ANTISUBMARINE ATTACK: COMPUTER PROGRAM 13-64P S. A. Denenberg, et al

AD-757 029

Center for Naval Analyses Arlington, Virginia

28 August 1964



### ANTISUBMARINE ATTACK: COMPUTER PROGRAM 13-64P

By S.A. Demenberg and A. Hershaft

Research Contribution No. 60

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# Research Contribution

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**CENTER FOR NAVAL ANALYSES** 

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### ABSTRACT

An IBM 7090 computer program is described which calculates the distribution of distances between the point of activation of a weapon and a moving target submarine taking into account the estimated component attack errors. The model used is more flexible and realistic than similar past efforts and is expected to produce more reliable submarine kill probabilities. The miss distances are computed by Monte Carlo simulation of the actual tracking and firing tactics. They are plotted by an SC 4020 plotter, first in ascending order, then as a cumulative frequency distribution. Flow charts, a listing of the FORTRAN program, and a sample calculation are included.

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### I. INTRODUCTION

The determination of the probability of killing an evading submarine has long been a major problem of antisubmarine warfare. Past attack models have been usually restricted to specific tactical situations or sensor/weapon systems and required rather awkward assumptions about the nature of distribution of the various attack component errors.

The effects of antisubmarine weapons as a function of distance are comparatively well known. Therefore, the major difficulty in the determination of kill probabilities lies in the calculation of the probability of placing a weapon within a given distance from the target, in terms of the expected errors in the various stages of attack.

This program provides a distribution of these distances by Monte Carlo simulation of the actual antisubmarine tracking and firing tactics. It is based on a model (reference (a)) which is both flexible enough to cover most tactical situations and sensor/weapon systems and realistic enough to yield reliable kill probability values. The use of the Monte Carlo technique voids the need for unreasonable distortion of component error distributions.

#### II. GENERAL DESCRIPTION

### Model

The tactical situation is shown in figure 1. The attack unit is at the origin of the coordinate system. The true course of the submarine is parallel to the x-axis. At the time  $t_1 = 0$ , the submarine is at the true point  $P_1$  with polar coordinates  $(r_1, \alpha)^*$ . The submarine proceeds from  $P_1$  at a speed  $U_1$  and arrives at the point  $P_2$  at time  $t_2$ . It then executes a turn of radius  $R_t$  thru  $\gamma$  degrees of are at a velocity  $U_2$ . When the turn thru  $\gamma$  is completed at time  $t_3$  at point  $P_3$ , the submarine continues on a tangential course at speed  $U_3$ , reaching point  $P_4$  at a depth Z at time  $t_4$ .

The time  $t_4$  is set equal to the actual activation<sup>\*\*</sup> time of the attack weapon, thus making  $P_4$  a variable position dependent on  $t_4$ . If  $t_4$  is less than  $t_2$ , \* All angles are measured from the vertical or the range line, positive direc-

tion to the right. Deflections are measured from the range line, positive to the right.

\*\* Activation here denotes the step in which the weapon begins to exert its effect on the target (e.g., beginning of search for a homing torpedo or detonation for a depth charge).



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 $P_4$  will be somewhere between  $P_1$  and  $P_2$ . If  $t_4$  is greater than  $t_2$  but less than  $t_3$ ,  $P_4$  will be somewhere on the circular arc between  $P_2$  and  $P_3$ . Finally, if  $t_4$  is greater than  $t_3$ ,  $P_4$  will be located somewhere along the tangent to the circular arc depending on the time elapsed between  $t_3$  and  $t_4$ .

Due to errors in tracking, the attack unit presumes the submarine to be at the point  $P_1^{\prime}$  with the polar coordinates  $(r_1^{\prime}, \alpha^{\prime})$  at time  $t_1^{\prime} = t_1 = 0^*$ . The attack unit loses contact with the submarine at  $P_1^{\prime}$  where it has measured the submarine's speed as  $U_1^{\prime}$  and its course as  $\delta^{\prime}$ . The attacker assumes that the submarine continues from  $P_1^{\prime}$  at the speed  $U_1^{\prime}$  on the course  $\delta^{\prime}$  and calculates  $P_2^{\prime}$ , where  $P_2^{\prime}$  is the assumed location of the submarine at  $t_3^{\prime}$ , the desired time of activation of the weapon.

The aimpoint of the weapon  $P_3^{*}$  is specified by an offset angle  $n^{*}$  and an offset distance h<sup>\*</sup> from the predicted point  $P_2^{*}$ . ' as to weapon placement errors, the weapon arrives at the point  $P_4^{*}$  at depth Z', and activates at time  $t_4^{*}$ . The time  $t_4$  is set equal to  $t_4^{*}$  so that the distance between  $P_4$  and  $P_4^{*}$ becomes the miss distance between the submarine and the weapon.

#### Program

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A miss distance  $d_i$  is calculated for each Monte Carlo iteration. At the end of the iteration process, two graphs are plotted:

Graph 1: The miss distances  $d_i$  are plotted in sequential ascending order. Graph 2: The cumulative frequency distribution of the miss distances is plotted as follows:  $D_M$  is an input to the program and is used to specify the largest value on the x-axis. If  $D_M = 0$  or is not specified, the largest  $d_i$  or  $d_{max}$  is found.

> $D_{M}$  is then chosen as the smallest number of the form  $1 \times 10^{n}$ ,  $2 \times 10^{n}$ ,  $5 \times 10^{n}$ ,  $-2 \le n \le 38$ , which is greater than  $d_{max}$ . Once  $D_{M}$  has been chosen, the x-axis of Graph 2 is divided into  $N_{s}$ equal increments, where  $N_{s}$  is also an input to the program.

Primed variables are used to describe quantities in the observed system. Unprimed variables denote quantities in the true or actual system.

Each increment represents a range of miss distances. The frequency of occurrence for each range of miss distance is calculated and the cumulative frequencies are plotted.

The largest and smallest values of  $d_i$  and the number  $d_i > D_M$  are printed out. All values of  $d_i > D_M$  are ignored; they are not plotted on Graph 1 and they are not used in determining the cumulative frequency distribution of Graph 2.

### III. METHOD OF SOLUTION

The inputs for the program consist of the following parameters:

Address	Symbol	Description
1	ID	Identification number which can be assigned to a computer run and which will appear on the graphs and the printed output. ID is an integer such that $0 \le ID \le 32$ , 767
2	N	Number of Monte Carlo iterations.
3	D <sub>M</sub>	The value of miss distance that will be used as the largest value on the x-axis of Graph 2 (feet)*
4	N <sub>S</sub>	Number of equal increments on the x-axis of the cumulative frequency plot (one increment has length = $D_M/N_S^{**}$ )
5	NB	Number of "empty" passes thru random number generators.***
6	<b>r</b> <sub>1</sub>	Distance from attack unit to $P_1$ , the submarine's true position when the last contact is made (feet)
7	^r1	Observed position bias error in range (feet)
8	σr <sub>1</sub>	One standard deviation of position error in range (feet)

• If not entered,  $D_M$  is chosen as the smallest number of the form  $1 \ge 10^n$ ,  $2 \ge 10^n$ ,  $5 \ge 10^n - 2 \le n \le 38$  which is greater than the largest calculated miss distance.

