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HDL-TR-1610

RADIO-WAVE PROPAGATION MEASUREMENTS OVER SEA WATER

by

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August 1972



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Security Classification				kai: Minik
DOCUME (Security classification of title, body of abstract a	NT CONTROL DATA		he overall report is classifi	od)
1. ORIGINATING ACTIVITY (Corporate author) Harry Diamond Laboratories			security classification	ION
Washington, D.C. 20438		25. GROUP	IICTASSITTED	
3. REPORT TITLE	<u> </u>		<u></u>	
RADIO-WAVE PROPAGATION MEA	SUREMENTS OVE	R SEA WATE	R	
4. DESCRIPTIVE NOTES (Type of report and inclusive date	s)			
5. AUTHOR(S) (First name, middle initiel, last name)				
M.M. Algor				
6. REPORT DATE	1	O. OF PAGES	Th. NO. OF REFS	
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& PROJECT NO.		HDL-TR-161	.0	
e. AMCMS Code: 5910.22.63353	95. OTHER R	EPORT NO(S) (Any	other numbers that may be	638
HDL Proj: 11612	this repor	9		
11. SUPPLEMENTARY NOTES	12. SPONSOR	ING MILITARY AC	TIVITY	
	U.S	. Army Mat	eriel Command	
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ABSTRACT

Propagation loss was measured at three frequencies (30, 140, and 412 MHz) over various sea-water paths out to 40 nautical miles between a moderately elevated shore-based receiving site and a floating transmitter platform essentially at the water's surface and subject to wave motion.

The measured losses agreed well with theory, assuming a "standard atmosphere" for the test conditions. Certain anomalies and ocean-wave effects were noted. In general, meteorological conditions were relatively constant and "normal" for eastern Florida in summer.

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1. INTRODUCTION

This experiment was conducted in order to determine the frequency region most conducive to transhorizon communications over a sea-water path of about 20 to 50 nautical miles (naut mi), considering various practical factors. Unlike many investigations reported earlier, a special requirement of this study was that one terminal be floating essentially at the water surface, and that the other terminal have a limited elevation ranging between 50 and 100 ft.

Simple theory (see section 8, "BIBLIOGRAPHY") shows that the effective radio horizon for a 100-ft elevation is about 12 naut mi, whereas that for the surface terminal is much less, and may even vary in accordance with its location on the peak or trough of a wave. The literature includes little concerning propagation at low elevations in this "near-shadow" region between "line-of-sight" mobile applications and "deep-shadow" communications over hundreds of miles wherein high-power tropo-scatter fixed stations are commonly used. Accordingly, additional objectives were to (1) determine reasonable system parameters, (2) examine signal levels and fading characteristics at several frequencies and distances, and (3) identify the effects, if any, caused by ducting, surface-wave action, and other meteorological conditions within the available time limits of the field test.

2. SITE SELECTION

The arrangement considered most expedient for the experiment was that of using an existing shore-based radar facility as a receiving site in combination with a small, floating transmitter terminal. This transmitter would be serviced and moved to various distances by an attending vessel. Such a facility was located at Boca Raton, Florida, where a Navy-owned site overlooking the beach is operated by the Georgia Institute of Technology as an experimental radar test station. This site included such advantages as a tower structure on which receiving antennas could be mounted, a working radar system with which true ranges could be determined, electrical power, and other normal incidental facilities. Also, an available "work boat" was assured--a 45-ft commercial salvage vessel which had been chartered from time to time by the Georgia Institute of Technology to assist in radar studies. A contract was therefore arranged for Georgia Tech to supply facilities, the chartered work boat, incidental services, and radar

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and meteorological data. Their engineering personnel arranged for installation on the tower of the several (government-furnished) antennas necessary for the propagation study.

Although some space for instrumentation was available in existing buildings at the test site, this space was not considered suitable for equipment survival because of high humidity and temperature in a salt-spray environment (only 100 to 200 ft from the surf). Use of an available airconditioned 28-ft semi-trailer was considered desirable as a mobile laboratory, in which receiving and recording equipment, as well as associated test and calibration instruments, could be installed. The trailer, which was also used for packing and transporting delicate equipment to the test site, was moved to location by a commercial trucking firm. The controlled environment made possible by this arrangement was later considered almost a necessity for this locality.

3. FREQUENCY SELECTION

The frequency range of potential interest in this study is loosely bounded on the low end by increased power losses in the small (3 to 4 ft maximum height) antenna permitted on the floating terminal. At 30 MHz, for example, which was the arbitrarily assumed limit, an estimated one-half of the transmitter power was dissipated in the antenna loading coil. Below this frequency, additional system problems are also more likely to occur from long-distance sky-wave interference. The highest practical frequency is determined by the stateof-the-art in generating useful power from a small, reliable source, and by increasing propagation losses per mile (assuming no unusual ducting effects). This limit was again arbitrarily set at 1500 MHz. Four essentially clear-channel transmitting frequencies were assigned in this range for the experiment: 30.25, 140.25, 412.00, and 1220.00 MHz. An additional frequency at 36.20 MHz was permitted for a two-way communications link to assist in conducting the test.

It was originally intended to record transmissions at all four frequencies simultaneously in order to correlate fading. Technical problems in constructing the transmitter and receiving converter for 1220 MHz, however, made the use of this frequency impossible within existing time and budget limitations. Later operating difficulties made it possible to record only two of the remaining frequencies at any one time, although this inconvenience did not cause the loss of much practical data.

4. TRANSMITTING SYSTEM

Several crystal-controlled transmitters were constructed in individual water-tight boxes mounted on a common ground plane of light aluminum. The use of separately mounted vertical whip antennas made rechecking of power outputs and antenna impedances convenient. The whole assembly was secured to a 9-ft surf board for flotation, as shown in figures 1 and 2.

Originally the floating platform was self-powered by a regulated storage battery supply in a watertight case suspended by a "U" bracket underneath the assembly. The bracket also insured a good sea-water ground for the an-Unfortunately, this added about 120 lb (in air) to tennas. the platform weight and required the use of a sling and powered hoist for manipulating it over the side of the boat. Experience on a calm day showed this arrangement to be virtually uncontrollable and physically dangerous with even slight boat motion; it would be absolutely impossible in an appreciable sea. Field modifications therefore were made to relocate the battery supply aboard the attending boat, thus lightening the float to about 40 lb. The lesser weight and size made it possible to lift the platform manually over the side with acceptable safety, even in fairly heavy seas. The resulting transmitting system is shown in figure 3. Voltage drop was reduced in the connecting battery cable by using the insulated outer metal braid of RG58/U coaxial cable for each of a pair of conductors 250 ft long, attached at intervals to the tether rope. This presented something of a problem in unreeling and recovery, but a procedure was worked out. By limiting to two the number of transmitters in use at one time, the drop was kept to about 2 volts at 2 amperes average drain. Although the 250-ft tether distance was much less than that originally planned, this separation seemed adequate to minimize antenna/boat interaction, provided the boat was not directly in line with the transmission path. In records made while the platform was being transported to the boat's side to switch transmitters, no significant effect was noticed beyond 10 or 20 ft in this orientation. The extra voltage drop produced a terminal voltage at the transmitters close to their lower design limits, where output power began to change rapidly with voltage. Fortunately, the total test period during a day was small compared with the battery's useful life per charge of about 3 hr; a spare was available if needed. Thus, it was possible to measure rf power outputs under known voltage conditions with reasonable assurance that the readings would remain the same throughout a series of tests.



Figure 1. Transmitter float assembly



Figure 2. Transmitter float in use.

As indicated in figure 3, the battery supply included a low-differential regulator, overload protection, and a lowfrequency keyer which served to identify the transmitted signals and provide a periodic zero-reference for the recorder. Although it was not usually needed, a duplicate power system was available as a backup.

The antennas were vertically-polarized stubs over a ground plane that floated barely above the water surface, and was sometimes under it. At the lowest frequency, 30 MHz, it was necessary to insure a more definite grounding to the sea water, as the metal plate was by itself too small to permit proper antenna loading after the battery bracket was removed. Changes in transmitter current were detected as waves washed over the platform, indicating a variable load. This was largely eliminated by galvanized mesh wrapped around the platform and under the surf board. The 30-MHz antenna was kept below 3-ft total height by the use of a tapered helical loading coil in its base. Although a good match could be obtained, this loading coil became quite warm after prolonged operation. Considering the area and temperature rise, it was estimated that about one-half the generated power was being lost as heat. The other antennas presented no problem, except that at 412-MHz elevated ground-plane radials were needed to prevent excitation of the coaxial feed, and thus provide a consistent match.

