

AD 748655

A FORTRAN PROGRAM FOR CALCULATING THE FREQUENCIES AND
MODE SHAPES OF AN ARBITRARY SHAPE CYLINDRICAL TYPE
SHELL BY UTILIZING A FINITE ELEMENT SOLUTION

BY
GEORGE GEORGOPoulos
DEPARTMENT OF MECHANICAL AND AEROSPACE ENGINEERING
CENTER FOR ACOUSTICAL STUDIES
NORTH CAROLINA STATE UNIVERSITY
RALEIGH, NORTH CAROLINA



LARRY H. ROYSTER
DEPARTMENT OF MECHANICAL AND AEROSPACE ENGINEERING
CENTER FOR ACOUSTICAL STUDIES
NORTH CAROLINA STATE UNIVERSITY
RALEIGH, NORTH CAROLINA

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This report describes a Fortran IV program capable of obtaining a finite element numerical solution to the free axisymmetric vibrations of a cylindrical type shell of arbitrary shape.

14. KEY WORDS	LINK A		LINK B		LINK C	
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ABSTRACT

This report describes a Fortran IV program capable of obtaining a finite element numerical solution to the free axisymmetric vibrations of a cylindrical type shell of arbitrary shape.

INTRODUCTION

Present flexensional designs may be grouped into one of five different classes (1). In order to derive a mathematical model for any of the above mentioned flexensional transducers, it is essential to determine the vibrational characteristics of the shell itself. A finite difference approach for each shell's dynamic response has been investigated at the Center for Acoustical Studies in the Department of Mechanical and Aerospace Engineering at North Carolina State University. An attempt in improving the widely used finite difference method led to the present investigation of the finite element method which is widely used in determining stresses and strains in Aerospace Research and Development.

The program utilizes a finite element analytical model to calculate the total Mass and Stiffness matrices of an arbitrary shape cylindrical type shell (2). After the total Mass and Stiffness matrices are calculated, displacement boundary conditions are introduced by removing appropriate rows and columns corresponding to points of the shell which are rigidly restrained from motion. Finally, subroutine NROCT is used for the numerical solution of the shell's free axisymmetric vibration matrix equation, and the eigenvalues, frequency coefficients, natural frequencies, and eigenvectors are then printed out.

PROGRAM UTILIZATION

The program is written in Fortran IV (G or H level) to be used on an IBM 370/165 computer. The storage capacity required depends upon the number of finite elements desired. As an example, the sample program presented in this paper having a total number of 6 elements requires a storage of 100 K for the evaluation of the stiffness and mass matrices of each element. These numbers are stored on a disk. In addition, a storage of 160 K, together with a time parameter of $2\frac{1}{2}$ minutes is required for the main program for a complete run. A typical element geometry and coordinate notation is given in figure 1. A geometrical element assembly is given in figure 2.

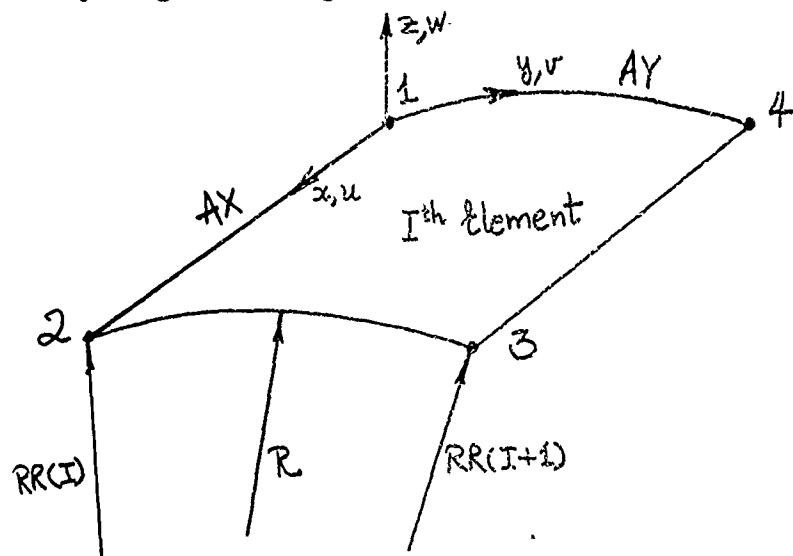


Figure 1. Individual finite element.

$$R = RR(I) + (RR(I+1) - RR(I)) \frac{y}{AY}$$

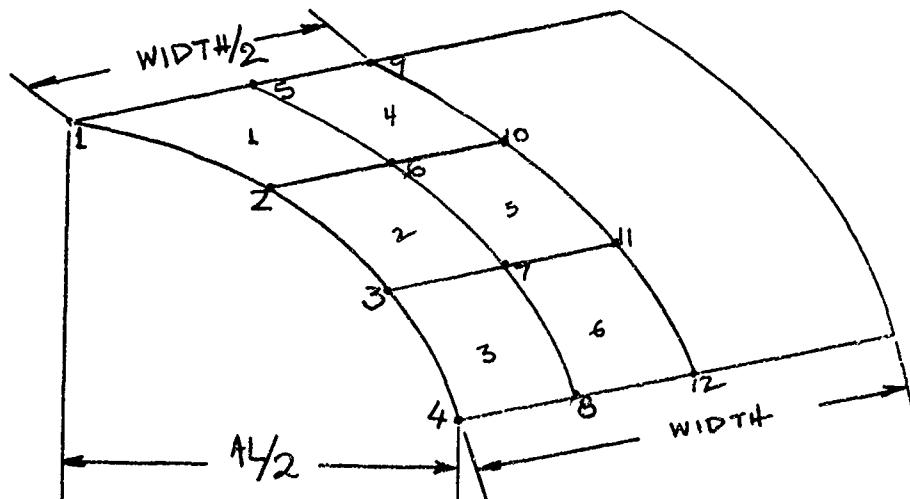


Figure 2. Finite element assembly of a shell.