\*\* If not entered, N<sub>S</sub> will be set equal to 500.

<sup>\*\*\*</sup> N<sub>E</sub> passes thru the random number generators are made only for the first data set processed by the program.

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Address	Symbol	Description
9	r <sub>t</sub>	Radius of turn that submarine executes at $P_2$ (yards)
10	α	True bearing from attack unit to submarine at point of last contact (degrees)
11	$\Delta \alpha$	Observed position bias error in bearing (degrees)
12	°α	One standard deviation of position error in bearing (degrees)
13	Ý	Number of degrees of arc in turn of radius rt.
14	σ <sub>γ</sub>	If positive, $\sigma_{.,}$ is one standard deviation of error in
		the turn angle $\forall$ (degrees). $\otimes$ will be replaced by a normal distribution about $\forall$ . If negative, $\forall$ will be replaced by a uniform distribution from 0 to $\forall$ . If zero, $\forall$ will not be changed.
15	∆ <b>8</b>	Observed course bias error, where true course $\delta = 90$ (degrees)
16	σð	One standard deviation of course error (degrees)
17	u <sub>1</sub>	True speed of the submarine from $P_1$ to $P_2$ (knots)
18	<sup>u</sup> 2	True speed of the submarine from $P_2$ to $P_3$ (knots)
19	<sup>u</sup> 3	True speed of the submarine from $P_3$ to $P_4$ (knots)
20	<sup>2</sup> u 1	Observed bias error of submarine speed u <sub>1</sub> (knots)
21	σ <sub>u1</sub>	One standard deviation of error in submarine speed u <sub>1</sub> (knots)
22	t <sub>2</sub>	True time at which submarine starts turn (seconds)
23	ີ t <sub>ກ</sub>	If positive, $\sigma_{t_2}$ is one standard deviation of error in
	-	the time $t_2$ (seconds). $t_2$ will be replaced by a normal distribution about $t_2$ . If negative, $t_2$ will be replaced by a uniform distribution from 0 to $t_2$ . If zero, $t_2$ will not be changed.
24	t'3	- Desired time of activation of the weapon (seconds)
25	n•	Aimpoint offset angle (degrees)

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Address	Symbol	Description
26	h'	Aimpoint offset distance (feet)
27	∆¢ <sub>r</sub> •	Weapon placement bias error in range (feet)
28	σ <sub>ε</sub> r'	One standard deviation of weapon placement error in range (feet)
29	∆e <sub>d</sub> ,	Weapon placement bias error in lateral displacement (feet)*
30	σ <sub>e</sub> d•	One standard deviation of weapon placement error in lateral displacement (feet)*
31	<sup>Δε</sup> β'	Weapon placement bias error in bearing (degrees)*
32	σ <sub>ε</sub> βι	One standard deviation of weapon placement error in bearing (degrees)*
33	Z	True depth of submarine when weapon is activated (feet)
34	۵ <b>z</b>	If $\sigma_{7}$ is positive, $\Delta \mathbf{Z}$ is considered to be the observed
		depth bias error (feet). If $\sigma_{Z}$ is negative, $\Delta Z$ is con-
		sidered to be the maximum operating depth of the evading submarine (feet).
35	σz	If positive, $\sigma_{Z}$ is one standard deviation of error in the
	-	depth Z (feet). The observed depth of the submarine, Z', will be calculated as a normal distribution about $Z + \Delta Z$ (feet). If negative, Z' will be calculated as a uniform distribution from 0 to $\Delta Z$ , the maximum operat- ing depth of the submarine (feet). If zero, Z' will be set equal to Z (feet).
36	<b>v</b> *	Velocity of the weapon (feet/seconds).

In the following discussion,  $R_N$  is a Gaussian-distributed (mean = 0, standard deviation = 1) random number which is always less than 4 standard deviations.  $R_U$  is a uniformly-distributed (mean = 0) random number.

If  $\Delta \varepsilon_{d}^{*} = \sigma_{\varepsilon_{d}^{*}} = 0$ , then Option 2 (see page 8) will be used.

If  $\Delta \epsilon_{\beta^*} = \sigma_{\epsilon_{\beta^*}} = 0$ , then Option 1 (see page 8) will be used.

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The miss distance d will be computed once the x-y coordinates of  $P_4$  and  $P_4^{\prime}$  are determined.

1. It is first necessary to calculate the x and y coordinates of  $P_3^{o}$ . In order to do this, certain variables in the observed system must be computed.

Since  $r_t$ ,  $\Delta u_1$ ,  $\nabla u_1$ ,  $u_1$ ,  $u_2$ , and  $u_3$  will be used in subsequent calculations, they must be scaled to be consistent with the units of the rest of the input parameters.

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$$U_i = 1.6878065u_i, i = 1, 2,$$
  
 $\Delta U_1 = 1.6878065\Delta u_1$   
 $\sigma_{U_1} = 1.6878065\sigma_{u_1}$   
 $R_* = 3r_e$ 

 $\mathbf{U}_{1}^{\bullet} = \mathbf{U}_{1} + \mathbf{U}_{1} + \mathbf{R}_{N_{1}} \mathbf{C}_{U_{1}}$ 

Then

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$$\alpha^{\circ} = \alpha + \Delta \alpha + R_{N_2} \sigma_{\alpha}$$
  

$$r^{\circ}_1 = r_1 + \Delta r_1 + R_{N_3} \sigma_{r_1}$$
  

$$\delta^{\circ} = 90 + \Delta \delta + R_{N_4} \sigma_{\delta} \quad (\delta = 90^{\circ} \text{ in the true system})$$

It is now possible to calculate the x and y coordinates of  $P'_3$ ,  $x'_3$  and  $y'_3$ , from the geometry of figure 1.

$$x_{3}^{*} = r_{1}^{*} \sin \alpha^{*} + U_{1}^{*} t_{3}^{*} \sin \delta^{*} + h^{*} \sin \eta^{*}$$
$$y_{3}^{*} = r_{1}^{*} \cos \alpha^{*} + U_{1}^{*} t_{3}^{*} \cos \delta^{*} + h^{*} \cos \eta^{*}$$

2. The next step is the determination of  $x_4^*$  and  $y_4^*$ , the x and y coordinates of  $P_4^*$ . This calculation depends on how the weapon placement error is described:

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Option 1: The weapon placement error is described by range and deflection ( $e_r$ , and  $e_d$ , respectively)

