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SHADZO: A COMPUTER PROGRAM FOR ESTI-MATING THE POSITION AND SHAPE OF THE SURFACE SHADOW ZONE IN SONAR OPERATIONS

Bernard de Raigniac, et al

SACLANT ASW Research Centre La Spezia, Italy

15 November 1972

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NORTH ATLANTIC TREATY ORGANIZATION SACLANT ASW RESEARCH CENTRE Viale San Bartolomeo 400 I 19026 - La Spezia, Italy

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Bernard de Raigniac and John Padley

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SHADZO: A COMPUTER PROGRAM FOR STIMATING THE POSITION AND SHAPE OF THE SURFACE SHADOW ZONE IN SONAR OPERATIONS

by

Bernard de Raigniac and John Padley

ABSTRACT

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SHADZO is a composite program which calculates the position and shape of the first surface shadow zone as a function of the source depth for a given sound speed profile. The program is small enough to be run on a shipboard mini-computer in a few minutes.

INTRODUCTION

It has been found from SACLANTCEN's reverberation studies that information on the position and extent of the surface shadow zone^{*} is needed during at-sea experiments. Thus, a program has been developed which, given the sound speed profile, calculates the pertinent characteristics of the shadow zone and can be run on a shipboard mini-computer in a few minutes. In order to make the maximum pessible information available to the scientists aboard ship, the program also includes the estimation of shadow zone shape.

SHADZO (surface SHADow ZOne program) is a composite program which calculates the position and shape of the surface shadow zone, as a function of the source depth, for a given sound speed profile. These characteristics are obtained by direct investigation of the limiting rays, rather than by representation of the sound field by ray-tracing with a high density of rays.

This memorandum describes the theoretical basis for, and the implementation of, the two basic parts of SHAZDO: (1) a part that calculates the distance (i.e., the inner range limit), the extent and the maximum thickness as functions of source depth, and (2) a part that estimates the shape of the shadow zone for selected source depths. A flow chart, a listing, and explanatory diagrams of SHAZDO are given in Appendix A.

2

^{*} The surface shadow zone treated here is the first (i.e., shortest-range shadow zone; the recurring surface shadow zones at longer ranges are not covered.

1. THEORY: POSITION AND SHAPE OF THE SURFACE SHADOW ZONE

1.1 Background

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When the sound source is located above the critical depth^{*}, z_{crit}, there is a shadow zone along the surface at certain ranges. This surface shadow zone has been discussed by Mellterg, who calls it "shadow layer", in Ref. 1 . Mellberg provides formulae for the maximum thickness and horizontal extent of the shadow zone, based on a 2-layer, constant gradient model of the medium. The present memorandum provides a further description of the characteristics of the shadow zone, based on a multi-layer, constant-gradient model.

Figures 1 and 2 illustrate the formation of the surface shadow zone in a medium approximated by a two-layer, constant-gradient model. Figure 1a shows the rays which limit the shadow zone, both in range and depth, when the source is between the surface and the minimum-speed-depth, z_m . At the surface, the shadow zone is bounded by rays which have zero grazing angle. The maximum depth, or maximum thickness of the shadow zone, is the depth at which the ray that was horizontal at the source becomes horizontal again. When the source is located between the minimum-speed depth z_m and the critical depth, z_{crit} , as in Fig. 1b, a shadow zone of smaller range extent and smaller maximum thickness will occur.

Figure 2 illustrates the distance, extent and maximum thickness of the shadow zone, again for a 2-layer model. The multi-layer model will be introduced next, and then these three characteristics will be discussed in turn.

The critical depth is the depth at which the sound speed is the same as at the sea surface

In SHADZO, 3 multi-layer, constant-gradient model of the medium is used. The rays propagate along circle segments in each layer, as illustrated in Fig. 3. The radius of the path in the ith layer is given by:

$$R_{1} = \frac{k}{g_{1}}$$
 [Eq. 1]

where

k = Snell's constant of the ray = c/cos@ (at any depth) g_i = gradient in the ith layer

$$= \frac{c_i - c_{i-1}}{\Delta z_i}$$

The horizontal distance travelled by the ray in the ith layer is then:

$$\Delta d_{i} = R_{i} (\sin \alpha_{i-1} - \sin \alpha_{i})$$

= $\Delta z_{i} \frac{\sqrt{k^{2} - c_{i-1}^{2}} - \sqrt{k^{2} - c_{i}^{2}}}{c_{i} - c_{i-1}}$. [Eq. 2]

1.2 Distance

The distance to the shadow zone. 's illustrated in Fig. 2, is defined as the inner range limit of the shadow zone at the surface. Appendix A of Ref. 2 provides formulae for the distance, for both 2-layer and multi-layer constant-gradient models.

From Eq. 2, we see that the total horizontal distance, d, travelled by a ray in traversing n layers between the source depth and the surface is given by

$$d = \sum_{i=1}^{n} \Delta d_{i} = \sum_{i=1}^{n} \Delta z_{i} \frac{\sqrt{k^{2} - c_{i-1}^{2}} - \sqrt{k^{2} - c_{i}^{2}}}{c_{i} - c_{i-1}}$$

To avoid computing errors when $c_i \approx c_{i-1}$, this expression may be transformed into

$$d = \sum_{i=1}^{n} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{k^{2} - c_{i-1}^{2}} + \sqrt{k^{2} - c_{i}^{2}}} . \qquad [Eq. 3]$$

d may be expressed as a function of grazing angle at the surface, γ , by writing $k = c_0 / \cos \gamma$. Thus, we see that the distance to the shadow zone, D, is obtained from Eq. 3 simply by setting $\gamma = 0$; then, we have $k = c_0$ and

$$D = \sum_{i=1}^{n} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{c_{0}^{2} - c_{i-1}^{2}} + \sqrt{c_{0}^{2} - c_{i}^{2}}} . \qquad [Eq. 4]$$

1.3 Extent

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The horizontal extent of the shadow zone at the surface is determined by two rays having zero grazing angle, as illustrated in Fig. 2. It can be seen from Fig. 2 that the horizontal distance travelled by the long-range limiting ray in going between source depth and critical depth is a measure of the extent of the shadow zone. Thus, the extent is given by

$$E = 2 \sum_{i=n+1}^{k} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{c_{0}^{2} - c_{i-1}^{2}} + \sqrt{c_{0}^{2} - c_{i}^{2}}} \qquad [Eq. 5]$$

where it is assumed that there are n layers between the source depth and the surface and k layers between the critical depth and the surface.

