		133 97		110 102		111 100		108 101	97 92	90 89	95 83	94 85	90 86	94 86	94 89	92 86	95 94	83 90
;]		103 113 aft F	74	110	78	114	132 97 5:00		110 101				108 101	96 92	90 88	94 84	92 84	89 85	83 88	92 88	91 85	94 93	82 89
		105 71	98 104	•			118 108		105 98	88 80		97 102	103 99	93 88	87 83	90 78	90 79	85 79	91 79	88 81	87 78	89 82	79 82
)	73		105	72	103	95	120 111		106 100		107 96		104 100	94 89	88 86	93 82	90 83	88 83	93 83	91 86	90 83	90 88	80 86
	shaft ck to				09:50)																	
	ver a	_		•																			
;	114	97 100		-	105 92		121 98		100 90		99 86		92 90	87 78	80 72	81 68	81 63	79 63	85 63	83 62	83 63	83 77	73 70
5	120 115 er a	112	107				128 113		107 104		106 100		98 104		88 90	92 90	90 88	88 89	93 89	92 90	91 87	93 97	83 92
		102				114 111	126 111	101 102	106 102		105 98		95 102	92 90	85 88	94 87	99 85	87 85	91 85	91 88	91 85	92 94	80 89

LABORATORY BACK-TO-BACK TEST (SHEET 2)

TURE (°C)

26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 T

83	76	66	59	69	72	53	54	80	71	82	75	98	72	74	69	75	73	77	72	72	70	36
90	79	72	71	71	66	59	58	82	69	86	87	90	84	70	68	71	72	78	84	84	68	
82	75	66	59	69	71	53	53	79	70	81	75	98	71	72	69	75	73	76	72	71	70	37
89	79	71	71	71	66	59	58	82	69	87	88	90	84	71	69	73	73	78	84	84	69	
79	76	75	67	75	74	71	69	80	74	82	83	96	77	76	67	76	75	76	75	77	76	38
82	76	70	67	67	65	57	56	79	66	82	83	86	82	70	68	70	71	74	80	77	66	
80	75	65	59	68	71	53	54	81	71	81	75	97	70	73	67	74	73	76	73	72	70	38
86	79	70	71	70	66	59	58	82	68	85	88	89	84	70	68	73	73	77	83	82	68	
73	69	61	55	63	66	50	50	75	64	74	68	89	64	65	61	65	65	69	67	66	64	35
70	69	62	62	68	63	54	52	69	58	69	68	82	69	55	61	57	57	66	72	66	58	
83	77	68	61	72	75	55	55	83	72	83	74	98	72	74	68	74	72	77	75	74	71	36
92	82	77	77	73	75	70	69	80	73	88	91	98	87	71	70	72	73	79	80	77	68	
80	75	66	60	69	72	55	54	81	72	81	77	97	72	76	64	76	74	75	73	74	71	38
89	86	74	73	72	74	74	69	84	82	87	91	95	85	71	68	73	74	78	85	83	69	

H	EET	2																
												PUMP			NIF			UMMY NPUT
7	20	20	40	49	45	42	4.4	4.8	44	47	40	FLOW TOTAL ROLLER	DDECC	i .	PRES		l P	RESS
_	38	39	40	41	<u> </u>	43	44	43	40	4/	40	TOTAL ROLLER	PRESS	MAII	<u> </u>	1 к/п	1./,	I R/H
														ja Ja				
5	98	72	74	69	75	73	77	72	72	70	36	22.5	70	lı ə	40	40	21	20
7	90	84	70	68	71	72	78	84	84	68	30	23.4	70 67	43 48	42	41	21	20
5	98	71	72	69	75	73	76	72	71	70	37	22.5	7 1	43	40	36	21	20
5 3	90	84	71	69	73	73	78	84	84	69	٠,	23.4	71 67	48	42	41		
3	96	77	76	67	76	75	76	75	77	76	38	22.2	72 68	44	41	37 41	21	20
3	86	82	70	68	70	71	74	80	77	66		23.4	68	49	42	41		
5	97	70	73	67	74	73	76	73	72	70	38	22.4	70 68	42	37	40	20	21
3	89	84	70	68	73	73	77	83	82	68		23.4	68	48	40	42		
												1						
} }	89 82	64 69	65 55	61 61	66 57	65 57	69 66	67 72	66 66	64 58	35	22.2 23.4	74 67	44 48	42 42	39 40	23	21
	<i>-</i>			0 1	71	71	33	15	55	70		-J.7	٠,	70	76	40		
.	98 98	72 87	74 71	68 70	74 72	72 73	77 79	75 80	74 77	71 68	36	22.8 23.7	73 67	44 48	42 42	39 40	23	21
		·			•	. •			•				,					
	97 95	72 85	76 71	64 68	76 73	74 74	75 78	73 85	74 83	71 69	38	22.8 23.7	71 67	43 48	42 42	38 40	22	21
_			-															91



														TAB	LE
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
8/21/71	14:40	08:05	2700	250	DUMMY TEST	71	102 103	114	122 114 ower		107 106 5:15			118 113	130 112
8/21	15:45	08:35	2700	250	DUMMY TEST	96 97	101 101	115 114	119 114	103	104 105			114 111	126 111
8/21	16:20	09:05	3240	250	DUMMY TEST	98	100 102	113	117 113	101	103 105			111 110	125 110
8/21	16:50	09:35	3240	250	DUMMY TEST		100 102		118 114		103 105		110 103	112 112	126 110
8/21	17:45	10:05	3500	425	DUMMY TEST	103 96	op in 98 101 op	115 102	117 102		103 104	100 107	110 102	113 109 on	125 109
8/21	19:05	10:35	3500	425	DUMMY TEST	99	97 100	114	117 112	101	102 104	100		112	124 110
8/21	19:35	11:05	3500	425	DUMMY TEST	101 97	93 98		117 112		103 105		109 103	113 112	125 111
8/21	20:05	11:35	3500	425	DUMMY TEST	101 97	93 98		117 112		103 105			113 112	126 111
8/21	21:27	11:38	3700	425			ert o			t 21: ity	:24				
8/21	23:22	11:45	3500	425		Sto	op ch	eck 1	acil	•		.15			
8/23	02:15	11:45	2200	250	DUMMY TEST	60 90	86 97	101	104 110	84 108		86	94 100	96 107	107 107



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY BACK TEMPERATURE (°C) 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 3 115 118 130 106 110 93 109 101 108 97 91 97 95 95 96 97 98 85 78 69 63 72 ' 95 104 113 112 103 103 83 99 102 103 92 90 90 89 88 88 82 76 93 89 96 92 75 74 ' 126 102 106 89 106 111 114 98 104 93 87 96 94 69 91 93 94 95 92 82 76 67 61 103 111 90 89 88 86 74 111 102 103 83 99 101 102 91 89 81 76 74 92 90 94 92 109 111 125 99 104 87 104 96 102 91 84 94 95 90 91 95 95 93 80 73 65 60 67 94 92 103 110 110 101 102 82 98 101 101 90 88 90 91 89 86 96 80 74 74 74 6 93 67 110 112 126 100 104 87 104 97 102 91 84 95 95 91 95 96 93 81 73 65 91 59 90 103 112 110 101 103 82 98 101 101 90 89 91 89 86 94 92 96 93 80 74 74 74 power at 17:15 110 113 125 100 104 88 105 97 103 91 84 94 92 90 92 90 92 93 82 75 68 61 70 88 93 91 109 100 101 81 97 102 101 89 87 88 90 85 80 76 102 109 95 93 74 74 7 on power at 18:35 109 112 124 100 104 86 104 96 103 91 84 94 92 91 91 95 95 93 80 75 68 61 70 7 110 100 101 81 97 101 101 88 87 87 89 87 81 78 76 102 109 85 93 90 94 92 77 7

 				-	,-			,-		• •	,-	-,	-	70	,_	"	75	0_	17	10	' '
	107 107	82 98	88 99	74 77	88 93	62 96	80 97	76 85	69 81	77 77	75 77	67 77	73 77	73 77	75 77	76 91	64 82	60 77	54 74	49 68	55 71

95 92 91 91

89

90

89

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89 90

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95 96

93 91

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94 81

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70 7

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97 103 91 84

102 102

97 103 91

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109 113 125 100 104 87 105

126 100 104 87 105

111 101

103 112

109 113

103 112

103 82 98

111 101 103 82 98 102 102 90 88

OR	Y B	ACI	K-T	O-8	AC	KT	EST	(SH	EET	3)										
																					PU
28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	FLOW TOTAL ROL
	•								,	-								•			
69	63	72	75	58	57	84	74	84	78	101	75	77	70	77	75	79	76	77	73	41	22.4
76	75	74	75	76	71	69	87	76	90	95	98	88	75	69	76	76	80	87	72		23.7
67	61	69	73	57	56	81	72	81	76	97	73	74	6 7	75	74	76	73	76	72	41	23.1
76	74	74	70	64	63	85	86	76	88	90	98	87	74	69	75	76	79	85	85		23.8
65	60	67	70	56	54	78	69	79	75	96	7ů	72	64	74	72	73	70	71	70	41	22.5
74	74	74	69	64	63	84	72	87	90	92	86	74	68	74	75	78	85	85	71		23.4
65	59	67	70	56	54	78	69	79	75	96	70	72	64	73	72	73	70	71	69	41	22.5
74	74	74	71	66	63	84	73	88	91	98	85	74	74	76	76	79	85	84	71		23.7
68	61	70	73	57	56	80	70	81	75	97	71	73	65	74	72	75	71	74	71	41	22.5
76	74	74	77	68	69	79	74	88	94	85	84	66	77	77	81	86	85	71	71		23.4
68	61	70	74	57	55	81	70	81	74	96	71	72	65	73	72	75	71	72	70	39	22.5
78	76	77	77	69	71	85	74	88	93	97	87	73	68	76	76	79	87	85	70		23.4
68	61	70	74	57	55	81	71	82	75	97	72	74	64	75	73	75	72	73	71	39	22.5
79	76	77	78	70	71	86	76	90	95	98	88	77	68	77	77	79	88	86	71		23.4
68	61	70	74	57	55	81	71	82	75	97	72	73	64	75	73	75	72	73	71	39	22.5
79	76	77	78	70	71	86	76	90	95	98	88	77	68	77	77	79	88	86	71		23.4
54 74	49 68	55 71	58 71	45 66	44 68	66 79	57 68	66 79	65 79	80 91	58 82	60 63	47 68	63 63	61 66	53 74	58 79	60 74	58 63	32	21.6

3)																
											PUMI			NIFO		DUA	YMY
. 44			7.4	4.0		11				115	FLOW			RESS		PRI	ESS
38_	39	40	41	42	43	44	45	46	47	48	TOTAL ROLLE	RIPRESS	MAIN	L/H	R/H	L/H	R/H
.01 95	75 98	77 88	70 75	77 69	75 76	79 76	76 80	77 87	73 72	41	22.4 23.7	71 67	44 48	41 42	38 40	22	21
97 90	73 98	74 87	6 7 74	75 69	74 75	76 76	73 79	76 85	72 85	41	23.1 23.8	74 67	42 48	43 42	39 40	23	22
96 92	70 86	72 74	64 68	74 74	72 75	73 78	70 85	71 85	70 71	41	22.5 23.4	73 67	44 48	42 42	38 41	22	21
96 98	70 85	72 74	64 74	73 76	72 76	73 79	70 85	71 84	69 71	41	22.5 23.7	73 67	44 48	42 42	38 41	22	21
97 85	71 84	73 66	65 77	74 77	72 81	75 86	71 85	74 71	71 71	41	22.5 23.4	72 67	42 48	43 42	38 40	21	30
96 97	71 87	72 73	65 68	73 76	72 76	75 79	71 87	72 85	70 70	39	22.5 23.4	72 67	42 48	42 42	38 40	21	23
97 98	72 88	74 77	64 68	75 77	73 77	75 79	7 2 88	73 86	71 71	39	22.5 23.4	72 67	42 48	42 42	38 40	21	23
97 98	72 88	73 77	64 68	75 77	73 77	75 79	72 88	73 86	71 71	39	22.5 23.4	72 67	42 48	42 42	38 40	21	23
30	58 82	60 63	47 68	63 63	61 66	53 74	58 79	60 74	58 63	32	21.6	79	46	44	40	21	23



														1	A
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	
8/23/71	02:45	12:15	2200	250	DUMMY TEST	68 91	95 92			100 107	_	100 105	109 99	114 107	
8/23	03:15	12:45	2200	250	DUMMY TEST	69 95	95 96 top cl	111	110	107 109	103	107		117 111 at 03	1
8/23	04:05	13:15	2200	250	DUMMY TEST	68 94	100 100	117	120	105 110	105	104	113 102		14
8/23	04:35	13:45	2200	250	DUMMY TEST	68 94	101 101	•		106 110	-	105 107	113 102	116 112	
8/23	05:05	14:15	2700	250	DUMMY TEST	70 96	96 98			106 111		105 108	113 104	116 113	
8/23	05:35	14:45	2700	250	DUMMY TEST	70 95	96 102			105 112	105 106	104 109		116 113	
8/23	06:28	14:58	2700	250		St	art or or or	eck f	aci]	lity					
8/23	08:25	15:28	2700	250	DUMMY TEST	70 83	96 101		118 113		103 104	108	102	114 111	11
8/23	10:00	15:58	3240	425	DUMMY TEST	5t 70 96	95 102	116	119	104 113	105	103	on po 112 105	_	12
8/23	10:30	16:28	3240	425	DUMMY TEST	71 97	96 99			105 113			112 105	115 115	
8/23	11:00	16:58	3240	425	DUMMY TEST	73 98	97 99			107 113				118 115	



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA:L

TEMPERATU

											_											122	
3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	2
	118 109	100 107				114 107	125 107		104 99				94 99	91 87	83 85	90 86		85 85	90 82	89 87	89 85	88 93	+
111	110	109	103	107	101	117 111	110									98 87		93 86	95 83		94 85	94 94	1
						at 03															- 1		
	120 112					116 110							99 101		89 87	97 87	93 86	91 85	94 84	94 89	94 87	92 95	~ ~
	121 112					116 112							102 101		89 88	98 88	93 87	91 86		-	94 87	92 96	- 0.
						116 113									89 89		95 89		95 87		97 91	94 96	
	120 113					116 113							107 103			-	95 90	93 89	95 87		96 91	93 96	₩ ••
ı pow		t 06:	:15																				
ı pow	er a	t 07:	:55																				
_	118 113		103 104	108	102		110	101					104 101		86 87	96 87	93 87	90 86		93 89	94 87	91 94	2
ncres	ıse t	tail]	load	C	on po	wer a	et 09	: 30															
116 114	119 114	104 113	105 107	103 110	112 105	113 113	127 113	103 103	107 105	84 84	107 100	89 105	102 105	92 92	87 90	96 90	95 94		94 88	96 94	96 93	94 99	& ()
116 114	119 114	105 113	105 107	103 111	112 105	115 115	128 113	103 104	107 105	90 84	107 100	94 105	106 105		87 91				93 88		94 90	93 99	& 0,
	121 114	107 113	107 108	105 111	114 106	118 115	131 113	106 104	109 105	93 84	110 100	101 105	108 105	96 92	89 91	99 92	97 94	95 90	96 89		99 93	95 99	5

ISSION TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 4)

TEMPERATURE (°C)

						•																	
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	_4
89 84	85 85	90 82	89 87	89 85	88 93	83 88	78 79	67 74	57 7 2	70 72	73 74	54 66	53 67	83 77	70 71	82 79	69 91	94 93	68 84	66 71	78 72		6
94 85	93 86	95 83	95 88	94 85	94 94	85 89	79 81	68 76	60 74	72 67	76 66	55 67	54 70	84 85	73 74	84 88	74 88	99 96	72 86	75 74	71 68	76 74	7
93 86	91 85			94 87	92 95	84 89	78 79	67 77	60 74	71 74	75 75	55 68	53 69	83 84	72 74	83 88	74 93	98 96	71 85	74 74	70 68	76 74	7
93 87	91 86			94 87	92 96	84 90	78 81	67 77	60 74	71 74	75 76	59 68	53 70	83 85	72 76	83 89	74 93	98 96	71 87	74 74	70 74	75 75	7
95 89	93 88	95 87	96 92	97 91	94 96	85 91	77 81	67 76	60 74	71 74	74 76	55 68	53 69	83 85	77 76	83 89	74 93	99 97	71 87	73 74	69 74	75 74	•
95 90	93 89	95 87	96 92	96 91	93 96	84 92	77 81	67 77	59 74	70 74	73 76	54 68	53 69	82 85	71 76	82 89	74 93	99 98	71 87	73 74	69 74	74 75	,
93 87	90 86			94 87	91 94	81 89	77 79	77 72	69 71	75 71	76 69	74 60	70 58			83 85	85 90	98 95	79 85	79 76	67 67	81 77	
95 94	92 90	94 88	96 94	96 93	94 99	84 93	77 84	69 80	61 79	73 79	76 80	57 73	55 74	83 88	72 77	84 89	75 93	99 99	72 90	73 74	68 70	75 76	
94 94	90 90	93 88	94 94	94 90	93 99	84 93	78 85	70 81	62 7 9	73 80	77 80	57 74	55 74	84 88	72 79	84 91	71 96	98 99	72 90	74 78	68 70	76 78	
97 94				99 93	95 99	88 93	79 85	71 80	63 79	75 80	78 80	59 74	57 74	85 88	73 79	86 91	77 96	101 99	73 91	75 78	70 69	76 79	
	89 84 94 95 98 97 99 99 99 97	89 85 84 85 94 93 85 86 93 91 87 86 93 93 89 88 95 93 89 89 95 93 97 95	89 85 90 84 85 82 94 93 95 85 86 83 93 91 94 86 85 84 95 93 95 89 88 87 95 93 95 90 89 87 95 93 95 90 89 87 95 92 94 94 90 88 94 90 88	89 85 90 89 84 85 82 87 94 93 95 95 85 86 83 88 93 91 94 94 87 86 84 89 95 93 95 96 90 89 87 92 95 93 95 96 90 89 87 92 93 87 92 94 90 88 94 94 90 88 94 97 95 96 99	89 85 90 89 89 84 85 82 87 85 94 93 95 95 94 85 86 83 88 85 93 91 94 94 94 94 87 86 84 89 87 95 93 95 96 97 90 89 87 92 91 95 96 99 99 97 95 96 99 99	89 85 90 89 89 88 94 93 95 95 94 94 93 91 94 94 94 92 93 91 94 94 94 92 93 91 94 94 94 92 95 93 95 96 97 96 95 93 95 96 97 96 95 93 95 96 91 96 95 93 95 96 91 96 95 93 95 96 91 96 93 89 87 92 91 96 93 89 87 92 91 96 93 90 89 87 92 91 96 93 90 88 94 93 99 94 90 88 94 93 99 94 90 88 94 90 99	89 85 90 89 89 88 83 94 93 95 95 94 94 89 85 86 83 88 85 94 89 93 91 94 94 92 84 86 85 84 89 87 95 89 93 91 94 94 92 84 87 86 84 89 87 96 90 95 93 95 96 97 94 85 90 89 87 92 91 96 91 95 93 95 96 96 93 84 90 89 87 92 91 96 92 93 90 92 93 94 91 89 87 86 84 89 87 94 89 95 92 94 93 94 93 99 93 94<	89 85 90 89 89 88 83 78 94 93 95 95 94 94 85 79 85 86 83 88 85 94 89 81 93 91 94 94 94 92 84 78 86 85 84 89 87 95 89 79 93 91 94 94 94 92 84 78 87 86 84 89 87 96 90 81 95 93 95 96 97 94 85 77 89 88 87 92 91 96 91 81 95 93 95 96 96 93 84 77 90 89 87 92 91 96 92 81 93 90 92 93 94 91 81 77 94 90 88 94 <th>89 85 90 89 89 88 83 78 67 94 93 95 95 94 94 85 79 68 85 86 83 88 85 94 89 81 76 93 91 94 94 94 92 84 78 67 86 85 84 89 87 95 89 79 77 93 91 94 94 94 92 84 78 67 87 86 84 89 87 96 90 81 77 95 93 95 96 97 94 85 77 67 89 88 87 92 91 96 91 81 76 95 93 95 96 96 93 84 77 67 95 93 94 94 94 94 89 79 72 95 92<th>89 85 90 89 89 88 83 78 67 57 94 93 95 95 94 94 85 79 68 60 93 91 94 94 94 89 81 76 74 93 91 94 94 94 92 84 78 67 60 86 85 84 89 87 95 89 79 77 74 93 91 94 94 94 92 84 78 67 60 87 86 84 89 87 96 90 81 77 74 95 93 95 96 97 94 85 77 67 60 60 78 81 76 74 74 95 93 95 96 97 94 85 77 67 67 69 81 77 76 74 74 74 74 74</th><th>89 85 90 89 89 89 88 83 78 67 57 70 94 93 95 95 94 94 85 79 68 60 72 93 91 94 94 94 89 81 76 74 67 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 96 93 84 77</th><th>89 85 90 89 89 88 83 78 67 57 70 73 74 94 93 95 95 94 94 85 79 68 60 72 76 85 86 83 88 85 94 89 81 76 74 67 66 93 91 94 94 92 84 78 67 60 71 75 86 85 84 89 87 95 89 79 77 74 74 75 93 91 94 94 92 84 78 67 60 71 75 87 86 84 89 87 96 90 81 77 74 74 74 76 95 93 95 96 97 94 85 77 67 60 71 74 74 76 95 93 95 96 96 93</th><th>89 85 90 89 89 89 88 83 78 67 57 70 73 54 66 94 93 95 95 94 94 85 79 68 60 72 76 55 85 86 83 88 85 94 89 81 76 74 67 66 67 93 91 94 94 92 84 78 67 60 71 75 55 86 85 84 89 87 95 89 79 77 74 74 75 68 93 91 94 94 94 92 84 78 67 60 71 75 55 87 86 84 89 87 96 90 81 77 74 74 74 76 68 95 93 95 96 97 94 85 77 67 60 71 74</th><th>89 85 90 89 89 89 88 83 78 67 57 70 73 54 53 94 93 95 95 94 94 85 79 68 60 72 76 55 54 93 91 94 94 92 84 78 67 60 71 75 55 53 86 85 84 89 87 95 89 77 77 74 74 75 66 67 70 93 91 94 94 94 92 84 78 67 60 71 75 55 53 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 93 91 94 94 92 84 78 67 60 71 74 74 76 68 70 95 93 95 96</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 93 91 94 94 92 84 78 67 60 71 75 55 53 83 86 85 84 89 87 95 89 79 77 74 74 75 68 69 84 93 91 94 94 92 84 78 67 60 71 75 55 53 83 87 86 84 89 87 96 90 81 77 74 74 74 74 76 68 70 85</th><th>89 85 90 89 88 83 78 67 57 70 73 54 53 83 70 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 86 85 84 89 87 95 89 79 77 74 74 75 66 67 70 85 74 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 87 86 84 89 87 96 90 81 77 67 60 71</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 85 84 89 87 95 89 79 77 74 74 75 55 53 83 72 83 87 86 84 89 87 95 90 81 77 74 74 74 76 68 69 85 76 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 89 89 89 89 89 89 89 89 89 89</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 76 66 67 70 85 74 88 88 88 85 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 96 90 81 77 74 74 76 68 70 85 76 89 93 85 86 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 92 81 77 74 74 76 68 69 85 76 89 93 85 76 89 93 85 76 89 93 85 76 89 85 76 89 93 85 76 85 76 89 93 85 76 85 76 89 93 85 86 86 86 86 86 86 86 86 86 86 86 86 86</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 94 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 84 74 99 85 86 83 88 85 94 89 81 76 74 66 67 70 85 74 88 88 96 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 87 86 84 89</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 85 84 89 87 95 89 89 79 77 74 74 75 55 53 83 72 83 74 98 71 87 86 84 89 87 96 90 81 77 74 74 75 68 69 85 76 89 93 96 87 95 86 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 86 84 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 98 87 99 99 99 99 99 99 99 99 99 99 99 99 99</th><th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 66 74 72 72 73 74 66 67 77 71 71 79 91 93 84 71 74 75 68 69 84 74 88 73 84 74 88 74 98 71 74 74 75 68 69 84 74 88 74 88 74 98 71 74 74 75 68 69 85 76 89 93 96 87 74 88 87 79 87 74 88 87 86 84 89 87 92 91 96 91 81 77 74 74 74 76 68 69 85 76 89 93 96 87 74 88 87 87 87 88 88 89 87 92 91 96 88 87 92 81 77 74 74 74 75 68 69 85 76 89 93 96 87 74 88 88 88 97 87 87 87 88 88 89 87 92 91 96 81 81 81 81 81 81 81 81 81 81 81 81 81</th><th>89 85 90 89 89 88 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 71 72 94 93 95 95 94 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 74 68 93 91 94 94 94 92 84 78 67 60 71 75 75 66 69 84 74 88 93 96 85 74 68 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 71 74 76 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 84 74 88 93 96 85 74 74 95 93 95 96 97 91 96 91 81 76 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 81 77 74 74 74 75 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 96 91 81 76 74 74 75 76 88 69 85 76 89 93 96 87 74 74 95 93 95 96 97 92 91 96 97 97 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 99 99 95 88 79 71 63 75 76 76 74 70 82 76 83 85 98 97 97 74 74 96 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 99 90 78 70 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 75</th><th>89 85 80 89 88 88 83 78 67 97 71 72 72 73 54 53 83 70 82 69 94 68 66 78 70 72 76 94 93 95 86 83 88 83 78 67 79 77 74 74 75 68 69 84 74 88 78 96 87 74 74 75 95 93 95 96 89 99 99 95 88 79 71 77 69 75 76 76 75 76 76 76 78 82 76 83 74 98 77 74 74 75 96 79 99 88 94 99 99 95 88 79 97 87 77 78 78 79 78 79 79 78 79 79 78 79 79 79 79 79 79 79 79 79 79 79 79 79</th></th>	89 85 90 89 89 88 83 78 67 94 93 95 95 94 94 85 79 68 85 86 83 88 85 94 89 81 76 93 91 94 94 94 92 84 78 67 86 85 84 89 87 95 89 79 77 93 91 94 94 94 92 84 78 67 87 86 84 89 87 96 90 81 77 95 93 95 96 97 94 85 77 67 89 88 87 92 91 96 91 81 76 95 93 95 96 96 93 84 77 67 95 93 94 94 94 94 89 79 72 95 92 <th>89 85 90 89 89 88 83 78 67 57 94 93 95 95 94 94 85 79 68 60 93 91 94 94 94 89 81 76 74 93 91 94 94 94 92 84 78 67 60 86 85 84 89 87 95 89 79 77 74 93 91 94 94 94 92 84 78 67 60 87 86 84 89 87 96 90 81 77 74 95 93 95 96 97 94 85 77 67 60 60 78 81 76 74 74 95 93 95 96 97 94 85 77 67 67 69 81 77 76 74 74 74 74 74</th> <th>89 85 90 89 89 89 88 83 78 67 57 70 94 93 95 95 94 94 85 79 68 60 72 93 91 94 94 94 89 81 76 74 67 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 96 93 84 77</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 74 94 93 95 95 94 94 85 79 68 60 72 76 85 86 83 88 85 94 89 81 76 74 67 66 93 91 94 94 92 84 78 67 60 71 75 86 85 84 89 87 95 89 79 77 74 74 75 93 91 94 94 92 84 78 67 60 71 75 87 86 84 89 87 96 90 81 77 74 74 74 76 95 93 95 96 97 94 85 77 67 60 71 74 74 76 95 93 95 96 96 93</th> <th>89 85 90 89 89 89 88 83 78 67 57 70 73 54 66 94 93 95 95 94 94 85 79 68 60 72 76 55 85 86 83 88 85 94 89 81 76 74 67 66 67 93 91 94 94 92 84 78 67 60 71 75 55 86 85 84 89 87 95 89 79 77 74 74 75 68 93 91 94 94 94 92 84 78 67 60 71 75 55 87 86 84 89 87 96 90 81 77 74 74 74 76 68 95 93 95 96 97 94 85 77 67 60 71 74</th> <th>89 85 90 89 89 89 88 83 78 67 57 70 73 54 53 94 93 95 95 94 94 85 79 68 60 72 76 55 54 93 91 94 94 92 84 78 67 60 71 75 55 53 86 85 84 89 87 95 89 77 77 74 74 75 66 67 70 93 91 94 94 94 92 84 78 67 60 71 75 55 53 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 93 91 94 94 92 84 78 67 60 71 74 74 76 68 70 95 93 95 96</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 93 91 94 94 92 84 78 67 60 71 75 55 53 83 86 85 84 89 87 95 89 79 77 74 74 75 68 69 84 93 91 94 94 92 84 78 67 60 71 75 55 53 83 87 86 84 89 87 96 90 81 77 74 74 74 74 76 68 70 85</th> <th>89 85 90 89 88 83 78 67 57 70 73 54 53 83 70 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 86 85 84 89 87 95 89 79 77 74 74 75 66 67 70 85 74 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 87 86 84 89 87 96 90 81 77 67 60 71</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 85 84 89 87 95 89 79 77 74 74 75 55 53 83 72 83 87 86 84 89 87 95 90 81 77 74 74 74 76 68 69 85 76 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 89 89 89 89 89 89 89 89 89 89</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 76 66 67 70 85 74 88 88 88 85 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 96 90 81 77 74 74 76 68 70 85 76 89 93 85 86 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 92 81 77 74 74 76 68 69 85 76 89 93 85 76 89 93 85 76 89 93 85 76 89 85 76 89 93 85 76 85 76 89 93 85 76 85 76 89 93 85 86 86 86 86 86 86 86 86 86 86 86 86 86</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 94 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 84 74 99 85 86 83 88 85 94 89 81 76 74 66 67 70 85 74 88 88 96 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 87 86 84 89</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 85 84 89 87 95 89 89 79 77 74 74 75 55 53 83 72 83 74 98 71 87 86 84 89 87 96 90 81 77 74 74 75 68 69 85 76 89 93 96 87 95 86 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 86 84 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 98 87 99 99 99 99 99 99 99 99 99 99 99 99 99</th> <th>89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 66 74 72 72 73 74 66 67 77 71 71 79 91 93 84 71 74 75 68 69 84 74 88 73 84 74 88 74 98 71 74 74 75 68 69 84 74 88 74 88 74 98 71 74 74 75 68 69 85 76 89 93 96 87 74 88 87 79 87 74 88 87 86 84 89 87 92 91 96 91 81 77 74 74 74 76 68 69 85 76 89 93 96 87 74 88 87 87 87 88 88 89 87 92 91 96 88 87 92 81 77 74 74 74 75 68 69 85 76 89 93 96 87 74 88 88 88 97 87 87 87 88 88 89 87 92 91 96 81 81 81 81 81 81 81 81 81 81 81 81 81</th> <th>89 85 90 89 89 88 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 71 72 94 93 95 95 94 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 74 68 93 91 94 94 94 92 84 78 67 60 71 75 75 66 69 84 74 88 93 96 85 74 68 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 71 74 76 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 84 74 88 93 96 85 74 74 95 93 95 96 97 91 96 91 81 76 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 81 77 74 74 74 75 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 96 91 81 76 74 74 75 76 88 69 85 76 89 93 96 87 74 74 95 93 95 96 97 92 91 96 97 97 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 99 99 95 88 79 71 63 75 76 76 74 70 82 76 83 85 98 97 97 74 74 96 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 99 90 78 70 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 75</th> <th>89 85 80 89 88 88 83 78 67 97 71 72 72 73 54 53 83 70 82 69 94 68 66 78 70 72 76 94 93 95 86 83 88 83 78 67 79 77 74 74 75 68 69 84 74 88 78 96 87 74 74 75 95 93 95 96 89 99 99 95 88 79 71 77 69 75 76 76 75 76 76 76 78 82 76 83 74 98 77 74 74 75 96 79 99 88 94 99 99 95 88 79 97 87 77 78 78 79 78 79 79 78 79 79 78 79 79 79 79 79 79 79 79 79 79 79 79 79</th>	89 85 90 89 89 88 83 78 67 57 94 93 95 95 94 94 85 79 68 60 93 91 94 94 94 89 81 76 74 93 91 94 94 94 92 84 78 67 60 86 85 84 89 87 95 89 79 77 74 93 91 94 94 94 92 84 78 67 60 87 86 84 89 87 96 90 81 77 74 95 93 95 96 97 94 85 77 67 60 60 78 81 76 74 74 95 93 95 96 97 94 85 77 67 67 69 81 77 76 74 74 74 74 74	89 85 90 89 89 89 88 83 78 67 57 70 94 93 95 95 94 94 85 79 68 60 72 93 91 94 94 94 89 81 76 74 67 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 93 91 94 94 92 84 78 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 97 94 85 77 67 60 71 95 93 95 96 96 93 84 77	89 85 90 89 89 88 83 78 67 57 70 73 74 94 93 95 95 94 94 85 79 68 60 72 76 85 86 83 88 85 94 89 81 76 74 67 66 93 91 94 94 92 84 78 67 60 71 75 86 85 84 89 87 95 89 79 77 74 74 75 93 91 94 94 92 84 78 67 60 71 75 87 86 84 89 87 96 90 81 77 74 74 74 76 95 93 95 96 97 94 85 77 67 60 71 74 74 76 95 93 95 96 96 93	89 85 90 89 89 89 88 83 78 67 57 70 73 54 66 94 93 95 95 94 94 85 79 68 60 72 76 55 85 86 83 88 85 94 89 81 76 74 67 66 67 93 91 94 94 92 84 78 67 60 71 75 55 86 85 84 89 87 95 89 79 77 74 74 75 68 93 91 94 94 94 92 84 78 67 60 71 75 55 87 86 84 89 87 96 90 81 77 74 74 74 76 68 95 93 95 96 97 94 85 77 67 60 71 74	89 85 90 89 89 89 88 83 78 67 57 70 73 54 53 94 93 95 95 94 94 85 79 68 60 72 76 55 54 93 91 94 94 92 84 78 67 60 71 75 55 53 86 85 84 89 87 95 89 77 77 74 74 75 66 67 70 93 91 94 94 94 92 84 78 67 60 71 75 55 53 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 93 91 94 94 92 84 78 67 60 71 74 74 76 68 70 95 93 95 96	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 93 91 94 94 92 84 78 67 60 71 75 55 53 83 86 85 84 89 87 95 89 79 77 74 74 75 68 69 84 93 91 94 94 92 84 78 67 60 71 75 55 53 83 87 86 84 89 87 96 90 81 77 74 74 74 74 76 68 70 85	89 85 90 89 88 83 78 67 57 70 73 54 53 83 70 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 54 84 73 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 86 85 84 89 87 95 89 79 77 74 74 75 66 67 70 85 74 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 87 86 84 89 87 96 90 81 77 67 60 71	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 85 86 85 84 89 87 95 89 79 77 74 74 75 55 53 83 72 83 87 86 84 89 87 95 90 81 77 74 74 74 76 68 69 85 76 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 81 76 74 74 74 76 68 69 85 76 89 89 89 89 89 89 89 89 89 89 89 89 89	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 88 88 85 82 87 85 93 88 79 74 76 66 67 70 85 74 88 88 88 85 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 95 89 79 77 74 74 75 68 69 84 74 88 93 93 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 88 98 87 86 84 89 87 96 90 81 77 74 74 76 68 70 85 76 89 93 85 86 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 91 81 76 74 74 76 68 69 85 76 89 93 85 76 89 83 87 92 91 96 92 81 77 74 74 76 68 69 85 76 89 93 85 76 89 93 85 76 89 93 85 76 89 85 76 89 93 85 76 85 76 89 93 85 76 85 76 89 93 85 86 86 86 86 86 86 86 86 86 86 86 86 86	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 94 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 94 93 95 95 94 94 85 79 68 60 72 76 55 54 84 73 84 74 99 85 86 83 88 85 94 89 81 76 74 66 67 70 85 74 88 88 96 93 91 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 87 86 84 89	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 84 85 82 87 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 84 85 86 83 88 85 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 85 84 89 87 95 89 89 79 77 74 74 75 55 53 83 72 83 74 98 71 87 86 84 89 87 96 90 81 77 74 74 75 68 69 85 76 89 93 96 87 95 86 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 86 84 89 87 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 98 87 99 99 99 99 99 99 99 99 99 99 99 99 99	89 85 90 89 89 88 83 78 67 57 70 73 54 53 83 70 82 69 94 68 66 74 72 72 73 74 66 67 77 71 71 79 91 93 84 71 74 75 68 69 84 74 88 73 84 74 88 74 98 71 74 74 75 68 69 84 74 88 74 88 74 98 71 74 74 75 68 69 85 76 89 93 96 87 74 88 87 79 87 74 88 87 86 84 89 87 92 91 96 91 81 77 74 74 74 76 68 69 85 76 89 93 96 87 74 88 87 87 87 88 88 89 87 92 91 96 88 87 92 81 77 74 74 74 75 68 69 85 76 89 93 96 87 74 88 88 88 97 87 87 87 88 88 89 87 92 91 96 81 81 81 81 81 81 81 81 81 81 81 81 81	89 85 90 89 89 88 85 93 88 79 74 72 72 74 66 67 77 71 79 91 93 84 71 72 94 93 95 95 94 94 89 81 76 74 67 66 67 70 85 74 88 88 96 86 74 68 93 91 94 94 94 92 84 78 67 60 71 75 75 66 69 84 74 88 93 96 85 74 68 93 91 94 94 94 92 84 78 67 60 71 75 55 53 83 72 83 74 98 71 74 76 87 86 84 89 87 96 90 81 77 74 74 74 75 68 69 84 74 88 93 96 85 74 74 95 93 95 96 97 91 96 91 81 76 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 92 81 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 81 77 74 74 74 75 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 92 91 96 96 91 81 76 74 74 75 76 88 69 85 76 89 93 96 87 74 74 95 93 95 96 97 92 91 96 97 97 77 74 74 74 76 68 69 85 76 89 93 97 87 74 74 95 93 95 96 97 99 99 95 88 79 71 63 75 76 76 74 70 82 76 83 85 98 97 97 74 74 96 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 99 90 78 70 97 95 96 99 99 95 88 79 71 63 75 78 59 57 85 73 86 77 101 73 75 75	89 85 80 89 88 88 83 78 67 97 71 72 72 73 54 53 83 70 82 69 94 68 66 78 70 72 76 94 93 95 86 83 88 83 78 67 79 77 74 74 75 68 69 84 74 88 78 96 87 74 74 75 95 93 95 96 89 99 99 95 88 79 71 77 69 75 76 76 75 76 76 76 78 82 76 83 74 98 77 74 74 75 96 79 99 88 94 99 99 95 88 79 97 87 77 78 78 79 78 79 79 78 79 79 78 79 79 79 79 79 79 79 79 79 79 79 79 79

r (Sh	EET	4)															
												PUMP			NIFOL	D		YMM
												FLOW			RESS		PR	PUT ESS
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL ROLLER	PRESS	MAIN	L/H R	/H	L/H	R/H
69	94 93	68 84	66 71	78 72	70 76	69 71	81 76	71 82	68 79	68 66	33	23.6 23.6	76 66	45 48	43 41	39 40	23	21
74 88	99 96	72 86	75 74	71 68	76 74	74 74	79 78	74 85	73 83	72 68	34	23.4 23.7	73 66	44 47	42 41	40 40	23	21.5
74 93	98 96	71 85	74 74	70 68	76 74	74 74	78 78	72 85	73 82	72 68	35	23.4 23.7	75 66	45 48	43.5 41.5		23.5	22
74 93	98 96	71 87	74 74	70 74	75 75	74 76	78 79	72 87	73 85	7 2 70	34	23.1 23.7	73 66	44 47	42.5 42	39 40	23	21.5
74 93	99 97	71 87	73 74	69 74	75 74	73 75	78 79	71 85	73 84	71 70	35	22.8 23.7	73 66	44 47	42 41.5	39 40	23	21.5
74 93	99 98	71 87	73 74	69 74	74 75	73 76	77 79	71 85	73 85	71 74	35	22.8 23.7	74 66	44 48	42.5 42	39 40	23	21.5
85 90	98 95	79 85	79 76	67 67	81 77	79 77	77 77	77 84	80 81	79 69	32	23.1 23.4	75 67	45 47	43 43	40 40	24	22
75 93	99 99	72 90	73 74	68 70	75 76	73 76	78 80	73 88	73 84	72 69	36	22.8 23.7	74 67	45 47	43 41.5		23	21.5
71 96	98 99	7 2 90	74 78	68 70	76 78	74 78	78 80	73 89	74 87	73 72	37	22.8 23.7	73 67	44 47	42.5 41.5		23	22
77 96	101 99	73 91	75 78	70 69	76 79	75 79	80 81	74 89	75 137	74 72	37	22.8 23.7	73 67	44 47	42.5 41.5		23	22



				•			_		-						_
DATE	OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	H.P.		1	2	3	4	5	6	7	8	9	
8/23/71	11:30	17:28	3240	425	DUMMY TEST	73 98	97 99			107 113		105 111		118 115	
			,			St	top f	acili	ty p	roble	em				
9/7	11:05	17:58	2200	250				on po heck							
9/7	12:10	18:28	2200	250		S1	tart	on po nspec	wer t st	at 11	:40 :rs				
9/9	14:55	18:58	2400	250	D UMMY TEST		104		115	93 110	112	96 107		108 112	
9/9	15:25	19:28	2400	250	DUMMY TEST	_	107 98			97 110		99 107		111 113	
9/9	16:20	19:58	2700	250	DUMMY TEST	96	109 99		120	ue sp 98 111	117			r at 113 113	12
9/9	16:50	20:28	2700	250	DUMMY TEST		109 100	115 116		98 111		102 108			
9/9	17:40	20:58	1950	250	DUMMY TEST	95	109 98		118	ue sp 96 109	115	99 106		wer 111 111	
9 /9	18:10	21:28	1950	250	DUMMY TEST		109 98			96 109	_	99 106		111 112	
9/9	18:40	21:58	3000	250	DUMMY TEST		108 100			98 111		101 108		113 114	



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LAB

TEMPERATURE (°C)

ì	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
	-								_														
7		105 111			131 113		109 105		110 100		108 105	96 92	89 91	99 92	97 94	95 90	96 89	99 94	99 93	95 99	88 93	79 85	71 80
le	m																						
	: 35																						
-	1it :40																						
ne	rs																						
14	:25																						
	112		105			-	100	88		92	98	87	80		82	80	84	82	80	79	85	72	61
0	105	107	103	112	110	101	102	82	99	99	101	89	87	87	83	Øδ	92	92	85	55	83	82	7'
7	115	99	108	111	123	100	103	92	94	96	102	81	84	91	87	85	89	87	84	82	88	75	61
	105				_		102	82		99	101	89	88		83		92	93	85	55	84	82	71
_	lit		_		15:5									. •		•			0 -				
.1		101 117			124 111	101 102	105 102			98 100	103 102	92 90	85 88		90 85	89 87	91 94	90 94	89 90	84 57	91 85	76 82	6' 7
							57-						-		-	·				•			
	118					102				99	104	93	86	95	91	88	92 0):	91	89	84	91 85	76	6'
.1		108				102	T03	94	99	101	102	91	89	89	85	89	94	94	89	57	85	83	7
-	lit		_		at 1		100	01	O).	95	101	90	83	۵ı	85	82	87	26	82	79	86	74	6
16	115 104					100	103 101		96	97	101			86	81	84	90	90	93	55	83	81	7
																	•				<u> </u>		
)6)9	115				123 111		103 101	92 82	95 97	95 98	102 100		83 86		85 81				83 93			74 82	6 7
													85		91				•		90	75	į
)8 L1		101			112	101 101	103	93 83	98	98 100	103 101				85			90 94	89		87	82	7



DATA: LABORATORY BACK-TO-BACK TEST (SHEET 5)

ATURE (°C)

80 86 74

57 87 82

82

75

54 83

83 90

65 60

74 74

76 76

66

60

5	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
5	88 93	79 85	71 80	63 79	75 80	78 80	59 74	57 74	85 80	73 79	86 91	77 96	101 99	73 91	75 78	70 69	76 79	75 79	80 81	74 89	75 87	74 72	37
'9	85	72	64	58	67	69	65	62	77	67	77	75	90	68	71	62	68	68	63	69	68	70	38
i5	83	82	77	77	74	76	71	71	91	77	85	89	96	88	71	75	74	74	78	85	81	67	
))2 ;5	88 84	75 82	66 76	61 76	69 74	72 75	57 71	54 70	80 85	71 77	80 89	78 95	94 95	72 88	76 77	65	73 80	72 79	67 80	72 86	72 85	74 71	40
34	91	76	67	62	71	73	58	55	82	72	82	80	96	73	76	66	75	73	68	73	74	75	42
57	85	82	76	76	64	76	71	71	87	78	90	95	97	88	77	70	80	80	81	88	87	72	
34	91	76	67	62	71	73	58	54	82	73	82	79	97	73	76	66	75	73	68	73	74	75	41
57	85	83	77	77	64	76	72	70	88	79	91	96	98	90	78	70	82	81	81	88	87	71	
79	86	74	65	6c	68	71	56	53	79	70	79	78	93	71	72	63	72	71	66	70	71	73	40
55	83	81	74	74	71	73	71	69	85	77	89	94	95	87	77	68	79	78	78	86	84	70	

93 71 95 88

71

98 89

96

72 63 72

77 68 79

73 65 73

77 70 82

71 66 70 71

72 67

79 79 87 86

80 81 88 86

71

72

73 40

39

71

74

71

79 70 79 78

80 71 80

87 78 90 95

87 79 90 95

78

68 71 56 53 71 74 71 69

69 72 56 53 72 74 71 70

HE	ET	5 1					•				·					
					_			-		PUMP		M	NIFO	LD		MMY
										FLOW			PRESS			PUT
39	40	41	42	43	44	45	46	47	48	TOTAL ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
73 91	75 78	70 69	76 79	75 79	80 81	74 89	75 87	74 72	37	22.8 23.7	73 67	44 43	42.5 41.5	39 39	23	22
68 88	71 71	62 75	68 74	68 74	63 78	69 85	68 81	70 67	38	23.1 22.5	78 64	47 44	44.5 36.5		24	21.5
72 88	76 77	65 69	73 80	72 79	67 80	72 86	72 85	74 71	40	23.1 22.8	76 64	46 44	44.5 36.5		24	21.5
73 88	76 77	66 70	75 80	73 80	68 81	73 88	74 87	75 72	42	22.8 22.5	76 64	45 44	43.5 37	40 35	23	21
73 90	76 78	66 70	75 82	73 81	68 81	73 88	74 87	75 71	41	22.8 22.5	75 64	45 44	43.5 37	40 35	23	21
71 87	72 77	63 68	72 79	71 78	66 78	70 86	71 84	73 70	40	22.8 22.5	77 64	46 44	44 37	40 35	23.5	5 21
71 88	7 2 7 7	63 68	72 79	71 79	66 79	70 87	71 86	73 71	40	22.8 22.5	76 64	46 44	44 37	40 35	23.5	5 21
71 89	73 77	65 70	73 82	72 80	67 81	71 88	72 86	74 71	39	22.8 22.5	76 64	46 45	43 37	40 35	23	21
					_			-								

V

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		,	2	3	4	5	6	7	8	9	1
9/9/71	18:50	22:08	3000	250		St	op c	heck	str						
9/9	19:35	22:28	3000	250	DUMMY TEST	94 96	107		118	97	19:15 116 106			113 110	
9/9	20:45	22:58	3000	250	DUMMY TEST	94 85	107		118	95	y on 115 104		108		14
9/9	21:15	23:28	3000	250	DUMMY TEST	95 96		114 115		97 110	-	100 107	-	113 114	12
9/9	21:45	23:58	1950	250	DUMMY TEST	95 85		114 115			116 104	100 106	-	112 111	12
9/9	22:15	24:28	1950	250	DUMMY TEST	95 85		115 114		97 108		101 106		113 111	12 11
9/9	22:45	24:58	3000	250	DUMMY TEST	94 86		114 116		97 111		101 108		113 114	12 11
9/9	23:15	25:28	3000	250	DUMMY TEST	86	99	115	119	110	116 106 split	108	104	114	11
9/9	24:00	25:58	3000	250	DUMMY TEST	94 85					116 104			111 110	12 11
9/10	00:30	26:28	3000	250	DUMMY Test	95 86 St		115	119	110	117 105 ners			113 113	12 11.
						50	OP I	nabe		OT CT	ner p				



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK-

TEMPERATURE (°C)

1	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33
											·	-										
5 102 9 10	2 105 + 100	-	96 97	98 98	104 100	93 86	85 85	95 85	92 83	86 86	92 91	90 91	90 86	83 54	91 85	75 80	66 74	60 74	70 71	72 72	55 70	52 68
	9 103 0 100	91 81		97 98	101 100	90 87	83 86	93 86	89 84			88 91	88 87	82 54	89 85	74 80	64 73	58 73	68 70	70 72	54 69	51 68
	104		95 97		103 100	92 89	84 87	94 88	91 85	87 88	91 95	88 94	89 89	83 54	90 87	75 82	65 74	58 74	68 71	71 73	54 70	52 68
	104		94 96	97 98	103 100	92 88	85 86	93 86	88 81		90 90	87 91		82 52	88 83	75 80	64 74	58 74	68 70	71 72	54 69	51 68
	105		95 96		103 100		86 86	93 86	88 81		90 91	87 92		83 52	89 83	76 81	65 74	58 74	69 71	72 72	54 70	51 68
5 101 2 101	105	93 83		98 101	103 102		85 89	95 89	92 87		91 96	86 97		83 53	91 88	74 82	64 75	57 7 5	68 71	71 74	53 71	50 68
	103	92 82		97 100	102 101		83 88	93 88	90 86			86 95			89 87	73 82	62 74	56 74	•	69 72	52 70	-
3 99	103	• 91 80	93 96	97 98	102 99	90 86	83 85	92 85	89 83			84 93	88 86	81 53	89 87	73 80	63 72	57 72	67 69	70 71	53 68	50 66
5 101 1 100		93 81	95 97	98 99	103 100	92 88	85 86	94 87	91 85		91 94		89 88	83 53	91 85	75 81	64 75	58 75	68 69	71 71	54 68	50 67



																-				
ORY	BA	CK.	·TO	-BA	\CK	TES	ST (S	SHE	ET	6)										
				_															PUMP	
2211																			.ow	100000000000000000000000000000000000000
31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS
) 72 . 72	55 70	52 68	81 85	71 77	81 87	77 91	96 95	71 92	73 73	65 68	72 7 9	72 78	66 78	71 85	72 82	74 68	37	22.8 22.5		75 64
} 70) 72	54 69	51 68	79 85	69 77	79 88	76 93	94 95	69 87	71 74	64 68	71 79	70 78	65 79	70 85	70 81	72 68	37	22.8 22.5		76 64
71 . 73	54 70	52 68	80 85	70 77	80 89	77 94	95 96	70 88	73 75	64 68	72 81	71 80	65 80	71 89	70 84	73 69	36	22.8 22.5		76 64
71 72	54 69	51 68	80 85	70 77	80 88	77 93	94 94	70 87	72 74	65 68	72 80	71 79	65 7 9	71 85	71 84	73 68	35	22.8 22.5		76 64
72 72	54 70	51 68	81 85	71 77	81 89	77 94	95 95	71 88	73 74	66 68	73 81	72 79	66 79	71 86	71 84	73 69	35	22.8 22.5		76 64
71 74	53 71	50 68	80 87	70 78	80 90	77 94	96 98	70 89	73 76	64 69	73 82	71 81	65 81	71 87	71 85	73 69	34	22.8 22.5		76 64
69 72	52 70	49 68	79 87	68 77	79 89	75 94	94 96	69 88	71 76	63 68	71 82	70 80	64 80	69 87	70 84	71 69	34	22.8 22.5		76 64
70 71	53 68	50 66	79 84	68 76	79 87	75 88	94 94	69 85	70 74	64 66	70 79	69 78	64 77	69 84	70 84	72 68	34	22.8 22.5		76. 64
71 71	54 68	50 67	80 85	70 77	80 88	76 93	95 95	70 88	73 74	65 67	72 79	71 78	65 78	70 85	71 82	73 67	34	22.8 22.5		76 63

