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USER'S MANUAL
AEROTHERM GRAPHITE SURFACE
KINETICS COMPUTER PROGRAM

Volume II - Fortran Variables, Flow Charts,
and Program Listings

January 1972

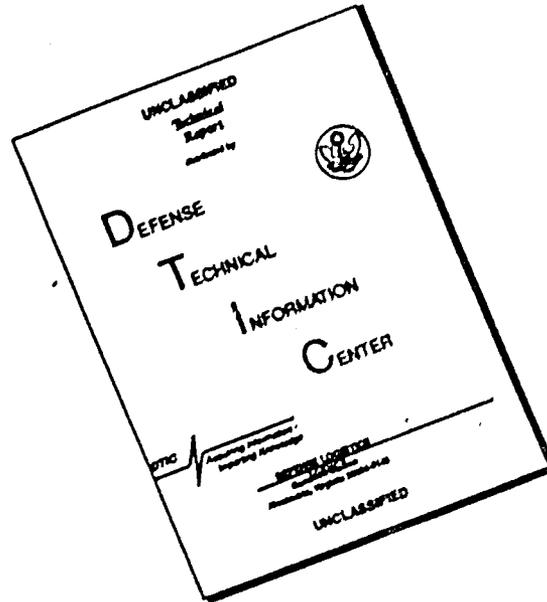


Air Force Rocket Propulsion Laboratory
Director of Laboratories
Edwards, California 93523
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United States Air Force

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USER'S MANUAL

AEROTHERM GRAPHITE SURFACE
KINETICS COMPUTER PROGRAM

VOLUME II

FORTRAN VARIABLES,
FLOW CHARTS, AND PROGRAM LISTINGS

Prepared under the Sponsorship of
Air Force Rocket Propulsion Laboratory
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FOREWORD

This report is one of two computer program user's manuals prepared by Aerotherm Division of Acurex Corporation under USAF Contract F04611-69-C-0081. Included herein is Volume II of the manual for the Aerotherm Graphite Surface Kinetics (GASKET) computer code. This volume presents definitions of Fortran variables, flow charts, and program listings. The work was administered under the direction of the Air Force Rocket Propulsion Laboratory with Mr. Robert J. Schoner as the Project Officer.

Mr. John W. Schaefer was the Program Manager and Mr. Mitchell R. Wool was Program Engineer. The GASKET code was developed by Dr. Kimble J. Clark.

This technical report has been reviewed and is approved.

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Chief, Technology Division

ABSTRACT

A Fortran IV computer code is described which computes thermochemical ablation rates of pyrolytic graphite surfaces, as a function of surface temperature and pressure, assuming all heterogeneous reactions at the surface are kinetically controlled. The calculation of the chemical state at the surface utilizes a film coefficient model which accounts for the unequal diffusion of species. All homogeneous reactions between gas-phase species adjacent to the surface are assumed to be in equilibrium. The specific surface reactions which are taken to be kinetically controlled include the reactions of condensed-phase carbon with water vapor, carbon dioxide, and hydrogen. Several options are available for computation of the boundary-layer edge state required in the diffusion model, including isentropic expansion or compression and normal or oblique shock wave calculation procedures.

This computer code is designated as the Aerotherm Graphite Surface Kinetics (GASKET) program and provides surface mass balance quantities needed for ablation predictions by the Aerotherm Charring Material Ablation (CMA) code or the Aerotherm Axisymmetric Transient Heating and Material Ablation (ASTHMA) code.

Volume I of this report contains descriptions of the fundamental physical events modeled, the mathematical equations solved, the information required for input, and the results output by the computer code. An input (card format) user's guide is provided along with sample input and output listings to enable an unfamiliar user to successfully operate the code and understand the results. Volume II of this report, presented herein, contains supplemental information on the specific Fortran IV routines. Included are program listings, flow charts, and definitions of Fortran variables.

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SECTION 1
INTRODUCTION

The computer program described in this user's manual is the Aerotherm Graphite Surface Kinetics (GASKET) computer program. This code was developed from an earlier Aerotherm computer program, the Equilibrium Surface Thermochemistry (EST) computer program, and was designed to solve the specific problem of kinetically controlled graphite ablation using a very simplified form of input data.

The purpose of Volume I of this user's manual was to enable an unfamiliar user to affectively utilize the GASKET program. It contained a general description of the problem the GASKET program solves, an input data deck preparation guide, and sample problem input and output. Volume II of this manual, included herein, contains the following additional program documentation:

- Definitions of all Fortran variables used
- Flow charts of program logic for each Fortran routine
- Listings of Fortran IV source decks
- Listings of the diffusion factor data and equilibrium thermochemical data built into the program

These are given in Sections 2, 3, 4 and 5, respectively. Three other documents of potential value to a reader desiring a more detailed exposition of the theoretical fundamentals of the GASKET program are References 1, 2, and 3.

SECTION 2

FORTRAN VARIABLE NAMES

The names and definitions of all Fortran variables used in the Aerotherm Graphite Surface Kinetics (GASKET) computer program are given in this section. Since the GASKET code is divided into many relatively small routines, the majority of all variables are included in common statements. These variables are defined first. In addition to the names and definitions of each variable, an abbreviated name of each routine in which each variable is used is given. The key relating the abbreviations to the names of the various routines is given below.

The remainder of the Fortran variables not appearing in common statements are presented for the specific routine in which they are utilized. The order corresponds to the order shown in the following key to routine identification.

KEY TO ROUTINE IDENTIFICATION

A	ACE	MAIN ROUTINE
AF	AFMAT	CONVERGENCE CONTROL
AL	ALPST	MASS BALANCE INITIALIZATIONS PERFORMED
B	BELCH	ESTABLISH ELEMENT/BASE SPECIES CORRESPONDENCE
C	CRECT	PERFORMS NECESSARY CORRECTIONS
IM	IMELM	INPUT OF ELEMENTAL DATA
IN	INPUT	GENERATION OF THERMOCHEMICAL DATA
KT	KINET	ADDS KINETIC RATE TERMS TO MASS BALANCE EQUATIONS
KN	KININ	INPUTS CONTROL CARD
M1	MAT1	SETS UP BASE SPECIES MASS BALANCE EQUATIONS
M2	MAT2	SETS UP NON-BASE EQUATIONS
M3	MAT3	SETS UP CONDENSED SPECIES EQUATIONS
O	OUTPT	PUTPUTS THERMODYNAMIC PROPERTIES, SPECIES MOLE FRACTIONS, AND PUNCH CARDS
P	PROPS	CALCULATES AND OUTPUTS K AND Z MASS FRACTIONS, Z DEPENDENT ENTHALPIES AND DERIVATIVE THERMODYNAMIC PROPERTIES
R	RERAY	INVERTS SOLUTION MATRIX
SC	SCALE	CHECKS THE SIZE OF CORRECTIONS AND ADJUSTS CORRECTION ARRAY
SQ	SQUEE	SQUEEZES CARD OUTPUT FORMAT TO INCLUDE OPTIONAL OUTPUT
SW	SWAP	RELOCATES THE SOLUTION MATRICES
T	THERM	CALCULATION OF SPECIES THERMODYNAMIC PROPERTIES
Z	ZIPIN	SETS INTERNAL CONTROL INTEGER ARRAYS

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINE(S) IN WHICH VARIABLE IS UTILIZED
AA	PRODUCT OF PRESSURE TIMES MOLECULAR WEIGHT.	A,AF,Z,T,M1,M3,SC,P,0
ACHSO	STATIC PRESSURE SQUARED	0,P,Z
ALP(K)	INPUT MASS QUANTITY OF ELEMENTS, EQ 25 OF NASA CR-1064.	AL,M1,M3
ALPT(N)	NUMBER OF ATOMS OF ELEMENT WITH ATOMIC NUMBER JAT(N) IN A SPECIES. IN	
ATA	FIRST FOUR ALPHANUMERIC CHARACTERS IN ELEMENT NAME BEING INPUT.	B
ATB	SECOND FOUR ALPHANUMERIC CHARACTERS IN ELEMENT NAME BEING INPUT.	B
ATC	LAST FOUR ALPHANUMERIC CHARACTERS IN ELEMENT NAME BEING INPUT.	B
B(N)	ERRORS USED WITH COEFFICIENTS TO YIELD CORRECTIONS IN CHEMISTRY ITERATIONS.	A,AF,M1,M2,M3
BE(J)	TEMPORARY VALUES OF THE ERRORS IN THE MASS-BALANCE EQUATIONS.	M1,M2,M3
BY	TEMPORARY VALUE OF THE LOG OF THE PARTIAL PRESSURE FOR EACH BASE SPECIES.	M1,M2
B1	SAVED VALUE OF B(I) DURING INVERSION, EQUALS SURFACE EQUILIBRIUM ERROR FOR THAT OPTION.	A,AF
C(K)	ATOMS OF ELEMENT K IN CURRENT SPECIES.	IN
CIJ(K,KK)	GRAM ATOM OF ELEMENT K IN BASE SPECIES KK.	IN,P
CMF	THE FACTOR BY WHICH ALL CORRECTIONS ARE DAMPED DURING CHEMISTRY ITERATIONS.	A,SG,C
CP(J)	SPECIFIC HEAT.	T,M1,M2,P,0
CPF	FROZEN SPECIFIC HEAT.	M1,M2,M3
CPG	FROZEN SPECIFIC HEAT OF GAS.	M1,M2,P
DKPT(M)	SUMD/RT	KT
OMCHI	NOT USED IN PRESENT VERSION OF PROGRAM	Z
OMCLO	NOT USED IN PRESENT VERSION OF PROGRAM	Z
OUM(M)	DUMMY ARRAY	KT
OUM1	LOCALLY USED DUMMY VARIABLE	A,AF,AL,T,M1,M2,SC
OUM2	LOCALLY USED DUMMY VARIABLE	T,M1,M2,C
E(N)	ERRORS IN CHEMISTRY EQUATIONS (MASS BALANCE ERRORS FOR N EQUAL TO OR LESS THAN IS*, EQUILIBRIUM ERRORS FOR N GREATER THAN IS*, WHERE IS* IS THE NUMBER OF ELEMENTS INCLUDING ELECTRON).	A,M1,M2,M3,SC,0
EAK(M)	ACTIVATION ENERGY FOR M TH KINETICALLY-CONTROLLED REACTION, SEE EON. (46).	KT,T
EB(K)	MAGNITUDE OF LARGEST CONTRIBUTION TO K TH MASS-BALANCE.	M1,M2,M3,SC
EBL(K)	MINIMUM CONTRIBUTION ACCEPTED TO K TH MASS BALANCE, EB/(10**8).	M1,M2,M3
EL	MAXIMUM EQUILIBRIUM ERROR.	A,AF,M1,M2,M3

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINES IN WHICH VARIABLE IS UTILIZED
ENC	MAXIMUM MASS BALANCE ERROR.	ATAP,M3
EP	ERROR IN OVERALL PRESSURE BALANCE.	M1,M2,M3
ERK(M)	TEMPERATURE EXPONENT FOR M TH KINETICALLY-CONTROLLED REACTION. SEE EQN. (45).	KT,T
FAMA(I)	FIRST FOUR CHARACTERS OF BASE SPECIES CHEMICAL SYMBOL FOR EACH ELEMENT.	B
FAMB(I)	LAST FOUR CHARACTERS OF BASE SPECIES CHEMICAL SYMBOL FOR EACH ELEMENT.	B
FAMOA(J)	FIRST FOUR ALPHANUMERIC CHARACTERS FOR THE CHEMICAL SYMBOL OF THE J TH SPECIES.	IN,F,AL,SC,P,O
FAMOB(J)	LAST FOUR ALPHANUMERIC CHARACTERS FOR THE CHEMICAL SYMBOL OF THE J TH SPECIES.	IN,V,AL,V,O
FF(J)	DIFFUSION FACTOR INTRODUCED BY THE APPROXIMATION FOR DIFFUSION COEFFICIENTS BY EQ 19 OF NASA CR-1062.	Z,IN,AL,T,M1,M2,C,P,O
FFA	EXPONENT ON MOLECULAR WEIGHT CORRELATION OF DIFFUSION FACTORS.	IN,AL
FFF	RATIO OF GAS MOLECULAR WEIGHT TO ν_{M2} .	T,M1,M2,C
FFIN(J)	VALUE OF THE DIFFUSION FACTOR OF THE J TH INPUT SPECIES.	IN,AL
FKF(M)	PREEXPONENTIAL FACTOR FOR M TH KINETICALLY-CONTROLLED REACTION. SEE EQN. (46).	KT,O,T
FLIO	FRACTION OF A SPECIES WHICH IS LIQUID.	A,T,M3,O
FNU(K)	TEMPORARY VALUE OF $\nu_{M2}(J,K)$ FOR CURRENT VALUE OF J.	M2
GAH	ISENTROPIC EXPONENT	O,P,Z
GAMR	INPUT MASS FRACTION/Z FRACTION WEIGHTING FACTOR EXPONENT.	KN,Z
GAMX	UNEQUAL DIFFUSION EXPONENT ON DIFFUSION FACTORS.	Z,IN,AL,P,O
GAMF(K)	DEFINED BY EQ 79 OF NASA CR-1064.	AL,M1,M2
GAMH(I)	DEFINED BY EQN. (80) OF NASA CR-1064.	M1,M2,M3
GAMK(I,J)	DEFINED BY EQN. (81) OF NASA CR-1064.	M1
H(J)	ENTHALPY OF THE J TH SPECIES.	T,M1,M2,P,O
HCH	SAVED VALUE OF MIXTURE TOTAL ENTHALPY.	O,P,Z
HG	GAS ENTHALPY	O
HIP	ENTHALPY INPUT.	Z,M3,O
HMELT	ENTHALPY OF FUSION FOR SPECIES WHICH IS CURRENTLY CHANGING PHASE (SOLID/LIQUID).	T,M3,O
HOS	ENTHALPY OF SPECIES IN CLOSED SYSTEM ASSIGNED ENTHALPY SOLUTION.	M1,M2
IB(K)	INDEX ON SPECIES WITH LARGEST CONTRIBUTION TO K TH MASS BALANCE. SUBSEQUENTLY ORDERED ON IB WITH DUPLICATES SET TO 1000.	M1,M2,SC,C

LIST OF FORTRAN VARIABLES APPEARING IN COMMON STATEMENTS		
VARIABLE NAME	DESCRIPTION	ROUTINES IN WHICH VARIABLE IS UTILIZED
IC(I)	CONTROL FLAG FOR BASE SPECIES IDENTICAL TO IFC(I) EXCEPT DURING SEARCH FOR SURFACE SPECIES IN SURFACE EQUILIBRIUM OPTION.	TWINZISC
IC(N)	NEGATIVE INDEX OF ELEMENT CORRESPONDING TO K TH BASE SPECIES.	B
IDC	UNITY ALWAYS. UNUSED IN PRESENT VERSION OF PROGRAM.	IT
IER	EQUATION NUMBER TO REPRESENT NEWLY APPEARING CONDENSED SPECIES.	AF,M2,SC
IFC(J)	CONTROL FLAG (0=GAS, -1= NONPRESENT CONDENSED, +1= PRESENT CONDENSED. PRIOR FLAGS DECREMENTED BY 1 IF SPECIES CONTAINS NONPRESENT ELEMENT OR INCREMENTED BY 1 IF IT IS A BASE SPECIES REPRESENTING A NONPRESENT ELEMENT).	A,Z,N,AL,T,M1,M2,M3,SC,C,P,0
IFCJC	CONTROL FLAG FOR THE CURRENT SURFACE SPECIES.	WIMZMS
IPL	HAS NO CURRENT FUNCTION	
IFRZ	CONTROL FLAG INDICATING FROZEN COMPOSITION CALCULATION.	AVZ0
II	INDEX USED TO COUNT SPECIES NOT CONSIDERED AS BASE SPECIES.	Z,IN
IL	INDEX ON FIRST CHEMISTRY EQUATION TO BE SOLVED #1 FOR UNKNOWN T AND #2 FOR KNOWN T.	Z,AF,MS
IM(K)	ROW AND COLUMN INDEX IN INVERSION OF C _{ij} TO U _m .	IN,B
IN	NUMBER OF EQUATIONS BEING SOLVED (HAS THE VALUE OF THE LOCAL VARIABLE ISPW IF TEMPERATURE IS UNKNOWN OR ISPO-1 IF TEMPERATURE IS KNOWN).	E,AF,M3
IOAT(N)	INDEX OF N TH OMITTED ELEMENT.	AL
IP	FLAG INDICATING THE IMPORTANCE OF EACH SPECIES IN THE MASS BALANCE M ₁ ,M ₂ ,SC,C	
IR(Y)	NEGATIVE INDEX OF BASE SPECIES CORRESPONDING TO ELEMENT K.	B,AL,M1,M2
IRE	INDEX ON NEWLY APPEARING CONDENSED SPECIES.	AF,M2,M3,SC,D
IS	NUMBER OF ELEMENTS INCLUDING ELECTRON.	A,IN,IN,B,AL,T,M1,M2,M3,SC,C,P
ISP	NUMBER OF ELEMENTS INCLUDING ELECTRON PLUS ONE.	IN,B,AL,M2
ISP0	ISP2 + NUMBER OF PRESENT CONDENSED SPECIES.	A,AF,M1,M2,M3,SC
ISP2	NUMBER OF ELEMENTS INCLUDING ELECTRON PLUS TWO.	A,M1,M2,M3
IT	VALUE OF ITS AT CONVERGENCE.	A,0
ITS	COUNTER FOR CHEMISTRY ITERATIONS.	A,AF,Z,T,M1,M2,M3,P,0
IXC	CURRENT INDEX OF B PRIME CHAK ARRAY.	Z
IXG	NOT USED IN PRESENT VERSION OF PROGRAM	Z
J	INDEX USED TO COUNT THE CARBOATE BASE SPECIES.	Z,IN,B
JAN	TAPE UNIT NUMBER WHERE THERMOCHEMICAL SPECIES DATA ARE STORED.	A,IN
JAT(N)	ATOMIC NUMBER OF AN ELEMENT WHICH CONTAINS ALPT(N) ATOMS IN A SPECIE.	IN
JS	INDEX ON SURFACE CONDENSED SPECIES.	AVAF,IN,M1,M2,M3,P

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINES IN WHICH VARIABLE IS UTILIZED
JJRN	SPECIES INDEX OF N TH CANDIDATE CONDENSED SPECIES.	M2,M3
KATK	ATOMIC NUMBER IDENTIFIER OF THE K TH ELEMENT INPUT.	IN,IN,AL,MI,M2,P
KIN	NUMBER OF TAPE FROM WHICH DATA IS READ.	KVZ,IN,IN,AL
KK	TEMPORARY VALUE OF SPECIES POSITION INDEX (I.E. J TH SPECIES).	IN
KKJ	FLAG DESIGNATING WHETHER PRESSURE OR MACH NUMBER IS USED IN ISENTROPIC EXPANSION.	A
KKA	FLAG FOR CARD OUTPUT FORMAT CONTROL.	Z=0
KPHA(N)	PHASE INDEX FOR SPECIES, 1 = GAS, 2 = SOLID, 3 = LIQUID.	IN
KOUT	NUMBER OF TAPE ONTO WHICH DATA IS WRITTEN.	A,AF,Z,IN,IN,AL,T,MI,SC,P=0
KR(N)	CONTROL INTEGER ARRAY	A,AF,Z,IN,IN,AL,T,MI,M2,M3,SC,C,P=0
KRALP	CONTROL FLAG WHICH INDICATES THE NEED FOR MASS BALANCE INITIALIZATION.	A,Z,T
KRK(I)	INPUT CONTROL INTEGER ARRAY.	IN,KR,T,KN,O,T
KRZZ	CONTROL FLAG CALLING LOGIC WHICH INSERTS θ PRIME VALUES IN MATRIX TO REDUCE TEMPERATURE INCREMENTS IN θ PRIME MATRIX.	Z
LAHI	INTEGERS USED TO ESTABLISH ELEMENT BASE SPECIES CORRESPONDENCE.	I,8,AL
LIM(I,J)	WORKING MATRIX FOR BASE SPECIES-ELEMENT CORRESPONDENCE EVALUATION.	θ ,C
LL(K)	ARRAY OF FLAGS DESIGNATING WHICH KINETIC REACTIONS ARE CONTROLLING. SEE SECTION 2.2 OF NASA CR-1004.	KT
MA(M)	ARRAY OF IDENTIFICATION NUMBERS FOR THE KINETICALLY-CONTROLLED REACTIONS.	KT
MELT	INDEX ON PHASE CHANGING SPECIES.	I,M3=0
MODE	STORED VALUE FOR KR(I).	A,AF,Z,T,MI,M2,M3
MOL	UNUSED VARIABLE IN PRESENT VERSION OF PROGRAM.	
MT	NUMBER OF KINETICALLY-CONTROLLED REACTIONS.	KT,O,T,Z
MX	NUMBER OF θ PRIME ENTRIES INSERTED IN θ PRIME MATRIX TO DECREASE TEMPERATURE INCREMENTS.	Z
N	NUMBER OF SPECIES.	AF,Z,IN,IN,AL,T,MI,SC,C,P=0
NAB	UNUSED VARIABLE IN PRESENT VERSION OF PROGRAM.	
NCC	COUNTER WHICH IDENTIFIES CALCULATION NUMBER IN THE SEQUENCE OF STATE CALCULATIONS ASSOCIATED WITH A GIVEN PROBLEM.	IN,IN,KN
NCV	NONCONVERGENCE FLAG, 0=CONVERGENCE, 1=NONCONVERGENCE.	A,AF,Z,AL,T,P=0
NFF	NUMBER OF SPECIES FOR WHICH DIFFUSION FACTORS, FF(I), ARE TO BE READ IN.	Z,IN,AL
NFIA(I)	FIRST FOUR ALPHANUMERIC CHARACTERS IN THE CHEMICAL SYMBOL OF SPECIES FOR WHICH DIFFUSION FACTOR, FF(I) IS BEING READ IN.	IN,AL

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINES IN WHICH VARIABLE IS UTILIZED
NPB(I,M)	EAST POINT ALPHANUMERIC CHARACTERS IN THE CHEMICAL SYMBOL OF SPECIES FOR WHICH DIFFUSION FACTOR, FF(J), IS BEING READ IN.	IN,ML
NOAT	CURRENT NUMBER OF OMITTED ELEMENTS.	Z,AL
NOATD	OMITTED ELEMENTS IN PREVIOUS SOLUTION.	AL
NO	TRANSFER VECTOR ON RETURN FROM APMAT TO EST	APAF
NXC	NOT USED IN PRESENT VERSION OF PROGRAM	Z
NXG	NOT USED IN PRESENT VERSION OF PROGRAM	Z
P	PRESSURE	Z,IN,AL,T,M1,M3,SC,P,O
PCM	SAVED CHAMBER PRESSURE	O,Z
PKP(M)	EXPONENTIAL OF SUMP-SUMM.	KT
PKR(M)	EXPONENTIAL OF SUMM.	KI
PMR(M)	PRESSURE TIMES MOLECULAR WEIGHT TIMES REACTION RATE COEFFICIENT FOR M TH KINETIC REACTION.	KT
PMU(I,M)	PRODUCT STOICHIOMETRIC COEFFICIENTS FOR I-TH BASE SPECIES AND M-TH KINETIC REACTION. SEE EQN. (44).	KT
PNUS(K)	SUMMATION $\sum_{J=K} V_{U(J)} V_{U(J)}$ OVER ALL GASES J.	T,M1,M2,SC,C
PR(I)	STATIC PRESSURE	KN,O,P,Z
RA(N)	HEAT OF FORMATION OF CURRENT MOLECULE AT 298 DEG. K FROM JANAF BASE STATE, CAL/MOLE.	IN
RAT(M)	THE MAXIMUM OF THE TWO VARIABLES PKP(M) AND PKR(M).	KT
RR(J,N)	THERMOCHEMICAL DATA CONSTANT, ENTHALPY AT 3000 DEG. K FOR THE J TH SPECIES.	IN,T
RC(J,N)	THERMOCHEMICAL DATA CONSTANT IN SPECIFIC HEAT CURVE FIT EQUATION FOR J TH SPECIES (SEE CARD SET 6 OF INPUT GUIDE).	IN,T
RD(J,N)	THERMOCHEMICAL DATA CONSTANT IN SPECIFIC HEAT CURVE FIT EQUATION FOR J TH SPECIES (SEE CARD SET 6 OF INPUT GUIDE).	IN,T
RE(J,N)	THERMOCHEMICAL DATA CONSTANT IN SPECIFIC HEAT CURVE FIT EQUATION FOR J TH SPECIES (SEE CARD SET 6 OF INPUT GUIDE).	IN,T
REFM	REFERENCE MOLECULAR WEIGHT IN DIFFUSION FACTOR CORRELATION, EITHER INPUT OR ASSIGNED INTERNALLY.	IN,AL
RF(J,N)	THERMOCHEMICAL DATA CONSTANT IN SPECIFIC HEAT CURVE FIT EQUATION FOR J TH SPECIES (SEE CARD SET 6 OF INPUT GUIDE).	IN,T
RHO	MIXTURE DENSITY	O,P,Z
RMU(I,M)	REACTANT STOICHIOMETRIC COEFFICIENT FOR I TH BASE SPECIES AND M TH KINETIC REACTION. SEE EQN. (44).	KT,T
ROUGH	INPUT MASS TRANSFER COEFFICIENT.	KN,O,T
RV	R PRIME	M1,M2,SC

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINE(S) IN WHICH VARIABLE IS UTILIZED
SA1	SHOCK ANGLE RELATIVE TO UPSTREAM VELOCITY VECTOR. SEE SECTION 2.1.3.	U
SA2	SHOCK ANGLE RELATIVE TO DOWNSTREAM VELOCITY VECTOR. SEE SECTION 2.1.3.	U
SBT(J)	ENTROPY OF THE J TH SPECIES.	T+O
SCH	SAVED VALUE OF MIXTURE TOTAL ENTROPY.	O+Z
SM1	STATIC ENTHALPY UPSTREAM OF SHOCK WAVE.	O+Z
SIP	CURRENT SYSTEMS ENTROPY.	Z+O
SLA(N,N)	TEMPORARY STORAGE LOCATIONS FOR MATRIX ELEMENTS.	A+AF+SW
SLAM(K)	DEFINED BY EQ 83 OF NASA CR-1004.	T+M+Z+SC+O
SLB(N)	TEMPORARY STORAGE LOCATION FOR VECTOR B(N).	A+AF+SW
SMELT	ENTROPY OF FUSION FOR SPECIES WHICH IS CURRENTLY CHANGING PHASE.	T+O
SORCF(N)	THIRTY ALPHANUMERIC CHARACTERS GIVING THE SOURCE OF THE THERMOCHEMICAL DATA FOR THE CURRENT SPECIES.	IN
SPI	STATIC PRESSURE UPSTREAM OF SHOCKWAVE.	O+Z
SQMAX	MACH NUMBER SQUARED	O+P+Z
SRI	DENSITY UPSTREAM OF SHOCKWAVE.	O+Z
SUMC	SUMMATION OF VN(J) FOR ALL CONDENSED SPECIES.	T+M1+M2
SUML	LOG (SUMN/P)	T+M1+M2
SUMN	SUMMATION OF PARTIAL PRESSURES FOR ALL GAS PHASE SPECIES.	T+M1+M2
SV1	VELOCITY UPSTREAM OF SHOCK WAVE.	O+Z
SVA	SECOND TERM ON R.H.S. OF EQN. (14) TIMES DOWNSTREAM DENSITY.	M3+Z
SVB	SV1*2.0/1.4869	M3+Z
SVC	TERM RELATED TO CONSERVATION OF ENERGY ACROSS A SHOCKWAVE, EQN. (13)	M3+Z
SVD	STATIC PRESSURE DOWNSTREAM OF SHOCKWAVE.	M3+Z
T	STATIC TEMPERATURE IN DEG K.	A+AF+Z+T+M3+SC+P+O
TAU(K,K)	INTERMEDIATE ARRAY USED IN FORMING UM.	IN+O
TBT	TEMPERATURE BELOW WHICH NO ADDITIONAL NON-ABLATING SURFACE CALCULATIONS WILL BE PERFORMED.	Z
TC(J)	-0.100 KP/0.100 LOG T FOR FORMATION REACTION OF J TH SPECIES.	T+M2+SC+O
TF(I)	FAIL TEMPERATURE OF SPECIES J.	AF+AL+C+KN+M1+M2
TH1	NOT USED IN PRESENT VERSION OF PROGRAM	Z
TILE	TEN ALPHANUMERIC CHARACTERS USED FOR PROBLEM IDENTIFICATION.	Z+P+O
TK(K,N)	GRAM ATOMS OF ELEMENT K PER UNIT MASS OF COMPONENT N.	IN+O+AL

LIST OF FORTRAN VARIABLES
 APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINE(S) IN WHICH VARIABLE IS UTILIZED
TEO	NOT USED IN PRESENT VERSION OF PROGRAM	Z
TMAX	MAXIMUM TEMPERATURE ALLOWED FOR CURRENT ITERATION.	AF,Z,T,M3,SC
TMIN	MINIMUM TEMPERATURE ALLOWED FOR CURRENT ITERATION.	AF,Z,T,M3,SC
TTMAX	SAVED VALUE OF MAXIMUM ALLOWED TEMPERATURE FOR THIS SOLUTION.	AF,T,M3
TTMIN	SAVED VALUE OF MINIMUM ALLOWED TEMPERATURE FOR THIS SOLUTION.	AF,T,M3
TQ(K,N)	GRAM ATOMS OF BASE SPECIES K PER UNIT MASS OF COMPONENT N (SEE W(N) FOR DEFINITION OF COMPONENTS).	IN,B,AL
TU(J,N)	UPPER TEMPERATURE OF TEMPERATURE RANGE FOR INPUTTING THERMODYNAMIC PROPERTY DATA FOR SPECIES J, N=1 OR 2 FOR LOWER AND UPPER TEMPERATURE RANGES, RESPECTIVELY.	IN,T
UM(K,KK)	MOLECULES OF BASE SPECIES K IN ELEMENT KK.	IN,IN,B
VA	TEMPORARY VALUE OF VN(J)/FF(J).	IN,AL,T,M1,M2,SC,C,P,O
VEL	FLOW VELOCITY	O,Z
VINT	INITIAL GUESS OF SPECIES PARTIAL PRESSURE = P*(10**6).	IN
VISC	MIXTURE VISCOSITY	
VLAM(I,I)	LAMBDA, DEFINED IN EQN. (83) OF NASA CR-1064.	C,M2,T
VLNK(I)	LOG KP FOR FORMATION REACTION OF J TH SPECIES.	T,M2,O
VMACH	MACH NUMBER	U
VMU2	COEFFICIENT MU2 DEFINED IN EQ 22 OF NASA CR-1062.	P
VN(I)	PARTIAL PRESSURE OF THE J TH SPECIES.	AF,IN,AL,T,M1,M2,M3,SC,C,P,O
VNU(J,K)	STOICHIOMETRIC COEFFICIENT ON K TH BASE SPECIES IN FORMATION OF J TH SPECIES.	IN,AL,T,M2,M3,SC,C,P
W(N)	COMPONENT MASS FRACTION AT WALLS; W(1) IS EDGE OAS; W(2) IS UNUSED; W(3) IS SURFACE MATERIAL; OR RELATIVE COMPONENT MASSES FOR CLOSED SYSTEM CALCULATIONS	Z,AL,T,SC,O
WALUP(I)	UNUSED VARIABLE IN PRESENT VERSION OF PROGRAM.	
WAT(K)	ATOMIC WEIGHT OF K TH ELEMENT.	IN,IT,P
WM	MOLECULAR WEIGHT OF MIXTURE.	Z,T,P,O
WR(I)	INTERNAL ARRAY SPECIFYING RELATIVE AMOUNT OF COMPONENTS 1,2, AND 3.	KNTZ
WS	SURFACE MATERIAL MASS RATES	Z,AL,T,M1
WTG	PRESSURE * GAS MOLECULAR WEIGHT.	AF,T,M1,M2,SC,C,O
WTL	SUMMATION OF VN(J) * WTM(J) FOR ALL CONDENSED SPECIES.	AF,T,M1,M2,SC,C,O
WTM(I)	MOLECULAR WEIGHT OF SPECIES J.	IN,AL,T,M1,M2,SC,C,P,O
X(N)	CORRECTIONS OF NONLINEAR VARIABLES IN CHEMISTRY SOLUTION.	AF,M3,SC

LIST OF FORTRAN VARIABLES
APPEARING IN COMMON STATEMENTS

VARIABLE NAME	DESCRIPTION	ROUTINE(S) IN WHICH VARIABLE IS UTILIZED
XC	NOT USED IN PRESENT VERSION OF PROGRAM	Z
XO	NOT USED IN PRESENT VERSION OF PROGRAM	Z
Y(I)	NATURAL LOG OF PARTIAL PRESSURE (PO FOR PRESENT CONDENSED SPECIES) IN VOLUME FRACTION	
YENT	LOG OF VINT.	IN
Z	INPUT THERMODYNAMIC STATE VARIABLE	KN
ZK(K)	BOUNDARY LAYER EDGE Z MASS FRACTION	AL

 LIST OF FORTRAN VARIABLES
 APPEARING IN
 MAIN ROUTINE ACE

VARIABLE NAME	DESCRIPTION
I	LOOP INDEX.
ICT	CYCLE COUNT ON POST ITERATION MODIFICATION TO INVERSION SOLUTION.
IG	FLAG CALLING FOR DEBUG OUTPUT FROM SUBROUTINE RERAY.
IT	PERFORMS NO FUNCTION.
ITT	TEMPORARILY SAVED VALUE OF THE VARIABLE IT.
IOI	TEMPORARY ALTERNATE VALUE OF IOQ DEPENDING ON POST ITERATION MODIFICATIONS TO INVERSION SOLUTION.
IOQ	DEBUG (1-2) AND NONCONVERGENT (1-1) FLAG ON CALL TO AND RETURN FROM RERAY, RESPECTIVELY.
JJC	TEMPORARILY SAVED VALUE OF THE VARIABLE JC.
MOE	FLAG SET IN ACE AND USED IN CRECT. (ZERO RESULTS IN EMPHASIZING EQUILIBRIUM EQUATIONS DURING CONVERGENCE; ONE RESULTS IN EMPHASIZING MASS BALANCES).

 LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE AFMAT

VARIABLE NAME	DESCRIPTION
DTD	DOWNWARD TEMPERATURE STEP USED IN SEEKING SURFACE EQUILIBRIUM SOLUTION.
DTU	UPWARD TEMPERATURE STEP USED IN SEEKING SURFACE EQUILIBRIUM SOLUTION.
I	LOOP INDEX.
XI	TEMPORARY VALUE OF X(I).

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE K2PST

VARIABLE NAME	DESCRIPTION
ALPH	TEMPORARY VALUE FOR THE K IN ELEMENT OF THE SUMMATION $\sum_{i=1}^N$ $\sum_{j=1}^N$, WHERE N IS COMPONENTS 1, 2 AND 3.
FFAD	VARIABLE ASSIGNED IN A DATA STATEMENT TO THE CHARACTERS FFA; USED TO LOCATE INPUT VALUE OF FFA.
I	LOOP INDEX.
IK	LOOP INDEX.
INF	LOWER LIMIT INDEX OF THE DIFFUSION FACTOR SET TO BE READ, EQUAL TO 1 PLUS THE TOTAL NUMBER PREVIOUSLY READ.
I1	ISALPHANUMERIC VARIABLE.
I2	ISALPHANUMERIC VARIABLE.
I3	ASSIGNED EQUAL TO I5 OR I6 DEPENDING ON OUTPUT LABEL DESIRED.
I4	ASSIGNED EQUAL TO I5 OR I7 DEPENDING ON OUTPUT LABEL DESIRED.
I5	SET EQUAL TO PM IN DATA STATEMENT FOR LABELING OF OUTPUT DIF- FUSION FACTORS.
I6	SET EQUAL TO PA * N IN DATA STATEMENT FOR LABELING OF OUTPUT DIFFUSION FACTORS.
I7	SET EQUAL TO PM * N IN DATA STATEMENT FOR LABELING OF OUTPUT DIFFUSION FACTORS.
JL	LOCAL INDEX USED IN DIFFUSION FACTOR INPUT LOGIC.
K	LOOP INDEX
L	LOOP INDEX.
LAMT	LOCAL VARIABLE.
NP	N+1
PIN	INITIAL PARTIAL PRESSURE GUESS = P/10.
PLOG	ALOG OF PIN.
PMU2	$\sum_{i=1}^N \sum_{j=1}^N \frac{W(i) \cdot W(j)}{FF(j)}$ SUMMED OVER ALL SPECIES $N = \text{VMU2} * P$.
REFD	THE FOUR CHARACTERS REFM ASSIGNED IN A DATA STATEMENT FOR OUTPUT LABELING.
TEST	MASS BALANCE CLOSURE CRITERIA.
TFMAX	MAXIMUM WALL TEMPERATURE OF CANDIDATE SURFACE SPECIES.
YC	INITIAL VALUE OF Y(I).

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE SECT

VARIABLE NAME	DESCRIPTION
I	LOOP INDEX.
IG	ELIMINATION INDEX IN BASE SPECIES - ELEMENT CORRESPONDENCE LOGIC.
IMI	LOCAL INDEX.
IMJ	TEMPORARY VALUE OF IMI.
IZ	LOOP INDEX.
JM	TEMPORARY COMPUTED INDEX FOR ARRAY IN.
K	LOOP INDEX.
L	LOOP INDEX.
LMD	BINARY BIT DIVISION.
LANT	LOCAL VARIABLE.
UGN	NORMALIZING FACTOR IN GAUSSIAN ELIMINATION.
V	LOCAL VARIABLE.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE CRECT

VARIABLE NAME	DESCRIPTION
OYI	VALUE OF OY FOR THE J TH SPECIES DURING LOOP ON THAT SPECIES.
I,IM,K	LOOP INDICES.
LIM	LOOP LIMIT = N (TOTAL NUMBER OF SPECIES).
M	LOCAL INDEX EQUAL TO IB(N).
M1	COUNT ON PRINCIPAL SPECIES AFTER ORDERING ON IB.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE IMELM

VARIABLE NAME	DESCRIPTION
AO	ALPHANUMERIC VARIABLE 'HOT'
AG	ALPHANUMERIC VARIABLE 'GRA'
ALPTO(I,J)	VALUE OF ALPT(I) STORED IN DATA FOR J TH SPECIE.
AMOD(J)	VALUE OF AMCA STORED IN DATA FOR J TH SPECIE.
AMOD(J)	VALUE OF AMOB STORED IN DATA FOR J TH SPECIE.
ATAS(I)	SAVED VALUE OF ATA(I).
ATSS(I)	SAVED VALUE OF ATB(I).
ATCS(I)	SAVED VALUE OF ATC(I).
BO	ALPHANUMERIC VARIABLE 'ORY'
BO	ALPHANUMERIC VARIABLE 'PHIT'
CO	ALPHANUMERIC VARIABLE 'ICE'
CG	ALPHANUMERIC VARIABLE 'E '
FFIND(I)	ARRAY FOR FFIN(I) STORED IN DATA.
I	LOOP INDEX ON ELEMENT.
ICAR	INDEX DESIGNATING POSITION OF ELEMENT CARBON IN INPUT ELEMENTAL COMPOSITION ARRAY.
IOF	INDEX DESIGNATING POSITION OF ELEMENT OXYGEN IN INPUT ELEMENTAL COMPOSITION ARRAY.
ISS	SAVED VALUE OF IS AFTER ADDITION OF FICTITIOUS ELEMENTS GRAPHITE AND HOT DRY ICE.
J	LOOP INDEX ON ELEMENTS.
JATD(I,J)	VALUE OF JAT(I) STORED IN DATA FOR J TH SPECIE.
K	LOOP INDEX ON COMPONENTS OR ELEMENTS.
L	LOOP INDEX ON COMPONENTS.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE INPUT

VARIABLE NAME	DESCRIPTION
ANOA	TEMPORARY LOCATION OF THE FIRST FOUR CHARACTERS OF A SPECIES CHEMICAL NAME, LATER ASSIGNED TO FAMOA FOR EACH SPECIES.
ANOB	TEMPORARY LOCATION OF THE LAST FOUR CHARACTERS OF A SPECIES CHEMICAL NAME, LATER ASSIGNED TO FAMOB FOR EACH SPECIES.
BLANK	FOUR BLANK CHARACTERS ASSIGNED TO THIS VARIABLE, USED FOR OUTPUT IF NO OTHER SURFACE SPECIES IS AVAILABLE, ASSIGNED TO FAMOB(NM).
CHAR	THE FOUR CHARACTERS CALLED CHAR, ARE ASSIGNED TO THIS VARIABLE AND USED FOR OUTPUT IF NO OTHER SURFACE SPECIES IS AVAILABLE, THEY ARE ASSIGNED TO FAMOATRM).
I	LOOP INDEX.
IML	TEMPORARY VALUE OF IM(L).
INF	LOWER LIMIT ON THE NUMBER OF DIFFUSION FACTORS TO BE READ IN ANY ONE PASS, EQUAL TO 1 PLUS THE TOTAL NUMBER PREVIOUSLY READ.
JM	J-1 WHERE J IS THE BASE SPECIES COUNT.
K	LOOP INDEX.
KKK	TEMPORARY VALUE OF SPECIES POSITION INDEX (I.E. J TH SPECIES).
KPHAD(I,J)	VALUE OF KPHA(I) STORED IN DATA FOR J TH SPECIE.
L	LOOP INDEX.
LAMKK	TEMPORARY VALUE OF LAH(KK)
NEX	NUMBER OF EXCESS SPECIES (SPECIES LIMIT IS 179).
NFIA(I)	ARRAY FOR NFIA(I) STORED IN DATA.
NFIB(I)	ARRAY FOR NFIB(I) STORED IN DATA.
NJ-N	LOOP INDEX
RAD(I,J)	VALUE OF RA(I) STORED IN DATA FOR J TH SPECIE.
RRO(I,J)	VALUE OF RR(K,I) STORED IN DATA FOR J TH SPECIE.
RCD(I,J)	VALUE OF RC(K,I) STORED IN DATA FOR J TH SPECIE.
RRO(I,J)	VALUE OF RD(K,I) STORED IN DATA FOR J TH SPECIE.
RED(I,J)	VALUE OF RE(K,I) STORED IN DATA FOR J TH SPECIE.
RFD(I,J)	VALUE OF RF(K,I) STORED IN DATA FOR J TH SPECIE.
SORCU(I,J)	VALUE OF SORCE(I) STORED IN DATA FOR J TH SPECIE.
TUD(I,J)	VALUE OF TU(K,I) STORED IN DATA FOR J TH SPECIE.
UGM	NORMALIZING FACTOR IN GAUSSIAN ELIMINATION.
WT	TEMPORARY VALUE OF A SPECIES MOLECULAR WEIGHT, ASSIGNED TO WTM FOR EACH SPECIES.
YC	INITIAL VALUE OF Y(J).

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE KINET

VARIABLE NAME	DESCRIPTION
AP	$EXEL/(EAL-1.)-1./ELK$, FIGHTING FACTOR IN LINEARIZING EQUILIBRIUM ASPECT OF KINETICALLY CONTROLLED MASS BALANCE.
ELK	NATURAL LOGARITHM OF EXEL.
EXEL	$(PKR1M+1.E-36)/(PKR1M+1.E-36)$ RATIO OF FORWARD TO REVERSE DRIVING POTENTIAL IN KINETIC EQUATIONS.
FFX(M)	SECOND BRACKETED QUANTITY IN EQN. (47), FOR M TH KINETIC REACTION.
FKK(I,J)	INHIBITING SPECIE PARTIAL PRESSURE COEFFICIENT FOR I TH BASE SPECIE AND J TH KINETIC REACTION, SEE EQN. (47).
HHCL	ALPHANUMERIC QUANTITY REPRESENTING THE REACTION INHIBITING SPECIE 'CLH'.
HHF	ALPHANUMERIC QUANTITY REPRESENTING THE REACTION INHIBITING SPECIE 'FH'.
I	LOOP INDEX
IL	LOWER LIMIT ON JO-LOOP, EQUAL TO I OR L.
IP	UPPER LIMIT ON JO-LOOP, EQUAL TO IS OR L.
J	LOOP INDEX
K	FLAG, EQUAL TO 0 OR MA(M), LOOP INDEX.
KR7	SAVED VALUE OF KH(7).
L	LOOP INDEX
M	LOOP INDEX
MT	MA(K)
MM	LOOP INDEX
MP	MM+1
PPX(M)	FIRST BRACKETED QUANTITY IN EQN. (47), FOR M TH KINETIC REACTION.
PRMU(I,M)	$PMU(I,M)-RMO(I,M)$
PSI(I,J)	INHIBITING SPECIE PARTIAL PRESSURE COEFFICIENT FOR THE I TH BASE SPECIE AND J TH KINETIC REACTION, SEE EQN. (47).
RT	1.9869×10^{-3}
SUMD	SUMMATION OVER BASE SPECIES OF $PRMU(I,M) \cdot PH(I)$, SEE NASA CR-1064.
SUMK	SUMMATION OVER BASE SPECIES OF $PRMU(I,M) \cdot VLNK(I)$, SEE NASA CR-1064.
SUMP	SUMMATION OVER BASE SPECIES OF $PH(I) \cdot Y(I)$, SEE NASA CR-1064.
SUMR	SUMMATION OVER BASE SPECIES OF $RMU(I,M) \cdot Y(I)$, SEE NASA CR-1064.
VK1	$PKR(M)-PKP(M)$
VK2	AA TIMES THE REACTION RATE COEFFICIENT DEFINED BY EQN. (46).

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE KINEM

VARIABLE NAME	DESCRIPTION
I	LOOP INDEX
J	LOOP INDEX
K	LOOP INDEX
KRA(I,J)	SEQUENCE OF INTERNAL CONTROL INTEGER ARRAYS-SEE KH(I).
KRKS	SAVED VALUE OF KRA(3,J) WHICH CONTROLS HOW THERMOCHEMICAL DATA IS GENERATED.
KRKS5	SAVED VALUE OF KRA(3,J) WHICH CONTROLS HOW THERMOCHEMICAL DATA IS GENERATED.
KTC	NO. FROZEN-EDGE TEMPERATURES PLUS NO. SURFACE TEMPERATURES PLUS SEVEN.
KTF	NUMBER OF ENTRIES IN FROZEN-EDGE TEMPERATURE ARRAY.
KTS	NUMBER OF ENTRIES IN SURFACE TEMPERATURE ARRAY.
NCT	NUMBER OF STATE CALCULATIONS REQUIRED TO DETERMINE THE EDGE STATE.
NCT1	NCT+1
NCT2	NCT+KTF
NCT3	NCT2+1 OR NCT+1
NCT4	NCT2+KTS OR NCT+KTS
NCT5	NCT3+1
NS	TOTAL NUMBER OF CANDIDATE GAS-PHASE SPECIES PLUS CONDENSED-PHASE CARBON.
PC	IDEAL CHAMBER PRESSURE, SPECIFIED WITH PROPELLANT FLAME TEMPERATURE.
PRA(I)	SEQUENCE OF PRESSURES USED IN STATE CALCULATIONS.
TFA(I)	ARRAY OF FROZEN-EDGE TEMPERATURES.
TSA(I)	ARRAY OF SURFACE TEMPERATURES.
WPA(I,J)	SEQUENCE OF INTERNAL VARIABLES DESIGNATING RELATIVE AMOUNTS OF COMPONENTS 1, 2, AND 3.
Z(I)	SEQUENCE OF THERMODYNAMIC VARIABLES (TEMPERATURE, ENTHALPY) USED IN STATE CALCULATIONS.
ZE	INPUT THERMODYNAMIC VARIABLE, PERTAINING TO CHAMBER, SHOCKWAVE, OR BOUNDARY LAYER EDGE.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE MATZ

VARIABLE NAME	DESCRIPTION
BJC	VALUE OF Y(J) WHEN J IS A BASE SPECIES CURRENTLY BEING CONSIDERED AS A SURFACE SPECIES.
I,IK,K	LOOP INDICES.
JCS	SAVED VALUE OF JC.
WSS	SAVED VALUE OF WS.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE MATZ

VARIABLE NAME	DESCRIPTION
ABSVA	ABSOLUTE VALUE OF CONTRIBUTION OF A SPECIES TO A MASS BALANCE.
BJC	FOR NON-BASE SURFACE SPECIES BJC IS IDENTICAL TO E(JC).
EAM	ABSOLUTE VALUE OF EQUILIBRIUM ERROR FOR A SPECIES.
EF4	ABSOLUTE ERROR OF CONDENSED SPECIES BEING INTRODUCED DURING CURRENT ITERATION.
FFJ	LOCALLY DEFINED VARIABLE.
I,J,IK	LOOP INDICES.
IE	EQUATION INDEX FOR CONDENSED SPECIES.
IO	FOR EACH NON-BASE GASEOUS SPECIES INITIALIZED TO ZERO, SET TO UNITY IF SPECIES IS SIGNIFICANT IN ANY MASS BALANCE.
K,KI	LOOP INDICES.
LIM	LOOP LIMIT = N (NUMBER OF SPECIES).
VP	LOCALLY DEFINED VARIABLE.
WT	FOR PRESENT NON-BASE SPECIES AND CERTAIN NON PRESENT SPECIES (THOSE CONSIDERED AS POSSIBLE SURFACE SPECIES), WT = SPECIES MOLECULAR WEIGHT/GAS PHASE MOLECULAR WEIGHT.

LIST OF FORTRAN VARIABLES
APPEARING IN
SUBROUTINE MAT3

VARIABLE NAME	DESCRIPTION
AGER	ABSOLUTE VALUE OF RATIO OF A MASS BALANCE ERROR TO LARGEST TERM IN THAT MASS BALANCE.
ART(I)	SAVED VALUE OF A(I)K(I)J(I).
CPA	LOCALLY DEFINED VARIABLE.
OTV	SELECTED VALUE OF A(I)K(I)J(I) USED FOR NORMALIZING A(I)M(I)N(I).
ENS	ERROR IN ENTHALPY FOR ASSIGNED ENTHALPY SOLUTION.
EP	ERROR IN MASS BALANCE RELATION.
I, IE, K	LOOP INDICES.
ISP3	NUMBER OF ELEMENTS INCLUDING THE ELECTRON PLUS THREE.
IV	LOOP INDEX
J	LOCALLY DEFINED INDEX.
JM	LOOP INDEX
JZ	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.
KX	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.
KZ	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.
L(I)	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.
M	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.
NEM	NUMBER OF SIGNIFICANT SPECIES PLUS NUMBER OF NON PRESENT ELEMENTS.
SHMLT	ENTHALPY OF FUSION OF A SPECIES IF TEMPERATURE EQUALS FUSION TEMPERATURE OF THAT SPECIES.
TEST	VARIABLE IN UNUSED PORTION OF CURRENT PROGRAM VERSION.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE OUPPT

VARIABLE NAME	DESCRIPTION
UPRM	TEMPORARY VALUE OF μ PRIME (CMAR).
FAF	VALUE OF DIFFUSION EXPONENT (GAMEX) PUNCHED OUT ON CARDS.
FLUX	VEL*RHU, MASS FLUX, LBM/FT ² SEC
FSOL	FRACTION OF CONDENSED PHASE SPECIES WHICH IS SOLID, EQUAL TO 1-FLIQ.
GAM	GAM/(GAM+1.)
HBP	SYSTEM ENTHALPY IN BTU/LBM.
HEN	HEN*1.8
EPS	0.01 ALWAYS UNUSED IN PRESENT VERSION OF ROUTINE.
HPPP	HEN/1.8
HKIN	SHOWHPP*1.8, KINETIC ENTHALPY.
HL	ENTHALPY OF LIQUIDS ONLY, BTU/LE.
HFL	ENTHALPY BASED ON Z ^o MASS FRACTIONS (INCLUDES GAMEX DEPENDENCE).
I, J	LOOP INDICES.
IO	INTEGER ARRAY FOR COMPRESSED PUNCHED CARD OUTPUT FORMAT.
KR1	IDENTIFICATION NUMBER FOR PUNCHED CARD OUTPUT.
KR2	SAVED VALUE OF KR1*10.
KSC	FLAG USED ON PUNCHED CARD OUTPUT.
L	LOOP INDEX
M	LOOP INDEX
PMU2	PRESSURE TIMES MU2 OF EQ 22 OF NASA CR-1062
RHO	DENSITY OF GAS PHASE SYSTEM, LBM/FT ³ .
SH1	STATIC ENTHALPY UPSTREAM OF SHOCK WAVE.
SHI	SHOCK ANGLE IN DEGREES.
SI	ENTROPY OF GAS PHASE SPECIES, CAL/EM DEG.K.
SHIP	(HOMO) SYSTEM ENTHALPY, SAVED DURING OUTPUT CALCULATIONS.
SL	ENTROPY OF LIQUIDS, CAL/EM DEG.K.
SPL	SUMMATION OF VN(J) FOR CONDENSED SPECIES
SSIP	SYSTEM ENTROPY SAVED DURING OUTPUT CALCULATIONS, CAL/EM DEG.K.
TIME	VALUE OF TIME SINCE LAST CALL OF ETIME.
TT	SYSTEM TEMPERATURE, DEG. R.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE OHNT

VARIABLE NAME	DESCRIPTION
VELSQ	SQUARE OF FLOW VELOCITY FROM ISENTROPIC EXPANSION OR SHOCK CALCULATIONS.
VKIN	UNUSED VARIABLE IN COMPRESSED CARD FORMAT.
W _G	MOLECULAR WEIGHT OF GAS PHASE SYSTEM.
W _L	MOLECULAR WEIGHT OF LIQUIDS, NOT USED IN PRESENT VERSION OF PROGRAM.
WSD	MAXIMUM VALUE OF W_L / W_G , I.E. WSD PARAMETER USED TO AVOID DIVISION BY ZERO IN CALCULATION OF HIP .
WTLS	SAVED VALUE OF THE SUMMATION $W_N(J) * WTM(J)$ OVER ALL CONDENSED SPECIES.
WTM	MASS OF CONDENSED / MASS OF GAS IN SYSTEM.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE PROPS

VARIABLE NAME	DESCRIPTION
AISTR	1.0 ALWAYS. SEE NASA CR-1063.
ALF	DERIVATIVE OF THE LOG MOLECULAR WEIGHT WITH RESPECT TO LOG TEMPERATURE AT CONSTANT PRESSURE.
AMUS	$VN(I) * WM(I) / (FF(I) * (WDZ - VN(I) * FF(I) * WD7))$ SUMMED OVER ALL SPECIES.
BFTA	DERIVATIVE OF LOG MOLECULAR WEIGHT WITH RESPECT TO LOG PRESSURE AT CONSTANT TEMPERATURE.
CAPC(I)	1.0 ALWAYS, UNUSED IN CURRENT VERSION OF ROUTINE.
CEJ	$VN(I) * C(I) * C(I) * C(I)$ SUMMED OVER ALL BASE SPECIES.
CPHAI(I)	CPH ALWAYS, UNUSED IN CURRENT VERSION OF ROUTINE.
CPE	SPECIFIC HEAT FOR ELECTRON.
CPGPH	SUMMATION OF $VN(I) * CPT(I)$ OVER ALL GAS-PHASE SPECIES.
CPTIL	PROPERTY OF THE GAS MIXTURE WHICH REDUCES TO CPH FOR EQUAL COEFFICIENTS. SEE EQ 26 OF NASA CR-1062.
CSP	SPECIFIC HEAT OF THE EQUILIBRIUM MIXTURE.
DRAM	$4.1868 * 10^4 * SMT(I) / (OMEGA * P)$ REFERENCE DIFFUSION COEFFICIENT INTRODUCED IN APPROXIMATION FOR UNEQUAL DIFFUSION COEFFICIENTS.
FFI	TEMPORARY VALUE OF DIFFUSION FACTOR FOR A SPECIES (GAMEX DEPENDENCE REMOVED).
GAME	$VM-1$.
GAMP	RATIO OF SPECIFIC HEATS (ISENTROPIC EXPONENT).
HF	STATIC ENTHALPY OF GAS AT BOUNDARY-LAYER EDGE.
HMH	TOTAL SYSTEM ENTHALPY.
HTIL	PROPERTY OF THE GAS MIXTURE WHICH REDUCES TO SYSTEM ENTHALPY FOR EQUAL DIFFUSION COEFFICIENTS. SEE EQ. 28 OF NASA CR - 1062.
HTZ	ENTHALPY OF SYSTEM BASED ON Z ⁰ MASS FRACTION (INCLUDES GAMEX DEPENDENCE).
I*IK*IK*	LOOP INDICES
IE	INDEX IDENTIFYING ELECTRON.
II	UNITY ALWAYS, UNUSED IN PRESENT VERSION OF ROUTINE.
ISM	IS-1
OMEGA	$1.0717 / 106.7 * 10^4 * 1.59$ PARAMETER USED IN TRANSPORT PROPERTY CALCULATIONS INTRODUCED IN EUN. (9) NASA CR-1063.
PMUZ	$VN(I) * WM(I) / FF(I) ** GAMEX$ SUMMED OVER ALL SPECIES N _z
PMUJ	$VN(I) * FF(I)$ SUMMED OVER ALL GASEOUS SPECIES N _z EQUALS $VMUI * P$.

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LIST OF FORTRAN VARIABLES
APPEARING IN
SUBROUTINE PROPS

VARIABLE NAME	DESCRIPTION
PMU2	$VN(J) * WTM(J) / FF(J)$ SUMMED OVER ALL SPECIES N, EQUALS $VMU2 * P$.
PMU6	$VN(J) / (FF(J) * (WD4 - VN(J) * FF(J) * WD8))$ SUMMED OVER ALL SPECIES N.
PSP	$((1. + GAME/2. * SQMAK) / (1. + GAME/2. * ACHSQ)) ** (GAM/GAME)$
SC	SCHMIDT NUMBER
TCOND	MIXTURE THERMAL CONDUCTIVITY
TMU3	$VN(J) / FF(J)$ SUMMED OVER ALL SPECIES N.
TT	STATIC TEMPERATURE IN DEGREES RANKINE.
VR	LOCALLY DEFINED VARIABLE.
VC	$VN(I) * FF(I)$
VI(K)	ELEMENTAL MASS FRACTION OF K TH ELEMENT.
VK(K)	MASS FRACTION OF K TH BASE SPECIES.
VMU	MIXTURE VISCOSITY
VMU1	COEFFICIENT MU1 DEFINED IN EQ. 22 OF NASA CR-1062.
VMU3	PROPERTY OF THE GAS MIXTURE WHICH REDUCES TO 1/WH FOR EQUAL DIFFUSION COEFFICIENTS; EQN. (26) NASA CR-1062.
VMU6	CONTRIBUTION TO MIXTURE THERMAL CONDUCTIVITY GIVEN BY (PMU6 * (PTIL / (.9869 - 2.5 * TMU3)) / P.
VMU12	PRODUCT OF THE TWO COEFFICIENTS MU1 AND MU2 DEFINED IN EQN. (22) OF NASA CR-1062.
WD2	$1.62 * A * STAR / PMU1$
WD4	$.244 * WMU2$
WD5	$0.32 * A * STAR / PMU1$
WD7	$WDZ / (PMU1 * WMU2)$
WD8	$WD4 / (PMU1 * WMU5)$
WDZ	CONSTANT .3385 WHICH ENTERS INTO CALCULATION OF MIXTURE TRANSPORT PROPERTIES.
WTE	WTM(I) FOR THE ELECTRON.
ZI(K)	QUANTITY FOR ELEMENT K WHICH IS INTRODUCED AS A RESULT OF THE APPROXIMATION FOR BINARY DIFFUSION COEFFICIENTS AND REDUCES TO VI(K) FOR EQUAL DIFFUSION COEFFICIENTS; SEE EQ 25 OF NASA CR-1062.
ZK(K)	QUANTITY FOR BASE SPECIES WHICH IS INTRODUCED AS A RESULT OF THE APPROXIMATION FOR BINARY DIFFUSION COEFFICIENTS AND REDUCES TO VK(K) FOR EQUAL DIFFUSION COEFFICIENTS; SEE EQ 25 OF NASA CR-1062.

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LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE WERY

VARIABLE NAME	DESCRIPTION
C	MATRIX TO BE INVERTED.
D	SET OF CONSTANT VECTORS CONVERTED TO SOLUTION VECTORS.
DIV	ROW NORMALIZING FACTOR IN GAUSSIAN ELIMINATION.
DIVC	PRODUCT OF DIV AND ELEMENT OF ROW.
I,II,J	LOOP INDICES.
IS	FLAG IN ARGUMENT TO CONTROL DEBUG OUTPUT OR NONCONVERGENCE FLAG RETURN.
IX	FLAG USED IN DIAGNOSTIC OUTPUT.
JJ,K	LOOP INDICES.
K	TEMPORARY VALUE OF ϵ .
KOUT	PRINTED OUTPUT TAPE DESIGNATION.
L(N)	INDEX OF COLUMNS DURING INVERSION.
LL(N)	ROW INDEX OF PIVOT FOR N TH COLUMN.
LLC(N)	COLUMN INDEX OF PIVOT FOR N TH ROW.
LS	INDEX USED TO REARRANGE COLUMNS.
M	LOOP INDEX.
N	NUMBER OF ROWS IN C_1 .
NN	$N-1$.
NN	NUMBER BY WHICH COLUMNS EXCEED ROWS IN C_1 .
NP	$N+NN$.
NI	$N+1$.
NNN	NUMBER OF COLUMN VECTORS IN D .
S(N)	LARGEST CONTRIBUTION TO TERM IN N TH COLUMN.
SD(N)	RATIO OF RESIDUAL TERM IN N TH COLUMN TO S(N).

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LIST OF FORTRAN VARIABLES
APPEARING IN
SUBROUTINE SCALE

VARIABLE NAME	DESCRIPTION
ABX	ABSOLUTE VALUE OF LOG CORRECTION ON TEMPERATURE.
BULP	ALOG (BUMP).
BUMP	MAXIMUM VN PERMITTED AFTER ONE ITERATION OF ANY SPECIES PREVIOUSLY LESS THAN DUMP
CLIM	CONSTRAINT PARAMETER RELATED TO TOTAL ABLATION RATE.
CLIP	ABS(CLIM/WFM11)
CMF	THE VALUE OF CMF AFTER CONSIDERATION OF CONSTRAINTS ON THE CONNECTION TO THE PARTIAL PRESSURE OF THE J TH SPECIES.
DTM	LIMIT VALUE OF DELTA (I./T).
DUMP	$P_0(10^{**}-7)$. LIMIT PRESSURE IN CONTROLLING DAMPING OF SOLUTION.
DWTG	CORRECTION TO GAS MOLECULAR WEIGHT.
DWTL	CONNECTION TO CONDENSED-PHASE MOLECULAR WEIGHT.
DYI	VALUE OF DY FOR THE J TH SPECIES DURING LOOP ON THAT SPECIES.
I,K,J,K	LOOP INDICES.
JA	SAVED VALUE OF IB(J).
L	NUMBER OF ELEMENTS INCLUDING ELECTRON PLUS THE NUMBER OF NON BASE, PRESENT CONDENSED SPECIES PLUS 2.
LIM	LOOP LIMIT = N (TOTAL NUMBER OF SPECIES).
LL	ALWAYS EQUALS 1.
M	LOCAL INDEX EQUAL TO IB(N).
NI	COUNT ON PRINCIPAL SPECIES AFTER ORDERING IB.
NVL	CONSTRAINT PARAMETER RELATED TO TOTAL ABLATION RATE.
TM	MAXIMUM OR MINIMUM TEMPERATURE IF DELTA T IS POSITIVE OR NEGATIVE, RESPECTIVELY.
XI	DAMPED VALUE OF DELTA LOG T.

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE SWAP

VARIABLE NAME	DESCRIPTION
A	OUTPUT MATRIX
R	OUTPUT VECTOR
I, J	LOOP INDICES
SI	INPUT MATRIX
SL	INPUT VECTOR

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE SWEE

VARIABLE NAME	DESCRIPTION
	INPUT NUMBER
R	WORKING VARIABLE FOR FINDING DIGITS TO BE SAVED
I	INTEGER ARRAY FOR ROOTS - OUTPUT
NC	NUMBER OF COLUMNS IN FIELD
INUS	DATA ASSIGNED THE SYMBOL IN*
INP	DATA ASSIGNED THE SYMBOL IN*

LIST OF FORTRAN VARIABLES
 APPEARING IN
 SUBROUTINE THERM

VARIABLE NAME	DESCRIPTION
BC(N)	IDENTICAL TO THE VARIABLE IC(I) EXCEPT N APPLIES ONLY TO THE BASE SPECIES.
BCK	IDENTICAL TO THE VARIABLE VCK(J) EXCEPT N APPLIES ONLY TO THE BASE SPECIES.
I	LOOP INDEX.
IK	LOOP INDEX.
IK(I)	ALPHANUMERIC ARRAY USED IN PRINTOUT OF REACTION KINETICS DATA.
IKY	ALPHANUMERIC QUANTITY USED IN PRINTOUT OF REACTION KINETICS DATA.
IV	REACTANT OR PRODUCT STOICHIOMETRIC COEFFICIENTS.
J	LOOP INDEX.
K	LOOP INDEX.
LINE(I)	PRINTOUT QUANTITY SPECIFYING STOICHIOMETRIC COEFFICIENTS FOR REACTION KINETICS.
M	LOOP INDEX
PIN	PRESSURE * (10**3).
RT	UNIVERSAL GAS CONSTANT * TEMPERATURE, CAL/MOLE.
TFMAX	FLAG TO INDICATE THAT AT LEAST ONE CONDENSED PHASE SPECIES IS AVAILABLE FOR SURFACE EQUILIBRIUM CALCULATIONS.
VR,VL	INTERPOLATION VALUES USED TO EVALUATE THERMODYNAMIC PROPERTIES FROM CURVE FIT CONSTANTS. BOTH ARE FUNCTIONS OF CURRENT TEMP.
VD,VE	INTERPOLATION VALUES USED TO EVALUATE THERMODYNAMIC PROPERTIES FROM CURVE FIT CONSTANTS. BOTH ARE FUNCTIONS OF CURRENT TEMP.