1.4 Maximum Thickness

As discussed in Ref. 1 and illustrated in Figs. 1 and 2, the maximum depth of the shadow zone is the depth where a ray that was horizontal at the source becomes horizontal again. At this depth, z_t , the sound speed is equal to c_s , the sound speed at source depth.

1.5 Shape

The shape of the shadow zone can be defined as the envelope of the downward-refracted rays, as illustrated by the dashed curves in Fig. 1. This envelope is relatively difficult to calculate exactly, so an estimate of the shape is obtained as follows. First, at close_y-spaced depths, we determine the locus of points at which ruys vertex (i.e. become horizontal). For the case shown in Fig. 1b, we see that this locus would provide a reasonable estimate of the envelope^{*}. Figure 4 illustrates the case of a limiting ray, such as might be encountered in the presence of a strong negative gradient; in this case, the locus of vertices is not a good estimate. To improve the estimate, at each depth, the intersections of rays vertexing at shallower depths are determined. Finally, at each depth, that point (vertex or intersection) is used which results in the smallest extent of the shadow zone. The estimation of sh_{α} , w zone shape from these vertices and intersections is illustrated in Fig. 4.

6

It would be clearly not provide a reasonable estimate for the case in Fig. 1a; nowever, this case is not addressed here, as the snape estimation part of SHADZO has been implemented only for cases in which $z_s > z_m$.



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FIG. 1 FORMATION OF THE SHADOW ZONE







Server Lines &





FIG. 4 ESTIMATION OF SHADOW ZONE SHAPE

2. DESCRIPTION OF THE SHADZO PROGRAM

2.1 Hardware Configuration

The program was written to run under the Hewlett-Packard Real-Time System [Ref. 3], and thus requires a minimum hardware configuration of:

H-P 2116B Computer with 16K Memory
H-P 12578A Direct Memory Access
H-P 12579A Extended Arithmetic Unit
H-P 12591A Memory Protect
Fixed Head Disc or Drum Storage Unit
Time Base Generator
Operator Console (ASR-33 or ASR-35 Teleprinter)

In addition, the SHADZO program requires a Tektronix T4002/4802 Graphic Computer Terminal with Tektronix Joystick 015-0175000 and Hard Copy Unit 4601. The Tektronix Terminal can be used in place of the operator console, if an additional paper-tape input device is available. In the absence of a Tektronix Terminal, the program can still produce a printed output on any output writer.

2.2 Software Configuration

The program requires a Real-Time System generated to provide a minimum background disc-resident area of 20K (octal) locations. The Tektronix Terminal should be allocated logical unit number 16 and should be used with the Real-Time teleprinter driver DRV00.

2.3 Program Inputs

The data are input to the program via a punched tape containing the temperature or sound speed profile. Table 1 gives an example of such a profile, as well as the required format.

TABLE 1

TYPICAL DATA TAPE



In the conversion from temperature profile to sound speed profile [according to the Leroy formula (Ref. 4)], the salinity and longitude are considered constants, being pre-set to 38.6 parts/ thousand and 40° , respectively. Source depth values are input via the Operator Console.

2.4 Program Details

The SHADZO² program is written in Fortran II, with the exception of the routines for the Tektronix Terminal, which are standard SACLANTCEN library routines written in Assembler Code.

The program consists of four basic sections, as follows:

<u>Section One</u> Reading of the data tape tape, and conversion of temperatures to sound speeds it necessary.

<u>Section Two</u>: Calculation and printing of distance, extent and maximum thickness.

Section Three: Calculation and graphical display of distance, extent and maximum thickness.

Section Four: Calculation and graphical display of shadow zone shape.

The first section is performed once for each set of data; the other sections are performed as many times as required.

Sections two and three can be run with two alternative models of the sound speed profile: (1) a multi-layer, constant-gradient model, using all of the sound speeds calculated from the Leroy formula; and (2) an approximation using two constant-gradient layers.

Term in Text

Term 1.º Program

Sound speed Maximum thickness Distance Extent Velocity Thickness Range Extension

Because of the restriction in H-P Fortran II which allows only five characters per identifier, the program name actually used is "SHAZO". There are some discreparcies between the terminology used in the text of this memorandum and the terminology used in the program and its outputs shown below. The correspondence is as follows :

A flow chart and listing of the program, together with diagrams indicating the significance of variable names for points on the sound speed profile, are given in the appendix.

2.5 Program Outputs

The outputs from the program are prints and plots, as described below.

2.5.1 Prints

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a. Sound speed profile: A sample output is given in .Table 2.

TABLE 2

EXAMPLE OF SOUND SPEED PROFILE GUTPUT

SHADOW ZONE PREDICTIONS

XBT FL 11	DATE	29-7-71	TIME 1-40
DEPTHS	VELOCITIES		
METRES	METRES/SEC		
. øø	1537.3		
6.00	1535.2		
8.00	1533.5		
12.00	1532.1		
16.00	1525.0		
18.00	1520.8		
20.00	1516.4		
24.00	1513.5		
28.00	1511.4		
40.00	151Ø.Ø		
64.00	1507.8		
180.00	1509.7		
250.00	1510.7		
400.00	1513.Ø		
450.00	1513.7		
2500.00	1548.Ø		

b. Distance, extent and maximum thickness: An example is given in Table 3 for the multi-layer model. The output from the two-layer model has a similar format.

