

AD-759 482

A METHOD FOR OBTAINING AERODYNAMIC COEFFICIENTS FROM YAWSONDE AND RADAR DATA

R. H. Whyte, et al

Ballistic Research Laboratories
Aberdeen Proving Ground, Maryland

March 1973

DISTRIBUTED BY:

NTIS

National Technical Information Service
U. S. DEPARTMENT OF COMMERCE
5285 Port Royal Road, Springfield Va. 22151

BRL MR 2280

AD

BRL

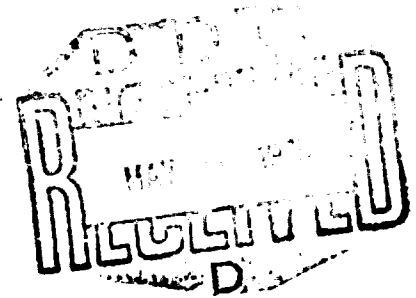
MEMORANDUM REPORT NO. 2280

A METHOD FOR OBTAINING AERODYNAMIC
COEFFICIENTS FROM YAWSONDE AND RADAR DATA

by

R. H. Whyte
W. H. Mermagen

March 1973



Approved for public release; distribution unlimited.

Reproduced by
NATIONAL TECHNICAL
INFORMATION SERVICE
U S Department of Commerce
Springfield VA 22151

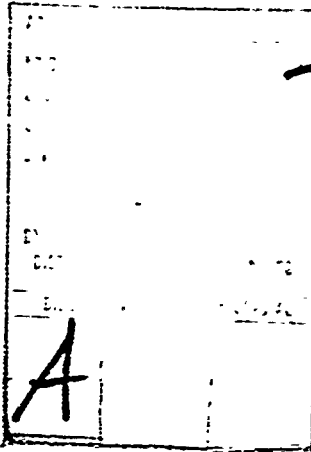
USA BALLISTIC RESEARCH LABORATORIES
ABERDEEN PROVING GROUND, MARYLAND

AL 759482

Destroy this report when it is no longer needed.
Do not return it to the originator.

Secondary distribution of this report by originating
or sponsoring activity is prohibited.

Additional copies of this report may be obtained
from the Defense Documentation Center, Cameron
Station, Alexandria, Virginia 22314.



The findings in this report are not to be construed as
an official Department of the Army position, unless
so designated by other authorized documents.

UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) U. S. Army Ballistic Research Laboratories Aberdeen Proving Ground, Maryland 21005		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE A METHOD FOR OBTAINING AERODYNAMIC COEFFICIENTS FROM YAWSONDE AND RADAR DATA			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
5. AUTHOR(S) (First name, middle initial, last name) Robert H. Whyte William H. Mermagen			
6. REPORT DATE MARCH 1973		7a. TOTAL NO. OF PAGES 36	7b. NO. OF REFS 12
8a. CONTRACT OR GRANT NO.		9a. ORIGINATOR'S REPORT NUMBER(S) BRL MEMORANDUM REPORT NO. 2280	
b. PROJECT NO. RDT&E 1T061102A53D		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
c.			
d.			
10. DISTRIBUTION STATEMENT Approved for public release; distribution unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY U. S. Army Materiel Command Washington, D. C. 20315	
13. ABSTRACT A numerical integration method for the reduction of yawsonde data from instrumented projectiles in free flight has been developed. Yawsonde data represent two-dimensional information (solar aspect angle and spin) while the actual motion is three-dimensional (pitch, yaw, and spin). The method obtains a best fit of the aerodynamic coefficients in the equations of motion using numerical integration. The coefficients are iteratively adjusted in the manner developed by Chapman and Kirk. Trajectory information is derived from radar track data and is reduced to provide axial force coefficients and earth-fixed velocity components. The trajectory data reduction uses the same numerical integration method as the angular data reduction. The results of the trajectory or swerve reduction are used as inputs to the angular reduction. Linear aerodynamic coefficients have been derived from the flight of an M549, 155mm rocket assisted projectile. Values of non-linear aerodynamic coefficients have also been obtained using the numerical integration method but their validity remains to be proven. Both the angular and the trajectory reductions include the effects of wind.			

DD FORM 1473

NOV 68

REPLACES DD FORM 1473, 1 JAN 64, WHICH IS OBSOLETE FOR ARMY USE.

UNCLASSIFIED

Security Classification

UNCLASSIFIED
Security Classification

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Yawsonde Aerodynamics Radar Data Reduction Numerical Methods Data Reduction Angular Motion Swerving Motion						

ii

UNCLASSIFIED
Security Classification

BALLISTIC RESEARCH LABORATORIES

MEMORANDUM REPORT NO. 2280

MARCH 1973

A METHOD FOR OBTAINING AERODYNAMIC COEFFICIENTS
FROM YAWSONDE AND RADAR DATA

R. H. Whyte
General Electric Company

and

W. H. Mermagen
Exterior Ballistics Laboratory

Approved for public release; distribution unlimited.

RD&E Project No. 1T061102A33D

ABERDEEN PROVING GROUND, MARYLAND

!

TABLE OF CONTENTS

	Page
ABSTRACT	3
LIST OF ILLUSTRATIONS	7
LIST OF SYMBOLS	9
I. INTRODUCTION	11
II. THEORETICAL CONSIDERATIONS	12
A. Equations of Motion	12
B. Solar Aspect Angle Relation	16
III. YAWSONDE REDUCTION PROCEDURE	17
IV. RESULTS AND DISCUSSION	18
A. Swerve Reduction	19
B. Angular Reduction	20
V. CONCLUSIONS	23
REFERENCES	29
DISTRIBUTION LIST	31

LIST OF ILLUSTRATIONS

Figure		Page
1.	Geometric Relationship of the Missile Axis to the Solar Vector in a Trajectory Coordinate System	24
2.	Schematic of the 155mm, M549 Rocket-Assisted Projectile. .	25
3.	Yawsonde Flight Data from an M549 Projectile	26
4.	A Small Data Interval Showing Goodness of Fit with Only Linear Coefficients	27
5.	A Comparison between C_m Obtained from Yawsonde Data and Wind Tunnel Tests	28