LIST OF FORTRAN VARIABLES
APPEARING IN
SUBROUTINE ZIPIN

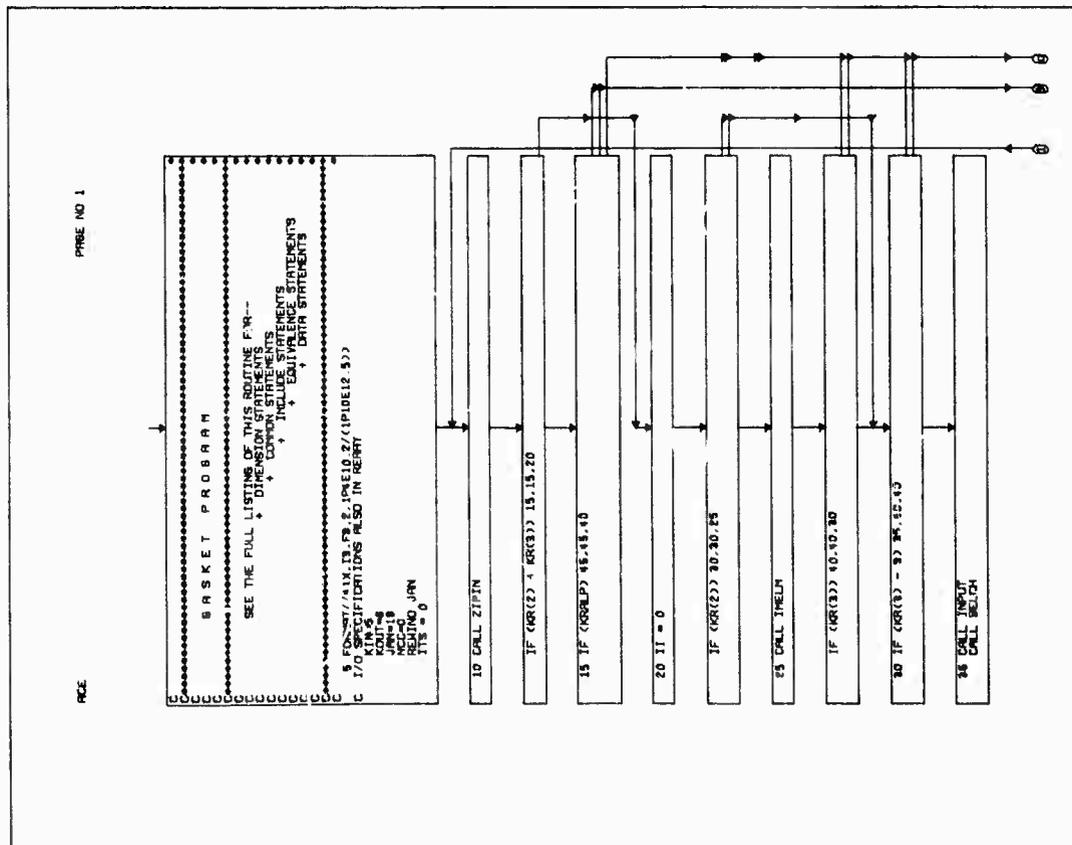
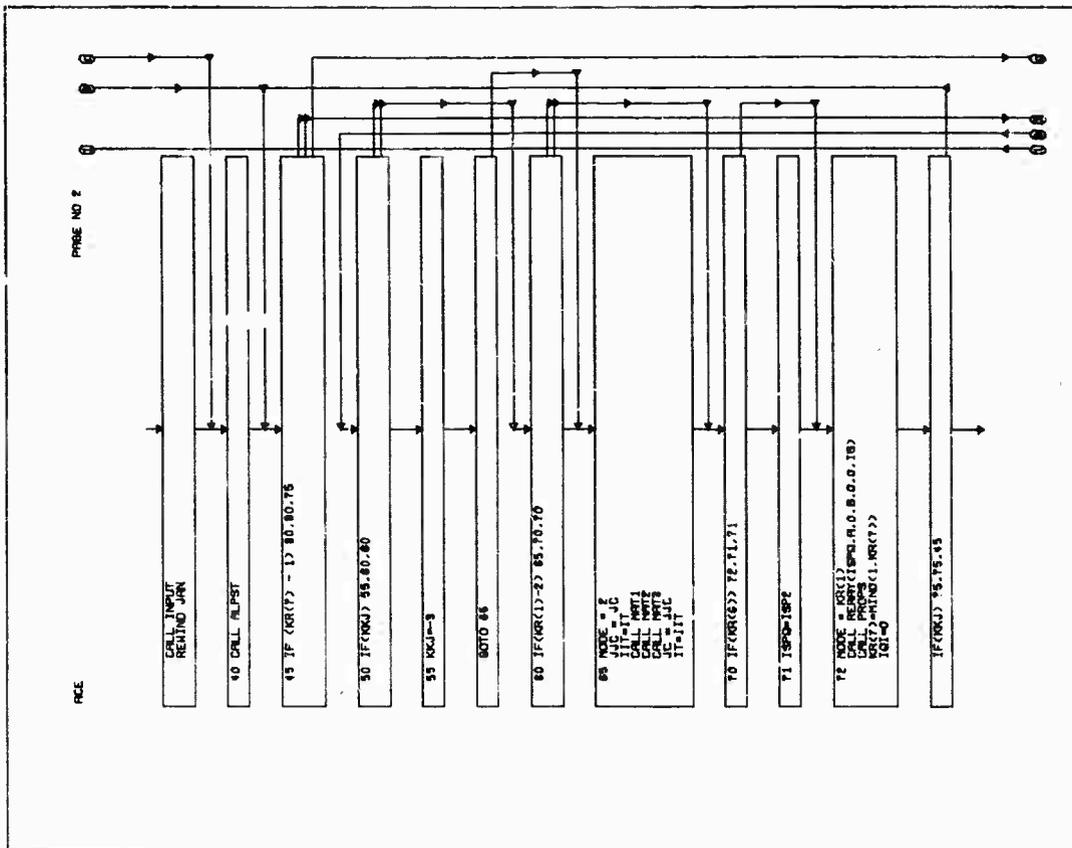
VARIABLE NAME	DESCRIPTION
GAM	GAM-1.
GAMR	TEMPORARY VALUE OF DIFFUSION EXPONENT. IF GAMR = 0 THEN GAMEX = GAMER.
HSP	INPUT STATIC ENTHALPY UPSTREAM OF SHOCKWAVE.
HTR	INPUT TOTAL ENTHALPY UPSTREAM OF SHOCKWAVE.
I	LOOP INDEX.
IIT	VARIABLE USED IN INTEGER LOGIC TO DISCOVER THE SMALLEST INTEGER MULTIPLIER OF 500 DEG. K.
IK	LOOP INDEX.
KR4	VALUE OF KR(4) SAVED TO COMPARE WITH SUBSEQUENTLY READ VALUE OF KR(-).
KRR	SAVED VALUE OF KR(8).
KV	FLAG INDICATING HOW VELOCITY AND STATIC AND TOTAL ENTHALPIES ARE CALCULATED UPSTREAM OF SHOCKWAVE.
PR	TEMPORARY VALUE OF PRESSURE. IF PR NOT EQUAL TO 0, ASSIGN P = PR.
PR1	INPUT PRESSURE UPSTREAM OF SHOCKWAVE.
PSV	SAVED VALUE OF CHAMBER PRESSURE.
RECORD	240 CHARACTERS OF TITLE INFORMATION (3 CARDS).
RHO	INPUT DENSITY UPSTREAM OF SHOCKWAVE.
U	INPUT FLOW VELOCITY UPSTREAM OF SHOCKWAVE.
WR	TEMPORARY VALUES OF RELATIVE COMPONENT MASSES. IF WR(1) + WR(2) + WR(3) NOT EQUAL TO 0, THEN ASSIGN W = WR.
Z	TEMPORARY VALUE OF THERMODYNAMIC VARIABLE. IF Z NOT EQUAL TO 0 ASSIGN I = Z OR HIP = Z DEPENDING ON OPTION BEING EMPLOYED.

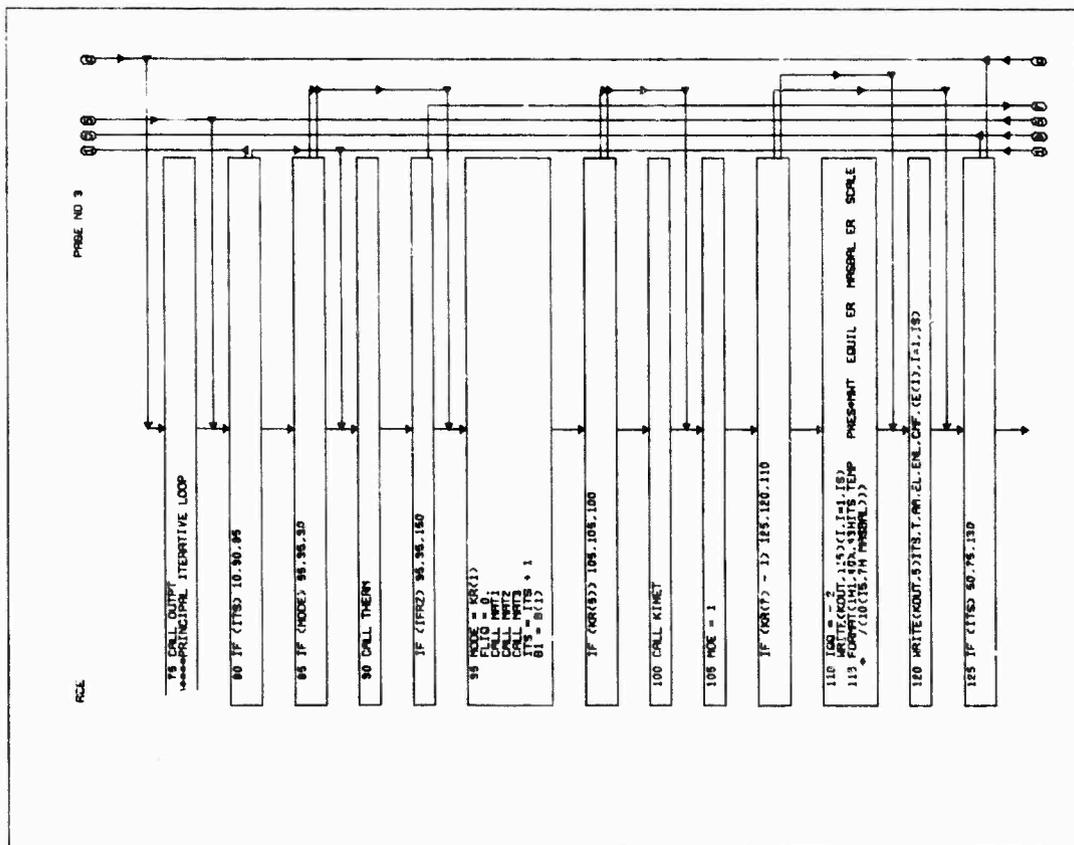
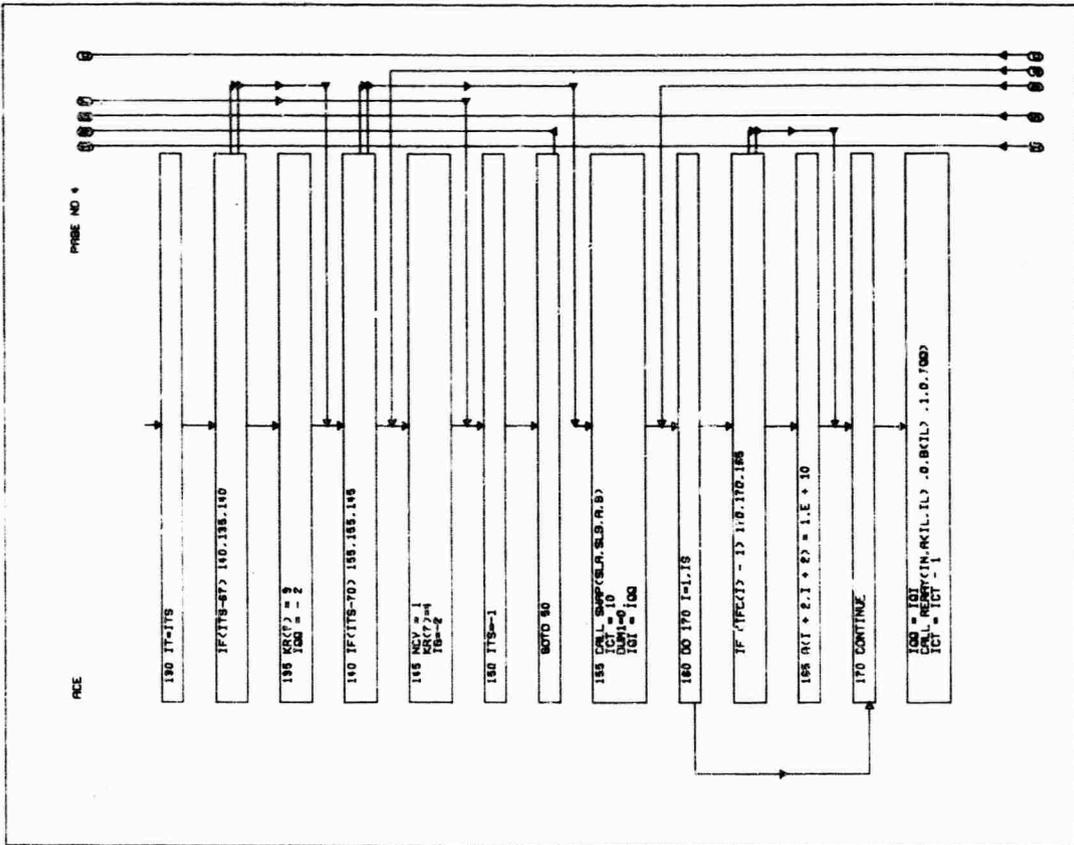
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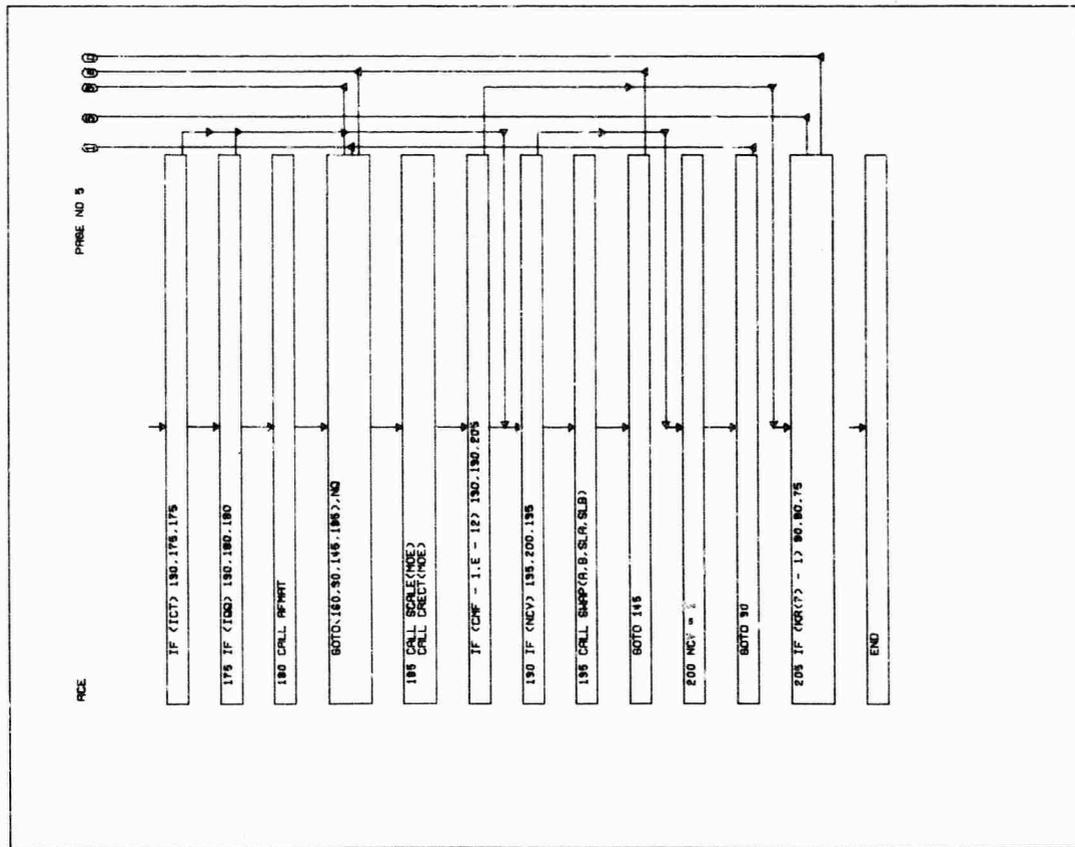
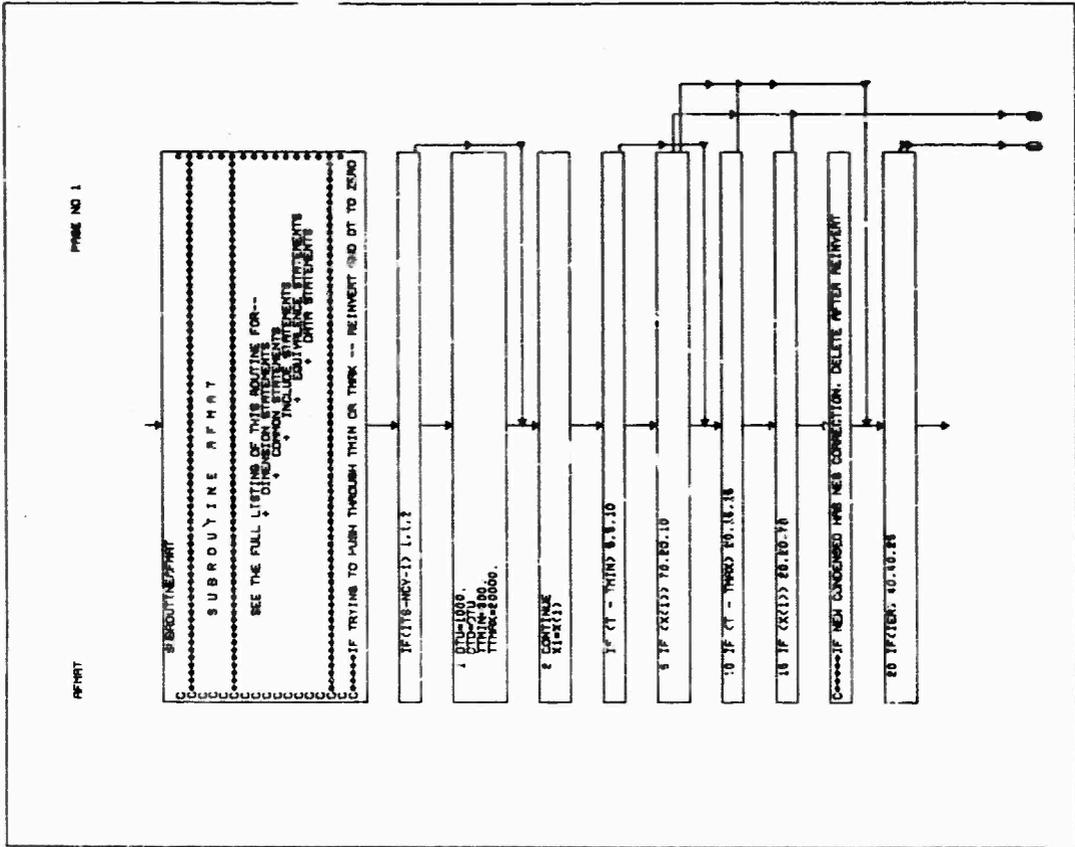
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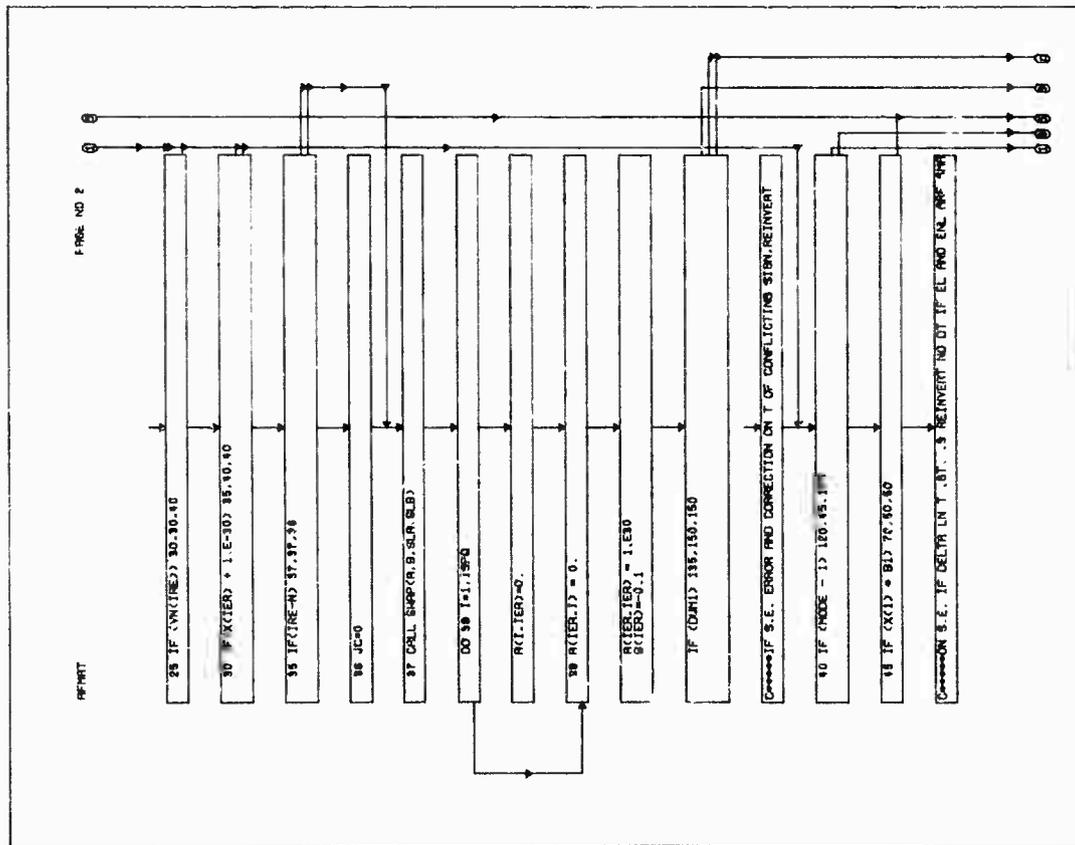
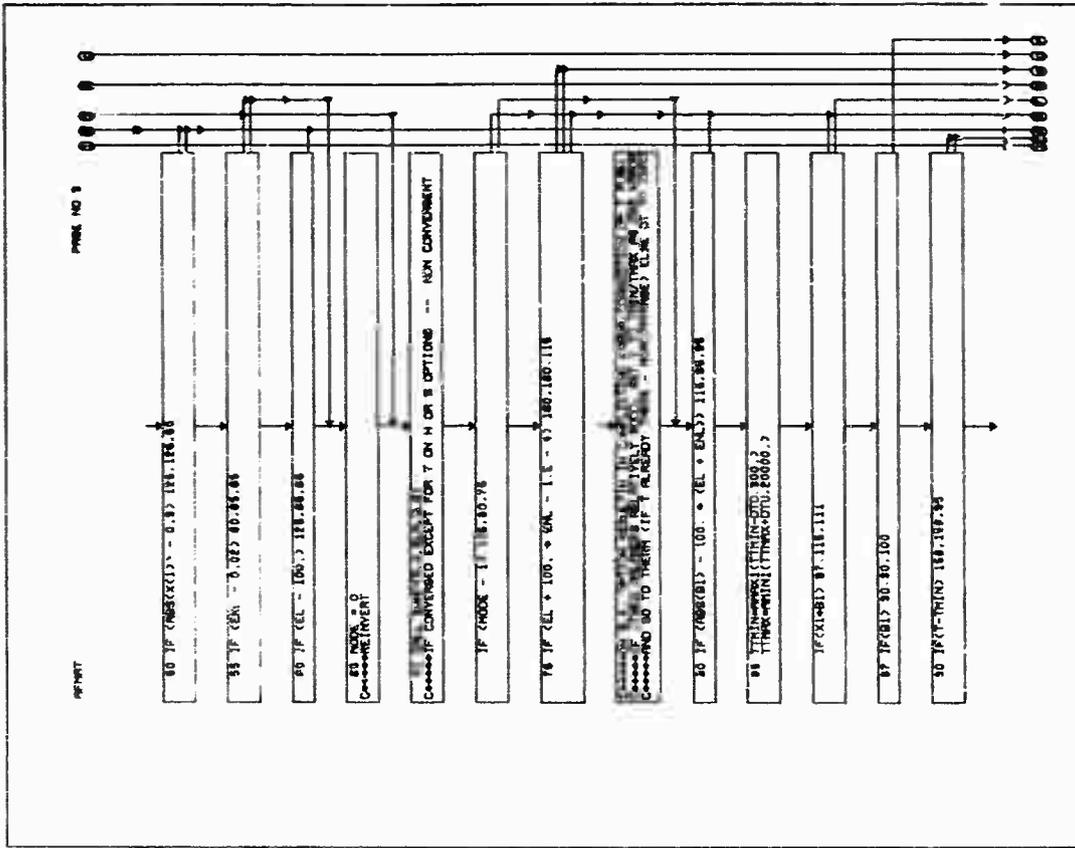
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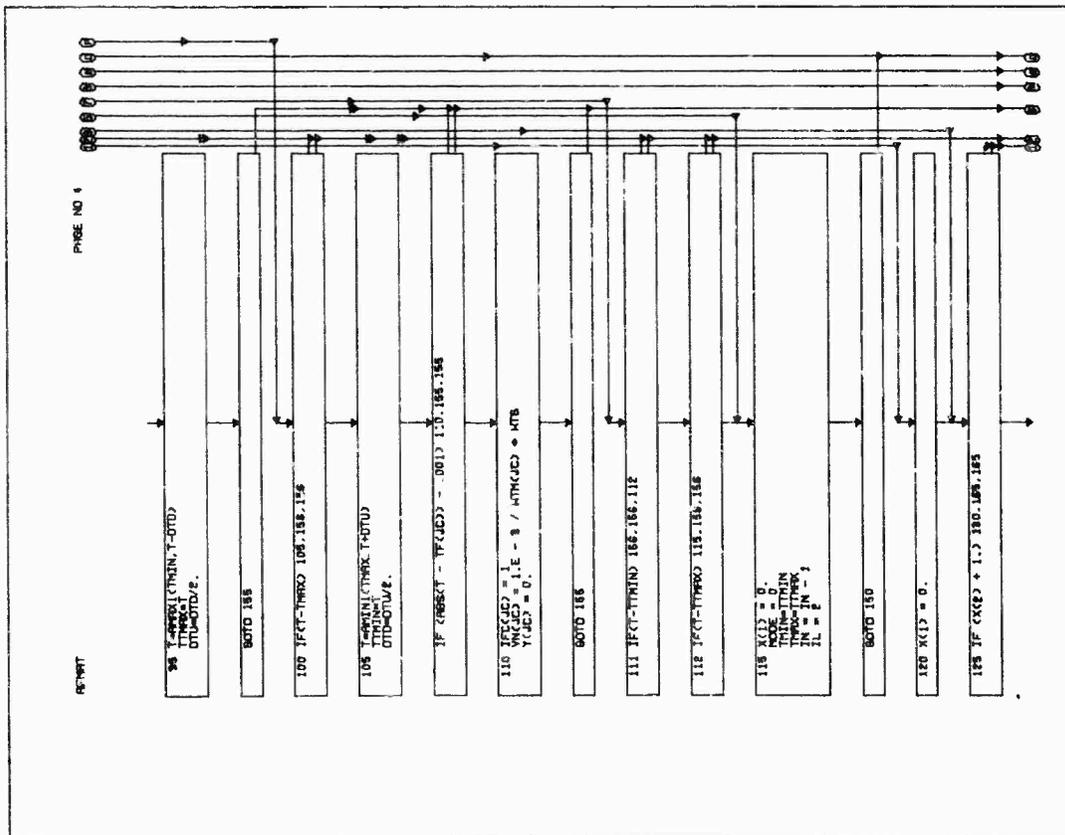
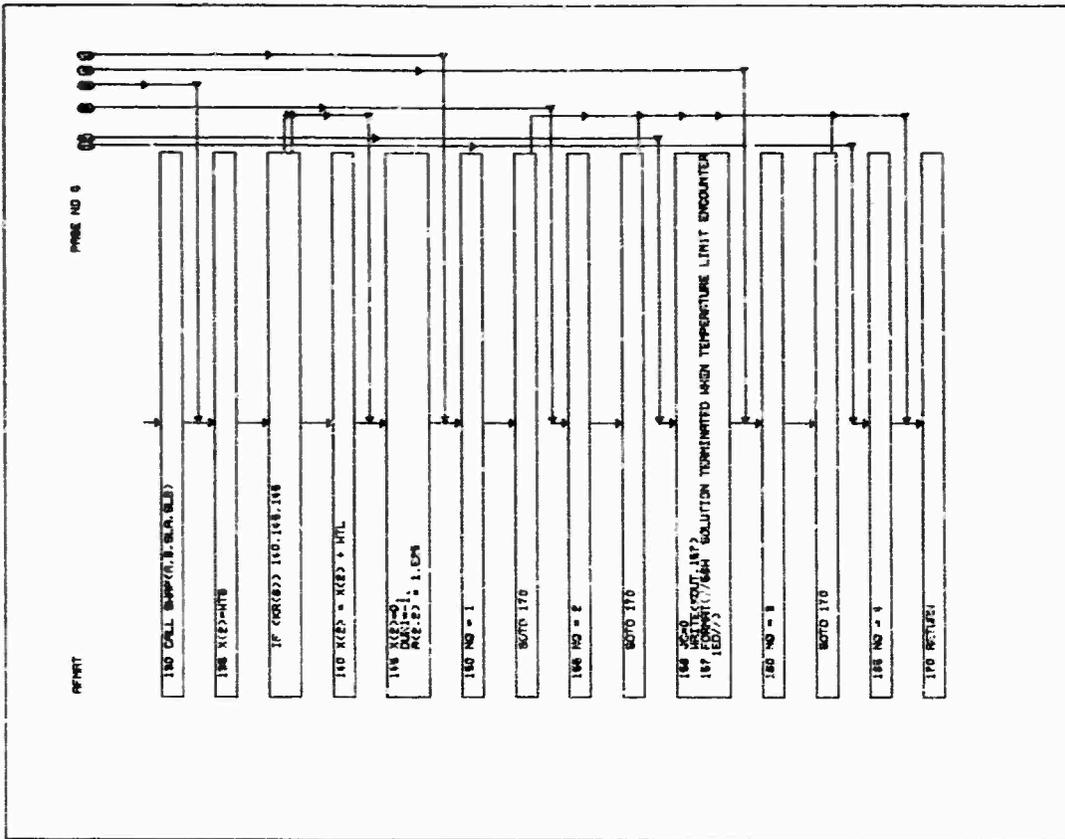
Computer generated flow charts were produced and are given in this Section. The flow charts show transfers as lines on the right edge of the figures and do-loop blocks as lines on the left edge of the figures. The order of presentation corresponds to that used in Section 2 for Fortran variable name definitions.