TABLE 3

EXAMPLE OF SHADOW ZONE CHARACTERISTICS GUTPUT

MULTILAYER MODEL

SOURCE DEPTH	EXTENSION	RANGE	THICKNESS	S. VELOCITY
METRES	METRES	METRES	METRES	M/SEC
1 \$\$.\$	35826.4	794-3	57-5	15\$8.4\$
266.6	34794.9	1310.0	39.8	1510.00
366.6	33733.8	1849.6	27.8	1511.48
499.9	32649.1	2387.4	24.9	1513.02
500.0	31511.9	2951.6	22.6	1514.52
699.0	30341.5	3536.8	20.3	1516.20
706.0	29122.7	4146.2	19.3	1517.87
800.0	27849.2	4782.9	18.6	1519.55
900.0	26513.1	5451.0	17.8	1521.22
1000.0	25164.4	6155.3	17.0	1522.90
1100.0	23610.1	6902.5	16.2	1524.57
1200.0	22012.7	7701.2	15.3	1526.25
1300.0	20288.1	8563.5	14.4	1527.92
1400.0	18490.3	9567.4	13.4	1529.59
1500.0	16292.9	10561.1	12.5	1531.27
1600.0	13865.9	11774.6	9.6	1532.94
1700.0	10908.2	13253.4	6.7	1534.62
18dd d	6755 2	1 5 2 2 0 0	2 0	1526 20

2.5.2 Plots

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All graphical outputs are plotted on the Tektronix Terminal and have a similar format. The results are plotted on a 5×5 grid and a scale factor for each parameter is printed on the display; this scale factor is the number of metres equivalent to one division of the display (i.e., full scale is five times the scale factor). At the end of each display, a copy is produced on the Hard Copy Unit. The origin of the plot is the upper left hand corner; the vertical parameter is depth and the other relevant parameter is plotted horizontally.

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with the star starting and the

a. Distance, extent and maximum thickness: one plot is produced for each parameter. Examples are given in Fig. 5.

b. Shape: One plot is produced. If more than one source depth is requested, all outputs are plotted on the same graph to the same scale. An example is given in Fig. 6.

2.6 Operation

To run the program, load the data tape in the tape reader and enter the program (under the Real-Time System, this is effected by typing "ON, SHADZO" on the Operator Console). If the last point on the temperature or sound speed profile is not deep enough to allow the critical depth to be calculated, the computer prints:

THE LAST POINT OF THE B.T. IS ABOVE THE CRITICAL DEPTH

and the program ends. In this case, the data tape must be retyped. Once a correct data tape has been read and the sound speed profile has been calculated and listed as shown in Table 2, the computer will print:

FOR SHADOW ZONE SHAPE TYPE 1 OTHERWISE TYPE -1 *

2.6.1 Distance, Extent and Maximum Thickness:

If -1 is replied to the question about shadow zone shape, the computer outputs:

FOR GRAPHIC OUTPUT TYPE 1 OTHERWISE TYPE -1

All questions of this type should be answered by either -1 or 1, followed by carriage return, line feed.

and after the response to this request, the computer outputs:

all all all a star and a second star and

FOR MULTILAYER TYPE 1, FOR 2 LAYER TYPE -1

When the type of model has been selected, if no graphic output was requested, then the computer prints:

TYPE IN S. DEPTH: START, STEP, END

The source depths for which output is required should then be typed in, giving the minimum depth first, and with values separated with commas. No output is produced for source depths greater than the critical depth. When the source depth has been input, the results are calculated and printed.

If graphic output is selected, then the three graphs are displayed and after the last output, the joystick is enabled and the computer prints:

TO EXPAND PLOT POSITION CURSOR AT MAXIMUM SOURCE DEPTH REQUIRED AND TYPE 1 OTHERWISE TYPE ∅

If an expansion is required, then the horizontal line of the cursor should be placed at the maximum source depth for the new plots and 1 should be typed. A new set of lisplays is then produced, and the expansion option is repeated. (It is not possible at this stage to increase the maximum source depth of the display. If this is required, the program must be continued and reprocessing of the same data requested. See below). If expansion of the plots is not required, type 0.

2.6.2 Shadow Zone Shape

If the shape is requested, then the source depths are requested as for the printer output above. The source depths must be below the depth of minimum sound speed; if the starting depth is less than this value, then it is automatically adjusted to this value. If the source depth exceeds the critical depth, the calculation stops. If only one source depth is required, the second and third parameters should be zero. The cumputer then calculates and displays the shape.

2.6.3 Termination

After the relevant output has finished, the computer prints:

TYPE \$ TO REPROCESS, 1 TO PROCEDS NEW DATA OK 2 TO STOP

If the response is 0, the program returns to the point at which it asks if the shadow zone shape is required. If the response is 1, a new data tape is read and processing restarts. If the response is 2, the program ends.



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FIG. 5 EXAMPLES OF DISTANCE (RANGE), EXTENT (EXTENSION) AND MAXIMUM THICKNESS PLOTS



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- "Real Time Software, A Reference Text for Programmers", Hewlett-Packard Co. Document No. HP 02005-90002, October 1971.

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4. Leroy, C.C., "Development of Simple Equations for Accurate and More Realistic Calculation of the Speed of Sound in Sea Water", SACLANTCEN Technical Report No. 128, November 1968, NATO UNCLASSIFIED. [AD No. 845 866]

APPENDIX A

DETAILED PROGRAM INFORMATION

A.1 Flow Chart

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A.2 Explanatory Diagrams and Program Listing

Note: The word "velocity" used in this Appendix corresponds to the words "sound speed" used in the Main Text.

A.1 Flow Chart

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SHADZO FLOW CHART

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A.2 Explanatory Diagrams and Program Listing