Option 2: The weapon placement error is described by range and bearing  $(\varepsilon_r, and \varepsilon_{\beta}, respectively)$ 

Option 1

$$\epsilon_{\mathbf{r}} = \Delta \epsilon_{\mathbf{r}} + R_{N_{5}} \sigma_{\epsilon_{\mathbf{r}}}$$

$$\epsilon_{\mathbf{d}} = \Delta \epsilon_{\mathbf{d}} + R_{N_{6}} \sigma_{\epsilon_{\mathbf{d}}} \qquad (\epsilon_{\mathbf{d}}, \text{ is measured positive to the right along the range line from the attack unit to the submarine)}$$

$$\mathbf{r}_{3}^{*} = \sqrt{(\mathbf{x}_{3}^{*})^{2} + (\mathbf{y}_{3}^{*})^{2}}$$

$$\mathbf{x}_{4}^{*} = \mathbf{x}_{3}^{*} + \epsilon_{\mathbf{r}}, \frac{\mathbf{x}_{3}^{*}}{\mathbf{r}_{3}^{*}} + \epsilon_{\mathbf{d}}, \frac{\mathbf{y}_{3}^{*}}{\mathbf{r}_{3}^{*}} \qquad *$$

$$\mathbf{y}_{4}^{*} = \mathbf{y}_{3}^{*} + \epsilon_{\mathbf{r}}, \frac{\mathbf{y}_{3}^{*}}{\mathbf{r}_{3}^{*}} - \epsilon_{\mathbf{d}}, \frac{\mathbf{x}_{3}^{*}}{\mathbf{r}_{3}^{*}} \qquad *$$

$$\mathbf{r}_{4}^{*} = \sqrt{(\mathbf{x}_{4}^{*})^{2} + (\mathbf{y}_{4}^{*})^{2}}$$

**Option 2** 

$$\varepsilon_{\mathbf{r}^{*}} = \Delta \varepsilon_{\mathbf{r}^{*}} + R_{N_{5}} \sigma_{\varepsilon_{\mathbf{r}^{*}}}$$

$$\varepsilon_{\beta^{*}} = \Delta \varepsilon_{\beta^{*}} + R_{N_{6}} \sigma_{\varepsilon_{\beta^{*}}}$$

$$r_{3}^{*} = \sqrt{(x_{3}^{*})^{2} + (y_{3}^{*})^{2}}$$

$$r_{4}^{*} = r_{3}^{*} + \varepsilon_{\mathbf{r}^{*}}$$

$$\beta^{*} = \arctan \frac{x_{3}^{*}}{y_{3}^{*}}$$

$$x_{4}^{*} = r_{4}^{*} \sin (\beta^{*} + \varepsilon_{\beta^{*}})$$

$$y_{4}^{*} = r_{4}^{*} \cos (\beta^{*} + \varepsilon_{\beta^{*}})$$

<sup>\*</sup> The derivation of these equations is somewhat lengthy and is therefore not included.

The time of activation of the weapon is calculated taking into account the delay due to weapon placement error.

$$t'_4 = t'_3 + \frac{r'_4 - r'_3}{v'}$$

3. The x and y coordinates of  $P_4$ ,  $x_4$  and  $y_4$ , must now be determined:

Since  $t_2$  and  $\vee$  will be used in subsequent calculations, they must first be transformed in accordance with the convention defined on page 5.

If 
$$\sigma_{t_2} > 0$$
, then  $T_2 = t_2 + R_{N_7} \sigma_{t_2}$   
If  $\sigma_{t_2} < 0$ , then  $T_2 = R_{U_1} t_2$   
If  $\sigma_{t_2} = 0$ , then  $T_2 = t_2$   
If  $\sigma_{\gamma} > 0$ , then  $\Gamma = \gamma + R_{N_8} \sigma_{\gamma}$   
If  $\sigma_{\gamma} < 0$ , then  $\Gamma = R_{U_2} \gamma$   
If  $\sigma_{\gamma} = 0$ , then  $\Gamma = \gamma$ 

Since  $T_2$  and  $\Gamma$  have now been determined,  $t_3$  is given by:

$$t_3 = T_2 + \frac{\pi}{180} \Gamma \frac{R_t}{U_2}$$

As was noted previously, the location of  $P_4$  is dependent upon  $t_4^{i}$ ; thus, there exist three possibilities:

a) 
$$t_4^* \leq T_2$$
  
then  $x_4 = r_1 \sin \alpha + U_1 t_4^*$   
 $y_4 = r_1 \cos \alpha$ 

b) 
$$T_2 \leq t_4 \leq t_3$$
  
then let  $\theta = \left(\frac{t_4 - T_2}{t_3 - T_2}\right) \Gamma$   
 $x_4 = r_1 \sin \alpha + U_1 T_2 + R_t \sin \theta$   
 $y_4 = r_1 \cos \alpha - R_t (1 - \cos \theta)$ 

c)  $t'_4 > t_3$ 

then let  $S = U_3 (t'_4 - t_3)$ 

$$x_4 = r_1 \sin \alpha + U_1 T_2 + R_t \sin \gamma + S \cos \gamma$$
  
$$y_4 = r_1 \cos \alpha - R_t (1 - \cos \gamma) - S \sin \gamma$$

4. The final step is the calculation of the miss distance:

If  $\sigma_Z > 0$ , then  $Z' = Z + \Delta Z + R_{N_9} \sigma_Z^*$ If  $\sigma_Z < 0$ , then  $Z' = R_{U_3} \Delta Z$ If  $\sigma_Z = 0$ , then Z' = ZThen  $d = \sqrt{(x_4 - x'_4)^2 + (y_4 - y'_4)^2 + (Z - Z')^2}$ 

• See page 6 to review the definition of  $\sigma_Z$ .

### IV. USER'S INSTRUCTIONS

See the list of input parameters on page 4. The user should submit a data submittal form (see appendix C). These forms have space for the submitter's name, the date, the program number (13-64P), the security classification if any, the parameter addresses and values, and an estimate of the computer running time (see section VIII).

Input flexibility has been attained by allowing the user to vary any or all of the parameters in a computer run. In any one set of data the parameters remain fixed, of course, but there is no programmed limit to the number of data sets a user may submit in a run. The only restriction is that each data set must terminate with one blank card, and the last set in the run must terminate with two blank cards.

A further advantage enjoyed by the user is that for each data set after the first, he need submit only those parameter values in a set that are different from those in the previous set.\* This is accomplished by identifying each parameter by a .nique "address" in the computer memory (see appendix E). Initially every address is cleared to zero so that only non zero input parameters need be entered.

### V. SAMPLE PROBLEM

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A situation was fabricated for illustrative purposes whereby most of the bias errors were chosen as one percent of the true value and standard deviations were taken as ten percent of the true value. The output is shown in appendix D; and the problem submittal form in appendix C.