Sealing against sea water seepage was somewhat difficult. On "fixed" joints, Dow Corning 3145 RTV adhesive sealant was very satisfactory, if properly applied. "Removable" connectors for coaxial line and dc power were made successfully leakproof by being sprayed first with silicone compound in a volatile solvent, and then liberally "buttered" with Dow Corning type 103 silicone compound. One major problem occurred during the first day of testing at sea, when an unnoticed pin-hole leak in the 412-MHz transmitter caused that unit to be disabled. Corrosion was so great that complete rebuilding was necessary. Therefore, tests during the first two weeks used only the 30- and 140-MHz fre-A much slower leak, after about 3 weeks, caused auencies. erratic functioning of the 140-MHz transmitter. In this case, field repairs made it possible to complete the series of tests, but at an 8.2-dB reduction in rf power output.

Listed below are the rf power outputs actually obtained with the three transmitters:



(MHz)	<u>(W)</u>
30.25	- 15 (≈8 W radiated)
140.25	- 15 (2.25 W after repairs)
412.00	- 6 (after rebuilding)

Schematics of the three units and of their power supply are included in appendix A.

5. RECEIVING SYSTEM

The receiving site (at Boca Raton, Florida) is shown in figure 4. The antennas on top of the tower are for Sand X-band radar systems with which range was measured. About half-way up the tower are the three antennas installed for the propagation experiment. Their mid-points are 54 ft above mean sea level. In the center of the tower is a 10-ft dish used for 412-MHz (and also intended for 1220 MHz), flanked by the 3-element 30-MHz beam and the 140-MHz log-periodic array. The three antennas were mounted on a common support which could be adjusted in azimuth approximately ± 30° by a remote control box in the instrumentation trailer. Without such adjustment, it would have been very difficult to maintain the transmitter float centered in the receiving beams, since the off-shore terminal was subject to Gulf Stream drift up to 3 or 4 knots. Figures 5 through 8 are additional views of the antenna systems. Listed below are the gains of the three antennas, in dB above isotropic, at each of the four originally assigned frequencies, as well as their effective cross sections in square meters.

Frequency (MHz)	Gain (dB)	Area (m²)	Antenna <u>Type</u>
30.25	8.0	49.2	3-element Yaqi
140.25	10.5	4.04	log-periodic ^a
412.00	19.0	3.37)	single wide-band feed on 10 ft dish ^b
1220.00	30.0	4.81)	

^aScientific-Atlanta Model20-2 (120 to 150 MHz).

^bScientific-Atlanta Model 22-10 Reflector, with Model 27-0.4/10 Feed (0.4 to 1.7 MHz).



Figure 4. Receiving site, Boca Raton, Florida

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Figure 5. Antennas for 30 and 412 MHz.



Figure 6. Antenna boom assembly.



Figure 7. Mounting of down-converters and filters.



Figure 8. 140-MHz log-periodic antenna.

Low-noise, crystal-controlled down-converters for both 140 and 412 MHz were constructed in weather-tight boxes and mounted on the support beam for the antennas as shown in figure 7. By mounting them thus, high-frequency losses in the 100-ft cables to the instrument van were avoided, and overall noise figure improved. To minimize inadvertent mixing with rather high-level radar backscatter, coaxial lowpass filters were inserted at the input of each converter, together with directional couplers for calibration purposes. Schematic diagrams of the two converters are included in appendix A.

The receiving system block diagrams, divided by frequency for simplicity, are shown in figures 9, 10, and 11. Outputs from the two converters and the direct output of the 30-MHz antenna were connected by cables approximately 100 ft long to three separate Hammarlund SP-600 receivers. Various outputs from these receivers then went to a Brush Series 1707, Mark 200, 8-channel oscillograph. The only outputs useful for signal measurement purposes were those directly from the second detectors. Difficulties experienced in calibrating AGC curves, tracking one receiver with another, and observing small changes in signal strength, led to the use of the receivers as essentially constant-input detectors at such a low level that AGC was ineffective, so that operation was in a more-or-less linear mode. Auxiliary predetector outputs at 455kHz were useful in combination with the true_rms voltmeters in determining the level of received signal power to equal the equivalent input noise power - a fundamental measure of receiving sensitivity. Listed below is the approximate signal power to double the (455 kHz) output signal-plus-noise power for an estimated IF bandwidth of 3 kHz.

(MH2	z)	(dBm)
412		-126
140		-124
30		-100

The two higher frequencies were limited by converter input noise figure. At 30 MHz, on the other hand, sensitivity was limited by atmospheric noise and other interference. During test transmissions, signals were always well above these thresholds at any range used.

A stable signal generator and accurate frequency counter were used to spot exact frequencies for reception.







Figure 10. 140-MHz receiving system.



A reference power meter aided in setting levels for received signal strength calibration. Figures 10 and 11 show that a calibration cable was run up the tower for each converter. The total loss through it and the directional coupler to the converter input was adjusted to be exactly 20 dB, to facilitate determination of the injected signal from the setting of the generator in the trailer.

The trailer and interior instrumentation are shown in figures 12 through 15.

6. EXPERIMENT

Field operations extended over the period 28 August through 24 September 1970, with a subsequent week in October to dismantle and return the instrumentation van. Propagation data were taken on five occasions; but the first of these was deemed unreliable because of procedural difficulties in calibration. A sixth occasion was aborted before data could be obtained because of damage to the propellor of the support boat. The table below summarizes pertinent information on the respective occasions.

- <u>3 Sept</u> Range to 20 naut mi data questionable leak disabled 412-MHz transmitter - handling difficulty made evident need to redesign. - calm day.
- 8 Sept Range to 30 naut mi some data uncertain calm day - waves: 1 to 2 ft swells - range limited by boat speed and navigation uncertainties.
- <u>10 Sept</u> Range to 40 naut mi good data calm day range limited by boat speed and navigation uncertainties waves: 1 to 2 ft swells on light chop.
- <u>16 Sept</u> Range to 10 naut mi good data seas 10 to 16 ft limited safe range - 412 MHz transmitter again in operation.
- 21 Sept Aborted after 8 naut mi no test damaged propeller.
- 22 Sept Range to 15 naut mi good data 140 MHz transmitter with reduced output power operation in rain squall - range limited by weather, 8 to 10 ft seas and low boat speed. many scattered thunder storms.



Figure 12. Instrumentation trailer.



Figure 13. Receiver rack and 8-channel recorder.



Figure 14. Rear of receiver and recorder racks.



Figure 15. Calibration and communication equipment.

Between tests, much time was spent calibrating or modifying equipment and waiting for satisfactory weather.

Since the attending work boat was used for other charters and salvage operations when not actually needed by the experiment, all apparatus had to be installed and removed for each test occasion. This included the transmitter float assembly, battery supply and spare, cable reel, communications transceiver and antenna, radar corner reflector and mast, and tool chest. Although the boat was equipped with marine band and "citizens band" transceivers, the nature of the experiment made it desirable to utilize the specially assigned frequency of 36.20 MHz for communications regarding the test. Using this essentially clear channel and about a 10-watt output at each terminal, voice contact between the boat and the instrumentation trailer was of high quality out to the maximum range tried of 40 naut mi, even though only vertical whip antennas were used. Even the lower powered "citizen's band" equipment would have been adequate if other co-channel signals had been absent. These frequencies are close to the lowest one used in the test.

To enhance the radar return from the low and relatively small 45-ft work boat, a wire mesh corner reflector was installed on the highest mast (20 ft) which could be securely jury-rigged to the deck. Positive identification in case of multiple targets could be made by rotating the reflector to modulate the return distinctively. Even with enhancement, the maximum radar detection range was about 22 to 25 naut mi. Two methods were used to extend this. The first was the extrapolation of a plotted true course from previous radar data, on the basis of time at a measured ground speed and direction. This was considered useful for only moderate extensions of 5 to 10 miles because of variations possible in the Gulf Stream, which had varying velocities up to 3 or 4 knots and wandering direction. Intermediate stops for test purposes also caused errors because of continuing drift. A second method of obtaining check points extended positive range measurement beyond 30 miles. This was the use of large ocean-going freighters or high-flying aircraft as common objects identified both by radar and by visual sighting from the support boat. These fortuitous targets were radardetectable at at least 30 naut mi ranges. If they also happened to be within 5 miles or so of the support boat, a shrewd quess of range and bearing was sufficient additional data. By these two means, distances out to 40 naut mi were obtained with reasonable accuracy. Another method was prepared, but not used, in which a kite was designed to lift a corner reflector to heights of several hundred feet for better radar visibility. Available time and the limited speed of the support boat did not permit an attempt at greater ranges, however. Equipment for more conventional electronic position-finding was not available.