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PARAMETERS USED IN CALCULATION OF RANGE, EXTENSION AND THICKNESS



PARAMETERS USED IN CALCULATION OF SHAPE

PAGE 87.21 FTN.L С С THIS PEUGRAM JAS DEVELOPED AT -C С SACLANT AS& RESEARCH CENTRE С VIALE SAM BARTOLOWED.489 С 19826, LA SPEZIA Ċ ITALY. С PE05242 SmAL0(3,75) С С J.F. 27-14-71 Ċ DINENSIG: 0(40),V(40),C(40),IASCI(10),INA4E(6) DIMENSION PA(100) .EX(120) С THIS PROGRAM PREDICTS THE RANGE AND EXTENSION С С OF THE SHADD' ZONE FOR VARIOUS SOURCE DEPTHS. С С READ DATA TAPE AND CUNVERT TEMPERATURES TO С VELOCITIES IF NECESSARY. С PHI=42. SAL=38.6 10 D0 23 I=1,6 20 INAME(1)=200433 READ (5,3%) (INAME(1), I=1,6) 30 FORMAT(BAL) RED (5.#) 10AY .HONTH . IYEAK . IHOUK . MINUT READ (5+*) MODE N=1485(200E) DO 35 I=1.N 35 READ(5.*))(I) + (I) IF (MODE) 48+54 49 CALL BIRAN (V.D.N.SAL, PHI) 50 CALL FINTP (V.N. ITURN) DTURN=C(ITURN) VTURN=V(ITURN) С C C OUTPUT HEADING AND VELOCITY PROFILE CALL EXEC(3,11668,-1) WRITE(6,62)(INAME(I) + I=1,6), IDAY + MONTH, IYEAR, IHOUR • MINUT 60 FORMAT(24X. "SHADOW ZUNE PREDICTIONS",//,7X, "XBT ",6A1, 12**"J4[E"+13+2("-"+12)+12X+"TIME"+J3+"-"+I2+//+ 1 5X, "DEPTHS" . 10X, "VELOCITIES"/5X, "METRES", 10X, 2 3 "METRES/SEC"+/) WRITE(6,70)(D(I),v(I),I=1,N) 70 FORMAT(x)F16.2,F17.1) С FIND CHITICAL DEPTH ETC. С С IF (V(N)-V0) 30,100 80 WRITE(1.90) 90 FORMAT ("THE LAST POINT OF THE B.T. IS ABOVE THE ", "CFITICAL DEPTA") 1

say Baha das taun taun taun tahan baha dan baha dan baha dan baha da dara baha dan baha mata dara dara dara dar

```
PAGE "ROZZ
      STOP
  1-2 7=7(1)
      りょニス.
      IZ=1
      00 12# I=2-179RN
      IF (#*=* (E)) 1196123
  116 -2=:()
      D4=3(1)-
      I≠=1
  120 CENTINE
      CALL FITAL (ToD, V2+UCAIT, ICRIT, M+ ITURN)
      VCHITERS
      WRITE (E. 130) DORIT
  132 F@R#AT(/$12%$"CRITICAL DEPTH ="$F8.2. " METRES"/)
С
С
          REQUEST TYPE OF CALCULATION AND OUTPUT
С
  147 SPITE(1+145)
  145 F A ME STADOR ZUNE SHAPE TYPE 1 OTHERWISE TYPE -1 +*)
      READ(1+=) (SHAP
      IF (19422) 154,720
  155 FG-844T ("Fux GRAPHIC OUTPUT TYPE 1 OTHERAISE TYPE -1 +")
      RE40(1+#) IGRAP
      WRITE (1,159)
  167 FURHAT ("FUR HULTILAYER TYPE 1, FOR 2 LAYER TYPE -1 +")
      READ(1.=)LAYER
      IF (IGRAF) 170,350
С
 С
С
С
          PRINTER DUTPUT
С
  17% #FITE(1,18%)
  162 FORWAT ("TYPE IN S.DEPTH: START, STEP, END")
      RE= ) (1+=) 501+502+503
С
С
          OUTPUT HEADING ETC.
С
      CALL EXEC(3,11058,-1)
      IF (LAYER) 190,210
  199 N-ITE (5.203)
  200 FORMAT(CEX."THO LAYER MODEL"/)
      GO TC 230
  213 *** (75(-,22%)
  220 FOR HAT (ECX. "HOUTILAYER HOUEL"/)
  23 # APITE (6,249)
  24/ FORMAT (" SUDRCE DEFTH"4X"EXTENSION"7X"RANGE"6X"THICKNESS"
          5%,"5. VELOCITY"/+4/, "METRES"+0/, "METRES", 9%, "METRES"+
     i
     2
          6X . "METKES" . 1JA . "H/SEC")
С
С
          CALCULATE SOURCE DEPTH ETC.
С
      NX=(503-501)/502+1.
      DC 344 1=1+NX
      SUEP=3(1+FLUAT(I-1)#502
```

and the first of the state of the

PAGE TARAS

```
IF (04-50Er) 254-344
   254 IF (5027-00711) 268,349
   264 IF (SUEP-UTURA) 272+232
   278 CALL FITAL (U. V. SDEP . VEL. IDEP . ITUNN . 1)
       CALL FIVAL (VODAWELODEP, ISAN, ITURN)
       60 10 298
   28% CALL FIVAL (U.V.SUEP, VEL. (DEP, N. ITUKA)
       CALL FIVAL (V.O.VEL DEP, 19, 10, ITURN)
       CALL FIVAL (0, V.DEP, VEL, 17, ITURN, 1)
       CALL FIVAL (V, D, VEL, DEP-18+17, ITURN)
   290 IF (LAYER) 342, 312
 С
 С
           TWU LAYER MODEL
 С
   330 CALL TEO (VE . VCEIT, DCEIT, SDEP, DE, DTUEN, VTURN, RANGE, EXT, THICE)
С
C
           HULTILAYER BODEL
С
  310 CALL HULTI (VO+VEL, VCKIT+DCKIT+SDEP+ICRIT+IDEP+V+D+RANGE+EXT)
С
С
           PRINT RESULTS
C
  32# ##1TE (6+33#) SDEP+EXT+RANGE+TH1CK+VEL
  334 FORMAT (F10.1.3F14.1.F15.2)
  34% CONTINUE
      GO TO 1522
С
 С
С
С
          GRAPHIC OUTPUT
С
  350 SUHAX=UCHIT#2.95
      SGAIN= (SUAAA-De) /100.+DD
С
С
          FIND AAXIMUM VALUES
С
  368 IF (LAYER) 374.380
 37% CALL Truly-, YCHIT, UCKIT, SUMAX, DO, DTURN, VTURN, RAMAX, EX, TH)
      CALL T=0(y#+VCRIT+UCRIT+SDMIN+D0+OTURN+VTURN+RA+EXMAX+THMAX)
      GO FO 420
 389 IF (SOM4X-OTURN) 393,493
 390 CALL FIVAL (U.V.SDMAX, VEL. IDEP, ITURN . 1)
     CALL FIVAL (V.D. VEL. JEP. I. J. N. ITURN)
     GO TO 410
 480 CALL FIVAL (D. V. SCHAX, VEL. IDEP, N. ITURN)
     CALL FIVAL (V.J.VEL.JEP, 19, 19. ITURN)
     CALL FIVAL (D.V.DEP.VEL.17, ITURN.1)
     CALL FIVAL (V+D+VEL+DEP+IS+17+ITURN)
 410 CALL AULTI (VO.VEL, VCHIT, OCHIT, SDMAX, ICRIY, IDEP,
         V,0,1144月二人,三人)
     CALL FIVAL (U, V, SOMIN, VEL, IUEP, ITURN, 1)
     CALL, FIVAL (V+U+VEL+UEP+I9+N+ITURN)
     CALL MULTI (VA.VEL.VCKIT, DCHIT, SDMIN, ICRIT, IDEP,
    1
         V+D+H4+EXM4K)
```