ST (S	HE	ET	6										· · · · · · · · · · · · · · · · · · ·			
											PUMP)		NIFOLD		MMY
											FLOW			RESS	P	IPUT RESS
38	39	40	41	42	43	44	45	46	47	48	TOTAL ROLLES	PRESS	MAIN	L/H R/H	L/H	R/H
06	71	72	6 E	70	70	"	7 1	7 0	æl.	0.7	00.0			ha ha		
96 95	71 92	73 73	65 68	72 79	72 78	66 78	71 85	72 82	74 68	37	22.8 22.5	75 64	45 44	43 40 37 35	23	21
94 95	69 87	71 74	64 68	71 79	70 78	65 79	70 85	70 81	72 68	37	22.8 22.5	76 64	45 44	44 40 37 35	23	21
95 96	70 88	73 75	64 68	72 81	71 80	65 80	71 89	70 84	73 69	36	22.8 22.5	76 64	46 44	44 40 36 35	24	21
94 94	70 87	72 74	65 68	72 80	71 79	65 79	71 85	71 84	73 68	35	22.8 22.5	76 64	46 44	44 40 36 35	24	21
95 95	71 88	73 74	66 68	73 81	72 79	66 79	71 86	71 84	73 69	35	22.8 22.5	76 64	46 44	44 40 37 35	23	21
96 98	70 89	73 76	64 69	73 82	71 81	65 81	71 87	71 85	73 69	34	22.8 22.5	76 64	46 44	43 40 37 35	23	21
94 96	69 88	71 76	63 68	71 82	70 80	64 80	69 87	70 84	71 69	34	22.8 22.5	76 64	46 44	44 40 36 35	23	21
94 94	69 85	70 74	64 66	70 79	69 78	64 77	69 84	70 84	72 68	34	22.8 22.5	76 64	46 44	44 41 36 35	23	21
95 95	70 88	73 74	65 67	72 79	71 78	65 78	70 85	71 82	73 67	34	22.8 22.5	76 63	46 42	44 40 36 35	į	
						<u>.</u>										

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1_	2	3	4	5	6	7	8	9	10
12/13/71	26:28 2400 250				Start on power at 21:55										
12/13	22:10	26:43	2400	250	DUMMY TEST	83 79	93 66		106 112	84 101	99 98	85 99	91 96	97 102	113 101
12/13	22:25	26:58	2400	250	DUMMY TEST	85 81	96 67		110 113		105 102		97 100	102 108	120 105
12/13	22:55	27:28	2400	250	DUMMY TEST		102 68		116 115		112 104			109 110	127 107
12/13	23:25	27:58	2700	250	DUMMY TEST	-	102 69		118 114	_	114 104	-		110 110	129 107
12/13	23:55	28:28	2700	250	DUMMY TEST	89 81	101 69		118 115		114 104			110 111	129 108
12/14	00:25	28:58	3000	250	DUMMY TEST	90 81	102 69	_	118 115		116 105		•	111 112	130 108
12/14	00:55	29:28	3000	250	DUMMY TEST	90 81	103 69		119 116	100 108				111 112	131 108
12,14	01:25	29:58	2700	250	DUMMY TEST	90 80	103 68		119 115		116 105			111 111	131 108
12/14	01:55	30:28	2700	250	DUMMY TEST	90 80	103 68		119 115		115 105			112 111	131 108
12/14	02:25	30:58	2700	250	DUMMY TEST	90 80	103 68	113 109	119 115		115 105			111 111	131 108



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABO

TEMPERATURE (°C)

6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
1:55																						
) 99 . 98		91 96	97 102	113 101	83 93	87 93		76 89		86 94	71 82	69 80	72 81	69 78	82 81	69 73	62 80	69 73	69 81	-	59 76	51 57
-	91 102	97 100	102 108	120 105	89 96			81 92		93 98	78 86	75 84	78 85	76 82	87 84	75 77	66 84	75 78	75 85	77 84	64 75	55 65
		105 102	-	127 107	96 98	100 99			91 101		85 88		87 87	85 85	93 87	83 79	76 87	83 80	82 88	86 86	71 77	60 66
			110 110			101 98			92 102	101 99	86 88		90 88	88 85	98 88	88 80	74 88	85 80	83 90	87 85	71 76	60 61
	98 105	106 102	110 111	129 108	97 98	101 99			92 102	101 100		83 86	89 88	88 85	98 88	87 80	73 87	85 80	83 90	86 86	71 76	60 64
	97 106		111 112	130 108	98 99	102 99	88 99	89 95	93 103	102 100	85 89	84 87	91 88	89 86	98 89	89 82	74 88	86 82	84 91	87 85	72 77	60 63
		108 103	11I 112	131 108	99 99				94 103	104 101			91 89	90 87	99 89	89 82	75 89	87 82		88 88	72 77	60 66
116 105	100 106	107 102	111 111	131 108	98 99	103 100	88 99	89 95		102 101			91 89			88 81	74 68	86 81	84 90	•	72 77	60 63
			112 111	131 108					93 103	102 100			91 88	89 85	98 88	88 80	74 88		84 90	87 87	72 77	60 62
115 105	100 105	107 102	111 111	131 108	99 99	103 99	88 98	89 95	93 103	102 100	87 88	85 86	91 88	89 85		88 80	74 87	86 81	84 90	86 86	72 77	59 61



EST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 7)

APERATURE (°C)

30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 25 26 27 46 52 50 56 74 79 54 62 65 90 65 66 64 62 61 55 62 66 83 87 78 66 47 51 94 83 71 63 74 81 67 62 63 62 55 62 94 84 58 66 94 65 54 62 66 67 63 63 62 67 : 93 66 68 63 55 63 67 54 64 92 65 62 63 67] 92 65 62 66 67] 76 81 92 65 67 63 62 54 62 66 95 84 59 66 76 81 75

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K	TES	T (S	HE	ET 7	71															
									-					PUMP		MA	NIFC	OLD		MMY
14	27	20												OW			RES	5		PUT ESS
0	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
i4 '7	62 77	76 88	56 78	58 57		54 68	53 60	46 70	52 77	57 70	57 63	17	21.9 21.9	5.2	79 63	74 74	42 36	35 35	21	18
039	64 82	82 91	59 82	60 63	55 66	57 71	56 62	50 74	56 79	60 64	61 60	39	22.2 22.2	5.3	76 63	42 44	42 36	35 34	20	18
16 32	67 80	90 93		66 59		62 72	61 65	54 76	62 82	65 74	67 60	16	22.8 22.5	5.3	73 63	4 <u>1</u> 44	40 36	3 ⁴ 35	20	18
76 31	68 79	91 94		67 59		63 71	62 63	55 74	62 81	66 74	68 59	16	22.5 22.5	5.3	72 63	4 <u>1</u> 44	38 36	33 35	20	18
76 32	67 80	91 94	65 84	67 58		63 72	62 65	55 75	62 81	66 75	67 60	15	22.8 22.5	5.3	72 63	41 44	38 36	33 35	20	18
77 32	67 82	94 96		67 63		63 72	62 66	54 76	62 81	66 71	67 59	14	22.8 22.5	5.3	72 63	41 44	38 36	33 35	20	18
77 82	68 84	93 95	66 84	68 59	63 71	63 74	62 66	55 76	63 82	67 74	67 60	14	22.8 22.5	5.3	72 63	41 44	38 37	33 35	20	18
77 82	67 82	92 95		67 58		63 73	62 66	54 76	64 82	66 71	67 59	13	22.8 22.5	5.3	72 63	41 44	38 36	33 35	20	18
77 82	67 79	92 95		67 59	62 66	62 75	61 65	54 76	62 81	66 68	67 59	14	22.8 22.5	5.3	72 63	41 44	39 36	33 35	20	18
76 82	68 79	92 95		67 59		62 72	61 64	54 76	62 81	66 75	67 59	13	22.8 22.5	5.3	72 63	44 44	39 36	33 35	20	18

A Sanda Parket

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		,	2	3	4	5	6	7	8	9	10
12/14/71	02:55	31:28	3000	250	DUMMY TEST	90 81	103 70		119 116		116 105			112	13:
12/14	03:25	31:58	3000	250	DUMMY TEST	92 81 St	70	110	116	100 109 tail	105	106	103		10
12/14	04:15	32:28	3560	450	DUMMY TEST	91 82 Ste	•	110	116	100 109 tail	105	106	103		10
12/14	05:45	32:58	2400	250	DUMMY TEST	87 82	99 70		114 116		98 104				
12/14	06:15	33:28	2400	250	DUMMY TEST	91 81	103 70		119 116		115 105				
12/14	06:45	33:58	2400	250	DUMMY TEST	90 80	102 70		118 115	_	113 105	_		_	
12/14	07:15	34:28	2700	250	DUMMY TEST	90 80	102 70		118 115		115 105			111 110	
12/14	07:45	34:58	2700	250	DUMMY TEST	90 80	102 69	112 109	118 115		114 105			111 110	
12/14	08:15	35:28	3000	250	DUMMY TEST	90 81	102 70	113 110			115 105			111 112	
12/14	08:45	35:58	3000	250	DUMMY TEST	91 82	103 70	115 110	121 116		118 105			114 112	
						Sto	op :	inspe	ct s	train	ers				



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LAB

TEMPERATURE (°C)

5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
			108 103	112 112	131 108		103 100		90 96	94 104	103 101	88 89	85 87	91 89	90 87	98 89	99 81	75 89	87 82	84 91	87 87	72 77	60 63
.09	116 105 load	106	103	112 111 power	108	99	99			93 104		87 89		91 89	89 86	98 89	99 81	75 88	87 81	84 91	87 87	72 77	60 63
.09	116 105 load	106	103	113 110 power	109	100	100	87 99	90 96	94 105	103 101	87 89	85 87		91 87	99 91	99 83	75 90	88 83	85 92	89 88	73 77	62 63
			101 102	105 110		93 98	96 99		84 95	86 101	95 100	81 88	78 86	83 88		88 87	78 79	69 85	79 80	77 87	79 87	67 77	56 62
	_		107 102			99 99		88 99			102 100	88 89	85 86			95 87	85 79	74 85	85 80	84 87	86 87	72 77	60 64
			106 102	109 110		97 98		87 99			101 100	86 88	83 86			94 87	84 79	73 85	84 80	82 87	84 87	71 77	57 63
	115 105		107 102					88 100			101 100	87 89	84 86			97 88	87 81	74 87	86 81	83 90	86 87	72 77	59 62
	114 105		107 102			97 99		88 99			101 100	87 89	84 86		87 86	97 88	86 81			83 91	86 87	72 77	59 61
)9)9	115 105	100 105	107 102	111 112	130 109	98 99	102 100	88 100	88 96		102 100	88 89	85 87		89 87		89 81		87 82	84 91	87 88	•	60 62
				114 112			105 100					91 89	87 87		93 : 87	105 90	93 83	77 89	90 83	87 91	92 88	73 77	61 62

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iners

SMISSION TEST DATA; LABORATORY BACK-TO-BACK TEST (SHEET &)

TEMPERATURE (°C)

21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 98 99 75 87 84 87 72 60 53 60 66 37 45 78 66 77 67 63 66 69 49 48 51 81 54 82 79 95 84 64 66 72 65 65 65 65 66 78 62 79 95 84 64 66 72 65 65 66 72 82 89 73 62 55 62 68 41 47 79 66 78 68 94 67 68 64 69 79 77 77 63 67 71 53 49 53 81 54 </th
89 81 89 82 91 87 77 63 66 69 49 48 51 81 54 82 79 95 84 64 66 72 65 89 89 75 87 84 84 87 72 60 53 60 66 39 45 78 66 76 68 92 65 67 62 64 63 89 81 88 81 91 87 77 63 66 69 51 48 51 81 54 82 79 95 84 60 66 72 65 89 81 88 81 91 87 77 63 66 69 51 48 51 81 54 82 79 95 84 60 66 72 65 89 81 83 90 83 92 88 77 63 67 71 53 49 53 81 54 82 79 96 85 60 66 71 64 88 79 85 80 87 87 77 62 66 69 52 48 51 80 54 81 78 83 82 58 66 72 64 87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 65 88 81 87 89 85 80 87 87 77 62 66 70 51 47 50 80 54 81 79 94 84 64 67 72 66 88 81 87 81 91 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 81 88 81 87 81 91 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 81 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 66 89 52 47 50 81 54 81 79 94 83 64 67 71 64 64 81 81 81 81 81 81 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 81 90 87 77 62 66 70 51 47 70 52 48 50 81 54 81 79 94 83 64 67 71 64 81 90 87 77 62 66 70 51 47 70 52 48 50 81 54 81 79 94 83 64 67 71 64 81 81 81 81 81 81 81 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 81 81 81 81 81 81 81 81 81 81 81 81 81
89 81 88 81 91 87 77 63 66 69 51 48 51 81 54 82 79 95 84 60 66 72 65 67 89 89 89 89 75 88 85 89 73 62 55 62 68 41 47 79 66 78 68 94 67 68 64 65 64 91 83 90 83 92 88 77 63 67 71 53 49 53 81 54 82 79 96 85 60 66 71 64 88 78 79 85 80 87 87 77 62 66 69 52 48 51 80 54 81 78 93 82 58 66 72 64 87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 66 72 64 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 66 72 64 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 67 81 81 81 81 81 81 81 81 81 81 81 81 81
91 83 90 83 92 88 77 63 67 71 53 49 53 81 54 82 79 96 85 60 66 71 64 64 88 78 69 79 77 79 67 56 49 55 62 36 42 72 61 71 64 86 61 63 56 59 58 87 79 85 80 87 87 77 62 66 69 52 48 51 80 54 81 78 93 82 58 66 72 64 87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 67 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 67 88 81 87 89 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 57 77 61 66 69 57 77 64 77 64 77 64 77 64 77 64 66 69 57 78 80 54 82 79 94 84 64 67 72 66 78 88 81 87 81 90 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 64 77 10 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 64 70 81 81 81 81 81 81 81 81 81 81 81 81 81
87 79 85 80 87 87 77 62 66 69 52 48 51 80 54 81 78 93 82 58 66 72 64 65 87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 87 88 81 87 81 90 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 71 64 67 91 83 64 67 71 64 67 91 84 64 67 71 64 66 69 57 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 67 90 81 88 82 91 88 77 62 67 70 52 48 50 81 54 81 79 95 84 59 67 72 64 64 63 64 67 90 81 88 82 91 88 77 62 67 70 52 48 50 81 54 81 79 95 84 59 67 72 64 65 63 81 90 81 81 81 81 81 81 81 81 81 81 81 81 81
87 79 85 80 87 87 77 64 66 69 57 57 60 80 57 82 80 94 84 60 67 73 66 94 84 73 84 82 84 71 57 54 58 54 32 43 76 64 75 67 90 63 66 61 62 61 87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 88 81 87 81 90 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 71 64 72 83 84 85 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 71 64 72 83 84 85 81 87 81 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 71 64 72 83 84 85 85 85 85 85 85 85 85 85 85 85 85 85
87 79 85 80 87 87 77 63 66 69 57 48 52 81 57 82 81 93 83 64 66 76 65 87 87 74 86 83 86 72 59 52 58 55 37 44 77 64 76 67 91 64 66 62 64 62 88 81 87 81 90 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 79 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 70 64 70 81 81 81 81 81 81 81 81 81 81 81 81 81
6 88 81 87 81 90 87 77 62 66 70 51 47 50 80 54 82 79 94 84 64 67 72 66 7 97 86 73 86 83 86 72 59 51 58 55 37 43 77 64 76 67 91 64 66 62 63 62 8 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 9 100 89 74 87 84 87 72 60 52 59 55 37 44 77 64 76 67 92 64 66 63 64 63 9 81 88 82 91 88 77 62 67 70 52 48 50 81 54 82 79 95 84 59 67 72 64
6 88 81 87 81 91 87 77 61 66 69 52 47 50 81 54 81 79 94 83 64 67 71 64 9 100 89 74 87 84 87 72 60 52 59 55 37 44 77 64 76 67 92 64 66 63 64 63 9 81 88 82 91 88 77 62 67 70 52 48 50 81 54 82 79 95 84 59 67 72 64 8 105 93 77 90 87 92 73 61 52 60 56 38 45 79 66 78 67 96 65 67 66 65 63
7 90 81 88 82 91 88 77 62 67 70 52 48 50 81 54 82 79 95 84 59 67 72 64 3 105 93 77 90 87 92 73 61 52 60 56 38 45 79 66 78 67 96 65 67 66 65 63

15	HE	ET (8)							_								
												PUMP		MA	NIFC	LD		YMM
												WC			RESS		PR	PUT ESS
3_	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
3	65 84	67 64	63 66	64 72	63 65	55 76	62 82	67 74	67 60	14	22.8 22.5	5.3	72 63	42 44	39 36	33 35	20	18
):	65 84	67 60	62 66	64 72	63 65	55 75	62 81	67 74	68 60	13	22.8 22.5	5.3	72 63	42 44	39 36	33 35	20	18
	67 85	68 60	64 66	65 71	64 64	55 76	63 82	67 74	68 60	16	22.8 22.5	5.3	72 63	42 44	39 36	33 33	20	18
	61 82	63 58	56 66	59 72	58 64	51 75	58 81	62 74	63 59	15	22.8 22.5	5.3	76 63	րր Դի	42 37	35 35	22	19
	65 84	67 60	63 67	64 73	63 66	55 77	62 82	67 76	68 60	15	22.8 22.5	5.4	72 64	42 44	41 37	34 35	20	18
	63 83	66 64	61 66	62 76	61 65	53 76	60 81	65 74	66 59	14	22.8 22.5	5.4	73 63	42 44	40 37	3 4 35	20	18
	64 84	66 64	62 67	64 72	62 66	54 76	61 81	65 74	66 59	13	22.5 22.5	5.4	73 63	42 44	40 36	34 35	21	18
	64 83		62 67			54 76	61 81	65 74	66 59	13	22.8 22.5	5.4	73 63	42 44	40 36	34 35	21	18
	64 84	66 59	63 67	64 72	63 64	54 76	61 81	65 74	66 59	13	22.8 22.5	5.4	73 63	42 44	40 36	3 ¹ 4 35	21	18
	65 84	67 59	66 67	65 72	63 64	55 77	63 81	66 74	67 59	13	22.8 22.5	5.4	72 63	114 142	39 36	33 35	20	18
																		err Ugan



DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1 2	3	3 4	5	. 6	7		3 9
8/10/72 8/11	09:40	35:58 37:13	500	250		Start 1 hour Start Stop	tes -	on por t at on on por check	vari wer	ous at 0	power 9:25		d cor
8/11	10:35	37:33	500	250		Start Stop		on pot					
8/11	20:05	37:53	500	250		Start Stop		on pow	tor	que s	split		
8/12	08:25	37:53	550	250	DUMMY TEST		107	break 109 114	84	103 101	-	96	
8/12	08:55	38:23	550	250	DUMMY TEST	98 100 : 98 70 :		112 112		107 100	93 101		102 105
8/12	09:25	38:53	1200	250	DUMMY TEST	94 96 3 98 71		108 114		103 102	90 104	96 99	100 107
8/12	09:55	39:23	1600	250	DUMMY TEST			109 115		103 104	-	97 103	
8/12	10:25	39:55	2000	250	DUMMY TEST			110 117		106 107	93 109	99 105	102 111
8/12	10:23	40:23	2500	250	DUMMY TEST	100 76	116	112 118 ect st	113	108 110 ners	112	101 108 tart	115
8/12	14:30	40:23	1950	250	DUMMY TEST	90 93 :	103	107 108		101	89 95		97 96



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY B.

TEMPERATURE (°C)

9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 3

onditions

08:25

9	115 106	87 96	92 97	77 71	80 93	80 94	91 97	75 87	74 85	77 81	68 75	77 77	76 79	70 71	37 76	68 82	69 82	65 79	59 71	54 71	57 73	43 65	57 60
2 5	118 105	91 96	95 96	80 72	80 93	85 95	95 97	81 89	88 89	89 87	71 80	81 83	79 82		34 79	73 82	74 90	70 82	61 72	54 72	61 73	44 69	58 68
0	117 107	85 98	91 98	79 74	78 94	80 97	91 98	75 90	74 .90	79 89	71 85	79 86	76 85	74 79	34 82	70 85	70 93	64 84	57 72	51 73	56 7 5	41 71	54 69
0	118 109	87 100	92 101	79 76	78 96	82 101	92 101	76 93	74 94	79 93		82 90	76 90	76 82	35 85	72 88	72 96	64 85	57 75	51 76	56 76	42 71	54 71
1 2	121 111	89 102	93 103	80 77		83 103		78 95	76 96	82 95	78 94	85 94	79 92			75 90	74 99	65 87	58 76	52 77	57 78	42 72	55 73
3	123 114	91 105	96 106			86 107			77 99	84 99	83 98	89 98	82 95	85 88	36 90	77 93	76 105	66 90	59 79	53 80	58 81	43 75	56 75
1	power	at 1	4:30																				
7	116 98	84 89	89 89	75 63	75 85	80 89	89 90	76 80	73 78	74 74	68 70	78 69	74 71	71 65	33 70		71 80	6 3 68	56 63	50 63	55 63		54 60



RA	TO	RY	BA	CK-	TO	-BA	CK	TE	ST (SHE	ET	9)										
22					2.1	2.5			20	20	10	49	10	10	4.4	4.8	44	47	40	FLOTAL	PUMP	T
29_	30	31	32	33	34	35	30	37	38	39	40	_ 41_	42	43	44	45	40	47	40		RV 655	
14 "I	57 73	43 65	57 60	46 63	72 82	65 59	71 81	70 76	79 86	66 83	70 72	49 66	65 68	63 71	56 83	62 85	69 73	66 67	25	20.7 22.5	5.5	
4	61 73	44 69	58 68	49 71		66 72	75 87	61 72	82 87	67 89	68 90	59 87	62 85	62 68	55 73	63 76	68 87	67 89	25	21.9 22.5	5.5	
1	56 75	41 71	54 69	45 71	70 89	62 73	69 89	67 90	80 93	63 90	66 82	50 71	61 74	60 78	53 90	59 90	66 80	63 71	25	20.7 22.5	5.5	
1 6	56 76	42 71	54 71	45 73	70 9 2	62 76	69 93	66 93	81 96	62 93	65 85	51 72	60 78	59 81	53 92	59 93	65 81	63 74	26	21.0 22.5	5.6	
7		42 72	55 73	46 74		63 78	70 95	57 94	83 99	64 95	66 87	52 73	61 80	60 82	54 95	60 96	66 83		26	21.0 22.8	5.6	
3		43 75	56 75		72 96	64 81	72 98	68 99	86 103	65 99	67 90	53 77	63 82	62 86	55 97	61 99	66 86	65 79	27	21.9 22.8	5.6	(
}	55 63	41 62	54 60	44 63	69 75		68 75	65 72	78 81	61 76	62 63			58 61	51 74	57 79	61 65	62 62	25	20.7 22.2	5.4	(

			110										PUMP		M	ANIF	OLD	ום	JMMY
												FI	ow			PRES		11	NPUT
37	38	39	40	41	42	43	44	45	46	47	48			PRESS			H R/H		RESS
<u> </u>					-									V N.200		/ .		-/-	
												1							
														Ш					
70	79	66	70	49	۷5	62	-	60	(0	"	0.5			0.					
76	86	83	72	66	65 68	63 71	56 83	62 85	69 73	66 67	25	20.7 22.5	5.5	80 65	43 44	42 38	37 37	22	19
														Ú	ļ.		•		
61 72	82 87	67 89	68 90	59 87	62 85	62 68	55 73	63 76	68	67	25	21.9		75	42	40	36	21	19
1 =	O į	09	90	01	0)	60	13	10	87	89		22.5	5.5	65	44	38	36		
67	80	63	66	50	61	60	53	59	66	63	25	20.7		78	42	40	36	21	19
90	93	90	82	71	74	78	90	90	80	71		22.5	5.5	64	43	37	35	ΣŦ	19
•	0.5	6 0	-																
66 93	81 96	62 93	65 85	51 72	60 78	59 81	53 92	59 93	65 81	63 74	26	21.0	5.6	77 64	42 43	40 37	36 35	21	19
								-					,,,,		,,,	31	37		
57 94	83		66	52	61	60	54	60	66	64	26	21.0	_	77 64	42	40		21	19
74	99	95	87	73	80	82	95	96	83	75		22.8	5.6	64	43	37	35		
68	86	65	67	5 3	63	62	55	61	66	65	27	21.9		76) ₁ O	1.0	27	0.3	10
9	103	99	90	77	82	62 86	97	99	86	79	- 1	22.8	5.6	76 64	42 42	40 37	37 35	21	19
55 72		61 76	62 63	51 61	60 61	58 61	51 74	57 79	61 65	62 62	25	20.7	5.4	80 65	44 44	42	38	22	19
_		. •		~~	-		1 7	17		U.E.		EE . E	J.4	כט	44	38	36		

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5_	6	7	8	9	
8/12/ 7 2	15:00	40:53	1950	250	DUMMY TEST	89 98	92 71	101 110	105 113	79 106	99 102	87 104	92 100	96 105	
8/12	15:30	41:23	1950	250	DUMMY TEST	90 100	94 72	102 111	106 115	80 107	100 103	87 106	93 101	96 108	
8/12	16:00	41:53	1950	250	DUMMY TEST	91 100	95 72	103 111	107 115		101 103	88 106	-	97 109	
8/12	16:30	42:23	1950	250	DUMMY TEST	94 100	96 73	103 112	107 115		101 104	89 106	-	98 109	-
8/12	17:00	42:53	2400	250	DUMMY TEST	95 101	96 74		109 116	83 110		90 108	-	99 111	•
8/12	17:30	43:23	2400	250	DUMMY TEST	95 101	96 74		108 116		103 106	90 109	96 104	99 111	:
8/12	18:00	43:53	2700	250	DUMMY TEST	96 102	96 75		109 117		104 106	91 109		100 112]
8/12	18:30	44:23	2700	250	DUMMY TEST	96 100	97 74			84 109		91 107		100 110	
8/12	19:00	44:53	3000	250	DUMMY TEST	96 101	97 74		109 116	85 110		91 108		100 110	1
8/12	19:30	45:23	3000	250	DUMMY TEST	96 101	98 74			85 111		91 108		100 111	1
8/12	20:00	45:53	3000	250	DUMMY TEST	96 101	98 74		110 116	85 111		91 108		100 111	1.



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABO

TEMPERATURE (°C)

6 7	8 9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	
99 87 102 104	92 96 100 105	113 107		87 97	75 73	75 93		87 98		70 90	75 89	68 85	77 85	72 85	71 78	33 81		68 93	60 85	54 72	1
100 87 103 106	93 96 101 108	115 108			75 74	75 95	78 99	88 100	72 92	70 92	75 91	68 87	78 87	72 86	72 80	34 83		68 94	60 86	54 73	
101 88 103 106	94 97 101 109	116 108			76 74	76 95	79 99	89 100	73 92			69 87	78 88	73 87	73 80	35 83	66 86		61 86	55 73	1
	94 98 102 109	116 108		89 100	76 75	77 95	79 99	89 100	74 92	72 93	76 92	69 88	79 88	73 87	73 80	36 83	66 86		60 86	55 74	1
	96 99 103 111			91 101	78 76	78 97	81 101	91 102	75 94	73 94	79 94	74 91	82 91	76 89	77 82	36 86	69 87	71 96	61 87	55 75	1
	96 99 104 111			91 101	78 76	78 97	81 102	91 102	75 95	73 95	79 94	74 92	82 92	76 89	77 82	37 86	69 87	71 97	61 87	56 76	1
104 91 106 109	96 100 105 112	120 111		92 103	79 76	78 98	82 102	91 10 2	76 95	74 95	80 95	77 93	84 94		79 83	37 87	71 89	72 99	62 87	56 76	1
104 91 105 107	97 100 103 110	120 109		92 100	79 75	79 96	82 101	91 101	76 93	74 93		77 91	84 91	77 87	93 83	37 85	71 87	72 96	62 86	56 73	,
105 91 105 108	97 100 103 110	121 110	87 100	92 101	79 75	79 97	83 102	92 102	76 94	74 94	81 94	79 93	85 93	79 88	81 82	37 86	72 87	72 96	62 86	56 73	
	97 100 103 111	121 110	87 101	92 101	80 75	80 97	83 102	92 102	76 94	74 94	81 94	79 93	85 93	79 88	81 82	37 86	72 87	72 96	62 86	56 73	
	97 100 103 111	121 110			80 75	80 97	83 102	92 102	76 94	74 94	81 94	79 93	85 93	79 88	81 82	37 86	72 87	72 9 6	62 86	-	

ST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 10)

ERATURE (°C)

25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47
65 85	68 93	60 85	54 72	47 73	52 74	40 71	51 68	43 71	66 88	58 73	65 90	65 90	76 93	59 89	62 80	45 69	59 67	58 71	50 88	55 90	60 72	60 73
65 85		60 86	54 73	48 75	52 75	39 71	51 71		66 90	58 75		66 93	77 95	59 91	62 83	45 71	59 80	58 80	50 90	55 92	60 81	60 75
66 86	69 95	61 86	55 73	49 75	53 76	41 72	52 71		67 90	59 76			77 95		62 84	46 71	61 80	59 80	51 90	56 92	60 81	61 75
66 86	70 95	60 86	55 74	49 76	53 76	40 72	52 71		67 91.	59 76	66 93	67 93	78 96	60 91	63 84	46 71	59 80	58 80	51 90	56 93	61 82	61 76
69 87	71 96	61 87	55 75	49 76	54 77	41 73	53 71	44 73	68 92	60 78	67 94	66 95	80 97	61 93	63 85	47 72	59 81	58 82	52 92	57 94	61 83	61 76
69 87	71 97	61 87	56 76	50 76	54 78	41 73	53 72		68 93	60 79	67 94		80 98	61 93	63 87	47 74	59 81	58 83	52 93	57 95	61 85	62 78
71 89	72 99	62 87	56 76	50 77	54 78	41 73	53 72		68 93	60 79	67 95	66 96	81 99	61 93	64 87	-	59 82	58 82	52 92	57 95	61 83	62 79
71 87	72 96	62 86	56 73	50 74	54 75	41 71	53 70		68 91	60 76	67 93	66 95	81 96	61 92	64 84		59 81	58 81	52 90	57 93	61 82	62 76
	72 96	62 86	56 73	50 74	54 75	41 71			68 91	60 76	68 93	66 95	82 96	61 92	65 84		60 81	59 81	52 90	58 93	61 82	62 76
	72 96	62 86	56 73	50 74	54 75	41 71	53 72	45 72	68 92	60 76	68 93		82 96	61 92	65 84	48 70	60 81	59 81	52 90	58 93	61 82	62 76
72 87	72 96		56 73	50 74	54 75	41 71	53 72		68 92	60 76			82 96		65 84	48 70	60 81	59 81	52 90	58 93	61 82	62 76

(

	T (SHE	ET	101															
								III				•	UMP		MA	NIFO	LD		YMM
												FLOV	V		•	RESS			PUT ESS
<u>'</u>	38	39	40	41	42	43	44	45	46	47	48	TOTAL RO	LLER	PRESS	MAIN	L/H	R/H	L/H	R/H
;)	76 93	59 89	62 80	45 69	59 67	58 71	50 88	55 90	60 72	60 73	25	19.8 22.5	5.5	81 65	կկ կկ	42 38	38 36	22	19
5 3	77 95	59 91	62 83	45 71	59 80	58 80	50 90	55 92	60 81	60 75	25	20.7 22.8	5.6	81 65	իր Դի	42 38	38 35	22	19
5	77 95	60 91	62 84	46 71	61 80	59 80	51 90	56 92	60 81	61 75	26	20.7 22.5	5.5	81 65	44 43	42 38	38 35	22	19
7	78 96	60 91	63 84	46 71	59 80	58 80	51 90	56 93	61 82	61 76	26	20.7 22.5	5.5	81 65	44 43	42 38	38 35	22	19
5	80 97	61 93	63 85	47 72	59 81	58 82	52 92	57 94	61 83	61 76	26	21.0 22.8	5.6	81 65	44 43	42 38	38 35	22	19
5	80 98	61 93	63 87	47 74	59 81	58 83	5 2 9 3	57 95	61 85	62 78	26	21.0 22.8	5.6	81 65	44 43	42 38	38 55	22	19
5 5	81 99	61 93	64 87	47 71	59 82	58 82	52 92	57 95	61 83	62 7 9	26	21.0 22.8	5.6	81 65	44 44	42 38	38 35	22	19
5	81 96	61 92	64 84	47 70	59 81	58 81	52 90	57 93	61 82		26	21.0 22.8	5.6	81 65	44 43	42 38	38 35	22	19
6 5	82 96	61 92	65 84	48 70	60 81	59 81	52 90	58 93	61 82	62 76	26	21.0 22.8	5.6	81 65	44 43	42 38	38 35	22	19
6 6	82 96	61 92	65 84	48 70	60 81	59 81	5 2 90	58 93	61 82	62 76	26	21.0 22.8	5.6	80 65	44 43	42 38	38 35	22	19
	82 96	61 92	65 84	48 70	60 81	59 81	52 90	58 93	61 82	62 76	26	21.0 22.8	5.6	80 65	44 43	42 38	38 35	22	19

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
8/12/72	20:30	46:23	3000	250	DUMMY TEST	96 101	98 74	105 113		85 111	105 105			100 111	
8/12	21:00	46:53	3000	250	DUMMY TEST	96 101	98 75	105 113		85 111				100 111	
€, 12	21:30	47:23	3000	250	DUMMY TEST	96 101	98 75	105 113		85 111				100 111	12
٤, 12	22:00	47:53	3000	250	DUMMY TEST	96 101	98 75	105 113		84 111	-		-	00 111	12 11
0, .2	2:18	48:11	3000	250	DUMMY TEST	96 101	98 75	105 113		84 111	-	92 108		100 111	12 11
L/12	23:10	48:41	3560	425	DUMMY TEST	St 97 101	-	107 112	111	87 109		94	100		
/12	23:40	49:11	1100	425	DUMMY TEST	97 98	102 72	104 108	108 113		101 100	88 98	-	97 105	11 10
1/12	23:52	49:23	3700	425	DUMMY TEST	Ra	n 12	minu	tes a	it th	is po	wer			
.3	01:00	49:5 3	1950	250	DUMMY TEST		-	chang heck			ad	on	powe	r 00	: 30
8/13	01:25	49:53	1950	250	DUMMY TEST	St 74 93	art 94 69	on p 103 103	ower 108 108	at 0 56 98	1:25 102 93	89 90	94 91	98 97	11 9
5,13	01:55	50:23	1950	250	DUMMY TEST	75 99	99 72	104 109	109 114	84 105	103 101		96 99	99 105	11 10



					TA	BLE	D	Π.	RO	LLE	RG	EAR	TR	AN	SMI	55	101	1 TE	ST	DAT	A:L	AB	0
																		TEMP					
6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	2
			100 111		87 101	92 101			83 102	92 102		74 94	81 94	79 93	85 93	79 88	81 82	37 86	72 87	72 96	62 86		7
105 105	91 108	97 103	100 111	121 110	87 101	92 101	80 75	80 97	83 102	92 102	76 94	74 94		79 93	85 93	79 88	81 82	37 86	72 87	72 96	62 86		5
				121 11		92 101				92 102	-			79 93		79 88			72 87	73 96	62 86	56 73	5 71
						91 101				92 102			81 94	79 93	85 93	79 88	81 82	38 86	72 87	73 96		56 73	
	108	1.03	111	110	101					92 102				79 93		79 88	81 82	38 86	72 87	73 96	62 86	56 73	50
ad		_		it 22:			00	0-	06	25	=0		0=	01.	00	00	0.5	25	7/	-/	"	(-	٠.
				123 119						95 102			94	84 92		83 87	82		86	76 96		60 74	7:
101 100			97 105	115 106		90 96	78 71	77 93		91 98	75 90	73 90	76 87	66 80		72 80	68 74	36 80	64 82	68 90	63 83	59 73	
is po	wer																						
ad	on	powe	er 00	:30																			
1:25 102 93		94 91	98 97	116 98		90 90	77 86	76 63	79 90	90 90	73 81	71 81	81 79	69 73	79 74	73 71	72 66	35 73	67 73		61 73	56 65	45

64 56 45 80 71 71

68 70 81 90

103 90 96 99 117 86 91 78 78 80 91 74 72 77 78 75 73 73 35 101 102 99 105 105 97 96 71 92 96 97 89 89 88 83 84 89 75 89

ORY BACK-TO-BACK TEST (SHEET 11)

								Ť												PUMP	
																			FLC	W	
0	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL R	OLLER	PRESS
4 5	41 71	53 72	45 72	68 92	60 76	68 93	66 96	82 96	61 92		48 70	60 81	59 81	52 90	58 93		62 76	26	21.0 22.8	5.6	80 65
4 5		53 72	45 72	68 92	60 76	68 93		82 96		65 84			59 81		58 93	61 82	62 76	26	21.0 22.8	5.6	80 65
4	41 71	54 72			61 76			82 96		65 84	48 70		59 81		58 93		62 76	27	21.0 22.8	5.6	80 65
¥ 5	41 71	54 72	-	68 92	61 76	68 93		82 96		65 84			59 81	52 90	58 93	62 82	62 76	27	21.0 22.8	5.6	80 65
}	41 71		45 72		61 76			82 96	62 92	65 84	48 70		59 81		58 93	62 82	62 76	26	21.0 22.8	5.6	80 65
) }	43 73	57 73		73 90	63 76			86 97		67 84	50 68	64 81	63 81	55 89		65 81	65 75	26	21.0 22.	5.5	79 65
	43 73	56 72	47 73	71 87	62 73	70 90	68 93	77 91	63 88	66 82	46 66	62 79	61 79	53 85	59 89	63 79	64 72	26	20.7 22.5	5.5	81 65
	40 65	52 64	44 65	68 82	59 65	67 82	66 85		60 82	63 72	46 62	60 65	58 65	51 73	57 65	61 82	61 67	25	20.7 21.9	5.2	80 65
	41 68	53 68	44	69 85	60 71	68 91	67 91	79 87	61 71	64 76	47 76	70 82	59 76	54 82	57 87	62 76	62 76	25	20.7 22.5	5.5	80 65

T (SHE	ET	11)															
												PUMP		MA	NIFO	LD	DUA	
												ow			RESS		PRE	
38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
82 96	61 92	65 84		60 81		52 90	58 93	61 82	62 76	26	21.0 22.8	5.6	80 65	44 43	42 38	28 35	22	19
82 96	61 92	65 84	48 70	60 81	59 81	52 90	58 93	61 82	62 76	26	21.0 22.8	5.6	80 65	44 43	42 38	38 35	22	19
82 96	62 92	65 84	48 70	60 81	59 81	52 90	58 93	62 82	62 76	27	21.0	5.6	80 65	74 74	42 38	38 35	22	19
82 96	62 92	65 84	48 70	60 81	59 81	52 90	58 93	62 82	62 76	27	21.0	5.6	80 65	44 43	42 38	38 35	22	19
82 96	62 92	65 84	48 70	60 81	59 81	52 90	58 93	62 82	62 76	26	21.0	5.6	80 65	44 43	42 38	38 35	22	19
86 97	65 91	67 84	50 68	64 81	63 81	55 89	61 93	65 81	65 75	26	21.0	5.5	79 65	44 44	42 38	38 36	20	19
77 91	63 88	66 82	46 66	62 79	61 79	53 85	59 89	63 79	64 72	26	20.7 22.5	5.5	81 65	111 111	42 38	38 36	21	19
78	60	62	1,6	60	E0	5 1	57	61	61	25	20.7		g _O	1, 1,).o	27	22	10
78 35	82	63 72	46 62	60 65	58 65	51 73	57 65	61 82	61 67	25	20.7 21.9	5.2	80 65	ħħ ħħ	42 38	37 36	22	19
79 37	61 71	64 76	47 76	70 82	59 76	54 82	57 87	62 76	62 76	25	20.7	5.5	80 65	11 11 11 11 11 11 11 11 11 11 11 11 11	42 38	37 36	22	19

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DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	Ŋ
8/13/72	02:05	50:33	1950	250		St	op c	heck	faci	lity					
8/13	02:35	50:53	1950	250	DUMMY TEST		ert 96 71		106		100	87 103		97 105	10 10
8/13	03:05	51:23	1950	250	DUMMY TEST	75 98	97 72	103 110			101 102				11 10
8/13	03:35	51:53	1950	250	DUMMY TEST	75 98	98 72			83 106	102 102			98 107	11 10
8/13	04:05	52:23	1950	250	DUMMY	75 98	97 71	104 110	108 114	83 106				98 107	11 10
8/13	04:35	52:53	2400	250	DUMMY TEST	74 97		103 110			102 102				11 10
8/13	05:05	53:23	2400	250	DUMMY TEST	74 98	97 71	104 110		83 107	102 J.03			99 108	11 10
8/13	05:35	53:53	2400	250	DUMMY TEST	73 99	97 71	104 111		83 107	103 103			99 108	11 10
8/13	06:05	54:23	2700	250	DUMMY TEST	74 99	97 71	104 111		84 108			96 102	99 109	11 10
8/13	06:35	54:53	2700	250	DUMMY TEST	73 98	97 71	104 111	108 115	84 108	103 104	90 106		100 109	11 10
8/13	07:05	55:23	2700	250	DUMMY TEST	73 99	97 71	104 111		84 108				99 110	10



TABLE XXI. ROLLER GEAR TRANSMISSION TEST TEMPERA 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 heck facility on power at 02:15 102 106 82 100 87 93 97 109 82 69 74 68 33 64 88 75 76 78 90 89 114 106 101 103 99 105 106 97 97 71 93 81 80 103 107 84 101 88 94 98 116 84 34 66 89 76 76 114 106 102 104 100 107 107 97 81 81 97 72 34 66 108 83 102 89 94 98 117 84 90 74 81 82 110 114 106 102 104 100 107 107 97 98 71 33 67 108 83 102 89 94 98 117 84 71 76 90 77 114 106 102 104 100 107 107 97 81 82 90 89 98 71 107 82 102 89 94 96 116 85 89 76 33 67 81 82 114 106 102 103 100 107 107 97 97 71 33 68 108 83 102 89 96 99 118 86 82 84 110 114 107 103 103 101 108 108 98 98 72 76 76 32 69 104 108 83 103 90 96 99 118 86 72 78 115 107 103 104 101 108 108 77 81 108 84 103 90 96 99 119 86 83 85 92 92 115 108 103 106 102 109 108 99 95 100 108 84 103 90 96 100 119 86 32 70 91 78 77 81 72 78



73 95

91 78 77 82

99 73 95 100

115 108 104 106 102 109 109 99

108 84 103 91 96 99 119 86

115 108 104 106 102 110 109

91 74

100 92

92 92

72 78

92 91

82 85

31 71

83 85

ON TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 12)

TEMPERATURE (°C)

23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46
76 76	33 81	64 80	68 90	59 81	54 71	47 71	52 67	39 69	51 74	47 70	66 87	58 71	65 90	65 93		58 88	61 79	73 71	58 77	57 76	49 84	54 89	59 77
72 77	34 81	66 81	68 90	60 81	54 71	47 72	54 74	39 69	51 74	43 70	67 88	58 73	66 90	65 93	77 93	59 89	64 80	44 71	58 77	57 77	50 85	55 90	60 77
13 17	34 81	66 82	70 91	61 81	55 71	48 72	53 74	39 69	52 74	43 70	67 88	59 72	66 91		78 93	59 8 9	64 80	45 7 2	59 77	57 77	50 83	55 9 0	60 78
'1 '7	33 81	67 82	69 91	60 81	54 71	48 72	54 73	39 69	51 74	43 70	67 88	59 72	66 91	65 93	78 93	59 89	64 80	45 72	58 72	57 77	50 83	55 90	60 78
3	33 81	67 82	69 91	60 82	54 71	47 71		38 68	51 74	42 69	67 87	58 71			78 93	59 88	61 79	45 72	60 76	58 77	49 85	55 90	59 77
6 8		68 84	70 93	61 82		47 73	53 75		51 74	42 70	67 88	58 74		64 93	79 94		64 79	46 73	58 77	58 77	50 84	56 90	60 78
6		69 85	70 93	61 82	54 71	46 73	54 74	38 68	51 74	42 71	67 89	58 73		64 93		59 90	62 81	46 73	58 78	57 78	49 83	55 91	60 78
5	32 83	70 85	71 93	61 82		47 74		37 70	51 75	41 70	67 89	58 74	67 92	64 93	80 95	59 91	61 81	46 74	59 78	57 78	49 84	55 91	60 79
3	32 82	70 85	71 93	61 85	54 72		54 74	37 70	51 74	42 71	68 89	58 74	67 92	64 93	80 96	59 91	61 82	46 74	59 79		49 85		60 79
	31 83	71 85	72 94	61 84	54 71		52 74	37 70	51 74	41 7 1	68 90	58 74	67 92				61 81		58 78	57 78	49 85	55 91	60 79

it (SHE	ET 1	12)															
												PUMP		MA	NIF	OLD		MMY
)W			PRES		PR	IPUT RESS
38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/F	R/H	L/H	R/H
76 92	58 88	61 79	73 71	58 77	57 76	49 84	54 89	59 77	58 71	24	20.] 22.5		80 5 65	<u>ት</u> ት	42 38	38 36	22	19
77 93	59 89	64 80	44 71	58 77	57 77	50 85	55 90	60 77	60 71	24	20.1 22.5		80 65	717 717	42 38	38 36	22	19
78 93	59 8 9	64 80	45 7 2	59 77	57 77	50 83	55 9 0	60 78	60 72	24	20.1 22.5		80 65	ታተ ታተ	42 38	37 36	22	19
78 93	59 89	64 80	45 72	58 72	57 77	50 83	55 90	60 78	60 71	23	20.1 22.5		80 65	71 71 71 71	42 38	37 36	22	19
78 93	59 88	61 79	45 72	60 76	58 77	49 85	55 90	59 77	59 71	22	20.4 22.5		80 65	44 44	42 38	38 36	22	19
79 94	59 90	64 79	46 73	58 77	58 77	50 84	56 90	60 78	60 71	24	20.4 22.5		80 65	44 44	42 38	38 36	22	19
79 95	59 90	62 81	46 73	58 78	57 78	49 83	55 91		60 73	21	20.4 22.5		80 65	44 44	42 38	38 36	22	19
80 95	59 91	61 81	46 74	59 78	57 78	49 84	55 91	60 79	60 72	21	20.7 22.5		80 64	44 44	42 38	38 36	22	19
80 96	59 91	61 82	46 74	59 79	57 79	49 85	55 91	60 79	60 73	20	20.7 22.5		80 64	71 71	42 38	38 36	22	19
80 95	59 91	61 81	47 74	58 78	57 78	49 85	55 91	60 79	60 72	20	20.7 22.5		80 64	44 44	42 38	38 36	22	19



DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.			1	2	3_	4	5	6	7_	8	9	10
8/13/72	07:35	55:53	3000	250	DUMMY TEST	74 98	98 72	105 113	110 115	85 110	105 105	92 103	98 104	101 110	122
8/13	08:05	56:23	3000	250	DUMMY TEST	75 100		107 113			107 106	94 107	100 105	103 112	124 111
8/13	08:35	56:53	3000	250	DUMMY TEST	St	op	check	dum	my l	ube p	oump			
8/13	10:33	56:56	3000	250				on po inspe				5			
						ĺ									
ļ															



TABLE XXI. ROLLER GEAR TRANSMISSION TES

TEMPE

5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	
85	105	92	98	101	122	88	93	80	78	84	93	76	74	82	83	87	81	83	32	
110	105	103	104	110	110	100	101	74	96	102	102	93	94	94	94	94	87	84	85	
86	107	94	100	103	124	89	95	81	80	86	95	77	76	83	84	88	84	83	33	
111	106	107	105	112	111	102	102	76	97	103	103	94	95	95	95	95	89	95	86	

my lube pump

at 10:30 strainers

ANSMISSION TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 18)

TEMPERATURE (°C)

20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	4:
83	87	81	83	32	76	75	62	55	48	53	37	52	42	69	59	68	65	83	61	62	48	60	58
94	94	87	84	85	89	97	85	74	76	77	71	71	71	91	75	93	94	99	93	77	71	79	79
84	88	84	83	33	75	76	63	56	48	54	38	52	42	70	61	69	64	85	61	63	49	60	59
95	95	89	85	86	3 1	99	87	74	76	77	72	71	74	92	77	94	95	99	93	83	71	80	80

SHE	ET	181				***	~-~-				-						
											PUMP		M	ANIFO	LD		MMY
											low			PRES		P	NPUT RESS
39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAI	N L/H	R/H	L/H	R/H
61 93	62 77	48 71	60 79	58 79	51 89	56 93	61 79	61 74	21	20.7 22.5	5.5	79 64	† † † †	42 38	38 36	22	18
61 93	63 83	49 71	60 80	59 80	51 90	57 94	62 80	62 74	20	19.5 22.5	5.6	69 64	38 43	36 38	33 36	19	16

All ASSESSMENT OF THE PARTY OF

RATE SALESTINE

					11.57										
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	
12/4/72	15:20	56:56	1100	250	DUMMY TEST	97 96			118 112	91 104	97 106			110 96	1
12/4	15:50	57:26	1100	250	DUMMY TEST	93 94	-		109 109	81 100	90 101	88 91		99 92	1
12/4	16:20	57:56	1100	250	DUMMY TEST	92 92			108 108		87 100	86 92		97 91	1
12/4	16:50	58:26	1100	250	DUMMY TEST	92 92			108 108		87 100	85 94		97 91	1
12/4	17:20	58:56	1950	250	DUMMY TEST	92 93			111 111		88 102	89 96	96 96		1.
12/4	17:50	59:26	1950	250	DUMMY TEST	92 93	107 65		110 110		88 101	89 97	97 96	99 94	1:
12/4	18:20	59:56	1950	250	DUMMY TEST	92 93		78 10 6	111 111		88 101	90 99	97 96		1:
12/4	18:50	60:26	1950	250	DUMMY TEST	92 94			111 111	82 101	89 102	90 99		100 94	1:
12/4	19:20	60:56	1950	250	DUMMY TEST	93 94			111 111		89 102			100 94	1:
12/4	19:50	61:26	1950	250	DUMMY TEST	93 94			112 111		89 103			101 95	1:
12/4	20:20	61:56	1950	250	DUMMY TEST	93 94			112 111		89 103			101 95	11



	TRANSMISSION TEST
	TO A NICALICE IONI TECT
	I I A N S M I S S I I I I I I I I I I I I I I I
NOLLEN GLAR	

																				TEMP	ER/
4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
5 118 9 112	91 104	97 106			110 96	128 110		102 96	82 68	85 92	92 98	102 97	90 86	86 84	85 86	82 81	86 81	81 81	86 82	90 83	88 93
1 109 3 109	81 100	90 101	88 91		99 92	117 101	87 91	92 91	80 64	77 87	81 93	91 92	75 81	74 80	80 80	73 74	76 74	7 2 7 5	76 75	80 77	71 8:
) 108 108	79 99	87 100	86 92	_	97 91	114 99	84 90	89 90	77 63	75 86	78 92	89 92	72 80	71 78	74 78	69 73	7 3 72	67 73	72 74	76 76	73 81
108		87 100	85 94	94 94	97 91	114 100	84 90	89 90	76 73	75 86	78 92	89 92	72 80	71 78	74 78	69 73	73 72	67 73	72 74	75 76	70 81
} 111 111		88 102	89 96			117 101	86 92	91 92	78 65	76 87	81 93	91 93	74 82	73 80	77 81	75 79	76 78	75 80	77 80	82 82	7: 85
110	82 101	88 101	89 97	97 96		117 101	86 92	91 92	78 75	76 87	81 93	91 93	74 82	73 80	77 80	75 79	77 78	75 79	77 80	82 82	7€ 8٤
111	82 101	88 101	90 99	97 96	99 94	118 101	86 92	91 92	78 65	77 87	81 93	91 93	74 82	73 80	77 80	75 79	77 78	75 79	77 80	82 81	75 88
111	82 101		90 99		100 94	118 101	87 92	92 92	78 64	77 88	82 93	92 93	74 82	73 80	78 80	75 79	77 78	75 79	77 80	82 81	7€ 8€
111 111	83 102	89 102			100 94	119 102		92 92		78 88	82 93		74 82	73 80	78 80	75 79	77 78	75 79	78 80	82 82	76 89
112 111	83 102	89 103		98 97		119 102		93 93		78 88		92 94	75 82	73 80	78 81	75 79	77 78	75 79	78 81	82 82	76 85
112	83 102	89 103	-	98 97	101 95	119 102		93 92		78 88		92 94	75 82	73 80	78 81	75 79	77 78	75 79	78 81	82 82	76 89

EST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 14)

MPERATURE (°C)