LIST OF SYMBOLS

A	= reference area
$C_{\dot{\omega}_p}$	= spin deceleration coefficient
C_m	= pitching moment coefficient
$C_{m\dot{q}}$	= damping in pitch coefficient
C_{n_p}	= Magnus moment coefficient
C_D	= drag coefficient
C_N	= normal force coefficient
C_X	= axial force coefficient
C_{Y_p}	= Magnus force coefficient
L	= reference diameter
g	= acceleration due to gravity
I_x	= axial moment of inertia
I	= transverse moment of inertia
m	= mass
p	= spin rate
\bar{q}	= dynamic pressure
t_i	= direction cosines of solar vector in earth-fixed coordinate system ($i = 1,2,3$)
u, v, w	= velocity components along missile x, y, z axes, respectively
V	= total missile velocity
$V_{w_{xe}}, V_{w_{ye}}$	= components of wind velocity along earth x, y axes, respectively

LIST OF SYMBOLS (continued)

V_{xe}, V_{ye}, V_{ze} = velocity components along earth x,y,z axes, respectively

x_e, y_e, z_e = earth fixed axes

$\bar{\alpha}$ = total angle of attack

δ_e, γ_e = trajectory elevation, azimuth, respectively

ϵ = $\sin \bar{\alpha}$

$\theta_{fp}, \psi_{fp}, \phi_{fp}$ = fixed plane missile orientation angles

ρ = density

σ = solar aspect angle

Superscripts

(\cdot) = differentiation with respect to time

($\ddot{}$) = second derivative with respect to time

Subscripts

v = velocity dependent

w = wind condition

a = force or moment coefficient slope

I. INTRODUCTION

During the past several years yawsondes have been used to measure in-flight dynamical behavior of projectiles over long flight paths^{1*}. The yawsonde produces large volumes of data on the solar aspect angle and spin of the shell during flight. Yawsonde data are two-dimensional. The angle between the projectile axis and the sun as well as the spin are determined along the flight path. The actual angular motion of the shell, however, is three-dimensional consisting of pitch, yaw, and spin. The basic problem is to extract the three-dimensional behavior of the shell from two-dimensional data. Additional information on the trajectory and meteorological conditions are required as inputs.

The conventional method for reducing data from free flight tests is to fit solutions to the equations of motion to the range data². Such procedures assume that the equations of motion can be solved in closed form or in an approximate way (quasi-linear). The conventional method can be applied to yawsonde data using a technique called WOBBLE³. A modified version of WOBBLE has been used with limited success¹. Still another method, developed by Haseltine⁴, uses an analog computer set up with the equations of motion. The operator adjusts the coefficients of the equations until the motion predicted by the analog computer agrees with the flight data.

Chapman and Kirk⁵ recently developed a method for fitting differential equations of motion directly to the data using a unique approach for adjusting the coefficients of the equations. This method does not require that the equations of motion have an analytical solution. Whyte and Beliveau have investigated the method of Chapman and Kirk and applied it to data from aerodynamic spark range firings with excellent results⁶.

In this report it will be shown that the numerical integration technique can be applied to yawsonde data to obtain linear aerodynamic coefficients over extended portions of the flight of a single projectile. Actual reductions were performed on a variety of projectile types. Here the discussion is limited to the work done on the 155mm, M549 rocket assisted projectile. This projectile was chosen so that direct comparisons could be made with the results of aerodynamic range and wind tunnel tests.

This report will discuss the aerodynamic equations for angular and swerving motion and the numerical integration method itself. The results of axial force and angular motion reduction will be presented and compared with linear theory reduction of range and wind tunnel tests. The effect of including wind and velocity dependent coefficients in the method is described and discussed.

*References are listed on page 29.

II. THEORETICAL CONSIDERATIONS

Linearized theory has been used to describe the motion of symmetric missile with outstanding success during the past two decades. The theory is, however, restricted to small angle motion with small velocity and spin changes and nearly linear aerodynamic coefficients. Nonlinear coefficients may be determined by linear theory from overlapping fits if sufficient data are available or if sufficient number of range tests of the same projectile are made.

None of the above restrictions apply to the method of Chapman and Kirk. This method is conceptually and practically attractive since aerodynamic coefficients can be determined by fitting the differential equations of motion directly to the observed angular motion data. The force coefficients can be obtained by fitting the equations of swerving motion directly to positional data. The general method can be summarized briefly as follows. The equations of motion appropriate to the behavior of the projectile are numerically integrated using estimated values of the coefficients and the initial conditions. The same equations of motion are partially differentiated on each coefficient forming a set of parametric equations. The parametric equations are then numerically integrated to obtain values of the partial derivatives with respect to each coefficient. A differential corrections equation is set up from a Taylor expansion of the dependent variables of the equations of motion. The data are then compared to the computed values of the dependent variables in a least squares sense and corrections to the coefficients are obtained from the differential corrections equations. The coefficients of the equations of motion are adjusted by these corrections and the process begins again with new values of coefficients. The method iterates until convergence is achieved.

A. Equations of Motion

The equations of motion of a symmetric missile have been derived in a fixed plane coordinate system⁷. The rotation of the earth is ignored and the aerodynamic coefficients are assumed to have the form of a power series (as functions of $\sin \alpha$).

$$C_{m\alpha} = a_0 + a_3 \epsilon^2 + a_5 \epsilon^4 + a_v (V - V_0) \quad (1)$$

$$C_{n p\alpha} = b_0 + b_3 \epsilon^2 + b_5 \epsilon^4 \quad (2)$$

$$C_{m q} = d_0 + d_2 \epsilon^2 \quad (3)$$

The static and Magnus coefficient expansions include fifth order coefficients and may even, in some cases, require higher order terms. The motion of the center of mass of the projectile is described by the force equations (4-6).

$$\dot{u} = -\bar{q} A C_x/m + g \sin \theta_{fp} - \dot{\theta}_{fp} w + \dot{\psi}_{fp} \cos \theta_{fp} v \quad (4)$$

$$\begin{aligned} \dot{v} = & -\bar{q} \frac{A}{m} C_{N\alpha} \frac{v_w}{V_w} + \bar{q} \frac{A}{m} \frac{pL}{2V_w} C_{Yp\alpha} \frac{w}{V_w} \\ & - \dot{\psi}_{fp} \cos \theta_{fp} [u + w \tan \theta_{fp}] \end{aligned} \quad (5)$$

$$\begin{aligned} \dot{w} = & -\bar{q} \frac{A}{m} C_{N\alpha} \frac{w}{V_w} - \bar{q} \frac{A}{m} \frac{pL}{2V_w} C_{Yp\alpha} \frac{v}{V_w} - g \cos \theta_{fp} \\ & + \dot{\psi}_{fp} v \sin \theta_{fp} + \dot{\theta}_{fp} u \end{aligned} \quad (6)$$

The angular motion of the projectile is described by the moment equations (7-9).