Tringate C CALCULATE SCALE FACTORS -C 42% ISCODEISCAL (SUMAX) ISCT = ISCAL (T-1+AX) ISC34=ISCAL (RAHAR) ISCEX=ISCAL(EXHAX) DO 552 J=1-3 Ĉ :C OUTPUT GRATICULE C CALL GRAT (INA-ETISCSD, DCRIT, LAYER, ISHAP) CALL DARK (628,644) CALL ALPHA IF (J-2) 432-462,492 432 #RITE (16+442) ISCTH 449 FORMAT ("THICKHESS SCALE =", IS," H/UNITH) CALL DARK (912, 15) CALL ALPHA WRITE(16+450) 45ë Forhat ("Triickvesse") GC TO 524 453 ##ITE (16,474) ISCRA 476 FORMAT ("RANGE SCALE =", IS, "A/UNIT") CALL 048K (412,15) CALL ALPHA WRITE(15,489) 439 FORMAT ("RANGE+") GO TO 520 499 SPITE (16+52%) ISCEX 500 FORMAT ("EATENSION SCALE =", 15," M/UNIT") CALL DERK (912,15) CALL ALPHA WRITE(16,518) 510 FORMAT ("EXTENSION") 529 STEP=(SUHAX-D3)/180. C C OUTPUT RESULTS С DC 550 I=1.1.44 SDEP=D%+FLOAT(1) #STEP IF (J-2) 525.539 525 IF (LAYER) 538,548 53% CALL THO (V%+VCHIT+UCRIT+SUEP+DØ+DTURN+VTURN+ 1 RA(I) • EX(I) • Tri) 60 TO 500 540 IF (SDEF-DTURN) 552,550 55% CALL FIVAL (U, V, SDEP, VEL, IDEP, ITURN, 1) CALL FIVAL (V.D. VEL, DEP. 19. M. ITURN) GO TO 570 560 CALL FIVAL (D.V. SDEP. VEL. IDEP. N. ITURN) CALL FIVAL (V,D, VEL . DEP, IJ, IN, ITURN) CALL FIVAL (D, V, DEP, VEL, 17. ITURN . 1) CALL FIVAL (V.D. VEL. DEP, 18, 17. ITURN) 57% CALL MULTI (VØ+VEL, VCRIT+DCHIT+SDEP, ICRIT, IDEP, V,D,

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15

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PASE STAS

```
1
          RA(I)=EX(I))
      THEDER
С
С
          CALCULATE CO-UNDIMATES FOR DISPLAY
  584 IF (J-2)592+524+610
                                           47 9 4 5 5 1 9 9
9 9 9 9 5 5 1 9 9
9 9 9 9 9 9 9 9 9
9 9 9 9 9 9
  594 [x=(T#/FLU4T([SCT=))*26#+23.
      60 TO 620
  5#2 [X=(44(1)/FLOAT(15C-A))#202.+23.
      GG TO 520
  612 IX=(Ex(I)/FLUAT(ISCEX))#24:+23.
  627 IY=531.-(592-/FL04)(ISCSD))#125.
      IF(I-2)630-041
  637 CALL DARK (IX, II)
      60 TO 550
  64% CALL BRIGH(IX-IY)
  65A CGATINE
      CALL HERDC
  667 CONTINUE
      CALL 04mk (30+331)
      CALL ALPHA
С
С
          RECUEST IF EXPANSION IS REQUIRED
С
      #PITE(16+574)
  67a FORMAT ("TO EXPAND FLOT PUSITION CURSUX AT MAXIMUM SOURCE "•
           "GEPTH REQUIRED AND TYPE 1"+/+32X+"OTHERMISE TYPE O")
     1
      CALL CURSI (ICHAR, IA.IY)
                                                               5
      IF (IC-12x-49)710+630
С
C
          CALCULATE HER MAXIMUM SOURCE DEPTH
С
  69# SDMAX=(631.-FLOAT(1Y))/120.*/LOAT(ISCSD)
      IF (5044A-UCX1146.45) 108,690
  690 SUMAX=0CHIT#0.95
  700 GU TO 300
  710 CALL ENASE
      CALL HUME
      60 10 1500
 С
С
С
          CALCULATION AND DISPLAY OF SHADDY ZONE SHAPE
С
  720 HRITE(1+180)
      READ(1+*)501+502+503
      IF (SU1-010-1-1.)730.14%
  730 SD1=0TUkri+1.
  740 IF (502) 752 . 750 . 160
  757 MX=1
      60 IU 705
  75# IF (SD3+501) 170,770,780
  770 41x=1
      Gú IU 705
  780 Mx=(503-501)/502+1.
С
```