ALPST

PAGE NO 1

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SUBROUTINE ALPST
SUBROUTINE ALPST
SEE THE FULL LISTING OF THIS ROUTINE FOR --
DIMENSION STATEMENTS
COMMON STATEMENTS
INCLUDE STATEMENTS
CAUTION STATEMENTS
DATA STATEMENTS
*****
10 CONTINUE, ELI = 8PM, ELS = 8PM, ELS = 8PM, ELS = 8PM
IN FACTOR, UPDATE OF DIFFUSION FRACTION, IS, MP, ELS, X, H, P, Y, U, I, D
20 CONTINUE, I = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10
30 CONTINUE, I = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10
40 CONTINUE, I = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10
DATA MP, I, J, K, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z
TYPE = 20000
*****

```

IF (KOR) = 73 85, 10, 10

85 IF (MP) 10, 10, 85

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10 TIME = TIME + TIME

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IF (MP) = MP, 10, 10, 85

85 IF (MP) = MP, 10, 10

8010 85

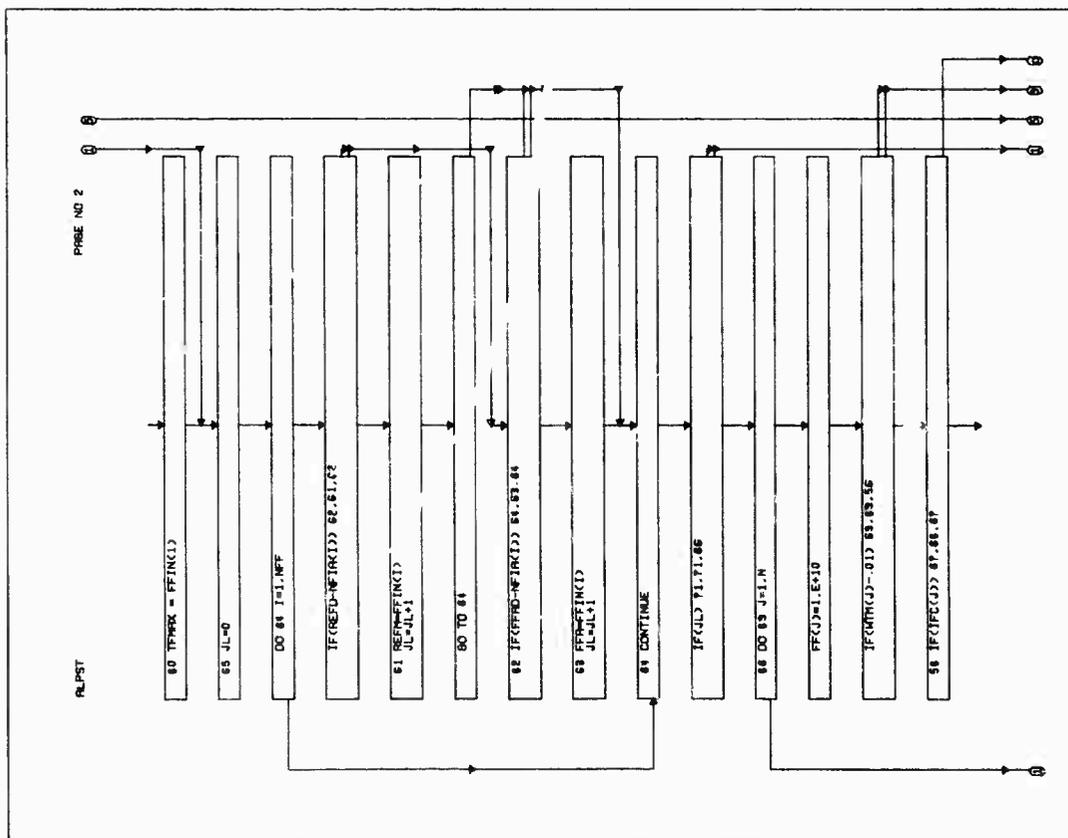
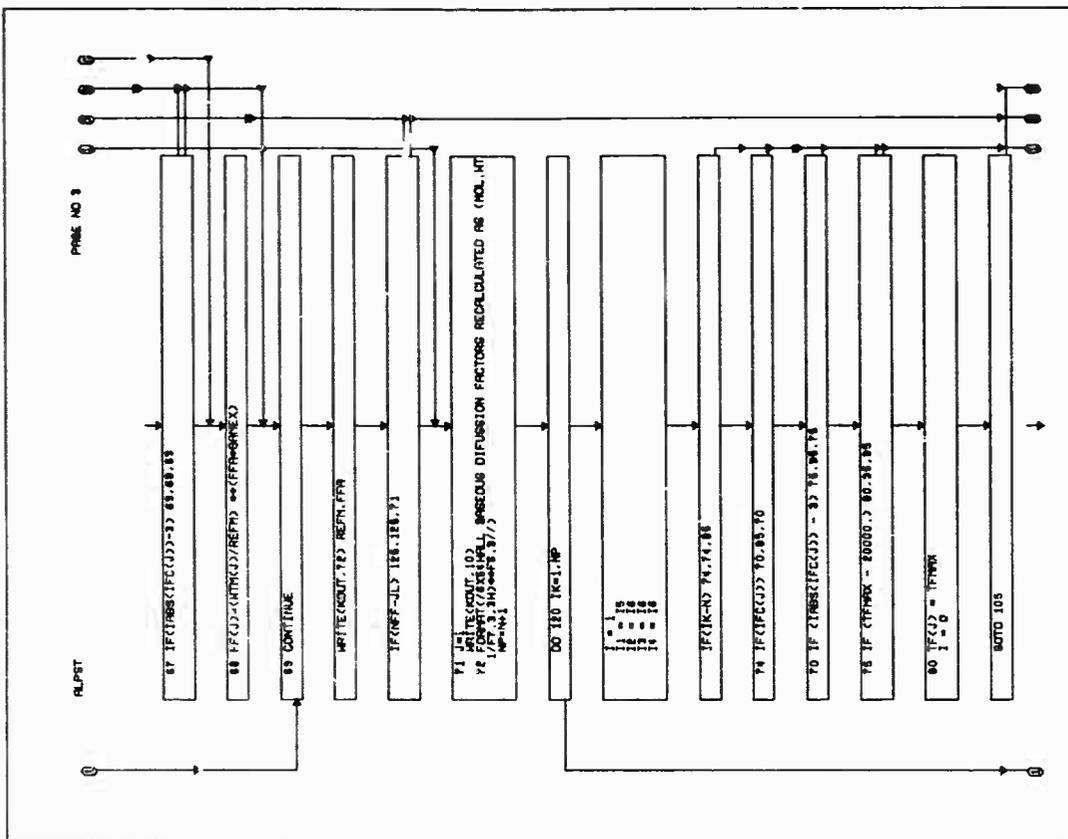
85 TIME = 1

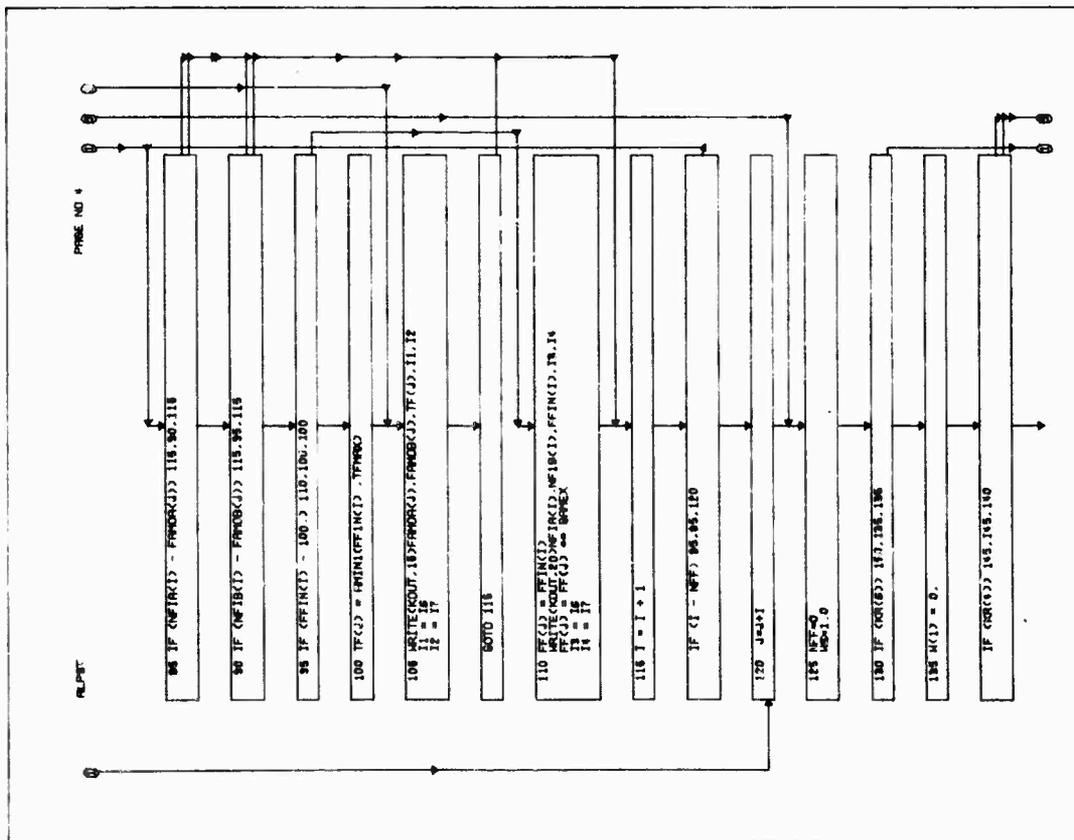
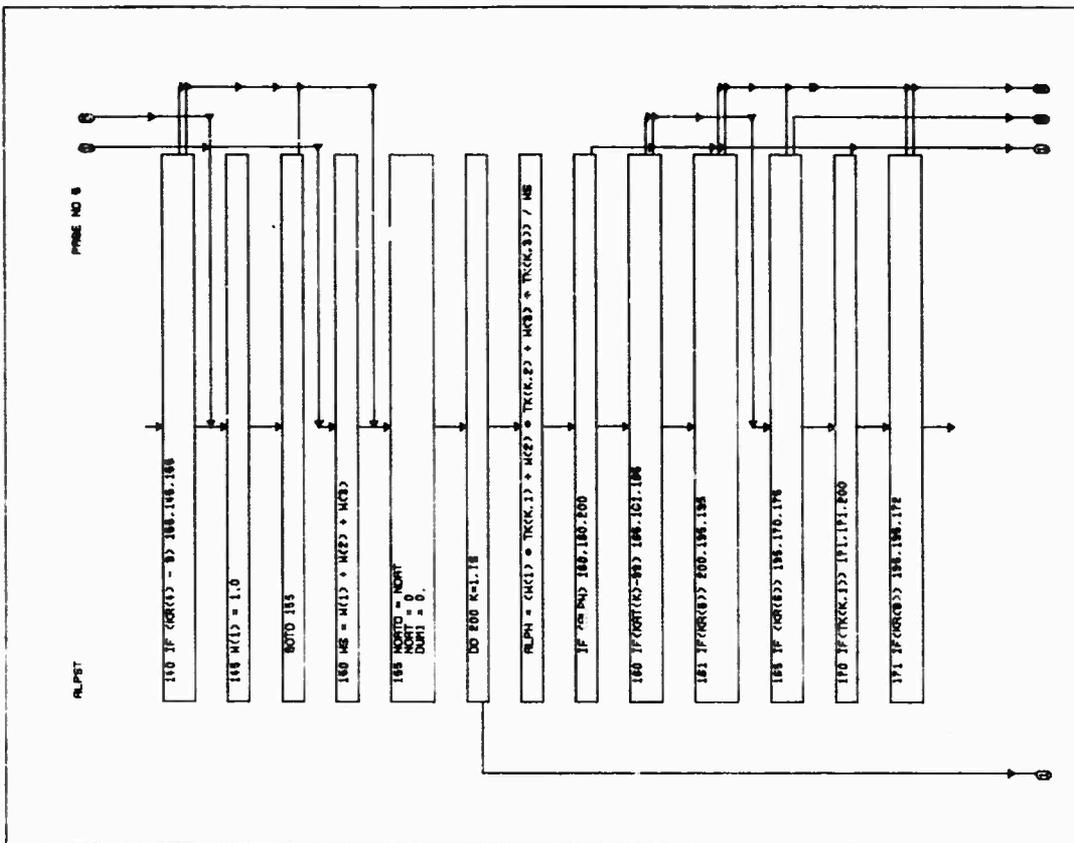
IF (MP) = MP, 10, 10, 85

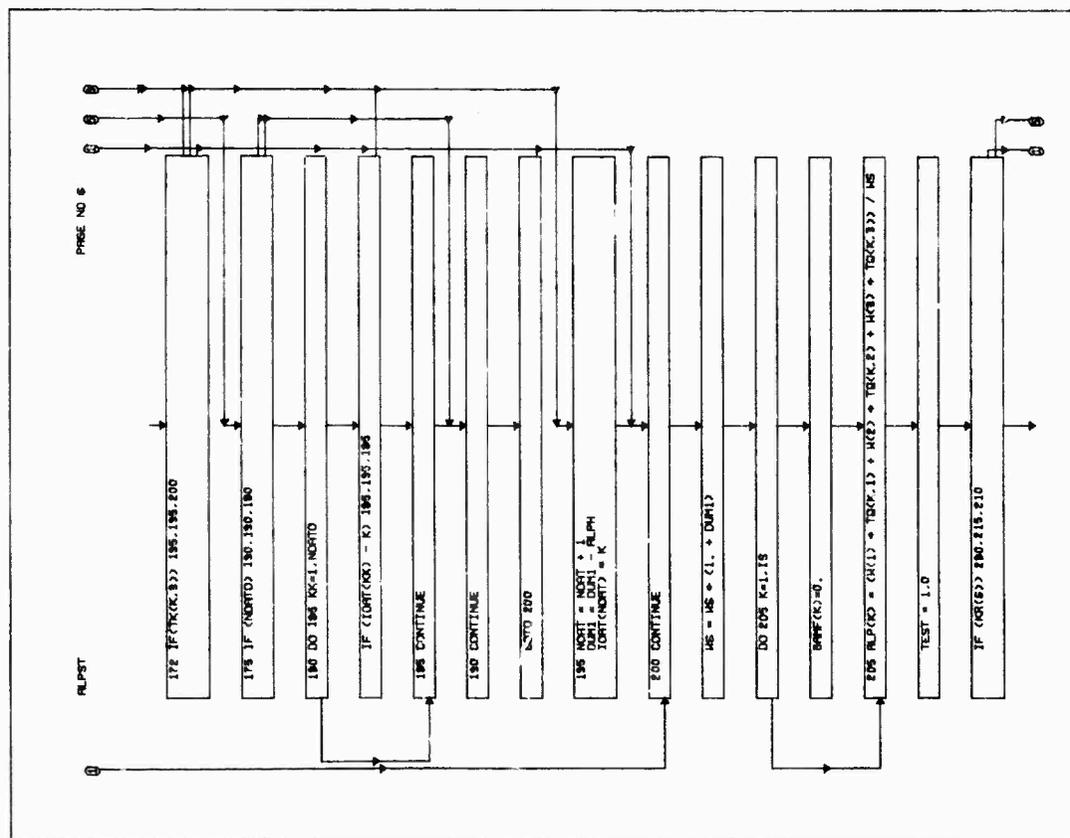
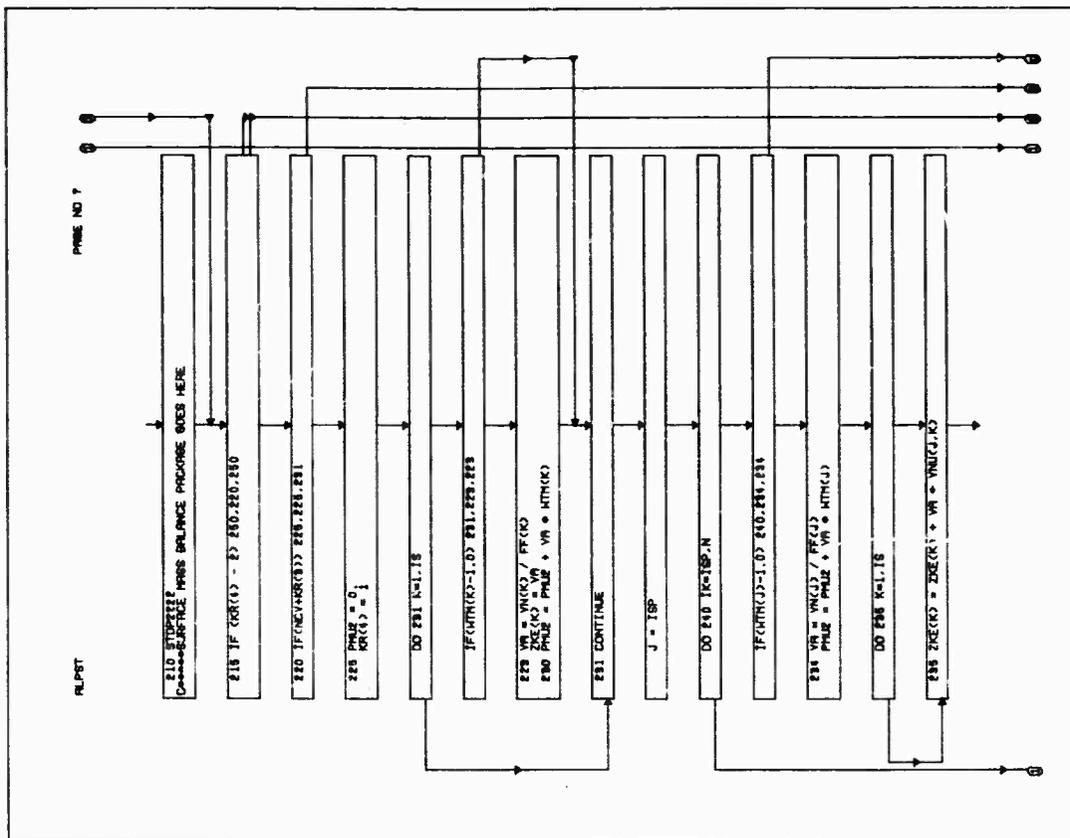
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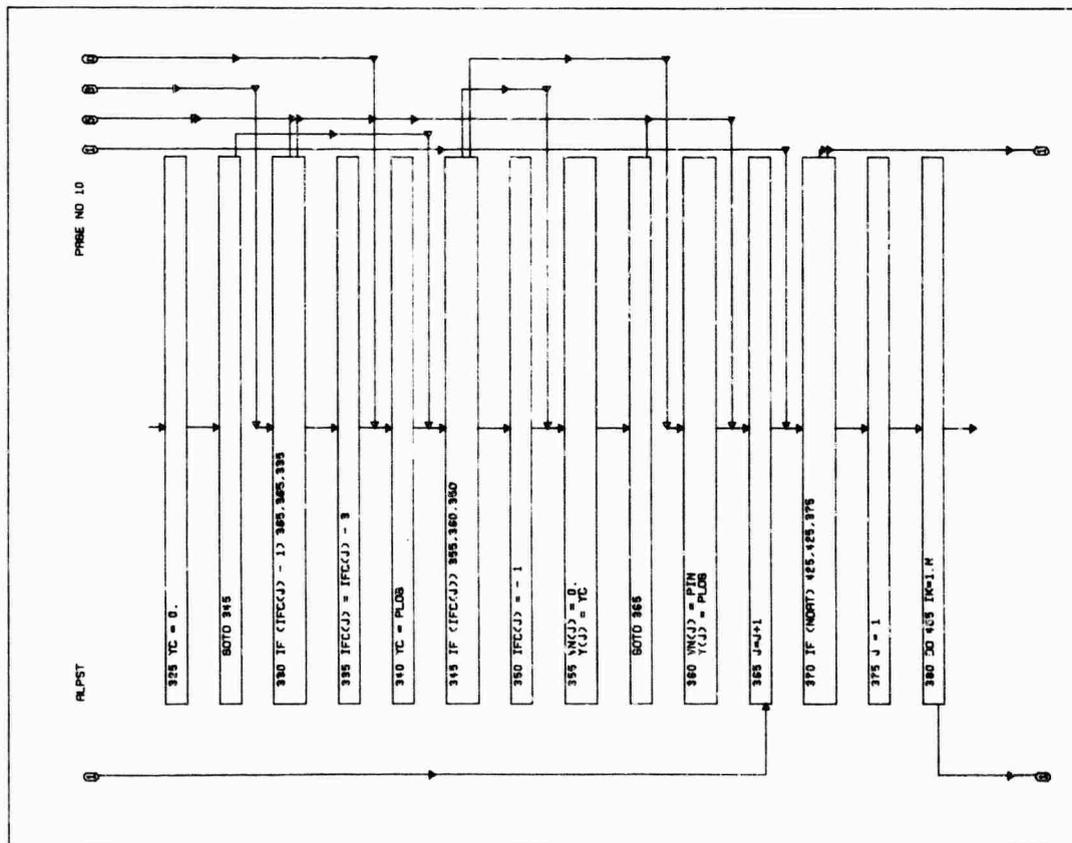
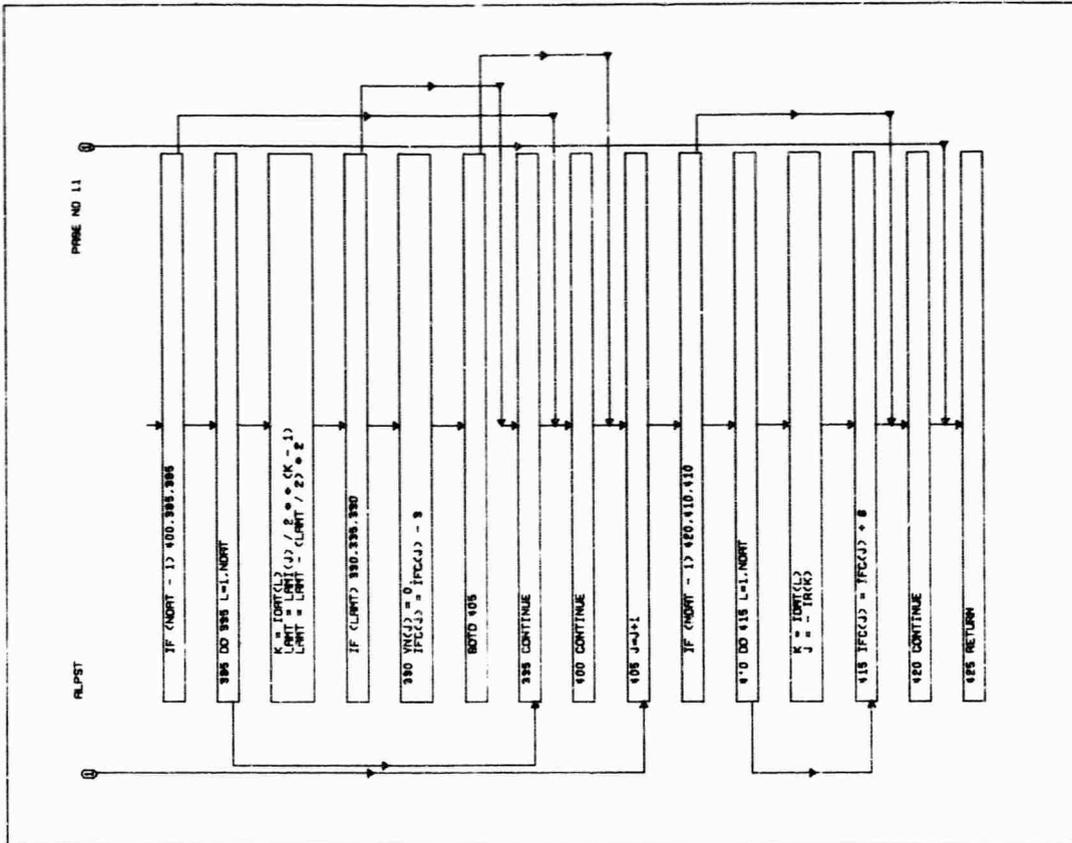
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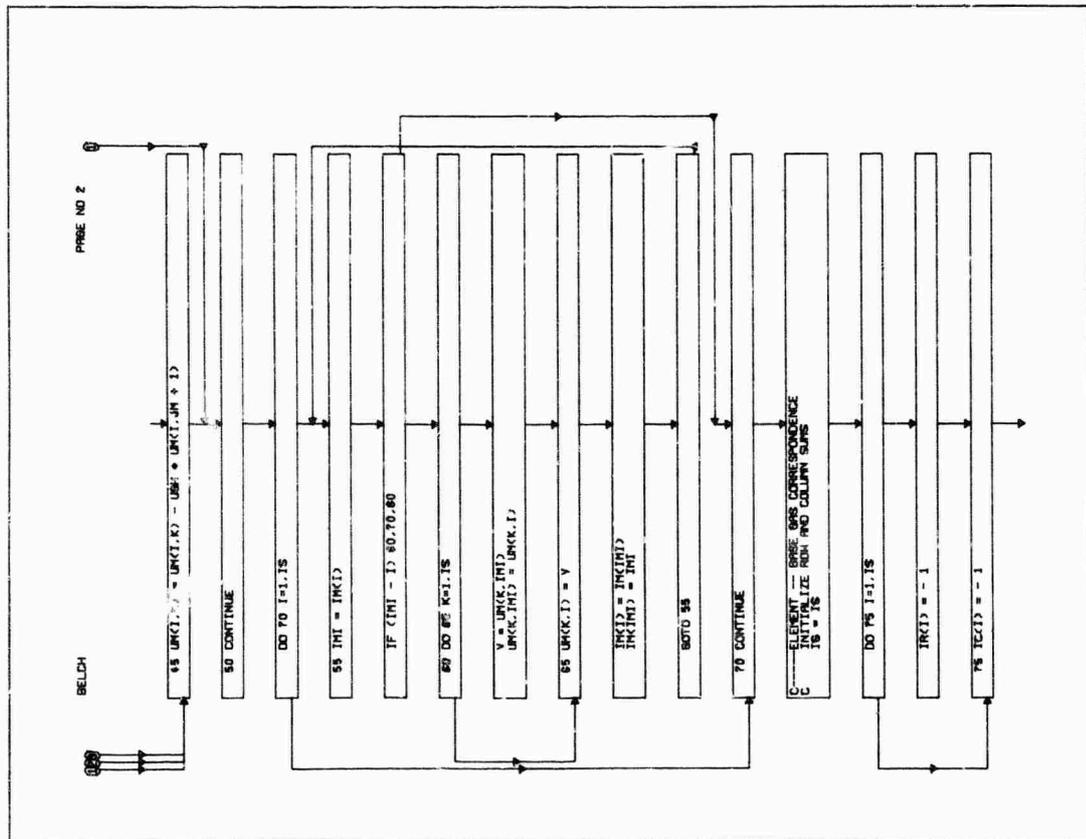
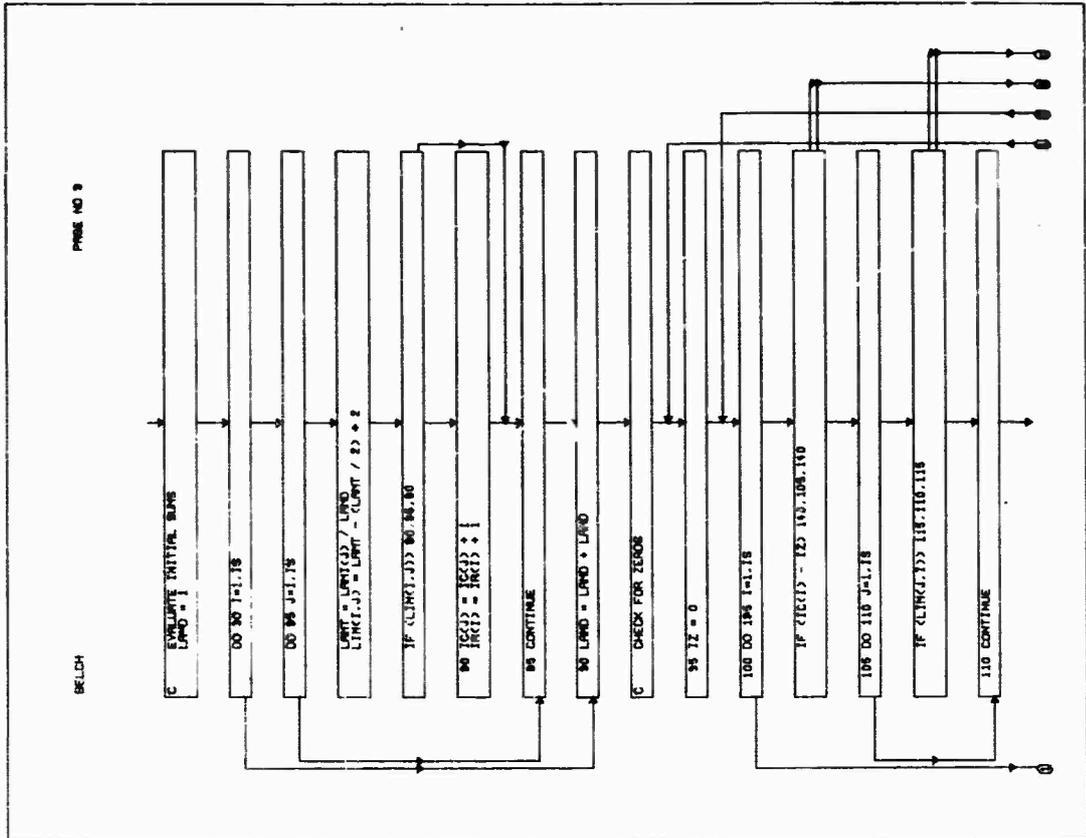
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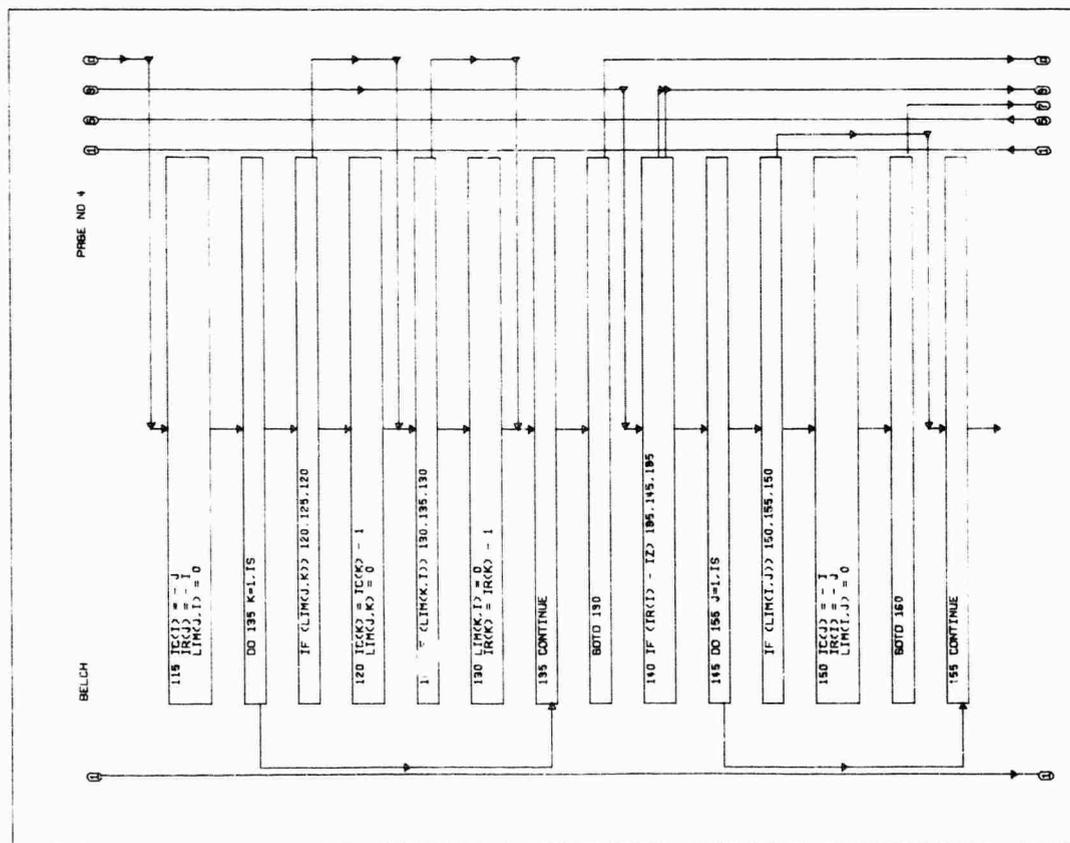
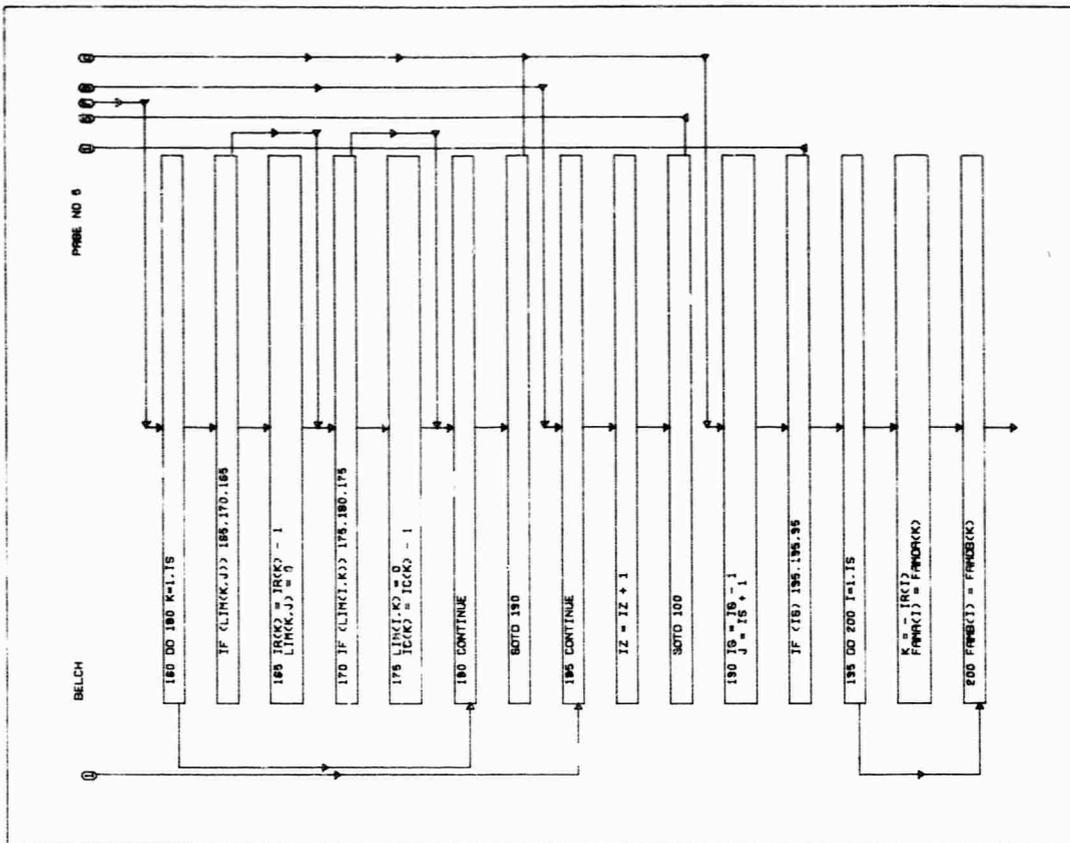


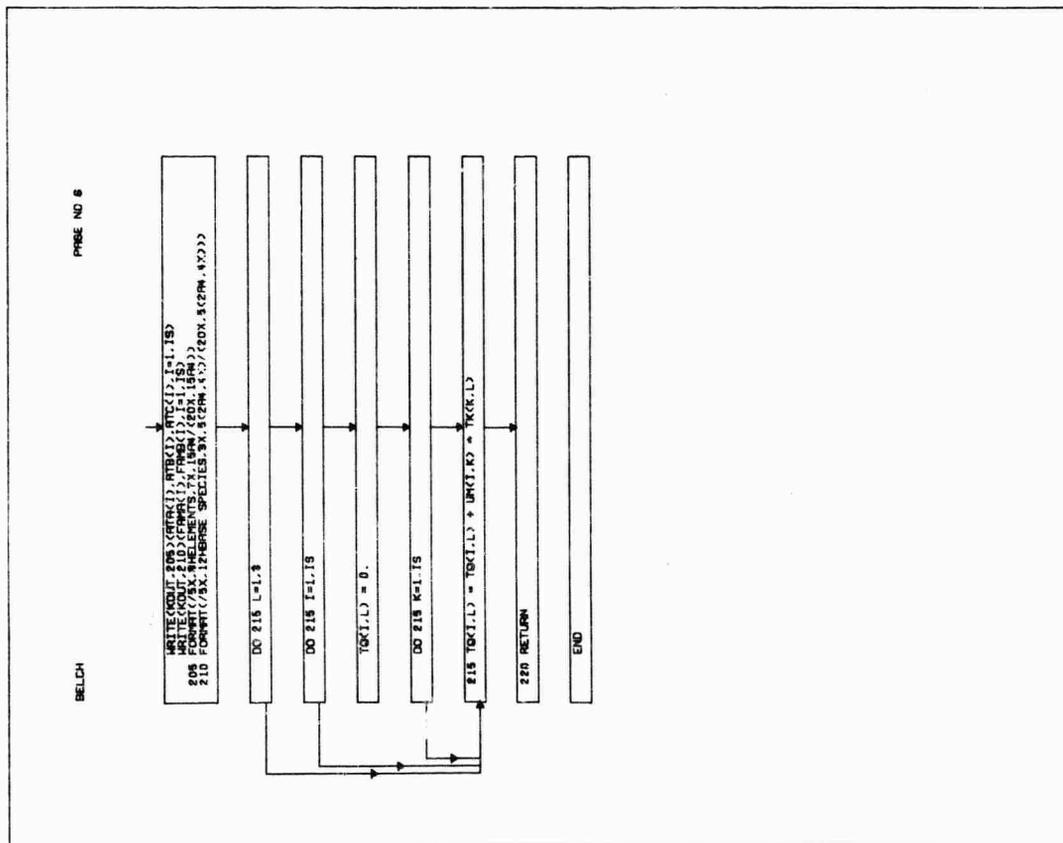
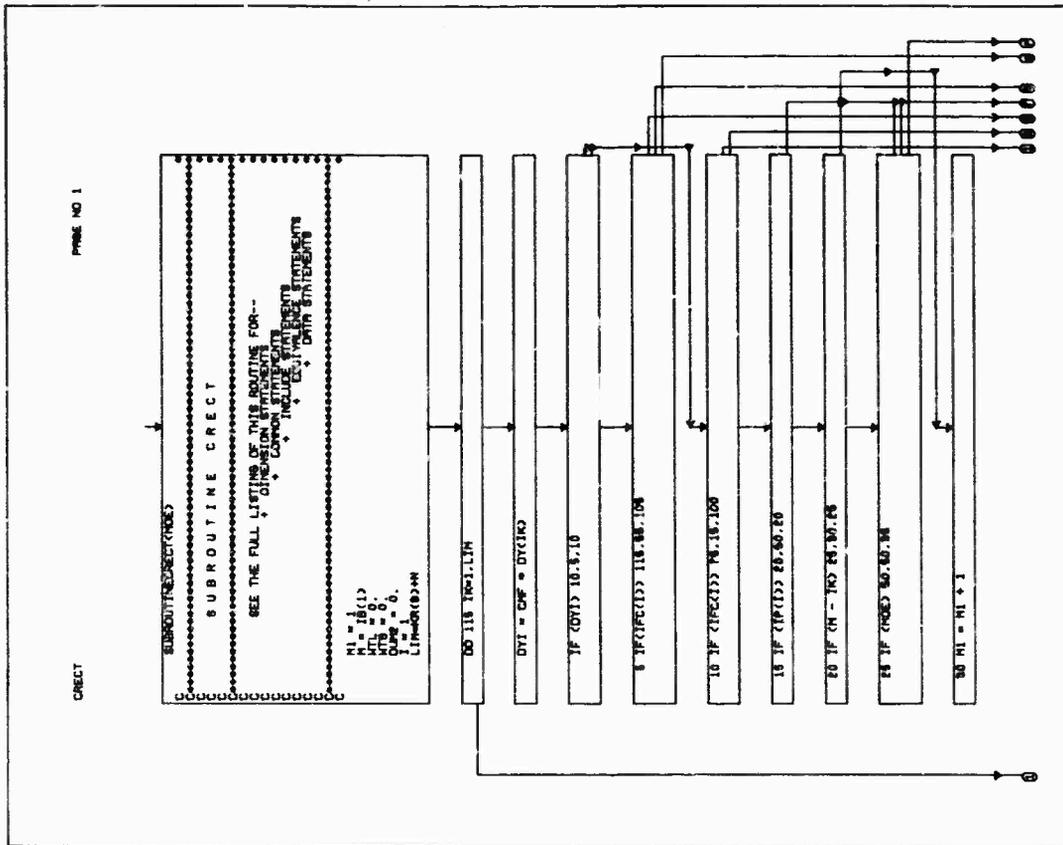


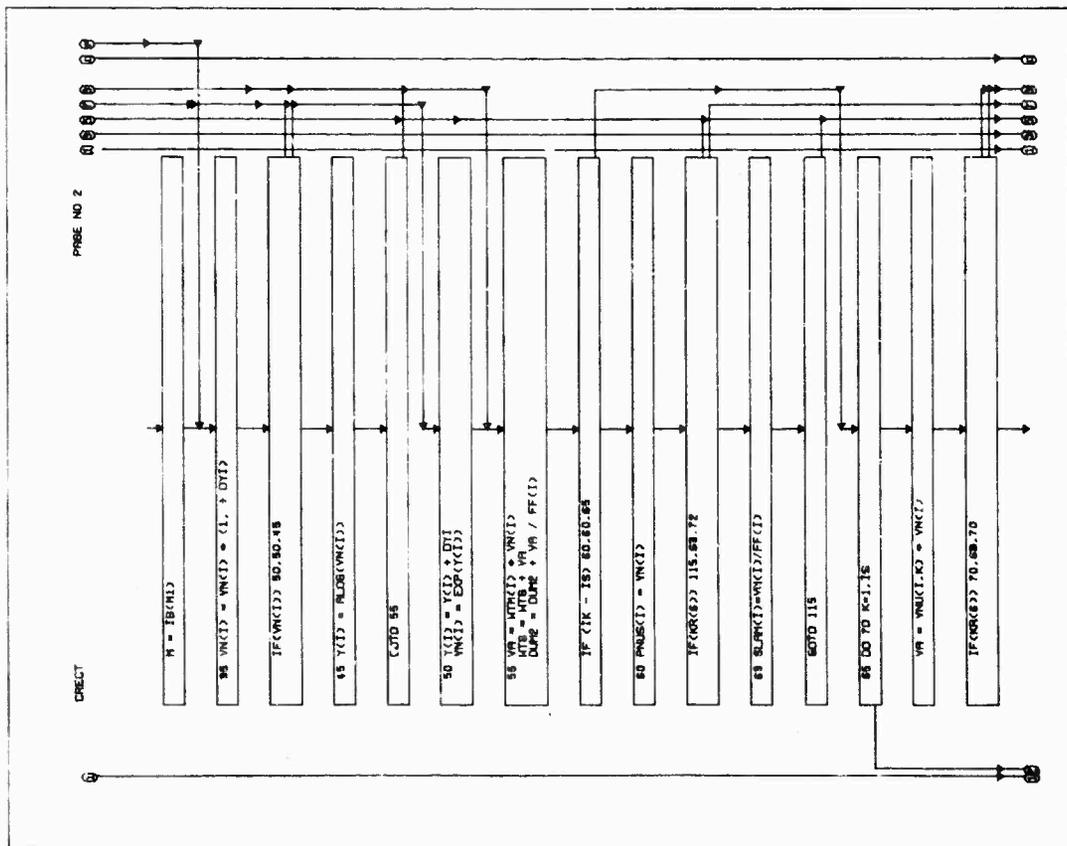
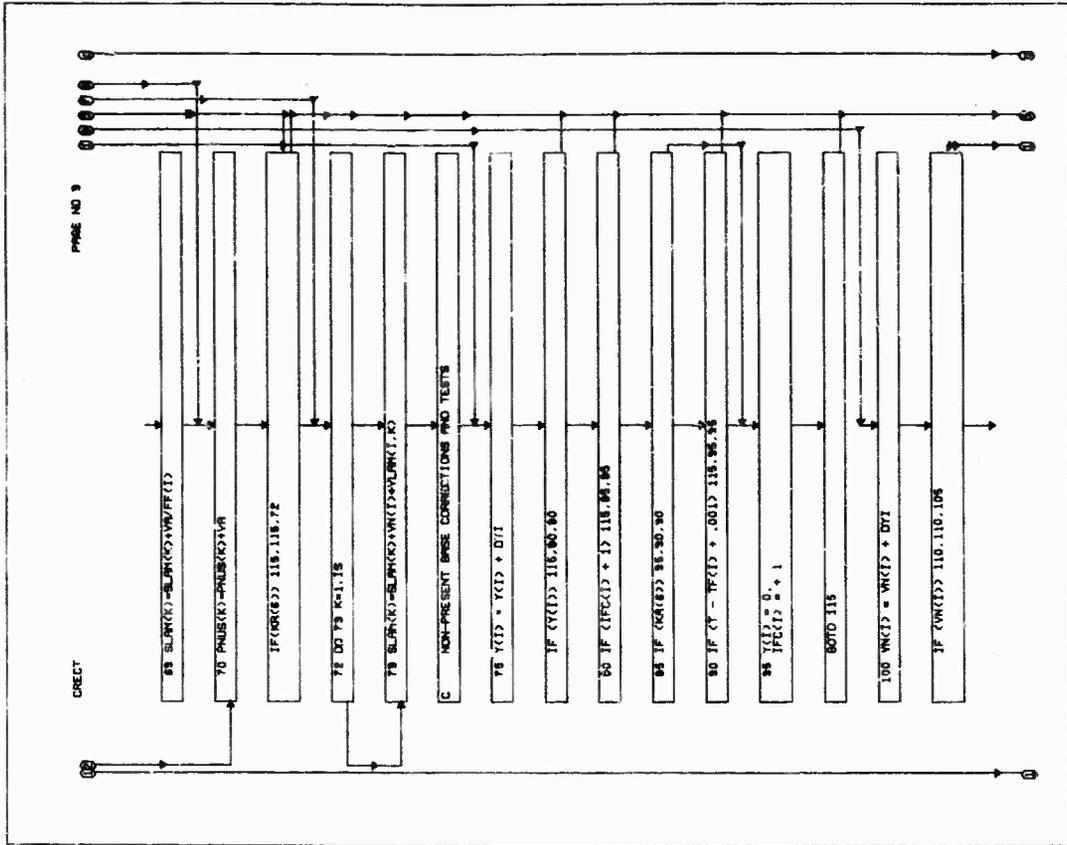


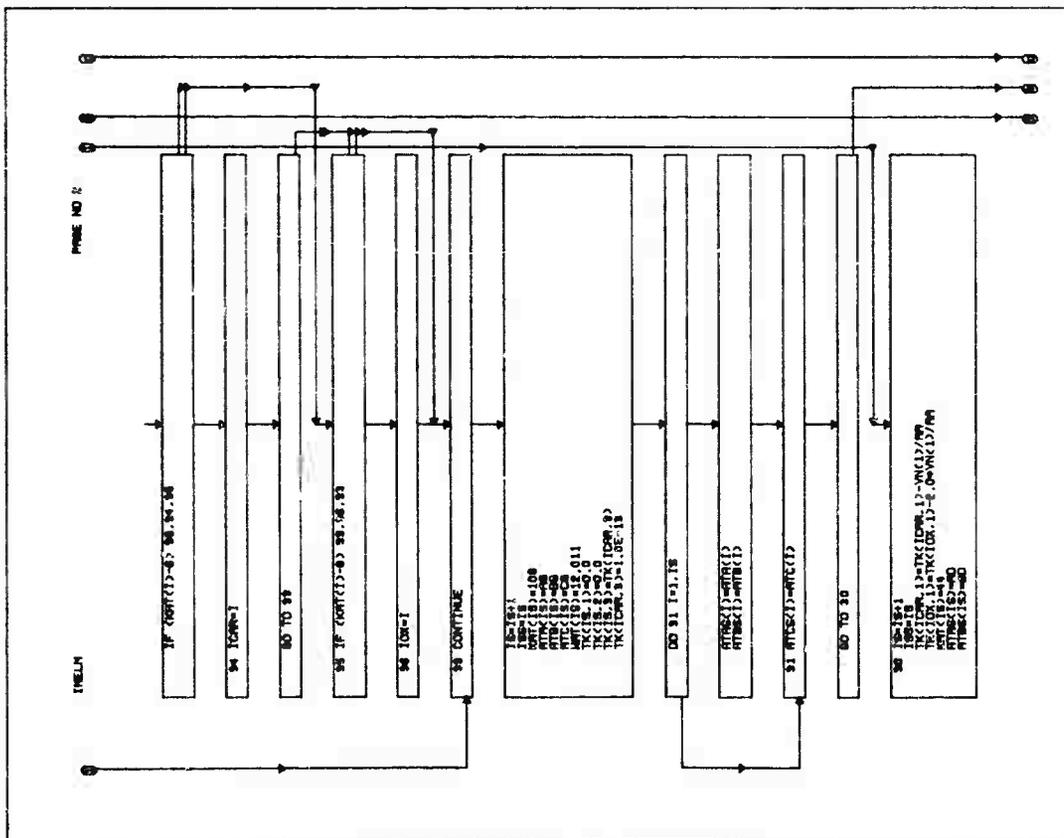
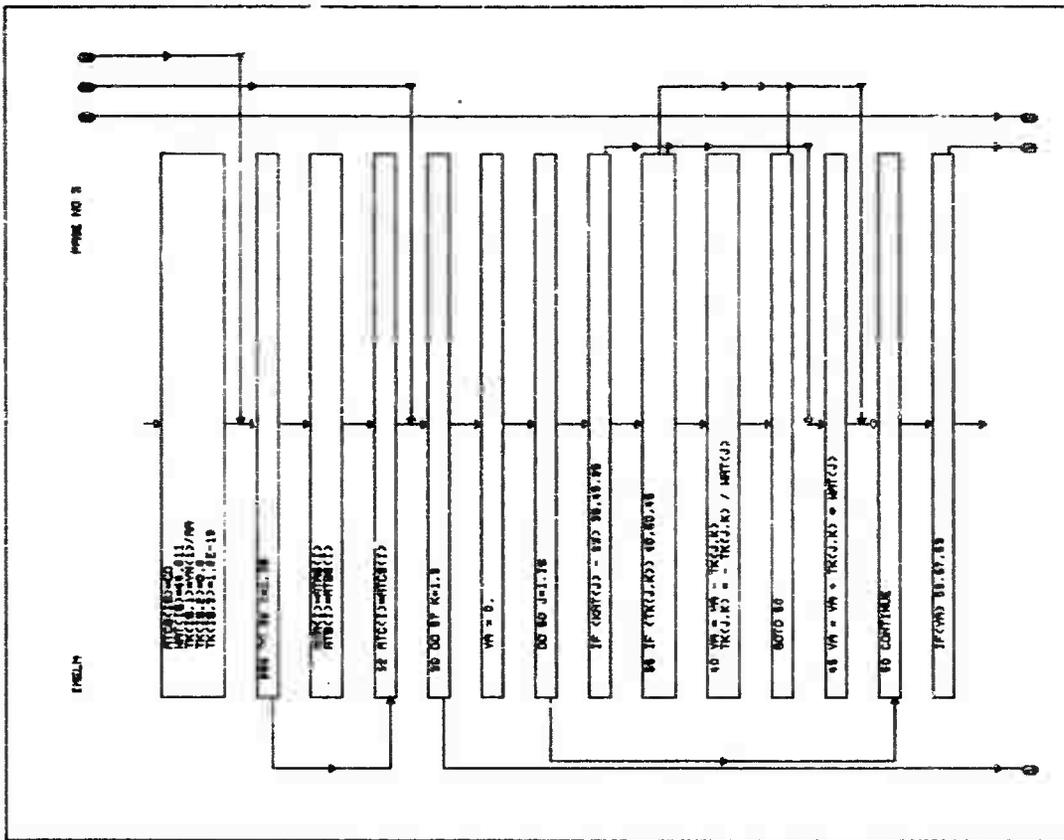


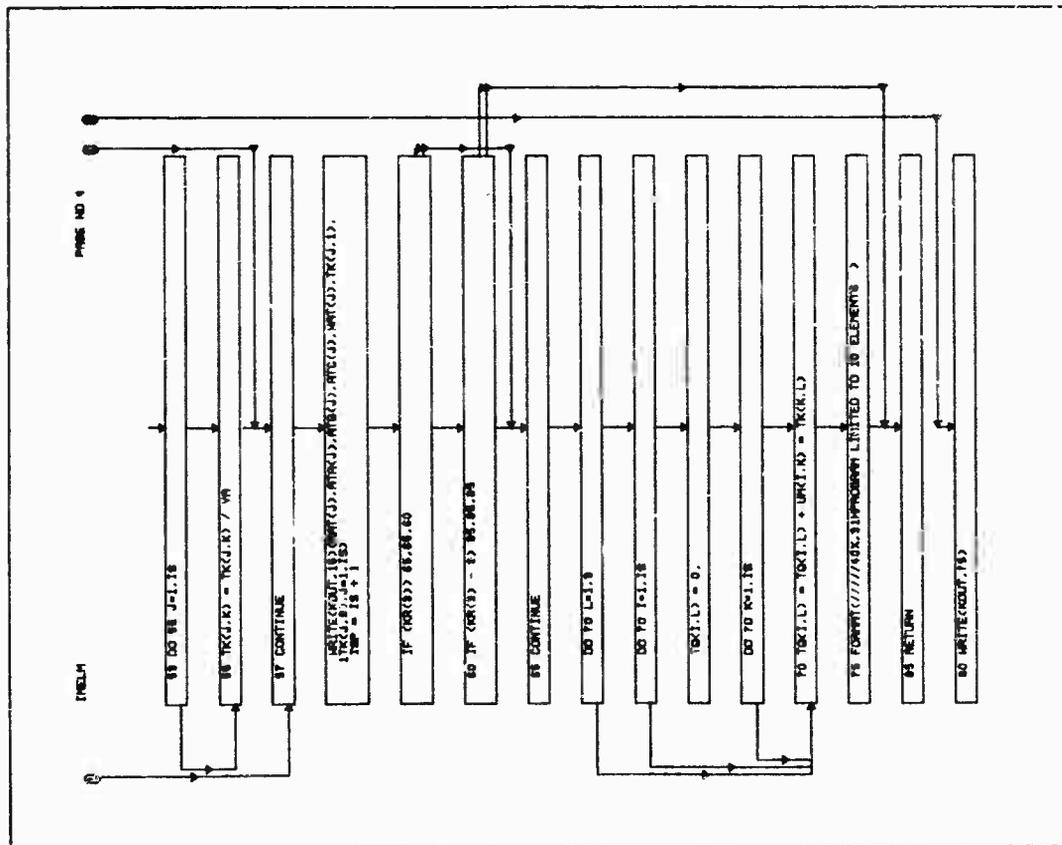
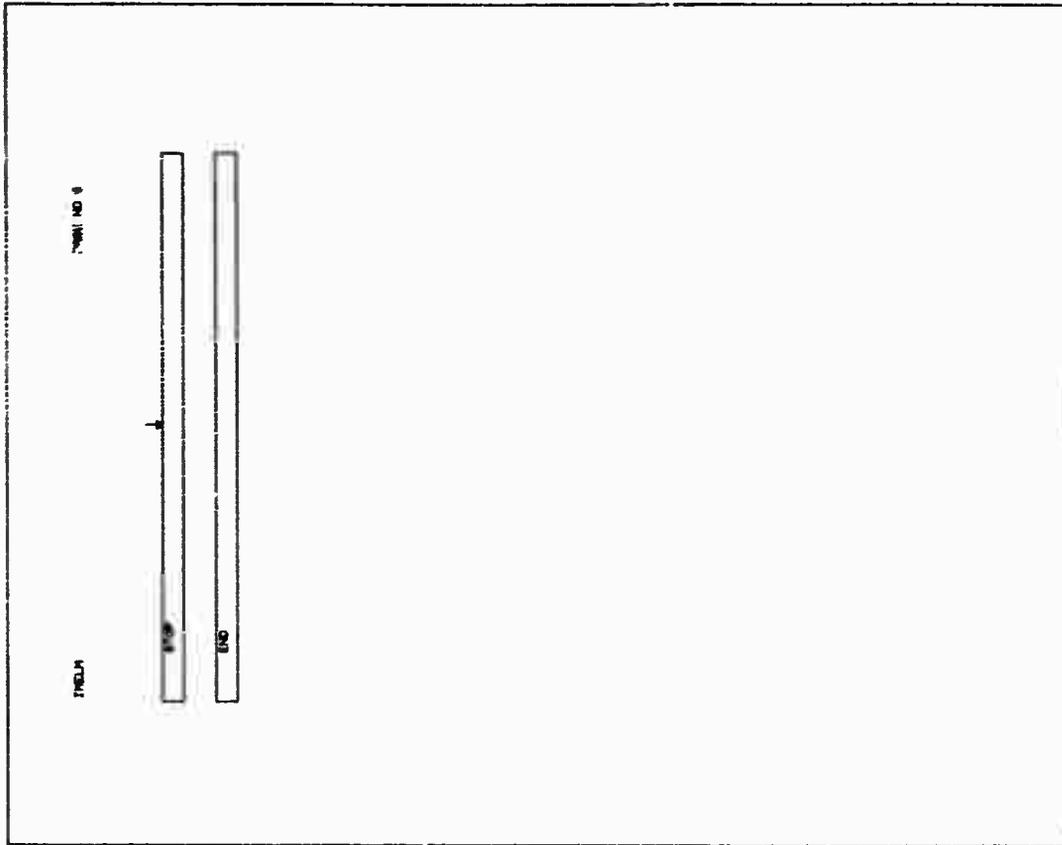


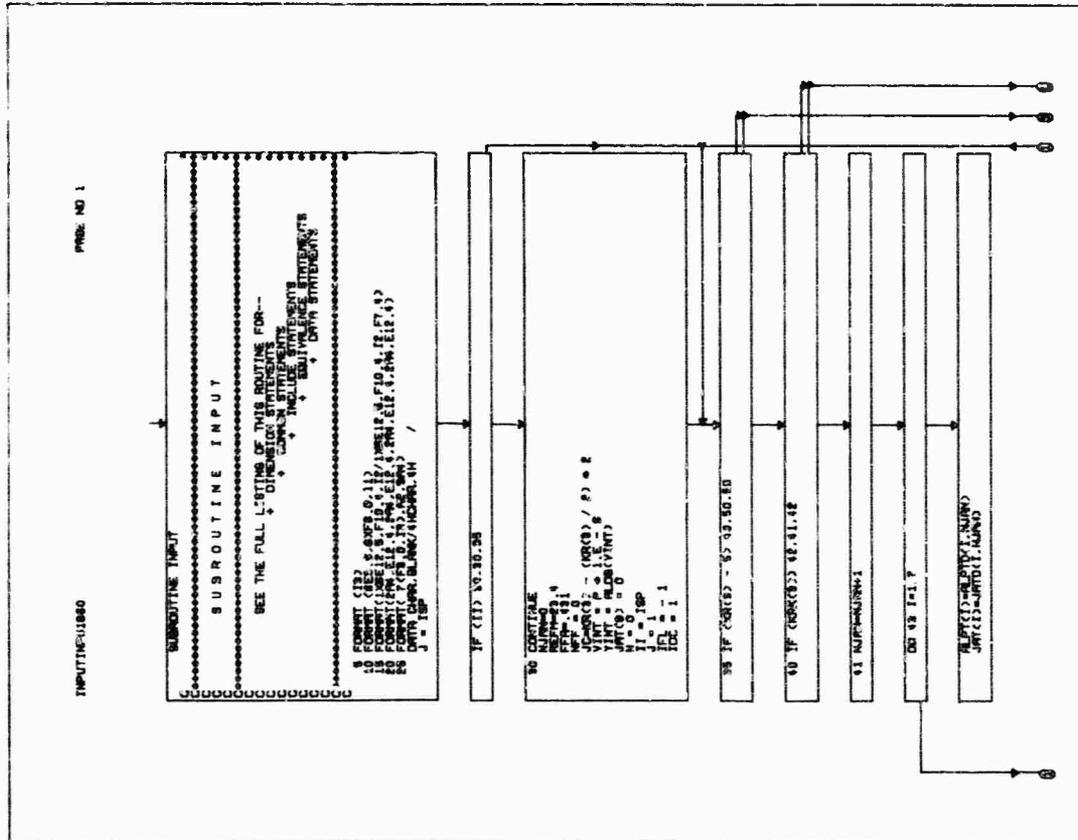
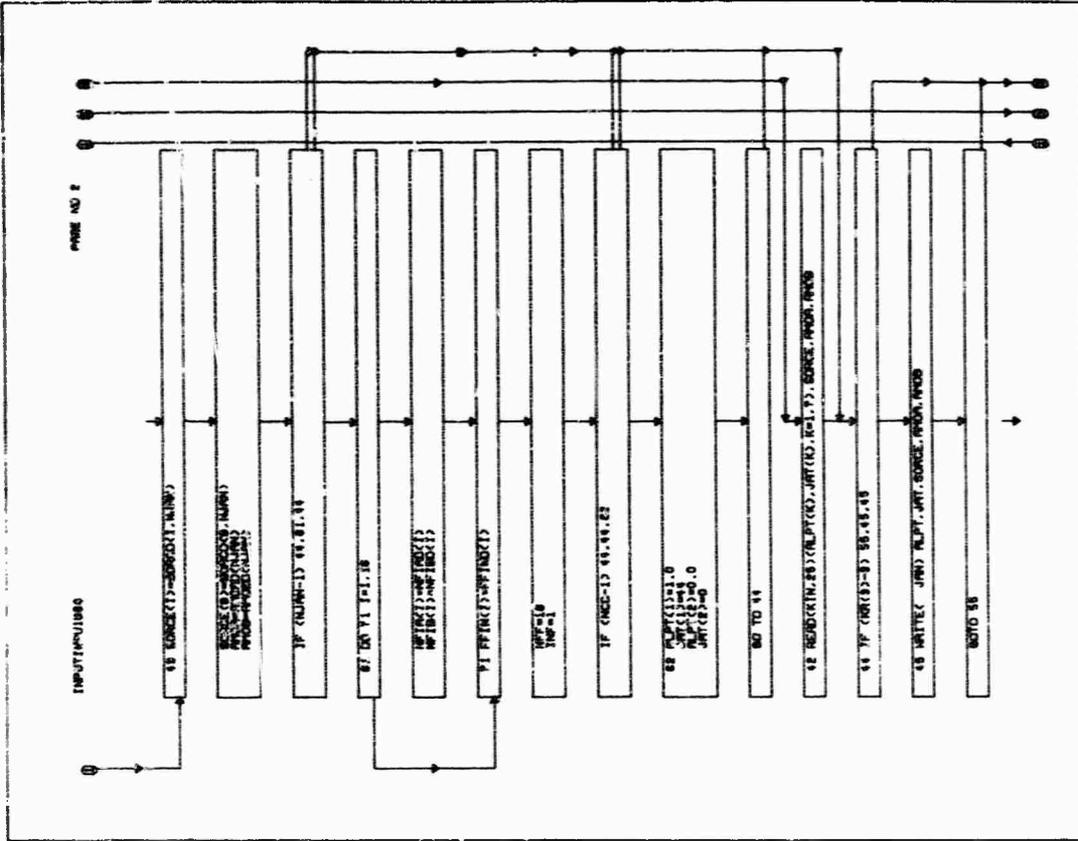


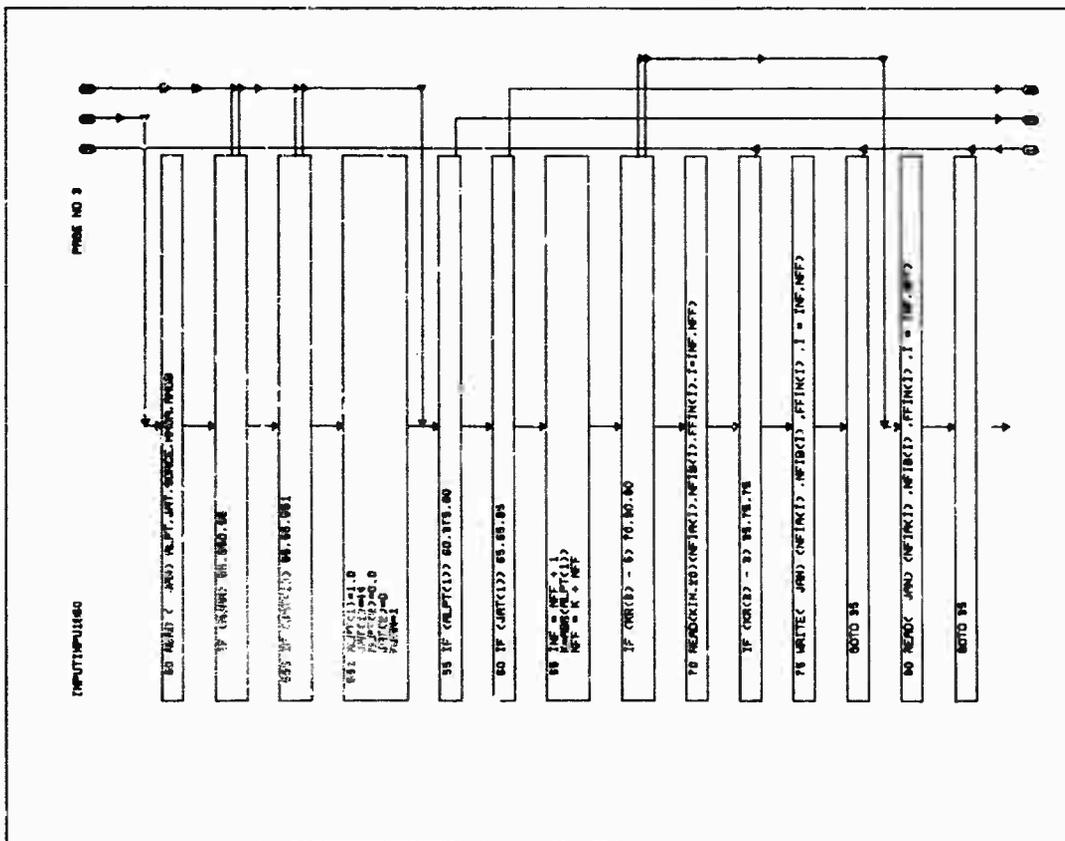
