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TRACE TRAJECTORY ANALYSIS AND ORBIT
DETERMINATION PROGRAM. VOLUME VII.
USER'S GUIDE, PART B: APPENDICES
(REISSUE B)

Willard D. Downs, III, et al

Aerospace Corporation

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The TRACE Trajectory Analysis and Orbit Determination Program is a general-purpose orbital analysis program. It was written and continues to be developed specifically to assist technical personnel in the analysis and design of satellite orbits and tracking systems. Volume VII is intended to serve as an input usage guide that defines all input required to perform TRACE functions such as trajectory generation, data/observation generation, orbit determination, and statistical analysis. A comprehensive		

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Sequential Batch
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description for each specific input item is given, and input data structures are shown. The Usage Guide is published in two parts, A and B.

The TRACE documentation series is summarized as follows:

Volume I: General Program Objectives, Description, and Summary
Volume II: Coordinate and Timekeeping Systems with Associated Transformations
Volume III: Trajectory Generation Equations and Methods
Volume IV: Measurement Data Generation and Observational Measurement Partial
Volume V: Differential Correction Procedure and Techniques
Volume VI: Orbital Statistics via Covariance Analysis
Volume VII: Usage Guide, Parts A and B
Volume VIII: Not to be published
Volume IX: Detailed Program Structure
Volume X: Lunar Gravity Analysis
Volume XI: LGA Data Processor
Volume XII: Sequential Least Squares Procedures and Techniques

PREFACE

Certain volumes of the TRACE documentation series were published by The Aerospace Corporation as Technical Operating Reports. Volume III: Trajectory Generation Equations and Methods was published as TOR-0066(9320)-2, Vol. III, and Volume V: Differential Correction Procedure and Techniques was published as TOR-0066(9320)-2, Vol. V.

Volume I: General Program Objectives, Description, and Summary was published as TR-0059(9320)-1, Vol. I, and Volume X: Lunar Gravity Analysis was published as TR-0059(9320)-1, Vol. X. Future volumes in this series will be published as Technical Reports.

This report is published in two parts, A and B.

The TRACE Program could not have been developed to its present status without the assistance of many people working in the fields of astrodynamics and software design. The authors acknowledge with gratitude and analysis and/or programming efforts of A. B. Bierman, R. J. Farrar, W. A. Feess, E. H. Fletcher, R. B. Freund, T. P. Gabbard, C. G. Gibson, P. T. Gray, P. T. Guttman, J. A. Pearson, C. M. Price, W. F. Rearick, N. W. Rhodus, A. J. Rusick, L. J. Tedeschi, L. Wong, and K. R. Young. In addition, consultations with W. T. Kyner, A. Troesch, and H. H. Wertz have led to many significant improvements and added capabilities in the program.

This report supersedes the appendices to TR-0059(9320)-1, Vol. VII, 30 June 1971. *NR at DDC*

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APPENDIX A

DESCRIPTION OF THE GENERAL-PURPOSE INPUT ROUTINE GAIL1

A. 1 FUNCTION AND CAPABILITIES

A. 1. 1 Purpose and Description

The purpose of GAIL1* is to read a set of Hollerith punched data and/or header cards into core with one FORTRAN call statement. To achieve this, the data fields are converted to binary, while the header information is stored in Hollerith code; each piece of the data is converted and stored according to a specific conversion code. These data may be integers, real variables, arrays, alphanumeric data (short or long headers), matrices, or end-of-case indications.

The data cards can be printed as received, or they can be placed on a scratch I/O device and then listed when an end of file (EOF) is detected on the input file.

The subroutine will always return control to the driver program except in the case of tape errors, system malfunctions, or completely erroneous punched data cards that disobey all FORTRAN I/O format rules. Therefore, the user must supply and test a status cell after an exit from the subroutine to determine which of the following occurred:

- Normal end of case
- Some type of error
- End of file reached on the input device

* GAIL1 was originally developed by R. B. Gladson of The Aerospace Corporation for the CDC 6000 computer series. It has been modified for IBM 360 and 370 computer series.

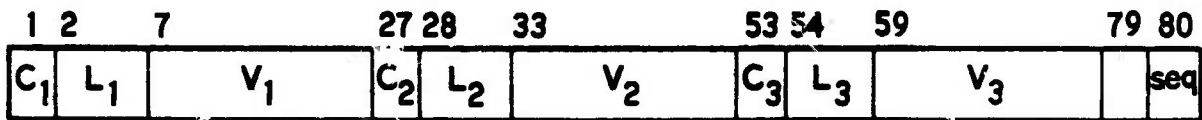
A. 1. 2 Method

All data fields are converted according to FORTRAN I/O format specifications. Real variables are converted by the F specification, whether or not the exponent (E or D) is included with the variable. Integers are converted by the I format, and alphanumeric data by the A format. This allows for alternate methods of entering real variables and integers from the FORTRAN standards. This variety of methods (Sec. A. 1. 3. 7) enables the user to enter numbers in a manner more reasonable and mathematical than did previous input routines.

A. 1. 3 Usage

A. 1. 3. 1 Data Card Format

The data card format consists of three fields, each containing three subfields; a conversion code; a location; and a value (as in the following example):

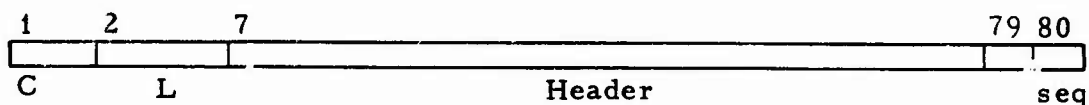


Subfield	Data Field 1	Data Field 2	Data Field 3
Conversion Code (C _i)	1	27	53
Location (L _i)	2-6	28-32	54-58
Value (V _i)	7-26	33-52	59-78

Columns 79 and 80 are not processed by the routine and can be used for card sequencing if the user desires. The conversion code (C_i) is one of the alphabetic characters (Sec. A. 1. 3. 7); it specifies the type of conversion to be used on the value field. The location subfield specifies the cell in which the converted value subfield is to be stored.

A. 1. 3. 2 Header Card Format

The header card format consists of a conversion code in Column 1, a sequence number in Columns 2 through 6, and any Hollerith information in Columns 7 through 78. Columns 79 and 80 are not used.



A. 1. 3. 3 Decimal Points

The use of a decimal point is valid in both integer and real variable entries; however, it is not mandatory to enter one. If the decimal point is missing from an entry, it is assumed to be at the right of the last digit punched in the value field; for example:

$$321. = 321 = 321E0$$

A. 1. 3. 4 Signs

If signs (+ or -) are used, they are placed in a column by themselves and immediately precede the value. Overpunches are not valid; e. g. :

1	2	7	
27	28	33	
53	54	59	
C	LOCATION	VALUE	
		+7.1621	

Valid

1	2	7	
27	28	33	
53	54	59	
C	LOCATION	VALUE	
		7.1621	

Invalid

A. 1. 3. 5 Values (V_i Subfield)

It is not necessary for the entire subfield to be filled, since the first blank following the first nonblank denotes the end of the value. Superfluous low-order zeros should be omitted.

If alphanumeric information is entered, it is stored in core as it appears in the value subfield. Thus, for this type of data entry, leading blanks are retained. If they appear, the blanks themselves are also stored in core.

A. 1. 3. 6 Location (L_i Subfield)

The location is specified by either a variable, an array name, or the element subscripts in a single-dimension array or matrix.

A. 1. 3. 6. 1 Variable, Array, or Matrix Name

If the location contains at least one nonnumeric character that is not a comma as the third character, it is interpreted as a variable, array, or matrix name. The contents of the value subfield are stored in the cell for the variable or in the first cell of the array or matrix. This location then becomes the origin of all numeric and matrix element locations that follow until another variable, array, or matrix name is encountered. Care must be taken to enter an array or matrix name before entering numeric or matrix element locations.

A.1.3.6.2 Single Numeric Entry

If a location contains a single numeric value, the entry is treated as a subscript. With its previously established origin, this subscript is used to compute the location in which the entry in the value subfield is stored. For instance, if the established origin is NAME and the value in the location subfield of the input is 6, the entry in the value subfield is stored in cell NAME(6). (Single numeric entries must be left-justified, and leading zeros are optional.) In the following example,

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	NAME	3,716
	6	6,173

legitimate numeric entries would be shown as:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	5	
	12	
	03	

and illegitimate numeric entries would be shown as:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	1	
	30① 1	
	① 1	

- Not a valid subscript.
- Store as 30.
- Not recognized as a relative address; it is flagged as an error.

The symbol ① indicates 1 space between digits, and ② indicates n spaces.

A. 1.3.6.3 Matrix Element Entry

A matrix element is stored by specifying two separate two-digit numeric entries, separated by a comma, in the location subfield. For example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
	03, 04	-3.17

-3.17 goes to element (3,4) of the matrix

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
	15, 01	+7.38

+7.38 goes to element (15,1) of the matrix

The elements are stored in the column major sort by using the formula

$$\text{ORIGIN}((j - 1)I + i)$$

where I is the total number of rows in the matrix and (i, j) is the element in question.

A. 1.3.6.4 Blank Location

If the location is left blank, the entry in the value subfield is stored in the cell immediately following the one in which the last value was stored.

Thus, an entire array may be entered by using a name in the location subfield for the initial entry and leaving location subfields blank for the subsequent value subfield entries. The following is an example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
	XYZ	4.0
		5.1
		6.2

4.0 stored in XYZ(1)
5.1 stored in XYZ(2)
6.2 stored in XYZ(3)

A. 1. 3. 7 Conversion Code (C_i Subfield)

The entry in the conversion code subfield specifies the method of converting the data in the value subfield. Care should be taken to apply the proper code with each item of data; if the proper code is not applied, a premature termination will occur in a FORTRAN format statement. The eight conversion codes currently available are described in the following subsections.

A. 1. 3. 7. 1 Blank: Real Variable

The number in the value subfield is converted to and stored as a real variable. Entries can be made to the value subfield by any of four methods: Three of them are in the normal FORTRAN E, D, and F types of real variable input formats, e. g. :

C	LOCATION	VALUE	
		3.615	= 3.615
		.3615E01	= 3.615
		3615E-03	= 3.615
		3615D-03	= 3.615
		.3615D01	= 3.615

The fourth method allows for the input of real variables in scientific nomenclature ($a \times 10^b$). The number is written in the value subfield and is followed by an X, then by a 10, and then by the power of ten to which the number is to be scaled (a sign must precede the exponent). Some examples follow:

- $14200 = 1.4200 \times 10^4$ is input as

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		1.4200X10+4

or, in the normal mode, as

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		14200

or as

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		1.4200E4

- $.00762 = .762 \times 10^{-2}$ is input as

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		.762X10-2

A. 1.3.7.2 I: Integer

The number in the value subfield is converted to a fixed-point integer. A decimal point is allowable; if it is used, only the integer portion is converted. Before the value is converted by the FORTRAN I format, the decimal point and any digit(s) to the right are stripped off; e. g.:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
I		71.35

is stored as 71.

A. 1.3.7.3 D: Short Header (20 Characters)

The contents of the value subfield are interpreted as 20 alphanumeric characters. They are stored in two consecutive cells in ascending order, beginning at the location specified by the location subfield. The characters are stored in the same relative positions as in the value subfield; thus, leading, trailing, and embedded blanks are legitimate. For example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
D		ABC①DEF②GHIJ④234

is stored in two consecutive words, with ABC①DEF②G in the first word, and HIJ④234 in the second.

A. 1.3.7.4 H: Long Header (72 Characters)

A card with an H in Column 1 is considered a long header card. If the location subfield is blank, the card is ignored (treated as a comments card). If the location subfield contains a left-justified integer 1, Columns 7 through 78 of the card are stored directly in seven consecutive words in ascending core storage.

The H conversion code is the only one for which a numeric location subfield is mandatory. If the location subfield is not blank or the integer 1, the header is not stored, an error comment is printed, and the error termination procedure is invoked.

A. 1. 3. 7. 5 L: Sparse Matrix Input Definition

This input specifies only that matrix elements may be following, either on the same and/or on subsequent cards. It does not store any items of data; it only warns the subroutine that matrix elements might be stored and indicates where. The location subfield must contain the name of the matrix in which the items are to be located in core.

The value subfield must contain two-digit integers separated by a comma. The entries are the size of the matrix [I_{max} and J_{max}], and the comma must be the third character of the subfield. If it is not, an error comment is printed, and an error flag set.

The I_{max} and J_{max} values are retained to compute the successive subscripted locations of the matrix elements until they are redefined. Blank location subfields may follow this definition if successive elements of the matrix are to be loaded. It must be remembered that the matrix is stored in column major. For example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
L	GØØD	03, 07

indicates that a 3×7 matrix GØØD is being defined and that following data values are to be stored in GØØD until another symbolic location name is encountered. Storage is to be made according to $GØØD((j - 1)I + i)$.

A. 1.3.7.6 M: Full Matrix Input Definition

The use of this conversion code is identical to that of L, except that the entire matrix is preset to zero before any of the elements are loaded.

For example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
M	GØØD	03,07

presets the 3×7 matrix GØØD to zero; it is prepared to store the matrix elements following it until another symbolic location name is encountered.

A. 1.3.7.7 B: Octal

The value subfield is converted as a logical word. It is not necessary to include leading zeros, but the first octal digit must always occupy the left-most position in the subfield. If fewer than 20 digits are input, the value will be right-justified in the memory location. For example:

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
B		123

is stored as 00000000000000000123₈ in core.

A. 1.3.7.8 E: End of Case

This defines the end of case, when control is returned to the object program from which it was called. The rest of the subfield and the remaining fields on the card are ignored.

A. 2 ERROR COMMENTS

The input errors that the subroutine can recognize are listed in Table A-1. In each case, an appropriate error comment is printed, the remaining cards in the data set are scanned until an E conversion code is found, and the run is terminated. The errors are not listed in any specific order.

Table A-1. Errors Recognizable by Input Subroutine

Error Message	Type of Input Error
<p>HEADER CARD NO. EXCEEDS MAXIMUM NO. ALLOWABLE.</p> <p style="text-align: center;">← Card Image (80 Characters) →</p>	<p>If the location subfield is not blank or the integer 1, the card is not stored; it is printed as shown, and the error termination procedure takes over.</p>
<p>ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FROM BLANK LOCATION FIELD. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.</p> <p style="text-align: center;">← Field in Error →</p>	<p>The first value input had a blank location subfield, and no symbolic origin had been established.</p>
<p>ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FOR A MATRIX ELEMENT. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.</p> <p style="text-align: center;">← Field in Error →</p>	<p>A matrix element is to be stored, but no location definition of the matrix has been made by a previous M or L card.</p>
<p>MATRIX SIZE UNDEFINED.</p> <p style="text-align: center;">← Field in Error →</p>	<p>A matrix element is to be stored, but no size definition of the matrix has been made by a previous M or L card.</p>
<p>ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FOR NUMERIC LOCATION FIELD. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.</p> <p style="text-align: center;">← Field in Error →</p>	<p>The first value input had a numeric location subfield. No symbolic origin had been established before this point.</p>
<p>UNDEFINED SYMBOL USED IN LOCATION FIELD.</p> <p style="text-align: center;">← Field in Error →</p>	<p>A symbol not previously defined was used in the location subfield.</p>
<p>MISPLACING COMMA IN MATRIX DEFINITION.</p> <p style="text-align: center;">← Field in Error →</p>	<p>During an attempt to define a matrix (M or L conversion code), the third character in the value subfield was not a comma.</p>
<p>ILLEGAL CONVERSION CODE.</p> <p style="text-align: center;">← Field in Error →</p>	<p>An undefined conversion code was entered.</p>
<p>INVALID CHARACTER IN VALUE FIELD.</p> <p style="text-align: center;">← Field in Error →</p>	<p>There is an invalid character in the value field.</p>

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APPENDIX B

TRACE DATA DECK STRUCTURE EXAMPLES

B.1 ORBIT DETERMINATION RUN (ITIN=2)

B.1.1 Single-Vehicle with OBSERVATION Card Input

The deck setup for an orbit determination run for one vehicle is shown in Fig. B-1. All observational measurements are input in the OBSERVATION block.

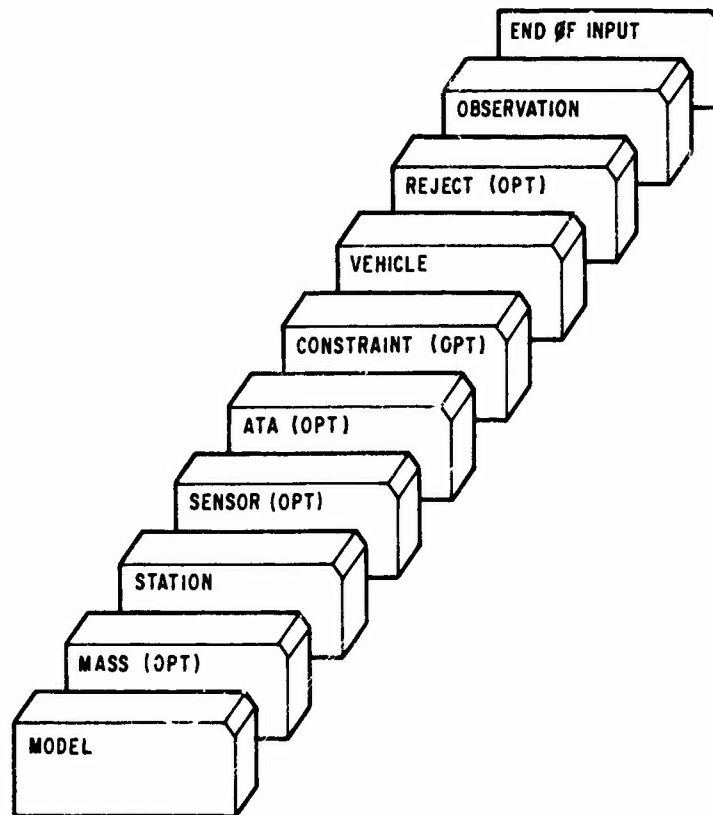


Fig. B-1. Deck Setup for a Single-Vehicle Orbit Determination Run with OBSERVATION Card Input

B.1.2 Multiple-Arc with OBSERVATION Card Input

The deck setup for an orbit determination of more than one vehicle in which measurements from the many vehicles are used (but each observation is associated with only one vehicle) is shown in Fig. B-2. In this case, only one model group (MODEL, MASS, STATION, SENSOR, ATA, and CONSTRAINT data blocks) is input; it is followed by the VEHICLE blocks for all vehicles, and then by pairs of REJECT and OBSERVATION blocks for each vehicle.

Each OBSERVATION card should have a vehicle number (Sec. 15), and VEHID and BTIME are required in each VEHICLE block. For convenience, in the VEHICLE block, the input data not overridden carries over from one vehicle to the next (characteristic of GAIL1 input).

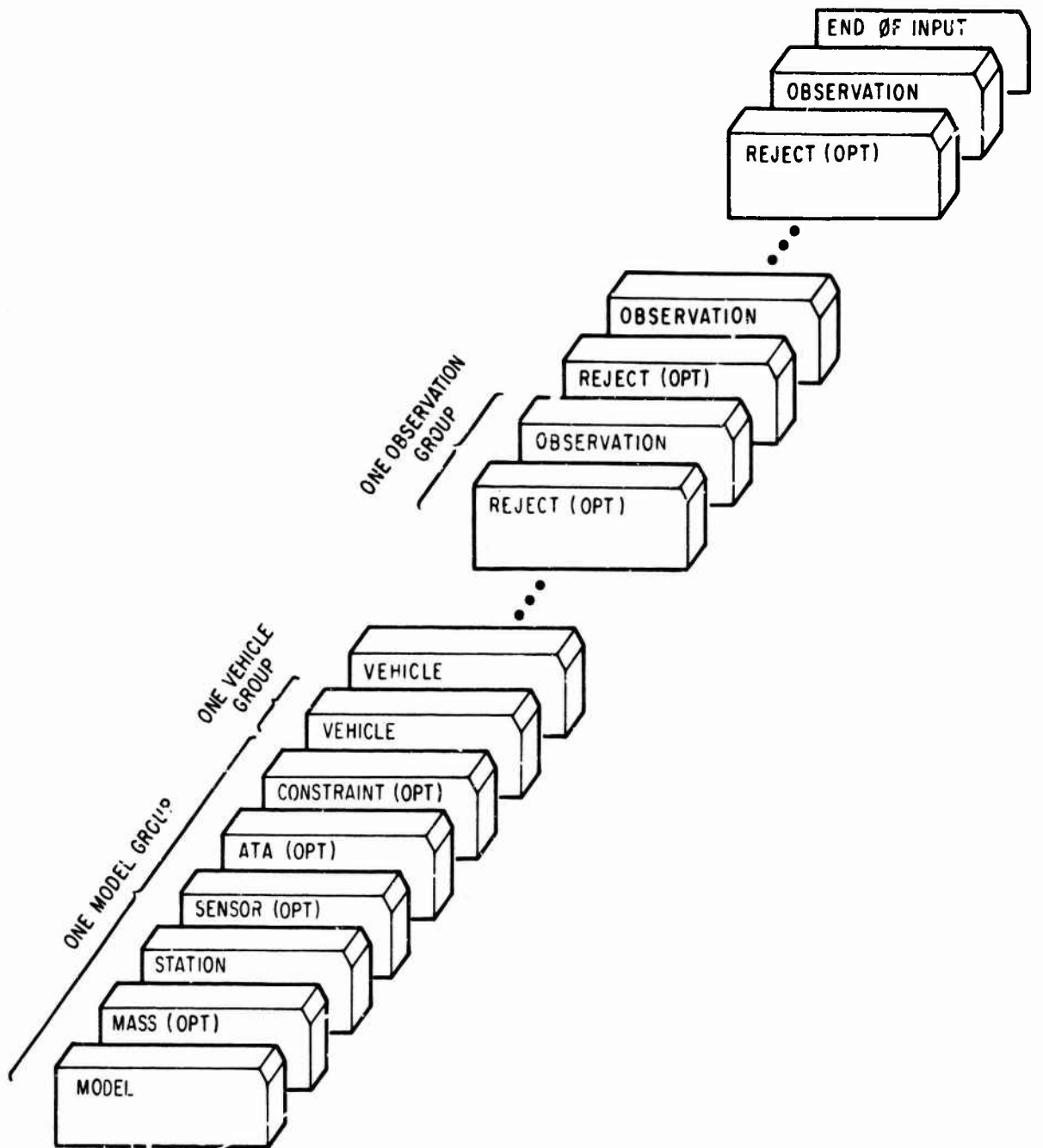


Fig. B-2. Deck Setup for a Multiple-Arc Orbit Determination Run with OBSERVATION Card Input

B.1.3 Single-Vehicle with Card Image Observation File Input

The deck setup for an orbit determination run for one vehicle, using observational measurements found on a card image observation file (TAPE4) is shown in Fig. B-3. This setup is indicated by the input item BCDIN#0 (Sec. 11.2.1) in the VEHICLE data block and the fact that the OBSERVATION card is followed by the END OF INPUT card.

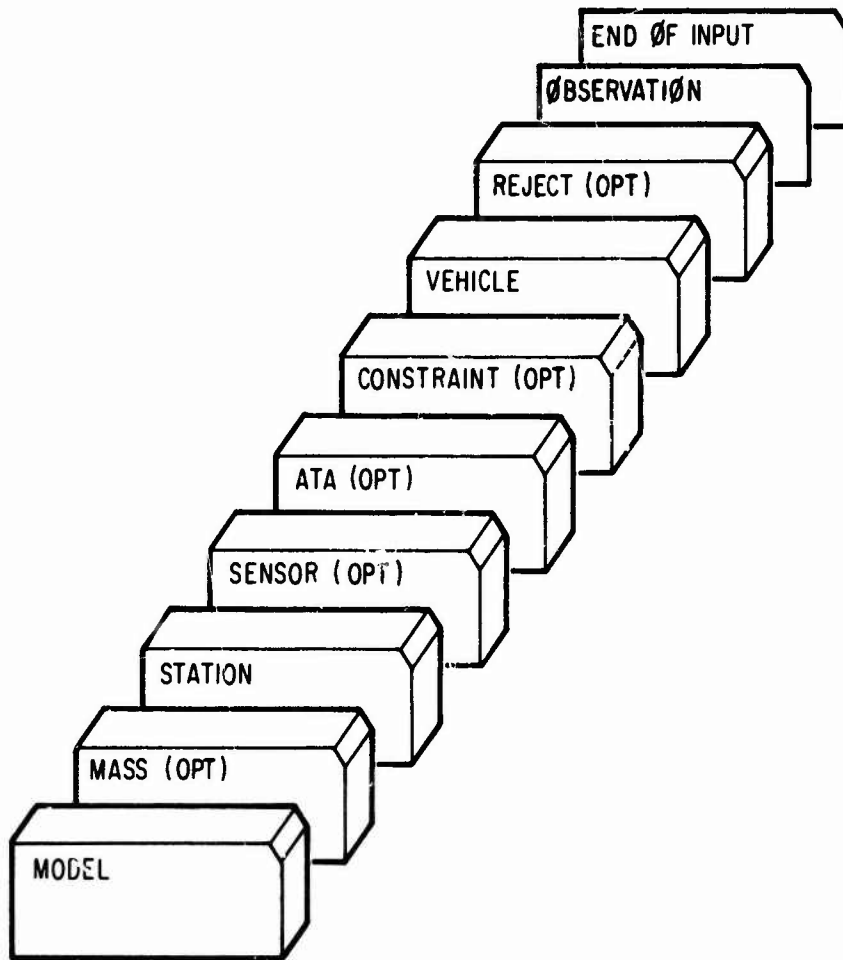


Fig. B-3. Deck Setup for a Single-Vehicle Orbit Determination Run with Card Image Observation File Input

B.1.4 Multiple-Arc with Card Image Observation File Input

In an orbit determination run with observational measurements from several vehicles (each item of data is associated with only one vehicle), the data deck requires only one set of model group data blocks (Fig. B-4). For each vehicle there must be a VEHICLE block followed by the pairs of REJECT and OBSERVATION blocks.

In the VEHICLE block, input data not overridden will carry over from one vehicle to the next. BTIME is required in each VEHICLE block to show the last integration time (more than likely, the last observation time). VEHIID, which should match the vehicle number on the observation card images for that vehicle, is also required.

For this case, observations are input by the card image observation file (TAPE4). This is indicated by BCDIN≠0 (Sec. 11.2.1) and by a single OBSERVATION card for each vehicle.

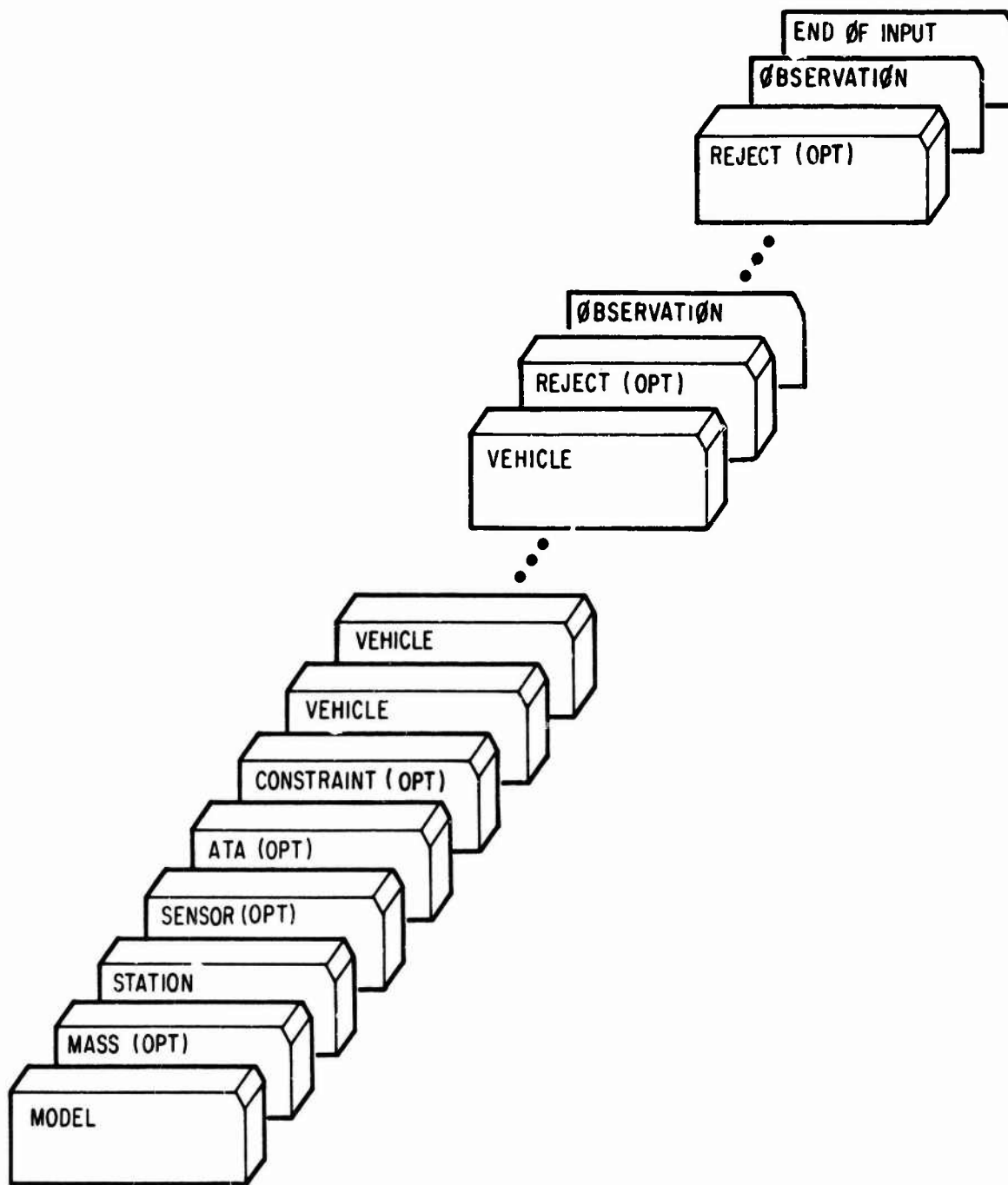


Fig. B-4. Deck Setup for a Multiple-Arc Orbit Determination Run with Card Image Observation File Input

B.1.5 Single-Vehicle Differential Correction with Binary Observation File Input

Orbit determination for one vehicle with an input binary observation file (TAPE3) requires one model group of input data blocks and the VEHICLE block only from the vehicle group (Fig. B-5). The input item BTIME (Sec. 11.2.1) in the VEHICLE block contains the last observation time (or a later time) on the file. This time is considered in determining the final integration time. Note that no REJECT or OBSERVATION data blocks are allowed when a binary observation file is used.

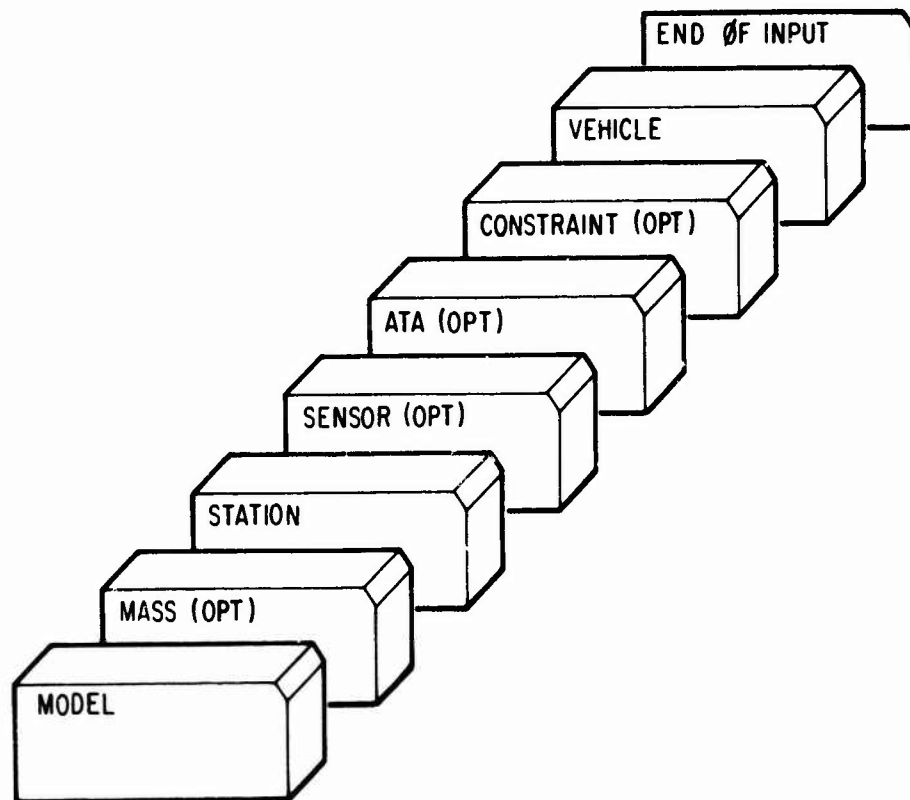


Fig. B-5. Deck Setup for a Single-Vehicle Differential Correction Run with Binary Observation File Input

B.1.6 Multiple-Arc with Binary Observation File Input

The deck setup for a multiple-arc orbit determination run with binary file observation input is shown in Fig. B-6. Observational measurements from many vehicles are used, but each item of data is associated with only one vehicle. One model group is input, and one VEHICLE block per vehicle is input. Each VEHICLE block contains the input item BTIME (Sec. 11.2.1), which indicates the last observation time (or a later time) on the binary observation file (TAPE3) for this vehicle. These times are considered in determining the final integration time for each vehicle.

Since all vehicles are assumed to be independent, a complete set of appropriate VEHICLE data should be provided for each. Input data not overridden is carried from one vehicle to the next. Again, note that no REJECT or OBSERVATION data blocks are allowed when a binary observation file is used.

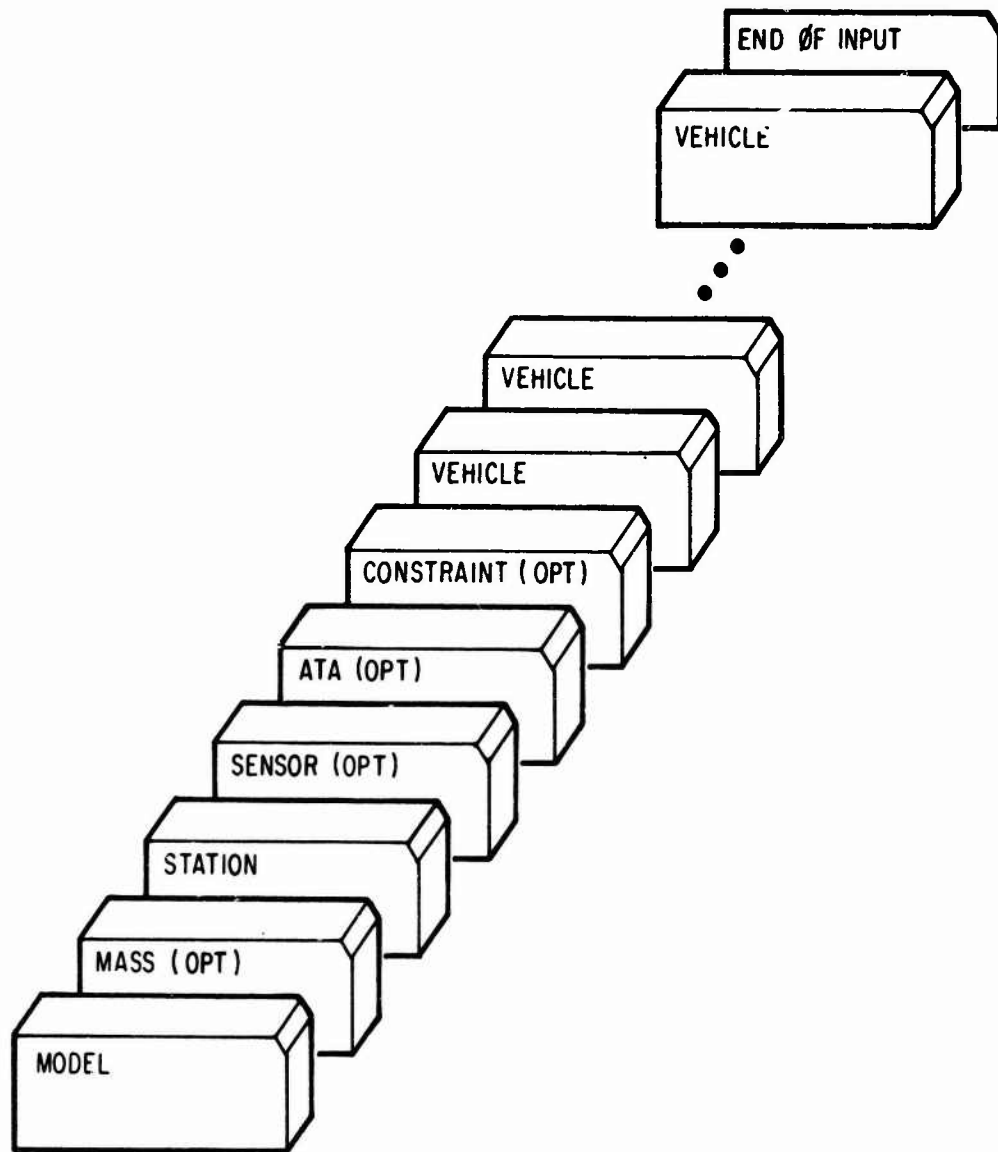


Fig. B-6. Deck Setup for a Multiple-Arc Orbit Determination Run with Binary Observation File Input

B.2 EPHEMERIS GENERATION RUN (ITIN=3)

B.2.1 Single-Vehicle

The deck setup for a single-vehicle ephemeris generation run (Fig. B-7) consists of the following: the MODEL and the (optional) MASS data blocks from the model group and the VEHICLE block. The VEHICLE block must contain the input item PTIM (Sec. 11.3.1.1), which indicates the print times and the final integration time.

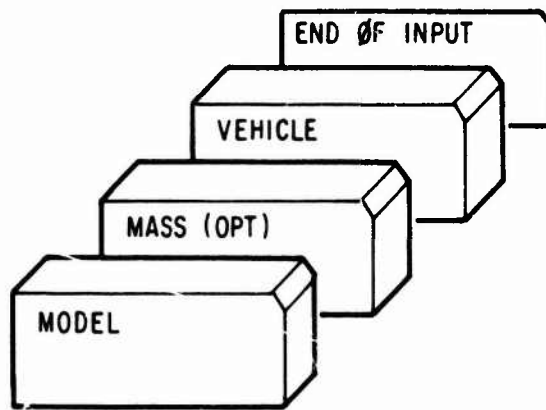


Fig. B-7. Deck Setup for a Single-Vehicle Ephemeris Generation Run

B.2.2 Multiple-Arc

The deck setup for an ephemeris generation run with several vehicles (Fig. B-8) consists of one set of MODEL and the (optional) MASS data blocks and one block of VEHICLE data per vehicle. The input item PTIM (Sec. 11.3.1.1) is specified in each VEHICLE block to indicate the print times and the final integration time for each vehicle. In the VEHICLE block, input data not overridden is carried over from one vehicle to the next.

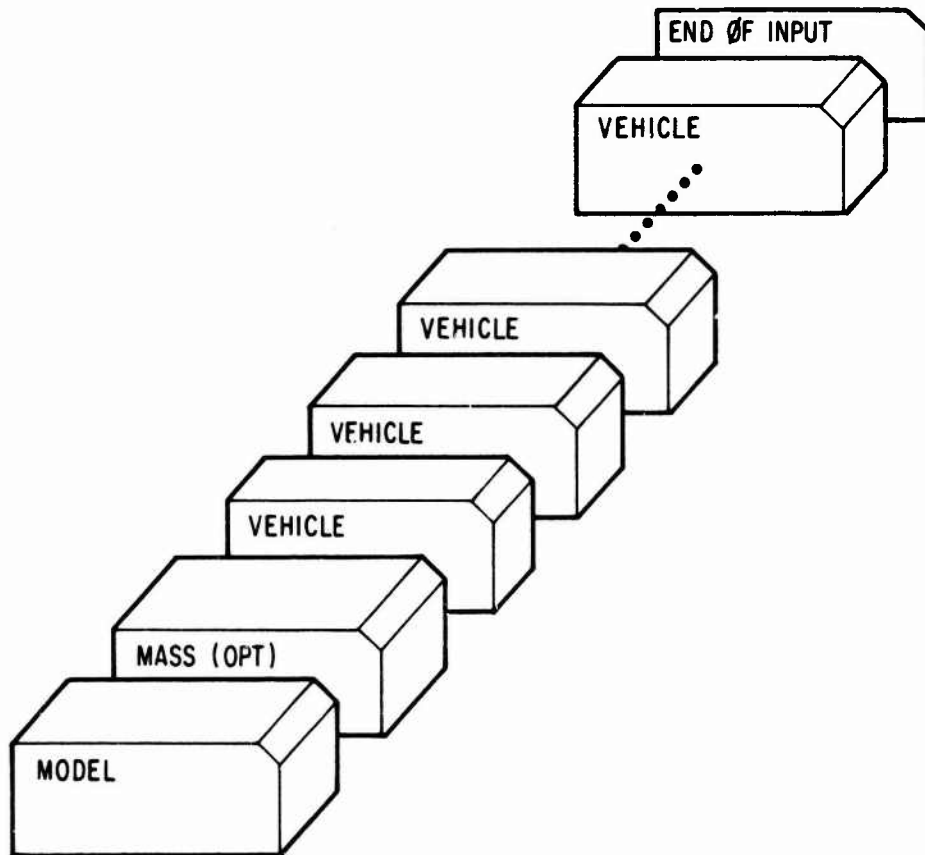


Fig. B-8. Deck Setup for a Multiple-Arc Ephemeris Generation Run

B.3 MEASUREMENT DATA GENERATION RUN (ITIN=4)

B.3.1 Single-Vehicle

The deck setup for a single-vehicle measurement data generation run (ITIN=4) requires one set each of the model and vehicle groups of input data blocks, including MODEL, STATION, VEHICLE, DATA GENERATION, and the optional MASS and SENSOR blocks (Fig. B-9).

The DATA GENERATION input block includes both DATA GENERATION I and II cards (Sec. 12) unless the VEHICLE block contains the input item JRIST=1 (Sec. 11.4.1). In this case, the DATA GENERATION II cards are omitted.

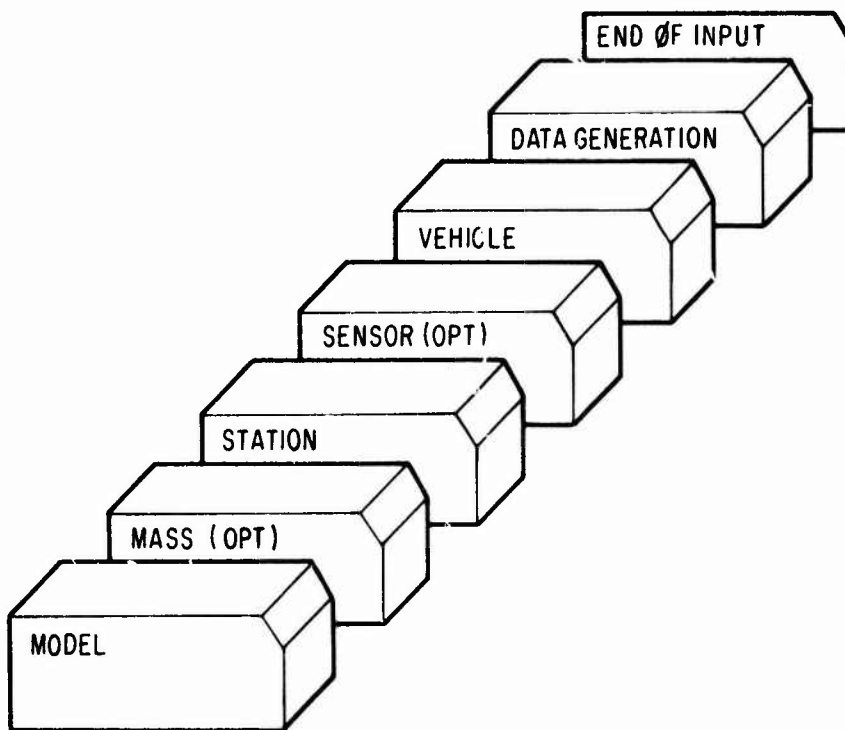


Fig. B-9. Deck Setup for a Single-Vehicle Data Generation Run

B.3.2 Multiple-Arc

The multiple-arc data generation deck (Fig. B-10) contains one set of model group data blocks and one set per vehicle of the vehicle group data blocks (VEHICLE and DATA GENERATION cards). If the VEHICLE block contains the input item JRIST=1 (Sec. 11.4.1), the DATA GENERATION II cards are omitted from the DATA GENERATION data block (Sec. 12).

Note that all vehicles are assumed to be independent; therefore, a complete set of VEHICLE and DATA GENERATION blocks should be provided for each vehicle. For convenience, in the VEHICLE block, input data not overridden is carried over from one vehicle to the next.

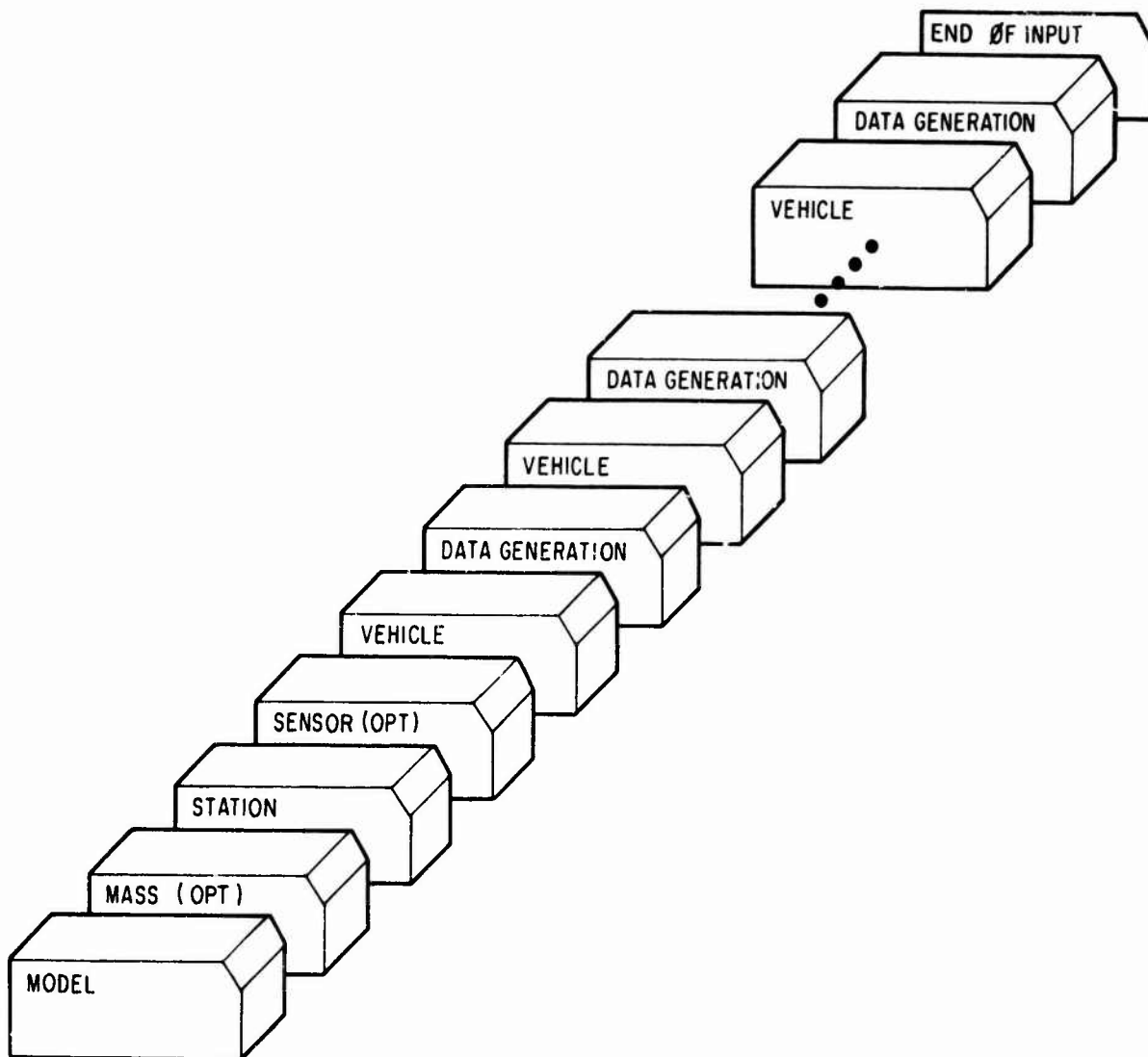


Fig. B-10. Deck Setup for a Multiple-Arc Data Generation Run

B.4 COVARIANCE ANALYSIS RUN (ITIN=5)

Deck setups for single-vehicle covariance analysis runs always contain the same basic model groups of input data blocks (MODEL, MASS, STATION, SENSOR, ATA, and COVQ), whereas the vehicle data blocks (VEHICLE and DATA GENERATION) and observation data blocks (REJECT and OBSERVATION) are variable. Various deck setups for covariance runs are shown in Figs. B-11 through B-15.

Input/output options are specified in the MODEL data block by input items $\emptyset\text{PB}\emptyset\text{X}$ and $\text{PRC}\emptyset\text{V}$ (Sec. 2.5.1). The model P/Q parameter specifications are found in the input items $\emptyset\text{PRAM}$, MPRAM , and GPRAM (Sec. 2.1.5).

A priori input for the normal matrix $\text{A}^{\text{T}}\text{A}$ or the variance-covariance matrix $(\text{A}^{\text{T}}\text{A})^{-1}$ is specified in the ATA data block (Sec. 6). A priori input for Q-parameters is specified via the COVQ data block (Sec. 8).

Vehicle-dependent P- and Q-parameters and the print schedule are specified by input items VPRAM (Sec. 11.1.14) and PTIM (Sec. 11.5.1).

Observational measurement times may be specified by:

- OBSERVATION cards
- Card image observation file (TAPE4)
- Binary observation file (TAPE3)
- DATA GENERATION data block input.

When the observational measurement times are specified by card image tape or card images, measurement times may be rejected by inputs to the REJECT data block.

In case of an update to an input $\text{A}^{\text{T}}\text{A}$ or $(\text{A}^{\text{T}}\text{A})^{-1}$ matrix, no measurement times are required [$\emptyset\text{PB}\emptyset\text{X}(\text{D})$ and $\emptyset\text{PB}\emptyset\text{X}(\text{E})$, Sec. 2.5.1].

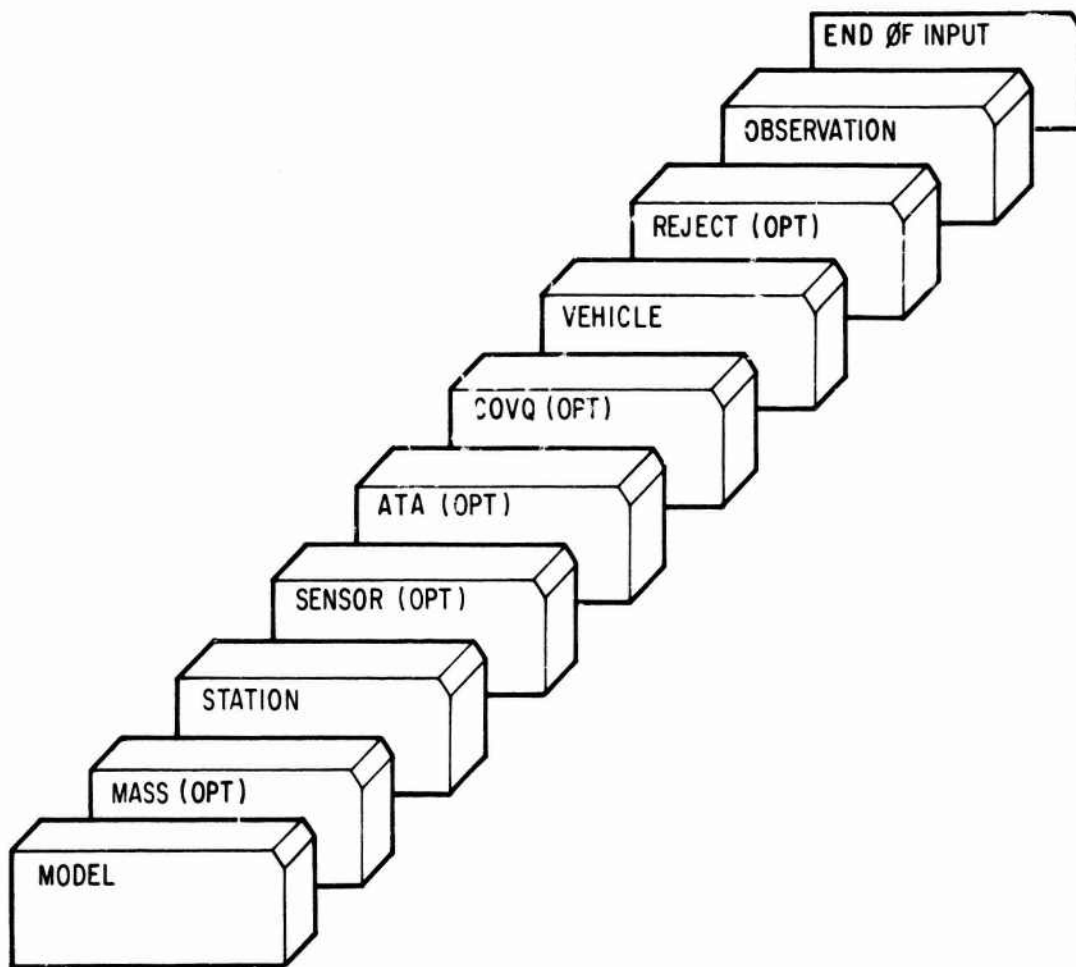


Fig. B-11. Deck Setup for a Covariance Analysis Run with OBSERVATION Card Input

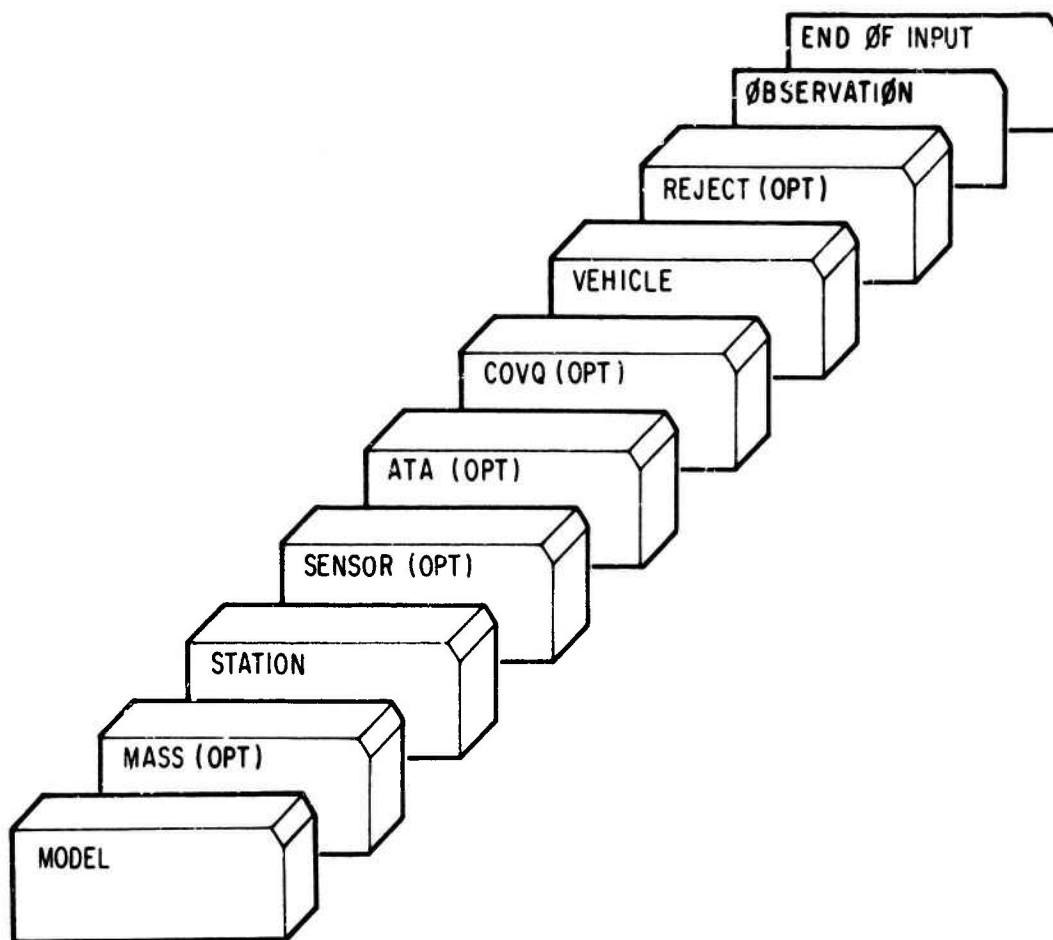


Fig. B-12. Deck Setup for a Covariance Analysis Run with Card Image Observation File Input

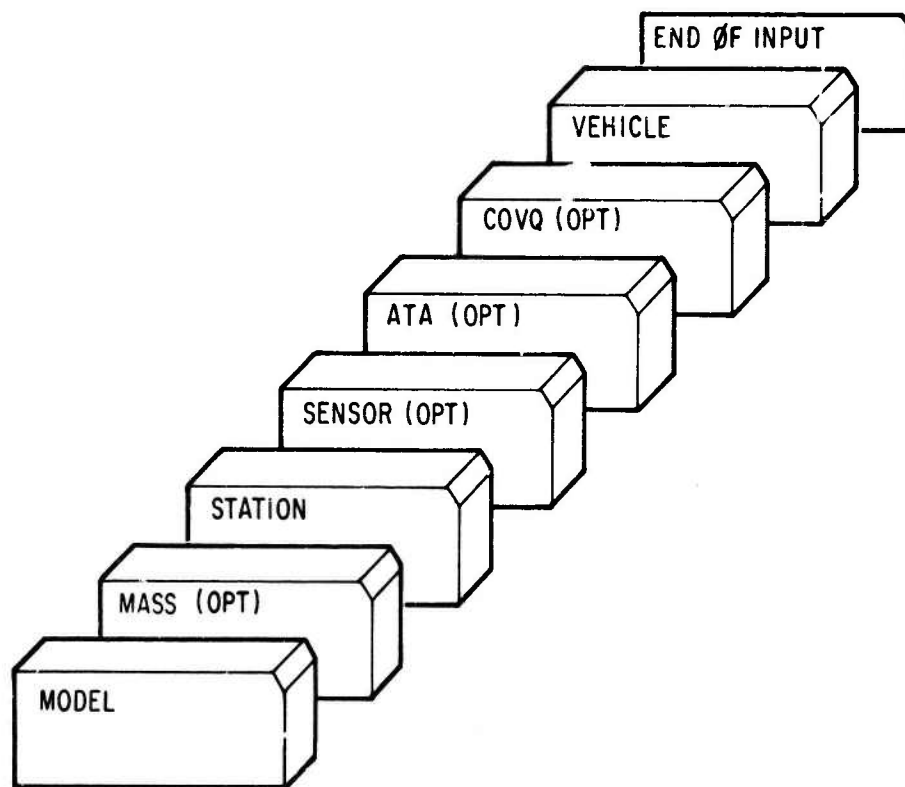


Fig. B-13. Deck Setup for a Covariance Analysis Run with Binary Observation File Input

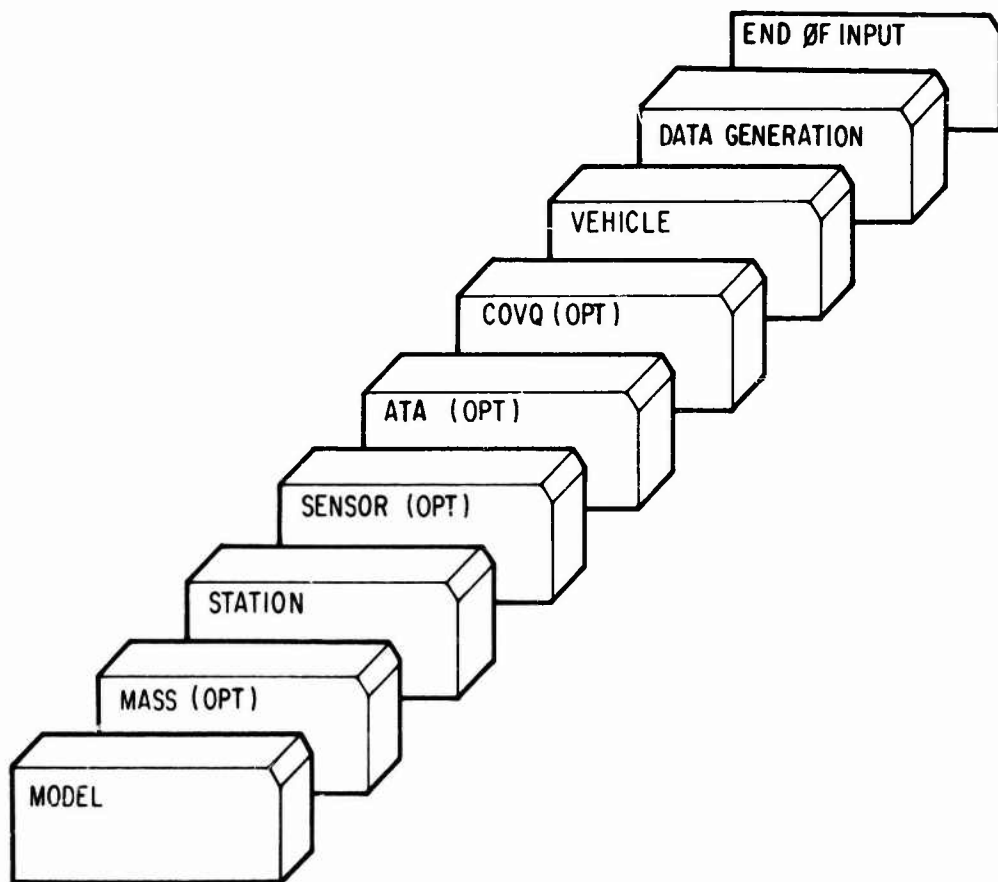


Fig. B-14. Deck Setup for a Covariance Analysis Run with Data Simulation

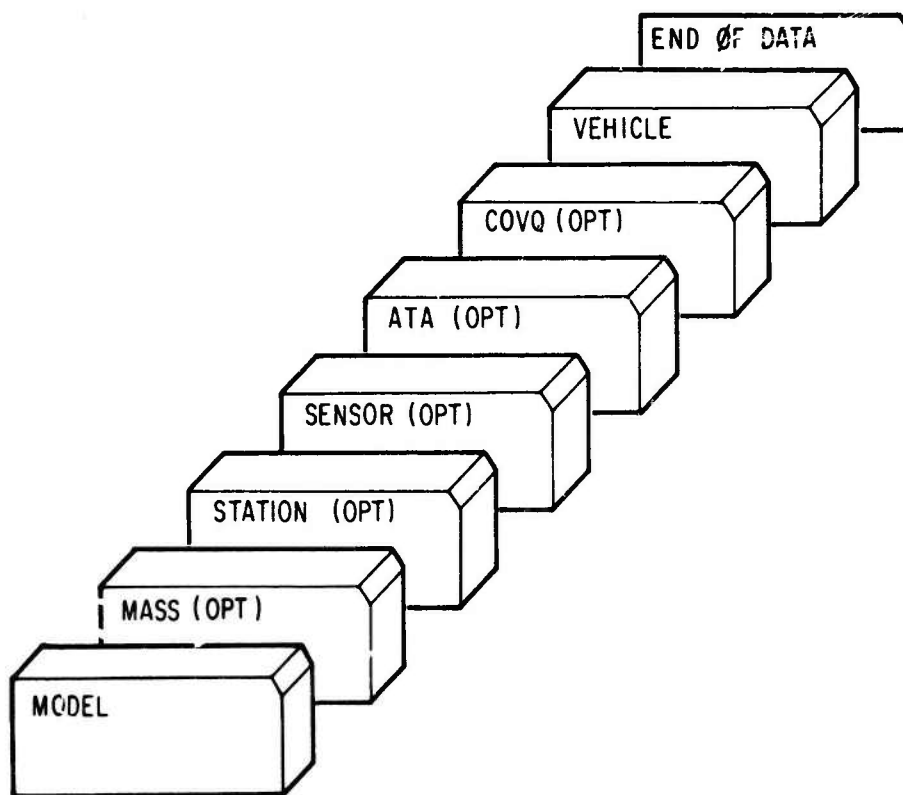


Fig. B-15. Deck Setup for a Covariance Analysis Update Only Run

B.5 MULTIPLE ITINERARY

B.5.1 Ephemeris and Data Generation (ITIN=34)

The deck setup for a case in which an ephemeris generation and a data generation are desired for the same vehicle, using the same model group blocks, is shown in Fig. B-16. Included in the MODEL and VEHICLE data blocks are all input items required for both the ephemeris generation and the data generation runs. Even though an ephemeris generation run does not require STATION, SENSOR, or DATA GENERATION input blocks, they are included in the deck setup because a data generation run does require them.

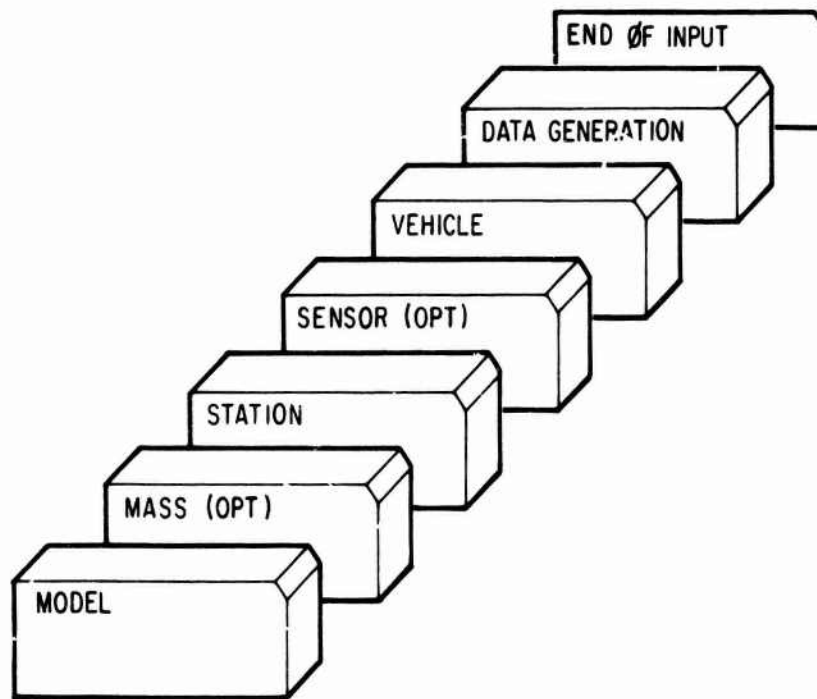


Fig. B-16. Deck Setup for a Multiple-Itinerary Run (ITIN = 34)

B.5.2 Multiple Itinerary (ITIN=3452345)

The deck setup for Example B (Sec. 1.4.1) is shown in Fig. B-17. In this case, the initial ITIN functions 3, 4, and 5 cause the generation of the nominal ephemeris, the look angles, and the covariance analysis, respectively. Reconstruction takes place starting from the nominal initial values. When the iterations terminate, the trajectory for the converged solution is used to repeat the three processing functions.

The MODEL and VEHICLE data blocks contain the necessary input items for all functions. The STATION cards are necessary for ITIN functions 2, 4, and 5. The optional ATA data block can contain $A^T A$ or $(A^T A)^{-1}$ (Sec. 6). It is used for the orbit determination and/or the covariance analysis functions. The DATA GENERATION cards are necessary to generate the look angles, and the OBSERVATION block contains the measurements used in the covariance analysis and orbit determination steps.

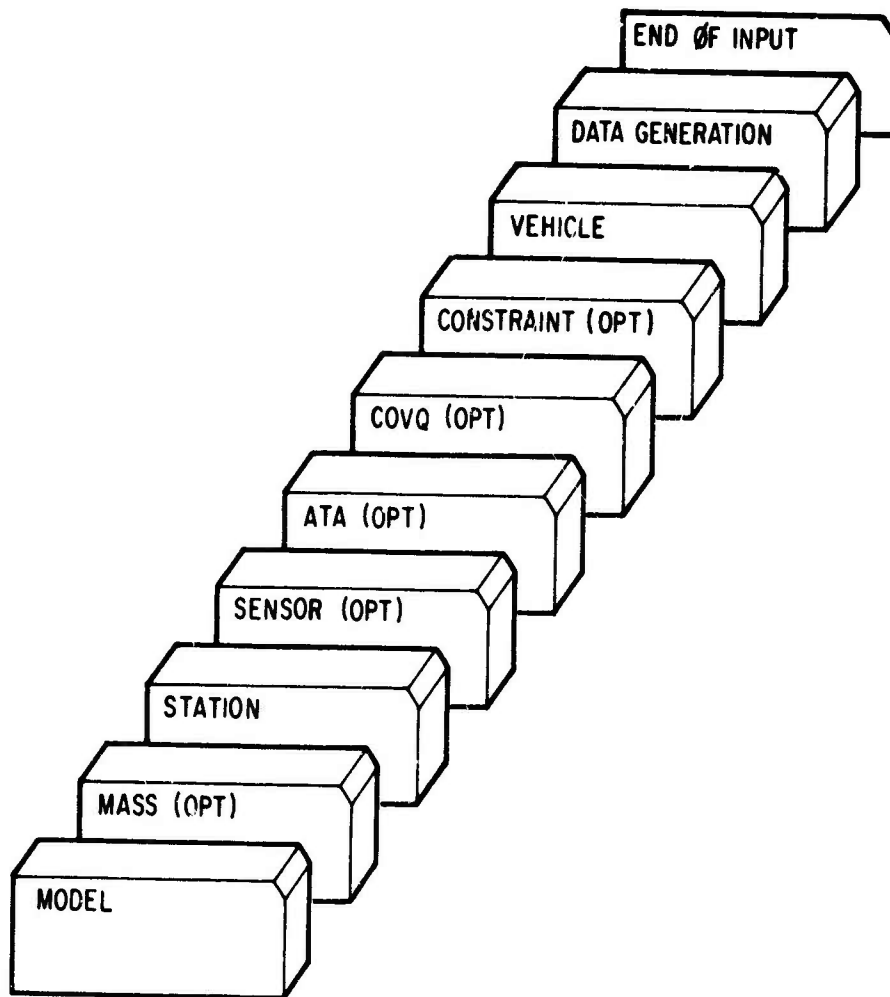


Fig. B-17. Deck Setup for a Multiple-Itinerary Run (ITIN = 3452345)

B.5.3 Multiple Itinerary (ITIN=323)

The deck setup for Example A (Sec. 1.4.1) is shown in Fig. B-18. A trajectory is generated from the input initial conditions, and an ephemeris is generated and output. Then, another trajectory is reconstructed from the observational data, and comparable ephemeris output is printed. The VEHICLE data specifies the nominal initial conditions for the trajectory, the amount of printed output, and the vehicle parameters to be differentially corrected in the reconstruction.

The observational measurements can be input by cards, card image file, or binary observation file (Sec. 11.2.1). If a card image file is used, the OBSERVATION block consists of a single card, with OBSERVATION in Columns 1 through 11. If the binary observation file is used, no REJECT or OBSERVATION data blocks are allowed.

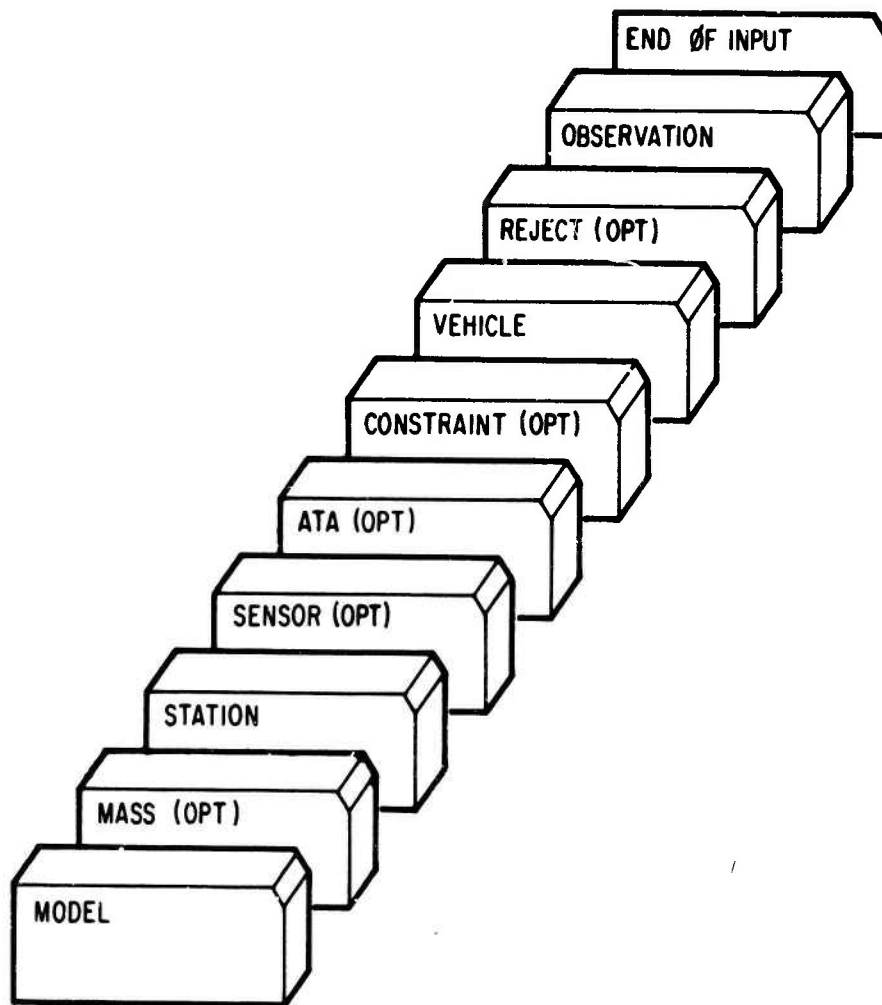


Fig. B-18. Deck Setup for a Multiple-Itinerary Run (ITIN = 323)

B.6 STACKED CASES (ITIN=34 FOLLOWED BY ITIN=2)

This data deck setup is used for Cases A and B of Appendix C (Fig. B-19). In Case A, an ephemeris is generated, and observational measurements are simulated. These measurements are written on a card image observation file (TAPE4) and are then used in the orbit determination run of Case B. Note that in the first case, from the MODEL block to the first END OF INPUT, the data block setup is as described in Secs. B.2.1 and B.3.1. The VEHICLE data also includes input item ETAPE≠0 (Sec. 11.4.1), so the observations measurements are written on the card image observation file.

The ITIN=2 function is considered an entirely new case because nothing is retained from the first case; new model, vehicle, and observation group inputs are therefore included. The STATION input must be repeated, and the OBSERVATION card must be followed by the END OF INPUT card. Input item BCDIN≠0 (Sec. 11.2.1), specified in the second VEHICLE block, indicates that the observations are on the card image observation file, and BTIME (Sec. 11.2.1) indicates the time of the last observation.

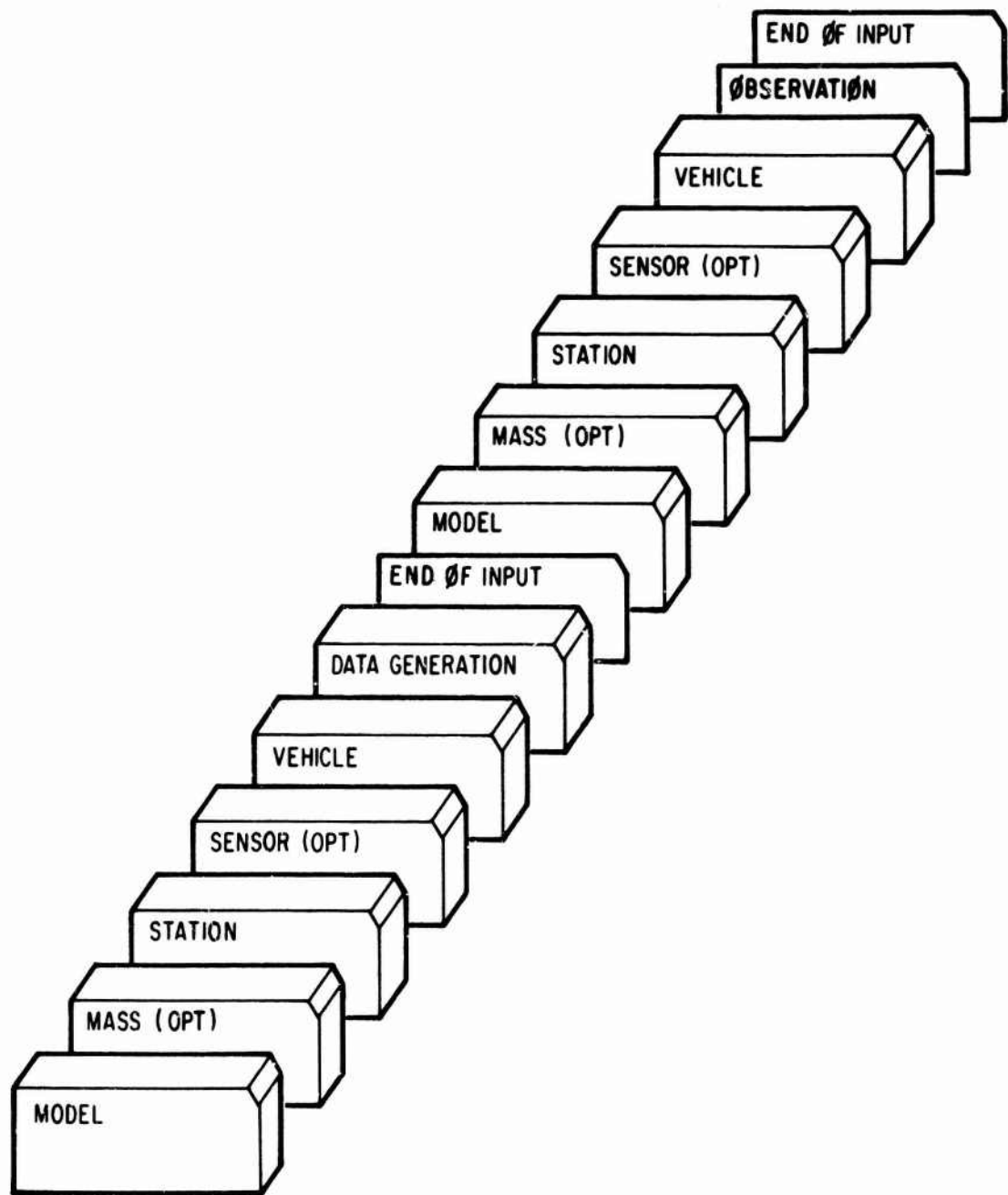


Fig. B-19. Deck Setup for Stacked Cases (ITIN = 34, ITIN = 2)

B.7 SIMULTANEOUS VEHICLES

B.7.1 Orbit Determination (ITIN=2, MULTV≠0)

The deck setup is shown (Fig. B-20) for many vehicles in simultaneous orbit that have the same model. The VEHICLE data blocks are input sequentially. Each requires a VEVID (Sec. 11.1.2) and the final integration time specified by BTIME (Sec. 11.2.1), but the integration times of the first vehicle must span those of any subsequent vehicles. Since the REJECT cards are time-dependent, not vehicle-dependent, only one block is input.

Only one OBSERVATION block, containing the measurements from all vehicles, can be input. In this case, actual OBSERVATION cards are shown. If this data were input by the card image observation file (TAPE4), the block of cards would be replaced by a single OBSERVATION card. If it were input by the binary observation file (TAPE3), there would be no REJECT or OBSERVATION data blocks.

The optional ATA block may contain an $A^T A$ or $(A^T A)^{-1}$ matrix (Sec. 6). If MULTV=2 or 3, the STAGE data block (Sec. 14) is optional, and if MULTV=2, the DEWM data block (Sec. 7) is optional.

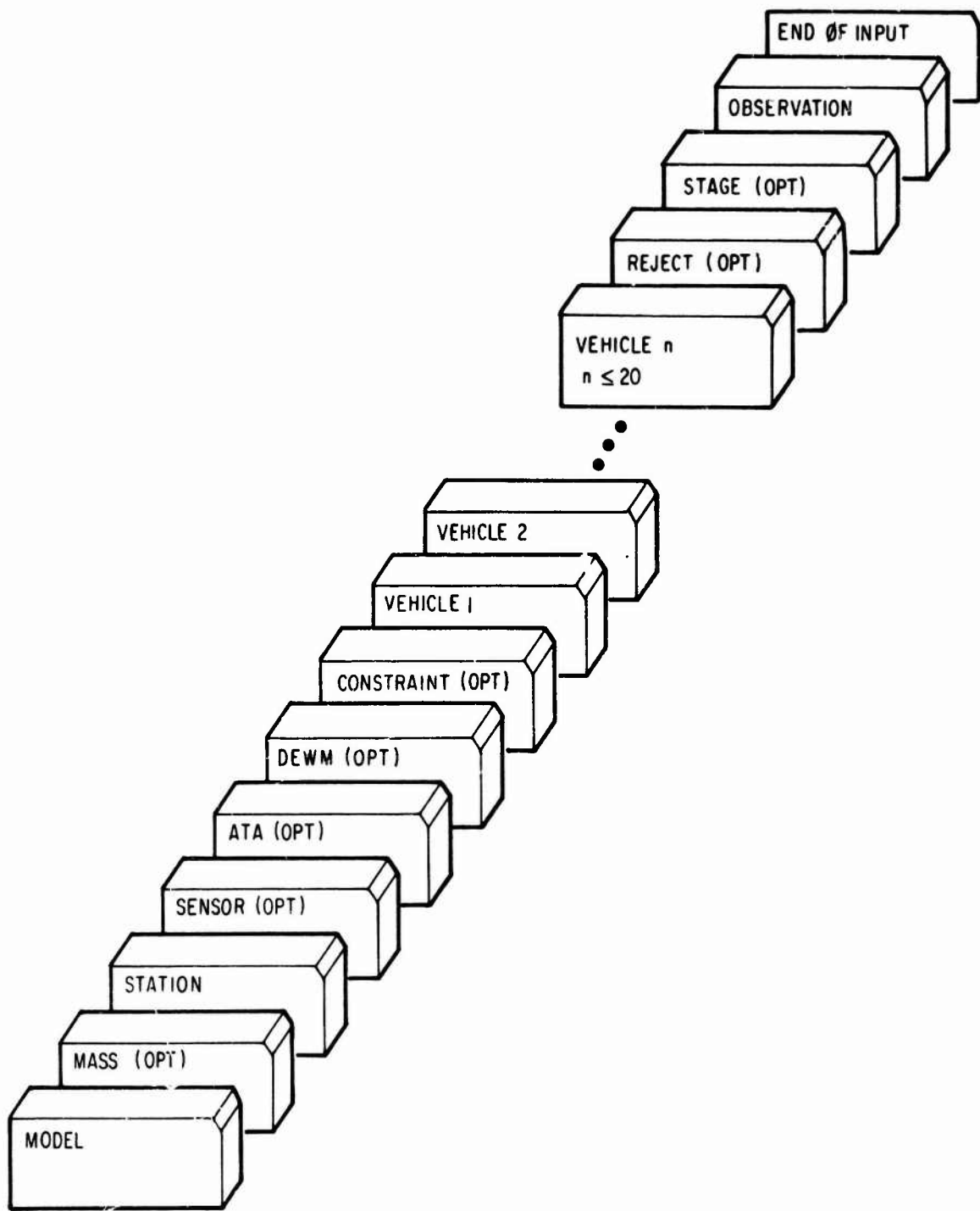


Fig. B-20. Deck Setup for a Simultaneous-Vehicle Differential Correction Run with OBSERVATION Card Input

B.7.2 Data Generation (ITIN=4, MULTV≠0)

The deck setup for generating data for vehicles simultaneously in orbit that have the same model is illustrated in Fig. B-21. Each VEHICLE data block contains a VEHID (Sec. 11.1.2).

Only one DATA GENERATION block is input; it contains DATA GENERATION I (Sec. 12.1) and II (Sec. 12.2.2) cards.