### VI. KEYPUNCH INSTRUCTIONS

See the list of input parameters on page 4 and the sample problem submittal form in appendix C. Input card formats are described in appendix E.

### VII. OPERATOR'S INSTRUCTIONS

Run under control of the Bell System on the IBM 7090 computer. Graphs are made by the Stromberg-Carlson microfilm recorder. A charactron (CRT) tape must be mounted on tape unit A8 in the low-density mode. When the program is run at the David Taylor Model Basin all that is necessary for plotting is a "BCRT" control, card (columns 8 thru 12) and the "AMPLOS" subroutine. When the program is run at CEIR, NAVIC or NAVCOSSACT, the "BCRT" control card is not to be used and the "AMPLOS" subroutine is to be replaced by the "CXPLOT" and "AMPLOF" subroutines; the CRT tape on A8 can then be taken to DTMB or Stromberg-Carlson for processing.

• The exception to this rule is N<sub>E</sub>, the number of empty passes through the random number generator (see page 4).

# VIII. TIMING

The table presented below gives a conservative estimate of the computer running time for one data set as a function of  $N_{I}$ , the number of Monte Carlo iterations.

N <sub>I</sub> (Number of Monte-Carlo Iterations)	Computer Running Time (in minutes)
100	2
1000	2
2000	3
3000	3
4000	4
5000	5
6000	5
7000	6
8000	6
9000	6

Reference:

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(a) Operations Evaluation Group, "Design of Antisubmarine Attack Models," in preparation.

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= arctan (x<sup>1</sup>/y<sup>1</sup>) - r<sup>1</sup>/<sub>4</sub> xm (c<sup>2</sup> · r<sub>2</sub>) = r<sup>1</sup>/<sub>4</sub> cus(-<sup>2</sup> · r<sub>2</sub>)

\*\***\*** 

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 $\Gamma = R_{U_2} \vee$ 

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 $T_2 = R_{U_1} t_2$ 

GENERATE RUI

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 $T_2 = t_2 + R_{N_7} q_2$ 

GENERATE R<sub>N7</sub>

**°** 

r<sub>2</sub> = t<sub>2</sub>

TEST ,'

\* E. J = W

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A-2

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A-3





APPENDIX B

## FORTRAN STATEMENTS

CO	NPUTER PROGRAM 13-64P ANTI-SUBNARINE ATTACK AH/SAD	
	DIMENSION X1(9000),DD(9000),X2(1000),YY(1000),40(36),G1	(12).62(15)
	EQUIVALENCE (QO(3).DSUBM).(QO(6).RSUB1).(QQ(7).DELR1).(	QQ(8).51681
	X), (QQ(9), RTARN), (QQ(10), ALPHA), (QQ(11), DELALP), (QQ(12),	SIGALP).
	X(QQ(13).GAMMA).(QQ(14).SIGGAM).(QQ(15).DELDEL).(QQ(16).	SIGDEL).
	X(00(17)-U1KNOT)-(00(18)-U2KNOT)-(00(19)-U3KNOT)-(00(20)	ADELUATA
	¥100/211.51604.100/221.51602.100/231.516721.00/24.51	
		166001
		• 5102521•
	X(QQ(33),ZEE),(QQ(34),DELZ),(QQ(35),SIGZ),(QQ(36),VPR(ME	. )
	DO 10 I=1+36	
	10 GO(I)=0.	
	KEE=0	
	NSUBS=500	
	CALL LGCHAR(8,4H SAD)	
	P1=3.14159	
8	G1(12)=740610306060	
8	G1(11)=275121473060	
	G1(10)#016060606060°	
	G1(9) = 603126601360	
	G1 (7)=6060606060	
	C1/E/= 316363916893	
	01(J)-J10E0JE143EJ C1/A)-38434A21A84A	
	VI ( 4 / 4 2 3 6 2 6 V 3 1 4 3 6 V	
	GI(2)=JI4D2/0040D1	
8	G1(1)=242551606060	
	G2(15)=741006306060	
	G2(14)=G1(11)	
8	G2(13)=026060606060	
	G2(12)=G1(9)	
	G2(10)=G1(7)	
8	G2(9)=236444644321	
8	G2(8)=633165256026	
	G2(7)=512550642545	
8	G2(6)=237060243162	
8	G2(5)=635131226463	
Ä	62(4)=314645604626	
Ā	G2(3)=604431626260	
	62/21=243162632166	
ž	C2(1)=239562606060	
	20 CALL DATA(00. IND)	
	18/1ND\60.60.30	
	VETVETVETVETVETVETVETVETVETVETVETVETVETV	
	ALL LCCLARIE AN CADE	
	LALL LULTAKIGIGT 340/	
	CALL ENDJUB	
	SO IDENT#QQ(1)	
	N2/R1=dd(5)	
	NSUB5=QQ(4)	
	IF(KEE) 52.51.52	
	51 NEMPTY=QQ(5)	
	52 PRINT 60	
	60 FORMAT (1H1, 41H CNA PROGRAM 13-64P ANTI-SUBNARINE ATT	ACK ///
	X8H ADDRESS. 5X, 5HVALUE, 11X, 11HDESCRIPTION/)	
	GENPTY=NENPTY	
	PRINT 70.(I,QQ(I),I=1.4),GENPTY,(I.QQ(I),I=6.10)	
	70 FORMAT(15,F15,4,5X,21HIDENTIFICATION NUMBER/	
	XI5, F15.4.5X, 29HNO. OF MONTE-CARLO ITERATIONS/	