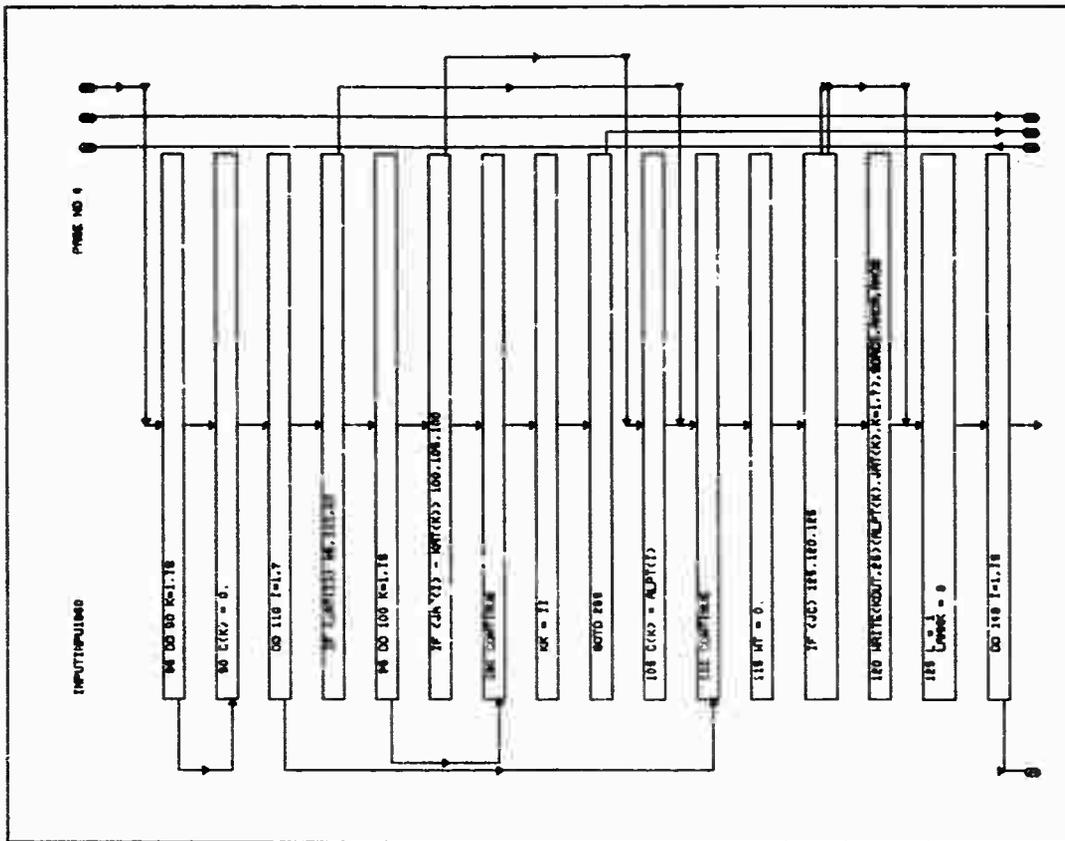


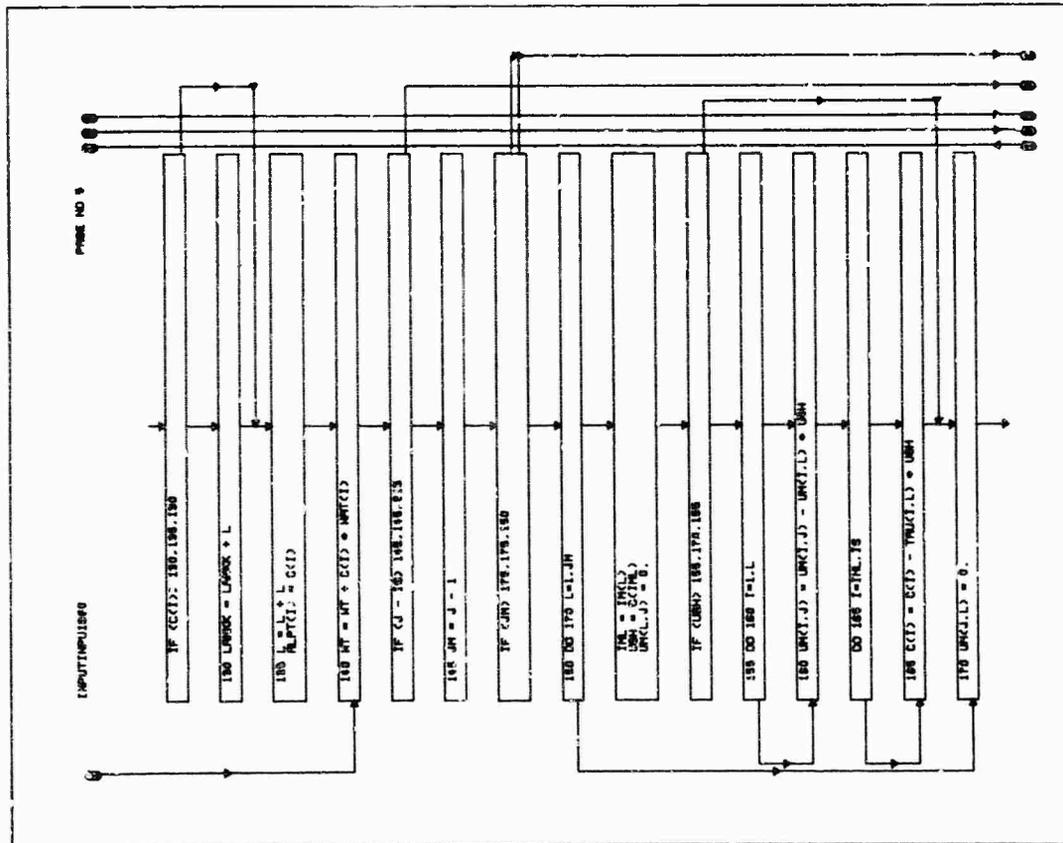
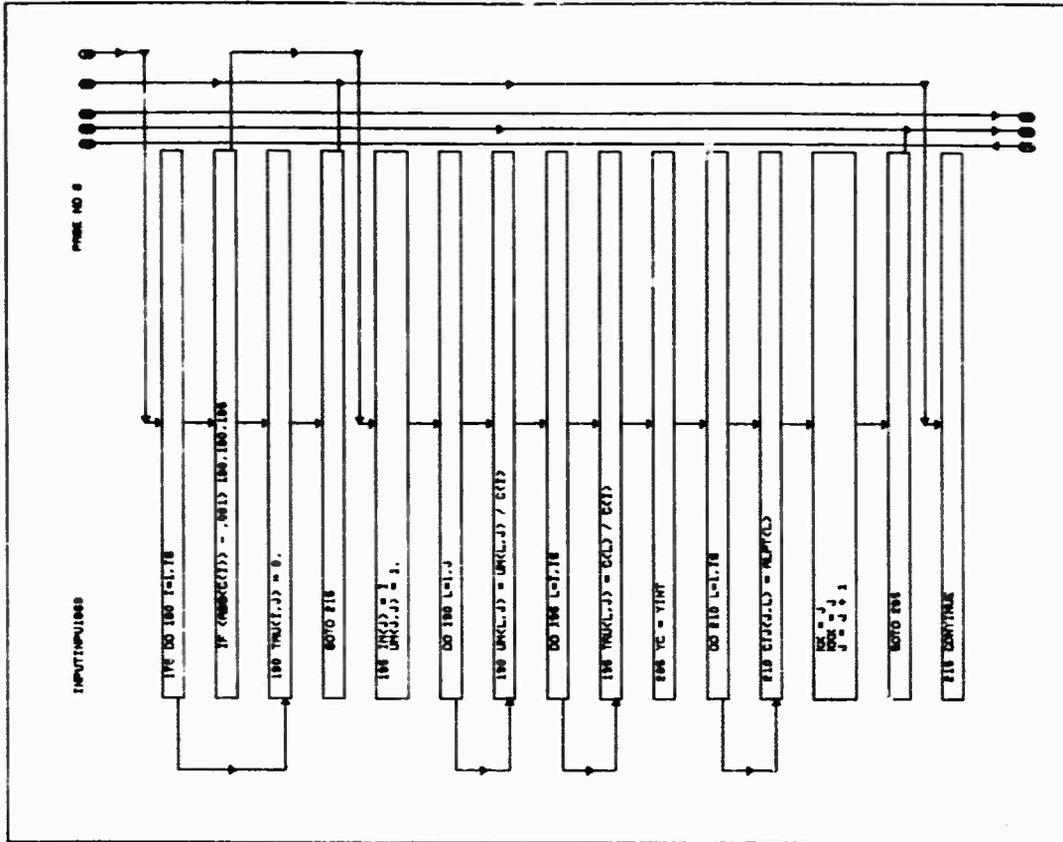


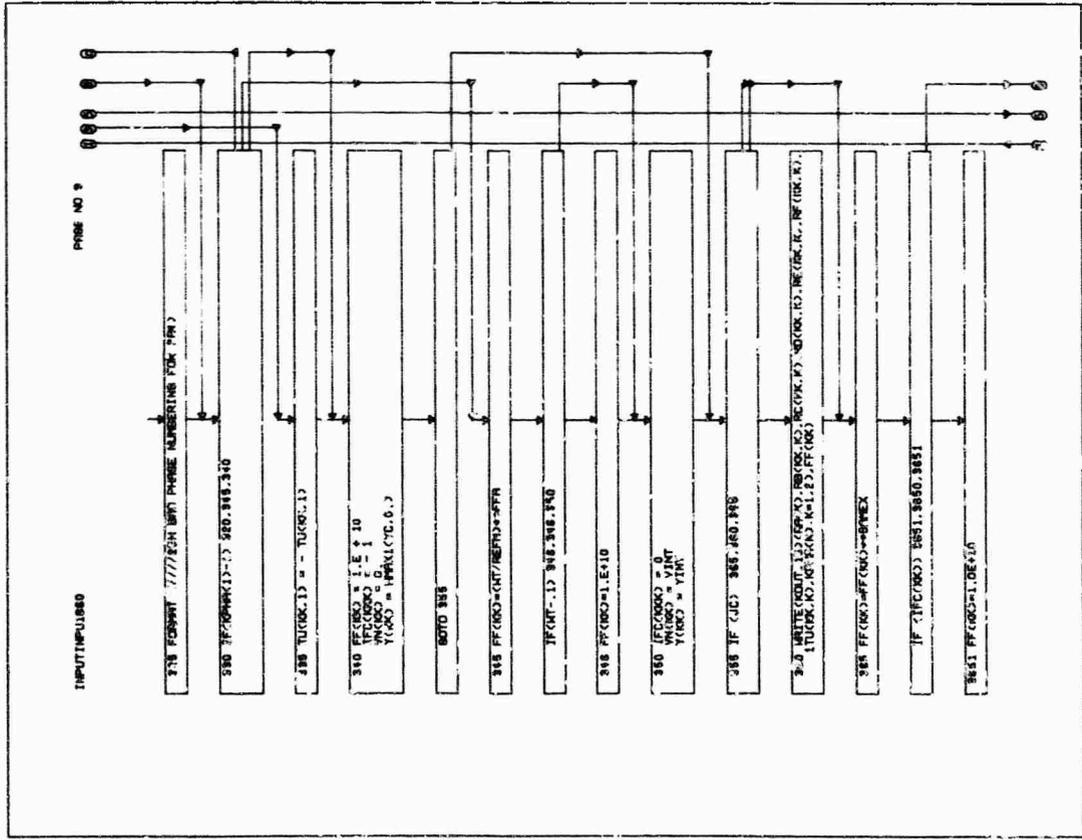
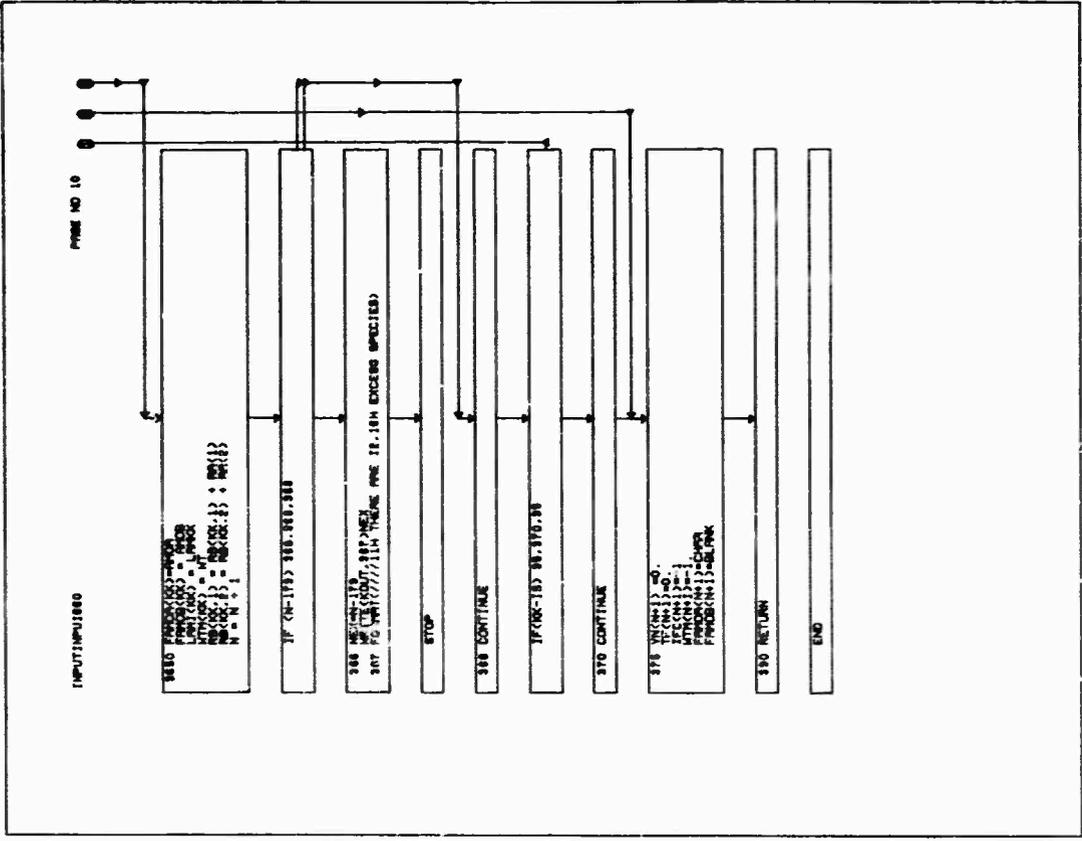


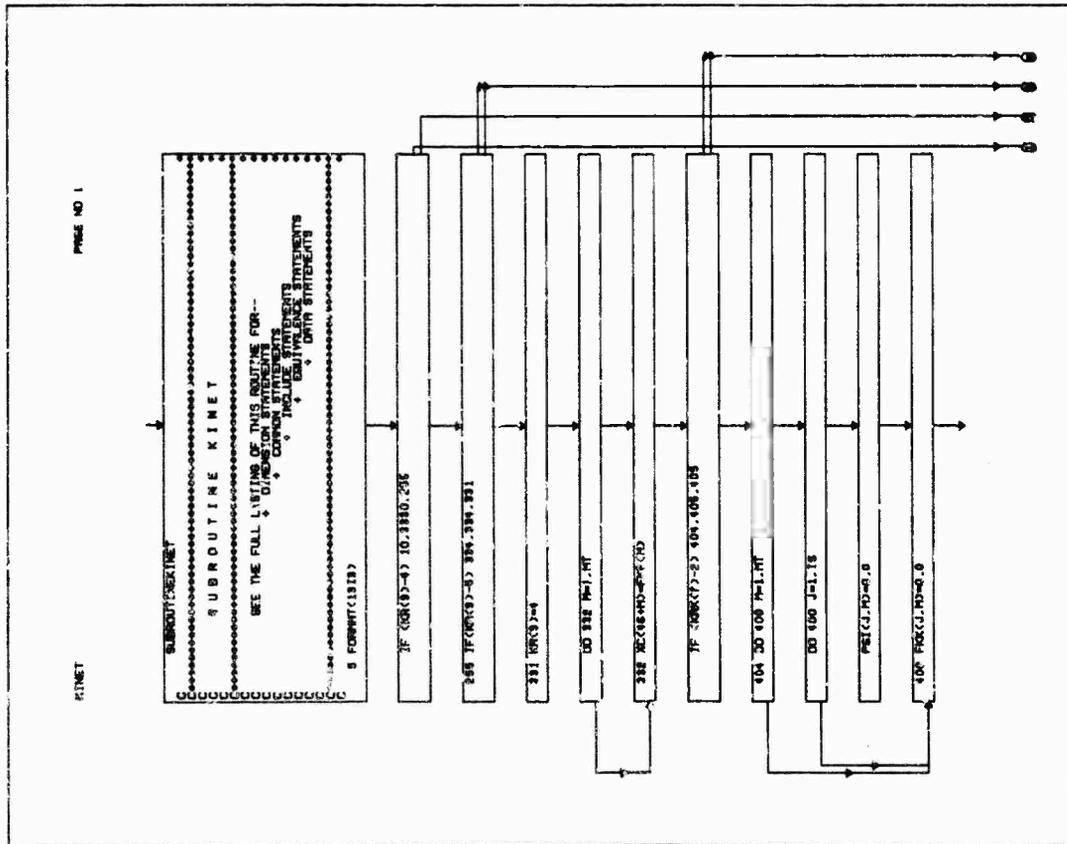
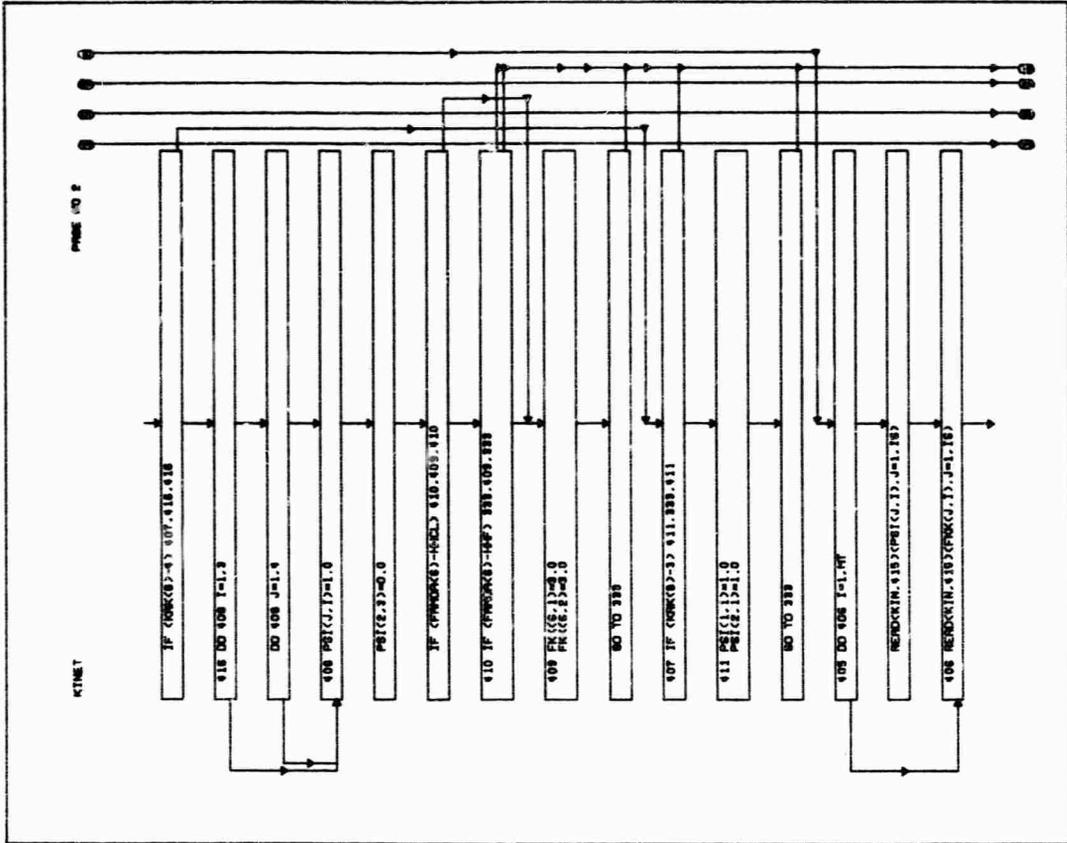


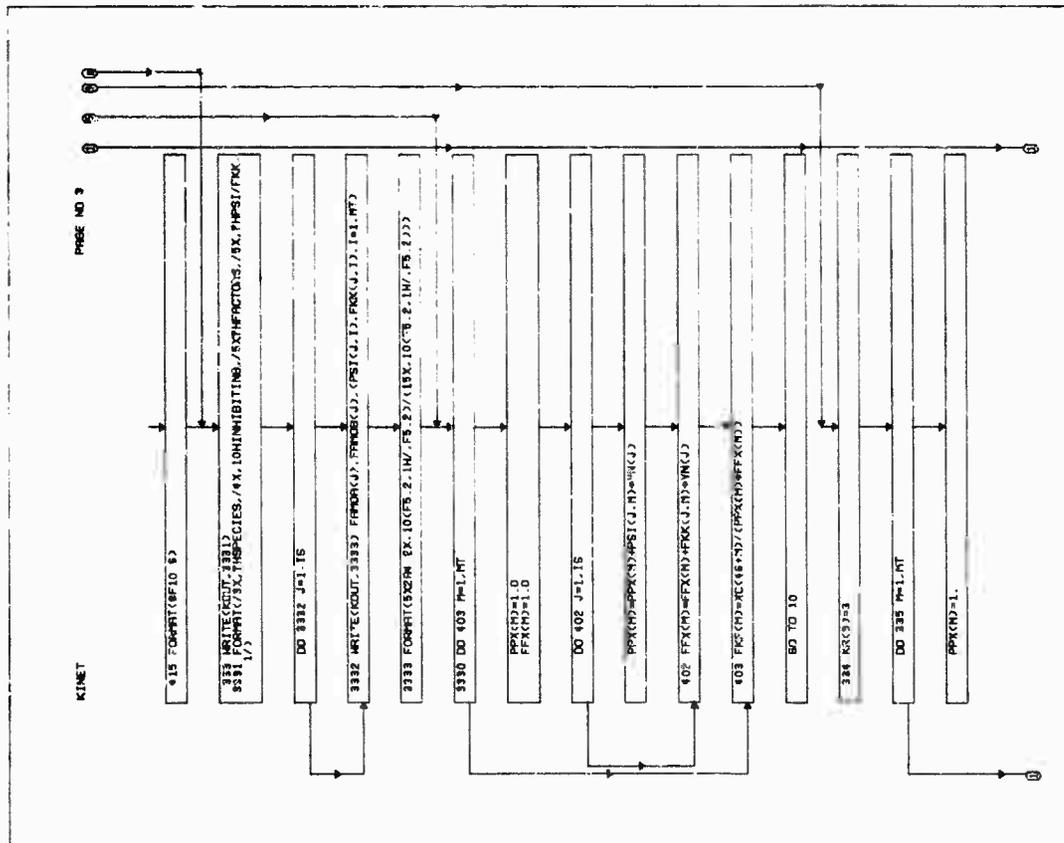
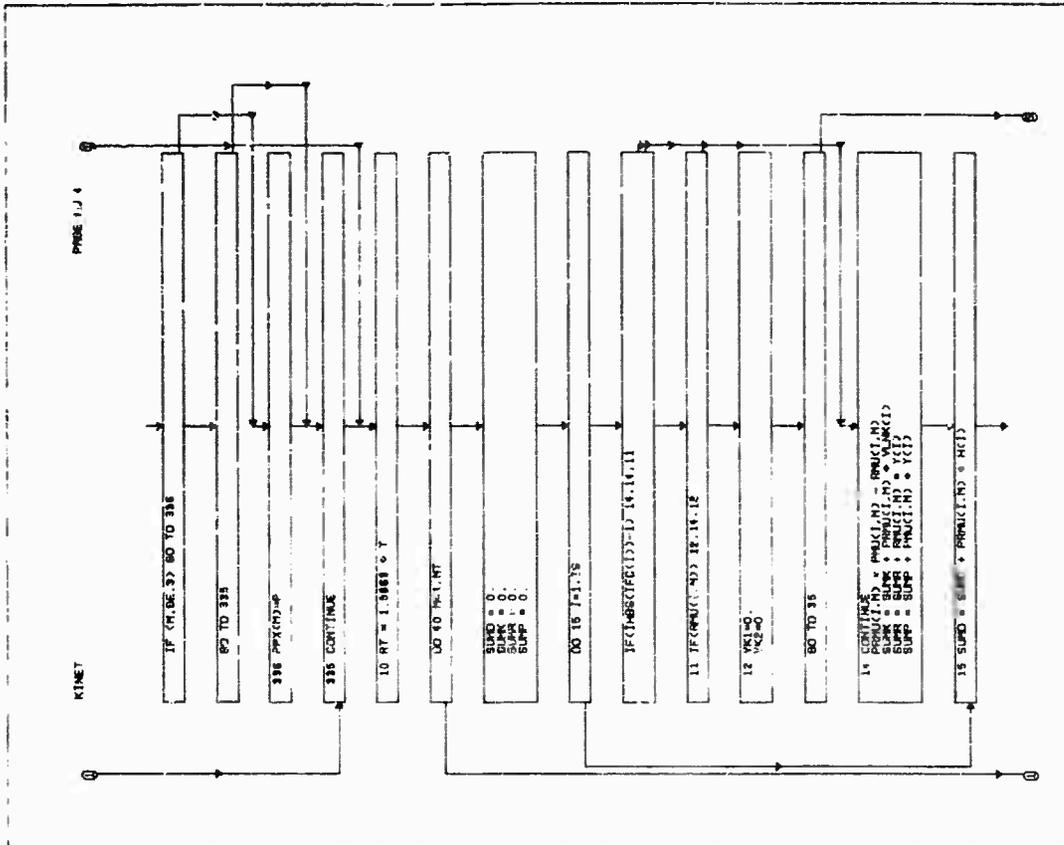


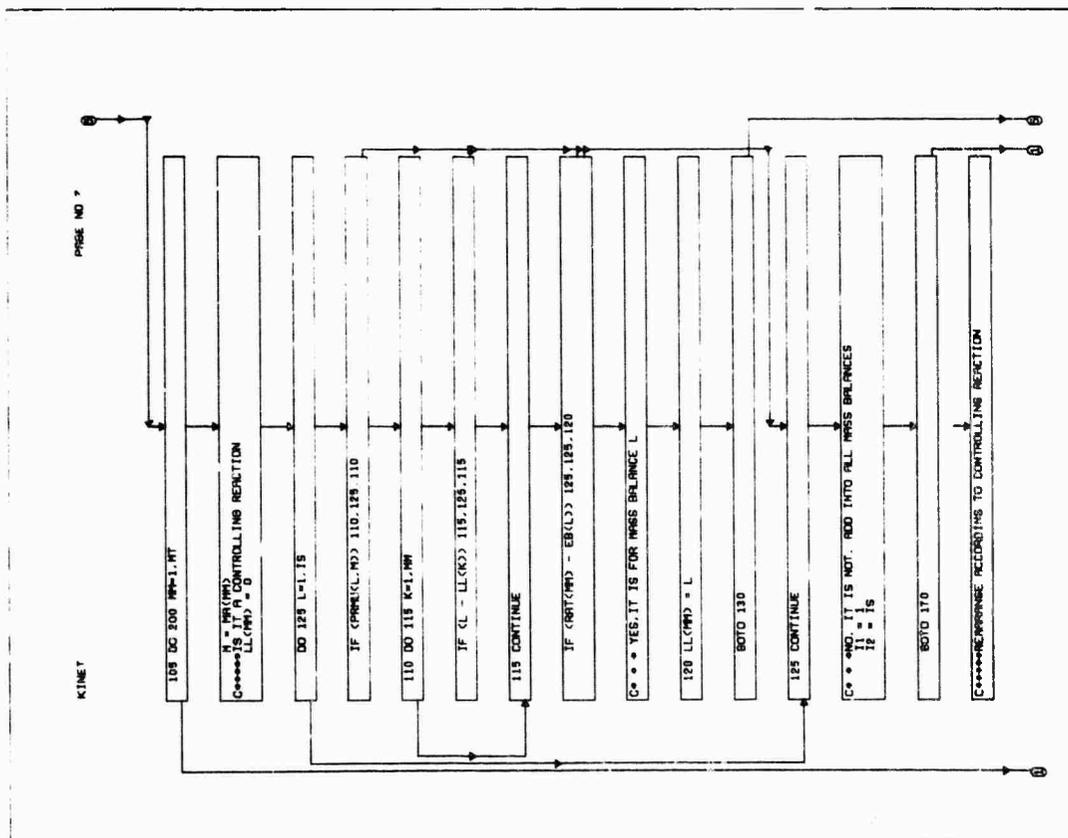
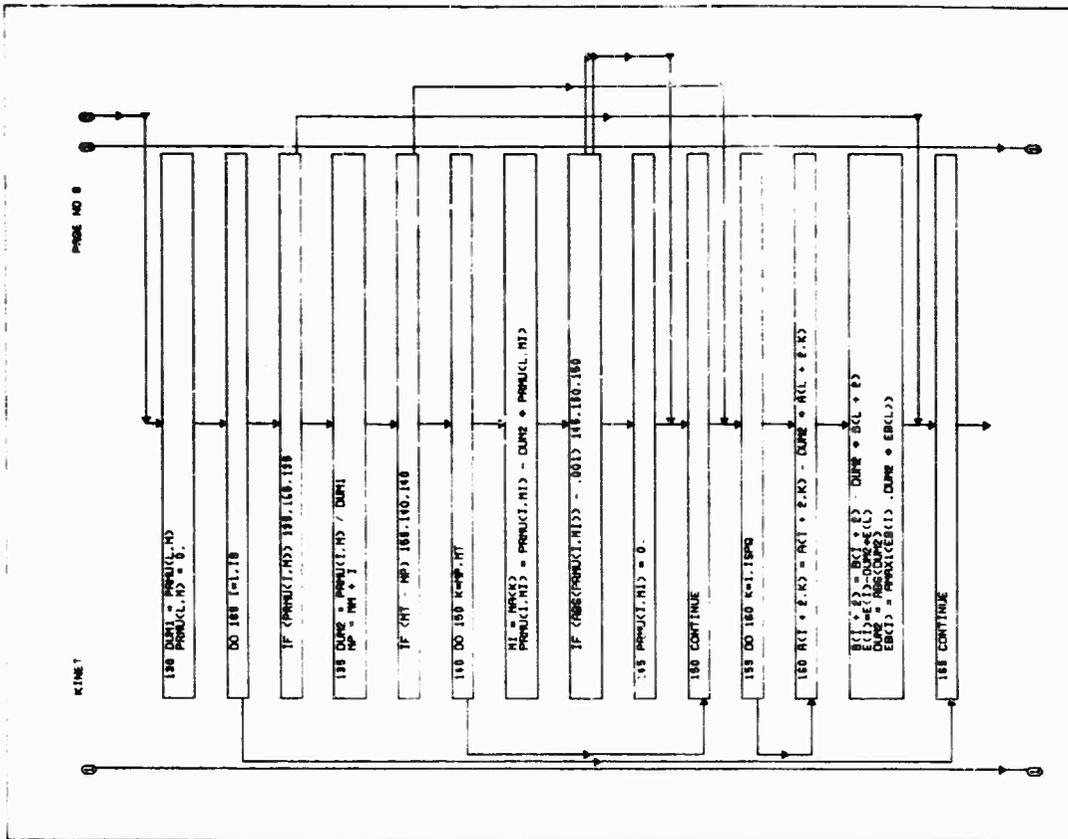


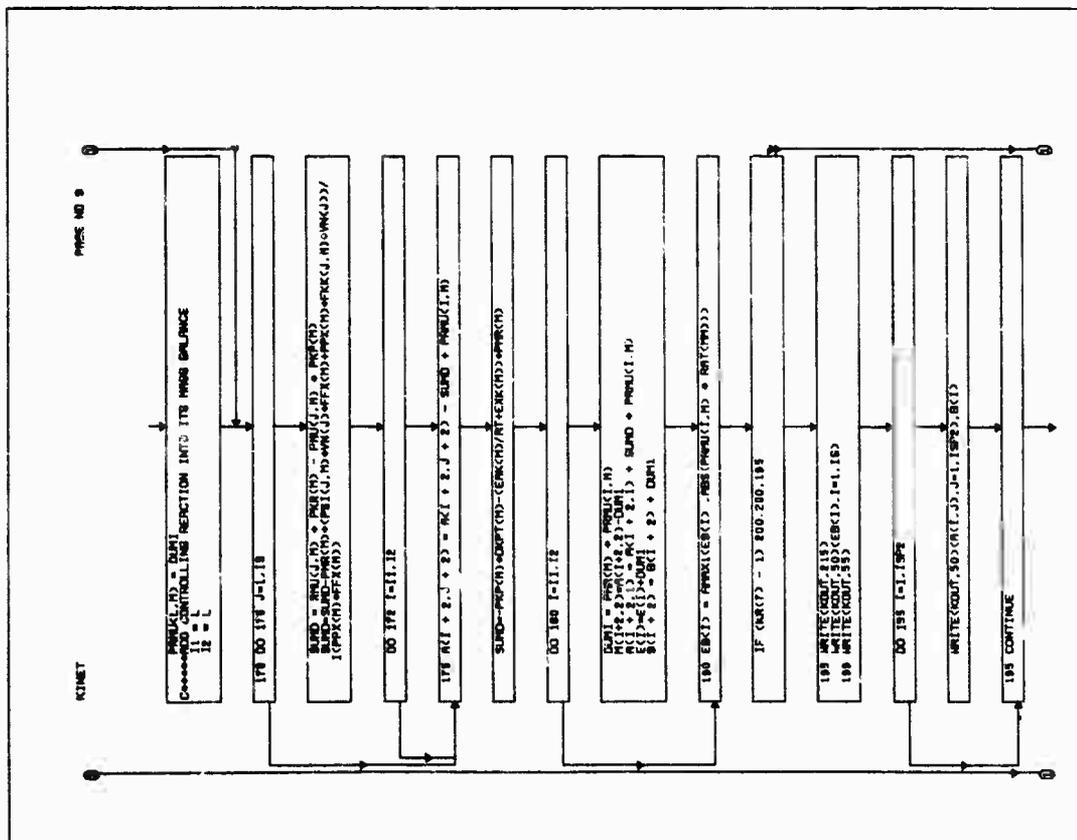
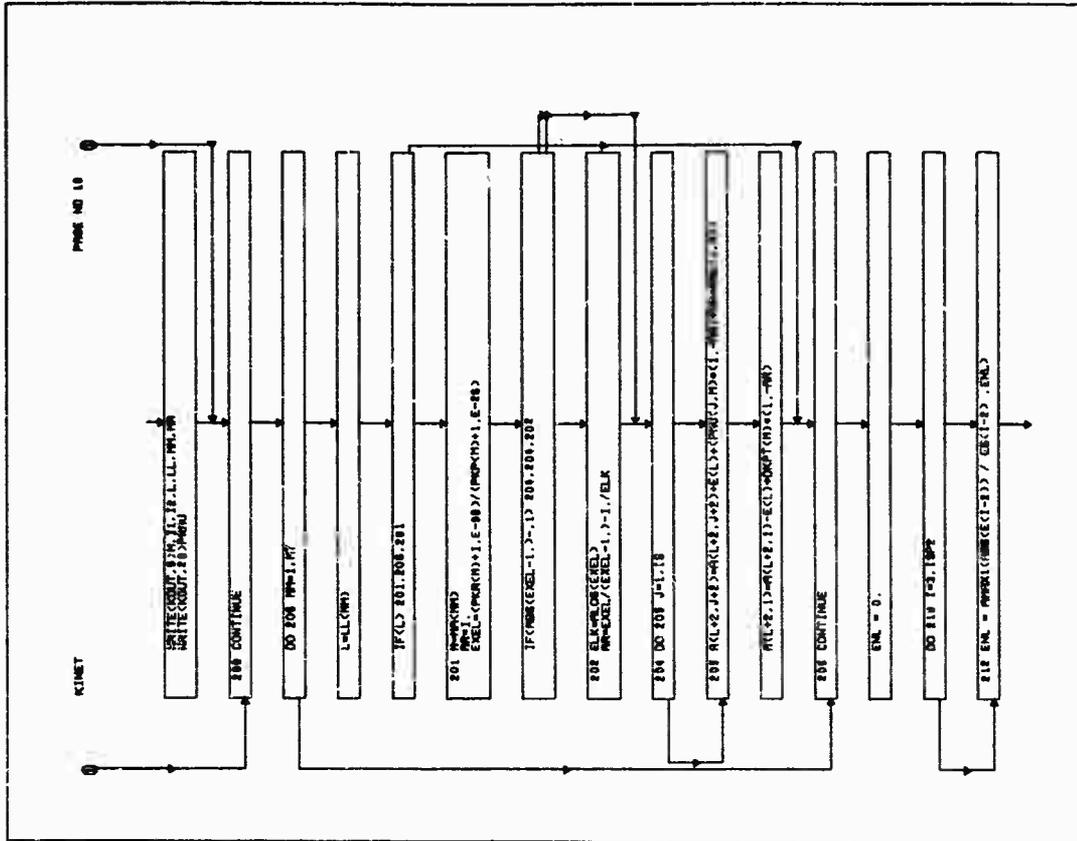






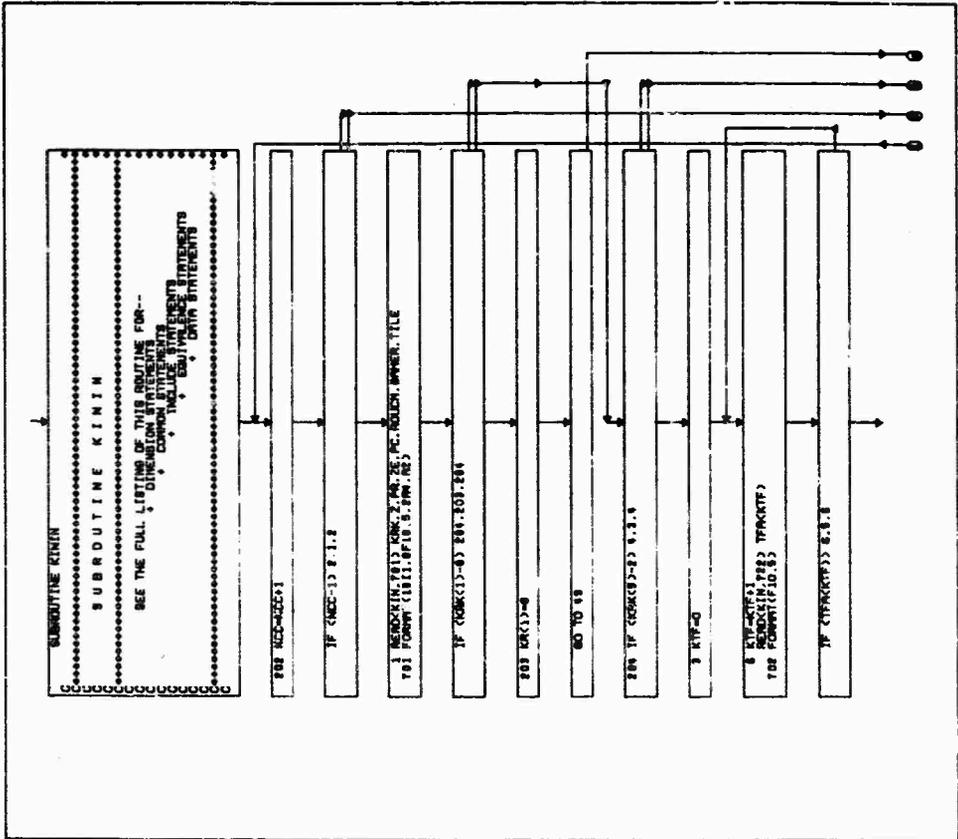






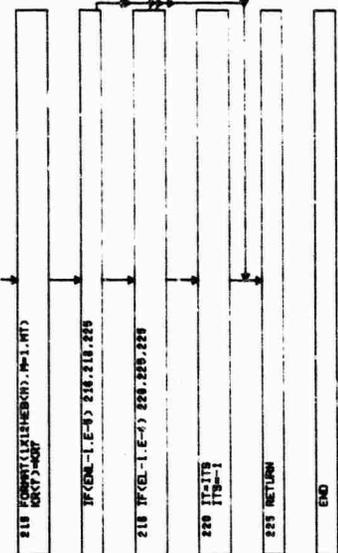
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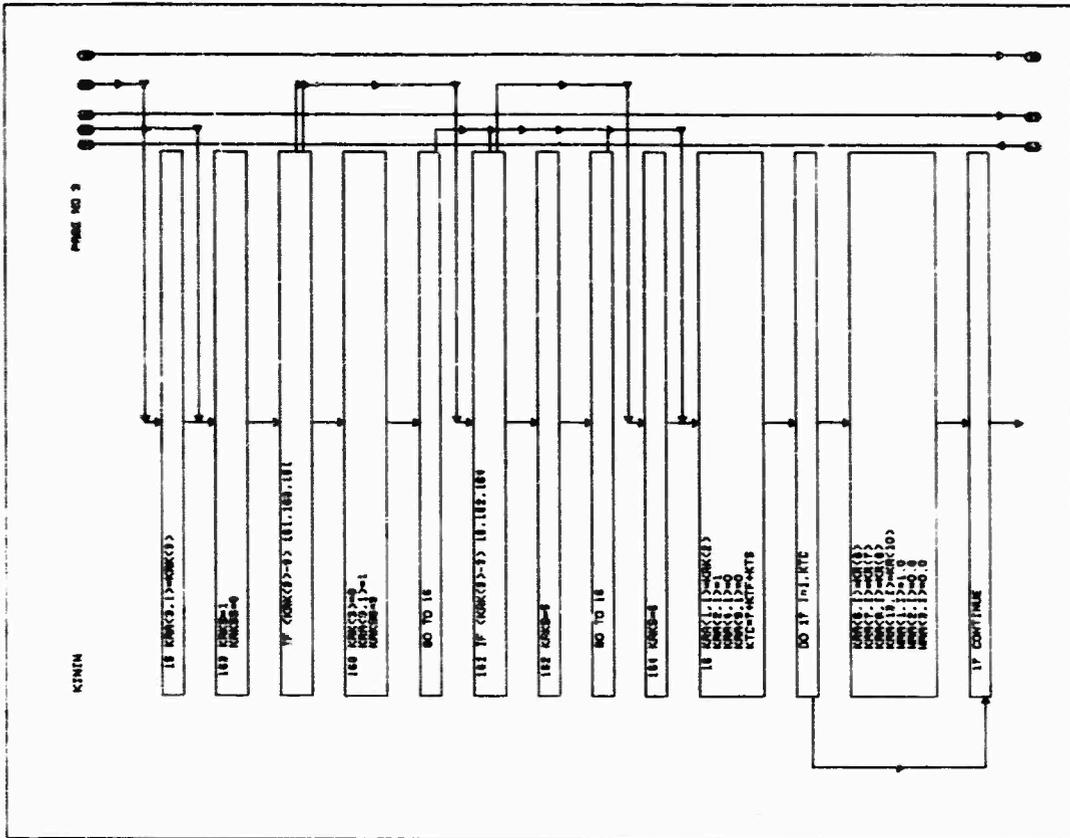
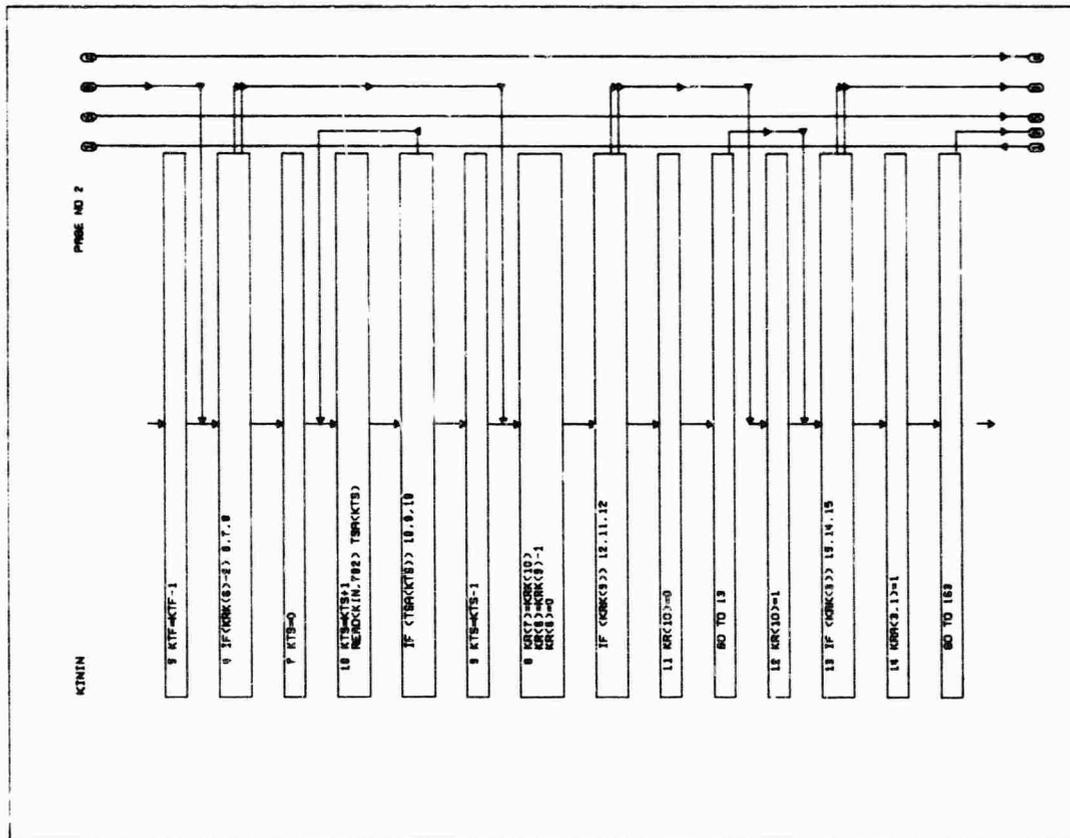
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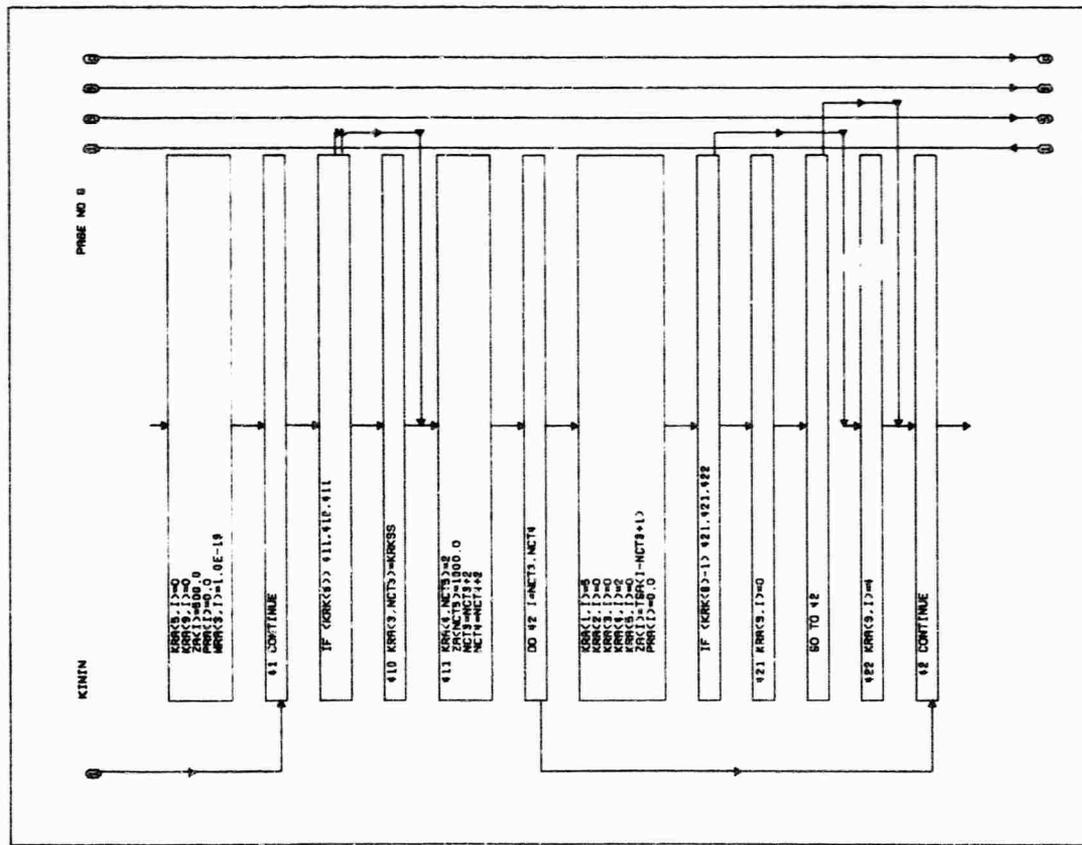
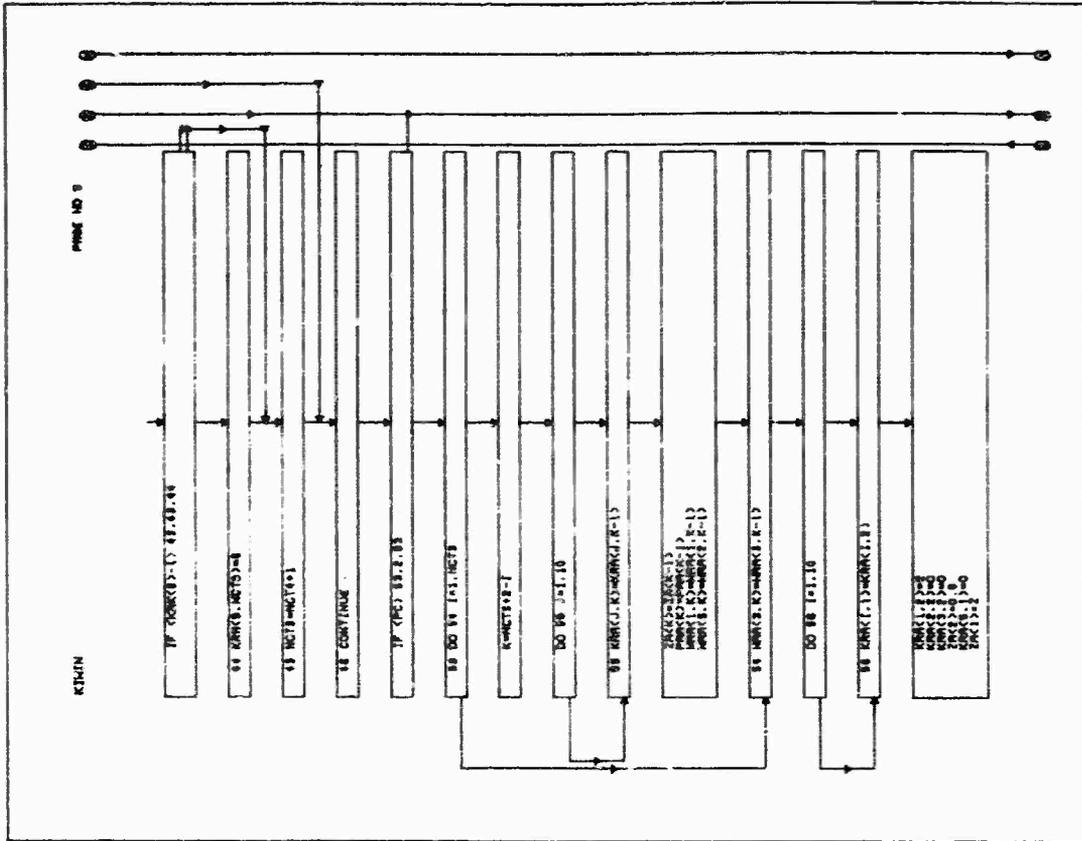


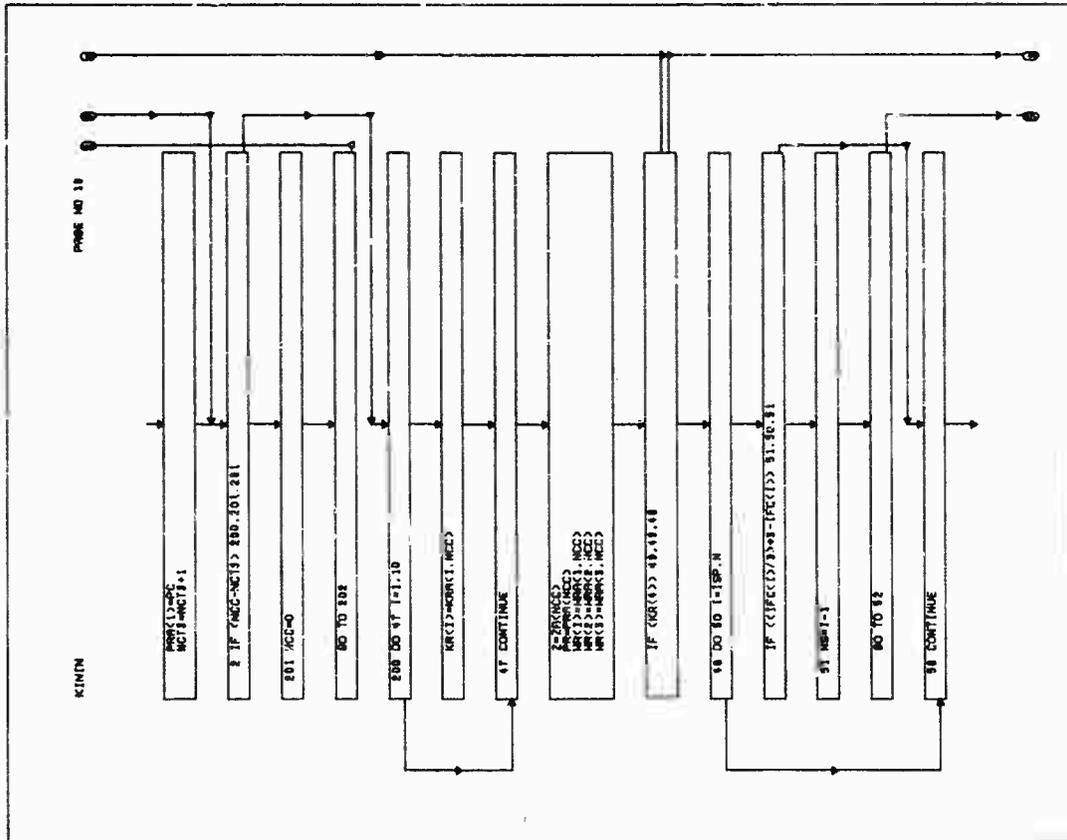
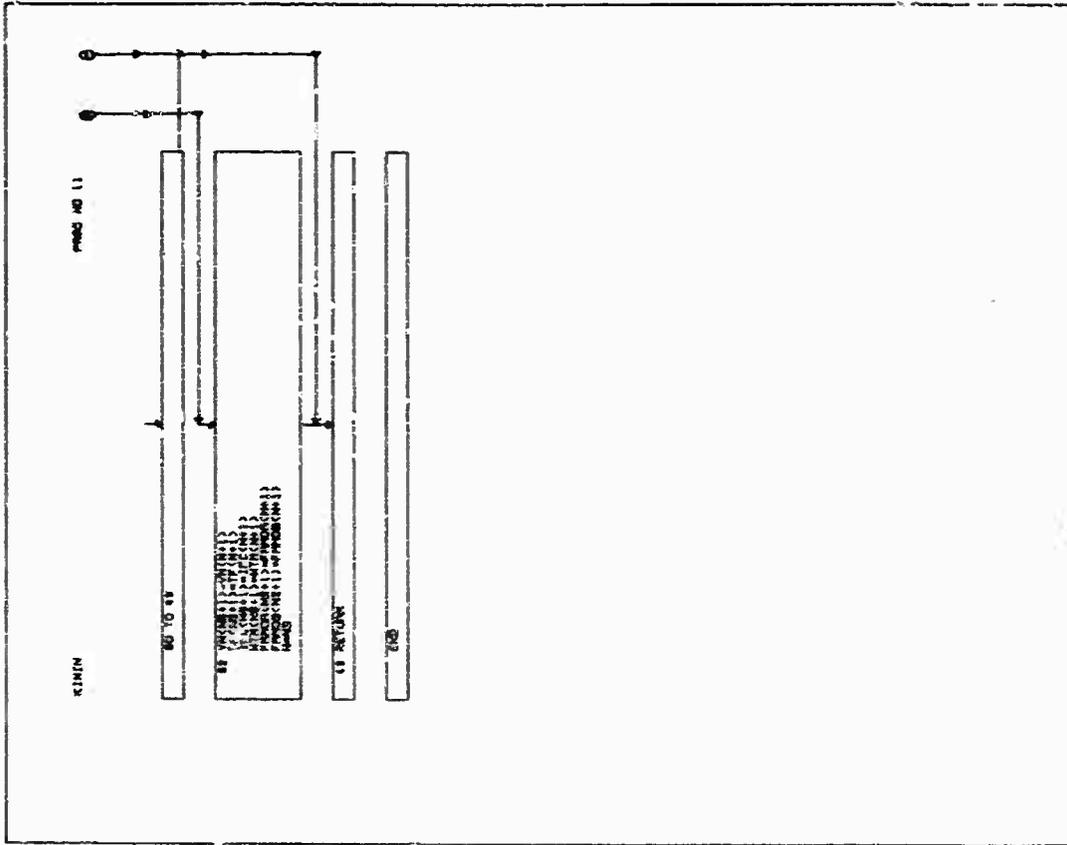
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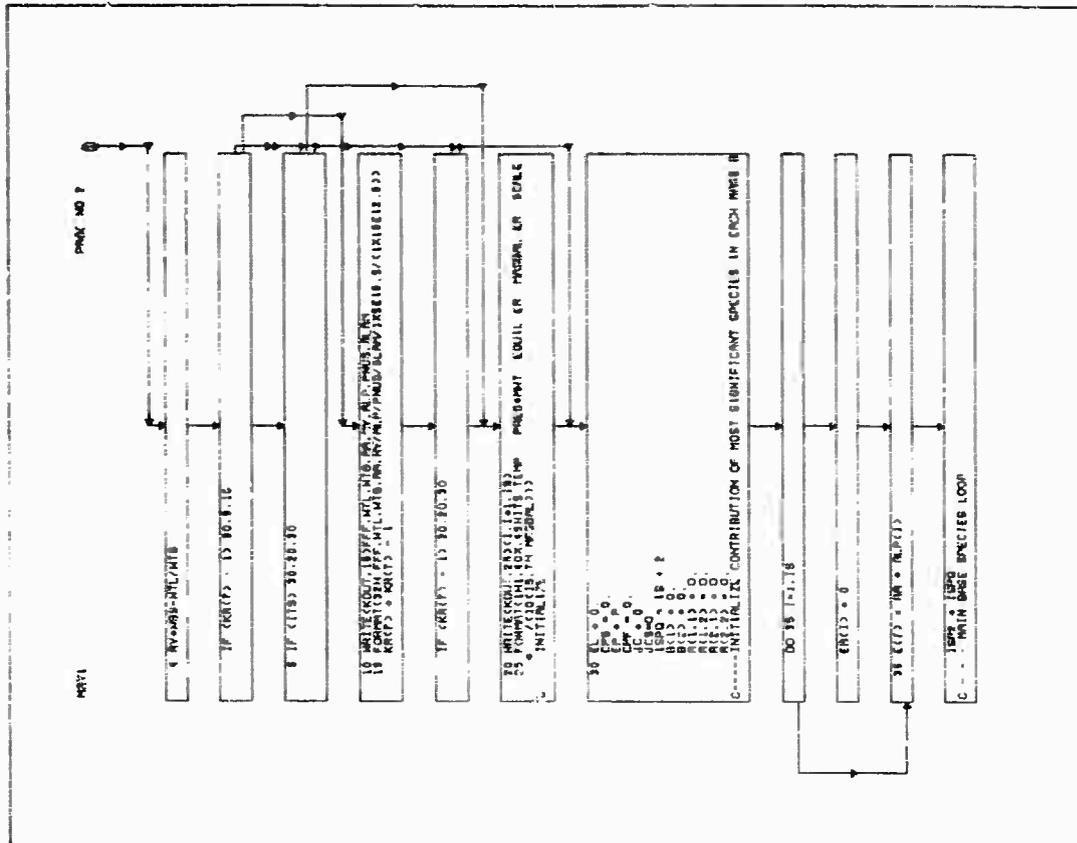
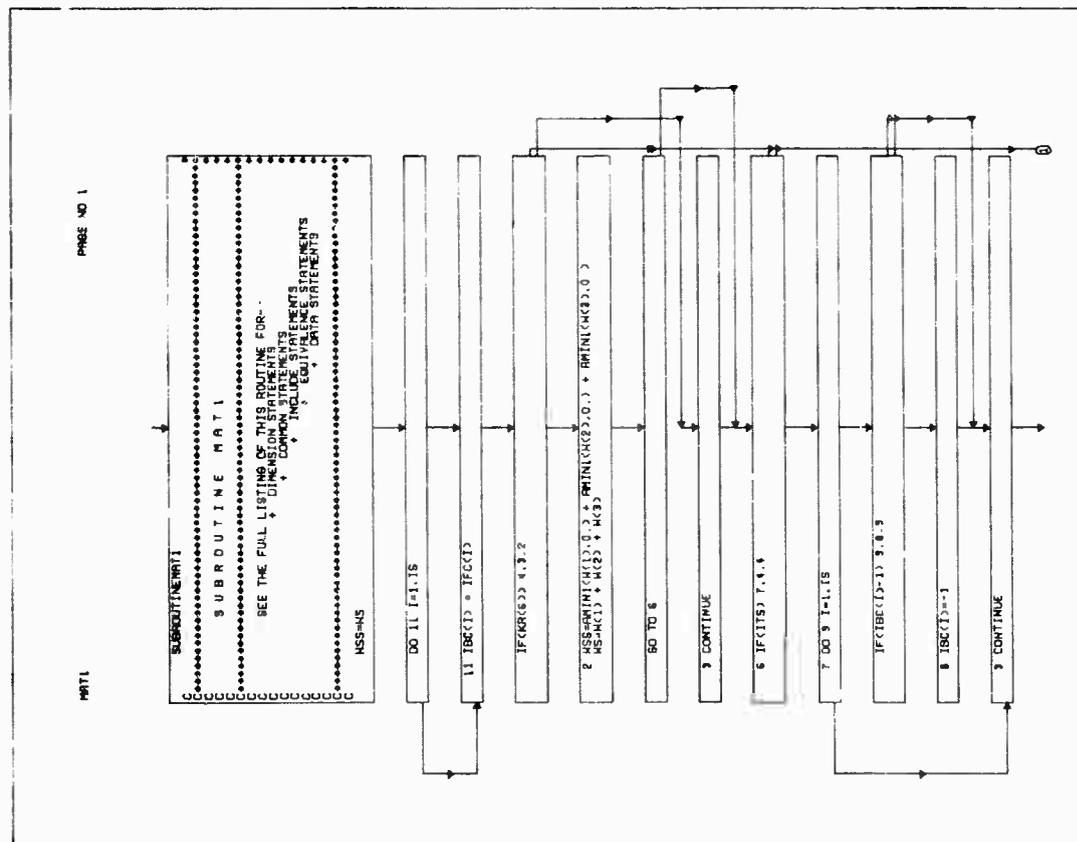
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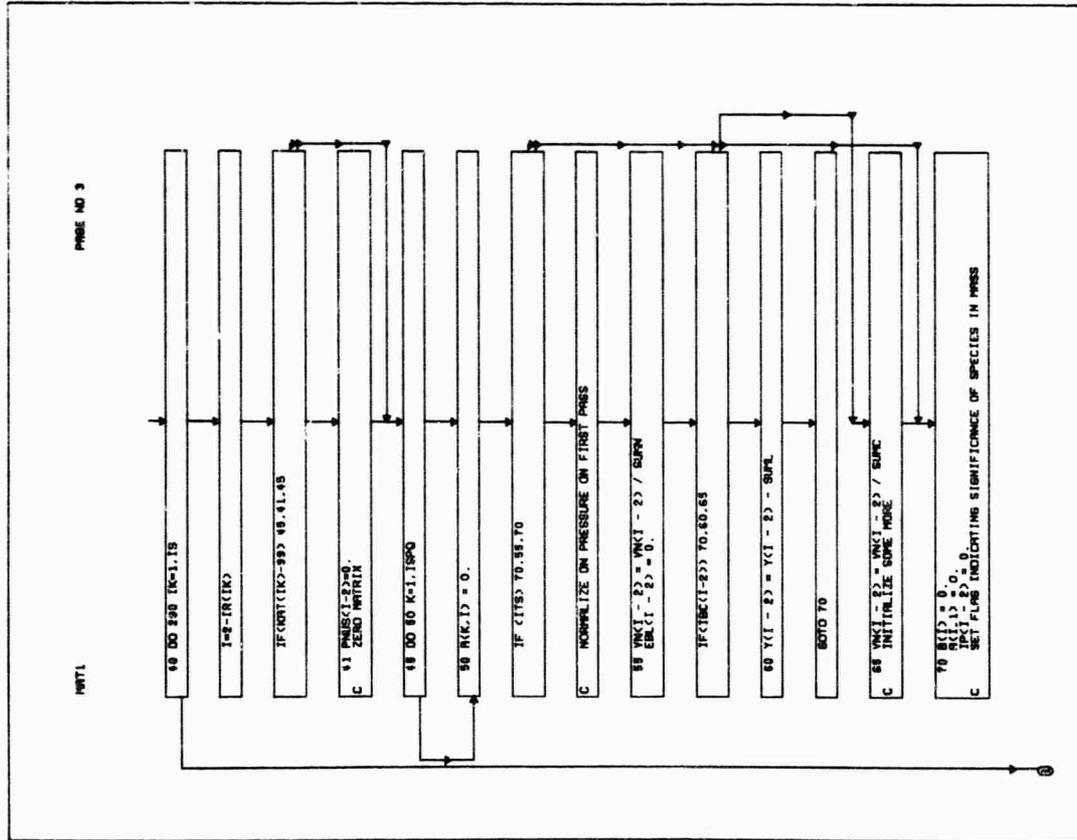
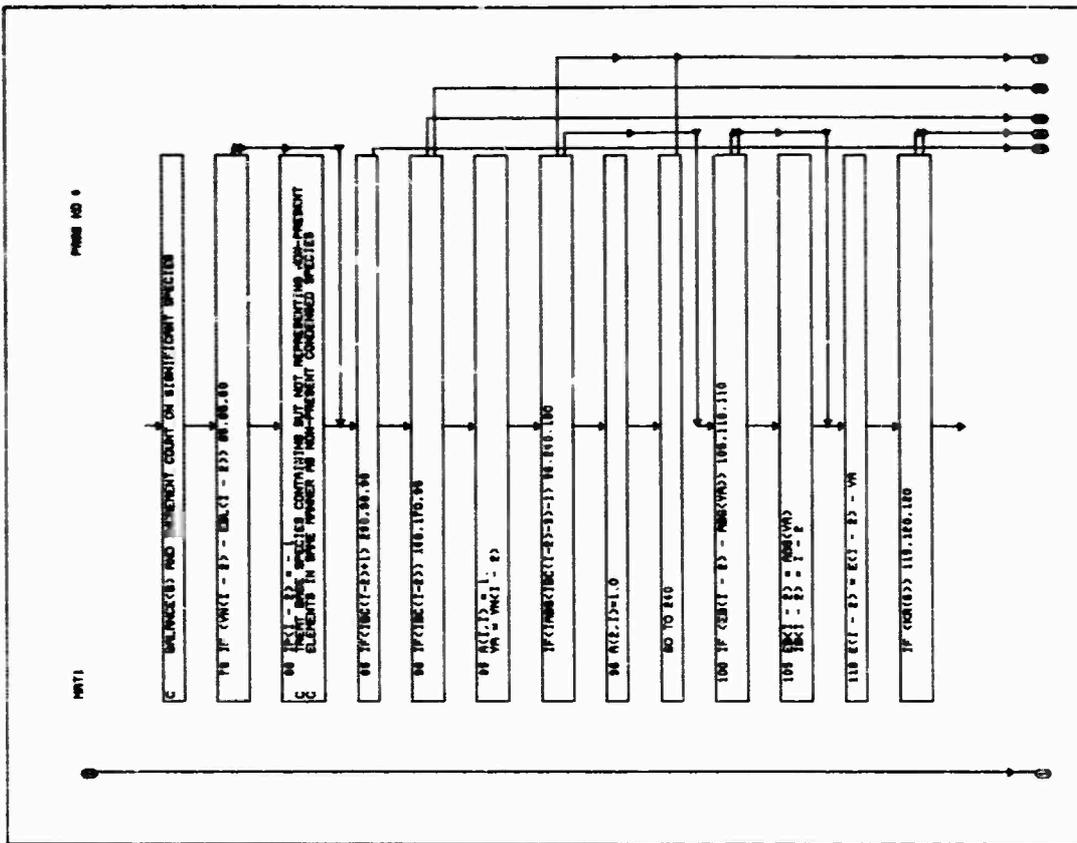


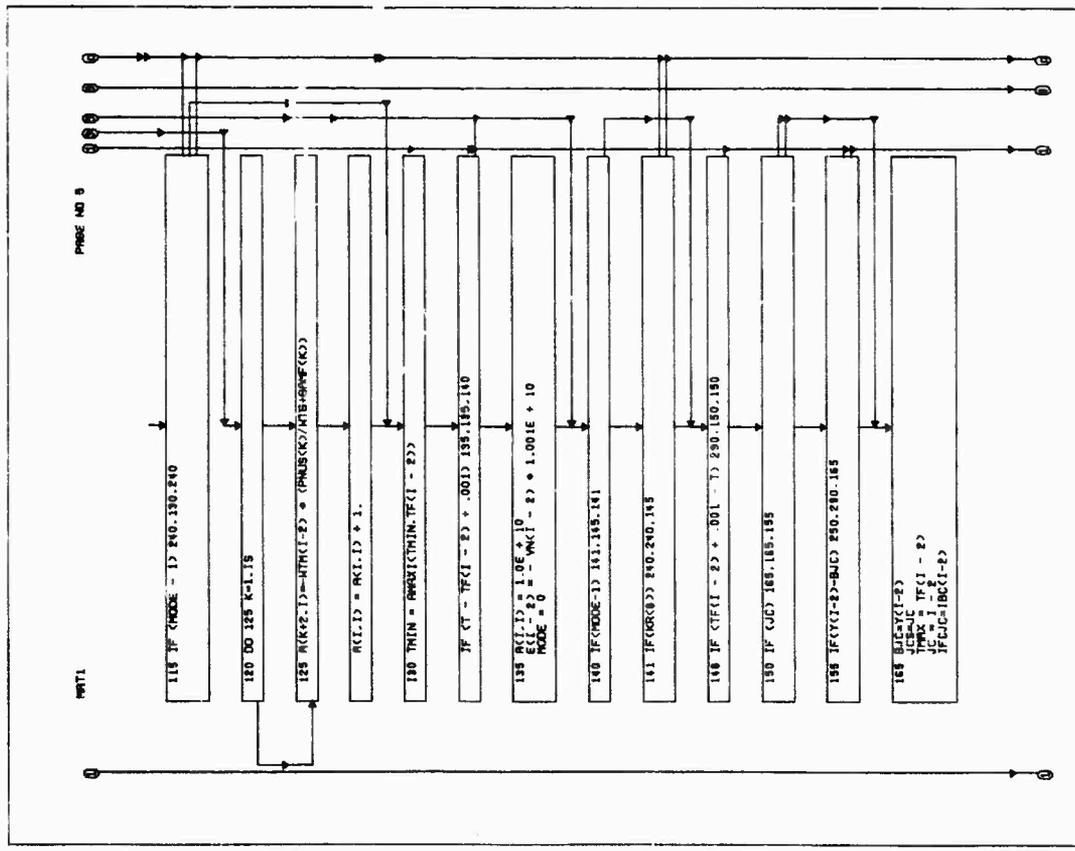
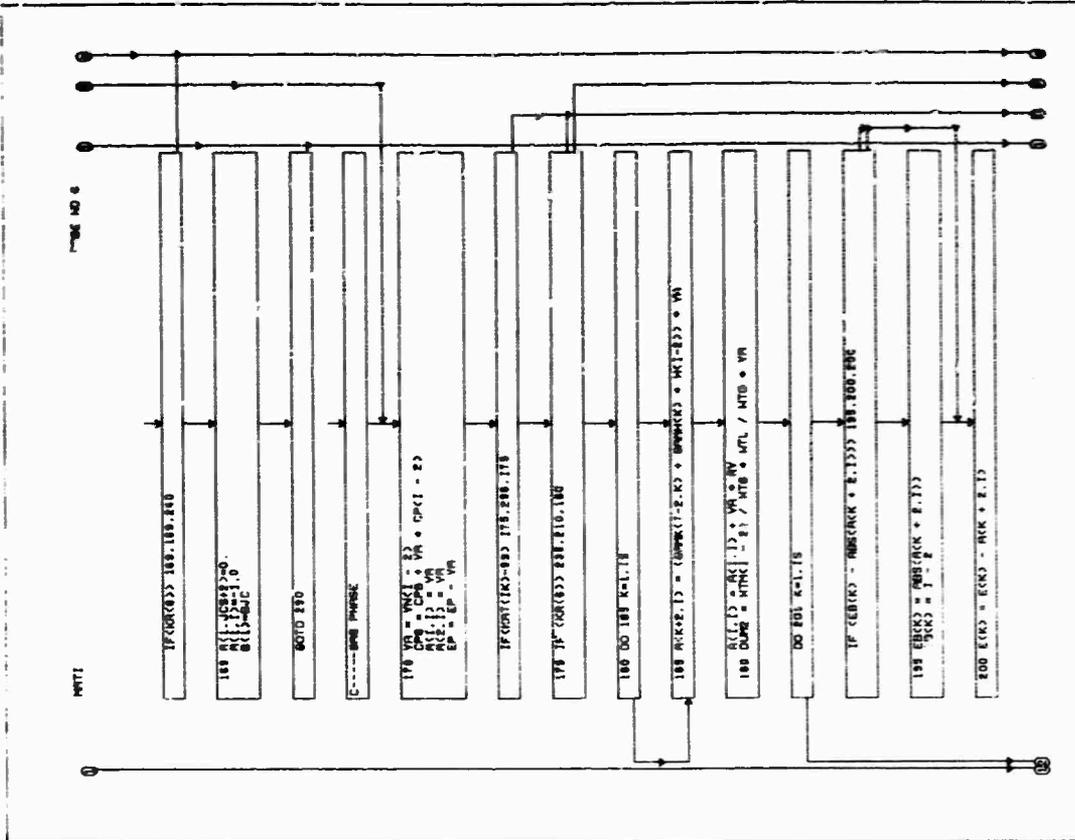


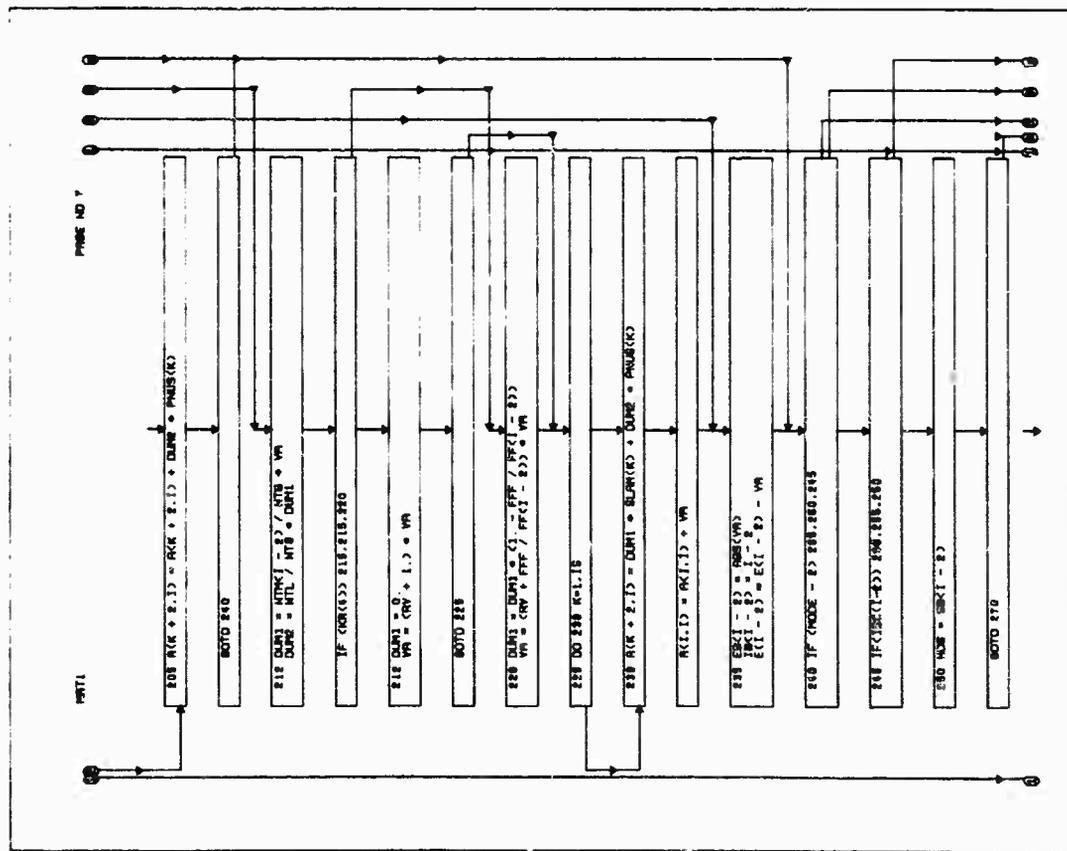
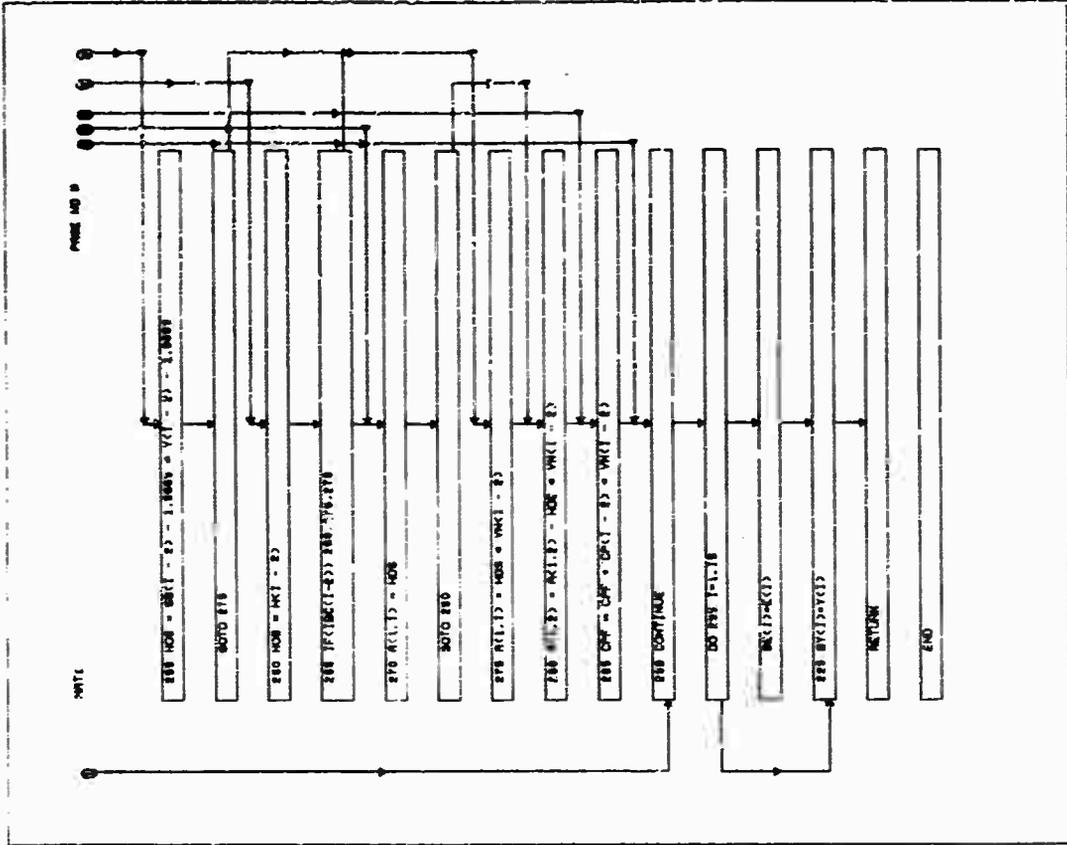


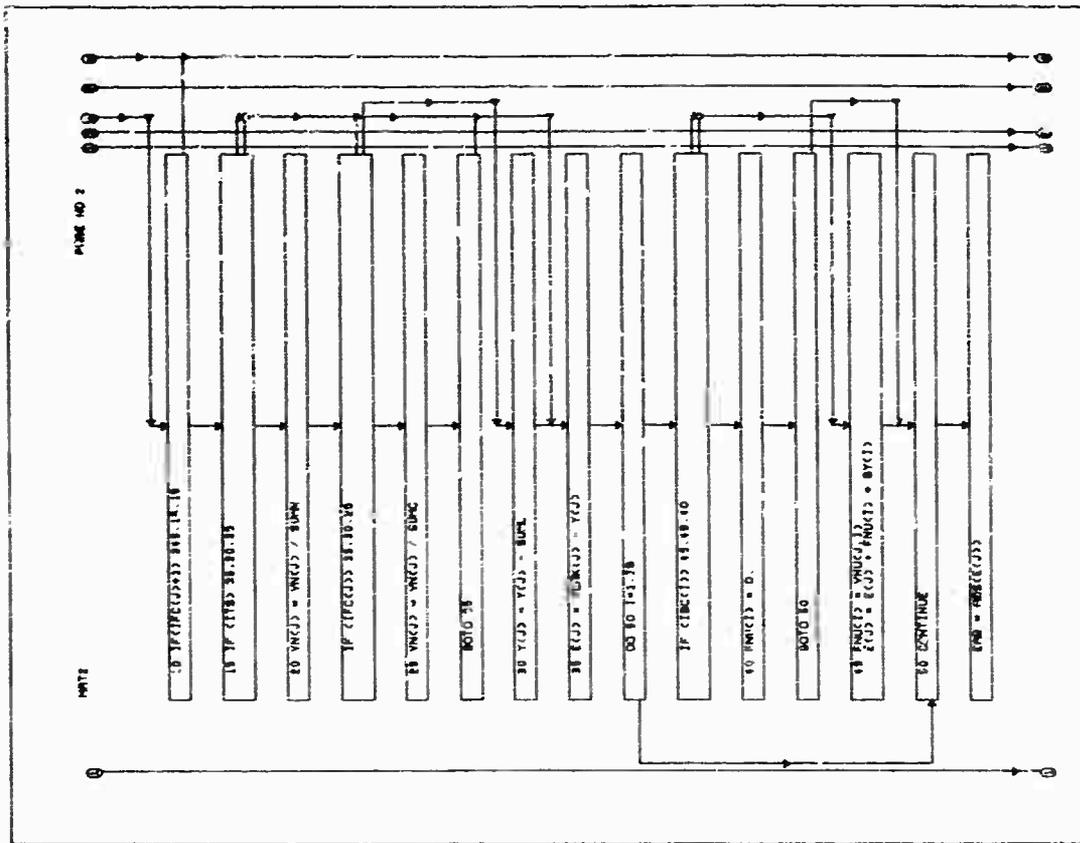
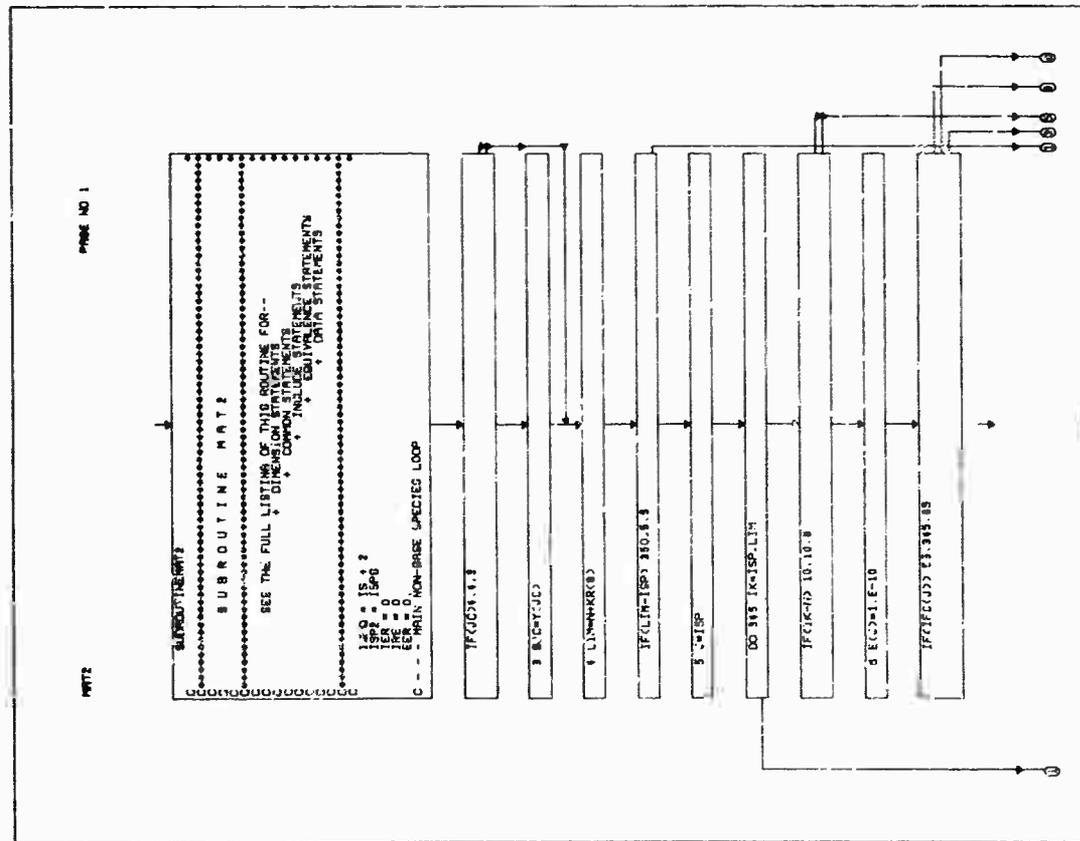


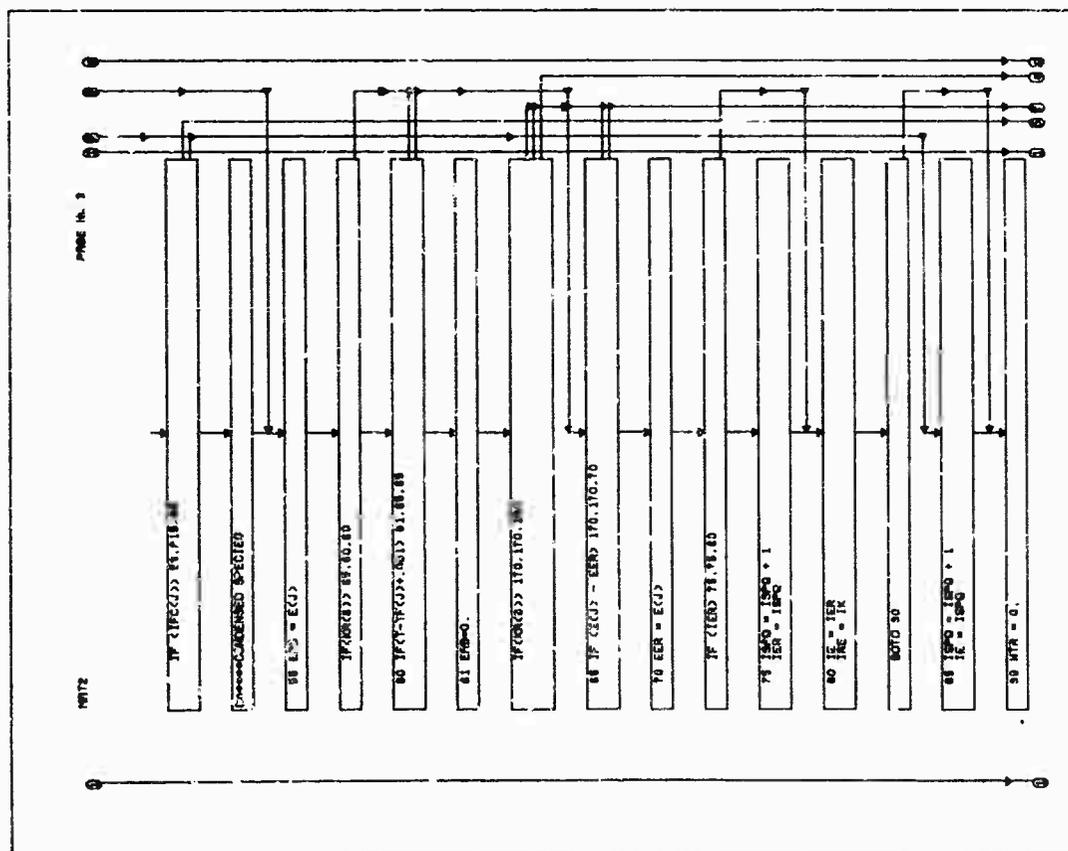
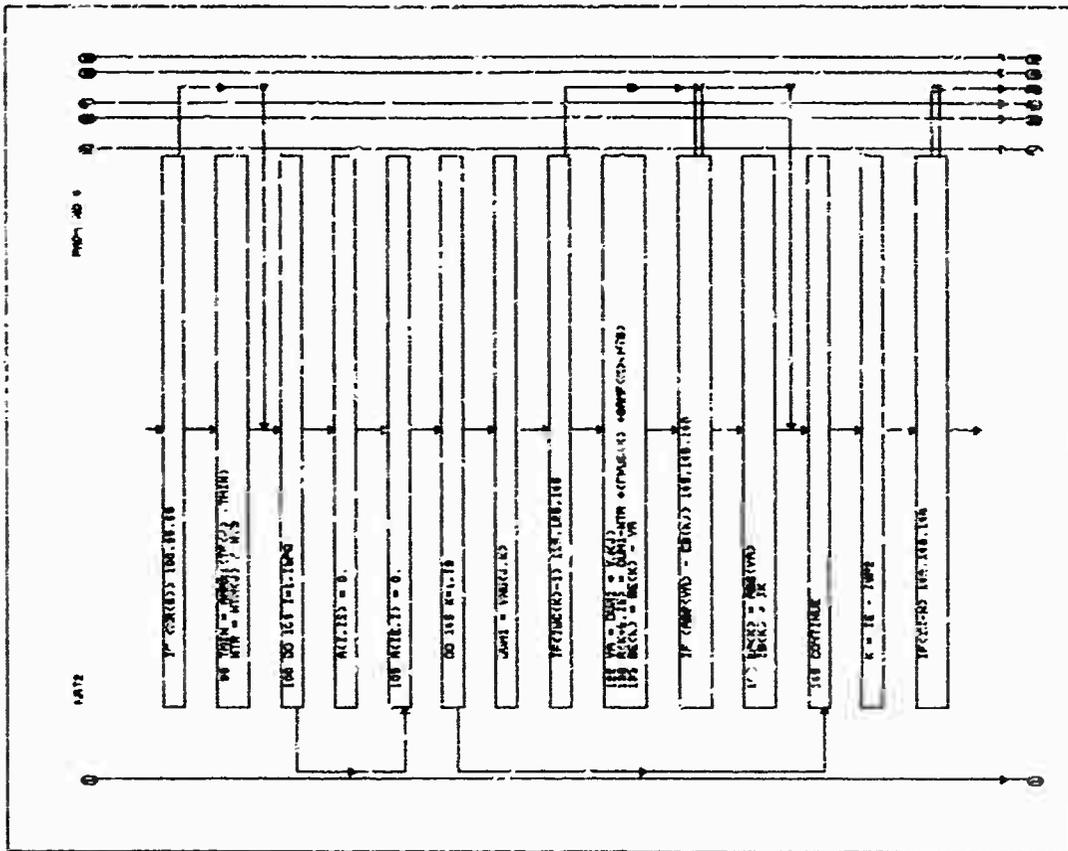


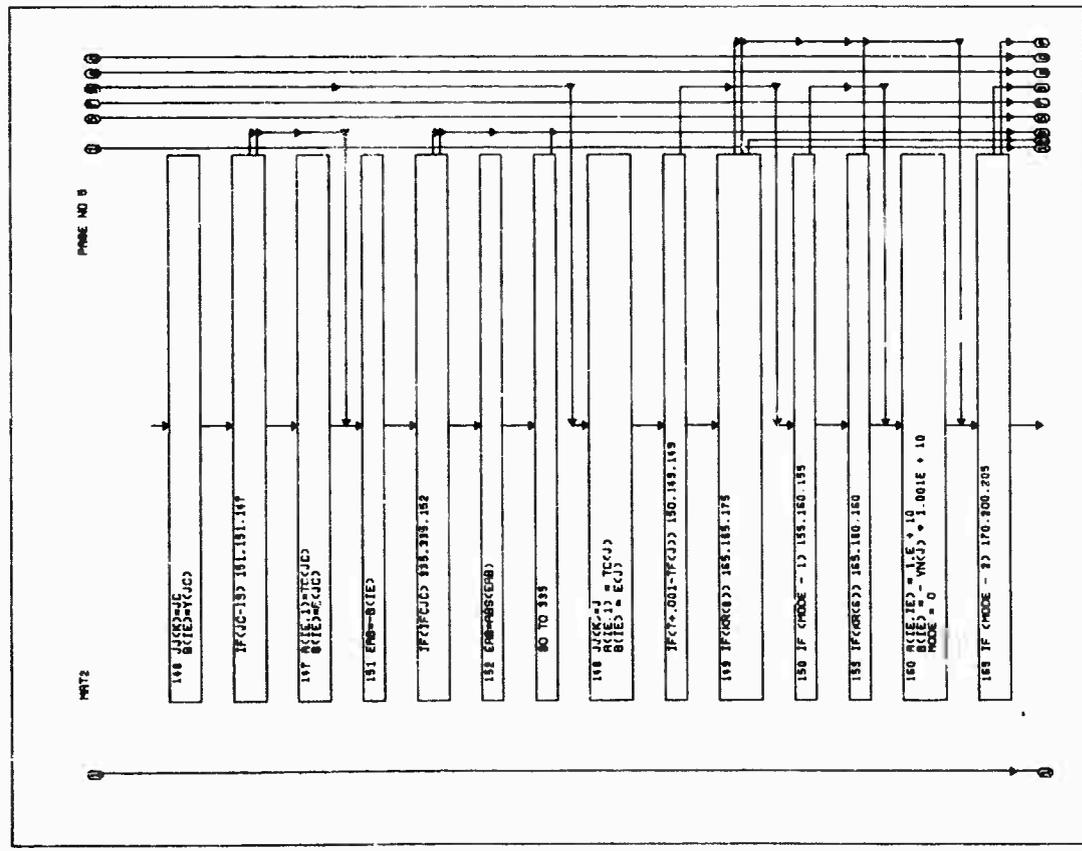
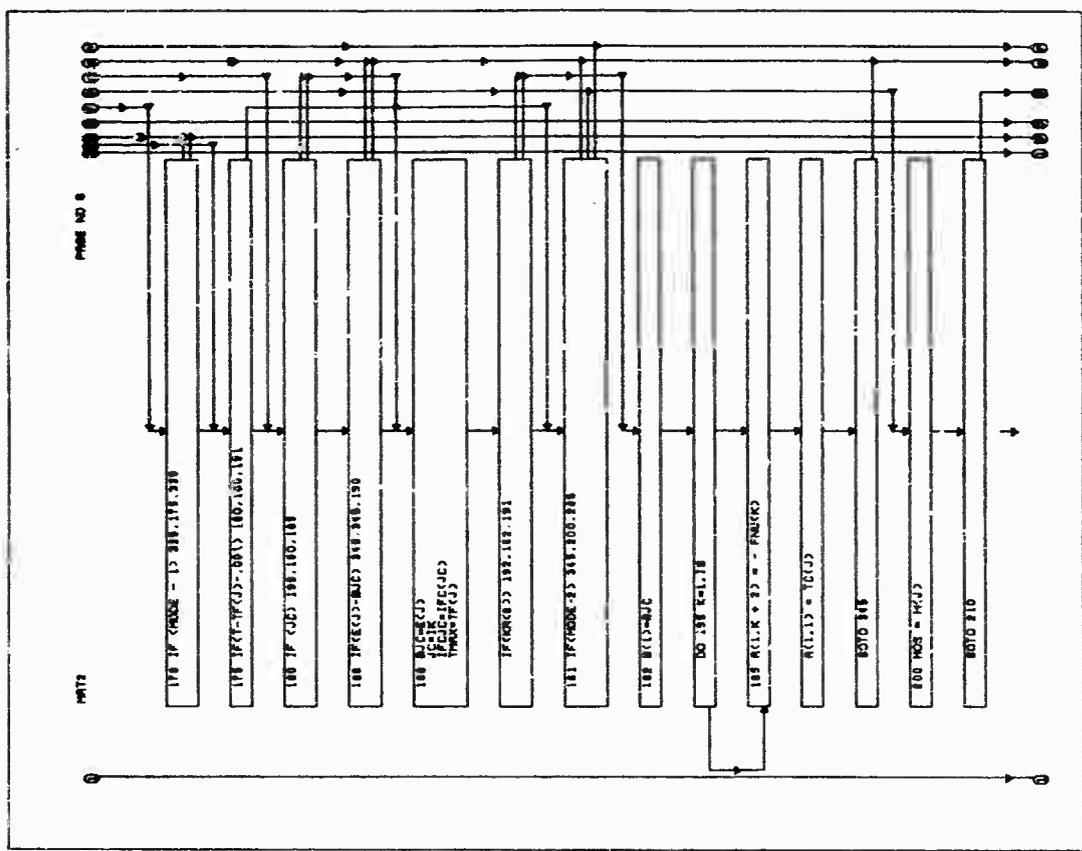


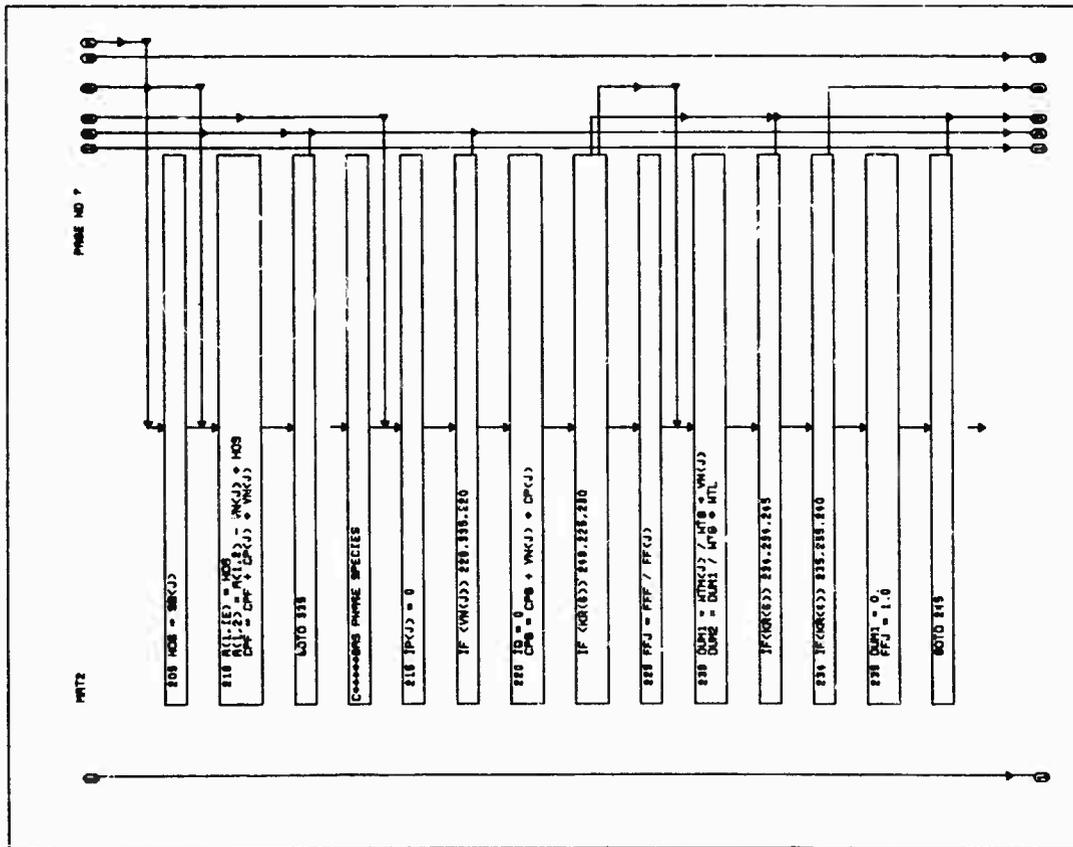
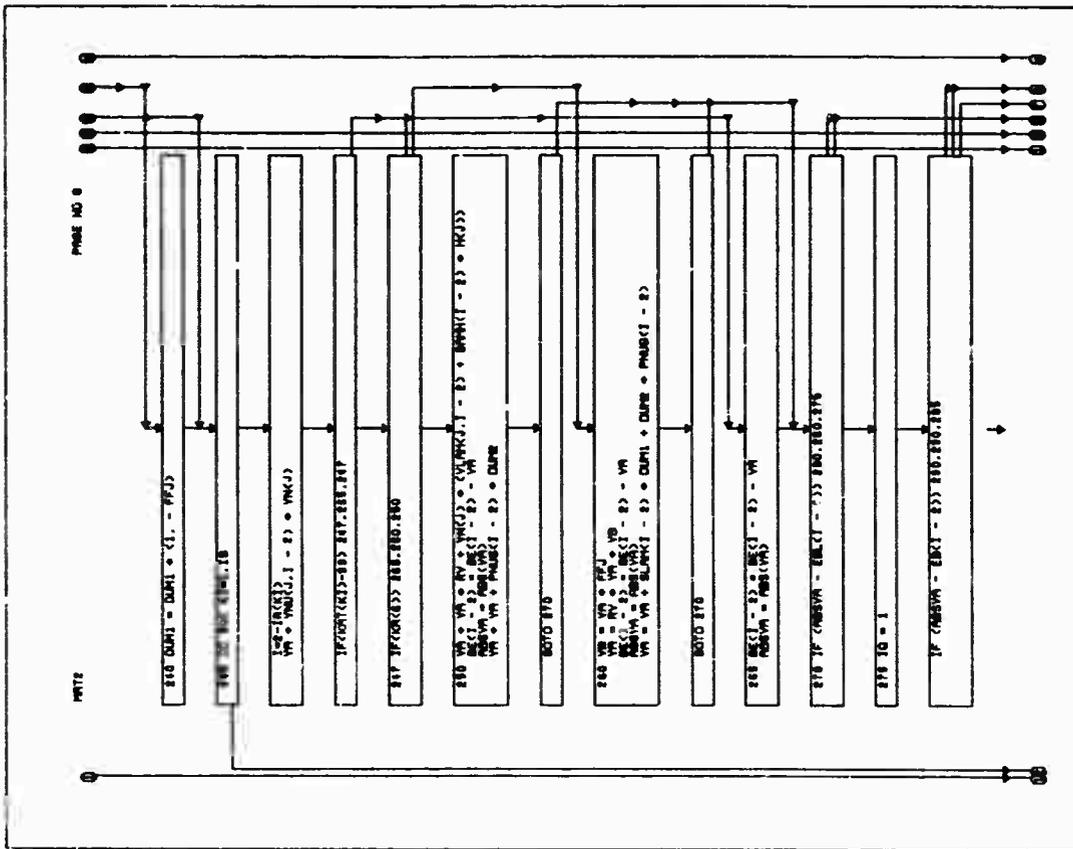


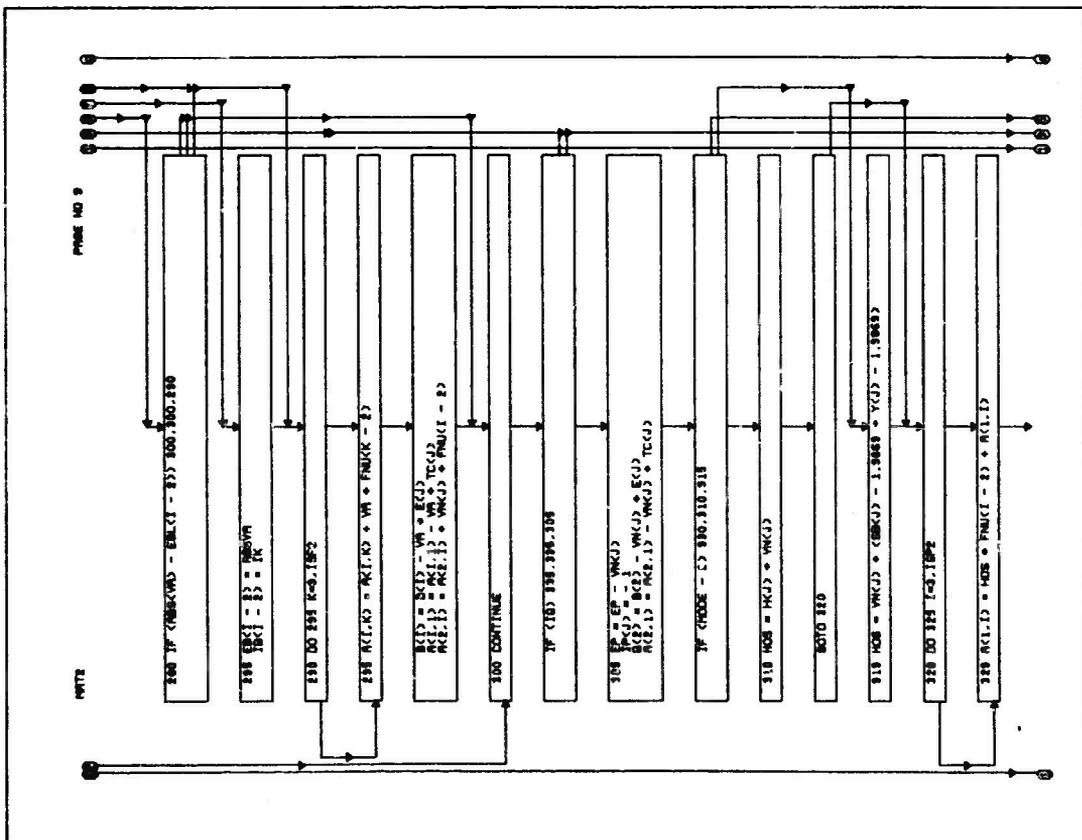
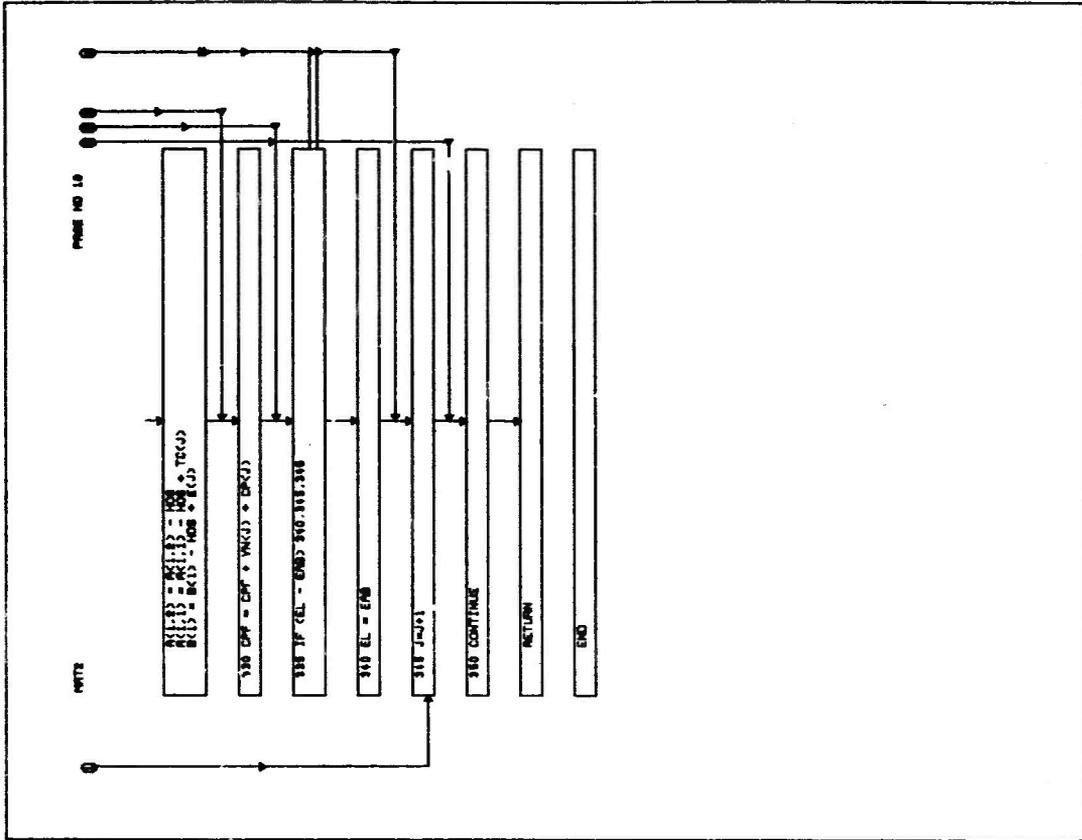






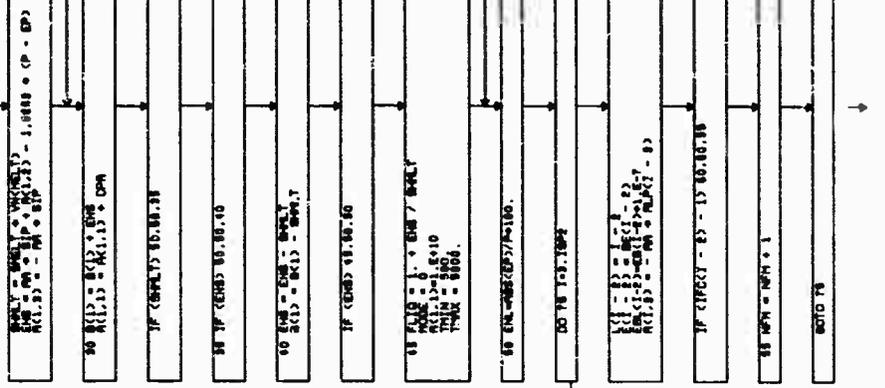






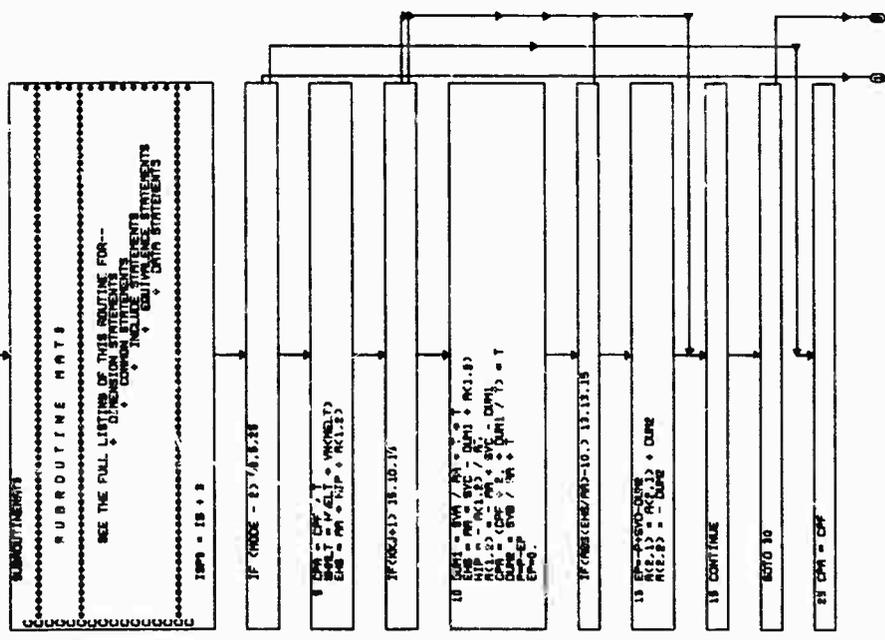
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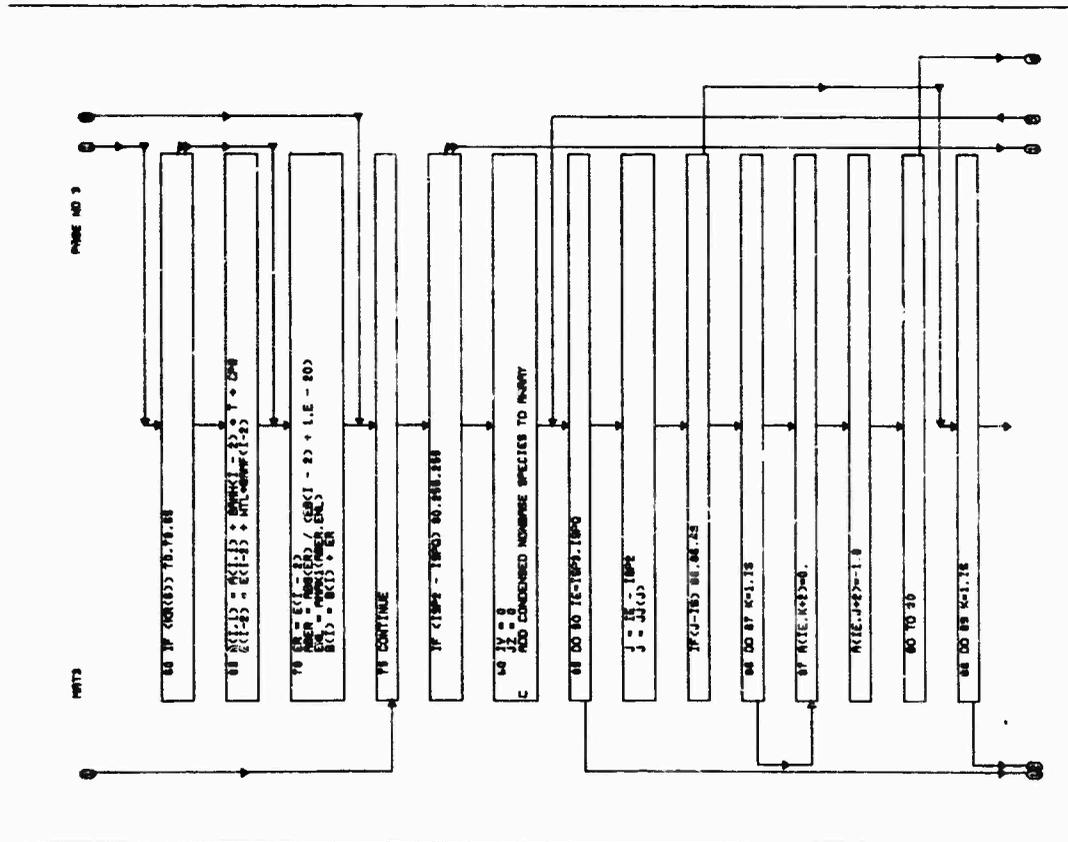
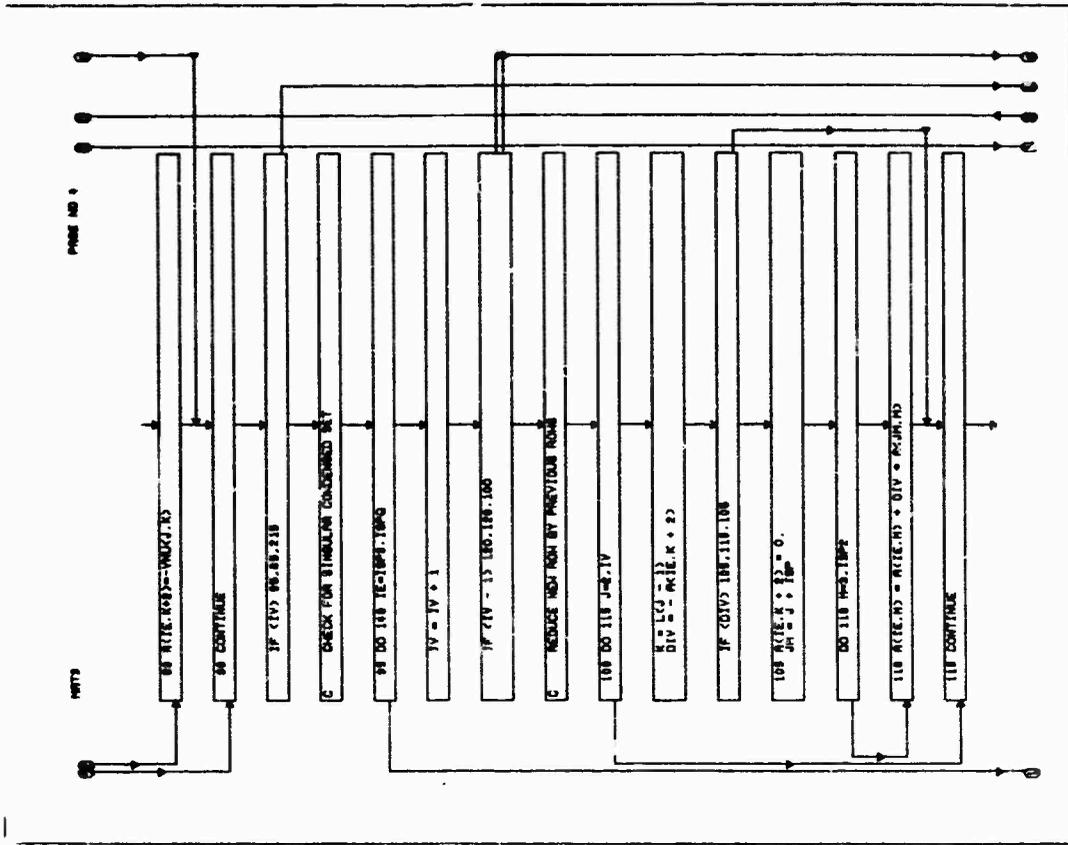