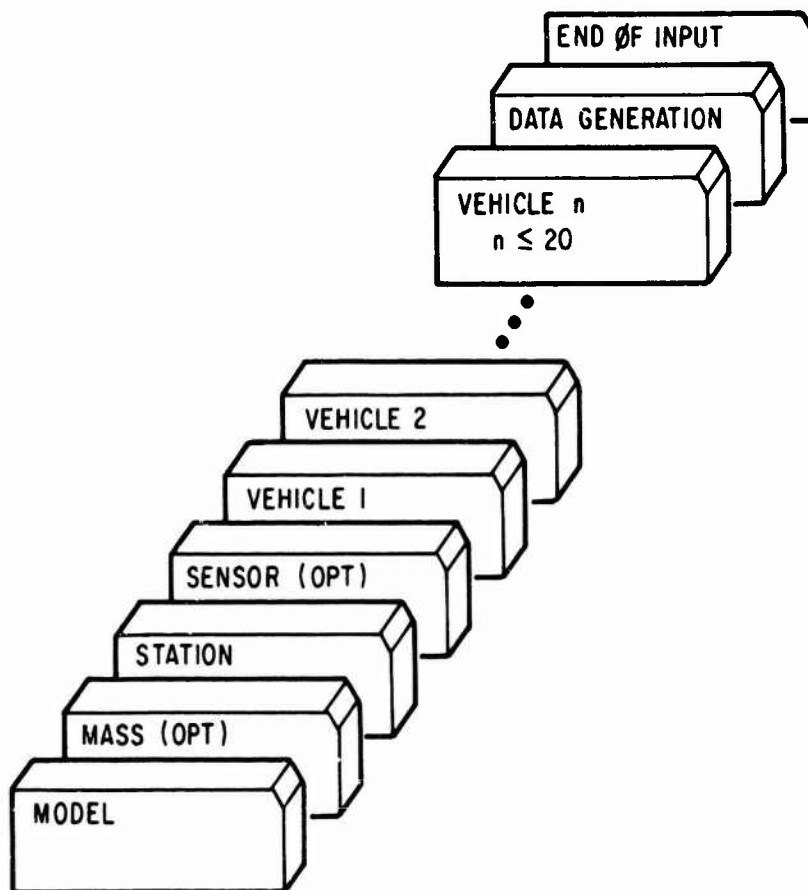


Fig. B-21. Deck Setup for a Simultaneous-Vehicle Data Generation Run

B.7.3 Covariance Analysis (ITIN=5, MULTV=1,2)

The deck setup for a simultaneous-vehicle covariance analysis run (Fig. B-22) is basically the same as that for a single vehicle (Sec. B.4). The main difference is that, since the vehicles are in simultaneous orbit, all VEHICLE data blocks are input before the DATA GENERATION, REJECT, or OBSERVATION data blocks.

Each vehicle requires a VEVID (Sec. 11.1.2), and the first requires the input of PTIM (Sec. 11.5.1). The integration times of the first vehicle must span those of any subsequent vehicles.

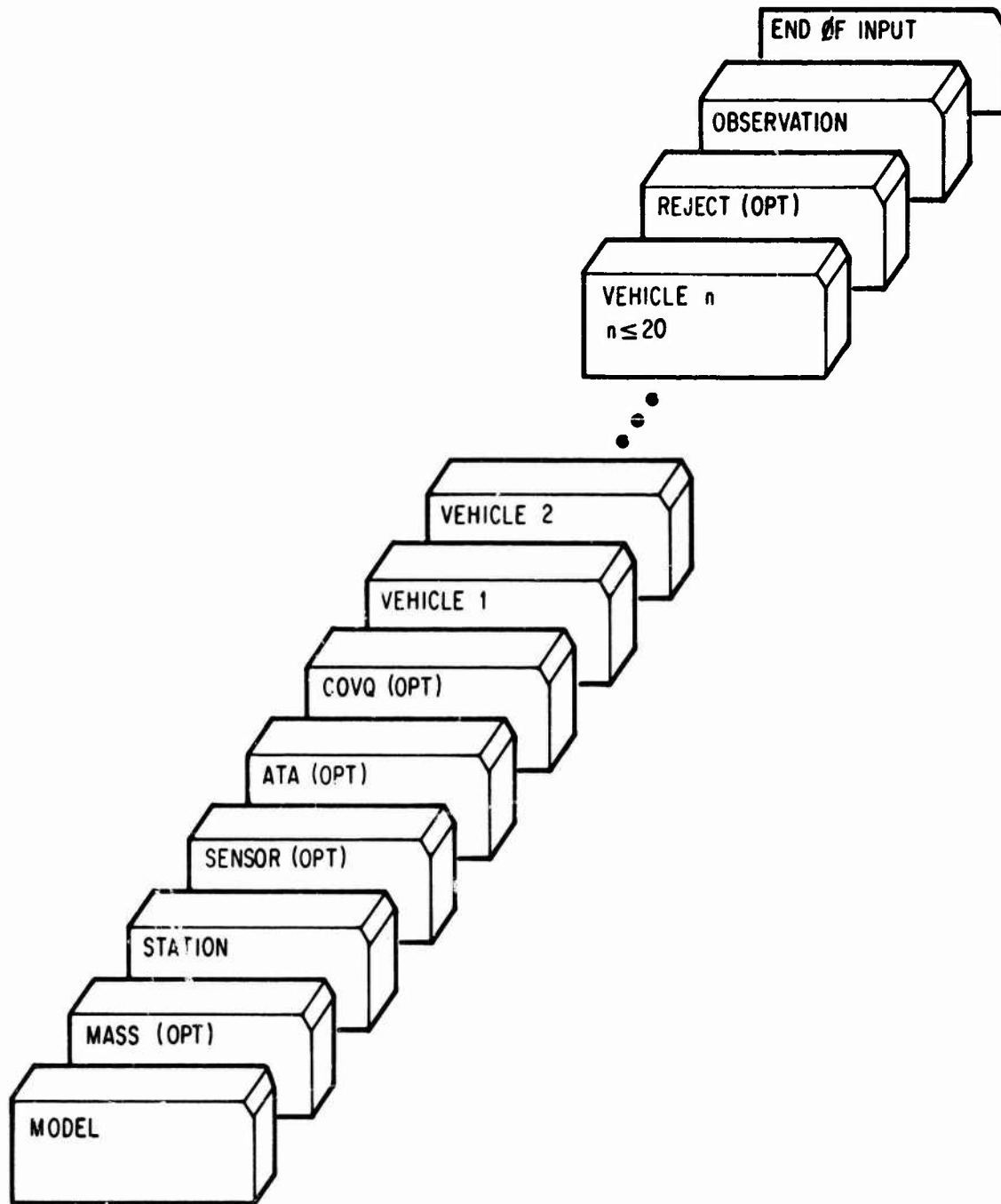


Fig. B-22. Deck Setup for a Simultaneous-Vehicle Covariance Analysis Run with OBSERVATION Card Input

C. SAMPLE OUTPUT DESCRIPTIONS

C. 1	INTRODUCTION	C-1
C. 2	TEST CASE A: ECI SINGLE-VEHICLE EPHEMERIS GENERATION AND SIMULATED MEASUREMENT DATA GENERATION RUN (ITIN = 34)	C-3
C. 3	TEST CASE B: ECI SINGLE-VEHICLE ORBIT DETERMINATION RUN (ITIN = 2)	C-31
C. 4	TEST CASE C: ECI SIMULTANEOUS-VEHICLE COVARIANCE ANALYSIS RUN (ITIN = 5)	C-63
C. 5	TEST CASE D: MCI SINGLE-VEHICLE EPHEMERIS GENERATION RUN (ITIN = 3)	C-141
C. 6	TEST CASE E: ECI SINGLE-VEHICLE, POWERED FLIGHT EPHEMERIS GENERATION RUN (ITIN = 3)	C-159
C. 7	TEST CASE F: ECI SIMULTANEOUS-VEHICLE ORBIT DETERMINATION RUN (ITIN = 2)	C-213
C. 8	TEST CASE G: ECI SIMULTANEOUS-VEHICLE DATA GENERATION RUN (ITIN = 4)	C-305

TABLES

C-1.	Definitions of Initialized Integration Quantities (Note: Repeated for User's Convenience)	C-12 C-168
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C-3.	Definitions of Powered Flight Output Quantities	C-180


SAMPLE OUTPUT DESCRIPTIONS

C.1 INTRODUCTION

The printed output produced by the TRACE Program is described here for typical differential correction, ephemeris generation, data generation, and covariance analysis runs. The samples that follow are of actual output listings, annotated to reference specific portions of the output data. Wherever applicable, the output items described are cross-referenced to the corresponding input definition section in this document. If an item occurs in more than one sample listing, a citation is given only for the first appearance.

The sample test cases included here are:

- Test Case A ECI single-vehicle ephemeris generation and simulated measurement data generation run (ITIN = 34)
- Test Case B ECI single-vehicle orbit determination run (ITIN = 2)
- Test Case C ECI simultaneous-vehicle covariance analysis run (ITIN = 5)
- Test Case D MCI single-vehicle ephemeris generation run (ITIN = 3)
- Test Case E ECI single-vehicle, powered flight ephemeris generation run (ITIN = 3).
- Test Case F ECI simultaneous-vehicle orbit determination run (ITIN = 2)
- Test Case G ECI simultaneous-vehicle data generation run (ITIN = 4)

The symbol , used throughout the sample output, indicates that some output has been omitted. Note that many output pages without descriptive interruption have been included only to provide continuity. Cases A through D were run on TRACE Version 6.96 and Cases E through G on Version 7.27.

MODEL DATA
 INFOPM1
 N 02,00
 O 03,00
 P 04,00
 Q 02,02
 RITIN 34
 RSPLT5
 HD 2.0
 END

INTER*4
 1082.76E-5
 -2.693E-6
 -1.56E-6
 1.544E-6

MTERMS04,60
 0
 0
 0
 -0.765E-6

MMIN 2.0 MMAX 2.0

***** LUNAR GRAVITY MODEL *****

SM = 6.802326500E-05 ER**3/MIN**2 = 1.7313995407E+14 FT**3/SEC**2 = 4.902777030E+12 M**3/SEC**2

⑧

***** EARTH GRAVITY MODEL *****

SM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2

⑨

N	M	CNY	SNM	**	N	M	CNM	SNM
2	0	1.0827600E-03	0.	**	4	0	-1.5600000E-06	0.
3	0	-2.6930000E-06	0.	**	2	2	1.5440000E-06	-7.6500000E-07

***** PHYSICAL CONSTANTS *****

GM(EP**3/MIN**2) = 5.530393500E-03
 GMM(KM**3/MIN**2) = 0.
 SGM(FP**3/MIN**2) = 6.802326500E-05
 PFT(FT/EP) = 2.093573900E+07
 FTKM(FT/KM) = 3.281839000E+03
 CSUR0(FT/SEC**2) = 3.217400000E+01
 CKFP = 1.000000000E-07

OMEGE(RAD/MIN) = 4.375269100E-03
 OMEGA(RAD/MIN) = 4.375269100E-03
 OMEGL(RAD/MIN) = 0.
 ERKH(KY/ER) = 6.378164900E+03
 FTNH(FT/NM) = 6.076115500E+03
 DGREE(DEG) = 5.729577951E+01
 F = 3.352329869E-03

GMLAT(DEG) = 7.830000000E+01
 GMLNG(DEG) = 2.910000000E+02
 AM(ER) = 2.725062770E-01
 ERNH(NM/ER) = 3.443933600E+03
 AE(ER) = 1.000000000E+00
 SLT = 2.820176300E+03
 PI = 3.141592654E+00

⑦

***** INPUT/OUTPUT CONVERSION FACTORS *****

VF(I/O-ER) = 2.09257380E+17
 AF(I/O-ER/MIN**2) = 5.81270500E+03

⑩

ITEM	DESCRIPTION	REFERENCE SECTION
4	<p><u>Card images of the input MODEL data:</u></p> <p>NFØRM, NTERM, TERMS (geopotential inputs) ITIN (function indicator) RSPLT (rise/set plot indicator) HØ, HMIN, HMAX (numerical integration inputs)</p>	<p>2.1.2.2 2.1 2.4.1.1 2.1.4</p>
5	<p><u>Lunar gravity model, including the moon's gravitational constant in three unit systems.</u> In this case, the moon's gravity model is spherical</p>	<p>2.1.2 2.1.1</p>
6	<p><u>Earth's gravity model, including the earth's gravitational constant in three unit systems.</u> In this case, the gravity model is expressed by a spherical harmonic expansion with C and S coefficients, and there is no normalization</p>	<p>2.1.2 2.1.1</p>
7	<p><u>Input physical constants and OMEGL:</u> OMEGL (lunar rotation rate)</p>	<p>2.1.1</p>
8	<p><u>Input/output conversion factors for distance, velocity, and acceleration; always using er/min, er/min² internally</u></p>	<p>2.1.1</p>

***** INTERPATION INPUTS *****

IFORM = 1 ICENT = 1 NSTEP = 2
NPCMP = 0 IR = 8 ER = 1.0000000E-10
HMIN = 2.0000000E+00 HMAX = 2.0000000E+00 HO = 2.0000000E+00

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPDOT = 0
PRHC = 0 YONPR = 0 CLASS = 0 LEMSP = 0 PTMS = 10000

***** CRASH ALTITUDE *****

FCI CRASH ALTITUDE(FT) = 3.0000000E+05 MCI CRASH ALTITUDE(FT) = 3.0000000E+03

***** STATION LOCATIONS *****

STATION	SIG	REF	PA-REF	DATUM	TYPE	RADIUS	LATITUDE X	LONGITUDE Y	HEIGHT Z	P	Q
001	0	1	1	-0	-0	3.4800000E+01	2.3950000E+02	6.0000000E+02	6.0000000E+02		
004	0	1	1	-0	-0	5.7600000E+01	2.0760000E+02	4.2600000E+02	4.2600000E+02		
005	0	1	1	-0	-0	2.1600000E+01	2.0170000E+02	9.4100000E+02	9.4100000E+02		
006	0	1	1	-0	-0	4.2900000E+01	2.8835000E+02	7.6400000E+02	7.6400000E+02		
009	0	1	1	-0	-0	7.5500000E+01	2.9140000E+02	3.9600000E+02	3.9600000E+02		

ENTER SEGMENT 01 AT 76.3 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 76.3 CP SECS., 228.4 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
9	<u>Integration inputs and ICENT</u> ICENT (central force term evaluation indicator)	2.1.4
10	<u>Special options:</u> TAPE2 PRHØ TAPE7 NØDPR TELEM CLASS LEMSP NPDDØTEINTEG(13) (the period decay rate is printed at every integration step) PTNS = nINTEG(16) (the trajectory equations are printed every n integration steps)	2.1.4 2.1.2.4 2.1.1.3 2.1.1.4 2.1.1.4 2.2.1.1, 2.4.1.1.6, 2.5.1 2.1.4
11	<u>ECI and MCI crash altitudes at which to stop integrating</u>	2.1.4
12	<u>Printout of the station locations as input. If CLASS ≠ 0, the actual locations are left blank</u>	4
13	<u>Program segment identification. Frequently, when different segments are entered, a remark is printed indicating the segment and its time of entry (from the beginning of the run). The amount of time taken for the segment last executed is also printed</u>	

* Information Processing Division, TRACE66 Orbit Determination Program, Vol. III: Trajectory Generation Equations and Methods, TOR-0066(9320)-2, Vol. III, The Aerospace Corp., El Segundo, Calif. (25 April 1970). This report is Ref. 2 of Part A.

***** V-TITLE UAJA *****

70-170
 H1 IVEH101
 IDAY 16
 MIN 727
 IC 351.5
 4 354.475
 IIDRAG1
 IETAPF4
 DPRCDEX
 PTIM 0
 4 40
 FND

IYEAR 1964
 TZNE 0
 SEC 0
 2 0
 5 21351065.
 DRAS .0116

IMNTH 6
 HR 0
 ICTYP2
 3 90
 6 25855.914

2 1 1320
 5 3 760

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6
 CARD 7
 CARD 8
 CARD 9
 CARD 10
 CARD 11
 CARD 12

DATA GENERATION I		DATA GENERATION II		DATA GENERATION III		DATA GENERATION IV		DATA GENERATION V		
STATION	INTERVAL (SEC.)	MIN.ELE. (DEG.)	MAX.ELE. (DEG.)	MAX.RANGE (N.M.I.)	START TIME DA -R	START TIME MIN	STOP TIME HR	STOP TIME MIN	AZIMUTH1 (DEG.)	AZIMUTH2 (DEG.)
001	60.00	-0.00	-0.00	-0.	-0 -0	-0.0000	00 22	-0.0000	-0.0	-0.0
004	60.00	-0.00	-0.00	-0.	-0 -0	-0.0000	00 22	-0.0000	-0.0	-0.0
005	60.00	-0.00	-0.00	-0.	-0 -0	-0.0000	00 22	-0.0000	-0.0	-0.0
006	60.00	-0.00	-0.00	-0.	-0 -0	-0.0000	00 22	-0.0000	-0.0	-0.0
009	60.00	-0.00	-0.00	-0.	-0 -0	-0.0000	00 22	-0.0000	-0.0	-0.0

DATA GENERATION II

STATION PNG P.J P
 AZT P.D 0
 ELF 0.J A.C
 001 *X X X*
 004 *X X X*
 005 *X X X*
 006 *X X X*
 009 *X X X*

70-170
 EPOCH
 YR/MO/DAY
 1964/ 8/16
 17
 X,Y,Z,DX,DY,DZ
 2.1122117338E+07
 -3.11902823823E+05
 0.
 -3.63661425026E+02
 -2.46271357753E+03
 2.57357947412E+04

INITIAL CONDITIONS

A,D,B,A,R,V
 3.5160000000E+02
 0.
 9.0000000000E+01
 3.5447500000E+02
 2.1351065000E+07
 2.5859140000E+04
 A,F,I,O,U,TAU
 2.16545058487E+07
 1.40128272088E-02
 9.5250000000E+01
 3.5159999932E+02
 3.63314213347E-11
 6.3805877822E+02
 AF,AG,N,L,CHI,PSI
 1.38625022642E-02
 -2.04703623737E-03
 6.74602827921E-02
 3.5160000000E+02
 -1.60895386758E-01
 1.08958142631E+00

PLANETARY PERTURBATIONS

ATMOSPHERF MODEL ** LOCKHEED
 D1 = 5.93000000E+00 D2 = -1.56800000E+01 FLUX = 0.

TIME
 7.27000000E+02
 CDA/M
 1.16000000E-02

M/CDA
 6.62068966E+01

ITEM	DESCRIPTION	REFERENCE SECTION
14	<p>Card images of the input <u>VEHICLE</u> data:</p> <p>H1 VEHID YEAR, MNTH, DAY, TZNE, HR, MIN, SEC ICTYP, IC IDRAG DRAG ETAPE PRCDE PTIM</p>	11.1.1.1 11.1.1.2 11.1.1.3 11.1.1.4 11.1.1.8 11.1.1.9 11.4.1 11.3.1.2 11.3.1.1
15	Output from the <u>DATA GENERATION I</u> and <u>II</u> cards	12
16	<u>Printout of the VEHICLE input H1 header card</u>	11.1.1
17	<u>Epoch time</u>	11.1.3
18	<p><u>Trajectory initial conditions</u> are printed in four coordinate frames based on BCI coordinates. The initial condition values shown are the results of transformations applied to the input values. The transformation for the input coordinate set (in this case, α, δ, β, A, r, and v) consists of the conversion from decimal to octal numbers, the conversion of units from ft, deg, and sec to er, rad, and min; and the performance of the corresponding inverse conversions for output. The three other types of element sets require coordinate system transformations, in addition to the number and unit system transformations noted above. Accuracy of the values printed is therefore subject to numerical truncation roundoff errors</p> <p>Quantities in the left-hand column are position and velocity components in the basic vernal equinox coordinate system in ft and ft/sec. The second column gives the usual ADBARV spherical system coordinates (i.e., Type 2 initial conditions) in ft, ft/sec, and deg. The third column contains orbit semimajor axis, eccentricity, inclination, right ascension of ascending node, argument of perigee, and time of last perigee passage in MME. Other units are ft and deg. The right-hand column gives the vehicle coordinates in the f and g element set (valid for orbits such that $0 \leq e < 1$) (Refs. 1 and 2)</p>	11.1.4
19	<u>Names of any solar system bodies</u> included in the computation of perturbative accelerations	2.1.2.3
20	<u>Identification of the atmospheric model</u> to be used	11.1.8
21	<u>Time at which to initially use the C_D A/W</u> indicated in the next column in MME	11.1.9
22	<u>The reciprocal of the ballistic coefficient C_D A/W</u>	11.1.9
23	<u>Ballistic coefficient $W/C_D A$</u>	11.1.9
24	<u>The D_1, D_2, and flux expressions for the Lockheed atmospheric density model</u> (for this case)	2.1.2.4.1

ENTER SEGMENT 10 AT 78.9 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .5 CP SECS., 3.5 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1 (25)

IVFP	0	ICENT	1	IDRAG	1	ALPHG	5.662162703E+00	COAM	1.160000000E-02
JVEP	0	JNORM	1	IR	0	ALG-DEG	3.244180258E+02	ER	1.000000000E-10
MVEP	0	MAJOR	0	ISRP	0	TJDATE	2.438623500E+06	HMIN	2.000000000E+00
KVEP	0	MASS	0	NFQS	3	TSTART	7.270000000E+02	HMAX	2.000000000E+00
LVEP	0	NT	4	RECMP	0	TSTOP	1.320000000E+03	MO	2.000000000E+00
ICENTY	1	JNORMX	0	NMASSX	0	FLIGHT	5.930000000E+02	NTX	0.
				NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE * (27)

727.0000 TFR0
1320.0000 TSTOP

*** TRAJECTORY START (28)

***** ECI *****

SEG11 ENTRY TIME IS 78.93100

T =	727.00000	Y =	.25000	NSTEP =	0
	2.11220178379E+07		-3.636604250258F+02		-3.049966727469E+01
	-3.119028238232E+06		-2.462703577527E+03		4.503734134821E+00
	0.		2.573579474117F+04		-1.368599519737E-03

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.093040E+01	-3.049970E+01	4.503503E+00	1.174270E-04	-3.083040E+01	1.455570E-04	2.051445E-04	
ATMOSPHERIC	1.504282E-03	3.413128E-05	2.311366E-04	-1.486027E-03	1.344411E-17	-1.501618E-03	-8.948284E-05	
TOTAL	3.093040E+01	-3.049967E+01	4.503734E+00	-1.368600E-03	-3.083040E+01	-1.356061E-03	1.956617E-04	

REFERENCE
SECTION

ITEM	DESCRIPTION	REFERENCE SECTION
25	<u>Remark indicating the relative number of the vehicle being integrated (not VEHIID)</u>	
26	<u>Quantities associated with the current vehicle (Table C-1)</u>	
27	<u>Event table, including times to start and stop integrating</u>	
28	<u>Start of integration</u>	
29	<u>Integration frame for the current vehicle (in this case, ECI)</u>	
30	Time T; step size H; number of integration steps from NSTEP to T; and position, velocity, and acceleration components in Columns 1, 2, and 3, respectively, for this event (epoch) print (in MME, min, ft, ft/sec, and ft/sec ²)	
31	<u>Forces at T</u>	

Table C-1. Definitions of Initialized Integration Quantities

Symbol	Definition	Reference Section
IVEP	Number of C and S parameters (GPRAM)	2.1.5.2
JVEP	Number of other model parameters (ØPRAM)	2.1.5.3
MVEP	Number of mass parameters (MPRAM)	2.1.5.1
KVEP	Number of vehicle-dependent parameters (VPRAM)	11.1.14
LVEP	Number of delayed parameters (i.e., THRUST, DRAG, etc.)	11.1.14
ICENTX	Central force flag for the moon	
ICENT	Central force flag for the earth	
JNORM	Normalization for the earth gravity model	2.1.2.2
MAJOR	Flag for the integration of the variational equations	
NMASS	Number of masses in the earth gravity model	
NT	Number of terms in the earth gravity model	2.1.2.2
JNORMX	Normalization for the lunar gravity model	11.1.8
IDRAG	Flag indicating the atmospheric model used	2.1.4
IR	Ratio of Runge-Kutta to Cowell step size (H0/IR)	2.1.2.6
ISRP	Flag for solar radiation pressure	
NEQS	Total number of equations to be integrated	
RECMP	Flag for recomputation of perturbations	2.1.4
NMASSX	Number of masses in the lunar gravity model	
NASA	Coordinate and timekeeping transformation option flag	2.1.4

Table C-1. Definitions of Initialized Integration Quantities (Continued)

Symbol	Definition	Reference Section
ALPHG	Right ascension of Greenwich (rad at midnight of epoch day)	
ALG-DEG	Right ascension of Greenwich (deg at midnight of epoch day)	
TJDATE	Julian date of epoch day	
TSTART	Trajectory start time (MME)	
TSTOP	Trajectory stop time (MME)	
FLIGHT	Duration of flight (TSTOP - TSTART, min)	
SSTEP	Number of integration steps specified per rev when the regularized time variable is used	11.1.6
CDAW	Reciprocal of the ballistic coefficient	
ER	Error control in integration ($ER = 1. \cdot 10^{-S}$, where S is the number of significant figures)	2.1.4
HMIN	Minimum absolute step size for integration	2.1.4
HMAX	Maximum absolute step size for integration	2.1.4
H0	Initial integration step size: A negative value indicates backward integration	2.1.4
NTX	Number of terms in the lunar gravity model	2.1.2.2
SORD	Power of the regularization transform	11.1.6
CPAW	Solar radiation pressure coefficient	11.1.4
UTD	Correction that relates iteration time to ephemeris time, sec	2.1.4

NOFF	T =	DOURLED	X	Y	7	(EXTERNAL	UNITS)	RADIAL	IN-TRACK	CROSS-TRACK		
* * NOFF	T =	739.250000	T =	755.250000	H =	.500000								
NOFF	DT =	7.715056082307E+02	NOFF	DT =	-2.174312233991E+07	NOFF	DT =	3.220848060321E+06	NOFF	DT =	9.155402131023E-02	NOFF	DT =	9.155402131023E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.538916113278E+02	NOFF	DT =	3.92365839274E+03	NOFF	DT =	-2.499914410016E+04	NOFF	DT =	-2.499914410016E+04
NOFF	DT =	8.160132498351E+00	NOFF	DT =	2.111878462148E+07	NOFF	DT =	-3.136242581735E+06	NOFF	DT =	1.057768166002E-01	NOFF	DT =	1.057768166002E-01
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.676358013866E+02	NOFF	DT =	-2.462617183232E+03	NOFF	DT =	2.573513681870E+04	NOFF	DT =	2.573513681870E+04
NOFF	DT =	9.505088844192E+02	NOFF	DT =	-2.173661142815E+07	NOFF	DT =	3.240165570270E+06	NOFF	DT =	9.162694120100E-02	NOFF	DT =	9.162694120100E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.545031738123E+02	NOFF	DT =	2.392907285641E+03	NOFF	DT =	-2.500214730405E+04	NOFF	DT =	-2.500214730405E+04
NOFF	DT =	9.050141615365E+02	NOFF	DT =	-2.111560357750E+07	NOFF	DT =	-3.157478550731E+06	NOFF	DT =	1.052970851538E-01	NOFF	DT =	1.052970851538E-01
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.715253959224E+02	NOFF	DT =	-2.462027934117E+03	NOFF	DT =	2.573440021394E+04	NOFF	DT =	2.573440021394E+04
NOFF	DT =	9.495001485312E+02	NOFF	DT =	-2.173012707833E+07	NOFF	DT =	3.259487366782E+06	NOFF	DT =	9.058326290414E-02	NOFF	DT =	9.058326290414E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.550446520700E+02	NOFF	DT =	2.392890505067E+03	NOFF	DT =	-2.500511078411E+04	NOFF	DT =	-2.500511078411E+04
NOFF	DT =	9.940033497745E+02	NOFF	DT =	2.111248671667E+07	NOFF	DT =	-3.176721703786E+06	NOFF	DT =	1.070233809849E-01	NOFF	DT =	1.070233809849E-01
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.753122137674E+02	NOFF	DT =	-2.460866515650E+03	NOFF	DT =	2.573357343278E+04	NOFF	DT =	2.573357343278E+04
NOFF	DT =	1.03848003411E+03	NOFF	DT =	-2.172366357365E+07	NOFF	DT =	3.278795075491E+06	NOFF	DT =	8.716727127885E-02	NOFF	DT =	8.716727127885E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.555426278197E+02	NOFF	DT =	2.3924411765957E+03	NOFF	DT =	-2.500804218916E+04	NOFF	DT =	-2.500804218916E+04
NOFF	DT =	1.082981321138E+03	NOFF	DT =	2.110940072490E+07	NOFF	DT =	-3.149593658598E+06	NOFF	DT =	1.04842981835E-01	NOFF	DT =	1.04842981835E-01
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.790299919716E+02	NOFF	DT =	-2.459392224658E+03	NOFF	DT =	2.573269351510E+04	NOFF	DT =	2.573269351510E+04
NOFF	DT =	1.127448861730E+03	NOFF	DT =	-2.171717340606E+07	NOFF	DT =	3.298071998920E+06	NOFF	DT =	7.865032799414E-02	NOFF	DT =	7.865032799414E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.560585150084E+02	NOFF	DT =	2.391835442467E+03	NOFF	DT =	-2.5010988583350E+04	NOFF	DT =	-2.5010988583350E+04
NOFF	DT =	1.171948128798E+03	NOFF	DT =	2.110628623951E+07	NOFF	DT =	-3.245162695717E+06	NOFF	DT =	1.065998433399E-01	NOFF	DT =	1.065998433399E-01
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.827440448012E+02	NOFF	DT =	-2.458042729758E+06	NOFF	DT =	2.573181925916E+04	NOFF	DT =	2.573181925916E+04
NOFF	DT =	1.216406397456E+03	NOFF	DT =	-2.171059451433E+07	NOFF	DT =	3.317312624163E+06	NOFF	DT =	6.158998121460E-02	NOFF	DT =	6.158998121460E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.566534977233E+02	NOFF	DT =	2.3915833030237E+03	NOFF	DT =	-2.501399732251E+04	NOFF	DT =	-2.501399732251E+04
NOFF	DT =	1.260903267159E+03	NOFF	DT =	-2.110309216343E+07	NOFF	DT =	-3.234350508507E+06	NOFF	DT =	9.425052306976E-02	NOFF	DT =	9.425052306976E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	-3.865133472910E+02	NOFF	DT =	-2.4457180753738E+03	NOFF	DT =	2.573099833463E+04	NOFF	DT =	2.573099833463E+04
NOFF	DT =	1.305351933197E+03	NOFF	DT =	-2.170388599938E+07	NOFF	DT =	3.3365225691455E+06	NOFF	DT =	3.443219649954E-02	NOFF	DT =	3.443219649954E-02
NOFF	DT =	1.000000000000E+00	NOFF	DT =	3.5735311955035E+02	NOFF	DT =	2.391889239496E+03	NOFF	DT =	-2.501711161410E+04	NOFF	DT =	-2.501711161410E+04

T =	1320.250000	4 =	1.000000	NSTEP =	644
	-1.067370314174E+07			1.478330439997E+01	
	3.489513873940E+0F			-4.744146117512E+00	
	-1.859775247439E+07			2.520901666549E+01	

FORCES
 GEOPOTENTIAL
 ATMOSPHERIC
 TOTAL
 (INTERNAL UNITS)
 2.950655E+01 1.478331E+01 -4.744146E+00 2.520901E+01 -2.960652E+01 3.682527E-02 7.125906E-03
 5.699119E-06 -4.914114E-06 2.914771E-07 2.851771E-06 6.484690E-08 -5.685813E-06 1.827404E-07
 2.950655E+01 1.478330E+01 -4.744145E+00 2.520902E+01 -2.960652E+01 3.681958E-02 7.126088E-03

48

79

644

15

REFERENCE
SECTION

ITEM	DESCRIPTION
32	<u>Change in step size</u> , indicated by a remark, the time of change, the new step size, and the number of integration steps to this time
33	<u>Nodal crossing</u> showing the time (MME) and position components on the first line and the step size (min) and velocity components (ft/sec) on the second line
34	<u>Event detection print</u> (Item 30)
35	<u>Forces</u> at time T

*** TRAJECTORY TERMINATION (35)

*** THIS CASE TOOK 1.805 SECONDS TO INTEGRATE A SPAN OF 593.2500 MINUTES ***

*** FROM 727.000 TO 1320.250 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 60.7 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.9 CP SECS., 9.0 PP SECS.

REFERENCE
SECTION

DESCRIPTION

ITEM

- 36 Remark at trajectory termination
- 37 Number of seconds to integrate the time span of the current vehicle

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	ME,MY,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,....	ALPHA,....	REV,...	REMARKS
MO/DAY/YR	MIN FROM EPOCH	X (FT)	DX (FT/SEC)	LATITUDE (DEG)	ALPHA (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIG-IT	Y (FT)	DY (FT/SEC)	LONGITUDE (DEG)	DELTA (DEG)	PERIOD	.
SEC	SEC FROM MIDNIG-IT	Z (FT)	DZ (FT/SEC)	ALTITUDE (MM)	BETA (DEG)	PER-DECAY	.
	STEP SIZE(MIN)	R (FT)	V (FT/SFC)	S-VEH-LAT(DEG)	AZIMUTH(DEG)	NOD-RES	.

*** * CI TRAJECTORY * * * (30)

(30)

ITEM	DESCRIPTION	REFERENCE SECTION
38	<p><u>TRACE ephemeris output key.</u> Date column includes the current month, day, year, hour, minute, and second. The next column contains the times from epoch and midnight of current date and the current step size. The following columns contain the components and magnitude of the radius vector from body center to satellite (ft) and the components and magnitude of the velocity vector (ft/sec). LAT contains the latitude, longitude, altitude, and subvehicle latitude; ALPHA is self-explanatory; and REV always contains the rev count plus (at an ascending node) the period for one revolution, the period-decay rate, and the nodal regression. The remarks column is used to indicate the reason for printing (if other than the print time vector)</p>	11.3.1
39	<p><u>The integration frame for this vehicle</u></p>	11.1.6

*** CASE 140
70-170 (41)

*** PPOCH PRINT

DATE,...	ME,MM,ST,OT	X,Y,Z,PR	JK,JY,DZ,AV	LAT,...	ALPHA,...	REV,...
8/16/64	0.00000	2.11220179E+07	-3.63550425E+02	0.00000000	351.59999959	.02333
12/ 7	727.00000	-3.11902824E+06	-2.46270358E+03	204.93437636	0.00000000	0.00000
0.00000	42620.00000	0.	2.57357947E+04	69.99982	90.00000000	0.00000
	.25000	2.13510650E+07	2.58559140E+04	0.00000000	354.47499959	0.00000
A =	2.16545058E+07	MEAN ANOM =	3.60000000E+02	APOGEE =	3.61381331E+03	
E =	1.40128272E-02	ECCENTRIC =	3.60000000E+02	HEIGHT =	1.69879706E+02	
I =	9.55250000E+01	TRJE ANOM =	3.60000000E+02	PERIGEE =	3.51393342E+03	
O =	3.51600000E+02	KE2L PER =	8.89412222E+01	HEIGHT =	6.99998225E+01	
U =	3.61314213E-11	ANOM PER =	8.90819493E+01	U-DOT =	8.51446431E-01	
TAU =	6.38058778E+02	NOJL PER =	8.90175033E+01	U-DOT =	-4.21677378E+00	

*** REQUESTED POINTS (43)

DATE,...	ME,MM,ST,OT	X,Y,Z,PR	DX,DY,DZ,AV	LAT,...	ALPHA,...	REV,...	ASC NODE
8/16/64	0.00000	2.11220179E+07	-3.63550425E+02	0.00000000	351.59999959	1.00000	(44)
12/ 7	727.00000	-3.11902824E+06	-2.46270358E+03	204.93437636	0.00000000	0.00000	
0.00000	43620.00000	0.	2.57357947E+04	69.99982	90.00000000	0.00000	
	.25000	2.13510650E+07	2.58559140E+04	0.00000000	354.47499959	0.00000	
DATE,...	ME,MM,ST,OT	X,Y,Z,PR	DX,DY,DZ,AV	LAT,...	ALPHA,...	REV,...	ASC NODE
8/16/64	33.00000	-1.54411960E+07	-1.76837291E+04	45.25874547	177.13628383	1.37406	(45)
12/40	760.00000	7.72413983E+05	4.32636701E+03	22.19807322	45.06635191	0.00000	
0.00000	45600.00000	1.54963330E+07	-1.74819005E+04	164.46761	89.43019977	0.00000	
	1.00000	2.18838176E+07	2.52399240E+04	45.24996466	187.82931795	0.00000	

DATE,...	ME,MM,ST,OT	X,Y,Z,PR	DX,DY,DZ,AV	LAT,...	ALPHA,...	REV,...	DSC NODE
8/16/64	44.50561	-2.17431233E+07	3.53894348E+02	-0.00000609	171.57394639	1.50000	
12/51	771.50561	3.22084829E+06	2.39236543E+03	13.75145825	-0.00000605	0.00000	
30.33659	46290.33659	-2.32091378E+00	-2.49991441E+04	173.57223	89.99888575	0.00000	
	1.00000	2.19503829E+07	2.51158488E+04	-0.00000609	185.52555726	0.00000	

ITEM	DESCRIPTION	REFERENCE SECTION
40	<u>Number of the case on the trajectory file (TAPE2)</u>	
41	<u>Printing the input VEHICLE H1 header card</u>	11.1.1
42	<u>Epoch print (Item 38) plus three other columns.</u> The first contains the classical elements a , e , i , Ω , ω , and τ in ft, deg, and MME. The second column contains the mean, eccentric, and true anomalies in deg and the Keplerian, anomalistic, and nodal periods in min. The last contains the radial distance and height above the oblate earth at both perigee and apogee in nmi. The nodal regression rate $\dot{\Omega}$ and the rate of advance of the line of apsides $\dot{\omega}$ are printed in deg/day	11.1.4
43	<u>Output requested by PRCDE and PTIM follows</u>	11.3.1.1 11.3.1.2
44	<u>Ascending node print (Item 38)</u>	
45	<u>Print requested by PTIM (Item 38)</u>	11.3.1.1

DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	ASC MODE
8/16/64	533.90326	2.11030922E+07	-3.86509399E+02	-0.00000908	351.20640839	7.00000	
21/ 0	1260.90328	-3.23435018E+06	-2.45718136E+03	70.77953108	-0.00000902	88.95515	
54.19710	75654.19710	-3.36225350E+00	2.57309983E+04	69.773369	90.02172268	-0.01166	
	1.00000	2.13495087E+07	2.58509459E+04	-0.00000908	354.47846382	-0.05220	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	533.00000	3.79739708E+06	-2.48359677E+04	77.70761100	325.17057615	7.21919	
21/20	1280.00000	-2.642257032E+06	3.29827419E+03	39.87645005	77.62732148	0.00000	
0.00000	76800.00000	2.10921800E+07	5.24858129E+03	120.95062	89.20585407	0.00000	
	1.00000	2.15937032E+07	2.55978010E+04	77.70489301	333.35817387	0.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	578.35194	-2.17038859E+07	3.57354474E+02	-0.00000287	171.26037154	7.50000	
21/45	1305.35194	3.33652580E+06	2.39188090E+03	239.61090808	-0.00000285	0.00000	
21.11633	78321.11633	-1.09188644E+00	-2.50171116E+04	170.02827	89.97667859	0.00000	
	1.00000	2.19588494E+07	2.51337365E+04	-0.00000287	189.52164962	0.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	593.00000	-1.11943977E+07	2.15332700E+04	-57.64199647	162.54791699	7.66061	
22/ 0	1320.00000	3.52054757E+06	-2.02713773E+03	227.2284232	-57.46778205	0.00000	
0.00000	79200.00000	-1.84833097E+07	-1.31305126E+04	156.74357	90.64933992	0.00000	
	1.00000	2.18244258E+07	2.53125855E+04	-57.63441492	190.29659789	0.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	593.25000	-1.08737031E+07	2.17582556E+04	-56.61936726	162.20745342	7.66358	
22/ 0	1320.25000	3.48950387E+06	-2.09859177E+03	226.82327764	-58.44804353	0.00000	
15.00000	79215.00000	-1.85977524E+07	-1.27744781E+04	156.24017	90.65737993	0.00000	
	1.00000	2.18240956E+07	2.53182358E+04	-58.61193880	190.50496505	0.00000	
A =	2.16900275E+07	MEAN ANOM =	2.42343660E+02	APOGEE =	3.61624033E+03		
E =	1.30320787E-02	ECCENTRIC =	2.41586307E+02	HEIGHT =	1.72322910E+02		
I =	9.55158745E+01	TRUE ANOM =	2.41038959E+02	PERIGEE =	3.52319860E+03		
O =	3.51255664E+02	KEPL PER =	8.91301580E+01	WEIGHT =	7.92811798E+01		
U =	3.57853864E+02	ANOM PER =	8.90942174E+01	D-DOT =	8.45137218E-01		
TAU =	1.26022945E+03	NOPL PER =	8.89399172E+01	U-DOT =	-4.19310098E+00		

*** FND OF TRAJECTORY *** (47)

ENTER SEGMENT 60 AT 82.0 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS 1.2 CP SECS., 5.7 PP SECS.

(48)

**REFERENCE
SECTION**

DESCRIPTION

ITEM

- 46 Post-event prints. In this case, the event was termination. The output contains the items described in the ephemeris output key (Item 38) and the three additional columns in Item 42
- 47 A remark indicating the end of the trajectory ephemeris

* VEHICLE CASE 1 *

* * DATA GENERATION FOR VE-HID

(40)

AUG. 16, 1964 (48)

005 RISE AT 12 4R 9 MIN 25.84 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 171.00 DEGREES (80)
 005 12 HR 9 MIN 60.00 SEC 5.579456AE+02(RNS) 1.7220949E+02(AZI) 2.7696341E+00(ELE) (81)
 005 12 HR 10 MIN 60.00 SEC 3.0639967E+02(RNS) 1.7349238E+02(AZI) 1.1207660E+01(ELE)
 005 12 HR 11 MIN 60.00 SEC 4.0440078E+01(RNS) 1.8787277E+02(AZI) 5.7359071E+01(ELE)
 005 MAX EL AT 12 4R 12 MIN 10.67 SEC ELEVATION = 79.53 DEGREES, AZIMUTH = 261.09 DEGREES (82)
 005 12 HR 12 MIN 60.00 SEC 2.2308304E+02(RNS) 3.4729596E+02(AZI) 1.8427180E+01(ELE)
 005 12 HR 13 MIN 60.00 SEC 4.6962138E+02(RNS) 3.4946770E+02(AZI) 5.8783741E+00(ELE)
 005 12 HR 14 MIN 60.00 SEC 7.2045819E+02(RNS) 3.5019139E+02(AZI) 5.8590576E-01(ELE)
 005 SFT AT 12 4R 15 MIN 8.67 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 350.26 DEGREES (83)
 005 TOTAL VISIBILITY OF PASS = 5.71 MIN. OF STAT. = 5.71 MIN. OF VEH. = 5.71 MIN. PASS = 1 (84)

004 RISE AT 12 HR 18 MIN 13.00 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 217.13 DEGREES
 004 12 HR 18 MIN 60.00 SEC 5.6327235E+02(RNS) 2.2792597E+02(AZI) 2.8602274E+00(ELE)
 004 12 HR 19 MIN 60.00 SEC 5.3398100E+02(RNS) 2.4905712E+02(AZI) 6.3954642E+00(ELE)
 004 MAX EL AT 12 HR 20 MIN 52.02 SEC ELEVATION = 7.79 DEGREES, AZIMUTH = 273.67 DEGREES
 004 12 HR 20 MIN 60.00 SEC 5.0416315E+02(RNS) 2.7756289E+02(AZI) 7.7513388E+00(ELE)
 004 12 HR 21 MIN 60.00 SEC 5.8891714E+02(RNS) 3.0319002E+02(AZI) 5.7174502E+00(ELE)
 004 12 HR 22 MIN 60.00 SEC 7.4975558E+02(RNS) 3.2004020E+02(AZI) 2.4155542E+00(ELE)
 004 SFT AT 12 HR 23 MIN 44.72 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 320.24 DEGREES
 004 TOTAL VISIBILITY OF PASS = 5.53 MIN. OF STAT. = 5.53 MIN. OF VEH. = 11.24 MIN. PASS = 1

009 RISE AT 15 4R 27 MIN 48.62 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 25.05 DEGREES
 009 15 HR 27 MIN 60.00 SEC 9.6357395E+02(RNS) 2.7675197E+01(AZI) 3.2563539E-01(ELE)
 009 15 HR 28 MIN 60.00 SEC 3.0680157E+02(RNS) 4.2787894E+01(AZI) 1.5396814E+00(ELE)
 009 MAX EL AT 15 4R 29 MIN 36.13 SEC ELEVATION = 1.75 DEGREES, AZIMUTH = 52.44 DEGREES
 009 15 HR 29 MIN 60.00 SEC 9.1169530E+02(RNS) 5.8771469E+01(AZI) 1.6615190E+00(ELE)
 009 15 HR 30 MIN 60.00 SEC 9.7715571E+02(RNS) 7.3590588E+01(AZI) 6.8709925E-01(ELE)
 009 SFT AT 15 4R 31 MIN 26.30 SEC ELEVATION = 0.00 DEGREES, AZIMUTH = 79.35 DEGREES



REF:

ITEM	DESCRIPTION	REFERENCE SECTION
48	Identification of the vehicle (Item 40) for which the program is <u>simulating measurements</u> (and its VEHD)	11.1.2
49	<u>Date</u> on which the data to follow applies	
50	<u>Rise message</u> . The time at which the vehicle becomes visible from a particular location is obtained by interpolation and is printed in hr, min, and sec (the elevation and local azimuth angles are printed in deg)	4 12
51	<u>Simulated data</u> showing the station; the time of day in hr, min, and sec; and the measurements generated, as indicated by the DATA GENERATION II card (Item 15). The time results from incrementing the START by Δt ; both are found on the DATA GENERATION I card	12
52	<u>Maximum elevation point</u> . The time of the maximum elevation angle is obtained by interpolation and is printed, with the corresponding elevation and azimuth angles, in deg	
53	<u>Set message</u> . When the vehicle is no longer visible from a station, the time of invisibility is obtained by interpolation and is printed, with the corresponding elevation and azimuth angles, in deg	12
54	<u>Duration message</u> . After each pass, a message is printed giving the elapsed time of visibility for the pass in min and the current totals for station and vehicle. The number of the pass for the station is also printed	

***** VISIBILITY SUMMARY *****

STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION	STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION	STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION
001	1	3.34	004	1	5.53	005	1	5.71
006	2	13.09	009	5	33.35			

TOTAL NUMBER OF PASSES WERE 10. TOTAL VISIBILITY TIME FOR THE VEHICLE WAS 67.03 MIN.

REFERENCE
SECTION

12

DESCRIPTION

ITEM

55 Visibility Summary. After the data for the spans indicated by the DATA GENERATION I cards has been generated, a summary is printed. It includes the number of passes and the total visibility time for each station and vehicle

DY	HR	MN	001	004	005	006	009
16	12	5					
16	12	10			R		S
16	12	15					
16	12	20			R		S
16	12	25					
16	12	30					
16	12	35					
16	12	40					
16	12	45					
16	12	50					
16	12	55					
16	13	0					
16	13	5					
16	13	10					
16	13	15					
16	13	20					
16	13	25					
16	13	30					
16	13	35					
16	13	40					
16	13	45					
16	13	50					
16	13	55					
16	14	0					
16	14	5					
16	14	10					
16	14	15					
16	14	20					
16	14	25					
16	14	30					
16	14	35					
16	14	40					
16	14	45					
16	14	50					
16	14	55					
16	15	0					
16	15	5					
16	15	10					
16	15	15					
16	15	20					

CONT'D
NEXT
COLUMN



DY	HR	MN	001	004	005	006	009
16	15	25					
16	15	30					X
16	15	35					
16	15	40					
16	15	45					
16	15	50					
16	15	55					
16	16	0					
16	16	5					
16	16	10					
16	16	15					
16	16	20					
16	16	25					
16	16	30					
16	16	35					
16	16	40					
16	16	45					
16	16	50					
16	16	55					
16	17	0					
16	17	5					R S
16	17	10					
16	17	15					
16	17	20					
16	17	25					
16	17	30					
16	17	35					
16	17	40					
16	17	45					
16	17	50					
16	17	55					
16	18	0					
16	18	5					
16	18	10					
16	18	15					
16	18	20					
16	18	25					R S
16	18	30					
16	18	35					R S
16	18	40					



REFERENCE
SECTION

DESCRIPTION

ITEM

2.4.1.1

56 Rise-set printer plot. When RSPLT is input $\neq 0$, the passes are given in a printer plot, using RSPLT as the scale. On the page shown, R means rise, S means set, X stands for rise and set in the same interval, and a + indicates continued visibility

MODEL DATA
 DITIN 2
 JKSIG 1
 SIGMA100
 INFOPM1
 0 02,00
 0 03,00
 0 04,00
 0 02,02
 H0 2.0
 IMAXTT2
 GPL0T6.
 END

I2 2 .1
 INTERM4
 1082.76E-5
 -2.693E-6
 -1.56E-6
 1.544E-6
 HMIN 2.0
 2 15.

I3 3 .1
 MTERMS04,60
 0
 0
 0
 -0.765E-6
 HMAX 2.0

CARD	1
CARD	2
CARD	3
CARD	4
CARD	5
CARD	6
CARD	7
CARD	8
CARD	9
CARD	10
CARD	11
CARD	12

***** LUNAR GRAVITY MODEL *****
 SM = 6.802326500E-05 ER**3/MIN**2 = 1.7313995407E+14 FT**3/SEC**2 = 4.9027777038E+12 M**3/SEC**2
 SPHERICAL MODEL

***** EARTH GRAVITY MODEL *****
 SM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2
 NO NORMALIZATION WITH 4 TERMS.

N	M	CNM	**	N	M	CNM	SNM
2	0	1.08276010E-03	0.	**	4	0	-1.56000000E-06
3	0	-2.69300010E-06	0.	**	2	2	1.54400000E-06

***** PHYSICAL CONSTANTS *****
 SM(ER**3/MIN**2) = 5.530393500E-03
 SM(KM**3/MIN**2) = 0.
 SGM(ER**3/MIN**2) = 6.802326500E-05
 SGM(KM**3/MIN**2) = 3.092573900E+07
 SRTM(FT/ER) = 3.280839900E+03
 SRTM(F./KM) = 3.217403000E+01
 SSURE0 (FT/SFC**2) = 1.071003000E-07
 OMEGA(RAD/MIN) = 4.375269100E-03
 OMEGA(RAD/SEC) = 4.375269100E-03
 OMEGA(RAD/HR) = 0.
 SRKM(KM/ER) = 6.378164900E+03
 FTNM(FT/NH) = 6.076115500E+03
 DSURE0(ER) = 5.729577951E+01
 DSURE0(SEC) = 3.352329869E-03
 GMLAT(DEG) = 7.830000000E+01
 GMLNG(DEG) = 2.910000000E+02
 AM(ER) = 2.725062770E-01
 ERNM(NM/ER) = 3.443933600E+03
 AE(ER) = 4.000000000E+00
 SLT = 2.820176300E+03
 PI = 3.141592654E+00

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input <u>MODEL</u> data. Those emphasized here are associated with a differential correction run, the others having been discussed earlier:</p> <p>ITIN MAXIT GPLOT KSIG, SIGMA</p>	<p>2.1 2.2.2 2.2.1 2.2.6</p>

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = 2.09257300E+J7 VF(I/O-FR/MIN) = 3.40762300E+05 AF(I/O-ER/MIN**2) = 5.61270500E+03

***** INTEGRATION INPUTS *****

IFORM = 1 ICENT = 1 NSTEP = 2
NPCMP = 0 IR = 0 ER = 1.00000000E-10
HMIN = 2.00000000E+00 HMAX = 2.00000000E+00 HO = 2.00000000E+00

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 MPOOT = 0
PRHO = 0 NODPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

***** STATION LOCATIONS *****

STATION	SIG	REF	RA-REF	DATUM	TYPE	LATITUDE	LONGITUDE	HEIGHT	P	O
						X	Y	Z		
						RADIUS	LATITUDE	LONGITUDE		
001	0	1	1	-0	-0	3.48000000E+01	2.39500000E+02	6.0000000E+02		
004	0	1	1	-0	-0	5.75000000E+01	2.07800000E+02	4.2600000E+02		
005	0	1	1	-0	-0	2.15000000E+01	2.01700000E+02	9.4100000E+02		
006	0	1	1	-0	-0	4.29000000E+01	2.08350000E+02	7.0400000E+02		
009	0	1	1	-0	-0	7.65000000E+01	2.91400000E+02	3.9600000E+02		

ENTER SEGMENT 01 AT 07.3 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 07.3 CP SECS., 256.0 PP SECS.

***** VEHICLE DATA *****

IVEHID1	JDAY	MIN	IC	IC	IC	IICRAG1	ORAG	IYEAR	IMNTH	HR	IICRAG2	CARD
16	727	351.5	354.5	21351000	0	0	0	1964	8	0	0	1
					5		.011	SEC				2
												3
												4
												5
												6
												7
												8
												9
												10
												11
												12
												13
												14
												15
												16
												17
												18

2

ITEM	DESCRIPTION	REFERENCE SECTION
2	<p>Card images of the input <u>VEHICLE</u> data. The data emphasized here are those for a differential correction run, the others having been discussed earlier:</p> <p>VPRAM BCDIN</p>	<p>11.1.14 11.2.1</p>

***** OBSERVATIONS *****

STAPASS	VR	MO	DY	HR	MIN	SECONDS	T	C	FIELD 1	FIELD 2	FIELD 3	MJD	ST	VEHID	MESSAGE
0050001	64	8	16	12	10	0.0000	1	0	3.39014234E+06	1.72209494E+02	2.76963411E+00	38623	43868.000	1	
0050001	64	8	16	12	11	0.0000	1	0	1.87384769E+06	1.73492974E+02	1.12076600E+01	38623	43860.000	1	
0050001	64	8	16	12	12	0.0000	1	0	5.37420728E+05	1.87872771E+02	5.73590711E+01	38623	43920.000	1	
0050001	64	8	16	12	13	0.0000	1	0	1.35547828E+05	3.47295855E+02	1.84271805E+01	38623	43980.000	1	
0050001	64	8	16	12	14	0.0000	1	0	2.85347371E+05	3.49467701E+02	5.87837413E+00	38623	44040.000	1	
0050001	64	8	16	12	15	0.0000	1	0	4.37758711E+05	3.50191395E+02	5.85905759E-01	38623	44100.000	1	
0040001	64	8	16	12	19	0.0000	1	0	4.03011936E+05	2.27925924E+02	2.86022743E+00	38623	44340.000	1	
0040001	64	8	16	12	20	0.0000	1	0	3.24453020E+06	2.49067115E+02	6.39546421E+00	38623	44400.000	1	
0040001	64	8	16	12	21	0.0000	1	0	3.56338996E+06	2.77562594E+02	7.75133841E+00	38623	44460.000	1	
0040001	64	8	16	12	22	0.0000	1	0	3.57832848E+06	3.03190025E+02	5.71745024E+00	38623	44520.000	1	
0040001	64	8	16	12	23	0.0000	1	0	4.55562572E+05	3.20040201E+02	2.41955425E+00	38623	44580.000	1	
0090001	64	8	16	15	28	0.0000	1	0	5.50983100E+06	4.27878335E+01	1.53988145E+00	38623	55740.000	1	
0090001	64	8	16	15	30	0.0000	1	0	5.53956587E+06	5.87714689E+01	1.66151901E+00	38623	55800.000	1	
0090001	64	8	16	15	31	0.0000	1	0	5.33731692E+06	7.35905880E+01	6.87099257E-01	38623	55860.000	1	
0090002	64	8	16	15	57	0.0000	1	0	4.88932835E+06	3.17928740E+01	3.24975259E+00	38623	61020.000	1	
0090002	64	8	16	15	58	0.0000	1	0	4.13176431E+05	4.86814080E+01	6.40911377E+00	38623	61080.000	1	
0090002	64	8	16	15	59	0.0000	1	0	3.82064868E+05	7.06168216E+01	8.13172504E+00	38623	61140.000	1	
0090002	64	8	16	17	0	0.0000	1	0	4.06008072E+05	9.29956332E+01	7.28281979E+00	38623	61200.000	1	
0090002	64	8	16	17	1	0.0000	1	0	4.76570178E+05	1.10695971E+02	4.62626881E+00	38623	61260.000	1	
0090002	64	8	16	17	2	0.0000	1	0	5.76533468E+05	1.23037331E+02	1.49506641E+00	38623	61320.000	1	
0090003	64	8	16	18	25	0.0000	1	0	5.17267297E+05	2.36501787E+01	2.04242981E+00	38623	65300.000	1	
0090003	64	8	16	18	26	0.0000	1	0	3.84061613E+05	3.20603692E+01	7.36520897E+00	38623	65360.000	1	
0090003	64	8	16	18	27	0.0000	1	0	2.67830231E+06	4.87761502E+01	1.50081673E+01	38623	65420.000	1	
0090003	64	8	16	18	28	0.0000	1	0	2.01580569E+05	8.45829217E+01	2.30015375E+01	38623	65480.000	1	

REFERENCE
SECTION

DESCRIPTION

ITEM

11.2.1
15
11.1.2

3 Observations. Each line represents one OBSERVATION card (or card image) containing the station pass identification, the last two digits of the year; the month, day, hour, minute, and second; the data set type; the covariance code; three measurements; the system time in seconds from midnight; the vehicle identification (which should be the same as the input VEHID); and any pertinent message

If the observations are input by binary tape, nothing is printed at this point

EPOCH
 YR/MO/DAY
 1964/ 8/16
 0.
 0.
 0.
 0.

X,Y,Z,X,Y,DZ
 2.11253789414E+07
 -3.15721902173E+05
 0.
 -3.68511052786E+02
 -2.45051350318E+03
 2.57351640070E+04

A,B,A,R,V
 3.5150000000E+02
 0.
 9.0005000000E+01
 3.4540000000E+02
 2.1360000000E+07
 2.5856000000E+04

A,F,I,O,U,IAU
 2.16730437072E+07
 1.44441834610E-02
 9.9500000000E+01
 3.51499999932E+02
 3.51162206121E-01
 6.38024929616E+02

AF,AG,N,L,CHI,PSI
 1.42983433809E-02
 -2.04739161253E-03
 6.73737489112E-02
 3.51510035590E+02
 -1.62725471159E-01
 1.00082155146E+00

NO PLANETARY PERTURBATIONS.

** ATMOSPHERE MODEL ** LOCKHEED
 D1 = 5.93000000E+00 D2 = -1.56840000E+01 FLUX = 0.
 TIME 7.27000000E+02
 COA/W 1.00000000E-02
 W/COA 1.00000000E+02

THESE ARE THE 7 PARAMETERS IN THE PARAM MATRIX. 7 ARE P PARAMETERS AND 0 ARE 3 PARAMETERS

NAME	P/O	CURRENT VALUE	BOUND	SIGMA	CONVERSION
0001 ALPHA	P	3.51500000E+02	1.00000000E+00	0.	5.72957795E+01
0001 DELTA	P	0.	1.00000000E+00	0.	5.72957795E+01
0001 PETA	P	9.00050000E+01	1.00000000E+00	0.	5.72957795E+01
0001 A7	P	3.54500000E+02	1.00000000E+00	0.	5.72957795E+01
0001 P	P	2.13600000E+07	1.00000000E+05	0.	2.09257300E+07
0001 V	P	2.58560000E+04	1.00000000E+01	0.	3.48762300E+05
0001 PPAG	P	1.00000000E-02	1.00000000E-02	0.	1.00000000E+00

ENTER SEGMENT 10 AT 88.2 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .9 CP SECS., 3.7 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

IVFP	JVFP	MVFP	KVFP	LVFP	ICFNT	JNORM	MAJOR	NT	JNCPMX	IRAG	IR	ISRP	NEQS	RECOMP	NVASSX	NASA	ALPHG	ALG-DEG	TJDATE	TSTART	TSTOP	FLIGHT	SSSTEP	CDAW	ER	HMIN	HMAX	H0	NTX	SORD
0	0	0	7	0	1	0	0	0	0	1	9	3	24	0	0	0	5.662162703E+00	3.244180256E+02	7.27000000E+02	1.303000000E+03	5.76000000E+02	1.00000000E+02	1.00000000E-10	2.00000000E+00	2.00000000E+00	2.00000000E+00	0.	1.50000000E+00		

ITEM	DESCRIPTION	REFERENCE SECTION
4	<p>Parameter list indicating the quantities to be differentially corrected. Shown in tabular form are the name, P- or Q- parameter indicator, current value, input bound and sigma, and input/output conversion factor for each</p>	<p>2.1.5 5 11.1.14</p>

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

727.0000 TZF30
1303.0000 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS	80.39200	Y =	727.000000	X =	.250000	ECI	NSTEP =	0
ALPHA	1.508758303287E-01	0.	7.026655280390E-03	-3.685310520857E+02	-3.046630747846E+01	-7.831510004013E-04	-3.046630747846E+01	
	1.009540444471E+00	0.	-1.056662594666E-03	-2.450633503183E+03	4.553085330712E+00	-5.241378230337E-03	4.553085330712E+00	
	0.	0.	0.	2.573696400698E+04	-9.269647818762E-04	-1.097983001491F-19	-9.269647818762E-04	
DELTA	0.	-0.	-7.298456764874E-02	1.090761671814E-02	7.796797467675E-08	7.796797467675E-08	7.796797467675E-08	
	0.	-0.	1.090761671814E-02	-6.469626029979E-06	-1.1652339188860E-08	-1.1652339188860E-08	-1.1652339188860E-08	
	1.020732529732E+00	0.	-7.332203652761E-02	-5.439841155098F-06	-5.282946063561E-03	-5.282946063561E-03	-5.282946063561E-03	
BETA	0.	0.	-7.332203652761E-02	1.090761671814E-02	1.784801233243E-07	1.784801233243E-07	1.784801233243E-07	
	0.	0.	1.090761671814E-02	7.298456764874E-02	-2.667557346189E-08	-2.667557346189E-08	-2.667557346189E-08	
	0.	0.	-5.439841155098F-06	7.105664137797E-03	1.576498926150E-11	1.576498926150E-11	1.576498926150E-11	
A7	0.	0.	1.090761671814E-02	7.298456764874E-02	-2.679811016287E-08	-2.679811016287E-08	-2.679811016287E-08	
	0.	0.	7.298456764874E-02	7.105664137797E-03	-1.793048486660F-07	-1.793048486660F-07	-1.793048486660F-07	
	0.	0.	7.105664137797E-03	0.	-6.686192638061E-09	-6.686192638061E-09	-6.686192638061E-09	
P	5.890138633619E-01	0.	0.	0.	1.025158804091E-02	1.025158804091E-02	1.025158804091E-02	
	-1.478034111296E-01	0.	0.	0.	-1.545030064381E-03	-1.545030064381E-03	-1.545030064381E-03	
	0.	0.	0.	0.	8.2734466422207E-05	8.2734466422207E-05	8.2734466422207E-05	
V	0.	0.	-1.425321210109E-02	9.478007051295E-02	9.054266773255E-08	9.054266773255E-08	9.054266773255E-08	
	0.	0.	-9.478007051295E-02	9.953961945770E-01	6.029741570225E-07	6.029741570225E-07	6.029741570225E-07	
	0.	0.	9.953961945770E-01	0.	-4.823534210103E-06	-4.823534210103E-06	-4.823534210103E-06	
DRAC	0.	0.	0.	0.	4.179048465007E-07	4.179048465007E-07	4.179048465007E-07	
	0.	0.	0.	0.	2.785612136380E-06	2.785612136380E-06	2.785612136380E-06	
	0.	0.	0.	0.	-1.796317601821E-05	-1.796317601821E-05	-1.796317601821E-05	

3

REFERENCE
SECTION

DESCRIPTION

ITEM

5 Variational equations $\partial r/\partial p$, $\partial i/\partial p$, and $\partial \dot{i}/\partial p$ at epoch in internal units (er, min, rad). They are also printed at trajectory termination

FDPCFS MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.080465E+01-3.046633E+01 4.55292E+00 1.171816E-04-3.080465E+01 1.451160E-04 2.844807E-04
 ATMOSPHERIC 1.056906E-03 2.29158E-05 1.619194E-04-1.044146E-03 9.154040E-05-1.056032E-03-6.290061E-05
 TOTAL 3.080465E+01-3.046633E+01 4.553095E+00-9.269648E-04-3.080465E+01-9.099163E-04 2.215801E-04

STEP	DOURLED	T	H	NSTEP
7.71558352017E+02	-2.176582988905E+07	3.2629A0322285E+06	3.000000	-3.728897320902E-02
1.00000000000E+00	3.537911412926E+02	2.373231948850E+03	1.000000	-2.497833032549E+04
9.161292664234E+02	-2.112218520003E+07	-3.175314737377E+06	-3.175314737377E+06	-5.806079124474E-02
1.00000000000E+00	-3.725292228421E+02	-2.459571977882E+03	-2.459571977882E+03	2.573654906246E+04
8.505792101379E+02	-2.176031672252E+07	3.282341969531E+06	3.282341969531E+06	-8.851345013359E-02
1.00000000000E+00	3.543221992190E+02	2.373711998480E+03	2.373711998480E+03	-2.498046437024E+04
9.052495437519E+02	-2.111904558180E+07	-3.191441488025E+06	-3.191441488025E+06	-1.089142397749E-01
1.00000000000E+00	-3.764451039999E+02	-2.459571977882E+03	-2.459571977882E+03	2.573654906246E+04
9.497914183555E+02	-2.175484343843E+07	3.301710320733E+06	3.301710320733E+06	-8.255062273435E-02
1.00000000000E+00	3.547775373964E+02	2.373711998480E+03	2.373711998480E+03	-2.498254698085E+04
9.943614921564E+02	2.111597158074E+07	-3.214574854071E+06	-3.214574854071E+06	-9.254330858625E-02
1.00000000000E+00	-3.802618536119E+02	-2.45889786818E+03	-2.45889786818E+03	2.573547481009E+04
1.038895652446E+03	-2.174940212352E+07	3.321068564613E+06	3.321068564613E+06	-3.594279181329E-02
1.00000000000E+00	3.551846390693E+02	2.379099125130E+03	2.379099125130E+03	-2.498458774175E+04
1.083465655387E+03	2.111292961254E+07	-3.233696657703E+06	-3.233696657703E+06	-2.891419523730E-02
1.00000000000E+00	-3.840137775150E+02	-2.447423489211E+03	-2.447423489211E+03	2.573484356653E+04
1.127992265585E+03	-2.174394390575E+07	3.340398114736E+06	3.340398114736E+06	-2.690685863653E-04
1.00000000000E+00	3.556059319688E+02	2.378469780292E+03	2.378469780292E+03	-2.498663224190E+04
1.172562116777E+03	2.110985991176E+07	-3.252795144273E+06	-3.252795144273E+06	4.289666407977E-02
1.00000000000E+00	-3.877669615493E+02	-2.446106012914E+03	-2.446106012914E+03	2.573422081092E+04
1.217081055379E+03	-2.173840712948E+07	3.359694127784E+06	3.359694127784E+06	-2.373125985496E-02
1.00000000000E+00	3.561029584792E+02	2.378167572974E+03	2.378167572974E+03	-2.458873582126E+04
1.261050421331E+03	2.110671163950E+07	-3.271871847250E+06	-3.271871847250E+06	9.209807904329E-02
1.00000000000E+00	-3.915807895113E+02	-2.445278185376E+03	-2.445278185376E+03	2.573385461179E+04

T	H	NSTEP
1303.000000	1.000000	625
-2.120523953293E+07	-5.058055711570E+03	2.816695826715E+01
2.851378919969E+06	3.152604898451E+03	-3.773118593270E+00
4.702934850006E+06	-2.440058016364E+04	-6.204912227728E+00

ALPHA	-1.3623+2841631E-01	-9.088436656835E-03	6.484328686607E-04					
	-1.017212811139E+00	-1.449786187164E-02	4.845908917901E-03					
	3.071118860762E-04	7.194849538475E-06	-1.32293103298866E-06					
DELTA	-2.223629979567E-01	6.923775580704E-02	1.090259254687E-03					
	3.486708901093E-02	-1.07600899338E-02	-1.648846072365E-04					
	-1.029532701896E+00	-1.573248918873E-02	4.892409574229E-03					
BETA	-5.950846829238E-01	2.127862353480E-01	6.238380127628E-03					
	4.991370083584E-01	-2.670819115936E-02	-2.831687948173E-03					
	-4.166991554943E+00	-6.517231652939E-02	1.904434799678E-02					
A7	2.073376608690E-02	-9.399691661485E-03	-9.550779774932E-05					
	1.633897159981E-01	-7.026605970557E-02	-7.787934028991E-04					
	-6.352352055773E-03	-7.178167747321E-03	2.945430374262E-05					
R	2.257114554561E+01	-8.641203558098E+00	-1.469266634679E-01					
	-1.577246371543E+01	1.141847806475E+00	8.041463864869E-02					
	1.256670101207E+02	2.064367198044E+00	-5.882053793044E-01					
V	2.921975565344E+02	-1.160413882949E+02	-2.075062236619E+00					
	-2.102592031205E+02	1.524962195283E+01	1.093134873450E+00					
	1.689179548620E+03	2.854457430755E+01	-7.873182542686E+00					
DRAG	-1.788370615598E-01	8.611654347690E-02	1.902624164764E-03					
	1.512410902734E-01	-1.119862927215E-02	-8.612346895912E-04					
	-1.262497928033E+00	-2.316321440878E-02	5.765712037801E-03					
FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOCENTRICAL	2.908905E+01	2.915696E+01	-3.773118E+00	-6.204916E+00	-2.908805E+01	-1.798890E-02	-1.910441E-03	
ATMOSPHERIC	3.519705E-06	5.741910E-07	-6.553724E-07	3.391798E-06	-1.217397E-08	-3.51301E-06	2.166337E-07	
TOTAL	2.908905E+01	2.916696E+01	-3.773119E+00	-6.204912E+00	-2.908805E+01	-1.799241E-02	-1.910224E-03	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 6.931 SECONDS TO INTEGRATE A SPAN OF 576.0000 MINUTES ***

*** FROM 727.000 TO 1303.000 MINUTES FROM MIDNIGHT OF EPOCH *** 11.2 PP SECS.
ENTER SEGMENT 20 AT 95.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 7.1 CP SECS.**

02SERVATION RESULTS

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RNG	ADJUSTMENT	RNG	ADJUSTMENT	MJD	ST
0050001	1964	8	15	12	10	1.0300	7.2193E+02	RNG	-5.7748E-01	AZ	38623	43000.000
0050001	1964	8	15	12	11	1.0000	-1.3801E+03	RNG	-1.0051E+00	AZ	38623	43860.000
0050001	1964	8	15	12	12	1.0000	-1.2039E+04	RNG	-3.1996E+00	AZ	38623	43920.000
0050001	1964	8	15	12	13	1.0000	-6.0736E+03	RNG	1.2433E+00	AZ	38623	43980.000
0050001	1964	8	15	12	14	1.0000	-3.8208E+03	RNG	5.5980E-01	AZ	38623	44040.000
0050001	1964	8	15	12	15	1.0000	-2.5545E+03	RNG	7.4055E-01	AZ	38623	44100.000
0040001	1964	8	15	12	19	1.0000	-1.7570E+04	RNG	-1.1783E-01	AZ	38623	44340.000
0040001	1964	8	15	12	20	1.0000	-1.7816E+04	RNG	-1.9713E-03	AZ	38623	44400.000
0040001	1964	8	15	12	21	1.0000	-1.3983E+04	RNG	1.4065E-01	AZ	38623	44460.000
0040001	1964	8	15	12	22	1.0000	-7.2058E+03	RNG	1.7872E-01	AZ	38623	44520.000
0040001	1964	8	15	12	23	1.0000	-1.4353E+03	RNG	1.3477E-01	AZ	38623	44580.000
0090001	1964	8	15	15	25	1.0000	-1.2982E+05	RNG	3.4447E+00	AZ	38623	55680.000
0090001	1964	8	15	15	29	1.0000	-4.0641E+04	RNG	3.9272E+00	AZ	38623	55740.000
0090001	1964	8	15	15	30	1.0000	5.8452E+04	RNG	7.9207E+00	AZ	38623	55800.000
0090001	1964	8	15	15	31	1.0000	1.4832E+05	RNG	7.4197E+00	AZ	38623	55860.000
0090002	1964	8	15	16	57	1.0000	-3.5218E+05	RNG	4.9318E+00	AZ	38623	61020.000
0090002	1964	8	15	16	58	1.0000	-2.2774E+05	RNG	7.0022E+00	AZ	38623	61080.000
0090002	1964	8	15	16	59	1.0000	-3.7413E+04	RNG	8.5014E+00	AZ	38623	61140.000
0090002	1964	8	15	17	0	1.0000	1.7160E+05	RNG	7.7989E+00	AZ	38623	61200.000
0090002	1964	8	15	17	1	1.0000	3.2728E+05	RNG	5.5789E+00	AZ	38623	61260.000
0090002	1964	8	15	17	2	1.0000	4.1849E+05	RNG	3.7989E+00	AZ	38623	61320.000
0090003	1964	8	15	18	25	1.0000	-6.8548E+05	RNG	2.8032E+00	AZ	38623	66300.000
0090003	1964	8	15	18	26	1.0000	-6.5811E+05	RNG	4.9128E+00	AZ	38623	66360.000
0090003	1964	8	15	18	27	1.0000	-5.3709E+05	RNG	9.3424E+00	AZ	38623	66420.000
0090003	1964	8	15	18	29	1.0000	-2.2054E+05	RNG	1.9821E+01	AZ	38623	66480.000
0090003	1964	8	15	18	29	1.0000	2.2744E+05	RNG	1.7870E+01	AZ	38623	66540.000
0090003	1964	8	15	18	30	1.0000	5.7607E+05	RNG	8.3089E+00	AZ	38623	66600.000
0090003	1964	8	15	18	31	1.0000	6.5874E+05	RNG	3.9667E+00	AZ	38623	66660.000
0090003	1964	8	15	18	32	1.0000	7.1266E+05	RNG	2.1718E+00	AZ	38623	66720.000
0060001	1964	8	15	18	33	1.0000	-7.159E+05	RNG	1.8713E+00	AZ	38623	66780.000
0060001	1964	8	15	18	34	1.0000	-7.0566E+05	RNG	3.0210E+00	AZ	38623	66840.000
0060001	1964	8	15	18	35	1.0000	-5.6270E+05	RNG	5.8862E+00	AZ	38623	66900.000
0060001	1964	8	15	18	35	1.0000	-4.3949E+05	RNG	1.5855E+01	AZ	38623	66960.000
0060001	1964	8	15	18	37	1.0000	3.2051E+04	RNG	2.9397E+01	AZ	38623	67020.000
0060001	1964	8	15	18	38	1.0000	5.8605E+05	RNG	9.2096E+00	AZ	38623	67080.000

REFERENCE SECTION

DESCRIPTION

ITEM

6 Observation residuals. Each line corresponds to one input observation set or card and contains the station-pass identification in year, month, day, hour, minute, and second; three pairs of measurement residuals and identification; the modified Julian date; and the system time in seconds from midnight

The residuals are the unnormalized differences between the input measurements (modified by bias and/or refraction corrections) and the corresponding values for the same measurement types computed from the integrated trajectory position at the observation time. The observation names are abbreviated as follows:

RNG	Range	CM3	Three-way cumulative doppler
AZ	Azimuth	DOP	Doppler
EL	Elevation	TWD	Two-way doppler
TRA	Topocentric right ascension	SRR	SGLS range rate
TD	Topocentric declination	AX	X-antenna
THA	Topocentric hour angle	AY	Y-antenna
GRA	Geocentric right ascension	CC3	JPL two- or three-way doppler
GD	Geocentric declination	TNT	Tranet doppler
U	u	GCR	Geocenter range difference
V	v	V2	Vehicle-vehicle range
H	Height	V2D	Vehicle-vehicle range rate
X	\bar{x}	S2	Station-vehicle-vehicle range
Y	\bar{y}	S2D	Station-vehicle-vehicle range rate
Z	\bar{z}	S3	Station-vehicle-vehicle-vehicle range
P	P	S3D	Station-vehicle-vehicle-vehicle range rate
Q	Q	V3	Vehicle-vehicle-vehicle range
RD	Range rate	TDA	Time difference of arrival
PD	P rate	TDA	Time of arrival
QD	Q rate	N	Time-of-arrival counter
ACC	Accelerometer		
CM1	One-way cumulative doppler		

0060001	1964	8 15 18 39	3.0000	7.0206E+05	RNG	2.9163E+00	AZ	-5.2355E+00	EL	38623 67140.000
0060001	1964	8 15 18 40	3.0000	7.3429E+05	RNG	1.1680E+00	A7	-3.3719E+00	EL	38623 67200.000
0060001	1964	8 15 18 41	3.0000	7.4494E+05	PNG	5.2410E-01	AZ	-2.4719E+00	EL	38623 67260.000
0090004	1964	8 15 19 54	3.0000	-9.2242E+05	RNG	3.9277E-02	AZ	3.1053E+00	EL	38623 71680.000
0090004	1964	8 15 19 55	3.0000	-9.1014E+05	RNG	-5.0427E-02	AZ	5.2478E+00	EL	38623 71700.000
0090004	1964	8 15 19 56	3.0000	-8.4236E+05	RNG	-8.0807E-01	AZ	1.4012E+01	EL	38623 71700.000
0090004	1964	8 15 19 57	3.0000	-2.1213E+05	RNG	-9.8093E+01	AZ	2.1983E+01	EL	38623 71820.000
0090004	1964	8 15 19 58	3.0000	7.5414E+05	RNG	-3.4655E+00	AZ	-2.1948E+01	EL	38623 71880.000
0090004	1964	8 15 19 59	3.0000	9.8336E+05	RNG	-1.2950E+00	AZ	-7.2931E+00	EL	38623 71940.000
0090004	1964	8 15 20 0	3.0000	9.1358E+05	RNG	-7.5093E-01	AZ	-4.0585E+00	EL	38623 72000.000
0090004	1964	8 15 20 1	3.0000	9.2012E+05	RNG	-5.3110E-01	AZ	-2.9022E+00	EL	38623 72060.000
0060002	1964	8 15 20 2	3.0000	-6.5857E+05	RNG	-6.0141E+00	AZ	1.6043E+00	EL	38623 72120.000
0060002	1964	8 15 20 3	3.0000	-5.1788E+05	RNG	-8.1363E+00	AZ	1.4180E+00	EL	38623 72120.000
0060002	1964	8 15 20 4	3.0000	-3.0667E+05	RNG	-1.0234E+01	AZ	8.5309E-01	EL	38623 72120.000
0060002	1964	8 15 20 5	3.0000	-4.0119E+04	RNG	-1.1161E+01	AZ	-1.0546E-01	EL	38623 72300.000
0060002	1964	8 15 20 6	3.0000	2.2402E+05	RNG	-1.0283E+01	A7	-1.0364E+00	EL	38623 72360.000
0060002	1964	8 15 20 7	3.0000	4.3282E+05	RNG	-8.3794E+00	AZ	-1.5689E+00	EL	38623 72420.000
0090005	1964	8 15 21 22	3.0000	-1.0705E+06	RNG	-3.6137E+00	AZ	3.1091E+00	EL	38623 76920.000
0090005	1964	8 15 21 24	3.0000	-8.6449E+05	RNG	-1.4787E+01	A7	6.6335E+00	EL	38623 77040.000
0090005	1964	8 15 21 25	3.0000	-3.6017E+05	RNG	-3.2194E+01	AZ	5.1185E+00	EL	38623 77100.000
0090005	1964	8 15 21 26	3.0000	4.5302E+05	RNG	-2.7804E+01	A7	-6.4851E+00	EL	38623 77160.000
0090005	1964	8 15 21 27	3.0000	8.7611E+05	RNG	-1.2828E+01	AZ	-6.4116E+00	EL	38623 77220.000
0090005	1964	8 15 21 28	3.0000	1.0081E+06	RNG	-6.4230E+00	AZ	-4.3884E+00	EL	38623 77280.000
0010001	1964	8 15 21 33	3.0000	-1.0512E+06	RNG	3.8996E+00	AZ	2.7464E+00	EL	38623 77580.000
0010001	1964	8 15 21 34	3.0000	-1.0094E+06	RNG	6.0810E+00	AZ	3.4880E+00	EL	38623 77640.000
0010001	1964	8 15 21 35	3.0000	-9.0848E+05	PNG	1.0721E+01	AZ	4.8261E+00	EL	38623 77700.000
0010001	1964	8 15 21 36	3.0000	-6.3781E+05	RNG	2.1169E+01	AZ	5.9965E+00	EL	38623 77760.000
0010001	1964	8 15 21 37	3.0000	-1.9800E+03	RNG	3.1735E+01	AZ	-7.3969E-01	EL	38623 77820.000
0010001	1964	8 15 21 38	3.0000	6.7253E+05	RNG	2.0250E+01	AZ	-8.5494E+00	EL	38623 77880.000
0010001	1964	8 15 21 39	3.0000	9.6476E+05	RNG	9.2024E+00	AZ	-6.7311E+00	EL	38623 77940.000
0010001	1964	8 15 21 40	3.0000	1.0652E+06	RNG	4.5307E+00	AZ	-4.7156E+00	EL	38623 78000.000

TOTAL FIT SUMMARY

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
001	8 RNG	8.6E+03	-1.1E+05	1.3E+01	8 EL	5.2E+00	5.2E+01	-4.6E-01
004	5 PNG	1.3E+04	-1.2E+04	6.5E-02	5 EL	1.4E-01	1.4E+00	-1.4E-01
005	6 PNG	6.0E+03	-4.3E+03	-4.4E-01	6 EL	2.2E-01	2.2E+00	-1.2E-01
006	15 PNG	5.6E+05	-4.0E+04	1.0E+00	15 EL	4.3E+00	4.3E+01	-4.8E-01
009	33 PNG	6.4E+05	3.4E+03	-2.6E+00	33 EL	6.9E+00	6.9E+01	1.1E-01

EVENT SEGMENT 30 AT 97.1 SECONDS. EXECUTION TIME FOR SEGMENT 20 WAS 1.8 CP SECS., 9.8 PP SECS.