Displacement vector δ_i per node is given as follows:

$$\delta_i = u_i, v_i, w_i, \frac{\partial u_i}{\partial x}, \frac{\partial v_i}{\partial x}, \frac{\partial w_i}{\partial x}, \frac{\partial u_i}{\partial y}, \frac{\partial v_i}{\partial y}, \frac{\partial w_i}{\partial y}$$

The program presented in Appendix A was written for the Class IV flexextensional transducer shell, but it can be easily changed so it can be used for the case of any other similar type shell. Before using this particular program, it must be noted that all element stiffness and mass matrices are evaluated outside the main program. Then they are put on a disk from which the main program picks them up for total mass and stiffness formulation and final dynamic solution. It is necessary to use proper JCL cards. The program instruction in Appendix A must be read very carefully before running the program. A set of data cards is needed for the element notation and final mass and stiffness formulation. The program presented in Appendix A was written for figure 1. element notation and figure 2. element combination. All elements to form data for set 1. must be numbered according to figure 1 and figure 2.

ELEMENT NO. 1	5	1	2	6	{	SET 1
ELEMENT NO. 4	9	5	6	10		
ELEMENT NO. 2	6	2	3	7		
ELEMENT NO. 5	10	6	7	11		
ELEMENT NO. 3	7	3	4	8		
ELEMENT NO. 6	11	7	8	12		

The boundary conditions are:

$$\begin{aligned} w_{y_i} &= 0 & i = 1, 4, 5, 8, 9, 12 \\ v_i &= 0 & i = " \\ v_{x_i} &= 0 & i = " \\ u_i &= 0 & i = 9, 10, 11, 12 \\ w_{y_i} &= 0 & i = " \\ w_{x_i} &= 0 & i = " \end{aligned}$$

These are applied to the corresponding vector index notation

	u	v	w	v_x	v_y	w_x	w_y	v_y	w_y
Node 1	1	②	3	4	⑤	6	7	8	⑨
Node 2	10	11	12	13	14	15	16	17	18
Node 3	19	20	21	22	23	24	25	26	27
Node 4	28	②	30	31	③	33	34	35	④
Node 5	37	③	39	40	④	42	43	44	⑤
Node 6	46	47	48	49	50	51	52	53	54
Node 7	55	56	57	58	59	60	61	62	63
Node 8	64	⑤	66	67	⑥	69	70	71	⑦
Node 9	⑦	⑧	75	76	⑨	⑩	⑪	⑫	⑬
Node 10	⑧	⑨	84	85	86	⑩	⑪	89	90
Node 11	⑨	92	93	94	95	⑩	⑪	98	99
Node 12	⑩	⑪	102	103	⑫	⑬	⑭	107	108

Therefore Set 3, corresponding to the total number of the above mentioned 30 boundary conditions (NBC=30), is easily formed as follows:

2 - 5 - 9 - 20 - 32 - 36 - 38 - 41	}	SET 3
45 - 65 - 68 - 72 - 73 - 74 - 77 - 78		
79 - 81 - 82 - 87 - 88 - 91 - 96 - 97		
100 - 101 - 104 - 105 - 106 - 108		

In order to form Set 2, the vector index notation is used again, but the circled numbers that correspond to the boundary conditions are omitted.

Therefore, the vector index notation is as follows

Node 1	1	-	(2)	3	-	(4)	5	6	-
Node 2	(7)	8	9	10	11	12	13	14	15
Node 3	16	17	18	19	20	21	22	23	24
Node 4	25	-	(26)	27	-	(28)	29	30	-
Node 5	(31)	-	(32)	33	-	(34)	35	36	-
Node 6	(37)	38	39	40	41	42	43	44	45
Node 7	46	47	48	49	50	51	52	53	54
Node 8	55	-	(56)	57	-	(58)	59	60	-
Node 9	-	-	(61)	62	-	-	-	(63)	-
Node 10	-	(64)	65	66	-	-	-	(68)	69
Node 11	-	(70)	71	72	73	-	-	(74)	75
Node 12	-	-	(76)	77	-	-	-	(78)	- (79)

Then Set 2 is formed as follows:

2 - 4 - 7 - 26- 28- 31- 32- 34
37- 56- 58- 61- 61- 61- 63- 63
63- 64- 64- 68- 68- 70- 74- 74
76- 76- 78- 78- 78- 79

} SET 2

Then the date cards consist of Set 1- Set 2- Set 1- Set 3 in that order.

Furthermore if a coordinate transformation is desired, then matrix AKL (I,J),
card MAIN 85, should be assigend properly and also cards DISK 27 and MAIN
266, 267, 268 should be removed from the program. In addition, card MAIN 54
should be equal to 1.

FINAL REMARKS

A 5 point numerical integration is carried out for each element's stiffness and mass matrix by using abscissas and weight functions of Legendre polynomials. After combining all the individual stiffness and mass matrices and introducing boundary conditions, the equation of motion for the shell is written as follows:

$$[[K] - \lambda [M]] \{ \delta \}^e = \{ O \}$$

where

$[K]$ = Total stiffness matrix

$[M]$ = Total mass matrix

$\{ \delta \}^e$ = Nodal vector

$$\lambda = E / (2 \cdot RHO \cdot (1 - POISS^2) \cdot \omega^2)$$

RHO = Density

E = Modulus of Elasticity

POISS = Poisson's Ratio

Since subroutine NROOT is used to determine λ , the largest λ is determined first, and as a result, the lowest natural frequency is calculated first and so is the corresponding eigenvector.