B-1

X15+F15+4+5X+35HLARGEST VALUE FOR X-AXIS ON GRAPH 2/ X15+F15+4+5X+37HNUMBER OF EQUAL INCREMENTS ON GRAPH 2/ 5.F15.4.5X.33MNUMBER OF EMPTY RANDOM NO. PASSES/ X5H X15+F15+4+5X+7HR SUB 1/ X15.F15.4.5X.13HDELTA R SUB 1/ X15+F15+4+5X+13H51GMA R SUB 1/ X15.F15.4.5X.7HR SUB 1/ X15+F15+4+5X+5HALPHAZ) PRINT 80,(1,QQ(1),I=11,20) 80 FORMAT(15+F15+4+5X+11HDELTA ALPHA/ X15.F15.4.5X.15HSIGNA SUB ALPHAZ X15++15+4+5X+5HGAMMA/ XIS.F15.4.5X.15HSIGMA SUE GAMMA/ XIS+F15+4+5X+11HDELTA DELTA/ XIS. F15. 4.5X. 15HSIGMA SUB DELTA/ X15+F15+4+5X+7HU SUB 1/ X15.F15.4.5X.7HU SUE 2/ X15+F15+4+54+7HU SUB 3/ XIS.F15.4.5X.13HDELTA U SUB 1/) PRINT 90.(1.GQ(1),1=21.30) 90 FORMAT(15,F15.4.5X,17HS1GMA SUB U SUP 1/ X15.F15.4.5X.7HT SUB 2/ X15.F15.4.5X.17HSIGMA SUB T SUB 2/ XIS+FIS+4+5X+13HT PRIME SUB 3/ XIS.F15.4.5X.9HETA PRIMEZ X15+F15.4.5X.7HH PRIME/ X15.F15.4.5X.25HDELTA EPSILON SUB & PRIMEZ X15+F15+4+54+24HSIGMA SUB EPSILON SUB & PRIMEZ X15.F15.4.5X.25HDELTA EPSILON SUN D PRIMEZ X15+F15+4+5X+29HSIGNA SUB EPSILON SUN D PRIME/) PRINT 100.(1.00(1).1=31.36) 100 FORMAT(15.F15.4.5X.28HDELTA EPSILON SUB BETA PRIME/ X15.F15.4.5X.32HSIGMA SUB EPSILON SUD BETA PRIMEZ X15+F15+4+5X+1H2/ X15+F15+4+5X+7HDELTA 2/ X15+F15+4+5X+11H51GNA SUH 2/ X15+F15+4+5X , 7HV PRIME////) IF (NEMPTY) 130.140.110 110 DO 120 I=1. NEMPTY CALL RANUMH (DUMMY) 120 CALL GRNUMA (DUMMY) 130 NEMPTY=0 140 UIFPS=1.6878065#U1KNOT U2FP5=1.68/8065#U2KNOT U3FPS=1.6878065+U3KNOT DELU1=1.6878065#DELUA SIGU1=1.6878065#51GUA RTURN#3. #RTARN DO 330 1+1.NSUEI CALL GRNUMA (RN1) CALL GRNUNA (RN2) CALL GRNUM4 (RN3) CALL GRNUMA (RNA) U1P=U1FPS+DELU1+RNI#SIGU1 ALPHAP= ALPHA+DLL ALP+RN2+SIGALP R1P=RSUE1+DELR1+RN3\*SIGR1 DELP=90.+DELDEL+RN4+SIGDEL X3P=R1P=SINDF(ALPHAP)+U1P=T3P=SINDF(DELP)+AITCHP=SINDF(ETAP)

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Y3P=R1P#COSDF(ALPHAP)+U1P#T3P#COSDF(DELP)+AITCHP#COSDF(ETAP) CALL GRNUMA (RNS) CALL GRNUMA (RN6) ERP=DELERP+RN5+51GERP R3P=SORTF(X3P++2+Y3P++2) IF (DELEBP) 170.150.170 150 IF (SIGEBP) 170.160.170 CALCULATIONS FOR OPTION 1 160 EDP=DELEDP+RN6=SIGEDP X4P=X3P+ERP#X3P/R3P+EDP#Y3P/R3P Y4P=Y3P+ERP\*Y3P/R3P-EDP\*X3P/R3P R4P=SORTF(X4P++2+Y4P++2) 60 TO 180 CALCULATIONS FOR OPTION 2 170 EBP=DELEBP+RN6#SIGE8P R4P=R3P+ERP ANGLE=ATANDF(Y3P/X3P) 1F (X3P) 172.174.174 172 ANGLE=ANGLE+180. 174 BETAP=90.-ANGLE X4P=R4P#SINDF(BETAP+EBP) YAP=RAP#COSDF(BETAP+ERP) 180 T4P=T3P+(R4P-H3P)/VPRIME TT2+TIME2 IF (SIGT2) 190.210.200 190 CALL RANUMB (RUI) TT2=RU1+TIME2 GO TO 210 200 CALL GRNUN4 (RN7) TT2=TIME2+RN7+SIGT2 210 GGANMA=GANMA IF (SIGGAM) 220.240.230 220 CALL RANUMB (HU2) GGAPMA=RU2+GAMMA GO TO 240 230 CALL GRNUM4 (RNB) GGAMMA=GANMA+RNH#SIGGAM 240 IF (T4P-TT2) 250,250,260 250 XFOUR=RSUBI #SINOF(ALPHA)+U1FPS#T4P YFOUR=RSUB1 +COSDF(ALPHA) GO TO 290 260 TIMEJ=TT2+(PI/180.)+GGAMMA+RTURN/U2FPS 1F(T4P+TIME3) 270,270,280 270 THETA=((T4P-TT2)/(TIME3-TT2))+GGAMMA XFOUR=RSUB1#SINDF(ALPHA)+U1FPS#TT2+RTURN#SINDF(THETA) YFOUR=RSUB1 +COSDF (ALPHA)-RTURN+(1.-COSDF (THETA)) GO TO 290 280 ESS=U3PPS+(T4P-TIME3) XFOUR=RSUB1 451NDF (ALPHA) +UIFPS+TT2+RTURN+SINDF (GGAMMA)+ESS+COSDF X(GGAMMA) YFOUR=RSUR1 +COSDF(ALPHA)-RTURN+(1.-COSDF(GGANNA))-E55+SINDF X(GGANNA) 290 ZPRIME=ZEE 1F (SIGZ) 300.320.310 300 CALL RANUNB (RU3) ZPRINE=RU3+DELZ 60 TO 320 310 CALL GRNUNA (RN9)