REFERENCE
SECTION

2.2.4

DESCRIPTION

ITEM

7 Edit summary. The RMS of the residuals for each measurement type from each station is computed by the residuals editor. Included in the printout are the station identification, the number of residuals included in the RMS (i.e., the total number for that station and type minus the number deleted by the editor on this iteration), the RMS, the RMS divided by the input weighting sigma, and the mean value of the residuals. The measurement type indicators are the same as those used for residuals (Item 6)

Because of storage constraints, the residuals editor accumulates residuals and makes editing checks only for the first 6 measurement types for the first 30 stations

ITERATION NUMBER 10
 201 OBSERVATIONS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS BEST SO FAR
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	ROUND	NEW VALUE	SIGMA
0001 ALPHA	3.514999399396E+02	3.29208724E-01	1.00000000E+00	3.51829208723932E+02	1.25190034E-04
0001 DELTA	0.	1.13160500E-01	1.00000000E+00	1.13160499953416E-01	2.10518024E-04
0001 BETA	9.0004993993992E+01	-2.26835100E-01	1.00000000E+00	8.97781648996747E+01	9.1989685E-05
0101 AZ	3.544999399396E+02	6.64006620E-02	1.00000000E+00	3.54566400661983E+02	7.31252969E-05
0001 R	2.1359993999998E+07	-1.23030329E+04	1.00000000E+05	2.13476969170890E+07	5.73271117E+01
0001 V	2.585599399399E+04	-5.17544231E-01	1.00000000E+08	2.58554824557692E+04	7.08926739E-02
0001 DRAG	1.0000000000000E-02	-8.77565717E-03	1.00000000E-02	1.22434282701928E-03	8.45819835E-06

CORRECTIONS HITTING ROUNDS. 5 ITERATIONS USED IN FINDING Z

RMS FOR THIS SOLUTION = 3.4716713914E+03

PREDICTED RMS FOR NEXT SOLUTION = 4.8322106976E+02

XT((ATA)X) = 2.37501378E+09 XT(ATB) = 2.37561893E+09 RATIO = 9.99745266E-01

CORRELATION MATRIX DETERMINANT = 7.26217525E-07

0001 ALPHA	0001 DELTA	0001 BETA	0001 AZ	0001 R	0001 V	0001 DRAG
1.000000000						
.177635916	1.000000000					
-.122165667	-.533863245	1.000000000				
.460579679	.205133632	-.234238491	1.000000000			
.169899883	.850313741	-.615787104	.161605940	1.000000000		
-.167862861	-.845366506	.632669139	-.162982940	-.999457463	1.000000000	
.165362253	.443753863	.054309304	.072642556	.406561987	-.378326785	1.000000000

ENTER SEGMENT 40 AT 97.3 SECONDS. EXECUTION TIME FOR SEGMENT 30 WAS .2 CP SECS., 2.6 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
8	Iteration number. TRACE makes the differential correction, or orbit determination, by computing a series of differential corrections of the parameters selected by the user. The iteration number is advanced each time a set is recomputed and indicates the number of times the orbit determination algorithm has been performed	2.2.2
9	Observation count. The number of individual measurements included in the current (best) least squares computation is indicated	2.2.2
10	Convergence indicator. If the weighted RMS for all residuals is less than that for any previous iteration, the correction process is converging, and the message shown is printed. If the current RMS is greater than the smallest RMS obtained on previous iterations, the message CURRENT ITERATION IS NOT GOOD (SOS X.XXXXXXXXE+XX) is printed at this point.	2.2.2
11	The current solution is shown, one parameter per line, starting with the name (Item 4). If the iteration has been successful (i.e., if the overall RMS has been lowered), the current value is the parameter value used in the iteration, partial derivatives, and residuals computations just completed. For the first iteration, it is the input value of the parameter. If an iteration is had, the value produced for the lowest RMS is recovered from memory and is printed as the current value	2.2.3
12	The correction, the solution of the system of normal equations associated with the current (best) iteration, is also shown on the line, as is the bound, the current value of the number used to limit the correction size. In general, these bounds are automatically increased on a good iteration and decreased on a bad one. The last two columns contain the new value (correct value plus correction) to be used for the next iteration and the a priori sigma for the parameter	
13	Indications that the correction sizes have been controlled by solving the system so that the constraint of the bounds is satisfied. The number of iterations to determine the Lagrange multiplier λ is also shown. If the normal equations were solved without applying the bounds, nothing would be printed at this point	
14	RMS. The quantity to be minimized in the differential correction process is the RMS of the normalized residuals for the current iteration	
15	Predicted RMS. If the fitting process is converging in a completely linear manner, this will be the RMS on the next iteration; it may be compared with the current RMS (Item 13) to measure the degree to which the process has already converged	
16	The equation being solved is $A^T W \Delta P = A^T W B$; therefore, the solution should also satisfy $\Delta P^T A^T W \Delta P = \Delta P^T A^T W B$. By comparing the ratio of the two sides of the preceding equation to 1, an estimation of the quality of the matrix inversion may be obtained and, implicitly, of the normal matrix conditioning. This comparison is valid only when bounds are not hit	
17	Determinant of the correlation matrix Correlation matrix, the correlation coefficients for the parameter set. These values are computed directly from the covariance matrix (i.e., the inverse normal matrix). Row sequence is the same as column sequence	

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMOLY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMOLY	PERIGEE HEIGHT
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HFLIGHT	ZDOT	VELOCITY	TAU	PSI	NOJAL PERIOD	U-DOT
1964/ 8/16	21130951.239	151.829208313	21646835.097	.0131185024774	15.42829991	3613.73818
12/ 7	-3034021.391	.113160500	.01455106322	-.0058187548808	15.65011327	170.65518
0.0000000	42162.172	89.778164900	95.433588709	.0674961437126	15.87348122	3511.48367
.1139230	-299.1917405	354.566400251	351.839972422	351.500462446	88.8339674	68.40067
205.1635851	-2430.4413683	21347636.917	344.240189981	-.15608012581	69.0346349	.8384569822
69.4456	25739.2581881	25955.4924559	723.1903256	1.04849975398	88.9701739	-4.2288007596

(10)

ENTER SEGMENT 10 AT 97.5 SECONDS. EXECUTION TIME FOR SEGMENT 40 WAS .2 CP SECS., 8.4 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

IVFP	0	ICENT	1	TDJAG	1	ALPHG	5.6621627703E+00	CDAM	1.224342827E-03
JVFP	0	JNORM	1	IP	8	ALS-DEG	3.244180258E+C2	ER	1.000000000E-10
MVFP	0	MAJOR	1	ISRP	0	TDATE	2.438423500E+06	HMIN	2.000000000E+00
KVFP	7	MASS	0	NEQS	24	TSTART	7.270000000E+02	HMAX	2.000000000E+00
LVFP	0	VT	4	RFMP	0	TSTOP	1.303000000E+03	H0	2.000000000E+00
ICENTX	1	JNORMX	0	NMASSX	0	FLIGHT	5.760000000E+02	NTX	0.
				NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

PREDETERMINED EVENT TABLE *

ASSOCIATED QUANTITIES

TIME(MME) TYPE

727.0000 TZFR0

1303.0000 TSTOP

*** TRAJECTORY START

* * * * * ECI * * * * *

SEG11 ENTRY TIME IS 97.69200

T = 727.00000 4 = .25000 NSTEP = 0

2.113015123784E+07 -2.991917404612E+02

-3.034021390711E+06 -2.430441368898E+03

4.216217155988E+04 2.5739255018813E+04

-3.052702432160E+01 -4.382852174980E+00

-5.077158946111E-02

REFERENCE
SECTION

DESCRIPTION

ITEM

18 Initial conditions and characteristics for the next iteration are fully explained in the epoch print (Item 42) of the previous case

Preceding page blank

ALPHA	1.449839349170E-01	6.968761729401E-03	-7.538634032513E-04
	1.009315734373E+00	0.	-5.251821922072E-03
	0.	0.	5.072796977429E-10
DELTA	-1.994334437437E-03	-7.305254656714E-02	1.013851645742E-05
	2.863518731332E-04	1.048902088855E-02	-1.455639639366E-06
	1.020152593830E+00	1.41271815228F-04	-5.288997732691E-03
BETA	0.	-7.338613986721E-02	2.910517841894E-08
	0.	1.050946047628E-02	-4.167985675079E-09
	0.	1.393241626287F-04	-5.589291141101E-11
AZ	0.	1.047523697341E-02	-4.189457598863E-09
	0.	7.305409839516E-02	-2.924014878256E-08
	0.	7.019930643232E-03	-1.055755549733E-09
R	9.898458823081E-01	0.	1.027953859891E-02
	-1.4217+0615554E-01	0.	-1.478110678485E-03
	1.975022023389E-03	0.	3.530004569560E-05
V	0.	-1.157169435817E-02	1.249910573710E-08
	0.	-9.400100628776F-02	9.763856698058E-08
	0.	9.955048501873F-01	-7.860128671986F-07
DRAG	0.	0.	4.833824156621E-07
	0.	0.	3.688586245117F-06
	0.	0.	-2.390669173616E-05

FOPCF5	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
50POTENTIAL	3.084011E+01	-3.052703E+01	4.382825E+00	-6.050145E-02	-3.084011E+01	3.353382E-04	2.680478E-04	
ATMOSPHERIC	1.721854E-04	3.440109E-06	2.625072E-05	-1.701378E-04	-6.617043E-07	-1.718791E-04	-1.024360E-05	
TOTAL	3.084011E+01	-3.052702E+01	4.382825E+00	-6.077155E-02	-3.084011E+01	1.634510E-04	2.578042E-04	

* STEP	DOUBLED	T =	737.000000	H =	.500000	NSTEP =	39
* STEP	COUPLED	T =	752.500000	H =	1.000000	NSTEP =	69
NOFF	T =	7.716776901297E+02	-2.174592635526E+07	3.128044651412E+06	6.185382931127E-02		
NOFF	DT =	1.000000000000E+00	4.363066598235E+02	2.341032215047E+03	-2.501100242896E+04		
NOFF	DT =	8.159439381329E+02	2.11280778157E+07	-3.048921452957E+06	-8.866507996913E-03		
NOFF	DT =	1.000000000000E+00	-2.531640793088E+02	-2.437807435119E+03	2.573986349851E+04		

NODE	T =	8.606439784349E+02	-2.174307672354E+07	3.147574109853E+06	6.346098681070E-02
DT =		1.00000000000E+00	4.36748958501E+02	2.341259412302E+03	-2.501098063800E+04
NODE	T =	9.049131125587E+02	2.112480922144E+07	-3.067826874256E+06	-3.145602691736E-02
DT =		1.00000000000E+00	-2.4570751312713E+02	-2.437496916786E+03	2.574034521037E+04
NODE	T =	9.496885345421E+02	-2.17402795561E+07	3.167115480898E+06	4.721287274225E-02
DT =		1.00000000000E+00	4.371065454945E+02	2.340923513896E+03	-2.501069558271E+04
NODE	T =	9.934809223146E+02	-2.112160903266E+07	-3.086737009615E+06	-5.239012997875E-02
DT =		1.00000000000E+00	-2.609021288274E+02	-2.436611339646E+03	2.574174086916E+04
NODE	T =	1.038572072318E+03	-2.173752250007E+07	3.186650039577E+06	2.199408100714E-02
DT =		1.00000000000E+00	4.374054250921E+02	2.340136156310E+03	-2.501146135307E+04
NODE	T =	1.082847949403E+03	2.111844585457E+07	-3.105634339711E+06	-6.394101090157E-02
DT =		1.00000000000E+00	-2.646769896776E+02	-2.435406338572E+03	2.574108312266E+04
NODE	T =	1.127534984272E+03	-2.173475444553E+07	3.206160942905E+06	6.063245481935E-03
DT =		1.00000000000E+00	4.377056630312E+02	2.339242337792E+03	-2.501022625244E+04
NODE	T =	1.171814315422E+03	2.111526079807E+07	-3.124507502435E+06	-8.281088097144E-02
DT =		1.00000000000E+00	-2.684624881963E+02	-2.434319116268E+03	2.571143064371E+04
NODE	T =	1.216497109383E+03	-2.173191504376E+07	3.225642388976E+06	1.371241885715E-06
DT =		1.00000000000E+00	4.380669398760E+02	2.338670267869E+03	-2.501004494494E+04
NODE	T =	1.260779610736E+03	2.111200155498E+07	-3.1433357829477E+06	-9.02722714295E-02
DT =		1.00000000000E+00	-2.723159956769E+02	-2.433715456936E+03	2.574183413167E+04

T = 1303.500000 I = 1.000000 NSTEP = 620

ALPHA		-2.158139373011E+07	-2.9365601441066E+03	2.857982166037E+01	6.694580358838E-04
		2.941512320333E+06	2.820751815171E+03	-3.8495256328281E+00	4.916945383847E-03
		2.928945390395E+06	-2.478242573033E+04	-3.8667091391020E+00	-1.632595318533E-06
		-1.405703253351E-01	-8.112355054985E-03	6.694580358838E-04	6.574985670973E-04
		-1.031332567536E+00	-6.414333182920E-03	4.916945383847E-03	-1.00964314532E-04
		3.631775022101E-04	5.226738622887E-06	-1.632595318533E-06	4.977361441106F-03
DELTA		-1.387890212820E-01	7.056569936537E-02	6.574985670973E-04	3.662521752306E-03
		2.12973468308E-02	-1.054634674355E-02	-1.00964314532E-04	-2.315171961345E-03
		-1.047049174250E+00	-9.559078210560E-03	4.977361441106F-03	1.832581016705E-02
BETA		-3.140554057470E-01	1.967200090466E-01	3.662521752306E-03	-3.906947413612E-05
		4.237426207680E-01	-2.575880859943E-02	-2.315171961345E-03	-3.846045274812F-04
		-3.917007913912E+00	-3.740467308669E-02	1.832581016705E-02	7.587327516339E-05
AZ		9.128512328766E-03	-8.972395236228E-03	-3.906947413612E-05	
		8.055012853788E-02	-7.104564900142E-02	-3.846045274812F-04	
		-1.608908734680E-02	-7.046327340826E-03	7.587327516339E-05	

R 1.144856139165E+01
 -1.359557914992E+01
 1.233937145524E+02

V 1.452254490322E+02
 -1.862350275205E+02
 1.708391085917E+03

DRAG -9.783352270257E-02
 1.920342549582E-01
 -1.842454554114E+00

-6.503537251800E+00
 1.144803978440E+00
 1.296812247239E+00

-1.176498466858E+02
 1.574794788511E+01
 1.867705432857E+01

1.255966284188E-01
 -1.663381409215E-02
 -2.315265667377E-02

-1.009066847643E-01
 7.112715583158E-02
 -5.802838680332E-01

-1.520343930412E+00
 1.000672309522E+00
 -8.008410938828E+00

2.186118776008E-03
 -1.149855285102E-03
 8.525382604848E-03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 2.910213E+01 2.857983E+01 -3.895257E+00 -3.867892E+00 -2.910213E+01 -1.142734E-02 -1.238510E-03
 ATMOSPHERIC 4.495445E-07 4.833679E-08 -7.803580E-08 4.400730E-07 7.376945E-10 -4.486663E-07 2.807590E-08
 TOTAL 2.910213E+01 2.857983E+01 -3.895257E+00 -3.867892E+00 -2.910213E+01 -1.142734E-02 -1.238510E-03

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 6.885 SECONDS TO INTEGRATE A SPAN OF 576.500 MINUTES ***
 *** FROM 727.000 TO 1303.500 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 20 AT 104.5 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 7.0 CP SECS., 11.3 PP SECS.

OBSERVATION RESIDUALS

ST APASS	YEAR	MO	DY	HR	MIN	SEC	RNG	AZ	EL	MJD	ST
0050001	1964	8	16	12	10	0.0000	2.2688E+04	AZ	-3.3328E-01	38623	43800.000
0050001	1964	8	15	12	11	0.0000	1.7605E+04	AZ	-8.0831E-01	38623	43860.000
0050001	1964	8	15	12	12	0.0000	-6.9197E+03	AZ	-4.2212E+00	38623	43920.000
0050001	1964	8	15	12	13	0.0000	-2.2796E+04	AZ	-1.0205E+00	38623	43980.000
0050001	1964	8	15	12	14	0.0000	-1.5651E+04	AZ	-6.6809E-01	38623	44040.000
0050001	1964	8	15	12	15	0.0000	-1.1783E+04	AZ	-5.1925E-01	38623	44100.000
0040001	1964	8	15	12	19	0.0000	3.0133E+04	AZ	-9.5596E-01	38623	44340.000
0040001	1964	8	15	12	20	0.0000	4.3115E+04	AZ	-1.3543E+00	38623	44400.000
0040001	1964	8	15	12	21	0.0000	5.8001E+04	AZ	-1.6029E+00	38623	44460.000

0940001	1964	8	15	12	22	0.0000	6.5667E+04	RNG	9.8096E-02	AZ	-1.4357E+03	EL	38623	44520.000
0040001	1964	8	15	12	23	0.0000	6.8526E+04	RNG	-1.075E-01	AZ	-1.1507E+00	EL	38623	44580.000
0090001	1964	8	16	15	28	0.0000	-6.1804E+03	RNG	3.0265E-01	AZ	-8.0133E-01	EL	38623	55680.000
0090001	1964	8	16	15	29	0.0000	-6.8573E+03	RNG	3.8295E-01	AZ	-8.4310E-01	EL	38623	55740.000
0090001	1964	8	16	15	30	0.0000	-2.751E+03	RNG	4.8660E-01	AZ	-8.4095E-01	EL	38623	55800.000
0090001	1964	8	16	15	31	0.0000	5.2159E+03	RNG	4.8157E-01	AZ	-7.9229E-01	EL	38623	55860.000
0090002	1964	8	15	16	57	0.0000	1.5211E+03	RNG	1.1618E-01	AZ	-1.0148E+00	EL	38623	61020.000
0090002	1964	8	16	16	58	0.0000	-8.432E+03	RNG	1.4345E-01	AZ	-1.1552E+00	EL	38623	61080.000
0090002	1964	8	16	16	59	0.0000	-1.3588E+04	RNG	2.1954E-01	AZ	-1.2119E+00	EL	38623	61140.000
0090002	1964	8	15	17	0	0.0000	-1.0744E+04	RNG	3.0655E-01	AZ	-1.1336E+00	EL	38623	61200.000
0090002	1964	8	15	17	1	0.0000	-2.2753E+03	RNG	3.5173E-01	AZ	-9.7480E-01	EL	38623	61260.000
0090002	1964	8	15	17	2	0.0000	7.9316E+03	RNG	3.6114E-01	AZ	-8.1401E-01	EL	38623	61320.000
0090003	1964	8	16	18	25	0.0000	2.0690E+04	RNG	1.9155E-01	AZ	-1.0434E+00	EL	38623	66300.000
0090003	1964	8	15	18	26	0.0000	6.5799E+03	RNG	1.6134E-01	AZ	-1.3569E+00	EL	38623	66360.000
0090003	1964	8	15	18	27	0.0000	-1.1036E+04	RNG	9.5496E-02	AZ	-1.0453E+00	EL	38623	66420.000
0090003	1964	8	15	18	28	0.0000	-2.882E+04	RNG	2.1144E-02	AZ	-2.2312E+00	EL	38623	66480.000
0090003	1964	8	15	18	29	0.0000	-2.6325E+04	RNG	1.2254E-01	AZ	-1.9183E+00	EL	38623	66540.000
0090003	1964	8	15	18	30	0.0000	-1.1609E+04	RNG	2.1121E-01	AZ	-1.3912E+00	EL	38623	66600.000
0090003	1964	8	15	18	31	0.0000	1.8438E+03	RNG	2.4202E-01	AZ	-1.0271E+00	EL	38623	66660.000
0090003	1964	8	15	18	32	0.0000	1.3232E+04	RNG	2.5305E-01	AZ	-7.9993E-01	EL	38623	66720.000
0060001	1964	8	16	18	33	0.0000	-7.6649E+04	RNG	-7.9060E-02	AZ	-5.3474E-01	EL	38623	66780.000
0060001	1964	8	15	18	34	0.0000	-8.8371E+04	RNG	-9.8217E-02	AZ	-5.9088E-01	EL	38623	66840.000
0050001	1964	8	16	18	35	0.0000	-1.0111E+05	RNG	1.1402E-02	AZ	-5.5867E-01	EL	38623	66900.000
0060001	1964	8	15	18	36	0.0000	-1.0593E+05	RNG	1.1116E+00	AZ	-4.8510E-04	EL	38623	66960.000
0060001	1964	8	16	18	37	0.0000	-4.1937E+04	RNG	3.7652E+00	AZ	-1.5507E+00	EL	38623	67020.000
0060001	1964	8	15	18	38	0.0000	3.2485E+04	RNG	2.1183E+00	AZ	-1.8628E+00	EL	38623	67080.000
0060001	1964	8	15	18	39	0.0000	6.4311E+04	RNG	1.2775E+00	AZ	-1.235E+00	EL	38623	67140.000
0060001	1964	8	16	18	40	0.0000	8.1036E+04	RNG	9.1514E-01	AZ	-8.3730E-01	EL	38623	67200.000
0060001	1964	8	15	18	41	0.0000	9.2000E+04	RNG	7.2426E-01	AZ	-6.2982E-01	EL	38623	67260.000
0090004	1964	8	15	19	54	0.0000	9.9279E+03	RNG	4.3546E-01	AZ	-1.2301E+00	EL	38623	71640.000
0090004	1964	8	16	19	55	0.0000	-8.4590E+03	RNG	5.2603E-01	AZ	-1.7714E+00	EL	38623	71700.000
0090004	1964	8	15	19	56	0.0000	-4.2404E+04	RNG	7.3920E-01	AZ	-2.8249E+00	EL	38623	71760.000
0090004	1964	8	15	19	57	0.0000	-8.3158E+04	RNG	-1.8402E-01	AZ	-1.1511E+00	EL	38623	71820.000
0090004	1964	8	15	19	58	0.0000	-3.2978E+04	RNG	1.6402E-01	AZ	-2.2512E+00	EL	38623	71880.000
0090004	1964	8	15	19	59	0.0000	-7.7099E+03	RNG	3.8521E-03	AZ	-1.4418E+00	EL	38623	71940.000
0090004	1964	8	16	20	0	0.0000	7.3660E+03	RNG	8.2113E-02	AZ	-1.0324E+00	EL	38623	72000.000
0090004	1964	8	15	20	1	0.0000	2.0179E+04	RNG	1.2390E-01	AZ	-8.0225E-01	EL	38623	72060.000
0060002	1964	8	15	20	2	0.0000	-4.1328E+04	RNG	-5.1514E-01	AZ	-6.0920E-01	EL	38623	72120.000
0060002	1964	8	15	20	3	0.0000	-2.7966E+04	RNG	-7.4698E-01	AZ	-7.0650E-01	EL	38623	72180.000
0060002	1964	8	15	20	4	0.0000	-4.9266E+03	RNG	-9.2915E-01	AZ	-8.1586E-01	EL	38623	72240.000
0060002	1964	8	15	20	5	0.0000	2.5070E+04	RNG	-9.3451E-01	AZ	-8.9165E-01	EL	38623	72300.000
0060002	1964	8	15	20	6	0.0000	5.4716E+04	RNG	-7.5543E-01	AZ	-8.8289E-01	EL	38623	72360.000
0060002	1964	8	15	20	7	0.0000	7.8674E+04	RNG	-5.1917E-01	AZ	-8.0346E-01	EL	38623	72420.000

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
0090005	1964	8 15 21 22	1.0070	-6.6495E+03	RNG	5.5421E-01	A7	5.5421E-01	A7	-1.0323E+00	EL	38623 76920.000
0090005	1964	8 15 21 23	1.0000	-2.4423E+04	RNG	6.1460E-01	AZ	6.1460E-01	AZ	-1.3509E+00	EL	38623 76980.000
0090005	1964	8 15 21 24	1.0000	-4.7316E+04	RNG	5.6663E-01	A7	5.6663E-01	A7	-1.7762E+00	EL	38623 77040.000
0090005	1964	8 15 21 25	1.0000	-6.0912E+04	RNG	-9.2395E-02	AZ	-9.2395E-02	AZ	-2.0151E+00	EL	38623 77100.000
0090005	1964	8 15 21 26	1.0000	-3.5964E+04	RNG	-4.7476E-01	A7	-4.7476E-01	A7	-1.9000E+00	EL	38623 77160.000
0090005	1964	8 15 21 27	1.0000	-8.7365E+04	RNG	-2.9727E-01	AZ	-2.9727E-01	AZ	-1.4333E+00	EL	38623 77220.000
0090005	1964	8 15 21 28	1.0000	1.0382E+04	RNG	-1.4865E-01	A7	-1.4865E-01	A7	-1.0030E+00	EL	38623 77280.000
0010001	1964	8 15 21 33	1.0000	-1.1744E+05	RNG	2.5720E-02	A7	2.5720E-02	A7	-3.7427E-01	EL	38623 77580.000
0010001	1964	8 15 21 34	1.0000	-1.2718E+05	RNG	1.5447E-01	A7	1.5447E-01	A7	-3.6870E-01	EL	38623 77640.000
0010001	1964	8 15 21 35	1.0000	-1.3317E+05	RNG	5.8531E-01	AZ	5.8531E-01	AZ	-2.7821E-01	EL	38623 77700.000
0010001	1964	8 15 21 36	1.0000	-1.1933E+05	RNG	1.9884E+00	A7	1.9884E+00	A7	-1.2593E-01	EL	38623 77760.000
0010001	1964	8 15 21 37	1.0000	-5.0370E+04	RNG	3.5855E+00	AZ	3.5855E+00	AZ	-9.2945E-01	EL	38623 77820.000
0010001	1964	8 15 21 38	1.0000	2.3855E+04	RNG	2.4054E+00	A7	2.4054E+00	A7	-1.4173E+00	EL	38623 77880.000
0010001	1964	8 15 21 39	1.0000	7.4482E+04	RNG	1.8260E+00	AZ	1.8260E+00	AZ	-1.1119E+00	EL	38623 77940.000
0010001	1964	8 15 21 40	1.0000	9.8614E+04	RNG	1.2881E+00	A7	1.2881E+00	A7	-8.7896E-01	EL	38623 78000.000

TOTAL EDIT SUMMARY

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN			
001	8	RNG	1.0E+05	1.0E+03	-4.3E+04	8	AZ	7.0E+00	2.0E+01	1.5E+00	8	EL	8.0E-01	8.0E+00	-6.8E-01
004	5	RNG	5.5E+04	5.5E+02	5.3E+04	5	AZ	7.2E-01	7.2E+00	5.4E-01	5	EL	1.3E+00	1.3E+01	-1.3E+00
005	6	RNG	1.7E+04	1.7E+02	-3.0E+03	6	AZ	4.5E+00	4.5E+01	1.1E+00	6	EL	1.8E+00	1.8E+01	-1.3E+00
006	15	RNG	6.8E+04	6.8E+02	-4.0E+03	15	AZ	1.3E+00	1.3E+01	3.6E-01	15	EL	9.4E-01	9.4E+00	-8.3E-01
009	33	RNG	2.6E+04	2.6E+02	-1.2E+04	33	AZ	3.6E-01	3.6E+00	1.9E-01	33	EL	1.4E+00	1.4E+01	-1.3E+00

ENTER SEGMENT 30 AT 106.3 SECONDS. EXECUTION TIME FOR SEGMENT 20 WAS 1.7 CP SECS., 10.0 PP SECS.
 ITERATION NUMBER 2
 201 OBSERVATIONS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS BEST SO FAR
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	BOUND	NEW VALUE	SIGMA
PHI	3.51829203723992E+02	-2.26699461E-01	1.500000000E+00	3.51602509263401E+02	1.20826357E-04
DELTA	1.13160493953416E-01	-1.05599386E-01	1.500000000E+00	7.56111375938326E-03	2.02968458E-04
BETA	8.9778164198747E+01	2.15475537E-01	1.500000000E+00	8.99936404363975E+01	8.98199728E-05
AZ	1.54566400661983E+02	-9.16232540E-02	1.500000000E+00	3.54474777407950E+02	7.36258673E-05
R	2.13476963170890E+07	5.46936314E+03	1.500000000E+05	2.13531662862318E+07	5.47662656E+01
V	2.58554824557692E+04	-2.40599258E+00	1.500000000E+01	2.58530764631926E+04	6.77420654E-02
DRAG	1.22434282701928E-03	8.29721686E-03	1.500000000E-02	9.521555968620821E-03	6.02311948E-06

RMS FOR THIS SOLUTION = 3.0655522444E+02

PREDICTED RMS FOR NEXT SOLUTION = 9.7959735872E+00

XT((ATA)X) = 1.68699091E+07 XT(ATB) = 1.8899091E+07 RATIO = 1.00000000E+00

CORRELATION MATRIX DETERMINANT = 8.39750581E-07

	0001	0001	0001	0001	0001	0001	0001
ALPHA	DELTA	BETA	AZ	R	V	DRAG	
1.000000000							
.126707585	1.000000000						
-.095784306	-.524526749	1.000000000					
.469347141	.172114292	-.281620817	1.000000000				
.105068389	.937164667	-.604628379	.113595954	1.000000000			
-.103952302	-.931937276	.621176562	-.115757975	-.999467638	1.000000000		
.009335237	-.329558072	.591698927	-.090391574	-.511015911	.536627303	1.000000000	

ENTER SEGMENT 40 AT 106.4 SECONDS. EXECUTION TIME FOR SEGMENT 30 WAS .2 CP SECS., 2.7 PP SECS.
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. ***

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMOLY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMOLY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	U-DOT
HEIGHT	ZDOT	VELOCITY	TAU	SI	NODAL PERIOD	
1964/ 8/16	21124233.035	351.602508852	21653940.572	.0137249932016	.45143749	3613.28299
12/ 7	-3118410.042	.007561114	.01389049192	-.0021378323792	.45779644	169.35013
0.0000000	2817.893	99.993640436	35.925222544	.0674629243904	.46420017	3514.27767
.0076121	-364.0479416	354.474776997	351.603240608	351.598074400	88.9377396	70.34480
204.9368856	-2462.4712545	21353156.286	359.543396168	-.16083438689	89.0784160	.8515526064
70.3456	25732.9607125	25853.0764632	726.8884727	1.08959477675	89.0140698	-4.2171134077

END OF LEAST SQUARES PROCESS - MAXIMUM ITERATIONS (2) REACHED. (10)

REFERENCE
SECTION

DESCRIPTION

ITEM

2.2.2

19 Indication of the reason for ending the least-squares process. In this case, it was because the maximum number of iterations had been reached. Other reasons for ending the process could be convergence or the lack of additional computer running time

R -3.04E+05	1	0	3.04E+05
A -5.92E+00		0	5.92E+00
F -2.43E+00		0	2.43E+00
77590+	R	A	0010001
77595			
77610			
77625	R	E	0010001
77640			
77655			
77670			
77695	R	E	0010001
77700			
77715			
77730			
77745			
77760	R	E	0010001
77775			
77790			
77805			
77820			
77835			
77850			
77865			
77880			
77895			
77910			
77925			
77940			
77955			
77970			
77985			
78000			
78015			
78030			
78045			
78060			
78075			
78090			
78105			
78120			
78135+			



REFERENCE SECTION

DESCRIPTION

ITEM

2.2.1
11.1.2
15

20 An example of the printer plot of the measurement residuals for the last iteration if GPLOT is input ≠ 0. Its order is by station input, then by measurement encounter.

Each page contains a maximum of six different measurements for a station. The first six, or fewer, lines contain the measurement type identifiers and the ranges of the residuals (the maximum negative value, a zero, and the maximum positive value) for the measurement types encountered first. The first line also has the VEHID printed between the maximum negative value and the zero. The identifiers and corresponding measurements are shown as follows (note that since only one character can be used as an identifier, some are repeated):

R	Range	3	Three-way cumulative doppler
A	Azimuth	*	Range rate
E	Elevation	*	Doppler
1	Topocentric right ascension	*	Two-way doppler
2	Topocentric declination	S	SGLS range rate
3	Topocentric hour angle	+	X-antenna
4	Geocentric right ascension	-	Y-antenna
5	Geocentric declination	J	JPL two- or three-way doppler
U	u	T	Tranet doppler
V	v	G	Geociever range difference
H	Height	V	Vehicle-vehicle range
X	x	+	Vehicle-vehicle range rate
Y	y	2	Station-vehicle-vehicle range
Z	z	-	Station-vehicle-vehicle range rate
R	Range	3	Station-vehicle-vehicle-vehicle range
P	P)	Station-vehicle-vehicle-vehicle range rate
Q	Q	(Vehicle-vehicle-vehicle range
D	Range rate	D	Time difference of arrival
7	P rate	O	Time of arrival
8	Q rate		
9	Accelerometer		
1	One-way cumulative doppler		

The left-hand column contains the system time in sec, incremented by GPLOT(2); the measurement identifiers are used to show the placement of the residual. In the far right-hand margin, the station-pass identification is shown.


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MODEL DATA
H1 DATA RELAY SATELLITE
MULTI1
COPBOX20110109 DPRCOVCXX RXX
DTIN 5
MOPRAM04,60 0 0
GM 1.096677E-8
MGPRAM06,60 0 03,010
P01,0102,00 0 05,012,236F-8
H MVS 5.5 MTEL---NO NORMALIZATION OMEGA.43752695E-2
GM .553039362E-2 OMEGA.43752695E-2
ERFT 20925741. DF 20925741.
INFOPM1
INTERM24
MTERMS04,60
D 02,00 -.1082637E-2
P 03,00 +2.566379E-5
D 04,00 +1.62E-6
P 05,00 +1.32665E-7
D 06,00 -6.49E-7
P 02,02 +1.56852217E-06
D 03,01 +2.09543973E-06
P 03,02 +2.45926844E-07
D 03,03 +7.66938326E-08
P 04,01 -5.78695539E-07
D 04,02 +7.37902535E-08
P 04,03 +5.3187620E-08
D 04,04 -6.53285555E-09
P 05,01 -4.28174235E-08
D 05,02 +1.21376037E-07
P 05,03 -2.01509731E-08
D 05,04 0
P 05,05 0
D 06,01 -1.41448651E-07
P 06,02 +3.73837758E-09
D 06,03 +2.48906140E-09
P 06,04 +4.92117519E-10
D 06,05 -8.8776842E-11
P 06,05 0
IKSIG 1
T4 19 I2 2
SIGMA10. I5 58
4 2 .01146
PPANDP X X 5 10.
END

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CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9
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CARD 39
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CARD 44

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0
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0
-8.97210795E-07
+1.62018557E-07
-2.66420655E-07
0.0
-4.64855128E-07
+1.58760886E-07
+4.18329853E-09
+2.37178570E-09
+2.56904982E-08
-2.75119085E-08
+4.95514785E-09
0
0
+9.42988666E-08
-4.73526613E-08
+7.25686409E-09
-1.89273502E-09
-2.98614379E-10
0
0
I3 3
I6 61
3 .01146
6 10.

```

(1)

REFERENCE
SECTION

DESCRIPTION

ITEM

1 Card images of the input MODEL data. The inputs used during a covariance analysis run are emphasized here. The input item MULTV indicates that simultaneous vehicles are used:

MULTV
 ØPBOX, PRCØV, PANDR
 ITIN
 ØPRAM
 GPRAM
 KJIG, SIGMA

2.1.6
 2.5.1
 2.1
 2.1.5.3
 2.1.5.2
 2.5.3

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LUNAR GRAVITY MODEL *****
SM = 6.602326500E-05 ER**3/MIN**2 = 1.7314003854E+14 FT**3/SFC**2 = 4.9027777038E+12 M**3/SEC**2
SPHERICAL MODEL

EARTH GRAVITY MODEL *****
SM = 5.530393620E-03 ER**3/MIN**2 = 1.4076545204E+16 FT**3/SEC**2 = 3.9860319162E+14 M**3/SEC**2
NO NORMALIZATION WITH 24 TERMS.

N	M	CM	SNM	**	N	M	CM	SNM
2	0	-1.04263710E-03	0.	**	5	2	1.21376037E-07	-2.75119005E-08
3	0	2.56637910E-06	0.	**	6	2	3.73837758E-09	-4.73526613E-08
4	0	1.62000910E-06	0.	**	3	3	7.66938326E-08	0.
5	0	1.32665010E-07	0.	**	4	3	5.31876720E-08	4.18329853E-09
6	0	-5.49000910E-07	0.	**	5	3	-2.01509731E-08	4.95514785E-09
3	1	2.09543973E-06	1.62018557E-07	**	6	3	2.48806140E-09	7.25686409E-09
4	1	-5.75696539E-07	-4.64855128E-07	**	4	4	-6.53285565E-09	2.37178570E-09
5	1	-4.24174235E-08	2.56904982E-08	**	5	4	0.	0.
6	1	-1.4144851E-07	9.42988666E-08	**	6	4	4.92117588E-10	-1.89273502E-09
2	2	1.56852217E-06	8.97210795E-07	**	5	5	0.	0.
3	2	2.4592694E-07	-2.66420655E-07	**	6	5	-8.87768432E-11	-2.98614379E-10
4	2	7.37902536E-08	1.58760806E-07	**	6	6	0.	0.

***** PHYSICAL CONSTANTS *****

GM(E**3/MIN**2)	=	5.531393520E-03	OMESE(RAD/MIN)	=	4.375269500E-03	GMLAT(DEG)	=	7.830000000E+01
GM(KM**3/MIN**2)	=	0.	OMEGA(RAD/MIN)	=	4.375269500E-03	GMLNG(DEG)	=	2.910000000E+02
SGM(E**3/MIN**2)	=	6.802325500E-05	OMEGL(RAD/MIN)	=	0.	AM(ER)	=	2.725062770E-01
ERFT(FT/ER)	=	2.092574100E+07	ERKM(<M/ER)	=	6.378164900E+03	ERNM(NM/ER)	=	3.443933600E+03
FTKM(FT/KM)	=	3.28183900E+03	FTNM(FT/NM)	=	6.076115500E+03	AE(ER)	=	1.000000000E+00
SSURD(FT/SEC**2)	=	3.217409000E+01	DGREE(DEG)	=	5.729577951E+01	SLT	=	2.820176300E+03
CKEP	=	1.001000000E-07	F	=	3.352329869E-03	PI	=	3.141592654E+00

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = 2.09257410E+07 VF(I/O-ER/MIN) = 3.48762308E+05 AF(I/O-ER/MIN**2) = 5.81278588E+03

***** INTEGRATION INPUTS *****

IFORM = 1 ICENT = 1 NSTEP = 2
NPGMP = 0 IR = 8 ER = 1.00000000E-10
HMIN = 1.56250000E-02 HMAX = 6.40000000E+01 MO = 1.00000000E+00

***** SPECIAL OPTIONS *****

TAPF2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPOOT = 0
PRHO = 0 NODPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

***** STATION LOCATIONS *****

STATION	SIG	REF	RA-REF	DATUM	TYPE	LATITUDE	LONGITUDE	HEIGHT	P	Q
						X	Y	Z		
1	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		
2	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		
3	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		

***** SENSOR PARAMETERS *****

STAPASS	PARAMETER	P-Q	INITIAL	VALUE	BOJND	SIGMA
1	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
1	LONG	Q	-0.	-0.	3.60000000E+02	1.67000000E-04
1	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
1	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02
1	ABIA	Q	-0.	-0.	3.60000000E+02	2.00000000E-01
1	EBIA	Q	-0.	-0.	3.60000000E+02	2.00000000E-01
2	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
2	LONG	Q	-0.	-0.	3.60000000E+02	1.67000000E-04
2	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
2	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02
3	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
3	LONG	Q	-0.	-0.	3.60000000E+02	1.67000000E-04
3	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
3	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02

2

ITEM	DESCRIPTION	REFERENCE SECTION
2	<p><u>Sensor parameter information.</u> Each line contains the station and pass identification, parameter name, P- or Q-parameter indicator, initial value, bound, and sigma</p>	5

ENTER SEGMENT 01 AT 110.7 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 110.7 CP SECS., 337.7 PP SECS.

***** VEHICLE DATA *****

IYEAR 1969	IMNT4 0	IDAY 22	CARD 1
TZNE 0	HR 0	IIN 0	CARD 2
SEC 0	IICTYP3	IVMHI01	CARD 3
IC 1.3834434E8	0.01520E-2	10.	CARD 4
-140.	180.	-7.18E2	CARD 5
MVPRAM04,60	1.E10	1.E7	CARD 6
0 X	1.E10	1.E7	CARD 7
0 Y	1.E10	1.E7	CARD 8
0 Z	1.E10	1.E3	CARD 9
0 CX	1.E10	1.E3	CARD 10
0 CY	1.E10	1.E3	CARD 11
0 CZ	1	0	CARD 12
PT 0	1	0	CARD 13
15	30		CARD 14
DRAG 0			CARD 15
FND			CARD 16

EPOCH	X,Y,Z,DX,DY,DZ	INITIAL CONDITIONS	AF,AG,N,L,CHI,PSI
YR/MO/DAY	A,B,A,R,V	A,E,I,O,U,T/AU	6.14005836449E-02
TZNE,HR,MIN,SEC	2.19975207933E+02	1.36344340000E+08	5.15212916005E-02
1969/ 8/22	-4.19511075994E-03	8.01529000000E-02	4.17761658205E-03
0.	8.99978948803E+01	1.00000000000E+01	2.19971722355E+02
0.	8.00000008710E+01	-1.40000000000E+02	-5.62366209025E-02
0.	1.49433038692E+08	1.80800000000E+02	-6.70202045299E-02
0.	1.61644425299E+03	9.30855966659E+03	

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

ITEM	DESCRIPTION	REFERENCE SECTION
3	<p>Card images of the input <u>VEHICLE</u> data. The items used by a simultaneous-vehicle or covariance analysis run are emphasized</p> <p>VEHID VPRAM PTIM</p>	<p>11.1.2 11.1.14 11.5.1</p>

```

***** VEHICLE DATA *****
IVEHID2
IIC1Y3
IC 1.38334198E8 0 180
75
END

EPOCH
YR/MO/DAY
YZNE,HR,MIN,SEC
1969/ 8/22
X,Y,Z,DX,DY,DZ
4.06703434460E+05
1.38245315589E+08
2.78671742142E+05
-1.00473057957E+04
2.78333870503E+02
8.55373878177E+02
A,D,B,A,R,V
8.83143155734E+01
1.15423120500E+00
9.00000000000E+01
8.51347337324E+01
1.38334198000E+08
1.00874919013E+04
INITIAL CONDITIONS
A,E,I,C,U,TAU
1.38334198000E+08
0.
5.00000000000E+00
7.50000000000E+01
1.80000000000E+02
-7.71343693000E+02
AF,AG,N,L,CHI,PSI
-8.27566114034E-15
-1.06388505267E-13
4.17807601469E-03
8.83639549683E+01
4.21732323555E-02
1.130028355519E-02
NO PLANETARY PERTURBATIONS.
** NO ATMOSPHERE MODEL **

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***** VEHICLE DATA *****
IVEHID3
IIC1Y3
IC 1.38334198E8 0 180
75.5
END

EPOCH
YR/MO/DAY
YZNE,HR,MIN,SEC
1969/ 8/22
X,Y,Z,DX,DY,DZ
3.4655958933E+07
1.33922786431E+08
0.
-9.76580732694E+03
2.52715256980E+03
0.
A,D,B,A,R,V
7.54915147128E+01
0.
9.00000000000E+01
8.99999996107E+01
1.38334198000E+08
1.00874919013E+04
INITIAL CONDITIONS
A,E,I,C,U,TAU
1.38334198000E+08
0.
0.
7.55000000000E+01
1.80000000000E+02
-7.18000000000E+02
AF,AG,N,L,CHI,PSI
-2.24851579148E-14
-8.22551413022E-14
4.17807601469E-03
7.54915147128E+01
0.
NO PLANETARY PERTURBATIONS.
** NO ATMOSPHERE MODEL **

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***** OBSERVATIONS *****
CARD 1
CARD 2
CARD 3
CARD 4
CARD 5

EPOCH
YR/MO/DAY
YZNE,HR,MIN,SEC
1969/ 8/22
X,Y,Z,DX,DY,DZ
3.4655958933E+07
1.33922786431E+08
0.
-9.76580732694E+03
2.52715256980E+03
0.
A,D,B,A,R,V
7.54915147128E+01
0.
9.00000000000E+01
8.99999996107E+01
1.38334198000E+08
1.00874919013E+04
INITIAL CONDITIONS
A,E,I,C,U,TAU
1.38334198000E+08
0.
0.
7.55000000000E+01
1.80000000000E+02
-7.18000000000E+02
AF,AG,N,L,CHI,PSI
-2.24851579148E-14
-8.22551413022E-14
4.17807601469E-03
7.54915147128E+01
0.
NO PLANETARY PERTURBATIONS.
** NO ATMOSPHERE MODEL **

```

REFERENCE
SECTION

DESCRIPTION

ITEM

4 Card images of the input VEHICLE data for the second vehicle and the printout of the initial conditions, perturbation remark, and atmospheric model (repeated for each vehicle used in the simultaneous-vehicle run). Note that inputs not overridden carry over from vehicle to vehicle. In this example, the VPRAM matrix carries over

Case A:
Items 17,
18, 19,
and 20

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

THESE ARE THE 34 PARAMETERS IN THE PARAM MATRIX. 18 ARE P PARAMETERS AND 16 ARE Q PARAMETERS

	NAME	P/Q	CURRENT VALUE	BOUND	SIGMA	CONVERSION
0001	X	P	-1.14512224E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	Y	P	-9.50031535E+07	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	Z	P	-1.09412622E+04	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	DX	P	5.38925583E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0001	DY	P	-7.02517998E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0001	DZ	P	1.51641425E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	X	P	4.06703434E+06	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	Y	P	1.38245316E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	Z	P	2.78671742E+06	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	DX	P	-1.00473058E+04	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	DY	P	2.78335871E+02	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	DZ	P	8.55375878E+02	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	X	P	3.46539509E+07	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	Y	P	1.33922796E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	Z	P	0.	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	DX	P	-9.76550733E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	DY	P	2.82715257E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	DZ	P	0.	1.00000000E+10	1.00000000E+03	3.48762300E+05
3	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
3	ALTI	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07
3	LONG	Q	-9.30000000E+01	3.50000000E+02	1.87000000E-04	5.72957795E+01
3	LAT	Q	4.30000000E+01	3.50000000E+02	1.37000000E-04	5.72957795E+01
2	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
2	ALTI	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07
2	LONG	Q	-9.30000000E+01	3.50000000E+02	1.87000000E-04	5.72957795E+01
2	LAT	Q	4.30000000E+01	3.50000000E+02	1.37000000E-04	5.72957795E+01
1	EBIA	Q	-0.	1.00000000E+10	2.00000000E-01	5.72957795E+01
1	ABIA	Q	-0.	1.00000000E+10	2.00000000E-01	5.72957795E+01
1	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
1	ALTI	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07

1 LONG Q -9.30000000E+01 3.50000000E+02 1.07000000E-04 5.72957795E+01
 1 LAT Q 4.30000000E+01 3.60000000E+02 1.37000000E-04 5.72957795E+01
 GM Q 5.33039362E-03 0. 1.09667700E-08 1.00000000E+00
 02,00 C Q -1.70263700E-03 0. 2.23600000E-08 1.00000000E+00

ENTER SEGMENT 10 AT 111.6 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .8 CP SECS., 4.5 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

IVEP	ICENT	1	IDRAG	0	ALPHG	5.761750222E+00	CDAM	0.
JVEP	JNORM	1	IR	4	ALG-DFG	3.301239703E+02	ER	1.00000000E-10
MVEP	MAJOR	1	ISRP	0	TJDATE	2.440455500E+06	HMIN	1.56250000E-02
KVEP	NMASS	0	NEQS	27	TSTART	0.	HMAX	5.40000000E+01
LVEP	VT	24	RECM	0	TSTOP	3.00000000E+01	H0	1.00000000E+00
ICENTX	JNORMX	0	NYASSX	0	FLIGHT	3.00000000E+01	NTX	0.
			NASA	0	SSTEP	1.00000000E+02	SORD	1.50000000E+00

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

0.0000 TZERO
 30.0000 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS 111.70100

T	=	0.000000	4	=	.125000	NSTEP	=	0
-1.14512244079E+08						4.830829047242E-01		
-9.600616352941E+07						4.050130141915E-01		
-1.094126223805E+04						4.614415693159E-05		
02,00 C						-2.444496288923E-06		
						-2.249446786235E-06		
						-7.0002904861358E-10		
GM						1.502752199719E-02		
						1.259095871980E-02		
						1.435431228069E-06		
X						1.156849534924E-05		

	0.	0.	2.243161066230E-05
	0.	0.	2.55524807094E-09
Y	0.	0.	2.243161066230E-05
	1.00000000000E+00	0.	3.619483449938E-06
	0.	0.	2.142254137494E-09
Z	0.	0.	2.55524807094E-09
	0.	0.	2.142254137494E-09
	1.00000000000E+00	0.	-1.518797879918E-05
DX	0.	1.00000000000E+00	0.
	0.	0.	0.
	0.	0.	0.
DY	0.	0.	0.
	0.	1.00000000000E+00	0.
	0.	0.	0.
DZ	0.	0.	0.
	0.	0.	0.
	1.00000000000E+00	1.00000000000E+00	0.

FORCES (MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 6.304004E-01 4.830829E-01 4.050130E-01 4.614416E-05 -6.304004E-01 -3.420336E-08 -6.976752E-09
 TOTAL 6.304004E-01 4.830829E-01 4.050130E-01 4.614416E-05 -6.304004E-01 -3.420336E-08 -6.976752E-09

MODE T = 1.12814106395E-01 -1.144723439480E+08 -9.605370662137E+07 -1.227973594797E-10
 DT = 1.250000000000E-01 5.892525173075E+03 -7.022437834961E+03 1.616414409103E+03
 * STEP DOUBLED T = 3.250000 H = .250000 NSTEP = 25
 * STEP DOUBLED T = 7.500000 H = .500000 NSTEP = 41
 * STEP DOUBLED T = 15.000000 H = 1.000000 NSTEP = 57

T = 30.000000 + = 1.000000 NSTEP = 71
 -1.031517926203E+08 6.717059485659E+03 4.358762082148E-01
 -1.079671375801E+08 -6.249427521532E+03 4.562150451684E-01
 2.892052284940E+06 1.605453243475E+03 -1.222115672862E-02

02, J0 C	-1.067305128407E-03	-7.009771297779F-05	-2.232865286960E-06					
	-9.641155372844E-04	-6.572210958654F-05	-2.339382147550E-06					
	2.767112854346E-05	2.780059370108E-06	1.864451829015E-07					
GM	6.562092629373E+00	4.310746463120F-01	1.373717558371E-02					
	5.927637541327E+00	4.0413486684247E-01	1.439248707537E-02					
	-5.693159818645E-02	-5.734773176488E-03	-3.870978531235E-04					
X	1.004477955644E+00	2.747868019029E-04	6.820129799268E-06					
	1.019931600779E-02	6.827010123838F-04	2.297611316839E-05					
	-9.630530433524E-05	-9.522323254205F-06	-6.182057231257E-07					
Y	1.019532349771E-02	6.821857296951E-04	2.290744045517E-05					
	1.002339935225E+00	1.860943686471E-04	8.890457780075E-06					
	-9.024715473606E-05	-9.252425235328E-06	-6.452862051509E-07					
Z	-9.588913321212E-05	-9.452713086250E-06	-6.089286477563E-07					
	-8.989650147419E-05	-9.194015111649F-06	-6.375017710560E-07					
	9.931728272075E-01	-4.546772525530E-04	-1.509178751809E-05					
DX	3.004034250283E+01	1.003725452967E+00	1.993488181183E-04					
	1.022939151825E-01	1.025315636076E-02	6.853948449331E-04					
	-1.43203441944E-03	-1.863767774393E-04	-1.838115336730E-05					
DY	1.02273425880E-01	1.025006160901E-02	6.848790387747E-04					
	3.002754670061E+01	1.003149681995F+00	2.616909180022E-04					
	-1.372021153866E-03	-1.8652844733097E-04	-1.9222631782016E-05					
DZ	-1.429954095661E-03	-1.879587038032E-04	-1.831147254788E-05					
	-1.370257148254E-03	-1.861776660532E-04	-1.916784830180E-05					
	2.993159056583E+01	9.931714844961E-01	-4.548297409590E-04					
FORCFS	MAGNITUDE	Y	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SEOPOTENTIAL	6.310460E-01	4.358762E-01	4.562150E-01	-1.222116E-02	-6.310860E-01	-1.739166E-07	-7.744879E-07	
TOTAL	6.310460E-01	4.358762E-01	4.562150E-01	-1.222116E-02	-6.310860E-01	-1.739166E-07	-7.744879E-07	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.129 SECONDS TO INTEGRATE A SPAN OF 30.0000 MINUTES ***
 *** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

TRAJECTORY INTEGRATION FOR CASE 2

IVER	1	ICENT	1	IIRAG	0	ALPMG	5.761750222E+00	COAM	0.
JVEP	1	JNORM	1	IR	9	ALG-DES	3.301239703E+02	ER	1.000000000E-10
MVEP	0	MAJOP	1	ISRP	0	TJDATE	2.440455500E+06	HMIN	1.562500000E-02
KVEP	6	VMASS	0	NFQS	0	TSTART	0.	HMAX	6.400000000E+01
LVEP	0	VT	24	RFCMP	0	TSTOP	3.000000000E+01	H0	1.000000000E+00
IDENTY	1	JNORMX	0	NMASSX	0	FLIGHT	3.000000000E+01	NTX	0.
				NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

* PREDETERMINED EVENT TABLE *

TIME(MME) TYPE ASSOCIATED QUANTITIES
 0.0000 T7F30
 30.0000 TSTOP

*** TRAJECTORY START

*** ENTRY TIME IS 112.85300 ***

T	=	0.000000	+	=	.125000	NSTEP	=	0
02,00 C		4.067034344501E+06			-1.004730578571E+04			-2.162744150928E-02
		1.382453155891E+08			2.783368705028E+02			-7.351517941123E-01
		2.786717421420E+06			8.553758781768E+02			-1.482002055073E-02
		0.			0.			1.274437767438E-07
		0.			0.			4.332058961582E-06
		0.			0.			2.623271566750E-07
GM		0.			0.			-6.727765114806E-04
		0.			0.			-2.286876416886E-02
		0.			0.			-4.610143886837E-04
X		1.000000000000E+00			0.			-1.909406277137E-05
		0.			0.			1.687467803763E-06
		0.			0.			3.401905643118E-08

Y	0.	0.	0.	1.687467803763E-06
	1.000000000000E+00	0.	0.	3.821588824887E-05
	0.	0.	0.	1.156376870886E-06
Z	0.	0.	0.	3.401905643118E-08
	0.	0.	0.	1.156376870886E-06
	1.000000000000E+00	0.	0.	-1.912181747751E-05
OX	0.	1.000000000000E+00	0.	0.
	0.	0.	0.	0.
	0.	0.	0.	0.
OY	0.	0.	0.	0.
	0.	1.000000000000E+00	0.	0.
	0.	0.	0.	0.
OZ	0.	0.	0.	0.
	0.	0.	0.	0.
	0.	1.000000000000E+00	0.	0.

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SEOPOTENTIAL	7.356192E-01	-2.162744E-02	-7.351518E-01	-1.482002E-02	-7.356192E-01	9.718920E-08	-1.118119E-06	
TOTAL	7.356192E-01	-2.162744E-02	-7.351518E-01	-1.482002E-02	-7.356192E-01	9.718920E-08	-1.118119E-06	

*	STEP	DOUPLED	T =	3.250000	H =	.250000	NSTEP =	25
*	STEP	DOUPLED	T =	7.500000	H =	.500000	NSTEP =	41
*	STEP	DOUPLED	T =	15.000000	H =	1.000000	NSTEP =	57

T = 30.000000 + = 1.000000 NSTEP = 71

02.00 C	-1.400121703040E+07	-9.999653462807E+03	7.44940033301E-02
	1.375556473079E+08	-1.043534296867E+02	-7.314849971285E-01
	4.298002445426E+06	8.214176207192E+02	-2.289719126977E-02
	-2.802572537901E-05	-4.741633923443E-06	-4.483036949437E-07
	1.952925550034E-03	1.393970673860E-04	4.372298978959E-06
	1.395939607512E-04	1.001955722892E-05	4.050207347041E-07
GM	1.482672897244E-01	2.508374933340E-02	2.373017363729E-03

	-1.031805027654E+01	-6.892533705414E-01	-2.314441681329E-02
	-2.461874755292E-01	-1.772837401649E-02	-7.246686026364E-04
X	9.914272990064E-01	-5.68081449113E-04	-1.839421018251E-05
	-3.635617942318E-04	-6.145012900747E-05	-5.744386322036E-06
	-1.073532393402E-05	-1.785119061049E-06	-1.795199097829E-07
Y	-3.693701264649E-04	-6.241723129230E-05	-5.873111043707E-06
	1.017234659442E+00	1.149388370508E-03	3.829710369053E-05
	6.163371735316E-04	4.427394692864E-05	1.793490631172E-06
Z	-1.086745890223E-05	-1.807419928568E-06	-1.824349837512E-07
	6.158432534138E-04	4.42521749907E-05	1.782610832439E-06
	9.914119190898E-01	-5.715525417284E-04	-1.892465283486E-05
DX	2.991448216747E+01	9.915082636154E-01	-5.550210678596E-04
	-9.267732775470E-03	-1.485972548969E-03	-1.732620244910E-04
	-2.567657963390E-04	-4.299783690502E-05	-5.414942578455E-06
DY	-9.29568322778E-03	-1.491780883369E-03	-1.742291272889E-04
	3.017196880907E+01	1.017148866298E+00	1.135887758193E-03
	6.627238215817E-03	7.092581074666E-04	5.341831321044E-05
DZ	-2.574248749686E-04	-4.312937141402E-05	-5.436843357366E-06
	6.624792105526E-03	7.087671875916E-04	5.333657382664E-05
	2.991449297218E+01	9.914167476987E-01	-5.710390014654E-04

FOPCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	7.356196E-01	7.445408E-02	-7.314850E-01	-2.285719E-02	-7.356196E-01	5.249624E-08	-1.712987E-06	
TOTAL	7.356196E-01	7.445408E-02	-7.314850E-01	-2.285719E-02	-7.356196E-01	5.249624E-08	-1.712987E-06	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.132 SECONDS TO INTEGRATE A SPAN OF 30.000 MINUTES ***

*** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

TRAJECTORY INTEGRATION FOR CASE 3

```

IVFP 1 ICFNT 1 ICRAG 0 ALP4G 5.761750222E+00 CDAM 0.
JWEP 1 JNORM 1 IR 0 ALG-DEG 3.301239703E+02 ER 1.000000000E-10
MVEP 0 SAJOR 1 ISRP 0 TJDATF 2.44045590CE+06 HMIN 1.562500000E-02
KVEP 6 NMASS 0 NEQS 27 TSTART 0. HMAX 6.400000000E+01
LVFP 0 VT 24 RECMP 9 H0 1.000000000E+00
ICENTX 1 JNORMX 0 NMASSX 0 FLIGHT 3.000000000E+01 NTX 0.
SSTEP 1.000000000E+02 SORD 1.500000000E+00

```

* PREDETERMINED EVENT TABLE *

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TIME(MME) TYPE ASSOCIATED QUANTITIES
0.0000 TZERO
30.0000 TSTOP

```

*** TRAJECTORY START

SFG1: ENTRY TIME IS 114.00500

	T	=	0.000000	W	=	.125000	NSTEP	=	0
02,00 C	3.465535083333E+07		-9.765607326943E+03				-1.842899424245E-01		
	1.339227954313E+08		2.527152569800E+03				-7.121605279939E-01		
	0.		0.				-1.006964949376E-08		
	0.		0.				1.088179954344E-06		
	0.		0.				4.205110486071E-06		
	0.		0.				0.		
GM	0.		0.				-5.732806837653E-03		
	0.		0.				-2.215356242819E-02		
	0.		0.				-3.132420288982E-10		
X	1.0000100010000E+00		0.				-1.553511309570E-05		
	0.		0.				1.392937542766E-05		
	0.		0.				-4.344817468047E-13		
Y	0.		0.				1.392937542766E-05		
	1.0000100010000E+00		0.				3.468423879095E-05		
	0.		0.				1.386397852185E-12		
Z	0.		0.				-4.344817468047E-13		

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0.	0.	1.386397862185E-12
1.000000000000E+00	0.	-1.914512569526E-05
0.	1.000000000000E+00	0.
0.	0.	0.
0.	0.	0.
0.	0.	0.
0.	1.000000000000E+00	0.
0.	0.	0.
0.	0.	0.
0.	1.000000000000E+00	0.

FORCFS	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	7.356191E-01	-1.842899E-01	-7.121695E-01	-7.121695E-01	-1.006965E-08	-7.356191E-01	1.746302E-07	-1.006965E-08
TOTAL	7.356191E-01	-1.842899E-01	-7.121695E-01	-7.121695E-01	-1.006965E-08	-7.356191E-01	1.746302E-07	-1.006965E-08

STEP	DOUBLED	T =	3.250000	H =	.250000	NSTEP =	25
STEP	DOUBLED	T =	7.500000	H =	.500000	NSTEP =	41
STEP	DOUBLED	T =	15.000000	H =	1.000000	NSTEP =	57

T = 30.000000 I = 1.000000 NSTEP = 71

1.682930795167E+07	-1.001256909845E+04	-8.949604214476E-02
1.373055756953E+08	1.227201690960E+03	-7.301551530551E-01
-1.628942793407E-02	-1.807336948206E-05	-9.983033663556E-09

02,00 C

4.070847007474E-04	2.437527762037E-05	5.342934860491E-07
1.916519326183E-03	1.286730581928E-04	4.385942515059E-06
5.917822114888E-14	7.662493042071E-15	7.272527446215E-16

GM

-2.144625249825E+00	-1.284151381294E-01	-2.814794016769E-03
-1.009679711925E+01	-6.778813727344E-01	-2.310821656102E-02
-1.414727134905E-07	-9.464543733016E-09	-3.197602452963E-10

X

9.925332139491E-01	-5.102966186224E-04	-1.812069354333E-05
5.257032259425E-03	3.161725696603E-04	7.080467209392E-06

Y	-2.214233915733E-10	-1.557665160814E-11	-5.973181391956E-13
Z	5.251231741357E-03	3.152017735133F-04	6.951250815456E-06
DX	1.016137602155E+00	1.092830260297E-03	3.607937322965E-05
DY	6.144239209723E-10	4.061547379242E-11	1.3317067303713E-12
DZ	-2.215154120324E-10	-1.559210221234E-11	-5.994337175659E-13
	6.146077081433E-10	4.064573851100E-11	1.321091289946E-12
	9.913970555523E-01	-5.727059617717E-04	-1.698043935721E-05
	2.992313041991E+01	9.921252091104E-01	-5.470746835051E-04
	4.732637541441E-02	4.205822502933F-03	2.093005529613E-04
	-2.353551543415E-09	-2.482414436165E-10	-1.823644774703E-11
	4.729770487385E-02	4.199991983422F-03	2.083297562321E-04
	3.016339232585E+01	1.016551615658E+00	1.129608695166E-03
	6.008616203347E-09	6.031274802870F-10	3.939547750913E-11
	-2.354115772231E-09	-2.483360037071E-10	-1.825260519300E-11
	6.089525257188E-09	6.033090279937E-10	3.942566661087E-11
	2.9913372110270E+01	9.913970528152E-01	-5.727063261363E-04

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 7.356195E-01-8.949604E-02-7.301552E-01-9.983034E-09-7.356195E-01 1.746305E-07-1.006966E-08
 TOTAL 7.356195E-01-8.949604E-02-7.301552E-01-9.983034E-09-7.356195E-01 1.746305E-07-1.006966E-08

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.137 SECONDS TO INTEGRATE A SPAN OF 30.000 MINUTES ***
 *** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 21 AT 115.1 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 3.5 CP SECS., 17.8 PP SECS.
 RUNNING TIME FOR SEG21 WILL INCLUDE THAT FOR SEG22, SEG23, AND SFG24.

1	1969	8	22	0	15	0.0000				
APERTIALS FOR RING							-7.521539222E-01	-6.574089152E-01	-9.396491570E-02	-1.125646282E+01
						-1.411202182E+00	0.	0.	0.	
						0.	0.	0.	0.	
						0.	0.	0.	0.	
						0.	0.	0.	0.	
						2.461772464E-01	7.055398750E-01	-2.196830241E+00	1.000000000E+00	
									3.571280823E-04	
									-6.211610330E-01	

3

ITEM	DESCRIPTION	REFERENCE SECTION
5	Partial derivatives of the measurement (in this case, range) with respect to all parameters at the <u>observation time</u> shown on the first line. The partials are printed across the page in the order shown in the parameter list. The units are internal units	Case B: Items 4 and 6

PARTIALS FOR AZ					
	-1.273004078E-01	1.367271389E-01	6.170396870E-02	-1.911401324E+00	2.053488895E+00
	9.256145215E-01	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	1.336097330E+00	-7.641923509E-01	1.000000000E+00	0.	0.
PARTIALS FOR EL					
	2.153833637E-02	-4.558491113E-02	-1.422546047E-02	2.454676206E-06	-6.855916569E-01
	2.197711353E+00	0.	1.456813612E-01	3.239806600E-01	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	1.000000000E+00	0.	0.	0.
1	1969 8 22 0 15	-3.437679833E-01	-9.905326916E-01	0.	-1.210363503E-01
		0.	1.000000000E+00	0.	0.
PARTIALS FOR RD					
	1.970208850E-03	-3.045492045E-03	7.317243200E-04	-7.174194756E-01	-6.986737655E-01
	-8.333085099E-02	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
2	1969 8 22 0 15	5.439230197E-04	-2.933598728E-01	4.764305084E-05	-3.402956952E-04
		0.	0.	0.	0.
PARTIALS FOR S2					
	-4.000359060E-01	-9.191539810E-01	-6.015897430E-03	-5.972374313E+00	-1.377284910E+01
	-1.204851861E-01	4.127522528E-01	1.923351610E+00	-6.161133578E-02	6.198561629E+00
	2.876534710E+01	-9.281750174E-01	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	1.000000000E+00	6.908732761E-01	3.450543492E-01
	-5.473487325E-01	0.	0.	0.	0.
3	1969 8 22 0 15	0.0000	-6.927454010E+00	1.257255710E-03	0.
		0.	0.	0.	0.
PARTIALS FOR S3					
	-4.000359060E-01	-5.131539810E-01	-8.015897430E-03	-5.972374313E+00	-1.377284910E+01
	-1.204851861E-01	-5.921544118E-01	9.957147359E-01	1.221985379E-01	-8.895918843E+00
	1.493335783E+01	1.8342388643E+00	1.206307960E+00	9.074322187E-01	-2.062590273E-01
	1.810305479E+01	1.349817808E+01	-3.098335541E+00	1.000000000E+00	7.610603632E-01
	2.078613361E-01	-5.821478754E-01	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	-7.504468632E+00	1.371640296E-03	0.

2.076613613E-01 -5.821478526E-01 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. -3.002659224E+01 5.495521975E-03 0.

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN
1	2 RNG	1.4E+08	1.4E+07	-1.4E+08
2	2 RD	1.8E+02	8.8E+02	1.7E+02
3	2 S2	4.1E+08	4.1E+07	-4.1E+08
	2 S3	4.5E+08	4.5E+07	-4.5E+08

N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
2 AZ	1.5E+02	1.4E+04	1.6E+02	2 EL	3.8E+01	3.3E+03	-3.8E+01

ENTER SEGMENT 72 AT 115.9 SECONDS. EXECUTION TIME FOR SEGMENT 21 WAS .7 CP SECS., 12.7 PP SEC



REFERENCE
SECTION

DESCRIPTION

ITEM

Case B:
Item 7

6 Edit summary. The restriction to the first 6 measurement types encountered for the first 30 stations still holds

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*****
* SIMULTANEOUS VEHICLE COVARIANCE ANALYSIS INPUT AND OUTPUT OPTIONS *
*****

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*****
* OPROX OPTIONS
*****
* A SORT OF DIAGONAL OF FULL ATA INVERSE INPUT
* C PRINT DP/OQ
* D NORMAL COVAR. ANALYSIS, OBSERVATIONS INPUT
* E NORMAL IPOATE - OUTPUT IS REAL TIME
* F GENERAT: PLOT TAPE
* H PRINT ENTIRE INTER-SATELLITE COV. MATRIX
*****
* PRCOV OPTIONS
*****
* A C(P), CORRELATION AND SORT OF DIAGONAL
* B PRINT C(X) AT CURRENT TIME WITH P EFFECTS
* C PRINT C(OP) AT CURRENT TIME FOR P EFFECTS
* G PRINT CORRELATION AND SORT OF DIAGONAL
* H PRINT C(X) AT CURRENT TIME WITH P+Q EFFECTS
* I PRINT C(OP) AT CURRENT TIME FOR P+Q EFFECTS
*****

```

7

ITEM	DESCRIPTION	REFERENCE SECTION
7	Indicates <u>input/output options</u> requested by ØPBØX and PRCØV for the simultaneous -vehicle error analysis run	2.5.1

ENTER SEGMENT 73 AT 116.3 SECONDS. EXECUTION TIME FOR SEGMENT 72 WAS .4 CP SECS., 16.5 PP SECS.

COVARIANCE MATRICES AT 0. MINUTES FROM MIDNIGHT OF EPOCH DATE 0

ATA(INVERSE) FOR P PARAMETERS

	0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z
0001 X	1.00000E+14	0.	0.	0.	0.	0.	0.	0.	0.
0001 Y	0.	1.00000E+14	0.	0.	0.	0.	0.	0.	0.
0001 Z	0.	0.	1.00000E+14	0.	0.	0.	0.	0.	0.
0001 DX	0.	0.	0.	1.00000E+06	0.	0.	0.	0.	0.
0001 DY	0.	0.	0.	0.	1.00000E+06	0.	0.	0.	0.
0001 DZ	0.	0.	0.	0.	0.	1.00000E+06	0.	0.	0.
0002 X	0.	0.	0.	0.	0.	0.	1.00000E+14	0.	0.
0002 Y	0.	0.	0.	0.	0.	0.	0.	1.00000E+14	0.
0002 Z	0.	0.	0.	0.	0.	0.	0.	0.	1.00000E+14
0002 DX	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 DY	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 DZ	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 X	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 Y	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 Z	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DX	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DY	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DZ	0.	0.	0.	0.	0.	0.	0.	0.	0.



REFERENCE
SECTION

DESCRIPTION

ITEM

- 8 Time statement, determined by PTIM, that applies to items 9 through 14.
Valid until another time statement is made
- 9 $(A^T A)^{-1}$ for P-parameters, identified by parameter name (PRCØV (A) = C).
This is the covariance matrix of P-parameters, based on measurement uncertainties (observation weights) only

ITEM	DESCRIPTION	REFERENCE SECTION
10	Correlation matrix for P-parameters, i.e., the matrix of Item 9 normalized to 1s on the diagonal ($\text{PRC}\Phi V(A) = C$)	2.5.1
11	<u>Square roots of the diagonal elements of $(A^T A)^{-1}$</u> (Item 9) in the order shown in the header of Item 9	2.5.1
12	<u>Pivot ratios encountered in the inversion of $A^T A$</u> are determined by referencing the original diagonal elements of the $A^T A$ matrix to the diagonal element used in pivoting that particular row and column. These will be printed if Items 9, 10, or 11 are printed	

DPJQ MATRIX

	3 1	3 1	3 1	3 1	3 1	3 1	3 1	2 1	2 1	2 1	2 1	2 1	2 1
	RBIA	ALT	ARIA	LONG	LAT	RBIA	ALT	RPIA	LONG	GM	ALT	LAT	LAT
	EBIA	ARIA	ARIA	RBIA	ALT	RBIA	ALT	LONG	GM	GM	LAT	LAT	02,00
0001 X	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0001 Y	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0001 Z	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0001 DX	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0001 DY	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0001 DZ	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 X	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 Y	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 Z	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 DX	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 DY	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0002 DZ	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 X	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 Y	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 Z	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DX	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DY	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0003 DZ	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

ATA(INVERSE) FOR P AND Q PARAMETERS (14)

0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ	0003 X	0003 Y	0003 Z	0003 DX	0003 DY	0003 DZ
0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ	0003 X	0003 Y	0003 Z	0003 DX	0003 DY	0003 DZ

ITEM	DESCRIPTION	REFERENCE SECTION
13	The $\partial P / \partial Q$ matrix printed when $\Phi P B \Phi X(C) = 1$; P and Z represent P- and Q-parameter lists, respectively	2.5.1
14	<u>Indicates that the next covariance matrix printed will include the effects of the Q-parameters.</u> Since $PRC \Phi V(G) = B$, the $(A^T A)^{-1}$ matrix is not printed, but the correlation matrix (Item 10) is	2.5.1

ITEM	DESCRIPTION	REFERENCE SECTION
15	<u>Square roots of the diagonal elements of the $(A^T A)^{-1}$ matrix, with the Q-parameter effects included</u>	
16	<u>Indicates time of the state covariance matrix partitions, as indicated by $PRC\Phi V(B)$ through (F) and $PRC\Phi V(H)$ through (L)</u>	2.5.1

⑪

CARTESIAN FOR	P	PARAMETERS	VEHICLES	1 AND	1	
1.0000000E+14	0.	0.	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	0.	0.	0.	0.	0.
0.0000000	1.0000000E+07	1.0000000E+14	0.	0.	0.	0.
0.0000000	0.0000000	1.0000000E+07	1.0000000E+05	0.	0.	0.
0.0000000	0.0000000	0.0000000	1.0000000E+03	1.0000000E+06	0.	1.0000000E+06
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03	0.
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03

⑫

ORBIT PLANE FOR	P	PARAMETERS	VEHICLES	1 AND	1	
1.0000000E+14	5.4719543E-01	1.6784568E-03	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	-6.2500000E-02	0.	0.	0.	0.
0.0000000	1.0000000E+07	1.0000000E+14	0.	0.	0.	0.
0.0000000	0.0000000	1.0000000E+06	1.0000000E+06	4.5966431E-09	1.0000000E+06	1.4961188E-10
0.0000000	0.0000000	0.0000000	1.0000000E+03	1.0000000E+06	1.0000000E+06	1.0000000E+06
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03	0.
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03

⑬

CARTESIAN FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1	
1.0000000E+14	0.	0.	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	0.	0.	0.	0.	0.
0.0000000	1.0000000E+07	1.0000000E+14	0.	0.	0.	0.
0.0000000	0.0000000	1.0000000E+06	1.0000000E+06	0.	0.	0.
0.0000000	0.0000000	0.0000000	1.0000000E+03	1.0000000E+06	0.	1.0000000E+06
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03	0.
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03

⑭

ORBIT PLANE FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1	
1.0000000E+14	5.4719543E-01	1.6784568E-03	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	-6.2500000E-02	0.	0.	0.	0.
0.0000000	1.0000000E+07	1.0000000E+14	0.	0.	0.	0.
0.0000000	0.0000000	1.0000000E+06	1.0000000E+06	4.5966431E-09	1.0000000E+06	1.4961188E-10
0.0000000	0.0000000	0.0000000	1.0000000E+03	1.0000000E+06	1.0000000E+06	1.0000000E+06
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03	0.
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000E+03

⑮

CARTESIAN FOR	P	PARAMETERS	VEHICLES	2 AND	2	
1.0000000E+14	0.	0.	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	0.	0.	0.	0.	0.
0.0000000	1.0000000E+07	1.0000000E+14	0.	0.	0.	0.

ITEM	DESCRIPTION	REFERENCE SECTION
17	<p><u>Cartesian covariance matrix for Satellite i with respect to itself in an upper triangular format. The lower triangular matrix printed is the normalized correlation matrix. The top item of each column is the square root of the diagonal element (of that column) in the unnormalized matrix. It is identified as a P-parameter matrix, indicating that only the effects of measurement uncertainties are included</u></p>	<p>2.5.1 [OPBØX(H), PRCØV(B)]</p>
18	<p><u>Orbit plane matrices (Item 17)</u></p>	<p>2.5.1 [OPBØX(H), PRCØV(C)]</p>
19	<p><u>Cartesian matrices (Item 17), but including both P- and Q-parameter effects</u></p>	<p>2.5.1 [OPBØX(H), PRCØV(H)]</p>
20	<p><u>Orbit plane matrices (Item 17), but including both P- and Q-parameter effects</u></p>	<p>2.5.1 [OPBØX(H), PRCØV(I)]</p>

0.000000	1.000000E+07	1.000000E+06	0.	0.
0.000000	0.000000	1.000000E+06	0.	0.
0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03
0.000000	0.000000	0.000000	0.000000	1.000000E+03

ORBIT PLANE FOR P AND 3 PARAMETERS VEHICLES 2 AND 2

1.6601563E-02	0.	0.	0.	0.
1.000000E+14	-3.125000E-02	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.
0.000000	1.000000E+07	2.9103630E-10	-1.1641532E-10	1.000000E+06
0.000000	0.000000	1.000000E+06	-4.6566129E-10	1.000000E+06
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03

CAPTESIAN FOR P AND 3 PARAMETERS VEHICLES 2 AND 2

1.000000E+14	0.	0.	0.	0.
1.000000E+14	0.	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.
0.000000	1.000000E+07	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	1.000000E+03	0.000000	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03
0.000000	0.000000	0.000000	0.000000	1.000000E+03

ORBIT PLANE FOR P AND 3 PARAMETERS VEHICLES 2 AND 2

1.6601563E-02	0.	0.	0.	0.
1.000000E+14	-3.125000E-02	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.
0.000000	1.000000E+07	2.9103630E-10	-1.1641532E-10	1.000000E+06
0.000000	0.000000	1.000000E+06	-4.6566129E-10	1.000000E+06
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03

CAPTESIAN FOR P AND 3 PARAMETERS VEHICLES 3 AND 3

1.000000E+14	0.	0.	0.	0.
1.000000E+14	0.	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.
0.000000	1.000000E+07	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	1.000000E+03	0.000000	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03
0.000000	0.000000	0.000000	0.000000	1.000000E+03

1.000000E+07	1.000000E+07	1.000000E+14	0.	0.	0.	0.
0.000000	1.000000E+07	1.000000E+06	1.000000E+06	0.	0.	0.
0.000000	0.000000	1.000000E+07	1.000000E+06	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

OPRIT PLNE FOR P PARAMETERS VHCLES 3 AND 3

1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	1.000000E+07	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

CAPTESIAN FOR P AND 3 PARAMTERS VEHICLES 3 AND 3

1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	1.000000E+07	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

OPRIT PLNE FOR P AND 3 PARAMETERS VEHICLES 3 AND 3

1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	1.000000E+07	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

REFERENCE
SECTION

DESCRIPTION

ITEM

- 21 The matrices described in Items 17 through 20 for Satellites i and j. Since they are asymmetrical, they are printed entirely and as S_{ij} . The matrices of Items 17 through 20 are variance-covariance matrices of particular satellite state vectors in the indicated coordinate systems; the matrices here are intersatellite covariance matrices

CARTESIAN FOR		P	PARAMETERS	VEHICLES	3 AND	1
COVARIANCE		0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.
CORRELATION		0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000



0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000

SPHERICAL COORDINATE PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 0.
 0.
 0.
 0.
 0.
 0.

CORRELATION
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000

CARTESIAN COORDINATE PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 0.
 0.
 0.
 0.
 0.
 0.

CORRELATION
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000
 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000

0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 CORRELATION
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 2

0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 COVARIANCE
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 CORRELATION
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 2

0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 COVARIANCE
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0.
 CORRELATION
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000

```

0. 0. 0. 0. 0. 0. 0. 0. 0.
CORRELATION
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000

```

COVARIANCE MATRICES AT 1.5000000000E+01 MINUTES FROM MIDNIGHT OF EPOCH DATE

ATA(INVERSE) FOR P PARAMETERS

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0001 X 0001 Y 0001 Z 0001 DX 0001 DY 0001 DZ 0002 X 0002 Y 0002 Z 0002 DX
0002 Z 0002 DX 0002 DY 0002 DZ 0003 X 0003 Y 0003 Z 0003 DX
0003 DY 0003 DZ
3.531205E+11
-3.95845E+11 4.60113E+11
-5.69830E+10 -4.98050E+10 7.98815E+11
-3.91601E+08 4.38308E+08 6.34054E+07 4.34672E+05
4.38931E+08 -5.10171E+08 5.58214E+07 -4.97127E+05 5.66192E+05
6.31783E+07 5.52199E+07 -8.85759E+08 -7.03628E+04 -6.15027E+04 9.83064E+05
5.33716E+08 -6.29350E+08 1.25865E+08 -5.82422E+05 6.87427E+05 -1.36915E+05 7.60206E+13
-2.40359E+08 2.95756E+08 -5.27310E+07 1.47751E+05 -1.88544E+05 2.55990E+04 -1.59975E+13 4.30231E+12
-1.30249E+07 1.63585E+07 -7.93590E+06 1.18180E+04 -1.50363E+04 8.05975E+03 4.45137E+12 2.19633E+12
9.91881E+13
-1.13203E+04 1.32332E+04 -2.35961E+03 1.26326E+01 -1.48246E+01 2.63983E+00 -2.19683E+08 -1.43406E+08
3.94952E+07 9.9974E+05
3.25854E+04 -3.67383E+04 -2.57392E+03 -3.72067E+01 4.20588E+01 2.56069E+00 -1.45203E+08 -8.58606E+08
1.99298E+07 -1.30267E+03 9.92470E+05
-2.02055E+03 2.31452E+03 2.47115E+00 2.21733E+00 -2.53874E+00 -9.66537E-03 3.98806E+07 1.99271E+07
-7.31579E+06 3.59396E+02 1.82549E+02 3.99932E+05
7.95618E+08 -9.14109E+08 5.95473E+07 -9.34592E+05 1.07601E+06 -9.15048E+04 3.12931E+12 -6.90444E+12
-5.9883E+12 2.78551E+08 -6.49518E+07 -3.41541E+07 5.08940E+13
-7.22552E+08 8.31115E+08 2.34831E+05 7.52724E+05 -8.75885E+05 -1.33712E+04 2.33184E+13 -5.15376E+12
-4.58690E+12 2.11323E+08 -4.39860E+07 -4.12697E+07 -3.60614E+13 7.19750E+13
-2.12015E+06 -7.63588E+06 5.25016E+07 1.13195E+04 -2.0989E+03 -6.68831E+04 -5.36032E+12 1.18309E+12
1.01227E+12 -4.75526E+07 1.01820E+07 9.19850E+06 8.31580E+12 6.27633E+12 9.88246E+13
2.45174E+04 -2.82214E+04 1.56221E+03 -2.76669E+01 3.18611E+01 -1.86213E+00 2.83191E+08 -6.25285E+07
-5.32841E+07 2.47599E+03 -4.95056E+02 -4.89451E+02 -4.35214E+08 -3.32488E+08 7.56176E+07 9.95984E+05

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0003 DY -1.81126E+03 2.10196E+03 7.25944E+01 1.67363E+00-1.93421E+00-1.75161E-01 2.11548E+08-4.67322E+07
-4.11377E+07 1.83381E+03-4.01785E+02-3.65425E+02-3.25154E+08-2.46756E+08 5.53336E+07-3.00220E+03
9.97878E+05
0003 OZ -2.08193E+03 2.34371E+03 1.67233E+02 2.38779E+00-2.69464E+00-1.05846E-01-4.74797E+07 1.04623E+07
9.10055E+06-4.31756E+02 9.38095E+01 9.10051E+01 7.51766E+07 5.09381E+07-1.27453E+07 6.77993E+02
4.93161E+02 9.99365E+05

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CORRELATION MATRIX

```

0001 X 1.000
0001 Y -.952 1.000
0001 Z -.107 -.062 1.000
0001 OX -1.000 .981 .108 1.000
0001 OY .952 -1.000 .982 -.962 1.000
0001 OZ .107 -.062 -1.000 1.000
0002 X .000 -.000 .000 1.000
0002 Y -.000 .000 .000 -.805 1.000
0002 Z -.000 .000 .000 .051 .106 1.000
0002 OX -.000 .000 .000 -.025 -.069 .004 1.000
0002 OY .000 -.000 .000 -.817 -.416 .002 -.001 1.000
0002 OZ -.600 .000 .000 -.000 .005 .010 -.001 .000 1.000
0003 X .000 -.000 .000 .503 -.467 -.084 .039 -.009 -.008
0003 Y 1.000 .000 .000 .315 -.293 -.054 .025 -.005 -.005
0003 Z -.596 1.000 .000 .000 -.062 .057 .010 -.005 .001 .001
0003 OX .117 .074 1.000 .000 .000 .033 -.030 .005 .002 -.000
0003 OY -.051 -.039 .000 .000 1.000 .024 -.023 -.004 .002 -.000
0003 OZ -.046 -.029 .000 .000 .006 -.003 1.000 .000 .002 -.000
0003 OZ -.000 .000 .000 .000 .000 .000 .000 .000 .000 .000
.011 .007 -.001 .001 .000 1.000

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SORT DIAG 5.942389E+05 5.763160E+05 8.937646E+05 6.592966E+02 7.524574E+02 9.914957E+02
8.718980E+06 2.074201E+06 9.959324E+06 9.990364E+02 9.962281E+02 9.999658E+02
7.134002E+06 8.483807E+06 9.930989E+06 9.979902E+02 9.989384E+02 9.999427E+02
PIVOT RATIOS 1.000000E+00 3.121352E+00 5.622979E+04 5.573979E+02 9.647004E+09 7.167672E+07

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1.031672E+00 2.757727E+06 1.607000E+10 4.199575E+09 3.746249E+10 1.520903E+08
4.494169E+11 5.827161E+11 4.195380E+10 1.175047E+10 6.545311E+09 3.455491E+08

A PIVOT RATIO EXCEEDS 10**5.

C-CHECK ATA MATRIX FOR ILL CONDITIONING.