REFERENCES

1. Larry H. Royster, "The Flextensional Concept: A New Approach to the Design of Underwater Transducers", Center for Acoustical Studies, Department of Mechanical and Aerospace Engineering, North Carolina State University, Raleigh, N. C., September, 1969.
2. Georgopoulos, George and L. H. Royster, "Development of a Finite Element Model for the Class IV Flextensional Underwater Transducer Shell", Technical Report No. 23, Department of Mechanical and Aerospace Engineering, North Carolina State University, Raleigh, N. C., September, 1972.

APPENDIX A

```

DIMENSION AKK(36,36)
C
C      AKK(NF,NF)          OF FREEDOM PER ELEMENT
C      NF=DEGREES OF CURVILINEAR COORDINATES
C      MF=NUMBER OF ELEMENTS IN X-DIRECTION (WIDTH)
C      NM=NUMBER OF ELEMENTS IN Y-DIRECTION (WIDTH)
C      NELEM=NUMBER OF ELEMENTS
C      POISS=POISSON'S RATIO
C      THICK=THICKNESS (IN)
C      AX=LENGTH OF THE ELEMENT IN X-DIRECTION (IN)
C      AY=LENGTH OF THE ELEMENT IN Y-DIRECTION (IN)
C      MF=3
NF=3.6
NM=2
NELEM=6
IJ=NELEM/NM
AX=0.75
AY=1.542
THICK=0.4
POISS=0.334
NAK=0
1 NAK=NAK+1
DO 2 I=1,IJ
CALL GSLGN(NAK,I,MF,NF,AX,AY,THICK,POISS,AKK)
WRITE(8,3) ((AKK(I1,J1),I1=1,NF),J1=1,NF)
3 FORMAT(/,4E15.7)
2 CONTINUE
IJ=1
IF (NAK.EQ.1) GO TO 1
CALL EXIT
END

```

12

SUBROUTINE GSLGN(NAK,I,MF,NF,AX,AY,THICK,POISS,AKK)

GSLG 1

```

DIMENSION AKK(36,36),AKL(36,36),AKM(36,36),BF(36,36),AA(5),H(5),RRGSLG
1(4)                                              2
C   AKK(NF,NF)                                     GSLG  3
C   AKL(NF,NF)                                     GSLG  4
C   AKM(NF,NF)                                     GSLG  5
C   BF(NF,NF)                                      GSLG  6
C   AA(NX)                                         GSLG  7
C   H(NX)                                         GSLG  8
C   RR(I,MAX+1)                                    GSLG  9
C   IF NAK=1 THEN AKK(NF,NF)=STIFFNESS           GSLG 10
C   IF NAK=2 THEN AKE(NF,NF)=MASS                GSLG 11
C   D=E/(2*RHO*(1.0-POISS*POISS))               GSLG 12
C   RR(I)=RADIUS OF CURVATURE AT I TH NODE      GSLG 13
C   (IN), DIMENSION OF RR(I)=                   GSLG 14
C   NUMBER OF ELEMENTS IN Y-DIRECTION+1          GSLG 15
C   RR(1)=4.79                                     GSLG 16
C   RR(2)=4.3                                     GSLG 17
C   RR(3)=3.50                                     GSLG 18
C   RR(4)=1.90                                     GSLG 19
C   R1=RR(I)                                       GSLG 20
C   R2=RR(I+1)                                     GSLG 21
C   NX=5                                           GSLG 22
C   NY=5                                           GSLG 23
C   NZ=5                                           GSLG 24
C   AA(1)=-0.90618                                GSLG 25
C   AA(2)=-0.538469                               GSLG 26
C   AA(3)=0                                         GSLG 27
C   AA(4)=0.539469                                GSLG 28
C   AA(5)=0.99618                                GSLG 29
C   H(1)=0.236927                                GSLG 30
C   H(2)=0.478629                                GSLG 31
C   H(3)=0.568889                                GSLG 32
C   H(4)=0.478629                                GSLG 33
C   H(5)=0.236927                                GSLG 34
C   X1=0                                           GSLG 35
C   X2=1                                           GSLG 36
C   Y1=0                                           GSLG 37

```

```

Y2=1
Z1=-THICK/2.0
Z2=THICK/2.0
IF (NAK.EQ.2) GO TO 10
DO 1 J1=1,NF
DO 1 I1=J1,NF
AKK(I1,J1)=0
CONTINUE
DO 2 KL=1,NZ
Z=AA(KL)*(Z2-Z1)/2.0+(Z2+Z1)/2.0
DO 3 J1=1,NF
DO 3 I1=J1,NF
AKL(I1,J1)=0
CONTINUE
DO 4 K=1,NY
Y=AA(K)*((Y2-Y1)/2.0+(Y2+Y1)/2.0
DO 5 J1=1,NF
DO 5 I1=J1,NF
AKM(I1,J1)=0
CONTINUE
DO 6 L=1,NX
X=AA(L)*((X2-X1)/2.0+(X2+X1)/2.0
CALL FSTIF(MF,NF,AX,AY,PDIS,S,R1,R2,X,Y,Z,BF)
DO 7 J1=1,NF
DO 7 I1=J1,NF
AKM(I1,J1)=AKM(I1,J1)+H(L)*GF(I1,J1)
CONTINUE
DO 8 J1=1,NF
DO 8 I1=J1,NF
AKL(I1,J1)=AKL(I1,J1)+H(K)*AKM(I1,J1)
CONTINUE
DO 9 J1=1,NF
DO 9 I1=J1,NF
AKK(I1,J1)=AKK(I1,J1)+H(KL)*AKL(I1,J1)
CONTINUE
GSLG 38
GSLG 39
GSLG 40
GSLG 41
GSLG 42
GSLG 43
GSLG 44
GSLG 45
GSLG 46
GSLG 47
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GSLG 67
GSLG 68
GSLG 69
GSLG 70
GSLG 71
GSLG 72
GSLG 73