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CALL FORAST(DD.NSUBI.1)
    DMAX=CO(NSUBI)
    SCALE=DSUBM
    IF (DSUBM) 340.340.380
340 DO 370 K=1.41
    SCALE=.001+10.++K
    IF (DMAX-SCALE) 380,380,350
350 SCALE=2. +SCALE
    IF (DMAX-SCALE) 380, 380, 360
360 SCALE=2.5*SCALE .
    IF (DMAX-SCALE) 380,380,370
370 CONTINUE
380 JJJ=0
    GGG=NSUBS
    DELX=SCALE/GGG
    D0 390 1=1.NSUBS
390 YY(1)=0.
    DO 420 I=1, NSUBI
    INDEX=DD(1)/DELX+0.99999999
    IF (INDEX-NSURS) 410,410,400
400 JJJ=JJJ+1
    GO TO 420
410 YY(INDEX)=YY(INDEX)+1.
420 CONTINUE
    GNORM=NSUB1-JJJ
    X2(1)=DELX/2.
    DO 430 J=2. NSUBS
    X2(J)=X2(J-1)+DELX
    {J-L}YY+(L)YY={L}YY
430 YY(J-1)=100.+YY(J-1)/GNORM
    YY (NSUBS)=100. +YY (NSUBS)/GNORM
    GI(8)=BINDF(IDENT.6)
    G2(11)=G1(8)
    XUPPER=X1(NSUBI)
    INURM=GNORM
    CALL FNPLOT(GI(12),12H(8H NUMBER),29H(23H MISS DISTANCE IN FEET
   X).1..XUPPER.0..SCALE.20.20.20.1.6H(F5.0).6H(F6.0))
    CALL CURVE(X1(INORM), DD(INORM), INORM, 6H
    CALL FNPLOT(G2(15),28H(23H MISS DISTANCE IN FEET),13H(9H PERCENT
   X).0.,SCALE.0.,100.,20,2,20,1,6H(F6.0),6H(F4.0))
    CALL CURVE(X2(NSUBS), YY(NSUBS), NSUBS, 6H
                                                  )
    PRINT 440.0MAX.DD(1).JJJ.SCALE
440 FORNAT(29H THE MAXIMUM MISS DISTANCE = F9.2.5H FEET/29H THE MINIMU
   XM MISS DISTANCE = F9.2.5H FEET//12H THERE WERE 14.30H MISS DISTAN
   XCES GREATER THAN F9.2.5H FRETT
    KEE=1
    GO TO 20
    END
```

320 DD([]=SQRTF((XFOUP-X4P)++2+(YFOUP-Y4P)++2+(ZEE-ZPRIME)++2)

ZPRIME=ZEE+DFLZ+RN9#SIG2

330 X1(I)=1

B-4

## APPENDIX C SAMPLE PROBLEM SUBMITTAL FORM

### OEG COMPUTER DATA SUBMITTAL FORM

Date: 1 August 1964 Submitted by: J. Doe

Program No. 13-64P Bet. Time 3 min. Classification Unel

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Special Instructions: -

Address	Value	Address	Value	Address	Value	Address	Value
	1500	21	3				
2	2000	22	100				
3	0	23	10				
4	100	24	300				
5	5	25	NS				
6	5010	26	50				
1	50	27	10				
8	500	28	50				
9	100	29	6				
10	20	30	0				
11	.2	31	9				
12	2 .	32	2				
13	60	33	50				
14	6	34	.5				
15	.9	35	5				
16	9	36	800				
17	31		b				
18	20		b				
19	30	1				1	
20	.3	1				1	

#### NOTES:

A value of zero must be entered as 0, not left blank.
 Decimal pts. may be omitted if understood to follow the rightmost digit.

The value 3 X 10<sup>-5</sup> may be entered as .00003 or 3-5, not as 3 X 10<sup>-5</sup>.
 The factor portion of a value may not contain more than 8 digits.
 The exponent portion of a value must lie within the range 539.
 Exponents may be omitted if zero. If not, they must be signed.

7. Mank cards should be indicated by:





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### APPENDIX D

SAMPLE PROBLEM OUTPUT

CNA PROGRAM 13-64P ANTI-SUBMARINE ATTACK

ADDRESS	VALUE	DESCRIPTION *
1	1500.0000	IDENTIFICATION NUMBER
2	2000.0000	NO. OF MONTE-CARLO ITERATIONS
3	0.	LARGEST VALUE FOR X-AXIS ON GRAPH 2
4	100.0000	NUMBER OF EQUAL INCREMENTS ON GRAPH 2
5	5.0000	NUMBER OF EMPTY RANDOM NO. PASSES
6	5000.0000	R SUB 1
7	50.0000	DELTA R SUB 1
8	500.0000	SIGMA R SUB 1
9	100.0000	R SUB T
10	20.0000	ALPHA
11	0.2000	DELTA ALPHA
12	2.0000	SIGMA SUB ALPHA
13	60.0000	GAMMA
14	6.0000	SIGMA SUB GAMMA
15	0.9000	DELTA DELTA
16	9.0000	SIGMA SUB DELTA
17	30.0000	U SUB 1
18	20.0000	U SUB 2
19	30.0000	U SUB 3
20	0.3000	DELTA U SUB 1
21	3.0000	SIGMA SUB U SUB 1
22	100.0000	, T SUB 2
23	10.0000	SIGMA SUB T SUB 2
24	300.0000	T PRIME SUB 3
25	45.0000	ETA PHIME
26	50.0000	H PRIME
27	10.0000	DELTA EPSILON SUB R PRIME
28	50.0000	SIGMA SUB EPSILON SUB R PRIME
29	0.	DELTA EPSILON SUB D PRIME
30	0.	SIGMA SUB EPSILON SUB D PRIME
31	3.0000	DELTA EPSILON SUB BETA PRIME
32	2.0000	SIGMA SUB EPSILON SUB BETA PRIME
33	50.0000	Ζ
34	0.5000	DELTA Z
35	5.0000	SIGMA SUB Z
36	800.0000	V PRIME

THE MAXIMUM MISS DISTANCE = 17728.80 FEET THE MINIMUM MISS DISTANCE = 1012.03 FEET

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THERE WERE 0 MISS DISTANCES GREATER THAN 20000.00 FEET

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D-3 (REVERSE BLANK)

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### APPENDIX E

### DATA SUBROUTINE

### 1. Introduction:

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Many computer programs require the flexibility of varying any or all of theparameters in a computer run. Although FORTRAN is fairly flexible in its arithmetic and control statements, its input-output statements are quite rigid. In order to read cards for instance, considerable effort must be expended by the FORTRAN programmer in writing his input statements. This subroutine eliminates some of that tedium. The concept of a "data set" is used. A data set consists of a sequence of punched cards terminated by one blank card. A parameter deck for a computer run may consist of several data sets. Such a parameter deck is terminated by two blank cards.

### 2. Parameter Addresses:

The primary advantage of this subroutine over FORTRAN input statements results from the use of "parameter addresses." An address is a relative location in the computer memory. It is the subscript of an array or **matrix**. For example, in an array called X, the parameter value  $X_{53}$  would be located at address 53. By

using the parameter addresses, a user of the program need submit only those parameter values in a data set that are different from those in the previous set.

Three types of addresses are permitted by this subroutine.

- (1) A numeric address consisting of one to five characters, each of which is a digit 0 - 9. Such an address (n) refers to the n<sup>th</sup> element in a specified array.