$$\ddot{\phi}_{fp} = \bar{q} \frac{AL}{I_x} \frac{pL}{2V_w} C_{Lp} + \ddot{\psi}_{fp} \sin \theta_{fp} + \dot{\psi}_{fp} \dot{\theta}_{fp} \cos \theta_{fp} \quad (7)$$

where the spin is $p = \dot{\phi}_{fp} - \dot{\psi}_{fp} \sin \theta_{fp}$

$$\begin{aligned} \ddot{\theta}_{fp} = & \bar{q} \frac{AL}{I} \left[a_0 + a_3 \epsilon^2 + a_5 \epsilon^4 + a_v (V - V_0) \right] \frac{w_w}{V_w} \\ & + \frac{\bar{q}AL^2}{2V_w I} \left[d_0 + d_2 \epsilon^2 \right] \dot{\theta}_{fp} \\ & + \bar{q} \frac{AL^2 p}{2V_w I} \left[b_0 + b_3 \epsilon^2 + b_5 \epsilon^4 \right] \frac{v}{V_w} \\ & - \dot{\psi}_{fp} p \frac{I_x}{I} \cos \theta_{fp} - \dot{\psi}_{fp}^2 \cos \theta_{fp} \sin \theta_{fp} \end{aligned} \quad (8)$$

$$\ddot{\psi}_{fp} = \left[-\bar{q} \frac{AL}{I} \left[a_0 + a_3 \epsilon^2 + a_5 \epsilon^4 + a_v (V - V_0) \right] \frac{v_w}{V_w} \right. \\ \left. + \bar{q} \frac{AL^2}{2V_w I} \left[d_0 + d_2 \epsilon^2 \right] \dot{\psi}_{fp} \cos \theta_{fp} \right. \\ \left. + \bar{q} \frac{AL^2 p}{2V_w I} \left[b_0 + b_3 \epsilon^2 + b_5 \epsilon^4 \right] \frac{w_w}{V_w} \right. \\ \left. + 2 \dot{\theta}_{fp} \dot{\psi}_{fp} \sin \theta_{fp} + \dot{\theta}_{fp} p \frac{I_x}{I} \right] / \cos \theta_{fp} \quad (9)$$

θ_{fp} and ψ_{fp} are angles which define missile orientation in the earth fixed plane coordinate system. θ_{fp} describes a rotation about the missile y-axis and ψ_{fp} is a rotation about the earth z-axis. It is convenient to express the force equations (4-6) in an earth fixed coordinate system. The transformations are equations (10-12).

$$V_{x_e} = u \cos \theta_{fp} \cos \psi_{fp} - v \sin \psi_{fp} + w \sin \theta_{fp} \cos \psi_{fp} \quad (10)$$

$$V_{y_e} = u \cos \theta_{fp} \sin \psi_{fp} + v \cos \psi_{fp} + w \sin \theta_{fp} \sin \psi_{fp} \quad (11)$$

$$V_{z_e} = -u \sin \theta_{fp} + w \cos \theta_{fp} \quad (12)$$

At this point we wish to take the effect of wind into account.

$$V_{x_e(w)} = V_{x_e} - V_{w x_e} \quad (13)$$

$$V_{y_e(w)} = V_{y_e} - V_{w y_e} \quad (14)$$

$$V_{z_e(w)} = V_{z_e} - V_{w z_e} \quad (15)$$

Differentiation of the transformation equations (10-15) and substitution into the force equations (4-6) gives the equations of motion of the center of mass in an earth fixed system:

$$\begin{aligned}
 \dot{V}_{x_e} = & -\bar{q} \frac{A}{m} \left[C_{x_0} + C_{x_2} \epsilon^2 \right] \cos \theta_{fp} \cos \psi_{fp} \\
 & + \bar{q} \frac{A}{m} C_{N_\alpha} \left(\frac{v_w}{V_w} \sin \psi_{fp} - \frac{w_w}{V_w} \sin \theta_{fp} \cos \psi_{fp} \right) \\
 & - \frac{\bar{q}A}{m} \frac{pL}{2V_w} C_{Y_{p_\alpha}} \left(\frac{w_w}{V_w} \sin \psi_{fp} + \frac{v_w}{V_w} \sin \theta_{fp} \cos \psi_{fp} \right) \\
 & - \frac{\bar{q}A}{m} \left[C_{x_v} (V_w - V_0) \right] \cos \theta_{fp} \cos \psi_{fp} \quad (16)
 \end{aligned}$$

$$\begin{aligned}
 \dot{V}_{y_e} = & -\bar{q} \frac{A}{m} \left[C_{x_0} + C_{x_2} \epsilon^2 \right] \cos \theta_{fp} \sin \psi_{fp} \\
 & - \bar{q} \frac{A}{m} C_{N_\alpha} \left(\frac{v_w}{V_w} \cos \psi_{fp} + \frac{w_w}{V_w} \sin \theta_{fp} \sin \psi_{fp} \right) \\
 & + \bar{q} \frac{A}{m} \frac{pL}{2V_w} C_{Y_{p_\alpha}} \left(\frac{w_w}{V_w} \cos \psi_{fp} - \frac{v_w}{V_w} \sin \theta_{fp} \sin \psi_{fp} \right) \\
 & - \frac{\bar{q}A}{m} \left[C_{x_v} (V_w - V_0) \right] \cos \theta_{fp} \sin \psi_{fp} \quad (17)
 \end{aligned}$$

$$\begin{aligned}
 \dot{V}_{z_e} = & \bar{q} \frac{A}{m} \left[C_{x_0} + C_{x_2} \epsilon^2 \right] \sin \theta_{fp} \\
 & - \bar{q} \frac{A}{m} C_{N_\alpha} \frac{w_w}{V_w} \cos \theta_{fp} \\
 & - \bar{q} \frac{A}{m} \frac{pL}{2V_w} C_{Y_{p_\alpha}} \frac{v_w}{V_w} \cos \theta_{fp} \\
 & + \frac{\bar{q}A}{m} \left[C_{x_v} (V_w - V_0) \right] \sin \theta_{fp} - g \quad (18)
 \end{aligned}$$

where

$$V_w = \left(V_{x_{e(w)}}^2 + V_{y_{e(w)}}^2 + V_{z_{e(w)}}^2 \right)^{1/2}, \text{ and } \bar{q} = \frac{1}{2} \rho V_w^2. \text{ The}$$

axial force coefficient has been expanded as

$$C_x = C_{x_0} + C_{x_2} \epsilon^2 \quad (19)$$

and the normal and Magnus force coefficients can be expanded

$$C_{N_\alpha} = n_0 + n_3 \epsilon^2 \quad (20)$$

$$C_{Y_{p_\alpha}} = m_0 + m_3 \epsilon^2 \quad (21)$$

A Mach number dependent axial force coefficient, C_{x_v} , has been included in equations (16-18) since large velocity changes are often encountered in flight data.