```

```

9    CONTINUE
2    CONTINUE
   GO TO 20
10   DO 11 I1=J1,NF
     DO 11 I1=J1,NF
       AKK(I1,J1)=0
11    CONTINUE
   DO 12 K=1,NY
     Y=AA(K)*(Y2-Y1)/2.0+(Y2+Y1)/2.0
   DO 13 J1=1,NF
     DO 13 I1=J1,NF
       AKL(I1,J1)=0
13    CONTINUE
   DO 14 L=1,NX
     X=AA(L)*(X2-X1)/2.0+(X2+X1)/2.0
     CALL FNASS(MF,NF,AX,AY,R1,R2,X,Y,BF)
   DO 15 J1=1,NF
     DO 15 I1=J1,NF
       AKL(I1,J1)=AKL(I1,J1)+H(L)*BF(I1,J1)
15    CONTINUE
14    CONTINUE
   DO 16 J1=1,NF
     DO 16 I1=J1,NF
       AKK(I1,J1)=AKK(I1,J1)+H(K)*AKL(I1,J1)
16    CONTINUE
12    CONTINUE
20   DO 19 I1=I1,NF
     DO 19 J1=I1,NF
       AKK(I1,J1)=AKK(I1,J1)+H(K)*AKL(I1,J1)
19    CONTINUE
      RETURN
     END

```

```

SUBROUTINE FSTIF(MF,NF,AX,AY,POISS,R1,R2,X,Y,Z,BF)
DIMENSION DD(3,3),BR(3,36),BD(36,3),RF(36,36)
C
C     BR(MF,NF)
C     DD(MF,MF)
C     BD(MF,MF)
C     RF(NF,NF)
C
C     DD(MF,MF)=E/(1.0-POISS*POISS)*DD(MF,MF)
C     STIFF(NF,NF)=E/(1.0-POISS*POISS)*1/2*THICK*AX*AY*BF(NF,NF)
C
C     R=21+(R2-R1)*Y
C     DR=(R2-R1)/AY
C     DD(1,1)=1
C     DD(1,2)=POISS
C     DD(1,3)=0
C     DD(2,1)=POISS
C     DD(2,2)=1
C     DD(2,3)=0
C     DD(3,1)=0
C     DD(3,2)=0
C     DD(3,3)=(1.0-POISS)/2.0
C     BB(1,1)=(-Y-6*X+6*X*Y+3*X*Y*6*X*Y+6*X*X*Y-6*X*X*Y-2*X*Y*Y)/AY
C
C     BB(2,1)=(-X-6*Y+3*X*Y+6*X*Y+6*Y*Y-2*X*X*Y-6*X*Y)/AY
C     BB(1,2)=0
C
C     BB(2,2)=(1.0+Z/R)*(-X-6*Y+3*X*X+6*X*Y+6*Y*Y-2*X*X*Y-6*X*Y)/AY-Z*STIF
C     10R*(1.0-X*Y-3*X*X-3*Y*Y+3*X*X*Y+3*X*Y*Y+2*X*X*Y+2*X*Y*Y-2*X*X*Y-Y-STIF
C     12*X*Y*Y)/((R*R))
C
C     BB(3,2)=(1.0+2*Z/R)*(-Y-6*X+6*X*Y+3*X*Y+6*X*X*Y-6*X*X*Y-2*X*Y*Y)/AX
C     BB(1,3)=-6*Z*(-1.0+Y+2*X-2*X*Y)/(AX*AX)
C     BB(2,3)=(1.0-C-X*Y-3*X*X-3*Y*Y+3*X*X*Y+3*X*Y*Y+2*X*X*Y+2*X*Y*Y-2*X*X*Y*STIF
C     1*X*Y-2*X*Y*Y)/R-6*Z*(-1.0+C+X+2*Y-2*X*Y)/(AY*AY)
C     BB(3,3)=-2*Z*(-1.0+6*X*Y-6*X*X*Y-6*X*Y)/(AX*AY)
C
C     BB(1,4)=1.0-Y-4*X+4*X*Y+3*X*X-3*X*X*Y
C     BB(2,4)=0
C     BB(3,4)=(-X+2*X*X-X-X*X*X)*AX/AY
C     BB(1,5)=0