PAGE 32:25

FIRD MAKINUM VALUES

```
Ĉ
С
  785 SEEP=S01
      CALL FIVAL (U.V.SDEP; VSDEP; ISDPT, N.; ITURN)
      CALL FIVAL (VODOVSDEPODMAXO 10100 ITURA)
      CALL FIVAL (DoVoDHAA, VIOII) ITURNOI)
      CALL FIVAL (V.D.VI.JUMAX, I.I.I.ITURN)
      DG 790 I=2.4
  799 C(I)=()(I)-0(I-1))*(v(I)+v(I+1))
      Z=()444-U+)/128.
      CALL DETES (2+DE+SULF, VSUEP, ISDPT, UMAX, IA, ITURH, N.
     1-
           CiD+ViUIST1iuIST2+RAU)
C.
C
           CALCULATE SCALE FACTORS
C
      ISCTH=ISCAL (JHAX)
      ISCRA=ISCAL(DIST2)
C
C
C
           OUTPUT GRATICULE
      CALL GRAT (INAME, ISCTH, DCRIT, LAYER, ISHAP)
      CALL DARK (6889544)
      CALL ALPHA
      WRITE (16,472) ISCRA
      CALL DARK (2.2)
      CALL ALPHA
      IF (NX-2)398+918
  89% MRITE(15+700)S01
  900 FOR MAT ("SOURCE DEPTH =""F6.1" HETERS +")
      60 TO 930
  912 #FITE (16, 920) S01, S03, SD2
  922 FORMAT ("SUURCE DEPTH =""F6.1" M TO""F6.1"
           " # IN STEPS UF", F6.1," M+")
     1
  930 CALL DARK (912,15)
      CALL ALPHA
      WRITE(16,480)
      DO 113% J=1. NX
С
С
           CALCULATE RESULTS
С
      S0E2=S01+FL0AT(J-1) #S02
      CALL FIVAL (D, V. SDEP, VSDEP, ISDPT, N. ITURN)
      CALL FIVAL (V, ). VSULP. DMAX. II. 10. ITURN)
      CALL FIVAL (D.V.JMAX.VI.II. ITURN.I)
      CALL FIVAL (V.O.VI.)MAX.IZ.II. ITURN)
       STED= (UMAX-D0)/100.
       Z0L01=9.
       ZOLJ2=1.
      RNE#1= ...
      RNE#2=1.E13
      RAD1=%.
      RAD2=%.
      00 1050 1=1.100
       Z=FLOAT(I) #STEP
       CALL Dr TPS (Z+DU+SDEP+VSDEP+ISDPT+UMAX+IU+ITURN+N+
           C+D+V+DIST1+DIST2+RAD)
      1
```

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	č	FIED HIGH POINTS TO RETAIN
	C	16/840:06.9-9-9-9-9-9-9-
	- 0a t	17 (76)[/ 7404747970
,	-740	
	05.4	E-17-220 011/2401
	334	2-12-20201// ##01 DAM25-2065-1424010232T/5812 -511
	064	
	959 07:5	
	212	
-	985	
	مد خير کر	
-		701.01=7
		RAD1=240
	99£	IF (RADZ) 1000+1010
	1370	RAMSE==NE#2
		GO TO 1828
	1912	E=(2-20L02)/RAD2
		RANGE=#XE#2-9402#5477(E#(2E))
	1959	IF (RANGE-UIST2) 1030, 1040
	1030	Ex(I)=aange
		60 TO 1252
	1942	R4E#2=0ISI2
		EX(1)=#1512
	1.655	KAUS-TAU Continue
	C 105%	
	Č	DISPLAY RESULTS
	С	
		00 125° I=1,100
		Z=FL04T(1)*STEP
		IA=(R=(I)/FLOAT(ISCRA))*200+23.
		IY=531(2/FLOAT(ISCTH))#120.
		IF (1-2) 126%, 1970
	1663	CALL DARR. (IX+IY)
	1474	
	1372	
	1000	
		1-121-11
		7=5101711
		TX = (FX(T)/F) (0 AT (TSCRA)) *2 AV + 23
		1x = 531 + (7/5) 041 (15010) + 120
	139%	CALL BEIGH(IK.IY)
	1100	CONTINUE
		CALL HARDC
		CALL ERASE
		CALL ALPHA
		CALL HOME
		GO TO 1500
	C	
	C ****	ፚኇኇኇዸኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇኇ
	C	
	L	REQUEST NEXT UPERATION

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1.5 K P F. 1. 1. 19

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C

1500 WRITE(1,1510)

1510 FORMAT("ITPE # TO REPROCESS: 1 TO PROCESS NEW DATA ",

1 "Or 2 TO STOP")

READ(1.4)1

IF(I-1)147.10.1520

1529 STOP

END
```

PAGE 1005

```
PAGE 2241
 FTHIL
 С
 С
            J.P. 22-11-71
 С
 С
            THIS IS THE FIRST SET OF SUBRUUTINES FOR THE
 С
        PPOGRA SHAZO
 С
        SUBROUTINE WULTI (VØ, VEL, VCKIT, DCRIT, SDEP, ICRIT, IDEP,
      1
            VOUORANGEOEXT)
       DIME ISIJN V(1) . J(1) . T(40)
 С
 С
            THIS SUEROUFINE CALCULATES THE RANGE AND EXTENSION OF
 С
       THE SHIDD& ZONE FOR THE NULTILAYER NODEL.
 С
       DCRI=D(IC-IT)
       (TIFJI)V=1HOV
       D0 10 I=<•ICHIT
    10 T(I) = S_{VK}T((V0 + V(I-1)) * (V0 - V(I-1))) + SQRT((V0 + V(I)) * (V0 - V(I)))
       DEP1=J(IUEP)
       VEL1=V(1DEP)
                                        Reproduced Irom
best available copy.
С
С
           CALCULATE EXTENSION
С
       IF (DEP1-UCFI) 20,30
    27 I=IDEP+1
       DEP2=D(I)
       VEL2=V(1)
       S=SJ~T((V0+VEL)*(V0-VEL))+SQRT((V0+VEL2)*(V0-VEL2))
       EXT=(DEP2-SDEP)*(VEL+VEL2)/S
       S=SQRT((V&+VCRI)*(V&-VCRI))
       EXT=EXT+(UCRIT-DCRI)*(VCRIT+VCRI)/S
       GU TO 40
   30 EXT=()CPIT-SUEP)*(VCRIT+VEL)/SORT((V0+VEL)*(V0-VEL))
   40 IF (DEP2-UCH1)50.70
   50 I1= IDEP+2
       DO 50 [=11,ICRIT
   60 EXT=EXT+(D(I)-U(I-1))*(V(I)+V(1-1))/T(I)
   70 EXT=EXT#2.
С
С
           CALCULATE RANGE
С
      S=SQRT((V0+VEL1)*(V0-VEL1))+SQRT((V0+VEL)*(V0-VEL))
      RA 13==(SULP-UEP1)*(VEL+VEL1)/S
      00 50 1=2, IUEP
   80 RANGE=-ANGE+(0(I)-0(I-1))*(V(I)+V(I-1))/T(I)
      RETUR.
      END
С
```

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1.1