4	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47
90 33	88 91		76 71		66 69	53 66	40 67		50 76	82 67	70 82	81 90				68 67	67 68		67 81	57 71	72 78	70 63	
30 17	74 85		65 73		56 66	46 66	35 61	46 63	41 63	71 78	62 64	70 79	66 85	79 85	59 79		48 62		61 67			63 68	
'6 '6	71 84	65 77	62 72	53 63	53 66	42 64	33 60	43 62	40 63	63 77	58 63	67 79	63 84	75 85	55 79		46 60		57 66			58 67	58 60
'5 '6	70 84	65 76	62 72	53 63	53 64	42 63	32 60	43 62	39 63	67 77	58 63	67 78	62 84	75 85	54 79	59 69	45 60	57 63	56 66	47 70	66 77	57 67	58 59
2	75 89	71 82	62 74	5¼ 63	54 66	43 66	33 61	44 63	40 63	68 78	59 64	68 79	62 85	78 88	55 79	59 71	47 63	59 63	57 66	48 71		58 68	
2	76 98	71 82	62 73	53 63	54 66	43 66	32 60	43 63	40 63	68 78	59 63	68 79	62 84	78 88	55 79	59 71	48 62		57 66			58 68	58 60
2	75 88	71 82		54 63		43 65			40 63	68 78	59 64	68 79	62 84	78 88	55 79		48 63		57 66	48 71		58 68	
1	76 88		63 74	54 63	54 66			44 63	40 63	68 78	59 64	68 79	62 84	78 88	56 80		48 63		57 66	48 7 1		59 68	
5	76 89	71 82	63 74	54 64	54 66	43 66	33 61	44 63	40 64	69 78	59 64	68 80	62 85	79 88	56 80	60 71	48 63	59 65	57 66	48 72	67 78	59 68	59 60
2	76 89		63 74	54 64	53 66	43 66	33 62	44 63	40 64	69 79	59 64	68 80	63 85	79 89	56 80	60 71		58 66	57 67			59 68	
	76 89		63 74		53 66			44 63	40 64	69 79		68 80				60 71		58 66				59 68	

IE:	ST (SHE	ET	14)						ULT:									
													PUMP			NIFO			YMY
.7	20	20	40	41	40	40	4.4	4.5	44	47	40		OW	DDECC		RESS		PRE	SS
37	38	39	40	41			44		46				ROLLER					-	
59 34	89 72	67 64	68 67	67 68	68 74	67 81	57 71	72 78	70 63	69 62	20	21.0	5.2	67 65	44 40	38 38	35 35	21	19
56 35	79 85	59 7 9	64 72	48 62	63 64	61 67	51 71	69 78	63 68	61 60	17	19.8 21.9	5.3	70 65	43 44	41 38	37 36	21	20
53 34	75 85	55 79	59 71	46 60	58 63	57 66	47 70	66 77	58 67	58 60	16	19.2 21.9	5.2	72 65	42 44	41 39	37 35	23	22
52 34	75 85	54 79	59 69	45 60	57 63	56 66	47 70	66 77	57 67	58 59	16	18.6 21.9	5.2	72 65	42 44	40 38	36 36	22	21
i2 15	78 88	55 79	59 71	47 63	59 63	57 66	48 71	67 78	58 68	59 60	16	18.6 21.9	5.3	70 65	4 <u>1</u> 44	38 38	36 36	22	21
12	78 88	55 7 9	59 71	48 62	58 64	57 66	48 71	67 78	58 68	58 60	16	18.9 22.2	5.3	70 65	ተተ ቱ0	39 38	35 35	22	21
24	78 88	55 79	59 71	48 63	58 64	57 66	48 71	67 78	58 68	58 60	16	19.2 22.2	5.3	69 65	40 44	39 39	35 35	22	21
2	78 88	56 80		48 63	58 63	57 66	48 71	67 78	59 68	59 60	16	19.2 22.2	5.3	69 65	40 44	39 38	35 35	22	21
2 5	79 88	56 80		48 63	59 65	57 66	48 7 2	67 78	59 68	59 60	16	19.2 22.2	5.3	69 66	41 44	39 38	35 35	22	21
3 5	79 89	56 80	60 71	48 63	58 66	57 67	48 72	67 79	59 68	59 61	16	19.2 22.2	5.3	69 66	41 44	39 38	35 35	22	21
3 5	79 89	56 80	60 71	48 63	58 66	57 67	48 72	67 79	59 68	59 61	16	19.2 22.2	5.3	69 66	41 44	39 38	35 35	22	21

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		1	1			1						
DATE	OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7
12/4 /72	20:50	62:26	1950	250	DUMMY TEST	94 94	108 66		112	83 102	90 103	91 99
12/4	21:20	62:56	1950	250	DUMMY TEST	94 94	108 66		112 112	83 102	90 103	91 97
12/4	21:50	63:26	1950	250	DUMMY TEST	94 94	108 66	_	112 112	84 102		91 98
12/4	22:20	63:56	2400	250	DUMMY TEST	94 95	108 68	_	113 112		91 105	92 98
12/4	22:50	64:26	2400	250	DUMMY TEST	94 95	109 67		113 112		91 105	93 101
12/4	23:20	64:56	2400	250	DUMMY TEST	94 94	108 68	_	113 112	-	91 1.04	93 101
12/4	23:50	65:25	2400	250	DUMMY TEST	94 94		109	113 112		91 104	93 101
12/5	09:15	65:26	2400	250	DUMMY TEST	95 95	110	83	f shi 115 115	86	92 107	96 97
12/5	09:45	65:56	2400	250	DUMMY TEST	94 96			113 115	85 107	92 109	93 99
12/5	10:15	68:26	2700	250	DUMMY TEST	95 97			113 116	85 110	95 110	93 103
12/5	10:45	66:56	2700	250	DUMMY TEST	96 97			113 116	86 110	93 111	93 106



TABLE XXI. ROLLER GEAR TRANSMISSION

	1	2	3	4	5	6	7	8	9	:0	_11	12	13	14	15	16	17	18	19	20	21	22	
MY T	94 94			112 111	83 102	90 103	91 99		101 95	119 103	88 93	93 93	79 65	78 88	82 96	93 94	75 83	74 81	78 81	75 79	77 79	76 80	
MY P	94 94			112 112	83 102	-			101 96	119 103	88 93	93 93	79 65	78 88		93 94	75 83	74 81	78 81	75 79	78 79	75 80	
νΩ Σ	94 94		-	112 112	84 102	90 103			101 95	119 103	99 93	03 93	80 65	89 88	92 96	03 94	85 83	84 81	89 81		89 79	85 80	
AX	94 95		_	113 112	-	91 105			102 97	121 103	89 94	94 95	80 66	80 90		94 95	76 84	75 82	80 83		81 83	81 84	
Y .	94 95	109 67		113 112	_	91 105	-		103 97	122 104	89 94	94 95	81 66	80 90		94 95	76 84	75 82	80 83		81 83	81 84	
ľ	94 94		_		85 104		93 101			122 104		95 95	81 66	80 90	84 95	94 95	76 84	75 83	80 83	80 83	81 83	81 84	
Y	94	68	109	112	104	-				122 104		95 95	81 66	80 90		94 95	76 84	75 83	80 83	80 83	81 83	81 84	
Y		110	83	f shi 115 115	86	92 107	-			124 106	91 97	96 97	76 69	80 92	87 98	97 97	83 85	80 82	74 81		80 81	76 82	i
Y	94 96					92 109	93 99	100 103	102 101	122 107	90 99	95 99	80 71	80 95	87 100	94 99	77 88	76 86	82 89		81 87	82 89	1
Y	95 97	108 72	83 113	113 116	85 110	95 110	93 103	100 104	103 102	123 109	90 100	95 100	81 72	80 95	86 101	95 100		76 88			82 90	85 92	{
Y	96 97	109 73	84 114	113 116	86 110	93 111	93 106	101 105	104 103	123 110	90 100	96 101	81 72	81 96	86 101	95 101			83 91			85 92	

AT	A:L	AB	ORA	NTO	RY	BA	CK-	TO	-BA	CK	TES	ST (S	SHE	ET	15)								
URE	(°C)																	_					_
26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	70
71 82	63 74	54 64	54 66	43 66	33 61	44 63	40 64	69 79	59 65	68 80	63 85	79 89	56 81	60 71	48 63	58 65	57 68	48 72	67 79	59 68	59 62	16	2
71 82	61 74	-	54 66	43 66	33 62	44 63	40 64	68 79	57 65	68 80	63 85	79 89	55 81	60 71	48 63		57 68	48 72	67 79	58 68	59 62	16	2
	61 74		54 66		33 61	44 63	40 64	68 78		68 80	63 85	79 89	55 80	59 71	48 63	58 65	57 67	48 72	67 78	58 68	58 61	16	2
77 87	62 75	55 65	55 67	44 67	34 63	45 64	41 65	69 79	58 66	69 81	63 85	81 91	56 82	61 74	49 64	59 66	58 69	49 74	67 80	58 69	59 62	16	1
77 88	62 76	55 66	54 67	44 66	34 62	-	41 66	69 80		69 82	63 85	82 91	56 82	60 75		60 66	58 70	49 74	68 80	58 69	59 62	17	1
	62 76	55 66	55 67	45 67	34 63	45 64	41 66	69 80	58 66		63 85	82 91	56 82	60 74		60 66	59 69	49 74	68 80	59 69	59 62	16	
76 88	62 76	55 66	55 67	45 67	34 63	45 64	41 66	69 80	58 66	69 82	63 85	82 91	56 82	60 74	49 64	60 66	59 69	49 74	68 80	59 69	59 62	16	
	72 85	63 76	62 66	51 69	41 68	51 66	49 67	77 79	65 66	76 79	65 80	84 91	64 81		74 66	-	63 68	55 74	70 79	65 68	66 61	22	
	64 79	57 69	57 71	47 70	37 65	47 68	43 68	70 82	60 68	71 83	65 85	83 94	58 79	63 76	52 68	62 68	60 71	51 77	69 82	61 71	62 63	19	
	65 80	57 70	56 72	46 71	38 66	47 69	43 70	70 84		70 86	65 89	84 96	58 87	63 78	51 70	62 70	60 74	51 79	70 84	61 73	62 66	19	
	64 81	57 71	57 73	46 72	37 67	47 70	43 71	70 85		70 87	65 90	84 98	58 87	63 79	52 71	62 70	60 75	51 80	69 85	61 74	62 66	18	

 $(\)$

E	ST (S	SHE	ET	15)															
												4	PUMP		M.	ANIF	OLD		MMY
210.1	Dec 144												ow	D	l.	PRES		PR	PUT ESS
37	38	39	40	41	42	43	44		46				ROLLER					L/H	
3 5	79 89	56 81	60 71	48 63	58 65	57 68	48 72	67 79	59 68	59 62	16	19.2	5.3	69 65	44 40	39 38	35 36	22	21
3	79 89	55 81	60 71	48 63	59 65	57 68	48 72	67 79	58 68	59 62	16	19.2 22.2	5.4	70 65	40 44	39 38	35 35	22	21
3	79 89	55 80	59 71	48 63	58 65	57 67	48 72	67 78	58 68	58 61	16	19.2 22.2	5.4	69 65	41 44	39 38	35 35	22	21
3	81 91	56 82	61 74	49 64	59 66	58 69	49 74	67 80	58 69	59 62	16	19.2 22.2	5.4	68 65	40 44	38 38	35 35	22	21
3	82 91	56 82	60 75	49 64	60 66	58 70	49 74	68 80	58 69	59 62	17	19.2 22.2	5.4	68 65	40 44	38 38	35 35	22	21
)	82 91	56 82	60 74	49 64	60 66	59 69	49 74	68 80	59 69	59 62	16	19.2	5.4	68 65	40 44	38 38	35 35	22	21
	82 91	56 82	60 74	49 64	60 66	59 69	49 74	68 80	59 69	59 62	16	19.2 22.2	5.4	68 65	40 44	38 38	35 35	22	21
	84 91	64 81	65 70	74 66	65 64	63 68	55 74	70 79	65 68	66 61	22	20.7 22.2	5.4	68 65	77 70	38 38	35 35	21	20
	83 94	58 79	63 76	52 68	62 68	60 71	51 77	69 82	61 71	62 63	19	19.5 22.2	5.4	68 65	71 70	38 38	35 35	21	20
	84 96	58 87	63 78	51 70	62 70	60 74	51 79	70 84	61 73	62 66	19	19.5 22.5	5.5	68 65	77 70	38 38	35 35	21	20
	84 98	58 87	63 79	52 71	62 70	60 75	51 80	69 85	61 74	62 66	18	19.5 22.5	5.5	68 65	40 43	38 38	35 35	21	20

D

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2 3	4	5	6	7	8	
12/5/72	11:15	67:26	1100	250	DUMMY TEST	97 95	109 84 71 111	112 114	83 105	91 106	89 104	97 102	1
12/5	11:45	67:56	1100	250	DUMMY TEST	97 95	108 83 69 110	111 113	82 105	90 106	88 97	97 100	!
12/5	12:15	68:26	1100	250	DUMMY TEST	97 93	108 83 70 110	111 112			87 93	96 99	:
12/5	12:45	68:56	1950	250	DUMMY TEST	96 95	108 83 71 111		85 106		92 95	99 101	1(
12/5	13:15	69:26	1950	250	DUMMY TEST	97 95	109 83 71 112				92 96	100 102	10
12/5	13:45	69:56	1950	250	DUMMY TEST	97 98	109 83 72 112	112 116			92 97	99 103	10
12/5	14:15	70:26	1950	250	DUMMY TEST	97 98	109 84 73 115		86 110		92 99	99 105	10 10
12/5	14:45	70:56	1950	250	DUMMY TEST	97 98	110 84 73 115	112 118	87 111	92 112	94 100		10 10
12/5	15:15	71:26	1950	250	DUMMY Test	97 98	110 84 74 115					100 106	10 10
12/5	15:45	71:56	1950	250	Dummy Test	97 97	109 84 72 114					100 106	10 10
12/5	16:15	72:26	1950	250	DUMAY TEST	97 98	108 84 72 114						



										-												
									TA	BLI	D	П.	RO	LLE	RG	EAR	TR	AN	SM	155	101	TE
																						TEMF
_2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
	84 111				89 104	97 102		118 107	87 97	92 97		79 93		-		74 85	77 86	71 80	75 80	70 81	75 82	79 82
						97 100		116 106	86 96	92 96	78 69	78 92	81 100	91 98	74 86		76 84		75 79		75 81	78 82
	83 110					96 99		116 103		91 94				91 96			76 83		75 78	69 78	74 79	77 81
	83 111					99 101	102 100						83 100	93 98			79 86	76 83	78 83	76 84	78 86	83 86
						100 102	102 100			94 99			83 100	94 99			80 87	77 85	79 85	77 85	79 87	84 87
	83 112					99 103							84 102				80 88	77 86	79 86	77 86	79 87	85 89
	84 115					99 105							84 104				80 90	77 88	79 88	77 89	79 90	85 91
	84 115					101 105	104 105	122 112	91 103	96 102	82 74	81 98	85 104	95 103	78 92			78 89	80 89	78 89	80 91	86 92
	84 115					100 106							85 104				81 91			78 89	80 91	85 92

109 84 113 86 92 93 100 103 121 89 95 81 80 84 94 77 72 114 117 110 111 97 106 103 111 101 102 74 97 104 103 91

 108
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84 91

84

91

79

79 77 88 89

76 80 77 90 90 88

76 80 77

89 90 88

\:L	AB	OR/	ATO	RY	BA	CK	.TO	-BA	CK	TE	ST (SHE	ET 1	61						- 124		Γ
°C)	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	FLO TOTAL R
53	56	56	46	31	46	42	69	58	69	66	78	57	62	48	61	59	59	68	60	61	18	19.2
79	69	70	70	66	68	69	82	69	85	88	92	85	78	68	69	73	78	83	71	65		22.5
52 79	57 68	55 71	45 71	36 66	46 68	1 ₁₂	68 82	58 68	69 85	65 88	77 91	57 85	62 78	47 68	60 68	58 74	49 77	67 82	59 71	60 63	13	18.9 22.2
61	55	55	44	36	45	42	68	57	68	63	76	56	61	47	59	58	48	67	58	60	18	19.2
78	68	69	68	64	66	68	81	67	83	87	79	84	77	66	62	73	76	81	77	63		22.2
62	56	55	45	37	46	42	69	58	69	64	80	57	62	49	60	58	50	68	59	61	18	19.2
78	68	70	70	65	67	68	82	68	84	89	93	84	77	68	68	73	77	82	71	64		22.2
62	56	56	46	36	46	43	69	58	69	65	80	57	62	50	61	59	50	69	60	61	18	19.2
80	70	71	71	66	69	70	84	69	85	89	94	85	79	69	69	76	78	84	72	65		22.5
63	57	56	46	37	46	44	70	59	70	64	81	57	62	49	62	60	59	69	60	62	18	19.2
87	71	73	72	67	70	71	85	70	87	89	95	87	80	71	71	77	80	85	76	66		22.5
63	57	56	46	37	47	43	70	59	70	65	81	58	62	50	61	59	50	69	60	62	18	19.2
83	73	76	75	69	74	73	88	73	89	91	98	90	82	73	72	79	82	87	76	67		22.8
64	57	57	46	37	47	44	71	60	71	66	82	58	63	51	62	61	51	70	61	62	18	19.5
84	74	77	76	70	72	74	89	73	90	91	98	90	82	74	73	79	83	88	76	68		22.8

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46 37 47 44 76 68 71 74

45 37 47 43 74 68 71 73

45 37 46 43 74 69 71 73

TES	T (SHE	ET 1	61									•						
													PUMP		MA	NIFC	OLD		YMN
												FL	ow		P	RES	5	PRI	PUT
37	38	39	40	41	42	43	4.4	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
66 88	78 92	57 85	62 78	48 68	61 69	59 73	59 78	68 83	60 71	61 65	18	19.2 22.5	5.5	68 65		38 39	37 35	21	21
65 88	77 91	57 85	62 78	47 68	60 68	58 74	49 77	67 82	59 71	ნ0 63	13	18.9 22.2	5.5	69 65	41 44	39 38	35 35	21	21
63 87	76 79	56 84	61 77	47 66	59 62	58 73	48 76	67 81	58 77	60 63	18	19.2 22.2	5.4	70 65	41 44	39 38	35 35	22	21
64 89	80 93	57 84	62 77	49 68	60 68	58 73	50 77	68 82	59 71	61 64	18	19.2 22.2	5.5	68 65	44 40	38 38	35 35	22	21
65 89	80 94	57 85	62 79	50 69	61 69	59 76	50 78	69 84	60 72	61 65	18	19.2 22.5	5.5	68 65	40 44	38 38	35 35	22	21
64 89	81 95	57 87	62 80	49 71	62 71	60 77	59 80	69 85	60 76	62 66	18	19.2	5.6	68 65	40 43	38 38	35 35	22	21
65 91	81 98	58 90	62 82	50 73	61 72	59 79	50 82	69 87	60 76	62 67	18	19.2 22.8	5.6	68 65	40 43	38 38	35 35	22	21
66 91	82 98	58 90	63 82	51 74	62 73	61 79	51 83	70 88	61 76	62 68	18	19.5 22.8	5.6	68 65	40 43	38 38	35 35	22	21
66 91	82 98	58 90	63 89	51 74	62 73	60 79	51 83	70 88	61 76	62 68	18	19.5 22.5	5.6	68 65	40 43	39 38	35 35	22	21
65 91	81 96	57 90	63 81	50 73	61 72	59 78	50 82	69 88	60 77	62 68	19	19.5 22.8	5.6	69 64	40 43	38 37	34 35	22	21
65 91	81 97	58 90	63 81	50 74	61 74	59 78	50 82	69 87	60 76	62 68	18	19.5 22.8	5.6	72 64	43 43	39 37	36 35	22	21

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DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10	11
12/5/72	16:45	72:56	1950	250	DUMMY TEST	97 97	109 73		113 117		92 111	92 98		103 103		89 101
12/5	17:15	73:26	1950	250	DUMMY TEST	97 97			113 117		92 111	93 98		102 103	121 111	90 101
12/5	17:45	73:56	2400	250	DUMMY TEST	97 97			113 116	86 110	93 111	94 97		103 103	123 109	91 100
12/5	18:15	74:26	2400	250	DUMMY TEST	98 97			113 116		93 110	94 97		104 123	123 110	92 100
12/5	18:45	7 ¹ 4:56	2400	250	DUMMY TEST	98 97	-		113 116	86 109	93 110	94 97		104 103	123 109	91 100
12/5	19:15	75:26	2400	250	DUMMY TEST	97 97		113	113 116	-	110	94 97	105	104 103	123 109	91 100
12/5	20:05	75:56	2400	250	DUMMY TEST	97 94	108	84	lk ar 112 112		92 101			103 96	on por 123 102	90 93
12/5	20:35	76:26	2700	250	DUMMY TEST	97 95			113 113	86 105		94 92	101 99	104 98	124 105	91 95
12/5	21:05	76:56	2700	250	DUMMY TEST	97 95			113 114	86 106	93 106	94 94	102 101		124 106	92 96
12/5	21:35	77 :26	1100	250	DUMMY TEST	97 93		85 108		83 102	90 103	89 90		100 94	118 103	88 93
12/5	22:05	77:56	1100	250	DUMMY TEST	96 92		84 107		82 101		88 88	96 96	99 93	116 102	86 92



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATOR

_8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	3
100 106	_	121 111	89 101		81 74	80 99		94 102	77 91	75 90	80 90	88 88	80 88	88 89	80 90	84 91	78 96	72 92	63 83	56 72	55 76	45 74	
_	102 103	121 111	90 101				84 104			75 90	80 90	77 88	79 88	77 89	79 90	83 91	78 97	72 92	63 84	56 73	56 76	45 74	31 65
	103 103	123 109					86 103			77 89	82 90		81 90	82 91	83 92	87 92	80 98	79 93	64 82	57 71	56 74	46 73	36 68
	104 123	123 110	92 100				86 103		78 89	77 88	83 89	82 89	81 89	82 90	83 91	87 92	80 98	78 93	64 82	57 71	56 74	46 73	
	104 103	123 109	91 100			81 96	86 10 3		78 89	77 88	83 89	82 89	81 89	82 90	83 91		80 97	79 93		58 71	56 74	46 72	-
	103	123 109 on po	100	101	72	81 96	86 103		78 89	77 88	83 89	82 89	81 89	82 90	83 91		81 97	79 93	64 81	58 71	56 74	46 72	
	103	123 102	90		82	80 89	85 9 6		77 82	76 81	82 82	81 81	81 81	80 82	82 84	87 84	79 91	77 85	64 74	58 64	57 66	47 65	37 60
		124 105		96 96			86 98	95 96	78 84	77 83	83 83			82 85		88 87	81 93	80 88	64 76	58 66	57 68	46 67	37 63
		124 106	92 96	96 97	82 67	81 92	86 98	96 97	78 85	77 84	83 85	83 85	82 85	82 86	84 88	88 88	81 94	80 89		58 67		47 68	
	100 94	118 103		92 93	80 65	78 89	81 96	92 95	75 83		77 81	71 75	75 75	70 76	75 77	79 79	73 88	66 79	62 74	56 65	55 67	45 66	
;		116 102		91 92					74 82		76 80	70 74	74 74	69 74	74 76	78 77	72 85			56 65		44 66	



TORY BACK-TO-BACK TEST (SHEET 17)

																				PUMP	
																			FL	ow	
30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS
45 74	37 68	46 71	43 74	70 88	59 72	70 89	65 91	81 96	57 90	62 82	49 73	61 72	59 78	50 82	69 87	60 75	61 68	18	19.5 22.8	5.6	70 64
45 74	37 69	46 71	43 73	70 88	59 72	70 89	65 91	81 97	57 90	62 82	50 73	61 73	59 78	50 82	69 87	60 76	61 68	18	19.5	5.6	69 64
46 73	36 68	46 70	43 71	70 85	60 71	70 88	65 91	83 96	58 88	63 81	51 71	61 71	60 77	50 81	70 85	61 74	62 67	19	19.8 22.8	5.6	69 64
46 73	37 68	46 70	43 71	70 85	60 71	71 88	65 91	83 96	58 88		51 71	62 71	60 77	51 80	69 85	60 74	62 66	18	19.8	5.6	69 64
46 72	37 68	47 70	44 71	70 85	60 71	71 88		83 96	58 88		51 71	62 70	60 77	51 80	69 85	60 74	62 66	18	19.5 22.8	5.6	.69 64
46 72	37 66	47 69	43 71	70 85	60 71	71 88	64 90	83 96	58 88	63 80		61 69	60 77	50 80	70 85	61 74	62 66	18	19.8 22.8	5.6	68 65
47 65	37 60	47 63	43 64	70 79	60 65	70 80	66 85	83 90	59 80	63 74	51 63	62 65	60 71	50 71	69 78	61 68	62 62	19	19.8 22.2	5.4	69 65
46 67	37 63	47 66	44 66	71 80	60 67	71 82	66 87	84 93	59 82	63 80	51 66	62 66	60 71	51 74	70 80	61 70	62 63	19	19.8 22.2	5.4	70 65
47 68		47 66	44 67	70 81		71 84		84 93			51 66	62 67	60 74		70 81	61 71	62 63	19	19.8 22.2	5.4	70 65
45 66		46 64		69 79	58 66	69 82	65 87		57 82	62 76	47 63	60 66	59 72	49 73	68 79	59 74	61 62	18	19.2	5.4	70 65
44 56		45 63		68 79	57 65	68 81	64 87	76 87	56 80	61 74	47 63	59 65	58 71	49 71	67 79	59 68	60 62	18	19.2 22.2	5.4	70 65

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E	ST (SHE	ET	17)								· · · · · · · · · · · · · · · · · · ·							
										-			PUMP		MA	NIF	OLD		MMY
_		1212											ow			RES		PR	PUT ESS
7_	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
1	81 96	57 90	62 82	49 73	61 72	59 78	50 82	69 87	60 75	61 68	18	19.5 22.8	5.6	70 64	40 43	39 37	36 35	22	21
5	81 97	57 90	62 82	50 73	61 73	59 78	50 82	69 87	60 76	61 68	18	19.5 22.8	5.6	69 64	40 43	39 37	35 35	22	21
5 L	83 96	58 88	63 81	51 71	61 71	60 77	50 81	70 85	61 74	62 67	19	19.8 22.8	5.6	69 64	40 43	39 37	35 35	22	21
;	83 96	58 88	63 80	51 71	62 71	60 7 7	51 80	69 85	60 74	62 66	18	19.8 22.8	5.6	69 64	40 43	39 37	36 35	22	21
	83 96	58 88	63 80	51 71	62 70	60 77	51 80	69 85	60 74	62 66	18	19.5 22.8	5.6	.69 64	40 43	39 38	35 35	22	21
	83 96	58 88	63 80	51 71	61 69	60 77	50 80	70 85	61 74	62 66	18	19.8	5.6	68 65	40 43	39 38	35 35	22	21
	83 90	59 80	63 74	51 63	62 65	60 71	50 71	69 78	61 68	62 62	19	19.8	5.4	69 65	41 44	39 38	36 36	22	21
	84 93	59 82		51 66	62 66	60 71	51 74	70 80	61 70		19	19.8 22.2	5.4	70 65	41 44	38 38	36 36	22	21
		58 84	63 77		62 67	60 74	51 76	70 81	61 71	62 63	19	19.8	5.4	70 65	41 44	39 38	35 36	22	21
	77 88	57 82		47 63		59 72	49 73	68 79		61 62	18	19.2 22.2	5.4	70 65	ትስ ትዕ	39 38	36 36	22	21
		56 80		47 63	59 65	58 71	49 71	67 79	59 68	60 62	18	19.2	5.4	70 65	41 44	39 38	36 36	22	21

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DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	
12/5/72	22:35	78:26	1100	250	DUMMY TEST		107 67			82 101	89 101	88 88	96 96	
12/5	23:05	78:56	1950	250	DUMMY TEST		107 67			84 103	90 103	91 90	99 97	10
12/5	23:35	79:26	1950	250	DUMMY TEST		108 68			84 104	91 104	92 91	99 98	1(
12/6	00:05	79:56	1950	250	DUMMY TEST		108 68			85 104	91 105	92 92	99 99	1C 9
12/6	00:35	80:26	1950	250	DUMMY TEST		108 69	84 109		85 104	91 104	92 92	98 99	10 9
12/6	01:05	80:56	1950	250	DUMMY TEST	-	107 69			84 104	91 104	92 92	99 99	10 9
12/6	01:35	81:26	1950	250	DUMMY TEST		108 69	84 109	112 113		91 104	92 92	99 99	10 9
12/6	02:05	81:56	1950	250	DUMMY TEST		108 69			85 104	91 104	92 92	99 99	10 ¹
12/6	02:35	82:26	1950	250	DUMMY TEST		108 69	84 109		85 104	-	92 92	99 99	10 ¹
12/6	03:05	82:56	1950	250	DUMMY TEST		108 69			85 104	92 105	92 92	99 99	101 97
12/6	03:35	83:26	1950	250	DUMMY TEST		108 69	-		85 104	-	92 92	99 99	10 ¹ 97



TABLE XXI. ROLLER GEAR TRANSMISSION TEST

TEMPER

2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	2:
107 67		110 110	82 101	89 101	88 88	96 96	99 93	116 101	86 92			77 88	80 95	91 93	74 81	73 80	75 80	70 73	74 73	69 74	74 76	78 78	7 ; 8;
107 67		111 112		90 103		99 97	101 96	119 103				79 89		93 95	76 83	75 81	79 81	76 79	78 79	75 80	78 82		71 89
108 68		112 112		91 104	92 91		102 97	120 104			81 66	79 90	83 98		76 83	75 82	80 82	76 80	78 80		78 83		7' 9(
L08 58	_		85 104	•	92 92		101 97	120 105	90 95			79 90		93 95	76 84	75 82	80 82		78 81		78 83		71 91
L08 69			85 104		92 92		104 97	120 104		94 95		80 91			76 84	75 83	80 82		78 81	75 81	78 83	83 84	71 91
.07 69			84 104	91 104			104 97	121 105				79 91	83 98		76 84	75 82	79 82	76 81	78 81	75 81	78 83		77 90
.08 69	84 109	112 113	85 104	91 104	92 92	99 99	104 97	120 105	89 95	94 95	81 66	80 91	83 98		76 84	75 83	80 83	76 81		75 81	78 83	83 84	77 90
08 69		112 113	85 104	91 104	92 92	99 99	104 97	121 105		94 95	81 66	79 91	83 98		76 85	75 82	80 82	76 81	79 80	75 81	78 83	84 84	77 90
08 69		112 113	-	91 104	-	99 99	104 97	120 _. 105				80 91	83 98		76 84	75 82	80 82	76 81		75 81	78 83		77 90
08 69		114 113		92 105			104 97	121 105			81 67	80 91	84 98	94 96	76 85	75 83	80 82	76 81	78 81	76 81	78 83	84 84	77 90
28 59	-	114 113	-	91 104	92 92		104 97	121 105		94 95		80 91	84 98		76 84	75 83	80 82	76 81	78 81	75 81	78 83	83 84	78 90



WISSION TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 18)

TEMPERA	TURE (°C)
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21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	4
4 3	69 74	74 76	78 78	72 85	65 77	61 74	56 64	54 67	44 66	36 61		42 64		57 65	68 81	64 85	76 87	56 80	61 74	48 63	59 65	58 70	49 71	
3		78 82		76 89	71 82	62 74	56 65		45 66			43 66			69 81			57 81		49 63	59 66	58 71	49 73	
}		78 83				63 76							69 80		69 82	65 87			62 76		61 66		50 74	
		78 83		77 91	72 83	6 3 76	57 66	56 68	45 67	37 63	46 64	43 66	69 80		69 82	64 87			62 76		60 66		50 74	61 81
		78 83		77 91	72 84	63 76	57 66	56 69				43 66		59 66		65 87		57 82	63 76		60 66	59 71	50 74	6{ 8(
	75 81	78 83				63 76	58 66	56 68	46 66	37 63	47 66	43 66	69 80		69 82	64 88		57 82	63 74		60 66	59 71	-	68 79
	75 81	78 83		77 90	72 84	63 76	52 66		46 66			44 66	69 80	59 67	70 82	65 88	81 91	58 82	63 74	49 65		60 71	50 74	68 80
	75 81	78 83		77 90	72 84	67 76		51 68	46 67	37 66	46 66		69 79	59 66	70 82	65 87	81 90		66 74•		61 66	60 71		68 80
	75 81	78 83		77 90	72 84	61 76	57 66	56 69				44 66	69 80			65 81	81 90	54 82	63 76		61 66		50 74	68 80
	76 81	78 83	84 84	77 90		63 76	57 66	56 69	46 68	38 63	47 66	45 67	69 80	59 67	70 8.3	65 88		57 82	63 75	49 66	61 66	59 71	50 74	68 80
	75 81		83 84	78 90	72 84	63 76	57 66	56 68	46 68	37 63	47 66	44 66	70 80	59 67	70 82	65 87	80 91	58 82	63 76	49 68	61 66	59 74	50 74	68 80

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(TES	T (S	HE	ET 1	8)															
														PUMP		MA	NIF	OLD		MMY
														.ow			PRES		PR	PUT
5	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/I	I R/H	L/H	R/H
ŧ	64 85	76 87	56 80	61 74	48 63	59 65	58 70	49 71	67 78	59 68	60 62	18	19.5 22.2	5.4	70 65	41 44	39 38	35 35	22	21
	64 85	80 90	57 81	62 74	49 63	59 66	58 71	49 73	68 79	59 69	61 63	18	19.1 22.2	5.4	70 65	41 44	39 38	35 35	22	21
	65 87	80 91	57 82	62 76	49 64	61 66	59 71	50 74	68 80	60 70	62 63	18	19.5 22.2	5.4	70 65	41 44	39 38	35 35	22	21
	64 87	80 91	57 82	62 76	49 66	60 66	59 71	50 74	68 80	60 69	62 63	18	19.2 22.2	5.4	69 65	40 44	38 38	35 36	22	21
	65 87	80 91	57 82	63 76	51 65	60 66	59 71	50 74	68 80	60 70	61 63	18	19.5 22.2	5.4	70 65	40 44	39 38	35 35	22	21
	64 88	80 90	57 82	63 74	49 64	60 66	59 71	50 74	68 79	60 70	61 63	19	19.5 22.2	5.4	70 64	42 44	39 38	35 35	21	21
	65 88	81 91	58 82	63 74	49 65	61 66	60 71	50 74	68 80	60 63	62 65	19	19.5	5.4	70 65	40 44	39 38	35 35	22	21
	65 87	81 90			50 64	61 66	60 71		68 80	60 69		19	19.5	5.4	72 64	44 44	39 88	35 35	22	21
	65 81		54 82			61 66	59 71	50 74	68 80	60 68	62 63	19	19.5	5.4	70 64	40 44	38 38	35 55	22	21
	65 88		57 82		49 66	61 66	59 71	50 74	68 80	60 70		19	19.5 22.2	5.4	70 64	40 1414	38 38	3 5 35	22	21
	65 87	80 91	58 82		49 68	61 66	59 74	50 74	68 80	60 71	62 63	20	19.5	5.4	70 64	42 44	40 38	36 35	22	21
					_														ار	

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/6/7 2	34:0 5	83:56	2400	250	DUMMY TEST	98 96			116 114		93 107		101 101	104 99	123 106
12/6	04:35	84:26	2400	280	DUMMY TEST	98 96	_		113 115		94 107	•	101 101	104 99	124 106
12/6	05:05	84:56	2400	250	DUMMY TEST	98 96	71	110	113 115 Walk	107	96 107 ind In	96	101 101 tion	99	123 106 Power
12/6	06:05	85:26	2400	250	DUMMY TEST	96 95		-	111 114	85 106	92 105		99 100	102 99	122 106
12/6	36:3 5	85:56	2400	250	DUMMY TEST	97 95			113 115		93 107	_	101 101	103 99	123 106
12/6	07:05	86:26	2700	250	DUMMY TEST	98 96	109 72		114 115		94 108		102 102	105 100	
12/6	07:35	86:56	2700	250	DUMMY TEST	98 97	73	112		108	94 109	101	102 103	105 101 Power	108
12/6	09:30	86:56	1100	250	DUMMY TEST	96 92	109	84	110	82 102	8train 88 101	88 94	96	98	117 102
12/6	10:00	87:26	1100	250	DUMMY TEST	100 92		-		90 105	97 107		106 103		126 107
12/6	10:30	87:56	1100	250	DUMMY TEST	97 99	76	113	115	89 109	53 111	103	100 103	100	120 110
12/6	11:15	88:26	1100	250	DUMMY TEST	98 95	110	88	112	86 104	92 104	92	fwd. 100 99	103	Dete 121 104



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORAT

	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	•
	101 101	104 99	123 106	91 96	96 96	88 68	81 92	86 100	95 98	78 96	72 84	82 84	81 84	81 85	81 85	83 87	87 88	80 93	78 88	64 77	69 68	67 70	
	101 101	104 99	124 106	91 97	96 97	83 68	82 93	86 100		76 86	74 85	83 85	82 85	82 85	82 86	83 87	88 88	80 93	78 88	64 77	69 68	68 70	
_	101 101 tion	99	123 106 Power	97	•	83 69	82 93	86 100		78 86	77 85	83 85	82 85	82 85	82 86	83 88	87 88	80 93	79 89	64 77	68 68	60 71	
	99 100	102 99	122 106	89 96		80 68	80 92	84 99	94 97	77 86	76 84	80 86	80 84	80 84	79 85	81 87	86 86	79 93	77 88	63 76	68 67	64 71	
-	101 101	103 99	123 106	91 97		81 69	82 92	85 99	95 98	78 87	76 85	82 87	81 85	81 85	80 86	84 88	87 88	81 93	78 89	64 78	69 68	67 71	,
	102 102	105 100		93 98	97 99		82 94	87 100	96 99	79 88	78 87	84 88	84 87	83 88	82 89	85 90	89 90	82 94	82 91	65 78	60 69		1
101	102 103		108	9: 99	97 99	83 71	82 95		96 100	79 89	78 88	85 89	88 89	83 89	84 90	-		82 94	82 91	65 79	60 69	58 72	
88 94	96	-	117 102	86 101	-	75 66	76 89	81 94		77 83	72 80	71 80	66 72	72 71	66 72	70 73	74 75	72 78	64 69	69 70	59 62	58 68	1
97 98	106 103	109 100	126 107	98 107	101 99	87 72	86 93						81 80		79 81	86 82	89 84	85 91		80 78	66 69	66 73	
103		100	110	109		73	96	93	91	80 90	78 90	81 90		78 84	72 84	78 86	81 86	77 95	71 87	73 84		60 79	57
92	100 99		121	91	0n 95 95	81	81	85	95 96			81 83	75 76	78 76	73 77	78 79		78 87	71 79	75 76	62 68	60 71	5



																			_	_			
TA	\:L/	ABC)RA	TO	RY	BA	CK-	TO	-BA	CK	TES	T (S	HE	ET 1	91								
E (º	C)																						
	27	28	29	30	31	32	33	34	35	34	37	38	39	40	41	42	43	44	45	46	47	48	FL TOTAL
<u>'</u> —'		20	27	30	31	32	33	34	33	30		30	37	40			43						
	64 77	69 68	67 70	47 68	39 64	48 66	45 68	71 81	60 68	71 84	66 89	83 93	69 84	64 77	61 66	63 69	51 73	52 77	59 82	61 71	63 66	21	19.5
	54 77	69 68	68 70	47 69	48 65	39 67	45 68	71 82	60 68	71 85	66 89	83 93	69 85	64 77	61 66	62 69	51 74	52 77	59 82	61 71	63 65	21	19.8 22.2
	64 7 7	68 68	60 71	47 74	39 65	48 67	45 68	70 82	60 68	71 85	66 89	83 93	58 84	64 77	61 66	63 69	51 74	52 77	70 82	61 72	63 66	21	19.8 22.2
	63 76	68 67	64 71	47 76	39 63	48 66	45 67	70 70	59 67	70 77	66 79	84 92	50 82	60 78	60 67	61 67	50 74	51 76	69 77	60 71	63 63	21	20.4 22.5
	54 78	69 68	67 71	48 76	39 66	48 68	45 69	70 8∠	60 69	72 84	66 88	84 93	59 84	63 79	63 67	63 69	52 75	53 77	61 82	62 72	62 66	21	21.0 22.5
	65 78	60 69	59 71	48 70	40 66	49 68	46 68	71 82	61 69	72 84	67 89	85 94	60 84	63 77	53 67	64 70	62 74	53 78	70 83	62 72	63 66	21	19.8 22.5
	55 79	60 69	58 7 2	48 71	39 66	50 69	46 69	72 84	61 70	72 86	67 89	85 95	60 85	64 79	53 68	63 70	62 76	52 78	70 84	62 76	63 66	22	20.1 22.5
	69 70	59 62	58 68	48 65	40 59	49 62	47 64	71 76	60 62	71 76	63 77	77 84	60 77	62 65	54 63	62 59	61 62	54 69	69 76	61 63	63 58	23	20.4 22.2
	30 78	66 69		54 71		54 7 0	52 70	81 83			72 87	88 92	69 85	72 77	63 69	72 69	71 74	63 77	73 84	70 72	73 66	23	22.4 22.5
	73 34	61 74	60 79	50 74	41 67		47 74	74 88	63 71	76 87	70 91	81 95			53 69	68 74	66 79		73 86	65 77	68 69	22	79.8 22.5
	75 76	62 68	60 71	50 69	41 66	51 68	48 69	76 80	64 68	77 82	70 87	82 89	65 81	69 74	54 65	69 69	68 71		72 80	67 71	69 64	23	19.8 22.5

S	T (S	HE	ET 1	91															
		-											PUMP		MA	NIFO	LD		YMN
													ow		P	RESS			PUT ESS
1	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
	83 93	69 84	64 77	61 66	63 69	51 73	52 77	59 82	61 71	63 66	21	19.5 22.2	5.4	69 64	40 44	38 38	38 35	22	21
	83 93	69 85	64 77	61 66	62 69	51 74	52 77	59 82	61 71	63 65	21	19.8 22.2	5.6	68	40	38	35	22	21
	83 93	58 84	64 77	61 66	63 69	51 74	52 77	70 82	61 72	63 66	21	19.8 22.2	5.5	68 64	й й 40	38 38	35 35	22	21
	84 92	50 82	60 78	60 67	61 67	50 74	51 76	69 77	60 71	63 63	21	20.4 22.5	5.5	70 65	42 44	39 38	35 36	21	22
	84 93	59 84	63 79	63 67	63 69	52 75	53 77	61 82	62 72	62 66	21	21.0 22.5	5.5	70 64	42 44	39 38	35 35	21	22
	85 94	60 84	63 77	53 67	64 70	62 74	53 78	70 83	62 72	63 66	21	19.8 22.5	5.5	70 64	42 44	39 38	35 35	21	22
	85 95	60 85	64 79	53 68	63 70	62 76	52 78	70 84	62 76	63 66	22	20.1 22.5	5.6	68 65	41 44	39 38	35 35	22	21
	77 84	60 77	62 65	54 63	62 59		54 69		61 63	63 58	23	20.4 22.2	5.4	68 65	ήή ήΟ	38 38	35 35	22	21
	88 92	69 85	72 77	63 69	72 69	71 74	63 77	73 84	70 72	73 66	23	22.4 22.5	5.5	67 65	44 40	39 38	35 36	22	21
	81 95	63 87	68 81	53 69	68 74	66 79	58 80	73 86	65 77	68 69	22	79.8 22.5	5.6	69 65	й й 40	39 38	35 35	22	21
	82 89	65 81	69 74	54 65	69 69	68 71	60 74	72 80	67 71	69 64	23	19.8 22.5	5.6	68 65	38 40	39 38	35 36	22	21

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1				- 4 11	T	Τ-									
DATE	OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	
12/6/72	11:45	88:56	1950	250	DUMMY TEST	99 97	111 74	88 111	114 115	89 107	96 108	96 96		106 100	
12/6	12:15	89:26	1950	250	DUMMY TEST	102 99		90 112	-		97 110	97 99		107 101	
12/6	12:45	89:56	1950	250	DUMMY TEST	101 99	_	91 113			98 110	97 99		108 102	
						St	op	ins	pect	test	t for	ward	sum	shi	p
12/6	15:30	90:26	1950	250	DUMMY TEST	100 97		91 110			96 104	96 94	103 100	106 97	
12/6	16:00	90:56	1950	250	DUMMY TEST	100 97	74	93 110	114		106	95 95	103 101	105 99	1; 1(
:						St	op :	inspe	ect s	train	ners				
12/6	17:30	91:26	1950	250	DUMMY TEST	99 95		86 107			94 101	93 93	100 97	103 95	14
12/6	18:00	91:56	1950	250	DUMMY TEST	100 96		88 108		87 103	94 104	93 94	100 98	103 96	12 10
12/6	18:30	92:26	1950	250	DUMMY TEST	100 96	109 75	0		88 103	95 104	- 1		103 96	12 10
12/6	19:00	92:56	1950	250	DUMMY TEST	100 96	75	89 108	113	88 103		94 94	101 98	103 96	12 10
						S	top :	inspe	ect s						
12/6	20:00	93:26	1950	250	DUMMY TEST	99 95			112 112	88 102		93 93	101 97	104 95	12; 10;
12/6	20:30	93:56	2400	250	DUMMY TEST	100 98			114 114		98 106	96 96	103 100		12! 106



TABLE XXI. ROLLER GEAR TRANSMISSION TEST

TEMPER

2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	4
		114 115							94 106				88 98		83 87	81 86					83 86		8 9
111 76	90 112	115 116	91 108	97 110	97 99	110 103	107 101	127 109	95 109	99 100	85 72	86 95	89 100	98 100	84 89	82 87	86 88		_	83 85	84 87		8 9
	113	117	109	110	99	104	102	110	109	100 101	86 73	86 96	90 101	99 101	85 90	83 89	87 89	83 86	84 86		85 89	89 89	8
)	ins	pect	test	t for	ward	sum	shi	p det	tecto	r													
		116 114								97 96				97 97	83 85	81 81	85 82	88 80	83 80	78 81	84 82	87 83	9
74	110	114	106	106					94 105	98 97				97 98	82 87	80 84	85 85	82 82	81 82		83 85	86 85	8 9
	inspe	ect s	trair	ners																			
			87 102							95 93	81 65				79 82		82 81		79 77		79 80	84 81	8
			87 103					122 104			82 67		85 96	95 96			82 82		79 79	77 79	79 82	84 83	7 9
		113 113						123 103		96 95			85 96	95 96	80 84		83 82		80 79		80 82		7
			88 103		94 94	101 98	103 96	123 104	90 103	96 95	82 66	84 90	85 96	95 96	80 84	78 82	83 82	79 79	80 79	77 80	80 82	85 83	7
) 2	lnspe	ect s	train	ers																			-
	87 107		88 102					123 103		96 93	82 65		85 94	95 94	80 81	77 80	82 81	79 77	80 77	77 78	79 79	84 80	8
16	89 110	114 114					106 99			98 97	84 68		88 99		82 85	79 83	86 84	84 83	83 84	83 84	84 86	89 87	8

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TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 20)

EMPERATURE (°C)

24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	
37 36	82 93	77 86	77 85	63 71	62 74	52 72	43 68	52 71	50 71	78 83	66 71	80 85	73 90	86 93	68 85	71 77	56 68	72 72	70 85	62 77	73 83	69 74	72 67	4
18 18	83 93	78 87	79 80	63 72	63 76			54 71		80 84	68 71	82 87	75 91	86 94	70 85	73 80	57 69	73 75	72 77	65 79	74 85	71 75	74 69	-
9	84 93	79 89	80 80	65 73		-		54 72	-	81 85	69 72	82 88	75 92	87 95	71 87	74 80	58 70		73 78		76 85	72 76	75 69	2
7 3	83 90	78 82	78 76	65 68	63 70		46 65	55 67	51 69	78 86	67 68		73 86		69 81	73 74		72 69	70 71	63 74	75 81	69 71	72 64	
6 5	82 92	76 80	76 78	63 70	62 72	53 71		54 69	50 69	77 82	66 69	78 85	73 90	85 92	68 84	71 79	55 67		70 74	62 76	73 82	69 74	71 67	:
4 1	79 88	73 80	73 72	61 66	60 68	52 67	45 63	52 66	49 66	74 78	64 67	75 81	72 87	83 89	65 79	69 74		69 69	67 71	60 70	72 78	66 71	68 64	
4 3	79 90	72 82	72 74	61 67	60 69		44 65	52 66	49 67	74 79	64 68	75 83		83 90	65 81	69 77		69 71		60 72	72 80	66 72		4
4 3	79 90	73 82	73 74	61 67			44 65	52 66	48 66	74 79			72 90		65 81	69 77	52 63	70 71		60 73	72 80	67 73	69 66	
5 3	79 90	73 82		61 67		52 68	44 66	52 66	49 67	75 80	64 68	76 84	72 90	83 90	65 82	70 76	52 63			61 74	71 80	67 74	69 66	
4 0	79 88	73 79	73 73	61 66	61 68			52 66	49 66	74 78		75 81	71 85	83 88	65 79	69 73	52 62			60 71	71 78	66 70	68 64	
9 7		80 87	75 77	63 68	61 71	53 70	45 66	53 68	50 68	76 81	65 70	77 84	73 90	86 92	66 82	71 77	54 66	70 73	69 74	61 74	72 81	67 74	70 67	

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1	20)															
										PUMP		MA	NIFO	LD		YMN
									FL	ow		P	RESS			PUT ESS
)	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		R/H
L 	56 68	72 72	70 85	62 77	73 83	69 74	72 67	24	20.4 22.5	5.6	68 65	<u>ተ</u> ተ ተ0		35 35	22	21
3	57 69	73 75	72 77	65 79	74 85	71 75	74 69	26	20.4 22.5	5.6	68 65	44 40		35 35	22	21
;	58 70	74 76	73 78	66 80	76 85	72 76	75 69	29	20.4	5.6	68 65	40 44		35 35	22	21
	57 66	72 69	70 71	63 74	75 81	69 71	72 64	29	20.4	5.5	67 65	40 44		35 36	22	27
	55 67	71 71	70 74	62 76	73 82	69 74	71 67	29	20.1 22.5	5.5	67 65	44 40		35 36	22	28
1	51 62	69 69	67 71	60 70	72 78	66 71	68 64	28	19.8 22.2	5.4	68 65	40 44		35 36	22	18
	51 63	69 71	67 72	60 72	72 80	66 72	69 66	29	19.8 22.2	5.4	68 65	40 44		35 36	22	18
	52 63	70 71	67 73	60 73	72 80	67 73	69 66	28	20.1	5.4	68 65	44 40	38 3 38 3	35 36	22	18
	52 63	69 71	68 72	61 74	71 80	67 74	69 66	28	19.8 22.2	5.4	68 65	40 44	38 3 38 3	35 36	22	18
	52 62	69 68	67 70	60 71	71 78	66 70	68 64	28	19.8	5.4	68 65	40 44	38 3 38 3	35 36	22	19
	54 66	70 73	69 74	61 74	72 81	67 74	70 67	29	19.8 22.5	5.5	67 65	40 44	38 3 38 3	35 36	22	19
-							-									

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DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	
12/6/72	21:00	94:26	2400	250	DUMMY TEST	100 97	111 76	90 110	114 114		98 106	-	104 100	106 99	
12/6	21:30	94:56	2400	250	DUMMY TEST	99 97		88 110			97 106		103 101	105 99	
12/6	22:00	95:26	2400	250	DUMMY TEST	99 96 St	74	87 109		89 105	105	93	103 100	105 98 on j	1(
12/6	23:10	95:56	2400	250	DUMMY TEST	97 94	107		111	85	92 103	92 92		102 97	12
12/6	23:40	96:26	2700	250	DUMMY TEST	97 95		85 110	_		93 106		101 100	103 98	
12/7	00:10	96:56	2700	250	DUMMY TEST	97 95		84 110	114 114				101 100	103. 99	12 10
12/7	o:40	97:26	1100	250	DUMMY TEST	97 92		85 107	111 110	83 102	-	88 90	97 96	100 94	11 10
12/7	01:10	97:56	1100	250	DUMMY TEST	97 92			110 110				97 96		11' 10
12/7	01:40	98:26	1100	250	DUMMY TEST	97 92	70	106	110 110	101	101	88	-	92	11(10)
12/7	03:20	98:56	1950	250	DUMMY TEST	94 95	106	81	110 115	82	89	89	97 103	100 100	118
12/7	03:50	99:26	1950	250	DUMMY TEST	95 95		82 110			91 106		96 100	101 98	120