```

```

36
1X*Y+X*X*X*X*X*/(R*R) * (-X+2*X*X-X*X*X) * AX/AY - Z*AX*DR* (X-X*Y-2*X*X+2*X*X*STIF STIF 37
BB(3,5)=(1.0+2*Z/R)*(1.0-Y-4*X+4*X*Y+3*X*X-3*X*X*Y) STIF 38
BB(1,6)=-Z*(-4.0+4*Y+6*X-6*X*Y)/AX STIF 39
BB(2,6)=AX*(X-X*Y-2*X*X+2*X*X*X*Y+X*X*X-X*X*X*Y)/R STIF 40
BB(3,6)=-2*Z*(-1.0+4*X-3*X*X)/AY STIF 41
BB(1,7)=AY*(-Y+2*Y*Y-Y*Y)/AX STIF 42
BB(2,7)=0 STIF 43
BB(3,7)=1.0-X-4*Y+4*X*Y+3*Y*Y-3*X*Y*Y STIF 44
BB(1,3)=Q STIF 45
BB(2,8)=(1.0+Z/R)*((1.0-X-4*Y+4*X*Y+3*Y*Y-3*X*Y*Y)-Z*AY*DR*(Y-X*Y-2*STIF 46
1*Y+2*X*Y*Y+Y*Y-Z*X*Y*Y)/(R*R) STIF 47
BB(3,8)=AY*(1.0+2*Z/R)*(-Y+2*Y*Y-Y*Y)/AX STIF 48
BB(1,9)=0 STIF 49
BB(2,9)=AY*(Y-X*Y-2*X*Y*Y+2*X*Y*Y+Y*Y*Y-X*Y*Y)/R-Z*(-4.0+4*X+6*Y-6*STIF 50
1*X*Y)/AY STIF 51
BB(3,9)=-2*Z*(-1.0+4*Y-3*X*Y*Y)/AX STIF 52
BB(1,10)=(Y+6*X-6*X*Y-3*X*Y-6*X*X+6*X*X*Y+2*X*Y*Y)/AX STIF 53
BB(2,10)=0 STIF 54
BB(3,10)=(X-3*X*X-X-6*X*Y+2*X*X*X+6*X*Y*Y)/AY STIF 55
BB(1,11)=0 STIF 56
BB(2,11)=(1.0+Z/R)*(X-3*X*X-6*X*Y+2*X*X*X+6*X*Y*Y)/AY-Z*DR*(X*Y+3*STIF 57
1*X*-3*X*X*Y-3*X*X*Y-2*X*X*X+2*X*X*X*Y+2*X*X*Y)/(R*R) STIF 58
BB(3,11)=(1.0+2*Z/R)*(Y+6*X-6*X*Y-3*X*Y-6*X*X+6*X*X*Y+2*X*Y*Y)/AX STIF 59
BB(1,12)=-6*Z*(1.0-Y-2*X*X*Y)/(AX*AX) STIF 60
BB(2,12)=(X*Y+3*X*X-X-3*X*X*Y-3*X*X*X+2*X*X*X*Y+2*X*Y*Y)/RSTIF 61
1-6*Z*(-X+2*X*Y)/(AY*AY) STIF 62
BB(3,12)=-2*Z*(1.0-6*Y+6*X*Y)/(AX*AY) STIF 63
BB(1,13)=-2*X*Y+3*X*X-3*X*X*Y STIF 64
BB(2,13)=0 STIF 65
BB(3,13)=(X*X*X*X)*AX/AY STIF 66
BB(1,14)=0 STIF 67
BB(2,14)=(1.0+Z/R)*(X*X-X*X*X)*AX/AY-Z*AX*DR*(-X*X+X*X*X*Y+X*X*X*X*Y) STIF 68
1*X*Y)/(R*R) STIF 69
BB(3,14)=(1.0+2*Z/R)*(-2*X+2*X*Y+3*X*X-3*X*X*Y) STIF 70
BB(1,15)=-2*Z*(-1.0+Y+3*X-3*X*Y)/AX STIF 71

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BB(2,15)=(-X*X+X*Y+X*X*X-X*X*Y)*AX/R          STIF 72
BB(3,15)=-2*Z*(2*X-3*X*X)/AY                      STIF 73
BB(1,16)=(Y-2*Y*Y+Y*Y*Y)*AY/AX                  STIF 74
BB(2,16)=0                                         STIF 75
BB(3,16)=X-4*X*Y+3*X*Y*Y                      STIF 76
BB(1,17)=0                                         STIF 77
BB(2,17)=(1.0+Z/R)*(X-4*X*Y+3*X*X*Y)-Z*AY+DR*(X*Y-2*X*Y*Y+X*Y*Y)STIF 78
1/(R*q)                                           STIF 79
BB(3,17)=(1.0+2*Z/R)*(Y-2*Y*Y+Y*Y)*AY/AX      STIF 80
BB(1,18)=0                                         STIF 81
BB(2,18)=(X*Y-2*X*Y*Y+X*Y*Y)*AY/R-Z*(-4*X+6*X*Y)/AY  STIF 82
BB(3,18)=-2*Z*(1.0-4*Y+3*Y*Y)/AX              STIF 83
BB(1,19)=(-Y+6*X*Y+3*X*Y-6*X*X*Y-2*Y*Y*Y)/AX  STIF 84
BB(2,19)=0                                         STIF 85
BB(3,19)=(-X+3*X*X+6*X*Y-2*X*X*X*-6*X*Y*Y)/AY  STIF 86
BB(1,20)=0                                         STIF 87
BB(2,20)=(1.0+Z/R)*(-X+3*X*X+6*X*Y-2*X*X*-6*X*Y*Y)/AY-Z*DR*(-X*Y+S*Y+13*X*Y+3*X*Y-2*X*X*Y-2*X*Y*Y*Y)/(R*R)  STIF 88
BB(3,20)=(1.0+2*Z/R)*(-Y+6*X*Y+3*X*Y-6*X*X*Y-2*X*Y*Y)/AX  STIF 89
BB(1,21)=-6*Z*(-Y-2*X*Y)/(AX*AX)               STIF 90
BB(2,21)=(-X*Y+3*X*X*Y+3*X*X*Y-2*X*X*Y*Y)/R-6*Z*(X-2*X*Y)STIF 92
1)/(AY*AY)                                         STIF 93
BB(3,21)=-2*Z*(-1.0+6*X+6*Y-6*X*Y)/(AX*AY)    STIF 94
BB(1,22)=-2*X*Y+3*X*X*Y                          STIF 95
BB(2,22)=0                                         STIF 96
BB(3,22)=(-X*X+X*X*X)*AX/AY                   STIF 97
BB(1,23)=0                                         STIF 98
BB(2,23)=(1.0+Z/R)*(-X*X*X*X*X*X*X*X*X*Y)/(R*STIF 1R)  STIF 99
BB(3,23)=(1.0+2*Z/R)*(-2*X*Y+3*X*X*Y)          STIF 100
BB(1,24)=-Z*(-2*Y+6*X*Y)/AX                      STIF 101
BB(2,24)=AX*(-X*X*Y+X*X*X*Y)/R                 STIF 102
BB(3,24)=-2*Z*(-2*X+3*X*X*X)/AY                STIF 103
BB(1,25)=(-Y*Y+Y*Y*Y)*AY/AX                   STIF 104
BB(2,25)=0                                         STIF 105
BB(3,25)=-2*X*Y+3*X*Y*Y                      STIF 106