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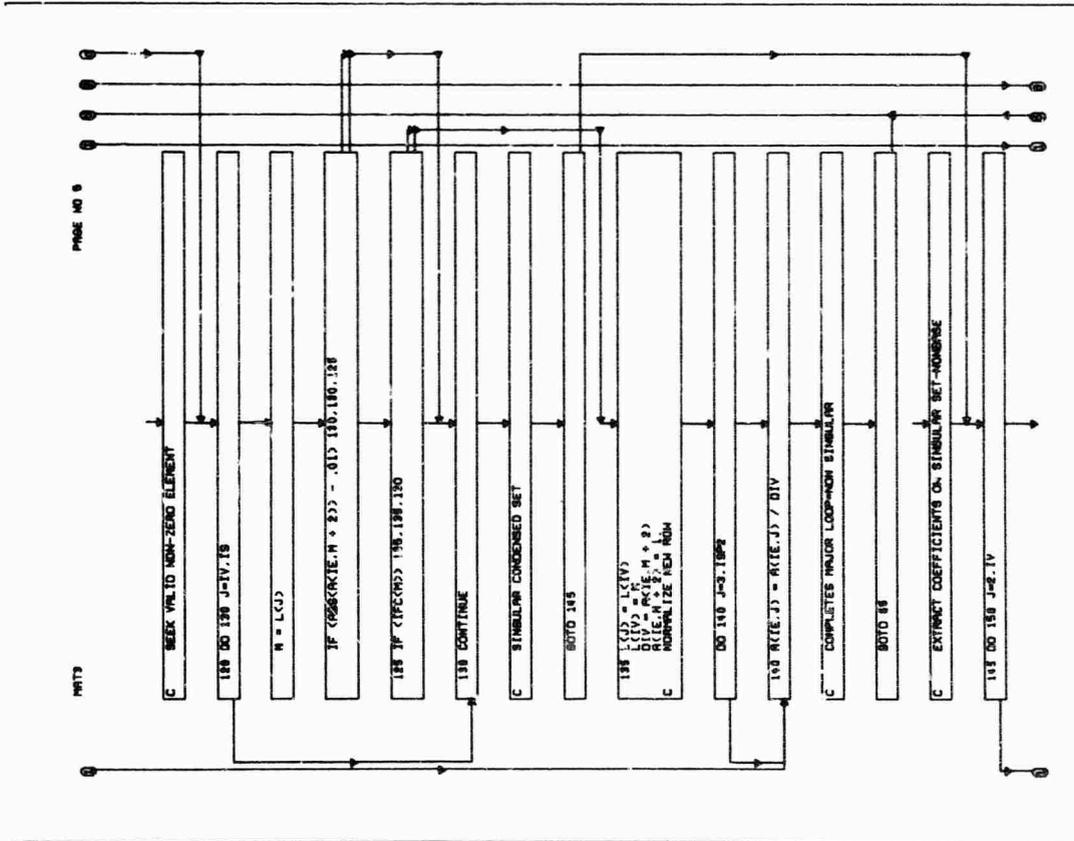
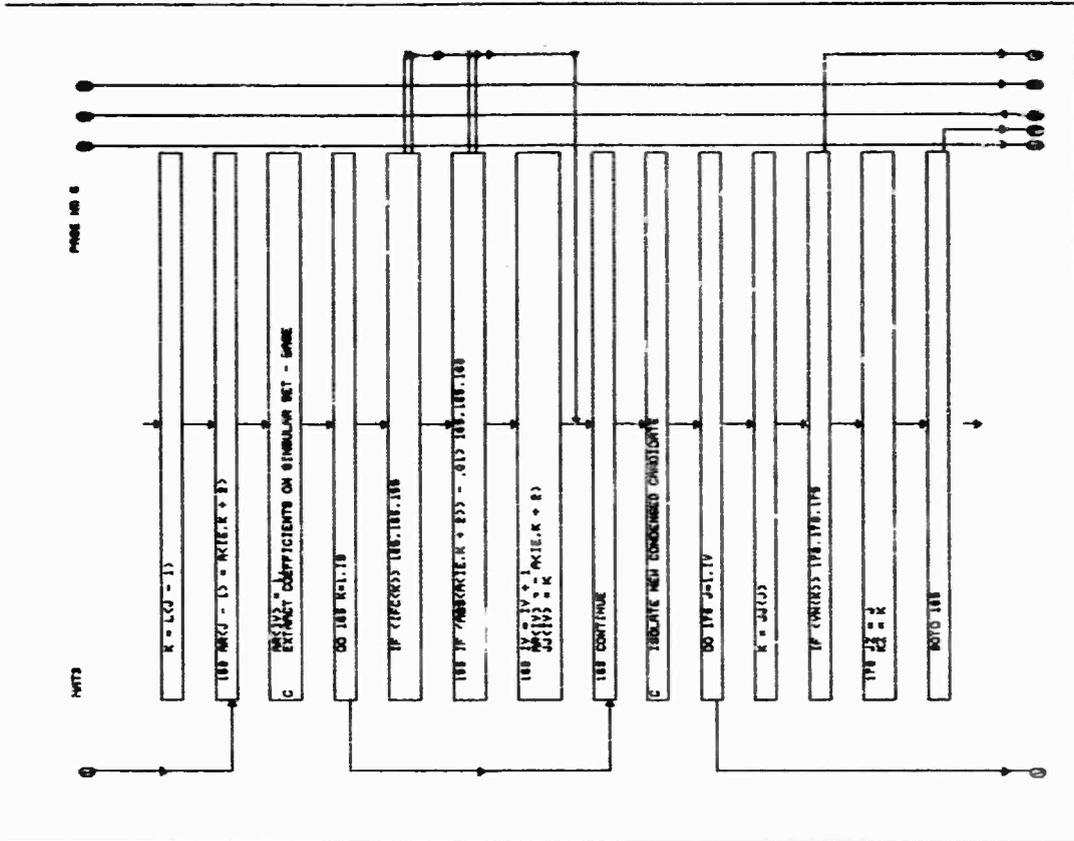


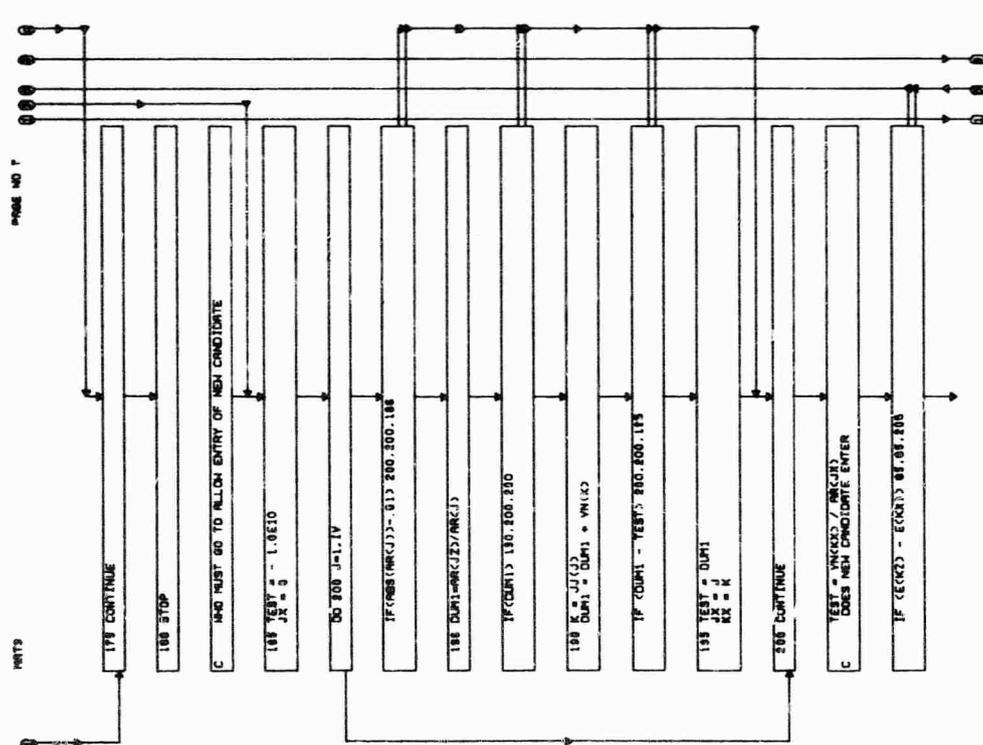
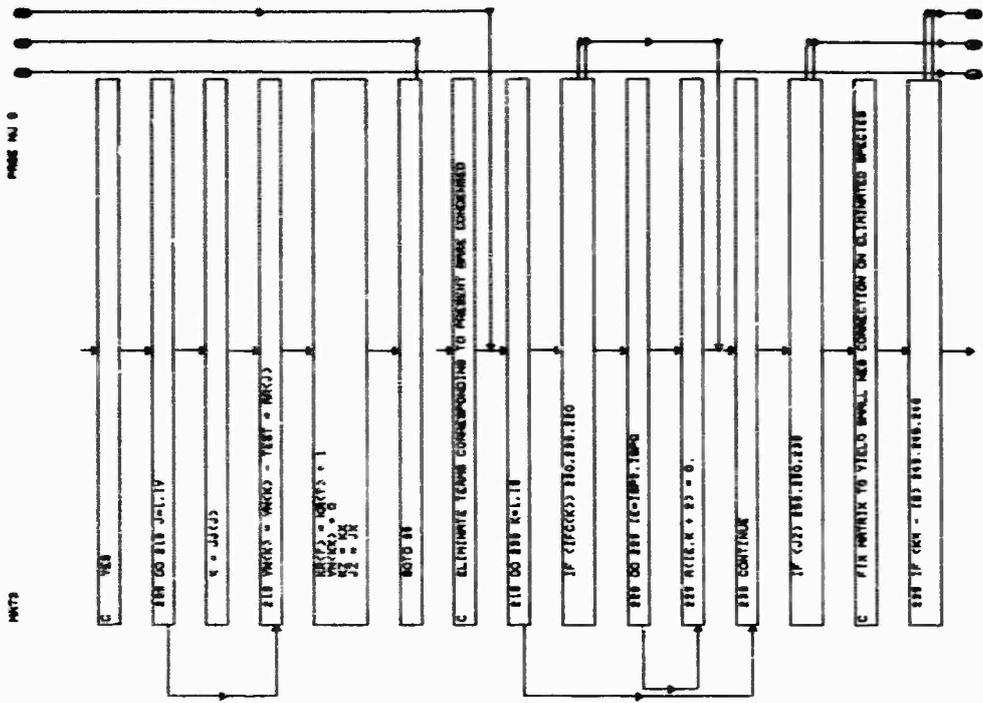
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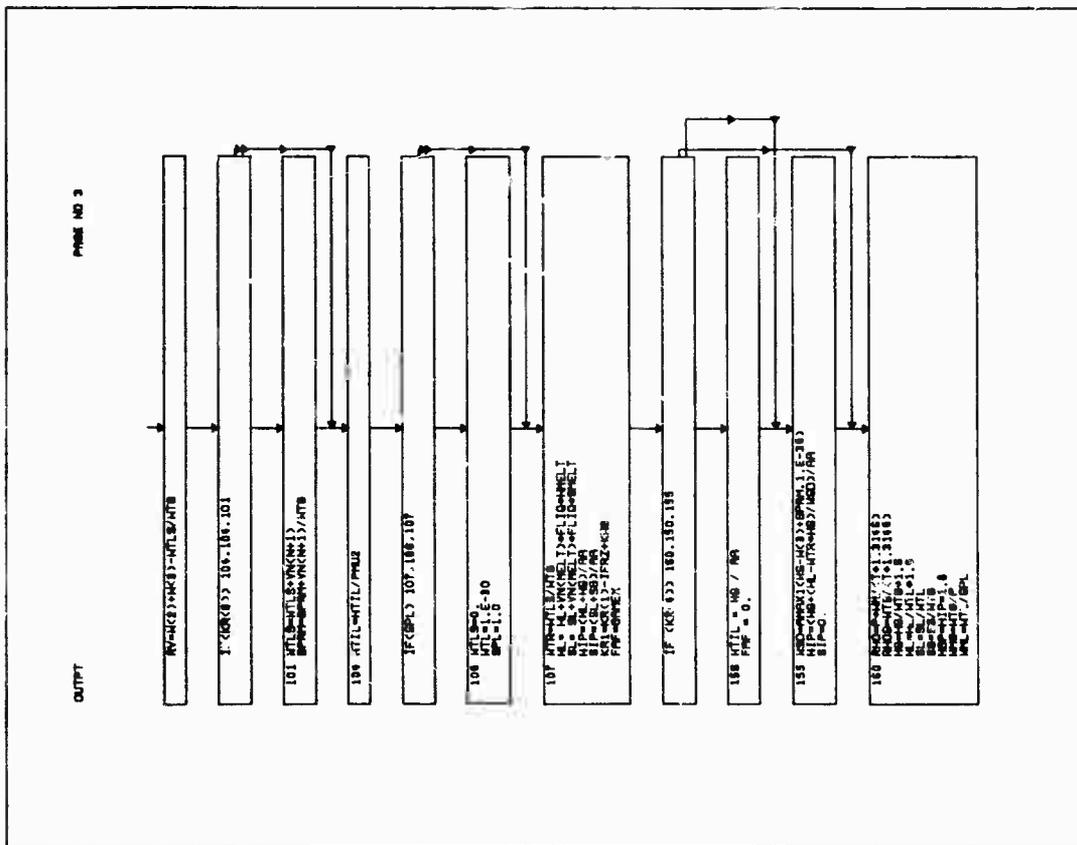
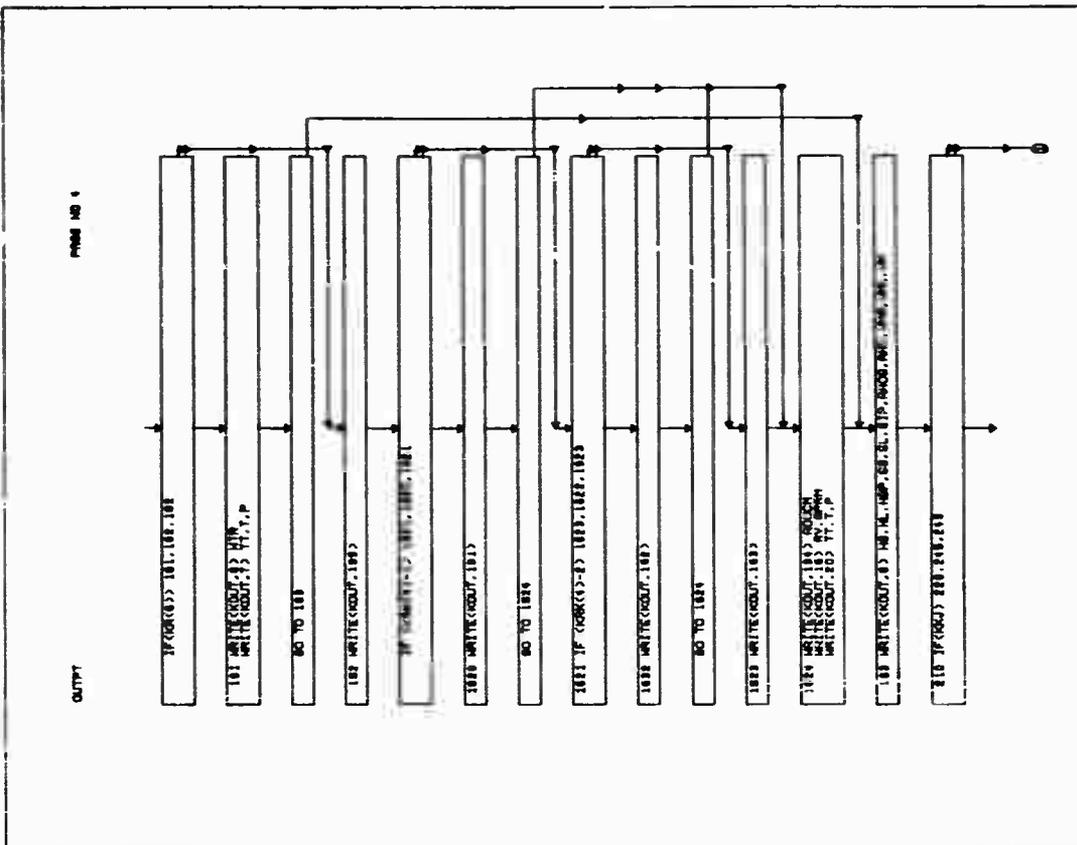
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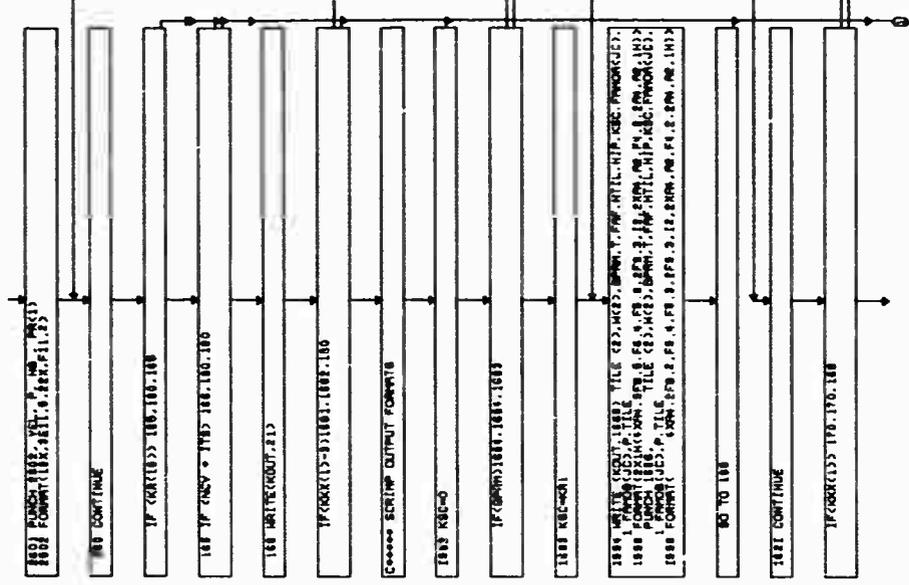






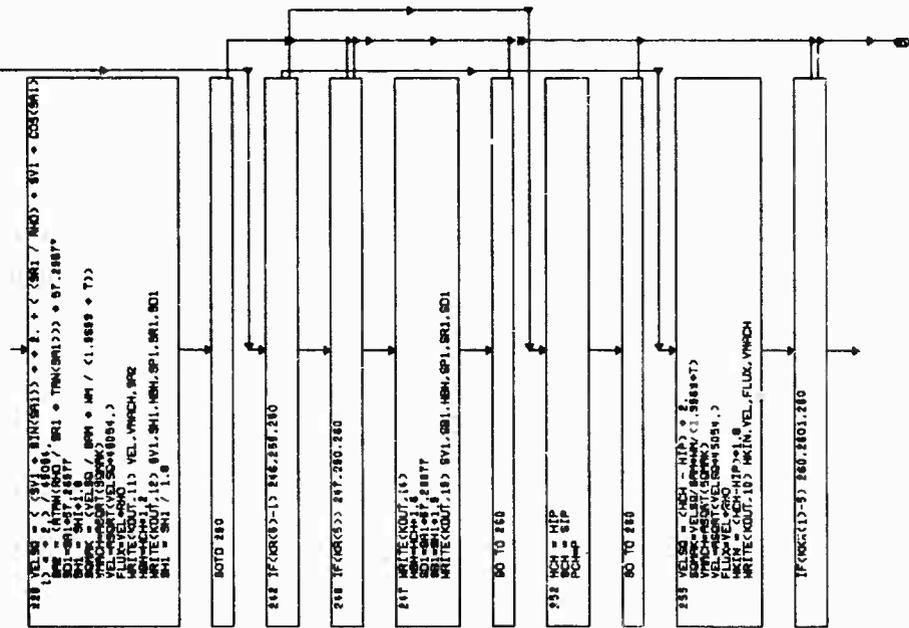
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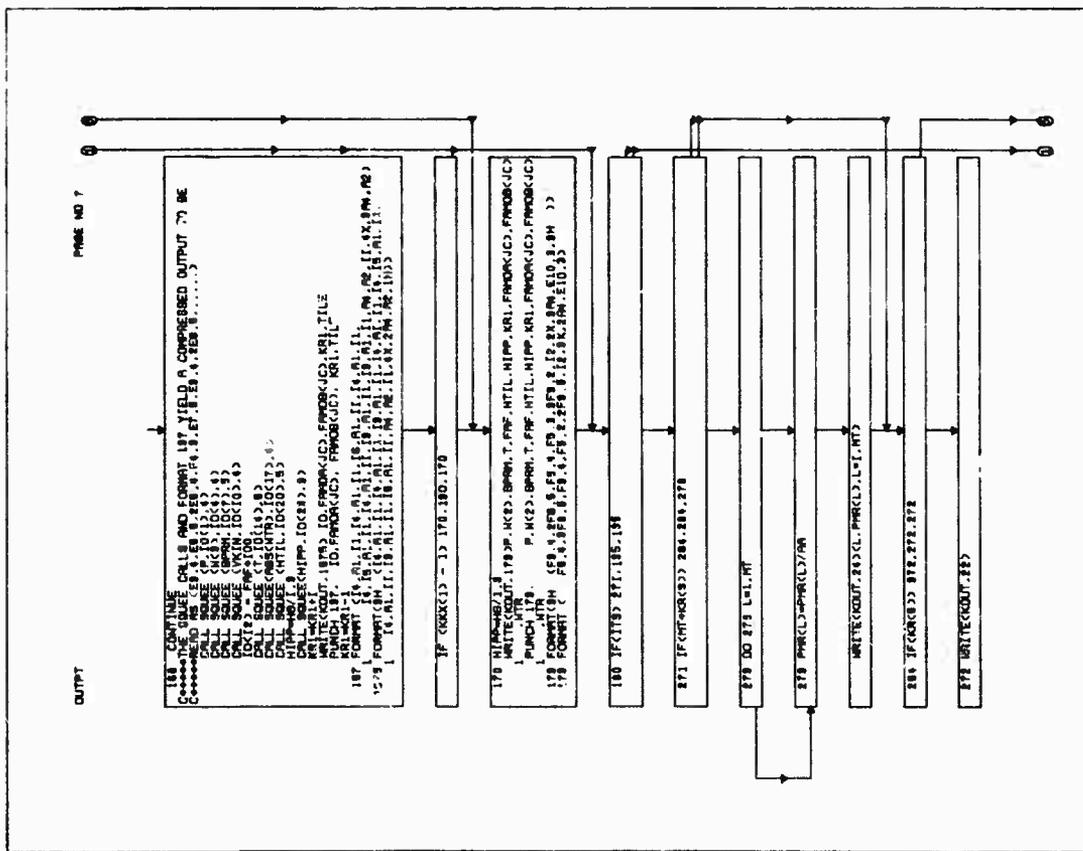
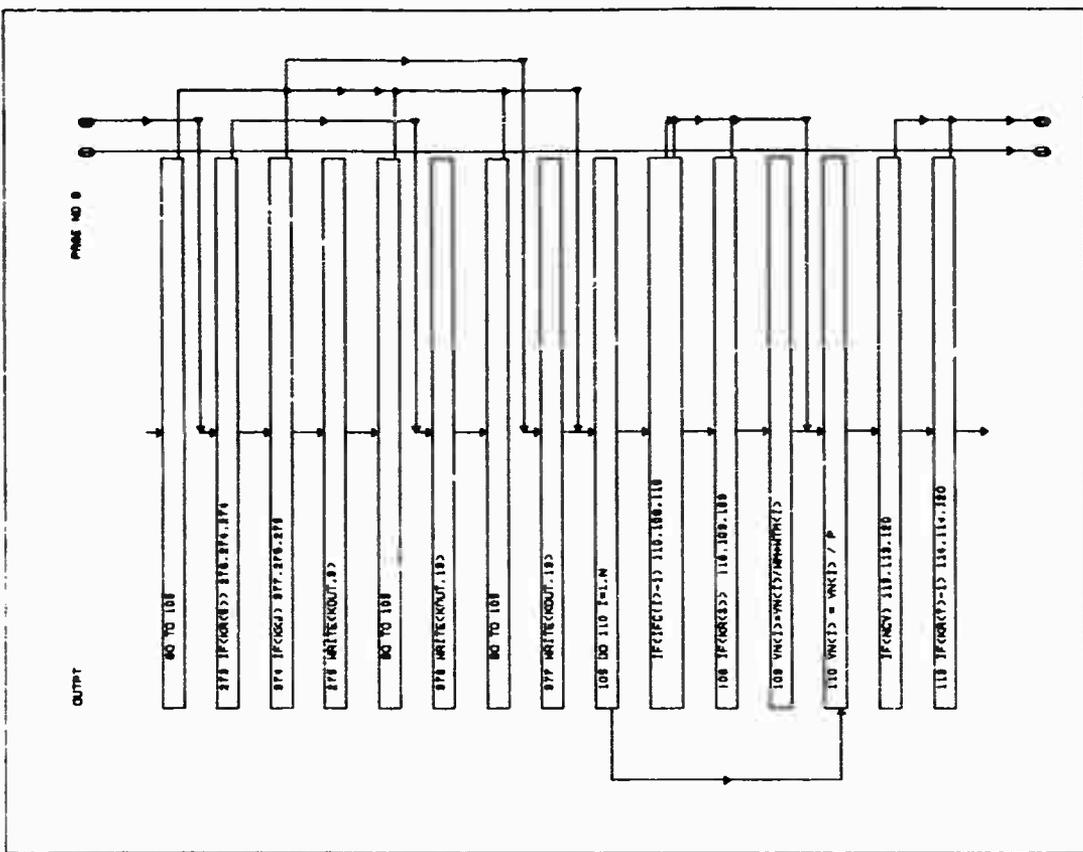
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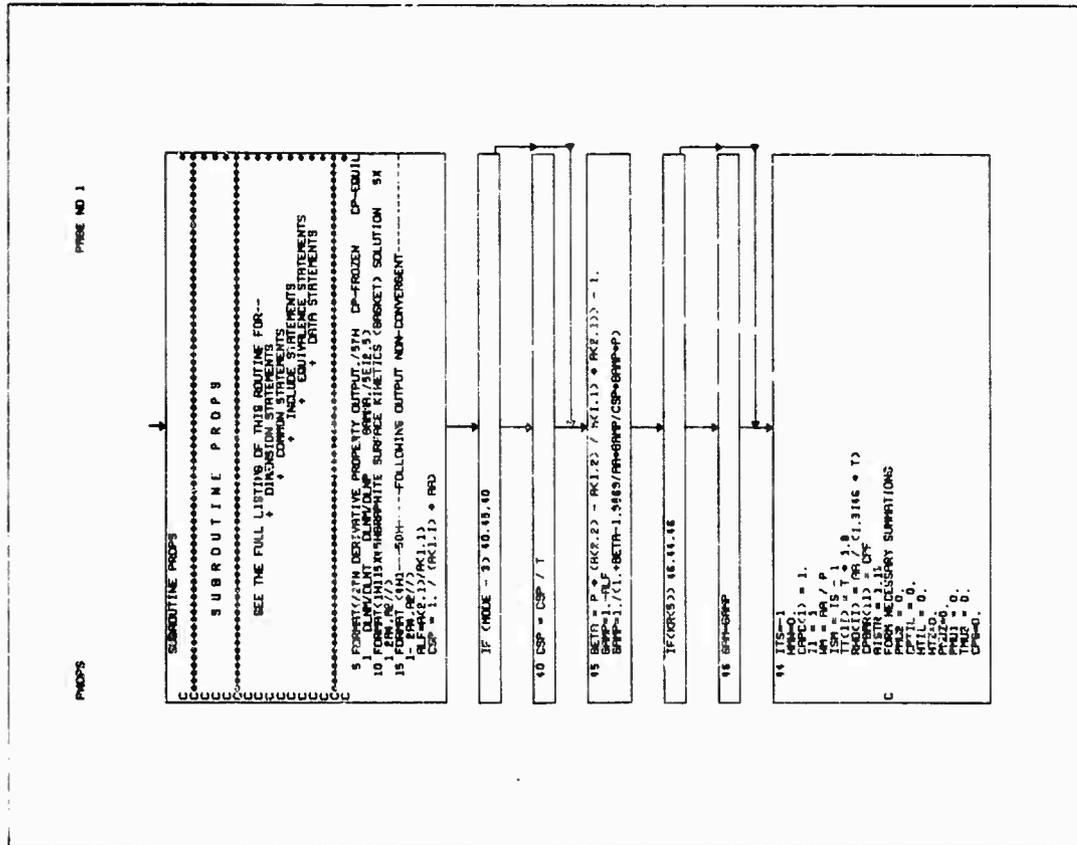
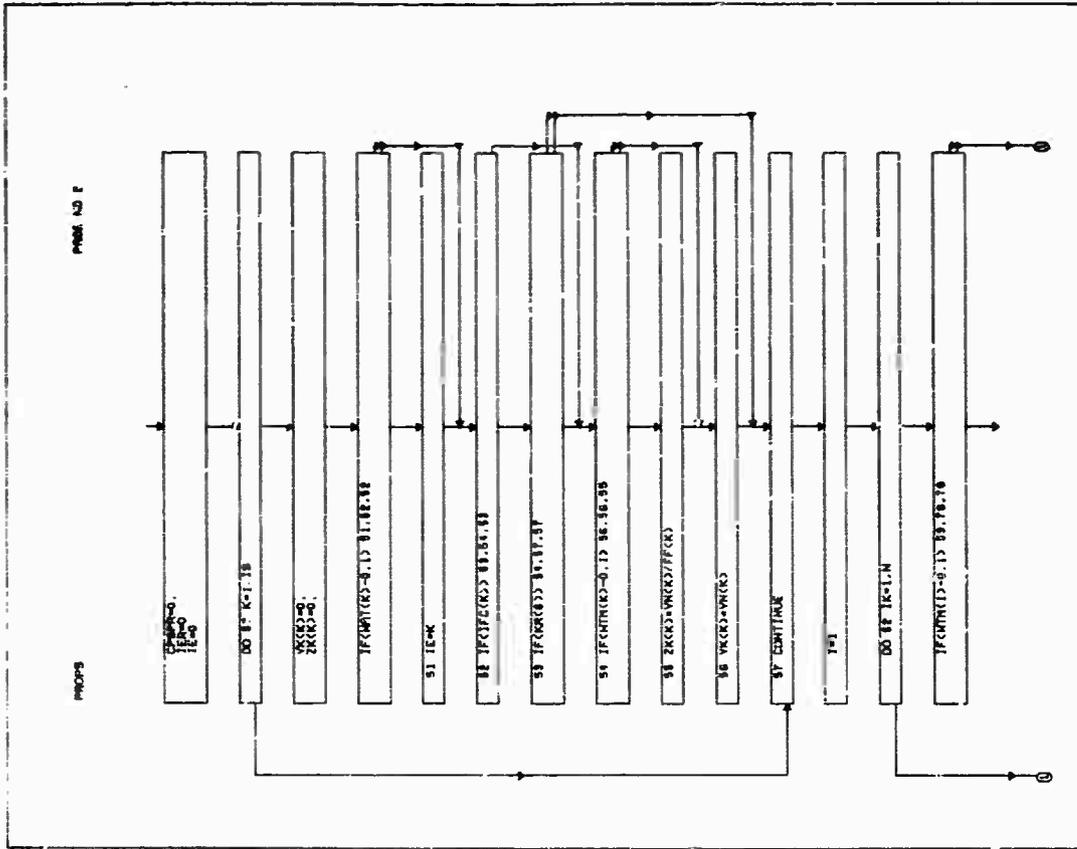


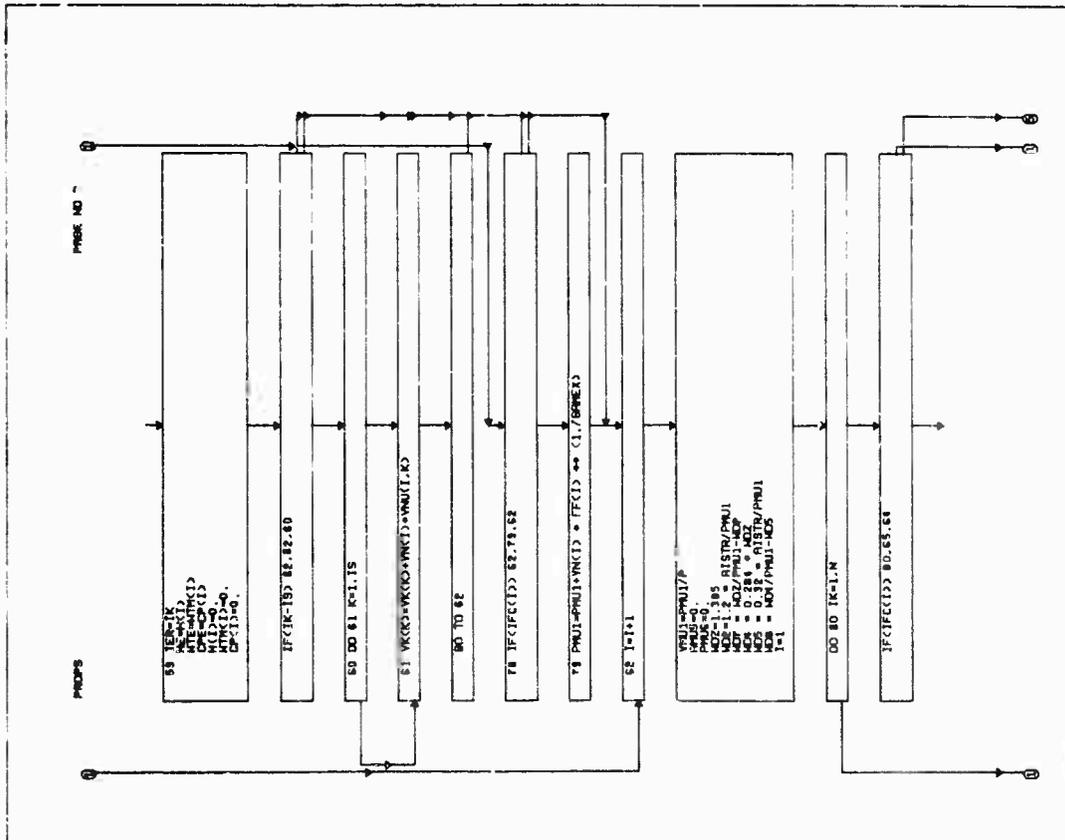
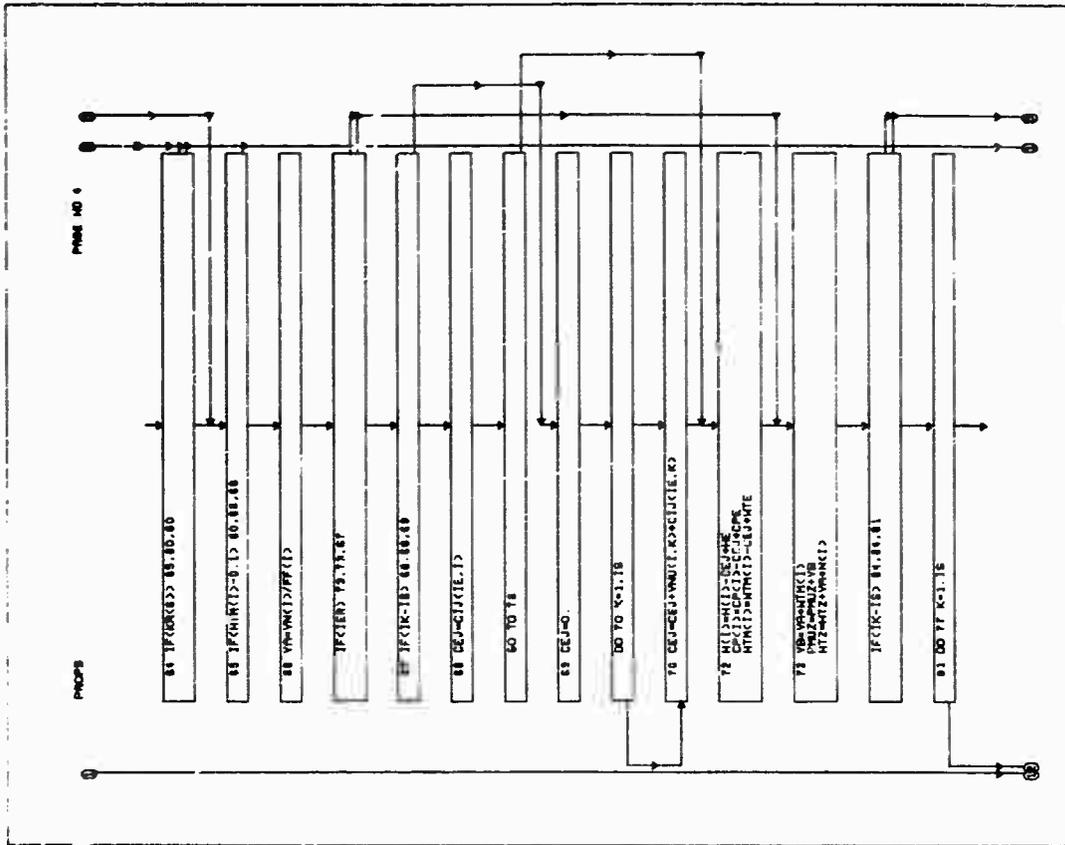
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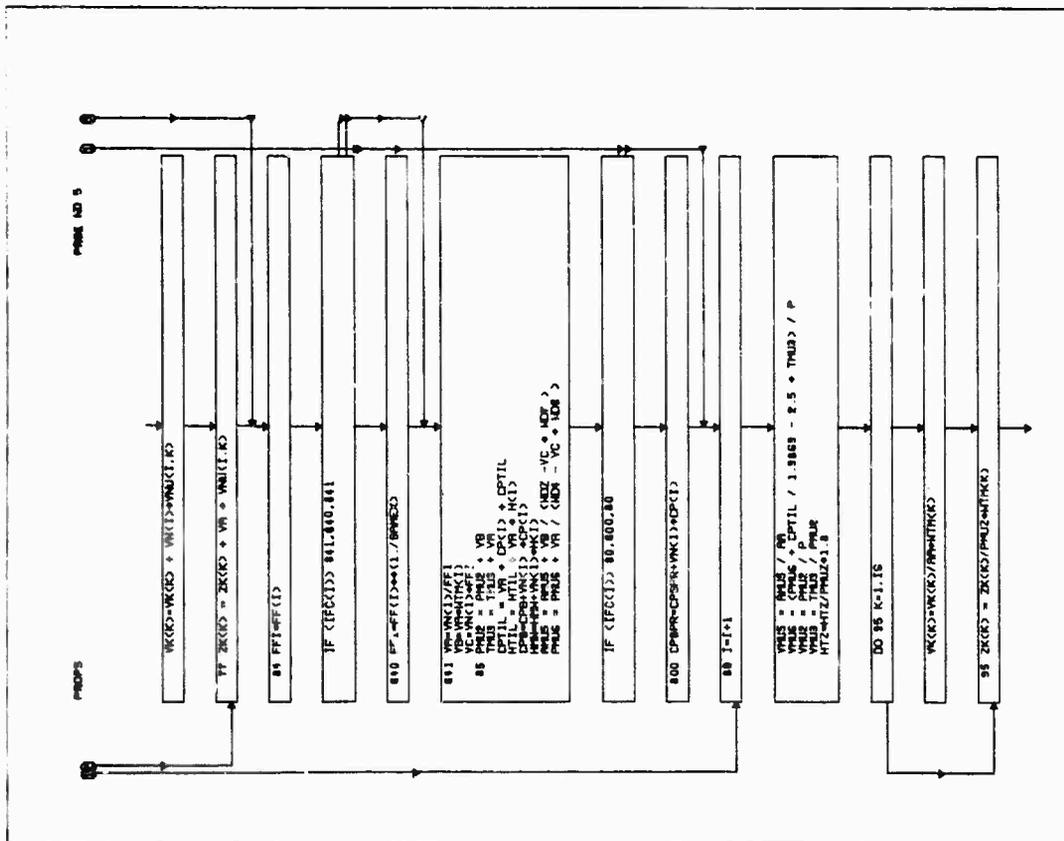
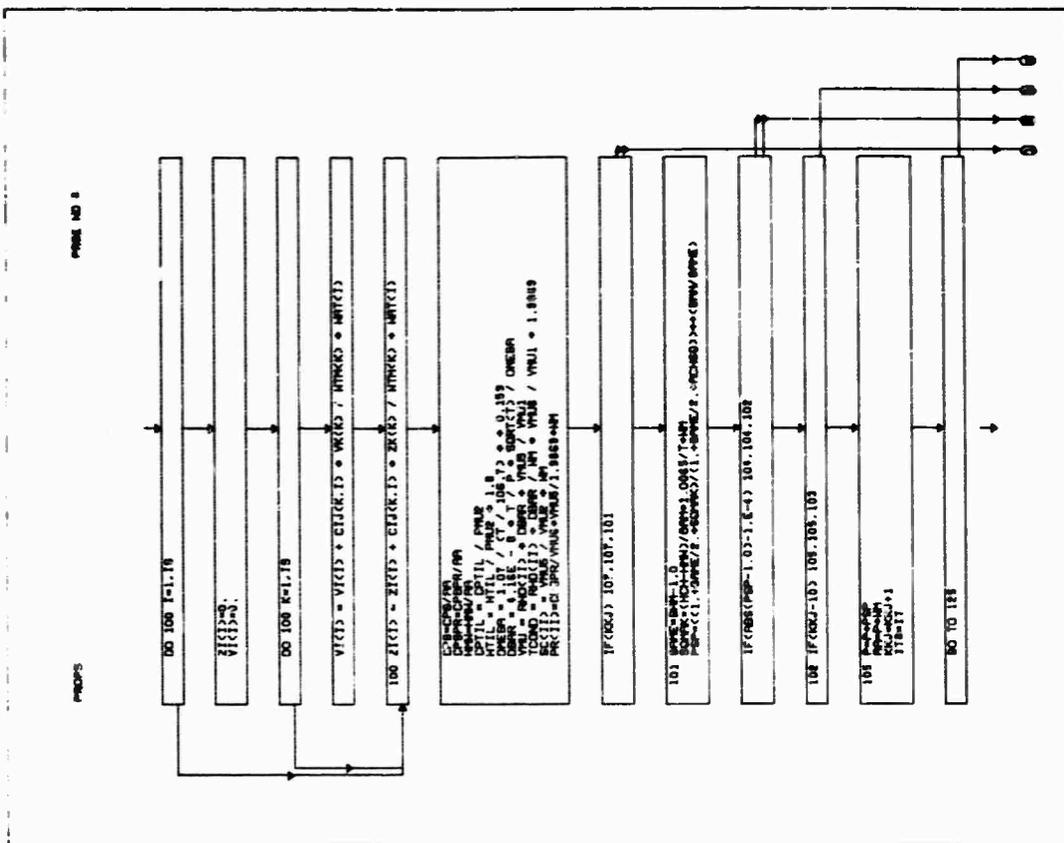
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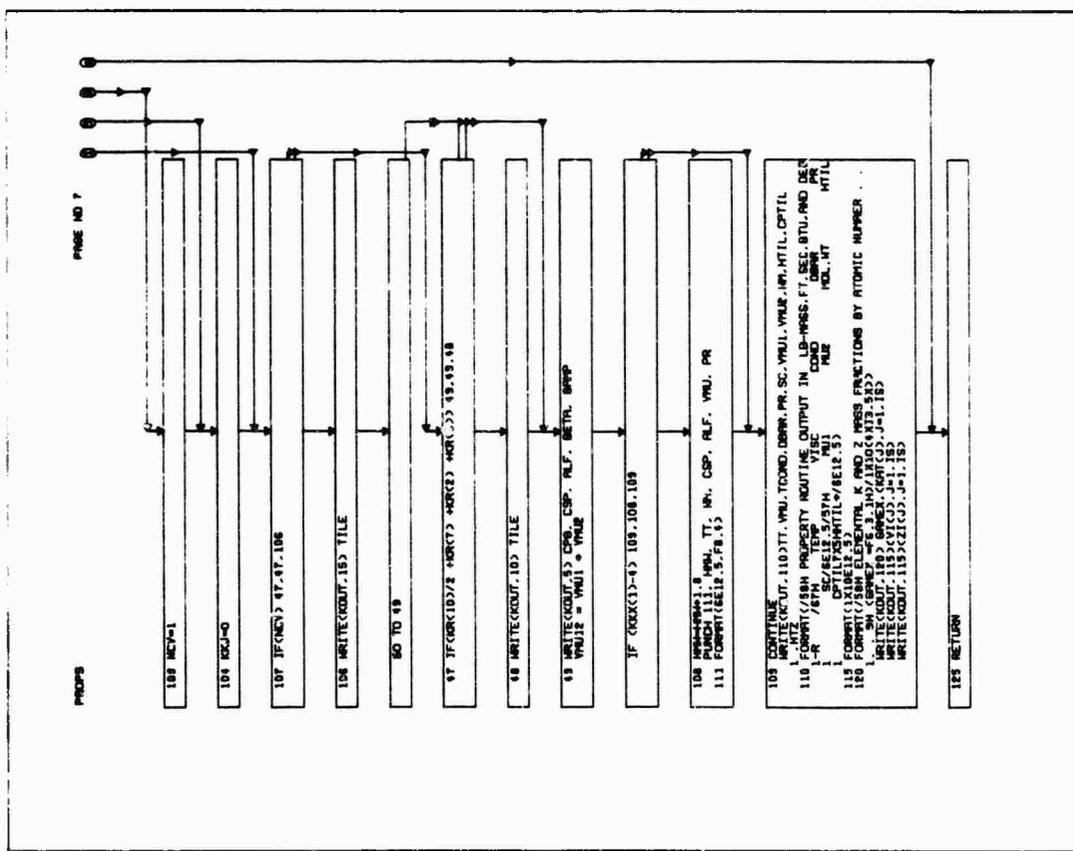
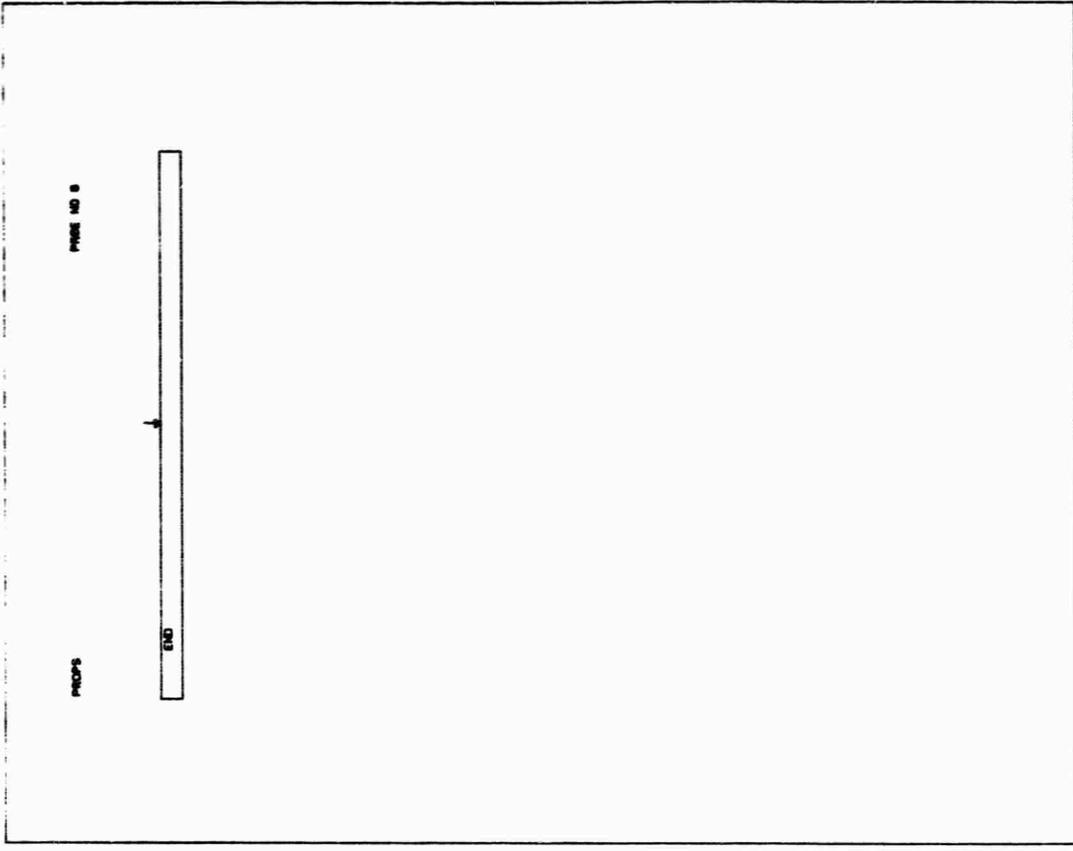






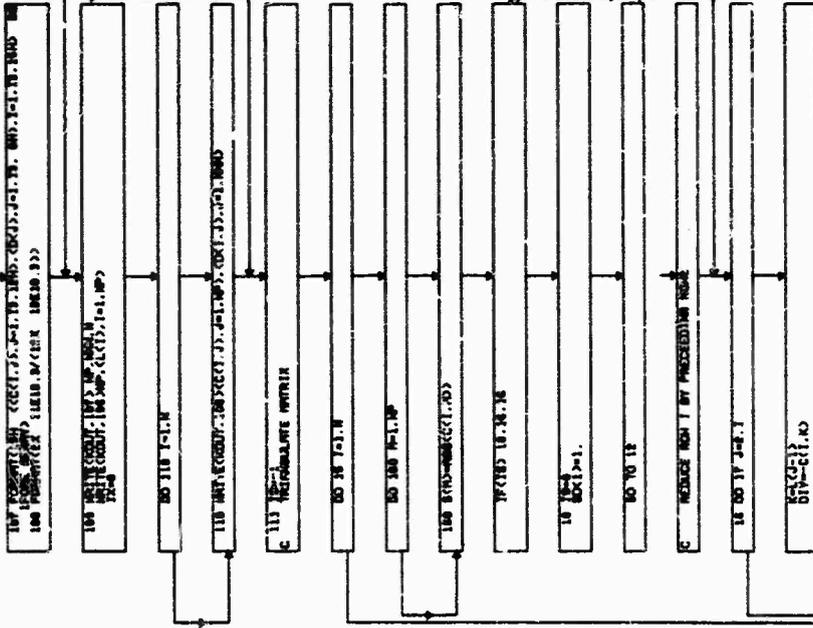






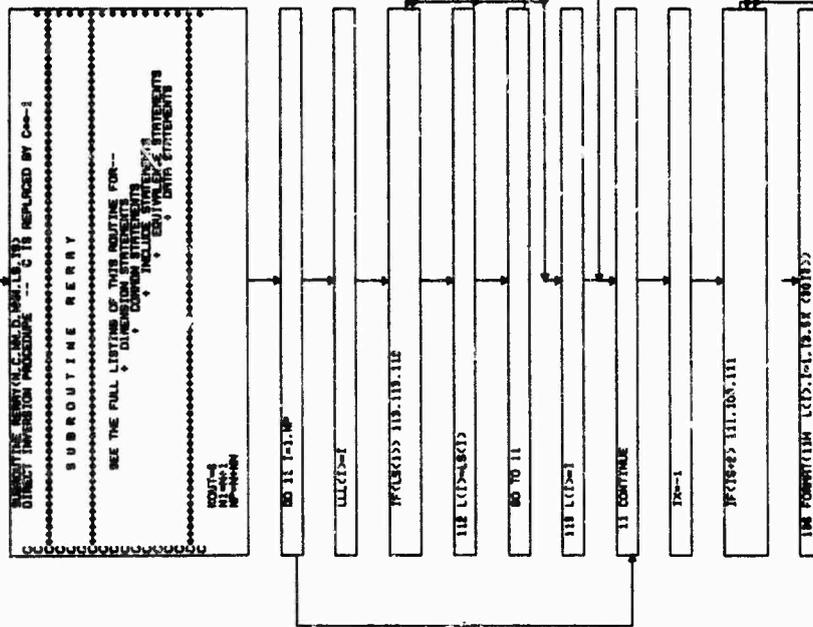
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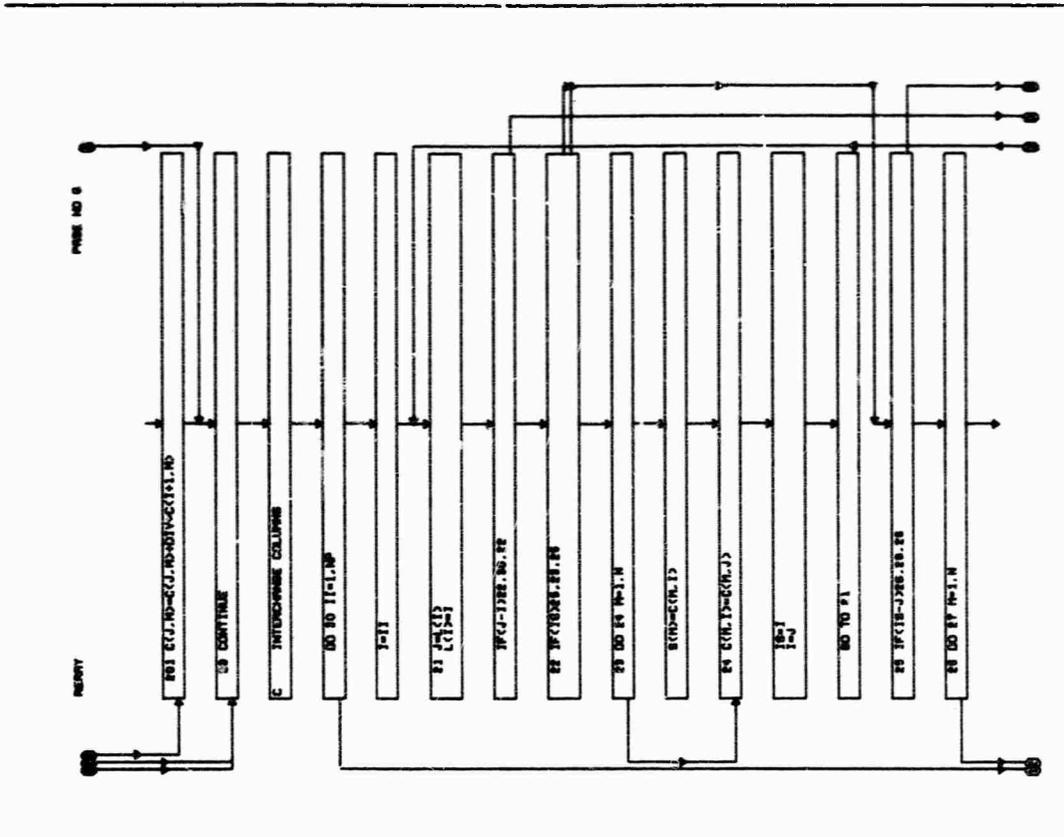
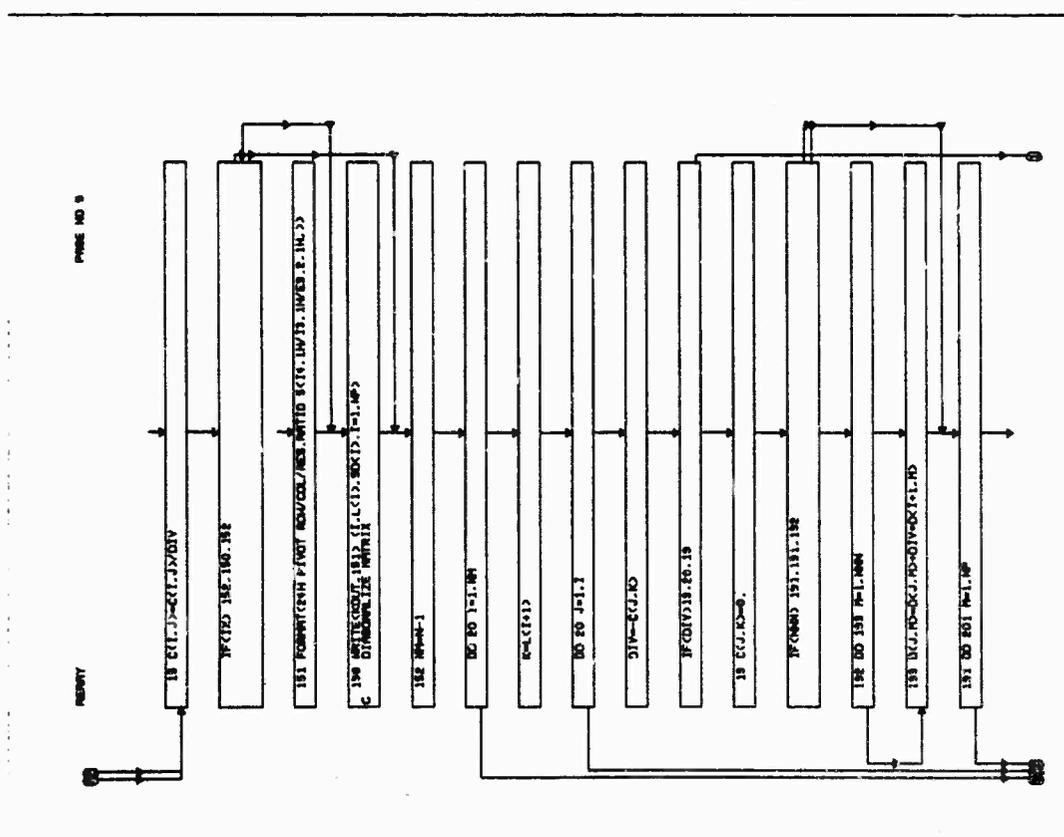
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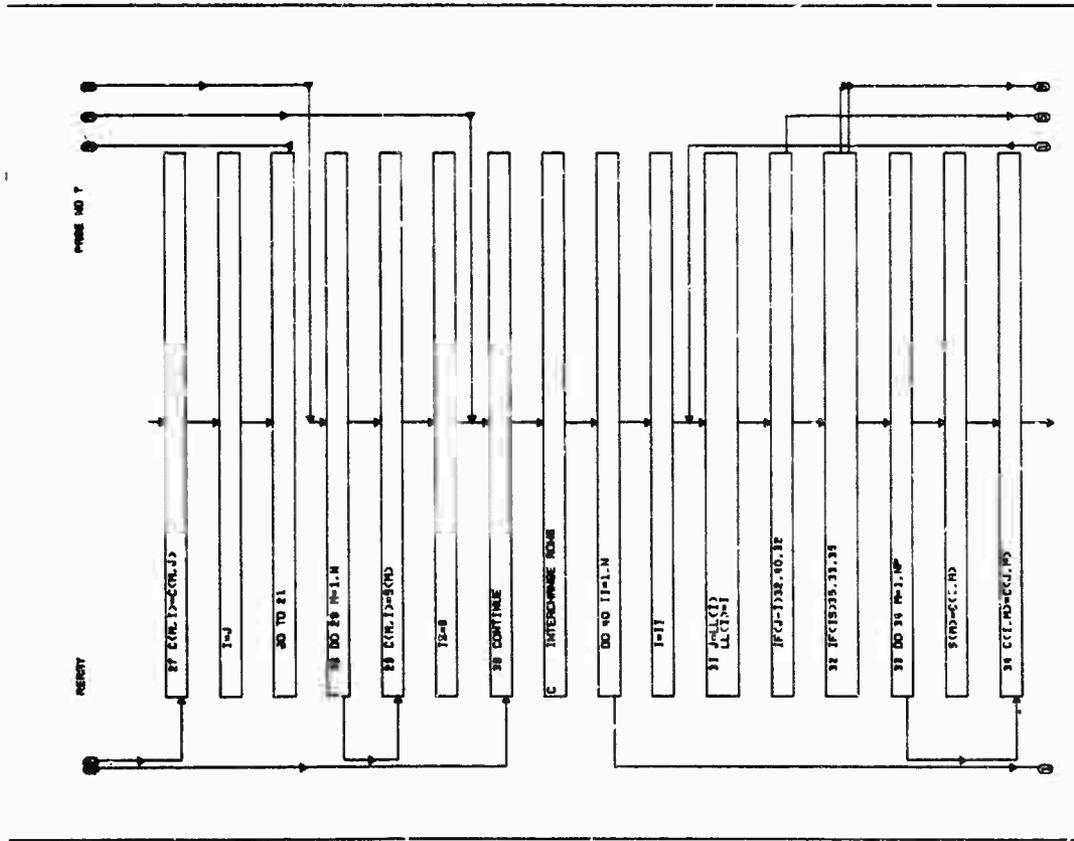
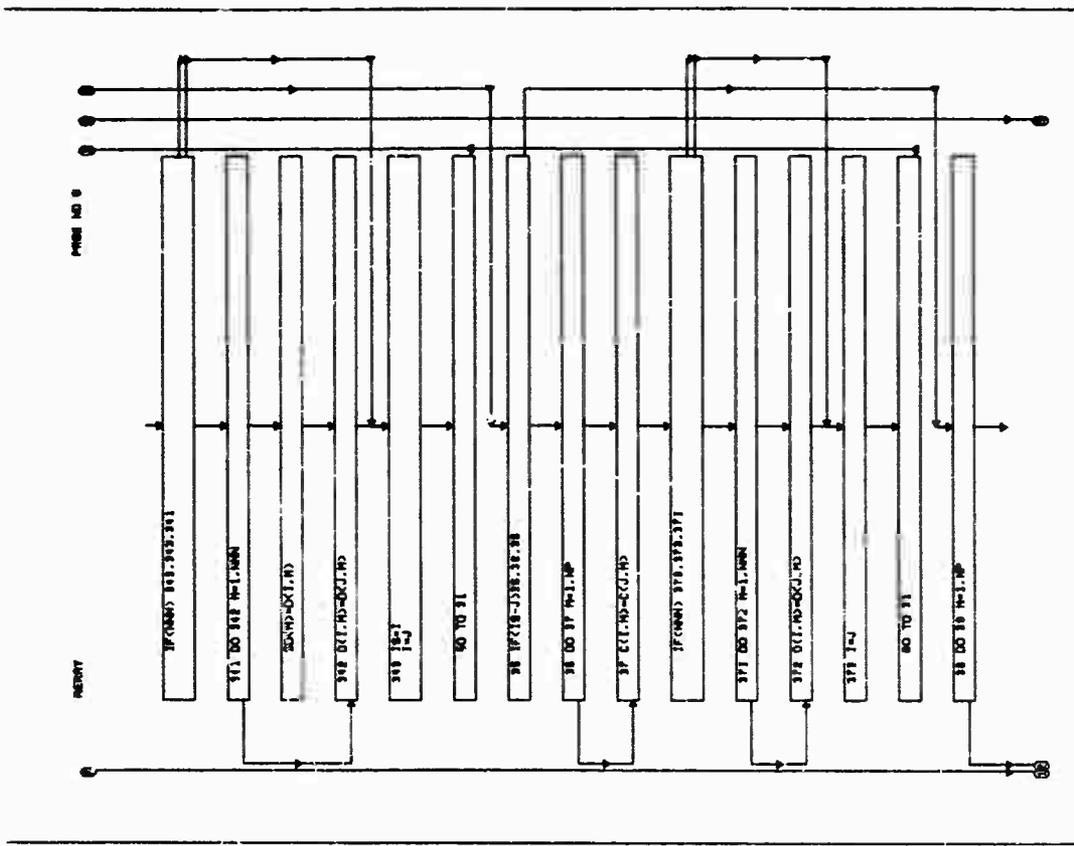


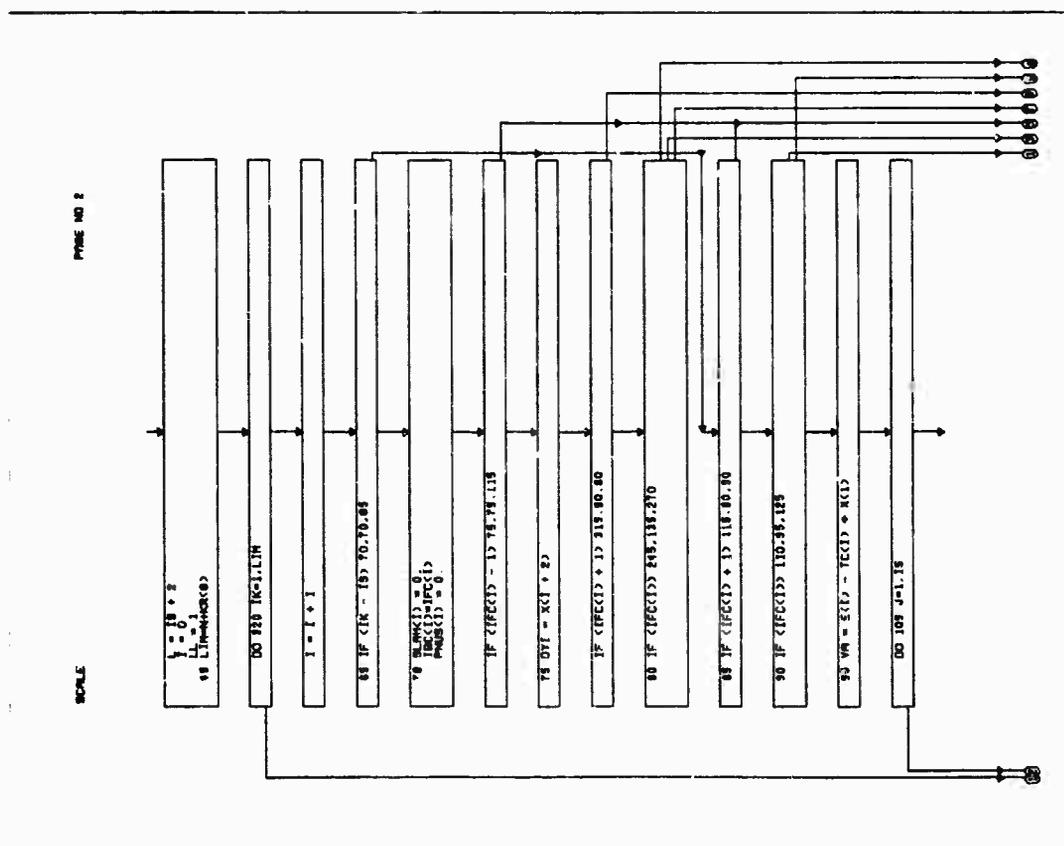
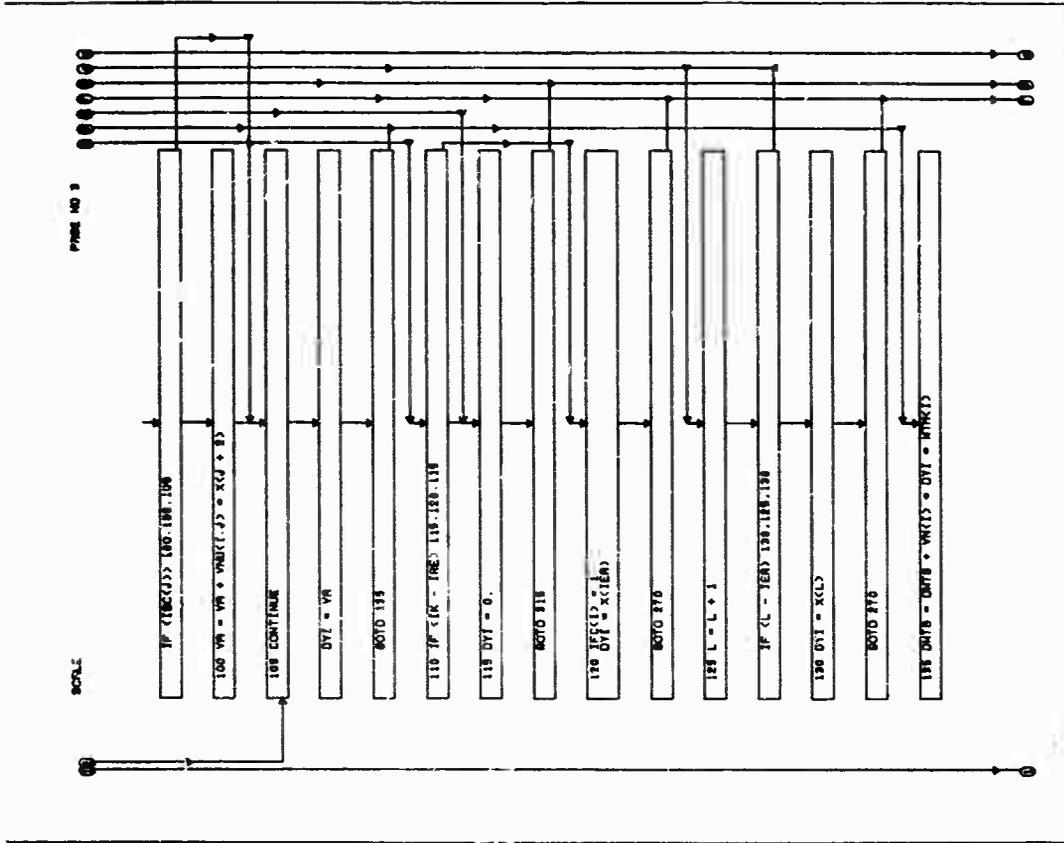
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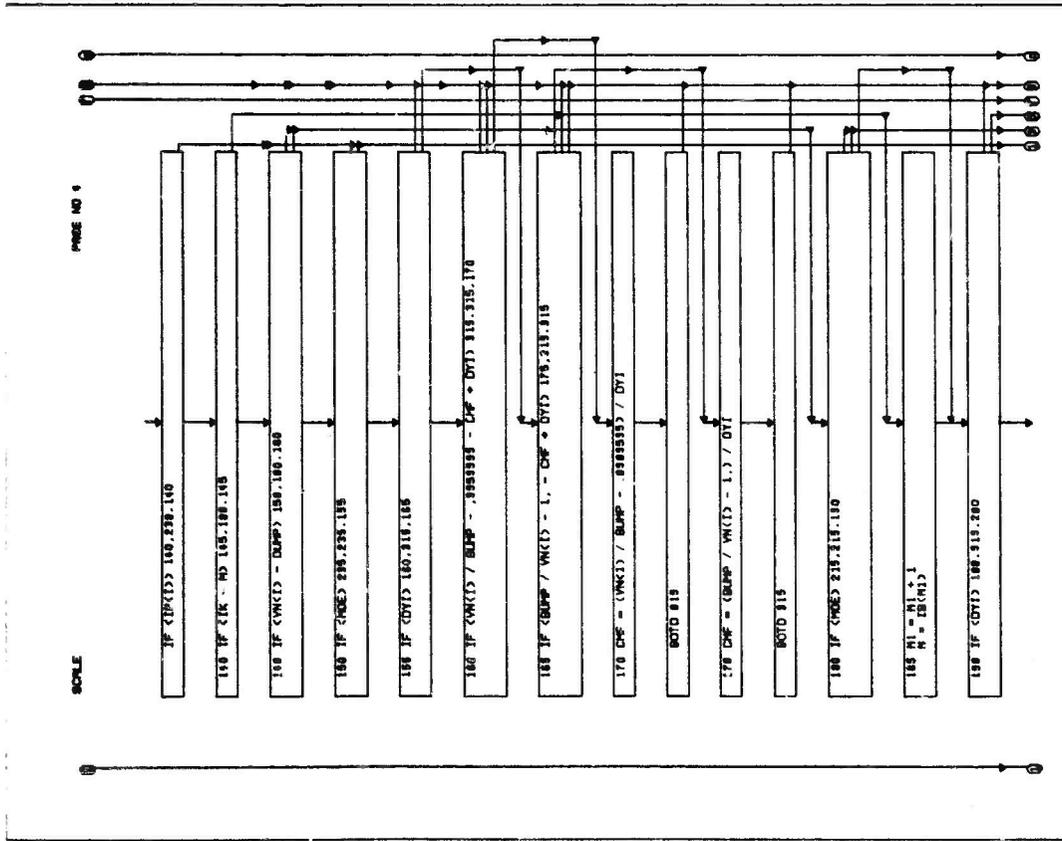
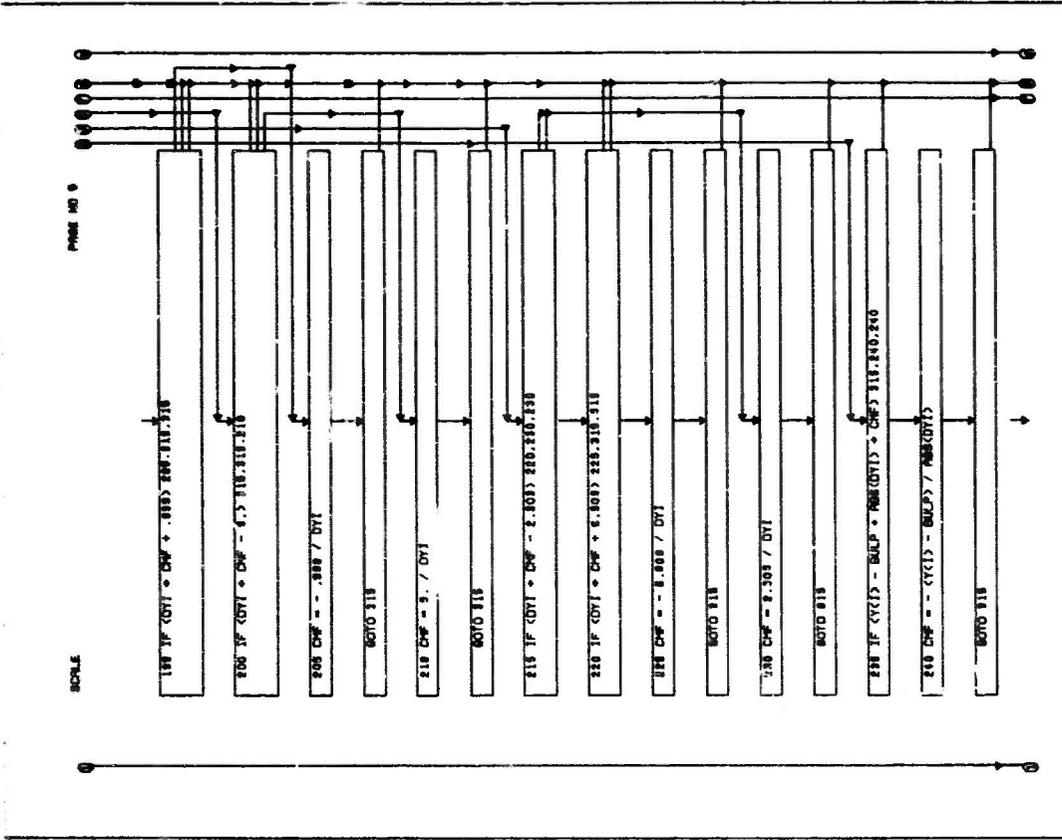
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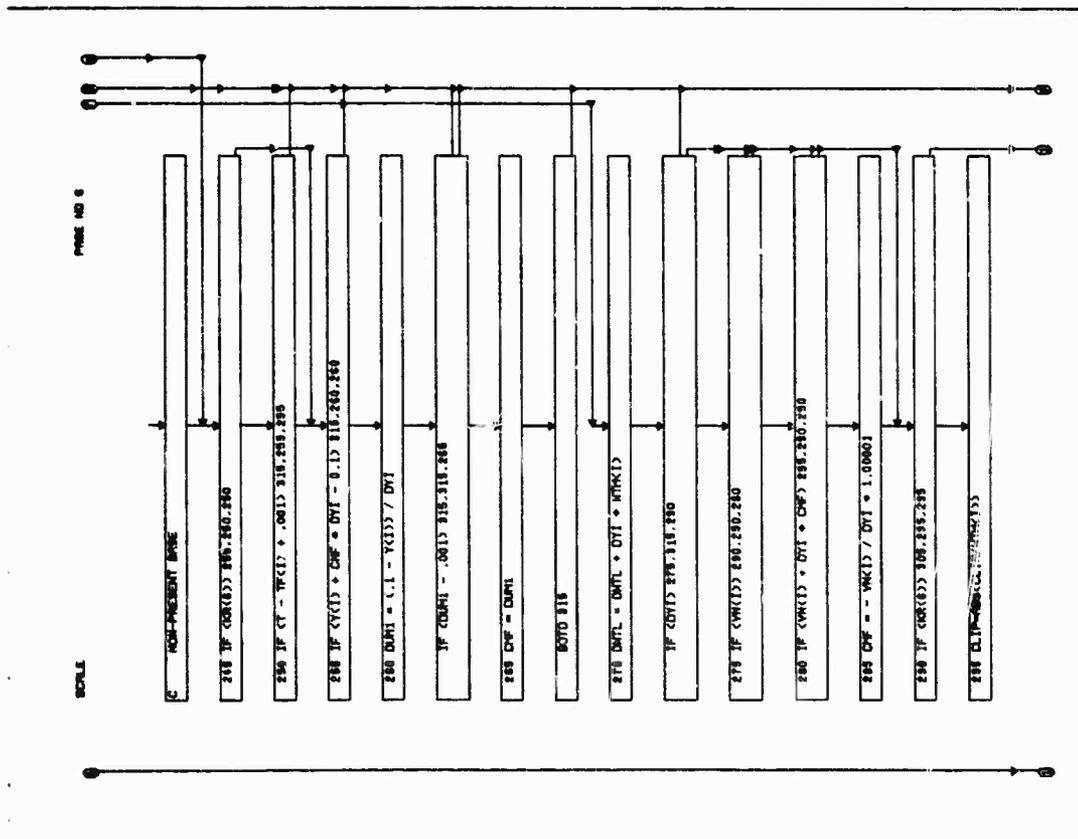
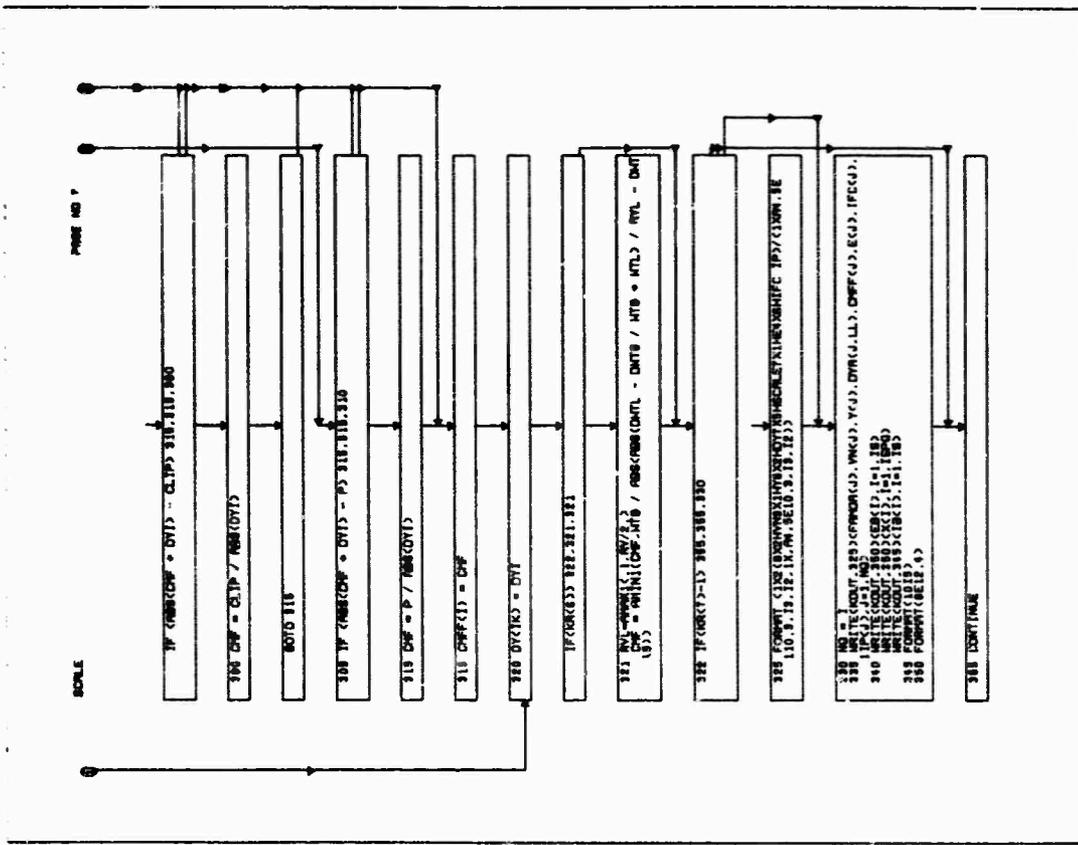












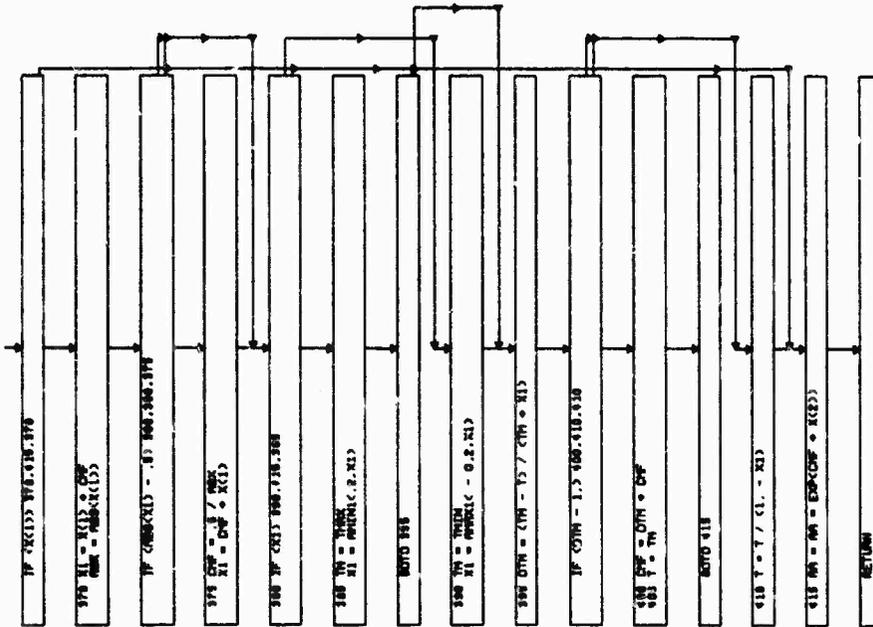
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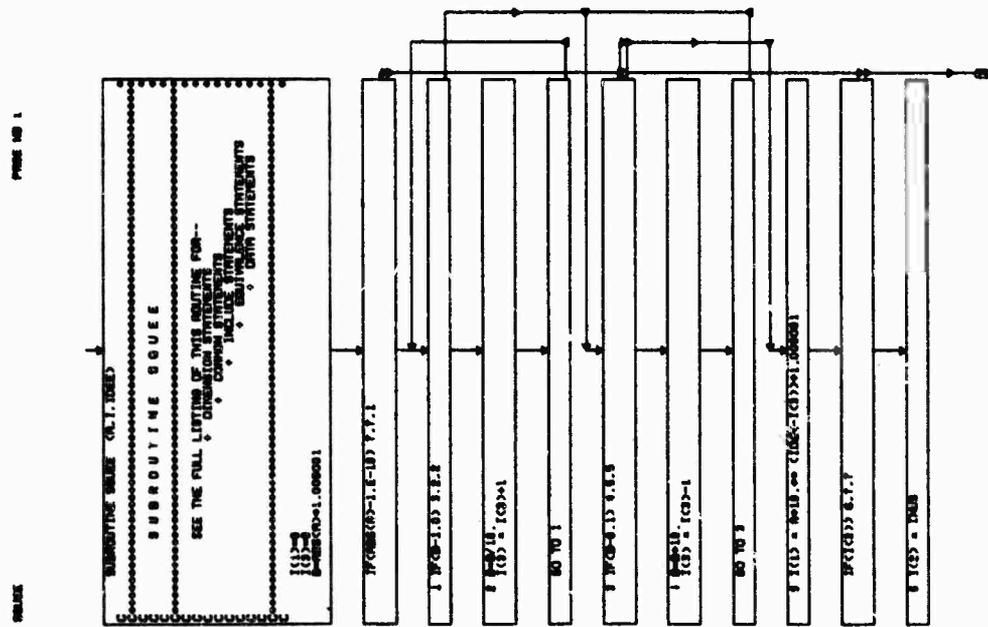
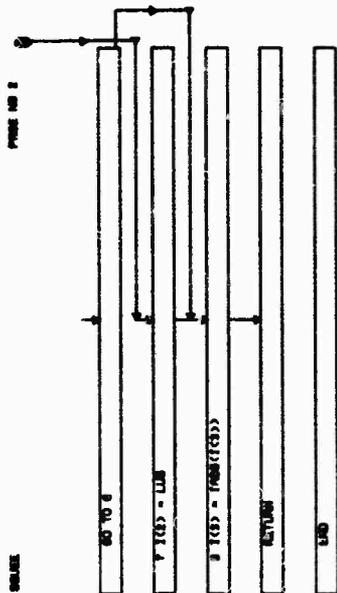
SCALE



PAGE NO 8

SCALE





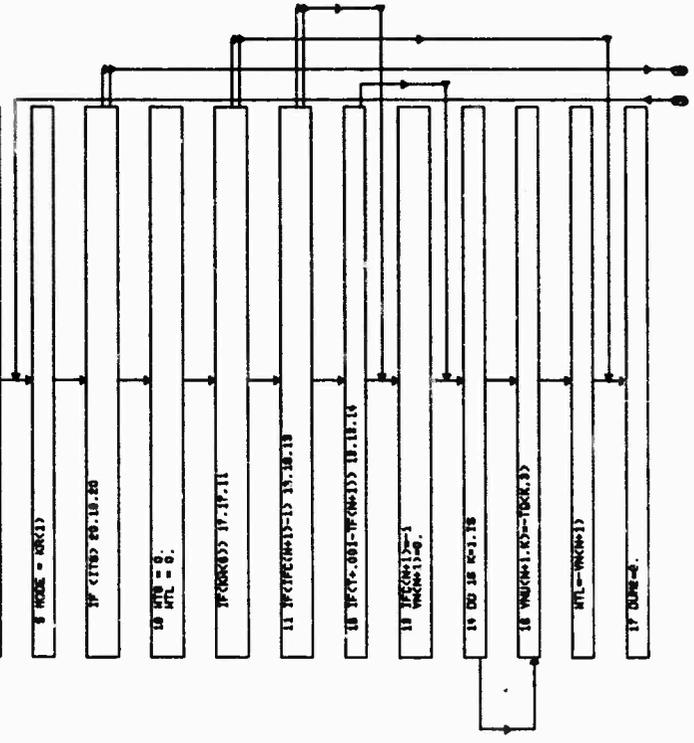
THERM

THERM