(2)

DPDQ MATRIX

	3	RBIA	1	ABIA	3	ALT	1	RBIA	1	LONG	3	LAT	2	RBIA	1	LONG	1	LAT	2	LONG	2	LAT									
0001 X	-2.36834E-05	-7.81713E-06	-2.60310E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00	1.26256E+00									
0001 Y	-2.80096E+05	1.12494E+06	7.51958E-01	-3.70436E-01	1.66467E+06	-3.85520E+05	3.40657E+07	-5.53076E+03	4.10495E-05	-1.71952E-06	-4.9197E+00	7.54816E+00	-5.93667E-05	-4.68304E-05	-6.66842E+00	1.16154E+01	7.38315E+05	-1.33785E+06	6.57451E-01	-5.49701E-01	1.98414E+06	2.99101E+07	-4.85482E+03								
0001 Z	7.21551E-06	4.44211E-06	1.09315E-01	-2.69904E+00	7.25517E-06	2.68415E-06	3.68664E-02	-7.18194E-01	-2.21382E+06	-5.85305E+05	9.49669E-02	5.75163E-01	-1.35229E+04	2.66546E+06	8.82286E+06	-1.46121E+03	1.04622E-07	5.75326E-08	5.99734E-03	1.23686E-02	8.69107E-08	4.44900E-08	1.00548E-02	1.59178E-02							
0001 DX	-5.84716E+01	8.43196E+01	-5.42129E-06	1.84740E-05	1.34747E-02	-1.09208E+01	-7.66387E+04	1.24547E+01	-1.37459E-04	2.10187E-04	-2.45183E-03	2.23575E-03	6.48182E-09	1.15911E-09	-3.30283E-03	5.41580E-03	-4.22238E+01	5.27373E+01	-5.01474E-06	1.33685E-05	8.67424E+01	-2.40302E+00	-6.69553E+04	1.06783E+01							
0001 07	-1.59490E-09	4.67495E-09	-1.29763E-04	1.26740E-03	1.64569E-09	2.88010E-09	3.74166E-04	1.24547E+01	-2.70105E+01	4.09316E+00	-7.35124E-07	8.87116E-06	1.50068E+01	2.30606E+01	-9.62948E+03	1.56446E+00	2.33352E-01	1.83193E-01	1.83504E+04	-5.10754E+04	-2.09430E-01	-1.44624E-01	-2.61938E+04	4.14898E+04							
0002 X	-2.19788E+04	3.07389E+04	-3.78264E-02	3.07754E-02	4.55747E+04	-1.6827E+04	-5.14906E+06	1.11816E+03	-5.35631E-02	-4.11798E-02	-4.16692E+03	1.12764E+04	-4.68654E-01	-3.23975E-01	-5.91370E+04	9.37507E+04	-2.59103E+05	-3.73758E+05	4.72482E-01	3.79354E-01	-5.43556E+05	5.45878E+07	-1.03153E+04	-4.75240E-02	-3.68741E-02	-3.65852E+03	1.03891E+04	3.68497E-02	2.55568E-02	4.60286E+03	-7.32752E+03
0002 Z	5.79101E+03	-6.25393E+03	1.02692E-02	-8.29786E-03	1.21035E+04	3.22602E+03	1.72902E+06	-3.30763E+02	2.20449E-06	1.69336E-06	1.67152E-01	-4.81607E-01	1.88484E-06	-1.32622E-06	-2.37883E-01	3.75423E-01	-1.55103E-01	2.15187E-01	-2.62990E-07	2.14921E-07	3.18425E-01	-7.93249E-02	-5.69598E+01	1.10034E-02							
0002 0Y	-4.31831E-07	-3.20196E-07	-3.77475E-02	8.52043E-02	4.09298E-06	-2.93216E-06	-5.42572E-01	8.26088E-01	2.28683E+00	-3.25725E+00	4.26399E-06	3.40614E-06	-4.75493E+00	1.32453E+00	4.96229E+02	-8.77074E-02	4.33556E-07	-3.30549E-07	-3.33537E-02	3.18057E-02	3.37780E-07	2.32458E-07	4.28123E-02	-6.74639E-02							
0003 X	-4.10956E-01	-3.13569E-01	-3.13871E+04	9.70410E+04	1.73991E-01	1.64868E-02	1.55675E+01	-2.70867E-03	5.49138E-02	-7.95335E-02	9.71464E-08	7.85397E-08	-1.16436E-01	1.19327E-01	2.20030E+04	-3.49852E+04	1.12986E+05	-1.63136E+05	2.05307E-01	-1.64980E-01	-2.38382E+05	6.57237E+04	2.93490E+07	-5.65024E+03							
0003 Y	8.09614E-01	-2.31324E-01	-2.32935E+04	5.45937E+04	1.33126E-01	9.21630E-02	1.66738E+04	-2.66749E+04	6.51453E+04	-1.23118E+05	1.58579E-01	1.26715E-01	1.79513E+05	5.00713E+04	2.12793E+07	-4.17091E+03	6.94281E-02	5.39569E-02	5.35700E+03	1.50055E+04	-3.04045E-02	-2.10249E-02	3.85076E+03	6.09083E+03							
0003 Z	-1.95040E+04	2.80104E+04	-3.65622E-02	2.91738E-02	4.09382E+04	-1.15718E+04	-4.96318E+06	9.50472E+02	-3.86795E-06	-2.88390E-06	-2.91864E-01	9.11457E-01	1.54838E-06	1.06605E-06	1.94912E-01	-3.10914E-01	9.99090E-01	-1.43312E+00	1.67305E-06	-1.49468E-06	-2.00575E+00	5.86590E-01	2.77277E+02	-5.54444E-02							

REFERENCE
SECTION

ITEM

DESCRIPTION

22 A remark printed when the $A^T A$ matrix is inverted if a pivot ratio exceeds 10^5 . It hints that the $A^T A$ may be ill-conditioned

0003 DY -2.87436E-06-2.16307E-06-2.14964E-01 5.16675E-01 1.26298E-06 8.74711E-07 1.59626E-01-2.53642E-01
 7.37147E-01-1.05361E+00 1.36986E-06-1.10765E-06-1.53908E+00 4.35296E-01 1.95535E+02-3.65703E-02
 0003 FZ 6.59625E-07 5.09326E-07 5.07943E-02-1.40773E-01-2.62087E-07-1.81147E-07-3.31229E-02 5.25211E-02
 -1.69743E-01 2.41374E-01-3.07621E-07 2.47328E-07 3.53863E-01-9.60879E-02-5.05561E+01 9.41950E-03

ATA(INVERSE) FOR P AND Q PARAMETERS

	0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ	
0001 X	1.000												
0001 Y	-.978	1.000											
0001 Z	-.091	-.112	1.000										
0001 DX	-.920	.862	.101	1.000									
0001 DY	.920	-.916	.077	-.981	1.000								
0001 DZ	.101	.073	-.887	-.107	-.981	1.000							
0002 X	.000	-.000	.000	-.000	-.000	-.000	1.000						
0002 Y	-.015	.016	-.007	-.001	-.001	-.001	-.000	1.000					
0002 Z	-.000	-.000	-.000	-.000	-.000	-.000	-.000	.106	1.000				
0002 DX	.000	-.000	.000	-.000	-.000	-.000	-.000	-.069	.004	1.000			
0002 DY	-.000	.000	-.000	-.000	-.000	-.000	-.000	-.017	-.415	.002	1.000		
0002 DZ	-.000	.000	-.000	-.000	-.000	-.000	-.000	.005	-.010	-.001	.000	1.000	
0003 X	-.002	.002	-.001	-.000	-.000	-.000	-.000	.503	-.466	-.084	.039	-.009	-.008
0003 Y	1.000	-.001	-.001	.000	-.000	-.000	-.000	.315	-.292	-.054	.025	-.005	-.005
0003 Z	-.596	1.000	.000	.000	.000	.000	-.000	-.062	.057	.010	-.005	.001	.001
0003 DX	.000	-.000	.000	.000	.000	.000	-.000	.033	-.030	-.009	.002	-.000	-.000
0003 DY	-.051	-.039	.008	1.000	-.000	-.000	-.000	.024	-.023	-.004	.002	-.000	-.000
0003 DZ	-.046	-.329	.006	-.003	1.000	-.000	-.000	-.005	.005	.001	-.000	.000	.000
0003 DX	.000	-.000	.000	-.000	-.000	-.000	.000	-.000	.000	.000	-.000	.000	.000
0003 DY	.011	.007	-.001	.001	.001	.000	1.000						

CORRELATION MATRIX

	0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ	0003 X	0003 Y	0003 Z	0003 DX	0003 DY	0003 DZ	
0001 X	1.000																		
0001 Y	-.978	1.000																	
0001 Z	-.091	-.112	1.000																
0001 DX	-.920	.862	.101	1.000															
0001 DY	.920	-.916	.077	-.981	1.000														
0001 DZ	.101	.073	-.887	-.107	-.981	1.000													
0002 X	.000	-.000	.000	-.000	-.000	-.000	1.000												
0002 Y	-.015	.016	-.007	-.001	-.001	-.001	-.000	1.000											
0002 Z	-.000	-.000	-.000	-.000	-.000	-.000	-.000	.106	1.000										
0002 DX	.000	-.000	.000	-.000	-.000	-.000	-.000	-.069	.004	1.000									
0002 DY	-.000	.000	-.000	-.000	-.000	-.000	-.000	-.017	-.415	.002	1.000								
0002 DZ	-.000	.000	-.000	-.000	-.000	-.000	-.000	.005	-.010	-.001	.000	1.000							
0003 X	-.002	.002	-.001	-.000	-.000	-.000	-.000	.503	-.466	-.084	.039	-.009	-.008						
0003 Y	1.000	-.001	-.001	.000	-.000	-.000	-.000	.315	-.292	-.054	.025	-.005	-.005						
0003 Z	-.596	1.000	.000	.000	.000	.000	-.000	-.062	.057	.010	-.005	.001	.001						
0003 DX	.000	-.000	.000	.000	.000	.000	-.000	.033	-.030	-.009	.002	-.000	-.000						
0003 DY	-.051	-.039	.008	1.000	-.000	-.000	-.000	.024	-.023	-.004	.002	-.000	-.000						
0003 DZ	-.046	-.329	.006	-.003	1.000	-.000	-.000	-.005	.005	.001	-.000	.000	.000						
0003 DX	.000	-.000	.000	-.000	-.000	-.000	.000	-.000	.000	.000	-.000	.000	.000						
0003 DY	.011	.007	-.001	.001	.001	.000	1.000												

0003 DZ 6.378695E+05 7.439833E+05 1.004205E+06 6.596158E+02 7.525788E+02 9.915107E+02

0.718984E+06 2.076192E+06 9.959324E+06 9.990364E+02 9.962284E+02 9.999658E+02
 7.134112E+06 8.483860E+06 9.930992E+06 9.974902E+02 9.989385E+02 9.999427E+02

STATE COVARIANCE AND CORRELATION MATRIX PARTITIONS AT 1.500000000E+01 MNOED

CARTESIAN FOR	P	PARAMETERS	VEHICLES	1 AND	1
3.2175436E+08	-3.606708E+00	-5.102480E+07	2.208294E+04	1.6676030E+04	2.4263728E+03
1.7937529E+04	4.191498E+08	-4.529713E+07	-2.707472E+04	-1.9063559E+04	-3.4465145E+03
-9821182	2.0473149E+04	7.270032E+08	6.225284E+03	5.4383081E+03	4.6664559E+03
-1670885	-0.020075	2.697942E+04	4.3609561E+05	-4.888323E+05	-7.0230478E+04
.001931A	-0.020026	.0003494	6.6037536E+02	5.6810087E+05	-6.1300055E+04
.0012336	-0.012072	.0002574	-0.9021153	7.5372467E+02	9.0642773E+05
.0001352	-0.001695	.0001741	-0.1070705	-0.0020047	9.9319068E+02

ORBIT PLNE FOR	P	PARAMETERS	VEHICLES	1 AND	1
2.7777930E+06	3.791996E+07	7.0223517E+07	-2.3640455E+03	3.2425201E+02	6.0705633E+02
2.9627340E+03	7.3241417E+00	-3.669880E+06	-4.4261641E+04	6.1262670E+03	4.3502473E+03
.4729304	2.7063152E+04	7.2760224E+08	-5.2678386E+02	4.2365401E+01	3.9236209E+03
.8787046	-0.050272	2.6974103E+04	1.1898322E+04	5.1393048E+04	9.5165149E+04
-0.073151	-0.014936	-0.001790	1.0907943E+02	9.9268444E+05	-4.9926390E+03
.001098	.0002272	.0000016	.4720854	9.9633551E+02	9.0604146E+05
.0002053	.0001619	.0001465	.8785925	-0.0050463	9.9299620E+02

CARTESIAN FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1
6.2200139E+10	-7.1403303E+10	1.6742802E+09	4.5846001E+06	3.3563025E+06	5.5123725E+05
2.4939956E+05	8.6394210E+10	-3.2655144E+10	-5.6863541E+06	-4.1999294E+06	-8.4880572E+05
-0.0741042	2.9391192E+05	2.1393226E+11	3.0695054E+06	2.505640E+05	1.5101347E+06
.0145141	-0.2402132	4.622812E+05	4.3647236E+05	-4.085900E+05	-7.0169303E+04
.0278250	-0.0292845	.0100450	6.6066055E+02	5.6030829E+05	-6.1341510E+04
.0178514	-0.0149554	.0071855	-0.9809513	7.5306225E+02	9.0644313E+05
.0022254	-0.0023077	.0033047	-0.1069383	-0.0019269	9.9319843E+02

ORBIT PLNE FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1
2.6822083E+09	1.1571932E+10	2.1456475E+10	-7.2146624E+05	9.0954600E+04	1.0545159E+05
5.1790041E+04	1.5695296E+11	3.4073570E+10	-9.5157091E+06	1.3155750E+06	1.1250127E+06
	2.0298145E+11	-2.3165101E+06	3.1210067E+05	3.1210067E+05	1.3087766E+06

.5641743 3.9604666E+05 1.2473137E+04 5.1313597E+04 9.5096076E+04
 .9199946 .1954444 4.5053463E+05 9.9269543E+05 -4.9831336E+03
 -.1247332 -.2151330 -.0460383 1.1168320E+02 9.8605522E+05
 .0019177 .0033340 .0005953 .4611439
 .0035051 .0024606 .0029254 .0574802 9.9300313E+02

CAPTESIAN FOR P PARAMETERS VEHICLES 2 AND 2
 7.6105349E+13 -1.6289492E+13 4.5017469E+12 3.1628196F+08 -3.0290905E+08 1.3216039E+07
 3.5903182E+12 2.2519239E+12 -6.7715842F+07 6.7798093E+07 1.0688901E+07
 8.7238379E+06 1.8949135E+06 9.9778350E+06 9.9762234E+05 -1.3567849E+03 5.4543889E+01
 -.9853870 .1131100 9.9778350E+06 .0018047 9.9881046E+02 9.8498301E+05 9.9797595E+05
 .0517171 -.0357800 .0074431 -.0013687 9.9246310E+02
 -.0349857 .0350526 .0419553 .0000547 .0000552 9.9898746E+02
 .0015155 .0055469 .0419553 .0000547 .0000552

OPRIT PLNE FOR P PARAMETERS VEHICLES 2 AND 2
 5.0255705E+12 1.9042156E+13 2.9388060E+12 8.3808996E+07 7.6922440E+07 1.2424508E+07
 2.2418007E+06 7.4159309E+13 -2.9536344E+12 3.1663350E+08 2.9974764E+08 -1.1871329E+07
 .9862954 8.6121605E+06 1.0002953E+07 9.9752616E+02 9.9874643E+02 9.9898883E+02
 .1310526 -.0342860 .0370427 .0059808 .0018047
 .0376652 .0349488 -.0012881 .0002332
 .0343559 .0017798 .0419025 .0002332
 .0055478 -.0017798 .0419025 .0002332

CAPTFSTAN FOR P AND Q PARAMETERS VEHICLES 2 AND 2
 7.6105407E+13 -1.6289492E+13 4.5017313E+12 3.1628212F+08 -3.0292179E+08 1.3215736E+07
 3.5907853E+12 2.2521128E+12 -6.7717793E+07 6.7951823E+07 1.0692555E+07
 8.7238413E+06 1.6970465E+06 9.9778352E+06 9.9752234E+05 -1.3568203E+03 5.4543046E+01
 -.9842692 .1142798 .0018047 9.9881046E+02 9.9246451E+02 9.9898746E+02
 .0517169 -.0337389 .0074435 -.0013688 .0000547
 .0362981 .0560918 .0419553 .0000547
 -.0349871 .0055421 .0419553 .0000547
 .0015154 .0055421 .0419553 .0000547

OPRIT PLNE FOR P AND Q PARAMETERS VEHICLES 2 AND 2
 5.0341812F+12 1.9042550E+13 2.9387430E+12 8.3963136E+07 7.6918836E+07 1.2424516E+07
 7.4159327E+13 -2.9536373E+12 3.1664063E+08 2.9974748E+08 -1.1871329E+07

2.2436981E+06
 .9854816
 .1309390
 .0377035
 .0343252
 .0055431

CAPTEIAN FOR P PARAMETERS VEHICLES 3 AND 3
 5.0629232E+13 -3.6557197E+13 8.4278945E+12 1.4277494E+08 -4.9555185E+08 3.5499598E+07
 7.1154221E+06 7.2805002E+13 6.4011415E+12 3.4237504E+07 1.1819530E+09 2.7160446E+07
 -.6021277 8.5325433E+06 9.8986190E+13 6.1106247E+07 1.3776988E+08 4.1398887E+08
 .1190505 .0754026 9.9491804E+06 9.9620641E+05 -1.7982520E+03 2.5247148E+02
 .0201037 .0040202 .0061537 9.9810141E+02 1.0037179E+06 5.7554781E+02
 -.0695155 .1392645 .0138217 -.0017983 1.0018572E+03 9.9796212E+05
 .0049942 .0031864 .0416528 .0002932 .0005751 9.9898054E+02

ORBIT PLNE FOR P PARAMETERS VEHICLES 3 AND 3
 5.8638558E+13 3.8077557E+13 7.8605884E+12 1.0612806E+09 1.4011883E+08 3.3304398E+07
 7.657818E+06 6.4795676E+13 -7.0862562E+12 6.6990658E+08 2.6343999E+08 -2.9811547E+07
 .6177334 8.0433538E+06 9.9491804E+06 1.4674912E+08 -3.4343804E+07 4.1398887E+08
 .1031754 -.0884818 .0147293 1.0027977E+06 3.8494283E+03 6.1253480E+02
 .1383996 .0831058 .0327741 1.0013979E+03 9.9712662E+05 -1.4870627E+02
 .0183243 .0327741 -.0034568 .0030496 9.9856228E+02 9.9796212E+05
 .0043536 -.0037072 .0416528 .0006123 -.8001411 9.9898054E+02

CAPTEIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 3
 5.0630830E+13 -3.6555984E+13 8.4276196E+12 1.4278609E+08 -4.9552519E+08 3.5498540E+07
 7.1155344E+06 7.2805923E+13 6.4009328E+12 3.4245938E+07 1.1819727E+09 2.7159649E+07
 -.6020944 8.5325973E+06 9.8986237E+13 6.1106336E+07 1.3776539E+08 4.1398905E+08
 .1190447 .0753997 9.9491827E+06 9.9620649E+05 -1.7980722E+03 2.5246418E+02
 .0201050 .0040211 .0061535 9.9810144E+02 1.0037183E+06 5.7553882E+02
 -.0695108 .1382659 .0138212 -.0017982 1.0018574E+03 9.9796212E+05
 .0049940 .0031863 .0416528 .0002932 .0005751 9.9898054E+02

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 3
 5.8639947E+13 3.8075304E+13 7.8603321E+12 1.0613136E+09 1.4011235E+08 3.3303411E+07

7.6576725E+06	6.4737606E+13	-7.0860351E+12	6.6986348E+08	2.6344511E+08	-2.9810664E+07
.6177004	9.8986237E+13	9.8986237E+13	1.4674439E+08	-3.4341956E+07	4.139895E+08
.1031708	6.0497084E+06	9.9491827E+06	1.0027981E+06	3.0493235E+03	6.1251675E+02
.1384013	-.0884781	.0147288	1.0013981E+03	9.9712664E+05	-1.4078227E+02
.0183233	.0831022	-.0034567	.0030495	9.9796212E+05	9.9796212E+05
.0043535	.0327744	.0416528	.0006123	9.9856229E+02	9.9898054E+02
	-.0037071			-.0001410	

CARTESIAN FOR P PARAMETERS VEHICLES 2 AND 1

COVARIANCE					
8.934599E+06	-1.0595572E+07	2.6084191E+06	-5.7085902E+05	6.7375314E+05	-1.3448439E+05
-1.0831504E+08	1.2823072E+08	-2.9982556E+07	1.1551890E+05	-1.5208875E+05	2.8172856E+04
-2.4000922E+06	2.8437946E+06	-6.8108335E+05	1.3843679E+04	-1.7347943E+04	8.0536665E+03
2.4704883E+01	-2.9352397E+01	7.6393884E+00	1.5411378E+01	-1.8101439E+01	3.2920418E+00
-1.9641803E+03	2.3264094E+03	-5.5121137E+02	-3.5973200E+01	4.8461576E+01	2.8325075E+00
-4.6799327E+01	5.5381141E+01	-1.2793777E+01	2.2038050E+00	-2.5225904E+00	-3.9131161E-02

CORRELATION

.0000571	-.0031860	-.0000134	.0000014	+.0001103	-.0000026
-.0000593	.0033055	.0000139	-.0000814	.0001145	.0000027
.0000111	-.0005865	-.0000025	.0000003	-.0000206	-.0000005
-.0000991	.0000923	.0000021	.0000234	-.0000549	.0000033
.0901025	-.0001065	-.0000023	-.0000240	.0000541	-.0000034
-.0000155	.0000150	.0000000	.0000033	.0000029	-.0000000

ORBIT PLNE FOR P PARAMETERS VEHICLES 2 AND 1

COVARIANCE					
-7.9585977E+06	-1.7071423E+08	-3.8553223E+05	2.1637573E+04	2.2444095E+05	-6.0226233E+03
-4.2530105E+05	-7.8662167E+06	-1.4682637E+05	4.4653358E+04	8.8274587E+05	-2.0269566E+04
6.5781894E+04	1.2632631E+06	-2.4308708E+03	-2.4454433E+03	-5.6316699E+04	5.9439000E+03
-1.6285789E+02	-3.0901438E+03	-1.4150869E+01	-1.4279298E+00	-3.3534847E+01	1.2191114E+01
3.7535057E+00	7.2419108E+01	-3.1988955E-01	-1.0963108E+00	-2.1573836E+01	3.6749836E-01
2.3497174E-02	-2.5862197E-01	3.8244596E-01	2.4532861E-01	6.4853808E+07	-9.6722833E-01

CORRELATION

-.0013488	-.0000167	.0000022	-.0000554	.0000013	.0000000
-.0025138	-.0000338	.0000047	-.0001150	.0000027	-.0000000
-.0000054	-.0000006	-.0000008	-.0000005	-.0000000	.0000000
.0000885	.00000475	-.0000022	-.0000132	-.0000101	.0000023

.0001005 .0001029 -.0000157 -.0000541 -.0000217 .0000065
 -.0000027 -.0000024 .0000006 .0000124 .0000004 -.0000010

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE
 1.7929353E+09 -2.2310125E+09 1.2508071E+09 -4.2283156E+05 7.6356927E+05 -1.7023655E+05
 -2.1709684E+10 2.6947660E+10 -1.4682790E+10 -1.6705065E+06 -1.4765808E+06 -2.6216529E+05
 -4.8132437E+08 5.9814394E+08 -3.3032415E+08 -2.5820093E+04 -4.6767197E+04 1.5830111E+03
 4.9646370E+03 -5.1954654E+03 3.5873131E+03 1.58222968E+01 -1.7795963E+01 3.3600461E+00
 -3.9380451E+05 4.8912853E+05 -2.6849246E+05 -6.8400543E+01 1.6411591E+01 -2.4491887E+00
 -9.3774215E+03 1.1633327E+04 -6.2961199E+02 1.4329710E+00 -3.0941809E+00 -1.6421889E-01

CORRELATION

.0006241 -.0458860 -.0001334 .0000199 -.0015910 -.0000376
 -.0005701 .0493310 .0002040 -.0000211 .0016768 .0000396
 .0003100 -.0157337 -.0000715 .0000078 -.0005849 -.0000136
 -.0000734 -.0013329 -.0000039 .0000240 -.0001043 .0000022
 .0001131 -.0010325 -.0000152 -.0000236 .0000219 -.0000041
 -.0000127 -.0001391 .0000002 .0000034 -.0000025 -.0000002

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE
 -2.7339520E+09 -3.6620775E+10 -8.4749913E+09 2.2333139E+06 -8.1344371E+04 -2.6946647E+05
 -1.2978691E+08 -1.6937524E+09 -4.2657753E+08 1.4698314E+05 8.6860064E+05 -3.2641239E+04
 2.0074590E+07 2.7073002E+08 6.1238609E+07 -1.8794398E+04 -5.4056464E+04 7.8838342E+03
 -4.9700173E+04 -5.6323391E+05 -1.5544071E+05 3.8629511E+01 -5.9072546E+01 7.4095292E+00
 1.1454750E+03 1.5511296E+04 3.4602115E+03 -2.0329611E+00 -2.1444342E+01 4.7838349E-01
 7.1896143E+00 -3.6705656E+01 9.4110508E+01 2.4743495E-01 6.4850854E+00 -9.6693755E-01

CORRELATION

-.0235277 -.0002910 .0000388 -.0009669 .0000221 .0000001
 -.0412113 -.0004966 .0000583 -.0016872 .0000392 -.0000001
 -.0003039 -.0001099 .0000136 -.0003475 .0000077 .0000002
 .0003125 .0001528 -.0000168 .0003405 -.0000182 .0000022
 -.0000354 .0001012 -.0000054 -.0000597 -.0000216 .0000065
 -.0001209 -.0000038 .0000008 .0000075 .0000005 -.0000010

CARTESIAN FOR P PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -4.7072220F+07 5.5719171E+07 -1.2973433E+07 -9.5853022E+05 1.1031335E+06 -9.3143039E+04
 -3.5747314E+07 4.2308831E+07 -9.8167056E+06 7.6735626E+05 -8.6119579E+05 -1.3701253E+04
 8.0924852E+06 -9.5814814E+06 2.2473430E+06 1.3403693E+04 -4.5173460E+03 -6.7029143E+04
 -3.2652510F+02 3.8691540E+02 -9.2290050E+01 -2.1487343E+01 2.4755126E+01 -1.5277315E+00
 -7.6135299F+02 9.0141211E+02 -2.1116079F+02 5.57622450E+00 -5.4063330E+00 -5.7775586E-01
 3.0752677E+01 -3.6473753E+01 9.0161460E+00 2.3323757E+00 -2.6832796E+00 1.3464129E-01

CORRELATION
 -.0003688 .0002336 .0000453 -.0000162 .0000424 .0000017
 .0003825 .002422 -.000470 .0000189 .0000439 .0000018
 -.0000676 -.0000426 .0000084 .0000074 .0000079 .0000003
 -.0002040 .0001362 .0000020 .0000328 .0000084 .000003
 .0002057 .0001370 .0000005 .0000329 .0000085 .0000007
 -.0000132 -.0000016 -.0000060 .0000015 .0000005 .0000001

ORBIT PLANE FOR P PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -3.6119022E+06 -5.8997043E+07 -6.9181919E+04 3.1336702E+04 6.5621658E+05 -1.8235477E+05
 3.2605451E+05 5.2210135E+07 9.9138903E+04 6.2719971E+04 1.6428049E+06 -1.9951150E+05
 6.6835049E+05 1.2723825E+07 3.5376742E+04 -7.3386461E+03 6.6245082E+02 -6.8107633E+04
 -6.6810547F+01 -1.2718436E+03 -3.5651900E+00 6.6506855E-02 2.0495404E+00 -1.2271795E+00
 1.4944146E+01 2.8159102E+02 2.3602907E+00 1.2980074E+00 3.3492600E+01 -4.4945657E+00
 2.5914387E+00 4.8484593E+01 5.9594340E-01 1.3417492E-01 3.5220987E+00 -4.6467717E-01

CORRELATION
 -.0001592 .0001367 .0000227 .00000225 .0000051 .0000009
 -.0003329 .0002856 .0000473 .0000469 .0000104 .0000018
 -.0000003 .0000005 .0000001 .0000001 .0000001 .0000000
 .0000375 .0000714 .0000068 .0000006 .0000119 .0000012
 .0001122 .0002848 .0000001 .0000021 .0000337 .0000035
 -.0000240 -.0000250 .0000069 .0000012 .0000045 .0000005

CAPESTIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -9.4338096E+09 1.1707609E+10 -6.3640370E+09 -1.7344136E+06 5.2776631E+05 -2.1919405E+05
 -7.1635924E+09 9.8897466E+09 -4.8224169E+09 1.7832682E+05 -1.3179879E+06 -1.8934715E+05
 1.6221027E+09 -2.0137731E+09 1.0991525E+09 1.4688048E+05 9.4469452E+04 -4.5321068E+04

-6.5476689E+04 8.1352974E+04 -4.4829563E+04 -2.6881528E+01 2.0754286E+01 -2.4072221E+00
 -1.5260734E+05 1.8944432E+05 -1.0332328E+05 -6.9601579E+00 -1.5720116E+01 -2.6195112E+00
 6.1720029E+03 -7.8819708E+03 4.3192140E+03 2.8421303E+00 -2.3050970E+00 2.1819919E-01
 CORRELATION
 -.0053160 -.0033663 -.0006537 -.0002630 -.0006108 -.0000248
 .0055981 .0035444 -.0006887 .0002773 .0006434 -.0000262
 -.0019337 -.0012219 .0002389 .0000971 -.0002230 .0000093
 -.0003689 .0000316 .0000223 .0000408 .0000105 .0000043
 .0000984 .0000209 .0000126 .0000276 .0000208 -.0000031
 -.0000310 -.0000129 -.0000046 -.0000024 -.0000026 .0000002

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -1.1022504E+09 -1.4794515E+10 -3.4006298E+09 9.2481217E+05 7.3269624E+05 -2.885861E+09
 9.9505835E+08 1.3342944E+10 3.0768329E+09 -7.4310476E+05 1.7542074E+06 -1.0358416E+05
 2.0396584E+08 2.7297776E+09 6.3352011E+08 -1.7220284E+05 2.3454186E+04 -4.8460640E+04
 -2.0389803E+04 -2.7286356E+05 -6.3333280E+04 1.6546038E+01 -2.2868040E-01 -3.1911187E+00
 4.5605331E+03 6.0430028E+04 1.4460859E+04 -2.3557267E+00 3.3997695E+01 -4.0563125E+00
 7.9045116E+02 1.0424517E+04 2.5428107E+03 -4.9554408E-01 3.6091494E+00 -4.0898026E-01

CORRELATION
 -.0027793 .0023868 .0003939 .0000882 .0000153
 -.0048782 .0041853 .0006928 .0001530 .0000263
 -.0009857 .0008484 .0001413 .0000321 .0000056
 .0010814 .0008266 .0001479 .0000211 .0000044
 .0000950 .0002187 .0000024 .0000342 .0000034
 -.0000380 -.0000130 -.0000049 -.0000041 -.0000004

CARTESIAN FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE
 3.1709093E+13 -7.0437679E+12 -6.0675963E+12 1.2982352E+08 -1.3570345E+08 -2.7984726E+07
 2.378979E+13 -5.2895328E+12 -4.6791937E+12 1.0170699E+08 -9.7512713E+07 -2.1305368E+07
 -5.4229338E+12 1.2042102E+12 1.0245682E+12 -2.2138259E+07 2.2273272E+07 4.7706077E+06
 2.2762675E+08 -5.0548372E+07 -4.3862959E+07 9.0087824E+02 -8.6890320E+02 -2.0952304E+02
 5.1910930E+08 -1.1537144E+08 -1.0112271E+08 2.1737610E+03 -2.1477007E+03 -4.5707086E+02
 -2.1875391E+07 4.8614707E+06 4.2641136E+06 -9.8858506E+01 9.3499666E+01 1.8132437E+01

CORRELATION

.5108290	.3195837	-.0624798	.0261421	.0593944	-.0025101
-.5224418	-.3271035	.0638776	-.0267280	-.0607751	.0022565
-.0854628	-.0549602	.0103208	-.0043240	-.0101159	.0004278
.0182671	.0119339	-.0022278	.0009037	.0021723	-.0000991
-.0192156	-.0115150	.0022557	-.0008772	-.0021600	.0000943
-.0039375	-.0024995	.0004900	-.0002061	-.0004567	.0000182

OREIT PLNE FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE

-7.7038152E+12	-2.9331922E+13	-3.0946338E+12	-1.2612934E+08	-1.2118719E+08	-1.2869571E+07
7.0200599E+12	2.6802400E+13	2.6861559E+12	1.1953547E+08	1.8970563E+07	1.1696693E+07
1.4244650E+12	5.4397275E+12	5.3697096E+11	2.3170555E+07	2.1596085E+07	2.3862947E+06
-1.4528942E+08	-5.5441033E+08	-5.7692753E+07	-2.3652478E+03	-2.2481974E+03	-2.4034054E+02
3.3283377E+07	1.2717354E+08	1.2047932E+07	4.7293946E+02	4.7016226E+02	6.5628846E+01
5.7537103E+06	2.1953896E+07	2.2966167E+06	9.7430944E+01	9.6399917E+01	7.6318236E+00

CORRELATION

-.4487632	.3890160	.0638657	-.0647188	.0148681	.0025692
-.4455811	.3856208	.0634960	-.0642854	.0147880	.0025518
-.0404007	.0333600	.0053355	-.0057595	.0012062	.0002298
-.0165952	.0149616	.0023464	-.0023797	.0004772	.0000983
-.0158456	.0131482	.0021734	-.0022479	.0004714	.0000966
-.0016823	.0014546	.0002401	-.0002402	.0000658	.0000076

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE

3.1708788E+13	-7.0400897E+12	-6.0675144E+12	1.2982267E+08	-1.3563666E+08	-2.7987139E+07
2.3788748E+13	-5.2857404E+12	-4.6791277E+12	1.0170589E+08	-9.7462013E+07	-2.1384163E+07
-5.4228814E+12	1.2035774E+12	1.0245541E+12	-2.2138113E+07	2.2261783E+07	4.7703346E+06
2.2762463E+08	-5.0522799E+07	-4.3062391E+07	9.0087239E+02	-8.8684388E+02	-2.0551200E+02
5.1910437E+08	-1.1531191E+08	-1.0112139E+08	2.1737473E+03	-2.1466199E+03	-4.5704517E+02
-2.1875191E+07	4.8594540E+06	4.2640500E+06	-9.8857949E+01	9.34555788E+01	1.81313394E+01

CORRELATION

.5108159	.3195785	-.0624791	.0261419	.0593930	-.0025101
-.5215451	-.3255439	.0637589	-.0265830	-.0606723	.0022564
-.0854603	-.0549591	.0103207	-.0043240	-.0101158	.0004278
.0182657	.0119337	-.0022278	.0009037	.0021723	-.0000991
-.0192068	-.0115089	.0022545	-.0008767	-.0021589	.0000943

-0.0039372 -0.0024993 .0004400 -0.0002061 -0.0004567 .0000162

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE
 -7.7003770E+12 -2.9391763E+13 -3.0946592E+12 -1.2606707E+08 -1.2118864E+08 -1.2869568E+07
 7.0169590E+12 2.6802257E+13 2.6861788E+12 1.1947931E+08 1.0570694E+08 1.1696890E+07
 1.4233306E+12 5.4395981E+12 5.3697565E+11 2.3159065E+07 2.1596353E+07 2.3862941E+06
 -1.4522600E+08 -5.5440740E+08 -5.7693221E+07 -2.3640991E+03 -2.2482243E+03 -2.4034048E+02
 3.3269319E+07 1.2717289E+08 1.2048036E+07 4.7268483E+02 4.7015859E+02 6.5628833E+01
 5.7512874E+06 2.1953784E+07 2.2966346E+06 9.7387060E+01 9.6400943E+01 7.6318213E+00

CORRELATION
 -.4481793 .3895119 .0637832 -.0646358 .0148492 .0025659
 -.4455734 .3855153 .0634955 -.0642851 .0147879 .0025518
 -.0404006 .0333600 .0053956 -.0057596 .0012062 .0002298
 -.0165858 .0149544 .0023453 -.0023786 .0004769 .0000982
 -.0151456 .0131483 .0021734 -.0022479 .0004714 .0000966
 -.0015823 .0014546 .0002401 -.0002402 .0000658 .0000076

COVARIANCE MATRICES AT 3.000000000E+01 MINUTES FROM MIDNIGHT OF EPOCH DATE

ATA(INVERSE) FOR P PARAMETERS

0001 X	0001 Y	0001 Z	0001 OX	0001 OY	0001 OZ	0002 X	0002 Y
0002 Z	0002 DX	0002 DY	0002 OZ	0003 X	0003 Y	0003 Z	0003 OX
0003 JY	0003 OZ						
2.74180E+08	2.61362E+08						
-2.37417E+08	2.37305E+08	3.50382E+09	7.26134E+01	1.63858E+01			
-6.54772E+08	3.07262E+04	4.86406E+05	3.14774E+01	1.71392E+03			
-8.69804E+04	3.3531E+04	-4.89425E+05	-3.43168E+02	1.43786E+03			
5.22055E+04	-1.97944E+05	-2.31668E+06	-3.43168E+02	1.71392E+03			
4.64280E+05	1.97944E+05	-2.31668E+06	-3.43168E+02	1.71392E+03			
-1.85173E+07	1.56370E+07	4.16309E+07	1.12133E+04	-7.75487E+03	3.86454E+04	5.06787E+13	
-5.03252E+07	6.64976E+07	-1.32954E+07	-3.29124E+03	-3.18653E+03	-1.07060E+03	-1.43006E+13	4.16315E+12
0002 Z	1.25592E+06	-5.48692E+06	-1.46479E+03	7.28113E+02	4.45781E+03	3.62444E+12	2.34449E+12
9.85472E+13							
0002 OX	3.60854E+01	-3.37343E+02	1.54137E+03	4.13523E-01	-2.07000E-01	-1.28241E+00	4.50141E+00
3.29638E+08	8.72337E+05						-2.20514E+08
0002 OY	3.44405E+03	-2.84389E+03	-8.04082E+03	-2.22292E+00	1.52633E+00	7.52866E+00	3.84385E+09

0003 OY	.000	.000	-.000	-.000	.000	.000	-.040	.019	-.052	.211	-.069	-.040
0003 OZ	.330	-.379	.066	-.320	1.000	1.000						
	-.000	-.000	.000	.000	-.000	-.000	.008	-.004	.011	-.044	.014	.010
	-.070	.079	-.014	.067	.066	1.000						
SOFT DIAG	1.655839E+04	1.617287E+04	1.617287E+04	5.919305E+04	5.919305E+04	5.919305E+04	6.521352E+04	6.521352E+04	4.047937E+00	4.047937E+00	4.139949E+01	4.139949E+01
	7.118896E+06	2.040379E+06	2.040379E+06	9.927094E+06	9.927094E+06	9.927094E+06	9.339897E+12	9.339897E+12	5.468333E+02	5.468333E+02	9.960463E+02	9.960463E+02
	5.499283E+06	7.144043E+06	7.144043E+06	9.670707E+06	9.670707E+06	9.670707E+06	6.691744E+02	6.691744E+02	6.711585E+02	6.711585E+02	9.932010E+02	9.932010E+02
PIVOT RATIOS	1.000000E+00	4.816559E+00	4.816559E+00	2.595729E+02	2.595729E+02	2.595729E+02	1.104760E+01	1.104760E+01	6.856481E+03	6.856481E+03	4.384970E+05	4.384970E+05
	1.084038E+00	1.706543E+03	1.706543E+03	2.332865E+05	2.332865E+05	2.332865E+05	3.553952E+05	3.553952E+05	9.176784E+08	9.176784E+08	8.817966E+08	8.817966E+08
	5.163285E+11	4.367208E+11	4.367208E+11	9.103338E+10	9.103338E+10	9.103338E+10	3.629283E+10	3.629283E+10	2.661656E+10	2.661656E+10	2.029161E+09	2.029161E+09

A PIVOT RATIO EXCEEDS 10**5.
CHECK ATA MATRIX FOR ILL CONDITIONING.

DP3Q MATRIX

	3	2BIA	3	ALT	3	LONG	3	LAT	3	LAT	2	RBIA	2	ALT	2	LONG	2	LAT	
	1	EBIA	1	ABIA	1	RBIA	1	ALT	1	LONG	1	LONG	1	LAT	1	GM	1	LAT	
0001 X	-1.36166E-07	9.82418E-08	-1.07344E-02	2.77248E-02	-7.98281E-08	-5.34169E-08	-1.26714E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02	1.69283E-02
0001 Y	-3.04659E+05	1.12220E+06	7.04946E-01	-3.32361E-01	1.67562E+06	-3.88605E+05	-7.37786E+08	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05	1.19618E+05
0001 Z	2.42393E-07	1.77291E-07	1.86347E-02	-5.04820E-02	2.33144E-07	1.66317E-07	2.80470E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02	-4.42651E-02
0001 7	7.74029E+05	-1.33554E+06	7.17292E-01	-7.00006E-01	1.99861E+06	4.68807E+05	9.83876E+08	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05	-1.59587E+05
0001 0X	1.30531E-07	1.04323E-07	9.37512E-03	-2.42138E-02	7.53989E-08	-3.95194E-08	-3.99831E-03	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02	1.77770E-02
0001 0Y	-2.25138E+06	-5.65948E+05	7.90663E-02	7.00460E-01	-2.17888E-01	1.41389E-11	-7.45217E-12	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06	-1.27020E-06
0001 0Z	-4.95094E+01	7.98241E+01	1.56679E-05	1.76723E-06	1.22609E+02	-1.68258E+01	4.87537E+05	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01	-7.90119E+01
0002 X	-3.35414E-11	-3.04562E-11	-3.03000E-06	7.44403E-05	3.54277E-12	-5.29331E-12	-1.12258E-06	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07	-1.46189E-07
0002 Y	-6.01379E+01	6.02504E+01	-3.46392E-05	3.89463E-05	1.02787E+02	2.23995E+00	-7.78884E+05	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02	1.26362E+02
0002 Z	-2.26479E-10	-1.67423E-10	-1.56488E-05	4.52137E-05	1.58214E-11	-1.82432E-11	-4.33584E-06	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07	-5.18667E-07
0002 7	9.27173E+00	-1.31976E+01	7.74036E-06	-1.16702E-08	1.53275E-02	2.88572E+01	1.78814E+05	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01	-2.93748E+01
0002 X	1.88923E-01	1.39187E-01	1.43891E+04	-4.03207E+04	-2.20610E-01	-1.60751E-01	-2.80761E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04	4.08919E+04
0002 Y	-5.59664E-02	4.16128E-02	-3.95103E+03	1.18111E+04	-4.72274E-01	-3.26487E-01	-5.96598E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04	9.46643E+04
0002 Z	2.59128E+05	-3.68515E+05	4.69449E-01	-3.77849E-01	-5.38424E+05	1.52481E+05	1.63130E+08	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04	-2.51173E+04
0002 7	-5.25513E-02	-3.9329E-02	-3.95516E+03	1.07647E+04	1.87987E-02	1.27759E-02	2.26058E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03	-3.89874E+03
0002 0X	3.12906E+03	-1.57148E+04	1.93967E-03	-3.13514E-03	-2.12576E+04	9.00187E+03	1.37964E+07	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03	-5.05363E+03
0002 0Y	1.68888E-07	3.60508E-07	6.53070E-03	-2.86625E-02	2.57045E-06	2.10727E-06	3.28304E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01	-3.78436E-01
0002 0Z	-7.64613E-01	4.36583E+00	-2.08567E-06	1.80642E-06	5.72372E+00	-2.99631E+00	-2.96219E+03	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00	1.29209E+00
0002 7	1.488873E-05	1.09119E-05	1.11541E+00	-3.17868E+00	-2.71561E-06	-5.92078E-07	-3.27181E-01	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00	1.10693E+00

0003 Z	1.000	.000	.001	-.000	-.042	.048	.019	-.047	-.036	.011
	-.001	1.000	-.001	-.000	-.032	.010	-.053	.214	-.061	-.049
0003 CX	.089	1.000	-.001	.000	-.040	.019	-.052	.211	-.069	-.048
	-.001	-.001	1.000	-.000	.000	-.004	.011	-.044	.014	.010
0003 DY	.310	-.001	-.001	.000	.000	1.000				
	-.001	-.001	-.001	-.000	.000	.067				
0003 DZ	.330	-.001	-.001	-.000	.000	.067				
	-.000	-.000	-.000	1.000						
	-.070	-.079	-.079	-.079						
SQRT DIAG	2.331531E+05	3.093226E+05	4.680919E+05	2.062853E+01	1.750148E+01	4.161849E+01				
	7.115913E+06	2.042353E+06	9.927094E+06	9.339901E+02	5.468413E+02	9.960463E+02				
	5.499440E+06	7.144174E+06	9.870712E+06	8.691755E+02	8.711595E+02	9.932011E+02				

STATE COVARIANCE AND CORRELATION MATRIX PARTITIONS AT 3.000000000E+01 MNOED

CARTESIAN FOR	P	PARAMETERS	VEHICLES	1 AND	1
1.9378948E+08	-1.8779915E+08	-9.2356584E+07	4.2205168E+04	-3.3341856E+03	-1.5358508E+05
	1.9162336E+08	9.1805733E+06	-2.4879282E+04	-5.0279636E+03	6.4513164E+04
1.3920829E+04		7.1258805E+08	-1.5345976E+05	7.0338859E+04	7.7506512E+05
	1.3842809E+04		7.2405166E+01	-3.1832935E+01	-3.4423029E+02
	.0245443	2.6694345E+04		1.6839958E+01	1.4584082E+02
	-.2112170	-.6756013	8.5091275E+00	4.1036518E+00	1.7256827E+03
	.3562999	-.0855110	-.9116359	.8555160	
	-.0583652	.1121873	-.9738315		4.1541338E+01
	-.2655849				

OPRIT PLNE FOR	P	PARAMETERS	VEHICLES	1 AND	1
7.5416975F+06	1.8191153E+07	6.8709125E+07	5.9283546E+03	-2.2023952E+03	7.5866952E+04
	3.65225704E+08	-1.2824916E+07	-2.4087103E+04	2.3470338E+03	-1.9970407E+04
2.7462151F+03		7.2519215E+08	7.5337461E+03	-2.4320681E+04	8.0396694E+05
	1.9111961E+04		1.7323869E+01	-4.0186420E+00	1.6865922E+02
	3465935	2.6929392E+04		7.9231670E+00	-4.9077642E+01
	.290804	-.0249185	4.1621952E+00	2.8148121E+00	1.7896838E+03
	.5146533	-.3024007	.6721435		
	-.2843125	.0435279	-.3208483		
	.6530257	-.02465998	.7057051		4.2304619E+01

CARTESIAN FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1
6.9493670F+10	-7.1830395E+10	4.2433311E+09	4.2629431E+06	4.4721147E+06	-1.3030894E+06
	7.7301799E+10	-2.9825505E+10	-4.6071619E+06	-5.0536823E+06	1.4814488E+06
2.5361632F+05		2.1202344E+11	1.9324431E+06	3.8624062E+06	-1.1995292E+06

-0.9800333 2.7803201E+05 3.4519835E+02 2.7106465E+02 -4.3066653E+02
 .0349575 -0.2329706 3.6431550E+02 3.6431550E+02 3.9940895E+01
 .8703673 .8919757 1.8579514E+01 1.9087051E+01 1.7619041E+03
 .8887948 -.9523012 .7643631 .0498526 4.1975041E+01
 -.1177634 .1259406 -.5522244

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 1 AND 1
 2.6202313E+09 1.432274E+10 2.1031839E+10 -7.5854122E+05 -1.6429767E+05 -1.5345161E+05
 1.5434906E+11 3.3389114E+10 -9.8017970E+06 -6.6493119E+05 -1.8663139E+06
 5.1189135E+04 2.0124362E+11 -2.44816375E+06 -1.3476150E+05 -5.6679600E+05
 .5673725 3.9353569E+05 4.4860854E+05 4.0897672E+01 2.8767719E+02
 .0159828 .1837788 .0371734 9.9889791E+06 1.4363980E+04
 -.5872281 -.9857535 -.2192140 9.2414762E+02 9.0564079E+05
 -.7565154 -.3991950 -.7081282 -.1617016 5.1123642E+02
 -.0703347 -.1112393 -.0296434 .0322353 .0283005 9.9279444E+02

CARTESIAN FOR P PARAMETERS VEHICLES 2 AND 2
 5.4232313E+13 -8.0642703E+12 3.0686477E+12 1.5211476E+09 3.4773012E+09 -1.4371358E+08
 7.3642592E+06 1.2937805E+12 2.4813391E+12 -2.1902841E+08 -5.2168989E+08 4.5161370E+07
 -.9625553 1.1375362E+06 9.9779704E+13 3.4338042E+08 7.601017E+08 7.6011698E+08
 .0539501 .2137734 9.9889791E+06 9.2414762E+02 9.0564079E+05 1.4363980E+04
 .2235120 -.2093502 .0371734 9.2414762E+02 9.0564079E+05 1.4363980E+04
 .9235150 -.8970681 .0205239 -.1617016 5.1123642E+02 9.9279444E+02
 -.0196556 .0399892 .0766479 .0322353 .0283005 9.9279444E+02

ORBIT PLNE FOR P PARAMETERS VEHICLES 2 AND 2
 3.6829691E+12 1.3463305E+13 3.9702101E+12 -8.2344615E+08 4.5444216E+08 7.1922790E+07
 5.1631479E+13 -6.9103222E+11 -3.2118127E+09 1.8109750E+09 1.5259108E+08
 1.9191053E+06 7.18355048E+06 9.9991358E+13 3.8165380E+08 -4.5264635E+08 7.7204580E+08
 .9763272 -.0095174 9.9991358E+13 2.8421270E+05 1.3576694E+09 2.2111891E+04
 .2068868 -.8394383 .0715926 5.3311611E+02 8.2789488E+05 -2.2259905E+04
 -.8049489 .2759922 -.0497496 .2798882 9.0988729E+02 9.8894463E+05
 .2602507 .0213543 .0776382 .0417079 -.0246008 9.9445695E+02
 .0375851

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 2 AND 2
 5.4232538E+13 -8.0635165E+12 3.9686515E+12 1.5211418E+09 3.4772715E+09 -1.4371197E+08
 1.3017608E+12 2.4816414E+12 -2.1911644E+08 -5.2169022E+08 4.5164722E+07

7.3642744E+06
 -.9595855
 .0539502
 .2235106
 .9235950
 -.0196564

9.9779717E+13
 3.437671E+08
 0.5404907E+05
 9.2414019E+02
 -.1617088
 .0322329

1.1409473E+06
 .2177471
 -.2079106
 -.8943767
 .0399902

1.8481321E+08
 -7.6397725E+04
 2.6136848E+05
 5.1124218E+02
 .8283004

7.6011794E+08
 2.9573381E+04
 1.4364187E+04
 9.8564067E+05
 9.9279447E+02

ORBIT PLANE FOR

P AND Q PARAMETERS

VEHICLES 2 AND 3

VEHICLES 2 AND 3

CAPTESIAN FOR

P PARAMETERS

VEHICLES 3 AND 3

VEHICLES 3 AND 3

ORBIT PLANE FOR

P AND Q PARAMETERS

VEHICLES 3 AND 3

VEHICLES 3 AND 3

CAPTESIAN FOR

P PARAMETERS

VEHICLES 3 AND 3

VEHICLES 3 AND 3

6.1031314E+06
 -.5733652
 .0805773
 .4683543
 .1655679
 -.0533156
 4.6289908E+13
 9.8460456E+13
 9.9227242E+06
 .0876953
 .4423394
 -.0494922
 .0807653
 9.0946735E+08
 6.9611223E+05
 8.3433341E+02
 -.4158968
 .0691841
 -2.5137905E+09
 7.0946735E+08
 6.9611223E+05
 8.3433341E+02
 -.4158968
 .0691841
 -2.8093463E+08
 9.2208069E+08
 -2.9547162E+05
 7.2507207E+05
 8.5151164E+02
 .0690750
 5.4425434E+08
 7.0328222E+08
 5.7170863E+04
 5.6255964E+04
 9.8097338E+05
 9.9044100E+02

OPRIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 3

4.0406056E+13
 6.3565756E+06
 .5795723
 .2235658
 -.0858605
 .3891022
 .0795186
 2.4193298E+13
 4.3132055E+13
 9.8460456E+13
 6.5674998E+06
 -.0554076
 -.2273492
 .4422301
 .0595193
 1.4101377E+13
 -3.6759404E+12
 9.8460456E+13
 9.9227242E+06
 .1248799
 -.0680947
 .0715500
 -4.4113075E+08
 -1.2068248E+09
 1.0015534E+09
 6.5328301E+05
 8.0825925E+02
 .4097575
 .0809194
 2.1674032E+09
 2.5450780E+09
 -5.9201545E+08
 2.9022200E+05
 7.6790130E+05
 8.7629978E+02
 -.0572156
 5.0963408E+08
 3.8910804E+08
 7.0328222E+08
 6.4778664E+04
 -4.9658733E+04
 9.8097338E+05
 9.9044100E+02

CAPTESIAN FOR P PARAMETERS VEHICLES 2 AND 1

3.1232090E+06
 -5.7815657E+07
 -3.1591471E+06
 8.1295620E+02
 -1.6500722E+03
 -2.1045612E+02
 2.9443001E+05
 5.9950272E+07
 2.9093819E+06
 -7.7942765E+02
 1.0481929E+03
 2.0354249E+02
 -2.9135322E+07
 -5.3566248E+06
 2.7709021E+06
 -4.5706182E+02
 5.3717277E+03
 1.0370547E+02
 -6.9105460E+03
 -1.5894972E+03
 3.0540392E-01
 -2.3378132E+00
 -7.3030366E-02
 -8.1240811E+03
 -1.5820805E+03
 7.7654782E+02
 -1.2608278E-01
 1.4914903E+00
 2.8508172E-02
 -4.0640668E+04
 1.2684075E+04
 4.8614804E+03
 -8.9877067E-01
 7.6940044E+00
 2.1078724E-01
 -.00000152
 .0000148
 .0000039
 -.0000086
 .0000070
 .8000051

CORRELATION

.0000305
 .0000029
 -.0001482
 .0001901
 -.0002688
 -.0001328
 -.0000227
 .0000210
 .0000104
 -.0000187
 .0000169
 .0000118
 .0000632
 -.0000609
 -.0000165
 .0000388
 -.0000332
 -.0000234
 -.0002319
 .0001481
 .0003936
 -.0005374
 .0007109
 .0003623

OPRIT PLNE FOR P PARAMETERS VEHICLES 2 AND 1

-3.2101955E+06
 -9.2249597E+07
 1.2148586E+07
 6.4650181E+03
 -2.4010691E+03
 -2.4010691E+03
 1.7431795E+04

3.2847022E+06 1.1240000E+07 2.8084919E+07 2.5264449E+03 -6.8370400E+03 4.1128104E+04
 -3.5453554E+04 -2.1195159E+06 8.0711496E+05 2.2524983E+02 -1.8921858E+02 1.2019700E+03
 4.8391383E+02 -1.0633869E+03 5.6521594E+03 6.9654083E-01 -1.3624322E+00 8.0928454E+00
 -4.3420216E+01 -9.4332402E+02 7.0660722E+01 6.7854998E-02 -1.0115450E-02 1.143717E-01
 -1.1312092E+01 -1.6093321E+02 -2.8776739E+01 6.7724037E-03 8.0499974E-03 -4.1385660E-02

CORRELATION

-.0005031 .0001665 -.0000013 .0003305 -.0000174 -.0000041
 -.0022425 .0000810 -.0000111 -.0001050 -.0000543 -.0000065
 .0002351 .0001451 .0000030 .0003937 .0000029 -.0000011
 .0004094 .0007845 .0000054 .0003139 .0000179 .0000016
 -.0004445 -.0003380 -.0000067 -.0009079 -.0000039 .0000029
 .0002147 .0001353 .0000020 .0003588 .0000030 -.0000010

CAPTESIAN FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE
 -1.3072635E+09 2.1359723E+09 -6.6122571E+09 -1.2402219E+05 -2.0094045E+05 3.9707840E+04
 -2.2436245E+10 2.4454244E+10 -1.2137929E+10 -1.4625283E+06 -1.6254091E+06 4.8064544E+05
 -9.6219838E+08 9.7711148E+08 8.6831540E+07 -5.8759995E+04 -5.8768303E+04 1.9498230E+04
 2.699397E+05 -2.8156152E+05 3.853176E+04 1.6887681E+01 1.7622769E+01 -5.5622534E+00
 -1.6868081E+05 4.5522667E+04 1.0621093E+06 -3.2982160E+00 8.4643878E+00 8.4311686E-01
 -7.1151417E+04 7.4590888E+04 -1.3059782E+04 -4.4690406E+00 -4.6981252E+00 1.46661769E+00

CORRELATION

-.0006734 -.0745954 -.0003554 .0011080 -.0012516 -.0002719
 .0010432 .0771838 .0003518 -.0010962 .0003203 .0002702
 -.0019500 -.0231040 .0000188 .0000905 .0045118 .0000286
 .0009054 -.0689929 -.0003166 .0009835 -.0003472 -.0002423
 -.0014295 -.0745377 -.0003082 .0009991 .0006674 -.0002479
 .0001285 .0100362 .0000465 -.0001434 .0000393 .0000352

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE
 -2.3483103E+09 -3.4215789E+10 -5.5318956E+09 2.1612656E+06 1.3376933E+05 4.1591467E+04
 1.0115864E+09 6.9751266E+09 6.6956334E+09 -4.4987975E+05 -6.8392068E+04 -6.8018209E+04
 -4.9714549E+07 -8.4327316E+08 -5.1045140E+07 5.3131244E+04 2.5493703E+03 1.0595635E+04
 1.0160626E+05 -1.1027380E+04 1.0679347E+06 -1.1199628E+00 -7.8125594E+00 2.8602480E+00
 -2.8950820E+04 -3.9893282E+05 -8.0973104E+04 2.5223731E+01 1.6773461E+00 4.8419719E+00
 -5.8540882E+03 -7.1116741E+04 -2.1668442E+04 4.5093350E+00 3.5281451E-01 8.3781869E-01

CORRELATION
 -.0238004 .0027502 -.0009971 .0037233 -.0006216 -.0001150
 -.0452468 -.0002142 -.0002142 -.0000525 -.0011135 -.0001817
 -.0064189 .0029771 -.0000114 .0044656 -.0001984 -.0000486
 .0445822 -.0024810 .0002106 -.0000832 .0010985 .0001797
 .0164144 -.0022437 .0000525 -.0034542 .0004346 .0000836
 .0050796 -.0002221 .0002249 .0001259 .0001249 .0000198

CARTESIAN FOR P PARAMETERS VEHICLES 3 AND 1
 COVARIANCE
 -1.8155415E+07 2.2433560E+07 -3.1441192E+07 9.4384103F+03 -8.7797011E+03 -3.6094135E+04
 -3.1930248E+07 3.2459390E+07 2.5006973E+06 -5.8862105E+03 6.2647240E+02 1.4014430E+04
 7.2395136E+06 -7.3257214E+06 -8.6192345E+05 1.4623386E+03 -2.2015746E+02 -3.7037926E+03
 -1.2687544E+03 1.0737745E+03 1.8883965E+03 -9.3376403E-01 5.2499057E-01 2.9673554E+00
 -1.8737562E+03 1.7455359E+03 1.4683915E+03 -8.5921878F-01 4.0581661E-01 2.5799959E+00
 2.2010438E+02 -1.8034485E+02 -3.7750439E+02 1.8071642E-01 -1.0520995E-01 -5.7435009E-01

CORRELATION
 -.0002137 .000524 .0001092 -.0001581 .0000160
 .0002653 .000448 .0000931 .0001482 -.0000132
 -.0001930 .000138 .0000846 .0000646 -.0000143
 .0001817 -.0001017 -.0001315 -.0001186 .0000214
 -.0003506 .0000224 .0001533 .0001161 -.0000259
 -.0001424 .0001496 .0000856 .0000729 -.0000140

ORBIT PLNE FOR P PARAMETERS VEHICLES 3 AND 1
 COVARIANCE
 -1.8796040E+06 -4.8154533E+07 7.1111915E+07 3.7491541E+03 -1.4007103E+03 9.8390697E+03
 4.0708517E+06 2.7940878E+07 2.7021943E+07 1.3369839E+03 -6.6890432E+03 3.9255811E+04
 2.7938005E+05 3.9912467E+06 -2.6314535E+06 -9.2257022E+02 5.5496434E+02 -3.6400340E+03
 7.5987195E+01 -2.4214402E+03 2.1344342E+03 3.8671669E-01 -5.0272685E-01 3.0474027E+00
 -1.2724545E+02 1.0234537E+03 -1.8987911E+03 -2.7790057E-01 4.5328522E-01 -2.7459871E+00
 -2.8814194E+01 2.1453347E+02 -4.2035352E+02 -5.9881533E-02 1.0134343E-01 -5.9979105E-01

CORRELATION
 -.0001077 .0002257 .0000103 .0000342 -.0000529 -.0000106
 -.0003964 .0002226 .0000527 -.0001562 .0000611 .0000113
 .0000415 .0001528 -.0000098 .0000981 -.0000005 -.0000158

.0001417
 -.0000767
 .0000366
 .0000409
 -.0003618
 .0001413
 -.0000223
 .0000199
 -.0000091
 .0001150
 -.0002210
 .0000091
 -.0000762
 .0001930
 -.0000741
 -.00000149
 .0000364
 -.00000143

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -9.5886520E+09
 -1.1928532E+10
 1.2872958E+10
 -2.6795368E+09
 -3.2072065E+05
 -5.8692160E+05
 5.1360163E+04
 1.1192143E+10
 1.2872958E+10
 -2.0852031E+09
 3.0054090E+05
 5.9899544E+05
 -4.6009381E+04
 -1.1247665E+10
 -5.2911087E+09
 1.1505800E+09
 2.3016841E+05
 2.7939600E+04
 -5.5700999E+04
 -6.6512593E+05
 -7.6930121E+05
 1.7271647E+05
 -1.0177074E+01
 -3.5947322E+01
 2.7895226E+00
 -0.355705E+05
 -0.4270991E+05
 1.8873897E+05
 -1.5040705E+01
 -3.6327432E+01
 2.2222067E+00
 2.1638300E+05
 2.5200294E+05
 -5.6904837E+04
 5.9550021E+00
 1.1715750E+01
 -0.9420201E-01

CORRELATION

-.0059599
 .0065958
 -.0040024
 -.0058657
 -.0068980
 .0009525
 .0010244
 -.0010469
 .0012956
 .0006199
 -.0011727
 -.0009547
 .0001701
 -.0026147
 .0025301
 .0000713
 -.0022722
 -.0022351
 .0003270
 .0001967
 -.0001671
 -.0001223
 .0001516
 .0001175
 -.0000215

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE
 -1.3652682E+09
 1.5311329E+09
 2.5948243E+08
 -2.5822972E+04
 -1.2095153E+04
 -3.2930006E+03
 -2.0015227E+10
 1.4049993E+10
 4.0713392E+09
 -8.6223096E+05
 2.8987493E+05
 5.8256275E+04
 -3.1479570E+09
 8.1955842E+09
 4.4981908E+08
 2.0917799E+05
 -2.8701045E+05
 -6.6786493E+04
 1.2660391E+06
 -8.9739305E+05
 -2.5683337E+09
 5.3069577E+01
 1.7699408E+01
 -3.5504179E+00
 7.7789851E+04
 -9.8561522E+04
 -1.4303279E+04
 8.1263956E-01
 1.3286231E+00
 3.3208109E-01
 2.4249670E+05
 -1.5405704E+05
 -5.0211404E+04
 1.1342264E+01
 -4.4402149E+00
 -0.9645641E-01

CORRELATION

-.0041959
 -.0079991
 -.0011039
 .0078802
 .0026818
 .0008951
 .0045545
 .0054340
 .0027817
 .0054148
 -.0035377
 -.0005504
 .0005109
 .0010423
 .0001011
 -.0010257
 -.0003417
 -.0001187
 -.0006241
 -.0027101
 .0005769
 .0026411
 .0002370
 .0003292
 -.0002696
 .0008380
 -.0007301
 .0003004
 .0002374
 .0000790
 -.0000212

CARTESIAN FOR P	PARAMETERS	VEHICLES	3 AND 2
COVARIANCE			
2.2099148E+13	-3.4395954E+12	-6.2197762E+08	1.74413755E+09
1.6565361E+13	-2.8084893E+12	2.0249311E+09	7.2744922E+08
-3.7197699E+12	6.3182045E+11	2.2769325E+12	-4.7166258E+08
1.4905768E+07	-1.9471392E+07	-5.5782561E+08	1.9200818E+05
4.7325437E+08	-9.3138514E+07	-7.0281540E+08	2.0080918E+05
1.8933087E+07	2.9428271E+05	1.0211158E+08	-3.6748088E+04
CORRELATION			
.4917049	.3306273	-.0509045	.0024261
-.4954505	-.3628895	.0559755	-.0205160
-.0550267	-.4457183	.0229720	-.0669327
-.1157393	.3220593	-.0514352	.2490229
.5581215	.2091451	-.0314587	-.0959812
.0297320	-.0648027	.0104770	-.0501327
CORRELATION			
.0754704	.0754704	.0754704	.0754704
.0025958	.0025958	.0025958	.0025958
.0103211	.0103211	.0103211	.0103211
-.0401481	-.0401481	-.0401481	-.0401481
.0185117	.0185117	.0185117	.0185117
.0080773	.0080773	.0080773	.0080773

ORBIT PLANE FOR P	PARAMETERS	VEHICLES	3 AND 2
COVARIANCE			
-5.4445418E+12	-1.9471883E+13	6.5829534E+12	7.2253027E+08
5.1369829E+12	1.960803E+13	3.6226599E+11	-1.7454422E+09
1.0755021E+12	3.6074465E+12	1.9408642E+12	-1.0774311E+08
-1.6579252E+08	-5.1997125E+08	-7.2071049E+08	-3.9331202E+04
1.8166733E+07	-5.1115869E+06	4.6981564E+08	5.7072649E+04
1.5489345E+06	-1.0483846E+07	1.0331038E+08	1.3286683E+04
CORRELATION			
-.4463267	.4075830	.0564783	-.1068851
-.4263255	.4153590	.0534006	-.0895310
-.1350350	.0055164	.0195506	-.0891724
.2132185	-.4985293	-.0203675	-.0912781
-.3498633	-.1509871	.0545459	-.3033287
-.0429119	-.0150404	.0067506	-.0360067
CORRELATION			
.0108025	.0108025	.0108025	.0108025
-.0014731	-.0014731	-.0014731	-.0014731
.8184312	.8184312	.8184312	.8184312
.0251636	.0251636	.0251636	.0251636
.0488641	.0488641	.0488641	.0488641
.0846775	.0846775	.0846775	.0846775

CARTESIAN FOR P AND Q	PARAMETERS	VEHICLES	3 AND 2
COVARIANCE			
2.2099656E+13	-3.4359649E+12	-6.2201590E+08	1.74413449E+09
1.6565725E+13	-2.8044183E+12	2.0248845E+09	7.2745509E+08

-3.719500E+12	6.3090745E+11	2.2768961E+12	-4.7165319E+08	-1.5958678E+08	1.0320893E+08
1.4904914E+07	-1.9331267E+07	-5.5782101E+08	1.9200696E+05	-4.8937866E+04	-4.1525639E+04
4.7326349E+08	-9.295797E+07	-7.0280726E+08	2.0080692E+05	-1.0477024E+04	-4.3488413E+04
1.8933926E+07	2.8074875E+05	1.0211094E+08	-3.6747896E+04	9.3729922E+03	7.9424010E+03
CORRELATION					
.4917030	.3305263	-.0509055	.0024258	.0754714	.0025959
-.4934355	-.3612718	.0557274	-.0203600	-.0956767	.0002484
-.0550233	-.1467125	.0229716	-.0669320	-.0826275	.0103210
-.1457424	.3220442	-.0514340	.2490209	.2551799	-.0401478
.5580916	.2031397	-.0314586	-.0959752	-.0240669	.0185107
.0297330	-.0647994	.0104768	-.0501323	-.0514427	.0008773

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE					
-5.4401219E+12	-1.9472752E+13	-8.5828540E+12	7.2253798E+08	-2.0234121E+09	-2.7124325E+08
5.1339354E+12	1.9601572E+13	3.6219315E+11	-1.7454148E+09	-9.0227242E+08	-1.0476644E+08
1.0745013E+12	3.8076181E+12	1.9408418E+12	-1.0774571E+08	4.9246061E+08	6.6709613E+07
-1.6559894E+08	-5.1990950E+08	-7.2070555E+08	-3.9328983E+04	-2.2307227E+05	-2.8940939E+04
1.8099837E+07	-5.1079851E+06	4.6981484E+08	5.7070717E+04	1.6355833E+05	2.0914303E+04
1.5353686E+06	-1.0481338E+07	1.0331001E+08	1.3286445E+04	3.6105230E+04	4.6070975E+03
CORRELATION					
-.4454935	.4059175	.0563732	-.1066505	.0107517	.0008869
-.4263290	.4133667	.0534027	-.0895350	-.0008112	-.0014730
-.1350289	.0055152	.0195604	-.0891714	.0536157	.0104311
.2132117	-.4985082	-.0203677	-.0912716	.1221615	.0251625
-.3498430	-.1503905	.0545447	-.3033242	.2051314	.0400639
-.0425091	-.0150412	.0067304	-.0360061	.0239996	.0046775

** A BINARY PLOT FILE HAS BEEN GENERATED ON TAPE 12
WITH THE FOLLOWING COMMENTS AND RECORD FORMAT **

WORD	PARAMETER	IN VALUE	MAX VALUE
1	TIME(MIN)	0.	3.00000E+01
** ATA INVERSE WITH P-PARAMETER EFFECTS **			
2	0001 X	1.65584E+04	1.00000E+07
3	0001 Y	1.61729E+04	1.00000E+07
4	0001 Z	5.91930E+04	1.00000E+07
5	0001 DX	8.52135E+00	1.00000E+03
6	0001 DY	4.04794E+00	1.00000E+03
7	0001 DZ	4.13995E+01	1.00000E+03
8	0002 X	7.11930E+06	1.00000E+07
9	0002 Y	2.04038E+06	1.00000E+07
10	0002 Z	3.92709E+06	1.00000E+07
11	0002 DX	3.33930E+02	1.00000E+03
12	0002 DY	5.46933E+02	1.00000E+03
13	0002 DZ	3.96746E+02	1.00000E+03
14	0003 X	5.49928E+06	1.00000E+07
15	0003 Y	7.14904E+06	1.00000E+07
16	0003 Z	3.87071E+06	1.00000E+07
17	0003 DX	8.69174E+02	1.00000E+03
18	0003 DY	8.71158E+02	1.00000E+03
19	0003 DZ	3.93201E+02	1.00000E+03
* C(X) P - PARAMETER EFFECTS *			
20	1 X	1.39208E+04	1.00000E+07
21	1 Y	1.38428E+04	1.00000E+07
22	1 Z	2.65943E+04	1.00000E+07
23	1 DX	3.50912E+00	1.00000E+03
24	1 DY	4.10355E+00	1.00000E+03
25	1 DZ	4.15413E+01	1.00000E+03
* C(CP) P - PARAMETER EFFECTS *			
26	1 P	2.74522E+03	1.00000E+07
27	1 T	1.91120E+04	1.00000E+07
28	1 C	2.69244E+04	1.00000E+07
29	1 DP	4.16220E+00	1.00000E+03
30	1 DT	2.81491E+00	1.00000E+03
31	1 DC	4.23047E+01	1.00000E+03

* C(X)	P	-	PARAMETER EFFECTS *		
32	2		X	7.36426E+06	1.00000E+07
33	2		Y	1.13754E+06	1.00000E+07
34	2		Z	9.97730E+06	1.00000E+07
35	2		DX	9.24148E+02	1.00000E+03
36	2		DY	5.11236E+02	1.00000E+03
37	2		DZ	9.92754E+02	1.00000E+03
* C(OP)	P	-	PARAMETER EFFECTS *		
38	2		R	1.91911E+06	1.00000E+07
39	2		T	7.18550E+06	1.00000E+07
40	2		C	9.99958E+06	1.00030E+07
41	2		DR	5.33116E+02	1.00000E+03
42	2		DT	9.09897E+02	1.00000E+03
43	2		DC	7.94457E+02	1.00000E+03
* C(X)	P	-	PARAMETER EFFECTS *		
44	3		X	5.10298E+06	1.00000E+07
45	3		Y	5.80351E+06	1.00000E+07
46	3		Z	9.92272E+06	1.00000E+07
47	3		DX	8.34332E+02	1.00000E+03
48	3		DY	8.51509E+02	1.00185E+03
49	3		DZ	9.90441E+02	1.00000E+03
* C(OP)	P	-	PARAMETER EFFECTS *		
50	3		R	6.35637E+06	1.00000E+07
51	3		T	6.56739E+06	1.00000E+07
52	3		C	9.92272E+06	1.00000E+07
53	3		DR	8.08256E+02	1.00140E+03
54	3		DT	9.76299E+02	1.00000E+03
55	3		DC	9.90441E+02	1.00000E+03
**	ATA	INVERSE WITH P+Q	PARAMETER EFFECTS **		
56	0001		X	2.33153E+05	1.00000E+07
57	0001		Y	1.09323E+05	1.00000E+07
58	0001		Z	4.68092E+05	1.00000E+07
59	0001		DX	2.06295E+01	1.00000E+03
60	0001		DY	1.75015E+01	1.00000E+03
61	0001		DZ	4.16195E+01	1.00000E+03
62	0002		X	7.11991E+06	1.00000E+07
63	0002		Y	2.04235E+06	1.00000E+07
64	0002		Z	9.92709E+06	1.00000E+07
65	0002		DX	9.33390E+02	1.00000E+03

(2)

CONT'D

66 0002	0Y	5.46844E+02	1.00000E+03
67 0002	0Z	3.96046E+02	1.00000E+03
68 0003	X	5.49344E+06	1.00000E+07
69 0003	Y	7.14417E+06	1.00000E+07
70 0003	Z	3.97071E+06	1.00000E+07
71 0003	0X	9.59175E+02	1.00000E+03
72 0003	0Y	3.71160E+02	1.00000E+03
73 0003	0Z	3.93201E+02	1.00000E+03
* C(X) P+C PARAMETER EFFECTS *			
74 1	X	3.43490E+05	1.00000E+07
75 1	Y	2.79032E+05	1.00000E+07
76 1	Z	4.60450E+05	1.00000E+07
77 1	0X	1.85735E+01	1.00000E+03
78 1	0Y	1.90871E+01	1.00000E+03
79 1	0Z	3.19750E+01	1.00000E+03
* C(OP) P+C PARAMETER EFFECTS *			
80 1	P	5.1192E+04	1.00000E+07
81 1	T	3.93536E+05	1.00000E+07
82 1	C	4.46509E+05	1.00000E+07
83 1	0P	2.52350E+01	1.00000E+03
84 1	0T	4.24215E+00	1.00000E+03
85 1	0C	3.26218E+01	1.00000E+03
* C(X) P+C PARAMETER EFFECTS *			
86 2	X	7.36477E+06	1.00000E+07
87 2	Y	1.14075E+06	1.00000E+07
88 2	Z	9.97790E+06	1.00000E+07
89 2	0X	9.24148E+02	1.00000E+03
90 2	0Y	5.11242E+02	1.00000E+03
91 2	0Z	3.92734E+02	1.00000E+03
* C(OP) P+C PARAMETER EFFECTS *			
92 2	P	1.22107E+06	1.00000E+07
93 2	T	7.18554E+06	1.00000E+07
94 2	C	3.99358E+06	1.00000E+07
95 2	0P	5.33122E+02	1.00000E+03
96 2	0T	3.09948E+02	1.00000E+03
97 2	0C	3.94457E+02	1.00000E+03

* C(X)	P+C	PARAMETER	EFFECTS *
08	3	X	5.10313E+06
09	3	Y	6.80367E+06
100	3	Z	3.92272E+06
101	3	DX	3.34333E+02
102	3	DY	3.51512E+02
103	3	DZ	3.90441E+02
23			
* C(OPI)	P+C	PARAMETER	EFFECTS *
104	3	P	6.35558E+06
105	3	T	6.56750E+06
106	3	C	3.92272E+06
107	3	DP	3.08259E+02
108	3	DT	3.76370E+02
109	3	DC	3.90441E+02

REFERENCE SECTION
2.5.1
[ØPBØX(F)]

DESCRIPTION

ITEM

23 The record formats of TAPE12, containing the square roots of the diagonal elements of the matrices indicated. The minimum and maximum values on the tape for the computations are also printed


```

MODEL DATA
DTYIN 3
INFORM1
INTERM0
IPLANT1
22 .6944444444E-3
PLANT 2 0 16.28810076
17 1.
26 1.
25 1.
PLANT 16 1.00002516
IICENM1 ILNORM1
SGM .6802328701E-4 AM .27249217
INTL 1
M LUNAR MODEL
MYERMS04,60
D 02,00
H0 2
FND

```

```

21 1
24 .6944444444E-3
18 .6944444444E-3
TAPE7-1

```

```

HMAX 2

```

```

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9
CARD 10
CARD 11
CARD 12
CARD 13
CARD 14
CARD 15
CARD 16

```

***** LUNAR GRAVITY MODEL *****

SM = 6.802328701E-05 ER**3/MIN**2 = 1.731400L009E+14 FT**3/SEC**2 = 4.9027792902E+12 M**3/SEC**2
 NO NORMALIZATION WITH 1 TERMS.

```

N M 0 0.
2 0 0.
CNM ** N M CNM SNM
** **

```

***** EARTH GRAVITY MODEL *****

SM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2
 SPHERICAL EARTH

***** PHYSICAL CONSTANTS *****

```

SM(ER**3/MIN**2) = 5.530393500E-03 OMEGE(RAD/MIN) = 4.375269100E-03 GMLAT(DEG) = 7.830000000E+01
CMKM(KM**3/MIN**2) = 0. OMEGA(RAD/MIN) = 4.375269100E-03 GMLNG(DEG) = 2.910000000E+02
SGM(FR**3/MIN**2) = 6.802328701E-05 OMEGL(RAD/MIN) = 0. AM(ER) = 2.724921700E-01
ERFT(FT/ER) = 2.092573900E+07 ERKM(KM/ER) = 6.378164900E+03 ERNM(M/ER) = 3.443933600E+03
ETKM(FT/KM) = 3.280839900E+03 FTNM(FT/NM) = 6.076115500E+03 AE(ER) = 1.800000000E+00
SUBD(FT/SEC**2) = 3.217400000E+01 DGREE(DEG) = 5.729577951E+01 SLT = 2.820176300E+03

```

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input MODEL data. Emphasis is on the variables associated with a run in the lunar integration mode:</p> <p>PLANT ICENM LNϕRM, NTL SGM, AM</p>	<p>2.1.1.3 2.1.1.2.2 2.1.1.1</p>

CKEP = 1.0000000E-07 F = 3.3523298869E-03 PI = 3.141592654E+00

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = 2.09257380E+07 VF(I/O-ER/MIN) = 3.48762300E+05 AF(I/O-ER/MIN**2) = 5.81270500E+03

***** INTEGRATION INPUTS *****

IFORM = 1 ISENT = 1 NSTEP = 2
NPCMP = 0 IR = 8 ER = 1.00000000E-10
HMIN = 2.00000000E+00 HYAX = 2.00000000E+00 HO = 2.00000000E+00

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = -1 TELEM = 0 PTAPE = 0 NPDOT = 0
PRHO = 0 NOOPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.000000000E+03

ENTER SEGMENT 01 AT 121.7 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 121.7 CP SECS., 430.1 PP SECS.

***** VEHICLE DATA *****

IVEHID1	2	IMNTH	4	IDAY	16	CARD	1
IYEAR	1967	HR	0	MIN	2.4688333333E3	CARD	2
TZNE	0	IC	1.10617555345	2	-4.8269172572	CARD	3
SEC	0	4	-1.885658509E-3	5	1.010441446E-2	CARD	4
IICTYP	-11	2	2.8428333333E3	3	0	CARD	5
3	-3.3136952336	5	2876.	7	3876.	CARD	6
6	7.05817720489E-3	7	400.	7	400.	CARD	7
PHASE1		2		3		CARD	8
PTIM	1	5				CARD	9
4	720.	7				CARD	10
6	30.	7				CARD	11
6	30.	7				CARD	12
6	30.	7				CARD	13
DPRCDEX						CARD	14
DPRCDE	X					CARD	15
END						CARD	16

ITEM	DESCRIPTION	REFERENCE SECTION
2	Card images of the input <u>VEHICLE</u> data. The variables associated with a lunar integration run are emphasized:	11.1.4 11.1.6
	ICTYP PHASE	

```

***** HYPERBOLIC ORBIT. F AND G ELEMENT SET IS UNAVAILABLE AT PRESENT. *****
EPOCH
YR/MO/DAY      X,Y,Z,C,G,JY,OZ      A,O,B,A,R,V      A,E,I,O,U,TAU      AF,AG,N,L,CHI,PSI
1967/ 4/10     2.31475398135E+07    2.82907487377E+02  -1.07315621590E+07  0.
1.01005805972E+08  -1.93415182702E+07  -3.37887309789E+01  1.09681141984E+00  0.
0.              -6.93415182702E+07  1.77947341526E+02  3.87507025093E+31  0.
2.46688333330E+03  -6.57645633490E+02  6.97802462480E+01  3.34391443389E+02  0.
0.              3.52403882722E+03  1.24685322263E+08  9.09284281807E+01  0.
0.              2.46162611579E+03  4.34867242779E+03  2.88904557605E+03  0.
    
```

THE FOLLOWING BODIES ARE USED FOR PLANETARY PERTURBATIONS
MOON

** NO ATMOSPHERE MODEL **

***** PLANETARY TAPE CONSTANTS *****

BODY	MASS(EM)	DIST. SCALE FACTOR(ER)	VEL. SCALE FACTOR(ER/MIN)
SUN	3.32951300E+05	2.34548550E+04	1.62881008E+01
MOON	1.22999000E-02	1.00002516E+00	6.9444444E-04
VENUS	8.14979000E-01	1.00000000E+00	1.00000000E+00
MARS	1.07821000E-01	6.9444444E-04	1.00000000E+00
JUPITER	3.17887000E+02	2.34548550E+04	0.
SATURN	9.51290000E+01	2.74548550E+04	0.

3

*** PLUS ***

NUTATION(RAD) = 1.000000000E+00 NUTATION RATE(RAD/MSDYS) = 6.9444444E-04

REFERENCE
SECTION

DESCRIPTION

ITEM

- 3 A table of planetary constants, as preset or input, and of options requiring the planetary ephemeris tape. In this case, the options are moon perturbations and eclipsing

2.1.3

11.3.1.2

***** ECLIPSING CONSTANTS *****
 RE = 1.0000000E+00 RS = 1.09121800E+02 RM = 2.72506300E-01 ERAU = 2.34548650E+04 (4)
 ***** PLANETARY EPHEMERIS FILE INITIALIZED WITH 6 BODIES). (5) *****

ENTER SEGMENT 10 AT 122.3 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .5 CP SECS., 3.6 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

INVP	0	ICENT	1	IDRAG	0	ALP4G	3.585328504E+00	COAM	0.
JVFP	0	JNORM	1	IR	8	ALG-OES	2.054241915E+02	ER	1.000000000E-10
MVEP	0	MAJOR	0	ISRP	0	TJDATE	2.439598500E+06	HMIN	2.000000000E+00
KVEP	0	MASS	0	NEQS	3	TSTART	2.468833333E+03	HMAX	2.000000000E+00
LVEP	0	NT	0	RECP	0	TSTOP	3.268833333E+03	H0	2.000000000E+00
I:ENTX	1	JNORMX	1	NHASSX	0	FLIGHT	8.000000000E+02	NTX	0.
				NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

2468.8333 TZFR0
 3268.8333 TSTOP

*** TRAJECTORY START

***** MCI ***** (6)
 SEG12 ENTRY TIME IS 122.45500

PRECSSION MATRIX FROM MEE-EPOCH TO MEE-DATE

9.999999999993E-01	1.7494515030427E-05	4.5619121073485E-07	(7)
-1.0494516030427E-06	9.999999999994E-01	-2.3937529677164E-13	
-4.5619121073485E-07	-2.3937530062820E-13	9.9999999999989E-01	

SELENOGRAPHIC MATRIX FROM MEE-DATE TO MF-DATE

8.5791576365784E-01	5.1353198153613E-01	-1.62925255578576E-02	(8)
-4.4065053901101E-01	7.3097179531435E-01	-3.7860096960385E-01	
-1.8133677808800E-01	3.3263875116427E-01	9.2541658696247E-01	

ITEM	DESCRIPTION	REFERENCE SECTION
4	The constants for the determination of eclipsing, requested by PRCDE(H), are the radii of the earth, sun, and moon (in er) and the number of er/au (au = astronomical unit)	11.3.1
5	Indicates the planetary ephemeris file TAPE7 has been initialized (i. e., read) to the date of epoch, with two bodies (sun and moon)	16
6	Output comment specifying the coordinate system in which the numerical integration will be performed	11.1.6
7	Precession matrix used to rotate from MEE of midnight day of epoch to MEE of current date, printed whenever LEMSP = 0	2.1.4
8	Selenographic matrix from MEE to MF, printed when LEMSP = 0	2.1.4

MCI VECTORS AT T = 2458.83333 H = .250000 NSTEP = 0

2.314753981350E+07
 -1.010958059718E+08
 -6.9334131827016E+07

ECI VECTORS

-9.393036299099E+08
 5.322930504899E+08
 3.230949691360E+08

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

SELENOCENTRIC 1.113596E-02-2.067551E-03 9.021995E-03 6.193624E-03-1.113696E-02 3.469447E-17 1.387779E-16

OTHER BODIES 1.752257E-03 1.724183E-03-2.909101E-04-1.138740E-04 6.190841E-04 1.611891E-03-2.982365E-04

TOTAL 1.054485E-02-3.433605E-04 8.731075E-03 6.079750E-03-1.051788E-02 1.611891E-03-2.982365E-04

STEP DOUBLED T = 2475.33333 H = .500000 NSTEP = 25
 STEP DOUBLED T = 2483.83333 H = 1.000000 NSTEP = 41
 STEP DOUBLED T = 2500.83333 H = 2.000000 NSTEP = 57

*** CRASH *** ALTITUDE = -76344.0 TIME = 2880.83333 (10)

SF612 EXIT TIME IS 129.26430 TOTAL TIME IN SF612 WAS 2.80800 SECONDS TO PROCESS 247 STEPS

MCI VECTORS AT T = 2980.83333 H = 2.000000 NSTEP = 247

3.791675050137E+06
 -3.746030520623E+06
 -1.803319931610E+06

ECI VECTORS

-1.004436843417E+09
 -4.440455848847E+03
 -3.678980319840E+00

ITEM	DESCRIPTION	REFERENCE SECTION
9	The vectors \underline{r} , \underline{i} , and $\underline{\ddot{r}}$ in the integration coordinate frame and in the <u>ECI frame at epoch</u>	Case A: Item 30
10	<u>Indicates when and where the vehicle crashed into the moon</u>	2.1.3 2.1.4

5.640676741008E+08	4.338720210350F+03	3.636260229247E+00
3.591575454330E+08	3.245180355542E+03	1.751256984947E+00

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SELEMPOTENTI	5.470625E+00	-3.587125E+00	3.640842E+00	1.754169E+00	-5.470625E+00	7.203194E-09	4.973799E-14	
OTHER BODYFS	8.737533E-05	7.797226E-05	-3.102316E-05	2.433802E-05	8.100298E-05	2.006469E-05	-1.689197E-05	
TOTAL	5.470544E+00	-3.547047E+00	3.640811E+00	1.754145E+00	-5.470544E+00	2.007190E-05	-1.689197E-05	

*** VEHICLE CRASHED (U)

*** THIS CASE TOOK 2.876 SECONDS TO INTEGRATE A SPAN OF 412.0000 MINUTES ***

*** FROM 2468.833 TO 2880.833 MYNUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 125.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 3.0 CP SECS., 49.1 PP SECS.