```



```

      BB(3,36)=-2*Z*(2*Y-3*Y*Y)/AX
      CALL GTPRD(BB,DD,BD,MF,NF,MF)
      CALL GMPRD(BD,BB,BF,NF,MF,NF)
      RETURN
      END

      SUBROUTINE FMASS(NF,NF,AX,AY,R1,R2,X,Y,BF)
      DIHENSION AN(3,36),AS(36,3),BF(36,36)
      AN(NF,NF)
      AS(NF,MF)
      BF(NF,NF)
      MASS(NF,NF)=RHO*THICK*AX*AY*BF(NF,NF)
      DO 1 I1=1,MF
      DO 1 J1=1,NF
      AN(I1,J1)=C
      CONTINUE
      DO 2 I1=1,MF
      II=I1-1
      AN(I1+1,II+1)=1.0-X*Y-3*X*Y*Y+3*X*Y*Y+3*X*Y*Y+2*X*Y*Y*Y-2*X*Y*Y*Y
      12*X*X*Y-2*X*Y*Y*Y
      AN(I1+1,II+4)=AX*((X-X*Y-2*X*X+2*X*X*Y+X*X*X-X*X*X*X)
      AN(I1+1,II+7)=AY*((Y-X*Y-2*Y*Y+2*X*Y*Y+Y*Y*Y-X*Y*Y*Y)
      AN(I1+1,II+10)=XY+3*X*X-3*X*X*Y-3*X*X*Y-2*X*X*X*Y+2*X*X*Y+2*X*X*Y
      1*Y
      AN(I1+1,II+13)=AX*(-X*X*X*Y+X*X*X*X-X*X*X*X*X)
      AN(I1+1,II+16)=AY*((X*Y-2*X*Y*Y+X*Y*Y*Y)
      AN(I1+1,II+19)=-X*Y+3*X*X*Y+3*X*X*Y-2*X*X*X*Y-2*X*X*Y*Y
      AN(I1+1,II+22)=AX*(-X*X*Y+X*X*X*X)
      AN(I1+1,II+25)=AY*((-X*X*Y*Y+X*X*Y*Y)
      AN(I1+1,II+28)=XY+3*X*Y-3*X*X*Y-3*X*X*Y*Y-2*X*Y*Y*Y+2*X*X*X*Y
      1*Y
      AN(I1+1,II+31)=AX*((X*Y-2*X*X*Y+X*X*X*X)

```

```

AN(II+1,II+34)=AY*(-Y*Y+X*Y*Y+Y*Y*Y-X*Y*Y*Y)
2 CONTINUE
    CALL GMTR(A,N,AS,MF,NF)
    CALL GMPRD(AS,AN,BF,NF,MF,NF)
    RETURN
END

```

MASS	27
MASS	28
MASS	29
MASS	30
MASS	31
MASS	32

```

C NPOIN=NUMBER OF NODAL POINTS
C NFREE=DEGREES OF FREEDOM PER NODAL POINT
C NPK=NPOIN*NFREE
C NBC=NUMBER OF BOUNDARY CONDITIONS
C N=NPK-NBC
C AX=LENGTH OF THE ELEMENT IN X-DIRECTION (IN)
C AY=LENGTH OF THE ELEMENT IN Y-DIRECTION (IN)
C E=MODULUS OF ELASTICITY (LBF/IN**2)
C RHO=DENSITY (LBM/IN**3)
C POISS=POISSON'S RATIO
C THICK=THICKNESS (IN)
C AL=SHELL'S OPENNING LENGTH (IN)
C AX=0.75
C AY=1.542
C E=10300000
C RHO=C. C98
C RHO=RHO/386.4
C POISS=0.334
C THICK=0.4
C AL=6.60
C OMEGA=NATURAL FREQUENCY (RAD/SEC)
C FREQU=NATURAL FREQUENCY (CYCLES/SEC)
C COEF1=OMEGA*D1, FREQUENCY COEFFICIENT
C IF COORDINATE TRANSFORMATION IS DESIRED THEN AKL(I,J) IS THE
C DIRECTIONAL COSINE TRANSFORMATION MATRIX, THAT IS Ki=(AKL)T*K*(AKL), MAIN 45
C D=E/(RHO*2*(1.0-POISS*POISS))
C OMEGA=SQRT(D/VU(1));
C COEF1=OMEGA*D1
C NELEM=6
C NPOIN=12
C NBC=30
C NM=2
C NM1=1
C NM2=NM
C NFREE=9
C NPK=NFREE*NPOIN