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY

8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
04 00		126 106	94 105	98 97	85 68	85 92	89 99	98 98	82 85	80 84	86 85	85 84		84 84	85 86	89 87	83 93	81 88	75 77	63 69	62 71	53 70	45 66
03 01		_	94 105	98 97	84 68	84 92	88 99	97 98	82 85	80 84	86 85	85 84	82 84	83 84	84 86	89 87	82 93	80 88	75 77	61 68	60 71		42 66
03 00	98	105	93 104 at 2	96	84 68	84 92	87 99	97 97	81 84	79 83	85 84	84 83	82 84		84 86	89 87	82 93	79 87	74 77	61 68	59 70	50 69	41 65
99 99			89 103		81 66	80 90		94 96	78 83	75 81	81 82	80 81		77 81	80 83	84 84	78 91	74 84	70 74	57 66	56 67	47 67	
.00	_	_	91 104		83 67		86 99		79 85	76 83	83 85	84 84		82 85		88 87	81 93	78 88	71 77	58 67	57 68	47 68	38 63
.01 .00	-	123 106	91 105		83 68		91 100	95 97	79 85	77 84	83 85			82 85		•	81 93	79 88	71 77	58 67	52 69		38 63
97 96			87 101	92 93	79 65	78 89	81 94	91 94	76 82	73 81	78 81	71 74	74 74	69 75	73 76	78 78	72 85	65 77	69 74	57 69	55 69	45 66	36 62
97 96			87 100	91 93	79 65	78 88	81 93	91 94	75 82	73 81	77 80	71 73	74 73	69 74	73 75	74 77	72 85	64 77	68 74	56 63	54 66	44 66	36 61
96 95 on	92	101	87 100 : 02:5	92	78 64	77 88	80 93	91 94	74 82	72 80	76 79	70 73	72 73	69 74	73 75	77 77	72 85			-	54 66		35 61
	100	118		92	78 71	77 94	82 98	91 99	75 88	73 86	78 86	75 83	76 83	73 84	75 86	80 87	75 92	69 85		55 74	54 71	44 69	35 63
96 .00	101 98		88 105		80 69		83 98	93 98	77 86	74 85	79 85	76 82	76 82	74 82	76 85	84 86	77 93	71 88	68 81	56 70	54 72		35 66



ACK TEST (SHEET 21) PUMP DUMA MANIFOLD INPU PRESS FLOW PRES MAIN L/H R/H L/H R TOTAL ROLLER PRESS 5 36 37 42 43 44 45 46 47 5 78 20.1] D 84 5.4 22.2 19.8 22.2 5.4 19.8) 84 22.2 5.4 19.8 22.2 5.4 19.8 5.4 22.2 19.8 5.4 22.2

19.2 22.2 5.3 19.2 65 21.9 5.3 19.2 21.9 5.3 19.8 83 86 22.5 5.6 19.5 22.5 5.5

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
12/7/72	04:20	99:56	1950	250	DUMMY TEST	96 95	-		114 114	_	92 106	-		103 98	12 10
12/7	04:50	100:26	1950	250	DUMMY TEST	96 94	-		113 114		93 105			103 98	12 10
12/7	05:20	100:56	1950	250	DUMMY TEST	96 94			113 114		93 105	•		103 98	12 10
12/7	05:50	101:26	1950	250	DUMMY TEST	97 94	71	110	113 114	105	93 106	92	100	104 98	12; 10;
12/7	07:10	101:56	1950	250	DUMMY TEST	93 92	105	80			88 105	87 92	94	-	11(10!
12/7	07:40	102:26	1950	250	DUMMY TEST	93 93	-	81 110			88 106		95 100		116
12/7	08:10	102:56	1950	250	D UMM Y TEST	96 93		85 111		88 106	95 108		104 101	106 100	126 106
12/7	08:40	103:26	1950	250	DUMMY TEST	99 95		88 112		91 109			108 103		130 109
12/7	09:10	103:56	2400	250	DUMMY TEST	100 96		88 115			105 113		109 105		130 111
12/7	09:30	104:16	2400	250	+		_			ct Fa				em	
12/7	15:00	104:56	2400	250	DUMMY Test	96 98		85 115	114 118		105 113		105 106	107 105	127 112



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORAT

TEMPERATURE (°C)

	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	
	-		103 98		90 105		81 68	80 91	84 97	94 97	78 85	75 84	81 83	78 80		74 80		84 84	78 91	72 84	69 77		51 69	
				123 105	-		82 68	80 91		95 98	78 85	76 84	82 84	79 81	80 80	77 81	79 84	34 85	78 91	72 84	70 77	57 71	55 69	
				123 105			82 68	80 91		95 98	79 85	76 84	82 84	79 81	78 80	77 81	79 84	84 85	79 91	73 84	70 77	57 71	55 69	
				123 105			82 68		86 98	95 97	79 84	76 84	82 84	79 81	79 80	77 81	79 84	84 84	79 91	72 84	70 77	57 71	56 69	
n	ers 37	94	98	116		89	76 67			89		70	76 83	73 81	73 80	71 80	72 83	78 84	73 90	67 82	62 77	53 65	51 68	
	92	99	97	105	104	96	67	91	91	97	04	02	03	01	00	00	03	04	90			02	00	
ŀ				116 105		90 96	77 68	76 92		89 97	72 85	70 84	76 84	73 81	73 81	71 81	73 84	78 85	73 91	67 84	63 77		51 68	
i				126 106		99 98	83 70	82 93	88 100	98 99	83 87		84 85	82 83		80 82		87 86	81 92	76 85	72 79	60 68		
,			110 102	130 109	98 108		88 72		92 101		87 89	84 88	89 87	86 85	87 85	85 85		92 88	86 94	82 88	78 80	63 69		
3	100 100	109 105	111 104	130 111	100 110	102 102	88 74	86 97	93 104	102 103	88 91	85 90	92 90	89 90		88 90			87 98	87 93	79 82	64 70		
	ty Pi		e m																					
	14:20																12.21							
; }	97 101	105 106	107 105	127 112	96 111	99 104	84 75	83 97	89 104	99 103	86 92		86 91	86 90		81 90		90 92	85 98	82 93	83 82		63 77	

(h)

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<u> </u>	JK/	410	RY	BA	CK	-10	-BA	CK	TES	ST (S	SHE	ET 2	22)									0.45
																					-	PUMP
8	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	OW ROLLER
;2 '1	51 69	45 68	36 62	46 66	41 66	71 82	60 67	71 82	66 86	81 91	59 84	63 74	50 66	62 74	61 74	53 76	70 75	61 81	64 74	18	19.8 22.5	5.5
;7 '1	55 69	45 68	35 62	46 66	41 66	71 82	60 67	72 82	66 86	81 91	59 84	63 72	50 68	62 75	61 74	53 76	71 71	61 71	64 62	18	19.8 22.5	5.5
7	55 69	45 67	35 62		41 66	71 81		72 82		82 91		63 72		63 74	61 75		71 71	61 71	65 63	17	19.8 22.5	5.5
7	56 69	45 68	35 62		41 66	72 81		72 82	66 86	82 91	60 84	64 72		63 74	62 75	53 76	62 71	65 71	65 63	17	19.8 22.5	5.5
3 5	51 68	41 66	33 60	42 65	38 65	65 80		66 81		76 91	54 81	58 73	43 64	57 67	56 69	47 73	65 80	57 70	59 62	17	19.2 22.2	5.4
3 6	51 68	41 67	32 61	42 65	38 65	65 81	55 66	66 82	63 85	76 91	54 82	58 73	43 65	58 68	56 70	48 75	65 81	57 70	59 62	16	19.5 22.2	5.4
3	58 66	47 68	36 62	47 66		74 82	62 68	75 84	66 86	84 93	62 84	64 76	57 67	64 68	63 71	55 77	72 82	63 71	67 63	18	21.0 22.5	5.5
3	62 71	50 70	38 63	50 68	45 68	79 84	67 70	81 85	70 88	88 94	67 86	70 76	60 69	70 70	68 72	60 79	76 84	68 73	73 64	18	21.0 22.5	5.6
)	63 74	52 72	39 65	51 70	45 70	81 86	68 71	82 87	72 89	91 98	68 88	71 77	61 71	70 70	69 74	61 80	76 86	69 76	74 66	18	24.0 22.5	5.6

21.0

22.8

5.7

70 79 72 81 87 76

57 79 77 73 68 76

0

67 85 70 71 82 84 88 73 72 98 89 79

37 50 43 83 67 71 72 87

2 63 51 3 77 74

ES	T (S	HE	ET 2	22)				- 77											
													PUMP		M	ANIFO	OLD		MMY
													ow			PRES		PA	IPUT ESS
7	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAI	1 L/H	R/H	L/H	R/H
;	81 91	8ր 26	63 74	50 66	62 74	61 74	53 76	70 75	61 81	64 74	18	19.8 22.5	5.5	69 65	41 44	39 38	35 35	22	19
5	81 91	59 84	63 72	50 68	62 75	61 74	53 76	71 71	61 71	64 62	18	19.8 22.5	5.5	69 64	40 44	39 38	35 35	22	19
; r	82 91	60 84	63 72	50 68	63 74	61 75	53 71	71 71	61 71	65 63	17	19.8 22.5	5.5	69 64	## #0	39 38	35 35	18	22
5	82 91	60 84	64 72	50 66	63 74	62 75	53 76	62 71	65 71	65 63	17	19.8 22.5	5.5	69 64	41 44	39 38	35 35	22	19
5	76 91	54 81	58 73	43 64	57 67	56 69	47 73	65 80	57 70	59 62	17	19.2 22.2	5.4	73 65	43 44	42 38	37 35	22	20
3	76 91	54 82	58 73	43 65	58 68	56 70	48 75	65 81	57 70	59 62	16	19.5 22.2	5.4	74 65	43 43	41 38	37 35	23	20
5	84 93	62 84	64 76	57 67	64 68	63 71	55 77	72 82	63 71	67 63	18	21.0 22.5	5.5	69 65	41 43	39 38	36 35	21	19
3	88 94	67 86	70 76	60 69	70 70	68 72	60 79	76 84	68 73	73 64	18	21.0 22.5	5.6	68 65	41 43	39 38	36 35	21	19
2	91 98	68 88	71 77	61 71	70 70	69 74	61 80	76 86	69 76	74 66	18	24.0 22.5	5.6	79 65	48 43	46 37	42 35	24	21
'n	ŖŔ	72	72	57	70	77	70	70	72	75	20	21.0		70	42	40	36	22	19
O 14	88 98	73 89	72 79	57 73	79 68	77 76	70 81	79 87	72 76	67		22.8	5.7	65	44	38	37		

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
12/7/72	15:30	105:26	2400	250	DUMMY TEST	98 99	111 75		-	-	106 112			108 104	12
12/7	16:00	105:56	2400	250	DUMMY TEST	98 98	111 74			89 110	106 111	-		107 103	12 11
12/7	16:30	106:26	2700	250		97 98	109 74			88 111	108 112			106 104	12 11
12/7	17:00	106:56	2700	250	DUMMY TEST	97 98	109 74	115	117	111	109 112	100	106	105 105	12 11
12/7	18:10	107:26	1100	250		95 93	107 69	85	109		97 104		98	101 96	11 10
12/7	18:40	107:56	1100	250		96 93	109 69			84 104			99 100	102 96	12 10
12/7	19:10	108:26	1100	250		96 93	109 68			84 104	101 106	91 95		102 96	12 10
12/7	19:40	108:56	1950	250		95 94	109 69			86 106	105 108	_	102 101	105 99	12
12/7	20:10	109:26	1950	250		95 93	109 68	-	_	86 106			102 101	105 98	12 10
12/7	20:40	109:56	1950	250	DUMMY TEST	95 93	109 68			86 106				105 99	12 10
12/7	21:10	110 :26	1950	250		94 94	109 69			86 107	104 108	-	101 101		12



TABLE XXI. ROLLER GEAR TRANSMISSION TEST

TEMPER

2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	2
L11 75		-	-	106 112	-			128 111						100 103	87 92		88 91	87 89	85 89	84 90	88 92	92 92	8
111 74				106 111				128 110						100 103	86 91	85 90	88 90	86 89	85 89	84 90		90 92	8
.09 74				108 112	97 100	104 106	106 104	126 111	95 110	99 103	85 74	83 97	89 105	98 103	84 92	83 90		87 91	84 91	85 92		89 94	9
.09 74	115	117	111	112	100	106	105	125 111	110	103	84 74	82 97	88 105	97 103	83 92	80 91			83 91	84 92	86 94	88 94	8 9
_								r at	•				_								_		and the second
.07 69	110	109 113	83 104	97 104	90 94	98 99	101 96	118 104	91 103	93 95	79 67	78 91	82 95	93 96	78 85	75 83	79 82	73 75	77 75	70 77	76 78	80 79	7
.09 69	-			100 106				120 105					83 96	96 97	78 86	75 85	79 83		77 77	71 78	76 79	80 80	7
.09 68				101 106			102 96	120 105	91 104	94 96	81 68		83 96	96 97	78 86	75 85	80 82	74 77	77 77	71 78	76 80	80 80	7
09 69				105 108				123 106		97 98				99 99	80 88	77 86	83 85	80 83	80 82	77 83		86 86	8
09 68	83 110	113 113	86 106	105 107	94 94	102 101	105 98	124 106	91 ₁ 105	97 97	82 69	80 92	86 99	97 98	80 87	77 86	83 84	80 82	80 82	77 82	81 85	86 85	<u>د</u> د
09 68		113 114		104 107				124 106					86 99	99 98	80 87			8∂ 82		77 82		86 85	\$ 6
09 69		112 114						123 107					86 99		80 88	77 87	83 85	79 83	79 83	77 83	81 86	85 86	1 0

B

TRANSMISSION TEST DATA; LABORATORY BACK-TO-BACK TEST (SHEET 23)

TEMPERATURE (°C)

19	20	21	22	2 23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	
88 91				88 92	92 92	86 98	82 93	84 82	62 72	63 76	51 74	37 67	50 71	43 71	85 87	68 71	86 90		89 98	74 89	74 80	58 71	81 71	
88 90			84 90	86 92	90 92	85 97				62 75	50 73		49 70	43 71		67 71			88 97	71 89	71 74	57 71	79 69	7
86 91			85 92		89 24	84 98	82 94	79 82	59 72	61 76	49 74			42 71		64 71				69 89	70 81	55 72	76 70	
86 92	86 91		84 92	86 94	88 94	83 99	81 95	76 82	59 73	58 76	47 74			46 72	76 88	63 71	78 91	67 91	86 99		66 80	54 73	71 70	6 7
79 82	73 75	77 75	70 77	76 78	80 79	75 88	68 79	69 76	56 66	58 68	47 68	34 62	45 64	40 66	71 80	59 65	71 84	63 85	80 89	60 82	61 74	53 65	65 63	
79 33	74 77	77 77	71 78	76 79	80 80	75 89	69 80	70 77	56 66	57 69	46 68		45 65	40 66	71 82	59 66	72 85	63 88	80 90	60 84	61 77		65 64	
30 32	74 77	77 77	71 78	76 80	80 80	75 89	69 80	70 77	56 66	57 70	45 68		44 65		71 81	59 66	71 85	62 88	80 90	59 84	60 77		64 65	
}3 }5			77 83		86 86	80 89	75 85	70 78	57 68		45 69				71 83	60 68	72 87	62 89			61 77	54 68	65 68	6 7
13 14	80 82	80 82	77 82	81 85	86 85	80 93	74 86	69 79	57 68	58 70	46 69	32 63	44 66	40 68	71 84	59 68	71 87	62 89	83 93	59 85	60 77	54 68	64 68	6
<u>3</u>			77 82	81 85	86 85	80 93	74 86	67 79	57 68		46 69		44 66		71 84	59 68	71 87	61 89	83 93	59 86	60 77	54 68	64 67	
3 5	79 83	79 83	77 83	81 86	85 86			64 79			45 68		44 66		70 84	59 68	70 87	61 89		58 86		53 68	63 68	6

B

TES	ST (S	SHE	ET a	23)															
													PUMP			ANIFO			MMY
37	38	39	40	41	42	43	44	45	46	47	48		ROLLER	PRESS		PRES: N L/H		PI	RESS R/H
72 93	89 98	74 89	74 80	58 71	81 71	78 77	71 81	81 87	74 76	76 68	19	21.0 22.8	5.6	70 65	41 44	40 38	36 35	22	19
70 92	88 97	71 89	71 74	57 71	79 69	77 76	69 81	79 87	72 76	73 67	18	21.0 22.5	5.6	70 65	41 44	40 38	36 35	22	20
69 91	86 99	69 89	70 81	55 72	76 70	74 77	66 81	78 87	70 76	71 68	18	21.0 22.5	5.6	71 65	42 43	40 38	37 35	22	19
67 91	86 99	66 90	66 80	54 73	71 70	69 77	62 82	77 88	67 76	68 67	17	21.0	5.6	71 65	42 43	41 38	37 35	22	20
63 85	80 89	60 82	61 74	53 65	65 63	63 70	55 68	70 81	61 69	61 63	17	22.8 22.5	5.5	82 65	49 44	48 38	43 36	25	22
63 88	80 90	60 84	61 77	52 66	65 64	64 73	55 76	71 82	62 70	62 63	16	20.4 22.5	5.5	72 65	42 44	41 38	37 36	23	20
62 88	80 90	59 84	60 77	52 66	64 65	62 73	55 76	70 81	61 69	61 62	15	20.4	5.5	72 65	42 44	41 38	37 36	23	20
62 89		60 85	61 77	54 68	65 68	63 72	55 77	71 82	62 70	61 63	15	20.4	5.5	72 65	42 44	41 38	38 36	23	20
52 39	83 93	59 85	60 77		64 68	62 74	54 78	71 84	61 71	61 64	14	21.0	5.6	72 65	42 41	41 38	37 36	23	20
61 89	83 93	59 86	60 77	54 68	64 67	62 73	53 78	71 83	61 70	59 63	15	21.0 22.5	5.6	72 65	43 44	42 38	37 36	23	20
51 39	82 93	58 86	59 77	53 68	63 68	62 73	52 77	70 84	60 71	58 63	14	21.0 22.5	5.6	73 65	43 44	42 38	38 36	23	20

and the same of
NUMBER OF STREET

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/7/72	21:40	110:56	1950	250	DUMMY TEST	95 93	109 68		112 114	86 106	105 107	94 93	101 100	104 98	12: 100
12/7	22:10	111:26	1950	250	DUMMY TEST	95 94	-		112 114	86 106	106 108	94 95	101 102	104 99	12; 10;
12/7	22:40	111:56	1950	250	DUMMY TEST	94 94			112 115		105 108	94 95	101 101		12: 107
12/7	23:10	112:26	1950	250	DUMMY TEST	94 93			113 115		106 108	95 95	102 102	104 100	_
12/7	23:40	112:56	1950	250	DUMMY TEST	94 94	-		112 115		106 108	94 95	101 101		123 107
12/8	00:10	113:26	1950	250	DUMMY TEST	94 93			112 114		106 108	95 94	102 101		123 107
12/8	00:40	113:56	2400	250	DUMMY TEST	94 93	_		112 114		107 108	95 95	101 102		123 107
12/8	01:10	114:26	2400	250	DUMMY TEST	94 94				85 108		-	101 103	103 101	_
12/8	01:40	114:56	2400	250	DUMMY TEST	93 94			111 115	85 108	106 109	94 96	100 103	103 101	
12/8	01:55	115:11	2400	250	DUMMY TEST	93 94			111 115		106 109		100 103	103 101	
12/8	05:30	115:11	2400	250	DUMMY TEST	St 94 96		82	shi 112 115	86	106 107		100 102	103 100	123 107



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY BA

9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
	123 106	93 105	96 97	82 68		86 98	97 98	79 87	77 85	83 84	80 81	80 81	77 82	81 85	85 85		74 86	64 79	56 68	57 70	45 69	31 63	44 66
	123 107	-	-		80 95			79 88		83 85			77 83		85 86	79 93	74 86			57 70		31 63	44 66
	123 107		95 98		80 93			79 88		83 85	80 83	80 83	77 83	81 86	86 86	80 93	74 86	64 78	56 68	57 70		31 63	44 66
	123 107	93 106			80 93		97 99	79 88		83 85	80 83		77 83				74 85		56 68	57 70	-	31 63	
		93 106			80 93			80 88		82 85	80 83		77 83			80 93	74 86			57 70		32 63	
	123 107	93 106				86 99	97 99	79 88	78 86	82 85	80 82	81 82	77 82	81 86		80 93	74 86	64 79	55 68	57 70		31 63	41 6:
		93 106					97 99	79 88	77 87	83 86	82 85		80 86		86 88	81 94	78 90	63 79	56 68	56 71		31 63	
		92 108								82 87			79 87		85 90	80 95	76 90	63 79	55 68	56 71		31 63	
103 101	122 108	92 107	95 99	81 70	79 94	85 102	97 100	77 89	76 88	82 87	81 86	80 86	79 87	82 89	85 90	79 95	75 90	63 79	55 68	56 71	44 69	30 63	
103 101	122 108	92 107	95 99	81 70	79 94	85 102	9 7 100	77 89	76 88	82 87	81 86	80 86	79 87	82 89	85 9 0	79 95	75 90	63 79	55 68	56 71		30 63	
	123 107	92 106	96 99	80 69	80 93	86 100	95 100	77 87	76 86	82 86	82 85	80 85	79 85	82 87	86 89	81 94	78 89		57 67	59 70	47 69	33 62	4



ACK	TEST	SHEET	24
	11	Manage 1	77.77

سسبي															PUMP		MA	NIFC	die	DUI	MM
															ow			RESE	1	PR	PUT ESS
5	30	37	36	30	40	41	4.2	43	44	45	48	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	RA
442 647	77; 1:-	1.1 83	## ##	4£ 00	55 Pr	S.C.	33	8. 73	45	75 81	50 73	58 84	1,	22.5 22.5	5.8	73 65	43 44	43 38	37 36	23	50
44.	FY:	51 31	81 93	55 He	est,	5% 68	5.5 5.6	£.	~ (70 81	50 70	55 55	74	23.0 22.5	5.8	72 65	և <u>ց</u> <i>և</i> և	42 38	37 36	55	50
4	77	5). 34;	81: 33:	\$\\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	5	5.5 5.5	t.: në	: :	· ·	775 S.s.	50	5.5	14	21.0 22.5	5.6	72 65	4.3 կե	42 38	38 36	23	20
	-y -	56		ξιξ 21ξ	** <u>\$</u>	5 <u>£</u>	6.5 6.5	S.,	***	77; 54.	60	58 63	11.	21.0 22.5	5.6	72 65	113 113	42 38	38 36	22	20
	7:	30 50	\$£ \$ 3	5 5 57	50	5.1 5.1	t.;		%. ~.¢	23	50 71	5\$ 63	٦٤.	22.5	5.6	72 65	43 44	42 38	38 36	55	50
	77:	51. 34.	9 : 9 :	5.5 Se	55	51	£1.	50	5. 4.	70 St	60 70	58 83	14	21.0 22.5	5.6	72 65	43 44	42 38	38 36	82	20
	7: 58	5() 5()	\$ 3 55	57	4.8 77	63	53		51	52	<0 *:	57 65	11	21.0 22.5	5.6	72 65	43 44	4 <u>1</u> 38	37 36	52	50
	t 3 55	\$ 3 3 C	34 04	\$ T	58 77	5.2	63	60	50 70	65	40 71	57 63	14	20.7 22.5	5.6	72 65	43	41 38	37 35	55	20
	69 58	53 30	32 04	50 31	57 77	52	61 63	60		53	\$8 11	57	: 1	20.7 22.5	5,6	73 65	43	41	38 35	55	50
	69 88	59 90	82 95	50 57	51 78	52 69	61 68	60	50	68	58 71	57 64	1 h	20.7 22.5	5.6	73 65	43 43	41 38	38 35	55	20
	71 81	6.2 85	\$3 93	60	61 76	53	64	6.°	52 15	70 80	61 70	60	16	20.7 22.5	5.5	70 66	42 44	40	37 35	23	50

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DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
12/8/72	06:15	115:56	2400	250	DUMMY TEST	94 93				8 6 108	107 109	93 95			
12/8	06:45	116:26	2700	250	DUMMY TEST	94 95					108 110	94 95		_	_
12/8	07:15	116:56	2700	250	DUMMY TEST	93 95					109 112	94 99			
12/8	08:50	117:26	1100	250	DUMMY TEST	96 92					109 106	94 95	103 100		12; 10;
12/8	09:20	117:56	1100	250	DUMMY TEST	96 92					109 105	94 96	102 99	105 96	
12/8	09:50	118:26	1100	250	DUMMY TEST	97 92					109 105	94 96	102 99	105 96	
12/8	10:20	118:56	1950	250	DUMMY TEST	97 93				90 107	112 109	98 95	-		
12/8	10:50	119:26	1950	250	DUMMY TEST	98 93				90 107					
12/8	11:20	119:56	1950	250	DUMMY TEST	98 95					113 109	99 95			
12/8	11:50	120:26	1950	250	DUMMY TEST	98 94					113 109	99 95			
12/8	12:20	120:56	1950	250	DUMMY TEST	98 94					113 109	99 95			
	12/8/72 12/8 12/8 12/8 12/8 12/8 12/8 12/8	DATE OF DAY 12/8/72 06:15 12/8 06:45 12/8 07:15 12/8 09:20 12/8 09:50 12/8 10:20 12/8 11:20 12/8 11:50	DATE DAY TEST TIME 12/8/72 06:15 115:56 12/8 06:45 116:26 12/8 07:15 116:56 12/8 08:50 117:26 12/8 09:20 117:56 12/8 09:50 118:26 12/8 10:20 118:56 12/8 10:50 119:26 12/8 11:20 119:56 12/8 11:50 120:26	DATE OF DAY TEST TIME INPUT H.P. 12/8/72 06:15 115:56 2400 12/8 06:45 116:26 2700 12/8 07:15 116:56 2700 12/8 08:50 117:26 1100 12/8 09:20 117:56 1100 12/8 10:20 118:26 1100 12/8 10:50 119:26 1950 12/8 11:20 119:56 1950 12/8 11:50 120:26 1950	DATE OF DAY TEST TIME INPUT H.P. H.P. 12/8/72 06:15 115:56 2400 250 12/8 06:45 116:26 2700 250 12/8 07:15 116:56 2700 250 12/8 08:50 117:26 1100 250 12/8 09:20 117:56 1100 250 12/8 09:50 118:26 1100 250 12/8 10:20 118:56 1950 250 12/8 10:50 119:26 1950 250 12/8 11:20 119:56 1950 250 12/8 11:50 120:26 1950 250	DATE DAY TEST TIME INPUT H.P. H.P. 12/8/72 06:15 115:56 2400 250 DUMMY TEST 12/8 06:45 116:26 2700 250 DUMMY TEST 12/8 07:15 116:56 2700 250 DUMMY TEST 12/8 08:50 117:26 1100 250 DUMMY TEST 12/8 09:20 117:56 1100 250 DUMMY TEST 12/8 09:50 118:26 1100 250 DUMMY TEST 12/8 10:20 118:56 1950 250 DUMMY TEST 12/8 11:20 119:26 1950 250 DUMMY TEST 12/8 11:50 120:26 1950 250 DUMMY TEST 12/8 11:50 120:26 1950 250 DUMMY TEST	DATE OF DAY TEST TIME INPUT H.P. H.P. H.P. 1 12/8/72 06:15 115:56 2400 250 DUMMY TEST 93 12/8 06:45 116:26 2700 250 DUMMY TEST 95 12/8 07:15 116:56 2700 250 DUMMY TEST 95 12/8 08:50 117:26 1100 250 DUMMY TEST 96 12/8 09:20 117:56 1100 250 DUMMY TEST 92 12/8 09:50 118:26 1100 250 DUMMY TEST 97 12/8 10:20 118:56 1950 250 DUMMY TEST 93 12/8 10:50 119:26 1950 250 DUMMY TEST 98 12/8 11:20 119:56 1950 250 DUMMY TEST 98 12/8 11:50 120:26 1950 250 DUMMY TEST 98 12/8 11:50 120:56	DATE OF DAY TEST TIME INPUT H.P. H.P. H.P. H.P. TEST H.P. H.P. TEST H.P. H.P. TEST H.P. H.P. TEST H.P. J. 2 12/8/72 06:15 115:56 2400 250 DUMMY TEST H.P. 94 109 70 70 70 70 70 70 70 70 70 70 70 70 70	DATE DAY TEST TIME INPUT H.P. H.P. H.P. H.P. H.P. H.P. H.P. H.P	DATE OF DAY TEST TIME INPUT H.P. H.P. H.P. 1 2 3 4 12/8/72 06:15 115:56 2400 250 DUMMY TEST 94 109 82 112 12/8 06:45 116:26 2700 250 DUMMY PS 94 108 82 112 116 116 2700 250 DUMMY PS 94 108 82 112 116 116 116 2700 250 DUMMY PS 94 108 82 112 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 117 116 117 117 116 117 117 117 117 117 117 117 117 117 117 117 117 117 117 118 118 118 118 118 118 118	DATE OF DAY TEST TIME INPUT H.P. H.P. 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H.P. 1 2 3 4 5 6 7 8 12/8/72 06:15 115:56 2400 250 DUMMY TEST 94 109 82 112 86 107 93 100 12/8 06:45 116:26 2700 250 DUMMY TEST 94 108 82 112 86 108 94 101 12/8 07:15 116:56 2700 250 DUMMY TEST 93 109 82 112 86 108 94 101 12/8 08:50 117:26 1100 250 DUMMY TEST 96 112 86 113 88 109 94 103 12/8 09:20 117:56 1100 250 DUMMY TEST 96 110 87 113 87 109 94 102 12/8 09:50 118:26 1100 250 DUMMY TEST 97 11	DATE OF DAY TIME N.P. N.P.



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LAB

5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
5 6 08	107 109	93 95		_	124 107	92 107	96 99	81 70			95 100	78 88	76 87	82 87	81 85	81 86	80 85	82 88	86 89	80 94	77 89	64 79	57 68
86 09	108 110				123 109					86 102	96 100	78 89	77 88		82 88	81 88	81 89	83	87 91	81 96	80 91	63 79	56 69
86 11	109 112	•			124 111	-				87 105		78 92	77 90		84 90	82 90		84 93	88 93	81 99	81 94	64 82	56 71
88 05	109 106	-			123 105		97 96	83 69		87 96		82 86	79 84	83 85	77 77	80 77	74 79	80 80	83 80	80 90	72 80	73 77	60 68
87 .04	109 105	-			123 104			82 69		87 96		82 85	79 84	83 84	78 77	81 77	75 78	81 80	85 80	80 90	73 80	73 77	59 68
87 .04	109 105	•			123 105				81 91	87 96		82 85	79 83	83 83	77 77	81 77	75 78	81 80	84 80	80 89	73 80	72 77	59 68
90 .07	112 109	98 95	-		127 107		100 99			91 100		84 87		88 87	88 82	85 82	82 83	85 86	90 84	85 93	80 86	72 79	61 69
90 .07	113 109	98 95			128 108		101 99			91 100		85 88			85 83		82 84	86 86	90 85	85 92	80 87	71 79	61 69
9 1 107	113 109	99 95	107 102	109 101	128 108	98 107	101 99	87 71	84 95	92 100	101 100	86 89	83 87	88 88	85 83	86 84	83 84	86 87	91 85	86 93	8 <u>1</u> 87	70 80	6 <u>1</u> 70
	113 109				128 108					91 101		86 88		88 87	85 83	86 84	83 84	86 87	91 85	86 93	81 88	70 80	61 71
	113 109			109 101	128 108	98 107				91 101		86 88		88 87	86 83	86 84	83 84	86 87	91 85	86 93		70 80	

T DATA: LABORATORY BACK-TO-BACK TEST (SHEET 25)

RA	TU	RE	(9	(C)
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25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
80 94	77 89	64 79	57 68	57 70	45 69	32 62	44 65	40 67	70 83	58 68	70 85	61 88	83 94	58 85	58 77	52 67	63 66	60 73	51 78	69 83	60 71	58 63	15
81 96	80 91		56 69	56 72			44 67		70 84		69 87		83 95		58 78		62 67	60 74	51 79	69 84	59 72	58 64	14
81 99	81 94		56 71	57 75			44 69		70 87		70 84		83 99	57 84	57 79	54 73	63 69		52 82	70 82		58 66	15
80 90	72 80			61 70			47 65		75 81	62 66	75 84	63 86	83 90		63 74	58 66			57 75	74 81	63 75		16
80 90	73 80	73 77	59 68	61 70			47 65			62 66		63 87	83 90	62 83		57 66			57 76	74 81	64 69	63 62	16
80 89	73 80	72 77	59 68	61 70			47 66			62 66		63 86	83 90			57 66	67 70			73 81	63 69		15
85 93	80 86		61 69	63 72			48 67			64 68			87 93	62 84		60 68	68 67	66 73	58 78	76 82	64 76	_	16
35 92	80 87	71 79	61 69	62 72			48 67	43 69		64 68	76 85	63 87		62 85	65 77	61 68	68 68	66 72	57 78	76 83	65 71	-	16
36 93	81 87	70 80	6 <u>1</u>	63 73	50 72	35 65	49 68	43 70		63 68			88 94	63 85	64 77	61 69	68 68		58 79		65 71		17
36 93	81 88	70 80		63 73	50 71	35 66	49 67	43 69		64 68			88 94			61 69		67 74	57 79	76 84	65 71	63 66	16
36 93	81 87		62 70	63 73			48 68			63 68		63 88	86 94	63 86	65 77	61 69			57 79	76 84	65 78	63 65	17

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ST (ST (SHEET 25) PUMP MANIFOLD DUMMY																		
												PUMP				DUMMY			
00	20	40	4.9	40	40			4.0	.=	4.5	FLOW TOTAL ROLLER PRESS			PRESS MAIN L/H R/H			PRESS		
38	39	40	41	42	43	44	45		47	48		ROLLER	PKE33				L/H	R/H	
83 94	58 85	58 77	52 67	63 66	60 73	51 78	69 83	60 71	58 63	15	20.4 22.5	5.5	70 65	44 42	40 38	36 35	23	20	
83 95	57 87	58 78	52 69	62 67	60 74	51 79	69 84	59 72	58 64	14	20.4 22.5	5.6	71 65	ሰተ ተ5	40 38	37 35	23	20	
83 99	57 84	57 79	54 73	63 69	61 76	52 82	70 82	60 74	58 66	15	20.7 22.8	5.7	71 65	42 43	40 38	37 35	23	20	
83 90	62 83	63 74	58 66	68 64	66 70	57 75	74 81	63 75	63 62	16	21.3	5.5	71 65	42 44	41 38	37 35	22	20	
83 90	62 83	63 76	57 66	67 66	65 71	57 76	74 81	64 69	63 62	16	21.ú 22.5	5.5	70 65	## #5	41 38	37 35	22	20	
83 90	61 82	63 74	57 66	67 70	64 70	56 76	73 81	63 69	63 62	15	21.0	5.5	70 65	44 44	40 38	37 35	22	20	
87 93	62 84	65 77	60 68	68 67	66 73	58 78	76 82	64 76	63 63	16	21.3 22.5	5.6	70 65	42 44	40 38	37 35	21	19	
88 93	62 85	65 77		68 68	66 72	57 78	76 83	65 71	63 63	16	21.3 22.5	5.6	70 65	42 44	40 38	37 35	21	19	
88 94	63 85	64 7 7	61 69	68 68	66 74	58 79	77 84	65 71	63 64	17	21.6 22.8	5.6	70 65	42 44	40 38	37 35	21	19	
88 94	63 85	64 77	61 69	69 68	67 74	57 79	76 84	65 71	63 66	16	21.6 22.8	5.6	70 65	42 44	40 38	37 35	21	19	
86 94	63 86	65 77	61 69	68 68	66 74	57 79	76 84	65 78	63 65	17	21.6 22.5	5.6	70 65	14 14 14 14 14 14 14 14 14 14 14 14 14 1	40 38	37 35	21	19	
					-			_		_							-		

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10	
12/8 /72	12:50	121:26	1950	250	DUMMY TEST		112 73		116 115		113 109	-	106 103		128 108	
12/8	13:20	121:56	1950	250	DUMMY TEST				117 116		123 110		107 103	99 102	128 109	
12/8	13:50	122:26	1950	250	DUMMY TEST				117 116	92 109				110 102		
12/8	14:20	122:56	1950	250	DUMMY TEST					91 109	113 111			109 102		:
12/8	14:50	123:26	1950	250	DUMMY TEST					91 109	113 110		106 105	109 103	128 110	:
12/8	15:20	123:56	2400	250	DUMMY TEST				117 118		115 113		108 107		130 112	
12/8	15:50	124:26	2400	250	DUMMY TEST		-		113 117	88 111			103 107	105 105	125 112	1
12/8	16:20	124:56	2400	250	DUMMY TEST				111 118			-		103 105	123 111	1
12/8	16:50	125:26	2400	250	DUMMY TEST				112 117					104 105	123 112	
12/8	17:20	125:56	2400	250	DUMMY TEST				112 117					104 105	123 112	
12/8	17:50	126:26	2700	250	DUMMY TEST				113 118						124 112	; 11



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY BACK

TEMPERATURE (°C)

																								٠,
9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	3
)9)1	128 108	-	101 100	88 71	84 95		101 100	85 89	83 87	89 88	85 84	86 84	83 85	87 87	91 86	86 93	81 88	70 80	62 70	63 73	51 72	36 66	48 68	7
)9)2	128 109	-	101 100	85 72	84 95		101 100			88 89	86 85	86 85	84 85	87 88	92 87	86 94	81 89	71 81	62 71	63 74	51 73	36 66	48 69	7
)2 [0	129 110		102 101	85 73	85 95		102 101		85 88	89 90	86 86		84 85	87 88	92 87	87 94	81 89	71 81		63 75	51 73	37 67	50 70	4
)9)2	128 110	•	101 100	87 73	84 96		101 101		83 88		85 85	85 85	83 86	86 88	90 87	85 94	81 89	70 81	61 72	63 75	51 73	37 66	49 70	4
)9)3	128 110	98 110		87 73	84 96	91 102	101 102	85 91		88 90	85 86	85 86	83 86	86 89	91 87	86 94		70 82		63 76		37 67	49 70	4
10 05	130 112		102 103	86 75	85 98		101 5103		84 91	90 91	88 90		87 90	90 93	95 93	88 98	86 94	72 82		63 77	51 74	37 68	50 70	4
05 05	125 112	95 111		84 75	82 98	87 106	97 104	80 93	79 92	86 93	84 91	84 91	82 91	84 94	89 94	83 99	81 94	66 84	59 74	60 77	49 75	46 68		4
03 05	123 111	92 110	95 103	81 75	80 98	85 105	95 103	78 92	76 91	82 92	81 90	81 90		81 93	85 93	80 9 9	78 94	64 83	57 74	58 77	47 74	35 67		4
04 05	123 112	92 111	95 102	82 74	81 98	85 105	95 103	78 92	76 91	82 9 2	82 90	81 90	79 91	83 93	86 92	80 99	77 94	63 84	57 74	57 77			45 70	
	123 112						96 103	78 92	77 91	83 9 2	83 90	81 90	81 91	83 93	86 93	80 99	78 94	63 84	57 74	57 77	47 75		46 71	4 7
	124 112							79 93	77 92	83 94	85 92	83 92	83 93	85 95	88 95 1		81 96	64 84	57 74	58 78	47 76	35 69	46 71	1

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												PUMP				OLD		MMY
												.ow			RES		PR	ESS
8	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/I	I R/H	L/H	R/H
38 94	63 85	65 77	61 69	68 68	66 74	56 79	76 84	65 71	63 65	17	21.6 22.8	5.6	70 65	42 44	40 38	37 35	21	19
38 15	63 87	64 78	62 70	69 69	67 74	57 80	76 84	65 73	63 66	17	21.6	5.6	70 65	42 44	40 38	37 35	21	19
9	63 87	66 79	62 71	69 70	67 75	57 81	77 85	66 74	64 66	18	21.6 22.8	5.6	69 65	42 44	40 38	37 35	21	19
7 5	63 88	66 79	60 70	68 70	67 76	56 81	75 85	64 74	63 67	18	21.3 22.8	5.6	69 65	42 44	40 38	37 35	21	19
7 5	63 89	65 79	60 66	68 70	66 76	56 81	76 86	65 80	63 67	18	21.3	5.6	69 65	42 44	40 38	37 35	21	19
3	63 90	66 79	63 7 2	69 71	67 76	58 82	77 87	66 76	64 67	18	24.0 22.8	5.7	78 65	48 43	46 38	42 35	24	21
;	60 90	64 81	56 73	66 71	64 78	54 82	72 88	62 76	61 68	19	23.1 22.8	5.7	79 65	48 43	47 38	42 35	25	22
}	58 90	62 80	54 73		62 77	53 82	70 88	61 76	59 68	18	22.8	5.7	80 65	48 43	47 38	42 35	25	22
	58 89	61 79	52 73	63 71	61 77	52 82		60 76	59 68	18	20.7 22.8	5.7	71 65	42 43	41 38	37 35	22	20
	58 90	62 80	52 73	63 72	62 77	52 82	70 88	60 76	59 68	18	20.4	5.7	71 65	42 43	41 38	37 35	22	20
		62 82	52 74	63 71	61 79	53 83	70 89	61 76	60 69	18	20.4	5.7	71 65	42 43	40 38	37 35	22	20

D

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
12/8/72	18:20	126:56	2700	250	DUMMY TEST	96 98	•	116	113 118	112		100	•	104 106	14 11
12/8	19:20	127:26	1100	250	DUMMY TEST	99 93	110	91	- Ins 112 112	89	108 103	94	102	0n Pot 105 94	12 10
12/8	19:50	127:56	1100	250	DUMMY TEST		110 74		113 114		108 107	93 103	101 101	104 98	12 10
12/8	20:20	128: 26	1100	250	DUMMY TEST	97 94	110 74	-	113 114	•	108 107	93 103	101 101	104 98	12 10
12/8	20:50	128:56	1950	250	DUMMY TEST	99 98	112 76	-	116 117		112 111		105 105	109 103	12
12/8	21:20	129:26	1950	250	DUMMY TEST	99 98	113 76	-	116 117	-	112 112		106 106	109 104	12' 11:
12/8	21:50	129:56	1950	250	DUMMY TEST	100 98	110 78		113 118	-	109 113	95 101	102 107	105 105	12; 11;
12/8	22:20	130:26	1950	250	DUMMY TEST	98 98	108 77		112 116		107 109	-	100 103	103 101	12] 10{
12/8	22:50	130:56	1950	250	DUMMY TEST		107 77		111 116		106 109		100 103	102 101	120 109
12/8	23:20	131:26	1950	250	DUMMY TEST		107 76		110 115		106 108		99 103	102 101	120 108
12/8	23:50	131:56	1950	250	DUMMY TEST		107 76		110 115		105 108		99 102	102 100	120 108



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BA

TEMPERATURE (°C)

9	10	11	12	13	14	1;	5 16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	_
	124 112	03	96	82	82	87	96 104	79 93	77	83	8 5 93	82	83	85 96	89		81 96	63 85	57 75	47 78	47 76	35 69	46 72	•
Pos	er a	t 18	:50																					
	123 103			86 66	84 90	86 94	97 95		79 83		80 74			82 76			74 78	67 74	60 66	62 68	51 68	38 62	50 63	
	121 105						96 98	80 88	78 87		76 79	79 99	73 80	79 80	82 82	78 88	70 81	67 78	60 70	60 72	49 71	37 66	49 68	
	121 106					85 97	96 98	80 88	78 87	81 85	76 79	79 79		79 81		78 91		67 79	60 70		49 71		49 68	
3	127 110				-	90 102		84 92			84 86			86 89		85 96		70 82	62 73	63 77	52 75	39 68	51 71	
)	127 111					91 103		85 92			84 87			86 90		85 96		70 83	63 74	64 78	53 76	39 68	51 76	
;	123 113					87 104		80 94	89 92	85 92	80 88	82 88		83 92		81 96	75 91	66 85	60 76	61 79	51 77	40 71	51 74	
;	121 108	-		82 72		85 101		78 90	77 89	81 88	77 84	78 84		80 88	84 88	79 93	73 87	64 79	59 71	59 74	50 72	40 67	50 69	•
	120 109	92 108 :		81 72				77 90	76 88	80 88	76 84	78 84	73 84	79 87	82 87	78 93	72 87	64 80	59 71	60 74	50 72	40 68	50 69	1
	120 108			81 71				77 89		80 87	76 83	79 83	73 84	79 87	82 87	78 93	73 87	64 79	59 69	59 74	50 74	40 68	50 68	1
	120 108			81 71				77 89	76 87	79 87	75 83	79 83	73 83	78 86	82 86	78 93	72 87	64 79	58 69	59 73	50 74	39 68	49 68	1



ES	T (SHE	ET 2	27)															
													PUMP		N	ANIF	OLD		MMY
												FL	ow			PRES	S		PUT ESS
7	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MA	N L/I	H R/H	L/H	R/H
?	84 101	59 91	62 82	52 74	64 72	62 78	53 84	70 89	61 77	60 68	19	20.4 22.8	5.7	70 65	41 43	40 38	36 35	22	20
) 	84 88	62 82	66 76	54 63	68 66	66 73	56 74	73 80	65 69	63 63	20	22.8 22.2	5.4	80 65	48 44	46 38	42 36	25	22
	82 92	60 85	63 79	56 69	65 69	64 76	55 77	72 82	63 71	61 66	20	21.0 22.8	5.6	70 65	42 44	40 38	36 36	22	20
	82 92	60 85	63 79	56 69	65 69	64 76	55 79	72 84	63 72	61 66	20	21.0 22.8	5.6	70 65	42 44	40 38	36 36	22	20
	87 96	63 90	66 81	60 73	68 92	67 79	57 82	75 88	65 76	64 68	22	21.3	5.7	69 65	41 43	39 38	36 36	21	19
	87 96	64 90	67 82	61 74	69 73	67 79	58 82	76 88	66 77	64 69	22	21.3 22.8	5.7	69 65	41 43	39 38	36 36	21	19
	84 99	62 91	66 82	54 74	68 74	66 79	57 84	72 89	64 77	62 71	25	21.0	5.7	70 64	42 43	40 38	37 35	21	19
	82 94	60 88	63 82	53 69		64 79			63 74	61 68	24	21.0 22.5	5.6	72 65	42 43	40 38	37 35	22	19
	82 94	60 87	63 81	54 69	66 72	65 78	55 79	70 85	63 74	62 68	25	22.8 22.5	5.6	80 65	48 43	46 38	42 36	25	21
	81 94	60 87	64 79	54 68	66 71	63 77	55 79	70 85	62 76	62 71	25	22.8 22.5	5.6	80 65	48 43 :	46 38	42 36	25	21
	81 93	60 87	63 79	53 68	65 71	63 77	55 79	70 85	62 77	62 71	25	22.5 22.5	5.6	80 65	48 43	46 38	42 36	25	21

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	_1
12/9/73	24:20	132:26	1950	250	DUMMY TEST	98 94	108 75	87 111	112 114		107 107	-	100 101	103 99	
12/9	0:50	132:56	1950	250	DUMMY TEST	98 96	108 76	88 110			106 107		100 101	103 99	
12/9	01:20	133:26	1950	250	DUMMY TEST	98 96	108 76	88 110			106 107		100 101	103 99	
12/9	01:50	133:56	2400	250	DUMMY TEST	98 96	77	87 112	115	108	108	96	101 103	104 101	
12/9	05:40	133:56	2400	250	DUMMY TEST	98 97	110	_13.1		88	109 108	94	101 105	104 102	
12/9	06:10	134:26	2400	250	DUMMY TEST	108 97	120 78	98 112		101 108	122 108		116 103	118 101	-
12/9	06:40	134:56	2400	250	DUMMY TEST	97 98	106 79	88 112			106 109		99 102	102 100	
12/9	07:10	135:26	2400	250	DUMMY TEST	97 98		88 112	110 116		105 109		99 103	102 102	
12/9	07:40	135:56	2400	250	DUMMY TEST	97 99	106 79	88 113			106 110		99 105	102 102	
12/9	08:10	136:26	2700	250	DUMMY TEST	97 99		88 115			107 112		100 105	102 104	
12/9	08:40	136:56	2700	250	DUMMY TEST	97 100		88 115 - In	118	111	107 113	100	100 106	103 105	



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABOR

TEMPERATURE (°C)

6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	25
107 107		100 101		121 107	91 106	95 98	82 70	81 93	84 98	9 5 98	77 88	76 87	80 86	76 82	79 82	73 82	79 86	82 86	78 93	72 87	64 79	59 69	59 74
106 107		100 101		120 107	91 106		81 70	81 93		95 98	77 88	76 86	79 85	76 81	78 81	74 82	79 85	82 85	78 93	72 85	63 79	59 71	59 73
106 107		100 101			91 106			81 93		95 98	77 88	76 86	79 85	76 81	78 81	74 82	79 85		78 93		63 79	59 69	59 73
108 109 Shii	96	101 103	104 101						86 101	96 100	78 89	77 87	81 87	80 85	80 85	78 86	82 88	85 89	80 95		64 80	59 69	59 74
109 108	94	101 105	104 102					82 95		96 101		78 86	76 86		79 83	74 85	78 86	82 87	81 91		69 78	63 71	64 74
122 108		116 103	118 101				96 71	93 95		110 100	94 89	93 87	97 88	96 86	96 87	94 87	98 89	102 90	97 95	93 90	77 79	72 71	73 73
106 109	-	99 102	102 100		92 107			81 95		94 100	77 89	76 87	81 87	79 85	80 86	76 86	80 87	83 89	80 94	76 89	63 78	59 70	59 72
105 109		99 103	102 102					81 95		94 101			80 88	78 86	79 86	74 86	79 89	83 90	79 95	75 89	63 79	58 76	58 79
106 110	92 98	99 105	102 102			94 101	81 72	81 96	83 1 0 2	93 101	76 90	75 89	80 89	78 87	80 87	74 87	78 90	83 90	79 96	75 90	63 80		58 74
107 112	93 100	100 105	102 104				82 73			95 103		76 90			81 90				81 98			53 73	
LO7 L13 aine						95 103				96 103		76 90			82 91			86 94	81 98		63 81	53 73	_