Time is the independent variable in the above equations rather than distance along the trajectory (arc length). Distance is a more natural base for data taken in aerodynamic spark ranges, while time is the natural variable for yawsonde and radar data. The method of Chapman and Kirk is now used in a computer program called HEEVE to best fit equations (16-18) to the radar position-time data. Estimated values of θ and ψ are used to obtain fitted values of position, velocity, axial force, normal force, and Magnus force. Before the angular motion equations (7-9) can be fitted to the yawsonde data, a relationship between the solar aspect angle and the angles θ_{fp} , ψ_{fp} must be derived.

B. Solar Aspect Angle Relation

Yawsonde data give one-dimensional angular motion of the missile with respect to the sun. The solar aspect angle, σ , is the angle between the longitudinal axis of the projectile and a vector directed from the projectile to the sun. Let t_1, t_2, t_3 be the direction cosines of the solar vector in an earth fixed coordinate system (Fig. 1). θ_{fp} and ψ_{fp} locate the axis of the projectile in the same coordinate system. The solar aspect angle is obtained from the dot product of a unit solar vector and a unit vector along the missile axis,

$$\cos \sigma = t_1 \cos \theta_{fp} \cos \psi_{fp} + t_2 \cos \theta_{fp} \sin \psi_{fp} + t_3 \sin \theta_{fp} \quad (22)$$

Equation (22) provides the required relationship between the solar aspect angle, the orientation of the sun, and the angles of the missile axis relative to the earth.

The angular motion of the projectile is fitted to the angular equations (7-9) in a least squares sense by comparing computed values of σ using equation (22) to the measured values of σ . The method of Chapman and Kirk is used to adjust the coefficients of the angular motion equations until the probable error of fit is a minimum.

III. YAWSONDE REDUCTION PROCEDURE

In order to obtain aerodynamic coefficients from yawsonde flight data, the center of mass motion of the projectile must first be well determined. Measurements of the physical properties of the shell are taken before firing and meteorological data on density, temperature, and wind velocities are noted at the time of firing. First a reduction on the position time data is made to obtain a best description of the trajectory. The results of this reduction are used as inputs to the angular motion reduction. If necessary, the results of the angular motion reduction could be fed back into the position-time reduction for improved accuracy.

The sequence of data reduction using the numerical integration technique is as follows. First the raw radar position-time data are reduced to obtain a drag profile. The inputs to this swerve reduction are measured values of position (x_e, y_e, z_e) and time, physical properties of the projectile, meteorological data on winds, density and temperature, and the direction cosines of the solar vector in an earth fixed coordinate system. The swerve reduction also requires estimated values of axial force, normal force, Magnus force, spin profile, spin damping, and static moment coefficient. Such estimates can be obtained from the known aerodynamics of similar projectiles or from ballistic range measurements. The swerve reduction provides an output of axial force (related to drag) versus Mach number, the spin damping, and best fit computed values of position, velocity, dynamic pressure, and spin, all as functions of time.

The results of the swerve reduction are used as inputs to the angular reduction along with the solar aspect angle data from the yawsonde. The angular reduction also requires the physical properties of the projectile and the meteorological data as inputs. Initial estimated values of the static moment, Magnus moment, and damping moments must also be furnished. The angular reduction provides an output of

best fitted values of solar aspect angle versus time plus the zero-dynamic coefficients for static, Magnus and damping moments. Since the yawsonde data usually span extensive portions of the trajectory including many periods of precession and nutation, the data are fit sectionally. The results of sectional fitting are average values of the aerodynamic coefficients over the data intervals. The entire reduction procedure is summarized in the following table.

Table I. Reduction Inputs and Outputs

	Swerve Reduction	Angular Reduction
Inputs	Measured x_e, y_e, z_e, t , mass, diameter, air density, wind velocity, direction cosines of sun, spin profile. Estimated $C_X, C_N, C_Y, C_{l_p}, C_m$	Direction cosines t_1, t_2, t_3 . Measured solar aspect angle, mass, moments of inertia, air density, wind velocity. Fitted p, \bar{q}, V, V_w . Estimated $C_N, C_Y, C_m, C_{n_p}, C_{m_q}$
Outputs	Computed $x_e, y_e, z_e, V, V_w, \bar{q}, I$. Fitted C_X, C_{l_p}	Computed σ versus t . Fitted C_m, C_{M_q}, C_{l_p}

IV. RESULTS AND DISCUSSION

The results of fitting for the translational and angular motion of a 155mm, M549 rocket assisted projectile are discussed below. This projectile was fired at Wallops Island, Virginia, on March 11, 1971, at 2009 hours Universal Time from a 1/20 twist tube. The muzzle velocity as determined by smear cameras was 321 meters/sec. The gun elevation was 490 mils. The physical characteristics of the shell and the wind data are summarized as follows:

Weight	= 42.75 kg
Location of c.g.	= 32.21 cm from base
Axial moment of inertia	= 0.1477 kg-m ²
Transverse moment of inertia	= 1.8009 kg-m ²
Diameter	= 15.5 cm

Length = 87.4 cm
 Mean wind speed = 12.8 m/sec
 Mean wind direction = 300 deg. from true North

An outline of the projectile is shown in Figure 2.

A. Swerve Reduction

A swerve reduction was performed on the data obtained from an FPS-16 radar which tracked the projectile from 5.3 seconds after launch to impact. In the swerve reduction the yaw of repose was estimated. Swerve reductions were performed both with and without wind effects. The results of the swerve reductions are given in Table II. The probable error in each parameter is shown in parentheses below the parameter.

Table II. Results of Swerve Reduction

	V_{Muzzle} m/s	V_{Impact} m/s	C_X	C_{N_α}	$C_{Y_{p_\alpha}}$	$C_{X_{\alpha^2}}$	Probable Error
Without Wind	323 (.12)	262 (.12)	.109 (.0003)	1.6 (a)	-1.1 (a)	1.5 (a)	1.1 m
With Wind	311 (.09)	251 (.09)	.119 (.0003)	1.6 (a)	-1.1 (a)	1.5 (a)	.8 m

^aHeld constant

The muzzle velocity without wind effects agrees well with the smear camera value of muzzle velocity. The errors in the fit decrease when wind effects are taken into account. In order to accomplish the swerve reduction, values of normal force, Magnus force, and nonlinear axial force coefficients were estimated and held constant during the reduction.