- (2) An alpha address consisting of one to six characters, the first of which must be alphabetic (A-Z). The remaining may be alphabetic or numeric (A-Z or 0-9). Such an address refers to the  $n^{th}$  element in a specified array (1 ≤ n ≤ 26), where the first character of the address corresponds to n as the 26 letters of the alphabet correspond to the integers 1-26.
- (3) A matrix address consisting of two or more numeric fields separated by commas. For example, the address 53, 47 refers to the element in the 53rd row and the 47<sup>th</sup> column of a two-dimensional matrix. There is no limit to the number of dimensions in a matrix address.

### 3. Input Card Format:

A standard submittal form (see attachment) has been designed for the analyst. This form provides for entering parameter values with their associated addresses. The user indicates blank cards to separate data sets. The keypunch operator has the option of punching one address and value per card, or, if the addresses are sequential, of punching one address and several values on a card.



Only columns 1-72 of a card are used. Each column must contain one of the following: a digit (0.9), a "+" or "-" sign or a dash, a letter (A-Z), a period, a comma, or a blank. Each punched card must contain one parameter address. The address may start in column 1, or, if desired, may start in a later column, provided all columns before it are blank. The address is terminated by at least one blank column. Only one address is permitted on the card. Succeeding columns contain one or more parameter values, each separated by one or more blank columns. A value may be signed or unsigned. The length of the value field is variable. No blanks are permitted within a value field. A value may be punched with or without an exponent. An exponent is recognized by the presence of a plus or minus sign (or dash) between the fractional part and exponent part of the value. Decimal points (periods) may be punched in either the fractional or exponent parts of a value. If more than one value is punched on a card, those after the first will be entered at sequential addresses relative to the address of the first value.

### 4. Usage:

A data set is read by the use of the statement:

### CALL DATA (X, I)

in a FORTRAN program for the IBM 7090. The argument X is the name of an array in the program. The argument I is an indicator set by the subroutine. This indicator may be tested by the main program upon return from the sub-routine. It will have a value of 0 or 1 or 2.

- 0: The subroutine has read a data set. The main program will normally proceed to operate on this data.
- 1: The subroutine has read the second blank card which terminates the parameter deck. The main program will normally terminate at this point.
- 2: The subroutine has read a "bad" data card. The main program may terminate the run, or ignore the card and return to the subroutine to read the rest of the data set.

If the cards to be read contain matrix addresses, additional arguments must be included in the FORTRAN calling statement:

CALL DATA (X,  $D_1$ ,  $D_2$ ,  $D_3$ , ...,  $D_n$ , I)

where  $D_i$  is the i<sup>th</sup> dimension of the matrix X.

### 5. Method:

See the attached flow chart. DATA reads parameter values and loading addresses from cards. If sense switch 5 is up, it will read the values and addresses from tape (unit A2). It converts the values to floating point numbers, and stores them as elements of an array specified in the calling statement. The elements are specified by the addresses. If a card (or tape record) is read which contains non-permitted characters (see input card format above), DATA prints the statement "bad data card," followed by an image of the card itself.

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### 6. Coding Information:

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See the symbolic listing included in this appendix. DATA is written in the 7090 FAP language. It must be used in conjunction with the BELL system. It requires 401 words storage space.





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**E-6** 

# SYMBOLIC LISTING

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	FAP	
	ENTRY DATA	
DATA	SXA X1+1	
	SXA X2+2	
	SXA X4.4	
	CAL 1.4	
	ADD CORE	
	STO XLOC	
	AXT 1+1	
	SXA #+1+1	
	CAL ##,4	
	ANA MASK	
	SXA EXITAL	
	181 #+1+1+-1	
	67A A1	
	51A A1	
	67A 773	
	AYT 3.3	
A1	SVD 44.1	RETURN INDICATOR = 1
Â	TEY MADEAD.A	
	ATE CADA	READ A CARD
	TDA EVIT	
	TRA EALI	
	STY ADDRE	
	STZ VALUE	AUDRESS = 0
	STZ FYD	VALUE = 0
	STZ POINT	EAP # 0
	AXT 1.1	
	SXA FIFLD.1	FIELD # 1
	AXT 14.1	
A2	TNX HH-1-1	COLUMN OF TO
-	AXT 42.2	COLUMN GI 72
	SXA COLUMNA2	
8	LXA COLUMN .2	
	TNX 42.2.4	COLONN & COLONNAI
	SXA COLIMAN .2	
	LDQ CARD+12.1	
	RQL 3612	
	PXD 0.0	
	LGL 6	
	STO CHARAC	
	ORA FLOAT	
	FAD FLOAT	
	STO NUMB	
	AXT 4214	
	CLA CHARAC	
	CAS TABLE+42.4	
	TRA ++2	
	TRA #+3	
	TTV A-9-4 4	

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LXA FIELD.2 TRA F1+1+2 TRA F7 TRA F6 TRA F5 TRA F4 TRA F3 TRA F2 F1 TXH 8+4+41 STZ \*\* F1A AXT 2.2 SXA FIELD,2 TXH H+4+31 TXH 1+4+28 TXL BAD+4+2 AXT 3+2 SXA FIELD.2 TXI #+1+4+-2 SXA ADDRES+4 TRA B F2 TXH J+4+41 TXH H:4:31 TXH K+4+28 TXH BAD,4,2 TXH L+4+1 AXT 4+2 SXA FIELD,2 AXT 2+2 SXA DIMENS+2 CLA ADDRES TZE BAD THI BAD STZ ADDER F2A TRA B F3 TXH J+4+41 TXH 8,4,31 TXH K+4+28 TXH 8+4+2 TXH L+4+1 TRA BAD F4 TXH M.4.41 TXH N:4:31 TXH P,4,28 TXH BAD+4+2 TXH Q+4+1 TRA T F5 TXH 8,4.41 AXT 612 SXA FIELD.2 TXH U.4.31 TXH W+4+28 TXH BAD,4,2 TXH G.4.1

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TRA BAD