Certain limitations of the support vessel complicated the experiment. In calm water, approximately a 10-knot speed could be maintained. When heading into appreciable seas (the usual case with easterly winds), and correcting for Gulf Stream drift, the boat's speed was cut to about 2 to 4 knots ground speed; this is an impractical speed for covering much distance in interesting weather. In calm weather, the trip out to a 40-naut-mi range and return took 16 hr. On another day with swells between 8 and 16 ft, it required 11 hours to attain 10 naut mi and re-Although the lightened transmitter float (battery turn. removed) could be lifted manually over the boat's side at each test distance, the process was awkward and time The float could not be towed. A faster boat consuming. of different design would have been preferable, towing a stabilized streamlined test platform which would not have to be taken aboard. Even better would have been the use of a helicopter, which could lower the test platform at selected ranges. Although this would be more expensive per hour to operate, more data could be obtained over far greater ranges at a total cost saving. A boat would still be operational under more severe weather conditions, however.

At each range, during a test series, the transmitter float was drifted out beyond the immediate vicinity of the boat to the limit of its power cable (250 ft), with the boat maintaining just sufficient headway to keep it from being in line with the transmission path. Thus oriented, no effect of the boat's presence could be observed. As previously noted, only two transmitters were operated at a time to minimize voltage drop; however the common unit provided continuity for comparing the other two. Early tests were made with continuous recording periods of 10 to 15 minutes, but this was later reduced to one to three minutes (assuming no unusual effects), as the increased time gave no further information and it was desired to conserve both time and battery charge.

At the end of each recording period, an immediate measurement was made of the value and range of signal strength actually received at each frequency. To do this, a known level from the local signal generator was substituted for the signal at each receiver (fig. 9 to 11) to provide approximately the same average recording amplitude. The attenuator at the receiver's input was changed both plus and minus several one-dB steps to provide the detail needed to interpolate variations in the propagated signal. Done in this way, the receiver's characteristics did not affect the measurements.

It is of interest to note that the light-weight float rode large swells and shorter chop with a minimum of washover, when floating without any headway or tension on the tether rope. The effect of water washing over the ground plane and around the bases of the antennas could not be noticed in the received record compared with fluctuations believed caused by gross wave motion. Of course, occasional breaking chop and larger wind-blown water masses caused brief signal dropout by completely inundating the antenna support insulators (transmitters were protected from load shorts), but moisture remaining on the silicone-treated surfaces was not a problem. In fact, one period of successful operation was during a very heavy rain squall, in which severe drenching and splashing were present. The use of short antennas mounted only a few inches above the water surface is therefore not expected to be a great system problem, from this standpoint. The physical motions of the transmitter float and of wave conditions during a number of significant test periods were recorded on 16-mm motion picture film for later study. Although such data cannot be included with this report, it was of value in suggesting causes for certain propagation fluctuations, and in forming qualitative opinions regarding possible future test-float designs.

In the planning stage of the experiment, it was hoped that detailed meteorological data could be measured locally at each terminal of the transmission path for each test. This later proved to be too monumental an undertaking, complicated by the failure of certain sensors to perform as expected. Ιt was necessary, therefore, to rely on other publically available regional weather data compiled by Georgia Tech as part of their supporting services contract with HDL (DAAG39-70-0053). This is discussed in section 7. Qualitative weather conditions were also recorded by still camera at the offshore terminal. Three examples illustrate the range of conditions encountered (except for wind velocities and wave heights). The condition shown in figure 16 was most usually encountered, with sky mostly clear overhead and clouds over land surfaces and near the horizon. Figure 17 shows a typical overcast when general shower activity was forecast. A localized, very intense rain squall is shown in figure 18. Such squalls usually showed electrical activity which slightly affected the background noise in the lowest frequency receiver.



Figure 16. Typical good-weather conditions


Figure 17. Overcast, predicted shower activity



Figure 18. Typical local intense rain squall

7. RESULTS AND DISCUSSION

All three frequencies could be used for communications reliably to 20 nautical miles or more with low transmitter power. It is evident from the following data, however, that several penalties are incurred by the use of frequencies above 140 MHz. For quite different reasons, operation at 30 MHz and below is also not desirable. Considering all factors, a broad recommendation is made to use frequencies between 50 and 100 MHz, and preferably about 75 MHz. Other particulars will be presented.

Figures 19, 20, and 21 show for 30, 140, and 412 MHz, respectively, the received signal strengths at the antenna terminals in dB relative to one milliwatt (dBm), as a function of range in nautical miles to the transmitter platform. The solid curves are calculated values in accordance with Norton¹ on the basis of the real receiving antenna conditions, a "standard" atmospheric gradient (no inversion), and 10 watts radiated power over a smooth sea. The vertical lines represent the spread of observed signal strengths as a composite of all valid data for the range in question. Since the transmitter outputs differed somewhat from the value used in the calculations, the observed data has been normalized for 10 watts radiated power in each case. Also shown are the equivalent input noise levels of the receiving systems (as discussed in section 5) and the theoretical propagation for plane earth.

A better appreciation of the penalty of going to higher frequencies can be had by considering figure 22. The theoretical curves of the previous three figures are again used, but those for 140 and 412 MHz are further normalized for the same receiving aperture (49.2 square meters) as the 30 MHz receiving antenna. This means that the 140 MHz antenna should have 10.9 dB more gain, and the 412 antenna 11.75 dB more gain, than those actually used, in order to extract the same power as the 30 MHz antenna from a given field strength. The differences shown on figure 22, therefore, represent only the effects of propagation at the three frequencies. Although normalization could be made for any frequency and gain, the separation between curves would be unaffected. The theoretical curves shown were calculated for vertical $\lambda/4$ transmitting antennas at zero elevation. If one applies, instead, the restraint given in section 3,

¹Norton, K. A., Dec. 1941, The calculation of ground wave field intensity over a finitely conducting spherical earth, Proc. I.R.E., pp 623-639.







Figure 21. 412-MHz propagation.





namely, a 3- to 4-ft maximum antenna height, it is evident that certain improvements may be made in propagation at the higher frequencies. For example, a simple co-linear array can increase horizontal gain predictably, or a single radiating element can be elevated to the desired maximum height with resulting height-gain advantage, especially at the highest frequency. It is not certain, without further testing, that these theoretical advantages will all remain in the immediate presence of various surface wave conditions. In any case, the optimum frequency recommendation is unaffected.

Calculations¹ also showed some interesting facts regarding the height-gain properties of the receiving site, as tabulated below for a 50-ft elevation:

30	MHz	-1.2	dB
140	MH z	+2.8	dB
412	MHz	+18.5	dB

The height-gain advantage is range-dependent, but these figures apply for the longer ranges. At 30 MHz, a greater signal would have been received with the antenna at sea level. On the other hand, if the 412 MHz dish had been at about sea level, reception during actual test conditions would have been marginal beyond 10 naut mi. Presumably, at some frequency about median to 30 and 140 MHz, the effect of antenna height is inconsequential up to 50 ft or so.

Signal fading characteristics are an important subject for comment. Although it is a temptation to draw conclusions which cannot be strictly justified from the recorded data, the following general tendencies seem to exist:

(1) Higher frequencies have a greater fading range and a faster fluctuation in level.

(2) Fading range is not demonstrably a function of distance.

(3) Fading range may be somewhat greater with increased sea and wind states.

¹Norton, K. A., Dec. 1941, The calculation of ground wave field intensity over a finitely conducting spherical earth, Proc. I.R.E., pp 623-639.

(4) Fading at one frequency is essentially uncorrelated with fading at other frequencies, with certain uncommon exceptions.

(5) Fading may be separated into a slow component and a much faster component, more properly called "flutter." The two may have different causes.