```

```

NF=4*NFREE
NN=N
NN=N
      MAIN 57
      MAIN 58
      MAIN 59
      MAIN 60
      MAIN 61
      MAIN 62
      MAIN 63
      MAIN 64
      MAIN 65
      MAIN 66
      MAIN 67
      MAIN 68
      MAIN 69
      MAIN 70
      MAIN 71
      MAIN 72
      MAIN 73
      MAIN 74
      MAIN 75
      MAIN 76
      MAIN 77
      MAIN 78
      MAIN 79
      MAIN 80
      MAIN 81
      MAIN 82
      MAIN 83
      MAIN 84
      MAIN 85
      MAIN 86
      MAIN 87
      MAIN 88
      MAIN 89
      MAIN 90
      MAIN 91
      MAIN 92

D=E/(RHO*2*(1.0-POISS*POISS))
D1=AL*AL/THICK*SQRT((RHO*12)/E)
DO 1 I1=1,NF
DO 1 J1=1,NF
AKL(I1,J1)=0
1 CONTINUE
NAK=0
2 NAK=NAK+1
DO 3 I1=1,NPK
DO 3 J1=1,NPK
AKF(I1,J1)=0
3 CONTINUE
J=NLEM/NM
DO 43 I=1,IJ
IF (NAK.EQ.1) GO TO 5
C INSERT MASS
READ (8,4) ((AKK(I1,J1),J1=1,NF),I1=1,NF)
4 FORMAT (/4E15.7)
5 IF (NAK.GT.1) GO TO 6
C INSERT "STIFFNESS" MATRIX
READ (8,4) (((AKK(I1,J1),J1=1,NF),I1=1,NF))
6 DO 43 IR=1,NM1
IC=0
7 DO 9 ID=1,2
DO 8 IJK=1,NFREE
AKL(IJK+IC,IJK+IC)=1
8 CONTINUE
IC=IC+NFREE
9 CONTINUE
IF (IC.EQ.(2*NFREE)) GO TO 7
CALL GPRD(AKL,AKK,AKN,NF,NF,NF)
CALL GMPRD(AKM,AKL,AKN,NF,NF,NF)
DO 43 IP=1,NM2

```

```

      READ (1,10) L,J,K,M
10 FORMAT (4I5)
      LL=L*NFREE
      JJ=J*NFREE
      KK=K*NFREE
      MM=M*NFREE
      LLL=LL-NFREE+1
      JJJ=JJ-NFREE+1
      KKK=KK-NFREE+1
      MMK=MM-NFREE+1
      L1=1
      DO 12 I1=L1,LL
      M1=i
      DO 11 J1=LLL,LL
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
11    CONTINUE
      L1=L1+1
12    CONTINUE
      L1=1
      DO 14 I1=LLL,LL
      M1=NFREE+1
      DO 13 J1=JJJ,JJ
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
13    CONTINUE
      L1=L1+1
14    CONTINUE
      L1=1
      DO 16 I1=L1,LL
      M1=2*NFREE+1
      DO 15 J1=KKK,KK
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
15    CONTINUE
      L1=L1+1

```

```

16 CONTINUE
L1=1
DO 18 I1=LLL,LL
M1=3*NFREE+1
DO 17 J1=MMM,MM
AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
M1=M1+1
17 CONTINUE
L1=L1+1
18 CONTINUE
L1=NFREE+1
DO 20 I1=JJJ,JJ
M1=1
DO 19 J1=LLL,LL
AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
M1=M1+1
19 CONTINUE
L1=L1+1
20 CONTINUE
L1=NFREE+1
DO 22 I1=JJJ,JJ
M1=NFREE+1
DO 21 J1=JJJ,JJ
AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
M1=M1+1
21 CONTINUE
L1=L1+1
22 CONTINUE
L1=NFREE+1
DO 24 I1=JJJ,JJ
M1=2*NFREE+1
DO 23 J1=KKK,KK
AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
M1=M1+1
23 CONTINUE
L1=L1+1

```

```

24 CONTINUE
    L1=NFREE+1
    DO 26 I1=JJ,JJ
    M1=3*NFREE+1
    DO 25 J1=MM,MM
        AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
        M1=M1+1
    25 CONTINUE
        L1=L1+1
    26 CONTINUE
        L1=2*NFREE+1
        DO 28 I1=KKK,KK
            M1=I
            DO 27 J1=LLL,LL
                AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
                M1=M1+1
            27 CONTINUE
            L1=L1+1
        28 CONTINUE
            L1=2*NFREE+1
            DO 30 I1=KKK,KK
            M1=NFREE+1
            DO 29 J1=JJ,JJ
                AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
                M1=M1+1
            29 CONTINUE
            L1=L1+1
        30 CONTINUE
            L1=2*NFREE+1
            DO 32 I1=KKK,KK
            M1=2*NFREE+1
            DO 31 J1=KKK,KK
                AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
                M1=M1+1
            31 CONTINUE
            L1=L1+1