REFERENCE
SECTION

DESCRIPTION

ITEM

11 Remark giving reason for termination (in this case, because the vehicle crashed)

ITEM	DESCRIPTION	REFERENCE SECTION
12	<u>Key to additional ephemeris output provided in lunar runs</u>	
13	<u>Special output options requested by PRCDE</u>	11.3.1.2

*** CASE 1

*** PUNCH PRINT

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.0000	2.31475398E+07	-6.57546633E+02	-33.78873098	282.90748738	.77972	
17 / R	2468.83333	-1.01006806E+08	3.52403883E+03	-77.09251221	-33.78873098	0.00000	
50.00000	61730.00000	-6.93415183E+07	2.46162612E+03	19582.12025	177.94734153	0.00000	
	.25000	1.24685322E+08	4.34857243E+03	-33.78873098	69.78024625	0.00000	

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.07315622E+07 1.09681142E+00 3.87507025E+01 3.39391443E+02 9.09284222E+01 2.60928866E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.0000	8.09956508E+07	-2.94728354E+03	-12.17957226	311.64849893	.86253	
17 / R	2468.83333	-9.10722076E+07	3.05296783E+03	-48.35150066	-12.17957226	0.00000	
50.00000	61730.00000	-2.63056484E+07	9.54549037E+02	19582.12025	177.65893199	0.00000	
	.25000	1.24685322E+08	4.34857243E+03	-12.17957226	282.52768331	0.00000	
	58.16398	1.89276533E+01	4.23325212E+01	-6.56148470	-6.51581120		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.07267055E+07 1.12438170E+00 1.62595798E+02 2.68132925E+02 1.05503772E+02 2.61038237E+03

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.0000	2.31475398E+07	-6.57546633E+02	-33.78873098	282.90748738	.77972	
17 / R	2468.83333	-1.01006806E+08	3.52403883E+03	-77.09251221	-33.78873098	0.00000	
50.00000	61730.00000	-6.93415183E+07	2.46162612E+03	19582.12025	177.94734153	0.00000	
	.25000	1.24685322E+08	4.34857243E+03	-33.78873098	69.78024625	0.00000	

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.0000	8.09956508E+07	-2.94728354E+03	-12.17957226	311.64849893	.86253	
17 / R	2468.83333	-9.10722076E+07	3.05296783E+03	-48.35150066	-12.17957226	0.00000	
50.00000	61730.00000	-2.63056484E+07	9.54549037E+02	19582.12025	177.65893199	0.00000	
	.25000	1.24685322E+08	4.34857243E+03	-12.17957226	282.52768331	0.00000	
	58.16398	1.89276533E+01	4.23325212E+01	-6.56148470	-6.52038802		

14

REFERENCE
SECTION

DESCRIPTION

ITEM

14 Epoch print in lunar mode in MCI and MF (moon-fixed) coordinate frames (Item 38 of Case A plus one line at the end of the MF output, as in Item 12 of this case). The classical elements in MCI and MF coordinate frames are also shown

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,DZ,V	LAT,...	ALPHA,...	REV,...	MF
4/20/67	41.83356	5.32324080E+06	-6.08367879E+03	-3.31007435	333.16785725	.94144	+CRASH*
0/0	2880.66689	-2.02552741E+06	6.09263787E+03	-20.83214234	-3.31007435	0.00000	
40.01336	40.01336	-3.29409986E+06	1.58840219E+03	.49376	154.94370509	0.00000	
	2.00000	5.70509989E+06	8.75525015E+03	-3.31007435	72.21872601	0.00000	
	67.87118	-1.61428184E+01	1.24793857E+02	5.78130875	175.80364851		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)
 -1.08498492E+07 1.11275053E+00 1.80769519E+01 3.49374042E+02 1.887182229E+02 2.60561349E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,DZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/20/67	412.00000	3.79157606E+06	-2.6859808E+03	-18.70238820	315.36187189	.86771	PRE-EVMT
0/0	2880.83333	-3.74408062E+06	7.04557936E+03	-44.63812771	-18.70238820	0.00000	
50.00000	50.00000	-1.80390993E+06	4.55333714E+03	-12.56592	154.62950533	0.00000	
	2.00000	5.62574778E+06	8.81009729E+03	-18.70238820	55.93435572	0.00000	

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)
 -1.07774001E+07 1.11430955E+00 3.83112676E+01 3.40732834E+02 8.76630660E+01 2.60846103E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,DZ,V	LAT,...	ALPHA,...	REV,...	MF
4/20/67	412.00000	5.26223684E+06	-6.13368611E+03	-3.19484861	333.52754951	.94247	PRE-EVMT
0/0	2880.63333	-1.96458627E+06	6.14193076E+03	-20.47235007	-3.19484861	0.00000	
50.00000	50.00000	-3.13531907E+05	1.59145781E+03	-12.56592	154.71321546	0.00000	
	2.00000	5.62574778E+06	8.80400709E+03	-3.19484861	72.20012514	0.00000	
	57.92550	1.74346113E+01	3.03008926E+02	-6.41658430	-6.21646446		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)
 -1.08498490E+07 1.11277339E+00 1.80751758E+01 3.49375107E+02 1.88718806E+02 2.60561375E+03

*** VEHICLE CRASHED

*** END OF TRAJECTORY ***

C.6 TEST CASE E: ECI SINGLE-VEHICLE POWERED
FLIGHT EPHEMERIS GENERATION RUN (ITIN = 3)

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EEEEEEEEEE
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EEEEEE
EEEEEE
EE
EEEEEEEEEE
EEEEEEEEEE

CCCCCCCCCC
CCCCCCCCCC
CC
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CC
CCCCCCCCCC
CCCCCCCCCC

TRAJ-66 (AD104A)

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RRRRRRRR
RRRRRRRR
RR
RRRRRRRR
RRRRRRRR
RR
RR
RR
RR
RR
RR
(02/21/74)

TTTTTTTTTT
TTTTTTTTTT
TT
TT
TT
TT
TT


```

MODEL DATA
M1 TRPX MODEL
INFORMI
D 02000
D J3000
D J4000
CRASHJ.
LEMSPJ
ER 1.0E-11
END

```

```

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9

```

```

INTERMS
-1.0827E-3
2.693E-6
1.4E-6
HMIN C.O.390625
GM (.95339362E-2
INPCMPI
H0 0.015525
IPINS 100
DITIN 3
MTERMS04,60

```

***** GRAVITY MODEL *****

GM = .5531936200E-02 ER**3/MIN**2 = .147792018E+17 FT**3/SEC**2 = .3986422981E+15 M**3/SEC**2
 NO NORMALIZATION WITH 3 TERMS.

```

N M CNM ** W P CNM SNM
2 -1.7427 DE-02 0. ** 4 C .147792000E-05 0.
3 .26930 DE-05 0. ** **

```

--

***** GENERAL PERTURBATIONS GRAVITY MODEL *****

GM = .55304774E-02 ER**3/MIN**2 = .147660055E+17 FT**3/SEC**2 = .3986049304E+15 M**3/SEC**2

**** ZONAL HARMONICS ****

EJ2 = .103254900E-02 EJ3 = -.243507000E-05 EJ4 = -.123200000E-05

***** PHYSICAL CONSTANTS *****

```

GM(ER**3/MIN**2) = .5531936200E-02 D(EGE(RAD/MIN)) = .437526917E-02 GMLAT(DEG) = .793000000E+02
GM(KM**3/SEC**2) = 0. D(OMEGA(RAD/MIN)) = .437526917E-02 GMLNG(DEG) = .291000000E+02
SGM(ER**3/MIN**2) = 0. G(OMEGA(RAD/MIN)) = 0. AM(ER) = .272516277E+02
ERFT(FT/ER) = .29257390E+09 ER(KM/ER) = .637616499E+04 ERNM(NM/ER) = .344393360E+04
FTKM(FT/KM) = .328183990E+14 FTNM(FT/NM) = .607611559E+04 AE(ER) = .100000000E+01
GSUBJ(FT/SEC**2) = .321740000E+02 D(GREE( DEG)) = .372957795E+02 SLT(ER/MIN) = .292017637E+04
CKEP = .100000000E-11 F = .335232997E-02 PI = .314159265E+01

```



REFERENCE
SECTION

DESCRIPTION

ITEM

1 Card images of the input MODEL data. Emphasis is given to the variates associated with a powered flight run (ITIN = 3), the others having been discussed earlier:

NPCMP, PTNS, ER, CRASH

2.1.4

```

***** INPUT/OUTPUT CONVERSION FACTORS *****
OF(I/O-ER) = .2192573AE+9 VF(I/O-ER/MIN) = .34876230E+6 AF(I/O-ER/MIN**2) = .59127150E+04

***** INTEGRATION INPUTS *****
IPCMF = 1 INSTEP = 2
HMIN = .39062510E-02 HMAX = .64010000E+02 HCR = .15625100E-11
ER = .1000000E-10

***** SPECIAL OPTIONS *****
TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAFE = 0 NEDOT = 0
PRHO = 0 NODPR = 0 CLASS = 0 LEMSP = 0 PINS = 10

***** CRASH ALTITUDE TABLE *****
ECI CRASH ALTITUDE = 0. MCI CRASH ALTITUDE = .32000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
(IN FT)
BODY(1) CRASH ALTITUDE = .30000000E+05 BODY(2) CRASH ALTITUDE = 0.
BODY(3) CRASH ALTITUDE = .30000000E+05 BODY(4) CRASH ALTITUDE = 0.
BODY(5) CRASH ALTITUDE = 0. BODY(6) CRASH ALTITUDE = 0.
BODY(7) CRASH ALTITUDE = 0.

*****
ENTER SEGMENT 01 AT 12.6 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 12.6 CP SECS.

```

2

ITEM	DESCRIPTION	REFERENCE SECTION
2	Crash altitude table. ECI and MCI crash altitudes at which to stop integrating for the sun and moon, respectively	2.1.3 2.1.4
	Interplanetary crash altitude table. Crash altitudes at which to stop integrating for solar system bodies	2.1.3

***** VEHICLE DATA FOR CASE 1 *****

IVR00002	IMNTH 1	ICAY 1	CARD 1
IVR001971	MIN 0	SEC 0	CARD 2
PR 0	AL 99.9932723952402	CL 0	CARD 3
IIC0VP4	2	90	CARD 4
IC 0	5	1E25.92492397	CARD 5
IC 4	6		CARD 6
IIDRAG3	IKDRAG-1		CARD 7
DRAG 80			CARD 8
90			CARD 9
90			CARD 10
90			CARD 11
90			CARD 12
90			CARD 13
90			CARD 14
90			CARD 15
50			CARD 16
DPRCDE X X	ALTER1	2	CARD 17
PTIM 0	2	65.8313210075	CAKD 17
4	1		CARD 18
DALPH).0:2568050	5		CARD 19
IMPFRP3	IIOIPEF	POWER1.	CARD 20
MFFRP 16,15			CARD 21
500.			CARD 22
			CARD 23
			CARD 24
			CARD 25
			CARD 26
			CARD 27
			CARD 28
			CARD 29
			CARD 30
			CARD 31
			CARD 32
			CARD 33
			CARD 34
			CARD 35
			CARD 36
			CARD 37
			CARD 38
			CARD 39
			CARD 40
			CARD 41
			CARD 42
			CARD 43
			CARD 44
			CARD 45
			CARD 46
			CARD 47
			CARD 48
			CARD 49
			CARD 50
			CARD 51
			CARD 52
			CARD 53

ITEM	DESCRIPTION	REFERENCE SECTION
3	<p>Card images of input <u>VEHICLE</u> data. Emphasis is given to the variables associated with a powered flight run (ITIN = 3), the others having been discussed earlier:</p> <p>AL, DL, IØTPF, NPFRP, PFRP, DALPH, KDRAG ALTPR CDAS</p>	<p>11.1.5 11.3.1.2 11.1.8</p>

EPOCH
 YR/MC/DAY
 1971/ 1/ 1
 C.
 0.
 0.
 0.

X,Y,Z,DX,DY,DZ
 -.36312964377E+J7
 .216E255545E+J4
 C.
 -.1502777375E+J4
 -.0000000000E+J3
 -.13459535244E-1J

A,B,C,A,R,V
 .39993272396E+02
 0.
 .9010000000E+02
 .3000000000E+02
 .2032573300E+08
 .1525928924E+04

INITIAL CONDITIONS
 A,E,I,O,U,TAU
 .17491036770E+08
 .99653932592E+00
 .50536039439E-12
 .2799932724E+03
 .3600000000E+03
 -.14973983591E+02

AF,AG,AL,CHI,PSI
 .17293193251E+00
 -.98141957265E+00
 .21634939238E+02
 .99993272396E+02
 -.47433638210E-14
 .75512639055E-15

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

ENTER SEGMENT 02 AT 12.8 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .2 CP SECS.

ENTER SEGMENT 1' AT 12.8 SECONDS. EXECUTION TIME FOR SEGMENT 2 WAS .0 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

IVEP	1	ICENT	1	IDRAG	3	ALPHG	.174521183E+01	COAM	.800000000E+02
JVEP	0	JNORM	1	IR	9	ALG-DEG	.969932724E+02	ER	.100000000E-10
MVEP	0	MAJOR	0	ISRF	0	TJDATE	.244095257E+07	HMIN	.195312500E-02
KVEP	0	MASS	0	NEGS	3	TSTART	C.	HMAX	.600000000E+02
LVEP	0	NT	3	RECMP	2	TSTOP	.600000000E+02	HJ	.125000000E+00
ICENTX	1	JNORMX	0	MASSX	0	FLIGHT	.600000000E+02	NTX	0.
				NASA	0	SSTEP	.100000000E+03	SORC	.100000000E+01
				NRING	0	CPAN	C.	UTD	.350000000E+02
				IFORM	0				



REFERENCE
SECTION

DESCRIPTION

ITEM

4 Quantities associated with the current vehicle (Table C-1)

Table C-1. Definitions of Initialized Integration Quantities

Symbol	Definition	Reference Section
IVEP	Number of C and S parameters (GPRAM)	2.1.5.2
JVEP	Number of other model parameters (\emptyset PRAM)	2.1.5.3
MVEP	Number of mass parameters (MPRAM)	2.1.5.1
KVEP	Number of vehicle-dependent parameters (VPRAM)	11.1.14
LVEP	Number of delayed parameters (i. e., THRUST, DRAG, etc.)	11.1.14
ICENTX	Central force flag for the moon	
ICENT	Central force flag for the earth	
JNORM	Normalization for the earth gravity model	2.1.2.2
MAJOR	Flag for the integration of the variational equations	
NMASS	Number of masses in the earth gravity model	
NT	Number of terms in the earth gravity model	2.1.2.2
JNORMX	Normalization for the lunar gravity model	2.1.2.2
IDRAG	Flag indicating the atmospheric model used	11.1.8
IR	Ratio of Runge-Kutta to Cowell step size (H0/IR)	2.1.4
ISRP	Flag for solar radiation pressure	2.1.2.6
NEQS	Total number of equations to be integrated	
RECOMP	Flag for recomputation of perturbations	2.1.4
NMASSX	Number of masses in the lunar gravity model	
NASA	Coordinate and time-keeping transformation option flag	2.1.4

Table C-1. Definitions of Initialized Integration Quantities (Continued)

Symbol	Definition	Reference Section
ALPHG	Right ascension of Greenwich (rad at midnight of epoch day)	
ALC-DEG	Right ascension of Greenwich (deg at midnight of epoch day)	
TJDATE	Julian date of epoch day	
TSTART	Trajectory start time (MME)	
TSTOP	Trajectory stop time (MME)	
FLIGHT	Duration of flight (TSTOP-TSTART, min)	
SSTEP	Number of integration steps specified per rev when the regularized time variable is used	11.1.6
CDAW	Reciprocal of the ballistic coefficient	
ER	Error control in integration ($ER = 1. \cdot 10^{-S}$, where S is the number of significant figures)	2.1.4
HMIN	Minimum absolute step size for integration	2.1.4
HMAX	Maximum absolute step size for integration	2.1.4
H0	Initial integration step size: A negative value indicates backward integration	2.1.4
NTX	Number of terms in the lunar gravity model	2.1.2.2
SORD	Power of the regularization transformation	11.1.6
CPAW	Solar radiation pressure coefficient	11.1.4
UTD	Correction that relates iteration time to ephemeris time, sec	2.1.4

TIME (MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

TIME (MME)	TYPE	ASSOCIATED QUANTITIES	PREDETERMINED EVENT TABLE *
0.0000	TZERO		
		AL .59993272E+L2	DL 0.
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, WD, WD, DRAG
		AZ .16666667E+00	BETA
NO. 1	0.000000		.291666667E+03
	0.000000		.60000000E+04
	10.000000		.40000000E+06
PRIMARY			.24000000E+04
			.80000000E+02
			0.
			CONSTANT
			0.
			0.
			0.
			0.
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, WD, WD, DRAG
		AZ .13333333E+00	BETA
NO. 2	.166667		.291666667E+03
	10.000000		.60000000E+04
	1.000000		.37600000E+06
SECONDARY			.24000000E+04
			.80000000E+02
			0.
			0.
			CONSTANT
			1.
			-.59990000E+01
			0.
			0.
			0.
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, WD, WD, DRAG
		AZ .27751333E+00	BETA
NO. 3	.163333		.291666667E+03
	11.000000		.60000000E+04
	5.650000		.37360000E+06
SECONDARY			.24000000E+04
			.80000000E+02
			0.
			0.
			CONSTANT
			0.
			0.
			0.
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, WD, WD, DRAG
		AZ .16333333E+01	BETA
NO. 4	.277513		.291666667E+03
	16.550000		.60000000E+04
	93.349200		.36000000E+06
SECONDARY			.24000000E+04
			.80000000E+02
			0.
			0.
			GRAVITY TURN
			1.
			0.
			0.
			0.
			0.

ITEM	DESCRIPTION	REFERENCE SECTION
5	<u>Quantities associated with the predetermined event table (Table C-2)</u>	

Table C-2. Definitions of Predetermined Event Table Quantities

Symbol	Definition	Reference Section
TZERØ	Time to start integration	11.1.15
AL	Right ascension of launch α_L , deg	11.1.15
DL	Declination of launch δ_L , deg	11.1.15
STAGE	Stage number	11.1.15
T	Start time of this stage, minutes from epoch	11.1.15
ST	Start time t, sec	11.1.15
SdT	Δt , sec, where the start time of the next stage is $t + \Delta t$, min	11.1.15
TF	Termination time for this stage, minutes from epoch	11.1.15
WF	Final weight, lb	11.1.15
DV	Achieved change in velocity during this stage, ft/sec	11.1.15
HF	Cutoff altitude for this stage, ft	11.1.15
AA	Cutoff angle of attack for this stage, deg	11.1.15
AZ	Roll axis azimuth at the start of this stage	11.1.15
ISP	Specific impulse, sec	11.1.15
AE	Exit area, ft ²	11.1.15
W0	Initial vehicle weight for this stage, lb	11.1.15
WD	Weight flow rate, lb/sec	11.1.15
DRAG	Drag reference area, C_{DA} or A	11.1.15
BETA	Roll axis pitch attitude at the start of this stage	11.1.15

Table C-2. Definitions of Predetermined Event Table Quantities (Continued)

Symbol	Definition	Reference Section
RATES	= CONSTANT; WR, WP, WY are constant throughout this stage	11.1.15
	= GRAVITY TURN; this is a gravity turn stage (Item 11)	
	= FREE FLIGHT; this is a free flight stage (Item 12)	
WR	Roll axis turning rate, deg/sec	
WP	Pitch axis turning rate, deg/sec	11.1.15
WY	Yaw axis turning rate, deg/sec	
LIFTZ	Constant lift reference area coefficient C_{L0A} or A	
LIFTAL	Lift slope reference area coefficient $C_{L\alpha A}$ or A	
TSTØP	Time to stop integration (Item 5)	
PRIMARY ^a	Certain primary parameters (ISP, AE, W0, WD, DRAG, LIFTZ, and LIFTAL) are defined for a primary stage and are held constant until the next primary stage is reached	11.1.15
SECONDARY ^b	Secondary parameters (WR, WP, WY, TF, DV, HF, WF, AA, AZ, and BETA) can change at each secondary stage (for secondary stages occurring within a primary stage), while the primary parameters remain constant	11.1.15

^a Primary parameters define the vehicle configuration.

^b Secondary parameters control maneuvering of the vehicle specified by the primary parameters.

STAGE	T, ST, SDT	TF, MF, DV, HF, AF	ISP, AE, W3, WD, DRAG	RATES, WR, WP, WY, LIFTZ, LIFTAL
NO. 5	1.833333 110.000000 .600000	.184333333E+01	BETA .54000000E+02 .60000000E+04 .13600000E+06 .37570000E+04 .80000000E+02 0.	CONSTANT 0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, W3, WD, DRAG	RATES, WR, WP, WY, LIFTZ, LIFTAL
NO. 6	1.943333 110.500000 1.000000	.18666667E+01	BETA 0. 0. .13374580E+06 0. .80000000E+02 0.	FREE FLIGHT 0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, W3, WD, DRAG	RATES, WR, WP, WY, LIFTZ, LIFTAL
NO. 7	1.866667 112.000000 135.000000	.41166667E+01	BETA .30000000E+03 .60000000E+04 .11548500E+06 .75000000E+03 .80000000E+02 0.	CONSTANT 0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, MF, DV, HF, AA	ISP, AE, W3, WD, DRAG	RATES, WR, WP, WY, LIFTZ, LIFTAL
NO. 8	4.116667 247.000000 3353.000000	.50000000E+02	BETA 0. 0. .10000000E+05 .50000000E+02 0.	FREE FLIGHT 0. 0. 0. 0. 0.
PRIMARY				

60.0000 TSTOP

*** TRAJECTORY START
 *** POWERED FLIGHT

*** ENTRY TIME IS 12.6990C

TSEC = .000000 T = 0.000000 H = .015625 NSTEP = 0
 X, Y, Z X0, Y0, Z0 X00, Y00, Z00



-.56312964977JE+J7
 .206082555546E+J8
 0.
 -.150277773754E+04
 -.264798324310E+03
 -.134595352040E-10
 -.295181229789E+01
 -.1675210.7208E+02
 -.129863715108E-03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.22020E+01 5.588194E+02 -3.171343E+01 -1.298687E-04 -3.220200E+01 1.145514E-16 -1.298687E-04
 ATMOSPHERIC 1.529623E-16 1.506416E-16 2.65442E-17 2.159191E-22 1.838109E-22 -1.529623E-16 2.159191E-22
 THRUST 4.921208E+01 -9.539997E+00 4.846544E+01 0. 4.921208E+01 -3.979039E-13 -3.231174E-27
 TOTAL 1.711009E+01 -2.951812E+00 1.675200E+01 -1.298687E-04 1.701009E+01 -3.979029E-13 -1.298687E-04

REFERENCE
SECTION

DESCRIPTION

ITEM

6 Powered flight. This notation indicates that the vehicle is thrusting, i.e., that ISP and WD are non-zero. If ISP and WD are zero, the vehicle's trajectory is controlled by external forces only, i.e., the pull of the earth or the moon. In this case, the vehicle is considered to be in free flight.

7 Trajectory print at the beginning of this stage:

TSEC = time from epoch, sec

T = time from epoch, min

H = integration step size

NSTEP = number of integration steps

X, Y, Z = vehicle position at time t, ft

XD, YD, ZD = vehicle velocity at time t, ft/sec

XDD, YDD, ZDD = vehicle acceleration at time t, ft/sec²

STAGE NO. 1	T, ST, STAU	H, RHO, MACH, P, VA	LAT, LONG, R, V, AA	ISP, M, CDAM, CLAM	XI, WR, MP, WY
CONSTANT	0.00000	-74343156E-07	0.	.25492674E+03	-.17353254E+00
	0.00000	.23768946E-02	.36000000E+03	.43000000E+05	.98492814E+00
	0.00000	.35465123E-08	.20925738E+08	.44000000E-01	0.
		.14695972E+02	.15259289E+04	0.	0.
		.9535590E-05	.90000069E+02	0.	0.

TSEC = 1.00000 T = .166667 H = .015525 NSTEP = 11

	X, Y, Z	XD, YD, ZD	XCD, YCD, ZCD
	-.364E+3054873E+17	-.153495603531E+04	-.35064446474E+01
	.20E+64916957E+18	-.81505027405E+02	.200344323840E+02
	-.640979943981E-12	-.129721395149E-02	-.12941977535E-03

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOCENTRAL	3.219920E+01	5.610720E+00	-3.171659E+01	-1.298305E-04	-3.219927E+01	1.104126E-10	1.298405E-04	
ATMOSPHERIC	5.952140E-02	1.027157E-02	5.862842E-02	4.124370E-07	5.952132E-02	1.016091E-04	4.125050E-07	
THRUST	5.259766E+01	9.127455E+00	5.179985E+01	0.	5.259766E+01	-3.835217E-02	1.629603E-08	
TOTAL	2.033896E+01	3.506404E+00	2.003443E+01	-1.294181E-04	2.033893E+01	-3.825056E-02	1.294443E-04	

STAGE NO. 1	T, ST, STAU	H, RHO, MACH, P, VA	LAT, LONG, R, V, AA	ISP, M, CDAM, CLAM	XI, WR, MP, WY
CONSTANT	.166667	.90832625E+03	-.17888378E-07	.25611673E+03	-.17353254E+00
	10.00000	.23143607E-02	.36000000E+03	.37600000E+05	.98492814E+00
	10.00000	.16920852E+00	.20926646E+08	.45615542E+04	0.
		.14219973E+02	.15371184E+04	0.	0.
		.18720916E+03	.56033344E-01	0.	0.

ITEM	DESCRIPTION	REFERENCE SECTION
8	Quantities associated with the powered flight output at the beginning of <u>this stage (Table C-3)</u>	Item 7
9	<u>Trajectory print at the end of this stage</u>	Item 8
10	<u>Powered flight output at the end of this stage</u>	

Table C-3. Definitions of Powered Flight Output Quantities

Symbol	Definition	Reference Section
T	Time from epoch, min	
ST	Time from epoch, sec	
STAU	Time from the beginning of this stage, sec	
H	Vehicle altitude, ft	
RHØ	Atmospheric density at altitude h, slug/ft ³	
MACH	Mach number (the ratio of the speed of the body to the speed of sound in the surrounding atmosphere)	11.1.15
P	Pressure at altitude h, lb/in ²	
VA	Absolute value of the relative velocity vector	
LAT	Vehicle geodetic latitude, deg	11.1.14
LØNG	Vehicle geodetic longitude, deg	11.1.14
R	Vehicle geocentric radius, ft	11.1.15
V	Vehicle velocity, ft/sec	11.1.15
AA	Angle of attack, deg	
ISP	$(ISP_i \cdot \dot{W} - Ae P(h))/\dot{W}$, where ISP_i (in sec), \dot{W} , and Ae are input quantities for the i^{th} stage and $P(h)$ is computed.	
W	Current vehicle weight, lb	
CDAW	$C_D A/W$	11.1.15
CLAW	$(C_{L0} + C_{L\alpha} \cdot \alpha)A/W$, where α is the angle of attack	11.1.15
XI	Roll axis = $\underline{\xi} = \begin{Bmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{Bmatrix}$	11.1.15
WR	Roll axis turning rate, deg/sec	11.1.15
WP	Pitch axis turning rate, deg/sec	11.1.15
WY	Yaw axis turning rate, deg/sec	11.1.15

*** POWERED FLIGHT

 SEG10 ENTRY TIME IS 12.96800

 ECI *****

TSEC = 1.00000 T = .166667 H = .001953 NSTEP = 11
 X,Y,Z X00,Y00,Z00

-.364648054873E+17
 .206054966957E+18
 -.648979943981E-12
 -.153495603531E+04
 -.815050274055E+12
 -.129418077535E-03

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	I,-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.215920E+01	5.610729E+00	-3.173659E+01	-1.298305E-04	-3.219920E+01	1.10+124E-10	-1.298405E-04	
ATMOSPHERIC	5.952149E-02	1.027157E-02	5.862842E-12	4.124376E-07	5.952132E-02	1.015091E-04	4.125050E-07	
THRUST	5.259766E+11	5.127405E+00	5.179965E+01	0.	5.259764E+11	-3.835217E-02	-1.629603E-04	
TOTAL	2.033399E+01	-3.506404E+00	2.003443E+01	-1.294181E-04	2.033393E+11	-3.825056E-02	-1.294443E-04	

STAGE	T,ST,STAU	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,CDAM,CLAW	XI,WR,WP,WY
NO. 2	.166667	.50832625E+03	-.17888378E-07	.25611673E+07	-.17353254E+00
CONSTANT	10.000000	.23143607E-02	.36000000E+03	.37600000E+16	.98482814E+00
	0.000000	.16827852E+00	.20926646E+18	.45615542E-14	0.
		.14219973E+02	.15371184E+04	1.	0.
		.18720916E+03	.56033344E-01		-.50000000E+01

NODE T = .17321522E+00
 DT = .19531250E+00
 .364683744089E+07
 -.1535570390157E+04
 .206164797969E+08
 -.772317138037E+02
 .621239748153E-13
 .102815667043E+00

TSEC = 11.000000 T = .183333 H = .001953 NSTEP = 20

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

--.364801726553E+17
 .206784252531E+18
 .759617574177E+19
 --.153848227290E+04
 --.613513300054E+12
 .230317250271E+01
 --.353462557153E+01
 .202080192221E+92
 .461727981082E+01

FORCES
 GEOPOTENTIAL 3.219859E+01 5.612935E+00 -3.170558E+01 -1.310070E-04 -3.219859E+01 -1.9617E-07 -1.298381E+04
 ATMOSPHERIC 7.316137E-02 1.261795E-02 -7.205949E-02 -8.109075E-04 -7.315575E-02 1.356065E-04 -8.111105E-04
 THRUST 5.298815E+01 -9.160178E+00 5.198565E+01 4.618222E+00 5.278659E+01 -3.536627E-02 4.618278E+01
 TOTAL 2.112799E+01 -3.534626E+00 2.020800E+01 4.617280E+00 2.051475E+01 -3.523086E-02 4.617338E+00

STAGE 2
 NO. 2
 CONSTANT

T, STAS, H, FHO, MACH, P, VA, LAT, LONG, R, T, AA, ISP, M, CDAM, CLAA, XI, MR, MP, MY
 .183333 .11058060E+04 .20937778E-05 .25637126E+03 --.17297220E+00
 1.000000 .23009341E-02 .36000000E+03 .37360000E+05 .98108057E+00
 1.000000 .18683094E+00 .20926844E+08 .45775654E-04 .87155743E-01
 .14119162E+02 .15397068E+04 .15397068E+04
 .20779337E+03 .43653501E+01

*** POWERED FLIGHT

* * * * *
 SEG18 ENTRY TIME IS 13.03790 ECI * * * * *

TSEC = 11.000000 T = .183333 H = .000244 NSTEP = 20

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

--.364801726553E+17
 .206784252531E+18
 .759617574177E+19
 --.153848227290E+04
 --.613513300054E+12
 .230317250271E+01
 --.353462557153E+01
 .202080192221E+92
 .461727981082E+01

FORCES
 GEOPOTENTIAL 3.219859E+01 5.612935E+00 -3.170558E+01 -1.310070E-04 -3.219859E+01 -1.9617E-07 -1.298381E+04
 ATMOSPHERIC 7.316137E-02 1.261795E-02 -7.205949E-02 -8.109075E-04 -7.315575E-02 1.356065E-04 -8.111105E-04
 THRUST 5.298815E+01 -9.160178E+00 5.198565E+01 4.618222E+00 5.278659E+01 -3.536627E-02 4.618278E+01
 TOTAL 2.112799E+01 -3.534626E+00 2.020800E+01 4.617280E+00 2.051475E+01 -3.523086E-02 4.617338E+00

STAGE	T,S,I,STAL	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,CDAM,CLAW	XI,MR,WP,WY
NO. 3	.183333	.11058060E+04	.20933778E-05	.25637126E+03	-.17287220E+00
CONSTANT	11.000000	.23009341E-02	.36000000E+03	.37360900E+05	.98198057E+00
	C.000000	.18683094E+00	.209226844E+08	.45775654E-04	.87155743E-01
		.14119162E+02	.15397068E+04	0.	0.
		.20779307E+03	.43653501E+01	0.	0.

STEP	DOUBLED	T =	H =	NSSTEP =
*	DOUBLED	.189681	H =	.003906
*	DOUBLED	.197982	H =	.009977
*	DOUBLED	.214583	H =	.001953
*	DOUBLED	.247786	H =	.003906

TSEC = 16.650800 T = .277513 H = .003906 NSTEP = 191

X,Y,Z

X0,Y0,Z0

X00,Y00,Z00

-.365675933541E+07
 .206064108510E+08
 .885024034732E+02
 -.155951933440E+04
 .590891818731E+02
 .289348443908E+02
 -.391945831400E+01
 .224672720221E+02
 .48116479747E+01

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.219392E+01	5.625178E+00	-3.169867E+01	-2.66327E-04	-3.219392E+01	-2.470050E-06	-1.302060E-04	
ATMOSPHERIC	1.819448E-01	3.117549E-02	-1.785510E-01	-1.586009E-02	-1.912516E-01	2.010433E-04	-1.586599E-02	
THRUST	5.539249E+01	9.575821E+00	5.434449E+01	4.827774E+00	5.518169E+01	2.458609E-02	4.827942E+00	
TOTAL	2.330864E+01	3.919468E+00	2.246727E+01	4.811647E+00	2.293651E+01	2.478537E-02	4.811946E+00	

STAGE	T,S,I,STIAU	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,CDAM,CLAW	XI,MR,WP,WY
NO. 3	.277513	.26210510E+04	.24392663E-03	.25827539E+03	-.17287220E+00
CONSTANT	16.650800	.21998930E-02	.35995999E+03	.35003808E+06	.98198057E+00
	5.0E-800	.30002963E+00	.209226844E+08	.46660853E-04	.87155743E-01
		.13356512E+02	.15609066E+04	0.	0.
		.33193661E+03	.88776889E-01	0.	0.

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.17100

TSEC = 16.653800 T = .277513 H = .007488 NSTEP = 101
 X,Y,Z X0,Y0,Z0 XCO,YCO,ZCO

-.365676923541E+J7
 .20654128512E+J8
 .885724034732E+J2

-.155551933440E+04
 .590891818731E+02
 .289348449908E+02

-.391945641149E+01
 .224672044732E+02
 .491243101494E+01

FORCES
 MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.219392E+01 5.625178E+00 -3.169867E+01 -2.663727E-04 -3.219392E+01 -2.477050E-06 -1.302068E-04
 ATMOSPHERIC 1.819449E-01 3.117549E-02 -1.785510E-01 -1.586009E-02 -1.912516E-01 2.017433E-04 -1.586599E-02
 THRUST 5.539249E+01 -9.575809E+00 5.434438E+01 4.828557E+00 5.518162E+01 2.460175E-02 4.828726E+00
 TOTAL 2.330873E+01 -3.19456E+00 2.246720E+01 4.812431E+00 2.257644E+01 2.487932E-02 4.812730E+00

STAGE NO. 4
 GRAVITY TURN (11)
 T,ST,STAL H,R40,MACH,P,VA LAT, LONG,R,V,AA ISP,M,COAM,CLAY XI,WR,WP,WY
 .277513 .26210510E+04 .24392863E-03 .25827539E+03 -.17287198E+00
 16.653800 .21993930E-02 .35995999E+03 .36003808E+06 .98107935E+00
 0.003800 .30002963E+00 .20928359E+08 .46660853E-04 .87169895E-01
 .13358512E+02 .15609066E+04 0.
 .33193661E+03 .88773158E-01 -.40254883E+00
 0.

* STEP OCCURRED T = .290209 H = .007977 NSTEP = 126
 * STEP OCCURRED T = .306810 H = .001953 NSTEP = 142
 * STEP OCCURRED T = .340013 H = .003906 NSTEP = 158
 * STEP OCCURRED T = .306420 H = .007813 NSTEP = 174

REFERENCE
SECTION

DESCRIPTION

ITEM

- 11 Gravity turn. This notation indicates that the pitch plane is fixed, i.e., that the pitch axis is fixed throughout the stage (the vehicle's body orientation is defined by the roll, pitch, and yaw axes)

TSEC = 37.041425 T = .617357 H = .007913 NSTEP = 271
 X,Y,Z X0,Y0,Z0 X00,Y00,Z00
 --.26894805976E+07 --.165353137363E+04 --.523071513431E+01
 .20612855857E+08 .599829537238E+03 .301543083636E+02
 .251071623358E+04 .254268688923E+03 .180934763362E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.215672E+01 5.685668E+00 -3.165367E+01 -3.997464E-03 -3.215672E+01 -2.337933E-05 -1.400003E-04
 ATMOSPHERIC 1.865508E+00 3.57639E-01 -1.766205E+00 -5.168669E-01 -1.792509E+00 -7.503355E-02 -5.112762E-01
 THRUST 6.718376E+01 -1.142215E+01 8.357418E+01 1.861434E+01 6.455557E+01 2.892963E+00 1.838115E+01
 TOTAL 3.555301E+ (1-5.230715E+00 3.015431E+01 1.809348E+01 3.367635E+01 2.817906E+00 1.786973E+01

STAGE T, ST, STAU H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, W, CDAN, CLAM XI, WR, WP, WY
 NO. 4 .617357 .14703844E+05 .69159383E-02 .27067544E+03 --.16673889E+00
 GRAVITY TURN 37.041425 .15106449E-02 .35999984E+03 .31110058E+06 .94627297E+00
 20.39 625 .86695869E+00 .20940442E+08 .91145875E-04 .277766616E+00
 .83964901E+01 .17772490E+04 0. 0.
 .91772245E+03 .16490276E+00 --.55408289E+00
 7.

TSEC = 83.916425 T = 1.398607 H = .007913 NSTEP = 301

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

-.377394742125E+07
 .206811551825E+08
 .493311155605E+05

-.198734950895E+04
 .252981478822E+04
 .21248307985E+04

-.982785276440E+01
 .56860752852E+02
 .668531214065E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.190506E+01 5.727514E+00 -3.138666E+01 -7.520497E-02 -3.190506E+01 -3.003464E-04 -2.128450E-04

ATMOSPHERIC 1.379395E+01 1.861784E-01 -1.089365E+00 -8.254415E-01 -1.107023E+00 -6.641848E-01 -4.858907E-01

THRUST 1.132224E+02 -1.574158E+01 8.933608E+01 6.775377E+01 9.786935E+01 5.473739E+01 3.958199E+01

TOTAL 8.831190E+01 -9.627853E+00 5.686035E+01 6.685312E+01 5.785727E+01 5.41293E+01 3.901509E+01

STAGE T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, RA ISP, M, COAM, CLAW XI, MR, MP, WY

NO. 4 1.398607 .56995094E+05 .13529935E+07 .29120340E+03 -.13903212E+00

GRAVITY TURN 83.916425 .38200033E-04 .35999780E+03 .19860058E+06 .78903208E+00

67.265625 .35906091E+01 .21022733E+08 .17803128E-03 .59841328E+00

.18530648E+00 .30549163E+04 . . . 0.

.35501050E+04 .23615894E+00 . . . -.30602977E+00

STEP DOUBLED T = 1.429857 H = .015625 NSTEP = 304

TSEC = 11'.000000 T = 1.833333 H = .015625 NSTEP = 33^

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

--.382962956769E+17 --.230522033241E+04 --.152285317936E+12
 .207693535782E+18 .436610387306E+04 .878655526931E+02
 .1320 11674266E+16 .441316756336E+04 .112924426454E+03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.161173E+01 5.732095E+00 -3.109706E+01 -1.983311E-01 -3.161173E+01 -7.155289E-04 -2.408080E-04
 ATMOSPHERIC 1.096775E-01 1.343257E-02 -7.891688E-02 -7.497224E-02 -8.051137E-02 -7.022966E-02 -2.479635E-02
 'RUST 1.655963E+02 -2.097406E+01 1.193315E+02 1.131977E+02 1.215666E+02 1.062614E+02 3.677242E+01
 TOTAL 1.438895E+02 -1.522853E+01 8.786955E+01 1.129244E+02 8.987438E+01 1.06195E+02 3.674738E+01

STAGE T, SI, STAU H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, W, CDAM, CLAW XI, MR, MP, MY

NO. 4 1.833333 .19414958E+06 .36051912E+01 .29165760E+03 --.12665776E+00
 GRAVITY TURN 110.00.000 .65685542E-06 .35999448E+03 .13600000E+06 .71880538E+00
 93.349200 .61184691E+01 .21119885E+08 .24902211E-07 .68357636E+01
 .36276746E-02 .66221561E+04 0. 0. 19060100E+00
 .64560562E+04 .24337381E+09 0.

*** POWERED FLIGHT
 * * * * *
 SEG18 ENTRY TIME IS 13.50200
 * * * * * ECI * * * * *

I/SEC = 11.00000 T = 1.83333 H = .001953 NSTEP = 330

X,Y,Z X0,Y0,Z0 XDD,YDD,ZDD
 --.382962556769E+17 --.230522033241E+14 --.332830650638E+00
 .207693535792E+18 .436610387306E+04 .332979489901E+01
 .132001167426E+16 .641316756336E+04 .325318098148E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.161173E+01 5.732195E+00 -3.108706E+01 -1.983311E-01 -3.161173E+01 -7.155289E-04 -2.408005E-04
 ATMOSPHERIC 1.096775E-01 1.343257E-02 -7.891688E-02 -7.497224E-02 -8.051137E-02 -7.022966E-02 -2.479635E-02
 THRUST 4.799042E+01 -6.078358E+00 3.449577E+01 3.280511E+01 3.523045E+01 3.079494E+01 1.065678E+01
 TOTAL 3.270347E+01 -3.328307E-01 3.329795E+00 3.253181E+01 3.538209E+00 3.072400E+01 1.063174E+01

STAGE NO. 5
 CONSTANT
 T,ST,STAU 1.83333
 110.00000
 0.00000
 H,RHO,MACH,P,VA 19414958E+06
 .65685542E-06
 .61184691E+01
 .36276746E-02
 .64560562E+04
 LAT, LONG, R, V, AA 36051912E+00
 .35999448E+03
 .21119885E+08
 .66221561E+04
 .24337381E+00
 ISP, M, CDAM, CLAW 53994207E+02
 .13600000E+06
 .24902211E-03
 0.
 0.
 0.
 XI, WR, MP, MY -12665776E+00
 .71860538E+00
 .68357636E+00

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TSEC = 11.600000 T = 1.843333 H = .01953 NSTEP = 336

X, Y, Z X0, Y0, Z0 X00, Y00, Z00
 -.3831 1276599E+07 -.230545103455E+04 -.43673 857491E+04
 .20719738754E+08 .436827993374E+04 .3926892555161E+01
 .134654956746E+06 .443285237602E+04 .330972257944E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.160320E+01 5.731847E+00 -3.107044E+01 -2.022339E-01 -3.160320E+01 -7.273982E-04 -2.436814E-01
 ATMOSPHERIC 1.006490E-01 1.229866E-02 -7.229698E-02 -6.894616E-02 -7.375664E-01 -6.460791E-02 -2.271563E-02
 THRUST 4.875982E+01 -6.180376E+00 3.507758E+01 3.335841E+01 3.982877E+01 3.132467E+01 1.779313E+01
 TOTAL 3.332230E+01 -4.367309E-01 3.926883E+00 3.308723E+01 4.151911E+00 3.125926E+01 1.077017E+01

STAGE NO. 5 T, ST, STAL H, RHO, MACH, P, VA LA, L, CNG, R, V, AA ISP, W, CDAM, CLAM XI, WR, WP, WY
 1.843333 .19619408E+06 .36771767E+00 .53994927E+02 -.12665776E+00
 CONSTANT 110.600000 .59038429E-06 .35999437E+03 .13374580E+05 .7180538E+00
 .61531690E+01 .21122729E+08 .25306629E-03 .6835636E+00
 .32390035E-02 .66368030E+04 0. 0.
 .64711691E+04 .27092423E+00 0. 0.

12

*** FREE FLIGHT ***

 SEG18 ENTRY TIME IS 13.56630

TSEC = 11.60000 T = 1.843333 H = .00244 NSTEP = 336

	X,Y,Z	XD,YD,ZD	XDD,YDD,ZDD
	- .38311276599E+17	- .230545103455E+04	.574411546184E+01
	.207719738754E+18	.4368279933374E+14	- .311505933932E+02
	.134674956746E+16	.443285237612E+14	- .27118070631E+19

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.160320E+01	5.731847E+09	-3.107841E+01	-2.022339E-01	-3.150321E+11	-7.273952E-04	-2.436814E-04	
ATMOSPHERIC	1.006490E-01	1.229866E-02	-7.223688E-02	-6.894616E-02	-7.375864E-02	-6.46791E-02	-2.271563E-02	
TOTAL	3.167703E+01	5.744155E+09	-3.115069E+01	-2.711800E-01	-3.157695E+11	-5.533531E-02	-2.295931E-02	

STAGE NO. 6	T, ST, STAU	M, RHO, MACH, P, VA	LAT, LONG, R, V, AA	ISP, W, CDAM, CLAM	XI, WR, WP, MY
	1.843333	.19699498E+06	.36771767E+00	?	-.12665776E+00
FREE FLIGHT	110.87000	.59038429E-06	.35999437E+03	.13374580E+06	.71809539E+00
	C. C. JCC	.61531680E+01	.21122729E+19	.25306629E+03	.68357636E+00
		.32390095E-02	.66368030E+14	?	?
		.64711631E+04	.27092423E+11	?	?

STEP DOUBLED	T = 1.849681	H = .007488	NSTEP = 361
STEP DOUBLED	T = 1.857982	H = .0071977	NSTEP = 377

REFERENCE
SECTION

DESCRIPTION

ITEM

- 12 Free flight. This notation indicates that the vehicle is not thrusting; its acceleration is caused by external bodies only. When the vehicle is thrusting, i.e., when ISP and WD are nonzero, it is considered to be in powered flight

TSEC = 112.000000 T = 1.866667 H = .000977 NSTEP = 386

X, Y, Z X0, Y0, Z0 XCD, YDC, ZDD

-.383423476890E+07
 .207789589512E+08
 .140863665853E+06

-.229741172949E+04
 .432469532185E+04
 .443247766411E+04

.574073159275E+01
 -.311139471337E+02
 -.264903787812E+00

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRAC<

GEOPOTENTIAL 3.158340E+01 5.731280E+00 3.105832E+01 -2.113492E-01 -3.154343E+01 -7.543195E-04 -2.527056E-0-

ATMOSPHERIC 7.779577E-02 9.451416E-03 5.563053E-02 -5.355461E-02 -5.677779E-02 -5.015867E-02 -1.765153E-02

TOTAL 3.164323E+01 5.740732E+00 3.111395E+01 -2.649038E-01 -3.164019E+01 -5.092292E-02 -1.790423E-02

STAGE T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, CDAM, CLAY XI, WR, WP, MY

NO. 6 1.866667 .20360331E+06 .38454428E+08 0. .12665776E+00

FREE FLIGHT 112.000000 .46115832E+06 .35999412E+08 .13374580E+05 .71880538E+00

1.400000 .51815487E+01 .21129338E+08 .25294121E-02 .68357636E+00

.24818540E-02 .66051456E+04 0. 0. 0.

.84388106E+04 .45772102E+08 0. 0. 0.

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.70800

TSEC = 112.00000 T = 1.866667 H = .00122 NSTEP = 386
 X,Y,Z X0,Y0,Z0 A00,Y00,Z00

-.383423476890E+07
 .207780589512E+08
 .140963685853E+06
 -.229741172949E+04
 .432469532185E+04
 .443247766411E+04
 -.219675022102E+01
 .139324201798E+02
 .425736149216E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.154347E+01 5.731281E+00 -3.105832E+01 -2.113492E-01 -3.159347E+01 -7.503195E-04 -2.927058E-04
 ATMOSPHERIC 9.009705E-02 1.054591E-02 -6.442698E-02 -6.202281E-02 -6.575565E-02 -5.810139E-02 -2.044263E-02
 THRUST 6.268062E+01 -7.538986E+00 +.505516E+01 4.284699E+01 4.673247E+01 4.022043E+01 1.386341E+01
 TOTAL 4.434920E+01 -2.596764E+00 1.393242E+01 4.257361E+01 1.438323E+01 4.016159E+01 1.3864271E+01

STAGE NO. 7
 CONSTANT

T,ST,STAU H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,W,COAM,CLAW XI,WR,WP,WY
 1.866667 112.000000 0.000000 20360331E+06 .38454428E+00 .29998015E+03 -.12665776E+00
 0.000000 0.000000 .61115832E-06 .35999412E+03 .11548500E+06 .71880538E+00
 .24818540E-02 .21129338E+08 .29293695E-03 0. .60357636E+00
 .64388106E+04 .66051456E+04 0. 0. 0.

STEP DOUBLED T = 1.869840 H = .000244 NSTEP = 411
 STEP DOUBLED T = 1.873991 H = .000488 NSTEP = 427
 STEP DOUBLED T = 1.882292 H = .000977 NSTEP = 443
 STEP DOUBLED T = 1.898893 H = .001953 NSTEP = 459
 STEP DOUBLED T = 1.932096 H = .003906 NSTEP = 475

TSEC = 118.563906 T = 1.975965 H = .003976 NSTEP = 486

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

-.384922582343E+07
 .218764958677E+08
 .17062656257E+06
 -.231285933147E+04
 .442215320756E+04
 .471544839794E+04
 -.255743145381E+01
 .60586177275E+02
 .444626616191E+02

FORCES
 MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.149106E+01 5.728487E+00 -3.095460E+01 -2.548245E-01 -3.14916E+01 -8.87133E-04 -2.789860E-04
 ATMOSPHERIC 3.031712E+02 3.596350E-03 -2.125757E-02 -2.131455E-02 -2.172825E-02 -2.06839E-02 -6.653651E-07
 THRUST 6.544814E+01 -8.289515E+00 4.704447E+01 4.473881E+01 4.312664E+01 4.218989E+01 1.368571E+01
 TOTAL 4.734288E+01 -2.557431E+00 1.605862E+01 4.446266E+01 1.661385E+01 4.215893E+01 1.367877E+01

STAGE NO. 7
 T, ST, STAU 1.975965
 118.563906
 6.503906
 H, RHO, MACH, P, VA
 .23451026E+06
 .13888424E-06
 .69724422E+01
 .63747380E-03
 .67071013E+04
 LAT, LONG, R, V, AA
 .46506004E+00
 .35999289E+03
 .21160244E+00
 .6865829E+04
 .15741246E+01
 ISP, M, CDAM, CLAM
 .29999490E+03
 .11060757E+06
 .30164087E-03
 ?
 XI, WR, WP, MY
 -.12665776E+00
 .71887538E+00
 .68357636E+00
 0.
 0.
 0.

* STEP DOUBLED T = 1.998503 H = .007813 NSTEP = 491
 * STEP DOUBLED T = 2.568815 H = .01625 NSTEP = 563
 * STEP DOUBLED T = 2.831315 H = .03250 NSTEP = 582

TSEC = 18.378906 T = 3.006315 H = .031250 NSTEP = 586

X,Y,Z X0,Y0,Z0 X00,Y00,Z00

-.403011248067E+37
 .211276732021E+38
 .562590189677E+36

-.262491720264E+04
 .631051391112E+04
 .827314231983E+04

-.861493221508E+01
 .511206184033E+02
 .762797813285E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.047258E+01 5.666731E+00 -2.993037E+01 -7.995558E-01 -3.047255E+01 -2.527709E-03 -4.387555E-04

ATMOSPHERIC 1.035905E-36 1.055633E-07 -6.427877E-37 -8.054691E-07 -6.729490E-07 -7.738346E-07 -1.504130E-09

THRUST 1.127579E+02 -1.428166E+01 8.105899E+01 7.707864E+01 8.428078E+01 7.361773E+01 1.383926E+01

TOTAL 9.222816E+01 -8.614932E+00 5.112762E+01 7.627908E+01 5.390820E+01 7.361520E+01 1.383882E+01

STAGE NO. 7

CONSTANT 180.378906 68.378906

T,ST,STAU 3.006315 180.378906 68.378906

H,RHO,MACH,P,VA .58467941E+08 .12012368E-11 .12036283E+02 .32685824E-07 .19640072E+05

MAT, LONG,R,V,AA .15088004E+01 .35997403E+03 .21510369E+08 .10731154E+05 .79260581E+01

ISP,W,CDAM,CLAW .37000000E+03 .64200823E+03 .47351420E-03 0.

X,WR,WP,WY -.12665776E+00 -.71880538E+00 .68357606E+00 0.
 0.
 0.

TSEC = 247.00000 T = 4.116667 H = .031259 NSTEP = S22
 X,Y,Z X0,Y0,Z0 X00,Y00,Z00
 -.4209E+07 2756395E+07 -.409506972969E+04 -.58982E+02 216885E+02
 .217466698666E+08 .148220688719E+05 .148220688719E+05 .337494301321E+03
 .13622961196E+07 .101294576360E+05 .101294576360E+05 .345867499614E+03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 2.8626J7E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.962607E+01 -5.154654E-03 -3.617778E-04
 ATMOSPHERIC 3.040219E-07 3.212708E-08 -1.936998E-07 -2.321154E-07 -2.101540E-07 -2.167214E-07 -2.962929E-08
 THRUST 5.085458E+02 -6.441128E+01 3.655455E+02 3.476299E+02 3.917646E+02 3.229610E+02 2.490610E+01
 TOTAL 4.868322E+02 -5.698232E+01 3.374943E+02 3.457075E+02 3.631385E+02 3.223558E+02 2.830574E+01

STAGE NO. 7
 CONSTANT 247.000000
 135.000000
 T,ST,STAL 4.116667
 H,RHO,MACH,P,VA .12666332E+07
 .15694309E-13
 .26861893E+02
 .7121247E-09
 .23745743E+05
 LAT, LONG, R, V, AA .35430573E+01
 .35992879E+03
 .22192103E+08
 .23772689E+05
 .66601955E+01
 ISP, H, CDAM, CLAW .31000000E+03
 .14235007E+05
 .21355813E-02
 0.
 XI, NR, MP, MY -.12665776E+00
 .71889538E+00
 .68357636E+00
 0.
 0.

*** FREE FLIGHT

 SEG18 ENTRY TIME IS 14.19900

 ECI *****

TSEC = 247.00000 T = 4.116667 H = .003906 NSTEP = 622

X, Y, Z X0, Y0, Z0 X00, Y00, Z00
 - .4209 2756395E+07 - .409508972969E+04 .542925433743E+01
 .217466698666E+08 .148220688719E+05 -.280511831564E+02
 .138229621196E+07 .181294576360E+05 -.176241280538E+01

FORCES
 GEOPOTENTIAL 2.862607E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.962607E+01 -5.154654E-03 -3.617778E-04
 ATMOSPHERIC 2.704845E-07 2.158307E-08 -1.723323E-07 -2.065102E-07 -1.969714E-07 -1.945937E-07 -1.835362E-08
 TOTAL 2.862607E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.962607E+01 -5.154654E-03 -3.617778E-04

STAGE NO. 8	T, ST, STAU	H, RHO, MACH, P, VA	LAT, LONG, R, V, AA	ISP, M, CDAM, CLAW	XI, HR, MP, MY
FREE FLIGHT	4.116667 247.000000 6.000000	.12666302E+07 .15694309E-13 .26861883E+02 .71212477E-09 .23745743E+05	.35430573E+01 .35992879E+03 .22192103E+08 .23772689E+05 .66601955E+01	.007613 .015625 .031250 .062500 .125000	.12665776E+00 .71860538E+00 .68357636E+00 0. 0. 0.

STEP	DOUBLED	T =	H =	NSTEP
*	DOUBLED	4.218229	H =	647
*	DOUBLED	4.351042	H =	663
*	DOUBLED	4.616667	H =	679
*	DOUBLED	5.147917	H =	695
*	DOUBLED	6.210417	H =	711

TSEC = 455.12500 T = 7.585417 H = .125000 NSTEP = 722

X, Y, Z X0, Y0, Z0 X00, Y00, Z00
 -.45277400816E+07
 .24286764386E+08
 .507374050676E+07
 -.309059255393E+04
 .976697315619E+04
 .174450958375E+05
 .431202169556E+01
 -.211394267967E+02
 -.44272917503E+01

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 2.22428E+01 4.312022E+00 -2.113943E+01 -4.427209E+00 -2.202428E+01 -9.645462E-03 -6.098423E-04
 ATMOSPHERIC 1.450350E-11 9.470552E-13 -7.266496E-12 -1.251610E-11 -9.571156E-12 -1.073079E-11 -1.293165E-12
 TOTAL 2.202428E+01 4.312022E+00 -2.113943E+01 -4.427209E+00 -2.202428E+01 -9.645462E-03 -6.098423E-04

STAGE NO. 8 T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, COAM, CLAM XI, WR, WP, MY
 7.585417 .43718419E+07 .11647006E+02 0. - .12665776E+00
 455.125000 .11611533E-17 .35963422E+03 .10000000E+02 .71880538E+00
 208.125000 .22867990E+02 .25294744E+08 .19000000E-02 .68357636E+00
 .14622127E-13 .20230593E+05 0. 0.
 .20215166E+05 .16602444E+02 0. 0.

* * STEP DOUBLED T = 8.335417 H = .250000 NSTEP = 727
 * * STEP DOUBLED T = 16.585417 H = .500000 NSTEP = 759

TSEC = 2895.12500 T = 48.095417 H = .501100 NSTEP = 822

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

-.4032 9077577E+07 .321067992127E+04 .233621780400E+01
 .114713387665E+08 -.156926695027E+05 -.660601992485E+01
 .262898693199E+08 -.343549883446E+04 -.15258368317E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 1.679333E+01 2.336218E+00 -6.606020E+00 -1.525837E+01 -1.679033E+01 -1.063766E-02 -1.807568E-07
 ATMOSPHERIC 2.093489E-14 -5.170835E-15 1.969874E-14 4.394857E-15 1.247432E-14 -1.665074E-14 -1.112176E-15
 TOTAL 1.679333E+01 2.336218E+00 -6.606020E+00 -1.525837E+01 -1.679033E+01 -1.063766E-02 -1.807568E-07

STAGE NO. 8 T, ST, STAU H, RHO, MACH, P, VA LAT, LONG, R, V, PA ISP, M, CDAM, CLAW XI, MR, MP, MY

FREE FLIGHT 48.095417 .90701690E+07 .65443395E+02 0. - .12665776E+00
 2885.125000 .25697565E-20 .35742859E+03 .10000000E+05 .71889538E+00
 2638.125000 .18424087E+02 .28937958E+08 .19000000E-02 .68357636E+00
 .25564904E-15 .16382031E+05 0. 0.
 .16286782E+05 .14878560E+03 0. 0.

* STEP HALVED H = .031250 NSTEP = 843
 * STEP HALVED H = .001953 NSTEP = 851
 * STEP DOUBLED H = .003906 NSTEP = 875
 * STEP DOUBLED H = .007813 NSTEP = 891

TSEC = 3521.687500 T = 58.694792 H = .007813 NSTEP = 922

X,Y,Z X0,Y0,ZD XDD,YDD,ZDD

-.166732935561E+07
 .943211344875E+06
 .207907323820E+08
 -.140043390622E+03
 .396515264094E+03
 -.396445296446E+03
 .341867385106E+01
 -.769078914648E+01
 -.27282309426E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.219367E+01 2.562390E+00 -1.452622E+00 -3.205563E+01 -3.219067E+01 7.515197E-03 5.882027E-03
 ATMOSPHERIC 7.991473E+00 8.562898E-01 -6.239167E+00 4.773390E+00 4.402453E+00 -6.426181E+00 1.325098E+00
 TOTAL 2.855933E+01 3.418680E+00 -7.690789E+00 -2.728223E+01 -2.778822E+01 -6.419667E+00 1.330980E+00

STAGE T,ST,STAU H,RHO,MACH,P,VA LAT,ALONG,R,V,AA ISP,M,COAM,CLAW XI,WR,WP,WY
 NO. 8 58.694792 .22711804E+05 .84768075E+02 0. .12665777E+00
 FREE FLIGHT 3521.687500 .11549419E-02 .35743894E+02 .10000000E+03 .71889538E+00
 3274.687500 .63980809E+00 .20878888E+03 .93751835E-03 .68357636E+00
 .60269598E+01 .57793198E+03 0.
 .65624157E+03 .80313335E+02 0.
 0.

* STEP DOUBLED T = 58.905729 H = .015625 NSTEP = 948

*** CRASH *** ALTITUDE = -73.7 TIME = 59.26510

TSEC = 3555.90625C T = 59.265104 H = .015625 NSTEP = 971

X, Y, Z X0, Y0, Z0 X00, Y00, Z00
 -.167028474648E+J7
 .952864961547E+J6
 .297672681792E+J8
 -.445051684661E+02
 .469037333572E+02
 -.799623060046E+03
 .155265287701E+01
 -.837465445471E+01
 .60656.861740E+00

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.226082E+01 2.575318E+00 -1.469169E+00 -3.212428E+01 -3.226081E+01 9.535701E-03 1.316452E-03
 ATMOSPHERIC 3.346699E+01 -1.022455E+00 -6.905486E+00 3.273084E+01 3.235781E+01 -6.378252E+00 5.685078E+00
 TOTAL 8.538977E+00 1.552863E+00 -8.374654E+00 6.065609E-01 9.699672E-02 -6.368716E+00 5.687195E+00

STAGE T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, W, COAM, CLAW XI, WR, WP, WY
 NO. 8 59.265104 -.73664165E+02 .04744933E+02 0. 0. -12665776E+00
 FREE FLIGHT 3555.906250 .23820223E-02 .35445970E+02 .19000000E+05 .71880538E+00
 3398.90250 .73214290E+00 .20856188E+08 .13064915E-02 .68357636E+00
 .14735135E+02 .80223295E+03 0. 0.
 .81760725E+03 .12160724E+03 0. 0.

*** VEHICLE CRASHED

*** THIS CASE TOOK 2.008 SECONDS TO INTEGRATE A SPAN OF 59.2651 MINUTES ***

*** FROM 0.000 TO 59.265 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 14.9 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 2.0 CP SECS

*** CASE 1

*** STAGE NO. 1 POWERED FLIGHT.

*** EPOCH PRINT

DATE,...	ME, MN, ST, DT, ..	X, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	0.00000	-.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000
0/ 0	0.00000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.00000	0.00000	0.	0.	90.00000000	-.00000000	0.00000
IT	.01563	-.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
	0.00000	-.264798324E+03	.953505100E-05	.20925738E+08	.00000000	0.00000
	0.00000	-.134595352E-10	-.134595352E-10	.15255289E+04	180.00000000	0.00000
A =	.10481007E+08	MEAN ANOM =	.18000000E+03	APOGEE =	.34439336E+14	
E =	.99653893E+00	ECCENTRIC =	.18000000E+03	HEIGHT =	-.72759576E-14	
I =	.50538039E-12	TRUE ANOM =	.18000000E+03	PERIGEE =	.59701863E+11	
O =	.27999327E+03	KEPL PER =	.29947727E+02	HEIGHT =	-.34379634E+04	
U =	.36000000E+03	ANOM PER =	.29923367E+02	O-DOT =	-.23468143E+17	
TAU =	-.14973864E+02	NCOL PER =	-.80903654E+04	U-DCT =	.46936206E+07	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000 DSC NODE
0/ 0	0.00000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.00000	0.00000	0.	0.	90.00000000	-.00000000	0.00000
IT	0.1563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
	0.00000	-.264798324E+03	.953505180E-05	.209257380E+08	.00000914	
	0.00000	-.134595352E-10	-.134595352E-10	.152552895E+04	180.00000000	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000
0/ 0	0.00000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.00000	0.00000	0.	0.	90.00000000	-.00000000	0.00000
IT	0.1563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
	0.00000	-.264798324E+03	.953505180E-05	.209257380E+08	.00000914	
	0.00000	-.134595352E-10	-.134595352E-10	.152552895E+04	180.00000000	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000 BETA =90
0/ 0	0.00000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.00000	0.00000	0.	0.	90.00000000	-.00000000	0.00000
IT	0.1563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
	0.00000	-.264798324E+03	.953505180E-05	.209257380E+08	.00000914	
	0.00000	-.134595352E-10	-.134595352E-10	.152552895E+04	180.00000000	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	0.1667	.364648055E+07	.219266463E+08	100.03505026	-.00000000	.50012 PRE-EVNT
0/ 0	0.1667	.236164967E+08	-.115198329E+01	-.00000000	350.99939712	0.00000
10.00000	1.00000	.648979044E-02	-.648979944E-02	83.00000000	.149+9128	0.00000
IT	0.1563	.153495604E+04	-.187008891E+03	90.00000000	-.00000000	0.00000
	0.00000	-.815050274E+02	-.319594589E+00	.209257380E+08	.00000914	
	0.00000	-.129721395E-02	-.129721395E-02	.153711845E+04	170.97909818	

** STAGE N02 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,Y,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	.16667	-364648055E+07	.209266463E+08	100.03505026	-00000002	.50012 PST-EVNT
0/ 0	.16667	.206064967E+08	-.105198329E+01	-.00000002	355.99999712	0.00000
10.00000	10.00000	-.648979944E-02	-.648979944E-02	83.00445863	.14949128	0.00000
IT	0.00000	-.153455604E+04	.187208891E+03	90.00004871	-.00000002	0.00000
	0.00000	-.815150274E+02	-.319594589E+00	.209266463E+08	.00004871	
	0.00000	-.129721395E-02	-.129721395E-02	.15371184E+04	175.97909915	

DATE,...	ME,MM,ST,DT,...	X,Y,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	.16088	-.364594764E+07	.209265825E+08	100.03359944	-00000010	1.00000 ASC NODE
0/ 0	.16088	.206064252E+08	-.944889931E+00	-.00000010	355.99999741	0.00000
9.65268	9.65268	-.380570178E-01	-.380570178E-01	83.26653377	.13899276	0.00000
IT	0.00000	-.153337424E+04	.180131102E+03	89.98966829	-.0000010	0.00000
	0.00000	-.884386592E+02	-.297220354E+00	.209265825E+08	.00468976	
	0.00000	.275116281E+00	.275116281E+00	.15362901E+04	.00127042	

** STAGE N03 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,Y,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	.18333	-.364801727E+07	.209268438E+08	100.03922736	-00000209	1.00002 PRE-EVNT
0/ 0	.18333	.206064253E+08	-.148552410E+01	-.00000209	355.99999615	0.00000
11.00000	11.00000	.759617574E+00	.759617574E+00	82.24440256	.18199226	0.00000
IT	0.00000	-.153848227E+04	.207779937E+03	89.91353307	.00000209	0.00000
	0.00000	-.61313300E+02	-.388646428E+00	.209268438E+08	.08649693	
	0.00000	.230317253E+01	.230317250E+01	.1539768E+04	.00127042	

DATE,...	ME,MM,ST,DT,...	X,Y,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	.27751	-.365676934E+07	.209283591E+08	100.06282704	-00024393	1.00008 PRE-EVNT
0/ 0	.27751	.206064129E+08	-.497880143E+01	-.00024393	355.999998637	0.00000
16.65080	16.65080	.885024035E+02	.885024035E+02	77.76944063	.43136952	0.00000
IT	0.00000	-.155951933E+04	.330671819E+03	88.91321737	.00024393	0.00000
	0.00000	-.59081819E+02	-.915797851E+00	.209283591E+08	1.08678265	
	0.00000	.299248459E+02	.299348450E+02	.15609066E+04	.00127042	

** STAGE N04 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XU'	X,XD - BF	ADBARV	LAT,...	RF	REV,...
71/ 1/ 1	.27751	-365676934E+07	.209283591E+08	100.06282704	.00024393		1.00008 PSI-EVNT
0/ 0	.27751	.236064129E+08	-.497880143E+01	.30024229	359.59938637		0.00000
16.65080	16.65080	.89502435E+02	.89502435E+02	77.76944063	.43136952		0.00000
IT	.00049	-.15551933E+04	.330671819E+03	88.91321737	.00024393		0.00000
	.00000	.590891819E+02	-.915797851E+00	.21928359E+08	1.08678265		
	.00000	.299348458E+02	.239348450E+02	.15609766E+04	359.98731403		

** STAGE N05 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	RF	REV,...
71/ 1/ 1	1.83333	-.382962957E+07	.211194722E+08	100.44733648	.36051912		1.00152 PRE-EVNT
0/ 1	1.83333	.207693536E+08	-.203619817E+04	.35810607	359.99447592		0.00000
50.00000	11.00000	.132001167E+06	.132001167E+06	44.39255546	31.95291160		0.00000
IT	.00000	-.23052233E+04	.471172581E+04	18.60042295	.360-9673		0.00000
	.00000	.36610387E+04	-.652191264E+02	.21119885E+08	71.39995367		
	.00000	.441316756E+04	.441316756E+04	.66221561E+04	359.87395794		

** STAGE N06 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	RF	REV,...
71/ 1/ 1	1.84333	-.383010277E+07	.211222999E+08	100.44973745	.36771767		1.00154 PRE-EVNT
0/ 1	1.84333	.207719735E+08	-.207550356E+04	.36525644	359.99477005		0.00000
50.60000	11.60000	.134654957E+06	.134654957E+06	44.39599709	32.4215625		0.00000
IT	.00195	-.23054513E+04	.471396926E+04	18.52105861	.36769451		0.00000
	.00000	.366827993E+04	-.65799504E+02	.21122729E+08	71.47933142		
	.00000	.443285238E+04	.443285238E+04	.66368030E+04	359.87210867		

** STAGE NO6 FREE FLIGHT

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	1.84333	.393111277E+07	.211222999E+08	100.44973745	.36771767	1.00154 PST-EVNT
0/ 1	1.84333	.207719739E+08	-.207550356E+04	.36525644	359.99437905	0.00000
50.60700	110.60000	.134454957E+06	.134654957E+06	44.39593709	32.42115525	0.00000
IT	0.0024	-.236545103E+04	.471396926E+04	18.52105861	.36769451	0.00000
	0.00000	.436827993E+04	-.657995004E+02	.21122729E+08	71.47933142	
	0.00000	.443285238E+04	.443285238E+04	.66368030E+04	359.8720567	

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	1.86667	-.382423477E+07	.211288685E+08	100.45533699	.38454428	1.00156 PRE-EVNT
0/ 1	1.86667	.297780590E+08	-.216829048E+04	.38197044	359.99412018	0.00000
52.00000	112.00000	.140860686E+06	.140860686E+06	44.64680220	33.50879573	0.00000
IT	0.0098	-.229741173E+04	.466979315E+04	18.52144592	.38451526	0.00000
	0.00000	.432469532E+04	-.667517840E+02	.21129338E+08	71.47898762	
	0.00000	.443247766E+04	.443247766E+04	.66051456E+04	359.86615682	

** STAGE NO7 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	Y, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	1.86667	-.385523477E+07	.211288685E+08	100.45533689	.38454428	1.00156 PST-EVNT
0/ 1	1.86667	.297780590E+08	-.216829048E+04	.38197044	359.99412018	0.00000
52.00000	112.00000	.140860686E+06	.140860686E+06	44.64680220	33.50879573	0.00000
IT	0.0012	-.229741173E+04	.466979315E+04	18.52144592	.38451926	0.00000
	0.00000	.432469532E+04	-.667517840E+02	.21129338E+08	71.47898762	
	0.00000	.443247766E+04	.443247766E+04	.66051456E+04	359.86615682	

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	2.50926	-.392502172E+07	.213229035E+08	100.60722986	.93736644	1.00304 ALTITUDE
0/ 2	2.50926	.29985412E+08	-.56098777E+04	.93076557	359.98432596	0.00000
30.55537	15.55537	.346419427E+06	.346419427E+06	48.79672439	65.83132101	0.00000
IT	0.00781	-.242912805E+04	.549683473E+04	13.03154002	.93691791	0.00080
	0.00000	.513751169E+04	-.114406799E+03	.21322719E+08	77.06326925	
	0.00000	.532016311E+04	.632016311E+04	.84993614E+04	359.77118465	

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT, .. BF	REV, ...
71/ 1/ 1	2.11667	-.421902756E+07	.221502326E+08	100.95434915	.54365730	1.01010 PRE-EVNT
0/ 4	2.11667	.217666999E+08	-.275284719E+05	3.51943193	359.92873242	0.00000
7.00000	247.00000	.136229621E+07	.136229621E+07	46.3324252	208.46032340	0.00000
IT	0.3125	-.09508973E+04	.153296421E+05	4.01470358	3.54169824	0.00000
	0.00000	.148221689E+05	-.430311423E+03	.22192103E+08	65.99298726	
	0.00000	.181294576E+05	.181294576E+05	.23772689E+05	359.68194179	

** STAGE NO8 FREE FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	4.11667	-.420902756E+07	.221502326E+08	100.95494915	3.54305730	1.00100 PS1-EVNT
0/ 4	4.11667	.217466699E+08	-.275284719E+05	3.51947193	355.9289242	0.00000
7.00000	247.00000	.136229621E+07	.136229621E+07	46.33324252	208.46852340	0.00000
IT	0.00000	-.99508973E+04	.153296421E+05	4.91471358	3.54159824	0.00000
	0.00000	.148226689E+05	-.430311423E+03	.221921035+08	85.3928826	
	0.00000	.181294576E+05	.191294576E+05	.23772689E+05	353.68194109	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	1.00000	-.535725302E+07	.250410757E+08	101.87111104	16.27262178	1.04520
0/10	1.00000	.254656666E+08	-.285898245E+06	16.16941149	355.37039410	0.00000
0.00000	60.00000	.755101321E+07	.755101321E+07	50.30394244	1019.56372963	0.00000
IT	0.00000	-.250593693E+04	.730032520E+04	4.17329854	16.24813785	0.00000
	0.00000	.694337280E+04	-.955244985E+03	.271152575+08	86.00253432	
	0.00000	.167316140E+05	.167316140E+05	.18287620E+05	358.20997309	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	20.00000	-.626639554E+07	.276216554E+08	103.10523879	31.01306034	1.08606
0/20	20.00000	.269170814E+08	-.917136080E+06	30.84341104	355.09927732	0.00000
0.00000	120.00000	.165032787E+08	.165032787E+08	65.13077807	1856.80055099	0.00000
IT	0.00000	-.631813950E+03	-.137313681E+04	4.67150321	30.95377740	0.00000
	0.00000	-.152293522E+04	-.100535374E+04	.321893655+08	85.98811216	
	0.00000	.129543823E+05	.129543823E+05	.13059101E+05	359.69736548	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	30.00000	-.620301387E+07	.248964075E+08	104.40571346	42.81896468	1.11891
0/30	30.00000	.241491464E+08	-.135186798E+07	42.62707544	356.89190746	0.00000
0.00000	180.00000	.229489003E+08	.229489000E+08	88.80033478	2138.41488247	0.00000
IT	0.00000	.897797859E+03	-.744067525E+04	5.45554743	42.74530274	0.00000
	0.00000	-.744407440E+04	-.345639678E+03	.33886733E+08	85.97824063	
	0.00000	.839962769E+04	.839962769E+04	.11252579E+05	353.18151679	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	30.46080	-.617882377E+07	.246872878E+08	104.47423928	43.34255508	1.12037 BETA =90
0/30	30.46080	.239400040E+08	-.136080566E+07	43.15051870	356.84491671	0.00000
27.64828	1827.64828	.231795030E+08	.231795030E+08	89.99999998	2139.0569986	0.00000
IT	0.00000	.869667865E+03	-.768607748E+04	5.50227972	43.26388890	0.00000
	0.00000	-.768434860E+04	-.301786151E+03	.33889990E+08	85.90722200	
	0.00000	.816887289E+04	.816887289E+04	.11248823E+05	352.99876142	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	40.0000	- .532247715E+07	.169215416E+08	106.30196664	54.46367021	1.15147
0/43	4.0000	.18193311E+08	-.122979671E+07	54.28147881	356.28131009	0.00000
0.00000	2400.0000	.263696781E+08	-.123394318E+05	113.01680978	1909.07518547	0.00000
IT	0.0000	.212152567E+04	.825788879E+03	6.88478785	54.39869198	0.00000
	.0.0000	.122645884E+05	.275350575E+04	.32475179E+08	85.97384661	
	.0.0000	.275350575E+04		.12747658E+05	350.66392397	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	57.33000	-.364770982E+07	.102241106E+08	110.89338712	68.49908177	1.19104
0/50	50.0000	.955571695E+07	-.291676494E+06	68.36754050	358.36549204	0.00000
0.00000	3000.0000	.257909635E+08	.257909635E+08	128.77783877	1132.30783299	0.00000
IT	50000	.348247104E+04	-.165352809E+05	16.94809311	68.46658268	0.00000
	0.0000	-.164337566E+05	.233391386E+04	.27745113E+08	85.97558601	
	.0.0000	.228348324E+04	-.528348324E+04	.17609973E+05	348.147633412	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	57.73839	-.176316903E+07	.194796138E+07	142.80980743	84.06308754	1.23782
0/57	57.73839	.133784248E+07	.105073019E+07	84.82337916	28.342+1.935	0.00000
44.30322	3464.36322	.211408933E+08	-.211408933E+08	133.94875247	65.839F5548	0.00000
IT	50000	.465090148E+04	-.188284286E+05	42.27186987	84.06234386	0.00000
	0.0000	-.186539368E+05	.335071274E+04	.21256394E+08	85.07660146	
	0.0000	.157932975E+05	-.157932975E+05	.24880283E+15	306.132+2.812	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	71.52121	-.532405122E+16	.198675710E+17	104.41408869	40.82340990	1.11341
1/40	71.52121	.195474318E+17	-.355285070E+16	40.633314898	349.86113391	0.00000
31.27278	4231.27278	.173189692E+17	.173189692E+17	.00001183*320587	53125F0	0.00000
IT	0.0000	.337717893E+14	.133550268E+15	1.58747422	40.63314818	0.00000
	0.0000	.131398287E+15	-.238824198E+14	.26594922E+17	41.77011922	
	.0.0000	.116418961E+15	.116418961E+15	.17877171E+15	275.96732891	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	58.49359	-.166539023E+07	.154898731E+07	150.56035928	84.78039672	1.24073
0/58	58.49359	.939917806E+06	.112143072E+07	84.74542953	35.90365360	0.00000
29.61531	3509.61531	.20733952E+08	.207933952E+08	89.59999768	4.10932927	0.00000
IT	0.0000	.181513069E+02	.592691162E+03	219.68206520	84.78035423	0.00000
	0.0000	.478851345E+03	-.147758025E+03	.21881146E+08	93.34636740	
	0.0000	.361831513E+02	-.361831513E+02	.51337591E+03	176.42546380	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,...	REV,...
71/ 1/ 1	59.26355	-.167028059E+07	.156655643E+07	150.29613526	84.74496754	1.24061
0/59	59.26355	.952860555E+06	.111520467E+07	84.70175662	35.44641190	0.00000
15.81307	3555.81307	.207673427E+08	.207673427E+08	170.15119798	-.00000000	0.00000
IT	0.0000	.446501753E+02	.143355999E+03	188.08189942	84.74496659	0.00000
	0.0000	.76852404E+02	-.937581765E+02	.20856181E+08	90.72249595	
	0.0000	.799678312E+03	-.799678312E+03	.80234215E+03	207.61895725	

DATE,...	ME,MM,ST,OT,...	X,XO	X,XO - BF	A0BARV	LAT,.. BF	REV,...
71/ 1/ 1	59.26510	-.167028475E+07	.156656975E+07	150.29609254	84.74493305	1.24061 PRE-EVNT
0/59	59.26510	.952864962E+06	.111519594E+07	84.70972190	35.44536989	0.00000
15.90625	3555.90625	.207672682E+08	.207672682E+08	170.19291151	-.01212356	0.00000
IT	.01563	-.445151685E+02	.142585416E+03	187.86028726	84.74493322	0.00000
	0.00000	.469037336E+02	-.935627250E+02	.20856108E+08	90.72247930	
	0.00000	-.799623060E+03	-.799623060E+03	.802232995E+03	207.61874875	

** VEHICLE CRASHED

DATE,...	ME,MM,ST,OT,...	X,XO	X,XO - BF	A0BARV	LAT,.. BF	REV,...
71/ 1/ 1	59.26510	-.167028475E+07	.156656975E+07	150.29609254	84.74493305	1.24061 PRE-EVNT
0/59	59.26510	.952864962E+06	.111519594E+07	84.70972190	35.44596993	0.00000
15.90625	3555.90625	.207672682E+08	.207672682E+08	170.19291151	-.01212356	0.00000
IT	.01563	-.445051685E+02	.142585416E+03	187.86028726	84.74493322	0.00000
	0.00000	.469037336E+02	-.935627250E+02	.20856108E+08	90.72247930	
	0.00000	-.799623060E+03	-.799623060E+03	.802232995E+03	207.61874875	

A =	.10433128E+03	MEAN ANOM =	.184939510E+03	APOGEE =	.34340636E+04
E =	.93997235E+00	ECCENTRIC =	.18246567E+03	HEIGHT =	.15781792E+01
I =	.90722479E+02	TRUE ANOM =	.18000917E+03	PERIGEE =	.47475385E-1
O =	.32246886E+03	KEPL PER =	.29742324E+02	HEIGHT =	-.34324379E+14
U =	.27523168E+03	ANOM PER =	.29790353E+02	U-00T =	.46957538E+09
TAU =	.43986596E+02	NCOL PER =	.31748549E+08	U-00T =	-.18605385E+11

*** END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 15.3 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .4 CP SECS.