```
SUBROUTINE THO (VM. VCHIT. DCRIT, SDEP. DØ, DTURN,
     1
           VTURN+PANGE+EXT+THICK)
С
С
           THIS SUBROUTINE CALCULATES THE RANGE, EXTENSION AND
С
      THICANESS OF THE SHAUDW ZONE FOR THE 2 LAYER MODEL.
С
      IF (DTJen-SUEP) 10.20
   10 VEL=VTURN+ (VCRII-VIURN) * (SUEP-DTURN) / (DCRIT-DTURN)
      S=SORT((V&+VEL)*(V&+VEL))
      EXT=2.*(UCFIT-SUEP)*(VCRIT+VEL)/S
      S=S+S2+T((V&+VTURA)*(VO-VTURN))
      PANGE=(SDEP-DTURN)*(VTURN+VEL)/S
      RANGE=FANGE+DTURN*(V#+VTURN)/SQRT((V#+VTURN)*(V#+VTURN))
      THICK=D0+(DTURN-D0)*(V0-VEL)/(V0-VTURN)
      GC TO 30
   20 VEL = VTURN+ (VO-V (UKN) * (SDEP-DTURN) / (DO-DTURN)
      S=SQRT((v_{\ell}+v_{UKN})*(v_{UKN}))
      RANGE=SDEP*(V0+VEL)/S
      EXT=2.*(UCRIT-DTURN)*(VCRIT+VTURN)/S
      S=S+SQPT((V0+VEL)*(V0-VEL))
      EXT=EXT-2.*(SDEP-UTURN)*(VEL+VTURN)/S
      THICK=DTURN+(DCRIT-DTURN)*(VEL-VTURN)/(V0-VTURN)
   30 RETURN
      END
                     Reproduced From
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С
С
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PAGE DWD3
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```
SUBROUTINE BTRAN(V.D.N.S.PHI)
      DIMENSION V(1).D(1)
С
С
           THIS SUBROUTINE CALCULATES THE SOUND VELOCITIES V(I)
С
      AT DEPTHS D(I) FROM THE TEMPERATURE VALUES INITIALLY
С
      STORED IN ARRAY V. S IS THE SALINITY AND PHI THE
С
      LONGDITUUE
С
      DO 10 I =1+iv
      V(I) = 1 + 93 + 3 + 4 (V(I) - 10 + ) - 0 + 006 + (V(I) - 10 + ) + (V(I) - 10 + )
           -2.34*(v(I)-18.)*(v(I)-18.)+1.2*(S-35.)-0.01*
     1
           (V(I)-18.)*(S-35.)+D(I)/61.+1.E-7*D(I)*D(I)
     2
           +2.E-1/*U(I)*U(I)*(V(I)-18.)*(V(I)-18.)+1.E-4*
     3
           Ŋ(I) * - HI/ → 2. oE - 4*V(I) * (V(I) - 5.) * (V(I) - 25.)
   10 CONTINE
      RETJAN
      END.
С
С
```

PAGE #304

•