```

```

32 CONTINUE
  L1=2*NFREE+1
  DO 34 I1=KKK,KK
    M1=3*NFREE+1
    DO 33 J1=MMM,MM
      AKF(I1,J1)=AKF(I1,J1)+AKN(I1,M1)
      M1=M1+1
  33 CONTINUE
    L1=L1+1
  34 CONTINUE
    L1=3*NFREE+1
    DO 36 I1=MMM,MM
      M1=1
      DO 35 J1=LLL,LL
        AKF(I1,J1)=AKF(I1,J1)+AKN(I1,M1)
        M1=M1+1
  35 CONTINUE
    L1=L1+1
  36 CONTINUE
    L1=3*NFREE+1
    DO 38 I1=MMM,MM
      M1=NFREE+1
      DO 37 J1=JJJ,JJ
        AKF(I1,J1)=AKF(I1,J1)+AKN(I1,M1)
        M1=M1+1
  37 CONTINUE
    L1=L1+1
  38 CONTINUE
    L1=3*NFREE+1
    DO 40 I1=MMM,MM
      M1=2*NFREE+1
      DO 39 J1=KKK,KK
        AKF(I1,J1)=AKF(I1,J1)+AKN(I1,M1)
        M1=M1+1
  39 CONTINUE
    L1=L1+1

```

```

40 CONTINUE
L1=3*NFREE+1
DO 42 I1=MM,MM
M1=3*NFREE+1
DO 41 J1=MM,MM
AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
M1=M1+1
41 CONTINUE
L1=L1+1
42 CONTINUE
43 CONTINUE
IF (NAK.GT.1) GO TO 45
READ (1,44) (VC(I1),I1=1,NBC)
44 FORMAT (8I10)
45 DO 46 I1=1,NBC
LA=VC(I1)
IN=NPK-LA-I1+1
IF (IN.LE.0) GO TO 46
DO 46 J1=1,IN
LB=LA+1
CALL RINT(AKF,NPK,NPK,LA,LB)
CALL CINT(AKF,NPK,NPK,LA,LB)
LA=LB
46 CONTINUE
IF (NAK.GT.1) GO TO 48
DO 47 I1=1,N
DO 47 J1=1,N
A(I1,J1)=AKF(I1,J1)
47 CONTINUE
NM=NELEM
NM1=1
NM2=NELEM
GO TO 2
48 DO 49 I1=1,N
DO 49 J1=1,N
RM(I1,J1)=AKF(I1,J1)

```

```

49 CONTINUE
      WRITE (3,55)
      CALL NROOT(N,RM,A,VU,ARA)
      DO 50 I=1,NN
      OMEGA=SQRT(D/VU(I))
      FREQU=OMEGA/6.28
      COEF1=OMEGA*D1
      WRITE (3,53) I,VU(I),OMEGA,FREQU,COEF1
50  CONTINUE
      WRITE (3,55)
      READ (1,44) (VC(I1),I1=1,NBC)
      A1=0
      I1=1
      I2=1
      DO 52 I=1,NPK
      IF ((VC(I1)-I)*EQ.0) GO TO 51
      WRITE (3,54) I,(ARA(I2,J2),J2=1,6)
      I2=I2+1
      GO TO 52
51  WRITE (3,54) I,A1,A1,A1,A1,A1
      I1=I1+1
52  CONTINUE
53  FORMAT (1X,'I='',I3,2X,'VU(I)'',E13.6,2X,'OMEGA'',E13.6,2X,'FREQU=''',MAIN
1,E13.6,2X,'COEF1'',E13.6,2X,')
54  FORMAT (1X,'I='',I3,6E20.5,')
55  FORMAT (1H1)
      CALL EXIT
END

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三

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I = 27	0 . 00080 = 00	0 . 277873E = 00	0 . 948004E = 01	0 . 102200E = 00	0 . 763962 = 0
I = 28	0 . 616206E = 05	0 . 239645E = 02	-0 . 358355E = 02	-0 . 50756E = 02	-0 . 121240
I = 29	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 30	0 . 262605E = 00	0 . 220764E = 00	0 . 122943E = 02	0 . 489287E = 02	-0 . 282233E = 0
I = 31	-0 . 960066E = 02	0 . 226702E = 02	0 . 226702E = 01	0 . 489287E = 02	-0 . 282233E = 0
I = 32	0 . 275545E = 01	0 . 652267E = 01	0 . 571091E = 02	0 . 252292E = 01	0 . 262250
I = 33	0 . 127002E = 02	0 . 140007E = 02	-0 . 127072E = 00	-0 . 106072E = 00	-0 . 242065
I = 34	0 . 127002E = 02	0 . 140007E = 02	-0 . 127072E = 02	-0 . 106072E = 02	-0 . 242065
I = 35	-0 . 126703E = 00	0 . 140007E = 02	-0 . 127072E = 00	-0 . 106072E = 00	-0 . 242065
I = 36	0 . 221437E = 00	0 . 226257E = 00	0 . 230967E = 01	0 . 151346E = 01	0 . 250537
I = 37	0 . 547172E = 02	0 . 547172E = 02	-0 . 507322E = 02	-0 . 507322E = 02	0 . 281202
I = 38	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 39	-0 . 329232E = 00	0 . 221437E = 00	0 . 226257E = 00	0 . 151346E = 01	0 . 250537
I = 40	-0 . 154778E = 01	0 . 18152E = 02	0 . 18152E = 02	0 . 773820E = 02	0 . 805454
I = 41	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 42	0 . 456005E = 01	0 . 154778E = 01	-0 . 26102E = 03	0 . 255005E = 02	-0 . 190805E = 02
I = 43	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 44	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 45	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0
I = 46	0 . 700324E = 01	-0 . 578107E = 01	0 . 205600E = 01	0 . 574603E = 02	-0 . 29310E = 01
I = 47	0 . 103762E = 00	0 . 74603E = 00	0 . 35884E = 01	0 . 127074E = 00	-0 . 203032
I = 48	0 . 257246E = 01	0 . 6746213E = 02	0 . 22284E = 02	0 . 6746213E = 02	-0 . 250577
I = 49	0 . 0	0 . 0	0 . 0	0 . 0	0 . 0

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