(6) At 30 MHz, flutter may be correlated with the passage of long period (approximately 2 to 4 seconds) coherent wave fronts, or "swells." Although not determinable from present data, flutter at the higher frequencies may be the result of similar scatter from appropriately shorter period waves ("chop") local to the transmitter, thus explaining in part the observation of item 2 that such variations are not distance-dependent.

Other than the above, efforts to correlate propagation with varying meteorological conditions have not been possible. In general, atmospheric conditions during the entire series of tests were remarkably constant. Figures 19 through 21 show no significant behavior different from that of a standard atmosphere model; no evidence of ducting was observed at the frequencies and ranges employed. The meteorological data compiled by the Georgia Institute of Technology for this time period is given in appendix B, which is Attachment II of their final contract report. Some ducting tendencies may be seen in the plotted radiosonde data (fig. II-1 through II-3, and table II-1 of appendix B), but it is not evident for the days and times of valid data. Of possible interest is figure II-4 of appendix B, which relates required ducting conditions for various frequencies. Also included in appendix B are records of air and water temperatures, general weather log, and national weather maps for the test period.

An inspection of the spread of data points plotted in figures 19, 20, and 21 shows that signal level varies more at higher frequencies, but that for a given frequency, the variation is not obviously a function of distance. The nature of the flutter, and the manner in which it changes with frequency, can be observed in figures 23 and 24. The data were taken at 10 naut mi under conditions of 10 to 16ft seas and mixed chop. Figure 24 shows four instances, rarely observed, of signal drop-out due to waves washing over the 412 MHz antenna. The 30 MHz signal shows cyclic variations which strongly suggest dependence on the larger wave components in period, as observed in the motion-picture record of that test. Dependence of flutter at higher frequencies on wave action is less obvious, perhaps because of



Figure 23. Recording 16 Sept. 70, 10 naut mi, 412 and 140 MHz.



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the more random nature of the smaller waves. In these two figures, occasional correlation of flutter at all three frequencies may be noted, at periods (2 to 4 sec) corresponding to the larger ocean waves. In general, however, fading at any two frequencies is poorly correlated.

An analysis of auto and cross-correlation of data obtained on 22 September 1970, was made by Georgia Tech, and was submitted as Attachment III of their final contract report. This is also reproduced herein as appendix C.

In contrast to figures 23 and 24, figure 25 is data also at 10 naut mi, but on a relatively calm day, 10 September 1970. The 412 MHz transmitter was not operable at this time. Repetitive swells were about two ft in height, and of a period comparable to the 30-MHz variation. Although flutter at 30 MHz is reduced, it is interesting that 140-MHz flutter is increased and is now strongly periodic. It is suggested that this may be the result of a well-defined, low-amplitude chop, which is here more evident than in the generally more turbulent conditions of the previous figures. Other calm sea data, also on 10 September 1970, are shown in figures 26 and 27 for 25 and 40 naut mi, respectively. Throughout this distance, amplitude of long-period swells remained fairly constant.

An example of anomalous propagation occasionally found may be seen in figures 26, 27, and 28 on the 140 MHz channel. This is a beat-frequency-like flutter extending over several seconds and going through a seeming zero-beat. A possible cause is multi-path interference by reflection from aircraft, since a major air traffic route crossed the propagation path, and the effect was noted only at distances beyond line-of-sight. The presence of the effect simultaneously on 412 MHz in figure 28 seems to eliminate the possibility of a co-channel interfering signal as the cause. The phenomena was not observed at 30 MHz.

Another interesting propagation anomaly is illustrated in figure 29. At a propagation range of only 2 naut mi, a heavy rain squall, similar to that shown in figure 18, passed over the transmitting terminal and included the entire propagation path. The upper record shows flutter characteristics at 140 MHz while the entire path was clear. The lower record is of the same frequency about 15 minutes later when the entire path was through heavy rain. Not only was the average path loss increased by about 10 dB, but the nature of the flutter was changed and smoothed. These conditions tended to remain after the squall moved inland and the propagation path became clear. Conclusions



Figure 25. Recording 10 Sept 70, 10 naut mi, 30 and 140 MHz.



Figure 26. Recording 10 Sept 70, 25 naut mi, 30 and 140 MHz.



Figure 27. Recording 10 Sept 70, 40 naut mi, 30 and 140 MHz.



Figure 28. Recording 22 Sept 70, 15 naut mi, 140 and 412 MHz.



Figure 29. Recording 22 Sept 70, 2 naut mi, 140 MHz - effect of rain.

cannot be drawn from this one event; the squall changed many meteorological conditions locally. Perhaps pertinent to the reduced flutter, the heavy rain caused all but the longer-period waves to be dramatically reduced in amplitude, although the wind remained brisk. At this location, major wave amplitudes were judged to be 6 to 8 ft, and remained about the same during the rain. Unfortunately, before and after data at other frequencies were not obtained.

In order to allow computer analysis of fading data at the various frequencies, all transmissions on 22 September 1970, were made without keyed-off periods previously used for base-line determination, except for calibration purposes. This explains differences in appearance of figures 28 and 29. Zero-signal levels for each trace have been added subsequently.

In summary, tests under conditions of limited variability showed all frequencies to propagate in a generally predictable manner, assuming a standard atmospheric gradient over a 4/3 radius earth. Rapid fading, or flutter, appears to be related to wave conditions local to the float-mounted transmitting antenna. Consideration of factors such as required transmitter power, transmitting and receiving antenna size and gain, receiver equivalent noise level, and fading characteristics all lead to a choice of about 75 MHz as a preferred frequency for communication out to 20 to 50 naut mi.

A recommended system design can be tentatively worked out by interpolation from figure 22 and the following assumptions:

Range: 30 naut mi for reliable communication

Frequency: 75 MHz

Antennas: A float-mounted $\lambda/4$ vertical whip, and a 4-element Yagi at any elevation up to 50 ft or so.

Receiver: Equivalent input noise power - 120 dBm in a bandwidth of 8 kHz.

From figure 22, assume the theoretical received power at 75 MHz and a 49.2 m² antenna area to be -80 dBm. The 4element Yagi, with an estimated practical gain of 10 dB over isotropic, has an effective area of 12.7 m², which is about 6 dB less than the 49.2 m² antenna. Allowing 6 dB further reduction for "practical" differences between theoretical and measured propagation, results in a probable signal received of -92 dBm.

It is now possible to assume a radiated power of one watt (instead of the normalized 10-watt value), allow a fading range of 10 dB, and still have a received signal 8 dB above receiver noise. This design would probably be useful a large part of the time out to about 50 naut mi. With reasonable dynamic properties of the float, antenna wash-over would not be a problem except in unusually severe weather.

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APPENDIX A. SCHEMATICS OF TRANSMITTING AND RECEIVING EQUIPMENT.

This appendix contains for record purposes the following schematics of transmitting and receiving equipment constructed by Harry Diamond Laboratories for radio-wave propagation measurements over sea water.

> Figure A-1 - Transmitter power supply Figure A-2 - 30-MHz transmitter Figure A-3 - 140-MHz transmitter Figure A-4 - 412-MHz transmitter Figure A-5 - 140-MHz receiving converter Figure A-6 - 412-MHz receiving converter



Figure A-1. Transmitter power supply.



- $L_3 = 20$ turns #22 wire. Form Diam. = $\frac{3}{8}$ inch.
- L₄ = 6.0 turns #22 wire. Form Diam. = $\frac{3}{6}$ inch. L₅ = 6.0 turns #14 wire. Form Diam. = $\frac{3}{6}$ inch.

NOTE

All Feedthroughs 1000pf unless otherwise stated.

Form Diam. = $\frac{3}{6}$ inch. L₇ = 6.0 turns #14 wire. Form Diam. = $\frac{3}{6}$ inch. C₁, C₃, C₄, C₆ = ARCO 463 = 9.0 to 180pf. C₂ & C₅ = 2.2 to 34.0pf. C₇ = CONSTRUCTED From 2 Brass Plates and 2 Mica Sheets. Size of Mica Sheets = 2 Mils Thick, $2\frac{1}{2}$ inches long and $1\frac{1}{2}$ inches wide. Size of brass plates = 0.040 inch thick, $2\frac{3}{6}$ inches long and $1\frac{3}{6}$ inches wide.