```
SUBROUTINE FINTP(V+V+ITUKA)
      DIMENSION V(1)
C
C
           THIS SUBROUTINE FINDS THE MINIMUM ELEMENT OF
C
C
      APRAY V AND PLACES ITS SUFFIX IN LOCATION ITURN
      VMIN=V(1)
      00 2% I=2,N
      IF (V(I)-V#14)10,20
   10 V~IN=V(I)
      IMIN=I
   20 CONTINUE
      ITURN=IAIN
      RETURN
      END
С
С
PAGE 0005
      SUBROUTINE FIVAL (A, B, VALUE, RESLT, ISSCK, N1, N2)
      DIMENSION A(1), B(1)
С
Ċ
           THIS SUBROUTINE FINDS THE VALUE IN ARRAY B WHICH
С
С
С
      CORRESPONDES TO "VALUE" IN ARRAY & AND PLACES IT IN
      RESLT. NI AND N2 ARE THE LIMITS OF THE ARRAY SUBSCRIPTS
      SO ARRANGED THAT NO IS THE SUBSCRIPT OF THE LARGEST
Ċ
      VALUE OF A.
С
      N=IABS(N1-N2)
      IF (N1-M2)10+20
   10 INCR=1
      GO TO 30
   20 INCR=-1
   30 06 50 11=1+N
      I=N1+INCK*I1
       J=I-INCR
      IF (VALUE-A(I)) 50+40
   40 DEL=(VALUE-A(I)) '(A(J)-A(I))
      \mathsf{RESLT} = \vdash (I) + \mathsf{DEL}^* (\exists (J) - \exists (I))
       ISSCR=I
      GO TO 60
```

50 CONTINUE

PAGE - 1-1

FT:s+	L	· · · · · · · · · · · · · · · · · · ·
C		J 27-13-11
		THIS IS THE SECOND SET OF SUBROUTINES FOR THE PRUGRA. SHAZO
c		SUBPOUTINE GRAT(INAME+ISCSUNDCRITHLAYER+ISHAP) DINE BIG - INAME(I)
		THIS SUBROUTINE PRODUCES THE BASIC GRATICULE FOR GRAPHIC DISPLAYS.
C		CALL ETASE
1	10	CALL HOME WRITE(15,17) ED24AI(1)
	•	C4L_ CHUBL
2		
2	. // 153	$F(r_{1}, r_{2}, r_{3}, \eta \in \eta)$
4	5	WFITE(16,55)(INAME(1),I=1,6)
5	5	FORMAT(12x+"X & T ",6(X,A1),"+")
		IF (LAYER) 50 + 80 + 100
6	8	WRITE (16,70)
7	0	$FORMAT(22x \cdot T + 0) = L + Y + R^{H}$
		GO TO 12/
ć	30	$WRITE(15\cdot y^{2})$
9	19	
1.0		
11	1901 1 A	THELEVIDELLOV ENJART/22/JHM JEET TELAY E DHY
12	5 A	
13	30	FORMAT (/ 27/ "CRITICAL DEPTH =""Fd.2" METRED")
	-	IF(IS-1P)1+2+160
14	Ψ	WRITE(16+150)
15	52	FORMAT (5X+"SOURCE +")
		GU TU 180
14	5Ø	WPIIE(15,176)
1 /	9	
17	Σγ Σúπ	971728754197715050 Framatynafoth scale - Hatsan Mzunith)
13	77	$(A \cup A \cup$
		$CAL' = Br(G^{-}(23 \cdot 31))$
		CALL 3+16m(1023,31)
		CALL 3HIGH (1023+631)
		CALL 9-16m(23.631)
		212 I=223+223+224
		CALL DARK (I-31)
		CALL = 3RIGH(1.53)
a .	A . A	
27	(V ()	
2	1 N	CALL = SPR((1 + n 3))
. <u>سا</u>	•	DO 232 I=151,511,120

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PAGE みぞう2

3

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2

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1

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i

•	-	CALL DARK (23+1)
		CALL 3-(100(55.1)
		00 224 J=87.991.15
	221	
:	224	
	23%	CALL SHIGH(1023+1)
		CALL 04xk (7+031)
		CALL ALPHA
		#RIFE(16+240)
	240	F0294T(###**//)
		IF (ISHAP) 250+270
	250	#PITE(15+25%)
	260	FOR AAT ("Sa/"U"/"U"/"R"/"C"/"F"?)
	27:	##ISF(15+28A)
	280	F02441(40#/474/404/474/444)
		REIJAN
		END
С		
С		
•		

PAGE viz 13

i

:

FUNCTION ISCAL (RAMAX) DI JENSIUN ISC(3) , XMAX(3) C 1 C 1 C THIS FUNCTION TAKES THE NEXT VALUE ABOVE RAMAX FROM 1 THE SEVILS 1+10++W, 2+10++N, 5+10++N WHERE N=1,2,3..... ISC(1)=1 ISC(2)=2 ť I5C(3) = 5XMAX(1)=5. XMAX(2)=10. XMAX(3)=20. 10 00 32 1=1.3 IF (XMAX(I)-RAMAX) 30,20 20 ISCAL=ISC(I) GO TO 50 30 CONTINUE DO 40 I=1+3 ISC(I) = 1c * ISC(I)40 XMAX(I)=10.*XMAX(I) 60 TO 10 50 RETURN END C C

40

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in the second second second second second second second second second in the second second second second second

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SU-PT)FIFE U+T+3(Z+SUEP,JSUEP,ISUPT+DMAX,IØ,ITURN,N,
         C.C., V.UISTINISTERAD)
     1
      01 < E \S 10 < C(1) + 0(1) + V(1)
С
С
          THIS SUBROUTINE CALCULATES THE DISTANCES TO THE
С
      VENTERES OF HAYS BRICH VORTEX AT A DEPTH Z AND ALSO
С
      THE RAPIUS OF THE WAYS AT THESE PUINTS
С
      С
С
          FIND VELOCITY AT DEPTH Z ETC.
С
      DS)?[=0(150PT)
      ¥50-T=+(150-T)
      CALL FIVAL (U+V+Z+SK+1ZPT+1TUK++10)
      IZPT=17PT+1
      DZPI=0(IZPI)
      VZPT= y(1ZPT)
С
С
          SK=SMELLS CONSTANT FUR THE RAY
С
      CALL FI ME(/+)+ST+ULZ+ILZPT+N+ITURN)
      ULZPT=0(ILZPT)
      VLZ^{2T=y}(ILZ^{2T})
С
С
          FIND THE DISTANCE TO THE FIRST FURNING POINT
С
      DIST1='.
      IF (1. E-4- 182E2+ 182ri) 3,1
    3 DISTI=(SUEF-USDPT) * (VSDEP+VSDPT)/(RSU(SK+VSDPT)+RSQ(SK+VSDEP))
    7 IF (ISDPT-IZPT) 10,30,10
   11 2=1237-1
      14021.FI (5 00
      IF (SK-1(1-1))17+13
   13 IF (SK-/(I))17.20
   17 DISTI= .
      DIST2=1.E1#
      GO TO 140
   20 DISTI=DISTI+C(I)/(KSQ(SK+V(I-1))+KSQ(SK+V(I)))
   30 IF(1.E-4-5K+VZPT)40.45
   4. 01571=015f1+(02PT-Z)*(VZPT+5K,/RSQ(SK,VZPT)
С
С
          FIND THE DISTANCE TO THE SECOND TURNING POINT
С
   45 IF (Z-)MAX162.50
   57 DIST2=UIST1
      GO TO 140
   60 IF ()L2+U(15U2F+1))70+90
   70 IF (1.E-4-5K+VSDEP) 80.140
   80 DIST2=UIST1+2.*(ULZ-SUEP)*(SK+VSDEP)/(RSQ(SK+VSDEP))
      GO TO 140
   90 DIST2=UIS(1+2.*(D(ISUPT+1)-SDEP)*(V(ISUPT+1)+VSDEP)/
          (RSQ(SK+V(ISDPT+1))+RSQ(SK+VSDEP))
     1
      IF (ILZ-T-150PT-1)100+122+100
  100 J=ISDP1+2
      DO 112 I=J.ILZPT
```

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PAGE Reas
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and a start and the start and a start a start a sta

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11# DIST2=01ST2+2.*C(1)/(RSQ(SK+V(I-1))+RSG(SK+V(I)))-

12# IF(1.E+4+5X+VLZPT)13#+14#

13# DIST2=01ST2+2.*(DL2+DLZPT)*(SK+VLZPT)/RSQ(SK+VLZPT)

C CALCULATE RADIUS AT TURNING POINTS

C 14# RAD=5<*(D2+T+D(1ZPT+1))/(V(1ZPT+1)+V2PT)

RETURN

END
```

.

*