				28)															
													PUMP		MAI	NIFO	LD		YMN
												FLO	ow		P	RESS			PUT
37	38	39	40	41	42	43	44	45	46	47	48	25 20.7		PRESS	MAIN	L/H	R/H	L/H	R/H
65 91	81 93	60 87	64 79	52 68	66 71	63 77	55 78	70 85	62 77	61 71	25		5.6	71 65	44 42	41 38	38 36	22	20
65 91	81 93	60 87	63 80	51 68	65 72	63 78	55 79	69 85	62 74	61 68	25	20.7 22.5	5.6	70 65	42 44	40 38	36 36	22	20
65 91	81 93	60 87	63 80	51 68	65 72	63 78	55 79	69 85	62 74	61 68	25	20.7 22.5	5.6	70 65	## #5	40 38	36 36	22	20
65 91	83 95	61 87	64 79	53 70	65 71	63 77	55 79	70 85	62 77	61 71	25	20.4 22.8	5.6	70 65	42 44	40 38	36 36	22	19
65 81	84 93	64 84	66 73	63 70	67 68	66 70	58 77	75 82	66 71	65 64	29	24.0 23.1	5.7	76 65	46 43	44 38	41 35	23	20
73 90	97 95	73 85	76 80	62 67	78 73	76 77	66 78	80 84	75 75	73 68	29	23.1 22.8	5.5	77 65	47 44	45 38	41 35	24	20
66 89	83 94	61 84	64 79	53 67	66 71	63 76	56 77	70 83	62 74	62 67	27	22.5 22.8	5.5	80 65	48 44	46 38	42 35	25	21
		60 85	63 80	52 68	65 70			69 84	62 74	60 68	27	22.5 22.8	5.6	80 65	48 44	47 38	42 35	25	21
	82 95	60 87	63 80	52 69	65 71	63 77	55 79	69 84	62 76	60	27	22.5 22.8	5.6	80 65	14 14 14	47 38	42 35	25	22
66 90	83 98	60 88	64 81	53 70	65 72	63 79	55 80	69 86	62 76	61 68	27	22.8 22.8	5.6	80 65	14 149	47 38	42 35	25	22
			64 82	53 71	65 73	63 79	55 80	69 86	62 77	61 69	27	22.8 22.8	5.6	80 65	49 44	47 38	42 35	25	22
	65 91 65 91 65 91 65 91 65 81 73 90 66 89 66 90 66 90 66	65 81 93 65 81 93 65 83 91 95 66 83 89 94 66 82 90 95 66 83 90 98 66 83	65 81 60 91 93 87 65 81 60 91 93 87 65 81 60 91 95 87 65 84 64 81 93 84 73 97 73 97 73 90 95 85 66 83 61 89 94 84 66 82 60 90 94 85 65 82 60 90 94 85 66 83 60 90 98 88 66 83 60	65 81 60 64 79 65 81 60 63 91 93 87 80 65 81 60 63 91 93 87 80 65 83 61 64 91 95 85 80 66 83 61 64 89 94 84 79 66 82 60 63 90 94 85 80 65 82 60 63 90 94 85 80 66 83 60 64 90 98 88 81 66 83 60 64 66 83 60 64 66 83 60 64	65 81 60 64 52 91 93 87 79 68 65 81 60 63 51 91 93 87 80 68 65 83 61 64 53 89 94 84 79 67 66 82 60 63 52 90 95 87 80 68 65 82 60 63 52 90 94 85 80 68 65 82 60 63 52 90 94 85 80 68 65 82 60 63 52 90 94 85 80 68 65 82 60 63 52 90 94 85 80 68 65 82 60 63 52 90 95 87 80 69 66 83 60 64 53 60 64 53 60 64 53	65 81 60 64 52 66 91 93 87 79 68 71 65 81 60 63 51 65 91 93 87 80 68 72 65 81 60 63 51 65 91 93 87 80 68 72 65 83 61 64 53 65 91 95 87 79 70 71 65 84 64 66 63 67 81 93 84 73 70 68 73 97 73 76 62 78 90 95 85 80 67 73 66 83 61 64 53 66 89 94 84 79 67 71 66 82 60 63 52 65 90 94 85 80 68 70 65 82 60 63 52 65 90 95 87 80 69 71 66 83 60 64 53 65 90 98 88 81 70 72	65 81 60 64 52 66 63 91 93 87 80 68 72 78 65 83 61 64 53 65 63 91 93 84 73 70 68 70 77 66 83 61 64 53 66 63 89 94 84 79 67 71 76 65 82 60 63 52 65 63 90 94 85 80 68 70 77 66 83 60 64 53 65 63 90 98 88 81 70 72 79 66 83 60 64 53 65 63 90 98 88 81 70 72 79 66 83 60 64 53 65 63 90 98 88 81 70 72 79 66 83 60 64 53 65 63	65 81 60 64 52 66 63 55 91 93 87 79 68 71 77 78 65 81 60 63 51 65 63 55 91 93 87 80 68 72 78 79 65 83 61 64 53 65 63 55 81 93 84 73 70 68 70 77 78 66 82 60 63 52 65 63 55 90 94 85 80 68 70 77 78 66 83 60 64 53 65 63 55 90 98 88 81 70 72 79 80 66 83 60 64 53 65 63 55 90 98 88 81 70 72 79 80 66 83 60 64 53 65 63 55 90 98 88 81 70 72 79 80	65 81 60 64 52 66 63 55 70 91 93 87 79 68 71 77 78 85 65 81 60 63 51 65 63 55 69 91 93 87 80 68 72 78 79 85 65 83 61 64 53 65 63 55 70 91 95 87 79 70 71 77 79 85 65 81 93 84 73 70 68 70 77 82 73 87 80 67 73 77 78 84 66 83 61 64 53 66 63 56 70 77 83 84 66 82 60 63 52 65 63 55 69 90 94 85 80 68 70 77 78 84 66 82 60 63 52 65 63 55 69 90 94 85 80 68 70 77 78 84 66 82 60 63 52 65 63 55 69 90 95 87 80 68 70 77 78 84 66 82 60 63 52 65 63 55 69 90 94 85 80 68 70 77 78 84 66 82 60 63 52 65 63 55 69 90 95 87 80 69 71 77 78 84 66 83 60 64 53 65 63 55 69 90 98 88 81 70 72 79 80 86 66 83 60 64 53 65 63 55 69 90 98 88 81 70 72 79 80 86	65 81 60 64 52 66 63 55 70 62 91 93 87 79 68 71 77 78 85 77 65 81 60 63 51 65 63 55 69 62 91 93 87 80 68 72 78 79 85 74 65 83 61 64 53 65 63 55 70 62 91 95 87 79 70 71 77 79 85 77 66 81 93 84 73 70 68 70 77 82 71 73 95 85 80 67 73 77 78 84 75 66 82 60 63 52 65 63 55 69 62 90 94 85 80 68 70 77 78 84 74 65 82 60 63 52 65 63 55 69 62 90 95 87 80 68 70 77 78 84 76 66 83 60 64 53 65 63 55 69 62 66 83 60 64 53 65 63 55 69 62 66 83 60 64 53 65 63 55 69 62 66 83 60 64 53 65 63 55 69 62	65 81 60 64 52 66 63 55 70 62 61 91 93 87 79 68 71 77 78 85 77 71 65 81 60 63 51 65 63 55 69 62 61 91 93 87 80 68 72 78 79 85 74 68 65 81 60 63 51 65 63 55 69 62 61 91 93 87 80 68 72 78 79 85 74 68 65 81 60 63 51 65 63 55 69 62 61 91 93 87 80 68 72 78 79 85 74 68 65 83 61 64 53 65 63 55 70 62 61 91 95 87 79 70 71 77 79 85 77 71 65 84 64 66 63 67 66 58 70 77 82 71 64 73 97 73 76 62 78 76 66 80 75 73 90 95 85 80 67 73 77 78 84 75 68 66 83 61 64 53 66 63 55 69 62 60 90 94 85 80 68 70 77 78 84 74 68 66 66 82 60 63 52 65 63 55 69 62 60 90 94 85 80 68 70 77 78 84 74 68 66 82 60 63 52 65 63 55 69 62 60 90 95 87 80 69 71 77 79 84 76 66 66 83 60 64 53 65 63 55 69 62 61 66 83 60 64 53 65 63 55 69 62 61 66 83 60 64 53 65 63 55 69 62 61 66 83 60 64 53 65 63 55 69 62 61 68 66 83 60 64 53 65 63 55 69 62 61	65 81 60 64 52 66 63 55 70 62 61 25 91 93 87 79 68 71 77 78 85 77 71 665 81 60 63 51 65 63 55 69 62 61 25 91 93 87 80 68 72 78 79 85 74 68 68 91 93 87 80 68 72 78 79 85 74 68 68 91 93 87 80 68 72 78 79 85 74 68 68 68 72 78 79 85 74 68 68 68 72 78 79 85 74 68 68 68 72 78 79 85 74 68 68 68 72 78 79 85 74 68 68 68 72 78 79 85 74 68 68 68 72 78 79 85 77 71 65 84 64 66 63 67 66 58 75 66 65 29 81 93 84 73 70 68 70 77 82 71 64 68 68 67 73 77 78 84 75 68 68 67 73 77 78 84 75 68 67 73 77 78 84 75 68 67 73 77 78 84 75 68 67 73 77 78 84 74 67 67 71 78 79 85 85 80 67 73 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 74 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 68 70 77 78 84 76 68 68 70 99 98 88 81 70 72 79 80 86 76 68 76 68 78 78 78 80 69 71 77 79 80 86 76 68 76 68 70 99 98 88 81 70 72 79 80 86 76 68 76 68 70 77 78 78 78 78 78 78 78 78 79 79 79 80 86 76 68 70 77 78 78 78 78 78 78 79 79 79 80 86 76 68 70 77 79 80 86 76 68 70 70 70 70 70 70 70 70 70 70 70 70 70	37 38 39 40 41 42 43 44 45 46 47 48 TOTAL 65 81 60 64 52 66 63 55 70 62 61 25 20.7 91 93 87 79 68 71 77 78 85 77 71 22.5 65 81 60 63 51 65 63 55 69 62 61 25 20.7 65 81 60 63 51 65 63 55 69 62 61 25 20.7 65 81 60 63 51 65 63 55 69 62 61 25 20.7 22.5 65 83 61 64 53 65 63 55 70 62 61 25 20.7 22.8 65 84	37 36 39 40 41 42 43 44 45 46 47 48 TOTAL ROLLER 65 81 60 64 52 66 63 55 70 62 61 25 20.7 22.5 5.6 65 81 60 63 51 65 63 55 69 62 61 25 20.7 22.5 5.6 65 81 60 63 51 65 63 55 69 62 61 25 20.7 22.5 5.6 65 81 60 63 51 65 63 55 70 62 61 25 20.7 22.5 5.6 65 81 60 63 51 65 63 55 70 62 61 25 20.7 22.5 5.6 65 83 61 64 53 65	Flow Total Roller Press Flow Total Roller Press Flow Total Roller Press Flow Total Roller Press Flow Flow	Flow PRESS MAIN	FIOW PRESS MAIN L/H	State Stat	FLOW PRESS MAIN L/H R/H L/H



DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/9/72	09:40	136:56	1100	250	DUMMY TEST	98 95	107 73	89 110	-	85 103		89 91	97 98	100 95	11 10
12/9	10:10	137:26	1100	250	DUMMY TEST	99 97	107 75	91 112	110 115	88 107	106 107	92 96		102 99	12 10
12/9	10:40	137:56	1100	250	DUMMY TEST	98 98	106 75	90 112	109 116	85 107	103 108	89 102		100 100	10
12/9	11:10	138:26	1100	250	DUMMY TEST	98 97	106 75	90 112		84 107		89 105		99 100	10
12/9	11:40	138:56	1950	250	DUMMY TEST	97 100	107 77	89 115		87 111		92 100	-	102 103	12: 11:
12/9	12:10	139:26	1950	250	DUMMY TEST	98 100	108 77	89 115		88 112		93 102		102 104	122 112
12/9	12:40	139:56	1950	250	DUMMY TEST	97 100	108 77	89 115	111 119	88 112	106 113	93 100	100 106	102 105	122
12/9	13:10	140:26	1950	250	DUMMY TEST	97 100	108 78	89 115	11). 119		106 114	93 100	100 106		122
12/9	13:40	140:56	1950	250	DUMMY TEST	98 100		89 115		88 112		93 100	100 107		122 112
12/9	14:10	141:26	1950	250	DUMMY TEST	98 101		89 115		88 112		93 100	100 107		122 112
12/9	14:40	141:56	1950	250	DUMMY TEST	98 100		89 115		88 112		93 100	100 107		122



TABLE XXI. ROLLER GEAR TRANSMISSION TEST

TEMPERA

5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
85 103		89 91		100 95		89 103	92 95	78 67	79 90		92 95	78 85	75 82	75 82	70 73	75 73	68 75	73 76	77 77	72 84
) 88 ; 107		92 96	100 102	102 99		92 107		82 72		83 99	93 99	79 89	78 87	82 87	75 80	79 80	73 81	79 82	83 83	78 91
) 85 5 107		89 102	97 102	100 100		89 107		80 72	80 94	81 99	02 100	87 90	83 89	88 89	82 80	87 80	70 81	74 83	80 84	74 92
3 84 5 107		89 105		99 100	117 108		91 99	79 72		80 99	91 100		73 89	77 87	71 80	75 80	69 81	73 82	78 83	73 92
1 87 8 111		92 100		102 103	121 111		-			84 103				81 91	77 86	78 86	76 87	77 90	83 91	
1 88 9 112		93 102	100 105	102 104		91 111				84 104					78 87	79 87	77 88	78 91	83 89	79 96
1 88 9 112		93 100		102 105	122 112	92 111				84 104	94 103	78 93		82 92	78 87	80 87	76 88	78 91	84 91	79 96
1 88 9 112		93 100	100 106			92 112		81 75		84 104	94 103			82 92	78 87	78 87	76 89	78 91	84 91	79 96
1 88 9 112		93 100	100 107	-	122 112					83 105					78 87	79 87	76 89	78 92	83 91	79 96
.1 88 .9 112	106 114	93 100	100 107	102 105		92 112	95 104	82 75	82 99		94 104	78 93	77 92	82 92	78 87	79 87	77 89	78 92	83 91	79 96
.1 88 .9 112	106 114	93 100		102 105		92 112				84 105		78 93	77 92	82 92	78 87	79 88	76 89	78 92	83 92	79 96
_																				

B

													1112									PU
																						QW
28	29	30	31	32	3 3	34	35	36	37	38	39	40	41	42	43	44	45	10	47	48	TOTAL	ROLL
63 68	64 TO	54	45 95	55.0	50 58	79	25 26	.5	22	76 37	11	52 70	52	23	50	-16 -1	10	52 59	93	28	23.7	-
ól 71	02 74	52 72	-2 o7	52	-3 -1	*2 34		72	-10 -58	12	35	7c 30	50	00 10	2	***	-14	25	24	27	22.0	100
59 72	59 76	51	-1	50	+0	70 35	20 	-9	15	73	30 37	33 31	32		23	-5	.9	52 '5	12	707	22.5	3.4
58 71	30 15	50 74) -9	50	÷0	35	:0	· 0	.5 ?1	***	: -	3	59	12	3	73	:d	:2 75	3 <u>1</u> 39	on i	22.5	
50 74	20	51 75	+1 70	51 2	47 75	10 32	5 <u>1</u>	-0	.3	12 16	.0	34	3	25	:0	50.0	73 33	02	23	***	22.5	
50 76	20 -8	71	-1	51 3	-7	39	*	<u>-</u>	-3	:2	-0	. 4	73	.0	·0	.3	:9	63.93	23	207	22.5	~ _ ;
i0 16	20 79	51 77	+2	50 73	-7 -5	39	51 75	.5	.3	-2 38	:1 :0	34	***	°5	00	36 32	TO 39	(4) (2)	25.	77	22.5	ns.
10	70 73	51	.T.	51	4.7 76	10 39	3 <u>1</u>	·2) <u>†</u>	:2	: <u>1</u>	34		70 75)4)1	50 12	19	23	52 71	25	22.5	*** ***
0 8	20	51	+2	***	+7	10 39	:2 *5	:2	14	.2	:0	54		30 75	31	-0	†g	33 77	n2 *2	26	22.8	
9	20	51	12	51	-7 -5	*9	72 75	32	34 34	:2 :8	10	34	100	o5 *5	30	56	T0 39	03 79	.5	18	22.5	-
9	00 7g	51 77	12	51	47 76	70	32 15	72	30	:2 35	o <u>1</u>	25 34	33	75	24 31	50	70	23 23	25	25	22.8 22.6	5.

L

TE	ST (S	SHE	ET	291									•						
													PUMP		M	NIFC)LD		MMY
												FL	.ow		9	PRES	5		PUT
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
62 79	76 87	62 81	62 70	52 63	63 64	62 68	56 71	70 79	62 69	63 63	28	23.7 22.5	5.5	82 65	50 44	48 38	43 36	25	22
68 90	82 92	63 85	67 80	53 68	68 70	66 77	57 77	71 84	65 74	64 68	27	22.8 22.8	5.6	92 65	40 44.	48 38	43 36	25	22
66 92	79 93	60 87	63 81	52 70	65 73	63 79	55 79	69 85	62 76	62 70	27	22.5 22.5	5.6	82 65	49 44	47 38	43 35	25	22
6 5 91	78 93	60 87	6 3 81	5 0 69	64 72	6 3 78	54 79	68 85	62 76	6 1 69	27	22.5 22.5	5.6	82 65	49 44	47 38	43 36	25	22
66 93	82 96	61 90	64 84	53 71	66 75	64 80	56 82	70 88	62 77	63 71	27	22.5	5.6	82 65	49 44	47 38	43 35	25	22
67 93	82 98	61 90	64 84	53 72	66 77	63 80	56 82	70 89	63 78	63 72	27	22.5 22.5	5.6	82 65	49 44	47 38	43 35	25	22
66 93	82 98	61 90	64 84	53 73	66 76	64 80	56 82	70 89	63 78	63 72	27	22.5 22.5	5.6	82 65	49 44	47 38	43 35	25	22
66 94	82 98	61 90	64 84	53 73	66 76	64 81	56 82	70 89	63 79	62 71	28	22.8 22.8	5.7	82 65	49 44	47 38	43 35	25	22
66 94	82 98	61 90	64 84	53 73	66 76	64 81	46 83	70 89	63 79	62 72	28	22.8 22.8	5.7	82 65	49 44	47 38	43 35	25	22
66 94	82 98	61 90	64 84	53 73	65 76	64 80	56 84	70 89	63 79	62 72	28	22.8 22.8	5.7	82 65	49 44	47 38	43 35	25	22
	82 98	61 90	65 84	53 73	66 76	64 81		70 90	63 79	62 72	28	22.8 22.8	5.7	82 65	49 44	47 38	43 35	25	22

U

D

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	
12/9/72	15:10	142:26	1950	250	DUMMY TEST	98 100	108 77		111 118		107 113		100	
12/9	15:40	142:56	1950	250	DUMMY TEST	98 100	107 77	_	111 118		106 113	93 100	100 106	
12/9	16:10	143:26	1950	250	DUMMY TEST	97 100	107 76		110 118		106 113	93 100	99 106	10 10
12/9	16:40	143:56	2400	250	DUMMY TEST	98 101	107 77		111 119	88 113	107 114		101 108	
12/9	17:10	144:26	2400	250	DUMMY TEST	98 101	107 77		111 119		107 114		101 108	
12/9	17:40	144:56	2400	250	DUMMY TEST	97 101	107 77		111 119		107 115		101 108	
12/9	18:10	145:26	2400	250	DUMMY TEST	97 101	107 77		111 119		107 115	-	101 108	
12/9	18:40	145:56	2400	250	DUMMY TEST	97 100	107 76		111 119	88 113	107 114	-	101 108	
12/9	19:10	146:26	2700	250	DUMMY TEST	98 101			112 118	89 112	108 114		101 106	
12/9	19:40	146:56	2700	250	DUMMY TEST	98 98	74	111	115		108	96	101 102	10
_			1	-2-	The desired					pect				On
12/9	20:50	147:26	1100	250	DUMMY TEST	97 95			109 114		105 105		98 100	



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK

TEMPERATURE (°C)

10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33
122 112	92 112	95 104		82 98	84 104	94 104	78 94	78 92	82 92	78 87	79 88	76 88	78 92		79 96	73 90	65 84	60 73	60 78	51 77	42 71	51 73	4 [,]
121 112	91 111	95 103		82 99	84 105	94 104		78 92	81 92	78 87	79 88	75 88	77 91	83 90	78 96	73 91	64 84	60 77	59 79	51 78	41 72	50 74	41 7'
121	91 111	94 103	81 75		84 104			76 92	81 92	77 87	78 88	75 88	77 91	83 90		73 91	69 84	59 76	59 79	50 78	40 71	49 74	4! 7'
123 114	93 113	96 105	82 76	82 100	85 106	95 105	79 94			81 91		79 92	80 94	84 97		77 93	65 85	60 77	59 79	50 78	40 72	50 74	4! 7
123 113	93 112	95 105			85 107					81 91		79 92	80 95	84 92	80 100	78 94	65 85		59 79	50 78	40 72	50 74	4: 71
123 114	93 112	95 105			85 107				83 94		80 91	79 92	80 95	84 92	80 100	78 94	65 85	59 77	59 79	50 78	40 72	50 74	4: 77
123 114	92 113	96 105			85 107			77 93	83 94	81 91	80 92	79 92	80 95	84 92		78 94	65 85	60 77	60 79	50 78	40 72	50 74	45 71
123 113	93 112	95 105		82 100	85 107	95 105	79 94		83 93	81 91	81 91	79 92	80 94	84 92	80 100	73 94	65 85		59 79	50 78	39 72	49 74	45 77
124 112	94 111	96 104	82 74	82 99	86 106	96 104	80 93	78 92	84 93	84 92	82 92	82 93	83 95	86 92	82 102	81 96	65 85	60 77	60 77	50 76	40 71	49 71	45 74
125 107 wer	94 106	99			86 103			78 87	84 87	84 86	82 86	82 87	83 90	86 87	82 95	81 91	65 79	60 71	60 72	50 71	40 67	50 68	45 70
118 105	90 104	93		80 92	82 96	93 97	76 85	75 84	79 83	73 76	76 77	71 78		80 81	76 90		65 77	59 58	59 71	50 70		49 67	

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	TE	ST (S	HE	ET	30)							•								
Ī												•		PUMP		MA	NIFC	LD		MMY
													FL	ow		1	PRESS	3		PUT ESS
_	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
	67 94	82 98	61 90	65 83	53 73	66 76	63 81	56 83	70 89	63 79	62 73	28	22.8 22.8	5.7	81 65	49 43	47 38	43 35	25	22
	66 94	82 99		64 85	53 74	66 77	64 81	56 84	70 90	63 79	62 73	27	22.8 22.8	5.7	81 65	49 43	47 38	43 35	25	22
	65 94	82 99	60 91	64 85	53 74	65 76	63 81	55 84	70 90	62 79	61 71	25	22.8. 22.8	5.7	81 74	48 43	47 39	43 35	25	22
	65 94	83 101		64 85	54 74	65 77	64 82	55 85	70 91	63 79	62 73	26	22.8 22.8	5.7	81 64	48 43	47 38	43 35	25	22
	66 95	83 101	60 92	64 85	54 76	66 7 7	64 82	55 85	70 91	62 79	61 72	26	22.8 22.8	5 .7	81 64	48 43	47 38	43 35	25	22
	65 95	83 101		64 85	54 75	65 77	63 82	55 85	70 91	63 79	61 72	25	22.8 22.8	5.7	81 64	48 43	47 38	20 35	25	22
	65 95	83 101	60 92	64 85	54 74	65 77	64 82	55 85	71 91	63 79	62 72	25	22.8 22.8	5.7	81 64	48 43	47 38	43 35	25	22
1	65 94	83 101				65 76	63 81	55 85	70 91	62 79	61 72	25	22.8 22.8	5.6	81 64	48 43	47 38	43 35	25	22
	65 95	84 102	61 91	64 85	54 76	66 77	64 82	56 85	71 89	63 79	62 73	25	23.1 22.5	5.5	81 65	48 43	47 38	43 35	25	22
	65 92			65 81		66 71	64 77		71 85		61 68	25	23.1 22.5	5.5	81 65	48 43	47 38	43 35	25	22
	65 87		60 84	63 78	53 66	65 68	63 74	55 75	70 82	62 71	62 66	24	22.8 22.5	5.5	80 65	48 44	47 38	42 36	25	22



DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/9/72	21:20	147:56	1100	250	DUMMY TEST	98 94	107 72	89 110	109 113	85 104	105 105	91 96	98 99		119 105 1
12/9	21:50	148:26	1100	250	DUMMY TEST	98 94	107 72	89 110		85 104	105 105	91 96	98 99		119 105 1
12/9	22:20	148:56	1950	250	DUMMY TEST	97 96	108 72	89 111	111 115	87 10′;	7.07 ±08	-	101 102		123 107 :
12/9	22:50	147:26	1950	250	DUMMY TEST	96 96	108 72	89 111	112 115				101 102		123 107 1
12/9	23:20	149:56	1950	250	DUMMY TEST	97 96	108 73	88 111	112 115		10 8 109	_	101 102		123 107 J
12/9	23:50	150:26	1950	250	DUMMY TEST	97 97	108 73	89 112	112 115		108 109	94 102	101 102		123 108 1
12/10	0:20	150:56	1950	250	DUMMY TEST	97 96	109 73	89 112	112 115		108 108	94 100	101 102	104 100	123 108]
12/10	0:50	151:26	1950	250	DUMMY TEST	97 96	109 72	89 111	112 115		108 108		101 102	104 100	123 108 1
12/10	1:20	151:56	1950	250	DUMMY TEST	97 96		89 111	112 115	88 107		-	101 102		123 108]
12/10	1:50	152:26	1950	250	DUMMY TEST	97 96	-	111	-	107	108 108	102			123 108 :
12/10	7:25	152:26	1950	250	DUMMY TEST	92 90	102	_	- En 106 110	3.1	Shif 101 97	ŧ 88 96	93 93	97 91	115 99



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABO

TEMPERATURE (°C)

	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	2
5	105 105		-		119 105		93 96	80 68	80 92	82 96	93 97	76 85	75 84	79 83	73 76	76 77	71 78	76 79	80 81	76 90	69 80	64 78	59 68	5
5	105 105		98 99		119 105			80 68			93 97	76 85	75 84	79 83	73 76	76 77	71 78	76 79	80 81	76 90		64 78	59 68	5,7
7	107 108		101 102	104 100	123 107		95 98	82 69	81 94	85 100	95 99	79 87	78 85	82 85	78 81	80 81	76 82	79 86	84 85	79 93	74 85	66 79	60 69	
8 7		-	101 102		123 107	93 106		82 70		85 100	95 99	80 87	78 86	83 86	79 81	80 81	77 83	79 86		80 94	75 85	66 79	60 70	7
8 7			101 102	104 100	-	93 106				85 101	96 100		78 86	83 86	79 82	80 82	77 83	79 86		80 94	75 85	66 79	60 70	-
8 7			101 102				96 99	83 70	82 94	85 101	96 100	80 88	78 86	83 86	79 82	80 82	77 83	79 86		80 94	75 85	66 79	60 70	€ :-
8 7			101 102				96 99	83 70	82 94	85 101	96 100	80 38	78 86	83 86	79 81	80 81	77 83	79 86		80 94	75 85	66 79	60 70	
8 7			101 102		123 108	94 107				86 101		80 88		83 86	79 82	80 82	77 83	80 86		80 94		66 79	60 70	•
8 7	108 108	94 102	101 102	104 100	123 108	94 107	96 99	83 70	82 94	86 101	96 100	80 88	78 86	83 86	79 82	80 82	77 83	80 86	85 86	80 94	75 85	66 79	60 70	•
7	108	102	101 102	104 100	123 108	94 1("	96 99	83 70	82 94	86 101	96 100	80 88	78 86	83 86	79 82	80 82	77 83	80 86	85 86	80 94	75 85	66 79	60 70	•
	Shif		00	07	775	. Q <i>e</i>	90	72	75	70	QQ	75	72	71	68	72	65	70	73	69	62	61	58	£
<u>1</u>			93 93	97 91	115 99	98	89 89	60	86	79 94		75 79			69		70		73	74	69	66	58 59	į

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A:LABORATORY	/ B	ACK-1	0.	BAC	CK	TEST	(SHEET 3	1)
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		-								-												
(°C)																						FL
27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL
64 78	59 68	59 71	49 70		49 67	45 69	70 82	60 68	70 85	65 88	80 91	60 84	63 79	53 66	64 68	63 76	55 76	70 8 2	62 72	62 66	24	22.8 22.5
64 78	59 68	59 71	49 70		49 67	45 69	70 82	60 68	70 85	65 88	80 91	60 84	63 70	53 66	64 68	63 76	55 76	70 82	62 72	62 66	24	22.5 22.5
66 79	60 69	59 72	50 71		49 68	45 70	71 83		71 85	65 88	83 93	61 85	64 79	55 68	65 69	64 77	55 78	71 83	63 72	63 66	24	22.8 22.8
66 79			50 71		50 68	45 71	72 84	62 70			83 94		64 79	55 68	66 70	64 77	55 78	71 84	63 74	63 66	24	23.1 22.8
66 79	60 70	60 72	50 71		49 68	45 71	72 84	62 70	72 85	65 89	83 94	61 85	64 80		65 70	64 77	55 78	72 84	63 74	63 67	24	23.] 22.{
66 79	60 70		50 71		49 68	45 71	72 84	62 70	72 85		83 94	61 85		55 68		64 77	55 78	72 84	64 74	62 66	24	22. 22.
56 79	60 70	60 72	51 71		49 68	45 71	72 84	62 70		65 90	83 94	61 86	64 79		65 71	64 77	55 79	71 84	64 74	61 66	24	22. 22.
66 79	60 70	60 72	50 71		49 68	45 71	72 84	62 70	•	65 90	_	61 85	64 80	55 68	66 70	64 77	55 78	72 84	64 74	62 67	24	22. 22.
66 79	60 70	60 72		39 66	49 68	45 71		62 70			83 94			55 68		64 77	55 78	72 84	64 74	62 67	24	22 22
66 79	60 70			39 66	49 68	45 71	72 84	62 70	72 86		83 94	61 85	64 80	55 68	66 70	64 77	55 78	72 84	64 74	62 67	24	22 22
61 66	58 59	59 62		40 57	50 64	45 60	67 71	58 59	68 71	62 74	73 82	59 73	60 65	50 57	63 59	60 62	53 6 6	67 72	61 62	60 58	25	21 22

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1	SHE	ET	31)												_			
												PUMP			NIFO			MMY
												OW			RESS		PR	PUT
8	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
0	60 84	63 79	53 66	64 68	_	55 76	70 82	62 72	62 66	24	22.8 22.5	5.5	80 65	48 44	47 38	42 36	25	22
0	60 84	63 70	53 66	64 68	63 76	55 76	70 82	62 72	62 66	24	22.5 22.5	5.5	80 65	43 44	47 38	42 36	25	22
3	61 85	64 79	55 68	65 69	64 77	55 78	71 83	63 72	63 66	24	22.8 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3	61 85	64 79	55 68	66 70	64 77	55 78	71 84	63 74	63 66	24	23.1 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3	61 85	64 80	55 68	65 70	64 77	55 78	72 84	63 74	63 67	24	23.1 22.8	5.6	80 65	48 43	47 38	42 35	25	22
34	61 85	64 80	55 68	65 70	64 77	55 78	72 84	64 74	62 66	24	22.8 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3	61 86	64 79	55 68	65 71	64 77	55 79	71 34	64 74	61 66	24	22.8 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3	61 85	64 80	55 68	66 70	64 77	55 78	72 84	64 74	62 67	24	22.8 22.8	5.6	80 65	48 43	47 38	42 3 5	25	22 .
13	61 35	64 80	55 68	66 70	64 77	55 78	72 84	64 74	62 67	24	22.8 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3	61 85	64 80	55 68	66 70	64 77	55 78	72 84	64 74	62 67	24	22.8 22.8	5.6	80 65	48 43	47 38	42 35	25	22
3 2	59 73	60 65	50 57	63 59	60 62	53 66	67 72	61 62	60 58	25	21.0	5.3	74 65	44 44	42 38	39 35	23	20

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	
12/10/72	07:55	152:56	1950	250	DUMMY TEST	96 94	107 72	86 110			107 105	-	100 100	1
12/10	08:25	153:26	1950	250	DUMMY TEST	96 96	108 72	87 111			107 106		101 100	1
12/10	08:55	153:56	2400	250	DUMMY TEST	96 96	109 73	88 112	113 115		109 108		102 102	1
12/10	09:25	154:26	2400	250	DUMMY TEST	96 96	109 73	88 112			110 110		102 103	10
12/10	09:55	154:56	2400	250	DUMMY TEST	96	110 73	88 112	_	-	110 110		103 103	1(
12/10	10:25	155:26	2400	250	DUMMY TEST	96 96	109 73	88 112			110 110	•	102 103	1(
12/10	10:55	155:56	2400	250	DUMMY TEST	96 96	110 73	88 112		89 109	110 109		103 103	1(
12/10	11:25	156:26	2700	250	DUMMY TEST		110 74	89 113			112 109		105 104	10
12/10	11:55	156:56	2700	250	DUMMY TEST		110 75	113		109	109	107		10
10/10	12.00	156.56	2000	1.05	Dines	00		- In					Chan	_
12/10	13:00	156:56	3000	425	DUMMY TEST		100 74	81 110		79 105		85 101	92 100	9
12/10	13:30	157:26	3000	425	DUMMY TEST	92 97	103 75	83 114	107 117	82 110	102 110	89 110	95 105	9 10

												TA	BLE	X	٦.	RO	LLE	≀ G	EAR	TR	AN	
TAIL H.P.		,	2	3	4	5	6	7	R	۰	10	11	12	13	14	15	16	17	18	19	20	
250	DUMMY TEST	96 94	107	86 110	111	86	107 105	93	100 100	102	122 105	92	95 96	80	80 92	85 99	93 97	78 85	77 84	81 84	78 79	
250	DUMMY TEST		108 72				107 106		101 100		123 106		95 97	82 69	81 92	85 100	95 98	79 87	78 85	82 85	79 80	
250	DUMMY TEST		109 73	88 112			109 108		102 102		125 107		97 98	83 70	82 93	87 101	97 100	80 88	79 86	84 86	83 83	
!50	DUMMY TEST		109 73	88 112	-	-	110 110		102 103		124 108	-	97 99	83 70	83 94	88 102	97 100	89 88	79 87	84 87	83 84	
50	DUMMY TEST	97 96	110 73	88 112			110 110		103 103	-	125 108		97 99		83 94	-	97 100	81 88	79 87	85 87	83 84	
O	DUMMY TEST	96 96	109 73	88 112	113 116	_	110 110	-	102 103		125 108		97 99	83 70	83 94	88 102	97 100	81 88	79 87	85 87	83 84	
)	DUMMY TEST	-	110 73	88 112		-	110 109		103 103		126 109		98 100	84 70	83 94	88 102	97 100	81 89	80 88	85 87	83 85	82 85
1	DUMMY TEST	_	110 74		115 116					107 102			99 100	85 71		89 103				88 89	87 87	_
	DUMMY TEST	98	75	113	116	109	109	107	104	102	110	109	98 100 to 42	71	96			81 90		87 89		85 86
	DUMMY TEST	90	100		104	79	98	85	92	95	113		87	-	74		87 98	70 86	69 85	72 86	70 81	70 81
	DUMMY TEST		103 75					89 110			118 110	85 111	90 102	78 73	77 97	81 105	90 102	73 92	72 92	78 93	78 89	76 89



TEST DATA: LABORATORY BACK-TO-BACK TEST (SHEET 32)

TEMPERATURE (°C)

_	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47
	83 83	80 91	74 82		60 66	60 69	50 68	39 62	49 65	45 66	72 80	61 67	71 83	64 87	82 90	61 81	63 76	53 65	65 67	63 72	54 74	71 80		62 64
	85 85	81 93		65 77	60 67	60 70		39 63	49 66	45 68	72 82	61 68	72 84	64 89	83 92	61 83	63 78	5 ¹ 66	65 69		55 76	71 82		62 65
	88 89	82 94				61 71	51 70	39 63	50 67	45 69	72 82	62 69	72 85	65 89	85 94	61 84	64 79	55 67	66 69	64 76	56 77	72 83		63 6€
ì	87 89	83 94			60 69	60 71	50 70	38 65	50 67	45 69	72 83	62 69	72 85		85 94	62 84	64 79	55 67	66 69	63 76	55 77	72 83	63 72	6: 6(
}	87 89	83 94	79 87	66 78		61 71	50 70	39 65	50 67	45 69	72 83	62 74	72 85	65 89	85 94	61 85	64 79	55 68	66 69	64 76	56 77	72 83	64 72	
}	87 89	83 94	80 88	66 78		61 71	50 70	39 65	50 68	46 69	72 83		72 86	65 89	85 94	61 85	64 79	55 67	66 69	64 69	56 77	72 83	63 73	
;	87 90	83 94	80 88	66 79	61 69	61 71	51 70	40 66	50 67	46 69	72 83	62 69	72 86	65 89	85 94	61 85	65 80	55 68	66 69	64 76	56 77	72 84	63 72	
3 2	90 92	86 96	83 91	67 79	61 69	62 72	51 71	40 66	51 68	46 70	73 84	63 70	73 87	65 72	87 96	62 87	66 80	56 68	65 70	64 77	56 79	72 84	64 74	
3 2	90 92	85 96	82 91	67 80	62 70	62 73	51 71	40 66	51 69	46 70	73 85	63 71	73 87	65 90	87 96	62 87	65 80	56 69	66 71	64 76	56 79	73 85	64 74	
1 5	74 85	71 89	67 80	58 74	58 69	57 74	48 71	39 67	49 68	45 69	66 79	55 65	67 80	62 81		56 81		42 63				65 91	58 68	
8	80 91	76 99		60 82		59 80	50 79	39 73	50 74	46 78	68 88	57 72	69 91	63 91	79 98	58 90		43 70			51 81	67 88	60 78	1

5	HE	et J	2)														_	
		-								1		PUMP			NIFO			MMY
)W			RESS		PR	ESS
_	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
5	61 81	63 76	53 65	65 67	63 72	54 74	71 80	62 70	62 64	23	21.5 22.5	5.5	74 65	717 717	42 38	38 35	22	19
3 2	61 83	63 78	54 66	65 69	63 74	55 76	71 82	63 71	62 65	23	21.0 22.5	5.5	73 65	77 77	42 38	38 35	22	19
5 4	61 84	64 79	55 67	66 69	64 76	56 77	72 83	63 72	63 66	23	21.0 22.5	5.5	72 65	77 77	42 38	38 35	22	19
5	62 84	64 79	55 67	66 69	63 76	55 77	7 2 83	63 72	63 66	23	21.3 22.5	5.5	72 65	717 717	42 38	38 35	22	19
5 4	61 85	64 79	55 68	66 69	64 76	56 77	72 83	64 72	63 66	23	21.6 22.8	5.6	72 65	77 77	42 38	38 35	22	19
5	61 85	64 79	55 67	66 69	64 69	56 77	72 83	63 73	62 66	23	21.3 22.5	5.6	73 65	71 71	42 38	38 35	22	19
5 4	61 85	65 80	55 68	66 69	64 76	56 77	72 84	63 72	63 66	23	21.3 22.5	5.6	73 65	71 71	42 38	38 38	22	19
7 6	62 87	66 80	56 68		64 77	56 79	72 84		64 67	23	21.6 22.5	5.6	73 65	717 717	42 38	38 35	22	19
7 6	62 87	65 80	56 69	66 71	64 76	56 79	73 85	64 74	63 67	24	21.6 22.8	5.6	72 65	## ##	42 38	38 35	22	19
5 0	56 81	59 70	42 63	61 64	58 68	50 72	65 91	58 68	59 61	22	20.1 22.5	5.5	78 66	46 44	44 38	39 36	23	20
9 8	58 90	61 83	43 70		59 80	51 81	67 88	60 78	60 70	23	21.4 22.8	5.6	77 66	46 44	44 38	39 36	23	20

					<u> </u>	Γ								-	_
DATE	OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	H.P.		1	2	3	4	5	6	7	8	9	
12/10/7	2 14:00	157:56	3000	425	DUMMY TEST	92 98	102 76	83 114	108 117		102 111	89 110		98 104	11
12/10	14:30	158:26	3000	425	DUMMY TEST	96 98		88 115	112 117				102 105	105 104	12
12/10	15:00	158:56	3000	425	DUMMY TEST	97 98	109 76	89 115	113 118		110 112			105 104	12
12/10	15:30	159:26	3000	425	DUMMY TEST	97 99	109 76	90 114	113 116				103 106		12 11
12/10	16:00	159:56	3000	425	DUMMY TEST	97 99	109 76	90 114	113 116				103 106		12 11
12/10	16:15	160:11	1950	425	DUMMY TEST	98 97	109 75	89 112	112 116	88 109	108 109	_	101 104		12
12/10	16:45	160:41	3000	425	DUMMY TEST	97 99		88 114	112 117				102 106		120
12/10	17:15	161:11	3000	425	DUMMY TEST	97 99			112 117				102 106		12(11:
12/10	17:45	161:41	3000	425	DUMMY TEST	97 99		88 114		89 111			103 106		12; 111
12/10	18:15	162:11	3000	425	DUMMY TEST	97 99	-	· 89	113 117		110 112		103 107		125 112
12/10	18:45	162:41	3000	425	DUMMY TEST	97 99	-	89 115	113 117	89 111			103 107		126 112



TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY

TEMPERATURE (°C)

. 9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
5 98 5 104	119 110	86	91 102	78		81		73		78 93	79 90	76	•	79 93	80	76 100	75 93	60 83	60 77	59 81	50 79	39 72
? 105 5 104	125 111		97 103			87 106	97 103		79 92	85 94	85 90	83 90			87 96	83 99	81 93	66 84	64 78	64 81	54 79	42 75
3 105 5 104						88 106	98 103			86 94		84 90			88 95	83 99	81 93	67 84	65 78	65 81	54 79	43 73
3 105 5 104		95 110				88 106	98 103			86 94		83 89	84 91		88 94	83 99	81 94	67 84	65 78	65 82		43 73
3 105 5 104		95 110				88 106	98 103		80 92	86 94	86 89	83 89		87 94		83 99	81 94	67 84	65 78	65 82	54 79	43 74
1 104 4 102									79 90		79 83	80 83	88 84	83 88	87 86							
2 105 5 104		95 110			83 97				79 92	85 93			84 91		87 91	83 99	81 93	67 84	65 78	65 82	55 79	43 74
2 105 6 104									79 92	85 93		84 90	84 91		89 94	83 99	81 94	67 85	64 78	64 82	54 79	43 74
3 105 6 104		94 110	98 102	84 73	83 98	88 107	98 103	81 92	80 92	85 93	85 90	84 90	83 91	87 94	88 94	83 99	82 94	67 85		65 82	54 79	43 74
3 105 7 105												84 90		87 95	89 95	83 99	82 94	67 85	65 78	65 82		43 74
3 105 7 105		94 111											84 92					67 85	65 79	65 82	54 80	43 75



TES	ST (S	HE	ET 3	3)															
													PUMP		MA	NIFO	LD		YMY
													ow			RESS		PR	PUT ESS
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
64 92	79 98	58 90	61 82	44 70	61 74	59 79	51 81	67 89	60 78	59 70	22	21.0 22.8	5.6	75 66	45 44	42 38	39 35	23	20
67 92	85 99	63 91	66 84	53 70	66 74	64 80	56 82	73 89	64 78	65 70	23	21.6 22.8	5.6	75 66	45 44	43 38	39 35	23	20
67 92	86 99	63 91	66 85	53 70	67 76	65 80	57 81	73 89	66 78	64 71	24	21.6	5.6	75 65	45 44	43 38	39 35	23	20
67 93	86 99	63 91	66 84	53 71	67 76	65 80	56 82	73 89	65 79	64 71	25	21.3 22.8	5.6	75 65	ት ት	43	38	23	20
67 93	86 99	63 91	66 84	53 71	67 76	65 80	56 82	73 89	65 79	64 71	25	21.3	5.7	75 65	44 43	43 38	38 35	23	20
											25	21. 3 22.8	5.7	74 65	<u>դ</u> դ	42 38	38 35	23	20
67 92	85 99	63 91	67 83	53 71	68 75	66 80	57 82	73 89	65 78	64 71	25	21.3	5.7	74 65	44 43	42 38	38 35	23	20
67 93		63 91	67 85	53 71	68 76	66 80	57 82		65 78	64 71	25	21.3 22.8	5.7	73 65	44 43	42 38	38 35	23	20
67 93	86 99	63 91	67 85	53 71	68 77	66 80	57 82	73 89	65 78	64 71	25	21.3	5.7	73 65	43 43	42 38	38 35	22	19
67 93		63 91	67 85	53 71	69 76	67 80	57 82	73 90	65 79	65 71	24	21.0	5.7	73 65	43 43	41 38	38 35	22	19
67 93		63 91	67 85	53 71	69 77	66 80	57 82	74 90	65 79	66 71	25	20.7 22.8	5.7	71 65	42 43	40 38	37 35	21	19

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/10/72	19:15	163:11	3000	425	DUMMY TEST	97 99	109 76	89 115	114	89 112	110 112		103 107		126 112
12/10	19:45	163:41	3000	425	DUMMY TEST	98 99	109 76	89 115		89 111			103 107	106 105	126 11
12/10	20:00	163:56	1950	425	DUMMY TEST	99 100	110 76	90 114	114 118	89 111	110 111	-	103 106		126 111
12/10	20:30	164:26	3560	425	DUMMY TEST	98 101	110 78	89 116	115 118	90 113	112 113		105 109		128 114
12/10	20:45	164:41	1950	425	DUMMY TEST	100 100	111 77	91 115	115 118	90 111	111 112	97 110		107 105	127 112
12/10	21:15	165:11	3560	425	DUMMY TEST	98 101	110 77	89 116		90 113		97 112		107 107	128 114
12/10	21:30	165:26	1950	425	DUMMY TEST	98 100	110 76	90 115		89 111		96 110			125 112
12/10	22:00	165:56	3560	425	DUMMY TEST	98 100 St	77	116		113		112	108		
12/10	22:40	166:11	1950	425	DUMMY TEST	98 96	109	89 110	112	87 104	107	93 102	100	103	124 104
12/10	22:55	166:26	3700	425	DUMMY TEST	96 96		89 111		89 112		96 105		_	128 107
12/10	23:10	166:41	1950	425	DUMMY TEST	98 97		91 101		88 106		84 105	104 101		125 107



			TA	BLE	EX	Π.	RO	LLE	R G	EAR	TR	ANS	SMI	55	ION	ITE	STI	DAT	A;L	ABO	OR/	NTO	RY
																TEMP	ERAT	URE	(°C)				
8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
L03 L07		126 112	95 111	98 103	85 74	84 98	88 107	99 104		80 92	85 94	86 90		84 92	87 95	90 94	84 100		67 85	65 79	65 82		42 75
			94 111				88 107				85 94		84 90			89 95	83 99	83 94	•	· .	65 82		43 75
	106 104						87 105				85 93	84 86	84 87	83 88		90 90							
	107 107			100 105		85 100		100 106			86 97		89 95			92 99	86 104	89 98	67 86	65 7 9	65 83	54 82	
			95 111					100 105		81 93		87 87	86 88	86 89	89 93	92 91							
			96 113				90 110				87 97		89 95			94 99	87 104	89 99	68 86	65 79	65 83	55 82	43 77
			94 111			84 98	87 106	98 104	81 94	80 92	85 93	82 86	82 86		85 91	88 90							
108		113	112	105	76	100	90 110	100 106	81 95	80 94	86 96	91 95	89 95	88 96	91 100	94 99	87 104	88 99	67 85	65 79	65 83	•	43 77
100	103	124	0n Pc 92 103	96	82	82		96 97	79 85	78 84	79 85	73 76	76 76	71 77	76 80	80 78							
103 102	105 100	128 107	95 106	99 98	83 68	84 94	88 103	98 99	80 87	79 86	83 89		85 84	83 86		91 87							
.04 .01	105 99	125 107	95 106	98 98	84 68	84 93	85 101	97 99	80 88		84 87		83 81			71 82							

KTE	ST (S	SHE	ET 3	54)															
													PUMP			NIFO	LD		AMY
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	OW ROLLER	PRESS		RESS L/H	R/H	PRI	ESS
67 93	86 100	63 91	67 85	53 71	69 75	66 81	57 82	74 90	65 79	65 71	24	20.7 22.8	5.7	70 65	42 43	40 38	37 35	22	19
66 93	86 100	63 91	67 85	53 72	69 76	66 81	57 82	73 90	65 79	65 71	24	20.7 22.8	5.7	70 65	41 43	40 38	36 35	18	22
												20.4 22.8	5•7	70 65	41 43	40 38	36 35	22	19
67 93	88 103	64 93	66 86	54 72	68 76	66 82	57 79	74 91	65 80	65 72	24	20.7 22.8	5•7	70 65	41 43	40 38	35 35	22	19
												20.4 22.8	5.7	70 66	42 43	40 38	35 35	22	19
67 93	88 103	64 93	67 85	54 73	69 77	66 82	57 85	74 85	66 80	65 72	25	21.0	5.7	70 65	42 43	40 38	35 35	22	19
												20.7 22.8	5.7	71 65	43 43	40 38	36 35	22	19
67 93	88 103	63 93	66 85	54 74	68 7 7	66 82	57 85	74 91	65 79	64 72	24	20.7 22.8	5.7	70 65	42 43	41 38	36 35	22	19
												21.0 22.5	5.4	72 65	7† 7† 7† 7†	42 38	38 35	23	20
												22.8 22.5	5.5	71 65	71 73	42 38	38 36	22	19
												22.5 22.5	5.5	78 65	48 44	45 38	42 35	24	21

し

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
12/10/72	23:25	166:56	3700	425	DUMMY TEST	98	109 75	112	116 115	108	111	107	104	101	129 118
1/9/73	11:15	166:56	1950	250	DUMMY TEST	56	115 73	107	121 126	91	116	110 109	109 113		113 117
1/9	11:45	167:26	1950	250	DUMMY TEST	52 95	108 69	103 115	_	-	107 110		100 106	103 103	125 111
1/9	12:15	167:56	1950	250	DUMMY TEST	95	108 69	102 115	119		111	92 107	99 106	102 103	
1/9	13:50	167:56	1950	250	DUMMY		107	102 111	113	82	106 104	90	98 100	102 98	12: 10:
1/9	14:20	168:26	1950	250	DUMMY TEST	54 94	108 70	111 113			106 1 8		98 103	102 100	
1/9	14:50	168:56	1950	250	DUMMY TEST		109 71	112 114			108 109		100 105	104 102	-
						2	Stop	- Ins	pect	Str	aine	rs			
1/10	10:10	168:56	1100	250	DUMMY TEST	66 94	108 95	109 117			103 111		96 106	100 102	
1/10	10:40	169:26	1100	250	DUMMY TEST	68 97	108 98	111 121		-	114 117		96 111	100 108	
1/10	11:10	167:56	1100	250	DUMMY TEST	72 96	110 97	112			106 114		98 109	102 105	



			TA	BLE	1	α.	RO	LLE	? G	EAR	TR	AN	SMI	SSI	01	ITE	ST	DAI	ΓA;l	AB	OR/	NTO	RY
																TEMP	ERA	TURE	(°C)				
	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
4	101	129	117	100 100			89 105	99 101	81 87	80 86	85 90	89 88	88 88	86 90	88 94	94 93							
9 3		113		110 107			91 105	103 107		84 91	90 89	83 85	86 88	81 85	85 95	90 88		79 89	81 85	63 74	69 76	53 77	38 67
0 6		125 111		97 101			82 103	94 102	76 91	75 87	84 86	75 81	78 85	73 81	77 92		77 88	69 88	62 80	53 69	57 71		32 63
9 6				96 101			87 104			73 87	80 86	73 82	77 85	70 80	75 91		76 87	66 88	62 86	53 69	57 70	43 72	31 63
8 0		123 105	-		78 66			92 97	76 84	73 80	79 77	70 72	75 74	68 71	72 84	77 75	74 78	65 78	62 74	54 65	58 66	43 67	
8		124 108	-	95 99			82 102	93 100	77 87	73 85	80 85	71 79	76 83		74 91		75 85	66 86	62 78	53 67	57 69	43 69	33 63
o 5		130 110		97 100	81 71		83 102	95 101	79 89	76 86	82 85	74 80	78 83	72 79	76 91	82 83	77 81,	68 85	63 79	54 69	58 70	44 70	32 63
6				92 104				90 104		73 90	78 87			65 80				62 85	63 83	66 79	65 79	56 78	57 78
6				92 109				91 109			77 92	65 85	72 88	63 85	69 96		69 90	60 91	62 89	64 85		55 84	57 84

90 82

74 66 71

85 82 94

76 73 62 64 67 84 88 89 88 82

66

82

58 61

81 80

6

8 102 121 89 94 81 86 80 93 76 75 9 105 115 105 106 77 103 104 106 96 92

K TE	ST	SHI	ET	35															
										-			PUMP		MA	NIFC	LD		YMM
												FL	ow		1	PRESS			PUT ESS
5 37	38	39	40	_41	42	43	44	45	46	47	43	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
												22.8 22.5	5.6	77 65	47 43	45 38	41 35	24	21
72 87	90 92	74 99	75 76	62 77		73 76	64 79	70 84	72 76	70 66	13	21.6 22.8	5.4	70 64	42 43	40 37	37 35	21	19
64 91	82 89	66 96	64 75	46 69		62 74	53 79	58 85	62 7 2	58 63	11	19.2 22.5	5.4	71 64	42 43	40 37	36 35	21	18
61 91	80 89	65 95	60 75	47 69		58 74	51 79	56 85	59 72	56 63	11	19.2 22.5	5.3	70 64	42 44	40 38	36 35	21	18
65 81	79 81	65 91	64 68	46 63	62 61	61 67	53 71	58 79	62 68	59 60	13	19.5 22.5	5.3	71 65	42 44	40 38	36 35	21	18
62 91	80 86	65 93	60 75	47 65	59 67	58 73	51 76	57 83	60 72	57 63	13	19.5 22.5	5.3	71 65	42 44	40 38	36 35	21	18
63 90	82 87	66 94	62 74	49 68	61 66	60 72	52 78	58 84	61 72	58 63	11	19.8 22.5	5.3	70 65	717 715	40 38	36 35	21	18
79 99	78 93	69 95	72 101	43 69	72 96	69 96	63 81	63 90	69 91	68 93	12	18.9 22.5	5.3	71 66	42 44	40 38	36 35	21	18
78 106	77 96	68 101	69 107	44 74	69 103	66 103	61 85	61 94	67 95	67 99	12	18.9 25.5	5.4	72 65	42 43	40 37	36 35	21	18
79 106	80 96	70 99	71 106	47 72	71 102	69 102	63 85	63 93	70 94	69 98	12	19.5 22.8	5.3	71 65	42 43	40 37	36 35	21	18



DATE	TIME	TOTAL TEST	TOTAL	TAIL H.P.											
<u> </u>	DAY	TIME	H.P.			1	2	3	4	5	6	7	8	9	10
1/10/73	11:40	170:26	1100	250	DUMMY TEST	72 96	110 97		115 121			91 109		102 105	122 114 1
1/10	12:10	170:56	1950	250	DUMMY TEST	74 99	111 99		116 125	-	_	93 113		104 1.10	125 119 1
רי/נ	12:40	171:26	1950	250	DUMMY TEST	75 99	111 100		116 125	91 118	-	93 113		104 110	126 119 1
1/10	13:10	171:56	1950	250	DUMMY TEST	76 99	111 101		117 125	92 119		94 114		105 110	126 119 1
1/10	13:40	172:26	1950	250	DUMMY TEST	65 90	109 93		115 123		107 105	92 110	100 110	103 108	124 116 1
1/10	14:10	172:56	1950	250	DUMMY	66 91	115 93		121 123	94 119		100 110		111 107	131 10 116 10
1/10	14:40	173:26	1950	250	DUMMY TEST	62 88	108 91		114 123	86 119		92 111		102 108	123 8 116 10
1/10	15:10	173:56	2400	250	DUMMY TEST	61 89	108 92							103 109	
1/10	15:40	174:26	2400	250	DUMMY TEST	61 87	108 90			86 118			99 110	103 107	125 9 116 10
1/10	16:10	174:56	2400	250	DUMMY TEST	60 87	108 90			86 118		92 111		103 107	125 8 116 10
1/10	16:40	175:26	2400	250	DUMMY TEST	60 86	108 90			85 118	107 115		99 110	103 107	124 8 116 10