Figure A-2. 30 MHz transmitter.



Q₁ = MMT-918 Q₂ = 2N3866 Q₃ = 2N3553 Q₄ = 2N5016 L₁ = 6.0 turns #22 wire. $\frac{1}{4}$ inch Diam. Form. L₂ = 4.0 turns #18 wire. $\frac{5}{16}$ inch Diam. Form. L₃ = 5.0 turns #18 wire. $\frac{5}{16}$ inch Diam. Form. L₄ = 6.0 turns #22 wire. $\frac{1}{4}$ inch Diam. Form. L₅ = 3.0 turns #18 wire. $\frac{5}{16}$ inch Diam. Form. C₁ = 7-45pf. C₂ = 1.8 - 12pf. C₃ & C₄ = Constructed from 2 Brass Plates and 2 Mica Sheets. Size of Mica Sheets = 2 Mils thick, $2^{1}/_{2}$ inches long, and $1^{1}/_{2}$ inches wide. Size of Brass Plates -0.040 inch thick, $2^{3}/_{8}$ inches long and $1^{3}/_{8}$ inches wide.

Figure A-3. 140 MHz transmitter.



Figure A-4. 412 MHz transmitter.



Circuit of the 2-meter converter. Resistors are '/-watt composition. Capacitors, unless otherwise noted, are disk ceramic.

CR6, CR7 - 1N914 or equivalent. L20, L21 - Same as L14, but CR₈ - 9.1-volt, 1-watt Zener

- diode (Motorola HEP-104 or equivalent).
- J₄ BNC or SO-239-type chassis connector.
- J₅ Phono connector.
- L₁₄ 4 turns No. 24 enamel to occupy 3/8 inch on J.W. Miller 4500-4 iron-slug Tap 1 turn from form. ground end.
- L_{15} , L_{16} , L_{19} 5 turns No. 24 enamel to occupy $\frac{3}{6}$ inch on same-type Miller form as L14.
- L₁₇, L₁₈ 15 turns No. 24 enamel wire, close-wound, on J. W. Miller 4500-2 ironslug form.

no tap.

- L_{22} 9 turns No. 30 enamel, close-wound, on J.W. Miller 4500-2 iron-slug form (J. W. Miller Co., 19070 Reyes Ave., Compton, Cal. 90221; write for catalog and prices).
- Q_7, Q_9, Q_{10} Junction FET, Motorola MPF102 (2N4416 suitable).
- Q8 Dual-gate MOSFET, Motorola MFE3008 (RCA 3N141 also suitable).
- RFC₄ $8.2-\mu$ H miniature rf choke (James Millen 34300-8.2).
- Y₂ 50.0 3rd-overtone crystal (International Crystal Co. type EX).

Figure A-5. 140 MHz receiving converter.



- C_1 , C_2 , $C_3 0.5$ to 3-pf. ceramic or glass trimmer (Centralab 829-3).
- C_4 , C_5 , $C_{12} 820$ -pf. disk ceramic (0.001- μ f. also suitable).
- C_7 , C_8 , C_9 , C_{10} , $C_{14} 0.001 \mu$ f. feedthrough capacitor (Erie 654-017102K. Centralab FT-1000 also suitable).
- C₆ 27-pf. dipped mica.
- C_{11} , C_{13} 5-pf. dipped mica.
- C₁₅, C₁₆ 1- to 10-pf. ceramic or glass trimmer (Centralab 829-10).
- CR1 U.h.f. mixer diode (Sylvania 1N82A).
- CR₂ Silicon signal diode (GE 1N4009).
- J_1 , J_2 Coaxial fitting. L_1 , L_2 , L_3 , L_8 No. 12 wire, $2\frac{1}{2}$ inches long. Tap L₁

- at 1 and $1\frac{1}{2}$ inches, L_2 at $\frac{1}{2}$ and 1 inch, L₃ at $^{3}/_{4}$ and $1^{1}/_{4}$ inches, L $_{8}$ at $\frac{1}{2}$ and $\frac{1}{4}$ inches.
- L₄ No. 26 enamel wound as per text on $\frac{3}{6}$ inch ironslug form (CTC 1534-2-2, slug coded red).
- L_5 , L_6 No. 26 enamel wound as per text on $\frac{3}{8}$ inch iron-slug form (CTC 1534-4-2, slug coded white).
- $L_7 4\frac{i}{2}$ turns No. 16 enamel, $\frac{3}{6}$ inch diam., $\frac{5}{6}$ inch long. Tap at 1 and 2 turns.
- Q_1, Q_2, Q_3, Q_4 See text.
- R_1 , R_2 5000-ohm miniature control. All other resistors $\frac{1}{2}$ watt or less, values as marked.
- R_3 , R_4 for text reference.
- Y₁ 5th-overtone crystal, 61.667 MHz (International Crystal Co.).

Figure A-6. 412 MHz receiving converter.

APPENDIX B. METEOROLOGICAL DATA AND PROPAGATION BIBLIOGRAPHY

(Attachment II of final report on contract DAAG39-70-0053, 17 Feb. 1971.)

The data assembled here are provided as partial documentation of the atmospheric propagation conditions during the series of experiments conducted at Boca Raton, Florida, in September 1970. The Bibliography is intended to provide a guide to some of the more applicable literature.

The data consist of twice-daily radiosonde readings obtained by the National Weather Service at Miami International Airport, daily weather summaries (both local and Weather Service, and graphs of refractivity data from the radiosonde flights. Detailed near-surface data are not currently available for the September period; however, efforts are still underway to obtain additional information.

Since the index of refraction of air is primarily a function of total pressure, temperature, and partial pressure of water vapor in the air, it is convenient to make use of an empirical relation for the index of refraction, n, in terms of these quantities in order to investigate the effects of refraction on radio propagation. A suitable empirical relation is (Reference 26)

n = 1 + (77.6
$$\frac{P}{T}$$
 + 3.73 × 10⁵ $\frac{e}{T^2}$) × 10⁻⁶, (1)

where P is the total pressure in millibars, e is the partial pressure of water vapor in millibars, and T is the absolute temperature in degrees Kelvin.

Although the second and third terms contribute only a few hundred parts per million to the refractive index, it is the variation of these terms with heights which brings about the "bending" of the radio waves. Thus, it is useful to define a quantity N, the refractivity, which is related to n by

$$N = (n-1) \times 10^{6} , \qquad (2)$$

or

$$N = 77.6 \frac{P}{T} + 3.73 \times 10^5 \frac{e}{T^2} .$$
 (3)

A number of variants to N have been used for various practical applications (Reference 26). One form of modified refractive index which has been widely used and is used here in Figure II-1 through II-3 is M, defined as

$$M = N_{h} + 0.048 h , \qquad (4)$$

where N_h is the value of refractivity at any height h in feet. When the M-gradient is zero, the ray curvature is zero in the flat-earth case. This is another way of saying that when the N-gradient is minus 48 units per 1000 feet, the ray has the same curvature as the earth.

Another variant which is often used is the B-modification, where B is defined as

 $B = N_{h} + 0.012 h , \qquad (5)$

where N_h and h are as defined above. This modification is used to illustrate departures from "standard" atmosphere, and this is a logical consequence of the four-thirds earth radius concept of the standard atmosphere definition.

The radiosonde data of Table II-1 were reduced to Nunits by the use of Equation 3 and tables from the Handbook of Chemistry and Physics (Chemical Rubber Corporation, Edition 49, 1968) and the Smithsonian Meteorological Tables, Sixth Revised Edition, Robert J. List (Publication 4014, Smithsonian Institution, Washington, D. C.). The data are plotted in Figures II-1A, II-2, and II-3 as Munits in order to explore the possibility of ducting levels (i.e., vertical lines). The graph in Figure II-4 is reproduced from Reference 26 and makes use of B-units. The lines shown in Figure II-1B are presented as graphical aids to the intepretation of the radiosonde data in the other figures. The labels on the lines of Figure II-lB show the effective earth radii which would result from M-profiles of the indicated slopes. These slopes should be interpreted as showing a general trend rather than an actual height dependence of м.

The M-profiles shown in Figures II-1A, II-2, and II-3 are believed to be generally descriptive of the elevated atmospheric conditions which actually existed at the Boca Raton Field Site during the measurement period. The surface point, however, probably does not accurately represent the surface conditions at the Field Site, since these data were taken inland near the Miami airport. Inspection of Figure



Figure II-1. Modified refractivity versus height for 3 September and for several assumed effective earth radii.