MODEL DATA
 H SCF MODEL
 #INFORM1

0	02,0	-1.0827E-3
0	03,0	2.676E-6
0	04,0	1.4E-6
0	05,0	2.8E-8
0	06,0	-3.7E-7
0	07,0	5.93E-7
0	08,0	-7.0E-8
0	02,02	1.537069E-6
0	03,01	1.951856E-6
0	03,02	4.162717E-7
0	03,03	9.20555E-8
0	04,01	-5.344206E-7
0	04,02	9.32884E-8
0	04,03	5.056833E-8
0	04,04	-4.432373E-9
0	05,01	1.168464E-7
0	05,02	4.3475E-8
0	05,03	3.028423E-9
0	05,04	-3.801453E-9
0	05,05	-8.3892E-11
0	06,01	-2.746737E-13
0	06,02	-2.000628E-8
0	06,03	1.097921E-8
0	06,04	-1.158042E-9
0	06,05	-1.424538E-10
0	06,06	3.199373E-12
0	07,01	9.22074E-8
0	07,02	4.564422E-8
0	07,03	5.555012E-9
0	07,04	-2.9078E-10
0	07,05	-2.003164E-11
0	07,06	-3.1557E-11
0	07,07	1.625731E-12
0	08,01	-1.013559E-7
0	08,02	7.74717E-9
0	08,03	-5.548181E-10
0	08,04	-8.95364E-11
0	08,05	1.458971E-11

MTERMS04, 60

0.
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0.
0.
-7.73576E-7
2.30983E-7
-2.318633E-7
1.36433E-7
-4.181365E-7
9.90846E-8
4.233845E-10
4.033772E-9
-1.42087E-7
-5.451433E-8
3.45103E-9
-2.025287E-9
-1.648367E-9
7.8695E-8
-1.927374E-8
1.057274E-9
-1.922802E-9
-4.115213E-10
-5.391516E-11
6.81522E-8
6.000909E-9
-2.905979E-9
-2.030027E-15
-6.59091E-11
5.2549E-11
-2.675614E-12
-3.29912E-8
-3.09899E-9
2.184649E-9
4.924497E-11
-3.107689E-13

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6
 CARD 7
 CARD 8
 CARD 9
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 CARD 15
 CARD 16
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 CARD 31
 CARD 32
 CARD 33
 CARD 34
 CARD 35
 CARD 36
 CARD 37
 CARD 38
 CARD 39
 CARD 40

1
 CONT'D

REFERENCE
SECTION

ITEM

DESCRIPTION

1 Card images of the input MODEL data. Emphasis is given to the variables associated with an SLS run (MULTV=2), the others having been discussed earlier:

MULTV, LPACK	2.2.11
PANDR, PATA, GPLØT, SSPR, MVET	2.2.11.1
ELEDD, KEDIT, FEDIT, NEDIT	2.2.11.3
JSGLS	2.2.11.4
GMKM, ERKM, F, ØMEGE, ØMEGA, GSUBØ, FTNM,	2.1.1
FTKM, SLT, PI, DGREE	2.2.9
MSGLS, FREQ, CNTI, ISGLS, PSGLS	2.1.2.4.1
D1, D2	2.2.1
CLASS	2.2.5
LGT	2.1.4
UTD, LEMSP	2.2.2
ACØN, RCØN	

```

0 08,06 -6.224239E-13
0 08,07 0.65730E-13
0 08,08 -1.858297E-13
GKMH 398671.2 ERKM -6378.145
OMEGA .4375265088E-2 OMEGA .4375265088E-2
FTNM 6076.115486 FTNM 3280.839895
PI 3.1415926536 DGREE57.295779512
IPSGLS2 FREQ 1.779736E9
TISGLS0 IJSGLS6
PLANT0 CLASS1
IPAXIT5 ACON 0.
UTD 41.1579 PATA 3
MULTV2 DOP30X4001
01 7.18 02 -15.738
DFANDR XX DSSPR XX
GPLOT4 10
I2 2 13 3
SIGMA20 2 0
4 .1 ILPACK1
IMPVET 2 FEOTIS
NEDITS
END
    
```

```

1.058450E-11
-3.585277E-13
1.202444E-13
.3352891869E-2
FSUB0 .3208766404E+2
SLT 2620.105179
1.047197551216
CNT1 1040754.
IPSGLS2
ILGT -1
RCON 1.E-3
DITIN 2
LEMS#3
FLUX 0.
IKSIG 1
14 37
3 0
ELEDD0
KEDIT.5
    
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①

CARD 41
CARD 42
CARD 43
CARD 44
CARD 45
CARD 46
CARD 47
CARD 48
CARD 49
CARD 50
CARD 51
CARD 52
CARD 53
CARD 54
CARD 55
CARD 56
CARD 57
CARD 58
CARD 59
CARD 60
CARD 61
CARD 62

***** GRAVITY MODEL *****

GM = .5530417752E-02 ER**3/MIN**2 = .1407646853E+17 FT**3/SEC**2 = .390601200E+15 M**3/SEC**2

NO NORMALIZATION WITH 41 TERMS.

N	M	CMM	SNM	**	N	M	CNM	SNM
2	0	-.1082700E-02	0.	**	4	3	.50568230E-07	.42338450E-09
3	0	.2676000E-05	0.	**	5	3	.30264230E-08	.34510300E-00
4	0	.1400000E-05	0.	**	6	3	.10979210E-07	.10572740E-00
5	0	.2800000E-07	0.	**	7	3	.55550120E-08	-.29059790E-08
6	0	-.3700000E-06	0.	**	8	3	-.55481810E-09	.21846490E-08
7	0	.5930000E-06	0.	**	4	4	-.44323730E-08	.40337720E-08
8	0	-.7000000E-07	0.	**	5	4	-.24014530E-08	-.20252870E-08
3	1	.19918560E-05	.23094833E-06	**	6	4	-.11580420E-08	-.19228020E-08
4	1	-.53442880E-06	-.41813650E-06	**	7	4	-.29078000E-09	-.20300270E-14
5	1	.11684640E-06	-.14248870E-06	**	8	4	-.89537400E-10	.49244970E-10
6	1	-.2746237E-12	.7869500E-07	**	5	5	-.83992800E-10	-.16493670E-09
7	1	.9220740E-07	.68152200E-07	**	6	5	-.14245380E-09	-.41152130E-09
8	1	-.10135590E-06	-.32991200E-07	**	7	5	-.20031640E-10	-.65909100E-10
2	2	.15370680E-05	-.77367600E-06	**	8	5	.14589710E-10	-.3102690E-12
3	2	.4162717E-06	-.23186330E-06	**	6	6	.31993730E-11	-.53915160E-10
4	2	.9328843E-07	.95084660E-07	**	7	6	-.31557700E-10	.72599000E-10
5	2	.4347511E-07	-.5451433E-07	**	8	6	-.62242390E-12	.18584580E-10
6	2	-.20006280E-07	-.19273740E-07	**	7	7	.16257310E-11	-.26756140E-11
7	2	.45644220E-07	.60009190E-08	**	8	7	.86573800E-12	-.35852770E-12
8	2	.7747170E-08	-.30999090E-08	**	8	8	-.18582970E-12	.12024440E-12
3	3	.9205550E-07	.13640300E-06	**				

***** GENERAL PERTURBATIONS GRAVITY MODEL *****

GM = .553041774E-32 ER**3/MIN**2 = .1407646851E+17 FT**3/SEC**2 = .3986011994E+15 M**3/SEC**2

***** ZONAL HARMONICS *****

EJ2 = .1082549000E-02 EJ3 = -.2435000000E-05 EJ4 = -.1232000000E-05

***** PHYSICAL CONSTANTS *****

GM(ER**3/MIN**2)	=	.553041775E-02	OMEGA(RAD/MIN)	=	.437526909E-02	GMLAT(DEG)	=	.783000000E+02
GMM(KM**3/SEC**2)	=	.398601200E+06	OMEGA(RAD/MIN)	=	.437526909E-02	GMLNG(DEG)	=	.291000000E+03
SGM(ER**3/MIN**2)	=	.680232650E-04	OMEGA(RAD/MIN)	=	0.	AM(ER)	=	.272506277E+08
ERT(FT/ER)	=	.209256726E+08	ERKM(KM/ER)	=	.637014500E+04	ERNM(NM/ER)	=	.344392279E+04
FTM(FT/KM)	=	.328063589E+04	FTNM(FT/NM)	=	.607511549E+04	AE(ER)	=	.100000000E+01
GSUB0(FT/SEC**2)	=	.32876640E+02	DGREE(DEG)	=	.57257795E+02	SLT(ER/MIN)	=	.282018318E+04
CXEP	=	.10000000E-10	F	=	.335289187E-02	PI	=	.314159265E+01

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = .20925673E+08 VF(I/O-ER/MIN) = .34076121E+06 AF(I/O-ER/MIN**2) = .58126868E+04

***** INTEGRATION INPUTS *****

ICENT = 1 NSTEP = 2
 IR = 8 ER = .10000000E-09
 HMIN = .15625000E-01 HMAX = .64000000E+02 H0 = .10000000E+01

***** SPECIAL OPTIONS *****
 TAPEZ = 0 TAPE7 = C TELEMS = 0 PTAPE = 0 NPDOT = 0
 PRHD = 0 NODPR = 0 CLASS = 1 LEMSP = 3 PTNS = 1010"

***** CRASH ALTITUDE TABLE *****
 (IN FT)

ECI CRASH ALTITUDE = .300000000E+06 MCI CRASH ALTITUDE = .300000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
 (IN FT)

BODY(1) CRASH ALTITUDE = .300000000E+06 BODY(2) CRASH ALTITUDE = 0.
 BODY(3) CRASH ALTITUDE = .300000000E+04 BODY(4) CRASH ALTITUDE = 0.
 BODY(5) CRASH ALTITUDE = 0 BODY(6) CRASH ALTITUDE = 0.
 BODY(7) CRASH ALTITUDE = 0.

***** STATION LOCATIONS *****

STATION	SIG	REF	KA-RBF	DATUM	TYPE
313	-0	-0	-0	-0	-0
343	-0	-0	-0	-0	-0
353	-0	-0	-0	-0	-0
363	-0	-0	-0	-0	-0
377	-0	-0	-0	-0	-0
393	-0	-0	-0	-0	-0

X	Y	Z	HEIGHT	P	Q
LATITUDE	LONGITUDE	HEIGHT			
RADIUS	LATITUDE	LONGITUDE			

2

***** ATA INPUT *****

ATA	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	CARD	
6.64827257E+4	1.68260013E+4	4.72859549E+4	5.46561358E+3	5.75322855E+4	6.18612704E+1	1.11908631E+2	4.24344483E+1	6.18612704E+1	3.45640484E+1	8.79832056E-2	7.94214544E-2	8.79832056E-2	4.31726187	6.12078309E+1	6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5	CARD 1		
5.61307652E+4	5.46561358E+3	5.75322855E+4	4.24344483E+1	6.18612704E+1	3.45640484E+1	8.79832056E-2	7.94214544E-2	8.79832056E-2	4.31726187	6.12078309E+1	6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5						CARD 2	
1.41434853E+2	4.72859549E+4	5.46561358E+3	5.75322855E+4	6.18612704E+1	3.45640484E+1	8.79832056E-2	7.94214544E-2	8.79832056E-2	4.31726187	6.12078309E+1	6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5						CARD 3	
3.04659113E-1	1.11908631E+2	6.18612704E+1	3.45640484E+1	8.79832056E-2	7.94214544E-2	8.79832056E-2	4.31726187	6.12078309E+1	6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5								CARD 4	
2.05906071E+1	6.18612704E+1	3.45640484E+1	8.79832056E-2	7.94214544E-2	8.79832056E-2	4.31726187	6.12078309E+1	6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5									CARD 5	
6.77190160E+1	6.12078309E+1	1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5																	CARD 6	
1.42139627E-1	7.63605610E-2	1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5																				CARD 7
1.78260973E-2	-2.65828841E-2	-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5																						CARD 8
-4.67529268E-2	-2.03299161E-2	-2.65828841E-2	-9.57123720E-5	-2.82000265E-5																								CARD 9
-9.57123720E-5	-2.82000265E-5																											CARD 10
2.69009967E-7																												CARD 11

3

END

REFERENCE
SECTION

ITEM	DESCRIPTION	REFERENCE SECTION
2	<u>Printout of the station locations as input.</u> If CLASS ≠ 0, the actual locations are left blank	4
3	<u>Card images of the input $A^T A$ matrix data.</u> In this case, $(A^T A)^{-1}$ is input because $\Phi P B \Phi X(A) = 4$	6

***** DEMM INPUT *****

MDWT 0
 ADWT 2
 SDRG .0355
 PSTSD28.CE-5
 KDRS .3017
 END

P1YP 1
 SOCG .0346
 OPH 5.0
 KOTS .3017

OSDEWTVES
 FERI 89.5
 PRES00
 KOCS .3017

ENTER SEGMENT 01 AT 1.5 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 1.5 CP SECS.

***** VEHICLE DATA FOR CASE 1 *****

MVPRAM04,6	20.	DRAG 9.21746269382517E-3	INCOAW0	3	26	CARD 1
0 X	20.	2 6 0	2 3 6	6	2545.474	CARD 2
0 Y	20.	5 0	5 6 6	6	17.18592	CARD 3
0 Z	20.	5 1	5 6 6	6	17.18592	CARD 4
0 DX	1.	IYEAR 1970	IMNTH 6	6		CARD 5
0 DY	1.	TZNE 0	HR 12	6		CARD 6
0 DZ	1.	SEC 17.18502	IICTYP4	3	86.946168659	CARD 7
0 DRAG	.1	2 -.000551476	6	6	25690.5594806	CARD 8
IIDRAG1		5 21561464.324	3	3	721.18592	CARD 9
START1970	4 0	2 1.	5 1000.	2 1.		CARD 10
4 12	4 12	5 PKCK 2507.9064333333	4 30.16990	5 .2307999		CARD 11
IVEHID06820	4 12	2 2	2 9.	3 43277.185		CARD 12
IDAY 26	4 12	5 8	5 54044.693	6 55427.551		CARD 13
MIN 1	4 12	11	8 70191.651	9 75572.998		CARD 14
IC 270.7883984	4 12	14	11 86334.067	12 5213.922		CARD 15
4 198.847449630	4 12	17	14 16071.740	18 21449.836		CARD 16
FTIM 0.	4 12	19	17 32264.094	21 37580.475		CARD 17
4 7.	4 12	20	20 48331.657	21 53706.294		CARD 18
INPKCK1	4 12	3				CARD 19
3 -.15717854	4 12	4				CARD 20
DN00E20.	4 12	5				CARD 21
4 48611.259	4 12	6				CARD 22
7 64809.871	4 12	8				CARD 23
10 80953.858	4 12	11				CARD 24
13 10693.093	4 12	14				CARD 25
16 26827.276	4 12	17				CARD 26
19 42956.330	4 12	19				CARD 27
22 59080.318	4 12	20				CARD 28
END	4 12	22				CARD 29

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6
 CARD 7
 CARD 8
 CARD 9
 CARD 10
 CARD 11
 CARD 12
 CARD 13
 CARD 14
 CARD 15
 CARD 16
 CARD 17
 CARD 18
 CARD 19
 CARD 20
 CARD 21
 CARD 22
 CARD 23
 CARD 24
 CARD 25
 CARD 26
 CARD 27
 CARD 28
 CARD 29
 CARD 30

ITEM	DESCRIPTION	REFERENCE SECTION
4	Card images of the deweighting inputs	7
5	Card images of the input VEHICLE data. Emphasis is on the variables associated with an SLS run (MULTV=2), the others having been discussed earlier: START NCDRAW NPKCK, PKCK DNØDE	11.2.2 11.1.9 11.1.11 11.2.3

```

EPOCH
YR/MO/DAY
TZNE,HR,MIN,SEC
1970/ 6/26
0.
.12000000000E+02
.10000000000E+01
.17165020000E+02
X,Y,Z,DX,DY,DZ
.21469037556E+08
.19942843795E+07
-.20753064537E+03
.1237737639E+04
.82186686159E+04
-.24378976487E+05
A,D,B,A,R,V
.53370435033E+01
-.55147600000E-03
.88946165659E+02
.19884744963E+03
.21561464324E+08
.25690559481E+05
A,E,J,O,I,TAU
.21400276170E+08
.21406144937E-01
.10884744963E+03
.18530723175E+03
.11572153345E+03
.70677056628E+03
AF,AG,N,L,CHI,PSI
.12286662127E-01
-.17528721006E-01
.66784616507E-01
.31944959249E+01
-.12931050634E+00
-.13929146541E+01
    
```

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

THESE ARE THE 13 PARAMETERS IN THE PARAM MATRIX. 7 ARE P PARAMETERS AND 6 ARE Q PARAMETERS

NAME	P/Q	CURRENT VALUE	BOUND	SIGMA	CONVERSION
6820 X	P	.21469038E+08	.20000000E+02	0.	.20925673E+08
6820 Y	P	.19942844E+07	.20000000E+02	0.	.20925673E+08
6820 Z	P	-.20753065E+03	.20000000E+02	0.	.20925673E+08
6820 DX	P	.12377378E+04	.10000000E+01	0.	.34876121E+06
6820 DY	P	-.82186686E+04	.10000000E+01	0.	.34876121E+06
6820 DZ	P	-.24378976E+05	.10000000E+01	0.	.10630000E+01
393 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
377 RBIA	Q	.14000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
363 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
353 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
343 RBIA	Q	.14000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
313 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08

ENTER SEGMENT 02 AT 1.6 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .1 CP SECS.

```

*****
** DATA STAGING INPUT **
*****
LS/F MDELTA DELTA T D YR MO DY HR MN SEC TSTART TSTOP YR MO DY HR MN SEC TUPDATE YR MO DY HR MN SEC
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 13 31 0.0000
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 14 39 0.0000
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 15 0 0.0000
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 16 30 0.0000
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 17 43 0.0000
-0. -0. -0.000 1 0 3 0 0 0 0 0.0000 0 0 0 0 0 0.0000 70 6 26 18 0 0.0000
*****

```

```

*****OBSERVATIONS FOR CASE 1 *****
** STAGE 1 **
** STAGE 2 **
** STAGE 3 **

```

```

*****
STAPASS YR MO DY HR MN SECONDS T C FIELD 1 FIELD 2 FIELD 3 MJD ST VEHID MESSAGE
393 16 70 6 26 14 39 20.0000 1 0 1.11338000E+02 1.11338000E+02 4.07000000E+00 40763 52760.000 6820
393 16 70 6 26 14 39 20.0000 0 0 -1.66357133E+04 0. 0. 0. 40763 52760.000 6820
393 16 70 6 26 14 39 36.0000 1 0 0. 1.17219000E+02 5.00400000E+00 40763 52776.000 6820
393 16 70 6 26 14 39 36.0000 0 0 -1.4605925E+04 0. 0. 0. 40763 52776.000 6820
393 16 70 6 26 14 40 28.0000 1 0 2.65523622E+06 1.42646000E+02 7.14700000E+00 40763 52828.000 6820
393 16 70 6 26 14 41 12.0000 1 0 4.42319686E+03 0. 0. 0. 40763 52828.000 6820
393 16 70 6 26 14 41 12.0000 1 0 2.71175853E+06 1.67016000E+02 6.69300000E+00 40763 52872.000 6820
393 16 70 6 26 14 41 24.0000 1 0 6.51818603E+03 0. 0. 0. 40763 52872.000 6820
393 16 70 6 26 14 41 24.0000 1 0 2.90812664E+06 1.74087000E+02 6.17200000E+00 40763 52884.000 6820
313 16 70 6 26 14 51 12.0000 1 0 1.54888790E+06 5.20920000E+01 1.51500000E+01 40763 53472.000 6820
313 16 70 6 26 14 51 12.0000 0 0 -2.20899318E+04 0. 0. 0. 40763 53472.000 6820
313 16 70 6 26 14 51 44.0000 1 0 9.57660763E+05 8.00630000E+01 2.76470000E+01 40763 53504.000 6820
313 16 70 6 26 14 51 44.0000 0 0 -1.31763271E+04 0. 0. 0. 40763 53504.000 6820
313 16 70 6 26 14 52 40.0000 1 0 1.29941929E+06 1.69412000E+02 1.96350000E+01 40763 53560.000 6820
313 16 70 6 26 14 52 40.0000 0 0 1.9833706E+04 0. 0. 0. 40763 53560.000 6820
313 16 70 6 26 14 53 4.0000 1 0 1.82430118E+06 1.81266000E+02 1.27740000E+01 40763 53584.000 6820
313 16 70 6 26 14 53 4.0000 0 0 2.31371122E+04 0. 0. 0. 40763 53584.000 6820
313 16 70 6 26 14 54 4.0000 1 0 3.29320539E+06 1.92343000E+02 4.29000000E+00 40763 53644.000 6820
313 16 70 6 26 14 54 4.0000 0 0 2.51645637E+04 0. 0. 0. 40763 53644.000 6820
*****

```

ITEM	DESCRIPTION	REFERENCE SECTION
6	Printout of the input STAGE data LS/F = M	14
7	Observations. The observation printout is fully explained in <u>Case B, Item 3</u>	11.2.1 15 11.1.2

```

** STAGE 4 **
STAPASS YR MO DY HR MN SECONDS T C FIELD 1 FIELD 2 FIELD 3 VEHID MESSAGE
393 17 70 6 26 16 7 20.0000 1 0 0 1.15749000E+02 3.67597000E+00 40763 58040.000 6820
393 17 70 6 26 16 7 20.0000 0 0 -2.13349341E+04 0. 40763 58040.000 6820
393 17 70 6 26 16 8 4.0000 1 0 2.78503609E+06 1.29323000E+02 7.19370000E+00 40763 58084.000 6820
393 17 70 6 26 16 8 4.0000 0 0 -1.74967044E+04 0. 40763 58084.000 6820
393 17 70 6 26 16 8 28.0000 1 0 2.41137139E+06 1.40589000E+02 5.15200000E+00 40763 58106.000 6820
393 17 70 6 26 16 8 28.0000 0 0 -1.36219328E+04 0. 40763 58106.000 6820
393 17 70 6 26 16 9 0.0000 1 0 2.10339598E+06 1.60903000E+02 1.11460000E+01 40763 58140.000 6820
393 17 70 6 26 16 9 0.0000 0 0 -5.46453380E+03 0. 40763 58140.000 6820
393 17 70 6 26 16 10 4.0000 1 0 2.40362008E+06 2.05002000E+02 8.68590000E+00 40763 58204.000 6820
393 17 70 6 26 16 10 4.0000 0 0 1.31430709E+04 0. 40763 58204.000 6820

```

```

** STAGE 5 **
** STAGE 6 **

```

```

STAPASS YR MO DY HR MN SECONDS T C FIELD 1 FIELD 2 FIELD 3 VEHID MESSAGE
343 18 70 6 26 17 44 20.0000 1 0 2.72901903E+06 6.66380000E+01 5.88300000E+00 40763 63860.000 6820
343 18 70 6 26 17 44 20.0000 0 0 -2.16764518E+04 0. 40763 63860.000 6820
343 18 70 6 26 17 44 40.0000 1 0 2.33840223E+06 7.44520000E+01 7.92490000E+00 40763 63880.000 6820
343 18 70 6 26 17 44 40.0000 0 0 -1.83778783E+04 0. 40763 63880.000 6820
343 18 70 6 26 17 45 56.0000 1 0 1.70083990E+06 1.32517000E+02 1.27960000E+01 40763 63956.000 6820
343 18 70 6 26 17 45 56.0000 0 0 4.92450460E+03 0. 40763 63956.000 6820
343 18 70 6 26 17 46 36.0000 1 0 2.16558399E+06 1.61521000E+02 8.87490000E+00 40763 63996.000 6820
343 18 70 6 26 17 46 36.0000 0 0 1.54988081E+04 0. 40763 63996.000 6820
343 18 70 6 26 17 47 32.0000 1 0 3.29381890E+06 1.81541000E+02 3.41400000E+00 40763 64052.000 6820
343 18 70 6 26 17 47 32.0000 0 0 2.23990942E+04 0. 40763 64052.000 6820

```


ENTER SEGMENT 10 AT 1.7 SECONDS. EXECUTION TIME FOR SEGMENT 2 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE
721.2864 TZERO
1000.0000 TSTOP

*** TRAJECTORY STAFF
* PREDETERMINED EVENT TABLE *
ASSOCIATED QUANTITIES

*** TRAJECTORY STAFF

STEP	ENTRY TIME	IS	T	ECI	H	H	NSTEP
1	1.76800	1	725.161417			.250000	30
2	1.76800	1	729.411417			.500000	46
3	1.76800	1	729.411417			.500000	46
4	1.76800	1	729.411417			.500000	46
5	1.76800	1	729.411417			.500000	46
6	1.76800	1	729.411417			.500000	46
7	1.76800	1	729.411417			.500000	46
8	1.76800	1	729.411417			.500000	46
9	1.76800	1	729.411417			.500000	46
10	1.76800	1	729.411417			.500000	46
11	1.76800	1	729.411417			.500000	46
12	1.76800	1	729.411417			.500000	46
13	1.76800	1	729.411417			.500000	46
14	1.76800	1	729.411417			.500000	46
15	1.76800	1	729.411417			.500000	46
16	1.76800	1	729.411417			.500000	46
17	1.76800	1	729.411417			.500000	46
18	1.76800	1	729.411417			.500000	46
19	1.76800	1	729.411417			.500000	46
20	1.76800	1	729.411417			.500000	46
21	1.76800	1	729.411417			.500000	46
22	1.76800	1	729.411417			.500000	46
23	1.76800	1	729.411417			.500000	46
24	1.76800	1	729.411417			.500000	46
25	1.76800	1	729.411417			.500000	46
26	1.76800	1	729.411417			.500000	46
27	1.76800	1	729.411417			.500000	46
28	1.76800	1	729.411417			.500000	46
29	1.76800	1	729.411417			.500000	46
30	1.76800	1	729.411417			.500000	46
31	1.76800	1	729.411417			.500000	46
32	1.76800	1	729.411417			.500000	46
33	1.76800	1	729.411417			.500000	46
34	1.76800	1	729.411417			.500000	46
35	1.76800	1	729.411417			.500000	46
36	1.76800	1	729.411417			.500000	46
37	1.76800	1	729.411417			.500000	46
38	1.76800	1	729.411417			.500000	46
39	1.76800	1	729.411417			.500000	46
40	1.76800	1	729.411417			.500000	46
41	1.76800	1	729.411417			.500000	46
42	1.76800	1	729.411417			.500000	46
43	1.76800	1	729.411417			.500000	46
44	1.76800	1	729.411417			.500000	46
45	1.76800	1	729.411417			.500000	46
46	1.76800	1	729.411417			.500000	46
47	1.76800	1	729.411417			.500000	46
48	1.76800	1	729.411417			.500000	46
49	1.76800	1	729.411417			.500000	46
50	1.76800	1	729.411417			.500000	46
51	1.76800	1	729.411417			.500000	46
52	1.76800	1	729.411417			.500000	46
53	1.76800	1	729.411417			.500000	46
54	1.76800	1	729.411417			.500000	46
55	1.76800	1	729.411417			.500000	46
56	1.76800	1	729.411417			.500000	46
57	1.76800	1	729.411417			.500000	46
58	1.76800	1	729.411417			.500000	46
59	1.76800	1	729.411417			.500000	46
60	1.76800	1	729.411417			.500000	46
61	1.76800	1	729.411417			.500000	46
62	1.76800	1	729.411417			.500000	46
63	1.76800	1	729.411417			.500000	46
64	1.76800	1	729.411417			.500000	46
65	1.76800	1	729.411417			.500000	46
66	1.76800	1	729.411417			.500000	46
67	1.76800	1	729.411417			.500000	46
68	1.76800	1	729.411417			.500000	46
69	1.76800	1	729.411417			.500000	46
70	1.76800	1	729.411417			.500000	46
71	1.76800	1	729.411417			.500000	46
72	1.76800	1	729.411417			.500000	46
73	1.76800	1	729.411417			.500000	46
74	1.76800	1	729.411417			.500000	46
75	1.76800	1	729.411417			.500000	46
76	1.76800	1	729.411417			.500000	46
77	1.76800	1	729.411417			.500000	46
78	1.76800	1	729.411417			.500000	46
79	1.76800	1	729.411417			.500000	46
80	1.76800	1	729.411417			.500000	46
81	1.76800	1	729.411417			.500000	46
82	1.76800	1	729.411417			.500000	46
83	1.76800	1	729.411417			.500000	46
84	1.76800	1	729.411417			.500000	46
85	1.76800	1	729.411417			.500000	46
86	1.76800	1	729.411417			.500000	46
87	1.76800	1	729.411417			.500000	46
88	1.76800	1	729.411417			.500000	46
89	1.76800	1	729.411417			.500000	46
90	1.76800	1	729.411417			.500000	46
91	1.76800	1	729.411417			.500000	46
92	1.76800	1	729.411417			.500000	46
93	1.76800	1	729.411417			.500000	46
94	1.76800	1	729.411417			.500000	46
95	1.76800	1	729.411417			.500000	46
96	1.76800	1	729.411417			.500000	46
97	1.76800	1	729.411417			.500000	46
98	1.76800	1	729.411417			.500000	46
99	1.76800	1	729.411417			.500000	46
100	1.76800	1	729.411417			.500000	46

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.404 SECONDS TO INTEGRATE A SPAN OF 279.6250 MINUTES ***

*** FROM 721.286 TO 1000.911 MINUTES FROM MIDNIGHT OF EPDCH ***

ENTER SEGMENT 81 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.4 CP SECS.

ENTER SEGMENT 82 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
8	<p>Predetermined event table indicating the first integration time span. This time span covers all stages</p> <p>TSTART, TSTOP</p>	11.2.2

***** STAGE 1 *****

STAPASS YEAR MO DY HR MN SEC RESIDUALS - EXTERNAL UNITS MME

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

PREDICTED RESIDUAL RMS = .
 ENTER SEGMENT 83 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS . CP SECS.

ITERATION NUMBER 1
 0 MEASUREMENTS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.2146907555645E+03	-0.	.2146907555645E+03	0.	.25784244E+03
6820 Y	.19942847794999E+07	-0.	.19942847794999E+07	0.	.21745334E+03
6820 Z	-.20753754537446E+03	-0.	-.20753754537446E+03	0.	.23985889E+03
6820 OX	.12377377639201E+04	-0.	.12377377639201E+04	0.	.55195925E+00
6820 OY	-.92186686159199E+04	-0.	-.92186686159199E+04	0.	.29661963E+00
6820 OZ	-.24308976466797E+05	-0.	-.24308976466797E+05	0.	.27633415E+00
6820 DRAG	.9217442938252E-02	-0.	.9217442938252E-02	0.	.51866171E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	I.C./SIGMA	T.C./SIGMA
6820 X	0.	.25784244E+03	0.	0.	0.
6820 Y	0.	.21745334E+03	0.	0.	0.
6820 Z	0.	.23985889E+03	0.	0.	0.
6820 OX	0.	.55195925E+00	0.	0.	0.
6820 OY	0.	.29661963E+00	0.	0.	0.
6820 OZ	0.	.27633415E+00	0.	0.	0.
6820 DRAG	0.	.51866171E-03	0.	0.	0.

RESIDUAL RMS = 0.
 RESIDUAL SOS = 0.
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SOS = 0.
 PREDICTED SOS = 0.

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>The <u>current value</u> is shown for parameter per line, starting with the name (test Case B, Item 4)</p> <p>The <u>current value</u> is the parameter value used in the iteration, partial derivatives, and residuals computation (see Appendix F). For the first iteration, it is the input value of the parameter. If an iteration is bad, the value is replaced for the next RMS is recovered from memory and is printed as the current value.</p> <p>The <u>correction</u> is the least squares correction to be applied to the current value for the next iteration.</p> <p>The <u>new value</u> is the sum of the current value plus the correction. This value will be used in convergence of this stage and will be applied to the next stage for all measurable parameters. The current value is shown for the vehicle parameters.</p> <p>The <u>total correction</u> is the value used to correct the parameters at this stage. This value includes the current correction.</p> <p><u>SIGMA</u> is the square root of the diagonal elements of the covariance matrix $(A^T A)^{-1}$ for the parameters at the end of this iteration.</p> <p><u>SIGMA ZERO</u> is the square root of the diagonal elements of the initial $(A^T A)^{-1}$ before decoupling for this stage.</p> <p><u>SIGMA DEWT</u> is the square root of the diagonal elements of the downweighted $(A^T A)^{-1}$ at the start of this iteration.</p> <p><u>T.C./SIGMA0</u> is the total correction/SIGMA ZERO</p> <p><u>T.C./SIGMA0</u> is the total correction/SIGMA DEWT</p> <p>The <u>current value correction</u> is the new value, total correction, and SIGMA are normal least squares output. SIGMA ZERO, SIGMA DEWT, T.C./SIGMA0, and T.C./SIGMA0 are extended least squares output and are obtained when PANDR11570.</p> <p><u>Residual RMS</u> is the weighted root mean square residuals for the current iteration.</p> <p><u>Residual SCS</u> is the sum of squares of the normalized measurement residuals for the current iteration.</p> <p><u>A priori RMS</u> is the weighted root mean square total of the parameter corrections for the previous iterations for the current stage.</p> <p><u>A priori SCS</u> is the sum of the squares of the total parameter corrections for the previous iterations for the current stage.</p> <p><u>Total SCS</u> is the sum of the residual SCS + a priori SCS.</p> <p><u>Predicted SOS</u> is the predicted sum of the normalized measurement residuals squared.</p>	2.2.3
		2.2.11.1
		2.2.4
		2.2.2

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.27234E-02	.92365E-03	.45841E-03	.44390E+03	.42808E+03	.10966E+04	
.17085E-03	.16370E-03	.35395E+02	-.84265E+02	.41722E+03	-.64479E+05	.93397E+07
-.65088E-03	.35921E-02	-.20210E+07	-.43786E+07	.41722E+03	-.64479E+05	-.93397E+07
-.84361E+00	-.43786E+07	-.20210E+07	-.43786E+07	.41722E+03	-.64479E+05	-.93397E+07
-.20527E+00	-.43786E+07	-.20210E+07	-.43786E+07	.41722E+03	-.64479E+05	-.93397E+07
-.25873E+00	-.21456E+00	-.42212E+04	.34712E+04	-.21921E+05	-.64479E+05	-.93397E+07
.70757E+02	.79235E+01	.42212E+04	.34712E+04	-.21921E+05	-.64479E+05	-.93397E+07
-.0.	-.0.	-.0.	-.0.	-.0.	-.0.	-.0.

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.66483E+05	.47296E+05	.57532E+05	.30466E+00	.87983E-01	.76361E-01	.26901E-06
.16826E+05	.54656E+04	.11191E+03	.79421E-01	.17826E-01	-.23209E-04	
.56131E+05	.42434E+02	.20591E+02	.14214E+00	.17826E-01	-.23209E-04	
.14043E+03	.61861E+02	.61208E+02	.14214E+00	.17826E-01	-.23209E-04	
.34564E+02	.43173E+01	.61208E+02	.14214E+00	.17826E-01	-.23209E-04	
.67719E+02	.43173E+01	.61208E+02	.14214E+00	.17826E-01	-.23209E-04	
-.6753E-01	-.10330E-01	-.26583E-01	-.95712E-04	-.22947E-04	-.23209E-04	.26901E-06

CORRELATION MATRIX

6820 X	1.00000
6820 Y	.30010 1.00000
6820 Z	.90759 -.10479 1.00000
6820 DX	.20676 .35355 .84528 1.00000
6820 DY	.45193 .95974 .28541 .49510 1.00000
6820 DZ	.95043 .67185 .92346 .93191 .21748 1.00000
6820 DRAG	-.34960 -.09159 -.21366 -.33433 -.14916 -.19676 1.00000

ENTER SEGMENT 84 AT 1.3 SECONDS. CALCULATING FOR SEGMENT 84 WAS 1.3 CP SECS.
ATA INVERSE UPDATED TO 811.2 MINUTES FROM MIDNIGHT OF EPOCH

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.55687E+05	.21730E+06	.14791E+07	.32479E+01	.13083E+07	.76683E-01	.25901E-06
.67521E+05	.49044E+06	.21726E+07	.44207E+00	.35908E-01	-.39061E-04	
.32434E+03	.75470E+03	.28152E+03	.32502E+00	.35908E-01	-.39061E-04	
.50349E+02	.15119E+03	.20548E+03	.32502E+00	.35908E-01	-.39061E-04	
.62691E+02	.53597E+02	.20548E+03	.32502E+00	.35908E-01	-.39061E-04	
-.5564E-01	-.15666E+0	-.45517E+07	-.66394E-03	-.77576E-04	-.39061E-04	.25901E-06

ITEM	DESCRIPTION	REFERENCE SECTION
10	<p data-bbox="363 468 396 1851">$A^T A$ is the current $A^T A$ matrix for this iteration</p> <p data-bbox="429 468 528 1851">$A^T B$ is the right-hand side of the normal matrix equation for the generalized least squares (GLS) problem when a priori statistics are included in the GLS solution of the linear system. The equation to be solved is</p> $(C_0^{-1} + A^T W A) \Delta P = A^T W B$ <p data-bbox="660 851 685 883">where</p> $A = \frac{\partial O_c}{\partial P}$ <p data-bbox="776 1000 801 1042">W = observation weighting matrix</p> <p data-bbox="826 1064 850 1106">P = vector of parameter corrections</p> <p data-bbox="867 1117 900 1170">B = residual vector ($A^T W O_{mc}$) for the last iteration</p> <p data-bbox="941 1212 1007 1851"><u>$A^T A$ inverse</u> is the covariance for the parameter set at this iteration. It is the inverse of the $A^T A$ matrix above</p> <p data-bbox="1049 1351 1106 1851"><u>Correlation matrix</u>, the correlation coefficients for the parameter set. These values are computed directly from the covariance matrix</p> <p data-bbox="1139 1468 1197 1851"><u>$A^T A$ inverse updated</u> is the covariance for the parameter set updated to the time of the next iteration</p>	

G AND G DOWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.33140E+05
 -.29250E-18
 0.
 .63892E-10
 -.38775E+02
 0.
 .39768E+06
 .31491E+05
 -.39779E+03
 .33054E-21
 0.
 .40832E+00
 -.74757E-13
 .45369E-01
 .43098E-01

PARAMETER SET COORDINATE SYSTEM

.76445E-11
 -.79472E-11
 -.24449E-10
 -.17971E-11
 .15439E-11
 .50051E-11
 .15841E-09
 .25451E-09
 .16992E-10
 .17956E-11
 .49086E-12
 .82090E-09
 .53052E-10
 .48041E-11
 .14962E-14
 .33296E-11
 .28538E-12
 .38366E-12
 .56905E-14
 .37105E-12

**** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MC/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	U-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-DOT
1970/ 6/26	21462602.415	5.482511795	21798793.913	.0122805196989	58.21461818	3664.19737
13/31	2050702.054	.071549899	.02134291985	-.017455917234	59.23505346	228.10753
1.2588000	593.249	88.94843245	108.847926486	.0667914375674	60.35334034	3511.04979
.0015603	1262.7637290	198.847926491	185.481982716	3.371622844	89.8318739	74.95996
248.4688068	-8214.9716254	21561236.311	119.645021943	-.13355668939	89.5929426	2.7925652809
104.6003	-24308.3525001	25689.5725442	736.4870267	-1.35162602397	89.7251141	-2.0666695725

LEAST SQUARES PROCESS CONVERGED.

EXIT SEGMENT 94 AT 3.3 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .000 SECS.

11

12

REFERENCE
SECTION

DESCRIPTION

ITEM

- 11 Deweighting matrix in the orbit plane coordinate system (RTC). The values in this matrix are used to deweight the $A^T A$ matrix. This deweighting allows for the uncertainty in the unmodeled parameters. Units are external
- 12 Parameter set coordinate system is the RTC deweighting matrix converted to the parameter set coordinate system (ECI). This converted matrix is added to the updated $A^T A$ inverse matrix. Units are external

ENTER SEGMENT 10 AT 3.3 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

811.0210 TZERO
 882.0300 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS	3.36790	ECI	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
NODE T =	.811021329896E+03	.214626327051E+08	.20580494770E+07	.161588981064E-04																
DT =	.125000000000E+00	.126203943514E+04	-.821494114187E+04	-.243783525152E+05																
STEP DOUBLED	T = 814.895930	T = .250000	H = .500000	NSTEP = 30																
STEP DOUBLED	T = 819.145980	T = .500000	H = .500000	NSTEP = 46																
NODE T =	.856943298638E+03	-.218897494550E+08	-.213361809386E+07	-.537143593949E-02																
DT =	.500000000000E+00	-.319620430707E+03	.814270199170E+04	.238298363442E+05																

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .683 SECONDS TO INTEGRATE A SPAN OF 71.1250 MINUTES ***

*** FROM 811.021 TO 882.146 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .5 CP SECS.

ENTER SEGMENT 82 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 2 *****

STAPASS YEAR MO DY HR MN SEC RESIDUALS - EXTERNAL UNITS MME

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

PREDICTED RESIDUAL RMS = 0.

ENTER SEGMENT 83 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP SECS.

ITERATION NUMBER 1
 0 MEASUREMENTS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.2146267415330E+08	-6.	.21462602415330E+08	0.	.29859908E+03
6820 Y	.20600020544027E+07	-0.	.20600020544027E+07	0.	.53540718E+03
6820 Z	.58324941054139E+03	-0.	.58324941054139E+03	0.	.13559432E+04
6820 DX	.12627637289684E+04	-0.	.12627637289684E+04	0.	.19112453E+01
6820 DY	-.02148716253522E+04	-0.	-.02148716253522E+04	0.	.42129759E+00
6820 DZ	-.24308352500073E+05	-0.	-.24308352500073E+05	0.	.34901981E+00
6820 DRAG	.92174626938252E+02	-0.	.92174626938252E+02	0.	.58941494E+03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMAD
6820 X	.23558149E+03	.29859908E+03	0.	0.	0.
6820 Y	.46615033E+03	.53540718E+03	0.	0.	0.
6820 Z	.12161926E+04	.13559432E+04	0.	0.	0.
6820 DX	.18021846E+01	.19112453E+01	0.	0.	0.
6820 DY	.36169753E+00	.42129759E+00	0.	0.	0.
6820 DZ	.27691647E+00	.34901981E+00	0.	0.	0.
6820 DRAG	.51866371E-03	.58941494E-03	0.	0.	0.

RESIDUAL RMS = 0.
 RESIDUAL SOS = 0.
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SOS = 0.
 PREDICTED SOS = 0.

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6820 X	682 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.16114E-02						
6820 Y	.16088E-03	.36029E-04					
6820 Z	.87962E-05	.51395E-06	.14740E-04				
6820 DX	.32316E-02	-.35608E-02	-.10851E-01	.96554E+01			
6820 DY	-.43220E+02	-.51557E-01	-.97442E-04	-.20794E+01	.12850E+03		
6820 DZ	-.12593E+01	-.12158E+00	-.33604E-02	-.73308E+01	.33698E+03	.99553E+03	
6820 DRAG	.93853E+02	.80820E+01	-.27226E+01	.18668E+04	-.25541E+05	-.75004E+05	.10104E+06
ATA	-0.	-0.	-0.	-0.	-0.	-0.	0.

ATA INVERSE

	6820 X	682 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.89161E+05						
6820 Y	.64041E+05	.28666E+06					
6820 Z	.19587E+06	.60989E+06	.18386E+07				
6820 DX	.31122E+03	.07971E+03	.25379E+04	.36529E+01			
6820 DY	.61616E+02	.16430E+03	.31659E+03	.47678E+00	.17745E+00		
6820 DZ	.99219E+02	.57766E+02	.20549E+03	.32496E+00	.36601E-01	.12181E+00	
6820 DRAG	-.45064E-01	-.15666E+01	-.45517E+01	-.66094E-03	-.77576E-04	-.30061E-04	.34741E-06

CORRELATION MATRIX

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	1.00000						
6820 Y	.40058	1.00000					
6820 Z	.46277	.84009	1.00000				
6820 DX	.54534	.85871	.97929	1.00000			
6820 DY	.48980	.72839	.55419	.59212	1.00000		
6820 DZ	.95204	.30538	.43422	.48716	.24891	1.00000	
6820 DRAG	-.25605	-.49643	-.56953	-.58671	-.31241	-.14613	1.00000

ENTER SEGMENT 84 AT 4.0 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.

ATA INVERSE UPDATED TO 879.00 MINUTES FROM MIDNIGHT OF EPOCH

	6820 X	6820 Y	6820 Z	6820 OX	6820 OY	6820 OZ	6820 DRAG
6820 X	.95809E+07						
6820 Y	.10097E+07	.18607E+06					
6820 Z	.13755E+06	.15107E+05	.88340E+05				
6820 OX	-.71989E+02	-.32306E+02	-.95064E+02	.11142E+00			
6820 OY	-.37618E+04	-.44852E+03	-.62902E+02	.49529E-01	.15454E+01		
6820 OZ	-.10980E+05	-.11553E+04	-.20265E+03	.13719E+00	.42122E+01	.12469E+02	
6820 DRAG	.12151E+01	.13110E+00	-.41728E-02	.10330E-04	-.49906E-03	-.14747E-02	.34741E-06

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.26229E+05							
-.79673E+04	.38750E+06						
0.	0.	.24916E+05					
.15384E+02	-.37674E+03	0.	.37047E+00				
-.30689E+02	.93222E+01	0.	-.18000E-01	.35908E-01			
0.	0.	.57586E+01	0.	0.	.31734E-01		

PARAMETER SET COORDINATE SYSTEM

.87797E-09							
.77093E-10	.64413E-10						
-.10427E-10	-.10049E-12	.59356E-10					
.34815E-11	-.11055E-11	-.39878E-11	.31126E-12				
-.16180E-10	-.84678E-12	-.13394E-12	-.79310E-13	.53885E-12			
-.47865E-10	-.444451E-11	.15397E-11	-.24524E-12	-.83169E-12	.27518E-11		

**** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MO/0Y	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	L	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	X00T	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	Y00T	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	Z00T	VELOCITY	TAU	PSI	MODAL PERIOD	U-DOT
1970/ 6/26	-861872.839	97.158392672	21737616.110	.0115440762591	330.12379221	3647.59745
14/39	6862499.928	71.116801417	.01957929700	-.0158140182847	329.55535415	211.36878
0.0000000	2.220527.828	50.568518390	108.876805463	.0670735009855	328.98203717	3507.50556
71.2343408	25757.4037672	271.463539434	185.611644975	276.252955068	89.4539728	71.27589
323.1034043	2520.8380076	21370691.970	120.517427874	-.13677947464	89.6928160	2.8239257659
83.5838	-29.0564957	25880.4813975	796.9697671	-1.38206143348	89.7249242	-2.0000000599

LEAST SQUARES PROCESS CONVERGED.

EXIT SEGMENT 84 AT 4.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

***** STAGE 3 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME
393 16	1970	6	26	14	39	21.0000	0.0	0.0
						PREDICTED RESIDUALS	0.0	0.0
393 16	1970	6	26	14	39	19.2503	.116394E+02 SRR	0.0
						PREDICTED RESIDUALS	.139247E+02	0.0
393 16	1970	6	26	14	39	36.0000	0.0	0.0
						PREDICTED RESIDUALS	.134860E+00 AZ	0.0
393 16	1970	6	26	14	39	35.2492	.144143E+02 SRR	0.0
						PREDICTED RESIDUALS	.174253E+02	0.0
393 16	1970	6	26	14	40	29.0000	-.568419E+03 RNG	0.0
						PREDICTED RESIDUALS	.563792E+03	0.0
393 16	1970	6	26	14	40	27.2438	.236239E+02 SRR	0.0
						PREDICTED RESIDUALS	.294388E+02	0.0
393 16	1970	6	26	14	41	12.0000	.467147E+03 RNG	0.0
						PREDICTED RESIDUALS	.868521E+03	0.0
393 16	1970	6	26	14	41	11.2384	.218359E+02 SRR	0.0
						PREDICTED RESIDUALS	.276626E+02	0.0
393 16	1970	6	26	14	41	24.0000	.741683E+03 RNG	0.0
						PREDICTED RESIDUALS	.118599E+04	0.0
393 16	1970	6	26	14	41	23.2371	.194904E+02 SRR	0.0
						PREDICTED RESIDUALS	.248938E+02	0.0
313 16	1970	6	26	14	51	12.0000	-.118038E+04 RNG	0.0
						PREDICTED RESIDUALS	.252318E+04	0.0
313 16	1970	6	26	14	51	11.2533	.891136E+01 SRR	0.0
						PREDICTED RESIDUALS	.151941E+02	0.0
313 16	1970	6	26	14	51	44.0000	-.580432E+03 RNG	0.0
						PREDICTED RESIDUALS	.143692E+04	0.0
313 16	1970	6	26	14	51	43.2484	.323296E+02 SRR	0.0
						PREDICTED RESIDUALS	.622789E+02	0.0
313 16	1970	6	26	14	52	39.2320	.119407E+04 RNG	0.0
						PREDICTED RESIDUALS	.238760E+04	0.0
313 16	1970	6	26	14	52	39.2320	.106648E+02 SRR	0.0
						PREDICTED RESIDUALS	.255109E+02	0.0
313 16	1970	6	26	14	53	4.0000	.133058E+04 RNG	0.0
						PREDICTED RESIDUALS	.274215E+04	0.0
313 16	1970	6	26	14	53	3.2305	.299246E+01 SRR	0.0
						PREDICTED RESIDUALS	.901653E+01	0.0
313 16	1970	6	26	14	54	4.0000	.137674E+04 RNG	0.0
						PREDICTED RESIDUALS	.295458E+04	0.0
313 16	1970	6	26	14	54	3.2296	-.186451E+00 SRR	0.0
						PREDICTED RESIDUALS	.154078E+01	0.0

DESCRIPTION

ITEM

13 Residuals - External Units. Each line corresponds to one input observation set or card and contains the station-pass identification in year, month, day, hour, minute, and second; three pairs of measurement residuals and identification; and the time in MME

The residuals are the unnormalized differences between the input measurements (modified by bias and/or refraction corrections) and the corresponding values for the same measured types computed from the integrated trajectory position at the observation time. The observation names are abbreviated as follows:

RNG	Range	CM3	Three-way cumulative doppler
AZ	Aximuth	DOP	Doppler
EL	Elevation	TWD	Two-way doppler
TRA	Topocentric right ascension	SRR	SGLS range rate
TD	Topocentric declination	AX	X-antenna
THA	Topocentric hour angle	AY	Y-antenna
GRA	Geocentric right ascension	CC3	JPL two- or three-way doppler
GD	Geocentric declination	TNT	Tranet doppler
U	u	GCR	Geocenter range difference
V	v	V2	Vehicle-vehicle range
H	Height	V2D	Vehicle-vehicle range rate
X		S2	Station-vehicle-vehicle range
Y		S2D	Station-vehicle-vehicle range rate
Z		S3	Station-vehicle-vehicle range
P	P	S3D	Station-vehicle-vehicle range rate
Q	Q	V3	Vehicle-vehicle-vehicle range
RD	Range rate	TDA	Time differences of arrival
PD	P rate	TDA	Time of arrival
QD	Q rate	N	Time-of-arrival counter
CM1	One-way cumulative doppler	ACC	Accelerometer

Predicted residuals for each observation $(\hat{\phi}) = \hat{r} \cdot [(C_0) \hat{r}]$ where $C_0 = (A^T A)^{-1}$ for this iteration

$$\hat{r} = \frac{\partial \phi}{\partial \underline{p}}$$

\underline{p} = parameter set

} (14)

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
313	RNG	.246498E+04	SFR	.311255E+02		
393	SRR	.234402E+02	RNG	.915407E+03		

PREDICTED RESIDUAL RMS = .2162231161E+03 (15)

ENTER SEGMENT 83 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 1
18 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.86187283924646E+06	-.26946076E+04	-.85917823167636E+06	.26946076E+04	.86664237E+01
6820 Y	.68624999275575E+07	.15963546E+03	.68626595639133E+07	.15963546E+03	.12336910E+02
6820 Z	.25229327327524E+08	.85484888E+03	.2622138267608E+08	.8548488E+03	.38966545E+02
6820 DX	.25737403767231E+05	-.87179446E+00	.25756532062771E+05	-.87179446E+00	.4193019E+01
6820 DY	.25258380106258E+04	-.10258623E+01	.25198121452701E+04	-.10259623E+01	.41057022E+01
6820 DZ	-.29056495734126E+02	-.31997651E+01	-.32256260837096E+02	-.31997651E+01	.85279079E+01
6820 DRAG	.92174626938252E-02	.24751907E-03	.94649817670962E-02	.24751907E-03	.41172570E+03

NAME	SIGMA ZEF0	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820 X	.30953062E+04	.31567975E+04	.26946076E+04	.87054636E+00	.35358098E+00
6820 Y	.43136142E+03	.46290205E+03	.15963546E+03	.37007322E+00	.74495796E+00
6820 Z	.29722097E+03	.33812934E+03	.85484888E+03	.29761399E+01	.25201713E+01
6820 DX	.33379987E+00	.38637129E+00	-.87179446E+00	-.26111399E+01	-.22563316E+01
6820 DY	.12431271E+01	.12692153E+01	-.10258623E+01	-.82922727E+00	-.80826505E+00
6820 DZ	.35311126E+01	.35782622E+01	-.31997651E+01	-.90614546E+00	-.89422321E+00
6820 DRAG	.58941497E-03	.58941494E-03	.24751907E-03	.41994028E+00	.41994028E+00

RESIDUAL RMS = .1334096648E+03
 RESIDUAL SDS = .3203664959E+06
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SOS = .3203664959E+06
 PREDICTED SDS = .1510667690E+02

ITEM	DESCRIPTION	REFERENCE SECTION
14	<u>Summary of predicted statistics</u> contains the station data type and the RMS value for each data type	Item 9
15	<u>Predicted residual RMS</u> is the resulting RMS value calculated from the RMS values of each data type	Item 14

ATA

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.46287E-01	.35232E-01	.67521E-01				
.12552E-01	.2825E-01	-.16916E+02	.20191E+05			
-.110536E-01	.37392E+01	.15566E+02	.90214E+04			
.19273E+02	.20377E+02	.37019E+02	-.13102E+05	.21591E+05		
.16679E+02	.13403E+02	.99403E+03	-.44431E+06	.61963E+04	.29194E+08	
-.776409E+01	.16306E+03	.95629E+02	.53025E+05	.14167E+05	-.50686E+05	-.16180E+07
-.42191E+03	-.3656E+01					.32037E+06
.10877E+03						

ATA INVERSE

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.75107E+02	.15220E+03	.15184E+04				
.50115E+01	-.82866E+02					
.20719E+03	.25883E+00	-.10874E+01	.17581E-02			
-.11061E+00	.37172E+00	.16065E+00	-.12867E-02	.16857E-02		
-.84013E-01	-.35833E+00	-.30283E+01	.31680E-02	-.16098E-02	.72725E-02	
-.34376E+00	-.16032E-02	-.54738E-02	-.38768E-05	.10328E-04	.23858E-06	.16952E-06
-.11839E-02						

CORRELATION MATRIX

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
1.00000						
.04687	1.00000					
.61354	-.17446	1.00000				
-.30438	.50037	-.65329	1.00000			
-.23611	-.73388	.10041	-.74742	1.00000		
-.46512	.34058	-.91132	.80597	-.45970	1.00000	
-.33180	-.32684	-.34118	-.22456	.61885	.00679	1.00000

ENTER SEGMENT 84 AT 4.45 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

YEAR/MC/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-FOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-FOT
1970/ 6/26	-859170.232	57.136J79080	21737496.946	.C11544785030	337.05894482	3647.45825
14/39	6862659.563	71.117991789	.C1954597749	-.C157724523242	329.49039975	211.21826
0.0J0C000	20221382.676	90.588645043	188.875801391	.C670741516302	328.91695641	3507.61554
71.2355249	25756.5320624	271.442104951	185.611994282	276.260879867	85.4532373	71.36555
323.0810907	2519.8121453	21371443.584	120.599870828	-.13678442616	89.5921573	2.823827869
83.7077	-32.2562608	25879.5177238	796.9865525	-1.35203486846	85.7241692	-2.080357473

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
313	5 RNG	1.2E+33	5.8E+01	4.3E+02	5 AZ	2.4E-02	0.	3.7E-03	5 EL	1.9E-02	0.	7.4E-03
313	5 SRR	1.6E+31	1.6E+02	1.1E+31	5 EL	1.7E-02	0.	3.4E-03	5 SRR	1.9E+01	1.9E+02	1.8E+01
393	5 AZ	1.4E-01	0.	1.3E-31	5 EL	1.7E-02	0.	3.4E-03	5 SRR	1.9E+01	1.9E+02	1.8E+01
393	3 RNG	6.1E+02	3.8E+01	2.2E+32								

EXIT SEGMENT 84 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.
 ENTER SEGMENT 10 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (MME) TYPE ASSOCIATED QUANTITIES
 879.3300 TZERO
 9*3.749 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS 4.57130
 STEP COUPLED T = 982.250000 H = .250000 NSTED = 25
 STEP COUPLED T = 889.250000 H = .500000 NSTED = 52
 NODE T = .903745091723E+03 .214557299934E+08 .012528979768E+07 -.144713230605E-04
 OT = .500000000000E+00 .128587890605E+04 -.62114667778E+04 -.243760029595E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .253 SECONDS TO INTEGRATE A SPAN OF 24.750 MINUTES ***

*** FROM 879.330 TO 903.750 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 4.8 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

ENTER SEGMENT 82 AT 4.9 SECONDS. EXECUTION TIME FOR SEGMENT 21 WAS .1 CP SECS.

REFERENCE SECTION		DESCRIPTION	ITEM
2.2.4		<u>Total edit summary</u> is fully explained in Case B, Item 7.	16

***** STAGE 3 *****

STAPASS	YEAR	MO	DAY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME	
393	1970	6	26	14	39	27.0000	0.	079.333	
393	1970	6	26	14	39	19.2503	-.442553E-01 SRR	0.	
393	1970	6	26	14	39	36.0700	0.	079.321	
393	1970	6	26	14	39	35.2092	0.	079.507	
393	1970	6	26	14	40	28.0000	-.305583E-01 SRR	0.	
393	1970	6	26	14	40	27.2438	-.146891E+02 RNG	0.	
393	1970	6	26	14	41	12.0000	-.230042E-01 SRR	0.	
393	1970	6	26	14	41	11.2384	-.16428E+01 RNG	0.	
393	1970	6	26	14	41	24.0000	-.170665E-03 SRR	0.	
393	1970	6	26	14	41	23.2371	0.	081.400	
393	1970	6	26	14	51	12.0000	-.352911E+01 RNG	0.	
393	1970	6	26	14	51	11.2533	-.222323E-01 SRR	0.	
393	1970	6	26	14	51	4.0000	-.659466E-01 SRR	0.	
393	1970	6	26	14	51	43.2484	-.246368E+02 RNG	0.	
393	1970	6	26	14	52	40.0000	0.	091.100	
393	1970	6	26	14	52	39.2320	-.189811E+02 RNG	0.	
393	1970	6	26	14	53	4.0000	0.	091.721	
393	1970	6	26	14	53	3.2315	-.334623E-01 SRR	0.	
393	1970	6	26	14	54	4.0000	-.229135E-01 AZ	0.	
393	1970	6	26	14	54	3.2296	0.	092.667	
393	1970	6	26	14	54	3.2296	-.538472E-03 SRR	0.	092.654
393	1970	6	26	14	54	3.2296	0.	093.067	
393	1970	6	26	14	54	3.2296	-.349994E-01 AZ	0.	094.067
393	1970	6	26	14	54	3.2296	0.	094.054	

ENTER SEGMENT 83 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT #2 WAS .1 CP SECS.

ITERATION NUMBER 2
18 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							-.85917782167725E+06	.35999910E+00	-.8591778167725E+06	.26949676E+04	.86647990E+01
6820	Y							-.68626595638133E+07	-.15450372E+01	-.686265980179761E+07	.15209842E+03	.12332311E+02
6820	Z							.21221382676408E+08	.87685625E+00	.20221383553264E+08	.85572574E+03	.38971069E+02
6820	DX							.25756932762771E+05	.40341242E-03	.25756532466183E+05	-.87137135E+00	.41930178E-01
6820	DY							.25198121452701E+04	-.33434910E-02	.25198088917790E+04	-.10292058E+01	.41030290E-01
6820	DZ							-.32256260830496E+02	.18162331E-02	-.32254444597435E+02	-.31979499E+01	.85289058E-01
6820	DRAG							.94649817670862E-02	-.40685814E-05	.94649131856769E-02	.2434549E-03	.41173917E-03

NAME	SIGMA ZERO	SIGMA LEWT	TOTAL CORR.	T.C./SIGMAR	T.C./SIGMAD
6820 X	.30953062E+04	.31567975E+04	.26949678E+04	.87066266E+04	.85370302E+00
6820 Y	.43136182E+03	.46290205E+03	.15009042E+03	.36649145E+03	.34152024E+00
6820 Z	.2972209 E+03	.33812934E+03	.8552574E+03	.28790901E+01	.25307645E+01
6820 DX	.3337981E+00	.38637129E+00	-.87130105E+00	-.26102503E+01	-.22590875E+01
6820 DY	.12431271E+01	.12682153E+01	-.10292088E+01	-.82791685E+01	-.41089935E+00
6820 DZ	.35311826E+01	.35782622E+01	-.31979499E+01	-.99563112E+01	-.99371563E+00
6820 DRAG	.58941494E-03	.58941494E-03	.24345049E-03	.41303753E+00	.41303753E+00
RESIDUAL RMS =	.6734028011E+00				
RESIDUAL SOS =	.8162485924E+01				
APRIORI RMS =	.9997706082E+00				
APRIORI SOS =	.695678883E+01				
TOTAL RMS =	.1515927481E+02				
PREDICTED SOS =	.1487141259E+02				

ATA

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.46320E-01	.35183E-01	.67555E-01	.20240E+05	.17517E+05	.21619E+05	.28914E+06
.12528E-01	.27983E-01	-.16989E+02	.90207E+04	.61704E+04	.56051E+06	.13779E+04
-.10610E-01	.37246E+01	-.37054E+02	-.13147E+05	-.57035E+05	.29092E+02	.81625E+1
.19313E+02	.23327E+02	.37054E+02	.90207E+04	.61704E+04	.56051E+06	.28914E+06
.16069E+02	.83387E+02	.98556E+03	-.43967E+06	-.57035E+05	.29092E+02	.81625E+1
-.76831E+01	.16168E+03	.16760E-01	-.57778E+02	-.55513E+02	.29092E+02	.81625E+1
-.41838E+03	.68118E-01					
-.70171E-01						

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.75179E+02	.15209E+03	.15107E+04	.17501E-02	.16835E-02	.72742E-02	.16993E-06
.48999E+01	-.84416E+02	-.10877E+01	-.12873E-02	-.16091E-02	.30184E-06	.16993E-06
.20715E+03	.25994E+00	.16293E+00	.31672E-02	-.16091E-02	.30184E-06	.16993E-06
-.11470E+00	-.37126E+00	-.30310E+01	-.38724E-05	.10208E-04	.16993E-06	.16993E-06
-.83529E-01	.35854E+00	-.54754E-02				
-.34426E+00	.16532E-02					
-.11803E-02						

CORRELATION MATRIX
 6820 X 1.00000
 6820 Y .04505
 6820 Z .61344
 6820 DX -.30470
 6820 DY -.23495
 6820 DZ -.46584
 6820 DRAG -.33084

1.00000
 -.17565
 .50075
 -.73372
 .34088
 -.32558
 1.00000
 -.65340
 .10189
 -.91189
 -.22430
 1.00000
 -.74823
 .88565
 .60903
 1.00000
 1.00000
 1.00000
 1.00000

ENTER SEGMENT 84 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. ***

YEAR/MO/DY	X	Y	Z	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	TRUE ANOMALY	KEPLERIAN PER	ANOMALY PER	NODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	O-DOT	U-DOT	
1970/ 6/26	-859177.872	6862658.018	20221383.553	97.136377710	71.117996552	94.568643087	271.442112057	25756.5324662	2137.1443.903	796.9865193	-1.39203476573	330.05906030	329.49050718	328.91777581	89.4532421	89.6926622	89.7241741	330.05906030	3647.45839	211.21842	3587.61666	71.36669	2.823826735	-2.0803563339	
14/39	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
71.2355296	25756.5324662	2519.8088018	-32.2544446	21737497.734	.01954597823	108.875796568	185.611985367	120.589749135	796.9865193	0.115444430051	-0.0157724792175	0.0670741479820	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805
323.0810893	2519.8088018	-32.2544446	25879.5177974	21737497.734	.01954597823	108.875796568	185.611985367	120.589749135	796.9865193	0.115444430051	-0.0157724792175	0.0670741479820	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805
83.7077	-32.2544446	25879.5177974	25879.5177974	21737497.734	.01954597823	108.875796568	185.611985367	120.589749135	796.9865193	0.115444430051	-0.0157724792175	0.0670741479820	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805	276.260794805

EXIT SEGMENT 84 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

* PREDETERMINED EVENT TABLE *
 * ASSOCIATED QUANTITIES

*** TRAJECTORY START ***
 * * * * * ECI * * * * *
 * * * * * T = 802.250000 H = .250000 NSTEP = 25
 * * * * * T = 889.250000 H = .500000 NSTEP = 52
 * * * * * T = 900745093793E+03 .214557320665E+08 .212527764462E+07 -.729249300990E-05
 * * * * * DT = .00000000000E+00 .128583828185E+04 -.821146372638E+04 -.243080023900E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .255 SECONDS TO INTEGRATE A SPAN OF 24.7500 MINUTES ***
 *** FROM 879.000 TO 903.750 MINUTES FROM MIDNIGHT OF EPOCH ***
 ENTER SEGMENT 61 AT 5.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.
 ENTER SEGMENT 82 AT 5.4 SECONDS. EXECUTION TIME FOR SEGMENT 61 WAS .1 CP SECS.

***** STAGE 3 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME
393 16	1970	6	26	14	39	20.0000	0.	879.333
393 16	1970	6	26	14	39	19.2503	-.362891E-01 SRR	879.321
393 16	1970	6	26	14	39	36.0000	0.	879.600
393 16	1970	6	26	14	39	35.2492	.368371E-01 SRR	879.507
393 16	1970	6	26	14	40	28.0000	-.127559E+02 RNG	860.467
393 16	1970	6	26	14	40	27.2438	-.275882E-01 SRR	860.454
393 16	1970	6	26	14	41	12.0000	-.221059E+01 RNG	861.200
393 16	1970	6	26	14	41	11.2384	-.311691E-02 SRR	861.107
393 16	1970	6	26	14	41	24.0000	-.543241E+01 RNG	861.400
393 16	1970	6	26	14	41	23.6371	-.438627E-01 SRR	861.387
313 16	1970	6	26	14	51	12.0000	-.290535E-01 AZ	891.200
313 16	1970	6	26	14	51	11.2533	-.473738E-01 SRR	891.188
313 16	1970	6	26	14	51	44.6000	-.264175E+02 RNG	891.733
313 16	1970	6	26	14	51	43.2484	-.734340E-01 SRR	891.721
313 16	1970	6	26	14	52	40.0000	-.170611E+02 RNG	892.667
313 16	1970	6	26	14	52	39.2320	-.002365E-01 SRR	892.654
313 16	1970	6	26	14	53	4.0000	-.185782E+02 RNG	893.067
313 16	1970	6	26	14	53	3.2305	-.338924E-03 SRR	893.054
313 16	1970	6	26	14	54	4.6000	-.171638E+02 RNG	894.067
313 16	1970	6	26	14	54	3.2296	-.344210E-02 SRR	894.054

ENTER SEGMENT 83 AT 5.5 SECONDS. EXECUTION TIME FOR SEGMENT #2 WAS .1 CP SECS.

ITERATION NUMBER 3
16 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							-.85517787167725E+06	.47835554E-03	-.85917787119919E+06	.26949680E+04	.86647932E+01
6820	Y							.6862698179761E+07	-.15530498E-03	.68626580178207E+07	.15809026E+03	.12332326E+02
6820	Z							.20221183553264E+08	-.37430598E-02	.20221383557007E+08	.85522948E+03	.38971070E+02
6820	DX							.25756532466183E+05	-.39323101E-05	.25756532462351E+05	-.87137489E+00	.41930145E-01
6820	DY							.25198088017790E+04	-.81119420E-07	.25198088016979E+04	-.10292059E+01	.41030546E-01
6820	DZ							-.3225444597435E+02	-.81730286E-05	-.322544452767464E+02	-.31973570E+01	.85289692E-01
6820	DRAG							.94609131856769E-02	-.552555057E-08	.94609076601712E-02	.24344497E-03	.41173920E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820 X	.30953062E+04	.31567975E+03	.26949688E+04	.87066282E+00	.35378317E+00
6820 Y	.63136182E+03	.46290205E+03	.15809026E+03	.36649109E+00	.34151991E+00
6820 Z	.2972209 E+03	.33812934E+03	.85572948E+03	.28791027E+01	.25307756E+01
6820 DX	.3337998 E+00	.38637129E+00	-.87130488E+00	-.26102618E+01	-.22550974E+01
6820 DY	.12431271E+01	.12692153E+01	-.10292059E+01	-.82791691E+00	-.81689941E+00
6820 DZ	.35311826E+01	.35782622E+01	-.31979570E+01	-.91563334E+00	-.89371791E+00
6820 URAG	.58941494E-03	.58941494E-03	.24344497E-03	.41302816E+00	.41302816E+00

RESIDUAL RMS =	.6607756855E+00
RESIDUAL SOS =	.7859241119E+01
APRIORI RMS =	.1000895035E+01
APRIORI SOS =	.7012936101E+01
TOTAL SOS =	.148717722E+02
PREDICTED SOS =	.148717717E+02

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

6820 X	.46320E-01	6820 Y	.6020 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 Y	.12528E-01	.35193E-01	.67555E-01	.20240E+05	.17517E+05	.21619E+05	.28914E+08
6820 Z	-.10609E-01	.27983E-01	-.16989E+02	.90208E+04	.61704E+04	.56050E+06	.61490E+00
6820 DX	.19313E+02	.37247E+01	-.16989E+02	.20240E+05	.17517E+05	.21619E+05	.28914E+08
6820 DY	.16069E+02	.21328E+02	.15509E+02	.90208E+04	.61704E+04	.56050E+06	.61490E+00
6820 DZ	-.76830E+01	.13397E+02	.37054E+02	-.13147E+05	.61704E+04	.56050E+06	.61490E+00
6820 DRAG	-.41838E+03	.16167E+03	.98555E+03	-.43966E+06	-.57036E+05	.30988E-02	.78592E+01
ATB	-.29748E-04	-.20918E-04	-.88262E-05	-.23391E-01	-.23512E-01	.30988E-02	.61490E+00

ATA INVERSE

6820 X	.75079E+02	6820 Y	.6020 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 Y	.49000E+01	.15209E+03	.15187E+04	.17581E-02	.0839E-02	.72742E-02	.16953E-06
6820 Z	.20715E+03	-.84417E+02	-.10677E+01	-.12873E-02	-.16091E-02	.30196E-06	.16953E-06
6820 DX	-.11070E+00	.25894E+00	-.16293E+00	.17581E-02	.0839E-02	.72742E-02	.16953E-06
6820 DY	-.83529E-01	-.37127E+00	-.30310E+01	.31672E-02	-.16091E-02	.30196E-06	.16953E-06
6820 DZ	-.34426E+00	.35854E+00	-.30310E+01	.31672E-02	-.16091E-02	.30196E-06	.16953E-06
6820 DRAG	-.11803E-02	-.16532E-02	-.54754E-02	-.38723E-05	.10289E-04	.30196E-06	.16953E-06

CORRELATION MATRIX

6820 X 1.00000
 6820 Y .04586 1.00000
 6820 Z .61344 -.17565 1.00000
 6820 DX -.30469 .50075 -.65340 1.00000
 6820 DY -.23495 -.73372 .11198 -.74823 1.00000
 6820 DZ -.46594 .34688 -.01189 .88565 -.45982 1.00000
 6820 DRAG -.33084 -.32558 -.34123 -.22430 .60902 .00860 1.00000

ENTER SEGMENT 04 AT 5.5 SECONDS. EXECUTION TIME FOR SEGMENT #3 WAS .0 CP SECS.

A7A INVERSE UPDATED TO 500.74 MINUTES FROM MIDNIGHT OF EPOCH

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.75352E+04	.48176E+03	.56034E+04	.23166E-01	.65730E-03	.52821E-02	.16953E-06
-.14908E+04	-.34064E+04	.10604E+02	.33877E-02	.12298E-02	-.54047E-05	
.60784E+04	-.25608E+01	.15167E+01	.92051E-02	.12298E-02		
.13201E+02	-.26673E+00	.52459E+01	-.15155E-04	-.59057E-05		
.19277E+01	-.13525E+01	-.11955E-01				
.51825E+01	.66550E-02					
-.23175E-01						

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.78246E+04	.13243E+05	74329E+04	.41201E-01
-.96415E+04	0.		-.20402E-01
0.	0.	0.	0.
.17437E+02	-.20776E+02		.10712E-01
-.91552E+01	.11281E+02		0.
0.	0.	.58474E+01	.19176E-01

PARAMETER SET COORDINATE SYSTEM

.16473E-1
 .69271E-11 .19750E-10
 .21336E-10 .61505E-11 .28057E-10
 .22445E-11 .11556E-11 .26535E-11
 .54055E-12 .11236E-11 .49211E-12 .32562E-12
 .11590E-11 .34357E-12 .14631E-11 .97225E-13
 .16999E-13 .15783E-12 .16999E-13 .17612E-13

***. ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ***

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	AN	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-DOT
1970/ 6/26	21495717.114	5.657163506	21797285.075	.0122957499983	58.24076095	3663.69744
15/ 0	2125373.124	.030751110	.02127520963	-.0173693664702	59.32922068	227.68846
44.694.030	282.643	88.951419980	118.840776953	.0667983727789	60.313449092	3511.84967
.0007562	1286.1091971	198.848776950	185.656927094	3.553493457	89.3225473	74.98629
226.151867	-8211.4289637	21560728.370	119.615715412	-.13733735965	89.6836302	2.7933472359
104.5167	-24304.0023914	25639.7712610	886.2034378	-1.39123356209	89.7157996	-2.0669831961

LEAST SQUARES PROCESS CONVERGED.

TOTAL ECIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
313	5 RNG	2.1E+01	1.0E+00	-6.6E-01	5 EL	8.9E-03	0.	-5.5E-03
313	5 SRR	5.3E-02	5.3E-01	2.1E-02	5 SRR	3.3E-02	3.3E-01	-3.4E-03
393	5 AZ	9.1E-02	0.	9.1E-02	5 EL	2.4E-02	0.	-1.3E-02
393	3 RNG	8.1E+00	4.1E-01	-3.2E+00	5 SRR	3.3E-02	3.3E-01	-3.4E-03

STATION 313 PAGE 1

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
RNG	0	-.422278908	.03141500E+00	-.6571398E+00	.40913610E+02
AZ	1	-.42256725E-1	.20993823E-03	-.31753214E-01	-.2125693E-01
EL	2	-.19483211E-1	.27881689E-03	-.5542366E-02	.83984781E-02
SRR	3	-.77414358E-1	.19583505E-02	.23503126E-01	.11842065E+00
53472	*
53482	*
53492	*
53502	*
53512	*
53522	*
53532	*
53542	*
53552	*
53562	*
53572	*
53582	*
53592	*
53602	*
53612	*
53622	*
53632	*
53642	*

STATION 393 PAGE 1

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
AZ	0	.65166516E-1	.50850711E-03	.99591862E-01	.11601722E+00
EL	1	-.53078909E-1	.79851344E-03	-.13133237E-01	.26012435E-01
SRR	2	-.69479148E-1	.1322093E-02	-.33686846E-02	.62741779E-01
RNG	3	-.18091632E+2	.29927194E+00	-.31780344E+01	.11735563E+02
52760	*
52770	*
52780	*
52790	*
52800	*
52810	*
52820	*
52830	*
52840	*
52850	*
52860	*
52870	*
52880	*

EXIT SEGMENT 84 AT 5.6 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

REFERENCE
SECTION

DESCRIPTION

ITEM

17 An example of the printer plot of the measurement residuals for the last iteration (see Case B, Item 20, for a full explanation)

2.2.1

11.1.2

15

ENTER SEGMENT 10 AT 5.6 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

* PREDETERMINED EVENT TABLE *

ASSOCIATED QUANTITIES

TIME(MME) TYPE
879.0000 IZERO
1621.2182 ISTOP

*** TRAJECTORY START

SEG#	ENTRY	TIME	IS	T	ECI	H	NSSTEP	DT
1	STEP	5.64200	00URLED	982.250000		.250000	25	
1	STEP	00URLED		809.250000		.500000	52	
1	NODE	T =	.900745093793E+03	.214557320668E+08	.212927764464E+07			-1.63423225258E-04
1	DT		.500000000000E+00	.126581028242E+04				-1.43060023909E+05
1	STEP	00URLED		T =	H =	1.000000	162	
1	NODE	T =	.946658588135E+03	-.218803714357E+08	-.22005923323E+07			.125779257434E-01
1	DT		.200000000000E+00	-.345907455384E+03	.014265712192E+04			.238320373837E+05
1	NODE	T =	.997458993524E+03	.214489766159E+08	.219046453027E+07			-.203249489554E+00
1	DT		.100000000000E+00	.131064337857E+04	-.020810237125E+04			-.243712204050E+05
1	NODE	T =	.11363669922E+04	-.218706977640E+08	-.226695434615E+07			-.589911761112E-01
1	DT		.100000000000E+00	-.371226613584E+03	.014293063106E+04			.238341151012E+05
1	NODE	T =	.108016391563E+04	.214421025123E+08	.225584277690E+07			-.863067201429E-01
1	DT		.100000000000E+00	.133502110587E+04	-.020410225153E+04			-.243065075936E+05
1	NODE	T =	.11260655271E+04	-.21860898722E+08	-.233339405702E+07			-.101487221398E+05
1	DT		.100000000000E+00	-.336800004154E+03	.014245997901E+04			.238364978992E+05
1	NODE	T =	.116985963199E+04	.214354461178E+08	.232115326113E+07			-.183242366425E-01
1	DT		.100000000000E+00	.135985239073E+04	-.019580465312E+04			-.243754490028E+05
1	NODE	T =	.121575693757E+04	-.218505799153E+08	-.239962253565E+07			-.349275773535E-03
1	DT		.100000000000E+00	-.421904305512E+03	.014166299668E+04			.238391830641E+05
1	NODE	T =	.125954792133E+04	.214287958496E+08	.238672039595E+07			-.147720489610E+00
1	DT		.100000000000E+00	.138359662734E+04	-.019456210999E+04			-.243743612622E+05
1	NODE	T =	.131543942259E+04	-.218400481221E+08	-.24651020583E+07			-.153969776460E-01
1	DT		.100000000000E+00	-.447494361867E+03	.014101306788E+04			.238419324156E+05
1	NODE	T =	.134922819215E+04	.214216538875E+08	.245314069009E+07			-.13185454353E+00
1	DT		.100000000000E+00	.140705124634E+04	-.018082963050E+04			-.243733933899E+05
1	NODE	T =	.13951173974E+04	-.218293481956E+08	-.253158939874E+07			-.198257516319E+00
1	DT		.100000000000E+00	-.473738187344E+03	.0135980303747E+04			.238448004244E+05

NODE	T =	.1438897737645E+04	.214142223518E+08	.251756189895E+07	.238869289165E-01
DT =	.1000000000000E+01	.143189662466E+08	.143189662466E+08	-.818469744355E+04	-.243722798809E+05
NODE	T =	.148477523597E+04	-.218185158357E+08	-.259856294727E+07	-.426712096486E-02
DT =	.1000000000000E+01	.1499282763766E+03	-.499282763766E+03	.812348091137E+04	.238474219867E+05
NODE	T =	.152855981410E+04	.214068999350E+08	.256374667414E+07	-.139505778209E+00
DT =	.1000000000000E+01	.145653788076E+04	.145653788076E+04	-.817537123394E+04	-.243710299133E+05
NODE	T =	.15744323333E+04	-.218172374883E+08	-.266469893192E+07	-.17896111444E-01
DT =	.1000000000000E+01	.161821345867E+04	-.52441908623E+03	.81378396726E+04	.239502272862E+05
NODE	T =	.1600000000000E+01	.213994585329E+08	.264837440794E+07	-.124191763445E+00
DT =	.1000000000000E+01	.148056649020E+04	.148056649020E+04	-.817509952422E+04	-.242996054642E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .915 SECONDS TO INTEGRATE A SPAN OF 742.750 MINUTES ***

*** FROM 879.030 TO 1621.750 MINUTES FROM MIDNIGHT OF EPOCH ***

*** TRACE56 EPHEMERIS OUTPUT KEY ***

DATE,...	ME,MM,ST,DT	X,Y,XD	X,XD - 8F	ADBARV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (NM)	PERIOD-DECAY	.
	STEP SIZE (MIN)	XO (FT/SEC)	XO (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	MOD-REG	.
IT	UTC - IT	YO (FT/SEC)	YO (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZO (FT/SEC)	ZO (FT/SEC)	V (FT/SEC)	O (DEG)		

*** CASE 1

 *** EPOCH PRINT
 *** REQUESTED PRINTS

 *** ECI TRAJECTORY ***

DATE,...	ME,MM,ST,DT,...	X,XC	X,XD - BF	ADBARV	LAT,...	REV,...
70/ 6/2E	U.00000	- .859177872E+06	.552943353E+07	97.13607771	71.23532964	.24863
14/39	879.00000	.- .86265812E+07	-.415447066E+07	71.11799655	323.08108931	0.00000
0.00000	52740.00000	.232213836E+08	.232213936E+08	90.56864399	83.70774013	0.00000
	.12500	.257565325E+05	-.164017950E+05	271.44211206	71.23274551	0.00000
IT	0.00000	.251961997E+04	-.236658767E+05	.21371444E+08	108.87579657	
	0.00000	-.322144446E+02	-.3222544446E+02	.25879519E+05	51.55699698	
A =	.21737498E+08	MEAN ANCM =	.33005906E+03	APOGEE =	.36474584E+04	
E =	.19545978E-01	ECCENTRIC =	.32949051E+03	HEIGHT =	.21121842E+03	
I =	.10887580E+03	TAUE ANOM =	.32891708E+03	PERIGEE =	.35076057E+04	
O =	.18561199E+03	KEFL PER =	.9453242E+02	HEIGHT =	.71365690E+02	
U =	.12358975E+03	ANCM PER =	.89692362E+02	U-DOT =	.28238268E+01	
TAU =	.79699652E+03	NCOL PER =	.19724174E+02	U-DOT =	-.20003583E+01	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
70/ 6/2E	21.74509	.214557321E+08	-.119366771E+08	5.656692696	-.00000039	.50000
15/ 0	90.74509	.212527759E+07	-.155488551E+08	-.00000039	226.15078160	0.00000
44.70563	5404.70563	-.147473157E+00	-.147473157E+00	88.95141266	104.51754274	0.00000
	.50000	.128561810E+04	-.744391549E+04	198.84877695	-.00000039	0.00000
IT	0.00000	-.821146374E+04	.649884239E+04	.21560734E+08	108.84667950	
	0.00000	-.243080024E+05	-.243080024E+05	.25689695E+05	46.15078174	
DELTA NODE =	.013	DELTA V =	-89.7141			

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
70/ 6/2E	111.45900	.214489767E+08	-.137216942E+08	5.93139148	-.00000693	1.50000
16/30	990.45900	.219146382E+07	-.871272125E+07	-.00000699	203.8355595	0.00000
27.53971	59427.53971	-.259150097E+01	-.259150197E+01	88.55178468	104.48516846	0.00000
	1.00000	.131864051E+04	-.41879149E+04	198.85054353	-.00000693	0.00000
IT	0.00000	-.326811268E+04	.833922557E+04	.21561537E+08	108.85038759	
	0.00000	-.243072214E+05	-.243072214E+05	.25689136E+05	23.8355595	

ITEM	DESCRIPTION	REFERENCE SECTION
18	<p><u>Delta Node</u> is the difference between the predicted node time and the <u>input node time</u></p> <p><u>Delta V</u> is the difference in velocity at the predicted and input node times</p>	2.2.11.1

DELTA NODE =		-.011		DELTA V =		-.0002				REV,....		OSC NODE	
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	BF	REV,....	OSC NODE					
70/ 6/26	201.16392	.214421628E+08	-.215528327E+08	6.09577563	..00001374	2.50000	2.50000	0.00000					
15/ 0	1080.16392	-.25584114E+07	-.572707417E+06	-.00001295	161.52212002	89.70841	89.70841	0.00000					
3.33519	04859.83519	-.487416521E+01	-.437416521E+01	88.95319054	104.46935725	0.00000	0.00000	.17460					
IT	1.00000	.133501531E+04	-.73338886E+03	198.85099714	-.00001394	106.8475333	106.8475333						
	.00000	-.820410289E+04	.985501748E+04	.215604439E+05	1.52212444								
	.00000	-.243065077E+05	-.243065077E+05	.25683439E+05									
DELTA NODE =		-.036		DELTA V =		-.0005							
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	BF	REV,....	OSC NODE					
70/ 6/26	29.85963	.214354463E+08	-.211570499E+08	6.48023193	..00000957	3.50000	3.50000	0.00000					
19/29	1163.85963	.232115205E+07	-.765241429E+07	-.00001951	159.21125520	89.69853	89.69853	-.00988					
51.57806	70191.57806	-.35766384E+01	-.357806384E+01	88.95336690	104.52073191	-.00988	-.00988	.17467					
IT	1.00000	.135984799E+04	.376464178E+04	198.85099939	-.00000957	106.8414924	106.8414924						
	0.00000	-.819960514E+04	.933449343E+04	.21560754E+08	108.8414924								
	0.00000	.243065490E+05	-.243065490E+05	.25683714E+05	339.21125844								
DELTA NODE =		-.073		DELTA V =		-.0012							
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	BF	REV,....	OSC NODE					
70/ 6/26	38.54792	.214287958E+08	-.215743469E+08	6.35351092	..00000043	4.50000	4.50000	0.00000					
20/59	1253.54792	.238602036E+07	-.147319236E+08	-.00000743	136.9017593	89.69101	89.69101	-.00752					
32.87528	75572.87528	-.159996576E+00	-.159996576E+00	88.95541135	104.59832840	-.00752	-.00752	.17449					
IT	1.00000	.138359652E+04	.640159544E+04	198.84955597	-.00000043	108.8305144	108.8305144						
	0.00000	-.819456211E+04	.752649396E+04	.21561224E+08	108.8305144								
	0.00000	.243064361E+05	-.243064361E+05	.25685933E+05	336.9017517								
DELTA NODE =		-.123		DELTA V =		-.0020							
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	BF	REV,....	OSC NODE					
70/ 6/26	470.22819	.214216533E+08	-.837383837E+07	6.52865239	..00000493	5.50000	5.50000	0.00000					
22/29	1349.22819	.245154134E+07	-.196052934E+08	-.00000480	114.59676720	89.68198	89.68198	-.00912					
13.69145	90933.69145	.190333638E+01	-.190533638E+01	88.95886518	104.64070810	-.00912	-.00912	.17288					
IT	1.00000	.140705351E+04	.877935830E+04	198.84899737	..00000493	6.50000	6.50000	0.00000					
	0.00000	-.818562935E+04	.453105004E+04	.21561477E+08	108.84899737								
	0.00000	-.243033933E+05	-.243033933E+05	.25684782E+05	294.59876556								
70/ 6/26	559.89774	.214142223E+08	-.862508573E+06	6.701141	..00000142	6.50000	6.50000	0.00000					
23/58	1438.89774	.251756217E+07	-.215444451E+08	-.00001141	92.29255136	89.67197	89.67197	-.00991					
53.86424	86333.86424	.531300917E+00	.531300917E+00	88.95938690	104.67714663	-.00991	-.00991	.17518					
IT	1.00000	.143185722E+04	.934165099E+04	198.84891398	..00000142	6.50000	6.50000	0.00000					
	0.00000	-.818409737E+04	.860814736E+03	.21561703E+08	108.79783419								
	0.00000	-.243022799E+05	-.243022799E+05	.256837465E+05	272.29254597								

DELTA NODE = -.203 DELTA V = -.0034

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	AOBARV	LAT,...	REV,...	DSC NODE
70/ 6/27	649.55981	.21406907E+08	.737797002E+07	6.80029536	-.0000350	7.50000	
1/28	1528.55981	.258304619E+07	.202606282E+08	-.00007366	69.99075908	89.66484	
33.50090	5313.50990	-.137648336E+01	-.137648336E+01	88.59906531	104.75522760	-.00713	
IT	1.0 J000	.145653643E+04	.943119771E+04	198.84691285	-.00000368	.17673	
	0.0 J000	-.217937142E+04	-.293325337E+04	.21562177E+08	108.8471296		
	0.00000	-.243010299E+05	-.243010299E+05	.25681972E+05	249.99075133		

DELTA NODE = -.233 DELTA V = -.0039

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	AOBARV	LAT,...	REV,...	DSC NODE
70/ 6/27	739.21396	.213994588E+08	.145146072E+08	7.05498926	-.0001259	8.50000	
2/58	1618.21396	.264837286E+07	.159460620E+08	-.00007251	47.69055222	89.65710	
12.83771	10692.83771	-.470774157E+01	-.470774157E+01	88.56197225	104.84394478	-.00775	
IT	1.0 J000	.148356096E+04	.751035070E+04	198.84814015	-.0001259	.17475	
	0.0 J000	-.817510032E+04	-.629802904E+04	.21562716E+08	128.845563644		
	.00000	-.242596055E+05	-.242596055E+05	.25680638E+05	227.690556648		

DELTA NODE = -.255 DELTA V = -.0043

TRAJECTORY TERMINATION

A =	.21783497E+08	MEAN ANCH	=	.69639794E+02	APOGEE	=	.36587057E+04
E =	.20530278E-01	ECENTRIC	=	.70750326E+02	HEIGHT	=	.22279347E+03
I =	.10884909E+03	TRUE ANOM	=	.71364713E+02	PERIGEE	=	.35114994E+04
O =	.18705511E+03	KEPL PER	=	.89737334E+02	HEIGHT	=	.75587163E+02
U =	.11848189E+03	ANCH PER	=	-.89611976E+02	0-DOT	=	.27994103E+01
TAU =	.16033909E+04	MODL PER	=	.99644152E+02	U-DOT	=	-.24171365E+01

END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 6.8 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .2 CP SECS.

ENTER SEGMENT 10 AT 6.0 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .3 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

* PREDETERMINED EVENT TABLE *

ASSOCIATED QUANTITIES

TIME(MME) TYPE
 900.7449 TZERO
 993.4592 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS	6.85500	.214557320664E+08	.212527764462E+07	.351509407213E-94
NODE T =	.900745093793E+03	.128580228169E+04	H =	-.243780023907E+05
DT =	.12500000000E+00	T = 904.744900	H =	NSTEP = 31
STEP DOUBLED		T = 908.994900	H =	NSTEP = 47
STEP DOUBLED		T = 944.994900	H =	NSTEP = 118
STEP DOUBLED		T = 944.994900	H =	NSTEP = 118
NODE T =	.946658580097E+03	-218803714253E+08	-220850624666E+07	-.295738054977E-01
DT =	.10000000000E+01	-345907508787E+08	H =	-.238320373956E+05
NODE T =	.990458993426E+03	.214489766135E+08	H =	-.125943909337E+08
DT =	.10000000000E+01	.131164349429E+04	H =	-.2443072284145E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .473 SECONDS TO INTEGRATE A SPAN OF 93.2500 MINUTES ***

*** FROM 500.745 TO 993.955 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 7.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .5 CP SECS.

ENTER SEGMENT 82 AT 7.4 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 4 *****

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RESIDUALS - EXTERNAL UNITS			MME
393 17	1970	6	26	16	7	20.0000	0.	.778958E-01	AZ	967.333
							0.	0.	EL	
393 17	1970	6	26	16	7	19.2528	.519859E+00	0.	SRR	967.321
							.22250E+01	0.		
393 17	1970	6	26	16	8	4.0000	.446224E+03	.747379E-01	AZ	968.067
							.679392E+03	0.	EL	
393 17	1970	6	26	16	8	3.2507	-.140781E+00	0.	SRR	968.054
							.501885E+01	0.		
393 17	1970	6	26	16	8	28.0000	.431812E+03	.927567E-01	AZ	968.467
							.528362E+03	0.	EL	
393 17	1970	6	26	16	8	27.2486	-.624195E+00	0.	SRR	968.454
							.775019E+01	0.		
393 17	1970	6	26	16	9	0.0000	.363279E+03	.756500E-01	AZ	969.000
							.221027E+03	0.	EL	
393 17	1970	6	26	16	8	59.2444	-.334749E+01	0.	SRR	968.587
							.117638E+02	0.		
393 17	1970	6	26	16	10	4.0000	.673896E+02	.113288E+00	AZ	970.067
							.516391E+03	0.	EL	
393 17	1970	6	26	16	10	3.2352	-.449521E+01	0.	SRR	970.054
							.604813E+01	0.		

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
393	SRR	.765986E+01	RNG	.513694E+03		
PREDICTED RESIDUAL RMS = .5960568927E+02						

ENTER SEGMENT 83 AT 7.4 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 1
9 MEASUREMENTS WERE USED IN THIS SOLUTION

CURRENT SOLUTION IS

NAME	X	Y	Z	OX	OY	OZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X	Y	Z	OX	OY	OZ	DRAG	.21455717113563E+08	-.46631199E+02	.21455670282464E+08	-.46631099E+02	.78929819E+02
6820	Y	X						.21253731238283E+07	-.2086587E+03	.2125164729618E+07	-.20865807E+03	.76947088E+02
6820	Z							.2826431437326E+03	.15964563E+01	.2842396005202E+03	.15964563E+01	.11451517E+03
6820	OX							.1286159197193E+04	-.19185345E+00	.12859673436397E+04	-.19185345E+00	.14809437E+00
6820	OY							-.8211428963711E+04	-.36884704E+00	-.82117978107534E+04	-.36884704E+00	.44335061E-01
6820	OZ							-.24318072381429E+05	-.1831393E-02	-.24308004212928E+05	-.1831393E-02	.93765791E-01
6820	DRAG							.94609075661712E-02	-.24678299E-03	.92141242731143E-02	-.24673299E-03	.32835328E-03

NAME	X	Y	Z	OX	OY	OZ	DRAG	SIGMA ZERO	SIGMA OENT	TOTAL CORR.	T.C./SIGMAO	T.C./SIGMAD
6820	X	Y	Z	OX	OY	OZ	DRAG <td>.86805251E+02</td> <td>.12145175E+03</td> <td>-.46631099E+02</td> <td>-.53949616E+00</td> <td>-.30559428E+00</td>	.86805251E+02	.12145175E+03	-.46631099E+02	-.53949616E+00	-.30559428E+00
6820	Y	X						.21949089E+02	.9551248E+02	-.20865807E+03	-.95061286E+01	-.21836540E+01
6820	Z							.74856045E+02	.13539311E+03	.15964563E+01	-.21327019E-01	-.11820952E-01
6820	OX							.15220332E+00	.25844331E+00	-.19185345E+00	-.12605076E+01	-.76574965E+00
6820	OY							.25647653E-01	.11173154E+00	-.36884704E+00	-.14381317E+02	-.73012195E+01
6820	OZ							.72678355E-01	.12624897E+00	-.1831393E-02	-.25198699E-01	-.14576251E-01
6820	DRAG							.4117392E-03	.49792486E-03	-.24678299E-03	-.59936724E+00	-.49562295E+00

RESIDUAL RMS = .2241036669E+02
 RESIDUAL SOS = .4520020818E+04
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SOS = .4520020818E+04
 PREDICTED SOS = .3056764551E+02

ATA

6820 X	6820 Y	6820 Z	6820 OX	6820 OY	6820 OZ	6820 DRAG
.67892E+01	.49502E-01	.00680E-01	.18992E+06	.74115E+06	.71263E+07	.46454E+08
.65287E+00	-.33768E-01	-.73920E+02	.36483E+06	.22793E+07	.16291E+08	.45200E+04
-.47921E+00	.93528E+02	-.73920E+02	.11551E+07	.52186E+07	.16291E+08	.46454E+08
.12797E+04	-.19105E+03	.43293E+03	-.26334E+07	.21334E+05	-.50032E+05	-.33427E+06
-.25357E+04	-.58664E+03	.98224E+03	.63761E+01	.21334E+05	-.50032E+05	-.33427E+06
-.79119E+04	-.13479E+04	.12971E+02	-.63761E+01	.21334E+05	-.50032E+05	-.33427E+06
-.18049E+05	.16012E+03	.12971E+02	-.63761E+01	.21334E+05	-.50032E+05	-.33427E+06
.16012E+03	.12971E+02	.12971E+02	-.63761E+01	.21334E+05	-.50032E+05	-.33427E+06

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.62259E+04						
6820 Y	.15792E+04	.59259E+04					
6820 Z	.872.7E+04	.20195E+04	.13114E+05				
6820 DX	.11196E+02	.42725E+01	.16196E+02	.21932E-01			
6820 DY	.30804E+01	.16927E+01	.45008E+01	.55049E-02	.19656E-02		
6820 DZ	.73431E+01	.22693E+01	.18233E+02	.13585E-01	.35492E-02	.87806E-02	
6820 DRAG	.14115E-02	-.42814E-04	.19356E-02	.32074E-05	.12856E-05	.16789E-05	.1782E-06

CORRELATION MATRIX

6820 X	1.00000					
6820 Y	.2662	1.00000				
6820 Z	.96483	.22903	1.00000			
6820 DX	.95780	.37493	.95498	1.00000		
6820 DY	.88028	.49620	.81651	.83843	1.00000	
6820 DZ	.93282	.31472	.95359	.97892	.85432	1.00000
6820 DRAG	.05446	-.00169	.05249	.06596	.39803	.05457

ENTER SEGMENT 84 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

.9 CP SECS.

YEAR/NO/DY	X	Y	Z	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	AF	AG	AN	LO	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	TRUE ANOMALY	KEPLERIAN PER	ANOMALY PER	MODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	U-DOT	U-DOT		
1970/ 6/26	21455670.282			5.656648001						21.77378.583	.012907020147						58.25019728		59.37827505				3663.69455							
15/ 0	2125164.473			.010755345						.02127289999	-.0173630330869						59.37827505		60.35229594				227.80501							
44.6940000		284.240		88.951761166						108.849501195	.0667981268134						60.35229594		85.9228781				3511.06657							
.0007604		1285.9673436		198.849501195						195.656386129	3.4553539325						85.9228781		89.6839588				74.97784							
226.1505472		-8211.7978108		21560661.200						119.636955905	-.13779605544						89.6839588		89.6839588				2.7934261179							
104.5057		-24308.0042128		25689.8112898						885.2885250	-1.39125344564						89.6839588		89.6839588				-2.0667979488							

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
393	5 AZ	8.8E-02	0.	6.7E-32	5 EL	2.0E-02	0.	-1.4E-03	5 SRR	2.5E+00	2.5E+01	-1.3E+00
393	4 RNG	3.6E+02	1.0E+11	3.3E+32								

EXIT SEGMENT 94 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .9 CP SECS.

ENTER SEGMENT 10 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

990.7449 TZERO
993.4592 TSTOP

*** TRAJECTORY START

SEG11	ENTRY TIME	IS	7.55890	ECI	0.212506845015E+07	0.2149001025045E-04
NODE	T =	.900745094888E+03	.123161444365E+04	H =	-.821183276665E+04	-.243300042222E+05
*	STEP	DOUBLED	T =	904.744900	H =	.250000
*	STEP	DOUBLED	T =	908.934900	H =	.500000
*	STEP	DOUBLED	T =	944.994900	H =	1.000000
NODE	T =	.946658421521E+03	-.248905759208E+08	H =	-.220031937841E+07	-.296414957309E-01
NODE	DT =	.100000000000E+01	-.346005828944E+03	H =	.814268754826E+04	.238317650900E+05
NODE	T =	.999459329121E+03	.214489503620E+08	H =	.219025912335E+07	-.126176140433E+00
NODE	DT =	.100000000000E+01	.131048471597E+04	H =	-.620846937396E+04	-.243072204709E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .474 SECONDS TO INTEGRATE A SPAN OF 93.250 MINUTES ***

*** FROM 990.745 TO 993.995 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 8.0 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .5 CP SECS.

ENTER SEGMENT 82 AT 8.1 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 4 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME
393 17	1970	6	26	16	7	20.0000	0.	967.333
393 17	1970	6	26	16	7	19.2528	-.507431E-01 SRR	967.321
393 17	1970	6	26	16	8	4.0000	.425502E+01 RNG	968.067
393 17	1970	6	26	16	8	3.2507	-.119395E+00 SRR	968.054
393 17	1970	6	26	16	8	29.0000	-.377171E+00 RNG	968.467
393 17	1970	6	26	16	8	27.2486	.341970E+00 SRR	968.454
393 17	1970	6	26	16	9	0.0000	-.269536E+01 RNG	969.000
393 17	1970	6	26	16	8	59.2444	-.458300E+00 SRR	968.987
393 17	1970	6	26	16	10	4.0000	-.701134E+01 RNG	970.067
393 17	1970	6	26	16	10	3.2352	-.466441E-02 SRR	970.054

ENTER SEGMENT 83 AT 0.11 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 2
9 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							.2145567 282464E+08	.92491652E-01	.21455670374955E+08	-.46738603E+02	.78930351E+02
6820	Y							.21251644729518E+07	.16091504E-01	.21251644090533E+07	-.20863478E+03	.76946620E+02
6820	Z							.28423961305022E+03	.87796232E-01	.28432739828369E+03	.16842526E+01	.11451511E+03
6820	DX							.12859673436397E+04	.24579873E-03	.12859675094384E+04	-.19161785E+00	.14009628E+03
6820	DY							-.02117978107534E+04	.50299954E-04	-.0211797804534E+04	-.36873674E+00	.44335549E-01
6820	DZ							-.24308004217828E+05	.12568941E-03	-.24308004087139E+05	-.17057099E-02	.93704034E-01
6820	DRAG							.92141246731143E-02	.88942603E-07	.92142136157169E-02	-.24669404E-03	.32034745E-03

NAME	X	Y	Z	DX	DY	DZ	DRAG	SIGMA ZERO	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0	
6820	X							.06805251E+02	.12145175E+03	-.46738608E+02	-.53043065E+00	-.10443273E+00
6820	Y							.21949089E+02	.95551248E+02	-.20863478E+03	-.95053959E+01	-.21634856E+01
6820	Z							.74856045E+02	.13505311E+03	.16842526E+01	.224997807E-01	.12471039E-01
6820	DX							.15220332E+01	.25054331E+00	-.19160785E+00	-.12588927E+01	-.76476859E+00
6820	DY							.25647653E-01	.11173154E+00	-.36879674E+00	-.14379356E+02	-.33007693E+01
6820	DZ							.72678355E-01	.12624897E+00	-.17057099E-02	-.23469297E-01	-.13510684E-01
6820	DRAG							.4173920E-03	.49792486E-03	-.24669404E-03	-.59915122E+00	-.49544432E+00

RESIDUAL RMS = .132433099E+01
 RESIDUAL SDS = .1578424666E+02
 APRIORI RMS = .1453812521E+01
 APRIORI SOS = .1479499593E+02
 TOTAL SDS = .3057124259E+02
 PREDICTED SDS = .3057910301E+02

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.87868E+01	.49481E-01	.30672E-01	.18985E+06	.74107E+06	.71243E+07	.46508E+08
.65260E+00	-.3752E-01	-.72996E+02	-.36473E+06	.22788E+07	.52219E+07	.16261E+08
-.47907E+00	.93493E+02	.13251E+03	-.11547E+07	.85895E+01	.24675E+02	.57351E+02
.12793E+04	-.19098E+03	.43280E+03	-.26348E+07			
-.25351E+04	.18639E+03	.98279E+03	-.10468E-02			
-.79097E+04	-.13415E+04	.10468E-02	-.36341E+01			
-.18059E+05	-.22579E-02					
-.27693E-01						

ATA INVERSE

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.62300E+04	.59208E+04	.13114E+05	.21932E-01	.19656E-02	.87806E-02	.10761E-06
.15792E+04	.21185E+04	.16196E+02	.55048E-02	.35491E-02	.16779E-05	
.87208E+04	.42725E+01	.45008E+01	.13585E-01			
.11196E+02	.16927E+01	.10233E+02	.32044E-05			
.30864E+01	.22692E+01	.19339E-02				
.73431E+01	.22692E+01					
.14102E-02	-.43631E-04					

CORRELATION MATRIX

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
1.00000	.26003	1.00000	1.00000	1.00000	1.00000	1.00000
.96483	.22907	.95498	.83841	1.00000		
.95780	.37484	.95498	.83841	1.00000		
.88127	.49619	.86550	.97051	.95429	1.00000	
.99282	.31472	.55350	.06590	.30879	.05451	1.00000
.05441	-.00173	.05143	.06590	.30879	.05451	1.00000

ENTER SEGMENT 84 AT 8.2 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .9 CP SECS.
 ATA INVERSE UPDATED TO 990.46 MINUTES FROM MIDNIGHT OF EPOCH

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.64488E+04	.20603E+04					
.22545E+04	.51398E+04	.21586E+05				
.10446E+05	.79367E+01	.25567E+02	.33597E-01			
.14193E+02	.25718E+01	.69484E+01	.85926E-02	.24916E-02		
.33610E+01	.29442E+01	.12150E+02	.15859E-01	.38137E-02	.87277E-02	
.71493E+01	.14985E-02	-.27622E-03	-.13003E-04	-.15558E-05	.92745E-06	.10781E-06
.67963E-02						

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.33140E+05	.39768E+06	.31481E+05	.40832E+00	.45369E-01	.43098E-01
-.28250E-18	0.	0.	-.74757E-13	0.	
0.	0.	0.	0.	0.	
.53892E-10	-.38775E+03	0.	0.	0.	
-.38775E+02	.33054E-21	0.	-.74757E-13	.45369E-01	
0.	0.	.60694E-10	0.	0.	

PARAMETER SET COORDINATE SYSTEM

.76544E-10	.15034E-09	.8207E-09	.33260E-11	.38724E-12	.37185E-12
-.84431E-11	.25440E-09	.50821E-10	.30326E-12	.56820E-14	
-.25985E-10	.16972E-10	.51080E-11	-.55433E-15		
-.19090E-11	.19085E-11	.47902E-15			
.15218E-11	.51099E-12				
.50021E-11					

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ***

YEAR/MO/OY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NOODAL PERIOD	U-DOT
1970/ 6/26	21448940.285	5.830716977	21796005.085	.0122908967746	58.37509577	3663.35866
16/30	2190322.224	.000496226	.02124174705	-.0173247199113	59.42292033	227.28738
27.5520000	186.731	88.952055837	108.851268834	.0668042571570	60.47652666	3513.96353
.0004996	1310.7168068	198.851268834	185.830547549	3.728592319	89.8146355	74.89225
203.8346400	-8208.4446951	21560485.867	119.522948988	-.14202902182	89.6757341	2.7942694148
104.4768	-24307.2205315	25689.2489736	975.8954835	-1.35087350274	89.7078954	-2.0868271786

LEAST SQUARES PROCESS CONVERGEC.

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
393	5 AZ	8.8E-02	0.	8.7E-02	5 SRR	2.9E+00	2.5E+01	-1.6E+00
393	4 RNG	3.6E+02	1.0E+01	3.3E+02	5 SRR	2.9E+00	2.5E+01	-1.6E+00

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
AZ	0	.573879758-01	.58955283E-03	.86865617E-01	.11634326E+00
EL	1	-.422317698-01	.81594036E-03	-.14347512E-02	.39362287E-01
SRR	2	-.55172833E+01	.77994378E-01	-.16175644E+01	.22821545E+01
RNG	3	.20522196E+02	.61460753E+01	.32782596E+03	.63512972E+03
58040	3				
58050	*				
58060	*				
58070	*				
58080	*				
58090	*				
58100	*				
58110	*				
58120	*				
58130	*				
58140	*				
58150	*				
58160	*				
58170	*				
58180	*				
58190	*				
58200	*				

***** END OF PLOT ***** .1 CP SECS.

***** EXECUTION TIME FOR SEGMENT 84 WAS 6.2 SECONDS. *****

EXIT SEGMENT 84 AT 3 2 *****

ENTER SEGMENT 10 AT 6.3 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (HME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

900.7449 TZERO
1710.8623 TSTOP

*** TRAJECTORY START

SEG	11	ENTRY	TIME	IS	ECI	H	H	H	H	NSTEP	NSTEP	NSTEP
				8.28500		.214556853175E+08	.212506645015E+07	.212506645015E+07	.212506645015E+07	.249701825611E-04	.249701825611E-04	.249701825611E-04
				.900745094888E+03		.128561444365E+04	-.821183276665E+04	-.821183276665E+04	-.821183276665E+04	-.243080042222E+05	-.243080042222E+05	-.243080042222E+05
				STEP DOUBLED		T = 904.744900	H = .250000	H = .250000	H = .250000	NSTEP = 31	NSTEP = 31	NSTEP = 31
				STEP DOUBLED		T = 908.994900	H = .500000	H = .500000	H = .500000	NSTEP = 67	NSTEP = 67	NSTEP = 67
				STEP DOUBLED		T = 944.994900	H = 1.000000	H = 1.000000	H = 1.000000	NSTEP = 118	NSTEP = 118	NSTEP = 118
				.946658421520E+03		-.218805759200E+08	-.220031937633E+07	-.220031937633E+07	-.220031937633E+07	-.296384232863E-01	-.296384232863E-01	-.296384232863E-01
				.109000000000E+01		-.346005828829E+03	-.814268754846E+04	-.814268754846E+04	-.814268754846E+04	-.238317650506E+05	-.238317650506E+05	-.238317650506E+05
				.990459328118E+03		.214489593552E+08	.219025912275E+07	.219025912275E+07	.219025912275E+07	-.126178562386E+00	-.126178562386E+00	-.126178562386E+00
				.100000000000E+01		.131048470487E+04	-.820846837513E+04	-.820846837513E+04	-.820846837513E+04	-.243772204715E+05	-.243772204715E+05	-.243772204715E+05
				.103636736627E+04		-.218709584259E+08	-.226677558889E+07	-.226677558889E+07	-.226677558889E+07	-.190145021537E+00	-.190145021537E+00	-.190145021537E+00
				.100000000000E+01		-.371291710440E+03	.814315097110E+04	.814315097110E+04	.814315097110E+04	.238338023711E+05	.238338023711E+05	.238338023711E+05
				.108016482728E+04		.214420970916E+08	.225564089033E+07	.225564089033E+07	.225564089033E+07	-.245077166401E-01	-.245077166401E-01	-.245077166401E-01
				.100000000000E+01		.133489785183E+04	-.820446492012E+04	-.820446492012E+04	-.820446492012E+04	-.243065056935E+05	-.243065056935E+05	-.243065056935E+05
				.112606667318E+04		-.218612080236E+08	-.233322742759E+07	-.233322742759E+07	-.233322742759E+07	-.287888275413E-01	-.287888275413E-01	-.287888275413E-01
				.100000000000E+01		-.396830883000E+03	.814267047935E+04	.814267047935E+04	.814267047935E+04	-.243065056935E+05	-.243065056935E+05	-.243065056935E+05
				.116986136344E+04		.214354619290E+08	.232095482429E+07	.232095482429E+07	.232095482429E+07	-.875129546175E-01	-.875129546175E-01	-.875129546175E-01
				.100000000000E+01		.135976454030E+04	-.819996368210E+04	-.819996368210E+04	-.819996368210E+04	-.243065056935E+05	-.243065056935E+05	-.243065056935E+05
				.121575870823E+04		-.218509581784E+08	-.239546042615E+07	-.239546042615E+07	-.239546042615E+07	.134356494788E-01	.134356494788E-01	.134356494788E-01
				.100000000000E+01		-.421900819519E+03	.814186376282E+04	.814186376282E+04	.814186376282E+04	-.238387888402E+05	-.238387888402E+05	-.238387888402E+05
				.125955022108E+04		.214288330962E+08	.238582544738E+07	.238582544738E+07	.238582544738E+07	-.185496524668E+00	-.185496524668E+00	-.185496524668E+00
				.100000000000E+01		.138354463825E+04	-.819191723647E+04	-.819191723647E+04	-.819191723647E+04	-.243043549345E+05	-.243043549345E+05	-.243043549345E+05
				.130544186880E+04		-.218404794534E+08	-.246502846690E+07	-.246502846690E+07	-.246502846690E+07	-.166951880178E+00	-.166951880178E+00	-.166951880178E+00
				.100000000000E+01		-.447456215326E+08	.814320437566E+04	.814320437566E+04	.814320437566E+04	.238441972547E+05	.238441972547E+05	.238441972547E+05
				.134923230822E+04		.214217126726E+08	-.245134926173E+07	-.245134926173E+07	-.245134926173E+07	-.172003887558E-01	-.172003887558E-01	-.172003887558E-01
				.100000000000E+01		.140703523253E+04	-.8191818057379E+04	-.8191818057379E+04	-.8191818057379E+04	-.243033845498E+05	-.243033845498E+05	-.243033845498E+05
				.139511535951E+04		-.218298360286E+08	-.253144436226E+07	-.253144436226E+07	-.253144436226E+07	-.672241114136E-01	-.672241114136E-01	-.672241114136E-01
				.100000000000E+01		-.473664783942E+03	.81410062519325E+04	.81410062519325E+04	.81410062519325E+04	.238443285028E+05	.238443285028E+05	.238443285028E+05

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NODE T = .1438903341775E+04
DT = .100000000000E+01
NODE T = .148478197219E+04
DT = .100000000000E+01
NODE T = .15285973776E+04
DT = .100000000000E+01
NODE T = .157444108760E+04
DT = .100000000000E+01
NODE T = .16182351636E+04
DT = .100000000000E+01
NODE T = .16640595975E+04
DT = .100000000000E+01
NODE T = .17078692196E+04
DT = .100000000000E+01

.214143730173E+08
.143197618436E+04
-.21819767521E+08
-.499183945199E+03
.214073028286E+08
.145659338644E+04
-.218079394785E+08
-.524274479972E+03
.213995838503E+08
.14806841045E+04
-.217962812645E+08
-.550156266870E+03
.213917629830E+08
.150503006250E+04

.251737365455E+07
-.818504397135E+04
-.259842659783E+07
.813865422107E+04
.258286156986E+07
-.817571371562E+04
-.266457146476E+07
.813890329923E+04
.264819264741E+07
-.817543636605E+04
-.273067911266E+07
.813757464437E+04
.271341376866E+07
-.817111856521E+04

-.243251352040E-01
-.243722684018E+05
.184823510083E-01
.238469054249E+05
-.192848794083E+00
-.243710155487E+05
-.166571505548E+00
.238496698736E+05
.190298708107E-01
-.242299580307E+05
-.468055256516E-01
.233525181497E+05
-.793433913314E-01
-.242298275954E+05

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*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .965 SECONDS TO INTEGRATE A SPAN OF 810.250° MINUTES ***

*** FROM 500.745 TO 1710.995 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 9.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.0 CP SECS

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	HR,MM,SS,DT	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (N°)	PERIOD-DECAY	.
	STEP SIZE (MIN)	XD (FT/SEC)	XD (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	MOD-REG	.
IT	UTC - IT	YD (FT/SEC)	YD (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZD (FT/SEC)	ZD (FT/SEC)	V (FT/SEC)	O (DEG)		

*** ECI TRAJECTORY ***

*** CASE 1 ***

*** EPOCH PRINT

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	0.00000	.214556703E+08	-.149364904E+08	5.65664470	.00076044	.50000
15/ 0	900.74490	.212516447E+07	-.155687417E+08	.00075574	226.15054724	0.00000
44.69400	54044.65400	.284239600E+03	.284239600E+03	86.55176117	104.50566791	0.00000
IT	.12500	.128996734E+04	-.744424983E+04	198.84950120	.00076028	0.00000
	.00000	-.821179781E+04	.649098865E+04	.2156061E+08	108.84950120	
	.00000	-.243080042E+05	-.243080042E+05	.2566881E+05	46.15024052	
A =	.21797339E+08	MEAN ANOM =	.58260157E+02	APOGEE =	.36636945E+04	
E =	.21272900E-01	ECENTRIC =	.59308276E+02	HEIGHT =	.22760581E+03	
I =	.10884950E+03	TRUE ANCP =	.60362206E+02	PERIGEE =	.35110666E+04	
O =	.18565639E+03	KEPL PER =	.89822878E+02	HEIGHT =	.74977836E+02	
U =	.11963700E+03	ANCP PER =	.89883959E+02	O-DCT =	.27934261E+01	
TAU =	.89620852E+03	NOOD PER =	.89716126E+02	U-DCT =	-.20667979E+01	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	0.00019	.214556853E+08	-.149365774E+08	5.65639613	.00000000	.50000
15/ 0	900.74509	.212506845E+07	-.155686657E+08	.00000000	226.15024052	0.00000
44.70569	54044.70569	.249001808E+04	.249001808E+04	88.95175381	104.50659261	0.00000
IT	.12500	.128561444E+04	-.744424894E+04	198.84950119	.00000000	0.00000
	.00000	-.92183277E+04	.649098959E+04	.21560667E+08	108.84953480	
	.00000	-.243080042E+05	-.243080042E+05	.25668805E+05	46.15024052	

DELTA NODE = .013 DELTA V = -89.7141

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	89.71443	.214489506E+08	-.197217459E+08	5.83054327	-.00001264	1.50000
16/30	990.45333	.219025757E+07	-.871248832E+07	-.00001255	203.83443330	0.00000
27.55988	59427.55988	-.472287522E+01	-.472287522E+01	88.95205094	104.47743549	0.00000
IT	1.00000	.131047919E+04	-.441872337E+04	198.85125894	-.0001263	0.00000
	.00000	-.820846896E+04	.83963313E+04	.21560490E+08	108.8487665	
	.00000	-.243072205E+05	-.243072205E+05	.256685245E+05	23.83443767	

DELTA NODE = .009 DELTA V = -89.7052

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
79/ 6/26	179.41993	.21420973E+08	-.215528130E+08	6.00524419	-.0001096	2.50000		
18/ 0	1088.16483	.22556395E+07	-.57242099E+06	-.0000108	181.52136040	89.70694		
9.88981	64809.88981	-.479559499E+01	-.479559499E+01	88.55338154	104.46478428	0.00000		
IT	1.00000	-.133489282E+04	-.731134537E+03	198.85171352	-.0001096	.17481		
	0.00000	-.821446546E+04	-.985537773E+04	.21560414E+08	108.84372393			
	0.00000	-.243165157E+05	-.243065057E+05	.25688546E+05	1.52136411			

DELTA NODE = .019 DELTA V = -89.6963

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/20	269.11646	.214354620E+08	-.271569164E+08	6.17970566	-.00000244	3.50000		
19/29	1169.86136	.232195455E+07	-.765274995E+07	-.00000242	159.21023533	89.69931		
51.68184	70191.68184	-.912413357E+00	-.912413357E+00	88.55340062	104.51999436	-.00964		
IT	1.00000	-.135976345E+04	-.316496424E+04	198.85161678	-.00000244	.17488		
	0.00000	-.819596379E+04	-.939474601E+04	.21560749E+08	108.83489710			
	0.00000	-.243054449E+05	-.243054449E+05	.25687410E+05	335.21029616			

DELTA NODE = .031 DELTA V = -89.6886

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/26	358.80582	.214288330E+08	-.157431650E+08	6.35290695	.00000435	4.50000		
20/59	1259.55072	.238582606E+07	-.147322709E+08	.00000433	136.89984942	89.69293		
33.04319	75573.04319	-.162767580E+01	-.162767580E+01	88.55544874	104.60096574	-.00727		
IT	1.00000	-.138354675E+04	-.640200088E+04	198.85029451	.00010435	.17450		
	0.00000	-.819491698E+04	-.752659943E+04	.21561240E+08	108.82137302			
	0.00000	-.243043549E+05	-.243043549E+05	.25686038E+05	316.89994754			

DELTA NODE = .045 DELTA V = -89.6802

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/26	448.48741	.214217126E+08	-.897332123E+07	6.52812349	.00000286	5.50000		
22/29	1349.23231	-.245134954E+07	-.196055704E+08	.00000284	114.59321131	89.66316		
13.93845	80953.93845	-.106826385E+01	-.106826385E+01	88.95872605	104.64674163	-.00887		
IT	1.00000	-.140703647E+04	-.877978738E+04	198.84962791	.00000286	.17280		
	0.00000	-.819018042E+04	-.453177263E+04	.21561514E+08	108.80471249			
	0.00000	-.243033845E+05	-.243033845E+05	.25684885E+05	294.59321034			

DELTA NODE = .089 DELTA V = -89.6688