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY

TEMPERATURE (°C)

														TEMPERATURE (°C)											
9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31			
102 105			94 106		87 103	81 103	93 106	77 96	75 93	80 90	68 82	75 85	67 82	71 94	77 83	73 88	63 88	64 88	67 82		57 81				
104 110			97 110	83 105	89 105	83 107	95 110	79 100	77 95		76 87			76 99	82 00	77 93	69 93	65 90	68 84	67 85	60 84				
104 110	126 119		97 110	83 80	89 106	83 108	95 110	79 100	78 96					76 100	82 90	77 93	68 94	65 90	68 85	66 85	59 83	61 83			
105 110			97 110				96 110			84 95	76 88	79 92	73 87	77 100	83 95	78 93	69 94	66 90	68 85	67 86	60 85	63 84			
103 108		89 105	95 105	81 76	82 103	82 105	93 106	76 96	75 92	81 92	74 85	77 89	71 84	75 96	80 87	76 90	66 91	62 88	55 81		47 80				
111 107			103 107				102 107				84 84			85 95	91 87	84 89	77 91		60 81	66 80	51 80	39 78	52 80		
102 108			94 107	81 77	81 103	82 106	93 106	76 96	74 92		73 84				80 87	75 90	66 91	61 87	54 81	57 80	45 80	34 79	46 81		
103 109	125 118						93 108		75 94	81 94	76 87	78 91	73 86	77 100	82 90	76 92	68 91	61 89	54 82	57 81	44 81	35 79	45 81		
103 107	125 116	91 105	95 107	81 76	81 103	83 107	94 107	77 96	75 92	81 92	77 85	78 90	73 84	77 98	82 88	76 91	68 90	61 87	54 81	57 79	44 79	34 78	45 79		
103 107	125 116					83 107	93 107			81 92	76 85	78 90	73 84	77 98	82 88	76 90	68 91	61 86	54 81	57 79	44 79	34 78	45 79		
103 107	124 116						93 107			81 92	76 85	78 89	73 84		82 87	76 91	68 91	61 87		57 79	45 79	34 78	45 79		

ES	ST (SHE	ET	36)						•									
													PUMP		MA	NIFO	LD		AMY
												FL	ow		P	RESS			PUT
7	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
19)5	80 96	70 99	71 107	48 72	72 103		63 87	64 93	70 94	69 98	13	19.5 22.5	5.3	71 65	42 43	40 37	36 35	21	18
30)7	83 94	71 104	72 106	48 105		71 103	65 89	66 95	72 96	70 100	14	19.5 22.5	5.3	71 64	42 42	40 37	36 35	21	18
30)7		70 104	73 106	49 105	73 103	71 103	65 89	65 95	72 97	70 100	14	19.5 22.5	5.5	71 64	42 42	40 37	36 35	21	18
31 07	84 98	71 105	73 108	50 106	74 105		66 90	66 96	73 98	71 101	16	19.5 22.5	5.5	71 64	42 42	40 37	36 35	21	18
56 05		67 104	65 105		63 104	62 104	53 86	59 93	62 95	60 99	16	19.2 22.8	5.4	70 64	42 42	40 37	36 35	21	18
58 54	88 94	72 101	67 103		67 100	66 101	58 85	65 92	67 94	63 97	17	19.8 22.5	5.5	70 64	42 42	40 37	36 35	21	18
64 04		67 101	63 103		61 101	60 101	51 85	53 92	59 94	58 97	17	18.9 22.5	5.4	71 64	42 42	40 37	36 35	21	18
63 04	81 94	66 104	62 105	46 73	59 102	58 103	51 87	57 93	59 95	58 98	17	19.2 22.5	5.5	70 64	42 42	40 37	36 35	21	18
		65 102			59 100			57 92	60 94	58 96	15	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18
		65 102			60 100		51 85	56 91	59 93		15	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18
63 03		65 102	62 104		60 100	58 102	51 85	56 91	59 93	57 96	15	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
1/10/73	17:10	175:56	2400	250	DUMMY TEST	60 86	108 90		114 122		107 115	92 111	99 110	103 107	124 116
1/10	17:40	176:26	2700	250	DUMMY TEST		108 90		115 122	86 119	108 115		100 110		125 116
1/10	18:10	176:56	2700	250	DUMMY TEST	86	108	119	122	86 119	108 115	110	100 110	108	126 117 ins
1/10	19:30	177:26	3000	425	DUMMY TEST	56 96	108 89	100 120	114 124	86 120	0ad t 108 116	93 112	100 112	104 110	125 118
1/10	20:10	177:56	3000	425	DUMMY TEST	57	109 87	100	116		110 114	95	02 p	106 108	128
1/10	20:40	178:26	3000	425	DUMMY TEST		109 87			88 118	111 115		102 110	106 108	_
1/10	21:10	178:56	3000	425	DUMMY TEST	-	109 87		116 123	88 118	111 116		102 110	106 108	
1/10	21:40	179:26	3000	425	DUMMY TEST	57 93	_	101 119			111 116		102 110		
1/10	22:10	179:56	3000	425	DUMMY TEST		109 87				111 116		103 110		
1/10	22:25	180:11	1950	425	DUMMY TEST		109 86			87 117		-	101 109	104 106	
1/10	22 :55	180:41	3000	425	DUMMY TEST	_	109 87				111 116	-	103 110		

ABLE	T	U .	RO	LLE	ì G	EAR	TR	ANS	SMI	ISS	101	1 TE	ST	DAT	[A-1	AR	OR4	ATO	RY	BA	CK.	TO	. B/
												TEMP											
12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35
95 107		81 102		93 107	76 96	74 92	81 92	76 85	78 89	73 84	77 98	82 87	76 91	68 91	61 87	54 81	57 79	45 79	34 78	45 79	38 79	68 93	57 87
95 108		81 103		94 108		75 92	82 93	79 86	81 91	76 85	79 100		77 90		61 87		57 80	44 80	34 78	45 80	38 80	68 93	57 88
95 108		81 103		94 108	77 97	75 93	82 93		81 91		79 100		77 92	•	61 87		56 179		33 78		38 79	68 93	57 88
strain	ers	. 0	n pow	rer 8	at 19):00																	
95 109		81 105		94 110	77 97	75 95	82 94	78 88	80 92		79 101		78 93	74 93	63 88		60 82		35 81	47 83		71 94	58 87
97 108	_	83 103		97 108	80 96	78 93	85 93		81 91	78 86			80 92		65 88		63 82		37 81		41 82	73 94	59 88
98 108	_	83 103		97 108	80 96	78 93			81 91		82 100		80 92				63 82	48 81	36 81		41 82	73 94	60 88
98 108	_	83 103	86 109	97 108	80 96	78 93	85 93	81 87	81 90	79 86	82 99	86 88	80 92	76 92	65 88	58 84	62 82	48 81	35 81	48 83	41 82	73 94	60 88
98 108		83 103	86 109		80 96	78 93	85 93	81 87	82 91	79 86	82 99	86 88	80 92	76 92	65 88	57 84	62 82	48 81	36 81	48 83	41 82	73 94	60 88
98 108	_	83 103			80 96	78 93	85 93		82 91	79 86	82 99	87 88	80 92	76 9 2	65 88		62 83		35 81	48 83		73 94	60 88
96 106		82 102		96 107	79 96	77 93	83 92	77 85	79 90	74 85	79 96	83 87											
98 108		83 103		97 109	80 96	78 93	85 93	83 87	85 91	80 86	83 100	87 88	80 93		65 88		62 83		35 81		40 82	72 95	59 88

TEST (SHEET 37)																			
		- ·											PUMP			NIFO			MMY
													WC			RESS		PRI	ESS
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
63 103			62 104	46 71		58 102	51 85	56 91	59 93	57 96	15	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18
62 102		-	62 104		59 101	58 102	50 85	56 92	59 94	57 97	14	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18
62 10 3			61 104		59 101		50 85	56 92	59 94	57 96	14	19.2 22.5	5.4	70 64	42 42	40 37	36 35	21	18
63 100	_	-	61 103	48 74		58 101	51 85	57 93	59 94	59 95	13	19.5 22.5	5.4	70 64	42 42	40 37	36 34	21	18
64 102	-		64 104	50 71		61 102	53 84	60 93	61 94	61 96	13	19.8 22.5	5.4	70 64	42 42	40 37	36 35	21	18
65 103			64 104	50 71		61 102	52 85	59 93	62 94	61 96	13	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
64 103	-	•	63 104	49 71	63 99	61 102	52 85	59 93	61 94	60 97	12	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
64 103		66 103	63 103	50 71	63 99	61 102	52 85	59 93	61 94	61 96	12	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
64 102		65 103	63 104	50 71	62 99	61 102	52 85	59 93	61 94	60 96	12	19.8 22.5	5.4	70 67	42 42	40 37	36 34	21	18
												19.5 22.5	5.4	70 64	42 42	40 37	36 34	21	18
64 102		65 104		50 71	62 100	61 102	52 85	59 93	61 94	60 96	12	19.8 22.5	5.4	70 64	42 42	40 36	36 34	21	18

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.			1	2	3	4	5	6	7	8	9	1
1/10/73	23:25	181:11	3000	425	DUMMY TEST	55 94				88 118	111 116	95 112	103 110	106 108	
1/10	23:55	181:41	3000	425	DUMMY TEST	55 94				88 118		95 113	103 110	106 108	
1/11	00:25	182:11	3000	425	DUMMY TEST	55 93				88 118			103 110	106 108	
1/11	00:55	182:41	3000	425	DUMMY TEST	54 93	-			88 118	111 116		102 110	106 108	
1/11	01:25	183:11	3000	425	DUMMY TEST	54 93				88 118	111 116		102 110	106 108	
1/11	01:55	183:41	3000	425	DUMMY TEST	54 93	85			88 118	111 115		102 110	106 108	
1/11	05:30	183:41	1950	425	DUMMY TEST	1		102	110	of sh 80 112	100	86 107	92 106	97 103	110
1/11	05:45	183:56	1950	425	DUMMY TEST	72 100				83 113	103 112		94 108	98 105	
1/11	06:15	184:26	3560	425	DUMMY TEST	76 105				87 120	110 119		101 112	104 110	_
1/11	06:30	184:41	1950	425	DUMMY TEST	63 93				83 118	105 115		97 107	100 110	
1/11	07:00	185:11	3560	425	DUMMY TEST	61 94				84 121	108 118		100 112	102 110	

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATO

				71 4	20	10.01
16	MI	76	$\kappa \wedge$	10	KE	(°C)

7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
95 .12					98 108					80 97		85 93	83 87	85 91		83 100	87 89		76 93	65 88	-	62 83	48 82
95 .13					98 108							85 93				83 100	87 89		76 92	65 88	58 84	62 83	48 82
95 13					98 108					80 97		86 93				83 100	87 89	80 92	76 92	65 88		62 83	47 82
95 12					98 108					79 97	78 93	85 93	83 87			83 100	87 89		76 93	64 89	57 84	61 82	46 81
95 12					97 108					79 96	77 93	85 93	83 87			83 100	86 89	80 92		64 88		61 82	45 81
95 12	102 110				97 108					79 96	77 93	85 93	83 87	8 5 91	80 86	83 100	86 89	80 92		64 88		61 82	45 81
86 97	92 106	97 103	116 112	82 102	88 104	72 74	78 101	77 101	88 105	72 93	70 89	72 85	63 79	64 82	61 79	65 90	69 80	69 84		64 84	72 84	71 85	60 82
38 LO					91 105					73 95	72 92	75 88	65 81	70 85	63 81	69 94	72 84	72 87	62 87	62 84	67 81		56 80
)3 L4	101 112	104 110	129 119	90 109	97 110	82 79	88 107	86 112	96 111	78 99	77 96	84 96	82 92	86 95	80 90	82 102	86 93	80 97	79 96	64 89	69 85	67 87	59 84
.0	97 107	100 110	123 116	87 105	92 107	79 77	79 103	81 107	91 108	72 96	72 95	78 94		70 90	70 85		79 87						
12	100 112	102 110	127 118	88 110	95 110	79 79	80 105	85 112	93 110	75 98	73 95	82 95	82 92	86 96	78 89	81 102	82 92	77 96	76 95	59 90		56 84	41 82

_	64				. +==	7 /	CLIF	227 -	101			-									
A	CK.	10	-8/	C	TES) [3HI	EIS	8												
																		PUMP			NIF
		24	2.5	24	27	20	20	40	41	40		4.4	4.5		4=	46		OW	DDECC		RES
2	33	34	33	30	37	38	39	40	41	42	43	44	45	40	4/	48	IOIAL	ROLLER	PRE33	MAIN	L/F
8	40 82	72 95	59 88	72 99	64 102		65 104			62 101	61 103	52 86	59 93	62 95	60 97	11	19.8 22.5	5.4	70 63	42 42	40 36
.8 .3	40 82	72 95	59 88		63 103		66 104			63 101	61 102	52 85	59 93	61 94	60 97	11	19.8 22.5	5.4	70 63	42 42	40 36
7	39 82	7 2 9 5	59 88		63 103		66 104			62 101	60 1 0 2	51 85	59 93	61 94	60 97	10	19.8 22.5	5.4	70 63	42 42	40 36
7 3	39 82	72 95	58 88		63 102		66 104			61 101	60 102	51 85	58 93	61 94	59 97	9	19.8 22.5	5.4	70 63	42 42	40 36
6 3	3 8 82	72 94	58 88		63 102		67 104			61 100	60 103	51 85	58 93	61 94	59 96	9	19.8 22.5	5.4	70 63	42	40 36
6 3	38 82	72 94	58 88		63 102		66 104			61 100	60 103	51 85	58 93	61 94	59 96	9	19.8 22.5	5.4	70 63	42 42	40 36
2 6	63 85	71 89	62 83	72 90	66 89	72 91	68 95	62 95	39 69	62 89	62 91	56 80	60 89	65 89	66 85	9	18.3 22.5	5.4	71 65	42 43	40 37
8	59 81	70 91	62 84	72 94	76 97	77 93	68 98	67 100	42 70	68 94	65 96	58 82	61 91	67 92	67 92	8	18.6 22.5	5.4	71 65	42 43	40 37
1	63 84	72 95	65 90	73 99	79 104		70 106		47 74	70 95	68 98	62 88	64 95	70 96	69 97	8	19.5 22.5	5.4	71 64	42 42	40 36
																	18.3 22.5	5.4	71 64	42 42	39 36
2 L	33 83	68 95	53 89	68 99	60 1 0 2	82 96	63 106	57 106	43 73	57 101	56 104	47 87	54 94	57 95	55 97	7	<u></u> 18.0	÷.4	71 63	42 41	40 36

E	ET 3	(8)															
											PUMP			NIFO			AMY
											ow			RESS		PRE	ESS
9	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
5 +	62 1 0 4	50 71	62 101	61 103	52 86	59 93	62 95	60 97	11	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
5	62 104	50 71	63 101	61 102	52 85	59 93	61 94	60 97	11	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
5	62 104	50 71	62 101	60 102	51 85	59 93	61 94	60 97	10	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
5	62 104	19 71	61 101	60 102	51 85	58 93	61 94	59 97	9	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
7	61 104	49 71	61 100	60 103	51 85	58 93	61 94	59 96	9	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
64	61 104	49 71	61 100	60 103	51 85	58 93	61 94	59 96	9	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
8	62 95	39 69	62 89	62 91	56 80	60 89	65 89	66 85	9	18.3 22.5	5.4	71 65	42 43	40 37	36 35	21	18
8	67 100	42 70	68 94		58 82	61 91	67 92	67 92	8	18.6 22.5	5.4	71 65	42 43	40 37	36 35	21	18
0 6	70 106	47 74	70 95	68 98	62 88	64 95	70 96	69 97	8	19.5 22.5	5.4	71 64	42 42	40 36	36 34	21	18
										18.3 22.5	5.4	71 64	42 42	39 36	35 34	20	17
36	57 106		57 101	56 104	47 87	54 94	57 95	55 97	7	18.9 22.5	5.4	71 63	42 41	40 36	36 34	20	18

Mary Control of the Control

	- 4														
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	_
1/11/73	07:15	185:26	1950	425	DUMMY TEST			99 118	113 124		105 114		97 109	100 105	1
1/11	07:45	185:56	3560	425	DUMMY TEST		106 84	97 121	114 124		108 118	-	100 112	102 110	1
1/11	08:00	186:11	1950	425	DUMMY TEST			98 117	113 122		104 113			99 104	1
1/11	08:15	186:26	3700	425	DUMMY TEST		106 84	97 120	114 124	84 121	108 117	-		102 108	1
1/11	08:30	186:41	1950	425	DUMMY TEST		106 82		113 122		105 112		97 108	100 105	נ
1/11	08:45	186:26	3700	425	DUMMY TEST	96	85	120	115 124	-	118	114	100 111 H.P	103 109	
1/11	10:20	186:56	1100	250	DUMMY TEST	76		109		83		88	97	101 105]
1/11	12:35	187:26	1100	250	DUMMY TEST	74 96		104 116		83 110				101 100	
1/11	13:05	187:56	1100	250	DUMMY TEST		111 85		117 123		110 116	-		104 106]
1/11	13:35	188:26	1100	250	DUMMY TEST			104 115	117 118		110 112			103 102	
1/11	14:05	188:56	1950	250	DUMMY TEST		112 85	104 120	119 123		112 115		103 110	107 107	

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BAC

<u>_</u>	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	
	122 116					81 106				78 93	71 85	75 90	70 85	75 97	78 87									
			95 110			86 112				83 96		83 97		81 102	85 95	78 96	77 95	59 90	52 85	56 84	41 82	39 81	41 84	3 8
	121 115		92 105			81 105			72 92	78 91	71 83	74 87	68 83	73 96	76 85									
	126 116		-			85 111				81 94		81 95	77 89	80 101	83 92									
1	122 115	85 113				80 105			71 92	77 91	70 83	74 87	66 82	72 95	76 85									
	117	110	95 110 ect s	78	105		110	97	94	82 94 on po	94	84 96 10:			85 93									
		88 107	-			81 104				78 89		74 86	67 85	72 95	76 85	72 89	65 89	71 38	58 84	62 82		38 82	51 84	4; 8
		89 102			79 100		92 102		73 88	77 83	68 77	75 80	66 77	71 89	75 78	73 82	63 82	65 82	56 77	60 75		37 75	48 77	4: 7
	125 117	94 114	98 109	83 79	83 104	85 105	97 108	81 97	78 95	83 90	78 84	80 86	71 85	76 95	82 85	77 90	68 90	67 90	57 83	61 80	48 80	37 79	48 81	4: 8:
	124 113	92 110	95 105	83 75	83 100	84 102	96 105	80 95	77 92	82 87	73 81	80 82	70 80	75 90	81 82	76 85	67 85	66 85	57 86	61 79	48 76			
	128 116	96 116	100 108	85 78	85 103	88 106	98 107	83 97	80 93	86 90	80 84	83 87	78 84	80 98	87 87	81 90	72 90	67 89	58 81	62 79	49 79	37 77	49 79	42

CK TEST (SHEET 39)

														PUMP		MA	NIFO	LD		YMM
													FL	ow		P	RESS			PUT ESS
36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
													18.3 22.5	5.4	71 64	42 42	39 36	35 34	21	18
65 99	59 102	82 98	62 106	56 106	43 74	55 102	54 105	46 88	53 94	57 95	54 98	5	18.9 22.5	5.4	71 63	42 41	40 36	36 34	21	18
													18.3 22.5	5.4	71 64	42 42	39 36	35 34	21	17
													18.9 22.5	5.4	70 63	42 41	39 36	35 33	21	17
													18.3 22.5	5.4	70 64	42 42	39 36	35 34	21	17
													18.9 22.5	5.4	70 64	42 41	40 36	36 34	21	17
73 95	68 95	79 95	70 99	67 99	49 76	67 93	65 97	58 85	63 92	65 92	63 93	17	19.8 22.5	5.5	70 64	42 42	40 37	36 35	21	18
72 90	65 93	78 89	70 94	63 95	51 67	64 90	62 93	55 78	62 87	62 89	61 89	18	19.2 22.5	5.3	70 65	43 42	40 37	37 35	21	18
74 98				66 105	53 76	68 98	66 102	57 87	63 93	64 94	62 95	15	20.1 22.8	5.5	70 64	42 42	40 36	36 34	21	18
73 87		82 93	69 97	66 104	52 69		66 99	56 82	62 90	63 93		16	19.2 22.2	5.4	70 64	42 42	40 36	36 34	21	18
	67 104			66 105	54 73	69 99				64 94		16	20.1 22.5	5.4	70 64	42 42	40 37	37 34	21	18

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6		. 8	9	
1/11/73	14:35	139:26	1950	250	DUMMY TEST	75 99		_	118 124				104 110	107 107	
1/11	15:05	189:56	1950	250	DUMMY TEST	75 99				89 116			104 109	107 106	
1/11	15:35	190:26	1950	250	DUMMY TEST	74 99				89 115				106 105	129
1/11	16:05	190:56	1950	250	DUMMY TEST	74 98			117 123				103 109		12
1/11	16:35	191:26	1950	250	DUMMY TEST	74 98	111 84			88 115					12(
1/11	17:05	191:56	1950	250	DUMMY TEST	75 98				88 115				106 105	
1/11	17:35	192:26	1950	250	DUMMY TEST	75 98			117 123		111 115	-	103 108		128
1/11	18: 35	192:56	1950	250	DUMMY TEST	74 98	111 85					•		106 105	
1/11	18:35	193:26	1950	250	DUMMY TEST	74 97				89 115				106 105	
1/11	1.9:35	193:56	2400	250	DUMMY TEST	74 98				89 117				106 108	129 117
1/11	19:35	194:26	2400	250	DUMMY TEST	74 98				88 117				105 108	

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK

10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33
129	96 115	100 108	66 76	. 55 103	58 101	95 107	83 97		87 90	50 54	85 88	77 81	50 96	87 87	81 90	73 90	67 88	58 81	62 78	-	38 79	49 79	
129 116	96 115	100	55 77	66 103	88 108	96 107	67 97	50 92	56 90	90 90	63 87	77 53	50 97	87 56	50 39	72 89	67 88		62 78	49 78	38 76	49 79	42 78
L29 115	95 115	99 107	65	85 103	87 106	97 107	52 96	79 92	85 90	79 81	83 87	76 63	79 97	56 56	80 89	72 89	66 87	57 80	61 78	48 78	37 76	49 79	42 78
L28 L16	95 110	99 107	35	65 103	57 106	97 106	52 36	79 32	65 69	79 83	83 87	76 63	79 96	66 66	79 69	71 89	65 87		61 78		37 76	49 78	
.28 .15	94 114	98 107	85 76	84 102	87 206	97 106	81 95	79 91	64 69	79 82	84 87	75 62	76 96	86 85	79 89	71 89	65 87		61 77			48 78	
.28 .15	94 114	98 107	85 76	85 102	87 106	97 106	81 95	79 91	84 89	79 82	84 86	75 82	78 96	85 85	79 88	71 89	65 87	57 80	61 78			48 78	
.28 .15	94 114	98 107	85 76	85 102	67 106	97 106	81 95	79 91	84 89	79 82	84 86	75 82	78 96	86 85	79 88	71 88	65 87	57 80	61 78	48 78		48 78	41 77
28 15	95 114	99 107	85 76	85 103	87 105	97 106	82 95	79 92	85 89	79 83	84 8E	76 83	79 96	86 85	79 88	71 88	65 87		61 77	48 77			41 77
28 15	95 114	99 107	85 76	85 103	87 105	97 106	82 95	92 80	85 89	79 83	85 87	76 82	79 96	86 85	9 88	71 88	66 86	56 79	61 77			48 77	
29 17	95 116	99 110	85 78	85 105	87 109	97 109	81 97	79 93	86 92	82 86	87 90	79 85	82 98	88 88	81 91	76 91	65 88	56 81	60 78		36 77	48 79	_
28 17		98 110					81 97	79 93	85 92	81 86	87 90	78 86	81 98	88 88	80 91	74 91	64 89	56 82	60 79	47 78		47 79	40 79

ES	T (S	HE	ET 4	101													ia.		
													PUMP		MA	NIFC	OLD		YMA
	•												.ow			RES		PRE	PUT
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	I./H	R/H	L/H	R/H
67 104	86 94	70 102	67 105	54 73	68 99	66 102	5 8 85	64 92	64 93	63 97	17	20.1 22.5	5.4	70 64	42 42	40 37	36 34	21	18
67 104	85 95		67 104	53 72		66 102	58 85	63 92	64 93	63 97	17	20.1	5.4	70 64	42 42	40 37	36 34	21	18
67 104	85 91,		67 105		68 98	66 102	58 85	63 91	64 93	62 97	17	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
66 104	84 94		66 104	52 72	67 98	65 102	57 85	63 91	64 93	62 97	16	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
66 104	84 94		65 104	52 71	67 98	65 101	56 85	62 91	63 93	61 96	16	19.8	5.4	70 64	42 42	40 37	36 34	21	18
66 103	84 94	68 101	65 104		67 98	65 101		63 91	63 93	61 96	17	19.8	5.4	70 64	42 42	40 37	36 34	21	18
66 103	84 94	68 101	65 104		66 98	65 101		63 91	62 93	61 96	17	19.8 22.5	5.4	70 64	42 42	40 37	36 34	21	18
	84 94		66 104	52 71	67 98	65 101	56 84	63 91	63 93	62 96	17	19.8	5.4	70 64	42 42	40 37	36 34	21	18
66 103	84 93		66 104		67 97	65 100	56 84	63 91	64 92	62 96	16	19.8	5.4	70 64	42 42	40 37	36 34	21	18
66 104	85 95		66 107			65 104	56 86	63 92	63 94	61 97	15	19.8 22.5	5.4	70 64	42 42	40 36	36 34	21	18
65 104	85 95		65 107	51 73	66 100	64 104	55 86		62 94	60 98	14	19.8 22.5	5.4	70 64	42 41	40 36	36 34	21	18

				1	,											TA
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5_	6	7	8	9	1() 11
1/11/73	20:5	194:56	2400	250	DUMMY TEST			_	117 124		111 117			_	128 117	9¼ 116
1/11	20:35	195:26	2400	250	DUMMY TEST	74 98		103 120	117 124		111 117				128 117	94 116
1/11	21:05	195:56	2400	250	DUMMY TEST	74 98		103 120	117 124		111 116	-	_	-	128 117	93 116
1/11	21:35	196:26	2700	250	DUMMY TEST			103 120			112 117				129 117	94 116
1/11	22:05	196:56	2700	250	DUMMY TEST	97	86	120			117	113	111	108	129 117	94 116
1/11	23:35	197:26	3000	425	DUMMY TEST		109		116	-	l loa 111 115	94	103	105	130 116	94 114
1/12	07:05	197:56	3000	425	DUMMY TEST	71 101		102 119			111 117	-	_		130 117	93 116
1/12	ია: 35 (198:26	300C	425	DUMMY TEST	70 101		101 119			111 117	-	_		129 117	93 116
1/12	01:05	198:56	3000	425	DUMMY TEST	70 101		101 119	116 123	86 117	111 117		_		130 117	93 116
1/12	01:50	199:41	3000	425	DUMMY TEST	100	74	119		117	111 116	112	110	107	130 117	93 116
2 /26	0	100.56	2000	Los	D1111-111				of s							shift
1/12	05:55	199:56	3000	425	DUMMY TEST	80 106		108 121		85 118	109 117	91 113			128 117	92 114

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK

															:		, -,						
_10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	3:
128	94 116	-		64 105		97 109	51 97	79 93	85 92	51 85	87 90	78 86	81 98	56 55	50 91	73 91	64 89	56 81	59 78	47 78	35 77	46 79	35 78
128 117	94 116	98 110	84 78	84 105	87 109	97 109	81 97	79 93	85 92	81 85	87 90	78 86	81 98	86 88	80 91	73 91	64 89	56 81	59 78	47 78	35 77	46 79	
128 117	93 116	98 110	84 78	84 105	87 109	96 109	81 98	78 93	85 92	80 86	8 £ 90	77 56	80 98	87 89	79 91	73 91	64 89	55 81	59 79	46 78		46 79	
L29 L17	94 116	98 109	84 78	84 105	87 110	97 109	51 97	75 93	86 92	83 87	59 91	80 87	83 99		50 91	76 92	64 88	55 81	59 79	45 78	34 76	46 79	39 78
							81 97						82 99	87 58	50 91	76 92	64 88	56 81	59 79	45 78		46 78	
							dummy.		-														
.30 .16	94 114	98 108	54 77	82 104	87 110	97 108	79 96	77 94	85 91	51 86	56 90	79 85	81 98	87 87	80 91	76 91	65 87			48 79		48 81	
30 17	93 116	98 109	83 77	82 104	87 110	97 109	79 96	77 94	85 91	81 86	86 90	79 86	81 95	87 87	80 91	75 91	64 87	58 82	62 80	48 80	35 78	47 81	40 80
29 17	93 116	98 109	83 77	81 104	87 109	97 108	79 96	77 94	85 91	81 86	86 90	79 86	82 98	86 88	80 91	75 91	(4 88	57 82	61 80	46 80	34 78	47 82	39 81
30 17	93 116	98 109	83 77	81 104	86 109	97 108	79 96	78 94	85 90	81 86	86 90	79 86	82 98	86 88	80 91	75 91	64 88	57 82		46 80	34 78		39 81
17	93 116	109	77	104	87 109	97 108	79 96	78 94	85 91	82 86	87 90	79 86	82 98	57 89	80 91	75 91	64 88	58 82	61 80	47 80	34 78		39 80
ts	hift	-		r 05:						12													
?8 .7	92 114				85 111		78 98	77 93	83 92	78 8 8	82 92	76 87	7 9 100	85 89	78 92		66 88			61 82	62 81	62 84	

ES	T (S	SHE	ET4	11)															
													PUMP			NIFO			AMY
													OW			RESS		PRI	SS
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
64 03		66 103	64 106	51 72	66 99	64 103	55 87	61 92	62 94	60 98	14	19.8 22.5	5.4	70 63	42 41	40 36	36 34	21	18
64 .03		66 103		51 72	66 99	64 103	55 87	61 92	62 94	60 98	14	19.8 22.5	5.4	70 63	42 41	40 36	36 34	21	18
64 L03		66 104		50 72	65 99	63 104	54 87	60 92	61 94	60 98	14	19.8 22.5	5.4	70 63	42 41	40 36	34,	21	18
64 103		68 104		50 72	65 99	64 104	64 87	54 92	61 94	61 98	14	19.8 22.5	5.4	70 64	42 42	40 36	37 34	21	18
64 103		68 104		50 72	65 99	64 104	54 87	61 92	61 94	60 98	14	19.8 22.5	5.4	70 64	42 42	40 36	37 34	21	18
64 101		68 104		49 71	64 98	62 103	53 85	61 93	62 94	60 95	12	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
64 102		67 104		49 72	62 99	61 104	52 86	60 93	61 95	60 95	12	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
63 102		67 104	62 107		61 99		52 86	59 93		59 96	10	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
63 102		67 104		49 72	60 99	60 104	52 86	59 93	61 94	59 96	10	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
65 102		67 104		49 72		60 104	52 86	59 93	61 95	59 95	11	19.8 22.5	5.4	70 63	42 42	40 36	36 34	21	18
79 103		73 104		47 74	72 100	70 102	63 87	66 94	70 95	70 96	11	19.8 22.5	5.5	71 64	42 42	40 37	3 6 3 5	21	18

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
1/12/73	06:10	200:11	1950	425	DUMMY TEST	74 100	107 77		113 123					101 108	12
1/12	06:40	260:41	3000	425	DUMMY TEST	70 100	107 77		114 124					102 109	12 11
1/ 1 2	07:10	201:11	3000	425	DUMMY TEST		107 77		115 124					103 109	12 11
1/12	07:40	201:41	3000	425	DUMMY TEST		107 76		115 124	84 118				103 109	12 11
1/12	08: 10	202:11	3000	425	DUMMY TEST		108 75	101 120	115 124			-		103 109	12 11
1/12	08:40	202:41	3000	425	DUMMY TEST	70 100	108 75	101 120	115 124	_	_	-		103 109	12 11
1/12	09:10	203:11	3000	425	DUMMY TEST	70 100	108 75	101 120	116 124	_				104 109	12 11
1/12	09:40	203:41	3000	425	DUMMY TEST	70 99	108 75			85 118					
1/12	09:55	203:56	1950	425	DUMMY TEST		108 73		114 122	118 115				102 105	12 11
1/12	10:25	204:26	3560	425	DUMMY TEST	70 100	108 76			86 120					13 11
										an sl	_			on p	
1/12	11:00	204:41	1950	425	DUMMY TEST	72 99	109 74	102 117						103 104	12

ABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK-TO-I

1 12	13 14	15 16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	:
8 93 7 109	80 80 78 105	82 93 108 109	76 98	75 94	80 92	72 85	77 90	71 85	76 99	81 88	75 92	66 93	63 90	60 84		49 82	37 81	50 85	42 84	72 95	
	80 80 79 105	84 93 110 110	76 98		82 92	77 88	83 92	76 87	79 100	83 90	77 92	72 93	62 90	57 83		46 81	33 79		39 82		4
	81 80 79 105	85 94 111 110	77 98	75 94	82 92	78 88	83 92	76 87	79 100	84 90	77 93	73 92	62 90	57 84		47 81	34 79		39 82		
		85 95 110 110	77 98	76 93	82 92	80 87	85 91	77 87	80 99	85 89	77 92	73 93	62 89	56 83		46 81	33 79	46 83	38 82	70 94	
		85 95 110 109	78 97	76 94	83 91	80 87	85 91	77 87	80 99	85 93	78 92	73 92	62 89		60 81	47 81	34 79		38 81		" " "
		85 95 110 109	78 97	76 94	83 92	80 87	85 91	77 87	80 99	85 93	78 93	73 93	62 89		60 81	47 81	34 79		38 82		5, 9
? 97 ' 110		86 96 110 109	78 97		84 92	81 87	87 91	77 87	81 99	86 91	78 9 2	74 92	63 89	58 84	61 81	47 81	34 79	46 82	39 82		5
97 110		86 96 110 109	78 97				85 9 2	78 87	81 99	85 96	78 92	74 92	63 39	58 83	61 81		34 79		39 81	71 94	5
		83 93 106 107			80 89	74 83	79 87	71 83	76 96	80 91	7 ¹ 4 89	66 90	62 87	58 82		48 80			38 81		5 8
98 112	83 81 79 106	88 97 114 111	80 98		86 94	86 92	91 97	82 91	86 102	87 92	81 96	79 96	63 90			49 82	35 79		40 82		5 9.
0:45 96 110	82 81 75 101	85 95 105 105	79 95		81 87	72 81	77 83	71 80	75 94	80 83	76 85	67 85	65 85		65 79		38 76		43 79		61 8;

'ES	T (S	SHE	ET 4	42)															
										-			PUMP			NIFC			MMY PUT
27	20	20	40	49	40	4.0	4.4	4.5	4.4		40		OW	DDECC		PRES		PR	ESS
37	38	39	40	41		43						IOIAL	ROLLER	PKE33	MAIN			L/H	
59 05	82 97		67 110			64 106	55 87	62 95	63 96	62 98	17	19.2 22.5	5.4	71 64	42 42	40 37	36 35	21	18
63 05	88 96		62 110	45 73		60 106	51 88	58 94	60 94	58 98	13	19.2 22.5	5.4	71 63	42 42	40 36	36 34	21	18
63 04			61 110			58 106	50 87	58 94	59 94	58 98	12	19.2 22.5	5.4	71 63	42 42	40 36	36 34	21	18
62 04			61 110	46 73		58 106	50 87	58 94	59 94	59 98	10	19.2 22.5	5.4	71 64	42 42	40 36	36 34	21	18
62 04		69 104	61 110		58 101	57 106	50 87	58 94	59 91	58 98	10	19.2 22.5	5.4	71 64	42 42	40 37	36 34	21	18
62 04		69 105				58 106	50 87	58 94	59 94	58 98	10	19.2 22.5	5.4	71 64	42 42	40 37	36 34	21	18
63 04		69 105		47 73		58 106	51 87	58 94	60 94	58 98	11	19.5 22.5	5.5	71 64	42 42	40 37	36 34	21	18
62 04		69 105	61 110	47 73	61 102	59 106	50 87	58 94	60 94	58 98	10	19.2 22.5	5.4	71 64	42 42	40 37	36 10	21	18
62 03		69 101			61 100	59 106	50 86	58 93	59 94	58 97	10	19.2 22.5	5.4	71 64	42 42	40 37	36 35	21	18
62 03		70 107			61 102		61 89	59 95	51 96	58 98	10	19.5 22.5	5.4	71 63	42 41	40 36	36 34	21	18
66 01		73 99			65 96	63 104	53 82	62 91	63 92		12	19.5 22.5	5.4	71 65	42 42	40 37	36 34	21	18

PROSESS PROTECTION

The second second

								yx:							
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
1/12/73	11:30	205:11	3560	425	DUMMY TEST	72 102				89 119		96 114	111 112		133 119
1/12	11:45	205:26	1950	425	DUMMY TEST	74 100				87 115		93 110		-	128 116
1/12	12:15	205:56	3560	425	DUMMY TEST	72 102				89 120		96 115	-		133 118
1/12	12:30	206:11	1950	425	DUMMY TEST	74 100				87 115		93 110	102 109	-	128 116
1/12	12:45	206:26	3700	425	DUMMY TEST	84 101				89 119		96 114			132 118
1/12	13:00	206:41	1950	425	DUMMY TEST	75 101				88 116		94 110			128 117
1/12	13:15	206:56	3700	425	DUMMY TEST	73 102				89 119		96 114		-	132 118
						St	op fo	or in	nspec	tion	of	chip	dete	ctors	5
						i									

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABOR.

6	7	8	9	10		12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29
15 19	-	111 112			97 118					100 110	83 99	82 95	89 93	88 92	93 95		89 102	92 91		82 96	67 89	63 84	
10 15		102 109			93 115					97 107		80 92	85 90		83 88	76 83	81 97	85 85					
L4 L9		106 112			96 118	101 110				100 111	83 99		90 95				88 102	92 92	84 95	83 96	68 89	63 84	68 82
LO L4		102 109			93 115	98 107				97 107		80 92	85 90	77 84	83 88	76 83	81 97	86 86					
.3 .9		105 112		132 118	96 117					99 110		81 93	88 92	89 88	•		88 100	89 91					
.1 .5	-	103 110	-		93 115				86 107	97 108		81 93	86 91	79 85	85 89	78 84		87 87					
.3 .8		105 112		132 118	96 118				90 113	99 110	83 98	81 94	88 92	89 91	94 95		88 101	90 92					
f	chip	dete	ctors	5																			

	TES	T (S	HE	ET 4	13)						-									
_														PUMP		M	ANIFO	LD		YMN
													FL	ow		. 3	PRESS		PR	PUT
5	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAI	I L/H	R/H	L/H	R/H
7	67 104	89 96	76 106	67 109	52 73	65 100	63 106	56 87	63 94	63 95	64 98	13	19.8 22.5	5.4	71 63	42 41	41 36	37 34	21	18
													19.5 22.5	5.4	70 64	42 42	40 34	36 35	21	18
7 0	66 104	89 97	76 106	66 109	53 74	64 101	63 106	55 88	63 94	64 95	63 98	13	20.1 22.5	5.4	70 63	42 41	40 36	37 34	21	18
													19.8 22.5	5.4	70 64	42 42	40 37	36 35	21	18
													19.8 22.5	5.4	70 63	42 41	41 36	37 34	21	18
													19.8 22.5	5.4	70 64	42 42	40 37	36 35	21	18
													20.1 22.5	5.4	71 64	42 42	41 36	37 34	21	18
												;								
								· · · · · · · · · · · · · · · · · · ·		-										

DATE	OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	2 3	1_ 1	4 5	;	6	7	_8	9	10
						N	lo lo	oad t	est				St	art	100%	R.P.M
1/15 /73	18:35	206:56	0	0	DUMMY TEST		108 65		5 11 3 7			106 90	89 79	97 78	102 81	
1/15	19:05	206:56	0	0	DUMMY TEST	76 67	114 67		l 11) 6			110 89	92 75	100 70	105 79	120 87
						St	op (check	st	raine	rs		re	star	t 10	00% R.
1/15	20:45	206:56	0	0	DUMMY TEST	68 52	109 57		11 6			104 83	87 66	95 65	98 71	114 79
1/15	21:15	206:56	0	0	DUMMY TEST	53	-	61	11	2 6	5	104 84	87 66	95 66	99 72	81
1/15	22:00	206:56	0	0	DUMMY TEST		109	93	k s 11 9 6		9	s 104 82	86 65	94 65		113 78
1/15	22:30	206:56	0	0	DUMMY TEST	53	109 58	65	11 6		6	104 85	68	94 67	98 73	114 80 R.P.M
1/15	23:30	206:56	0	0	DUMMY TEST	68	111 56	95		3 82	2		90	98	101 70	
						St	op e	and c	hecl	stre	i	ners				

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY B

!	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	,
	100%	R.P.M	. at	18:	05																			
1	102 81	117 89	91 90	95 93	82 76	88 92	82 100	93 9 8	84 92	79 86	80 74	72 78	77 79	68 78	74 78	78 78	75 77	67 76	76 80	70 70	68 71	55 70	45 65	
	105 79	120 87	95 87	98 90		90 90	86 96	97 94	90 89	83 84	83 74	76 74	80 76	71 74	77 75	82 75	78 78	71 78	80 79	74 70	71 69	58 69	49 65	
r	rt 10	00% R.	P.M &	at 20	:15																			
;	98 71	114 79	88 79	92 83	81 64			91 89		83 77	76 66	69 67	74 68	64 67	70 68	75 68		64 70	67 71	54 58		30 60	24 54	
;	72		80	84	81 66	77 83	81 94	92 90	83 83	77 78	77 68	69 69		65 69		75 70		64 72	67 74		53 62		22 55	
r	t 10	0% R.	P.M ε	it 21	: 30																			
;	98 70	113 78	88 79	92 82	79 64	76 82	80 93		82 81		76 66	68 67	74 69	63 67	70 68	74 68		63 71	66 71	52 58	52 59	29 61	21 54	
•	73	114 80 R.P.M	81	84	79 66 0		81 95		82 83		76 69			64 70		75 70	71 73	63 73	66 74	52 60	52 62		20 55	
}	101 70	117 79	91 79		83	78 82	84 93	94 89	86 82	78 76	79 66	68 67	77 69	67 67	73 69	78 68	75 70	67 70	69 71	54 58	54 60	29 60	21 53	

-	TES	T (S	HE	ET 4	4)	-														
-		•												PUMP		MA	NIFC	LD		AMY
														ow			RESS		PRE	PUT ESS
5	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
j	81	80	72	73	46	74	73	68	67	73	73	17	19.8		69	41	39	36	21	18
ŀ	87	85	81	74	74	71	72	59	90	74	68		22.5	5.5	65	42	37	35		
5	83 92	85 85	76 79	76 81	59 70	80 78	78 79	73 49	73 84	77 79	78 71	16	20.7	5.4	69 65	41 42	39 37	36 35	21	18
1	65 81	77 77	59 71	63 69	52 63	64 57	62 67	53 54	70 77	61 66	60 60	16	19.8	5.2	69 64	41 42	39 37	17 34	21	18
1 9	64 84	77 79	60 74	62 71	52 66	63 57	61 70	53 58	70 78	61 66	60 60	14	19.8 21.9	5.2	69 64	41 42	38 37	36 34	21	18
0 8	63 82	76 77	63 72	59 71	51 63	62 57	60 69	51 61	69 76	59 66	58 60	13	19.5 21.6	5.1	70 64	41 42	39 37	37 34	21	18
0	63 84	76 79	63 74	59 74	51 66	62 57	60 71	51 91	69 78	59 66	58 60	12	19.8 21.9	5.2	70 64	41 42	39 37	36 35	21	18
9	64 85	80 78	65 72	63 71	56 63	64 58	62 68	53 66	71 77	61 66	61 60	12	19.8 21.9	5.2	70 64	41 42	39 37	36 34	21	18

				•											
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5_	6	7	8	9_	
1/16/73	08:05	206:56	1100	250	DUMMY TEST			105 112		92 107	115 107			110 97	
1/16	08:35	207:26	1100	250	DUMMY TEST		_	97 115	114 119	89 110		93 108		106 100	
1/16	09:05	207:56	1100	250	DUMMY TEST			95 115		88 111	108 112	91 99		103 102	
1/16	09:35	208:26	1100	250	DUMMY TEST			-	113 120	88 112		91 110		103 102	
1/16	10:05	208:56	1950	250	DUMMY TEST			96 120	115 124	90 117		95 115	-	106 109	
1/16	10:35	209:26	1950	250	DUMMY TEST	71 100			114 121	89 114		93 111		105 105	
1/16	11:05	209:56	1950	250	DUMMY TEST				114 121	88 113		93 110		104 105	
1/16	11:35	210:26	1950	250	DUMMY TEST	71 99	111 73	95 116	113 121	88 112	109 112	92 109	101 105	104 104	Ľ Ľ
1/16	12:05	210:56	1950	250	DUMMY TEST				113 120			93 109		105 104	
1/16	12:35	211:26	1950	250	DUMMY TEST				113 121	89 114		93 108		104 105	
1/16	13:05	211:56	1950	250	DUMMY TEST				114 122	89 114	109 114			105 106	

TABLE XXI. ROLLER	GEAR TRANSMISSION	TEST DATA:LABORAT

7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	3
97 101	107 102			97 105	101 99	85 68		88 97	99 99	87 86	85 82	86 78	79 72	82 75	78 73		85 81	82 77	76 77	84 77	79 69	78 72	Ę
93 108			126 110		98 100			85 102	97 102	82 90	79 88	85 85	76 79	80 82	72 78	78 90	84 89	75 84	69 83	70 81	-	58 74	4
91 99					96 102			83 103			77 88		72 81		69 80		81 90	75 85	66 85	68 82	57 71	57 76	4 7
91 110					97 103								72 81				81 89	75 87	66 86	68 84	57 72		4 7
95 115	103 112	106 109	129 117	95 116	99 108	84 78		86 110				85 93	79 87	81 92	75 86		86 96	79 9 2	71 91	68 82	57 76	57 80	4' 7
93 111					97 105		83 99		96 105			83 90	77 83	80 87	73 82	77 95	84 92	77 89	69 90	66 84	56 72	56 76	4' 7
					97 104			84 106				82 89	76 82	79 85	72 81	76 93	83 90	77 87	68 87	66 82	56 71	56 75	47 7
92 109			126 112	-	97 103	82 74	83 98	84 105	95 105	78 91	76 89	82 88	76 82	78 85	72 80	77 93	82 90	77 87	68 88	67 82	56 71	56 75	¥ 7:
93 109	101 106	105 104	126 111	92 110	97 103	83 72	84 97	85 105	95 103	78 91	77 88	82 87	76 81	78 85	72 80	77 92	83 88	77 86	68 87	66 82	57 71	57 74	47 72
93 108	101 107	104 105	126 112	92 112	97 104	82 74	83 98	84 107	95 105	78 92	76 90	82 89	76 84	79 86	72 82	76 94	83 90	77 88	68 89	66 84	57 72	57 76	47 71
93 110	101 109	105 106	126 114	92 112	97 105	83 75	84 100	84 107	95 105	78 93	77 90	82 89	76 84	79 87	72 83	77 95	83 91	77 89	68 90	66 84	57 72	57 77	47 71

T	A;L	ABO	OR/	NTO	RY	BA	CK-	TO	-BA	CK	TES	T (SHE	ET4	5)								
E	(°C)																						
5_	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTA
· >	84 77	79 69	78 72	65	52 67	67	58 66	83 81	75 68	85 81	84 83	88 82	79 90	80 78	62 65	82 73	79 74	74 57	76 81	80 74	80 67	18	21.3
1	70 81	58 70	58 74	48 72	36 66	47 68	42 69	76 86	63 70	76 87	69 90	83 88	74 94	70 82	52 70	70 69	68 78	58 60	74 86	67 74	65 66	19	20.1 22.5
	68 82	57 71	57 76	47 73	35 67	46 69	¹ 41 70	73 87	61 71	73 89	67 91	81 90	72 95	66 82	51 70	64 70	03 79	55 62	72 87	64 76	63 67	19	19.8 22.5
	68 84	57 72	57 77	47 74	35 69	46 70	41 71	73 89	62 73	73 89	68 92	81 90	72 96	68 84	51 72	65 71	63 80	55 62	72 89	65 77	63 68	19	19.8 22.8
	68 82	57 76	57 80	47 79	35 80	46 74	41 76	73 9 2	62 76	73 92	68 94		73 103	68 88	51 77	68 75	65 82	56 64	72 92	65 79	63 70	20	19.8 22.5
	66 84	56 72	56 76	47 74	34 69	45 70	40 71	72 89	60 73	72 90	67 93	82 90	71 99	66 85	49 71	66 72	64 80	55 62	71 89	64 78	62 69	20	19.8 22.5
	66 82	56 71	56 75	47 73	34 68	45 69	40 70	72 87	60 72	72 89	67 92	82 9 0	71 98	66 84	48 70	65 71	63 80	55 62	71 87	64 77	62 68	22	19.8 22.5

)	84 77	79 69	78 72	65 69	52 67	67 64	58 66	83 81	75 68	85 81	84 83	88 82	79 90	80 78	62 65	8a 73	79 74	74 57	76 81	80 74	80 67	18	21.3
1	70 81	58 70	58 74	48 72	36 66	47 68	4.2	76 86	63 70	76 87	69 90	83 88	74 94	70 82	52 70	70 69	68 78	58 60	74 86	67 74	65 66	19	20.1
	68 82	57 71	57 76	47 73	35 67	46 69	141 70	73 87	61 71	73 89	67 91	81 90	72 95	66 82	51 70	64 70	03 79	55 62	72 87	64 76	63 67	19	19.8 22.5
	68 84	57 72	57 77	47 74	35 69	46 70	41 71	73 89	62 73	73 89	68 92	81 90	72 96	68 84	51 72	65 71	63 80	55 62	72 89	65 77	63 68	19	19.8 22.8
	68 82	57 76	57 80	47 79	35 80	46 74	41 76	73 92	62 76	73 92	68 94		73 103	68 88	51 77	68 75	65 82	56 64	72 92	65 79	63 70	20	19.8 22.5
	66 84	56 72	56 76	47 74	34 69	45 70	40 71	72 89	60 73	72 90	67 93	82 90	71 99	66 85	49 71	66 72	64 80	55 62	71 89	64 78	62 69	20	19.8 22.5
	66 82	56 71	56 75	47 73	34 68	45 69	40 7 0	72 87	60 72	72 89	67 92	82 90	71 98	66 84	48 70	65 71	63 80	55 62	71 87	64 77	62 68	22	19.8 22.5
	67 82	56 71	56 75	47 73	34 68	45 69	40 70	72 87	60 72	72 89	68 93	82 90	71 98	66 84	48 70	65 71	63 80	55 60	71 87	64 77	62 69	22	19.8 22.5
	66 82	57 71	57 74	47 72	34 67	45 69	40 70	72 87	61 72	72 88	68 91	82 89	71 97	66 88	48 69	66 70	64 80	55 58	71 87	64 77	63 69	55	19.5 22.5
	66 84	57 72	57 76	47	35 69	46 70	40 72	72 89	60 73	72 90	68 9 2	82 90	71 99	66 87	48 71	66 73	64 82	55 57	71 89	64 78	63 69	22	19.8 22.5
	66 84	57 72	57 77	47 74		46 70	40 73	72 89	61 71	72 90	68 92	82 91		66 88	48 72	66 73	64 83	56 57	71 89	64 78	63 69	23	19.8 22.5

TES	T (S	HE	ET4	5)										.· · · · ·					
	-										•		PUMP		MA	NIFC	LD	DUA	
												FL	ow		P	RES	5	PRE	
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		R/H
84 83	88 82	79 90	80 78	62 65	82 73	79 74	74 57	76 81	80 74	80 67	18	21.3 22.2	5.3	70 66	42 44	40 39	37 35	21	18
69 90	83 88	74 94	70 82	52 70	70 69	68 78	58 60	74 86	67 74	65 66	19	20.1 22.5	5.4	70 66	42 42	39 37	36 35	21	18
67 91	81 90	72 95	66 82	51 70	64 70	63 79	55 62	72 87	64 76	63 67	19	19.8 22.5	5.5	70 66	42 44	40 38	36 35	21	18
68 9 2	81 90	72 96	68 84	51 72	65 71	63 80	55 62	72 89	65 77	63 68	19	19.8 22.8	5.5	70 66	717 715	40 38	36 35	21	18
68 94	84 94	73 103	68 88	51 77	68 75	65 82	56 64	72 92	65 79	63 70	20	19.8 22.5	5.6	70 64	42 42	40 37	36 35	21	18
67 93	82 90	71 99	66 85	49 71	66 72	64 80	55 62	71 89	64 78	62 69	20	19.8	5.5	70 65	42 43	40 38	36 35	21	18
67 92	82 90	71 98	66 84	48 70	65 71	63 80	55 62	71 87	64 77	62 68	22	19.8	5.5	70 65	42 43	40 38	36 35	21	18
68 93	82 90	71 98	66 84	48 70	65 71	63 80	55 60	71 87	64 77	62 69	22	19.8 22.5	5.5	70 65	42 43	40 37	36 35	21	18
58 91	82 89	71 97	66 88	48 69	66 70	64 80	55 58	71 87	64 77	63 69	22	19.5 22.5	5.4	70 65	42 43	40 37	36 35	21	18
58 12	82 90	71 99	66 87	48 71	66 73	64 82	55 57	71 89	64 78	63 69	22	19.8 22.5	5.5	70 65	42 43	40 37	36 35	21	18
:8 2	82 91	71 100	66 88	48 72	66 73	64 83	56 57	71 89	64 78	63 69	23	19.8	5.5	70 64	42 43	40 37	36 35	21	18

Cold and services and

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1_	2	3	4	5	6	7	8	9
1/16/73	13:35	212:26	1950	250	DUMMY TEST		113 76	98 119	116 123	92 117	113 117		105 111	108 108
1/16	14:05	212:56	1950	250	DUMMY TEST	74 102	114 76	98 119		93 116			105 110	109 108
1/16	14:35	213:26	1950	250	DUMMY TEST	74 100	112 75	97 116		90 112			102 107	106 105
1/16	15:05	213:56	2400	250	DUMMY TEST	74 101	112 75	97 117		91 114			103 107	106 106
1/16	15:35	214:26	2400	250	DUMMY TEST	74 100	112 7 5	97 117		91 114			102 108	107 106
1/16	16:05	214:56	2400	250	DUMMY TEST	75 101	112 75	97 117		91 113			102 109	107 106
1/16	16:35	215:26	2400	250	DUMMY TEST	101	112 74	117	122	91 113	114		102 109	107
1/16	17:50	215:56	2400	250	DUMMY TEST	74	111	96	eck s 114 120	90	110	95 110	102	106 104
1/16	18:20	216:26	2700	250	DUMMY TEST			99 116		-	112 113	97 111	104 108	108 106
1/16	18:50	216:56	2700	250	DUMMY TEST	101	75	117		113	113	111		108 106
1/16	19:30	217:26	3000	425	DUMMY TEST	-	111	98		90	111		103 106	107 10 ¹

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY BACK.