Figure II-3. Modified refractivity versus height for 16 and 22 September.

II-4 shows that the region of interest extends to heights of several hundred meters; thus, more information is needed to actually define the near-surface refractivity. The data in Table II-2 are included to provide some information about the air-water interface which may be of value in defining the lower region. Reference 26 provides an approach to defining the height and strength of the surface evaporation layer from knowledge of air-water temperature difference and wind speed. Another possibility would be to refine the surface point of the M-profiles with the aid of the data of Table II-2. Neither of these approaches has been investigated.



Figure II-4. Limits for trapping as a function of layer thickness and intensity. (from reference 26, page 163)

DATE/TIME	HEIGHT (Meters)	PRESSURE (mb)	DRY BULB TEMP (°C)	DEW POINT (°C)	DEPRESSION (°C)	REFRACTIVITY (N Units)
3 Sept. 70, 0615 EST	0	1017	27.2		2.2	386.7
5 Sept. 70, 0015 ESI	155	1000	27.2		4.0	365.8
		947	22.4		1.5	351.1
		931	22.4		9.0	285.4
	1571	850	17.4		5.0	275.6
3 Sept. 70, 1815 EST	Ö	1017	28.8		4.9	367.7
	150	1000	26.2		4.4	354.9
		968	23.8		2.2	417.8
		948	23.8		9.0	291.2
	1563	850	17.6		5.6	272.3
8 Sept. 70, 0615 EST	0	1013	25.0		3.6	360.1
	121	1000	26.0		3.0	367 .7
		937	21.6		0.9	349.7
		925	21.6		4.9	312.2
	1555	850	16.8		3.3	285.1
8 Sept. 70, 1815 EST	0	1013	29.4		4.4	375.9
	119	1000	27.0		5.0	353.7
		949	23.0		1.9	349.0
	1535	850	16.8		4.8	276.2
10 Sept. 70, 0615 EST	0	1017	27.8		5.0	347.8
	150	1000	26.6		3.2	351.0
		934	21.2		1.9	326.2
		909	21.2		7.0	280.5
	1567	850	17.0		5.0	262.3
					1	

TABLE II-1. RADIOSONDE DATA FOR SEPTEMBER 1970. (MIAMI, FLA.)

DATE/TIME	HEIGHT (Meters)	PRESSURE (mb)	DRY BULB TEMP (°C)	DEW POINT (°C)	DEPRESSION (°C)	REFRACTIVITY (N Units)
10 Sept. 70, 1815 EST	0 150 1567	1017 1000 949 927 850	29.4 27.4 23.0 21.4 18.2		6.0 4.9 1.5 5.6 5.7	347.6 343.6 337.1 299.2 262.8
15 Sept. 70, 0615 EST	0 136 1551	1015 1000 850	26.1 26.1 17.2	23.6 24.4 14.6		298.5 386.3 300.6
15 Sept. 70, 1815 EST	0 133 430 1548	1015 1000 967 850	25.6 24.7 24.5 16.5	24.0 23.0 21.9 14.5		388.0 378.2 361.5 301.0
16 Sept. 70, 0615 EST	0 159 830 1578∽	1018 1000 925 850	26.7 26.5 20.5 17.3	24.5 22.5 17.3 10.7		390.2 371.0 328.7 283.2
16 Sept. 70, 1815 EST	0 157 1060 1576	1017 1000 902 850	27.8 26.9 20.3 17.7	25.6 23.5 15.7 12.8		396.1 378.7 358.9 292.0
17 Sept. 70, 0615 EST	0 157 1090 1340 1569	1017 1000 899 873 850	26.1 26.6 19.0 17.9 16.5	25.1 25.4 18.5 12.5 13.2		395.0 391.6 330.5 295.2 294.8
	7202	0.00	10.5	1.304		274.0

TABLE II-1. RADIOSONDE DATA FOR SEPTEMBER 1970. (MIAMI, FLA.) (Continued)
DATE/TIME	HEIGHT (Meters)	PRESSURE (mb)	DRY BULB TEMP (°C)	DEW POINT (°C)	DEPRESSION (°C)	REFRACTIVITY (N Units)
10 0 70 1915 FGT	0	1017	20 /	·	6.0	2/7 6
10 Sept. 70, 1815 EST	0	1017	29.4		6.0	347.6
	150	1000	27.4		4.9	343.6
		949	23.0		1.5	337.1
		927	21.4		5.6	299.2
	1567	850	18.2		5.7	262.8
15 0 0015 000		1015			1	000 F
15 Sept. 70, 0615 EST	0	1015	26.1	23.6		298.5
	136	1000	26.1	24.4		386.3
	1551	850	17.2	14.6	(a. w. ta	300.6
15 Sept. 70, 1815 EST	0	1015	25.6	24.0		388.0
15 00000 703 1015 201	133	1000	24.7	23.0		378.2
	430	967	24.5	21.9		361.5
	1548	850	16.5	14.5		301.0
	1340	050	10.5	14.5		501.0
16 Sept. 70, 0615 EST	0	1018	26.7	24.5		390.2
	159	1000	26.5	22.5		371.0
	830	925	20.5	17.3		328.7
	1578.	850	17.3	10.7		283.2
16 Sept. 70, 1815 EST	0	1017	27.8	25.6		396.1
	157	1000	26.9	23.5		378.7
	1060	902	20.3	15.7		358.9
	1576	850	17.7	12.8		292.0
17 Sept. 70, 0615 EST	0	1017	26.1	25.1	~ ~ ~	395.0
	157	1000	26.6	25.4		391.6
	1090	899	19.0	18.5		330.5
	1340	873	17.9	12.5		295.2
	1569	850	16.5	13.2		294.8
	1309					
	· [·]				}	

TABLE II-1. RADIOSONDE DATA FOR SEPTEMBER 1970. (MIAMI, FLA.) (Continued)

DATE/TIME	HEIGHT (Meters)	PRESSURE (mb)	DRY BULB TEMP (°C)	DEW POINT (°C)	DEPRESSION (°C)	REFRACTIVITY (N Units)
22 Sept. 70, 1815 EST	0 123 790 1538	1014 1000 927 850	28.9 26.8 21.5 17.5	23.3 24.5 21.3 15.4		376.5 385.5 351.5 303.3
23 Sept. 70, 0615 EST	0 129 700 1080 1545	1014 1000 938 898 850	25.0 26.6 20.5 20.0 17.7	24.5 23.6 19.5 12.2 6.0		392.2 379.2 345.1 341.8 266.4

TABLE 11-1. RADIOSONDE DATA FOR SEPTEMBER 1970. (MIAMI, FLA.) (Continued)

DATE	Min.	AIR TEMPERATURE Max.	(^o F) Avg.	SURF* TEMPERATURE (^O F)
2.0+	81	86	84	88
2 Sept.	1			
3 Sept.	82	87	85	88
4 Sept.	80	88	84	88
7 Sept.	81	87	84	87
8 Sept.	79	88	84	89
9 Sept.	79	86	83	88
10 Sept.	81	87	84	88
11 Sept.	80	86	83	90
15 Sept.	73	83	78	85
16 Sept.	80	85	83	85
17 Sept.	73	85	79	85
21 Sept.	73	84	79	85
22 Sept.	74	85	80	85
23 Sept.	79	85	82	85

TABLE II-2. AIR-WATER TEMPERATURES FOR SELECTED DAYS IN SEPTEMBER 1970

*Measured at 3 P.M. EST.