```

SUBROUTINE THERM
SUBROUTINE THERM
SEE THE FULL LISTING OF THIS ROUTINE FOR--
COMMON STATEMENTS
* INCLUDE STATEMENTS
* DATA STATEMENTS
DATA STATEMENTS

```



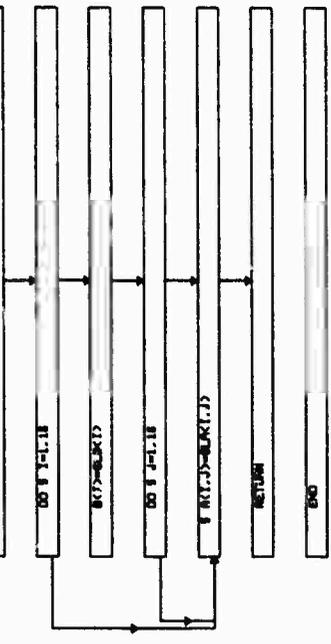
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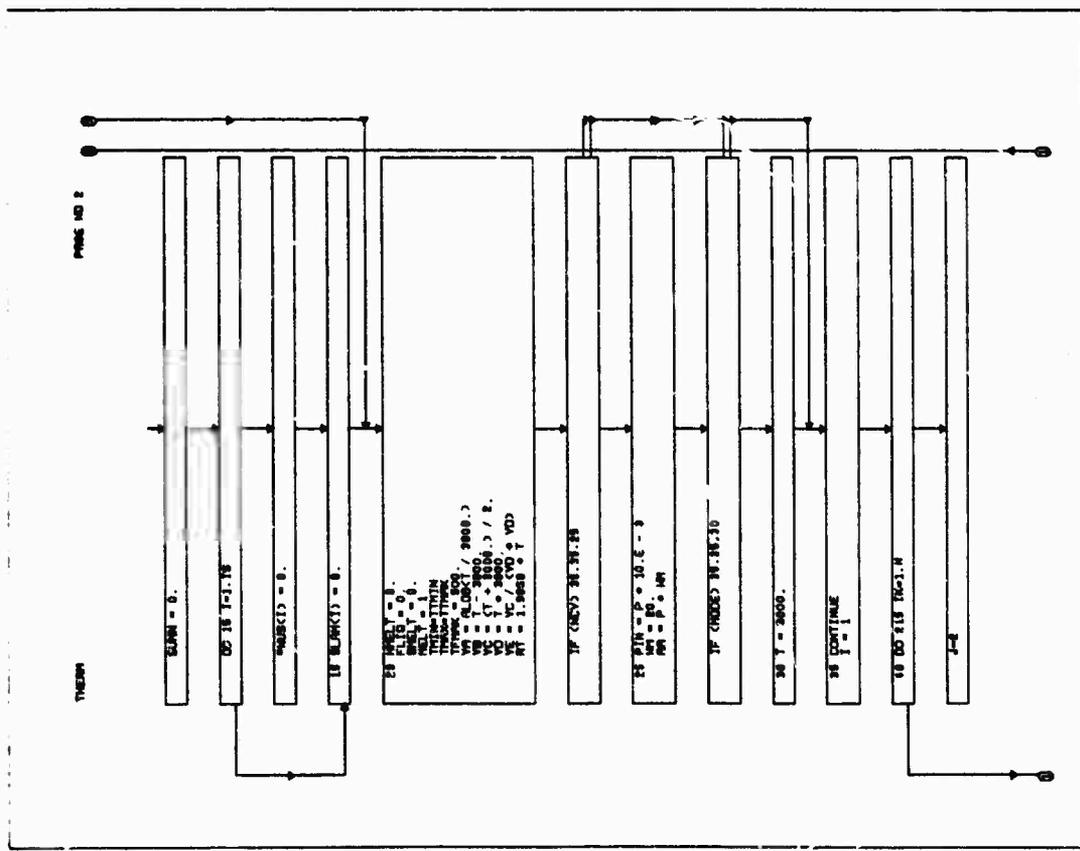
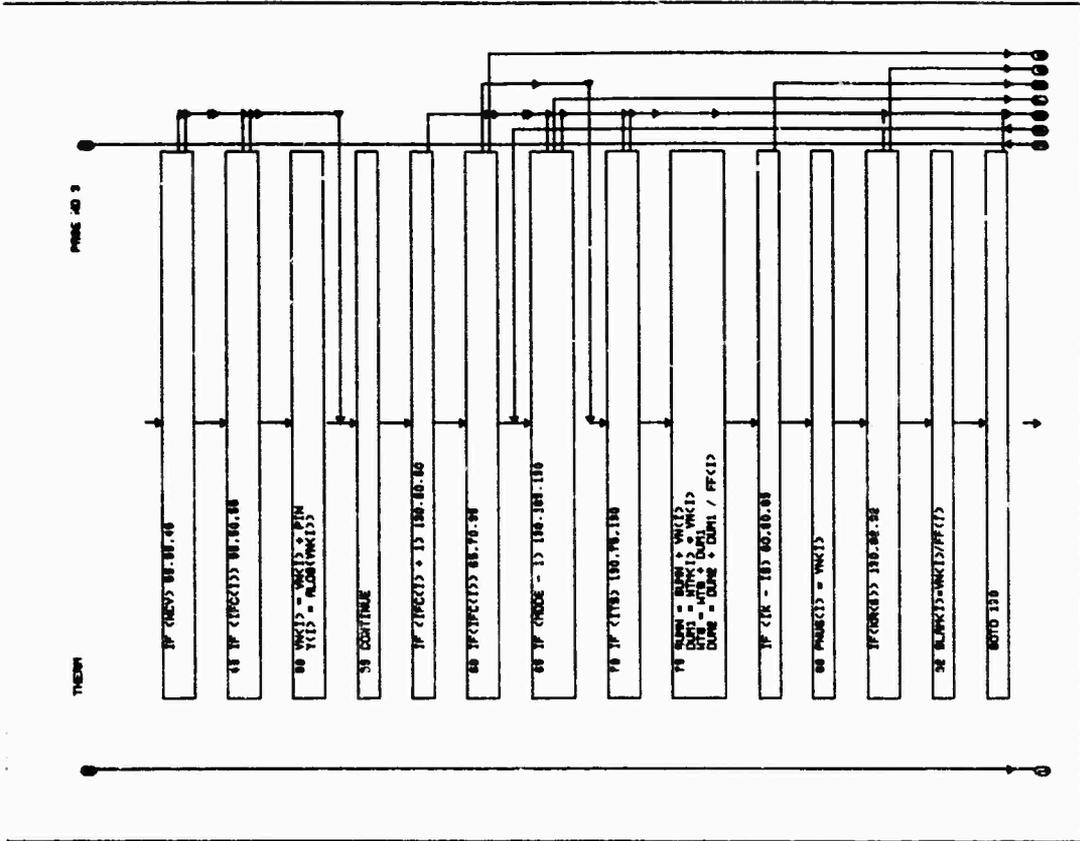
SNAP

```

SUBROUTINE SNAP
SUBROUTINE SNAP
SEE THE FULL LISTING OF THIS ROUTINE FOR--
COMMON STATEMENTS
* INCLUDE STATEMENTS
* DATA STATEMENTS
DATA STATEMENTS

```





PAGE NO 6

THEORY

100 IF CENDR - IS 100.100.100

100 WTRM = MATHC(MTRM.1P.135)

100 WTRM = MATHC(MTRM.1P.135)

100 IF CY = MATHC(MTRM.135) 100.100.100

100 J = 1

100 WTRM = MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135)

100 IF CENDR - IS 100.100.100

100 IF CTRMDS - IS 100.100.100

100 IF CYMTRMDS 100.100.100

100 IF CY + MATHC(MTRM.135) 100.100.100

100 WTRM = MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135) * MATHC(MTRM.135)

100 IF C - IS 100.100.100

100 WTRM = MATHC(MTRM.135)

STOP 100

PAGE NO 5

THEORY

00 00 00 00.1.10

WTRM = MATHC(MTRM.135)

1P(CMTRM) 00.07.00

0P(MTRM) - MATHC(MTRM.135) * MATHC(MTRM.135)

0P(MTRM) - MATHC(MTRM.135) * MATHC(MTRM.135)

1P(CMTRM) 100.100.100

00 00 00 00.1.10

0P(MTRM) - MATHC(MTRM.135) * MATHC(MTRM.135)

00 1P(CMTRM) - IS 100.100.100

100 1P(CMTRM) 100.100.100

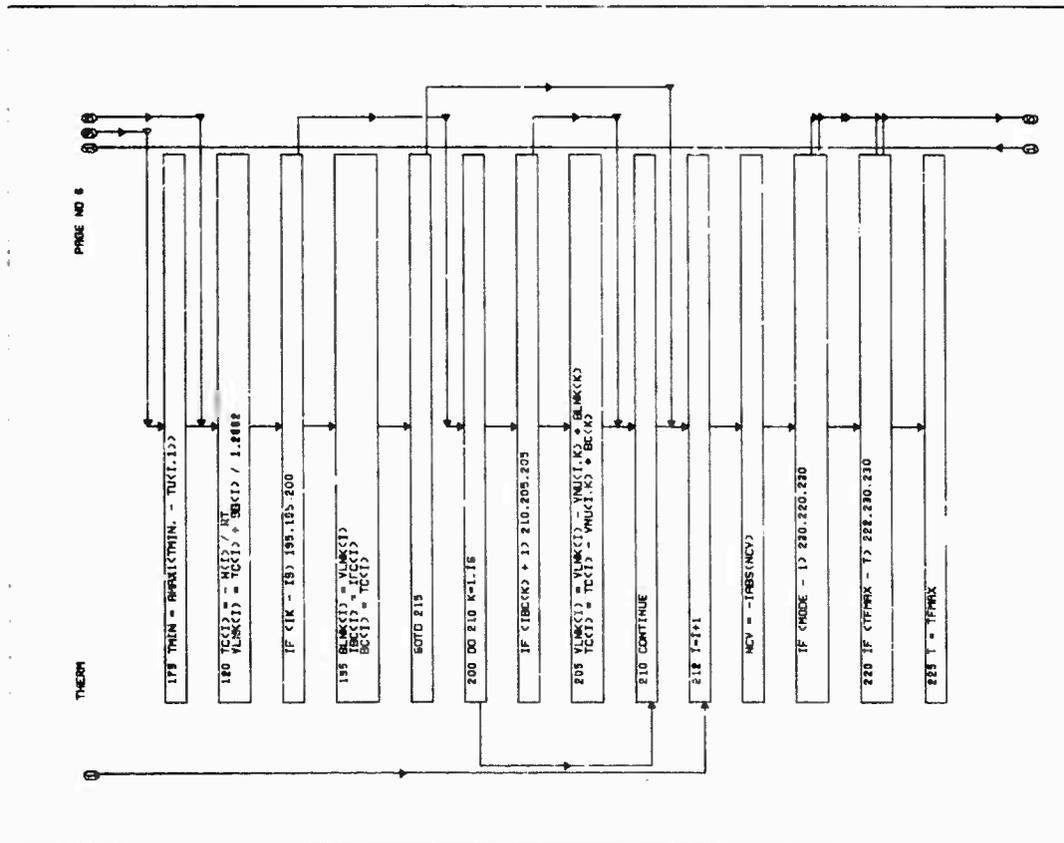
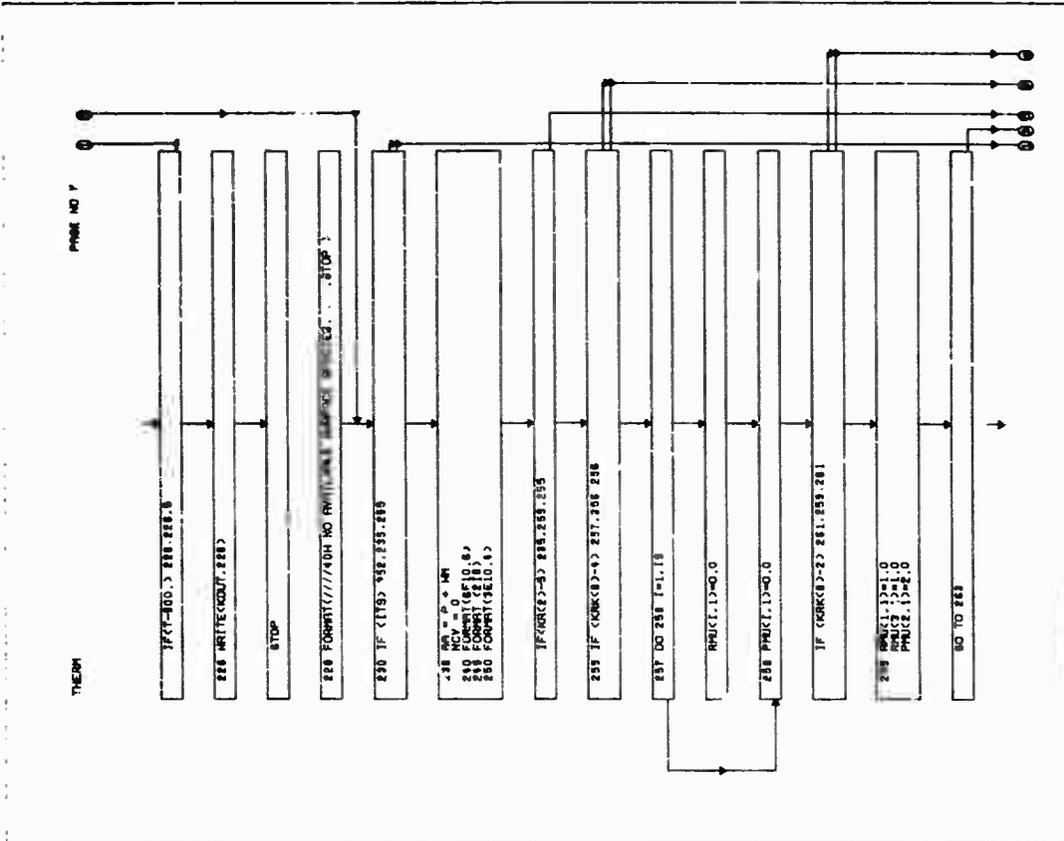
100 1P(CMTRM) 100.100.100

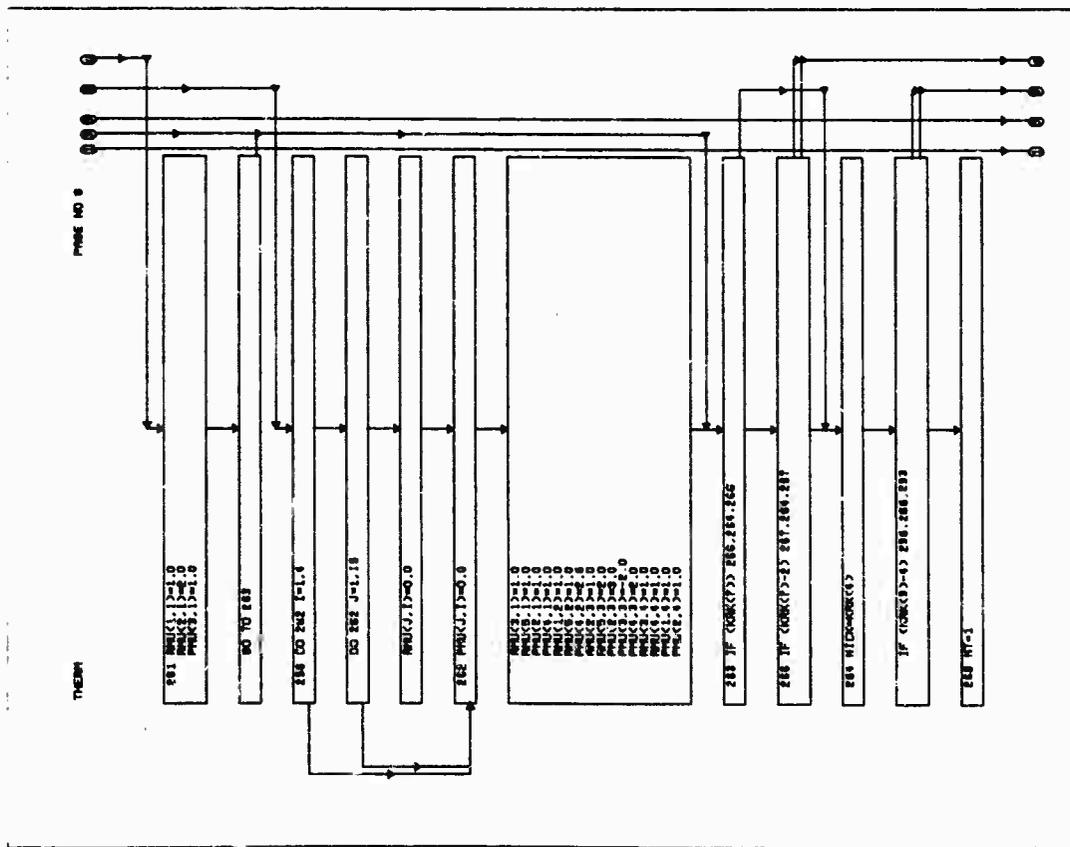
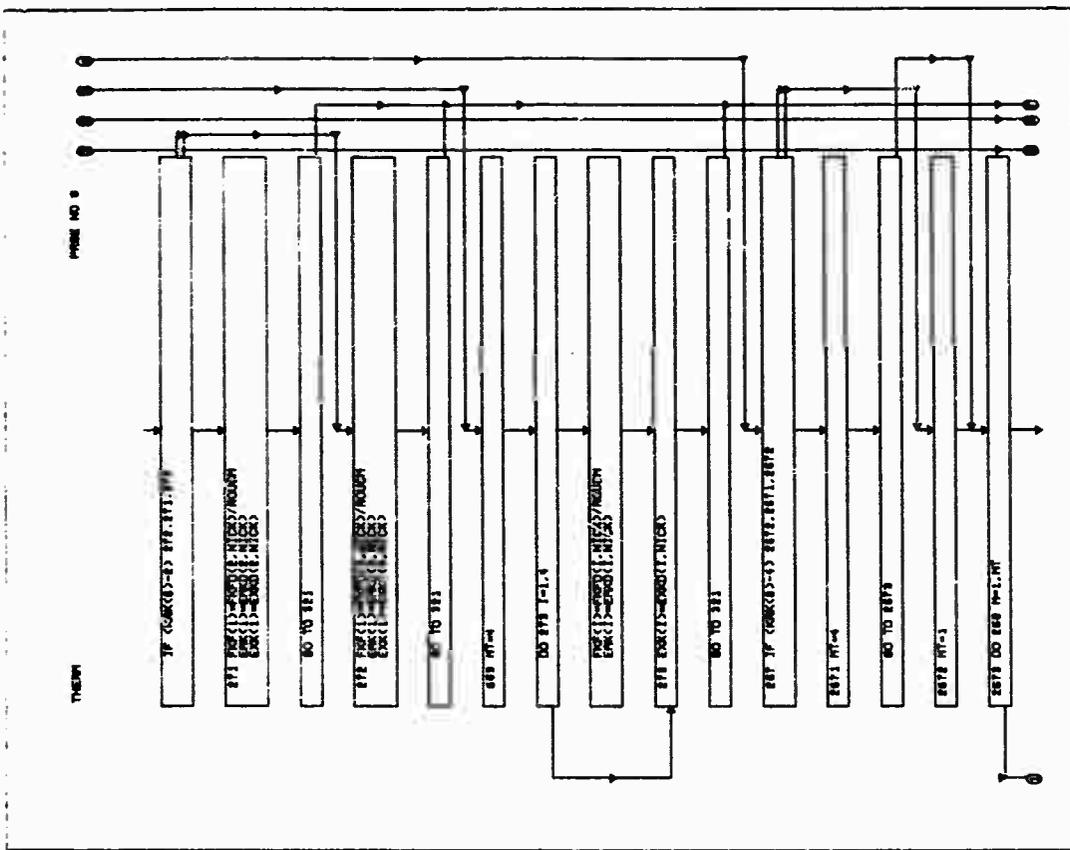
100 1P(CMTRM) * MATHC(MTRM.135) * MATHC(MTRM.135)

100 MATHC(MTRM.135) = 1

STOP 00

100 WTRM = MATHC(MTRM.135) * MATHC(MTRM.135)





PAGE NO 1

ZIPIN

```

SUBROUTINE ZIPIN
SUBROUTINE ZIPIN
SEE THE FULL LISTING OF THIS ROUTINE FOR--
COMMON STATEMENTS
+ DIMENSION STATEMENTS
+ EQUIVALENCE STATEMENTS
+ DATA STATEMENTS
.....
8 FORMAT(10I,6F10.5,2PA,2R)
10 FORMAT(2I5,6F10.5)
15 FORMAT(6E10.5)
CALL TIME
TIME=300
TIME=30000.
PA = 0.0
R = 0.0
RWD = 0
T1=0
.....

```

```

IF (ITS + 1) 30,38,20

```

```

20 WRITE(4) 6666667
K(1)=1.0
K(2)=0.
K(3)=0.
KX = - 1
NCV = 0
NFI = 20
V=300.
GIP = 0.
KRC(10) = 0

```

```

25 ITS = 0
IDC = 1
KCU = 0
KCU = 0
MS = 1.0
KRC=KRC(2)
CALL KININ
WRITE(KOUT,140)TILE,NR
KRC(3) = 0
KRC(4) = 0
KRC(5) = 0
KRC(6) = 0
KRC(7) = 0
KRC(8) = 0
KRC(9) = 0
KRC(10) = 0

```

```

IF (KRC(4)) 150,155,135

```

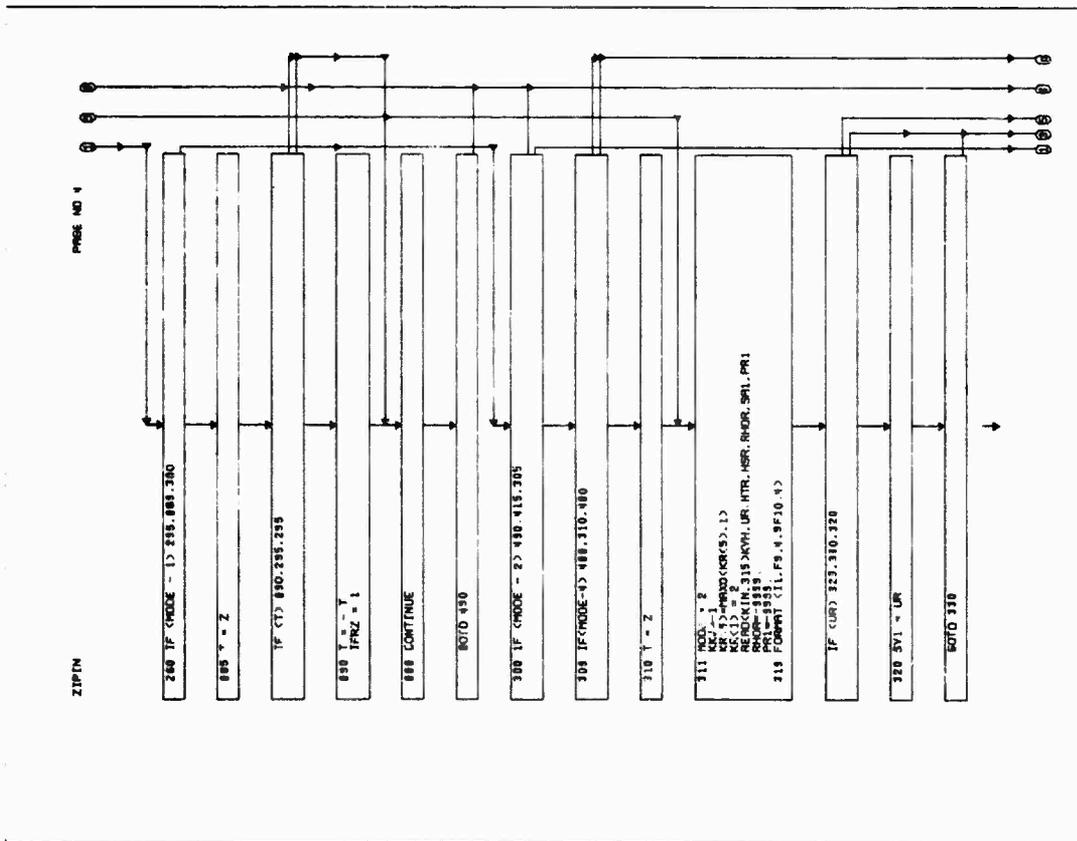
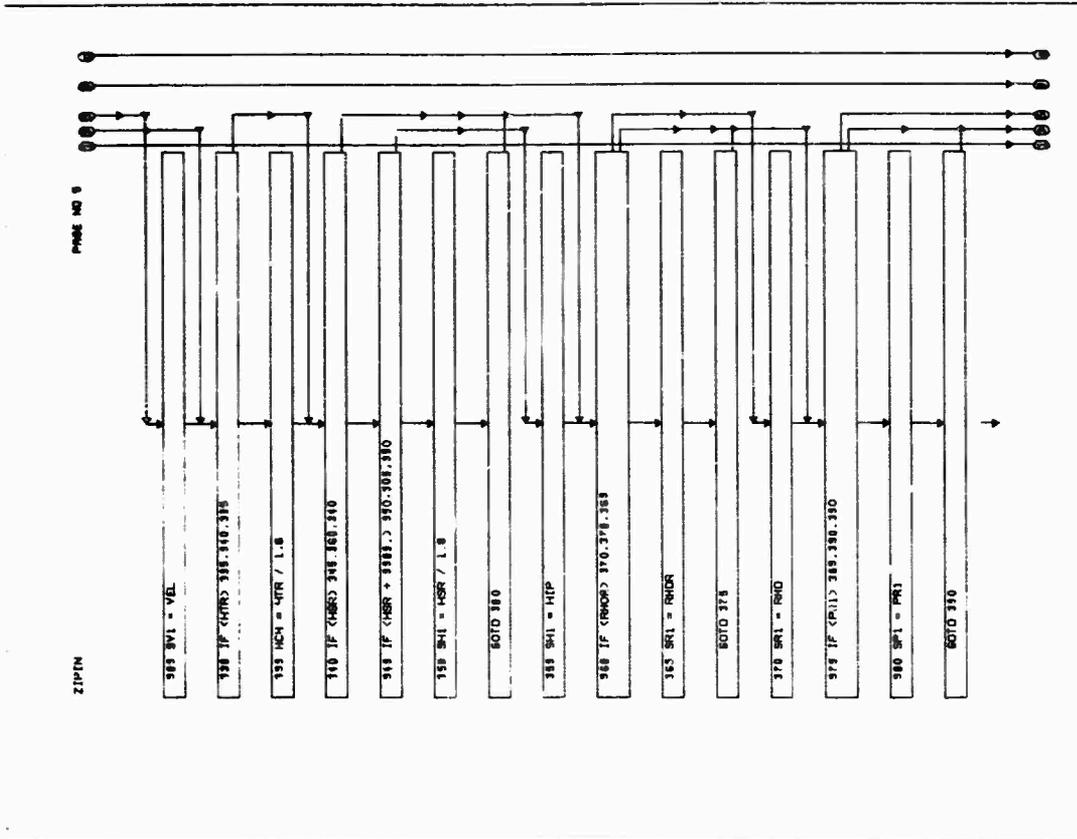
PAGE NO 12

THEM

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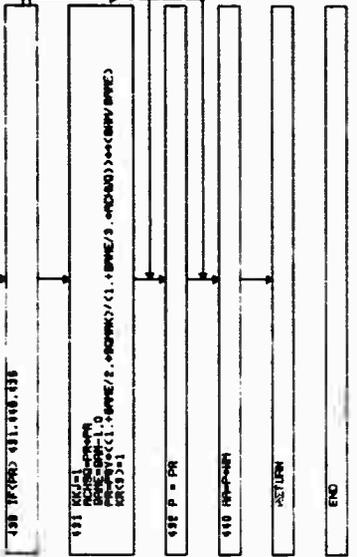
330 B=MC = HTL / (GTS * HS)
HTL = HTL / B=MC
335 RETURN
END

```

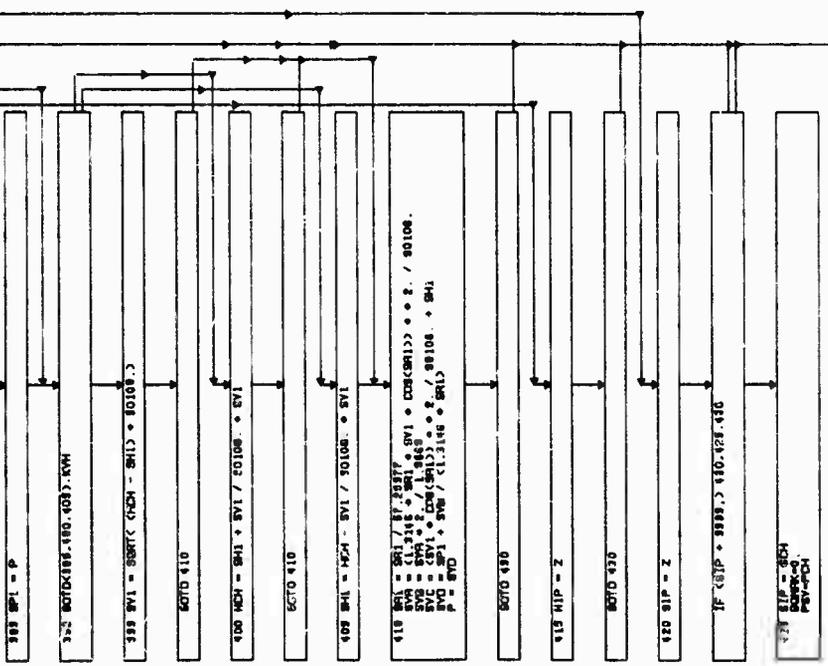
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SECTION 4

LISTINGS OF FORTRAN IV SOURCE DECKS

Listings of Fortran IV source code decks are presented in this section. The main routine is presented first and is then followed in alphabetic order by all program subroutines.

```

C      INCLUDE INC1,L111
C      INCLUDE INC3,L111
C      COMMON/CARMIN/ KRK(10),ROUCH,NCC
C      5 FORMAT(/A1X,I3,F8.2,IP#E10.2/(1P10E12.5))
C      I/O SPECIFICATIONS ALSO IN RERAY
      KIN=5
      KOUT=6
      JAN=18
      NCC=0
      REMINO JAN
      IT5 = 0
      10 CALL ZIPIN
      15 IF (KR(2) * KR(3)) 15,15,20
      20 II = 0
      25 CALL IMELM
      30 IF (KR(3)) 40,40,30
      35 CALL HELCH
      CALL INPUT
      REMINO JAN
      40 CALL ALPST
      45 IF (KR(7) - 1) 80,80,75
      50 IF (KKJ) 55,60,60
      55 KKJ=3
      60 IF (KR(1)-2) 65,70,70
      65 MODE = 2
      JJC = JC
      IIT=IT
      CALL MAT1
      CALL MAT2
      CALL MAT3
      JC = JJC
      IT=IIT
      70 IF (KR(6)) 72,71,71
      71 ISPO=ISP2
      72 MODE = KR(1)
      CALL RERAY((SPO,A,0,0,0,0,0,IG)
      CALL PROPS
      KR(7)=MINO(I,KR(7))
      IOI=I
      IF (KKJ) 75,75,45
      75 CALL OUTPUT
      C*****PRINCIPAL ITERATIVE LOOP

```

```

1      80 IF (IT) 10,90,85
ACE 85 IF (MODE) 95,95,90
ACE 90 CALL THERM 95,95,150
ACE 95 MCUE = KR(1)
ACE 110 = 0
ACE CALL MAT1
ACE CALL MAT2
ACE CALL MAT3
ACE 115 = IT5 * I
ACE 120 IF (KR(9)) 105,105,100
ACE 130 CALL KINET
ACE 140 MOE = 1
ACE 150 IF (KR(7) - 1) 125,120,110
ACE 160 IQQ = - 2
ACE 170 WRITE(KOUT,115)(I,1,I,15)
ACE 180 FORMAT(1M1,40X,40MITS,TEMP
ACE 190 * /((15,74, MASSBAL)))
ACE 200 WRITE(KOUT,5)IT5,T,AA,EL,ENL,CMF,(E(1),1,1,15)
ACE 210 IF (IT5) 50,75,130
ACE 220 IF (IT5-67) 140,135,140
ACE 230 IQQ = - 2
ACE 240 IF (IT5-70) 155,155,145
ACE 250 NCV = 1
ACE 260 KR(7)=4
ACE 270 IG=2
ACE 280 IY5=1
ACE 290 GOTO 50
ACE 300 CALL SWAP(SLA,SLB,A,B)
ACE 310 ICT = 10
ACE 320 IOK=0
ACE 330 IOI = 100
ACE 340 IF (ICT - 1) 170,170,165
ACE 350 A(I + 2,1 + 2) = 1.E + 10
ACE 360 CONTINUE
ACE 370 IOQ = IOI
ACE 380 CALL RERAY(IN,A(IL,IL),0,8(IL),1,0,100)
ACE 390 ICT = ICT - 1
ACE 400 IF (ICT) 190,175,175
ACE 410 IF (190) 190,180,180
ACE 420 CALL AFMAT
ACE 430 GOTO(160,90,145,185),N0
ACE 440 CALL SCALE(MOE)
ACE 450 CALL CRECT(MOE)
ACE 460 IF (CMF - 1.E - 12) 190,190,205
ACE 470 IF (NCV) 195,200,195
ACE 480
ACE 490
ACE 500

```

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ACE 51
ACE 52
ACE 53
ACE 54
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ACE 57
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ACE 60
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ACE 68
ACE 69
ACE 70
ACE 71
ACE 72
ACE 73
ACE 74
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ACE 96
ACE 97
ACE 98
ACE 99
ACE 100

```

```

195 CALL SWAP(A,5,SLA,SLB)
GOTO 145
200 NCV = 1
GOTO 20
205 IF (KR(7) - 1) 80,80,75
END

```

```

ACE 101 SUBROUTINEAFMAT
ACE 102 C
ACE 103 INCLUDE INCL.LIST
ACE 104 C
ACE 105 INCLUDE INCJ.LIST
ACE 106 C
ACE 107 C*****IF TRYING TO PUSH THROUGH TMIN OR TMAX -- REINVERT AND DT TO ZERO
1 DTU=1000.
DTO=DTU
TMIN=300.
TMAX=20000.
2 CONTINUE
ALX(1)
IF (T - TMIN) 5,5,10
5 IF (X(1)) 70,20,10
10 IF (T - TMAX) 20,15,15
15 IF (X(1)) 20,20,70
C*****IF NEW CONDENSED HAS NEG CORRECTION, DELETE AFTER REINVERT
20 IF (NER) 40,40,25
30 IF (N(LIRE)) 30,30,40
35 IF (X(1ER)) 45,30,35,40,40
38 IF (LIRE-N) 37,37,36
39 JC=0
3T CALL SWAP(A,8,SLA,SLB)
DO 38 I=1,ISPO
ALX(1ER)=0.
38 ALX(1) = 0.
ALX(1ER) = 1.E30
ALX(1ER)=0.1
IF (QUM) 135,150,150
C*****IF S.E. ERROR AND CORRECTION ON T OF CONFLICTING SIGN, REINVERT
40 IF (MODE - 1) 120,45,125
45 IF (X(1) * 81) 70,50,50
C*****ON S.E. IF DELTA LN T .GT. .9 REINVERT NU OT IF EL AND ENL ARE SHAA
50 IF (ABS(X(1)) - 0.9) 125,125,55
55 IF (ENL - 0.02) 60,65,65
60 IF (EL - 100.) 125,65,65
65 MODE = 0
C*****REINVERT
70 CALL SWAP(A,8,SLA,SLB)
C*****IF CONVERGED EXCEPT FOR T ON H OR 5 OPTIONS -- NON CONVERGENT
IF (MODE - 1) 115,80,75
75 IF (EL * 100 * ENL) 1.E - 4) 160,160,115
C*****ON 5.E. OPTION RESULTING IN CONFLICTING ERROR/CORRECTION OR T PUSH
C*****IF OTHER BALANCES RELATIVELY GOOD, SET T TO TMIN/TMAX AS PER ERRORA
C*****AND GO TO THERM (IF T ALREADY THERE - NONCONVERGE) ELSE OT TO ZERO
80 IF (ABS(B1) - 100. * (EL * ENL)) 115,85,85
85 TMIN=AMAX1(TMIN,OTD,300.)
TMAX=AMINI(TMAX,DTU,20000.)
AFMA 1
AFMA 2
AFMA 3
AFMA 4
AFMA 5
AFMA 6
AFMA 7
AFMA 8
AFMA 9
AFMA 10
AFMA 11
AFMA 12
AFMA 13
AFMA 14
AFMA 15
AFMA 16
AFMA 17
AFMA 18
AFMA 19
AFMA 20
AFMA 21
AFMA 22
AFMA 23
AFMA 24
AFMA 25
AFMA 26
AFMA 27
AFMA 28
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AFMA 30
AFMA 31
AFMA 32
AFMA 33
AFMA 34
AFMA 35
AFMA 36
AFMA 37
AFMA 38
AFMA 39
AFMA 40
AFMA 41
AFMA 42
AFMA 43
AFMA 44
AFMA 45
AFMA 46
AFMA 47
AFMA 48
AFMA 49
AFMA 50

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```

IF (X(1) < 0) X(1) = 0
87 IF (X(1) > 1) X(1) = 1
90 IF (X(1) < 0) X(1) = 0
95 IF (X(1) > 1) X(1) = 1
DTU=OTD/2.
GOTO 155
100 IF (X(1)-TMAX) 105,156,156
105 =MINI(TMAX,X(1)-OTU)
TMIN=T
OTU=OTD/2.
IF (ABS(T - T(JC))) < .001 110,155,155
110 IF (X(1) < 0) X(1) = 0
V(JC) = 1 - E - 3 / W(T(JC)) * WTG
Y(JC) = 0.
GOTO 155
111 IF (X(1)-TMIN) 156,156,112
112 IF (X(1)-TMAX) 115,156,156
115 X(1) = 0.
MODE = 0.
TMIN=TMIN
TMAX=TMAX
IN = IN - 1
IL = 2
GOTO 150
120 X(1) = 0.
125 IF (X(2) < 1.) 130,165,165
130 CALL SWAP(A,B,SLA,SLB)
135 X(2)=WTG
IF (KR(6)) 140,145,145
140 X(2) = X(2) * WTL
145 X(2) = 0.
DUM1=-1.
A(2,2) = 1.E25
150 NG = 1
GOTO 170
155 NG = 2
GOTO 170
156 JC=0
WRITE (KOUT,157)
157 FORM='//564 SOLUTION TERMINATED WHEN TEMPERATURE LIMIT ENCOUNTERED'
160 NG = 3
GOTO 170
165 NG = 4
170 RETURN
END

```

```

AFMA 51
AFMA 52
AFMA 53
AFMA 54
AFMA 55
AFMA 56
AFMA 57
AFMA 58
AFMA 59
AFMA 60
AFMA 61
AFMA 62
AFMA 63
AFMA 64
AFMA 65
AFMA 66
AFMA 67
AFMA 68
AFMA 69
AFMA 70
AFMA 71
AFMA 72
AFMA 73
AFMA 74
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AFMA 76
AFMA 77
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AFMA 80
AFMA 81
AFMA 82
AFMA 83
AFMA 84
AFMA 85
AFMA 86
AFMA 87
AFMA 88
AFMA 89
AFMA 90
AFMA 91
AFMA 92
AFMA 93
AFMA 94
AFMA 95
AFMA 96
AFMA 97
AFMA 98

```

```

SUBROUTINE ALPST
COMMON/ACEI/GAMEX,REFM,PCN,ACHSU,SOMAF,SKP
C
C INCLUDE INC1.LIST
C
C INCLUDE INC2.LIST
C
5 FORMAT(2A4,E12.5,2A4,E12.5,2A4,E12.5,2A4,E12.5)
10 FORMAT(29H UPDATE OF DIFFUSION FACTORS/10A,7HSPECIES16HDIFFUS10ALPS
IN FACTOR)
15 FORMAT(11X,2A4,6XF10.3,2A2)
20 FORMAT(11X,2A4,6XF10.5,2A2)
25 FORMAT(13,3F.7,6.5,F6.4)
30 FORMAT(BE10.4)
DATA 15,16,17,2M,2N,2NEW/
TFMAX = 20000.
IF (KR(3) - 7) 35,40,40
35 IF (X(1) < 0) X(1) = 0
40 INF = NFF
HEAO(KIN,25) NFF
NFF = NFF + 1
INF = INF + 1
HEAD(KIN,5) (NF1A(I),NF1B(I),FFIN(I),I=1,NF,NFF)
KR(3) = 9 - KR(3)
IF (NF1A(INF) ** NF1B(INF)) 55,45,55
45 TFMAX = FFIN(INF)
GOTO 65
55 INF = 1
IF (NF1A(1) - NF1B(1)) 65,60,65
60 TFMAX = FFIN(1)
65 JL=0
DO 64 I=1,NFF
IF (FFAO-NF1A(I)) 62,61,62
61 REFM=FFIN(I)
JL=JL+1
GO TO 64
62 IF (FFAO-NF1A(I)) 64,63,64
63 FFA=FFIN(I)
JL=JL+1
64 CONTINUE
DO 69 J=1,N
FF(J)=1.E-10
IF (M(J)-.01) 69,69,56
56 IF (FC(J)) 67,68,67
67 IF (LABS(FC(J))-3) 69,68,69
68 FF(J)=(M(J)/REFM) ** (FA*GAMEX)
69 CONTINUE
WRITE(KOUT,72) REFM,FFA

```