The spin damping coefficient, $C_{\dot{\alpha}_p}$, was determined for the flight by matching a computed spin history to a flight spin history derived from the yawsonde data. In this manner, $C_{\dot{\alpha}_p}$ was found to be $-0.025 \pm .001$.

B. Angular Reduction

A portion of the data from the yawsonde on board the projectile is shown in Figure 3. The data are solar aspect angle versus time between 5.0 and 17.0 seconds of the flight. The data clearly show a fast frequency and a slow frequency which can be identified as nutation and precession. The nutational amplitude damps out rather quickly while the precessional amplitude grows slowly. In order to obtain a reasonable value of damping moment at least several cycles of the precession must be included in the fit. The static moment will be the dominant factor.

A series of reductions were performed with variations in section length and data density. Data density refers to the number of data points per unit time included in the fit. Reductions were done with and without wind effects. Various combinations of linear and nonlinear coefficients were tried. The results of some reduction attempts are listed in Table III. On some reductions a velocity dependent static moment coefficient, a_v , was sought. On other reductions, the ratio of moments of inertia was a parameter of the fit.

The coefficients were not substantially affected by changes in section length or data density as can be seen by comparing runs 2, 3, and 7. The maximum length used was 14.41 seconds (run 7). For this length the probable error of fit was 0.31 degree. Runs 8 - 10 represent an attempt to extract nonlinear coefficients. A comparison between runs 1 and 2 shows the effect of wind. A change of 10% in static moment is observed and is considered significant. The changes in damping and Magnus moments are small and not significant.

The average total angle of attack for this flight was computed to be 1.72 degrees which represents small amplitude angular motion. Runs 2 - 7 show the linear static moment coefficient varying from 4.64 to 4.76 at an average Mach number of .74 over this part of the flight. The fit for run 7 can be seen in Figure 4 where the computed and measured solar aspect angle are plotted against time of flight. For the sake of short figures, only a section of the fit interval is displayed.

In Figure 5 the values of static moment coefficients from run 7 (linear) and run 10 (nonlinear) are compared to data from wind tunnel tests performed on the M549 projectile. The total static moment at an average angle of attack of 1.72 degrees is computed for an average Mach number of 0.74. Both the linear fit moment and the nonlinear fit moment agree well with wind tunnel results. To show the effect of not including wind, the static moment result of run 1 is also shown. The point is noticeably away from the wind tunnel data.

Wind tunnel Magnus moment measurements at the above values of Mach number and angle of attack give a $C_{n_p} = .0125$ while the Magnus moment

Table III. Aerodynamic Coefficients Derived from M549 Yawsonde Data

Run No.	Time Interval sec	$C_{m\alpha}$ or a_0	C_{mq} or d_0	$C_n p_\alpha$ or b_0	a_3	d_2	b_3	a_y
1	5.0 - 13.93	4.233 (.018) ^a	3.59 (.88)	-.796 (.045)				.0027
2 ^b	5.0 - 13.93	4.642 (.009)	2.80 (.49)	-.801 (.030)				-.0028
3	5.0 - 13.93	4.625 (.015)	2.81 (.79)	-.803 (.085)				-.0025
4	5.0 - 15.29	4.679 (.013)	1.65 (.64)	-.728 (.035)				-.0037
5	5.0 - 16.65	4.754 (.0125)	1.81 (.60)	-.735 (.029)				-.0051
6	5.0 - 18.03	4.763 (.0117)	3.65 (.58)	-.873 (.025)				-.0052

^aNumbers in () show probable error in parameters.

^bThe data density for run no. 2 was 80%. All other runs had only 20% data density.

Table III. Aerodynamic Coefficients Derived from M549 Yawsonde Data (continued)

Run No.	Time Interval sec	$C_{m\alpha}$ or a_0	C_{mq} or d_0	$C_{np\alpha}$ or h_0	a_3	d_2	b_3	a_v
7	5.0 - 19.41	4.709 (.012)	3.42 (.60)	-.869 (.023)				.0043
8	5.0 - 19.41	4.56 (.03)	3.78 (.76)	-.865 (.324)	100.19 (22.9)			.0039
9	5.0 - 19.41	4.56 (.03)	3.78 (1.11)	-.909 (.032)	113.65 (22.8)	1499.8 (1454.8)		.0039
10	5.0 - 19.41	4.68 (.09)	.897 (1.6)	-.49 (.16)	8.23 (7.8)		-254.3 (231)	.0038

computed from run 7 is $- .0124$. The damping moment coefficient from wind tunnel tests is $- 5.1$ while run 7 shows $+ 3.4$. In light of the yawsonde data shown in Figure 3, it would seem that Magnus and damping moments cannot be readily extracted from small amplitude motion where the nutational mode dominates the data.

V. CONCLUSIONS

A technique of numerical integration has been developed and applied to experimental radar and yawsonde data. The effects of wind and velocity dependent coefficients can readily be included in the method. Position-time radar data are readily reduced to aerodynamic coefficients with satisfactory results. Yawsonde data from a flight test of the M549 projectile easily yielded the static moment coefficient. Magnus and damping moment coefficients are difficult to extract from small amplitude, nutation-dominated motion. The capability of extracting three-dimensional angular motion from two-dimensional yawsonde data has been demonstrated.