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WEATHER

DATA SUMMARIES

FOR SELECTED DAYS

IN SEPTEMBER 1970

	DAY	SUN	MON	TUES	WED	THURS	FRI	SAT
	Wind Speed and Dir.	22 <i>EN</i> E	IGENE	8ENE	8 NE	9ENE	3 WNW	BNW
8:00 AM	Sky		CLR	P.C.	P.C.	P.C.	P.C.	
	Precip.		None	None	None	None	None	
	Wind Speed and Dir.	22 <i>E</i>	IL NE	IDNE	9ENE	8ENE	6E	6 N W
12:00 NOON	Sky		P.C.	P.C.	CLR	P.C.	P.C.	
	Precip.		NONE	NoNE	None	NONE	NoNE	
	Wind Speed and Dir.	RIENE	IDNÉ		II ENE	12 E	14 E	II SE
5:00 PM	Sky		PC.	CLR	P.C.	P.e.	CLOY	
	Precip.		NoNE	None	Nowe	NONE	None	
	Wind Speed and Dir.			Serie and a subsection of the subsection of the				,
	Sky	·						
	Precip.			•				
	t 24 hour ainfall		.00	.00	.00	.00	.00	

WEATHER LOG FOR WEEK OF AUGUST 30, 1970

NEATHER LOG FOR WEEK OF SUTEMBER 6,1970

	DAY	SUN	MON	TUES	WED.	THURS	FRI	SAT
	Wind Speed and Dir.	6 WNW	2 WHW	6 WNW	5N	2 W	4 NW	
8:00 AM	Sky			P.C.	P.C.	P.C.	P.C.	
	Precip.			None	NONE	NONE	NONE	
12:00 NOON	Wind Speed and Dir.	8E	8 NE	HNE	13 ENE	8 ENE	IO NNE	
	Sky			CLDY	P.C.	CLR	CLDY	
	Precip.			None	NONE	None	None	
	Wind Speed and Dir.	16 E	24 E	IZ ENE	IS SSE	23 ENE	IA NNE	
5:00 PM	Sky			P.C.	CLOY	P.C.	P.C.	
	Precip.			None	NONE	NoNE	NONE	
	Wind Speed and Dir.							
	Sky							
	Precip.							
	t 24 hour aimfall			.00	.00	.03	.00	

	DAY	SUN	MON	TUES	WED	THURS	FRI	SAT
	Wind Speed and Dir.		20 ENE	IBNE	35858	HENE	29ENE	•.
8:00 AM	Sky		CLDY	CLDY	CLDY	P.C.	CLOY	
	Precip.		LIGHT	None	None	NONE	NONE	
	Wind Speed and Dir.		14 E	NONE	26 E	20 ENE	IL ENE	
12:00 NOON	Sky		CLDY	CLDY	P.C.	P. C.	CLOY	
	Precip.		NONE	NONE	None	None	HEAVY	•
	Wind Speed and Dir.		3.NWE	8 E	IA ENE	3D ENE	11'SE	
5:00 PM	Sky		Overca st	CLOY	P.C.	P.C.	CLDY	11 12 - 4
ra	Precip.		LIGHT	None	NONE	NONE	LIGHT	
	Wind Speed and Dir.							
	Sky							
	Precip.							
	t 24 hour ainfall		.72	.24	.05	.00	.16	

WEATHER LOG FOR WEEK OF SEPTEMBER 13, 1970

WEATHER LOG FOR WEEK OF SEATEMBER 20, 1970

1.1.1	DAY	SUN	MON	TUES	WED	THURS	FRI	SA
	Wind Speed and Dir.		8 ENE	IBNE	8 SE			
8:00 AM	Sky		CLOY	PC.	P.C.			
	Precip.		NONE	None	Mop.			
	Wind Speed and Dir.		9E	13 E	IZ ENE			
12:00 NOON	Sky	and the second second	CLPY .	P.C.	P.C.			• • •
	Precip.		Noné	NONE	None			
	Wind Speed and Dir.		1 E	13 [°] E				
5:00 PM	Sky		CLDY	P.C.				-
	Precip.		None	NONE				
	Wind Speed and Dir.							
	Sky							
	Precip.							
Pas R	t 24 hour ainfall		.00	.00				

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Some Cooling Expected Over Much of Nation ٠ Scattered thundershowstorms were severe. Temthe Southwest. Cooler teau region. Fair skies will the northeastern states SMALL BOATS: Inland waers rumbled this afternoon peratures were high over temperatures prevailed in and in the Pacific Northbe the rule, but some ters along the southeast in all but the Pacific Coast much of the United Florida coast including the Northeast. The nationwest, and cooler air is thundershowers will be states and in the north-Biscayne and Florida bays eastern quarter of the na-States, particularly in the al weather forecast: Cool likely from the northern scattered from the Appa-- casterly winds 10-15 tion and some of these northern Plains region and weather will continue in Plains to the southern plalachians to the Rockies. knots with a light to moderate chop on the waters. Local, National, World FORECAST WEATHER MAP FOR WED. A.M. SEPT. 2, 1970 Over the Guif coastal waters - easterly winds 10 Map, Data and Forecasts By ESSA Weather Burson, Mami, knots, moving onshore 10M Temperatures during the afternoon. Seas 2-3 feet. Over the Atlantic coastal waters from Cape GREATER MIAMI 20 ir ut LOW Kennedy to Jupiter Light H L Procip 93 79 99 74 13 L Precip 77 19 80 27 77 11 - variable mostly east 1777 1777 1777 1777 1777 Coral Gables Miami Airport Miami Beach North Miami Beach South Miami winds 10 knots with seas Statistic in the state 2-3 feet. ALCOLVILLE . undani Bullalo New York Philadelphia Pittsburgh Washington FOREIGN FLORIDA 7873747278 31739474 FLORIDA Apalachicela 19 73 Clewision 19 74 Clewision 19 74 Daylona Bch 19 74 Daylona Bch 19 74 Homesical 19 73 Hammesical 19 FOR City Aberdeen Aucktand Berlin Birminshamt Crasblanca Coornhasen Dublin Geneva Hona Kong Lisben London Madrud Manita Moscow MIDDLE WEST COAST AND BREVARD AREAS -... Generally fair Ilirough Thuisday with a chance of shawers, Low 70 to 75. Afternoon highs 90 to 95. Variable winds 10 m.p.h. ... Migh 61 37 GLOUN 67746726884667766770667288778687 MIDWEST NAPLES AND LAKE OKEECHOREE AREAS -- Generally lair through Inucidaty with a signit charke of al-ternoon showers, Low in the mid 70s, Afternoon hush 50 10 92. Motify east winds 10 m.p.h. Rain probability 20 per cent. Chicano Cinclinati Cleveland Columbus Des Moines Detroit Duluth Indicaapelis Kansas City Milwautee Mols. St. P. Omaha St. Louis 78 42 83 65 78 42 74 51 89 67 74 43 89 67 75 44 95 75 71 44 95 75 71 44 98 66 88 69 -----:ij SHOWERS 67 BROWARD, PALM BEACH AND KEYS AREAS ---- Parily cloudy through Thursday with a chance of shokers, Low 75 to 80, Atternoon highs 85 to 90, Essterly winds 10 to 15 m.p.h. Rein probability 30 per cent. liow 64 t - أسط WEST FLORIDA — Generally fair, with a few shower's in the earterne southern por-tron and unternoon allowed to the few trong and unternoon and allow in the trong in the north and allow in the south. North lows 65-75 month and near 30 along the southcast cost and Keys. SOUTH 5 NORMA Bismarck Brownsville Denver Fl. Worth Houston Las Venas Las Anacles Okta. City San Antonie San Diego S. Francisce Gentia Asheville 14 55 93 77 79 82 77 72 101 84 77 107 81 75 107 81 75 107 81 75 107 81 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 84 75 108 85 108 75 108 75 108 75 108 75 108 75 108 75 108 75 108 75 87 93 91 93 97 84 84 Attanta Birmingham Charleston Charlotte Little Rock New Orleans Raleigh 94 53 216 737878797171 22 11 2 222 Phases of the Moon Moonrise Today 8:23 a.m. 1 PLORIDA: EXTENDED OUTLOOK ----Friday through Sunday: Parity Cloudy with widely scattered mainty alter-noon and evening thundershowers. Af-ternoon highs 8 to 95. Overnight lows meinhy in the 702. 7:39 p.m. Finas Sunset Today head ä 972**4*** EAST 7:40 v.m. Moonset Today 8:33 p.m. Sunset Today Albany, N.Y. 76 58 Bosten 72 55 ... Seattle Sept. & Sept. 15 Scot. 22 Aug. 31





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Oct. 7 Sept. 15 Sept. 22 Sept. 30

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In inches Rainfall since Jan. T in Inches Deficiency since Jan, 1 in Inches