11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33
						83 96	80 93	86 92	80 86	82 90	77 86	81 98	88 95	81 92	72 91	70 87	60 76	60 80	48 79	37 73	50 75	40 77
									81 86				88 95	82 91	74 90	71 86	61 76	61 80	48 78	38 72	50 74	41 75
_							78 89	85 89	79 82	81 86	75 82	78 93	86 90	79 89	70 88	68 84	58 73	58 76	47 74	36 69	48 70	40 72
-						80 92			81 85	81 88	78 84	80 95	88 92	80 90	73 89	68 83	58 72	58 76	47 74	36 70	48 70	40 72
•	99 105					80 92			81 85	82 88	78 84		88 91	80 91	73 90	68 84	58 73	58 77	47 75	36 69	48 71	40 72
	98 105					80 92											57 72	58 76			48 70	40 72
112	104												87 93	79 90	73 89	67 84	58 72	58 76	48 74	35 69	47 70	41 72
93	98 102		-				77 88	84 87	79 82	81 84			86 89	79 87	73 85	68 80	57 75	57 72	47 71	36 67	48 68	40 69
										84 88	81 84	84 96	90 92	82 90								41 70
112	104	73							83 86	84 88	81 84	84 96	90 92	82 90	77 89	ნ9 82			47 72			41 70
95	99	84					79 87	86 87	81 85	83 86	79 82	82 95	88 92	80 88			61 72	61 75			5 0 72	44 72
	97 115 97 115 94 111 94 112 93 113 94 112 17:0 93 111 96 112:0 96 112:0 97	97 101 115 107 97 101 115 107 94 98 111 103 94 98 112 105 94 99 112 105 94 98 113 105 94 98 113 105 94 98 111 102 96 100 112 104 96 100 112 104 96 100 112 104 96 100 112 104	97 101 86 115 107 78 97 101 87 115 107 77 94 98 85 111 103 74 94 98 85 112 105 74 94 99 84 112 105 74 94 98 85 113 105 74 94 98 85 112 104 74 17:00 93 98 84 117:00 93 98 84 111 102 72 96 100 86 112 104 73 ower at 19:00 95 99 84	97 101 86 87 115 107 78 101 97 101 87 88 115 107 77 101 94 98 85 86 111 103 74 98 94 98 85 86 112 105 74 99 94 99 84 86 112 105 74 99 93 98 85 86 113 105 74 99 94 98 85 86 113 105 74 99 17:00 93 98 84 85 111 102 72 97 96 100 86 87 112 104 73 98 96 100 86 87 112 104 73 98 over at 19:00 95 99 84 86	97 101 86 87 88 115 107 78 101 110 97 101 87 88 89 115 107 77 101 109 94 98 85 86 86 111 103 74 98 106 94 98 85 86 86 86 112 105 74 99 109 94 98 85 86 86 86 112 105 74 99 109 93 98 85 86 86 86 113 105 74 99 109 94 98 85 86 86 86 113 105 74 99 109 94 98 85 86 86 86 113 105 74 99 109 94 98 85 86 86 86 112 104 74 99 109 17:00 93 98 84 85 86 86 111 102 72 97 107 96 100 86 87 88 112 104 73 98 109 96 100 86 87 88 112 104 73 98 109 ower at 19:00 95 99 84 86 87	97 101 86 87 88 99 100 115 107 78 101 109 107 94 98 85 86 86 96 111 103 74 98 106 104 94 98 85 86 86 96 112 105 74 99 109 105 94 98 85 86 86 96 112 105 74 99 109 105 94 98 85 86 86 96 112 105 74 99 109 105 94 99 84 86 86 97 113 105 74 99 109 105 93 98 85 86 86 97 113 105 74 99 109 105 94 98 85 86 86 97 113 105 74 99 109 105 94 98 85 86 86 97 112 104 74 99 109 105 17:00 93 98 84 85 86 96 111 102 72 97 107 103 96 100 86 87 88 98 112 104 73 98 109 104 96 100 86 87 88 98 112 104 73 98 109 104 96 100 86 87 88 98 109 104 96 99 84 86 87 98	97 101 86 87 88 99 83 115 107 78 101 110 108 96 97 101 87 88 89 100 83 115 107 77 101 109 107 95 94 98 85 86 86 96 80 111 103 74 98 106 104 92 94 99 84 86 86 96 80 112 105 74 99 109 105 92 94 98 85 86 86 96 80 112 105 74 99 109 105 92 93 98 85 86 86 97 80 113 105 74 99 109 105 92 94 98 85 86 86 97 80 113 105 74 99 109 105 92 17:00 93 98 84 85 86 86 97 80 112 104 74 99 109 105 92 17:00 93 98 84 85 86 86 96 80 111 102 72 97 107 103 90 96 100 86 87 88 98 82 112 104 73 98 109 104 92 ower at 19:00 95 99 84 86 87 98 81	97 101 86 87 88 99 83 80 115 107 78 101 110 108 96 93 93 94 98 85 86 86 96 80 78 111 103 74 98 106 104 92 89 90 94 98 85 86 86 96 80 78 112 105 74 99 109 105 92 90 94 98 85 86 86 96 80 78 112 105 74 99 109 105 92 90 93 98 85 86 86 97 80 78 113 105 74 99 109 105 92 90 94 98 85 86 86 97 80 78 113 105 74 99 109 105 92 90 94 98 85 86 86 97 80 78 113 105 74 99 109 105 92 90 90 94 98 85 86 86 97 80 78 113 105 74 99 109 105 92 90 90 94 98 85 86 86 97 80 78 112 104 74 99 109 105 92 80 17:00 93 98 84 85 86 96 80 77 111 102 72 97 107 103 90 88 96 100 86 87 88 98 82 80 112 104 73 98 109 104 92 90 96 100 86 87 88 98 82 80 112 104 73 98 109 104 92 91 over at 19:00 95 99 84 86 87 98 81 79	97 101 86 87 88 99 83 80 86 115 107 78 101 110 108 96 93 92 92 97 101 87 88 89 100 83 81 87 115 107 77 101 109 107 95 92 92 92 94 98 85 86 86 96 80 78 85 111 103 74 98 106 104 92 89 89 89 94 98 85 86 86 96 80 78 85 112 105 74 99 109 105 92 90 90 90 94 98 85 86 86 96 80 78 85 112 105 74 99 109 105 92 90 90 90 93 98 85 86 86 96 80 78 85 112 105 74 99 109 105 92 90 90 90 91 105 92 90 90 90 91 105 92 90 90 90 91 105 92 90 90 90 91 105 92 90 90 90 90 90 90 90 90 90 90 90 90 90	97 101 86 87 88 99 83 80 86 80 115 107 78 101 110 108 96 93 92 86 97 101 87 88 89 100 83 81 87 81 115 107 77 101 109 107 95 92 92 86 94 98 85 86 86 96 80 78 85 81 111 103 74 98 106 104 92 89 89 89 82 94 98 85 86 86 96 80 78 85 81 112 105 74 99 109 105 92 90 90 85 94 99 84 86 86 96 80 78 85 81 112 105 74 99 109 105 92 90 90 85 93 98 85 86 86 96 80 78 85 81 113 105 74 99 109 105 92 90 90 85 93 98 85 86 86 97 80 78 85 81 113 105 74 99 109 105 92 90 90 85 94 98 85 86 86 97 80 78 85 81 113 105 74 99 109 105 92 90 90 85 94 98 85 86 86 97 80 78 85 81 113 105 74 99 109 105 92 90 90 85 94 98 85 86 86 97 80 78 85 81 112 104 74 99 109 105 92 80 90 85 95 96 100 86 87 88 98 82 80 87 83 112 104 73 98 109 104 92 90 90 86 96 100 86 87 88 98 82 80 87 83 112 104 73 98 109 104 92 91 90 86 00er at 19:00 95 99 84 86 87 98 81 79 86 81	97 101 86 87 88 99 83 80 86 80 82 115 107 78 101 110 108 96 93 92 86 90 97 101 87 88 89 100 83 81 87 81 83 115 107 77 101 109 107 95 92 92 86 89 89 89 82 86 89 81 111 103 74 98 106 104 92 89 89 89 82 86 81 112 105 74 99 109 105 92 90 90 85 88 81 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 113 105 74 99 109 105 92 90 90 85 88 112 104 74 99 109 105 92 80 90 85 88 17:00 93 98 84 85 86 96 80 77 84 79 81 111 102 72 97 107 103 90 88 87 82 84 96 100 86 87 88 98 82 80 87 83 84 112 104 73 98 109 104 92 90 90 86 88 000er at 19:00 95 99 84 86 87 98 81 79 86 81 83 00eer at 19:00	97 101 86 87 88 99 83 80 86 80 82 77 115 107 78 101 110 108 96 93 92 86 90 86 97 101 87 88 89 100 83 81 87 81 83 78 115 107 77 101 109 107 95 92 92 86 89 85 86 86 86 96 80 78 85 79 81 75 111 103 74 98 106 104 92 89 89 82 86 82 94 98 85 86 86 96 80 78 85 81 81 78 112 105; 74 99 109 105 92 90 90 85 88 84 91 12 105 74 99 109 105 92 90 90 85 88 84 112 105 74 99 109 105 92 90 90 85 88 84 112 105 74 99 109 105 92 90 90 85 88 84 112 105 74 99 109 105 92 90 90 85 88 84 112 105 74 99 109 105 92 90 90 85 88 84 112 104 74 99 109 105 92 90 90 85 88 84 112 104 74 99 109 105 92 80 90 85 88 84 112 104 74 99 109 105 92 80 90 85 88 84 112 104 74 99 109 105 92 80 90 85 88 83 17:00	97 101 86 87 88 99 83 80 86 80 82 77 81 115 107 78 101 110 108 96 93 92 86 90 86 98 98 97 101 87 88 89 100 83 81 87 81 83 78 82 115 107 77 101 109 107 95 92 92 86 89 85 98 94 98 85 86 86 86 96 80 78 85 79 81 75 78 111 103 74 98 106 104 92 89 89 82 86 82 93 94 98 85 86 86 86 96 80 78 85 81 81 78 80 112 105 74 99 109 105 92 90 90 85 88 84 95 96 112 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 113 105 74 99 109 105 92 90 90 85 88 84 96 115 104 74 99 109 105 92 80 90 85 88 84 96 115 104 74 99 109 105 92 80 90 85 88 84 96 115 104 74 99 109 105 92 80 90 85 88 83 96 17:00 93 98 84 85 86 96 80 77 84 79 81 76 80 113 102 72 97 107 103 90 88 87 82 84 81 93 96 100 86 87 88 98 82 80 87 83 84 81 93 96 100 86 87 88 98 82 80 87 83 84 81 84 96 115 104 73 98 109 104 92 90 90 86 88 84 96 115 104 73 98 109 104 92 91 90 86 88 84 96 115 104 73 98 109 104 92	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 15 107 78 101 100 108 96 93 92 86 90 86 98 95 97 101 87 88 89 100 83 81 87 81 83 78 82 88 115 107 77 101 109 107 95 92 92 86 89 85 98 95 94 98 85 86 86 96 80 78 85 79 81 75 78 86 111 103 74 98 106 104 92 89 89 82 86 82 93 90 94 98 85 86 86 96 80 78 85 81 81 78 80 88 112 105 74 99 109 105 92 90 90 85 88 84 96 91 93 98 85 86 86 96 80 78 85 81 81 77 80 87 113 105 74 99 109 105 92 90 90 85 88 84 96 91 94 98 85 86 86 96 80 78 85 81 81 77 80 87 113 105 74 99 109 105 92 90 90 85 88 84 96 91 94 98 85 86 86 97 80 78 85 81 81 77 80 87 113 105 74 99 109 105 92 90 90 85 88 84 96 91 94 98 85 86 86 97 80 78 85 81 81 77 80 87 113 105 74 99 109 105 92 90 90 85 88 84 96 91 95 98 84 85 86 86 96 80 77 84 85 81 81 77 80 87 112 104 74 99 109 105 92 80 90 85 88 84 96 93 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 90 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92	97 101 86 87 88 99 83 80 86 80 82 77 81 88 88 81 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 97 101 87 88 89 100 83 81 87 81 83 78 82 88 82 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 94 98 85 86 86 96 80 78 85 79 81 75 78 86 79 111 103 74 98 106 104 92 89 89 82 86 82 93 90 89 81 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 91 91 91 91 91 91 91 91 91 91 91	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 91 97 101 87 88 89 100 83 81 87 81 82 88 82 74 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 94 98 85 86 86 96 80 78 85 79 81 75 78 86 79 70 111 103 74 98 106 104 92 89 89 82 86 82 93 90 89 88 81 12 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 90 85 88 84 96 91 91 90 90 85 88 84 96 91 90 90 85 88 84 96 91 90 89 89 17:00 93 98 85 86 86 97 80 78 85 81 81 77 80 87 79 73 113 105 74 99 109 105 92 90 90 85 88 84 96 91 90 89 89 17:00 93 98 85 86 86 87 89 89 89 82 86 82 93 90 89 89 89 80 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 70 80 80 80 80 80 80 80 70 80 80 80 80 80 80 80 80 70 80 80 80 80 80 80 80 80 70 80 80 80 80 80 80 80 80 80 80 80 80 80	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 70 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 87 97 101 87 88 89 100 83 81 87 81 83 78 82 88 82 74 71 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 94 98 85 86 86 96 80 78 85 79 81 75 78 86 79 70 68 111 103 74 98 106 104 92 89 89 89 82 86 82 93 90 89 88 84 94 98 85 86 86 96 80 78 85 81 81 78 80 88 80 73 68 112 105 74 99 109 105 92 90 90 85 88 84 95 91 91 90 86 94 98 85 86 86 96 80 78 85 81 81 78 80 88 80 73 68 112 105 74 99 109 105 92 90 90 85 88 84 95 92 90 89 83 94 99 84 86 86 96 80 78 85 81 82 78 81 88 80 73 68 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 89 83 94 99 84 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 113 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 89 83 94 98 85 86 86 97 80 78 85 81 81 77 80 87 79 73 67 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 89 83 94 98 85 86 86 97 80 78 85 81 81 77 80 87 79 73 67 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 89 83 17:00 93 98 84 85 86 86 97 80 78 85 81 81 77 80 87 79 73 67 112 104 74 99 109 105 92 80 90 85 88 83 96 93 90 89 88 17:00 93 98 84 85 86 86 97 80 78 85 81 81 77 80 87 79 73 67 112 104 74 99 109 105 92 80 90 85 88 83 96 93 90 89 88 17:00 93 98 84 85 86 86 96 80 77 84 79 81 76 80 86 79 73 68 111 102 72 97 107 103 90 88 87 82 84 81 93 89 87 85 80 96 100 86 87 88 98 82 80 87 83 84 81 84 90 82 77 69 81 12 104 73 98 109 104 92 90 90 86 88 84 96 92 90 89 82 000 85 88 84 96 92 90 89 82 000000000000000000000000000	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 70 60 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 87 76 97 101 87 88 89 100 83 81 87 81 83 78 82 88 82 74 71 61 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 76 94 98 85 86 86 96 80 78 85 79 81 75 78 86 79 70 68 58 111 103 74 98 106 104 92 89 89 82 86 82 93 90 89 88 84 73 94 98 85 86 86 96 80 78 85 81 81 75 78 80 87 79 70 68 58 112 105 74 99 109 105 92 90 90 85 88 84 95 92 90 89 83 72 94 99 84 86 86 86 96 80 78 85 81 81 78 80 88 80 73 68 58 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 84 73 93 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 113 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 89 89 81 72 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 113 105 74 99 109 105 92 90 90 85 88 84 96 91 90 89 89 83 72 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 113 105 74 99 109 105 92 90 90 85 88 84 96 91 90 89 89 83 72 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 113 105 74 99 109 105 92 80 90 85 88 84 96 91 90 89 89 83 72 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 113 105 74 99 109 105 92 80 90 85 88 84 96 91 90 89 89 81 72 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 58 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 89 89 84 72 17:00 93 98 84 85 86 86 86 97 80 78 85 81 81 81 77 80 86 79 73 67 58 81 12 104 74 99 109 105 92 80 90 85 88 84 96 93 90 89 84 72 17:00 93 98 84 85 86 86 86 87 88 98 82 80 87 83 84 81 93 89 87 85 80 75 96 100 86 87 88 98 82 80 87 83 84 81 84 96 92 90 89 82 71 00000000000000000000000000000000000	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 70 60 60 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 87 76 80 97 101 87 88 89 100 83 81 87 81 83 78 82 88 82 74 71 61 61 61 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 76 80 94 98 85 86 86 96 80 78 85 79 81 75 78 86 79 70 68 58 58 111 103 74 98 106 104 92 89 89 89 82 86 82 93 90 89 88 84 73 76 94 98 85 86 86 96 80 78 85 81 81 75 78 86 79 70 68 58 58 112 105 74 99 109 105 92 90 90 85 88 84 95 92 90 89 83 72 76 94 99 84 86 86 86 96 80 78 85 81 82 78 81 88 80 73 68 58 58 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 80 84 73 77 93 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 80 84 73 77 93 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 90 89 83 72 76 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 90 89 83 72 76 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 112 104 74 99 109 105 92 80 90 85 88 84 96 91 90 90 89 83 72 76 95 98 84 85 86 87 88 98 82 80 87 83 84 81 84 90 82 77 73 68 57 72 96 100 86 87 88 98 82 80 87 83 84 81 84 90 82 77 69 59 58 112 104 73 98 109 104 92 90 90 86 88 84 96 92 90 89 82 71 74 90 90 105 104 92 90 90 86 88 84 96 92 90 89 82 71 74 90 90 105 104 92 91 90 86 88 84 96 92 90 89 82 71 74 90 90 90 85 88 84 96 92 90 89 82 71 74 90 90 90 85 88 84 96 92 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 86 88 84 96 92 90 89 82 71 74 90 90 90 80 80 80 80 80 80 76 69 60 60 60 60 60 80 80 80 80 80 80 76 69 60 60 60 60 60 60 80 80 80 80 80 80 76 69 60 60 60 60 60 80 80 80 80 80 80 80 80 76 69 60 60 60 60 60 80 80 80 80 80 80 80 76 69 60 60 60 60 60 60 80 80 80 80 80 80 76 69 60 60 60 60 80 80 80 80 80 80 76 69 60 60 60 60 60 80 80 80 80 80	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 70 60 60 48 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 87 76 80 79 97 101 87 80 110 100 96 93 92 86 90 86 98 95 92 91 87 76 80 79 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 76 80 78 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 76 80 78 111 103 74 98 106 104 92 89 89 82 86 82 93 90 89 88 84 73 76 74 111 103 74 99 109 105 92 90 90 85 88 84 95 92 90 89 83 72 76 74 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 84 73 77 77 77 77 77 77 77 77 77 77 77 77	97 101 86 87 88 99 83 80 86 80 82 77 81 88 81 72 70 60 60 60 48 37 115 107 78 101 110 108 96 93 92 86 90 86 98 95 92 91 87 76 80 79 73 97 101 87 88 89 100 107 95 92 92 86 89 85 98 95 91 90 86 76 80 78 78 72 94 98 85 86 86 96 80 78 85 88 84 95 91 90 105 92 90 90 85 88 84 95 92 90 89 88 84 73 77 75 69 91 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 84 73 77 75 69 112 104 73 98 109 104 92 90 86 85 88 84 96 92 90 89 87 85 86 86 97 80 17 07 105 109 105 92 90 90 86 88 84 96 91 90 89 88 84 72 76 74 69 17:00	97 101 86 87 88 99 83 80 86 80 98 98 77 81 88 81 72 76 80 79 73 75 97 101 87 88 89 100 83 81 87 81 83 78 82 88 82 74 71 61 61 61 48 38 50 115 107 77 101 109 107 95 92 92 86 89 85 98 95 91 90 86 76 80 78 72 74 94 98 85 86 86 96 80 78 85 89 89 82 86 82 93 90 89 88 84 73 76 74 69 70 94 98 85 86 86 96 80 78 85 81 81 78 88 84 95 92 90 89 88 84 73 76 74 69 70 94 98 85 86 86 86 96 80 78 85 81 81 78 88 84 95 92 90 89 88 84 73 76 74 69 70 94 98 85 86 86 86 96 80 78 85 81 81 78 88 80 88 80 73 68 58 58 47 36 48 112 105 74 99 109 105 92 90 90 85 88 84 95 91 91 90 86 85 85 85 84 73 76 74 69 70 94 98 85 86 86 86 96 80 78 85 81 82 78 81 83 78 82 88 80 73 68 58 58 47 36 48 112 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 84 73 77 75 69 71 93 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 47 35 48 113 105 74 99 109 105 92 90 90 85 88 84 96 91 91 90 89 83 72 76 74 69 70 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 47 35 48 113 105 74 99 109 105 92 90 90 85 88 84 96 91 90 90 89 83 72 76 74 69 70 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 48 13 13 105 74 99 109 105 92 90 90 85 88 84 96 91 90 89 83 72 76 74 69 70 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 57 58 48 13 12 104 74 99 109 105 92 90 90 85 88 84 96 91 90 89 83 72 76 74 69 70 94 98 85 86 86 86 97 80 78 85 81 81 77 80 87 79 73 67 58 58 48 35 47 17:00 93 98 84 85 86 86 97 80 78 85 88 84 96 91 90 89 83 72 76 74 69 70 17:00 93 98 84 85 86 86 97 80 78 85 81 81 77 80 87 79 73 67 58 58 48 35 47 17:00 93 98 84 85 86 86 97 80 78 85 86 86 84 96 91 90 89 82 77 69 59 58 47 66 86 97 80 86 86 84 81 83 96 92 90 89 82 71 74 74 72 68 69 70 17:00 93 98 84 85 86 86 97 80 88 82 80 87 83 84 81 84 84 90 82 77 69 59 58 47 36 86 90 80 80 80 70 89 82 71 74 74 72 68 69 80 80 80 80 80 76 69 80 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 89 80 80 70 80 80 80 70 80 80 80 70 80 80 80 70 8

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-	15) <u>(</u>	SHE	<u> </u>	101								T -	01111			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		011	V
													E 1	PUMP			NIFC RES	- 111	IN	MMY PUT
	37	38	39	40	41	42	43	44	45	46	47	48		ROLLER	PRESS					ESS R/H
	70 95	86 94	75 103	69 89	55 76	69 76	67 84	59 55	76 92	68 80	66 72	24	20.1 22.5	5.5	70 64	42 42	40 37	36 35	21	18
,	70 95		76 102	70 89	56 75	70 75	68 84	60 55	76 91	68 86	67 71	23	19.8 22.5	5.5	70 64	42 42	40 37	36 35	21	18
1	69 94	84 90	72 99	69 89	50 70	68 73	66 84	57 56	72 89	66 79	65 70	23	19.8 22.5	5.5	70 64	42 42	40 37	36 35	21	18
-	69 93	85 90	72 100	68 86	50 71	67 70	65 81	57 58	72 88	65 78	64 69	23	19.8	5.5	70 64	42 42	40 37	36 35	21	18
1	69 93		72 101	68 88	51 71	68 70	66 83	57 55	72 88	65 79	64 69	23	19.8 22.5	5.5	70 64	42 42	40 37	36 35	21	18
ŀ	68 93		72 100	68 85	50 71	67 70	65 81	57 55	72 88	66 78	64 69	23	19.8 22.5	5.5	70 64	41 42	40 37	36 35	21	18
200	68 93	85 90	7 2 100	68 87	50 71	67 70	65 81	57 55	7 2 88	65 78	64 69	23	19.8 22.5	5.5	70 64	41 42	40 37	36 35	21	18
		85 87		67 84	51 69	67 70	65 81	56 57	73 85	64 76	64 67	23	19.8 22.5	5.4	70 65	42 43	40 38	36 35	21	18
		87 90	74 99	68 85	53 71	69 72	66 81	58 57	74 88	65 78	66 69	22	20.1 22.5	5.4	70 65	42 42	40 38	36 35	21	18
		87 90	74 99	68 85	53 71	69 72	66 81	58 57	74 88	65 78	66 69	22	20.1 22.5	5.4	70 65	42 42	40 38	36 35	21	18
	70 93	86 90	76 99	69 84	50 68	68 71	66 80	57 56	75 87	66 77	66 69	22	19.8 22.5	5.4	70 65	42 42	40 37	36 35	21	18

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																1
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		,	2	3	4	5	6	7	8	9	10	
1/16	20:00	217:56	3000	425	DUMMY TEST	80 100	111 73	98 115	115 120		111 112				12 9 111	
1/16	20:30	218:26	3000	425	DUMMY	80 100		98 115		112 90	111 112	96 110	103 106	107 104	130 111	n :
1/16	21:00	218:56	3000	425	DUMMY TEST	81 100	111 73	97 115		90 112	111 112				129 112	
1/16	21:30	219 :26	3000	425	DUMMY TEST	81 100		97 115		90 112	111 112	95 110	103 106	107 104	12 9 112	Ľ.,
1/16	22:00	219:56	3000	425	DUMMY TEST	81 99		-	115 120	90 112		95 110				
1/16	22:15	220:11	1950	425	DUMMY TEST	81 100		98 114	114 12 0	89 110		9 4 108				
1/16	22:45	220:41	3000	425	DUMMY TEST	81 99	111 73	97 115	115 120	90 112	111 112	95 110	103 106	107 104	129 111	ij
1/16	23:15	221:11	3000	425	DUMMY TEST	81 99	111 73	97 115	115 120	90 112	1112	95 110	103 106	107 104	129 111	1
1/16	23:45	221:41	3000	425	DUMMY TEST	81 99	112 73	97 115	116 120	9 0 112	111 112	96 110	103 106	107 104	129 111	1
1/17	00:15	222:11	3000	425	DUMMY TEST	82 99		98 115	116 120	90 112	111 112	96 110	103 106	107 104	129	ı
1/17	00:45	222:41	3000	425	DUMMY TEST	81 99	111 73	97 115	116 120	90 112	111 112	95 110	103 106	107	129	1

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATORY

8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
				99 103			87 1 0 8	98 103	80 90	79 88	86 87	82 84		80 82	82 9 5	88 93	80 89	7 6 88	69 82	61 72	61 77	48 74	37 71
							87 108		81 90	79 88		82 85			83 95	89 93	81 89	76 87		61 71	61 77	48 74	
							87 108	98 103			86 88	82 84	83 86		83 95	89 93	81 89	76 88		61 72	61 77	48 74	37 71
							87 108	98 103		79 87	86 88	82 84	83 86	80 82	83 95		81 89	76 88	69 82	61 72	61 77	48 74	37 71
								98 103						80 82	83 95	89 93	80 89	76 88	-	61 72	61 77	48 74	
								96 103				78 81	80 85	74 80	79 91	85 90							
							97 108	98 103				83 84		80 82	82 9 4	88 9 2	28 38	76 87	69 71	60 71	61 77	48 74	37 69
								98 103			86 87	83 84	83 86	80 82	82 94	88 9 2	80 88	76 87	69 81	60 71	61 77	48 74	37 66
103 106	107 104	12 9 111	95 110	99 103	84 71	86 9 7	87 108	98 103	81 90	79 87	86 87	83 84	83 86	80 82	83 95	89 84	80 88	76 87	69 81	60 71	61 77	48 74	37 70
103 106	107 104	129 112	94 110	99 103	85 71	86 97	87 1 0 8	98 103	81 90	79 87	86 87	83 83	83 86	80 82	83 9 5	89 81				63 71	(1 77	48 74	37 70
103 106	107 104	12 9 111	95 110	99 103	84 71	85 97	87 108	98 104	81 90	79 87	86 87	83 84	83 87	80 82	83 95	88 8;5	80 89		69 81	62 71	60 77	48 74	

K TEST (SHEET 47)

	PUMP MANIFOLD DUMA														A A A & A					
													DUMMY							
0.4			00	40		, 1			4 =		. –	4.5		FLOW TOTAL ROLLER		PRESS MAIN L/H R/H		PRESS		
36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
77 91	69 94	86 90	76 99	6 9 85	50 68	68 72	66 81	57 60	75 87	66 77	66 69	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
77 90	70 93	86 90	76 99	6 9 84	50 68	69 70	66 79	57 60	75 87	66 77	66 68	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
77 91	69 94	86 90	76 99	69 84	50 68	68 72	66 80	57 59	75 87	66 77	67 68	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
77 91	69 94	86 90	76 99	6 9 84	50 68	68 72	66 80	57 59	75 87	66 77	67 68	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
76 90	69 93	86 90	76 99	69 84	50 68	68 71	66 79	57 59	75 87	66 77	66 68	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
													19.8	5•3	70 65	42 43	40 37	36 35	21	18
76 20	69 93	86 90	76 98	6 9 82	50 68	68 70	6\ 79	57 59	75 86	66 77	66 68	22	19.8 22.2	5.3	70 65	42 43	40 37	36 35	21	18
)6)0	69 93	86 90	76 98	69 82	50 68	68 70	66 79	57 59	75 87	66 77	66 68	22	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
'6 10	_	86 90	76 9 9	70 84	50 68	68 71	66 81	57 62	75 87	66 77	66 68	21	19.8 22.5	5.4	70 65	42 43	40 37	36 35	21	18
'6 10	69 93	86 90	76 99	69 82	50 68	68 71	65 80	57 61	75 87	66 77	66 68	21	19.8 22.5	5.3	70 64	42 42	39 37	36 35	21	18
'6 10	69 93	86 90	76 99	70 82	50 68	67 71	65 80	57 59	75 86	65 77	66 68	21	19.8 22.5	5.3	70 64	42 42	39 37	36 35	21	18

	TIME	TOTAL	TOTAL	TAIL				<u>.</u>							_
DATE	OF DAY	TEST TIME	INPUT H.P.	H.P.		,	2	3	4	5	6_	7	8	9	
1/17/73	01:15	223:11	3000	425	DUMMY TEST	81 99	111 72	98 115		-	111	95 110		107 104	
1/17	01:45	223:41	3000	425	DUMMY TEST	82 99		98 115			111 112	96 110		107 104	:
1/17	06:00	223:56	1950	425	DUMMY TEST	-		100 113	-		110 108	94 107		106 100	:
1/17	06:30	224:26	3560	425	DUMMY TEST	83 99		96 118	115 121		113 115	96 114		108 108]
1/17	06:45	224:41	1950	425	DUMMY TEST		111 75	97 115			109 112	93 111		105 105	
1/17	07:15	225:11	3560	425	DUMMY TEST	82 100		95 120			114 117	97 117		109 110	
1/17	07:30	225:26	1950	425	DUMMY TEST	•	111 77				111 116	95 114		107 109	1
1/17	00:8c	225:56	3560	425	DUMMY TEST	84 102	_	97 121				99 119	107 114	110 112	1
1/17	08:15	226:11	1950	425	DUMMY TEST			99 116	116 121		111 114	96 111		107 105	1
1/17	08:30	226:26	3700	425	DUMMY TEST			97 117			115 116	99 114		110 108	1
1/17	08:45	226: 41	1950	425	DUMMY Test	85 99		99 115			112 112	97 110		108 104	1:

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LABORATO

7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
95 .10		107 104							99 103		79 87	86 87		85 86		82 95	88 85	80 89	•	_	62 71	61 77	48 74
96 10		1.07							99 103		79 87			85 86		83 95	89 85	80 89		69 82	62 71	61 77	48 74
94 .07		106 100									81 84			80 77		78 86			7 1 77		73 60		59 62
		108 108								82 93	80 90					.88 202				•	63 77		49 79
93 11		105 105									79 89		77 83	81 87		80 92	86 89						
97 17	106 112	109 110									81 93	90 95	91 94	91 97		90 103		86 95	_		63 78	61 83	48 81
95 14		107 109									80 92		81 87	83 91	78 87	82 97	88 95						
99 19		110								84 97	82 95					92 105					64 81		49 84
96 11	103 107	107 105	128 113	95 112	99 104	86 73	86 98	87 108	101 105	82 92	81 90					82 95							
99 14		110 108									82 90					92 101							
		108 104								_	82 89	88 90				84 92	_						

CK	TE	ST (SHE	ET «	48)															
					· ·									PUMP			NIFC			YMA
													ľ	OW			RES		PRI	ESS
36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
76 90	69 93	86 90	76 99	69 84	49 68	68 71	65 80	57 60	75 87	65 77	66 68	21	19.8 22.2	5.3	70 64	42 42	39 37	36 35	21	18
76 90	69 93	86 90	76 99	69 84	49 68	68 71	65 80	57 60	75 87	65 77	66 68	21	19.8 22.2	5.3	70 64	42 42	39 37	36 35	21	18
8 2 78	78 77	86 78	ხი 85	78 76	5 3. 5 9	77 60	73 71	65 60	80 77	73 67	73 58	23	19.8 22.5	5.4	70 66	42 44	40 38	36 35	21	18
78 90	70 92	89 90 :	77 103	69 82	52 72	69 74	66 80	58 58	77 89	67 78	67 68	20	20.4 22.8	5.5	71 66	42 43	40 38	36 35	21	18
													19.6 20.8	5.5	70 64	42 43	40 38	36 35	21	18
78 91	68 92	90 92	77 105	68 83	54 72	68 71	66 80	58 62	77 90	66 78	68 68	17	20.4 22.8	5.5	70 65	42 42	40 37	36 35	21	18
													19.8 22.8	5.5	70 65	42 43	40 37	36 35	21	18
79 94	70 94	91 94]	79 107	71 85	55 77	69 76	68 82	60 62	78 93	68 81	68 71	20	20.4 22.8	5.6	70 64	42 42	40 37	37 35	21	18
													20.1	5.5	70 66	42 43	40 37	36 35	21	18
													20.4 22.8	5.5	70 65	42 42	40 37	36 35	21	18
													20.1 22.8	5.4	70 6 6	42 43	40 37	36 35	21	18

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			_		. :-										
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
1/17/73	09:00	226:56	3700	425	DUMMY TEST	99	78	117	117 121	115	114	98 114	109	110 107	133 114
1/17	10:05	226:56	1100	250	DUMMY TEST	86	111	102	113 117	88	108	92 95	100	ector 103 97	122 107
1/17	10:35	227:26	1100	250	DUMMY TEST	_		-	112 117		107 106	91 94	99 101	102 99	123 107
1/17	11:05	227:56	1100	250	DUMMY TEST				112 122			91 100		102 105	122 113
1/17	11:35	228:26	1100	250	DUMMY TEST			-	112 124	•		90 114	-	102 107	122 116
1/17	12:05	228:56	1950	250	DUMMY TEST				114 122			94 112		105 106	127 115
1/17	12:35	229:26	1950	250	DUMMY TEST				115 122	-		95 113		105 107	127 114
1/17	13:05	229:56	1950	250	DUMMY TEST				118 123	_		_	106 109	110 107	131 115
1/17	13:35	230:26	1950	250	DUMMY				118 123			99 114		110 108	131 115
1/17	14:05	230:56	1950	250	DUMMY TEST			-		91 114				106 107	128 115
1/17	14:35	231:26	1950	250	DUMMY TEST				115 122			95 113		106 107	128 115

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA:LA

5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	1
	-	98 114		110 107	133 114		102 105		99	112		83 92	82 90	90 92	92 91	91 94	87 88	91 100	93 89				
ction	of	chir	det	ectors	s and	stre	iner	s	Che.n.	ge ta	il lo	ad											
		92 95		103 97	122 107		96 98				95 99	81 85	81 83		76 74	79 77	75 74	79 85	81 76	78 79	72 79	73 77	7 7
		91 94		102 99	123 107		96 98			82 100		77 86	76 83		71 74	73 77	69 75	73 86	79 79	75 80	64 79	67 78	5
		91 100	-	102 105	122 113		95 105			82 107		76 93	75 90		69 82		66 83	73 92	77 85	73 85	63 85	66 84	5! 7:
	- 111	90 114	•	102 107	122 116		95 107		82 101	82 109	_	76 95	75 93	79 92	70 85	71 89	67 85	73 96	87 90	73 90	63 90	66 87	5! 7 ¹
-	-	94 112		105 106			97 105	83 75		85 109		78 93	77 90		76 85	78 87	73 84	77 95	84 86	78 90	69 90	67 89	60 81
-		95 113		105 107			98 105			86 110		79 93	78 90		77 85	79 88		78 95	85 87	78 90	70 90	68 84	61 75
-		98 114	106 109	110 107			102 106			89 110	101 106		82 91			83 89			90 87	83 91	76 90	72 85	64 76
94 115	114 116	99 114	106 110	110 108	131 115	99 114	103 106	89 76	88 101	90 110	101 107	84 94	83 92	88 92				:33 :36	91 89	83 91	77 91	73 85	65 76
			103 109	106 107			99 106			86 110			78 91		78 85		75 85			79 91	71 89	68 79	61 76
		95 113		106 107						86 110			78 90		78 85	79 88	75 84	79 35	86 87	79 90		68 84	

LABO	ORA	\TO	RY	BA	CK.	.TO	-BA	CK	TE	ST (SHE	ET 4	49)									
																					FL	PU W
28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROL
																					20.1 22.8	5.:
71 72	70 79	57 74	44 69	59 69	48 70	79 81	68 68	80 82	75 84	83 82	78 90	76 78	51 64	75 72	72 74	63 47	78 81	73 72	72 66	25	19.8 22.2	5.2
59 69	58 73	48 71	36 68	47 69	43 69	73 82	61 68	73 84	69 89	80 84	72 92	68 79	48 65	65 68	64 77	55 49	72 82	64 72	64 65	23	19.2 22.5	5.3
59 75	57 79	47 90	35 73	46 74	41 76	72 89	60 74	72 90	68 93	79 90	71 98	67 84	47 73	64 74	62 81	54 50	71 89	63 77	63 69	23	19.2 22.8	5.5
59 78	58 82	48 81	36 76	47 77	43 79	72 92	60 77	72 93	68 95	79 93	71 101	67 87	47 76	63 78	62 84	54 51	71 92	63 79	63 71	23	19.2 23.1	5.5
60 84	58 7 5	48 78	36 73	47 74	43 76	73 83	61 74	73 91	69 94	83 90	72 100	68 85	49 71	65 76	63 82	55 45	72 89	65 77	65 70	24	19.5 22.8	5.4
61 75	59 79	50 77	38 73	49 74	45 76	73 89	62 74	73 90	69 93	83 90	73 101	68 84	49 72	66 73	64 82	56 46	72 89	65 78	65 69	25	20.1 22.8	5.5
64 76	63 80	53 79	41 74	52 76	48 77	78 89	66 74	78 91	72 94	88 90	78 102	72 85	56 73	70 72	68 82	60 41	77 89	68 79	69 70	25	20.4 22.8	5.5

78 72 89 78 91 94 91 102

84 73

90 101

63 74 70 84 73 74 90 94 90 102 72 70 76 82

73 82

67 65

73 82

61 78

41 90

57 73 43 89

43 89

20.1

22.8

19.5

23.1

19.5

22.8

5.5

5.5

5.5

63 53 41

79 78

60 50

79 78

60 50 34

79 78 73 74

63 74

74 91

SHE	ET 4	49)															
											PUMP		MA	NIF	OLD		MMY
											ow		1	PRES	S		PUT
39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/F	R/H	L/H	R/H
										20.1 22.8	5.5	70 65	42 43	40 37	37 35	21	18
78 90	76 78	51 64	75 72	72 74	63 47	78 81	73 72	72 66	25	19.8 22.2	5.2	70 65	42 44	39 37	36 35	21	18
72 92	68 79	48 65	65 68	64 77	55 49	72 82	64 72	64 65	23	19.2 22.5	5.3	70 66	42 44	39 37	35 35	21	17
71 98	67 84	47 73	64 74	62 81	54 50	71 89	63 77	63 69	23	19.2 22.8	5.5	70 65	42 43	39 37	35 35	21	17
71 101	67 87	47 76	63 78	62 84	54 51	71 92	63 79	63 71	23	19.2 23.1	5.5	69	41 42	39 37	35 35	21	17
72 100	68 85	49 71	65 76	63 82	55 45	72 89	65 77	65 70	24	19.5 22.8	5.4	70 65	41 42	39 38	35 34	20	18
73 101	68 84	49 72	66 73	64 82	56 46	72 89	65 78	65 69	25	20.1	5.5	70 65	41 42	39 37	36 35	21	18
78 102	72 85	56 73	70 72	68 82	60 41	77 89	68 79	69 70	25	20.4 22.8	5.5	70 65	41 42	40 37	36 35	21	18
78 102	72 85	57 74	72 76	70 82	61 41	78 90	69 79	69 70	25	20.1 22.8	5.5	70 65	41 42	40 37	36 35	21	18
73 101	69 85	50 72	68 73	65 82	57 43	73 89	66 79	65 70	26	19.5 23.1	5.5	70 65	41 42	39 37	36 35	21	18
73 102	70 86	50 72	67 73	65 82	57 43	73 89	66 79	65 70	26	19.5 22.8	5.5	69 65	41 42	39 37	36 35	21	18

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1(
1/17/73	15:05	231:56	2400	250	DUMMY TEST		113 82			93 118	113 118			108 110	
1/17	15:35	232:26	2400	250	DUMMY TEST		113 82			93 117	113 118		-	108 110	_
1/17	16:05	232:56	2400	250	DUMMY TEST	87 104	113 82			93 117	113 118	- •	_	109 110	_
1/17	16:35	2 33:26	2400	250	DUMMY TEST	87 103	113 82			93 117	113 118	116	111	108 110	
1/17	20:00	233:56	2400	250	DUMMY TEST		top 111 74			91 109	111 109	95	103	30 107 101	
1/17	20:30	234:26	2700	250	DUMMY TEST		112 73			92 109	112 109			108 102	_
1/17	21:00	234:56	2700	250	D'JMMY TEST	85 98	113 74			93 110	113 110			109 103	
1/17	21:30	235:26	1950	250	DUMMY TEST	85 98				_	111 111	_	_	107 103	-
1/17	22:00	235:56	1950	250	DUMMY TEST		113 74				111 111				
1/18	01:35	236 :26	1950	250	DUMMY TEST	83	top 110 70		113	87	ower a 108 110	93	100		
1/18	02:05	236:56	1950	250	DUMMY TEST	97		95 115 lown	120	112		111	107		114

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA; LAS

																						, -,	
_5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
93 .18	113 118				131	97 116	101 109		88 102		99 108	82 95	80 93	87 95	85 90	85 92	82 89	86 100	90 91	83 93		69 85	62 77
93 .17	113 118				131	96 116					99 109			88 95		85 93	82 89	86 101	90 91	83 94		69 86	
93 17	113 118				131 118			87 78	88 103	89 114	99 109	82 96		88 95				86 131	91 94	83 93	80 94	69 86	63 77
17		116	111	110		97 116	101 109				99 109		80 93	88 95	85 90	85 93	82 89	36 191	91 94	83 94	80 94	69 86	
	powe															_							
91 09	111 109				128 111				86 95		97 101	80 87	79 84	85 86	82 80		78 80	81 90	88 80	81 84	76 84	69 78	61 74
92 09	112 109			108 102	130 110	97 109			87 95	88 105	98 101	82 87		87 86	83 79	86 83	80 80	83 90	89 81	81 83	76 82	•	62 71
	113 110	97 109			131 112	98 110					99 102		31 86	88 88	86 82		82 81		89 83	83 86	79 86	71 79	62 70
	111 111	96 109			129 112						98 103		79 87	85 87	80 80		76 81		87 82	80 86	72 85	69 80	
lΊ	111	110	106				99 102						79 87	85 87	80 81	82 85	76 81	81 91	87 83		71 85	70 80	61 71
_	wer a			- 21				^-	2-	01				0.		-/	~,	~/	00				
							96 100						75 85	81 85	75 79	76 82	71 79	76 89	82 85	77 82	68 80		57 68
.2		111	107	105	114		96 103						76 88	82 89	75 82	76 86	72 83	76 92	83 90	77 88	69 86		57 71
4																							

A:LABORATORY BACK-TO-BACK TEST (SHEET 50) OC) FLO TOTAL R 35 36 37 42 43 44 45 46 47 20.1 22.8 20.1 22.8 20.1 22.8 20.1 22.8 20.4 22.5 20.4 71 67 22.5 20.4 22.5 71 68 20.1 22.5 20.1 **S5** 22.5 46 34 19.5 22.5

19.8

22.8

46 35

74 69

res	ST (S	SHE	ET!	50)															
													PUMP		MA	NIFC	OLD		MMY
													.ow			RES		PR	PUT ESS
37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
70 94	88 92	75 10 5	71 87	52 74	68 75	66 84	58 43	74 90	67 79	67 71	27	20.1 22.8	5.5	70 65	41 42	40 37	36 35	21	17
71 94	88 92	75 105	71 87	52 74	69 76	67 84	59 43	75 91	67 79	67 72	29	20.1	5.5	70 65	41 42	40 37	36 35	21	17
71 94	88 9 2	75 105	71 88	52 74	69 76	67 84	59 43	75 91	67 79	67 72	27	20.1	5.5	70 65	41 42	40 37	36 35	21	18
71 95	88 9 2	75 105	71 87	52 74	69 75	66 84	59 43	75 91	67 80	66 71	26	20.1 22.8	5.5	69 65	41 42	40 37	36 35	21	18
69 89	96 84	75 95	69 81	52 66	68 68	66 78	57 41	74 82	67 74	66 66	24	20.4	5.5	70 66	42 44	40 38	36 36	21	18
70 90	87 84	75 95	70 82	53 65	67 69	65 79	58 41	75 82	67 74	66 68	24	20.4	5.4	70 66	42 44	40 38	36 36	21	18
70 90	88 84	76 96	71 82	54 66	68 69	66 79	58 41	75 83	68 74	67 67	24	20.4	5.3	70 66	42 44	40 38	36 36	21	18
70 91	85 86	75 96	70 82	52 68	69 69	66 79	58 41	74 85	67 75	66 68	24	20.1 22.5	5.4	70 66	42 44	40 38	36 36	21	18
70 91	85 87	75 96	69 84	52 69	68 70	66 80	58 42	74 85	66 76	66 68	24	20.1	5.4	70 66	42 44	40 38	36 36	21	18
66 88	82 83	72 94	65 77	48 67	64 66	62 74	53 40	71 82	63 71	62 63	17	19.5	5.4	70 66	41 43	39 38	36 36	21	18
65 90	82 87	72 98	64 80	48 70	64 69	61 77	53 41	71 85	63 74	62 66	17	19.8	5.5	70 66	41 43	39 38	36 36	21	18

I																
	DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10
	1/18/73	06:15	236:56	1100	250	DUMMY TEST			106 112		88 108			100 102	103 99	123 110
	1/18	06:45	237:26	1100	250	DUMMY TEST	92 99			114 119	90 109		-	101 105	104 101	125 111
	1/18	07:15	237:56	1100	250	DUMMY TEST			97 116	112 121		107 114				122 114
	1/18	07:45	238:26	1100	250	DUMMY TEST	81 98		97 117		86 114	106 116		99 110		122 115
	1/18	08:15	238:56	1950	250	DUMMY TEST	81 97		96 115	114 120	89 112		-	102 107		128 113
	1/18	08:45	239:26	1950	2 5 0	DUMMY TEST			97 116		89 112	111 113		102 108		128 114
	1/18	09:15	239:56	1950	250	DUMMY TEST			97 116		90 113			103 108		128 115
	1/18	09:45	240:26	1950	250	DUMMY TEST			97 117		89 114	110 115				128 115
	1/18	10:15	240:56	1950	250	DUMMY TEST	83 99		98 117		90 114	111 115				129 115
	1/18	10:15	241:26	1950	250	DUMMY TEST			99 117	116 122	91 114	111 115				129 116
	1/18	11:15	241:56	1950	250	DUMMY TEST					91 115			103 110		129 116

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TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORA

6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29
		100 102		123 110		96 100	82 71	88 95	82 100	95 100	79 87	78 84	82 83	73 75	77 78	72 75	76 87	80 77	77 80	68 78	73 78	76 73	74 76
.08 .10	_	101 105	104 101	125 111			85 70		83 102	96 101		78 86	82 85	72 78	75 81	69 78	75 89	81 80	78 81	66 80		63 72	61 76
.07 .14	-		103 104			95 103			83 106	96 105		76 89		71 82	76 85	68 82	73 92	79 90	74 85	64 85	65 82	57 74	55 78
			102 106						82 107			75 91	80 91	71 84	75 87	68 84	73 94	79 93	73 89	63 89	65 85		54 80
			106 104						86 108		80 91	77 88		79 83			78 92	85 90	79 88	7] 86	67 81	57 72	55 76
			106 105				84 73		86 108		80 92	78 89		80 84	80 87		79 93	87 89	79 89	71 87	68 82	58 73	57 78
		103 108		128 115			85 7 5	85 99	86 110		81 92	79 89	85 90	80 84	81 88		80 93	87 92	80 90	72 89	68 83	59 74	57 79
		102 108	106 106	128 115		98 104			86 110		80 92	78 89	85 90	80 84	80 88		79 95	86 89	79 90	71 89	68 83	59 75	57 78
11 15	95 112	103 109	106 107	129 115	95 115	98 105	84 75	85 100	86 110	97 106	80 94	78 90	85 91	80 85	80 88	76 85	79 95	86 87	79 90	71 90	68 84	60 75	58 79
11 15	96 114	103 109	107 107	129 116	95 115	99 106	86 76	86 100	87 110	98 107	81 94			81 85			80 96	87 88	80 91			61 74	
			107 108						87 110		81 94			81 86		77 86	80 96	87 88	80 92		-	61 74	

BACK TEST (SHEET 51)