```

DATE,... ME,MM,ST,DT,... X,XD X,XD - BF ADBARV LAT,... BF REV,...
70/ 6/26 538.15852 -.214143037E+08 -.861778912E+06 6.70467415 -.00001074 6.50000 DSC NODE
23/58 1438.90342 .251737354E+07 .215445325E+08 -.00000103 92.29030370 89.67349
54.20508 86334.20508 -.339226012E+00 -.339226012E+00 88.55926901 104.68671713 -.00966
IT 1.00000 .143190578E+04 .934202325E+04 198.84874451 -.00000104 .17518
0.00000 -.818104392E+04 .860547767E+03 .21561761E+08 108.84898579
.00000 -.243022684E+05 -.243022684E+05 .25683566E+05 272.29050475
DELTA NODE = .138 DELTA V = -89.6603
    
```

```

DATE,... ME,MM,ST,DT,... X,XD X,XD - BF ADBARV LAT,... BF REV,...
70/ 6/27 627.82241 .214070031E+08 .737884687E+07 6.87976210 -.00001074 7.50000 DSC NODE
1/28 1528.56731 .258286027E+07 .202603940E+08 -.000001967 99.98134783 89.66661
34.03862 5314.03862 -.401596464E+01 -.401596464E+01 88.55966903 104.76339940 -.00688
IT 1.00000 .145658878E+04 .943143079E+04 198.848764484 -.00001174 .17673
0.00000 -.817971359E+04 -.293868518E+04 .21562257E+08 108.84642285
.00000 -.243010156E+05 -.243010156E+05 .25682070E+05 249.98835147
DELTA NODE = .217 DELTA V = -89.6509
    
```

```

DATE,... ME,MM,ST,DT,... X,XD X,XD - BF ADBARV LAT,... BF REV,...
70/ 6/27 717.47862 .213595841E+08 .145154875E+08 7.05446814 -.00001198 8.50000 DSC NODE
2/58 1618.22352 .264819113E+07 .159453987E+08 -.000001190 47.58753614 89.65912
13.41117 10693.41117 -.447732963E+01 -.447732963E+01 88.56159726 104.88063967 -.00750
IT 1.00000 .148165295E+04 .761037231E+04 198.84887339 -.00001197 .17475
0.00000 -.817543706E+04 -.629855848E+04 .21562818E+08 108.84221351
.00000 -.242995881E+05 -.242995881E+05 .25680734E+05 227.68764020
DELTA NODE = .318 DELTA V = -89.6388
    
```

```

DATE,... ME,MM,ST,DT,... X,XD X,XD - BF ADBARV LAT,... BF REV,...
70/ 6/27 807.12481 .213517630E+08 .194805004E+08 7.22901183 -.000010266 9.50000 DSC NODE
4/27 1767.86971 .271341346E+07 .924555265E+07 -.000002264 25.38927320 89.64951
52.18270 16072.18270 -.954935475E+00 -.954935475E+00 88.96277893 104.91796446 -.00961
IT 1.00000 .150502887E+04 .465099874E+04 198.85016274 -.0000266 .17462
0.00000 -.817111871E+04 -.871556180E+04 .21563166E+08 108.83369697
.00000 -.242982755E+05 -.242982759E+05 .25679535E+05 205.38927410
DELTA NODE = .443 DELTA V = -89.6276
    
```

*** TRAJECTORY TERMINATION

A = .21784133E+08 MEAN ANOM = .6406895E+02 APOGEE = .36592199E+14
 E = .20633942E-01 CCENTRIC = .65142122E+02 HEIGHT = .22332311E+03
 I = .10885036E+03 TRUE ANCH = .66220110E+02 PERIGEE = .35111943E+04
 O = .18722902E+03 KEPL PER = .8974261E+02 HEIGHT = .75297496E+02
 U = .11837888E+03 ANCH PER = .8960599E+02 O-DCT = .27993325E+01
 TAU = .16930237E+04 NODL PER = .89637770E+02 U-DCT = -.24706795E+01

*** END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 9.5 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .3 CP SECS.
 ENTER SEGMENT 10 AT 9.5 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .3 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

990.4592 TZERO
 1067.0233 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS 9.56500
 NODE T = .9904593280355+03 .21446950327E+08 .219025916574E+07 .345415535802E-04
 DT = .125000000000E+00 .131049502801E+04 -.620846836465E+04 -.24372205316E+05
 * STEP DOUBLED T = 994.459200 H = .250000 NSTEP = 31
 * STEP DOUBLED T = 998.709200 H = .500000 NSTEP = 47
 * STEP DOUBLED T = 1020.209200 H = 1.000000 NSTEP = 69
 NODE T = .103636736719E+04 -.218709586538E+08 -.226677558081E+07 -.996434377020E-01
 DT = .100000000000E+01 -.371291430118E+03 .814315093846E+04 .238338021858E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .392 SECONDS TO INTEGRATE A SPAN OF 76.7500 MINUTES ***
 *** FROM 990.459 TO 1067.209 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .4 CP SECS.
 ENTER SEGMENT 82 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 5 *****

STAPASS YEAR MO DY HR MM SEC RESIDUALS - EXTERNAL UNITS MME

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

PREDICTED RESIDUAL RMS = 0.
 ENTER SEGMENT 03 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 02 WAS .0 CP SECS.

ITERATION NUMBER 1
 0 MEASUREMENTS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6020	X							.21448940284574E+00	-0.	.21448940284574E+00	0.	.19991533E+03
6020	Y							.2190322239458E+07	-0.	.2190322239458E+07	0.	.27639606E+03
6020	Z							.18673059803602E+03	-0.	.18673059803602E+03	0.	.61727697E+03
6020	DX							.13107168060238E+04	-0.	.13107168060238E+04	0.	.66193016E+00
6020	DY							-.82084446951081E+04	-0.	-.82084446951081E+04	0.	.22269565E+00
6020	DZ							-.24307220531520E+05	-0.	-.24307220531520E+05	0.	.23207673E+00
6020	DRAG							.92142136157169E-02	-0.	.92142136157169E-02	0.	.43152294E-03

NAME	SIGMA ZERO	SIGMA DEBT	TOTAL CORR.	T.C./SIGMA	T.C./SIGMA	T.C./SIGMA
6020	X	.80304656E+02	.19991533E+03	0.	0.	0.
6020	Y	.84025871E+02	.27639606E+03	0.	0.	0.
6020	Z	.14692307E+03	.61727697E+03	0.	0.	0.
6020	DX	.1832916E+00	.66193016E+00	0.	0.	0.
6020	DY	.49916415E-01	.22269565E+00	0.	0.	0.
6020	DZ	.93422328E-01	.23207673E+00	0.	0.	0.
6020	DRAG	.32834745E-03	.43152294E-03	0.	0.	0.

RESIDUAL RMS = 0.
 RESIDUAL SOS = 0.
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SOS = 0.
 PREDICTED SOS = 0.

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 OZ	6020 DRAG
6020 X	.42654E-02						
6020 Y	.43729E-03	.72200E-04					
6020 Z	.35167E-04	.47189E-05	.31884E-04				
6020 DX	.86672E-01	-.15421E-03	-.27604E-01	.32051E+02			
6020 DY	-.11819E+01	-.12293E+00	-.12498E-01	-.23336E+02	.35021E+03		
6020 OZ	-.34489E+01	-.35443E+00	-.27134E-01	-.71943E+02	.95440E+03	.28076E+04	
6020 DRAG	.17261E+03	.17276E+02	-.52806E+00	.55206E+04	-.47603E+05	-.13977E+06	.12492E+06
ATA	-0.	-0.	-0.	-0.	-0.	-0.	-0.

ATA INVERSE

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 OZ	6020 DRAG
6020 X	.39966E+05						
6020 Y	-.14428E+04	.76395E+05					
6020 Z	-.93284E+03	.11654E+06	.38103E+06				
6020 DX	.26085E+00	.13180E+03	.39062E+03	.43815E+00			
6020 DY	.14467E+02	.16500E+02	.44227E+02	.45480E-01	.49593E-01		
6020 OZ	.43655E+02	.66731E+01	.12154E+02	.15792E-01	.45049E-02	.53860E-01	
6020 DRAG	-.67963E-02	-.14995E-02	-.27622E-03	-.13003E-04	-.15558E-05	.92745E-06	-.18621E-06

CORRELATION MATRIX

6020 X	1.00000						
6020 Y	-.02611	1.00000					
6020 Z	-.00756	.68304	1.00000				
6020 DX	.00197	.72040	.95601	1.00000			
6020 DY	.32496	.26807	.32173	.30253	1.00000		
6020 OZ	.94492	.10493	.08484	.10280	.06716	1.00000	
6020 DRAG	-.07878	-.01256	-.00104	-.04552	-.01619	.00926	1.00000

ENTER SEGMENT 04 AT 10.1 SECONDS. EXECUTION TIME FOR SEGMENT 03 WAS .00 CP SECS.

ATA INVERSE UPDATED TO 1064.92 MINUTES FROM MIDNIGHT OF EPOCH

	6820 X	6820 Y	6820 Z	6820 OX	6820 OY	6820 OZ	6820 DRAG
6820 X	.70452E+06						
6820 Y	-.31155E+05	.33116E+05					
6820 Z	-.29886E+06	-.15288E+05	.16949E+06				
6820 OX	-.29719E+03	.18419E+00	.92422E+02	.16470E+00			
6820 OY	-.28220E+03	.16395E+02	.12679E+03	.11297E+00	.16424E+00		
6820 OZ	-.72510E+03	.38832E+02	.34171E+03	.29466E+00	.29235E+00	.81388E+00	
6820 DRAG	-.14836E+00	-.61493E-02	-.63494E-01	-.77262E-04	-.64775E-04	-.15291E-03	.19621E-06

G AND G OWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.29549E+05							
-.30492E+04	.39486E+06						
0.	0.	.28070E+05					
.84176E+01	-.38108E+03	0.	.38510E+00				
-.34574E+02	.35677E+01	0.	-.98430E-02	.40454E-01			
0.	0.	.46071E+01	0.	0.	.32204E-01		

PARAMETER SET COORDINATE SYSTEM

.78319E-09							
-.24473E-10	.55341E-10						
-.29040E-09	.11061E-10	.18480E-09					
-.18272E-10	-.87267E-12	.32239E-11	.63768E-12				
-.16232E-11	.12518E-11	.67533E-11	.32176E-12	.59577E-12			
-.41458E-10	.20712E-11	.19294E-10	.82234E-12	.86483E-12	.25299E-11		

**** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MC/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	U-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	
1978/ 6/26	7592292.341	43.413755895	21743202.958	.0107330266829	355.75494988	3648.41715
17744	7183127.603	60.643103110	-0.1954638714	-0.163359596314	355.67040241	212.67450
1.3979200	18581636.620	90.084563566	108.874728438	.1679477502187	355.58501467	3508.52480
60.8072627	24094.8386435	221.285960530	185.982094698	299.062715447	89.4884613	72.78214
222.9763031	-771.9219982	21319414.735	117.325670862	-1.1457743560	89.6713960	2.8210805775
73.5841	-9590.4692110	25944.8301693	979.5900679	-1.35109474719	89.7132075	-2.0786973168

LEAST SQUARES PROCESS CONVERGED.

EXIT SEGMENT 84 AT 10.1 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.
 ENTER SEGMENT 1. AT 10.1 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

*** TRAJECTORY START ***

TIME(MPE) TYPE ASSOCIATED QUANTITIES
 1064.9233 TZERO
 1083.1645 TSTOP

*** PREDETERMINED EVENT TABLE ***

SEG11 ENTRY TIME IS	STEP	DOUBLE	T	H	ECI	H	NSTEP
10.14930	DOUBLED		1067.273299			.250000	25
	DOUBLED		1071.523299			.500000	41
NODE T =			.214420970673E+08			.225564937777E+07	- .309551067894E-02
CT =			.133489802319E+04			- .82044643492E+04	- .243765058245E+15

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .213 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***

*** FROM 1064.023 TO 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 10.4 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 82 AT 10.4 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RESIDUALS - EXTERNAL UNITS			MME				
343 18	1970	6	26	17	44	23.0000	-.101891E+04	RNG	-.753545E-02	AZ	0.	-.124202E-01	EL	1064.333
							.872341E+03		0.			0.		
							.491889E+01	SRR	0.			0.		
343 18	1970	6	26	17	44	19.2525	.410377E+01		0.			0.		1064.321
							-.897623E+03	RNG	-.758193E-01	AZ	0.	-.210207E-01	EL	1064.667
							.779368E+03		0.			0.		
343 18	1970	6	26	17	44	39.2512	.751119E+01	SRR	0.			0.		1064.654
							.637908E+01		0.			0.		
343 18	1970	6	26	17	44	56.0000	.377207E+03	RNG	-.266531E-01	AZ	0.	-.524774E-01	EL	1065.933
							.341341E+03		0.			0.		
343 18	1970	6	26	17	45	55.2392	.211965E+02	SRR	0.			0.		1065.921
							.163673E+02		0.			0.		
343 18	1970	6	26	17	46	36.0000	.937313E+03	RNG	-.420406E-01	AZ	0.	-.651275E-01	EL	1066.600
							.745369E+03		0.			0.		
343 18	1970	6	26	17	46	35.2336	.103505E+02	SRR	0.			0.		1066.587
							.809252E+01		0.			0.		
343 18	1970	6	26	17	47	32.0000	.132342E+04	RNG	-.361294E-01	AZ	0.	-.661090E-01	EL	1067.533
							.970787E+03		0.			0.		
343 18	1970	6	26	17	47	31.2308	.298569E+01	SRR	0.			0.		1067.521
							.244620E+01		0.			0.		

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

343	RNG	.772325E+03	SRR	.890966E+01		
-----	-----	-------------	-----	-------------	--	--

PREDICTED RESIDUAL RMS = .6845373079E+02

ENTER SEGMENT 83 AT 10.5 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP SECS.

ITERATION NUMBER 1
10 MEASUREMENTS WERE USED IN THIS SOLUTION

CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.75922523410693E+07	.11517256E+04	.75934430666913E+07	.11507256E+04	.29649739E+02
6820 Y	.71831276326843E+07	-.10282883E+01	.71831257743959E+07	-.10282883E+01	.26396897E+02
6820 Z	.1858163662026E+08	-.83642102E+03	.18580800199004E+08	-.83642102E+03	.39504959E+02
6820 DX	.24094838643523E+03	-.20868619E+00	.2409462997333E+03	-.20868619E+00	.12497134E+00
6820 DY	-.77192159115084E+03	-.47311194E+00	-.77239501008648E+03	-.47301194E+00	.26259268E+00
6820 DZ	-.95904692105553E+04	-.14318469E+01	-.95919000578932E+04	-.14303469E+01	.21595331E+00
6820 DRAG	.92142136157169E-02	.14530979E-03	.93601234840369E-02	.14591979E-03	.40531016E-03

NAME	SIGMA ZBRD	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMAD
6820 X	.8393591E+03	.11507256E+04	.13709627E+01	.11243514E+01
6820 Y	.1819789E+03	-.10282883E+01	-.10046705E-01	-.73567279E-02
6820 Z	.4116934E+03	-.83642102E+03	-.29316670E+01	-.16714608E+01
6820 DX	.0583081E+00	-.20868619E+00	-.51421968E+00	-.42398563E+00
6820 DY	.40530984E+00	-.47301194E+00	-.11670379E+01	-.37215276E+00
6820 DZ	.90215315E+00	-.143008469E+01	-.15060355E+01	-.13510559E+01
6820 DRAG	.4315229-E-03	.14590979E-03	.33812755E+00	.33812755E+00

RESIDUAL RMS = .8777415238E+12
 RESIDUAL SOS = .7704371927E+05
 APRIORI RMS = 0.
 APRIORI SOS = 0.
 TOTAL SDS = .7704301827E+05
 PREDICTED SDS = .6706947746E+01

ATA

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.292172-01						
-.45035E-02	.19858E-01					
-.13258E-01	.53896E-02	.12439E-01				
.47193E+01	-.77598E+00	.20907E+01	.43095E+04			
.14339E+J1	.35932E+01	-.87515E+00	-.18952E+03	.29649E+03		
-.25336E+01	.64221E+00	-.59693E+00	-.19689E+04	.82272E+02	.93609E+03	
.86219E+02	.13-25E+03	.30750E+03	.25321E+06	-.10100E+05	-.10545E+05	.25437E+08
.46653E+02	-.37948E+02	-.24734E+02	.57163E+04	.21626E+04	-.34013E+04	-.51695E+05
						.77043E+05

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.87911E+03	.80634E+03	.15610E+01	.79855E-01	.43912E-02	.45636E-01	.16428E-06
.40469E+03	-.39026E+03	.26060E+01	.23439E+01	.24655E-01	-.61675E-02	
.69344E+03	-.17321E+00	-.26060E+01	.43912E-02	.79855E-01	.45636E-01	
-.17610E+01	-.76136E+01	-.31440E+01	.24655E-01	-.61675E-02	.45636E-01	
-.52524E+01	.65437E+00	-.53197E-02	-.13125E-04	-.79211E-05	-.16935E-04	
-.89767E+00	.50442E-03	-.53197E-02	-.13125E-04	-.79211E-05	-.16935E-04	
-.17762E-02	.50442E-03	-.53197E-02	-.13125E-04	-.79211E-05	-.16935E-04	

CORRELATION MATRIX

6820 X	1.00000					
6820 Y	.48066	1.00000				
6820 Z	.59202	-.34789	1.00000			
6820 DX	-.47525	-.04881	-.52785	1.00000		
6820 DY	-.62687	-.94880	.20996	.12434	1.00000	
6820 DZ	-.14020	.10671	-.36853	.91354	-.10106	1.00000
6820 DRAG	-.14780	.04383	-.33224	-.25912	-.19348	1.00000

ENTER SEGMENT 84 AT 10.5 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

YEAR/HR/MIN	X	Y	Z	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	AF	AG	N	L	CHI	PSI	MEAN ANCHALY	APOGEE ANOM	ECCENTRC ANOM	TRUE ANOMALY	KEPLERIAN PER	PERIGEE HEIGHT	PERIGEE ANOM	PERIGEE HEIGHT	PERIGEE ANOM	PERIGEE HEIGHT	PERIGEE ANOM	PERIGEE HEIGHT							
1970/ 6/26	7593443.067	7183125.774	1558080.199	43.405413599	60.640045934	50.084130607	221.286390669	2131094.951	25943.1793895	975.5843667	0.1107339327918	0.163491764330	0.670480122506	2.99065985031	-.14577756705	-1.35110311703	355.77927559	355.63515102	355.63515102	355.61020994	89.0891116	89.6707338	89.7028441	368.41899	212.70943	350.47433	72.73477	2.8211594419	-2.0786362756						
17/44				21743146.308	0.1955793658	108.875079899	185.982349502	117.304259930																											
1.3979200																																			
60.8042163																																			
222.9715808																																			
73.5339																																			

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN											
343	5	RNG	9.7E+02	4.9E+01	1.6E+02	5	AZ	4.4E-02	0.	-1.0E-02	5	EL	4.9E-02	0.					
343	5	SRR	1.1E+01	1.4E+12	9.5E+00														

EXIT SEGMENT 84 AT 10.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 10.15 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

1064.0233 TZERO
1083.1645 TSTOP

*** TRAJECTORY START

STEP	DOUBLED	T = 1067.273299	H = .250000	NSTEP = 25
STEP	DOUBLED	T = 1071.523299	H = .500000	NSTEP = 41
NODE	T = .108016365486E+04	.214420373113E+08	.225573039794E+07	-.303975478830E-02
DT =	.500000000L00E+00	.133527768483E+04	-.820457575669E+04	-.243964633952E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .214 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***

*** FROM 1064.023 TC 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 01 AT 10.8 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 02 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 01 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DY	HR	MN	SEC	RESIDUALS - EXTERNAL UNITS	MME
343	18	1970	6	26	17	44	23.0000	1064.333
343	18	1970	6	26	17	44	19.2525	1064.321
343	18	1970	6	26	17	44	43.0000	1064.667
343	18	1970	6	26	17	44	39.2512	1064.654
343	18	1970	6	26	17	45	56.0000	1065.933
343	18	1970	6	26	17	45	55.2392	1065.921
343	17	1970	6	26	17	46	36.0000	1066.600
343	18	1970	6	26	17	46	35.2336	1066.587
343	18	1970	6	26	17	47	32.0000	1067.533
343	18	1970	6	26	17	47	31.2318	1067.521

ENTER SEGMENT 83 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP S=CS.

ITERATION NUMBER 2
10 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	OY	OZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X	Y	Z	DX	OY	OZ	DRAG	.7593437666913E+07	-.17473217E+00	.75934428919591E+07	.11505579E+04	.29652415E+02
6820	Y							.71831257743959E+00	-.78528587E+00	.71831250091107E+00	-.25935742E+01	.28380447E+02
6820	Z							.185808193004E+08	-.22954129E+06	.18580795969463E+08	-.83665056E+03	.39509778E+02
6820	DX							.24994629957333E+05	-.22830740E+02	.24994632220407E+05	-.20642312E+00	.12498010E+09
6820	OY							-.7723980108648E+03	.10204461E+02	-.77239396964038E+03	-.47199149E+00	.28259765E+00
6820	OZ							-.9591901578832E+04	.34716790E+02	-.95918965862241E+04	-.14273752E+01	.21595791E+00
6820	DRAG							.93601234480069E-02	-.76051947E-06	.93593628885378E-02	-.1451927E-03	.40531444E-03

NAME	X	Y	Z	DX	OY	OZ	DRAG	SIGMA Z850	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820	X	Y	Z	DX	OY	OZ	DRAG	.83935591E+03	.11505593E+04	.13707545E+01	.11241806E+01
6820	Y							.18197897E+03	-.25935742E+01	-.14252760E-01	-.10438948E-01
6820	Z							.41169347E+03	-.83665056E+03	-.21322176E+01	-.16719196E+01
6820	DX							.40583091E+00	-.20642312E+00	-.50864328E+00	-.4193877E+00
6820	OY							.40530758E+07	-.47199149E+00	-.11645202E+01	-.97035550E+00
6820	OZ							.90215315E+00	-.14273752E+01	-.15821873E+01	.1347778E+01
6820	DRAG							.43152294E-03	.14514927E-03	.33636514E+00	.33636514E+00

RESIDUAL	RMS =
RESIDUAL	.6140155352E+00
APRIORI	.377015775E+01
APRIORI	.664943878E+00
APRIORI	.309502136E+01
TOTAL	.6865170811E+01
PREDICTED	.6855143305E+01

ATA

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.29190E-01						
6820 Y	-.44992E-02	.19864E-01					
6820 Z	-.13198E-01	.90833E-02	.12434E-01				
6820 DX	.47059E+01	-.37609E+00	.20929E+01	.43090E+04			
6820 DY	.14332E+01	.15533E+01	-.87924E+00	-.18967E+03	.29638E+03		
6820 DZ	-.25322E+01	.64200E+00	-.59786E+03	-.19687E+04	.82292E+02	.93600E+03	
6820 DRAG	.86061E+02	.13439E+03	.30760E+03	.25316E+06	-.10096E+05	-.10543E+06	.25438E+08
ATA	.46266E-02	-.13627E-01	-.29084E-02	.18222E+01	-.18706E+01	-.99047E+00	-.11216E+02

.37792E+1

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.87927E+03						
6820 Y	.40464E+03	.87545E+03					
6820 Z	.69369E+03	-.38972E+03	.15610E+04				
6820 DX	-.17610E+01	-.17305E+00	-.26069E+01	.15620E-01			
6820 DY	-.52532E+01	-.7696E+01	.23425E+01	.43922E-02	.79861E-01		
6820 DZ	-.89736E+00	.65443E+00	-.31448E+01	.24657E-01	-.61666E-02	.46638E-01	
6820 DRAG	-.17784E-02	.58270E-03	-.53233E-02	-.13125E-04	-.79253E-05	-.16948E-04	.16428E-06

CORRELATION MATRIX

6820 X	1.00000						
6820 Y	.48883	1.00000					
6820 Z	.59210	-.34756	1.00000				
6820 DX	-.47519	-.04879	-.52793	1.00000			
6820 DY	-.62689	-.94880	.20980	.12436	1.00000		
6820 DZ	-.14313	.10678	-.36857	.91355	-.10104	1.00000	
6820 DRAG	-.14797	.04370	-.33242	-.2591	-.16919	-.19362	1.00000

ENTER SEGMENT 84 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 ***** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. *****

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADTUS
HR/MIN	Y	DELTA	E	AG	ECCENTRC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADTUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-NOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-NOT
1970/ 6/26	7593442.892	43.489411209	21743146.599	.0107338089766	355.77973727	3648.44912
17/44	7183125.009	60.648047161	.01955756163	-.0163492876864	355.69563177	212.71063
1.3979200	18580799.969	90.084121532	108.875078675	.0670480199052	355.61068986	3508.47429
60.8042175	24094.6322204	221.286889441	185.982347975	299.065864625	89.4881134	72.73483
222.9719584	-772.3939896	21319094.431	117.303779372	-.1457752670	89.6773556	2.8211591892
73.5308	-9591.8965862	259*5.1801773	975.5842572	-1.39113308952	89.7020459	-2.8786364671

EXIT SEGMENT 84 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 11.0 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .0 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

* PREDETERMINED EVENT TABLE *

TIME (MME) TYPE ASSOCIATED QUANTITIES
 1064.0233 TZERO
 1083.1645 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS 10.98900 ECI ***** NSTEP = 25
 STEP DOUBLED T = 1067.273299 H = .250000 NSTEP = 41
 STEP DOUBLED T = 1071.523299 H = .500000 NSTEP = 41
 NODE T = .108016365736E+04 .214420405147E+08 .225573066533E+07 -.303506639194E-02
 DT = .5000000000 J0E+00 .133527982041E+04 -.620457386845E+04 -.243764682024E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .213 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***
 *** FROM 1064.023 TO 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 11.2 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 82 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - INTERNAL UNITS	MNE
343	18	1970	6	26	17	46	20.0000	1064.333
343	18	1970	6	26	17	46	19.2525	1064.321
343	18	1970	6	26	17	46	40.0000	1064.667
343	18	1970	6	26	17	46	39.2512	1064.654
343	18	1970	6	26	17	45	56.0000	1065.933
343	18	1970	6	26	17	45	55.7392	1065.921
343	18	1970	6	26	17	46	36.0000	1066.600
343	18	1970	6	26	17	46	35.2336	1066.587
343	18	1970	6	26	17	47	32.0000	1067.533
343	18	1970	6	26	17	47	31.2368	1067.521

ENTER SEGMENT 83 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 02 WAS .0 CP SECS.

ITERATION NUMBER 3
 10 MEASUREMENTS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X	Y	Z	DX	DY	DZ	DRAG	.75934428519591E+07	.60785110E-05	.75934428919652E+07	.11593509E+04	.29652486E+02
6820	Y	Z	DX	DY	DZ	DRAG		.7163125108160E+07	.10559320E-03	.71631250092156E+07	-.25934606E+01	.28388447E+02
6820	Z	DX	DY	DZ	DRAG			.18580759969463E+08	-.26003321E-03	.18580759969203E+08	-.83665082E+03	.39509776E+02
6820	DX	DY	DZ	DRAG				.24094632221407E+05	-.10117911E-05	.24094632219395E+05	-.20642413E+00	.12498007E+00
6820	DY	DZ	DRAG					-.7723939851228E+03	-.85849487E-06	-.77239395049887E+03	-.47199235E+00	.28259768E+00
6820	DZ	DRAG						-.9591595852041E+04	-.27485479E-05	-.9591896589527E+04	-.14273780E+01	.21595795E+00
6820	DRAG							.93593628885378E-02	.42636614E-09	.93593633149039E-02	.14514970E-03	.40531414E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0								
6820	X	Y	Z	DX	DY	DZ	DRAG	.83935591E+03	.10234573E+04	.11505509E+04	.13707545E+01	.11241807E+01
6820	Y	Z	DX	DY	DZ	DRAG		.18197897E+03	.24945168E+03	-.25934606E+01	.14251480E-01	-.10438523E-01
6820	Z	DX	DY	DZ	DRAG			.41169344E+03	.50041317E+03	-.83665082E+03	-.20322182E+01	-.16719201E+01
6820	DX	DY	DZ	DRAG				.40583081E+00	.49220109E+00	-.20642413E+00	-.50864577E+00	-.41938962E+00
6820	DY	DZ	DRAG					.40530584E+00	.48656132E+00	-.47199235E+00	-.11645223E+01	-.37005727E+00
6820	DZ	DRAG						.90215315E+00	.10590583E+01	-.14273780E+01	-.15821903E+01	-.13477804E+01
6820	DRAG							.43152294E-03	.43152294E-03	.14514970E-03	.33636613E+00	.33636613E+00

RESIDUAL RMS = .613068263E+00
 RESIDUAL SOS = .375852404E+01
 APRIORI RMS = .6651072091E+00
 APRIORI SOS = .3096573196E+01
 TOTAL SOS = .6855097244E+01
 PREDICTED SOS = .6855097244E+01

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.29198E-01						
6020 Y	-.44992E-02	.19864E-01					
6020 Z	-.13198E-01	.50833E-02	.12434E-01				
6020 DX	.47059E+01	-.27679E+00	.20929E+01	.43090E+04			
6020 DY	.14332E+01	.15533E+01	-.87923E+00	-.18967E+03	.29638E+03		
6020 DZ	-.25322E+01	.64200E+00	-.59786E+04	-.19687E+04	.82292E+02	.93680E+03	
6020 DRAG	.86061E+02	.13439E+03	.38760E+03	.25316E+06	-.10096E+05	-.10543E+06	.25438E+08
6020 ATB	.41392E-05	-.15072E-05	-.23650E-05	.72438E-03	.10839E-03	-.49068E-03	-.12140E-01

.37989E+11

ATA INVERSE

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.87927E+03						
6020 Y	.40464E+03	.60545E+03					
6020 Z	.69369E+03	-.30972E+03	.15610E+04				
6020 DX	-.17610E+01	-.37305E+00	-.26069E+01	.15629E-01			
6020 DY	-.52532E+01	-.76096E+01	.23425E+01	.43922E-02	.79864E-01		
6020 DZ	-.89735E+00	.65443E+00	-.31448E+01	.24657E-01	-.61666E-02	.46638E-01	
6020 DRAG	-.17784E-02	.30270E-03	-.53233E-02	-.13125E-04	-.79253E-05	-.16948E-04	.16428E-06

CORRELATION MATRIX

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	1.00000						
6020 Y	.48003	1.00000					
6020 Z	.59210	-.34756	1.00000				
6020 DX	-.47519	-.04879	-.52793	1.00000			
6020 DY	-.62689	-.94880	.20980	.12436	1.00000		
6020 DZ	-.14013	.10678	-.36857	.91355	-.10104	1.00000	
6020 DRAG	-.14797	.04370	-.33242	-.25910	-.06919	-.19362	1.00000

ENTER SEGMENT 84 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 DATA INVERSE UPDATED TO 1000.16 MINUTES FROM MIDNIGHT OF EPOCH

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.35499E+05	.45207E+05	.46072E+05	.15238E+00	.30491E-01	.42439E-01	.16428E-06
.10500E+05	.56209E+04	.79375E+02	.42516E-01	.14674E-01	-.19563E-04	
.39262E+05	.31827E+02	.15014E+02	.76353E-01	-.16543E-04		
.72910E+02	.35478E+02	.43562E+02	-.67130E-01			
.17093E+02	.63646E+01	-.25810E-01				
.37517E+02	-.11780E-01					
.33922E-01						

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6020

ORBIT PLANE COORDINATE SYSTEM

.43466E+04	.41290E+04	.25101E-01	.99104E-02
-.40126E+04	.40423E+04	-.11651E-01	
0.	0.	0.	
.99574E+01	-.86330E+01	.59505E-02	
-.50857E+01	.46549E+01	0.	
0.	0.	0.	

PARAMETER SET COORDINATE SYSTEM

.93055E-11	.10030E-10	.19853E-12	.85921E-13
.29501E-11	.84679E-12	.43619E-13	.52310E-13
.86308E-11	.11146E-11	.91182E-13	
.12938E-11	.44673E-12		
.28967E-12	.75130E-12		
.65715E-12	.56289E-13		

**** ORIGINAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MO/DY	X	Y	Z	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
1970/ 6/26	21442100.010	6.004383877	21794563.777	0.122634548163	0.0122634548163	50.53440016	3662.97539	
18/ 0	2255315.104	-0.003268904	-0.2120243000	-0.0172617768107	-0.0172617768107	59.55167132	226.93318	
9.8700000	-1229.335	88.952610047	108.892063768	0.0668108839665	0.0668108839665	60.67468046	3510.87230	
-0.0032009	1333.7543378	198.852063799	186.005499332	3.908663117	3.908663117	89.9057269	74.8217	
101.5205826	-8704.7343403	21560398.619	119.398763628	-1.14627750050	-1.14627750050	89.5668466	2.7958204713	
104.4612	-24306.4601608	25688.5299652	1065.5699717	-1.39045372068	-1.39045372068	89.6990060	-2.0671152148	

LEAST SQUARES PROCESS CONVERGED.

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
343	5	RNG	1.4E+01	6.8E-01	3.9E+00	5	AZ	5.4E-02
343	5	SRR	5.3E-02	5.3E-01	1.5E-02	5	EL	3.9E-02
								-3.5E-02

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM	STATION	PAGE
RNG	0	-.22439559E+02	.52546681E+00	.38337818E+01	.30107122E+02		1
AZ	1	-.11550817E+0	.15718191E-02	-.36917213E-01	.41673742E-01		
EL	2	-.78484652E-01	.71150079E-03	-.34909652E-01	.66539697E-03		
SRR	3	-.86777451E-1	.20406317E-02	.15254093E-01	.11728568E+00		
63860						3	
63870						1	
63880						2	
63890						0	
63900						1	
63910						2	
63920						3	
63930						0	
63940						1	
63950						2	
63960						3	
63970						0	
63980						1	
63990						2	
64000						3	
64010						0	
64020						1	
64030						2	
64040						3	
64050						0	

EXIT SEGMENT 84 AT 11.4 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

ENTER SEGMENT 10 AT 11.4 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (HME) TYPE ASSOCIATED QUANTITIES
 1064.0233 TZERO
 1000.4973 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS	11.44500	T	1067.273299	H	.250000	NSTEP	25
STEP	DOUBLED	T	1071.523299	H	.500000	NSTEP	41
NODE	T =	.100016365706E+04	.214420405147E+00	.225873006533E+07	-.302034997340E-02		
NODE	DT =	.500000000000E+00	.133527982039E+04	-.020457386045E+04	-.243064602024E+05		
STEP	DOUBLED	T	1099.023299	H	1.000000	NSTEP	95
NODE	T =	.112606600411E+04	-.218610693671E+00	-.233331033150E+07	-.113569520133E-01		
NODE	DT =	.100000000000E+01	-.396559160804E+03	.014287966114E+04	.238361056031E+05		
NODE	T =	.116985971938E+04	.214353907077E+00	.232404421003E+07	-.116727430991E+00		
NODE	DT =	.100000000000E+01	.136012302726E+04	-.020007391001E+04	-.243054003159E+05		
NODE	T =	.12157541890E+04	-.218050776070E+00	-.239954749100E+07	.49425186410E-02		
NODE	DT =	.100000000000E+01	-.421652153901E+03	.01428070449E+04	.238308596710E+05		
NODE	T =	.12595462676E+04	.214287470693E+00	.238991508462E+07	-.16802096610E+00		
NODE	DT =	.100000000000E+01	.138387961519E+04	-.019102095014E+04	-.243043112346E+05		
NODE	T =	.13054397824E+04	-.218402598802E+03	-.246510553981E+07	-.179400456070E+00		
NODE	DT =	.100000000000E+01	.447234823581E+03	.014424290767E+04	.238415978844E+05		
NODE	T =	.134922918673E+04	.214216117478E+00	.245143920516E+07	-.23712681070E-01		
NODE	DT =	.100000000000E+01	.140734666221E+04	-.019029397504E+04	-.243033419309E+05		
NODE	T =	.139511229908E+04	-.218295752978E+00	-.253351835767E+07	-.415719552178E-01		
NODE	DT =	.100000000000E+01	-.473470711191E+03	.014402947162E+04	.238444586609E+05		
NODE	T =	.143889929261E+04	.214141868977E+00	.251746397605E+07	-.702375450684E-01		
NODE	DT =	.100000000000E+01	.143219402940E+04	-.018151591834E+04	-.243022270766E+05		
NODE	T =	.14847776754E+04	-.218187507642E+00	-.259049755109E+07	.114596971397E-01		
NODE	DT =	.100000000000E+01	-.499017620021E+03	.0133889361458E+04	.238470651492E+05		
NODE	T =	.152856200160E+04	.214068712948E+00	.256295234820E+07	-.175603220512E+00		
NODE	DT =	.100000000000E+01	.145685763952E+04	-.0175937020043E+04	-.243009756176E+05		
NODE	T =	.157443554648E+04	-.218074960176E+00	-.266463922821E+07	-.180128986515E+00		
NODE	DT =	.100000000000E+01	-.524136099269E+03	.0133824973796E+04	.238498592982E+05		


```

NODE T = .161621695088E+04
DT = .100000000000E+01
NODE DT = .166406354981E+04
DT = .100000000000E+01
NODE DT = .170766130670E+04
DT = .100000000000E+01
NODE DT = .17537245239E+04
DT = .100000000000E+01
NODE DT = .179749767323E+04
DT = .100000000000E+01

.213994367270E+08
.14808981692E+04
-.217958962602E+08
-.5580046114581E+03
.213915999808E+08
.150524649161E+04
-.217843490327E+08
-.575642917481E+03
.213834988072E+08
.152916060097E+04

.264428399292E+07
-.61755587226E+04
-.273074395062E+07
.613782797751E+04
.27135056792E+07
-.617124063267E+04
-.279665859533E+07
.613756447812E+04
.277466378426E+07
-.816674010473E+04

.243835445813E-01
-.242995496028E-05
-.212157618508E-01
.238527373047E+05
-.114127474058E+00
-.242982391742E+05
-.932234176636E-02
.23852246979E+05
-.131203734526E+00
-.242971469914E+05

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*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .872 SECONDS TO INTEGRATE A SPAN OF 737.0000 MINUTES ***

*** FROM 1064.623 TO 1801.023 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 12.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .9 CP SECS

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	HE,MM,ST,OT	X,XO	X,XD - BF	ADBARV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (NH)	PERIOD-DECAY	.
	STEP SIZE (MIN)	XD (FT/SEC)	XD (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	NDD-REG	.
IT	UTC - IT	YD (FT/SEC)	YD (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZD (FT/SEC)	ZD (FT/SEC)	V (FT/SEC)	O (DEG)		

*** CASE 1

*** EPOCH PRINT

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADSBV	LAT,..	REV,...
70/ 6/26	0.00000	.759344289E+07	-.764806414E+07	43.40941121	60.80421747	.31365
17/44	1064.02330	.718312501E+07	-.712494034E+07	60.64004716	222.97195040	0.00000
1.39792	63841.39792	.185808000E+08	.185808000E+08	90.88412153	73.53052355	0.00000
	.12500	.240946322E+05	-.246075916E+05	221.28608944	60.80078890	0.00000
IT	0.00000	.772393990E+03	.151403765E+04	.2131994E+08	108.87507868	
	0.00000	-.959189659E+04	-.959189659E+04	.25945180E+05	5.54499517	
A =	.21743147E+08	ME AN ANCH =	.35577974E+03	APOGEE =	.36464491E+04	
E =	.19557962E-01	ECCENTRIC =	.35569563E+03	HEIGHT =	.21270963E+03	
I =	.19887508E+03	TRUE ANCH =	.35961069E+03	PERIGEE =	.35084743E+04	
O =	.18598235E+03	KEPL PER =	.89488113E+02	HEIGHT =	.72734801E+02	
U =	.11738378E+03	ANOM PER =	.89670736E+02	O-DOT =	.28211592E+01	
TAU =	.97558425E+03	NODL PER =	.89702846E+02	U-DOT =	-.20786365E+01	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADSBV	LAT,..	REV,...
70/ 6/26	16.14036	.214420405E+08	..215527613E+08	6.00549935	.21000006	.50000
10/ 9	1080.16366	.225573007E+07	-.572626326E+06	.00000006	101.52190964	0.00000
9.81942	64809.81942	.230045380E-01	.230045380E-01	88.95264149	104.45724719	0.00000
	.50000	.133127985E+04	-.731569387E+03	198.85206376	.00000006	0.00000
IT	0.00000	.620457386E+04	.985550169E+04	.21560367E+08	108.84336396	
	0.00000	-.243064602E+05	-.243064602E+05	.25688558E+05	1.52198952	

DELTA NODE = -.052 DELTA V = -.0009

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADSBV	LAT,..	REV,...
70/ 6/26	105.83642	.14353908E+08	-.201569485E+08	9.17996209	-.00000288	1.50000
19/29	1169.85972	.232104389E+07	.765249304E+07	-.00000236	159.21096388	0.00000
51.58320	70191.58320	-.107809356E+01	-.137809356E+01	88.95279537	104.50992605	0.00000
	1.00000	.136012187E+04	.306461904E+04	.98.85196623	-.00000288	0.00000
IT	0.00000	-.820007404E+04	.939502721E+04	.21560607E+08	108.85222696	
	0.00000	.243064602E+05	-.243064602E+05	.25688558E+05	339.21096495	

DELTA NODE = -.068 DELTA V = -.0011

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/26	195.52513	.214287+73E+08	-.157433235E+08	6.35324341	-.0001173	2.50000	
20/ 59	1259.54843	.238591366E+07	-.147319911E+08	-.00001165	136.90068910	69.69142	
32.90578	75572.90578	-.438376636E+01	-.438376636E+01	88.55481801	104.58844613	0.00003	
IT	1.00000	.138387453E+04	.640178899E+04	198.85063321	-.00001173	.17450	
	0.00000	-.813502954E+04	.752898666E+04	.21567164E+08	106.84888891		
	..00000	-.243043113E+05	-.243043113E+05	.25566050E+05	316.90068477		

DELTA NODE = -.092 DELTA V = -.0015

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/26	285.28599	.214216120E+08	-.897364123E+07	6.52839148	-.0001158	3.50000	
22/29	1349.22919	.245143774E+07	.196053251E+08	-.00001150	114.59425589	89.68236	
13.75138	80953.75138	-.432756937E+01	-.432756937E+01	88.55815109	104.63123614	-.00905	
IT	1.00000	.140734137E+04	.877973059E+04	198.84997498	-.0001157	.17289	
	0.00000	-.819129459E+04	.453222152E+04	.21561424E+08	106.84274223		
	3.30300	-.243033420E+05	-.243033420E+05	.256684898E+05	294.59425981		

DELTA NODE = -.107 DELTA V = -.0018

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/26	374.87599	.214141869E+08	-.862266509E+06	6.70494891	-.00010271	4.50000	
23/58	1438.89929	.251746366E+07	-.215444081E+08	-.0000269	92.29191156	89.67252	
53.95759	86333.95759	-.191202333E+01	-.101202333E+01	88.55875049	104.66947350	-.00984	
IT	1.00000	.143219280E+04	.984213692E+04	198.84909180	-.00010271	.17519	
	0.00000	-.818515932E+04	.861069873E+03	.21561656E+08	108.83250828		
	0.00000	-.243022270E+05	-.243022270E+05	.256683579E+05	272.29191248		

DELTA NODE = -.109 DELTA V = -.0018

DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE
70/ 6/27	464.53870	.214068712E+08	.737823384E+07	6.88094863	-.00010451	5.50000	
1/28	1528.56200	.258295298E+07	.232604898E+08	-.00000448	69.98936552	89.66746	
33.72002	5313.72002	.168762171E+01	.168762171E+01	88.55920725	104.74867934	-.00706	
IT	1.00000	.145685981E+04	.943171991E+04	198.84799115	-.00010451	.17674	
	0.00000	-.817983000E+04	-.293826764E+04	.21562135E+08	108.81834109		
	1.00000	-.243009755E+05	-.243009755E+05	.256682085E+05	245.98996398		

DELTA NODE = -.102 DELTA V = -.0017

DATE,...	ME,MM,ST,DT,...	X, X0	X, X0 - BF	A0BARV	LAT,...	BF	REV,...	DSC MODE
70/ 6/27	554.19355	.213594367E+08	.145148497E+08	7.05476158	.00000215		6.50000	
2/58	1618.21685	.264828417E+07	.159457968E+08	.00000214	47.68950143		89.65779	
13.01102	10693.01102	.804616523E+00	.804616523E+00	88.96119198	104.83843728		-.00767	
IT	0.00000	.148089974E+04	.761061800E+04	198.84921808	.00000215		.17476	
	0.00000	.81755575E+04	.629825321E+04	.21562683E+08	108.80199001			
	0.00000	.242595496E+05	.242995496E+05	.256800749E+05	227.68960070			

DELTA NODE = -.082 DELTA V = -.0014

DATE,...	ME,MM,ST,DT,...	X, X0	X, X0 - BF	A0BARV	LAT,...	BF	REV,...	DSC MODE
70/ 6/27	643.83821	.213916000E+08	.194798050E+08	7.22939829	-.00000283		7.50000	
4/27	1787.86151	.271350225E+07	.924628832E+07	.00000281	25.39162634		89.64801	
51.69044	16071.69044	.109712610E+01	.109712610E+01	88.96243023	104.89325314		-.00978	
IT	0.00000	.150524536E+04	.46515802E+04	198.85097959	-.00000283		.17482	
	0.00000	.817124078E+04	.871542997E+04	.21563016E+08	108.85076564			
	0.00000	.242982392E+05	.242982392E+05	.25679552E+05	205.39162729			

DELTA NODE = -.050 DELTA V = -.0008

DATE,...	ME,MM,ST,DT,...	X, X0	X, X0 - BF	A0BARV	LAT,...	BF	REV,...	DSC MODE
70/ 6/27	733.47438	.213834991E+08	.215317973E+08	7.40324268	-.00001245		8.50000	
5/57	1797.49768	.278846226E+07	.116429879E+07	.00001237	3.09516673		89.63890	
29.86058	21449.86058	.465457882E+01	.465457882E+01	88.96437666	104.93226575		-.00918	
IT	0.00000	.152915515E+04	.996256937E+03	198.85127777	-.00001245		.17436	
	0.00000	.816474083E+04	.982865865E+04	.21563253E+08	108.84890896			
	0.00000	.242971470E+05	.242971470E+05	.2567499E+05	183.09517995			

DELTA NODE = .025 DELTA V = -.89.6236

** TRAJECTORY TERMINATION

A =	E =	I =	O =	U =	TAU =	MEAN ANOM	ECCENTRIC	TRUE ANOM	KEPL PER	ANCH PFR	NOCL PER	APOGEE =	HEIGHT =	PERIGEE =	HEIGHT =	O-DCT =	U-DCT =
.21780897E+08	.20420730E-01	.1088225E+03	.18740337E+03	.1181982AF+03	.17826052E+C4	=	=	=	=	=	=	.36578764E+74	.22206649E+03	.35114730E+74	.75603138E+02	.28010077E+01	-.20714803E+01

*** END OF TRAJECTORY ***

MODEL DATA
DITIN 4
END

IMULTV2

LEMSP1

CARD 1
CARD 2

} ①

***** GENERAL PERTURBATIONS GRAVITY MODEL *****

GM = .553041774E-02 ER**3/MIN**2 = .1407660855E+17 FT**3/SEC**2 = .3986049304E+15 M**3/SEC**2

**** ZONAL HARMONICS ****

EJ2 = .108254900E-02 EJ3 = -.2435000000E-05 EJ4 = -.323200000E-05

***** PHYSICAL CONSTANTS *****

GM(ER**3/MIN**2) = .953039350E-02 OMEGA(RAD/MIN) = .437526910E-02 GMLAT(DEG) = .763000000E+02
GKM(KM**3/SEC**2) = 0. OMEGA(RAD/MIN) = .437526910E-02 GMLNG(DEG) = .291000000E+03
SGM(ER**3/MIN**2) = .680232550E-04 OMEGL(RAD/MIN) = 0. AM(ER) = .272506277E+03
ERFT(FT/ER) = .209257300E+08 ERKM(KM/ER) = .637816490E+04 ERNM(NM/ER) = .344393360E+04
FTKM(FT/KM) = .328083990E+04 FTNM(FT/NM) = .607611550E+04 AE(ER) = .100000000E+01
GSUB0(FT/SEC**2) = .321740000E+02 DGREE(DEG) = .572957795E+02 SLT(ER/MIN) = .202017630E+04
CKEP = .100000000E-10 F = .335232907E-02 PI = .314159265E+01

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = .209257308E+8 VF(I/O-ER/MIN) = .34876210E+06 AF(I/O-ER/MIN**2) = .58127050E+04

***** INTEGRATION INPUTS *****

ICENT = 1 NSTEP = 2
IR = 0 ER = .10000000E-09
HMIN = .15625000E-01 HMAX = .64000000E+02 H0 = .10000000E+01

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPDOT = 0
PRHO = 0 NODPR = 0 CLASS = 0 LEMSP = 1 PTNS = 10100

REFERENCE
SECTION

DESCRIPTION

ITEM

1 Card images of the input MODEL data:

ITIN
MULTV
LEMSP

2.1
2.1.4
2.1.4

***** CRASH ALTITUDE TABLE *****
 (IN FT)
 ECI CRASH ALTITUDE = .30000000E+06 PCI CRASH ALTITUDE = .30000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
 (IN FT)
 BODY(1) CRASH ALTITUDE = .30000000E+06 BODY(2) CRASH ALTITUDE = 0.
 BODY(3) CRASH ALTITUDE = .30000000E+04 BODY(4) CRASH ALTITUDE = 0.
 BODY(5) CRASH ALTITUDE = 0. BODY(6) CRASH ALTITUDE = 0.
 BODY(7) CRASH ALTITUDE = 0.