```

ALPS 1
ALPS 2
ALPS 3
ALPS 4
ALPS 5
ALPS 6
ALPS 7
ALPS 8
ALPS 9
ALPS 10
ALPS 11
ALPS 12
ALPS 13
ALPS 14
ALPS 15
ALPS 16
ALPS 17
ALPS 18
ALPS 19
ALPS 20
ALPS 21
ALPS 22
ALPS 23
ALPS 24
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ALPS 28
ALPS 29
ALPS 30
ALPS 31
ALPS 32
ALPS 33
ALPS 34
ALPS 35
ALPS 36
ALPS 37
ALPS 38
ALPS 39
ALPS 40
ALPS 41
ALPS 42
ALPS 43
ALPS 44
ALPS 45
ALPS 46
ALPS 47
ALPS 48
ALPS 49
ALPS 50

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```

IF (NFF-JL) 125,125,71
71 J=1
WRITE (KOUT,10)
72 FORMAT ('SMALL GASEOUS DIFFUSION FACTORS RECALCULATED AS (MOL,WTALPS
1/7,3,3H)=F0.3//)
MP=N+1
DO 120 IK=1,NP
  I = 1
  11 = 15
  12 = 15
  13 = 15
  14 = 15
  IF (IK-N) 74,74,85
  74 IF (IFC(J)) 70,85,70
  70 IF (IABS(IFC(J)) - 3) 75,85,75
  75 IF (IFMAX - 20000.) 80,85,85
  80 IF (J) = TMAX
  I = I + 1
  GOTU 105
85 IF (NFIA(I) - FAMOA(J)) 115,90,115
  90 IF (NFIB(I) - FAMOB(J)) 115,95,115
  95 IF (FFIN(I) - 100.) 110,100,100
  100 IF (J) = AMINI(FFIN(I)) + IFMAX
  105 WRITE (KOUT,15) FAMOA(J), FAMOB(J), I, J, I1, I2
  11 = 16
  12 = 17
  GOTU 115
110 FF(J) = FFIN(I)
  WRITE (KOUT,20) NFIA(I), NFIB(I), FFIN(I), I3, I4
  FF(J) = FF(J) ** GAMEX
  13 = 16
  14 = 17
  115 I = 1 + 1
  IF (I - NFF) 85,85,120
120 JS=J+1
125 NFF=0
  WS=1.0
130 IF (KRI(6)) 150,135,135
135 W(1) = 0.
  IF (KRI(4)) 145,145,140
145 W(1) = 1.
  GOTU 135
150 WS = W(1) * W(2) * W(3)
155 NOATO = NOAT
  DUM1 = 0.
  00 200 K=1,15
  ALPH = (W(1)) * TK(K,1) * W(2) * TK(K,2) * W(3) * TK(K,3) / WS
  IF (ALPH) 160,160,200
160 IF (KAT(K)-99) 165,161,165
161 IF (KRI(6)) 200,195,195
165 IF (KRI(6)) 195,170,175
170 IF (TK(K,1)) 171,171,200
171 IF (KRI(8)) 195,195,172
172 IF (TK(K,3)) 195,195,200
175 IF (NOATO) 190,190,180
180 DO 185 KK=1,NOATO
  IF (IOAT(KK) - K) 185,195,185
185 CONTINUE
190 GOTU 200
195 NOAT = NOAT + 1
  DUM1 = DUM1 - ALPH
  ICAT(NOAT) = K
200 CONTINUE
  WS = WS * (1. * DUM1)
  DO 205 K=1,15
  GAMF(K)=0.
  TEST = 1.0
  IF (K(6)) 200,215,210
210 STOP 222
  C*****SURFACE MASS BALANCE PACKAGE GOES HERE
215 IF (K(6)) 215,250,220,250
220 IF (NCV*RR(3)) 225,225,291
225 PMU2 = 0.
  KR(4) = 1.
  DO 231 K=1,15
  IF (WTH(K)-1.0) 231,229,229
229 VA = VNIK / FF(K)
  ZKE(K) = VA
230 PMU2 = PMU2 * VA * WTH(K)
231 CONTINUE
  J = 15P
  DO 240 IK=1,5P,N
  IF (WTH(J)-1.0) 240,234,234
234 VA = VN(J) / FF(J)
  PMU2 = PMU2 * VA * WTH(J)
  DO 235 K=1,15
235 ZKE(K) = ZKE(K) * VA * VNU(J,K)
240 J=J+1
  DO 245 K=1,15
245 ZKE(K) = ZKE(K) / PMU2
250 DO 270 I=1,15
  K=IK+1
  IF (KAT(I)-99) 255,250,255
255 IF (W(1)) 265,265,170
260 ALP(K) = 0.
  GOTU 270
ALPS 101
ALPS 102
ALPS 103
ALPS 104
ALPS 105
ALPS 106
ALPS 107
ALPS 108
ALPS 109
ALPS 110
ALPS 111
ALPS 112
ALPS 113
ALPS 114
ALPS 115
ALPS 116
ALPS 117
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ALPS 119
ALPS 120
ALPS 121
ALPS 122
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ALPS 125
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ALPS 128
ALPS 129
ALPS 130
ALPS 131
ALPS 132
ALPS 133
ALPS 134
ALPS 135
ALPS 136
ALPS 137
ALPS 138
ALPS 139
ALPS 140
ALPS 141
ALPS 142
ALPS 143
ALPS 144
ALPS 145
ALPS 146
ALPS 147
ALPS 148
ALPS 149
ALPS 150

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265 ALP(K) = ALP(K) + ZRE(K)
270 CONTINUE
275 TEST1 = W(2) * I(3)
280 DO 285 K=1,15
285 TEST = TEST + W(K) * W(K) + W(K)
290 IF (ABS(TEST) - .001) 300,300,290
STOP
291 WRITE(KOUT,295) W
291 CONTINUE
295 FORMAT(//// 5X39MSICK MASS BALANCE INITIATION, CHECK . . . /
1 10X73H1, REARRANGEMENT OF ELEMENTS BETWEEN EDGE AND WALL SOLUTIONALS 162
25 (KR(2),G1,0) /10X28M2, COMPONENT MASS FRACTION ( 3E12,%.11M) NUTALPS 163
3 EQUAL/1X71M10 ZERO FOR UNDEFINED COMPONENT (ALL ZERO GRAM-ATOMIC) 164
4-WEIGHTS PER GRAM) )
296 FORMAT(////5X79M10 VALID EDGE COMPOSITION AVAILABLE BECAUSE LAST SALPS 166
SOLUTION WAS NON CONVERGENT OR/11X73M10 FIRST GUESSES HAVE BEEN INALPS 167
2 INTRODUCED IN INPUT SUBROUTINE (KR(3)=1 TO 8) )
300 IF (KR(3)) 305,305,370
305 IF (NOAT) 370,370,310
C WEINITIALIZE SPECIES
310 PIN = P / 10
PLOC = ALOC(PIN)
J = 1
315 DO 365 IA=1,N
IF (IFC(J) * I) 320,365,330
320 IFC(J) = IFC(J) * 3
IF (J - 15) 340,340,325
325 YC = Y
330 IF (IFC(J) - 1) 365,365,335
335 IFC(J) = IFC(J) - 3
340 YC = PLOC
345 IF (IFC(J)) 355,360,350
350 IFC(J) = - 1
355 VNL(J) = 0.
Y(LJ) = YC
GOTO 365
360 VNL(J) = PLOC
Y(LJ) = PLOC
365 J=J+1
370 IF (NOAT) 425,425,375
375 J = 1
380 DO 405 IK=1,N
IF (NOAT - 1) 400,385,385
385 DO 395 L=1,NOAT
K = 10AT(L)
LAMT = LAM1(J) / 2 * (K - 1)
LAMT = LAMT - (LAMT / 2) * 2
IF (LAMT) 390,395,390
ALPS 151
ALPS 152
ALPS 153
ALPS 154
ALPS 155
ALPS 156
ALPS 157
ALPS 158
ALPS 159
ALPS 160
ALPS 161
ALPS 162
ALPS 163
ALPS 164
ALPS 165
ALPS 166
ALPS 167
ALPS 168
ALPS 169
ALPS 170
ALPS 171
ALPS 172
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ALPS 174
ALPS 175
ALPS 176
ALPS 177
ALPS 178
ALPS 179
ALPS 180
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ALPS 182
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ALPS 187
ALPS 188
ALPS 189
ALPS 190
ALPS 191
ALPS 192
ALPS 193
ALPS 194
ALPS 195
ALPS 196
ALPS 197
ALPS 198
ALPS 199
ALPS 200
390 VNL(J) = 0.
IFC(J) = IFC(J) - 3
GOTO 405
395 CONTINUE
400 CONTINUE
405 J=J+1
410 IF (NOAT - 1) 420,410,410
K = 10AT(L)
J = - IR(K)
415 IFC(J) = IFC(J) + 6
420 CONTINUE
425 RETURN
END
ALPS 201
ALPS 202
ALPS 203
ALPS 204
ALPS 205
ALPS 206
ALPS 207
ALPS 208
ALPS 209
ALPS 210
ALPS 211
ALPS 212
ALPS 213
ALPS 214
ALPS 215

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```

SUBROUTINEBELCH
C   INCLUDE INCL1LIST
C   INCLUDE INCL2LIST
C   15 IF (J - IS) 20,20,35
20  JM = J - 1
    WRITE (KOUT,25) JM,IS,(FAMOA(I),FAMOB(I),I=1,JM)
    WRITE (KOUT,35) (FAMOA(I),FAMOB(I),I=1,SP,N)
    STOP
25  FORMAT('//////ISH ONLY FOLLOWING 13,23H BASE SPECIES FOUND FOR 13,
30  19H ELEMENTS/(2X20A4)')
35  DO 45 L=2,15
    JM = ISP - L
    IF (JM - 1) 50,40,40
    UGH = TAU(INJ,K)
    DO 45 I=1,15
    45  UM(I,K) = UM(I,K) - UGH * UM(I,JH * I)
50  CONTINUE
    DO 70 I=1,15
    55  IM1 = IM(I)
    60  DO 65 K=1,15
    65  UM(K,IM1) = UM(K,I)
    70  CONTINUE
    IM(IM1) = IM1
    GOTO 55
C-----ELEMENT-- BASE GAS CORRESPONDENCE
C   INITIALIZE ROW AND COLUMN SUMS
    IG = IS
    DO 75 I=1,15
    75  IC(I) = - 1
    EVALUATE INITIAL SUMS
    LAMD = 1
    DO 90 J=1,15
    90 85 J=I,15
    LAMT = LAM(J) / LAMD
    LIM(I,J) = LAMT - (LAMD / 2) * 2
    80  IC(J) = IC(J) + 1
    85  IM(J) = IM(J) + 1
    85  CONTINUE
    90  LAMD = LAMD * LAMD
    CHECK FOR ZEROS
    95 17 = 0
    100 DO 185 I=1,15
    105 DO 110 J=1,15
    110 CONTINUE
    115 IC(I) = - J
    120 IC(K) = IC(K) - 1
    125 IF (LIM(K,I)) 130,135,130
    130 LIM(K,I) = 0
    135 CONTINUE
    140 IF (IR(I) - 12) 185,145,185
    145 DO 155 J=1,15
    150 IC(J) = - 1
    155 CONTINUE
    160 DO 160 K=1,15
    165 IR(K) = IR(K) - 1
    170 IF (LIM(I,K)) 175,180,175
    175 LIM(I,K) = 0
    180 GOTO 190
    185 CONTINUE
    190 IG = IG - 1
    J = IS + 1
    IF (IG) 195,195,95
    195 DO 200 I=1,15
    200 FAMB(I) = FAMB(I)
    WRITE (KOUT,205) (ATA(I),ATC(I),I=1,IS)
    205 FORMAT('5X,8HELEMENTS,7X,15A4/(20X,15A4)')

```

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BELC 51
BELC 52
BELC 53
BELC 54
BELC 55
BELC 56
BELC 57
BELC 58
BELC 59
BELC 60
BELC 61
BELC 62
BELC 63
BELC 64
BELC 65
BELC 66
BELC 67
BELC 68
BELC 69
BELC 70
BELC 71
BELC 72
BELC 73
BELC 74
BELC 75
BELC 76
BELC 77
BELC 78
BELC 79
BELC 80
BELC 81
BELC 82
BELC 83
BELC 84
BELC 85
BELC 86
BELC 87
BELC 88
BELC 89
BELC 90
BELC 91
BELC 92
BELC 93
BELC 94
BELC 95
BELC 96
BELC 97
BELC 98
BELC 99
BELC 100

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```

210 FORMAT(/5X,12HBASE SPECIES,3X,5(2A4,4X1)/(20X,5(2A4,4X1))
03 215 L=1,3
00 215 J=1,15
70(I,J,L) = 0.
DO 215 K=1,15
215 10(I,J,L) = T(I,J,L) * UM(I,K) * TR(K,L)
220 RETURN
END

WELC 101
WELC 102
WELC 103
WELC 104
WELC 105
WELC 106
WELC 107
WELC 108
WELC 109

SUBROUTINE CRECT(MOE)
DIMENSION DY(1)
INCLUDE INCI.LIST
INCLUDE INJ.LIST
EQUIVALENCE(A(1),DY(1))
M1 = 1
M = 10(1)
WTL = 0.
WTG = 0.
DUM2 = 0.
L = 1
LIM=KR(H)*N
DO 115 IK=1,LIM
OVI = CMF * OY(IK)
IF (OVI) 10,5,10
10 IF (IFC(1)) 115,55,105
15 IF (IFC(1)) 75,15,100
20 IF (IN - 1K) 25,30,20
25 IF (MOE) 50,50,35
30 M1 = M1 + 1
35 VN(1) = VN(1) * (1. + OVI)
IF(VN(1)) 50,50,45
45 GOTO 55
50 Y(1) = Y(1) + OVI
55 VA = WTM(1) * VN(1)
WTG = WTG + VA
DUM2 = DUM2 + VA / FF(1)
60 PNUS(1) = VN(1)
IF(KR(6)) 115,63,72
63 SLAM(1)=VN(1)/FF(1)
GOTO 115
65 DO 70 K=1,15
VA = VN(1)*K * VN(1)
IF(KR(6)) 70,68,70
68 SLAM(K)=SLAM(K)+VA/FF(1)
70 PNUS(K)=PNUS(K)+VA
IF(KR(6)) 115,115,72
72 DO 73 K=1,15
73 SLAM(K)=SLAM(K)+VN(1)*VLAM(I,K)
75 Y(1) = Y(1) + OVI
NON-PRESENT BASE CORRECTIONS AND TESTS
IF (Y(1)) 115,80,80

```

1 C REC
2 C REC
3 C REC
4 C REC
5 C REC
6 C REC
7 C REC
8 C REC
9 C REC
10 C REC
11 C REC
12 C REC
13 C REC
14 C REC
15 C REC
16 C REC
17 C REC
18 C REC
19 C REC
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21 C REC
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23 C REC
24 C REC
25 C REC
26 C REC
27 C REC
28 C REC
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30 C REC
31 C REC
32 C REC
33 C REC
34 C REC
35 C REC
36 C REC
37 C REC
38 C REC
39 C REC
40 C REC
41 C REC
42 C REC
43 C REC
44 C REC
45 C REC
46 C REC
47 C REC
48 C REC
49 C REC
50 C REC

```

SUBR(U)TIME IMELM
INCLUDE INC1.LIST
INCLUDE INC2.LIST
DIMENSION ATAS(10),ATBS(10),ATCS(10)
COMMON/CARKIN/ KRK(10),ROUCLM,NC
DATA AO,BO,CG,OH,MOT,AM,GR,AM,ICE,
DATA AO,BO,CG,OH,MOT,AM,GR,AM,ICE,
FORMAT(13),JA,AF10.5)
15 FORMAT(5HRELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS
SURFACE/17A)IMEL 14
1/6XGMAT,NO,3X7HELEMENT,4XPHATOMIC WTS,2HEDEGE OAS
IMEL 15
IF (MCC=1) 90,20,90 IMEL 16
20 MEAO(KIN,5)15 IMEL 17
25 IF (IS=10) 25,25,60 IMEL 18
250 IS=15 IMEL 19
IF (KAT(15)=4) 254,253,254 IMEL 20
TK(ICAR,1)=TK(ICAR,1)+TK(15,1) IMEL 21
IS=IS-1 IMEL 22
253 IMEL 23
TK(10A,1)=TK(10A,1)+2.0*TK(15,1) IMEL 24
GO TO 254 IMEL 25
51 READ(KIN,10)(KAT(J),ATA(J),ATB(J),ATC(J),MAT(J),TK(J,1),TK(J,2),TK(J,3))
IMEL 26
1(J,3),J=1,15) IMEL 27
DO 93 I=1,15 IMEL 28
IF (KAT(I)=6) 95,94,95 IMEL 29
94 ICAR=1 IMEL 30
GO TO 93 IMEL 31
95 IF (KAT(I)=8) 93,96,93 IMEL 32
96 ION=1 IMEL 33
93 CONTINUE IMEL 34
ISS=15 IMEL 35
ISS=IS IMEL 36
KAT(15)=106 IMEL 37
ATA(15)=AG IMEL 38
ATB(15)=OG IMEL 39
ATC(15)=CG IMEL 40
WAT(15)=12.011 IMEL 41
TK(15,1)=0.0 IMEL 42
TK(15,2)=0.0 IMEL 43
TK(15,3)=TK(ICAR,3) IMEL 44
DO 91 I=1,15 IMEL 45
ATAS(I)=ATA(I) IMEL 46
ATBS(I)=ATB(I) IMEL 47
ATCS(I)=ATC(I) IMEL 48
GO TO 30 IMEL 49
91

```

```

CREC 51
CREC 52
CREC 53
CREC 54
CREC 55
CREC 56
CREC 57
CREC 58
CREC 59
CREC 60
CREC 61
CREC 62
CREC 63
CREC 64
CREC 65
CREC 66
CREC 67
CREC 68
CREC 69
CREC 70

```

```

80 IF (IFC(1) = 1) 115,68,85
85 IF (KR(6)) 95,90,90
90 IF (Y - TF(1) + .001) 115,95,95
95 Y(1) = 0.
IFC(1) = + 1
GOTO 115
100 VN(1) = VN(1) + OYI
IF (VN(1)) 110,110,105.
105 WTL = WTL + VN(1) * WTM(1)
GOTO 115
110 VN(1) = 0.
IFC(1) = - 1
115 I=I+1
116 FFF=WTG/OWR2
DO 120 I=1,15
120 SLAM(I) = SLAM(I) * FFF
121 RETURN
END

```

```

90 IS=IS*1
ISS=IS
TK(ICAR*1)=TK(ICAR*1)-VN(1)/AA
TK(IOX*1)=TK(IOX*1)-2*OVN(1)/AA
KAT(15)=44
ATAS(15)=AD
ATBS(15)=BD
ATCS(15)=CU
WAT(15)=44*Q11
TK(15)=VN(1)/AA
TK(15,2)=0.0
TK(15,3)=1.0E-10
ATA(1)=ATAS(1)
ATB(1)=ATBS(1)
ATC(1)=ATCS(1)
30 DO 57 K=1,3
VA = 0.7
50 J=1,15
IF (KAT(J) - 99) 35,45,35
35 IF (TK(J,K)) 40,50,45
40 VA = VA - TK(J,K)
TK(J,K) = - TK(J,K) / #AT(J)
GOTO 50
45 VA = VA + TK(J,K) * #AT(J)
50 CONTINUE
IF(VA) 53,57,53
53 DO 55 J=1,15
55 TK(J,K) = TK(J,K) / VA
57 CONTINUE
WRITE(KOUT,15)(KAT(J),ATA(J),ATC(J),MAT(J),TK(J,1),
ISP = IS * 1
60 IF (KR(3) - 9) 85,65,85
65 CONTINUE
DO 70 L=1,15
DO 70 I=1,15
TO(I,L) = 0.
DO 70 K=1,15
70 TO(I,L) = TO(I,L) * UM(I,K) * TK(K,L)
75 FORMAT(//////A04,3I)PROGRAM LIMITED TO 10 ELEMENTS )
85 RETURN
80 STOP
END

```

```

IMEL 51
IMEL 52
IMEL 53
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IMEL 92
IMEL 93
IMEL 94
IMEL 95
IMEL 96
IMEL 97

```

```

SUBROUTINE INPUT
REAL NF(10),NF(10),NF(10),NF(10),NF(10),NF(10),NF(10),NF(10),NF(10),NF(10)
COMMON/ACE1/GAMEX,MEPH,PCF,ACHSG,SBMAK,SXP
INCLUDE INCL1.LIT
INCLUDE INC2.LIST
INCLUDE OATA
COMMON/CARKIN/ KRK(10),ROUCH,NCC
OATA (NFIAU(1),NFIBD(1),FFIND(1),1-1,14)/
14MC 44 0.68950,44CH4 44 0.95030,44HCN 44
24MCU 44 0.10170,44CO2 44 1.24950,44HH 44
34HCHN 44 0.15730,44H2 44 0.28302,44H2O 44
44HN 44 0.75530,44N2 44 1.02750,44O 44
54HHO 44 0.74210,44O2 44 0.95530
5 FORMAT (1,1)
10 FORMAT (6F9.6,6K6.0,1.)
15 FORMAT (14E12.5,F10.4,2,14E12.5,F10.4,12,F7.4)
20 FORMAT (24E12.4,24E12.4,24E12.4,24E12.4,24E12.4)
23 FORMAT (7F3.0,13,42,9A4)
OATA CHAN,BLANK,44CHAR,44
J = ISP
IF (1) 30,30,35
30 CONTINUE
NJAN=0
FFA=431
NFF = 0
JC=KR(3) - (KR(3) / 2) * 2
VINT = P * 1.E - 6
VINT = ALOU(VINT)
JAT(8) = 0
N = 0
I1 = ISP
J = 1
IFL = - 1
IOC = 1
35 IF (KR(3) - 5) 40,50,50
40 IF (KR(3) / 42,41,42
41 NJAN=NJAN+1
DO 43 I=1,7
ALPT(I)=ALPTO(I,NJAN)
JAT(I)=JATD(I,NJAN)
43 SOURCE(1)=SURCD(I,NJAN)
SOURCE(8)=SURCD(8,NJAN)
AMOA=AMOAD(NJAN)
AMOB=AMOB(D,NJAN)

```

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IMPU0001
IMPU0002
IMPU0003
IMPU0004
IMPU0005
IMPU0006
IMPU0007
IMPU0008
IMPU0009
IMPU0010
IMPU0011
IMPU0012
IMPU0013
IMPU0014
IMPU0015
IMPU0016
IMPU0017
IMPU0018
IMPU0019
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IMPU0021
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IMPU0027
IMPU0028
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IMPU0031
IMPU0032
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IMPU0035
IMPU0036
IMPU0037
IMPU0038
IMPU0039
IMPU0040
IMPU0041
IMPU0042
IMPU0043
IMPU0044
IMPU0045
IMPU0046
IMPU0047
IMPU0048
IMPU0049
IMPU0050

```

```

IF (NJAN-1) 44,61,44
61 DO 71 I=1,4
  NFIA(I)=NFIAO(I)
  NFIB(I)=NFIBO(I)
  FFIN(I)=FFIND(I)
  NFF=14
  IF (NCC=1) 44,44,62
62 ALPT(I)=0
  JAT(I)=44
  ALPT(2)=0
  JAT(2)=0
  GO TO 44
42 READ(KIN,25) (ALPT(K),JAT(K),K=1,7),SORCE,AMOA,AMOB
44 IF (KR(3)-3) 55,45,45
45 WRITE( JAN) ALPT, JAT, SORCE, AMOA, AMOB
  GO TO 55
50 READ( JAN) ALPT, JAT, SORCE, AMOA, AMOB
  IF (JAN) 55,55,55
551 ALPT(I)=0
  JAT(I)=44
  ALPT(2)=0
  JAT(2)=0
  NJAN=1
55 IF (ALPT(I)) 60,375,60
60 IF (JAT(I)) 65,65,85
65 INF = NFF + 1
  K=ABS(ALPT(I))
  NFF = K + NFF
  IF (KR(3) - 5) 70,80,80
70 READ(KIN,20) (NFIA(I),NFIB(I),FFIN(I),I=1,NF,NFF)
  IF (KR(3) - 3) 35,75,75
75 WRITE( JAN) (NFIA(I),NFIB(I),FFIN(I),I=1,NF,NFF)
  GO TO 35
80 READ( JAN) (NFIA(I),NFIB(I),FFIN(I),I=1,NF,NFF)
  GO TO 35
85 DO 90 K=1,15
90 C(K) = 0
  DO 110 I=1,7
  IF (JAT(I)) 95,110,95
95 DO 100 K=1,15
  IF (JAT(I) - KAT(K)) 100,105,100
100 CONTINUE
  KK = II
  GO TO 285
105 C(K) = ALPT(I)
110 CONTINUE
115 WT = 0
  IF (JC) 125,120,125

```

```

INPU0051
INPU0052
INPU0053
INPU0054
INPU0055
INPU0056
INPU0057
INPU0058
INPU0059
INPU0060
INPU0061
INPU0062
INPU0063
INPU0064
INPU0065
INPU0066
INPU0067
INPU0068
INPU0069
INPU0070
INPU0071
INPU0072
INPU0073
INPU0074
INPU0075
INPU0076
INPU0077
INPU0078
INPU0079
INPU0080
INPU0081
INPU0082
INPU0083
INPU0084
INPU0085
INPU0086
INPU0087
INPU0088
INPU0089
INPU0090
INPU0091
INPU0092
INPU0093
INPU0094
INPU0095
INPU0096
INPU0097
INPU0098
INPU0099
INPU0100

```

```

120 WRITE(KOUT,25) (ALPT(K),JAT(K),K=1,7),SORCE,AMOA,AMOB
125 LAMK = 0
  LAMK = 0
  DO 140 I=1,15
  IF (C(I)) 130,135,130
130 LAMK = LAMK + L
135 L = L + L
  ALPT(I) = C(I)
140 WT = WT + C(I) * MAT(I)
  IF (J - IS) 145,145,215
145 JM = J - 1
  IF (JM) 175,175,150
150 DO 170 L=1,JM
  IML = IML + L
  UGM = C( IML )
  IF (UGM) 155,170,155
  UML(J) = 0
  INPU0066
  IF (UGM) 155,170,155
155 DO 160 I=1,L
  INPU0068
  UML(I,J) = UML(I,J) + UGM
160 UO 165 I=IML,15
  INPU0070
  C(I) = C(I) - TAU(I,L) * UGM
165 C(I) = C(I)
  INPU0071
  UML(J,L) = 0
170 UML(J,L) = 0
  INPU0072
  DO 180 I=1,15
  INPU0073
  IF (ABS(C(I)) - .001) 180,180,185
180 TAU(I,J) = 0
  INPU0074
  GO TO 215
185 IML(J) = 1
  INPU0075
  UML(J) = 1
  INPU0076
  UO 190 L=1,J
  INPU0079
  UML(L,J) = UML(L,J) / C(I)
  INPU0080
  DO 195 L=1,15
  INPU0081
  TAU(L,J) = C(L) / C(I)
  INPU0082
  205 YC = YINT
  INPU0083
  DO 210 L=1,15
  INPU0084
  C1(J,L) = ALPT(L)
  INPU0085
  KK = J
  INPU0086
  J = J + 1
  INPU0087
  J = J + 1
  INPU0088
  GO TO 285
  INPU0089
  215 CONTINUE
  INPU0090
  250 IF (J - IS) 255,255,270
  INPU0091
  255 UO 260 I=1,JM
  INPU0092
  260 VNU(I,I) = UML(I,J)
  INPU0093
  265 VNU(I,I) = 0
  INPU0094
  270 DO 275 L=1,15
  INPU0095
  VNU(I,L) = 0
  INPU0096
  DO 275 I=1,15
  INPU0097
  VNU(I,L) = VNU(I,L) + C(I) * UML(I,I)
  INPU0098
  >75 VNU(I,L) = VNU(I,L) + C(I) * UML(I,I)
  INPU0100

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INPU0101
INPU0102
INPU0103
INPU0104
INPU0105
INPU0106
INPU0107
INPU0108
INPU0109
INPU0110
INPU0111
INPU0112
INPU0113
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INPU0115
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INPU0148
INPU0149
INPU0150

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```

280 KK = I1
    KK = I1
    I1 = I1 + 1
    YC = 0
285 IF (KR(3) - 5) 290,300,300
290 IF (KR(3)) 292,291,292
291 DO 293 K=1,2
    RA(K)=RAD(K,NJAN)
    RB(K,K)=RBD(K,NJAN)
    RC(K,K)=RCD(K,NJAN)
    RD(K,K)=RDD(K,NJAN)
    RE(K,K)=RED(K,NJAN)
    RF(K,K)=RFD(K,NJAN)
    TU(K,K)=TUD(K,NJAN)
293 KPHA(K)=KPHAO(K,NJAN)
    GO TO 294
292 READ(KIN,10)(RA(K),RB(K,K),RC(K,K),RD(K,K),RE(K,K),RF(K,K),TU(K,K),KPHA(K),K=1,2)
    I(KK,K)=KPHA(K),K=1,2)
294 IF (KR(3)-3) 305,295,295
295 WRITE( JAN) (RA(K),RB(K,K),RC(K,K),RD(K,K),RE(K,K),RF(K,K),TU(K,K),KPHA(K),K=1,2)
    I,K),TU(KK,K),KPHA(K),K=1,2)
    GO TO 305
300 READ( JAN) (RA(K),RB(K,K),RC(K,K),RD(K,K),RE(K,K),RF(K,K),TU(KK),KPHA(K),K=1,2)
    I,K),TU(KK,K),KPHA(K),K=1,2)
305 IF (KK - I1) 310,35,310
310 IF (KK) = 2000.
315 IF (KPHA(1) - KPHA(2)) 315,330,320
320 WRITE(KOUT,325)AMO,AMO
    STOP
325 FORMAT (///25H BAD PHASE NUMBERING FOR 244)
330 IF (KPHA(1)-1) 320,345,340
335 TU(KK,1) = - TU(KK,1)
340 FF(KK) = 1.0 + 10
    VNI(KK) = - 1
    VIK(KK) = 0.
    YIK(KK) = AMAXI(YC,0.)
    GOTO 355
345 FF(KK)=(WT/HEFM)**FA
    IF (WT=.1) 346,346,350
346 FF(KK)=1.E+10
350 IF (KK) = 0
    VNI(KK) = VINT
    YIK(KK) = VINT
355 IF (JC) 365,360,365
360 WRITE(KOUT,15)(RA(K),RB(K,K),RC(K,K),RD(K,K),RE(K,K),RF(K,K),TU(KK,K),KPHA(K),K=1,2),FF(KK)
    I,K),TU(KK,K),KPHA(K),K=1,2),FF(KK)
365 IF (IFC(KK)) *FF(KK)**GAMLX
    IF (IFC(KK)) 3651,3650,3651
3651 FF(KK)=1.0E+10
INPU0151
INPU0152
INPU0153
INPU0154
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INPU0157
INPU0158
INPU0159
INPU0160
INPU0161
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INPU0190
INPU0191
INPU0192
INPU0193
INPU0194
INPU0195
INPU0196
INPU0197
INPU0198
INPU0199
INPU0200
3650 FAMO(IKK)=AMO
    FAMO(B(KK))=AMOB
    LAM(IKK)=LAMK
    WTM(IKK)=WT
    RB(KK,1)=RB(KK,1)+HA(1)
    RB(KK,2)=RB(KK,2)+HA(2)
    N=N+1
    IF (N=174) 368,368,366
    366 N=N-179
    WRITE(KOUT,367)NEX
    367 FORMAT(///11H THERE ARE 12.15H EXCESS SPECIES)
    STOP
368 CONTINUE
    IF (IKK=15) 35,370,35
    370 CONTINUE
    375 VNI(N,1)=0.
    TF(IN,1)=0.
    IFC(IN,1)=-1.
    WTM(IN,1)=-1.
    FAMO(IN,1)=CHAM
    FAMO(IN,1)=BLANK
    390 RETURN
    ENO
INPU0201
INPU0202
INPU0203
INPU0204
INPU0205
INPU0206
INPU0207
INPU0208
INPU0209
INPU0210
INPU0211
INPU0212
INPU0213
INPU0214
INPU0215
INPU0216
INPU0217
INPU0218
INPU0219
INPU0220
INPU0221
INPU0222
INPU0223

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KINE 151
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KINE 197
KINE 198
KINE 199
KINE 200

130 JUMI = PRMU(L,M)
    PRMU(L,M) = 0.
    DO 143 I=1,15
    IF (PRMU(I,M)) 135,143,135
135 UUM2 = PRMU(I,M) / UUM1
    MP = MM * I
    IF (MT - MP) 155,140,140
140 DO 150 K=MP,MT
    MA(K)
    PRMU(I,M) = PRMU(I,M) - UUM2 * PRMU(L,M)
    IF (ABS(PRMU(I,M))) = .001) 145,150,150
145 PRMU(I,M) = 0.
150 CONTINUE
160 A(I * 2,K) = A(I * 2,K) - UUM2 * A(L * 2,K)
    B(I * 2) = B(I * 2) - UUM2 * B(L * 2)
    E(I)=E(I)-UUM2*E(L)
    UUM2 = ABS(UUM2)
    EB(I) = AMAX1(EB(I),UUM2 * EB(L))
165 CONTINUE
    PRMU(L,M) = UUM1
    C*****ADU CONTROLLING REACTION INTO ITS MASS BALANCE
    I1 = L
    I2 = L
170 DO 175 J=1,15
    SUMU = RMU(J,M) * PKM(M) - PMU(J,M) * PKP(M)
    SUMU-SUMU.PMR(M)*(PS1(J,M)*VN(J)*FFA(M)+PPA(M)*EKK(J,M)*VN(J))/
    1(PPA(M)+FFA(M))
    DO 175 I=1,12
175 A(I * 2,J * 2) = A(I * 2,J * 2) - SUMU * PRMU(I,M)
    SUMU=-PRP(M)*OKPT(M)-(EAK(M)/RI+EKK(M))*PMR(M)
    UG 180 I=1,12
    UUM1 = PMR(M) * PRMU(I,M)
    A(I * 2,2) = A(I * 2,2) - UUM1
    A(I * 2,1) = A(I * 2,1) * SUMU * PRMU(I,M)
    E(I)=E(I)+UUM1
    B(I * 2) = B(I * 2) + UUM1
180 EB(I) = AMAX1(EB(I),ABS(PRMU(I,M) * RAT(MH)))
    IF (KKT(7) - 1) 200,200,185
185 WRITE(KOUT,215)
190 WRITE(KOUT,55)
    DO 195 I=1,15P2
195 WRITE(KOUT,50)(A(I,J),J=1,15P2),B(I)
    CONTINUE
    WRITE(KOUT,51)(M,1,1,2,LL,MM,MA
200 CONTINUE
    DO 200 MM=I,MT
    L=LL(MM)
KINE 101
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39 WRITE(KOUT,61) M1,SUMK,OKPT(M),PKR(M),PKP(M),PMR(M),RAT(M)
40 MA(M) = M
41 FORMAT(13,2A,8E12,5)
45 FORMAT(12Z9HA(1),J,B(1),1,1,8,J,I,8 IN)
50 FORMAT(11E10,3)
55 FORMAT(12Z9HA(1),J,B(1),1,1,8,J,I,8 OUT)
    KR7=KR(7)
    KR(7)=0
    IF (KR(7) - 1) 80,80,65
65 CONTINUE
    WRITE(KOUT,50)PRMU
    WRITE(KOUT,215)
    WRITE(KOUT,50)(EB(I),1=1,15)
70 WRITE(KOUT,45)
    DO 75 I=1,15P2
75 WRITE(KOUT,50)(A(I,J),J=1,15P2),B(I)
80 CONTINUE
C*****ORDER REACTIONS
85 IF (MT - 1) 105,105,90
90 K = 0
    DO 100 M=2,MT
    IF (RAT(M) - RAT(M - 1)) 100,100,95
95 K = MA(M)
    MA(M) = MA(M - 1)
    MA(M - 1) = K
    UUM1 = RAT(M)
    RAT(M) = RAT(M - 1)
    RAT(M - 1) = UUM1
100 CONTINUE
C*****START SECOND MAJOR LOOP ON REACTIONS
105 DO 200 MM=I,MT
    M = MA(MM)
    LL(MM) = 0
    DO 125 L=1,15
    IF (PRMU(L,M)) 110,125,110
110 DO 115 K=1,MM
    IF (L - LL(K)) 115,125,115
115 CONTINUE
    IF (RAT(MM) - EB(L)) 125,125,120
C * * * YES, IT IS FOR MASS BALANCE L
120 LL(MM) = L
    GOTO 130
125 CONTINUE
C * * * NO, IT IS NOT. ADD INTO ALL MASS BALANCES
    I1 = 1
    I2 = 15
    GOTO 170
C*****REARRANGE ACCORDING TO CONTROLLING REACTION

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```
IF (I) 201,206,201
201 M=MA (MH)
   A=R=1.
   XL=(PKR(M)+1.E-36)/(PKP(M)+1.E-36)
   IF (ABS(EXEL-1)+.1) 20%204*202
202 ELK=ALOG(EXEL)
   AR=EXEL/EXEL-1+1./ELK
204 DO 205 J=1,15
205 A(L+2,J+2)=A(L+2,J+2)+E(LJ)*E(LJ)*(PMU(J,M)+(1.-AR)*AR*RMU(J,M))
206 CONTINUE
   ENL = 0.
   DO 210 I=3,15P2
210 ENL = AMAX1(ABS(E(I-2)) / EB(I-2), ENL)
215 FORMAT(1A12HEB(M),M=1,M1)
   KR(I)=KR7
   IF (ENL-1.E-5) 216,216,225
220 IT=ITS
   ITS=-1
225 RETURN
   END

SUMROUTIME *MIN
UTHEINSTEON *A(10,J),*MA(13,33),*ZA(133),*PRA(133),*TFA(8),*TSA(115)
INCLUDE INCL1.L15T
COMMON/CARIN/ KKK(10),ROUCH,NCC
COMMON/CUNCLU/ Z,GAMER,WR(3)
DATA (TFA(I),I=1, 8),500.,1000.,1500.,2000.,2500.,3000.,3500.,4000.,
1600./
DATA (TSA(I),I=1,15),1200.,1400.,1600.,1800.,2000.,2200.,2400.,2600.,
12600.,2800.,3000.,3200.,3400.,3600.,3800.,4000./
DATA KTF,KFY,78,15/
202 NCC=NCC+1
   IF (NCC-1) 21,21,2
1 HEAD(KIN,701)=KKK(2,PR,ZE,PC,ROUCH,GAMER,TILE
701 FORMAT(10I11,6F10.5,2A4,A2)
   IF (PKK(11)-8) 20,20,203,204
203 KR(I)=8
   GO TO 49
204 IF (KKK(5)-2) 4,3,4
   3 KTF=0
   6 ATF=KTF+1
   READ(KIN,702) TFA(KTF)
702 FORMAT(F10.5)
   IF (TFA(KTF)) 6,5,6
   5 KTF=KTF-1
   4 IF (KKK(6)-2) 8,7,8
   7 KTS=0
   10 KTS=KTS+1
   HEAD(KIN,702) TSA(KTS)
   IF (TSA(KTS)) 10,9,10
   9 KTS=KTS-1
   8 KR(7)=KKK(10)
   KR(8)=KKK(11)-1
   KR(9)=0
   IF (KKK(9)) 12,11,12
11 KR(10)=0
   GO TO 13
12 KR(10)=1
13 IF (KKK(J)) 15,14,15
14 KRA(I,J)=1
   GO TO 16J
15 KRA(13,1)=KKK(13)
163 KRKS=1
   KRKS=0
   IF (KKK(3)-9) 161,160,161
160 KRA(13,1)=1
   KRKS=4
   GO TO 16
161 IF (KKK(3)-3) 16,16,2,164
162 KRKS=5
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104	KKKS6	KRA(5,3)=0	KINI 101
16	KRA(1,1)=KK(2)	KRA(9,3)=0	KINI 102
	KRA(2,1)=1	ZA(3)=0.0	KINI 103
	KRA(6,1)=0	PRA(3)=0.0	KINI 104
	KTC=9.2E+05	NCT=3	KINI 105
	UO 17 11.0 TIC	UO TO 36	KINI 106
	KRA(6,1)=KK(16)	NCT=2	KINI 107
	KRA(7,1)=KK(7)	UO TO 36	KINI 108
	KRA(8,1)=KK(8)	23 IF (KK(11)-3) 29.26.29	KINI 109
	KRA(10,1)=KK(10)	28 KRA(5,1)=2	KINI 110
	KRA(1,1)=1.0	KRA(11,2)=3	KINI 111
	KRA(2,1)=0.0	KRA(12,2)=0	KINI 112
	KRA(3,1)=9.0	KRA(15,2)=0	KINI 113
17	CONTINUE	KRA(16,2)=1	KINI 114
		KRA(19,2)=0	KINI 115
		ZA(2)=0.0	KINI 116
		PRA(2)=ZE	KINI 117
			KINI 118
			KINI 119
18	IF (KK(11)) 19.18.19	30 KRA(1,3)=0	KINI 120
		KRA(2,3)=1	KINI 121
20	IF (KK(8)-4) 21.20.21	KRA(3,3)=KK(5)	KINI 122
		KRA(4,3)=0	KINI 123
		KRA(5,3)=0	KINI 124
		KRA(9,3)=0	KINI 125
		ZA(3)=0.0	KINI 126
		PRA(3)=0.0	KINI 127
		NCT=3	KINI 128
		UO TO 36	KINI 129
		NCT=2	KINI 130
		UO TO 36	KINI 131
21	NCT=1	29 KRA(5,1)=2	KINI 132
		KRA(1,2)=3	KINI 133
19	IF (KK(11)-2) 22.22.23	KRA(2,2)=0	KINI 134
22	KRA(5,1)=0	KRA(3,2)=0	KINI 135
	KRA(1,2)=4	KRA(4,2)=0	KINI 136
	KRA(12,2)=0	KRA(5,2)=1	KINI 137
	KRA(4,2)=0	KRA(9,2)=0	KINI 138
	KRA(15,2)=0	ZA(2)=0.0	KINI 139
	KRA(19,2)=0	PRA(2)=ZE	KINI 140
	ZA(2)=0.0	KRA(1,3)=4	KINI 141
	PRA(2)=0.0	KRA(2,3)=0	KINI 142
	IF (KK(11)-2) 27.26.27	KRA(3,3)=0	KINI 143
26	KPA(5,2)=3	KRA(4,3)=0	KINI 144
27	IF (KK(8)-4) 25.24.25	KRA(5,3)=0	KINI 145
24	KRA(1,3)=0	ZA(3)=0.0	KINI 146
	KRA(12,3)=1	PRA(3)=0.0	KINI 147
	KRA(13,3)=KK(5)	IF (KK(11)-5) 33.32.33	KINI 148
		32 KRA(5,3)=3	KINI 149
			KINI 150

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33 IF (KRK(4)=4) 35,34,35
34 KRA(1,4)=0
   KRA(2,4)=1
   KRA(3,4)=KRKS
   KRA(4,4)=0
   KRA(5,4)=0
   KRA(9,4)=0
   ZA(4)=0,0
   PRA(4)=0,0
   NCT=4
   GO TO 36
35 NCT=3
36 00 360 I=1,NCT
360 KRA(1,1)=0
   IF (KRK(5) = 38,37,38)
38 NCT1=NCT-1
   NCT2=NCT-KIF
   00 39 I=NCT1,NCT2
   KRA(1,1)=0
   KRA(2,1)=0
   KRA(3,1)=0
   KRA(4,1)=0
   KRA(5,1)=0
   KRA(9,1)=0
   ZA(1)=YA(1)-NCT
   PRA(1)=0,0
39 CONTINUE
   KRA(3,NCT1)=KRKS
   NCT3=NCT2-1
   NCT4=NCT2-KIS
   GO TO 40
37 NCT3=NCT-1
   NCT4=NCT-KIS
40 IF (KRK(6)) 45,46,45
45 NCT5=NCT3-1
   00 41 I=NCT3,NCT5
   KRA(1,1)=0
   KRA(2,1)=0
   KRA(3,1)=0
   KRA(4,1)=0
   KRA(5,1)=0
   KRA(9,1)=0
   ZA(1)=500,0
   PRA(1)=0,0
   WRA(3,1)=1,0E-19
41 CONTINUE
410 IF (KRK(5)) 411,410,411
411 KRA(3,NCT3)=KRKS
   411 KRA(4,NCT5)=2
   ZA(NCT5)=1000,0

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NCT3=NCT3-2
NCT4=NCT4-2
00 42 I=NCT3,NCT4
KRA(1,1)=5
KRA(2,1)=0
KRA(3,1)=0
KRA(4,1)=2
KRA(5,1)=0
ZA(1)=YA(1)-NCT3-1
PRA(1)=0,0
IF (KRK(81-1)) 421,421,422
421 KRA(9,1)=0
   GO TO 42
422 KRA(9,1)=4
42 CONTINUE
IF (KRK(81-1)) 43,43,44
44 KRA(9,NCT3)=6
43 NCT3=NCT4-1
46 CONTINUE
IF (PC) 53,2,53
53 00 54 I=1,NCT3
   K=NCT3-2-1
   00 55 J=1,2
   KRA(J,K)=KRA(J,K-1)
   ZA(K)=ZA(K-1)
   PRA(K)=PRA(K-1)
   WRA(1,K)=WRA(1,K-1)
   WRA(2,K)=WRA(2,K-1)
   WRA(3,K)=WRA(3,K-1)
54 00 56 I=1,10
   00 57 J=1,2
   KRA(I,1)=KRA(I,2)
   KRA(I,2)=2
   KRA(2,2)=0
   KRA(3,2)=0
   ZA(2)=0,0
   ZA(1)=2
   PRA(1)=PC
   NCT3=NCT3-1
   2 IF (NCT3) 200,201,201
201 .....
   GO TO 202
200 00 47 I=1,10
   KR(1)=KRA(1,NCT)
   Z=ZAINCC
47 CONTINUE
PR=PRA(NCT)
WR(1)=WRA(1,NCT)
WR(2)=WRA(2,NCT)
WR(3)=WRA(3,NCT)

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165 #JC=Y(I)-2)
JCS=JC
IMAX = TF(1 - 2)
JC = 1 - 2
JFC=JBC(1-2)
IF(KR(8)) 169,169,240
169 A(1,JC5+2)=0.
A(1,1)=1.0
B(1)=BJC
GOTO 290
C-----GAS PHASE
170 VA = VM(1 - 2)
CPG = CPG + VA * CP(1 - 2)
A(2,1) = VA
EP = EP - VA
IF(KAT(1K)-99) 175,235,175
175 IF (KR(6)) 235,210,180
180 00 185 K=1,15
185 A(K+2,1) = (GANK(1-2,K) + GANK(K) * H(1-2)) * VA
A(1,1) = A(1,1) + VA * RV
190 OUM2 = VM(1 - 2) / WTG * MTL / WTG * VA
DO 205 K=1,15
IF (EB(K) - ABS(A(K + 2,1))) 195,200,200
195 EB(K) = ABS(A(K + 2,1))
18(K) = 1 - 2
200 E(K) = E(K) - A(K + 2,1)
205 A(K + 2,1) = A(K + 2,1) * OUM2 * PNUMS(K)
GOTO 240
210 OUM1 = WTM(1 - 2) / WTG * VA
OUM2 = WTL / WTG * OUM1
IF (KR(4)) 215,215,220
215 OUM1 = 0.
VA = (RV + 1.) * VA
GOTO 225
220 UMI = OUM1 * (1. - FFF / FF(1 - 2))
VA = (RV * FFF / FF(1 - 2)) * VA
225 DO 230 K=1,15
230 A(K + 2,1) = UMI * SLAM(K) * DUM2 * PNUMS(K)
A(1,1) = A(1,1) + VA
235 EB(1 - 2) = ABS(VA)
18(1 - 2) = 1 - 2
E(1 - 2) = E(1 - 2) - VA
240 IF (MODE - 2) 285,260,245
245 IF(18C(1-2)) 290,255,250
250 M05 = SB(1 - 2)
GOTO 270
255 M05 = SB(1 - 2) - 1.9869 * Y(1 - 2) - 1.9869
GOTO 275
260 M05 = H(1 - 2)

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I=2-IR(1K)
IF(KAT(1K)-99) 45,41,45
PNUMS(1-2)=0.
ZERO MATRIA
45 DO 50 K=1,15
50 A(K,1) = 0.
IF (175) 70,55,70
NORMALIZE UN PRESSURE ON FIRST PASS
55 VM(1 - 2) = VM(1 - 2) / SUMN
EML(1 - 2) = 0.
IF(18C(1-2)) 70,60,65
60 GOTO 72 = Y(1 - 2) - SUML
65 VM(1 - 2) = VM(1 - 2) / SUMC
70 S(1) = 0.
A(1,1) = 0.
IPI(1 - 2) = 0.
SET FLAG INDICATING SIGNIFICANCE OF SPECIES IN MASS
BALANCE(S) AND INCREMENT COUNT ON SIGNIFICANT SPECIES
75 IF (VM(1 - 2) - EBL(1 - 2) 85,85,80
80 IPI(1 - 2) = 1
TREAT BASE SPECIES CONTAINING BUT NOT REPRESENTING NON-PRESENT
ELEMENTS IN SAME MANNER AS NON-PRESENT CONDENSED SPECIES
85 IF(18C(1-2)) 140,170,95
95 A(1,1) = 1.
VA = VM(1 - 2)
IF(148S(18C(1-2)-31-1)) 96,240,100
GOTO 240
A(2,1)=1.0
100 IF (EB(1 - 2) - ABS(VA)) 105,110,110
105 EB(1 - 2) = ABS(VA)
18(1 - 2) = 1 - 2
110 E(1 - 2) = E(1 - 2) - VA
IF (KR(6)) 115,120,120
115 IF (MODE - 1) 240,130,240
120 DO 125 K=1,15
125 A(K+2,1)=-WTM(1-2) * (PNUMS(K)/WTG+GAMP(K))
A(1,1) = A(1,1) + 1.
130 TFM = AMAT(TFM)+TF(1 - 2)
135 A(1,1) = 1.0E + 10 * VM(1 - 2) * 1.001E + 10
MODE = 0
140 IF(MODE-1) 141,145,141
141 IF(KR(8)) 240,240,145
145 IF (TF(1 - 2) * .001 - 7) 290,150,150
150 IF (JC) 165,165,155
155 IF(Y(1-2)-BJC) 290,290,165

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265 IF (IBC(I-2)) 290,275,270
270 A(I,I) = HOS
275 A(I,I) = -HOS * VN(I - 2)
280 A(I,2) = A(I,2) - HOS * VN(I - 2)
285 CPF = CPY * CP(I - 2) * VN(I - 2)
290 CONTINUE
DQ 295 I=1,15
BE(I)=E(I)
BY(I)=Y(I)
RETURN
END

MATI 151
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MATI 163

SUBROUTINE MAT2
C
C INCLUDE INCI-LIST
C
C INCLUDE INC3-LIST
C
C ISPO = IS * 2
C ISP2 = ISPU
C IER = 0
C IER = 0
C IER = 0
C --- MAIN NON-BASE SPECIES LOOP
C
C IF (JCI) 4,41J
C 3 4JCY(2C)
C 4 LIM=NR(R(I))
C 5 J=ISP
C 6 345 IK=ISP, LIM
C 7 E(J)=I, E-10
C 8 IF (IFC(J)) 55,345,85
C 9 IF (IFC(J,1)) 345,15,15
C 10 IF (IFC(J,1)) 345,15,15
C 15 IF (ITS) 35,20,35
C 20 VN(J) = VN(J) / SUMH
C 25 VN(J) = VN(J) / SUMC
C 30 Y(J) = Y(J) - SUML
C 35 E(J) = VLM(J) - Y(J)
C 40 FMU(I) = 0.
C 45 FMU(I) = VMU(J,1)
C 50 CONTINUE
C 55 E(J) = E(J) * FMU(I) = BY(I)
C 60 FMU(I) = ABS(E(J))
C 65 IF (IFC(J)) 55,215,85
C 70 FMU(I) = ABS(E(J))
C 75 IER = IER + 1
C 80 IER = IER

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TMAX=TF(J)
IF(KR(8)) 192,192,191
191 IF(MODE-2) 345,280,205
192 B(1)=B(J)
DO 195 K=1,15
195 A(1,K) = 2 * FNU(K)
A(1,1) = TC(I)
GOTO 345
200 MOS = H(J)
MAT2 110
205 MOS = SB(LJ)
MAT2 111
210 A(1,1E) = MOS
MAT2 112
A(1,2) = A(1,2) - VN(J) * MOS
MAT2 113
CPF = CPF * CP(J) * VN(J)
MAT2 114
GOTO 335
MAT2 115
C*****GAS PHASE SPECIES
MAT2 116
215 IPIJ = 0
MAT2 117
IF (VN(J)) 220,335,220
MAT2 118
220 IO = 0
MAT2 119
CPG = CPG * VN(J) * CP(J)
MAT2 120
IF (KR(6)) 245,225,230
MAT2 121
225 FFJ = FFF / FF(J)
MAT2 122
230 DUM1 = WM(J) / WTG * VN(J)
MAT2 123
DUM2 = DUM1 / WTG * WTL
MAT2 124
IF(KR(6)) 234,234,245
MAT2 125
234 IF(KR(4)) 235,235,240
MAT2 126
235 FFJ = 1.0
MAT2 127
GOTO 245
MAT2 128
240 DUM1 = DUM1 * (1. - FFJ)
MAT2 129
245 JO 300 KI=1,15
MAT2 130
1=2-1R(KI)
MAT2 131
VA = VNU(LJ) - 2 * VN(LJ)
MAT2 132
IF(KAT(KI)-99) 247,265,247
MAT2 133
247 IF(KR(6)) 265,260,250
MAT2 134
250 VA = VA * NV * VN(LJ) * (VLAR(J,I - 2) * GAMH(I - 2) * H(J))
MAT2 135
BE(I - 2) = BE(I - 2) - VA
MAT2 136
ABSVA = ABS(VA)
MAT2 137
VA = VA * PMS(I - 2) * DUM2
MAT2 138
GOTO 270
MAT2 139
260 VB = VA * FFJ
MAT2 140
VA = NV * VA * VB
MAT2 141
BE(I - 2) = BE(I - 2) - VA
MAT2 142
ABSVA = ABS(VA)
MAT2 143
VA = VJ * SLAM(I - 2) * DUM1 * DUM2 * PMS(I - 2)
MAT2 144
GOTO 270
MAT2 145
265 BE(I - 2) = BE(I - 2) - VA
MAT2 146
ABSVA = ABS(VA)
MAT2 147
270 IF (ABSVA - EBL(I - 2)) 280,280,275
MAT2 148
275 IO = 1
MAT2 149
MAT2 150

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ICE = IK
GOTO 90
85 ISPB = ISPU * I
IE = ISPO
90 WTR = 0.
IF (KR(6)) 100,95,95
95 THIN = AMAX1(TF(J) * THIN)
WTR = WTR(J) / WTG
100 DO 105 I=1,ISPO
105 A(1,1E) = 0.
DO 145 K=1,15
GUMI = VNU(J,K)
IF(IBC(K)-1) 125,125,145
125 VA = DUM1 * VN(J)
130 A(K,2,1E) = DUM1 * WTR * (PMS(K) * GAMF(K) * WTG)
135 BE(K) = BE(K) - VA
IF (ABS(VA) - EB(K)) 145,145,140
140 EB(K) = ABS(VA)
18(K) = IK
145 CONTINUE
IF(IK-N) 146,148,146
146 JJ(K)=JC
8(1E)=Y(JC)
IF(JC-15) 151,151,147
147 A(1E,1)=TC(JC)
8(1E)=E(JC)
151 EAB=B(1E)
IF(IFCJC) 335,335,152
152 EAB=ABS(EAB)
GOTO 335
148 JJ(K)=J
A(1E,1) = TC(J)
8(1E) = E(J)
IF(I=001-IF(J)) 150,149,149
149 IF(KR(6)) 165,165,175
150 IF (MODE - 1) 155,160,155
155 IF(KR(6)) 165,160,160
160 A(1E,1E) = 1-E * 10
8(1E) = - VN(J) * 1.001E * 10
MODE = 0
165 IF (MODE - 2) 170,200,205
170 IF (MODE - 1) 335,175,335
175 IF(T-IF(J)-001) 180,180,191
180 IF (JC) 190,190,185
185 IF(E(J)-BJC) 345,345,190
190 BJC=E(J)
JC=IK
IFCJC=IFC(JC)

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IF (ABSVA - EB(I - 2)) 290,290,285
280 IF (ABS(IVA) - EBL(I - 2)) 300,390,290
285 EB(I - 2) = ABSVA
IB(I - 2) = IK
290 00 295 K=1,ISP2
295 A(I,K) = A(I,K) * VA * FNU(K - 2)
B(I) = B(I) * VA * E(J)
A(I,1) = A(I,1) * VA * TC(J)
A(I,2) = A(I,2) * VA * FNU(I - 2)
300 CONTINUE
IF (I0) 335,335,305
305 EP = EP - VN(I,J)
B(2) = B(2) - VN(J) * E(J)
A(2,1) = A(2,1) - VN(J) * TC(J)
IF (MODE - 2) 330,310,315
310 M05 = M(J) * VN(I)
315 M05 = VN(I) * (EB(J) - 1.9869 * Y(J) - 1.9869)
320 00 325 I=3,ISP2 FNU(I - 2) * A(I,1)
A(I,2) = A(I,2) - M05 * TC(J)
A(I,1) = A(I,1) - M05 * E(J)
B(I) = B(I) - M05 * E(J)
330 CPF = CPF * VN(J) * CPI(J)
340 EL = EAB
345 J=J+1
350 RETURN
END
SUBROUTINE MAT3
DIMENSION L(10),AR(10)
INCLUDE INCLALIST
INCLUDE INCLALIST
ISP3 = IS * 3
IF (MODE - 2) 50,5,25
CPA = CPF * T
SHMLT = HMELT * VN(HMELT)
EMS = AA * HIP * A(1,2)
IF (KKJ=1) IS=10,15
DUM1 = SVA / AA * T * T
EMS = AA * SVC - DUM1 * A(1,2)
HIP = - A(1,2) / AA
CPA (CPF * 2 * DUM1 / T) * T
DUM2 = SVB / AA * T
P=PF-EP
EP=0
IF (ABS(EMS/AA)-10.) 13,13,15
EP=-P*SVB-DUM2
A(2,1) = A(2,1) * DUM2
A(2,2) = - DUM2
CONTINUE
GOTO 30
CPA = CPF
SHMLT = SVELT * VN(HMELT)
EMS = AA * SIP * A(1,2) - 1.9869 * (P - EP)
A(1,2) = - AA * SIP
B(1) = B(1) * EMS
A(1,1) = A(1,1) * CPA
IF (SHMLT) 50,50,35
IF (EMS) 50,50,40
EMS = EMS - SHMLT
B(1) = B(1) - SHMLT
IF (FHS) 45,50,50
FLIO = 1 * EMS / SHMLT
MODE = 0
A(1,1)=1.E+10
TMIN = 500.
TMAX = 500.
ENL=ABS(EP)/P*100.
DO 75 I=3,ISP2
L(I - 2) = 1 - 2
E(L - 2) = E(L - 2)
EBL(I-2)=E(L-2)*1.E-7
A(I,2) = AA * ALP(I - 2)
IF (IFC(I - 2) - 1) 60,60,55
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55 NFM = NCM * I
GOTO 75
60 IF (K(16)) T0.70.65
55 A(1,1) = A(1,1) * GAMMA(1 - 2) * T * CPG
E(1,2) = C(1,2) * WLGAMF(1,2)
70 ER = E(1,2)
BER = ABS(ER) / (EB(1,2) * 1.E - 20)
ENL = AMAXI(BER,ENL)
U(1) = B(1) * ER
75 CONTINUE
IF (ISP2 - 1) SP0: 80.255.255
80 IV = 0
JZ = 0
C A00 CONDENSED NONBASE SPECIES TO ARRAY
85 00 90 1E=1SP3,1SP0
J = 1E - ISP2
J = JJ(J)
IF (J-15) 86,86,88
86 00 87 K=1,15
87 A(IE,K+2)=0
A(IE,K+2)=-1.0
GO TO 90
88 00 89 K=1,15
89 A(IE,K+2)=-VNU(J,K)
90 CONTINUE
C CHECK FOR SINGULAR CONDENSED SET
IV = IV - 1
95 00 140 1E=1SP3,1SP0
IF (IV - 1) 129,120,100
C REDUCE NEW ROW BY PREVIOUS ROWS
100 00 115 J=2,IV
K = L(J - 1)
UJ = - A(IE,K * 2)
IF (DIV) 105,115,105
105 A(IE,K * 2) = 0.
JM = J * ISP
00 110 M=3,ISP2
110 A(IE,M) = A(IE,M) + OIV * A(J,M)
115 CONTINUE
C SEEK VALIO NON-ZERO ELEMENT
120 00 130 J=1V,15
M = L(J)
IF (ABS(A(IE,M * 2)) - .01) 130,130,125
125 IF (IFC(M)) 135,135,130
130 CONTINUE
C SINGULAR CONDENSED SET
GOTO 145
135 L(J) = L(IV)
L(IV) = M
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OIV = A(IE,M * 2)
A(IE,M * 2) = 1.
NORMALIZE NEW ROW
UO 140 J=3,ISP2
140 A(IE,J) = A(IE,J) / OIV
COMPLETES MAJOR LOOP=NON SINGULAR
CPO 85
EXTRACT COEFFICIENTS ON SINGULAR SET=NONBASE;
K = L(J - 1)
150 ARI(J - 1) = A(IE,K * 2)
ARI(IV) = 1.
EXTRACT COEFFICIENTS ON SINGULAR SET - BASE
00 165 K=1,15
IF (IFC(K)) 165,165,155
155 IF (ABS(A(IE,K * 2)) - .01) 165,165,160
160 IV = IV * 1
ARI(IV) = - A(IE,K * 2)
JJ(IV) = K
165 CONTINUE
ISOLATE NEW CONDENSED CANDIDATE
00 175 J=1,IV
K = JJ(J)
ITC JZ = J
KZ = K
GOTO 185
175 CONTINUE
180 STOP
C NO MUST GO TO ALLOW ENTRY OF NEW CANDIDATE
185 TEST = - 1.0E10
JX = 0
UO 200 J=1,IV
IF (ABS(ARI(J)) - .01) 200,200,186
186 DUMI=ARI(J)/ARI(J)
IF (DUMI) 190,200,200
190 K = JJ(J)
DUMI = DUMI * VNI(K)
IF (DUMI - TEST) 200,200,195
195 TEST = DUMI
JX = J
KX = K
200 CONTINUE
TEST = VNI(KX) / ARI(JX)
GOES NEW CANDIDATE ENTER
IF (E(KX) - E(KX)) 85,85,205
YES
205 00 210 J=1,IV
K = JJ(J)
210 VNI(K) = VNI(K) - TEST * ARI(J)
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22 FORMAT (2X,'JMCHEMICAL STATE ADJACENT TO THE SURFACE/3X,54H(MOLE FUR)OUTP0051
14 FUR GASES = MOLECULES / TOTAL GAS MOLECULES /3X,50H(MOLE FR FUR)OUTP0052
2 CONDENSED = BPRIME CONDENSED )
23 FORMAT (82A,2HIF8.5,11H LIQUID ANOF8.5,6H SOLID)
24 FORMAT (25A,2H FORA, RATE OF KINETICALLY CONTROLLED REACTIONS/OUTP0053
1 70H (MOLES OF REACTION / UNIT SURFACE AREA TIME RHOG DE CH) OUTP0054
2. . . . / (14,1H=E12.5,13,1H=E12.5,13,1H=E12.5,13,1H=E1 OUTP0055
32.S))
25 FORMAT ( 78TH SPECIES MOL.FRAC. 0-LN=RP/0-LN-T LOG-PP LOUUTP0056
IU-KP FLAG ERROR CP / (1A2A,4E13.5,5,5,2E13.5))
ASQRT(O)=SIGN(SQRT(ABS(O)),O)
TAN(O) = SIN(O) / COS(O)
MEPS = 0.01
FIND VKIN AS FIMST MINZERO FRF (M)
VKIN=ROUCH
703 CONTINUE
35 WM = AA / P
CALL ETIMEF(TIME)
WRITE(KOUT,S) IT,TIME
SSIP = SIP
KR8=KR(8)
IF(JC(N)-1ME) 61,61,62
41 JC=N-1
KR8=0
42 MG=0
ML = 0.
SG=N.
SPL=0.
HIP = 0.
WLS=MTL
SIP = 0.
PMU2 = 0.
MTL = 0.
BPRM=W(13)
TT=1.8
70 UO 45 J=I,N
MTL = HTL * VN(J) / FF(J) * H(J)
PMU2 = PMU2 * VN(J) / FF(J) * WTN(J)
VA = VN(J) * H(J)
IF (IFC(J)) 80,75,80
75 HG = HG * VA
SG=SG*VN(J)*(GB(J)-1.5869EY(J))
GOTO 95
80 ML = ML * VA
SPL=SL*VN(J)*S9(J)
SPL=SL*VN(J)
95 CONTINUE
41W(12)=W(13)-WLS/WTU

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101 WLS=MTL*VN(N+1)
BPRM=BPRM*VN(N+1)/WTU
104 HTL=MTL/PMU2
IF(SPL) 107,100,107
106 WLS=0
WLS=J.E-30
SPL=J.0
107 WTR=WLS/WTU
ML = ML*VN(MELT)*FLI+MHMELT
SC = SL*VN(MELT)*FLI+MSHMT
HIP=(ML+HG)/AA
SIP=(SL+SG)/AA
KRI=KR(1)-IFRZ*KRB
FAF=GAMEX
IF (KR(4)) 160,150,155
150 MTL = HG / AA
FAF = 0.
155 WSO=MAX1(MS-W(13)*BPRM,1.E-30)
HIP=(HG*(ML-WTR*HG)/WSU)/AA
SIP=0.
160 RHOG=PMW/(101.3146)
RHOG=WTG/(101.3146)
HG=HG/WTG*1.8
ML=ML/MTL*1.8
SL=SL/MTL
SG=SG/WTG
MRP=HIP*1.8
WKG=WTG/P.
WHL=MTL/SOL
IF(KR(6)) 181,182,182
181 WRITE(KOUT,6) WTR
WRITE(KOUT,7) TT,T,P
GO TO 183
182 WRITE(KOUT,195)
1820 WRITE(KOUT,191)
GO TO 1824
1821 IF (KR(4)-2) 1823,1822,1823
1822 WRITE(KOUT,192)
GO TO 1824
1823 WRTF(KOUT,193)
1824 WRITE(KOUT,194) ROUCH
WRITE(KOUT,18) RV,BPRM
WRITE(KOUT,20) TT,T,P
183 WRITE(KOUT,8) HG,ML,HBP,SG,SL,SIP,RHOG,RHO,WKG,WHL,W
210 IF(KR(J) 220,245,245
220 VLSO = ( (SVI * SIN(SAI)) * 2. * ( (SRI / RHO) * SVI * COS(SAI)) ) ) * 2. / 45054.
SA2 = (ATAN(RHO / SRI * TAN(SAI))) * 57.29577

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OUTP0101
OUTP0102
OUTP0103
OUTP0104
OUTP0105
OUTP0106
OUTP0107
OUTP0108
OUTP0109
OUTP0110
OUTP0111
OUTP0112
OUTP0113
OUTP0114
OUTP0115
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OUTP0122
OUTP0123
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OUTP0125
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OUTP0143
OUTP0144
OUTP0145
OUTP0146
OUTP0147
OUTP0148
OUTP0149
OUTP0150