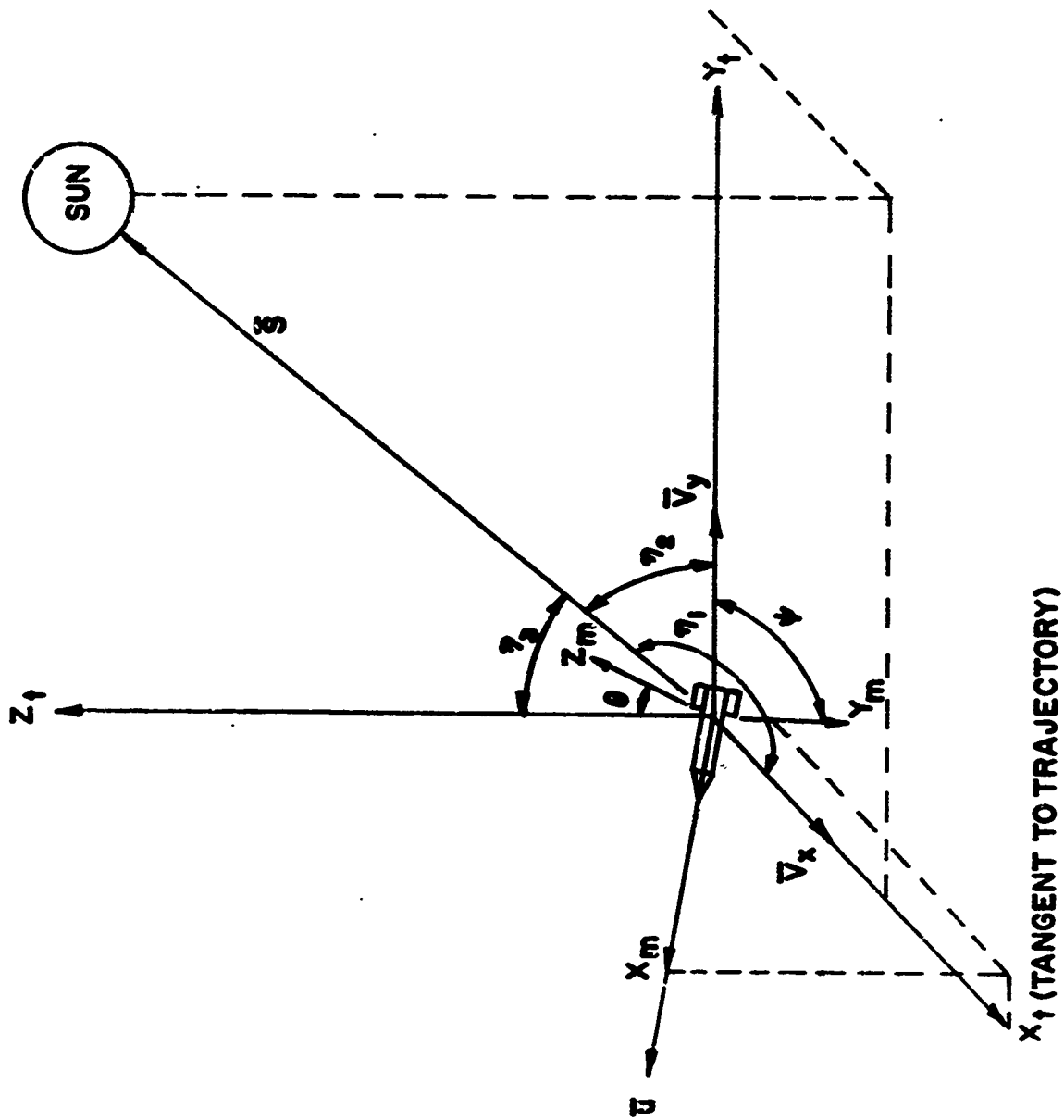
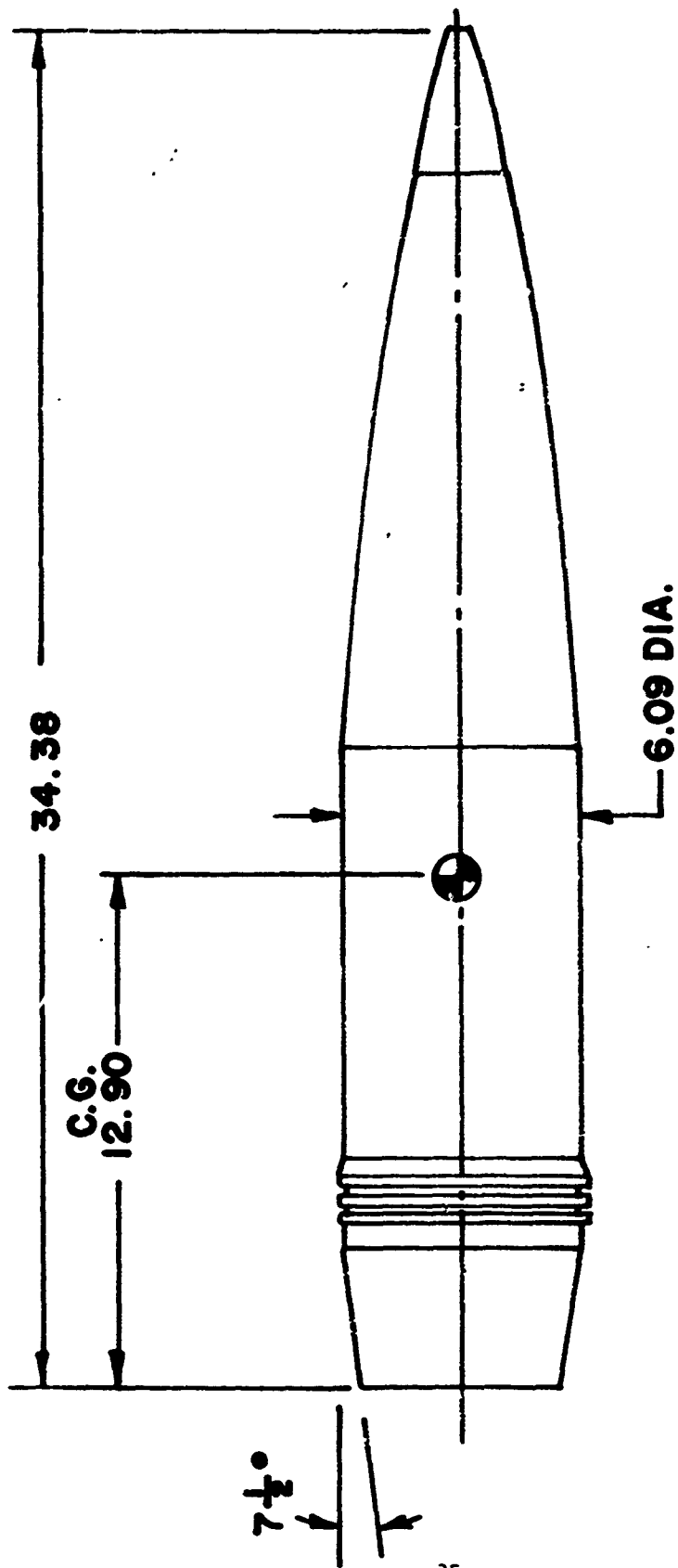


Figure 1. Geometric Relationship of the Missile Axis to the Solar Vector in a Trajectory Coordinate System