***** STATION LOCATIONS *****
 STATION SIG REF RA-RBF DATUM TYPE LATITUDE LONGITUDE HEIGHT P 0
 WTS -0 1 1 -0 -0 .3470000E+02 -.1205000E+03 -0.
 AND -0 1 1 -0 -0 .3880000E+02 -.7580000E+02 -0.
 OUM -0 -0 -0 -0 -0 -0. -0.
 ENTER SEGMENT 01 AT .2 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS .2 CP SECS.

***** VEHICLE DATA FOR CASE 1 *****
 IVEHID1 IBTAPES IICYP2
 IYEAR -1973 IMNTH 1 IDAY 1
 IC -96.7506126 3.7345133 88.2980214
 PTIM 0 06.6729057 134623991. 18361.7713
 PTIM 0 1 240 0
 END

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6
 CARD 7

2

3

REFERENCE
SECTION

- | ITEM | DESCRIPTION | REFERENCE
SECTION |
|------|--|----------------------|
| 2 | Printout of station locations as input. If CLASS #0, the actual locations are left blank. This example has a "dummy" station DUM, which is used to illustrate Data Set Types A and R | 4
Item 4 |
| 3 | Card images of input VEHICLE data. Emphasis is on the variable associated with simultaneous-vehicle data generation (ITIN=4), the others having been discussed earlier:

BTAPE | 11.4 |

Preceding page blank

EPOCH
 YR/MO/DAY
 TZME,HR,MIN,SEC
 -1973/ 1/ 1
 0.
 0.
 0.
 0.

INITIAL CONDITIONS
 A,O,B,A,R,V
 -46730612600E+02
 .37344513300E+01
 .86290021400E+02
 .86672905700E+02
 .13462399100E+09
 .10361771300E+05

A,E,I,O,U,TAU
 .13833420060E+09
 .40000229570E-01
 .49999999902E+01
 .21500001307E+03
 .35874044867E+03
 --10426790660E+03

AF,AG,N,L,CHI,PSI
 -.33262674454E-01
 -.22217399790E-01
 .4176749493E-02
 .2599335293E+03
 -.25042896151E-01
 -.35766944895E-01

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

***** VEHICLE DATA FOR CASE 2 *****

IVEHID3
 IC 280.619783
 .448793
 END

22.9501321
 166569812.

71.0381996
 8201.03786

CARD 1
 CARD 2
 CARD 3
 CARD 4

EPOCH
 YR/MO/DAY
 TZME,HR,MIN,SEC
 -1973/ 1/ 1
 0.
 0.
 0.
 0.

INITIAL CONDITIONS
 A,D,B,A,R,V
 .28061976300E+03
 .22950132100E+02
 .77038199600E+02
 .72448793000E+02
 .16656981200E+09
 .82010376600E+04

A,E,I,O,U,TAU
 .13833121061E+09
 .29981105851E+00
 .2860634287E+02
 .22986614029E+03
 .27001139933E+03
 -.47599867647E+03

AF,AG,N,L,CHI,PSI
 -.22850036562E+00
 .19409434856E+00
 .41782100534E-02
 .2600865736E+03
 -.19430910442E+00
 -.16498361915E+00

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

***** VEHICLE DATA FOR CASE 3 *****

IVEHID3
 IC -100.
 90.
 END

-28.6
 96853470.

90.
 13744.772

CARD 1
 CARD 2
 CARD 3
 CARD 4

DATA GENERATION I
 STATION INTERVAL (SEC.) MIN.ELE. (DEG.) MAX.ELE. (DEG.) MAX.RANGE (N.MI.) START TIME (DA HR MIN) STOP TIME (DA HR MIN) AZIMUTH1 (DEG.) AZIMUTH2 (DEG.)

VTS 900.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00
 AND 900.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00
 DUM 900.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00

DATA GENERATION II

* SIMULTANEOUS VEHICLE DATA GENERATION II KEY/HEADER *

* STA 1 --- PRIMARY STATION ID
 * STA 2 --- SECOND STATION ID
 * STA 3 --- THIRD STATION ID
 * T --- OBSERVATION DATA SET TYPE - 1 7 J K L M N O P Q R S T U
 * 01 --- OBSERVATION 1----- R RD V2 S2 S3 S3D V3 V3D T00A TOA 3MR MP F2 A
 * 02 --- OBSERVATION 2----- A V2D S2D RC E
 * 03 --- OBSERVATION 3----- E
 * V1 --- VEHICLE 1 ID NUMBER
 * V2 --- VEHICLE 2 ID NUMBER
 * V3 --- VEHICLE 3 ID NUMBER

STA	T	000	V1	V2	V3	STA	T	000	V1	V2	V3	STA	T	000	V1	V2	V3	STA	T	000	V1	V2	V3	STA	T	000	V1	V2	V3
1	XXX	123	1	2	3	1	XX	123	1	2	3	1	X	123	1	2	3	1	X	123	1	2	3	1	X	123	1	2	3
AND	7	X	1	2	3	J	X	123	2	3	3	J	X	123	1	3	3	J	X	123	1	3	3	J	X	123	1	3	3
DUM	J	XX	1	2	3	K	X	123	1	3	3	K	X	123	1	2	3	K	X	123	1	2	3	K	X	123	1	2	3
VTS	K	XX	2	3	1	L	X	123	1	2	3	L	X	123	1	2	3	L	X	123	1	2	3	L	X	123	1	2	3
AND	L	X	2	3	1	M	X	123	1	2	3	M	X	123	1	2	3	M	X	123	1	2	3	M	X	123	1	2	3
VTS	L	X	2	3	1	N	X	123	1	2	3	N	X	123	1	2	3	N	X	123	1	2	3	N	X	123	1	2	3
AND	M	X	2	3	1	O	X	123	1	2	3	O	X	123	1	2	3	O	X	123	1	2	3	O	X	123	1	2	3
DUM	N	X	2	3	1	P	X	123	1	2	3	P	X	123	1	2	3	P	X	123	1	2	3	P	X	123	1	2	3
AND	P	X	2	3	1	Q	X	123	1	2	3	Q	X	123	1	2	3	Q	X	123	1	2	3	Q	X	123	1	2	3
VTS	P	X	2	3	1	R	X	123	1	2	3	R	X	123	1	2	3	R	X	123	1	2	3	R	X	123	1	2	3
AND	Q	X	2	3	1	S	X	123	1	2	3	S	X	123	1	2	3	S	X	123	1	2	3	S	X	123	1	2	3
DUM	Q	X	2	3	1	T	X	123	1	2	3	T	X	123	1	2	3	T	X	123	1	2	3	T	X	123	1	2	3

DESCRIPTION

4 Simultaneous-vehicle DATA GENERATION II key/header printout

The observation names are abbreviated as follows for each data set type:

ITEM	Abbreviation	Description	TOA	Q	Notes
1	R	Station-vehicle range	3WR	R	Time difference of arrival of signal transmitted from vehicle to Station 1 minus vehicle to Station 2 Time of signal transmitted from Station 1 to Vehicle 1 plus time from Vehicle 1 to Station 2 Time from Vehicle 1 to earth to Vehicle 2 minus time from Vehicle 1 to Vehicle 2 Two-way range currently not used C-band range L-band range Vehicle-vehicle azimuth Vehicle-vehicle elevation Topocentric
7	Fa	Station-vehicle azimuth			
J	RD	Station-vehicle range rate			
K	VZD	Vehicle-vehicle range rate	MP	S	
L	S2D	Station-vehicle-vehicle range rate sum	R2	T	
M	S3D	Station-vehicle-vehicle range rate sum	RL		
N	V3	Vehicle-vehicle range rate sum	Ab	U	
O	V3D	Vehicle-vehicle range rate sum	Eb		
P	TDOA	Time difference of arrival of two signals, station to Vehicle 1 minus station to Vehicle 2	IOpb		

a Observation output for Data Set Type 1.

b Observation output for Data Set Type U. If TOP is entered, A and E contain vehicle-vehicle topocentric right ascension and declination.

Consider the following segments of DATA GENERATION II printout:

ITEM	STA	TOA	V1	V2	V3	STA	TOA	V1	V2	V3	STA	TOA	V1	V2	V3	STA
1	VTS	11:23	1	2	3	1	11:23	1	2	3	1	11:23	1	2	3	1
2	AND															
3	DUM															
4	VTS		1	2	3	1		1	2	3	1		1	2	3	1
5	AND															
6	AND															
7	DUM															
8	AND															
9	VTS		1	2	3	1		1	2	3	1		1	2	3	1
10	AND															
11	DUM															

- (1a) Station-vehicle R, A, E data generated between Station VTS and Vehicle 1 (ID No. 1).
- (1b) Station-vehicle A, E data generated between Station VTS and Vehicle 1 (ID No. 3).
- (1c) Station-vehicle R data generated between Station VTS and Vehicle 1 (ID No. 2).
- (2a) Station-vehicle range rate data generated between Station AND and Vehicle 1 (ID No. 1).
- (2b) Vehicle-vehicle range and range rate data generated between Vehicle 1 (ID No. 1) and Vehicle 2 (ID No. 2).
- (7a) Vehicle-vehicle range data generated between Vehicle 1 (ID No. 1), Vehicle 2 (ID No. 3), and Vehicle 3 (ID No. 2).
- (9a) Time-of-arrival data generated between Vehicle 1 (ID No. 1) to Station VTS minus Vehicle 1 (ID No. 1) and Station AND.
- (9b) Time-of-arrival data generated between Vehicle 1 (ID No. 2) to Station VTS minus Vehicle 1 (ID No. 2) and Station AND.

EPOCH	INITIAL CONDITIONS		
YR/MO/DAY	A, E, I, C, U, iAU	AF, AG, N, L, CHI, PSI	
TZNE, HR, MIN, SEC	B, A, R, V		
-1973/ 1/ 1	0.0000000000E+03	-.5206900E+54E-01	
0.	1.3533313361E+09	-.2952979756E+00	
0.	2.8500000000E+02	.41781232924E-02	
0.	1.9000000000E+02	.2600000000E+03	
0.	1.3535956029E+05	-.44262365465E-01	
0.	2.3867546102E+04	.25102434855E+00	
	1.3744772000E+05		

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

ENTER SEGMENT 02 AT	.4 SECONDS.	EXECUTION TIME FOR SEGMENT 1 WAS	.1 CP SECS.
ENTER SEGMENT 10 AT	.4 SECONDS.	EXECUTION TIME FOR SEGMENT 2 WAS	.0 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

*** TRAJECTORY START

*** ENTRY TIME IS .41100

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .067 SECONDS TO INTEGRATE A SPAN OF 247.000 MINUTES ***
*** FROM 0.000 TO 247.000 MINUTES FROM MIDNIGHT OF EPOCH ***

***** TRAJECTORY INTEGRATION FOR CASE 2 *****

*** TRAJECTORY START

*** ENTRY TIME IS .68200

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .066 SECONDS TO INTEGRATE A SPAN OF 247.000 MINUTES ***
*** FROM 0.000 TO 247.000 MINUTES FROM MIDNIGHT OF EPOCH ***

***** TRAJECTORY INTEGRATION FOR CASE 3 *****

*** TRAJECTORY START

*** ENTRY TIME IS .55500

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .072 SECONDS TO INTEGRATE A SPAN OF 243.000 MINUTES ***
*** FROM 0.000 TO 243.000 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 61 AT .6 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

VTS	AND	73	1	1	1	0	30	0.000000	L	.29908091E+09	.10000000E+01	.30000000E+01	2	R	TOA	S-V1-V2-V3
VTS	AND	73	1	1	1	0	30	0.000000	Q	-.39000497E-03	0.	0.	1	TOA	VS1-VS2	
VTS	AND	73	1	1	1	0	30	7.000000	Q	.54658442E-02	0.	0.	3	TOA	VS1-VS2	
VTS	AND	73	1	1	1	0	30	0.000000	Q	.13038526E-03	0.	0.	2	TOA	VS1-VS2	
AND		73	1	1	1	0	30	0.000000	7	.26648065E+03	0.	0.	1	RD	S-V1	
AND		73	1	1	1	0	30	0.000000	L	.32874355E+09	.30000000E+01	.20000000E+01	1	R	S-V1-V2-V3	
AND		73	1	1	1	0	30	0.000000	P	.33732343E+03	.10000000E+01	.10000000E+01	3	RD	S-V1-V2-V3	
AND		73	1	1	1	0	30	0.000000	P	.10367035E+00	0.	0.	2	TDOA	SV1V2-SV2	
AND		73	1	1	1	0	30	0.000000	L	.23673526E+09	.30000000E+01	.10000000E+01	2	R	S-V1-V2-V3	
AND		73	1	1	1	0	30	0.000000	P	.19616991E+00	0.	0.	2	TDOA	SV1V2-SV2	
AND		73	1	1	1	0	30	0.000000	P	-.11278630E+04	.10000000E+01	.30000000E+01	2	R	S-V1-V2-V3	
AND	VTS	73	1	1	1	0	30	0.000000	R	.24310022E+00	0.	0.	1	3MR	S1V1-S1V2	
AND	VTS	73	1	1	1	0	30	0.000000	R	.30768046E+00	0.	0.	3	3MR	S1V1-S1V2	
AND	VTS	73	1	1	1	0	30	0.000000	R	.18663151E+00	0.	0.	2	3MR	S1V1-S1V2	
DUM		73	1	1	1	0	30	0.000000	J	.73076107E+08	-.14185904E+03	.30000000E+01	1	R	RD	V1-V2
DUM		73	1	1	1	0	30	0.000000	S	.19426939E+08	0.	.30000000E+01	1	MULT	V1E2-V1V2	
DUM		73	1	1	1	0	30	0.000000	N	.20813402E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3	
DUM		73	1	1	1	0	30	0.000000	O	-.11886149E+04	.20000000E+01	.30000000E+01	1	R	V1-V2-V3	
DUM		73	1	1	1	0	30	0.000000	J	.73076107E+08	-.14185904E+03	.30000000E+01	1	R	RD	V1-V2
DUM		73	1	1	1	0	30	0.000000	S	.19426939E+08	0.	.30000000E+01	1	MULT	V1E2-V1V2	
DUM		73	1	1	1	0	30	0.000000	J	.12098517E+00	0.	.20000000E+01	2	R	RD	V1-V2
VTS		73	1	1	1	0	45	0.000000	J	.13575791E+09	.13792611E+03	.46073076E+02	1	RAE	S-V1	
VTS		73	1	1	1	0	45	0.000000	K	.19264435E+09	.27991368E+03	.30000000E+01	1	R	RD	S-V1-V2
VTS		73	1	1	1	0	45	0.000000	K	.19339766E+09	.85170668E+02	.30000000E+01	1	R	RD	S-V1-V2
VTS		73	1	1	1	0	45	0.000000	M	-.99126456E+03	.30000000E+01	.20000000E+01	1	R	RD	S-V1-V2-V3
VTS		73	1	1	1	0	45	0.000000	L	.15412109E+09	.96496525E+02	.51994251E+02	1	RAE	S-V1	
VTS		73	1	1	1	0	45	0.000000	L	.36196033E+09	.10000000E+01	.20000000E+01	3	R	S-V1-V2-V3	
VTS		73	1	1	1	0	45	0.000000	M	.92951331E+09	.14787171E+03	.90053600E+01	2	RAE	S-V1	
VTS		73	1	1	1	0	45	0.000000	K	.10579570E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3	
VTS		73	1	1	1	0	45	0.000000	K	.22705153E+09	.27769871E+03	.30000000E+01	2	R	RD	S-V1-V2
VTS		73	1	1	1	0	45	0.000000	L	.30073746E+09	.10000000E+01	.30000000E+01	2	R	TOA	VS1-VS2
VTS		73	1	1	1	0	45	0.000000	Q	-.34202135E-03	0.	0.	1	TOA	VS1-VS2	
VTS		73	1	1	1	0	45	0.000000	Q	.31835940E-02	0.	0.	3	TOA	VS1-VS2	
VTS		73	1	1	1	0	45	0.000000	7	.10569858E-02	0.	0.	2	TOA	VS1-VS2	
AND		73	1	1	1	0	45	0.000000	L	.28826838E+03	0.	0.	1	RD	S-V1	
AND		73	1	1	1	0	45	0.000000	L	.32783414E+09	.30000000E+01	.20000000E+01	1	R	S-V1-V2-V3	
AND		73	1	1	1	0	45	0.000000	M	.15744704E+03	.10000000E+01	.20000000E+01	3	RD	S-V1-V2-V3	
AND		73	1	1	1	0	45	0.000000	P	.10352322E+00	0.	.10000000E+01	2	TDOA	SV1V2-SV2	
AND		73	1	1	1	0	45	0.000000	L	.23663667E+09	.30000000E+01	.10000000E+01	2	R	S-V1-V2-V3	
AND		73	1	1	1	0	45	0.000000	F	.19647460E+00	0.	.30000000E+01	2	TDOA	SV1V2-SV2	
AND		73	1	1	1	0	45	0.000000	M	-.77122336E+03	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3	
AND	VTS	73	1	1	1	0	45	0.000000	F	.24365560E+00	0.	0.	1	3MR	S1V1-S1V2	
AND	VTS	73	1	1	1	0	45	0.000000	R	.31020740E+00	0.	0.	3	3MR	S1V1-S1V2	

REFERENCE SECTION

DESCRIPTION

Item 4

5 DATA GENERATION II output. Each line corresponds to a primary station, secondary station, year, month, day, hour, minute, second, data set type, generated observations, vehicle ID number, observation data abbreviations, and station and vehicle sequence numbers. The output description is:

Primary station ID	Secondary station ID	Year	Month	Day	Hour	Minute	Second	Observation type	OB1	OB2 (V3)	OB3 (V2)	V1	Observation data sets	Station and vehicle sequence Nos.
								Observation data for all data set types	Observation data for Data Set Types I, J, K, T, and U	V3 ID No. for Data Set Types L, M, N, and O	Observation data for Data Set Types 1 and T, O, P, S, and U	Zero for other data set types	V1 ID No.	Zero for other data set types

STA	ST2	Y	M	D	H	M	SEC	OT	OB1	OB2 (V3)	OB3 (V2)	V1	5
VTS		73	1	1	0	15	C.00000	1	.11908033E+09	.13875191E+03	.45901570E+12	1	RAE S-V1
VTS		73	1	1	0	15	C.00000	K	.19232075E+09	.00385637E+02	.30000000E+01	1	R RD S-V1-V2
VTS		73	1	1	0	15	C.00000	K	.19317728E+09	.15435345E+03	.20000000E+01	1	R RD S-V1-V2
VTS		73	1	1	0	15	C.00000	H	-.0533570E+03	.30000000E+01	.20000000E+01	3	RAE S-V1-V2-V3
VTS		73	1	1	0	15	C.00000	1	.15182447E+09	.96745079E+02	.49046998E+12	3	RAE S-V1-V2-V3
VTS		73	1	1	0	15	C.00000	L	.36190448E+09	.10000000E+01	.20000000E+01	3	R S-V1-V2-V3
VTS		73	1	1	0	15	C.00000	1	.90991238E+08	.15616627E+03	.10431786E+12	2	RAE S-V1
VTS		73	1	1	0	15	C.00000	H	.43460611E+03	.30000000E+01	.10000000E+01	2	RD S-V1-V2-V3
VTS		73	1	1	0	15	C.00000	K	.22697431E+09	.20139590E+03	.30000000E+01	2	R RD S-V1-V2
VTS		73	1	1	0	15	C.00000	L	.30021472E+09	.10000000E+01	.30000000E+01	2	R S-V1-V2-V3
VTS	AND	73	1	1	0	15	C.00000	0	-.44255651E+03	0.	0.	1	TOA VS1-VS2
VTS	AND	73	1	1	0	15	C.00000	0	.37450345E+02	0.	0.	3	TOA VS1-VS2
VTS	AND	73	1	1	0	15	C.00000	0	-.82450442E+03	0.	0.	2	TOA VS1-VS2
AND		73	1	1	0	15	C.00000	7	.24319331E+03	0.	0.	1	RD S-V1
AND		73	1	1	0	15	C.00000	L	.32959550E+09	.30000000E+01	.20000000E+01	1	R S-V1-V2-V3
AND		73	1	1	0	15	C.00000	H	.52080722E+03	.10000000E+01	.20000000E+01	3	RD S-V1-V2-V3
AND		73	1	1	0	15	C.00000	P	.10351092E+00	.30000000E+01	.10000000E+01	2	TOA SV1V2-SV2
AND		73	1	1	0	15	C.00000	L	.23913938E+09	.30000000E+01	.10000000E+01	2	R S-V1-V2-V3
AND		73	1	1	0	15	C.00000	P	.19553368E+00	0.	.30000000E+01	2	TOA SV1V2-SV2
AND		73	1	1	0	15	C.00000	H	-.14767996E+04	.10000000E+01	.30000000E+01	2	RD S-V1-V2-V3
AND	VTS	73	1	1	0	15	C.00000	R	.24258108E+00	0.	0.	1	3MR SV1-S1V2
AND	VTS	73	1	1	0	15	C.00000	R	.30497605E+00	0.	0.	3	3MR SV1-S1V2
DUM		73	1	1	0	15	C.00000	R	.18584647E+00	.22264991E+03	.30000000E+01	2	3MR SV1-S1V2
DUM		73	1	1	0	15	C.00000	J	.73240415E+08	0.	.30000000E+01	1	R RD V1-V2
DUM		73	1	1	0	15	C.00000	S	.19231125E+00	0.	.30000000E+01	1	R RD V1EV2-V1V2
DUM		73	1	1	0	15	C.00000	N	.20922348E+09	.20000000E+01	.30000000E+01	1	R V1-V2-V3
DUM		73	1	1	0	15	C.00000	0	-.12305741E+04	.20000000E+01	.30000000E+01	1	R RD V1-V2-V3
DUM		73	1	1	0	15	C.00000	J	.74096949E+08	-.1486823E+03	.20000000E+01	1	R RD V1-V2
DUM		73	1	1	0	15	C.00000	S	.11999225E+00	0.	.20000000E+01	1	MULT V1EV2-V1V2
VTS		73	1	1	0	30	C.00000	J	.13598307E+09	.10079242E+04	.30000000E+01	2	R RD V1-V2
VTS		73	1	1	0	30	C.00000	1	.11936148E+09	.13831957E+03	.45922510E+12	1	RAE S-V1
VTS		73	1	1	0	30	C.00000	K	.19243759E+09	.17959777E+03	.30000000E+01	1	R RD S-V1-V2
VTS		73	1	1	0	30	C.00000	K	.193.0217E+09	.12276780E+03	.20000000E+01	1	R RD S-V1-V2
VTS		73	1	1	0	30	C.00000	H	-.92418810E+03	.30000000E+01	.20000000E+01	1	RD S-V1-V2-V3
VTS		73	1	1	0	30	C.00000	1	.15301717E+09	.96589886E+02	.50530271E+12	3	RAE S-V1
VTS		73	1	1	0	30	C.00000	L	.36201577E+09	.10000000E+01	.20000000E+01	3	R S-V1-V2-V3
VTS		73	1	1	0	30	C.00000	1	.91846886E+08	.15199145E+03	.95632226E+11	2	RAE S-V1
VTS		73	1	1	0	30	C.00000	H	.75184476E+03	.30000000E+01	.10000000E+01	2	RD S-V1-V2-V3
VTS		73	1	1	0	30	C.00000	K	.22690480E+09	.45436889E+02	.30000000E+01	2	R RD S-V1-V2

AND	VTS	73	1	1	1	0	45	0	00000	R	19795073E+00	0	58217159E+02	0	30000000E+01	2	3MR	S1V1-S1V2
DUM		73	1	1	0	45	0	00000	J	72985924E+00	72985924E+00	0	58217159E+02	0	30000000E+01	1	R RD	V1-V2
DUM		73	1	1	0	45	0	00000	S	19606784E+00	19606784E+00	0	58217159E+02	0	30000000E+01	1	MULT	V1E2-V1V2
DUM		73	1	1	0	45	0	00000	N	20738614E+00	20738614E+00	0	58217159E+02	0	30000000E+01	1	R	V1-V2-V3
DUM		73	1	1	0	45	0	00000	O	11386526E+00	11386526E+00	0	58217159E+02	0	30000000E+01	1	R RD	V1-V2-V3
DUM		73	1	1	0	45	0	00000	J	73739227E+00	73739227E+00	0	58217159E+02	0	30000000E+01	1	R RD	V1-V2
DUM		73	1	1	0	45	0	00000	S	12239129E+00	12239129E+00	0	58217159E+02	0	30000000E+01	1	MULT	V1E2-V1V2
DUM		73	1	1	0	45	0	00000	J	13410022E+00	13410022E+00	0	58217159E+02	0	30000000E+01	2	R RD	V1-V2
VTS		73	1	1	1	0	00000	0	11996958E+00	11996958E+00	0	58217159E+02	0	30000000E+01	1	RAE	S-V1	
VTS		73	1	1	1	0	00000	0	19294123E+00	19294123E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	19346242E+00	19346242E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	10548312E+00	10548312E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	15513529E+00	15513529E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	36174258E+00	36174258E+00	0	58217159E+02	0	30000000E+01	1	RAE	S-V1	
VTS		73	1	1	1	0	00000	0	94284293E+00	94284293E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	13280911E+00	13280911E+00	0	58217159E+02	0	30000000E+01	2	RD	S-V1-V2-V3	
VTS		73	1	1	1	0	00000	0	22739873E+00	22739873E+00	0	58217159E+02	0	30000000E+01	2	R RD	S-V1-V2	
VTS		73	1	1	1	0	00000	0	30037339E+00	30037339E+00	0	58217159E+02	0	30000000E+01	2	R	S-V1-V2-V3	
VTS	AND	73	1	1	1	0	00000	0	29892326E+00	29892326E+00	0	58217159E+02	0	30000000E+01	1	TOA	VS1-VS2	
VTS	AND	73	1	1	1	0	00000	0	2897876E+00	2897876E+00	0	58217159E+02	0	30000000E+01	3	TOA	VS1-VS2	
VTS	AND	73	1	1	1	0	00000	0	19381818E+00	19381818E+00	0	58217159E+02	0	30000000E+01	2	TOA	VS1-VS2	
AND		73	1	1	1	0	00000	0	30847196E+00	30847196E+00	0	58217159E+02	0	30000000E+01	1	R	S-V1	
AND		73	1	1	1	0	00000	0	32687064E+00	32687064E+00	0	58217159E+02	0	30000000E+01	1	R	S-V1-V2-V3	
AND		73	1	1	1	0	00000	0	18598518E+00	18598518E+00	0	58217159E+02	0	30000000E+01	3	RD	S-V1-V2-V3	
AND		73	1	1	1	0	00000	0	13307188E+00	13307188E+00	0	58217159E+02	0	30000000E+01	2	TOA	SV1V2-SV2	
AND		73	1	1	1	0	00000	0	23884228E+00	23884228E+00	0	58217159E+02	0	30000000E+01	2	R	S-V1-V2-V3	
AND		73	1	1	1	0	00000	0	19624433E+00	19624433E+00	0	58217159E+02	0	30000000E+01	2	TOA	SV1V2-SV2	
AND		73	1	1	1	0	00000	0	41593905E+00	41593905E+00	0	58217159E+02	0	30000000E+01	2	RD	S-V1-V2-V3	
AND		73	1	1	1	0	00000	0	24424555E+00	24424555E+00	0	58217159E+02	0	30000000E+01	2	RD	S-V1-V2-V3	
AND		73	1	1	1	0	00000	0	31255447E+00	31255447E+00	0	58217159E+02	0	30000000E+01	1	3MR	S1V1-S1V2	
AND		73	1	1	1	0	00000	0	18978006E+00	18978006E+00	0	58217159E+02	0	30000000E+01	3	3MR	S1V1-S1V2	
AND		73	1	1	1	0	00000	0	72971656E+00	72971656E+00	0	58217159E+02	0	30000000E+01	2	3MR	S1V1-S1V2	
DUM		73	1	1	1	0	00000	0	19770251E+00	19770251E+00	0	58217159E+02	0	30000000E+01	1	R RD	V1-V2	
DUM		73	1	1	1	0	00000	0	20678609E+00	20678609E+00	0	58217159E+02	0	30000000E+01	1	MULT	V1E2-V1V2	
DUM		73	1	1	1	0	00000	0	10430021E+00	10430021E+00	0	58217159E+02	0	30000000E+01	1	R	V1-V2-V3	
DUM		73	1	1	1	0	00000	0	73492846E+00	73492846E+00	0	58217159E+02	0	30000000E+01	1	R RD	V1-V2	
DUM		73	1	1	1	0	00000	0	12419812E+00	12419812E+00	0	58217159E+02	0	30000000E+01	1	MULT	V1E2-V1V2	
DUM		73	1	1	1	0	00000	0	13311444E+00	13311444E+00	0	58217159E+02	0	30000000E+01	2	R RD	V1-V2	
VTS		73	1	1	1	15	00000	0	12026335E+00	12026335E+00	0	58217159E+02	0	30000000E+01	1	RAE	S-V1	
VTS		73	1	1	1	15	00000	0	19332685E+00	19332685E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	15	00000	0	19349638E+00	19349638E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	15	00000	0	11145255E+00	11145255E+00	0	58217159E+02	0	30000000E+01	1	R RD	S-V1-V2	
VTS		73	1	1	1	15	00000	0	15605897E+00	15605897E+00	0	58217159E+02	0	30000000E+01	3	RAE	S-V1	

AND	73	1	1	1	30	C.0C0000	F	.19478731E+00	0.	.10000000E+01	.30000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	1	30	C.300000	M	.25741756E+03	0.	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	VTS	73	1	1	1	30	C.300000	K	.24551276E+03	0.	.30000000E+01	1	3MR	S1V1-S1V2
AND	VTS	73	1	1	1	30	C.000000	R	.31670091E+00	0.	.00000000E+01	3	3MR	S1V1-S1V2
AND	VTS	73	1	1	1	30	C.000000	R	.19483468E+00	0.	.00000000E+01	2	3MR	S1V1-S1V2
DUH	73	1	1	1	1	30	C.050000	J	.73170498E+08	.15299603E+03	.30000000E+01	1	R RD	V1-V2
DUH	73	1	1	1	1	30	C.000000	S	.20047196E+00	0.	.30000000E+01	1	MULT	V1E2-V1V2
DUH	73	1	1	1	1	30	C.000000	N	.20424163E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3
DUH	73	1	1	1	1	30	C.300000	O	-.96633197E+08	.20000000E+01	.30000000E+01	1	R RD	V1-V2-V3
DUH	73	1	1	1	1	30	C.000000	J	.12882793E+00	-.38724718E+03	.20000000E+01	1	R RD	V1-V2
DUH	73	1	1	1	1	30	C.000000	S	.13177113E+09	0.	.20000000E+01	1	MULT	V1E2-V1V2
VTS	73	1	1	1	1	45	C.000000	I	.12097158E+09	-.11593280E+04	.30000000E+01	2	R RD	V1-V2
VTS	73	1	1	1	1	45	C.000000	K	.19435150E+09	.13677603E+03	.46297081E+02	1	RAE	S-V1
VTS	73	1	1	1	1	45	C.000000	K	.19347966E+09	.65807525E+03	.30000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	1	1	45	C.000000	M	-.12179918E+04	-.36374114E+02	.20000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	1	1	45	C.000000	I	.15763180E+09	.30000000E+01	.20000000E+01	1	RD	S-V1-V2-V3
VTS	73	1	1	1	1	45	C.300000	L	.36015758E+09	.10000000E+01	.20000000E+01	3	RAE	S-V1
VTS	73	1	1	1	1	45	C.000000	I	.99421133E+08	.13273377E+03	.57663450E+02	3	R	S-V1-V2-V3
VTS	73	1	1	1	1	45	C.300000	M	.20133077E+04	.30000000E+01	.10000000E+01	2	RAE	S-V1
VTS	73	1	1	1	1	45	C.300000	K	.22943874E+09	.98277818E+03	.30000000E+01	2	R RD	S-V1-V2-V3
VTS	73	1	1	1	1	45	C.300000	L	.30281866E+03	.10000000E+01	.30000000E+01	2	R	S-V1-V2-V3
VTS	AND	73	1	1	1	45	C.300000	O	-.19969139E-03	0.	.00000000E+01	1	TOA	VS1-VS2
VTS	AND	73	1	1	1	45	C.000000	O	.2329035E-02	0.	.00000000E+01	3	TOA	VS1-VS2
VTS	AND	73	1	1	1	45	C.300000	O	.41849420E-02	0.	.00000000E+01	2	TOA	VS1-VS2
AND	73	1	1	1	1	45	C.300000	7	.35892990E+03	0.	.00000000E+01	1	R	S-V1
AND	73	1	1	1	1	45	C.000000	L	.32369355E+09	.30000000E+01	.20000000E+01	1	R	S-V1-V2-V3
AND	73	1	1	1	1	45	C.000000	P	-.51437327E+03	.10000000E+01	.20000000E+01	3	RD	S-V1-V2-V3
AND	73	1	1	1	1	45	C.300000	F	.10011453E+00	.30000000E+01	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	1	1	45	C.000000	L	.24119277E+09	.30000000E+01	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	1	1	45	C.300000	P	.19352426E+00	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	73	1	1	1	1	45	C.300000	M	.56233790E+03	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	VTS	73	1	1	1	45	C.000000	R	.24618392E+00	0.	.00000000E+01	1	3MR	S1V1-S1V2
AND	VTS	73	1	1	1	45	C.300000	R	.31849686E+00	0.	.00000000E+01	3	3MR	S1V1-S1V2
DUH	73	1	1	1	1	45	C.000000	R	.19797874E+00	0.	.00000000E+01	2	3MR	S1V1-S1V2
DUH	73	1	1	1	1	45	C.000000	J	.73379915E+08	.27168059E+03	.30000000E+01	1	R RD	V1-V2
DUH	73	1	1	1	1	45	C.000000	S	.23160609E+00	0.	.30000000E+01	1	MULT	V1E2-V1V2
DUH	73	1	1	1	1	45	C.000000	N	.20339752E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3
DUH	73	1	1	1	1	45	C.000000	O	-.91993707E+03	.20000000E+01	.30000000E+01	1	RD	V1-V2-V3
DUH	73	1	1	1	1	45	C.300000	J	.72518074E+08	-.42276877E+03	.20000000E+01	1	R RD	V1-V2
DUH	73	1	1	1	1	45	C.300000	S	.13159454E+00	0.	.20000000E+01	1	MULT	V1E2-V1V2
DUH	73	1	1	1	1	45	C.300000	J	.13031761E+09	-.11816177E+04	.30000000E+01	2	R RD	V1-V2
VTS	73	1	1	1	2	0	C.300000	I	.12132278E+09	.13660084E+03	.463330219E+02	1	RAE	S-V1

VTS	73	1	1	2	0	0.	0.000000	K	.19498087E+09	.73933390E+03	.30000000E+01	1	R	RD	S-V1-V2
VTS	73	1	1	2	0	0.	0.000000	K	.19343767E+09	-.55559274E+02	.20000000E+01	1	R	RD	S-V1-V2
VTS	73	1	1	2	0	0.	0.000000	M	-.12502170E+04	.30000000E+01	.20000000E+01	1	RAE	S-V1	S-V1-V2-V3
VTS	73	1	1	2	0	0.	0.000000	L	.15827993E+09	.97079441E+02	.59035573E+02	3	R	RAE	S-V1-V2-V3
VTS	73	1	1	2	0	0.	0.000000	L	.35933941E+09	.10000000E+01	.20000000E+01	3	R	RAE	S-V1-V2-V3
VTS	73	1	1	2	0	0.	0.000000	H	.10143150E+09	.12941962E+03	.10435959E+02	2	RD	S-V1-V2-V3	
VTS	73	1	1	2	0	0.	0.000000	H	.21950644E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3	
VTS	73	1	1	2	0	0.	0.000000	K	.23037609E+09	.10560930E+04	.30000000E+01	2	R	RD	S-V1-V2-V3
VTS	73	1	1	2	0	0.	0.000000	L	.30403419E+09	.10000000E+01	.30000000E+01	2	R	TOA	VS1-VS2
VTS	73	1	1	2	0	0.	0.000000	O	-.1727309E-03	0.	0.	3	TOA	VS1-VS2	
VTS	73	1	1	2	0	0.	0.000000	O	.17414169E-02	0.	0.	1	TOA	VS1-VS2	
VTS	73	1	1	2	0	0.	0.000000	Q	.47775516E-02	0.	0.	2	TOA	VS1-VS2	
AND	73	1	1	2	0	0.	0.000000	7	.37221258E+03	0.	0.	1	R	S-V1	S-V1-V2-V3
AND	73	1	1	2	0	0.	0.000000	L	.3225569E+09	.30000000E+01	.30000000E+01	1	RD	S-V1-V2-V3	
AND	73	1	1	2	0	0.	0.000000	P	-.66429483E+03	.10000000E+01	.20000000E+01	3	RD	SV1V2-V2	
AND	73	1	1	2	0	0.	0.000000	P	.98498121E-01	0.	.10000000E+01	2	TDOA	SV1V2-V2	
AND	73	1	1	2	0	0.	0.000000	L	.24250527E+09	.30000000E+01	.30000000E+01	2	R	SV1V2-V2	
AND	73	1	1	2	0	0.	0.000000	P	.19193239E+00	.30000000E+01	.30000000E+01	2	TDOA	SV1V2-V2	
AND	73	1	1	2	0	0.	0.000000	H	.63699815E+03	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3	
AND	73	1	1	2	0	0.	0.000000	R	.24687563E+00	0.	0.	3	3MR	S1V1-S1V2	
AND	73	1	1	2	0	0.	0.000000	R	.32010604E+00	0.	0.	2	3MR	S1V1-S1V2	
AND	73	1	1	2	0	0.	0.000000	R	.20147407E+00	0.	0.	3	3MR	S1V1-S1V2	
DUM	73	1	1	2	0	0.	0.000000	J	.73658093E+08	.34560303E+03	.30000000E+01	1	R	MULT	V1EV2-V1V2
DUM	73	1	1	2	0	0.	0.000000	S	.20257490E+00	0.	.30000000E+01	1	R	MULT	V1EV2-V1V2
DUM	73	1	1	2	0	0.	0.000000	N	.20260269E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3	
DUM	73	1	1	2	0	0.	0.000000	C	-.85705472E+03	.20000000E+01	.30000000E+01	1	R	V1-V2-V3	
DUM	73	1	1	2	0	0.	0.000000	J	.72114887E+08	-.44929014E+03	.20000000E+01	1	R	V1-V2	
DUM	73	1	1	2	0	0.	0.000000	S	.13460225E+00	0.	.20000000E+01	2	R	V1-V2	
DUM	73	1	1	2	0	0.	0.000000	J	.12894459E+09	.12026570E+04	.30000000E+01	1	RAE	S-V1	
VTS	73	1	1	2	15	0.	0.000000	I	.12167973E+09	.13647210E+03	.46354953E+02	1	R	RD	S-V1-V2
VTS	73	1	1	2	15	0.	0.000000	K	.19567997E+09	.81284375E+03	.30000000E+01	1	R	RD	S-V1-V2
VTS	73	1	1	2	15	0.	0.000000	K	.19338245E+09	-.65424091E+02	.20000000E+01	1	R	RD	S-V1-V2
VTS	73	1	1	2	15	0.	0.000000	H	-.12877473E+04	.30000000E+01	.20000000E+01	1	R	RD	S-V1-V2
VTS	73	1	1	2	15	0.	0.000000	L	.15883500E+09	.97444505E+02	.60390027E+02	3	R	RAE	S-V1
VTS	73	1	1	2	15	0.	0.000000	L	.35839096E+09	.10000000E+01	.20000000E+01	3	R	RAE	S-V1
VTS	73	1	1	2	15	0.	0.000000	H	.10355129E+09	.12632100E+03	.11403183E+02	2	RD	S-V1-V2-V3	
VTS	73	1	1	2	15	0.	0.000000	H	.23568868E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3	
VTS	73	1	1	2	15	0.	0.000000	K	.23140453E+09	.11654852E+04	.30000000E+01	2	R	RD	S-V1-V2
VTS	73	1	1	2	15	0.	0.000000	Q	.30540477E+09	.10000000E+01	.30000000E+01	2	R	RD	S-V1-V2-V3
VTS	73	1	1	2	15	0.	0.000000	Q	-.16033571E-03	0.	0.	1	TOA	VS1-VS2	
VTS	73	1	1	2	15	0.	0.000000	O	.14488456E-02	0.	0.	3	TOA	VS1-VS2	
VTS	73	1	1	2	15	0.	0.000000	Q	.52880903E-02	0.	0.	2	TOA	VS1-VS2	
AND	73	1	1	2	15	0.	0.000000	7	.38368086E+03	0.	0.	1	RD	S-V1	

AND	73	1	1	2	15	0.000000	L	.32139325E+09	.30000000E+01	.20000000E+1	1	R	S-V1-V2-V3
AND	73	1	1	2	15	2.300000	M	-.60171509E+03	.10000000E+01	.20000000E+1	3	RD	S-V1-V2-V3
AND	73	1	1	2	15	0.000000	P	.96780416E-01	0.	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	2	15	0.000000	L	.24435289E+09	.30000000E+01	.10000000E+01	2	R	S-V1-V2-V3
AND	73	1	1	2	15	0.000000	F	.19003510E+00	0.	.30000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	2	15	0.000000	M	.10856871E+04	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	VTS	73	1	1	2	15	R	.24758452E+00	0.	0.	3	3MR	S1V1-S1V2
AND	VTS	73	1	1	2	15	R	.32152726E+00	0.	0.	3	3MR	S1V1-S1V2
AND	VTS	73	1	1	2	15	R	.20527397E+00	0.	0.	2	3MR	S1V1-S1V2
DUM	73	1	1	2	15	0.000000	R	.74000243E+08	.41367313E+03	.30000000E+1	1	R RD	V1-V2
DUM	73	1	1	2	15	0.000000	J	.20338112E+00	0.	.30000000E+1	1	MULT	V1EV2-V1V2
DUM	73	1	1	2	15	0.000000	S	.20195348E+09	.20000000E+01	.30000000E+1	1	R	V1-V2-V3
DUM	73	1	1	2	15	0.000000	N	-.80865004E+03	.20000000E+01	.30000000E+01	1	R	V1-V2-V3
DUM	73	1	1	2	15	0.000000	O	.71702719E+08	-.46459475E+03	.20000000E+01	1	R RD	V1-V2
DUM	73	1	1	2	15	0.000000	J	.13780630E+00	0.	.20000000E+01	1	MULT	V1EV2-V1V2
DUM	73	1	1	2	15	0.000000	S	.12785324E+09	-.12223232E+04	.30000000E+1	2	R RD	V1-V2
DUM	73	1	1	2	15	0.000000	J	.12204073E+09	.13639037E+03	.30000000E+1	2	R RD	V1-V2
VTS	73	1	1	2	30	0.000000	I	.19644140E+09	.87771709E+03	.46371649E+02	1	RAE	S-V1
VTS	73	1	1	2	30	0.000000	K	.19332331E+09	-.63967282E+02	.20000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	2	30	0.000000	K	-.13041290E+04	.30000000E+01	.20000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	2	30	0.000000	M	.15929667E+09	.97912020E+02	.61726800E+02	3	RAE	S-V1
VTS	73	1	1	2	30	0.000000	L	.35732420E+09	.10000000E+01	.20000000E+01	3	R	S-V1-V2-V3
VTS	73	1	1	2	30	0.000000	L	.10575846E+09	.12343942E+03	.12528176E+02	2	RAE	S-V1
VTS	73	1	1	2	30	0.000000	H	.25015015E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3
VTS	73	1	1	2	30	0.000000	K	.23250342E+09	.12530574E+04	.30000000E+01	2	R RD	S-V1-V2
VTS	73	1	1	2	30	0.000000	L	.30690409E+09	.10000000E+01	.30000000E+01	2	R	S-V1-V2-V3
VTS	AND	73	1	1	2	30	Q	-.14894119E-03	0.	0.	3	TOA	VS1-VS2
VTS	AND	73	1	1	2	30	Q	.11553282E-02	0.	0.	3	TOA	VS1-VS2
VTS	AND	73	1	1	2	30	Q	.57181029E-02	0.	0.	2	TOA	VS1-VS2
AND	73	1	1	2	30	0.000000	7	.39332379E+03	.30000000E+01	.20000000E+1	1	RD	S-V1
AND	73	1	1	2	30	0.000000	L	.32021463E+09	.10000000E+01	.20000000E+01	3	R	S-V1-V2-V3
AND	73	1	1	2	30	0.000000	M	-.92468045E+03	.30000000E+01	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	2	30	0.000000	P	.94894903E-01	0.	.10000000E+01	2	R	S-V1-V2-V3
AND	73	1	1	2	30	0.000000	L	.24581741E+09	.30000000E+01	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	2	30	0.000000	F	.18785724E+00	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	73	1	1	2	30	0.000000	M	.13010256E+04	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	VTS	73	1	1	2	30	R	.24830718E+00	0.	0.	1	3MR	S1V1-S1V2
AND	VTS	73	1	1	2	30	R	.32275950E+00	0.	0.	3	3MR	S1V1-S1V2
AND	VTS	73	1	1	2	30	R	.20933207E+00	0.	0.	2	3MR	S1V1-S1V2
DUM	73	1	1	2	30	0.000000	J	.74400675E+08	.47498540E+03	.30000000E+1	1	R RD	V1-V2
DUM	73	1	1	2	30	0.000000	S	.20402845E+00	.20000000E+01	.30000000E+01	1	MULT	V1EV2-V1V2
DUM	73	1	1	2	30	0.000000	N	.20114563E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3
DUM	73	1	1	2	30	0.000000	O	-.76517233E+03	.20000000E+01	.30000000E+01	1	RD	V1-V2-V3

DUM	73	1	1	2	30	0.000000	J	.71262561E+08	--.46669697E+03	.20000000E+1	1	R RD	V1-V7
DUM	73	1	1	2	30	0.000000	S	.14116155E+00	0.	.29000000E+1	1	MULT	V1E2-V1V2
DUM	73	1	1	2	30	0.000000	J	.12674496E+09	--.12401577E+04	.30000000E+01	1	R RD	V1-V2
VTS	73	1	1	2	45	0.000000	J	.12240409E+09	.13635547E+03	.46380655E+02	2	RAE	S-V1
VTS	73	1	1	2	45	0.000000	K	.19725706E+09	.93226284E+03	.30000000E+1	1	R RD	S-V1-V2
VTS	73	1	1	2	45	0.000000	K	.19327120E+09	--.49545634E+02	.20000000E+01	1	R RD	S-V1-V2-V3
VTS	73	1	1	2	45	0.000000	M	--.13050001E+04	.30000000E+01	.63045695E+02	3	RAE	S-V1
VTS	73	1	1	2	45	0.000000	L	.15966456E+09	.98494202E+02	.20000000E+01	3	K	S-V1-V2-V3
VTS	73	1	1	2	45	0.000000	L	.35611538E+09	.10000000E+01	.20000000E+01	3	K	S-V1
VTS	73	1	1	2	45	0.000000	L	.10803254E+09	.12077175E+03	.13790574E+02	2	RAE	S-V1
VTS	73	1	1	2	45	0.000000	L	.26316706E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3
VTS	73	1	1	2	45	0.000000	K	.23365425E+09	.13013821E+04	.30000000E+01	2	R RD	S-V1-V2-V3
VTS	73	1	1	2	45	0.000000	L	.30850723E+09	.10000000E+01	.30000000E+01	2	R	S-V1-V2-V3
VTS	73	1	1	2	45	0.000000	Q	--.14312540E-03	0.	0.	2	TOA	VS1-VS2
VTS	73	1	1	2	45	0.000000	Q	.66096704E-03	0.	0.	3	TOA	VS1-VS2
VTS	73	1	1	2	45	0.000000	C	.63709253E-02	0.	0.	2	TOA	VS1-VS2
VTS	73	1	1	2	45	0.000000	G	.41114054E+03	0.	0.	1	RD	S-V1
AND	73	1	1	2	45	0.000000	7	.31903356E+09	.30000000E+01	.20000000E+1	1	R	S-V1-V2-V3
AND	73	1	1	2	45	0.000000	H	--.10397644E+04	.10000000E+01	.20000000E+1	1	RD	S-V1-V2-V3
AND	73	1	1	2	45	0.000000	F	.92876895E-01	0.	.20000000E+1	3	RD	SV1V2-V2
AND	73	1	1	2	45	0.000000	L	.24778130E+09	.30000000E+01	.10000000E+1	2	TDOA	SV1V2-V2
AND	73	1	1	2	45	0.000000	P	.18542443E+00	.30000000E+01	.30000000E+1	2	R	SV1V2-V2-V3
AND	73	1	1	2	45	0.000000	H	.14852230E+04	0.	.30000000E+1	2	RD	S-V1-V2-V3
AND	73	1	1	2	45	0.000000	R	.24904023E+00	0.	0.	1	3MR	S1V1-S1V2
AND	73	1	1	2	45	0.000000	R	.32380190E+00	0.	0.	2	3MR	S1V1-S1V2
AND	73	1	1	2	45	0.000000	R	.21360342E+00	0.	0.	3	3MR	S1V1-S1V2
DUM	73	1	1	2	45	0.000000	J	.74852972E+08	.52882125E+03	.30000000E+1	1	R RD	V1-V2
DUM	73	1	1	2	45	0.000000	S	.20452135E+00	0.	.30000000E+01	1	MULT	V1E2-V1V2
DUM	73	1	1	2	45	0.000000	N	.20047468E+09	.20000000E+01	.30000000E+01	1	R	V1-V2-V3
DUM	73	1	1	2	45	0.000000	O	--.72663324E+03	.20000000E+01	.30000000E+1	1	RD	V1-V2-V3
DUM	73	1	1	2	45	0.000000	J	.70867111E+08	--.45398721E+03	.20000000E+01	1	R RD	V1-V7
DUM	73	1	1	2	45	0.000000	S	.14462348E+00	0.	.20000000E+01	1	MULT	V1E2-V1V2
VTS	73	1	1	2	45	0.000000	J	.12562171E+09	.12554543E+04	.30000000E+1	2	R RD	V1-V2
VTS	73	1	1	3	0	0.000000	1	.12276818E+09	.13636730E+03	.46382294E+02	1	RAE	S-V1
VTS	73	1	1	3	0	0.000000	K	.19811832E+09	.97898113E+03	.30000000E+01	1	R RD	S-V1-V7
VTS	73	1	1	3	0	0.000000	P	.19323837E+09	--.20978677E+02	.20000000E+1	1	R RD	S-V1-V2
VTS	73	1	1	3	0	0.000000	1	--.12883216E+04	.30000000E+01	.20000000E+01	1	RD	S-V1-V2-V3
VTS	73	1	1	3	0	0.000000	1	.15993836E+09	.99205832E+02	.64346221E+02	3	RAE	S-V1
VTS	73	1	1	3	0	0.000000	L	.35489472E+09	.10000000E+01	.20000000E+01	3	R	S-V1-V2-V3
VTS	73	1	1	3	0	0.000000	L	.11035482E+09	.10000000E+01	.20000000E+01	2	RAE	S-V1
VTS	73	1	1	3	0	0.000000	M	.27499577E+04	.30000000E+01	.10000000E+1	2	RD	S-V1-V2-V3
VTS	73	1	1	3	0	0.000000	K	.23494098E+09	.13332861E+04	.30000000E+1	2	R RD	S-V1-V2
VTS	73	1	1	3	0	0.000000	L	.31019113E+09	.10000000E+01	.30000000E+1	2	R	S-V1-V2-V3

DUM	73	1	1	3	15	0.000000	J	.7584816E+03	.6120895E+03	.3000000E+01	1	R RD	V1-V?
DUM	73	1	1	3	15	0.000000	S	.2050646E+00	.3000000E+01	.3000000E+01	1	MULT	V1E2-V1V2
DUM	73	1	1	3	15	0.000000	N	.1992266E+09	.2000000E+01	.3000000E+01	1	R	V1-V2-V3
DUM	73	1	1	3	15	0.000000	O	-.6627611E+03	.2000000E+01	.3000000E+01	1	R RD	V1-V2-V3
DUM	73	1	1	3	15	0.000000	J	.7106517E+00	-.3000000E+03	.2000000E+01	1	R RD	V1-V2
DUM	73	1	1	3	15	0.000000	S	.1516966E+00	0.	.3000000E+01	1	MULT	V1E2-V1V2
DUM	73	1	1	3	15	0.000000	J	.1234180E+09	-.12748707E+04	.3000000E+01	2	R RD	V1-V2
VTS	73	1	1	3	30	0.000000	J	.1234920E+09	.1365292E+03	.4636459E+02	1	RAE	S-V1
VTS	73	1	1	3	30	0.000000	K	.1999414E+09	.10398193E+04	.3000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	3	30	0.000000	K	.1932831E+09	.80598180E+02	.2000000E+01	1	R RD	S-V1-V?
VTS	73	1	1	3	30	0.000000	M	-.1196474E+04	.3000000E+01	.2000000E+01	1	R RD	S-V1-V2-V3
VTS	73	1	1	3	30	0.000000	L	.1602027E+09	.10109263E+03	.6688839E+02	3	RAE	S-V1
VTS	73	1	1	3	30	0.000000	L	.3521867E+09	.1000000E+01	.2000000E+01	3	R	S-V1-V2-V3
VTS	73	1	1	3	30	0.000000	L	.1151778E+09	.11397144E+03	.18162231E+02	2	RAE	S-V1
VTS	73	1	1	3	30	0.000000	M	.2959153E+04	.3000000E+01	.1000000E+01	2	R RD	S-V1-V2-V3
VTS	73	1	1	3	30	0.000000	K	.2372708E+09	.13594026E+04	.3000000E+01	2	R RD	S-V1-V2
VTS	73	1	1	3	30	0.000000	L	.31372013E+09	.1000000E+01	.3000000E+01	2	R	S-V1-V2-V3
VTS AND	73	1	1	3	30	0.000000	Q	-.1591218E-03	0.	0.	1	TOA	VS1-VS2
VTS AND	73	1	1	3	30	0.000000	Q	-.2659042E-04	0.	0.	3	TOA	VS1-VS2
VTS AND	73	1	1	3	30	0.000000	Q	.67154003E-02	0.	0.	2	TOA	VS1-VS2
AND	73	1	1	3	30	0.000000	7	.41375919E+03	0.	0.	1	R	S-V1
AND	73	1	1	3	30	0.000000	L	.31563249E+09	.3000000E+01	.2000000E+01	1	R RD	S-V1-V2-V3
AND	73	1	1	3	30	0.000000	M	-.1229078E+04	.1000000E+01	.2000000E+01	3	R RD	S-V1-V2-V3
AND	73	1	1	3	30	0.000000	P	.86336616E-01	0.	.1000000E+01	2	TOA	V1V2-SV2
AND	73	1	1	3	30	0.000000	F	.1768548E+00	.3000000E+01	.1000000E+01	2	R	S-V1-V2-V3
AND	73	1	1	3	30	0.000000	H	.19664913E+04	.1000000E+01	.3000000E+01	2	TOA	SV1V2-SV2
AND	73	1	1	3	30	0.000000	R	.2512685E+00	0.	0.	1	3MR	S-V1-V2-V3
AND	73	1	1	3	30	0.000000	R	.32578373E+00	0.	0.	3	3MR	S-V1-S1V2
AND	73	1	1	3	30	0.000000	R	.2272849E+00	0.	0.	2	3MR	S1V1-S1V2
DUM	73	1	1	3	30	0.000000	J	.76449332E+00	.64094564E+03	.3000000E+01	2	R RD	V1-V2
DUM	73	1	1	3	30	0.000000	S	.20512644E+00	0.	.3000000E+01	1	MULT	V1E2-V1V2
DUM	73	1	1	3	30	0.000000	N	.19864232E+09	.2000000E+01	.3000000E+01	1	R	V1-V2-V3
DUM	73	1	1	3	30	0.000000	C	-.63612328E+03	.2000000E+01	.3000000E+01	1	R RD	V1-V2-V3
DUM	73	1	1	3	30	0.000000	J	.69791027E+08	-.31827148E+03	.2000000E+01	1	R RD	V1-V2
DUM	73	1	1	3	30	0.000000	S	.15522807E+00	0.	.2000000E+01	1	MULT	V1E2-V1V2
DUM	73	1	1	3	30	0.000000	J	.12219299E+09	.12770729E+04	.3000000E+01	2	R RD	V1-V2
VTS	73	1	1	3	45	0.000000	J	.12384883E+09	.13667774E+03	.46345725E+02	1	RAE	S-V1
VTS	73	1	1	3	45	0.000000	K	.20088476E+09	.10547731E+04	.3000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	3	45	0.000000	K	.19338727E+09	.15316026E+03	.2000000E+01	1	R RD	S-V1-V2
VTS	73	1	1	3	45	0.000000	M	-.11198670E+04	.3000000E+01	.2000000E+01	1	R RD	S-V1-V2-V3
VTS	73	1	1	3	45	0.000000	L	.16019300E+09	.10231545E+03	.68126848E+02	3	RAE	S-V1
VTS	73	1	1	3	45	0.000000	L	.35077638E+09	.1000000E+01	.2000000E+01	3	R	S-V1-V2-V3

VTS	73	1	1	3	45	0.000000	1	.11744971E+09	.11206942E+03	.19751365E+12	2	RAE	S-V1
VTS	73	1	1	3	45	0.000000	H	.30526921E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3
VTS	73	1	1	3	45	0.000000	K	.23049465E+09	.13591647E+04	.30000000E+01	2	R	S-V1-V2
VTS	73	1	1	3	45	0.000000	L	.31553058E+09	.10060000E+01	.30000000E+01	2	R	S-V1-V2-V3
VTS	73	1	1	3	45	0.000000	0	-.17546611E-03	0.	0.	3	TDA	VS1-VS2
VTS	73	1	1	3	45	0.000000	0	-.32354544E-03	0.	0.	3	TDA	VS1-VS2
VTS	73	1	1	3	45	0.000000	0	.60109566E-02	0.	0.	2	TDA	VS1-VS2
AND	73	1	1	3	45	0.000000	7	.4143551E+03	0.	0.	1	RD	S-V1
AND	73	1	1	3	45	0.000000	L	.31460467E+09	.30000000E+01	.20000000E+01	1	R	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	M	-.12517182E+04	.10000000E+01	.20000000E+01	3	RD	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	F	.64192903E+01	0.	.10000000E+01	2	TDDA	SV1V2-SV2
AND	73	1	1	3	45	0.000000	L	.25732490E+09	.30000000E+01	.10000000E+01	2	R	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	P	.17355905E+00	0.	.30000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	3	45	0.000000	H	.19443000E+04	.10000000E+01	.30000000E+01	2	RD	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	R	.2521033E+00	0.	0.	1	3MR	S1V1-S1V2
AND	73	1	1	3	45	0.000000	R	.32606112E+00	0.	0.	3	3MR	S1V1-S1V2
AND	73	1	1	3	45	0.000000	R	.23201241E+00	0.	0.	2	3MR	S1V1-S1V2
DUM	73	1	1	3	45	0.000000	J	.77035928E+00	0.	0.	1	R	RD
DUM	73	1	1	3	45	0.000000	S	.20515634E+00	.66115652E+03	.30000000E+01	1	MULT	V1EV2-V1V2
DUM	73	1	1	3	45	0.000000	N	.19098007E+09	0.	.30000000E+01	1	R	V1-V2-V3
DUM	73	1	1	3	45	0.000000	0	-.61187073E+03	.20000000E+01	.30000000E+01	1	RD	V1-V2-V3
DUM	73	1	1	3	45	0.000000	J	.69538435E+00	-.2405636E+03	.20000000E+01	1	R	RD
DUM	73	1	1	3	45	0.000000	S	.15870724E+00	0.	.20000000E+01	1	MULT	V1EV2-V1V2
VTS	73	1	1	3	45	0.000000	J	.12104495E+09	-.12730272E+04	.30000000E+01	2	R	RD
VTS	73	1	1	3	45	0.000000	I	.12420012E+09	.13686996E+03	.30000000E+01	1	RAE	S-V1
VTS	73	1	1	3	45	0.000000	K	.20133696E+09	.10595292E+04	.20000000E+01	1	R	RD
VTS	73	1	1	3	45	0.000000	K	.19356279E+09	.23897568E+03	.20000000E+01	1	R	RD
VTS	73	1	1	3	45	0.000000	H	-.10259190E+04	.30000000E+01	.20000000E+01	1	RD	S-V1-V2
VTS	73	1	1	3	45	0.000000	L	.16008849E+09	.10376463E+03	.69340220E+02	3	RAE	S-V1
VTS	73	1	1	3	45	0.000000	L	.34935483E+09	.10000000E+01	.20000000E+01	3	R	S-V1-V2-V3
VTS	73	1	1	3	45	0.000000	L	.11981198E+09	.11032978E+03	.21361320E+02	2	RAE	S-V1
VTS	73	1	1	3	45	0.000000	M	.31493094E+04	.30000000E+01	.10000000E+01	2	RD	S-V1-V2-V3
VTS	73	1	1	3	45	0.000000	K	.23971565E+09	.13534423E+04	.30000000E+01	2	R	RD
VTS	73	1	1	3	45	0.000000	L	.31735248E+09	.10000000E+01	.30000000E+01	2	R	RD
VTS	73	1	1	3	45	0.000000	0	-.19718713E-03	0.	0.	1	TDA	VS1-VS2
VTS	73	1	1	3	45	0.000000	0	-.62179390E-03	0.	0.	3	TDA	VS1-VS2
VTS	73	1	1	3	45	0.000000	0	.50343907E-02	0.	0.	2	TDA	VS1-VS2
AND	73	1	1	3	45	0.000000	7	.41340336E+03	0.	0.	1	RD	S-V1
AND	73	1	1	3	45	0.000000	L	.31366028E+09	.30000000E+01	.20000000E+01	1	R	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	M	-.12524770E+04	.10000000E+01	.20000000E+01	3	RD	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	P	.62036786E-01	0.	.10000000E+01	2	TDOA	SV1V2-SV2
AND	73	1	1	3	45	0.000000	L	.26036763E+09	.30000000E+01	.10000000E+01	2	R	S-V1-V2-V3
AND	73	1	1	3	45	0.000000	F	.17033413E+00	0.	.30000000E+01	2	TDDA	SV1V2-SV2

AND	VTS	73	1	1	4	0	0.000000	M	.20019879E+04	.10000000E+01	0.	30000000E+01	2	RD	S-V1-V2-V3
AND	VTS	73	1	1	4	0	0.000000	R	.25274636E+00	0.	0.	0.	1	3MR	S1V1-S1V2
AND	VTS	73	1	1	4	0	0.000000	R	.32614652E+00	0.	0.	0.	3	3MR	S1V1-S1V2
AND	VTS	73	1	1	4	0	0.000000	R	.23677046E+00	0.	0.	0.	2	3MR	S1V1-S1V2
DUM		73	1	1	4	0	0.000000	J	.77636833E+00	.67276291E+03		.30000000E+01	1	R RD	V1-V2
DUM		73	1	1	4	0	0.000000	S	.20436045E+00	0.		.30000000E+01	1	MULT	V1E2-V1V2
DUM		73	1	1	4	0	0.000000	N	.19754050E+09	.20000000E+01		.30000000E+01	1	R	V1-V2-V3
DUM		73	1	1	4	0	0.000000	O	-.58913181E+03	.20000000E+01		.30000000E+01	1	R RD	V1-V2-V3
DUM		73	1	1	4	0	0.000000	J	.69362666E+00	-.14779062E+03		.20000000E+01	1	R RD	V1-V2
DUM		73	1	1	4	0	0.000000	S	.16210166E+00	0.		.20000000E+01	1	MULT	V1E2-V1V2
DUM		73	1	1	4	0	0.000000	J	.11990367E+09	-.12618947E+04		.30000000E+01	2	R RD	V1-V2

EXIT SEGMENT 61 AT 1.2 SECONDS. EXECUTION TIME FOR SEGMENT 61 MAC .5 CP SECS.

D. TRACE INPUT FORMS

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APPENDIX D
TRACE INPUT FORMS

INTRODUCTION

The engineering specification forms and load sheets that follow are very useful in expediting the preparation of TRACE input. Some of these forms bear former TRACE designations (TRACE-66 and TRACE66), which will be removed when the forms are updated.

TRAJECTORY ANALYSIS AND PROGRAMMING DEPARTMENT

TRACE66 (AD104A)

ENGINEERING REQUEST FORM

GENERAL INFORMATION:

REQUESTER _____ TELEPHONE _____ DATE _____

PROBLEM NUMBER OR J.O. _____ DATE _____

PROJECT _____

TYPE OF TRACE RUN:

EPHEMERIS GENERATION ()
ORBIT DETERMINATION ()
DATA GENERATION ()
COVARIANCE ANALYSIS ()

GENERAL INSTRUCTIONS:

IF A RERUN, USE DATA DECK LABELED _____

NEW DATA DECK TO BE SAVED: () YES () NO

DISPOSITION (TO BE COMPLETED BY PRODUCTION COORDINATOR)

SET UP BY _____ RUN IO _____ DATE _____

TAPE SAVED IF REQUIRED _____

JOB DISPOSITION AND RESULTS:

NOTE: ALL SPECIFIED INPUT UNITS MUST BE CONSISTENT.

TIME OF RUN:

CP _____ PP _____

DATE JOB COMPLETED _____

DATA DECK LABELED AS _____

TRACE 66
ORBIT AND FORCE MODEL SPECIFICATIONS

RUN TITLE: _____

EPOCH:	INITIAL CONDITIONS: INDICATE THE TYPE USED								VALUES
	11	12	13	14	15	16	17	18	
YEAR	_____	_____	_____	_____	_____	_____	_____	_____	_____
MONTH	_____	_____	_____	_____	_____	_____	_____	_____	_____
DAY	_____	_____	_____	_____	_____	_____	_____	_____	_____
TIME ZONE	_____	_____	_____	_____	_____	_____	_____	_____	_____
HOUR	_____	_____	_____	_____	_____	_____	_____	_____	_____
MINUTE	_____	_____	_____	_____	_____	_____	_____	_____	_____
SECOND	_____	_____	_____	_____	_____	_____	_____	_____	_____

NOTE: IF K TYP IS NEGATIVE, THEN THE UNITS OF THE INITIAL CONDITIONS ARE ASSUMED TO BE INTERNAL.
LUNAR INITIAL CONDITIONS ARE TYPES 11 THROUGH 18, CORRESPONDING TO THE ABOVE EARTH-REFERENCED TYPES 1 THROUGH 8.

GRAVITY MODEL: CHECK ONE.

SPHERICAL ()	STANDARD 6.6 ()	STANDARD 7.6 ()
C_2, C_3, C_4 ()	STANDARD 8.8 ()	OTHER (ATTACH) ()

SUN-MOON ATTRACTIONS: NO () YES ()

DRAG COEFFICIENT: $C_D A / W =$ _____ FT^2/LB

SEGMENTED DRAG COEFFICIENTS: $(C_D A / W)_i =$ _____

$(C_D A / W)_1 =$ _____ $t_1 =$ _____ MME	$(C_D A / W)_2 =$ _____ $t_2 =$ _____ MME
$(C_D A / W)_3 =$ _____ $t_3 =$ _____ MME	$(C_D A / W)_4 =$ _____ $t_4 =$ _____ MME
$(C_D A / W)_5 =$ _____ $t_5 =$ _____ MME	$(C_D A / W)_6 =$ _____ $t_6 =$ _____ MME
$(C_D A / W)_7 =$ _____ $t_7 =$ _____ MME	$(C_D A / W)_8 =$ _____ $t_8 =$ _____ MME

C_D TABLES: INDICATE THE OPTION TO BE USED AND ATTACH TABLES IF ANY

() NONE () $C_D = f(t)$ () $C_D = f(h)$

LINEAR WEIGHT LOSS: NO () YES () $\dot{W}_0 =$ _____ $W_{MIN} =$ _____ LBS
 $\dot{W} =$ _____ LBS/MIN $t_b =$ _____ MME $t_1 =$ _____ MME

INSTANTANEOUS WEIGHT CHANGES: NO () YES () ATTACH TABLES

ATMOSPHERE MODEL: CHECK ONE AND PROVIDE INPUTS AS REQUIRED

ARDC 1959 () US STD 1962 ()

EXPONENTIAL: () $\rho_0 =$ _____ $\beta =$ _____ $h =$ _____

NM1 () $c_1 =$ _____ $c_2 =$ _____ $c_3 =$ _____
 $c_4 =$ _____ $c_5 =$ _____ $c_6 =$ _____
 $n =$ _____ $i =$ _____

LOCKHEED-JACCHIA () $D1 =$ _____ $D2 =$ _____ FLUX = _____

EMSC 1967 () $\bar{F}_{10} =$ _____ $F_{10} =$ _____ $k_p =$ _____

JACCHIA 1964 () $\bar{F}_{10} =$ _____ $F_{10} =$ _____ $a_p =$ _____

JACCHIA 1964 (MOD) () $\bar{F}_{10} =$ _____ $F_{10} =$ _____ $a_p =$ _____

CR1 () $\bar{F}_{10} =$ _____ $F_{10} =$ _____ $k_1 =$ _____

IF a_p, F_{10}, k_p OR k_c ARE TO BE FUNCTIONS OF TIME, ATTACH TABLES.

SOLAR RADIATION PRESSURE: NO () YES ()

$A W =$ _____ FT^2/LB $C_p =$ _____ LBS/FT^2 $(C_p A W) =$ _____

ONBOARD ACCELEROMETER: NO () YES () ATTACH TABLES

FINITE THRUSTING: NO () YES () ATTACH TABLES

ORBIT ADJUSTS: NO () YES () ATTACH TABLES

INPUT LENGTH UNITS ARE IN _____ (ft, m, cm, km, etc.)

AEROSPACE FORM 6134 REV 9-71

TRACE66
ORBIT DETERMINATION SPECIFICATIONS

ALL PARAMETERS MUST BE SPECIFIED ON THE TRACE66 PARAMETER SPECIFICATION FORM.

OBSERVATIONS ARE TO BE INPUT BY:

- () CARDS
 - () CARD IMAGE TAPE
 - () BINARY OBSERVATION TAPE
- IF CARDS OR A CARD IMAGE TAPE ARE BEING USED AND THE OBSERVATION DATA TO BE USED IS A SUBSET OF THE DATA PROVIDED, THE BEGINNING AND END OF THE INTERVAL TO BE USED ARE GIVEN BY:

BEGINNING YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____
END YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____

STATION INPUTS: η_E AND η_R ARE THE INDICES OF REFRACTION USED TO COMPUTE REFRACTION CORRECTIONS FOR ELEVATION AND RANGE DATA. A "✓" INDICATES THE NOMINAL VALUES ARE TO BE USED, A "0" INDICATES NO CORRECTIONS AND IF A NON-STANDARD INDEX OF REFRACTION IS TO BE USED, IT MUST BE PROVIDED.

STA NAME	LAT (DEG)	LONG (DEG)	HEIGHT (FEET)	INTERFEROMETER		η_E (312×10^{-6})	η_R (350×10^{-6})
				P	Q		
_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____

OBSERVATION WEIGHTS (σ 's):

STA	DATA		DATA		DATA		DATA	
	TYPE	σ	TYPE	σ	TYPE	σ	TYPE	σ
_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____

SUPPLY THE REQUIRED INPUTS FOR THE FOLLOWING IF OTHER THAN NOMINAL.

- _____ MAXIMUM NUMBER OF ITERATIONS
- _____ RELATIVE CONVERGENCE TEST (.001)
- _____ ABSOLUTE CONVERGENCE TEST (0)
- _____ n FOR n-SIGMA EDITOR (100)

OPTIONS: CHECK THE OPTIONS DESIRED AND SUPPLY THE REQUIRED INPUT

- () SPEED OF LIGHT CORRECTION
 - () POSITIVE CORRECTION
 - () NEGATIVE CORRECTION
- () PRINT OBSERVATION RESIDUALS
- () PRINT OBSERVATION PARTIAL DERIVATIVES
- () PRINT ORDERED CORRELATION MATRIX
- () PRINT CORRELATION MATRIX AFTER LAST ITERATION
- () SUPPRESS CORRELATION MATRICES
- () PRINT $A^T A$ AND $(A^T A)^{-1}$ AFTER EACH ITERATION, OR LAST ITERATION ONLY
- () PUNCH $A^T A$ AFTER LAST ITERATION
- () PUNCH SOLUTION VECTOR
- () PRINTER PLOT OF OBSERVATION RESIDUALS AFTER LAST ITERATION
- DATA RATE IS _____ SEC
- () GENERATE AND SAVE OBSERVATION RESIDUAL TAPE

TRACE-66
TRAJECTORY OUTPUT SPECIFICATIONS

OUTPUT TIMES: TIMES ARE GIVEN AS MINUTES FROM EPOCH () OR MIDNIGHT ()

FROM _____	TO _____	EVERY _____ MIN
_____	_____	_____
_____	_____	_____
_____	_____	_____
_____	_____	_____
_____	_____	_____

SPECIAL OUTPUT TIMES: (✓)

$\beta = 90$ ()
 MIN , MAX. ALTITUDE ()
 SPECIAL LATITUDES ()
 SPECIAL LONGITUDES ()
 SPECIAL ALTITUDES ()
 OBSERVATION TIMES ()

SPECIAL

LAT.	LONG.	ALT.
_____	_____	_____
_____	_____	_____
_____	_____	_____
_____	_____	_____

OUTPUT REQUESTED: (✓)

STANDARD

a) EVERY TIME ()
 b) NOOES ONLY ()

ECLIPSING

a) STANDARD ()
 b) OPTIONAL ()

ELEMENTS

a) EVERY TIME ()
 b) NOOES ONLY ()

VARIATIONAL EQUATIONS

a) STANDARD ()
 b) OPTION B ()
 c) OPTION C ()

GEOMAGNETIC LAT. AND LONG. ()
 SUN-MOON ANGLES

a) STANDARD ()
 b) OPTION Y ()
 c) OPTION Z ()

GROUND TRACK TAPE ()
 DIFFERENCE TAPE ()

TRACE66

COVARIANCE ANALYSIS SPECIFICATIONS

ALL PARAMETERS MUST BE SPECIFIED ON THE TRACE66 PARAMETER SPECIFICATION FORM.
OBSERVATION GENERATION SPECIFICATIONS MUST BE SUPPLIED ON THE TRACE66 DATA GENERATION SPECIFICATIONS - SHEET 1.

IF OBSERVATIONS ARE TO BE INPUT RATHER THAN GENERATED, INDICATE THE SOURCE

CARDS CARD IMAGE TAPE BINARY OBSERVATION TAPE

IF CARDS OR A CARD IMAGE TAPE ARE BEING USED AND THE OBSERVATION DATA TO BE USED IS A SUBSET OF THE DATA PROVIDED, THE BEGINNING AND END OF THE INTERVAL TO BE USED ARE GIVEN BY:

BEGINNING YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC. _____
END YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC. _____

STATION INPUTS: η_E AND η_R ARE THE INDICES OF REFRACTION USED TO COMPUTE REFRACTION CORRECTIONS FOR ELEVATION AND RANGE DATA. A "V" INDICATES THE NOMINAL VALUES ARE TO BE USED, A "O" INDICATES NO CORRECTIONS, AND IF A NON-STANDARD INDEX IS TO BE USED, IT MUST BE PROVIDED.

STA NAME	LAT (DEG)	LONG (DEG)	HEIGHT (FEET)	INTERFEROMETER		η_E (112×10^{-6})	η_R (150×10^{-6})
				P	Q		

OBSERVATION WEIGHTS (σ 's):

STA	DATA TYPE	σ	DATA TYPE	σ	DATA TYPE	σ

OUTPUT TIMES: TIMES ARE GIVEN IN MINUTES FROM EPOCH () OR MIDNIGHT ()

FROM _____ TO _____ EVERY _____ MIN.

OUTPUT REQUESTED: () P Q

- | | | | |
|-------------------------------|------------------------------|------------------------------|--|
| $(P_0) = (A^T A)^{-1}$ | <input type="checkbox"/> () | <input type="checkbox"/> () | IF A "V" IS USED THE ENTIRE COVARIANCE MATRIX WILL BE PRINTED. IF A "D" IS USED, ONLY THE SQUARE ROOT OF THE DIAGONAL WILL BE PRINTED. |
| CARTESIAN | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| ORBIT PLANE | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| SPHERICAL | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| ELEMENT | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| PERIOD, AMPER | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| EQUINOCTIAL | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| MEASUREMENT COVARIANCE | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| PRINT $\partial P \partial Q$ | <input type="checkbox"/> () | <input type="checkbox"/> () | |
| SAVE PLOT TAPE | <input type="checkbox"/> () | <input type="checkbox"/> () | |

INPUT A PRIORI UNCERTAINTIES	P PARAMETER	Q PARAMETER
NO A PRIORI INFORMATION	()	()
A ^T A MATRIX GIVEN	()	()
(A ^T A) ⁻¹ MATRIX GIVEN	()	()
σ 's GIVEN	()	()
C(Q) MATRIX GIVEN	()	()

TRACE66
DATA GENERATION SPECIFICATION SHEET 1

STATIONS	_____	_____	_____	_____	_____	_____	_____	_____
SUPPLY VALUES FOR								
Δt (SEC)	_____	_____	_____	_____	_____	_____	_____	_____
E MIN (DEG)	_____	_____	_____	_____	_____	_____	_____	_____
E MAX (DEG)	_____	_____	_____	_____	_____	_____	_____	_____
R MAX (NM)	_____	_____	_____	_____	_____	_____	_____	_____
START TIME								
FROM	DAY	_____	_____	_____	_____	_____	_____	_____
MIDNIGHT	HR	_____	_____	_____	_____	_____	_____	_____
OF EPOCH	MIN	_____	_____	_____	_____	_____	_____	_____
STOP TIME								
FROM	DAY	_____	_____	_____	_____	_____	_____	_____
MIDNIGHT	HR	_____	_____	_____	_____	_____	_____	_____
OF EPOCH	MIN	_____	_____	_____	_____	_____	_____	_____
A_1 (DEG)	_____	_____	_____	_____	_____	_____	_____	_____
A_2 (DEG)	_____	_____	_____	_____	_____	_____	_____	_____
INDICATE THE REQUESTED DATA WITH A "✓"								
RANGE	_____	_____	_____	_____	_____	_____	_____	_____
AZIMUTH	_____	_____	_____	_____	_____	_____	_____	_____
ELEVATION	_____	_____	_____	_____	_____	_____	_____	_____
RANGE RATE	_____	_____	_____	_____	_____	_____	_____	_____
INTERFEROMETER \dot{P}	_____	_____	_____	_____	_____	_____	_____	_____
INTERFEROMETER \dot{Q}	_____	_____	_____	_____	_____	_____	_____	_____
INTERFEROMETER P	_____	_____	_____	_____	_____	_____	_____	_____
INTERFEROMETER Q	_____	_____	_____	_____	_____	_____	_____	_____
AZIMUTH RATE	_____	_____	_____	_____	_____	_____	_____	_____
ELEVATION RATE	_____	_____	_____	_____	_____	_____	_____	_____
f_s	_____	_____	_____	_____	_____	_____	_____	_____
LATITUDE	_____	_____	_____	_____	_____	_____	_____	_____
LONGITUDE	_____	_____	_____	_____	_____	_____	_____	_____
SURFACE RANGE	_____	_____	_____	_____	_____	_____	_____	_____
HEIGHT	_____	_____	_____	_____	_____	_____	_____	_____
DOPPLER RATE	_____	_____	_____	_____	_____	_____	_____	_____
LOOK ANGLE	_____	_____	_____	_____	_____	_____	_____	_____
KAPPA	_____	_____	_____	_____	_____	_____	_____	_____
ASPECT ANGLES	_____	_____	_____	_____	_____	_____	_____	_____
ATTENUATION	_____	_____	_____	_____	_____	_____	_____	_____
ξ, ζ, η	_____	_____	_____	_____	_____	_____	_____	_____
TOPOCENTRIC RT.	_____	_____	_____	_____	_____	_____	_____	_____
ASC. AND DEC.	_____	_____	_____	_____	_____	_____	_____	_____
GEOCENTRIC RT.	_____	_____	_____	_____	_____	_____	_____	_____
ASC. AND DEC.	_____	_____	_____	_____	_____	_____	_____	_____
HOOR ANGLE	_____	_____	_____	_____	_____	_____	_____	_____
u, v	_____	_____	_____	_____	_____	_____	_____	_____
\ddot{A}	_____	_____	_____	_____	_____	_____	_____	_____
\ddot{E}	_____	_____	_____	_____	_____	_____	_____	_____
TWO-WAY DOPPLER	_____	_____	_____	_____	_____	_____	_____	_____
ANTENNA X, Y ANGLES	_____	_____	_____	_____	_____	_____	_____	_____
TRANET DOPPLER	_____	_____	_____	_____	_____	_____	_____	_____
GEOCEIVER RANGE	_____	_____	_____	_____	_____	_____	_____	_____
Ranging or Diff(s)	_____	_____	_____	_____	_____	_____	_____	_____
SGLS RANGE RATE	_____	_____	_____	_____	_____	_____	_____	_____

AE' JSPACE FORM 6136 REV 8-71

STATION CARDS

1. THE LOCATION FIELDS MUST HAVE A DECIMAL POINT.
2. THE EXPONENT FIELDS ARE OPTIONAL, BUT IF USED MUST BE OF THE FORM \uparrow XX.

PROGRAMMER		KEYPUNCHED		VERIFIED		DATE		PAGE		OF
ST	I	E	R	D	T	FIELD 1	FIELD 2	FIELD 3	P	Q
1 2 3	5 7 9	11 13	15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	31 32 33 34 35 36 37 38 39 40 41 42 43 44 45	47 48 49 50 51 52 53 54 55 56 57 58 59 60 61	64 65 66	68 69 70	74 75 76	78 79 80	84 85 86
1 2 3										

TRACE - 66: DATA GENERATION I

- 1 A DECIMAL POINT MUST BE USED IN ALL FIELDS FLAGGED BY AN *
- 2 IF THE EXPONENT IS TO BE USED IN THE R_{max} FIELD, IT MUST BE OF THE FORM $\pm XX$

ST	ΔT (sec)*	E_{min} (deg)*	E_{max} (deg)*	R_{max} (mm)*	EXP	START TIME			STDP TIME			A_1 (deg)*	A_2 (deg)*
						DY	HR	MIN *	DY	HR	MIN *		
1	5	14	21	28	30	38	41	44	52	55	58	66	73
2	6	15	22	29	31	39	42	45	53	56	59	67	74
3	7	16	23	30	32	40	43	46	54	57	60	68	75
4	8	17	24	31	33	41	44	47	55	58	61	69	76
5	9	18	25	32	34	42	45	48	56	59	62	70	77
6	10	19	26	33	35	43	46	49	57	60	63	71	78
7	11	19	26	33	35	43	46	49	57	60	63	71	78

PROGRAMMER _____ KEYPUNCHED _____ VERIFIED _____ DATE _____ PAGE _____ DF _____

LEADSPACE FORM 351A REC-5 67

TRACE 66
 SIMULTANEOUS VEHICLE
 DATA GENERATION II CARDS

PROGRAMMER	KEYPUNCHED										VERIFIED										DATE										PAGE										OF																																																																													
	ST A	T	O	O	O	V	1	V	2	V	3	ST A	T	O	O	O	V	1	V	2	V	3	ST A	T	O	O	O	V	1	V	2	V	3	ST A	T	O	O	O	V	1	V	2	V	3	ST A	T	O	O	O	V	1	V	2	V	3																																																															
1 2 3	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122

TRACE 66 - SIMULTANEOUS VEHICLE STAGE INPUT

1. A DECIMAL POINT MUST BE USED IN ALL FIELDS FLAGGED BY AN *.

PRDGRAMMER	N*	AT*	KEYPUNCHED				VERIFIED				DATE				PAGE				OF
			T BEGIN	T END	T UPDATE	T CND	YR	MO	DA	SEC	YR	MO	DA	SEC	YR	MO	DA	SEC	
1 2 3 4	6 7 8 9	11 12 13 14 15 16 17	21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38	40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57	60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79	80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99													

RESPACE FORM 4448 REV 10-71