													PUMP							- 4	
															PUMP			NIFO			YMY
															ow		1	RESS		PRI	PUT
35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H	L/H	R/H
70 71	80 84	82 89	83 84	77 93	78 82	51 66	78 78	76 79	70 41	77 83	77 77	76 74	39	19.8 22.5	5.3	70 66	42 44	40 38	36 35	21	18
54 72	77 87	74 92	82 85	75 94	73 84	49 68	73 74	70 80	61 42	75 85	69 76	69 67	22	19.5 22.5	5.4	70 66	42 44	40 38	36 35	21	18
59 71	72 89	66 91	80 88	72 96	66 82	48 71	66 70	63 79	54 41	71 87	63 76	72 67	17	19.5 20.8	5.5	70 66	42 4 3	40 38	36 35	21	18
i9 '3	72 91	65 93	79 91	71 99	64 85	47 74	63 71	60 81	52 66	71 90	62 77	52 69	15	19.5 20.8	5.6	70 66	42 43	40 38	3 6 35	21	18
0 0	73 88	65 91	83 87	72 98	65 82	50 70	65 69	63 79	54 63	7 2 85	64 74	62 66	15	19.8 22.5	5.5	70 66	42 43	40 38	36 35	21	18
1	73 89	66 91	84 88	73 99	66 81	51 70	66 69	64 78	55 68	73 86	65 76	63 66	15	20.1 22.8	5.5	70 65	42 43	40 38	36 35	21	18
1.	74 89	66 92	85 89	73 99	67 81	52 71	67 69	64 78	55 68	73 87	65 76	63 67	15	20.1 22.8	5.5	70 65	42 43	40 38	36 35	21	18
1 2	74 90	66 92	84 89	73 100	67 82	51 72	67 70	64 79	55 65	73 87	65 77	63 68	16	20.1 22.8	5.5	70 65	42 43	40 38	36 35	21	18
2	74 90	67 93	84 90 :	73 100	67 84	51 72	67 7 1	65 79	56 63	73 88	66 77	64 75	20	20.1 22.8	5.5	70 65	42 43	40 38	36 35	21	18
	75 90	68 92	85 90]	74 101	68 81	53 73	68 72	66 79	57 7 7	74 89	66 79	65 73	21	20.1	5.5	70 65	42 43	40 38	36 35	21	18
	76 90	69 93	85 90]	74 102	69 81	53 74	69 72	67 79	58 73	75 89	67 80	66 74	23	20.1	5.5	70 65	42 42	40 37	36 35	21	18

	_															
	DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	1
	1/18/73	12:10	241:56	1950	250	DUMMY TEST	88 99			116 120	92 111	112 110		103 105		
	1/18	12:40	242 :26	1950	250	DUMMY TEST	87 100			116 120	92 112	111 112	96 110	104 106	107 104	
	1/18	13:10	242:56	1950	250	DUMMY TEST	88 100				92 112				107 103	
	1/18	13:40	243:26	1950	250	DUMMY TEST	88 100			116 121	91 112	111 112		103 106	107 104	
	1/18	14:10	243:56	2400	250	DUMMY TEST	89 101			117 122		113 114		105 108	108 106	
	1/18	14:40	244:26	2400	250	DUMMY TEST	89 101			118 122	93 114	113 115		106 109	109 106	
	1/18	15:10	244:56	2400	250	DUMMY TEST	89 101			118 122	94 114	114 114			109 106	
1	1/18	15:40	245 : 26	2400	250	DUMMY TEST	89 101					114 115	98 113	106 108	109 106	13 11
	1/18	16:10	245:56	2400	250	DUMMY TEST	89 101			117 122		113 114		105 109	109 106	
	1/18	16:40	246 :26	2700	250	DUMMY TEST	89 101			118 123	94 115	114 115	98 114	106 110	110 108	
	1/18	17:10	246:56	2700	250	DUMMY TEST	88 101		101 118	118 123		114 115		106 110	110 108	

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA;LA

TEMPERATURE (°C)

	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	
))	-	112 110	96 109	103 105	107 102	128 113	96 112	100 102				100 103			85 85	77 80	80 81	75 80	79 90	83 82	80 85		76 81	
;)		111 112	96 110	104 106	107 104	128 113	96 112	100 103	86 73	87 98	87 107	100 103	82 91	80 88	86 88	78 81	81 84	75 82		86 85	80 87		71 82	
;	92 112	111 112	96 110	103 106	107 103	129 13.4	96 112	100 103	86 73	87 98	87 107	100 104	82 92	80 89	86 88	78 81	81 84	75 81	80 92	86 83	80 88	71 85	71 83	(
		111 112	95 110	103 106	107 104	128 114	95 112	99 103	85 74	87 98	86 107	98 104	81 91	80 89	85 88	77 81	80 84	75 81	79 92	86 მე	80 88		70 82	•
4		113 114	97 112	105 108	108 106	130 115	97 114	101 105	86 75	88 100	88 110	101 106	83 93	81 90		86 84			82 95	89 86	82 90		71 84	€ 7
	93 114	113 115	97 113	106 109	109 106	130 115	98 115	102 106	87 7 5	88 100	89 110	101 106	83 93	81 91	87 91	82 85	85 88	79 85	83 95	90 86	82 91	75 90	72 84	£
	94 114	114 114	98 112	106 109	109 106	131 116	98 115	102 106	87 75	89 100	89 110	102 106	83 93	81 90	88 90	83 85	83 88	79 85	82 96	89 86	82 90	75 89	72 84	•
	94 114	114 115	98 113	106 108	109 106	131 116	98 115	102 106	87 75	89 100	89 110	102 106	83 93	81 90	88 90	83 85	83 88		82 95	90 8 6	82 91	75 89	72 85	ŧ
		113 114	97 112	105 109	109 106	130 116	98 115	101 106	87 76	88 100	88 110	101 106	83 93	81 90	87 90	83 85	83 88	79 85	82 95	89 86	82 91	74 89	71 84	€ 7
		114 115	98 114	106 110	110 108	132 117	99 116	102 107	88 77	89 101	90 112	104 107	84 94	81 91	89 92	85 87	84 90	82 87	85 98	91 88	83 92	79 91	72 85	€ 7
		114 115	98 114	106 110	110 108	132 117	99 116	102 107	87 76	89 101	90 112	104 107	83 94			85 87		82 87	85 98	91 88	83 92	79 91	72 85	6

1 /

		ORA	ATO	RY	BA	.CK-	10	-BA	CK	TES	<u> </u>	SHE	ET 5	2)								т
E (°C)																						F
27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL
76 81	65 71	64 77	5 <u>1</u> 77	40 71	53 72	45 73	79 85	67 69	80 87	75 90	89 87	78 95	75 79	54 69	75 70	72 77	63 60	78 85	71 77	71 71	26	20.1 22.8
71 82	63 72	62 78	49 78	38 71	51 71	42 73	77 86	65 71	77 88	71 92	86 88	76 101	71 81	54 70	70 70	68 79	60 63	76 86	67 78	68 72	24	20.1 22.8
71 83	63 72	61 78	48 79	38 72	50 72	4 <u>1</u> 74	77 87	65 71	77 89	71 92	86 89	76 96	72 81	53 71	71 71	68 7 9	60 68	76 87	68 78	68 73	25	20.1 22.8
70 82	63 72	61 78	48 78	37 71	50 71	41 74	77 87	65 71	76 89	70 92	85 89	75 103	70 81	52 70	70 71	68 79	59 66	75 87	68 78	67 72	25	20.1 22.8
71 84	63 73	62 79	4 9 79	38 73	51 73	42 75	77 88	65 72	77 90	71 92	87 90	76 100	72 82	53 71	71 71	68 80	61 71	76 88	68 80	68 73	25	20.4 23.1
7 2 84	64 74	63 79	50 80	40 74	53 74	45. 76	78 89	66 73	78 90	72 93	88 90	76 101	72 82	55 73	72 73	69 80	61 71	77 89	69 81	69 74	26	20.8 22.8
72 84	64 74	63 79	50 80	41 73	53 73	45 76	78 89	66 73	78 90	72 92	88 90	77 101	72 82	54 73	73 72	70 80	62 65	77 89	69 80	69 74	26	20.4 23.1
72 85	64 74	63 79	50 80	41 74	53 74	45 76	78 89	66 74		72 93	88 91	77 102	73 83	55 73	72 73	70 80	61 70	77 89	69 80	69 74	26	20.4 23.1
71 84	63 74	62 79	49 80	39 74	51 74	·3 75	77 89	66 73		71 93		76 101	72 82	54 72	71 72	69 80	61 67	76 89	69 80	68 74	26	20.4 22.8
72 85	63 74	62 79		38 74		42 76	78 90	66 73		71 92		77 103	72 82	55 74	71 72	69 80	61 68	77 90	69 81	68 75	24	20.4 23.1
72 85		62 80			51 74	42 77	78 90	66 73	78 91	71 93	88 91	77 103	72 84	55 74	71 73	68 81	61 71	77 90	69 81	68 76	24	20.4 23.1

ST	SHE	ET 5	21															
												PUMP		M	ANIFO	OLD	_	MMY
												ow			PRES		PR	PUT ESS
3	3 39	40	41	42	43	44	.45	46	47	48	TOTAL	ROLLER	PRESS	MAI	N L/F	R/H	L/H	R/H
89 87		75 79	54 69	75 70	72 77	63 60	78 85	71 77	71 71	26	20.1 22.8	5.5	70 66	42 44	40 38	36 36	21	18
86 88	76 3 101	71 81	54 70	70 70	68 79	60 63	76 86	67 78	68 72	24	20.1 22.8	5.5	70 66	42 44	40 38	36 36	21	18
86 89		72 81	53 71	71 71	6 8 7 9	60 68	76 87	68 78	68 73	25	20.1 22.8	5.5	70 66	42 44	40 38	36 36	21	18
8 <u>9</u>	75 103	70 81	52 70	70 71	68 79	59 66	75 87	68 78	67 72	25	20.1 22.8	5.5	70 66	42 44	40 38	36 36	21	18
8° 90	76 100	72 82	53 71	71 71	68 80	61 71	76 88	68 80	68 73	25	20.4 23.1	5.5	70 66	42 44	40 38	36 36	21	18
88 90	76 0 101	72 82	55 73	72 73	69 80	61 71	77 89	69 81	69 74	26	20.8 22.8	5.5	70 66	42 44	40 38	36 36	21	18
88 90	3 77 0 101	72 82	54 73	73 72	70 80	62 65	77 89	69 80	69 74	26	20.4 23.1	5.6	70 66	42 44	40 38	36 35	21	18
	3 77 102			72 73	70 80		77 89	69 80	69 74	26	20.4 23.1	5.6	69 66	42 43	40 38	36 35	21	18
	76 101	72 82		71 72		61 67	76 89	69 80	68 74	26	20.4 22.8	5.5	69 66	42 43	40 38	36 35	21	18
_	77	72 82	55 74	71 72	69 80	61 68		69 81	68 75	24	20.4 23.1	5.6	70 66	42 43	40 38	36 36	21	18
	3 77 103	72 84	55 74	71 73	68 81	61 71	77 90	69 81	68 76	24	20.4	5.6	70 66	42 43	40 38	36 36	21	18

					100											T
DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9	10	1
						St	art (מ מר	ower	at 1	7:50					
1/18/73	18:20	247:26	1950	250	DUMMY TEST	86 98	112	99	115	89 110	109	94 108		105 101	126 111	9l 110
1/18	18:50	247:56	1950	250	DUMMY TEST	86 97			-	90 109		94 108	102 104	106 102		-
											aine					
1/18	20:05	248:26	1950	-	DUMMY TEST	96		-	-	90 109		95 108	103 104	107 101	12 7 110	9:
1/18	20:35	248:56	1950	-	DUMMY TEST	85 97		-	115 119		111 110			107 101	128 111	9 <u>9</u>
						St	op cl	neck	sum	p str	aine	rs on	dum	my bo	x	
1/19	00:30	249:26	1950	250	DUMMY TEST	82 96			115 120			94 109		105 102	126 112	93 110
1/19	01:00	249:56	1950	250	DUMMY TEST	82 96			115 119	90 109		95 108		107 101		91 110
1/19	01:30	250:26	1950	250	DUMMY TEST	82 96			115 119		111 109	95 108		107 101		91 110
1/19	02:00	250:56	1950	250	DUMMY TEST	82 95				90 108	111 108	96 106		107 100	128 110	99
1/19	05 :55	250:56	1950	250	DUMMY TEST	88 100			112 118	85 107		91 102		102 98	122 109	89
1/19	06:25	251:26	1950	250	DUMMY TEST	81 98				86 113	106 114	91 112		102 106	123 115	

TABLE XXI. ROLLER GEAR TRANSMISSION TEST DATA: LABORATORY BACK-TO-BA

11	12	13	14	15	16	1 <i>7</i>	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35
94	98	84	85	85	97	80	78	83	75	79	72	77	83	78	70	68	60	59	49	37	48	43	75	63
110	100	71	95	104	101	89	85	85	78	81	78	88	80	84	82	79	68	74	74	68	69	70	83	68
94	98	85	85	86	98	80	78	84	76	79	73	78	84	78	69	69	60	58	48	36	46	42	75	63
110	101	71	96	105	102	89	86	85	79	82	79	89	81	85	83	80	69	74	75	69	69	71	85	69
9 5	99	85	85	86	98	81	79	85	77	80	74	79	85	79	70	70	59	58	48	36	47	42	76	63
1 10	100	70	95	105	101	88	85	85	78	81	78	88	82	84	82	79	68	73	74	68	68	69	83	67
9 5	99	86	85	86	98	81	79	85	76	80	74	79	85	79	7 0	69	60	59	49	37	48		76	63
110	100	70	95	105	101	89	85	85	78	81	79	88	86	85	82	79	68	74	74	68	68		84	68
9 3	97	82	83	85	97	80	78	82	75	78	72	77	83	78	69	69	58	57	47	35	46	41	75	62
	101	72	97	106	103	90	86	86	80	82	80	90	85	87	85	81	70	76	77	68	69	71	85	68
9 4	99	84	84	87	99	81	80	84	77	80	74	79	85	80	70	70	60	58	48	36	47	42	76	63
10	100	70	95	105	101	89	85	85	79	81	79	89	83	84	82	79	67	68	74	67	67	69	84	67
9 4	99	84	84	87	99	81	80	84	77	80	74	79	85	80	70	70	60	58	48	36	47	42	75	63
10	100	70	94	105	101	89	85	85	79	80	79	89	82	85	82	80	68	68	74	67	67	69	84	67
9 5 0 9	99 99	85 69	84 94	87 104		81 87	80 85	85 84	78 78	80 80	74 78	79 88	86 85	80 83	70 81	70 78	59 66	58 71	48 72	36 65	47 66	42 68	76 82	6 3
8 9	93	79	87	81	94	77	76	79	70	76	68	72	76	75	66	70	73	70	5 7	44	59	48	76	68
0 8	99	68	93	100	99	86	81	80	73	75	73	83	75	76	72	74	66	70	69	70	56	59	79	59
8 8 15	94 105			82 108			74 89	79 89	71 83	75 86	68 83	72 93	78 86	74 89	64 87	65 84	56 74	55 78	45 76		45 73	40 7 ¹ 4	71 87	59 71

V	TEC	T 16	UE	ET A	21											-				
	163) (3	HE		131			-						PUMP		MA	NIFO	LD	DU	MMY
													FL	OW	11722	1	PRESS			PUT
36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIN	L/H	R/H		
7 5 8 5	68 89	83 85	73 94	68 77	50 67	67 67	64 74	56 68	73 83	65 75	65 69	22	19.8	5.4	70 66	42 44	40 38	36 36	21	18
6)	09	0)	דע	1,	O1	01	17	00	0,5	17	J)			,			J	30		
75	68	83	74	69	51	67	64	56	74	65	65	21	19.8 22.8	5.4	70 66	42 44	40 38	36 36	21	18
8 6	90	86	95	78	68	69	76	69	85	76	70		22.0	7.4	00	44	30	30	1	
7 6 8 4	68	85	75	69	52	67	65	56	75	65	65	19	19.8		70	42	40	36	21	18
84	88	85	94	76	67	66	73	65	83	74	68		22.8	5.4	66	44	38	36		
7 6	68	85	75	69	53	67	65	56	74	65	65	20	20.1		70	42	40	36	21	18
85	90	85	95	77	68	67	75	70	84	76	69		22.8	5.4	66	44	38	36		
7 5	66	83	74	68	53	65	62	54	74	63	64	16	19.8		69	41	39	36	21	18
7 5 8 5	88	87	96	76	69	66	73	71	85	75	69		22.5	5.4	66	43	38	35		
7 6 8 5	67 88	85 85	75 95	69 76	53 68	66 66	64 73	55 74	75 84	65 74	64 68	16	20.1 22.8	5.4	69 66	41 43	39 38	36 35	21	18
رن	00	0)	97	10	00	00	د۱	17	04	1-7	00		22.0	7.4		.5	30			
7 5	67	85	75	69	53	66	64	55	75	65	64	16	20.1	- 1.	69 66	41 43	39 39	36 35	21	18
85	89	85	95	75	67	66	73	74	84	74	68		22.8	5.4	00	43	39	رد		
7 5	66	85	75	68	53	66	64	54	74	64	64	14	20.1		69	41	39 38	36	21	18
84	87	84	94	74	66	65	71	76	82	72	67		22.8	5.4	66	43	38	35		
7 7	80	81	75	76	48	75	72	65	74	73	73	33	19.5		70	42	40	36	21	18
79	80	80	89	71	72	69	70	52	74 79	70	66		22.5	5.3	66	44	38	35		
72	66	80	71	წ 6	45	64	62	52	70	62	62	16	19.2		70	42 43	39 38	36	21	18
89	91	89	96	79	73	69	77	66	87	76	66		23.1	5.6	66	43	38	35		

DATE	TIME OF DAY	TOTAL TEST TIME	TOTAL INPUT H.P.	TAIL H.P.		1	2	3	4	5	6	7	8	9
1/19/73	06:55	251:56	1950	250	DUMMY TEST	81 100	108 72		112 126	85 118	106 119	91 117		102 110
1/19	07:25	252:26	1950	250	DUMMY TEST	81 98	109 72		113 123	86 115		113	-	102 107
1/19	07:55	252:56	1950	250	DUMMY TEST	82 98		-		87 114		92 113		104 107
1/19	08:25	253:26	1950	250	DUMMY TEST	82 98				88 114	109 115			104 107
1/19	08:55	253:56	1950	250	DUMMY TEST	82 98		-	114 122	88 114	109 114	93 113		105 107
1/19	09:25	254:26	2700	250	DUMMY TEST	83 96			116 120	90 112		96 111		107 105
1/19	09:55	254:56	2700	250	DUMMY TEST	83 97			116 120	90 1.12	112 112	-	104 107	107 105
1/19	10:25	255:26	2700	250	DUMMY TEST	84 98	113 71		117 121	91 113	113 114	97 111	1.05 109	
1/19	10:55	255:56	2700	250	DUMMY TEST	84 98	72	117	122	114	113 114 load	112	105 109 on po	10'
1/19	11:35	256:11	3700	425	DUMMY TEST	90 100	114 76	103 115	118 120	94 113	116	99 110	107 107 107	110
1/19	12:35	256:56	400	40	DUMMY TEST	99 107	116	101	113	89 112	107	92 110	_	10
						St	op	End	of t	ench	test			

TABLE XXI.	ROLLER	GEAR	TRANSM	ISSION	TEST	DATA	:LAB	OF
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6	7	8	9	10	_11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	2
106 119	-			122 120		94 110		80 103	82 113	95 110	75 98	73 95	79 95	70 89	76 92	68 89	73 99	78 98	74 94	65 93	64 90	55 79	5.
106 115	-	98 109		123 116		95 105	82 76	81 100		96 107		74 91	80 91	71 85	77 87	69 85	73 95			65 90	65 85	55 76	5: 8(
						97 105	82 76	82 99	84 109	97 106	77 94	76 90	81 90	73 84	77 87	70 84	76 95		77 90		66 85		5 <u>:</u> 8(
109 115				126 116		97 105		82 100		98 106		77 90	82 90	74 84	78 87	71 84	76 95				67 85	57 74	5€ 79
				126 116		97 105		83 100		98 106	78 94	77 90	82 90	74 84	78 87	71 84	76 95		77 90		67 85	57 75	5€ 79
				129 114		99 103				101 103		79 88	86 89		82 87	79 83	82 95		81 89		68 81	58 71	57 74
				129 113		100 103				101 103		80 87		82 83		79 84		89 87	81 89	77 87	68 81	58 68	58 74
				130 114						101 105		81 89	87 90	83 85	83 88	80 85	84 96		82 90	77 89	70 82	60 72	58 77
113 114 pad	112	109	107	131 116 11:20	115	101 105	86 74	86 99	89 111	102 105	82 92	81 90	87 90	83 85	84 89	81 85	84 96	90 87	82 90	77 90	70 83	60 73	59 78
116	99 110	107 107	110 105	132 115 t 11:	98 113					102 105			88 87	86 84	87 87	83 85	86 95	92 84					
	110			120 115		96 105				96 105		78 92		70 82			73 93			65 87	69 86	60 75	58 78

RY	BA	CK.	TO.	BACK	TEST	SHEET	541
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																			PUMP		, t
																			.ow		
31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	W
33 76	44 78	40 79	70 93	58 77	70 94	64 94	79 94	70 93	64 84	44 79	61 74	59 81	51 69	69 92	60 79	60 71	15	19.2 23.1	5.7	70 65	42 42
33 71	44 74	40 76	71 90	59 79	70 91	63 93	79 91	70 101	64 83	46 74	62 72	59 79	50 68	69 90	61 78	60 68	13	19.2 22.5	5.4	70 66	42 43
34 71	45 74	40 76	73 90	60 73	72 91	64 93		72 100	65 82	49 74	63 71	61 79	52 71	71 89	62 77	61 68	14	19.5 22.5	5.4	69 65	41 42
34 70	46 73	41 76	73 89	60 72	73 90	65 93		72 100	66 82		64 70	61 79	52 69	72 89	62 77	61 67	14	19.2 22.5	5.4	69 65	41 42
34 70	46 74	41 76	73 89	61 73	73 90	65 93		72 100	66 81		64 71	62 78	52 72	72 89	62 77	62 68	14	19.2 22.5	5.4	69 65	41 42
35 68	46 70	41 71	74 85	62 70	74 87	66 90	86 87	73 99	57 80	52 69	54 70	62 77	54 66	73 85	63 75	63 66	15	19.8 22.5	5.3	69 66	42 43
36 68	47 70	42 71	75 85	62 70	74 87	66 90	86 87	74 99	68 79	52 69	66 69	64 76	54 68	73 85	63 75	63 66	15	19.8 22.2	5.3	69 66	42 43
36 69	47 72	42 73	75 87	63 71	75 89	68 91		75 100	69 80	53 71	65 70	64 77	55 63	75 86	65 77	64 70	17	19.8 22.2	5. ¹ 4	69 66	42 43
38 70	49 72	44 74	76 87	64 72	76 89	68 92	87 89	75 101	69 80	54 71	66 71	64 78	56 65	75 87	66 77	65 68	18	19.8 22.2	5.4	69 66	42 43
																		20.7 22.2	5.3	70 66	42 43
36 71	47 73	42 75	73 90	63 74	73 91	69 94	80 91	72 98	69 84	50 76	67 77	65 81	56 59	72 90	65 79	65 77	23	19.5 21.5	5.4	69 65	41 42

ET 5	41							erio Ed								
	- 1									PUMP		MANIFOLD			DUMMY INPUT PRESS	
									FL	ow		PRESS				
40	41	42	43	44	45	46	47	48	TOTAL	ROLLER	PRESS	MAIL	N L/F	R/H		R/H
64 84	44 79	61 74	59 81	51 69	69 92	60 79	60 71	15	19.2 23.1	5.7	70 65	42 42	39 37	36 35	21	18
64 83	46 74	62 '2	59 79	50 68	69 90	61 78	60 68	13	19.2 22.5	5.4	70 66	42 43	40 38	35 35	21	18
65 82	49 74	63 71	61 79	52 71	71 89	62 77	61 68	14	19.5 22.5	5.4	69 65	41 42	39 37	35 35	21	18
66 82	49 73	64 70	61 79	52 69	72 89	62 77	61 67	14	19.2 22.5	5.4	69 65	41 42	49 37	35 35	21	18
66 81	49 73	64 71	62 78	52 72	72 89	62 77	62 68	14	19.2 22.5	5.4	69 65	41 42	39 37	35 35	21	18
57 80	52 69	54 70	62 77	54 66	73 85	63 75	63 66	15	19.8 22.5	5.3	69 66	42 43	40 38	36 35	21	18
68 79	52 69	66 69	64 76	54 68	73 85	63 75	63 66	15	19.8 22.2	5.3	69 66	42 43	40 38	36 35	21	18
69 80	53 71	65 70	64 77	55 63	75 86	65 77	64 70	17	19.8 22.2	5.4	69 66	42 43	40 38	36 35	21	18
69 80	54 71	66 71	64 78	56 65	75 87	66 77	65 68	18	19.8 22.2	5.4	69 66	42 43	40 38	36 35	21	18
									20.7	5.3	70 66	42 43	40 38	36 35	21	19
69 84	50 76	67 77	65 81	56 59	72 90	65 79	65 77	23	19.5 21.5	5.4	69 65	41 42	39 37	35 35	20	18
	64 84 64 83 65 82 66 81 57 80 68 79 69 80	64 44 84 79 64 46 83 74 65 49 82 74 66 49 81 73 57 52 80 69 68 52 79 69 69 53 80 71 69 54 80 71	40 41 42 64 44 61 84 79 74 64 46 62 83 74 72 65 49 63 82 73 70 66 49 64 81 73 71 57 52 54 80 69 70 68 72 66 79 69 69 69 71 70 69 54 66 80 71 71	40 41 42 43 64 44 61 59 64 46 62 59 65 49 63 61 82 74 71 79 66 49 64 61 82 73 70 79 66 49 64 62 81 73 71 78 57 52 54 62 80 69 70 77 69 53 65 64 80 71 70 77 69 54 66 64 80 71 71 78 69 50 67 65 69 50 67 65	40 41 42 43 44 64 44 61 59 51 64 46 62 59 50 63 74 71 79 71 66 49 64 61 52 82 73 70 79 69 66 49 64 61 52 81 73 71 78 72 57 52 54 62 54 80 69 70 77 66 68 52 66 64 54 79 69 69 76 68 69 53 65 64 55 80 71 70 77 63 69 54 66 64 56 80 71 71 78 65 69 50 67 65 56 69 50 67 65 56	40 41 42 43 44 45 64 44 61 59 51 69 92 64 46 62 59 50 69 92 65 49 63 61 52 71 78 66 49 64 61 52 72 89 66 49 64 62 52 72 89 57 52 54 62 52 72 89 57 52 54 62 54 73 73 70 77 66 85 68 52 66 64 54 73 73 73 76 89 85 69 53 65 64 54 73 86 69 54 66 64 55 75 75 69 54 66 64 56 75 87 69 54 66 64 56 75 87 69 </td <td>40 41 42 43 44 45 46 64 44 61 59 51 69 92 79 64 46 62 59 50 69 92 79 63 74 72 79 68 90 78 65 49 63 61 52 71 89 77 66 49 64 61 52 72 62 89 77 66 49 64 62 52 72 72 62 81 73 71 78 72 89 77 57 52 54 62 54 73 63 63 80 52 66 64 54 73 63 63 75 68 52 66 64 54 73 65 65 75 69 53 65 64 55 75 75 65 80 71 70 77<td>40 41 42 43 44 45 46 47 64 44 61 59 51 69 92 79 71 64 46 62 59 50 69 61 60 83 74 72 79 68 90 78 68 65 49 63 61 52 71 62 61 82 74 71 79 71 89 77 68 66 49 64 61 52 72 62 61 82 73 70 79 69 89 77 67 66 49 64 62 52 72 62 62 81 73 71 78 72 89 77 68 57 52 54 62 54 73 63 63 80 69 70 77 66 85 75 66 69 53 65<td>40 41 42 43 44 45 46 47 48 64 44 61 59 51 69 60 60 15 64 46 62 59 50 69 61 60 13 63 74 '2 79 68 90 78 68 13 65 49 63 61 52 71 62 61 14 82 74 71 79 71 89 77 68 14 66 49 64 61 52 72 62 61 14 82 73 70 79 69 89 77 67 14 66 49 64 62 52 72 62 62 14 80 73 71 78 72 89 77 68 15 68 52 54 62 54 73 63 63 15 69 53<td>40 41 42 43 44 45 46 47 48 TOTAL 64 44 61 59 51 69 60 60 15 19.2 23.1 64 46 62 59 50 69 61 60 13 19.2 23.1 65 49 63 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 72 62 61 14 19.5 22.5 66 49 64 62 52 72 62 62 14 19.2 22.5 57 52 54 62 54 73 63 63 15 19.8 80 52 54 62 54 73 63</td><td>40 41 42 43 44 45 46 47 48 TOTAL ROLLER 64 44 61 59 51 69 60 60 15 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 65 49 63 61 52 71 62 61 14 19.2 22.5 5.4 66 49 64 61 52 72 62 61 14 19.2 22.5 5.4 66 49 64 62 52 72 72 62 62 14 19.2</td><td> PUMP FLOW TOTAL ROLLER PRESS A</td><td> PUMP FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW F</td><td> A</td><td>## PUMP FLOW /td><td> A</td></td></td></td>	40 41 42 43 44 45 46 64 44 61 59 51 69 92 79 64 46 62 59 50 69 92 79 63 74 72 79 68 90 78 65 49 63 61 52 71 89 77 66 49 64 61 52 72 62 89 77 66 49 64 62 52 72 72 62 81 73 71 78 72 89 77 57 52 54 62 54 73 63 63 80 52 66 64 54 73 63 63 75 68 52 66 64 54 73 65 65 75 69 53 65 64 55 75 75 65 80 71 70 77 <td>40 41 42 43 44 45 46 47 64 44 61 59 51 69 92 79 71 64 46 62 59 50 69 61 60 83 74 72 79 68 90 78 68 65 49 63 61 52 71 62 61 82 74 71 79 71 89 77 68 66 49 64 61 52 72 62 61 82 73 70 79 69 89 77 67 66 49 64 62 52 72 62 62 81 73 71 78 72 89 77 68 57 52 54 62 54 73 63 63 80 69 70 77 66 85 75 66 69 53 65<td>40 41 42 43 44 45 46 47 48 64 44 61 59 51 69 60 60 15 64 46 62 59 50 69 61 60 13 63 74 '2 79 68 90 78 68 13 65 49 63 61 52 71 62 61 14 82 74 71 79 71 89 77 68 14 66 49 64 61 52 72 62 61 14 82 73 70 79 69 89 77 67 14 66 49 64 62 52 72 62 62 14 80 73 71 78 72 89 77 68 15 68 52 54 62 54 73 63 63 15 69 53<td>40 41 42 43 44 45 46 47 48 TOTAL 64 44 61 59 51 69 60 60 15 19.2 23.1 64 46 62 59 50 69 61 60 13 19.2 23.1 65 49 63 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 72 62 61 14 19.5 22.5 66 49 64 62 52 72 62 62 14 19.2 22.5 57 52 54 62 54 73 63 63 15 19.8 80 52 54 62 54 73 63</td><td>40 41 42 43 44 45 46 47 48 TOTAL ROLLER 64 44 61 59 51 69 60 60 15 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 65 49 63 61 52 71 62 61 14 19.2 22.5 5.4 66 49 64 61 52 72 62 61 14 19.2 22.5 5.4 66 49 64 62 52 72 72 62 62 14 19.2</td><td> PUMP FLOW TOTAL ROLLER PRESS A</td><td> PUMP FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW F</td><td> A</td><td>## PUMP FLOW /td><td> A</td></td></td>	40 41 42 43 44 45 46 47 64 44 61 59 51 69 92 79 71 64 46 62 59 50 69 61 60 83 74 72 79 68 90 78 68 65 49 63 61 52 71 62 61 82 74 71 79 71 89 77 68 66 49 64 61 52 72 62 61 82 73 70 79 69 89 77 67 66 49 64 62 52 72 62 62 81 73 71 78 72 89 77 68 57 52 54 62 54 73 63 63 80 69 70 77 66 85 75 66 69 53 65 <td>40 41 42 43 44 45 46 47 48 64 44 61 59 51 69 60 60 15 64 46 62 59 50 69 61 60 13 63 74 '2 79 68 90 78 68 13 65 49 63 61 52 71 62 61 14 82 74 71 79 71 89 77 68 14 66 49 64 61 52 72 62 61 14 82 73 70 79 69 89 77 67 14 66 49 64 62 52 72 62 62 14 80 73 71 78 72 89 77 68 15 68 52 54 62 54 73 63 63 15 69 53<td>40 41 42 43 44 45 46 47 48 TOTAL 64 44 61 59 51 69 60 60 15 19.2 23.1 64 46 62 59 50 69 61 60 13 19.2 23.1 65 49 63 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 72 62 61 14 19.5 22.5 66 49 64 62 52 72 62 62 14 19.2 22.5 57 52 54 62 54 73 63 63 15 19.8 80 52 54 62 54 73 63</td><td>40 41 42 43 44 45 46 47 48 TOTAL ROLLER 64 44 61 59 51 69 60 60 15 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 65 49 63 61 52 71 62 61 14 19.2 22.5 5.4 66 49 64 61 52 72 62 61 14 19.2 22.5 5.4 66 49 64 62 52 72 72 62 62 14 19.2</td><td> PUMP FLOW TOTAL ROLLER PRESS A</td><td> PUMP FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW F</td><td> A</td><td>## PUMP FLOW /td><td> A</td></td>	40 41 42 43 44 45 46 47 48 64 44 61 59 51 69 60 60 15 64 46 62 59 50 69 61 60 13 63 74 '2 79 68 90 78 68 13 65 49 63 61 52 71 62 61 14 82 74 71 79 71 89 77 68 14 66 49 64 61 52 72 62 61 14 82 73 70 79 69 89 77 67 14 66 49 64 62 52 72 62 62 14 80 73 71 78 72 89 77 68 15 68 52 54 62 54 73 63 63 15 69 53 <td>40 41 42 43 44 45 46 47 48 TOTAL 64 44 61 59 51 69 60 60 15 19.2 23.1 64 46 62 59 50 69 61 60 13 19.2 23.1 65 49 63 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 72 62 61 14 19.5 22.5 66 49 64 62 52 72 62 62 14 19.2 22.5 57 52 54 62 54 73 63 63 15 19.8 80 52 54 62 54 73 63</td> <td>40 41 42 43 44 45 46 47 48 TOTAL ROLLER 64 44 61 59 51 69 60 60 15 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 65 49 63 61 52 71 62 61 14 19.2 22.5 5.4 66 49 64 61 52 72 62 61 14 19.2 22.5 5.4 66 49 64 62 52 72 72 62 62 14 19.2</td> <td> PUMP FLOW TOTAL ROLLER PRESS A</td> <td> PUMP FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW F</td> <td> A</td> <td>## PUMP FLOW /td> <td> A</td>	40 41 42 43 44 45 46 47 48 TOTAL 64 44 61 59 51 69 60 60 15 19.2 23.1 64 46 62 59 50 69 61 60 13 19.2 23.1 65 49 63 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 71 62 61 14 19.5 22.5 66 49 64 61 52 72 62 61 14 19.5 22.5 66 49 64 62 52 72 62 62 14 19.2 22.5 57 52 54 62 54 73 63 63 15 19.8 80 52 54 62 54 73 63	40 41 42 43 44 45 46 47 48 TOTAL ROLLER 64 44 61 59 51 69 60 60 15 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 64 46 62 59 50 69 61 60 13 19.2 23.1 5.7 65 49 63 61 52 71 62 61 14 19.2 22.5 5.4 66 49 64 61 52 72 62 61 14 19.2 22.5 5.4 66 49 64 62 52 72 72 62 62 14 19.2	PUMP FLOW TOTAL ROLLER PRESS A	PUMP FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW FLOW TOTAL ROLLER PRESS MAIN FLOW F	A	## PUMP FLOW FLOW	A

APPENDIX II

ULTRASONIC INSPECTION

The electron beam welds of the roller gear drive components were inspected by the pulse-echo ultrasonic inspection technique. This technique employs ultrasonic energy in the range of .25 - 25 Miz to detect flaws. This range is used because wavelengths of energy in this frequency range are of the same order of magnitude as the flaws in the welds.

The principle of pulse-echo ultrasonic inspection is depicted schematically in Figure 123. A short burst of ultrasonic energy is emitted from the piezoelectric crystal. When the pulse reaches surface "A" of the test specimen, a portion of the energy is reflected, due to an acoustic impedance mismatch, back to a pickup and displayed on the oscilloscope as the trace labeled "A" in Figure 123. The portion of the pulse not reflected from surface "A" continues through the material until it reaches the defect "Y" where the pulse is again reflected and displayed on the oscilloscope as trace "B". The remainder of the wave passes through the material and is reflected off the back surface and recorded as trace "C".

By drilling a flat bottomed hole of known depth and diameter in a sample similar to the specimens to be tested and performing an inspection on it, the ultrasonic inspection technique can be calibrated so that both depth and size of voids can be determined.

The particular method used for inspection of the electron beam welds of the roller gear components is known as the fullimmersion technique. In this method, the test specimen is fully immersed in water containing a wetting agent. The water acts as a conduction of the ultrasonic waves, thus eliminating the need for the probe to be in physical contact with the test specimen. This method allows automation to be employed in the inspection and produces more consistent results than the contact method. The equipment used for the inspection of the roller gear drive components is pictured in Figures 124 and 125. A schematic showing inspection of a first-row pinion is shown in Figure 126. The waveform at the bottom represents an actual waveform resulting from the inspection. The peak at the left represents the inner wall. The smaller peak in the center represents a void in the weld, while the peak on the right represents the outer wall of the component.

As a direct result of the experiences in this program, the following inspection procedure was developed.

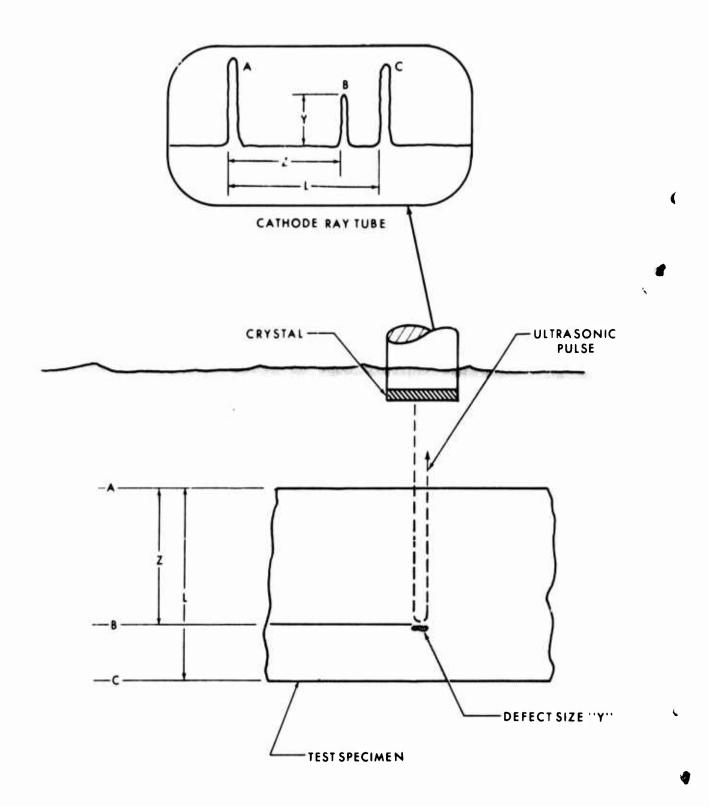


Figure 123. Schematic - Pulse-Echo Ultrasonic Inspection.

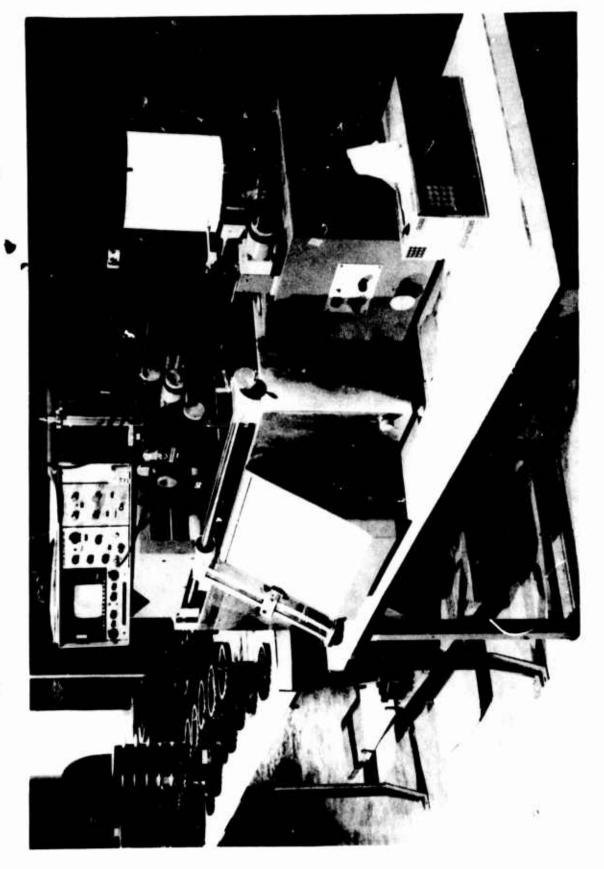
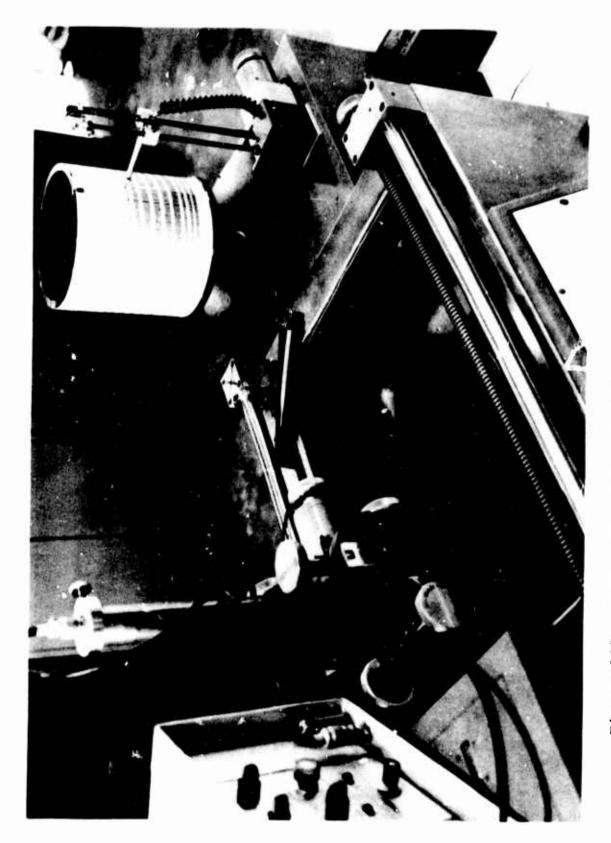


Figure 124. Ultrasonic Inspection Equipment.



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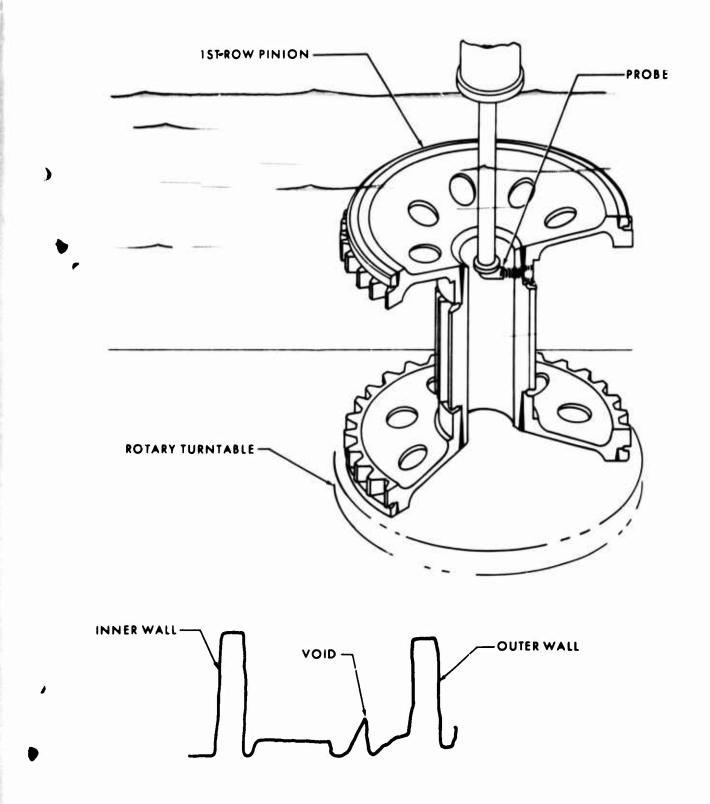


Figure 126. Schematic - Ultrasonic Inspection, First-Row Pinion.

Ultrasonic Inspection of Electron Beam Welded Gears

Scope

This procedure covers the requirements for conducting ultrasonic inspection tests by the immersion method and in accordance with Reference 5 to determine the presence of internal discontinuities in the electron beam welds currently used in the manufacture of roller gear drive components.

The procedure is applicable for the following components.

(a)	RG351-11181	Second-Row Pinion	Gear
		4.061 inches dia.	weld
		5.755 inches dia.	weld
		6.121 inches dia.	weld
		9.031 inches dia.	weld

- (b) RG351-11182 First-Row Pinion Gear 5.515 inches dia. weld 1.710/1.000 inches dia. butt weld
- (c) RG351-11183 Sun Gear 8.392 inches dia. weld

The standards for acceptance of defects detected by ultrasonic inspection shall be as specified on the drawings.

Requirements

The equipment used shall be an automated system with C-scan capability such as Sperry SR-154 or US-454.

The electronic equipment used shall be a Sperry Reflectoscope UM721 or UM771 with a 10-N Pulser/Receiver and a Fast Transique.

The search unit shall be suitable for immersion inspection.

The search unit for the diametral welds shall be Lithium Sulfate, 0.25 inch diameter, medium focus 10 MHz, #57A-2766.

The search unit for the butt welds (RG351-11182) shall be a J type, 0.25 inch flat focus, #J385-SIJ-10 MHz.

The calibration standard shall be representative of the test sample, particularly at the entry surface with regard to curvature and surface condition. For the diametral welds listed, the calibration standard shall be as shown in Figure 127.

The butt weld (RG351-11182) calibration standard shall be as shown in Figure 128.

Calibration

The calibration standard with the curvature and entry surface condition similar to the production part being tested shall be calibrated as follows:

Calibration for the diametral welds - the amplitude of the 0.020-inch-diameter test hole shall be set at 2 inches and the gate set to alarm at 90 percent of the test hole amplitude.

Calibration for the butt weld requires two "setups".

- 1. To determine voids equal to or greater than the response from a 0.020-inch-diameter test hole. The amplitude of the 0.020-inch-diameter test hole shall be set at 1.8 inches and the gate set to alarm at 90 percent of the test hole amplitude.
- 2. To determine voids equal to or greater than the response from a 0.013-inch-diameter test hole. With the amplitude of the 0.020-inch-diameter test hole set at 1.8 inches (the 0.013-inch test hole amplitude is 0.75 inch), the gate shall then be set to alarm at 90 percent of the 0.013-inch test hole amplitude.

Procedure

For each different type of gear and direction of scanning the corresponding calibration standard C-scan is required.

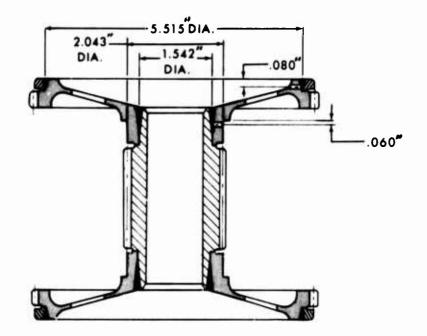
The surface from which the test is to be performed shall be clean and free from dirt, grease and scale.

Upon the component being immersed in the tank, all air bubbles shall be removed from the surface being tested.

The search unit shall be maintained normal to the test surface, with the search unit positioned as shown in Figures 129, 130, and 131.

The weldments shall be inspected at 10 MHz.

Complete coverage of the weld area shall be accomplished by indexing after each complete scan. The transducer shall be moved in such manner that each scan overlaps the previous pass by at least 25 percent of the effective beam diameter.



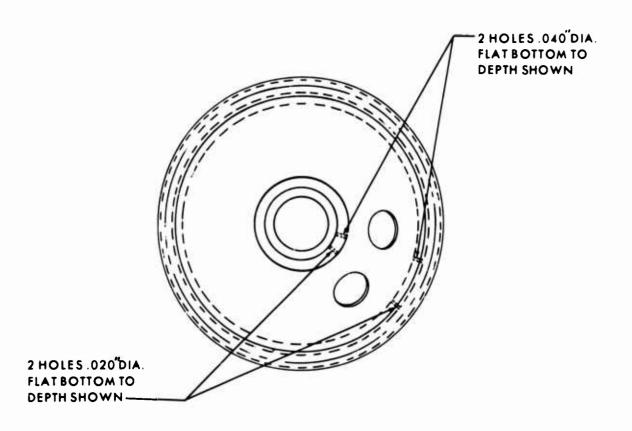
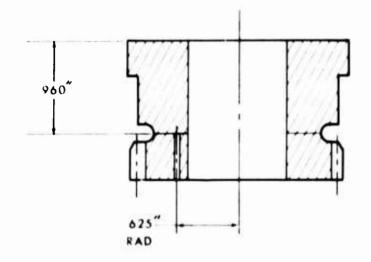


Figure 127. Calibration Standard - Diametral Weld,



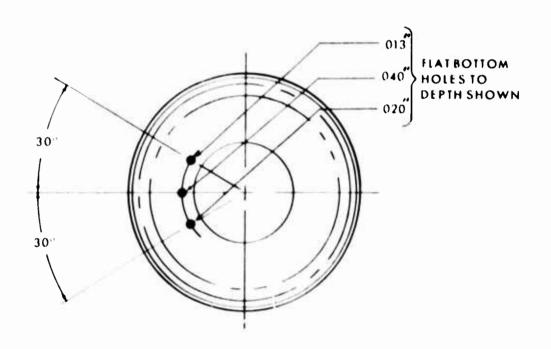


Figure 128. Calibration Standard - Butt Weld.

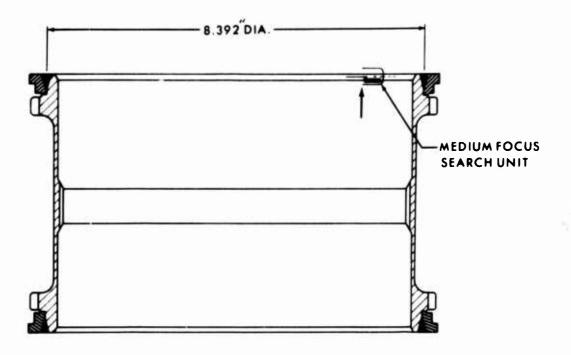


Figure 129. Sun Gear - Ultrasonic Inspection

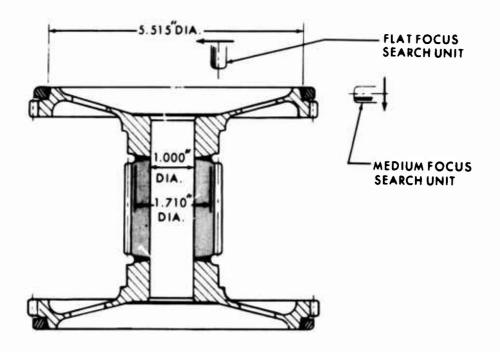
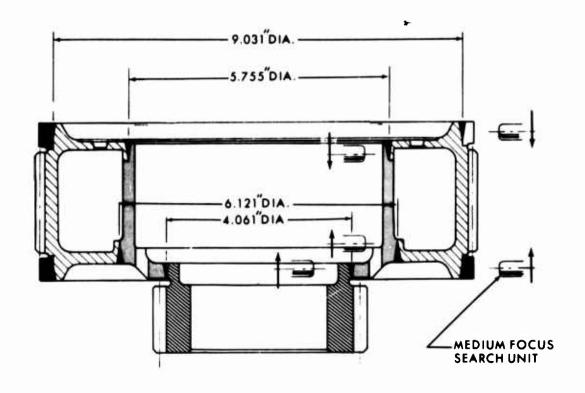


Figure 130. First-Row Pinion - Ultrasonic Inspection.



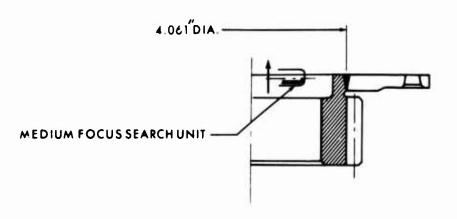


Figure 131. Second-Row Pinion - Ultrasonic Inspection.

The start position of scanning shall be indicated on the C-scan and marked on the gear with the direction of rotation.

A C-scan recording shall be made each time the calibration standard is run.

The production parts shall be run under the same conditions as the calibration standard, and a C-scan shall be made for each weld.

The C-scan shall be positively identified with the serial number of the production part and the appropriate weld.

All C-scans of the butt weld RG351-11182 shall be of a scale equal to twice the actual weld diameter (i.e., the C-scan weld outside diameter shall be 3.4 inch).

All C-scans of the diametral welds shall be recorded on an 8-inch-diameter drum.

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