ALL DIMENSIONS ARE IN INCHES

Figure 2. Schematic of the 155mm, M549 Rocket-Assisted Projectile

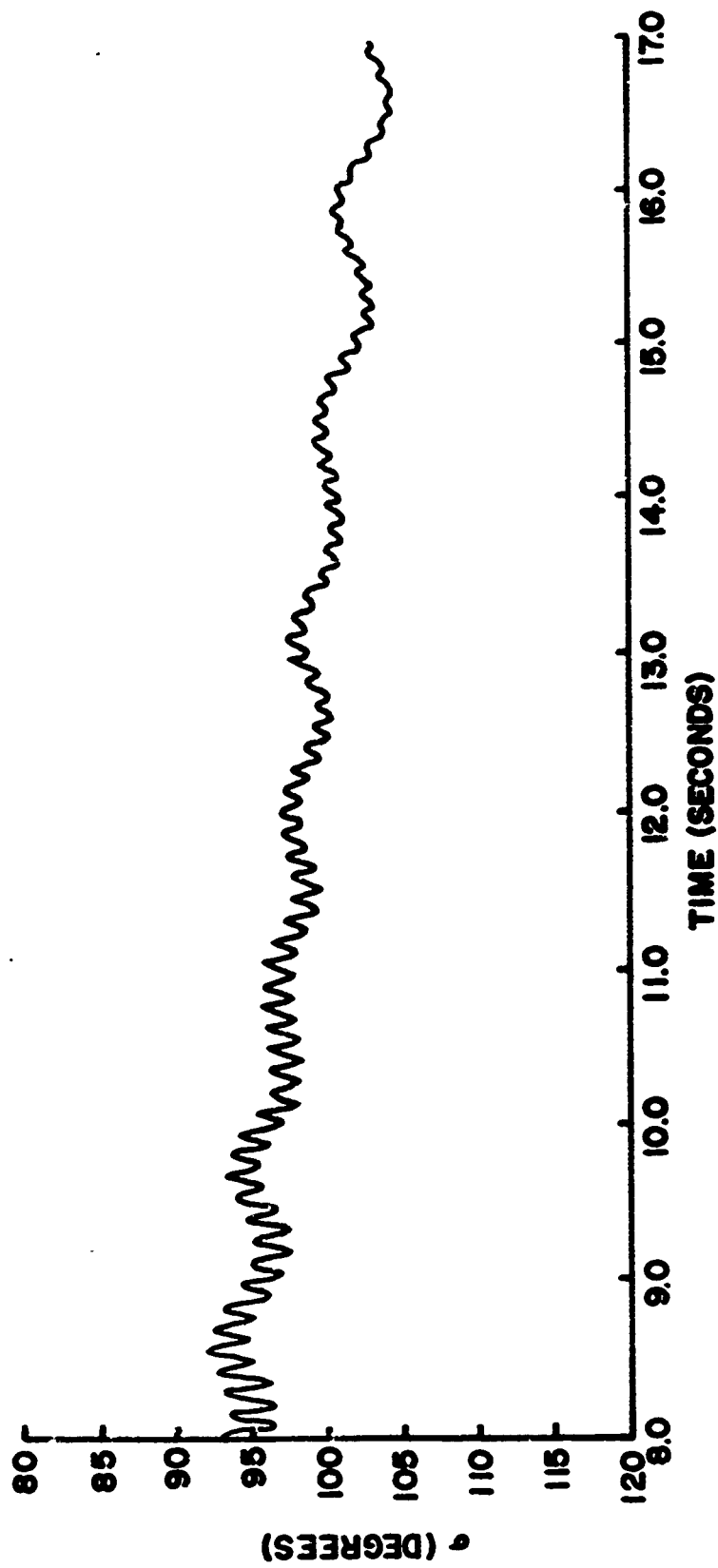


Figure 3. Yawsonde Flight Data from an M549 Projectile

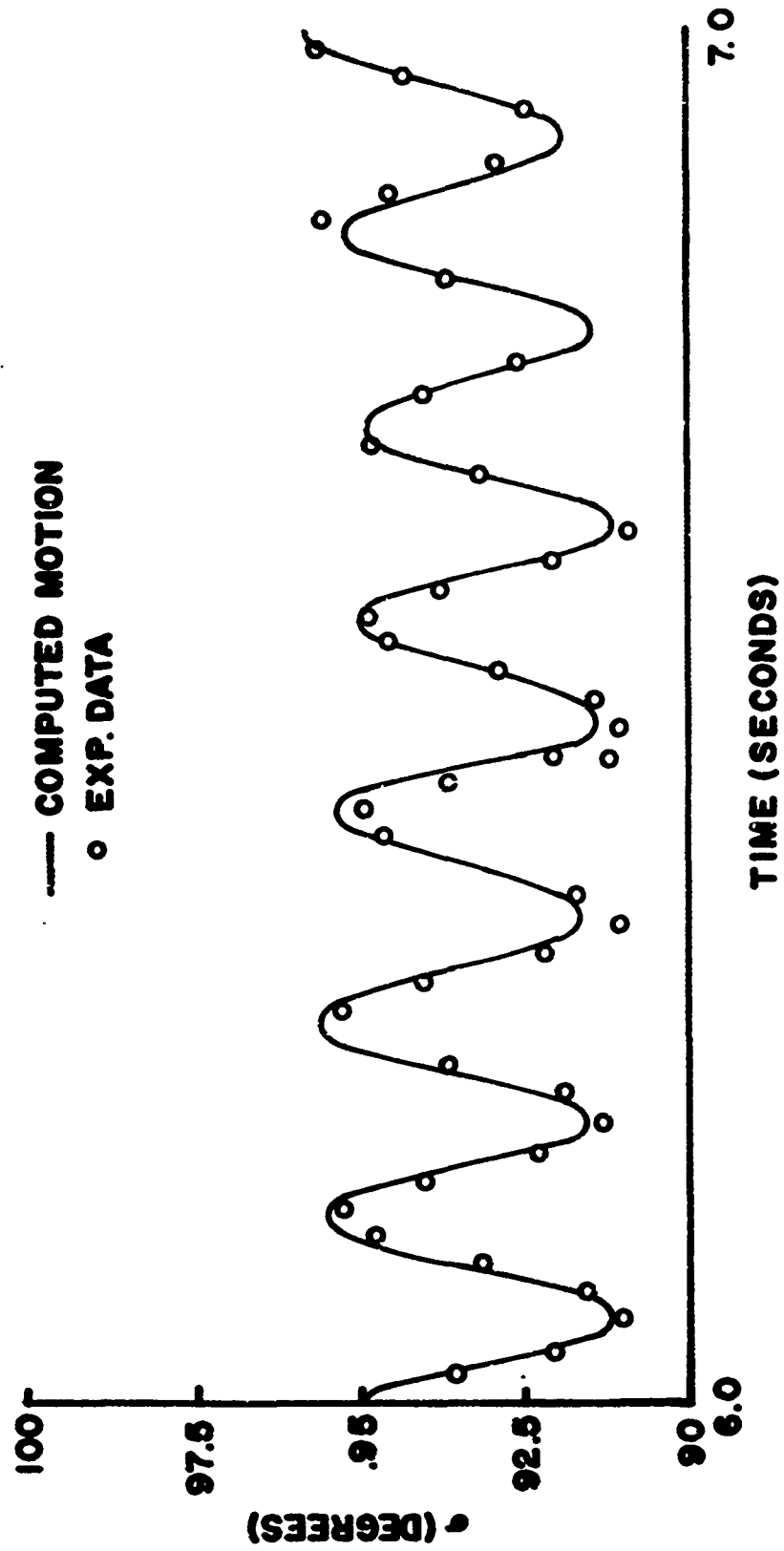


Figure 4. A Small Data Interval Showing Goodness of Fit with Only Linear Coefficients

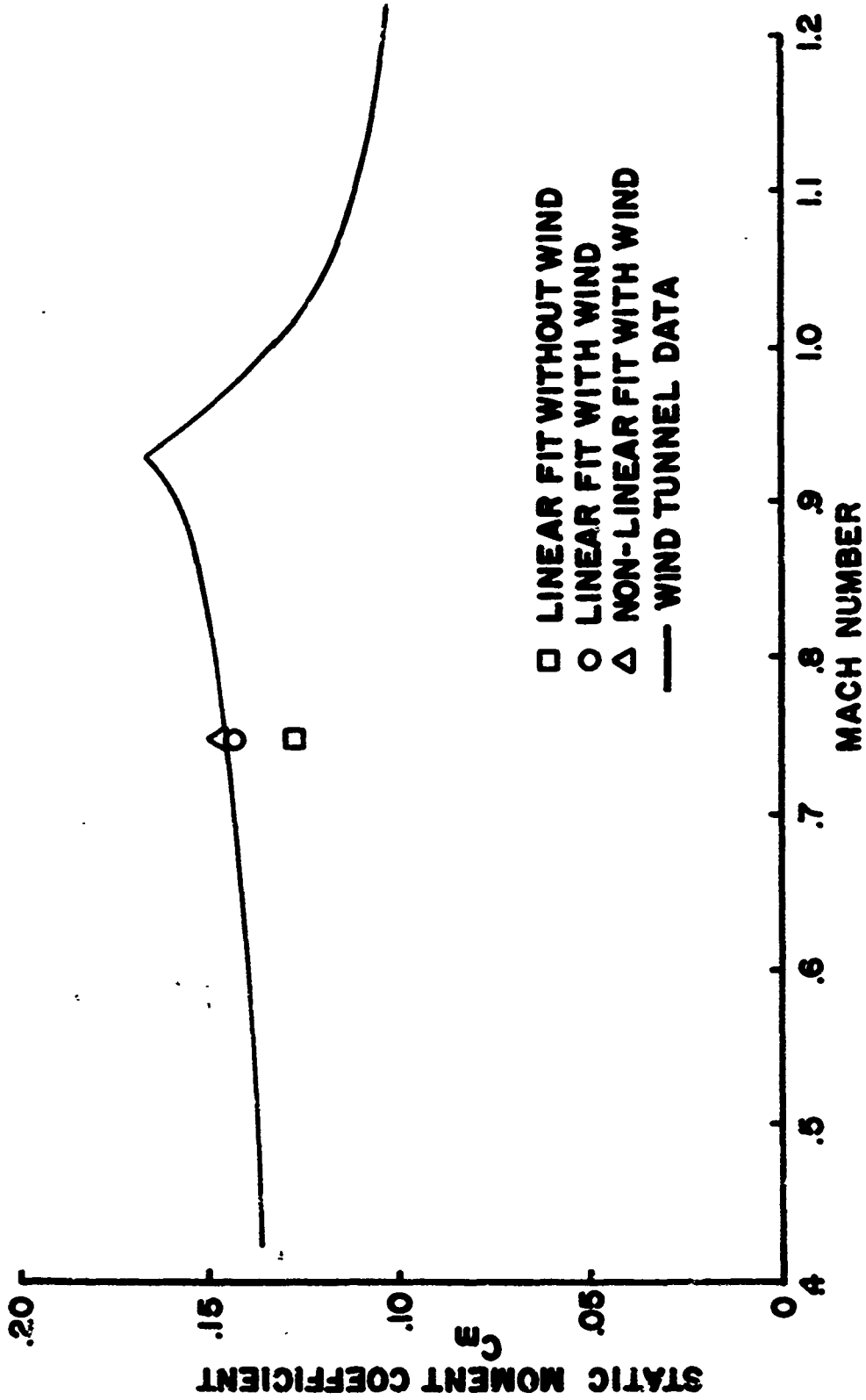


Figure 5. A Comparison between C_m Obtained from Yawsonde Data and Wind Tunnel Tests

REFERENCES

1. W. H. Mermagen, "Measurements of the Dynamical Behavior of Projectiles Over Long Flight Paths," *Journal of Spacecraft and Rockets*, Vol. 8, No. 4, April 1971, pp 380-385.
2. C. H. Murphy, "Free Flight Motion of Symmetric Missiles," Ballistic Research Laboratories Report No. 1216, July 1963, AD 442757.
3. R. S. Eikenberry, "Analysis of the Angular Motion of Missiles," Sandia Report SCCR 706051, February 1970.
4. W. R. Haseltine, "Yawing Motion of 5.0" Mk 41 Projectile Studied by Means of Yaw Sondes," Naval Weapons Center Report NWCTP 4779, August 1969.
5. G. T. Chapman and D. B. Kirk, "A Method for Extracting Aerodynamic Coefficients from Free-Flight Data," *AIAA Journal*, Vol. 8, No. 4, April 1970.
6. R. H. Whyte and A. Jeung, "Aerodynamic Reduction of Free Flight Transonic Range Data Utilizing Numerical Integration," General Electric Report 71APB514, April 1971.
7. B. Barnett, "Trajectory Equations for a Six Degree of Freedom Missile Using a Fixed Plane Coordinate System," Picatinny Arsenal Report TR3391, June 1966.