FIELD=7 (EXPONENT FIELD) FIELD=6 (VALUE FIELD) FIELD=5 (BLANKS AFTER ADDRESS) FIELD=4 (ARRAY ADDRESS) FIELD=3 (ALPHA ADDRESS) FIELD=2 (NUMERIC ADDRESS) FIELD=1 (BLANKS BEFORE ADDRESS) **RETURN INDICATOR = 0** FIELD = 2 · NUMERIC CHARACTER SIGN OR DASH ALPHA CHARACTER. FIELD = 3 ADDRESS = NTH ALPHA BLANK CHARACTER NUMERIC CHARACTER SIGN OR DASH PERIOD COMMA, FIELD = 4 DIMENSION = 2 TEST ADDRESS ADDER=0 BLANK CHARACTER NUMERIC CHARACTER SIGN OR DASH ALPHA CHARACTER PERIOD BLANK CHARACTER NUMERIC CHARACTER SIGN OR DASH PERIOD COMMA BLANK CHARACTER FIELD = 6NUMERIC CHARACTER SIGN OR DASH PERIOD

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TRA BAD TXH X+4+41 F6 BLANK CHARACTER TXH U+4+31 NUMERIC CHARACTER TXH Y+4+28 SIGN OR DASH TXH BAD+4+2 TXH G+4+1 TRA BAD PERIOD F7 TXH 2,4,41 BLANK CHARACTER TXH 88+4+31 NUMERIC CHARACTER SIGN OR DASH TXH EE.4.28 TXH BAD.4.2 TXL BAD+4+1 G AXT 1+2 PERICD, POINT = 1 SXA POINT +2 TRA B H LDQ ADDRES ADDRESS = 10 X ADDRESS + N MPY H10 XCA ACL CHARAC STO ADDRES TRA B I TXH 8.4.30 + SIGN CLA ADDRES SET SIGN OF ADDRESS SSM STO ADDRES TRA B AXT 5.2 J FIELD = 5 SXA FIELD.2 TRA B TXH L1+4+30 ĸ + SIGN CLA VALUE SET SIGN OF VALUE SSM STO VALUE TRA L1 AXT 1.2 SXA POINT.2 L POINT = 1 AXT 6,2 SXA FIELD,2 LI FIELD = 6 TRA B AXT 5+2 M FIELD = 5 SXA FIELD,2 TRA S LDQ ADDER N ADDER = 10 X ADDER + N X PROD MPY HIO STQ ADDER TSX T1+4 HPY CHARAC XCA ADD ADDER STO ADDER TRA B P TXH R.4.30 + SIGN CLA VALUE SET SIGN OF VALUE



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STO VALUE TRA R POINT = 1 AXT 1+2 SXA POINT+2 FIELD = 6 AXT 6.2 SXA FIELD.2 CHECK DIMENSION LXA EXIT+2 TXI #+1+2+-3 PXA 0.2 SUB DIMENS TNZ BAD T5X T1+4 ADDER=ADDER-PROD CLA ADDER SUB PROD STO ADDER CHECK ADDER TZE BAD THI BAD ADD ADDRES STO ADDRES CLA DIMENS ADD H1 STO DIMENS TRA F2A PROD = PRODUCT OF DIMENSIONS **T1** SXA T4+4 CLA H1 STO PROD STA T3 LXA DIMENS+2 TXI #+1+2+-1 LXA X4+4 CAL T3 ADD H1 12 STA T3 CLA ##+4 STA #+1 **T3** LDQ ## ROL 18 MPY PROD STQ PROD TIX 12+2+1 AXT ##+4 T4 TRA 1+4 CLA POINT TEST POINT TNZ V VALUE = 10 X VALUE + N LDQ VALUE FMP DEC10 SSP FAD NUMB LDQ VALUE LLS O STO VALUE TRA B VALUE = VALUE + N/(10\*\*POINT) LXA POINT+4 CLA NUMB

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FDP DEC10

CLA VALUE SSM STO VALUE TRA B

CLA XLOC SUB ADDRES STA ++2 CLA VALUE STO ++ TRA AA

AXT 7.2 SXA FIELD.2

TXH 66.4.30

CLA EXP

SSM STO EXP

TRA GG

CLA XLOC

SUB ADDRES STA Z1 CLA DEC10 LDQ EXP

CALL EXP(3

XCA FMP VALUE STO ##

STZ VALUE

CLA POINT

FMP DEC10 SSP FAD NUMB LDQ EXP LLS 0

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LDQ EXP

STO EXP

XÇA

LXA POINT,4 CLA NUMB FDP DEC10

TIX +-2,4,1 LDQ EXP LLS 0

TIX #-2.4,1 LDQ VALUE LLS O FAD VALUE STO VALUE TRA DD TXH B.4.30

XCA

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+ SIGN SET SIGN OF VA	LUE
X(ADDRESS) = V	ALUE

FIELD = 2 + SIGN SET SIGN OF EXP

.

X(ADDRESS) = VALUE X 10++EXP

VALUE = 0 TEST POINT

EXP = 10 X EXP + N

EXP = EXP + N/(10++POINT)

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	FAD EXP	
	STO EXP	
DD	CLA POINT	POINT = POINT + 1
	ADD H1	
	STO POINT	
	TRA B	
EE	CLA XLOC	X(ADDRESS) = VALUE X 1000EVD
	SUB ADDRES	THEOL A TOWNERP
	STA EE1	
	CLA DEC10	
	LDG EXP	
	CALL EXP(3	
	XCA	
	FMP VALUE	۰.
EE1	STO ##	
	PXD 0,0	VALUE = 0
	TXH #+2+4+30	+ SIGN
	SSM	SET SIGN OF VALUE
	STO VALUE	
FF	STZ EXP	EXP = 0
	AXT 5+2	FIELD # 5
	SXA FIELD.2	
	CAL ADDRES	ADDRESS = ADDRESS + 1
	ADD H1	
	SLW ADDRES	
GG	STZ POINT	POINT = 0
	TRA 8	
HH	LXA FIELD,1	
	TXL JJ+1+1	FIELD#1. EXIT
	TXL BAD+1+4	
	TXL A+1+5	FIELD=5, READ ANOTHER CARD
	TXH 11+1+6	•
	CLA XLOC	FIELD=6, X(ADDRESS) = VALUE
	SUB ADDRES	
	STA #+2	
	CLA VALUE	
	STO ##	
	TRA A	
11	TXH BAD,1,7	
	CLA XLOC	FIELD=7.
	SUB ADDRES	X(ADDRESS) = VALUE X 10++EXP
	STA III	
	CLA DEC10	
	LDQ EXP	
	CALL EXP(3	
	XCA	
	FMP VALUE	
111	STO ++	
	TRA A	
BAD	TSX HPRINT,4	
	PZE PRINT,0,15	
	AXT 2+1	
112	SXD ++,1	
(1	AXT ##+1	

E-12

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X2 X4 EXIT AXT ##+2 AXT +++4 TRA +++4 MASK OCT 77777700000 PRINT BCD 3 BAD DATA CARD... CARD BSS 12 ADDRES HTR ## VALUE HTR \*\* EXP HTR \*\* POINT HTR \*\* FIELD HTR \*\* COLUMN HTR \*\* TABLE OCT 60 BLANK 0CT 0CT 0CT 0CT 01234567 01234567 0CT 0CT 0CT 0CT 
 OCT
 10

 OCT
 11

 OCT
 20

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E-13

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CHARAC	HIK	**
DIMENS	HTR	**
ADDER	HTR	**
H10	HTR	10
DEC10	DEC	10.0
HI	HTR	1
PROD	HTR	**
AMASK	OCT	77777
FIOAT	OCT	28800000000
	LITD	**
NUMB	піп	
XLOC	HTR	**
CORE	OCT	100001
1.1	SYN	XI
		***
	END	

E-14

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#### OEG COMPUTER DATA SUBMITTAL FORM

Submitt	ed by:		Date:					
Program	n No		Est. Time		Classification			
Special	Instructions	:						
Address	Value	Address	Value	Address	Value	Address	Value	
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		╢──┼	یو براین را ۱۹۰۰ و دک <sup>ور</sup> می					
				+	• <b>•</b> •			
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	·····	++		╉──┼				

#### NOTES:

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A value of zero must be entered as 0, not left blank.
 Decimal pts. may be omitted if understood to follow the rightmost digit.

3. The value 3 X 10<sup>-5</sup> may be entered as .00003 or 3-5, not as 3 X 10<sup>-5</sup>. 4. The factor portion of a value may not contain more than 8 digits. 5. The exponent portion of a value must lie within the range  $\pm 39$ . 6. Exponents may be omitted if zero. If not, they must be signed.

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7. Blank cards should be indicated by: ----h

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E-15 (REVERSE BLANK)