1.48 33.41 3.54

Fair Weather Likely For East, West Coasts 20 2 0 3 0 2 20 2 200 0 2 8 Showers and locally Minnesota and from the eastward from Maine and Mexico to California. The showery weather is likely heavy thunderstorms are MIAMI AND VICINITY: central Gulf to Florica some light rain spreading national weather forecast: in the Mississippi Valley, Sunny today and Friday. occurring from Louisiana and southern Georgia. The to the Washington coast. The skics are generally Generally sunny weather the lower Ohio Valley and High 88. Easterly winds 10 and southeastern New only other precipitation in to 15 miles an hour. Show-Mexico to South Dakota the nation was some light clear from eastern Monis in prospect for much of the upper Great Lakes reer probability 30 per cent and extreme southern rain or drizzle moving tana and western New the nation. Cloudy and gion. during morning hours today. Local, National, World FORECAST WEATHER MAP FOR THURS. A.M. SEPT. 17, 1970 SMALL BOATS: Inland waters along the southeast Fibride coast including Bis-canne and Florida bays. — easterly winds to to 15 knots with a moderate choo on the waters. Mer. Data and Forecasts \$+ \$55A Waster Temperatures FLORIDA: Partly cloudy today with a chance of a few morning showers along the east coast and Keys. GREATER MIAMI along the fait cost and keys. FLORIDA EXTENDED OUTLOOK: Sat-urday through Monday -- Partly clou-dy with valtered afternoon finder Western periods of the state and a few snowers along the East cost and Keys, Attencion highs neer 90. Lows mainby un the 703. H L Precip. 86 75 94 Miami Beach 88 78 97 North Miami Beach 85 77 92 South Miami Precip. Coral Gables Miami Airport Miami Beach ະ ກັກ 11 73 EAST FOREIGN FLORIDA CITY HIGH 57 77 revs. Avernoon numb Acer 90. Lows Prantov in the 703. LANE UD CEECHDEREE AND INDIAN Cloucy incouch Friday with a Chance of atternoon Shevert. Lows in the 213 stillate near 70. Earlerly winds at creating incouch Friday with a chance of atternoon Shevert. Lows in the creating incouch Friday winds at creating incouch friday winds at the shever the shever shever the RO MERGE Party cloucy through Friday wind a chance of showers mainly dur-ing the shell and morting hurs. At a creating the shever shever we showers. Rain probability 30 per cent. 1.11 Albany, N.Y. 71 55 Apalachicola 67 75 Alamy, W.T. 73 33 Boston 89 53 Buffalo 73 44 New York 92 61 Philsburgh 13 67 Philsburgh 14 70 Washington 14 70 Bradenton 95 75 Cleviston 91 74 .71 Buffalo 2434418482834227442244274437 .54 Daylona Bch. 99 78 88 77 70 74 Ft. Laud. .87 -47 Ft. Myers Cam Gainesville MIDWEST 92 75 88 72 70 76 88 78 89 78 80 78 80 78 95 74 95 74 95 75 89 77 95 75 89 77 95 75 89 77 95 75 89 73 95 75 89 73 95 75 89 77 95 76 89 77 95 76 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 89 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 80 77 Gainesville Momestead Jacksonvilla Key Wett Laxriand Napies Ocaia Oriande Pensacola Sarasola St. Pete. Tailahassee Tampa Varo Bench W. P. Bch. .19 40 35 93 45 64 58 812 44 41 52 72 40 63 37 83 63 48 41 60 30 61 40 54 49 81 44 Chicago Cincinnati Uncinnati Cleveland Do K Moines Do K Moines Do Lotroit Duista Duistanapolis Kansas City Mois-St. P. Mois-St. Louis LOW Statistics 7:00 7:00 7:00 PAN AMERICAN PAN AR Acanuico Berbacos Acronuca Cuinacan Manacan Hermosilip Kienero Cuinacan Hermosilip Los Mochil Los Mochil Cuinacan Cuinacan Hermosilip Monterrey San Juan San Juan San Juan San Juan WEST SOUTH Bismarck Rrownswille Denver Houston Las Vepas Bits Vepas Colla, City Sathanic Sathanic Sathanic San Diego San Diego San Diego Sathanic Seattle 47 32 94 74 17 45 19 74 19 74 10 63 97 44 76 38 92 77 78 45 71 32 71 52 Asheville Atlanta Birmingham Charloston Charloste J'son, Miss. Little Rock Louisville Memohis New Orleatte Morfolis \$7 54 \$9 71 \$12 76 \$97 54 \$97 54 \$97 54 \$95 73 \$95 73 \$99 54 \$91 73 \$95 73 \$94 73 \$95 73 \$94 64 \$95 73 \$94 47 \$95 43 44% 94097844828 Phases of the Moon Moonrise Today 8:50 p.m. 1939 Local raisfall for 24 hours endine 7 p.m. Raisfall this month in Inches Raisfall excess this month Sunrise Today 7:07 a.m. .07 \$.92 Sunset Today 7:23 p.m. Moonset Friday 9:28 a.m. Raintain Easter Jan. 1 in Inches Rainfall since Jan. 1 in Inches Deficiency since Jan. 1 in inches 1,23 Norfolk Richmond Oct. 7 Sept. 15 Sept. 22 Sept. 30









APPENDIX C. AUTO- AND CROSS-CORRELATION INVESTIGATIONS OF THE DATA FROM 22 SEPTEMBER 1970

(Attachment III of final report on contract DAAG39-70-0053, 17 Feb. 1971.)

The data presented here were obtained from a limited analysis of the magnetic-tape records of the experiments on 22 September. They are believed to be representative of the general behavior of all the data recorded. They should be considered as guides to the direction which future, more detailed, analysis should take.

The auto- and cross-correlation plots shown in Figures III-1 through III-5 were made by re-playing the magnetic tape of the indicated data runs into a Fabri-Tek Model 1072 Signal Averager configured for computing such functions. Due to the design of the Model 1072, the resulting plots are only approximately normalized for signal distributions such as considered here; thus, care must be exercised in interpreting the value of the coefficients of the correlation functions obtained.

The correlation functions were computed and plotted for each frequency at each range point. These were reviewed for calibration difficulties, noise and hum problems, and repro-The examples shown in Figures III-l through ducibility. III-5 were chosen as being representative and illustrative of the general conclusions about the correlation properties of these data runs on 22 September. These general conclusions are as follows. (1) The received signals are approximately periodic and have periods of 2 to 3 seconds, although there are other competing periodic components, principally a component with period between 6 and 7 seconds. (2) The fluctuations of received signals at any two frequencies are virtually uncorrelated. (3) The recorded samples are obtained from a process that is only approximately statistically stationary.

Except for III-3 and III-5b, the plots were all made with a dwell time of 40 milliseconds using 256 channels, which resulted in an approximate sweep duration of 10 seconds. The amplitude and d-c level of the input signals were adjusted to minimize overflow problems in the A/D converter of the Model 1072. The noise reference was adjusted to have approximately the same rms value as the corresponding data record. The square-wave reference was adjusted to have a peak amplitude approximately equal to the "average of the peaks" of the corresponding data record.



Figure III-1. Comparison between auto-correlation plots
for (A) a noise signal (Gaussian, 0.5 Hz bandwidth
filter) and (B) the received signal on 30 MHz
(Run 2, 22 September.)



Figure III-2. Comparison between cross-correlation plots for (A) a square-wave signal (1 Hz period) and (B) the product of the received signals on 412 and 140 MHz (Run 2, 22 September.)







Figure III-5. Comparison between the auto-correlation plot of (A) the complete record of the received signal on 30 MHz for Run 2 (22 September) and (B) the smoothed time history of the received signal.

Sixteen sweeps of 10 seconds each were overlaid for each plot; since most of the samples on the magnetic tape are of one-minute duration, this required several passes of the tape. The only problem encountered with this overlaying process was that the tape-transients prevented the stripping of the d-c component with high-pass filters; such stripping would have provided a more accurate zero reference for the plots. This problem was not resolved due to the limited amount of time available for this analysis.

Figure III-3 and III-4 are included to illustrate the similarity between the auto-correlation functions of the signals at different frequencies (compare with Figure III-1), and also to demonstrate the reproducibility of some of the data records.

Figure III-5 illustrates a data run which exhibited rather different behavior near the end of the sample period for which no explanation has been found. The autocorrelation plot of Figure III-5A was made from the complete data record for that run and includes the last ten seconds of data which exhibit the unusual behavior. Figure III-5B shows a smoothed time history of this portion of the record. Figure III-1B shows the results obtained when the unusual signal is deleted.