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SOL=SA1*57.29577
SH1=SH1*1.8
SOMAK=(VELSU/GAM*WM/(1.9869*PI))
VMACH=ASORT(SOMAK)
VEL=ASORT(VEL50*45054.)
FLUA=VEL*DMU
WRITE(KOUT,11) VEL,VMACH,SA2
MBH=HCH*1.8
WRITE(KOUT,12) SVL,SH1,MBH,SP1,SRI,SOL
SH1=SH1/1.8
GOTO 260
245 IF(KR(5)=1) 246,255,250
246 IF(KR(5)) 247,260,260
247 WRITE(KOUT,14)
MBH=HCH*1.8
SOL=SA1*57.29577
SH1=SH1*1.8
WRITE(KOUT,15) SVL,SH1,MBH,SP1,SRI,SOL
GO TO 260
250 HCH=HIP
SCH=51P
PCHEP
GO TO 260
255 VEL50=(HUM-11P)*2.
VMACH=VELSU/GAM*WM/(1.9869*PI)
VMACH=ASORT(SOMAK)
VEL=ASORT(VEL50*45054.)
FLUA=VEL*DMU
MKN=(HCH-HIP)*1.8
WRITE(KOUT,10) MKN,VEL,FLUX,VMACH
IF(KR(1)=5) 260,260,1,260
2601 PUNCH 2602,VEL,P,HG,PK(1)
2602 FORMAT(1,3X,JE11.5,22X,F11.2)
260 CONTINUE
165 IF(NCV*ITS) 166,180,180
166 WRITE(KOUT,21)
W(2)=ROUCH
IF(KR(1)=3) 169,1,168,2,180
C****SCHHP OUTPUT FORMATS
1682 KSC=KRI
IF(BPRM) 1684,1684,1683
1683 KSC=KRI
1684 WRITE(KOUT,1685) TILE (2),W(2),BPRM,T,FAF,HTIL,HIP,KSC,FAMOA(JC)
WRITE(KOUT,1686) TILE (2),W(2),BPRM,T,FAF,HTIL,HIP,KSC,FAMOA(JC)
1685 FORMAT(2A1M(4X),2F9.3,2F9.3,12,2A4,A2,F.4,2,2A4,A2,1M)
PUNCH 1686,
1686 WRITE(KOUT,1687) FAF,HTIL,HIP,KSC,FAMOA(JC)
1687 FORMAT(4X,2F9.3,2F9.3,12,2A4,A2,F.4,2,2A4,A2,1M)
GO TO 180
248 CONTINUE
IF(KR(1)) 170,170,108
168 CONTINUE
CALLS ANU,FORMAT 167,TILE A COMPRESSEU OUTPUT TO DE
C****HEAD AS IE,4,4E8.5,2E6.4,F.4,2,E7.5,E6.4,2E8.5,.....)
CALL SOUEE (P,10(1),4)
CALL SOUEE (W(2),10(4),4)
CALL SOUEE (BPRM,10(7),5)
CALL SOUEE (VKIM,10(10),4)
10(13)=FAF*100.
CALL SOUEE (T,10(14),5)
CALL SOUEE (ABS(WTR),10(17),4)
CALL SOUEE (HTIL,10(20),5)
HIPP=HG/1.8
CALL SOUEE (HIPP,10(23),5)
KRI=KRI*1.1
WRITE(KOUT,1675) 10,FAMOA(JC),FAMOB(JC),KRI,TILE
PUNCH 167, 10,FAMOA(JC), FAMOB(JC), KRI,TILE
KRI=KRI-1
W(2)=0.
167 FORMAT (14,A1,11,14,A1,11,16,A1,11,14,A1,11,
16,15,A1,11,14,A1,11,16,A1,11,16,A1,11,14,A1,11,
1675 FORMAT(3M (14,A1,11,16,A1,11,16,A1,11,14,A1,11,14,A1,11,
14,A1,11,16,A1,11,16,A1,11,14,A1,11,14,A1,11,
14,A1,11,16,A1,11,16,A1,11,14,A1,11,14,A1,11,
170 HIPP=HG/1.8
170 WRITE(KOUT,175)P,W(2),BPRM,T,FAF,HTIL,HIPP,KRI,FAMOA(JC),FAMOB(JC)
WTR
170 PUNCH 170, P,W(2),BPRM,T,FAF,HTIL,HIPP,KRI,FAMOA(JC),FAMOB(JC)
W(2)=0.
175 FORMAT(3M (F8.4,2F9.3,2F9.3,12,2A4,A2,E10.3,3M )
176 FORMAT ( F8.4,2F9.3,2F9.3,12,2A4,A2,E10.3)
271 IF(MT*KR(9)) 284,284,278
278 DO 279 L=1,M
279 PMR(L)=PMR(L)/AA
284 WRITE(KOUT,24) (L,PMR(L),L=1,MT)
272 WRITE(KOUT,22)
60 TO 105
273 IF(KR(5)) 274,274,274
274 IF(KR(5)) 277,275,275
275 WRITE(KOUT,9)
GO TO 105
276 WRITE(KOUT,16)
GO TO 105
277 WRITE(KOUT,13)
105 DO 110 I=1,N
IF(IFC(11)-1) 110,106,110

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```

108 IF (KR(1)) 110,109,109
109 VN(1)=VN(1)/VH*WTH(1)
110 VN(1) = VN(1) / P
111 IF (CV) 113,113,120
113 IF (KR(7)-1) 114,114,120
114 IF (N-60) 115,115,116
115 WRITE (KOUT,270) (FMOA(I),FMOB(I),VN(I),I=1,N)
116 GOTO 125
117 WRITE (KOUT,269) (FMOA(I),FMOB(I),VN(I),I=1,N)
210 FORMAT (1/3:5X7SPECIES3X8HOLE FR.2X) / (5X2A**E12.5,5X2A**E12.5,5X2A**E12.5,5X2A**E12.5,5X2A**E12.5)
269 FORMAT (1/5:5X7SPECIES3X8HOLE FR.2X) / (5X2A**E12.5,5X2A**E12.5,5X2A**E12.5,5X2A**E12.5)
GO TO 125
120 WRITE (KOUT,25) (FMOA(I),FMOB(I),VN(I),VC(I),Y(I),VLMK(I)),I=1,N)
125 DO 130 I=1,N
126 IF (IFC(I)-1) 130,128,130
128 IF (KR(6)) 130,129,129
129 VN(I)=VN(I)/WTH(I)*RH
130 VN(I) = VN(I) * P
135 IF (FL10) 280,280,140
140 F50L=1.-FL10
WRITE (KOUT,23) FMOA(MELT),FMOB(MELT),FL10,F50L
280 IF (ITS) 285,315,315
285 IF (KR(5)) 290,310,290
290 IF (KKJ+KR(3)) 300,295,300
295 KKJ = 1
KR(1) = 3
MODE = 3
KR(2)=1
KR(5)=3
*CHSO=0.
ITS=1
GAMF = GAM / (GAM - 1.)
C**** FIRST GUESS OF STAGNATION PRESSURE BEHIND SHOCK
P = (1. + ((GAM - 1.) / 2.) * (SOMAK)) * * GAME) * P
CALL ETIME
300 SXP=SHIP
310 RETURN
315 SHIP = SHIP
SIP = SSIP
RETURN
END

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SUBROUTINE PROPS
DIMENSION TT(1), RMO(1), CPBAR(1), SC(1), CAPC(1)
DIMENSION ZK(10),Z1(10),VK(10),V1(10)
COMMON/ACE1/GAME,X,REF,H,PCM,ACHSO,SOMAK,SRP
INCLUDE INCL.LIST
INCLUDE INC3.LIST
5 FORMAT(1/2TH DERIVATIVE PROPERTY OUTPUT,1/5TH CP-FROZEN CP-EQUILPROP
1 OLNH/OLNT OLNH/OLNP GAMMA/SE12.5)
10 FORMAT(1H115X4SHGRAPHITE SURFACE KINETICS (GASKET) SOLUTION 5X
1 2A,A2/)
15 FORMAT (4H1---50M----FOLLOWING OUTPUT NON-CONVERGENT-----
1- 2A,A2//)
ALFA(2)/A(1,1)
CSP = 1. / (A(1,1) * AA)
IF (MODE = 1) 40,45,46
40 CSP = CSP / 1.40,45,46
45 BETA = P * (A(2,2) - A(1,2) / A(1,1) * A(2,1)) - 1.
GAMP=1.-ALP
GAMP=1./((1.+BETA-1.9869/AA*GAMP/CSP*GAMP*P)
IF (KR(5)) 46,44,46
46 GAMGAMP
44 ITS=-1
MMNS.
CAPC(1) = 1.
I1 = 1
WM = AA / P
ISM = IS - 1
TT(11) = T * 1.8
RMO(11) = AA / (1.3146 * T)
CPBAR(11) = CPF
AISTR = 1.13
JARM NECESSARY SUMMATIONS
PMUZ = 0.
MTL = 0.
MTZ = 0.
PMUZ=0.
PMUJ = 0.
TMU3 = 0.
CPG=0.
CPGPR=0.
IER=1
IE=0
DO 5T K=1,15
VK(K)=0.
ZK(K)=0.
IF (VAT(K)-0.1) 51,52,52

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2 PROP
3 PROP
4 PROP
5 PROP
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PROP 148
PROP 149
PROP 150

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      PMUZ=PMUZ*VB
      MTZ=MTZ*VA*H(I)
      I(I)=I(I)+84*H(I)
      81 UO 77 K=1,15
      VK(K)=VK(K)+VN(I)*VNU(I,K)
      77 ZK(K)=ZK(K)+VA*VNU(I,K)
      84 FF=FF(I)+((I./GAMEX)
      840 FF=FF(I)+841*840*841
      841 VA=VA*(I./FF(I)
      VC=VN(I)*FF(I)
      85 PMUZ = PMUZ * VB
      TMUZ = TMUZ * VA
      CPTIL = VA * CP(I) * CPTIL
      HTIL = HTIL * VA * H(I)
      CPG=CPG*VN(I)*CP(I)
      HNH=HNH*VN(I)*H(I)
      AMUS = AMUS * VB / (W02 - VC * W07 )
      PHU6 = PHU6 * VA / (W04 - VC * W08 )
      IF (I=1)
      80 CPGPR=CPGPR*VN(I)*CP(I)
      VMU5 = AMU5 / AA
      VMU6 = (PMU6 * CPTIL / 1.9869 - 2.5 * TMU3) / P
      VMU2 = PMU2 / P
      VMU3 = TMU3 / PMU2
      HIZ=HIZ/PMU2*1.8
      UO 95 K=1,15
      VK(K)=VK(K)/AA*WM(K)
      95 ZK(K) = ZK(K)/PMUZ*WM(K)
      D0 100 I=1,15
      ZI(I)=0.
      VI(I)=0.
      UO 106 K=1,15
      VI(I) = VI(I) * CIJ(K,I) * VK(K) / WM(K) * MAT(I)
      100 ZI(I) = ZI(I) - CIJ(K,I) * ZK(K) / WM(K) * MAT(I)
      CPG=CPG/AA
      CPGPR=CPGPR/AA
      HNH=HNH/AA
      CPTIL = CPTIL / PMU2 * 1.8
      HTIL = HTIL / PMU2 * 1.8
      OMEGA = 1.87 * T / P * SORT(I) / OMEGA
      DBAR = 4.16E - 8 * T / P * VMU5 / VMU1
      TCONO = RHO(I) * OBAR * VMU5 / VMU1
      SC(I) = VMU5 / VMU2 * W4
      PR(I) = CPGPR/VMU6*VNU(I,1.9869*WM
      IF (IKJ) 107,107,101
      101 GAME=GAN-1.0

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PROP 51
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PROP 100

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      IEM=K
      52 IF(IFC(K)) 53,54,53
      53 IF(IRR(6)) 54,57,57
      54 IF(WTM(K)-0.1) 56,56,55
      55 ZK(K)=VN(K)/FF(K)
      56 VK(K)=VN(K)
      57 CONTINUE
      I=1
      UO 62 K=1,N
      IF(WTM(I)-0.1) 59,78,78
      MEH=H(I)
      WTE=WM(I)
      CPE=CP(I)
      - (I)=0.
      WTM(I)=0.
      CP(I)=0.
      IF(IK=IS) 62,62,60
      UO 61 K=1,15
      VK(K)=VK(K)+VN(I)*VNU(I,K)
      61 GO TO 62
      78 IF(IFC(I)) 62,79,62
      79 PMU1=PMU1*VN(I)*FF(I) ** (I./GAMEX)
      62 I=1
      VMU1=PMU1/P
      AMU5=0.
      PHU6=0.
      WZ=I*J*85
      W02=I*2 * A1STR/PMU1
      W07 = 0.244 * W02
      W05 = 0.32 * A1STR/PMU1
      W08 = W0K/PMU1-W05
      I=1
      UO 90 K=1,N
      IF(IFC(I)) 80,65,64
      64 IF(IRR(6)) 65,80,80
      65 IF(WTM(I)-0.1) 80,66,66
      66 VA=VN(I)/FF(I)
      IF(IEM) 71,73,67
      67 IF(IK=IS) 68,68,69
      UO TO 72
      69 CEJ=0.
      UO 70 K=1,15
      70 LEJ=CEJ*VNU(I,K)*CIJ(IEM,K)
      72 H(I)=H(I)-CEJ*ME
      CP(I)=CP(I)-CEJ*CP
      WTM(I)=WM(I)-CEJ*WTE
      73 VB=VB*WM(I)

```

```

SUBROUTINE HERA(Y,C,M,N,O,M,N,LS,IS)
DIRECT INVERSION PROCEDURE -- C IS REPLACED BY C00-1
DIMENSION U(16,1),S(16),C(16,1),L(16),S(16),LL(16),LS(1)
KOUT=0
NI=0
NP=N*NN
DO 11 I=1,NP
  LLL(I)=1
  IF(LS(I)) I13=I13+112
  L(I)=LS(I)
  GO TO 11
113 L(I)=1
11 CONTINUE
IX=-1
IF(I13=2) I11=I09+111
106 FORMAT(11M,11,1,13,5K,(30,13))
107 FORMAT(11M,11,C(11,J),J=1,13,6M),I=1,13,6M),I=1,13,15M)
IF(OR(1,2)) NP=NP+N
108 FORMAT(2I,11E10,3/1124,10E10,3)
109 WRITE(KOUT,107) NP,NN,N
IX=C
WRITE(KOUT,106) NP*(1),I=1,NP)
DO 110 I=1,N
  WRITE(KOUT,108) C(1,J),J=1,NP),(D(1,J),J=1,NN)
111 IS=1
C TRIANGULATE MATRIX
DO 15 I=1,N
  DO 160 M=1,NP
    SIM=ABS(C(1,M))
    IF(I18,16,16)
  18 IS=0
  50(1)=1
  GO TO 12
  C REDUCE ROW 1 BY PRECEDING ROWS
  16 DO 17 J=2,1
    K=L(J-1)
    DIV=C(1,K)
    IF(DIV) 161,17,161
  161 C(I,K)=0
    DIV=C(1,K)
    DIV=C(1,K)*I
    SIM=ABS(C(1,M))
  162 C(I,M)=C(1,M)-SIM/DIV
    IF(NNN) I7=I7+163
  163 DO 164 M=1,NNN
  164 U(1,M)=D(1,M)+U1VED(J-1,M)
  17 CONTINUE
  C SEEK MAXIMUM PIVOT
  12 DIV=C
    K=L(I)

```

```

SOMAKS(MC=MMH)/GAM=1.0065/TAHM
PSP(11)=GAME/2.0*SUMAKI/(1.0+GAME/2.0*ACHSA))P=(GAM/GAME)
IF(ABS(PSP)-1.0)-1.5=-1.0*10**10
102 IF(NKJ=10) 105,105,103
105 P=PPSP
AA=PEP
KKJ=KKJ-1
ITS=11
GO TO 125
104 KC=1
107 IF(INV) 47,47,106
106 WRITE(KOUT,15) TITLE
GO TO 49
47 IF(KR(10)/2.0*KR(7)+KR(2)+KR(3)) 49,49,48
48 WRITE(KOUT,10) TITLE
49 WRITE(KOUT,5) CPG, CSP, ALF, BETA, GAM
VMU12=VMU1*VMU2
IF(12X(11)=4) 109,109,109
MM=MM+1.0
PUNCH(11,MM),TT,MM,CSP,ALF,VMU,PR
111 CONTINUE
110 CONTINUE
112 ZPTIL=ZPTIL+1
113 FMTIL=FMTIL+1
114 FMTIL=FMTIL+1
115 FMTIL=FMTIL+1
116 FMTIL=FMTIL+1
117 FMTIL=FMTIL+1
118 FMTIL=FMTIL+1
119 FMTIL=FMTIL+1
120 FMTIL=FMTIL+1
121 FMTIL=FMTIL+1
122 FMTIL=FMTIL+1
123 FMTIL=FMTIL+1
124 FMTIL=FMTIL+1
125 FMTIL=FMTIL+1
END

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```

J=I
DO 13 J=1,N
  M(L,J)
  IF (ABS (C(I,M))-0.1V)13,13,121
  K=M
  J=J+1
13 CONTINUE
  S(1)=0.1V/S(K)
  L(J)=L(I)
  L(I)=K
  IF (S(1)-1.E-8) 131,131,14
  SINGULAR MATRIX RETURN
  S=1
131 WRITE (KOUT,132) 1*K
  S(K)=1.E+30
  GO TO 12
132 FORMAT(115A213)
  14 0.1V=C(I,K)
  C(I,K)=1.E-8
  K=LL(J)
  LL(J)=LL(I)
  LL(I)=K
  LL(K)=I
  C NORMALIZE M0
  IF (NMI) 143,143,141
  141 DO 142 J=1,NNN
  142 U(I,J)=0.1V/J/0.1V
  15 C(I,J)=C(I,J)/0.1V
  IF (IX) 152,150,152
  151 FORMAT(25H PIVOT ROW/COL/RES.RATIO 5(14,1M/13,1M/9,2,1M,))
  150 WRITE (KOUT,151) (1,LL(I),S(1),1=1,MP)
  C DIAGONALIZE MATRIX
  152 NMF=N-1
  DO 20 I=1,M
    K=LL(I)
    DO 20 J=1,I
      0.1V=C(I,K)
      IF (0.1V) 19,20,19
      C(I,K)=0.
      IF (NMI) 191,191,192
      192 DO 193 M=1,NNN
      193 U(I,M)=0.1V+M*0.1V*U(I,I,M)
      191 DO 201 M=1,NNP
      201 C(I,M)=C(I,M)+0.1V*C(I,I,M)
      20 CONTINUE
  C INTERCHANGE COLUMNS
  DO 30 I=1,MP
    J=I
    DO 30 TO 21
      21 J=LL(I)
      L(I)=I
      L(J)=J
      IF (15-J) 26,28,26
      26 DO 27 M=1,N
      27 C(M,I)=C(M,J)
      I=J
      GO TO 21
      25 IF (15-J) 26,28,26
      28 DO 29 M=1,N
      29 C(M,I)=5(M)
      15=0
      30 CONTINUE
      C INTERCHANGE ROWS
      DO 40 I=1,N
      1=I
      31 J=LL(I)
      LL(I)=I
      LL(J)=J
      IF (J-I) 32,40,32
      32 IF (15) 35,33,35
      33 DO 34 M=1,MP
      34 S(M)=C(I,M)
      C(I,M)=C(J,M)
      IF (NMI) 34,34,34,34
      341 DO 342 M=1,NNN
      342 U(I,M)=U(J,M)
      343 15=1
      I=J
      GO TO 31
      35 IF (15-J) 36,38,36
      36 DO 37 M=1,NNP
      37 C(I,M)=C(J,M)
      IF (NMI) 37,37,37,371
      371 DO 372 M=1,NNN
      372 U(I,M)=0.1V+M
      373 I=J
      GO TO 31
      38 DO 39 M=1,NNP
      39 C(I,M)=5(M)
      IF (NMI) 39,39,39,391
      391 DO 392 M=1,NNN
      392 O(I,M)=S(M)
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  MERA 100
  
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393 IS=2
40 CONTINUE
41 I=I+1
407 FORMAT(15H) ((C(I,J),J=1,13,12H), (D(I,J),J=1,13, 6H),I=1,13,15H)
409 WRITE(ROUT,=07) NP,NNH+N
410 WRITE(ROUT,=08) (C(I,J),J=1,MP), (D(I,J),J=1,NNH)
411 RETURN
END

      NERA 151
      NERA 152
      NERA 153
      NERA 154
      NERA 155
      NERA 156
      NERA 157
      NERA 158
      NERA 159
      NERA 160
      NERA 161

SUBROUTINE SCALE(MOE)
  DIMENSION CMFF(180)
  DIMENSION DY(1),UYA(180,1)
  INCLUDE INCL.LIST
  INCLUDE INCL3.LIST
  EQUIVALENCE(A(1),OY(1),OYA(1))
  CLIM = AMAX1(U,M(2) * W(3)) * 0.2 * WTU
  UY1L = 0.
  UY1G = 0.
  JUMP = P * I.E - 7
  BUMP = P * I.E - 4
  BULP = ALQ*(BUMP)
  15 CMF = 1.
  20 K = 0
  DO 35 J=2,15
    IF (IB(J) - IB(J - 1)) 25,30,35
  25 JA = IB(J)
    IB(J) = IB(J - 1)
    IB(J - 1) = JA
    K = 1
  GOTO 35
  30 IB(J) = 1000
  35 CONTINUE
  IF (K) 40,40,20
  *2 IB(15, * 1) = 1800
  M = IB(1)
  N = 1
  L = 15 * 2
  I = 0
  LL = I
  LL = N + K * (I)
  DO 320 IK=1,LLIM
    I = I + 1
  65 IF (IK - 15) 70,70,85
  70 SLAM(I) = U.
    IBC(I) = IFC(I)
    MNUS(I) = 0.
  75 UY1 = A(I * 2)
    IF (IFC(I) * 1) 315,80,80
  80 IF (IFC(I) * 1) 315,80,80
  85 IF (IFC(I) * 1) 115,90,90
  90 IF (IFC(I) * 1) 110,95,125
  95 VA = E(I) - IC(I) * A(I)
  DO 105 J=1,15
    IF (IBC(J)) 100,100,105
  100 VA = VA * VNU(I,J) * X(J * 2)

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```

105 CONTINUE
    UYI = VA
    GOTU 135
110 IF (IK - IE) 115,120,115
115 UYI = 0
    GOTU 315
120 IFC(I) = I
    UYI = X(IEX)
    GOTU 270
125 L = L + 1
    IF (L - IEX) 130,125,130
130 UYI = X(L)
    GOTU 270
135 DMG = DMG + V(I) * DYI * WTM(I)
    IF (IP(I)) 140,235,140
140 IF (IK - M) 145,185,145
145 IF (VN(I) - OUMP) 150,180,180
150 IF (MOE) 235,235,155
155 IF (DYI) 160,315,165
160 IF (VN(I) / BUMP - .9999995 - CMF * DYI) 315,315,170
165 IF (BUMP / VN(I) - 1 - CMF * DYI) 315,315,315
170 CMF = (VN(I) / BUMP - .9999995) / DYI
    GOTU 315
175 CMF = (BUMP / VN(I) - 1.) / DYI
    GOTU 315
180 IF (MOE) 245,245,190
185 M = M + 1
    M = I8(M)
190 IF (DYI) 195,315,200
195 IF (DYI * CMF * .999) 205,315,315
200 IF (DYI * CMF - 9.) 315,315,210
205 CMF = -.999 / DYI
    GOTU 315
210 CMF = 9. / DYI
    GOTU 315
215 IF (DYI * CMF - 2.303) 220,230,230
220 IF (DYI * CMF - 6.909) 225,315,315
225 CMF = 6.909 / DYI
    GOTU 315
230 CMF = 2.303 / DYI
    GOTU 315
235 IF (Y(I) - BULP * ABS(OYI) * CMF) 315,240,240
240 CMF = -(Y(I) - BULP) / ABS(OYI)
    GOTU 315
NON-PRESENT BASE
245 IF (KR(6)) 255,250,250
250 IF (T - IF(I) * .001) 315,255,255
255 IF (Y(I) * CMF * OYI - 0.1) 315,260,260
260 UUMI = (.1 - Y(I)) / DYI
    IF (OUMI - .001) 315,315,265

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265 CMF = DUMI
    GOTU 315
270 UMTL = OMTL * UYI * WTM(I)
    IF (YI) 275,315,290
275 IF (VN(I)) 290,290,280
280 IF (VN(I) * UYI * CMF) 285,290,290
285 CMF = -VN(I) / DYI * 1.00001
290 IF (KR(6)) 305,295,295
295 CLIP = ABS(CLIP / WTM(I))
    IF (ABS(CMF * DYI) - CLIP) 315,315,300
300 CMF = CLIP / ABS(OYI)
    GOTU 315
305 IF (ABS(CMF * DYI) - P) 315,315,310
310 CMF = P / ABS(OYI)
315 CMF(I) = CMF
320 DY(IK) = OYI
    IF (KR(6)) J22=321,321
321 RVL = MAX(1.,R/2.)
    CMF = AMINI(CMF * WTG / ABS(ABS(DMTL - DMG * WTG / RVL * WTL) / RVL - DMG * WTG / WTL) * CMF(I),E(I)),IFC(J),E(J),IFC(J),E(J))
    GOTU 315
322 IF (KR(7)) 325,325,330
325 ECRAT (1,2,4,8,16,32,64,128,256,512,1024,2048,4096,8192,16384,32768,65536,131072)
330 M = 1
335 WRITE(KOUT,325) (FAMDA(I),VN(I),Y(I),DYA(J,LL),CMF(I),E(I)),IFC(J),E(J),IFC(J),E(J))
340 WRITE(KOUT,350) (E(I),I=1,IS)
    WRITE(KOUT,350) (X(I),I=1,ISPO)
345 FORMAT(10I5)
350 FORMAT(8E12,4)
355 CONTINUE
    IF (X(I)) J70=415,370
370 A1 = X(I) * CMF
    ABX = ABS(A1)
375 CMF = .5 / ABX
    A1 = CMF * X(I)
380 IF (X1) 390,415,385
385 TM = TMAX
    X1 = AMINI(.2,X1)
    GOTU 395
390 TM = TMIN
    X1 = MAX(1 - 0.2,X1)
395 UTM = (TM - T) / (TM * X1)
    IF (DT4 - 1.) 400,410,410
400 CMF = UTM * CMF
    405 T = TM
    GOTU 415
410 T = T / (1. - X1)

```

```

415 AA = AA * EXP(CMF * X(2))
      RETURN
      END

SCAL 151
SCAL 152
SCAL 153

SUBROUTINE SQUEE (A,I,IOEE)
  DIMENSION I(1)
  DATA LUS,INUS/1M,IN-/
  I(1)=0
  I(3)=0
  H=ABS(A)*1.000001
  IF(ABS(A)-1.E-10) 7,7,1
1  IF(B-1.0) 3,2,2
2  H=B/10.
  I(3) = I(3)+1
  GO TO 1
3  IF(B-0.1) 4,5,5
4  H=B*10.
  I(3) = I(3)-1
  GO TO 3
5  I(1) = A*10.** (IOEE-I(3))*1.000001
  I(1(3))=0,7,7
6  I(2) = INUS
  GO TO 6
7  I(2) = LUS
8  I(3) = IABS(I(3))
  RETURN
  END

```

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1  SQUE
2  SQUE
3  SQUE
4  SQUE
5  SQUE
6  SQUE
7  SQUE
8  SQUE
9  SQUE
10 SQUE
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SUBROUTINE IEMR
DIMENSION DLNK(20),BC(30),FKFD(4,5),EAKD(4,3),EAKO(4,3)
DIMENSION LINE(32),IA(19)
INCLUDE INCL1.LIST
INCLUDE INCL3.LIST
COMMON/CARKIN/ KRK(10),ROUCH,MCC
DATA (FKFD(I,1),I=1,4)/12,5,12,5,0,77,1,0/, (EAKO(I,1),I=1,4)/
14,6E+4,4,6E+4,5,5E+4,0,0/, (EAKD(I,1),I=1,4)/0,0,0,0,0,0,0,0/,
2/(FKFD(I,2),I=1,4)/1,36E+4,1,36E+4,3,4E+6,1,0/, (EAKO(I,2),I=1,4)/
36,55E+4,5,5E+4,1,295E+5,0,0/, (EAKD(I,2),I=1,4)/0,0,0,0,0,0,0,0/,
4/(FKFD(I,3),I=1,4)/1,98E+5,1,98E+5,4,94E+7,1,0/, (EAKO(I,3),I=1,4)/
56,55E+4,6,55E+4,1,295E+5,10,0/, (EAKD(I,3),I=1,4)/0,0,0,0,0,0,0,0/,
DATA I1/3H 1,3H 2,3H 3,3H 4,3H 5,3H 6,3H 7,3H 8,3H 9,
*3H *3H -1,3H -2,3H -3,3H -4,3H -5,3H -6,3H -7,3H -8,3H -9/
DATA I17/3H -//
5 MODE = KR(I)
IF (I17) 20,10,20
10 WTC = 0.
WTL = 0.
IF (KR(I)) 17,17,11
11 IF (IFC(N,1) = 1) 13,18,13
18 IF (I * .001 - IFC(N,1)) 13,13,14
13 IFC(N,1) = 1
VN(N,1) = 0.
14 DO 16 K=1,15
16 VNU(N,1,K) = TO(K,3)
WTL = -VN(N,1)
17 DUM2 = 0.
SUMN = 0.
DO 15 I=1,15
RNU(I) = 0.
15 SLAM(I) = 0.
20 FMELT = 0.
FLIQ = 0.
SMELT = 0.
MELT = 1
THIN=TTMIN
THMAX=TTMAX
TFMAX = 500.
VA = ALOG(T / 3000.)
VB = T - 3000.
VC = (T * 3000.) / 2.
VO = T * 3000.
VE = VC / (VD * VD)
VT = 1.984 * T
IF (NCV) 35,35,25
25 PIN = P * 10.E - 3
WM = 20.
  
```

1 SWAP
 2 SWAP
 3 SWAP
 4 SWAP
 5 SWAP
 6 SWAP
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 9 SWAP

C
 C

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SUBROUTINE SWAP(A,B,SLA,SLB)
DIMENSION A(10,1),B(1),SLA(16,1),SLB(1)
DO 5 I=1,16
B(I)=SLB(I)
*C 5 J=1,10
5 A(I,J)=SLA(I,J)
RETURN
END
  
```

```

AA = P * WM
IF (MODE) 35,35,30
30 I = 3000.
35 CONTINUE
I = 1
40 DO 215 IK=1,N
  J=2
  IF (NCV) 55,55,45
  45 IF (IFC(I)) 55,50,55
  50 VN(I) = VN(I) * PIN
  Y(I) = ALOG(VN(I))
  55 CONTINUE
  IF (IFC(I) * I) 130,60,60
  60 IF (IFC(I)) 65,70,95
  65 IF (MODE - 1) 130,185,130
  70 IF (ITS) 140,15,130
  75 SUMN = SUMN * VN(I)
  DUM1 = WM(I) * VN(I)
  DTG = DTG * DUM1
  DUM2 = DUM2 * DUM1 / FF(I)
  IF (IK - 15) 80,80,85
  80 PNU5(I) = VN(I)
  IF (KR(6)) 130,82,92
  82 SLAM(I) = VN(I) / FF(I)
  85 DO 90 K=1,15
    DUM1 = VNU(I,K) * VN(I)
    IF (KR(6)) 90,87,90
    87 SLAM(K) = SLAM(K) * DUM1 / FF(I)
    90 PNU5(K) = PNU5(K) * DUM1
    IF (KR(6)) 130,130,92
    92 DO 93 K=1,15
      93 SLAM(K) = SLAM(K) * VLAM(I,K) * VN(I)
    95 IF (IFC(I) - 1) 100,100,130
    100 IF (ITS) 145,105,125
    105 IF (KR(6)) 120,110,110
    110 IF (I - IF(I) * .001) 115,115,120
    115 IFC(I) = - I
    VNU(I) = 0.
  GOTO 65
  120 WTL = WTL * VN(I) * WTM(I)
  125 IF (MODE - 1) 130,140,130
  130 THIN = AMAX(TMIN,IF(I))
  135 IFMAX = AMAX(TF(I),IFMAX)
  140 IF (I - ABS(TU(I))) 135,140,140
  140 CP(I) = HCL(I,J) * I * HCL(I,J) / (I * I)
  HCL(I,J) = HCL(I,J) * WM * (RC(I,J) * VC * RE(I,J) / VD)
  SB(I) = HCL(I,J) * HCL(I,J) * VA * VB * (RO(I,J) * RE(I,J) * VE)
  145 IF (MODE - 2) 190,150,150

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```

150 IF (IFC(I) - 1) 190,155,190
155 IF (TU(I,1)) 160,190,190
160 IF (I * TU(I,1)) 170,165,175
165 SMELT = - SB(I) - SMELT
  MELT = I
  IF (J - 2) 190,135,190
  170 IMAX = AMIN(IMAX, - TU(I,1))
  GOTO 190
  175 TMIN = AMAX(TMIN, - TU(I,1))
  190 TC(I) = - T(I) / RT
  VLNK(I) = TC(I) * SB(I) / I.9869
  IF (IK - 15) 195,195,200
  195 BLNK(I) = VLNK(I)
  IFC(I) = IFC(I)
  BC(I) = TC(I)
  GOTO 215
  200 DO 210 K=1,15
    IF (IC(K) * I) 210,245,205
  205 VLNK(I) = VLNK(I) - VNU(I,K) * BC(K)
  TC(I) = TC(I) - VNU(I,K) * BC(K)
  210 CONTINUE
  215 I=I+1
  NCV = -I*85(NCV)
  IF (MODE - 1) 230,220,230
  220 IF (IFMAX - I) 225,230,230
  225 I = IFMAX
  226 RTE(KOUT,228)
  228 STOP
  230 IF (ITS) 355,235,355
  235 AA = P * WM
  NCV = 0
  240 FORMAT(8F10.6)
  245 FORMAT(2I3)
  250 FORMAT(3E10.4)
  255 IF (KR(9)-5) 335,255,255
  257 IF (KR(8)-4) 257,256,256
  257 DO 258 I=1,15
    HNU(I,1) = 0.0
  258 HNU(I,1) = 0.0
  259 HNU(I,1) = 1.0
  HNU(1,1) = 2.0
  HNU(2,1) = 2.0
  GO TO 263
  261 HNU(I,1) = 1.0
  HNU(2,1) = 2.0
  HNU(3,1) = 1.0

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• STOP •

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256  GO TO 263
      DO 262 I=1,4
        PHU(I,1)=1.0
      DO 262 J=1,15
        PHU(J,1)=0.0
      PHU(3,1)=0.0
      PHU(3,1)=1.0
      PHU(2,1)=1.0
      PHU(1,1)=1.0
      PHU(4,1)=1.0
      PHU(5,2)=1.0
      PHU(4,2)=2.0
      PHU(2,3)=1.0
      PHU(5,3)=2.0
      PHU(3,3)=3.0
      PHU(3,3)=2.0
      PHU(3,4)=1.0
      PHU(4,4)=1.0
      PHU(1,4)=1.0
      PHU(2,4)=1.0
      PHU(2,4)=1.0
      263  IF (KRR(17)-2) 266,264,269
      266  IF (KRR(17)-2) 267,264,267
      264  NICK=KRR(4)
      264  IF (KRR(16)-4) 268,269,269
      268  MT=1
      271  FRF(1)=FRF(2)+NICK)/ROUCH
      EAK(1)=EAKU(2)+NICK)
      EAK(1)=EAKU(2)+NICK)
      GO TO 321
      272  FRF(1)=FRF(3)+NICK)/ROUCH
      EAK(1)=EAKU(3)+NICK)
      EAK(1)=EAKU(3)+NICK)
      GO TO 321
      269  MT=4
      273  I=1,4
      FRF(1)=FRF(1)+NICK)/ROUCH
      EAK(1)=EAKU(1)+NICK)
      273  EAK(1)=EAKU(1)+NICK)
      GO TO 321
      267  IF (KRR(16)-4) 2672,2671,2672
      2671  MT=4
      GO TO 2673
      2672  DO 260 M=1,MT
      HEAD(KIN,250) FRF(M),EAK(M),EAK(M)
      260 FRF(M)=FRF(M)/ROUCH
      265  FORMAT (/JX,7HKINETIC)
      270  FORM. 3K,11HREACTION=--,17,9110/(11K,10110))
      THER0201  275  FORMAT (/JX,8MREACTANT)
      THER0202  280  FORMAT (5X,12HCOCFFI(1,15))
      THER0203  285  FORMAT (11X,24X,2X,40A3)
      THER0204  286  FORMAT(11M,REACTION#,#013)
      THER0205  287  FORMAT(11X,40A3)
      THER0206  290  FORMAT (/JX,7MRODUCT)
      THER0207  295  FORMAT (/JX,12MPRE-EXPONENT)
      THER0208  300  FORMAT(5X,8HFACTOR,4X,1P10E11,3/(15X,1P10E11,3))
      THER0209  305  FORMAT (/JX,10HACTIVATION)
      THER0210  310  FORMAT(5X,8HENERGY,4X,1P10E11,3/(15X,1P10E11,3)
      THER0211  315  FORMAT(73K,11HTEMPERATURE)
      THER0212  320  FORMAT(5X,8HEXPONENT,2X,1P10E11,3/(15X,1P10E11,3))
      THER0213  121  WRITE(KOUT,275)
      THER0214  WRITE(KOUT,280)
      THER0215  WRITE(KOUT,286) (M,M=1,MT)
      THER0216  WRITE(KOUT,287) (1AY,M=1,MT)
      THER0217  WRITE(KOUT,285)
      THER0218  DO 325 I=1,15
      THER0219  DO 324 M=1,MT
      THER0220  IY=1FIX(PHU(I,M))
      THER0221  IF (IY.EQ.0) IY=10
      THER0222  IF (IY.LT.0) IY=10+JABS(IY)
      THER0223  324  LINE(M)=IX(1Y)
      THER0224  WRITE(KOUT,285) FAMDA(1),FAMDB(1),LINE(M),M=1,MT)
      THER0225  WRITE(KOUT,288)
      THER0226  WRITE(KOUT,286) (M,M=1,MT)
      THER0227  WRITE(KOUT,287) (1AY,M=1,MT)
      THER0228  WRITE(KOUT,285)
      THER0229  DO 329 I=1,15
      THER0230  DO 329 M=1,MT
      THER0231  IY=1FIX(PHU(I,M))
      THER0232  IF (IY.EQ.0) IY=10
      THER0233  IF (IY.LT.0) IY=10+JABS(IY)
      THER0234  329  LINE(M)=IX(1Y)
      THER0235  WRITE(KOUT,285) FAMDA(1),FAMDB(1),LINE(M),M=1,MT)
      THER0236  WRITE(KOUT,285)
      THER0237  WRITE(KOUT,270) (M,M=1,MT)
      THER0238  WRITE(KOUT,295)
      THER0239  WRITE(KOUT,300) (FKF(M),M=1,MT)
      THER0240  WRITE(KOUT,303)
      THER0241  WRITE(KOUT,310) (EAK(M),M=1,MT)
      THER0242  WRITE(KOUT,315)
      THER0243  WRITE(KOUT,320) (EAK(M),M=1,MT)
      THER0244  335  SUMN = SUMN / P
      THER0245  SUMN = ALOU(SUMN)
      THER0246  FFF = WTG / SUM2
      THER0247  WTG = WTG / SUMN
      THER0248  WIL = WIL / SUMN
      THER0249  DO 340 I=1,15

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        PMUS(I)=PMUS(I)/SUMM
340 SLAM(I) = SLAM(I) / SUMM * FFF
      MSN(2)=M(3)
      SUMC = 1.0
      IF (KRALP * KR(2)) 355,358,345
345 IF (WTL / WIG - WS) 355,358,350
350 SUMC = WTL / (WIG * WS)
      WTL = WTL / SUMC
355 RETURN
      END

      SUBROUTINE ZIPI
      INCLUDE INCL.LIST
      COMMON/ALF/GAME,X,NEX,M,PCML,ACMSU,SONAK,SAP
      INCLUDE INCL.LIST
      COMMON/CARKIN/ KR(10),ROUCH,NCC
      COMMON/CONC/NO/ Z,GAMER,WR(J)
      S FORMAT (10I1,6F10.5,2A4,A2)
      I0 FORMAT (2I,J)
      I5 FORMAT (8F10.5)
      CALL ETIME
      MFF = 0
      YTMIN=300.
      YTMAX=20890.
      Z = 0.0
      PR = 0.0
      KK,J=0
      PSV=0
      II=0
      IF (IITS * J) 20,25,20
20 GAMEX=0.0606667
      M(1) = 1.0
      M(2)=0.
      M(3)=0.
      MY=0
      MA = - 1
      NCV = 0
      MOAT = 0
      WM = 20.
      Y=300.
      MIP = 0.
      SIP = 0.
      KR(10) = 0
25 ITS = 0
      IDC = 1
      KRALP = 0
      KRJ = 0
      KS = 1.0
      KR=KR(I)
      KR=KR(I)
      CALL KINEN
      KR(1) = KM(6)
      WRITE(KOUT,140)FILE,WR
      KR(8) = 0
      I00 FORMAT (1MVA35GHMHPITE SURFACE KINETICS (OASHET) 2A4A2.SKI011)
      KRZZ = 0
      TBT = 501.
      KR(4) = KR(4) - 1
      ZIPI
  
```

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1 ZIPI
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48 ZIPI
49 ZIPI
50 ZIPI
  
```

```

IF (KR(4)) 150,J45,145
145 IF (KR(6)) 155,155,150
150 KR(6) = KR(6) - 1
155 IF (KR(7)) 157,157,156
156 KR(7) = 5 * (KR(7) - 1) + 1
157 IF (ABS(WR(1)) * ABS(WR(2)) * ABS(WR(3))) * ABS(WR(4)) 165,165,160
160 W(1)=WR(1)
W(2)=WR(2)
W(3)=WR(3)
KRALP = 1
165 CONTINUE
216 IF (KR(1) = 5) 220,215,220
215 KR(1) = 1
KR(8) = 1
220 MODE = KR(1)
KRALP=KRALP+ABS(KR(8))+ABS(KR(4)-KR(4))
SVA = 0
SVB = 0
225 IFRZ = 0
IF (MODE = 8) 235,230,235
230 STOP
235 IF (GAMER) 240,275,240
240 GAMESTON(AHAXI(ABS(GAMER)),0,0001),GAMER)
IF (KR(3)) 250,250,245
245 IF (KR(3)-9) 272,250,272
250 J=1
DO 270 I=1,N
FF(J) = FF(J) + (GAMER/GAMEX)
270 J=J+1
272 GAMEX=GAMER
275 IF (Z) 280,276,280
276 IF (MODE=4) 277,311,430
277 IF (MODE=3) 430,278,430
278 IF (KP(5)) 430,430,279
279 SIP=51P
GO TO 430
280 IF (MODE = 1) 285,285,300
285 T = Z
290 T = - T
295 CONTINUE
GOTO 430
300 IF (MODE = 2) 430,415,305
305 IF (MODE=4) 420,310,420
310 T = Z
311 MODE = 2
KKJ=-1
KR(5)=MAX(KR(5),1)
KR(1) = 2
21PI 51
21PI 52
21PI 53
21PI 54
21PI 55
21PI 56
21PI 57
21PI 58
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21PI 60
21PI 61
21PI 62
21PI 63
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21PI 138
21PI 139
21PI 140
21PI 141
21PI 142
21PI 143
21PI 144
21PI 145
21PI 146
21PI 147
21PI 148
21PI 149
21PI 150
HEAD(KIN,315)KVM,UK,MTR,MSK,MMOR,SAL,PR1
MMOR=9999.
PRI=9999.
315 FORMAT (1,FY,4,5F10.4)
IF (UR) 325,330,320
320 SVI = UN
GOTO 330
325 SVI = VEL
330 IF (MTR) 345,340,335
335 MCH = MTR / 1.8
340 IF (MSR) 345,360,345
345 IF (MSR * 9999.) 350,355,350
350 SHI = MSR / 1.8
GOTO 360
355 SHI = MIP
360 IF (MMOR) J70,375,365
365 SRI = MMOR
GOTO 375
370 SRI = 240
375 IF (PRI) 385,390,380
380 SPI = PRI
GOTO 390
385 SPI = P
390 GOTO(395,400,405),KVM
395 SVI = SQRT( (MCH - SHI) = 90103.)
GOTO 410
400 MCH = SHI * SVI / 90108. * SVI
GOTO 410
405 SHI = MCH - SVI / 90108. * SVI
410 SAI = SAI / 57.29577
SVB = SVA * 2. / 1.9869
SVC = (SVI * COS(SAI)) * 2. / 90108. * SHI
SVD = SPI * SVB / (1.3146 * SRI)
P = SVD
GOTO 430
415 MIP = Z
GOTO 430
420 IF (SIP * 9999.) 430,425,430
425 SIP = SCH
SOMAK = 0
430 IF (PRI) 431,440,435
431 KRJ=1
ACHSOPR=PK
GAME=GAM-1.0
PRPSY=(1.0+GAME/2.*SOMAK)/(1.0+GAME/2.*ACHSQ))*(GAM/GAME)
KR(5)=1
435 P = PR

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440 AA=PMW
RETURN
END

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ZIPI 151
ZIPI 152
ZIPI 153
ZIPI 154

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C

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MEAL NFIA(1),NFIR(1),FF,IN(1),TAU(30,30)
EQUIVALENCE (NFIA(1),A(1)),(NFIR(1),A(5)),(FF,IN(1),A(10)),
(FAU(1),A(15))
DIMENSION IF(150),CIJ(150,1)
DIMENSION A(1),VLAM(150,1)

```

C

```

COMMON /SPECIE/ FAMA(150),FAMU(150),HB(150,2),HC(150,2),
RU(150,2),RE(150,2),RF(150,2),TU(150,2),VN(150),
Y(150),YK(150),VMU(150,3),FF(150),FC(150),
IP(150),CP(150),ML(150),SB(150),FC(150),VLAM(150),
E(150),LAMI(150),GAMK(10,1)

```

C

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COMMON /PARAM1/ KIN,KOUT,JAN,MUL,MAB,IBC,N,KKA(3),KR(10),TILE(3),
TTRIN,TTMAX,VISC,PR(1)

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C

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COMMON /PARAM2/ WM,SCM,RHO,VEL,FI,MFF,FFA,IS,ISP,PT,SIP,MIP,
EL,ENL,FLIG,NG,IFL,ISQ,KNALP,CP,IRE,IER,AA,ITS,
IM,EL,IT,MODE,MMELT,SMELT,THAX,THM,MMELT,SUMH,
JUML,JC,HG,CPG,SLA,SVB,SVS,SV0,SUMC,NIC,SAI,
VMACH,KRZZ,SPI,GAM,THI,MA,DMCHI,MCH,MCV,THY,
IFRZ,NOAT,SRI,IAG,SVI,KKJ,IKC,INAG,SHI,NOATO,
SAZ,FFF,MS,RV,CMF,VA,NOS,DUML,DUIM2,EP,IFC,JC,
ISP2,NISQ,VMU2,NIL

```

C

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COMMON /ARMAYS/ A(32,32),W(3),HC(50),KG(50),ZKE(30),
TLO(10),OMILO(10),MAL,PL(30),EM(30),ALPL(30),
UAM(30),GAMF(30),TQ(30,3),TK(30,3),MAT(30),
IR(30),I0AT(30),KAT(30),UM(30,30),ECL(30)
EQUIVALENCE (TU(15),TF(1)),(VMU(1),C(1)),

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C

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COMMON /KINEMIA/ MT,FKF(50),EAK(50),EXK(50),PMU(30,50),RMU(30,50),
PMH(50)

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C

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EQUIVALENCE (H(1),A(1)),(GAMK(1),VLAM(1))
END

```

C

```

COMMON /DIFFER/ IC(31),ALPT(30),C(30),SORCE(8),NA(2),IM(30),
IL,KK,J,VINT,YINT,JAT(10),LHM(30,30),FAMA(30),
FAMU(30),KPHA(2)

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C

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DIMENSION AFA(30),ATB(30),ATC(30)
EQUIVALENCE (TU(1),ATA(1)),(TU(31),ATB(1)),(U(6),ATC(1))
END

```

C

```

COMMON /DIFFER/ IR(1),FMU(30),PMUS(30),SLAM(30),BE(30),BY(30),
IBC(30),JJ(30),SLB(32),SLA(32,32)
END

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INCL 1
INCL 2
INCL 3
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INCL 7
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INCL 33
INCL 34
INCL 35

INCL 1
INCL 2
INCL 3
INCL 4
INCL 5
INCL 6
INCL 7

INCL 1
INCL 2

DATA (ALPTX(1),1521,1680)/
ALPT 95
ALPT 96
ALPT 97
ALPT 98
ALPT 99
ALPT 100
ALPT 101
ALPT 102
ALPT 103
ALPT 104
ALPT 105
DATA (ALPTX(1),1681,1840)/
ALPT 106
ALPT 107
ALPT 108
ALPT 109
ALPT 110
ALPT 111
ALPT 112
ALPT 113
ALPT 114
DATA (ALPTX(1),1841,2000)/
ALPT 115
ALPT 116
ALPT 117
ALPT 118
ALPT 119
ALPT 120
ALPT 121
ALPT 122
ALPT 123
ALPT 124
ALPT 125
ALPT 126
ALPT 127
ALPT 128
ALPT 129
DATA (ALPTX(1),2001,2160)/
ALPT 130
ALPT 131
ALPT 132
ALPT 133
ALPT 134
ALPT 135
ALPT 136
ALPT 137
ALPT 138
ALPT 139
ALPT 140
ALPT 141
ALPT 142
ALPT 143
ALPT 144
ALPT 145
ALPT 146
ALPT 147
ALPT 148

DATA (ALPTX(1),161,300)/
ALPT 199
JAY 1
JAY 2
JAY 3
JAY 4
JAY 5
JAY 6
JAY 7
JAY 8
JAY 9
JAY 10
JAY 11
JAY 12
JAY 13
JAY 14
JAY 15
JAY 16
JAY 17
JAY 18
JAY 19
DATA (ALPTX(1),301,440)/
JAY 20
JAY 21
JAY 22
JAY 23
JAY 24
JAY 25
JAY 26
JAY 27
JAY 28
JAY 29
DATA (ALPTX(1),441,600)/
JAY 30
JAY 31
JAY 32
JAY 33
JAY 34
JAY 35
JAY 36
JAY 37
JAY 38
JAY 39
JAY 40
JAY 41
JAY 42
JAY 43
JAY 44
JAY 45
JAY 46
JAY 47
JAY 48
DATA (ALPTX(1),601,760)/
JAY 49
JAY 50
JAY 51
JAY 52
JAY 53

2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/63	4M				SORC	71
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/66	4M				SORC	72
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/65	4M				SORC	73
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/65	4M				SORC	74
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/63	4M				SORC	75
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	76
DATA (SORC(1), 1= 609, 760) //									
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/63	4M				SORC	77
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/63	4M				SORC	78
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/68	4M				SORC	79
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/63	4M				SORC	80
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/63	4M				SORC	81
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/65	4M				SORC	82
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/65	4M				SORC	83
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/63	4M				SORC	84
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/63	4M				SORC	85
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/63	4M				SORC	86
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/63	4M				SORC	87
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/69	4M				SORC	88
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/61	4M				SORC	89
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/66	4M				SORC	90
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/61	4M				SORC	91
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	92
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	93
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/68	4M				SORC	94
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	95
DATA (SORC(1), 1= 761, 912) //									
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	96
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	97
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/69	4M				SORC	98
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	99
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	100
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/67	4M				SORC	101
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	102
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	103
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/68	4M				SORC	104
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/61	4M				SORC	105
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	106
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/69	4M				SORC	107
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/70	4M				SORC	108
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/70	4M				SORC	109
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	110
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/70	4M				SORC	111
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/68	4M				SORC	112
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/69	4M				SORC	113
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/61	4M				SORC	114
DATA (SORC(1), 1= 913, 1064) //									
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	115
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/64	4M				SORC	116
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/60	4M				SORC	117
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/63	4M				SORC	118
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/60	4M				SORC	119
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/61	4M				SORC	120
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/69	4M				SORC	121
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	12-4M/67	4M				SORC	122
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/65	4M				SORC	123
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/65	4M				SORC	124
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	9-4M/65	4M				SORC	125
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	3-4M/61	4M				SORC	126
2HJA-4HNAF	6HTAPE-4M	7/7-4M1	6-4M/68	4M				SORC	127

AMOA 17	AMOB 1	AMOB 20	AMOB 39
AMOA 18	AMOB 2	AMOB 21	AMOB 40
AMOA 19	AMOB 3	AMOB 22	AMOB 41
AMOA 20	AMOB 4	AMOB 23	AMOB 42
AMOA 21	AMOB 5	AMOB 24	AMOB 43
AMOA 22	AMOB 6	AMOB 25	AMOB 44
AMOA 23	AMOB 7	AMOB 26	AMOB 45
AMOA 24	AMOB 8	AMOB 27	AMOB 46
AMOA 25	AMOB 9	AMOB 28	AMOB 47
AMOA 26	AMOB 10	AMOB 29	AMOB 48
AMOA 27	AMOB 11	AMOB 30	AMOB 49
AMOA 28	AMOB 12	AMOB 31	AMOB 50
AMOA 29	AMOB 13	AMOB 32	AMOB 51
AMOA 30	AMOB 14	AMOB 33	AMOB 52
AMOA 31	AMOB 15	AMOB 34	AMOB 53
AMOA 32	AMOB 16	AMOB 35	AMOB 54
AMOA 33	AMOB 17	AMOB 36	
AMOA 34	AMOB 18	AMOB 37	
AMOA 35	AMOB 19	AMOB 38	
AMOA 36			
AMOA 37			
AMOA 38			

55	0-2-2533E+5	-1.9187E+5	-1.9187E+5	-2.6147E+5	-2.6147E+5	1.0240E+4	1.0240E+4	5/RA	112
56	0-2-8300E+5	-4.5522E+4	-4.5522E+4	-2.8000E+5	-2.8000E+5	-6.0064E+5	-6.0064E+5	5/RA	113
57	DATA IRBA(11)	1.1111E+7	1.1111E+7	2.1269E+4	2.1269E+4	3.0390E+4	3.0390E+4	4/RB	1
58	0-1-8100E+4	2.2420E+4	2.2420E+4	1.4448E+4	1.4448E+4	4.8480E+4	4.8480E+4	4/RB	2
59	0-1-0970E+4	2.1986E+4	2.1986E+4	2.1122E+4	2.1122E+4	1.3525E+4	1.3525E+4	4/RB	3
60	0-3-8400E+4	2.6476E+4	2.6476E+4	3.1054E+4	3.1054E+4	3.1837E+4	3.1837E+4	4/RB	4
61	0-5-0400E+4	5.0400E+4	5.0400E+4	2.7258E+4	2.7258E+4	3.1837E+4	3.1837E+4	4/RB	5
62	0-2-1580E+4	2.1580E+4	2.1580E+4	1.3478E+4	1.3478E+4	2.4165E+4	2.4165E+4	4/RB	6
63	0-1-9610E+4	1.9610E+4	1.9610E+4	3.7052E+4	3.7052E+4	5.2174E+4	5.2174E+4	4/RB	7
64	0-2-7000E+3	2.7000E+3	2.7000E+3	2.7052E+4	2.7052E+4	3.7052E+4	3.7052E+4	4/RB	8
65	0-1-4100E+5	1.4100E+5	1.4100E+5	5.1753E+4	5.1753E+4	2.3425E+4	2.3425E+4	4/RB	9
66	0-1-7540E+5	1.7540E+5	1.7540E+5	4.8162E+4	4.8162E+4	2.3425E+4	2.3425E+4	4/RB	10
67	0-4-1000E+4	4.1000E+4	4.1000E+4	1.6238E+5	1.6238E+5	3.6353E+4	3.6353E+4	4/RB	11
68	0-4-1000E+4	4.1000E+4	4.1000E+4	3.300E+4	3.300E+4	3.6353E+4	3.6353E+4	4/RB	12
69	0-1-6038E+5	1.6038E+5	1.6038E+5	5.0433E+4	5.0433E+4	3.7931E+4	3.7931E+4	4/RB	13
70	0-2-5900E+5	2.5900E+5	2.5900E+5	5.1151E+4	5.1151E+4	3.7931E+4	3.7931E+4	4/RB	14
71	0-2-9000E+3	2.9000E+3	2.9000E+3	3.7345E+4	3.7345E+4	3.7931E+4	3.7931E+4	4/RB	15
72	0-4-7500E+5	4.7500E+5	4.7500E+5	2.2708E+4	2.2708E+4	3.5728E+4	3.5728E+4	4/RB	16
73	0-2-3800E+4	2.3800E+4	2.3800E+4	4.5714E+4	4.5714E+4	6.0567E+4	6.0567E+4	4/RB	17
74	0-1-8340E+4	1.8340E+4	1.8340E+4	3.6552E+4	3.6552E+4	6.0567E+4	6.0567E+4	4/RB	18
75	0-1-5800E+4	1.5800E+4	1.5800E+4	7.9067E+4	7.9067E+4	2.3372E+4	2.3372E+4	4/RB	19
76	DATA IRBA(11)	1.1111E+7	1.1111E+7	2.3023E+4	2.3023E+4	7.9958E+4	7.9958E+4	4/RB	20
77	0-4-3000E+4	4.3000E+4	4.3000E+4	5.0000E+3	5.0000E+3	6.3955E+4	6.3955E+4	4/RB	21
78	0-5-8000E+5	5.8000E+5	5.8000E+5	3.4220E+5	3.4220E+5	1.6129E+5	1.6129E+5	5/RB	22
79	0-1-8280E+5	1.8280E+5	1.8280E+5	5.7000E+4	5.7000E+4	1.7637E+5	1.7637E+5	5/RB	23
80	0-1-6400E+4	1.6400E+4	1.6400E+4	1.9400E+4	1.9400E+4	3.1609E+5	3.1609E+5	5/RB	24
81	0-5-3000E+4	5.3000E+4	5.3000E+4	3.0700E+5	3.0700E+5	2.3994E+4	2.3994E+4	4/RB	25
82	0-1-1520E+5	1.1520E+5	1.1520E+5	2.3000E+4	2.3000E+4	3.4731E+4	3.4731E+4	4/RB	26
83	0-1-3900E+5	1.3900E+5	1.3900E+5	2.7000E+5	2.7000E+5	2.2298E+4	2.2298E+4	4/RB	27
84	0-5-7000E+4	5.7000E+4	5.7000E+4	2.740E+5	2.740E+5	3.213E+4	3.213E+4	4/RB	28
85	0-1-3000E+4	1.3000E+4	1.3000E+4	1.7000E+5	1.7000E+5	7.6928E+4	7.6928E+4	4/RB	29
86	0-9-6000E+4	9.6000E+4	9.6000E+4	1.4000E+5	1.4000E+5	1.6653E+5	1.6653E+5	4/RB	30
87	0-3-0000E+4	3.0000E+4	3.0000E+4	2.970E+5	2.970E+5	6.5474E+4	6.5474E+4	4/RB	31
88	0-3-0000E+4	3.0000E+4	3.0000E+4	4.000E+4	4.000E+4	6.9977E+4	6.9977E+4	4/RB	32
89	0-1-1840E+5	1.1840E+5	1.1840E+5	9.6000E+4	9.6000E+4	3.7024E+4	3.7024E+4	4/RB	33
90	0-3-9000E+4	3.9000E+4	3.9000E+4	2.4500E+5	2.4500E+5	4.9935E+4	4.9935E+4	4/RB	34
91	0-1-1000E+1	1.0000E+1	1.0000E+1	2.4500E+5	2.4500E+5	6.2370E+4	6.2370E+4	4/RB	35
92	0-9-0000E+0	9.0000E+0	9.0000E+0	5.350E+5	5.350E+5	4.6389E+4	4.6389E+4	4/RB	36
93	0-0-0000E+0	0.0000E+0	0.0000E+0	1.5120E+5	1.5120E+5	5.9073E+4	5.9073E+4	4/RB	37
94	0-1-8960E+5	1.8960E+5	1.8960E+5	3.0170E+5	3.0170E+5	5.8116E+4	5.8116E+4	4/RB	38
95	DATA IRBA(11)	1.5711E+7	1.5711E+7	5.6383E+4	5.6383E+4	1.0933E+5	1.0933E+5	5/RB	39
96	0-1-4200E+4	1.4200E+4	1.4200E+4	7.5180E+4	7.5180E+4	5.0276E+4	5.0276E+4	4/RB	40
97	0-8-5684E+4	8.5684E+4	8.5684E+4	2.1650E+5	2.1650E+5	5.3539E+4	5.3539E+4	4/RB	41
98	0-3-0100E+5	3.0100E+5	3.0100E+5	2.8433E+5	2.8433E+5	7.9427E+4	7.9427E+4	4/RB	42
99	0-6-1881E+5	6.1881E+5	6.1881E+5	1.5590E+5	1.5590E+5	5.1244E+4	5.1244E+4	4/RB	43
100	0-5-6900E+2	5.6900E+2	5.6900E+2	7.200E+4	7.200E+4	6.0342E+4	6.0342E+4	4/RB	44
101	0-5-0030E+5	5.0030E+5	5.0030E+5	0.0000E+0	0.0000E+0	5.1958E+4	5.1958E+4	4/RB	45
102	0-3-7300E+1	3.7300E+1	3.7300E+1	2.9928E+5	2.9928E+5	2.4128E+4	2.4128E+4	4/RB	46
103	0-1-4060E+5	1.4060E+5	1.4060E+5	2.956E+5	2.956E+5	6.7080E+4	6.7080E+4	4/RB	47
104	0-1-1584E+5	1.1584E+5	1.1584E+5	3.394E+4	3.394E+4	2.4452E+4	2.4452E+4	4/RB	48
105	0-3-300E+1	3.300E+1	3.300E+1	1.4745E+5	1.4745E+5	3.7066E+4	3.7066E+4	4/RB	49
106	0-2-540E+1	2.540E+1	2.540E+1	3.882E+5	3.882E+5	8.3389E+4	8.3389E+4	4/RB	50
107	0-8-0340E+5	8.0340E+5	8.0340E+5	1.137E+6	1.137E+6	3.2413E+4	3.2413E+4	4/RB	51
108	0-3-3710E+5	3.3710E+5	3.3710E+5	1.137E+6	1.137E+6	3.6145E+4	3.6145E+4	4/RB	52
109	0-5-3900E+5	5.3900E+5	5.3900E+5	1.6298E+6	1.6298E+6	6.6377E+4	6.6377E+4	4/RB	53
110	0-5-8650E+5	5.8650E+5	5.8650E+5	1.7000E+3	1.7000E+3	6.1598E+4	6.1598E+4	4/RB	54
111	0-5-8650E+5	5.8650E+5	5.8650E+5	1.7000E+3	1.7000E+3	3.6281E+4	3.6281E+4	4/RB	55

DATA (RD(1))=3434567/
1 7925E-4 1.681E-4 6.227E-4 1.866E-4 5.031E-4 4.966E-4 4 RD
2 1.823E-4 1.372E-4 1.505E-4 1.875E-4 2.420E-4 1.793E-4 5 RD
3 2.691E-4 3.952E-4 3.172E-4 2.817E-4 1.838E-4 1.841E-4 4 RD
4 1.5897E-4 1.6295E-4 2.1221E-4 1.9830E-4 1.5668E-4 3.9991E-4 4 RD
5 3.2487E-4 3.2372E-4 7.0295E-5 3.2054E-4 2.7136E-4 5.2336E-4 4 RD
6 3.5447E-4 4.4671E-4 3.8295E-4 3.299E-4 1.091E-4 2.8451E-4 4 RD
7 5.4716E-4 2.8051E-5 5.6255E-4 1.3392E-4 1.732E-4 3.8516E-4 5 RD
8 2.0588E-4 1.3766E-4 2.792E-4 1.44E-4 2.8758E-4 3.9299E-4 5 RD
9 5.0546E-4 1.3766E-4 2.937E-4 3.647E-4 1.9484E-4 3.570E-4 5 RD
10 9.1168E-4 3.6452E-5 2.9645E-4 3.387E-4 4.4887E-4 3.8802E-4 5 RD
11 8.9131E-4 7.431E-4 9.0743E-5 8.695E-4 2.1001E-4 9.1818E-4 5 RD
12 1.3817E-3 1.0181E-4 8.978E-4 7.765E-4 8.978E-4 8.978E-4 5 RD
13 3.886E-4 3.482E-5 1.170E-3 1.622E-3 2.852E-3 3.697E-4 5 RD
14 8.693E-4 6.6591E-5 2.0384E-4 2.695E-4 1.954E-4 4.1387E-4 5 RD
15 1.0929E-3 8.2045E-5 1.1002E-3 8.2494E-5 1.2641E-3 9.8751E-4 5 RD
16 2.8671E-4 2.5420E-5 1.3612E-3 2.3612E-3 1.2054E-4 3.1331E-4 5 RD
DATA (RD(1))=457870/
17 1.0099E-3 7.4218E-5 2.7814E-4 2.5846E-5 9.0931E-4 6.6485E-4 5 RD
18 9.3383E-6 8.3375E-7 5.4533E-4 4.8767E-5 2.9480E-5 2.4980E-5 4 RD
19 4.3665E-4 4.7646E-5 7.6355E-4 1.5687E-4 7.9459E-5 7.4334E-6 4 RD
20 2.9496E-4 2.6314E-5 3.3446E-4 2.9377E-5 1.8080E-4 1.3518E-4 4 RD
21 6.846E-4 5.3386E-5 3.5174E-4 3.3684E-4 3.3859E-4 3.6599E-4 4 RD
22 4.0749E-4 4.9525E-5 3.8752E-4 3.484E-4 3.1093E-4 2.8110E-4 4 RD
23 7.381E-4 5.2575E-5 2.7247E-4 1.8494E-4 8.235E-4 1.0169E-4 4 RD
24 1.4392E-4 1.2782E-5 1.6264E-4 9.5952E-5 2.9723E-4 7.4624E-4 4 RD
25 5.1301E-4 3.1675E-4 1.2054E-4 5.869E-5 4.857E-4 6.232E-4 4 RD
26 7.0958E-5 1.1075E-4 3.908E-5 1.814E-4 4.574E-4 3.792E-4 4 RD
27 1.192E-3 8.1598E-5 7.9677E-5 2.243E-4 1.2786E-4 3.6923E-4 4 RD
28 1.811E-4 9.5587E-5 3.991E-5 1.268E-4 1.699E-4 1.7877E-4 4 RD
29 2.4517E-4 9.7250E-5 5.028E-4 1.172E-4 1.672E-4 3.0975E-4 4 RD
30 3.7684E-4 3.6385E-5 1.0776E-4 2.4793E-4 1.450E-4 1.2933E-4 4 RD
31 0.0000E+0 0.4800E+0 1.1765E-2 1.0713E-2 1.284E-5 1.2228E-4 4 RD
32 4.6588E-4 1.1031E-4 1.7667E-3 1.2602E-3 6.7132E-4 4.1380E-4 4 RD
DATA (RD(1))=571078/
33 2.569E-2 9.2427E-3 1.2406E-2 4 RD
34 1.6211E-2 1.4457E-2 3.324E-8 4.7945E-8 4 RD
35 1.452E-4 1.6917E-3 1.0745E-4 1.1715E-4 4 RD
36 0.7773E-3 6.7855E-3 2.6593E-3 7.2347E-4 4.1935E-4 3.0361E-4 4 RD
37 3.4000E-5 5.9299E-6 3.1212E-3 2.4799E-4 7.0302E-3 5.6028E-4 4 RD
38 9.3363E-4 2.1428E-3 5.3912E-3 1.1641E-9 2.2394E-3 1.6019E-7 4 RD
39 7.8974E-4 1.2896E-8 3.7012E-3 1.8529E-4 5.3897E-3 4.8056E-7 4 RD
40 2.2871E-3 6.2543E-5 1.5555E-3 6.3336E-8 2.1540E-3 2.766E-6 4 RD
41 2.5913E-4 1.2666E-7 5.0039E-3 3.521E-8 2.576E-3 2.7940E-8 4 RD
42 1.0499E-2 4.2946E-9 6.1681E-2 3.5840E-3 2.958E-4 2.219E-8 4 RD
43 9.7907E-3 2.7946E-3 6.3162E-3 8.3815E-8 3.2700E-3 2.6077E-8 4 RD
44 2.6448E-2 7.8245E-3 1.4795E-2 1.487E-2 3.461E-2 6.4256E-3 4 RD
45 3.5912E-2 1.6868E-3 7.611E-2 1.958E-2 3.489E-2 3.0190E-3 4 RD
46 1.7105E-2 4.8290E-3 4.1028E-1 1.6885E-3 1.113E-3 4.6023E-3 4 RD
47 9.304E-3 1.6282E-3 1.424E-2 3.1987E-3 1.192E-2 3.1852E-3 4 RD
48 4.0598E-4 8.8853E-4 8.8418E-4 1.1652E-3 7.4406E-3 1.0431E-7 4 RD
DATA (RD(1))=1114/
49 7.925E-4 1.681E-4 6.227E-4 1.866E-4 5.031E-4 4.966E-4 4 RD
50 1.823E-4 1.372E-4 1.505E-4 1.875E-4 2.420E-4 1.793E-4 5 RD
51 2.691E-4 3.952E-4 3.172E-4 2.817E-4 1.838E-4 1.841E-4 4 RD
52 1.5897E-4 1.6295E-4 2.1221E-4 1.9830E-4 1.5668E-4 3.9991E-4 4 RD
53 3.2487E-4 3.2372E-4 7.0295E-5 3.2054E-4 2.7136E-4 5.2336E-4 4 RD
54 3.5447E-4 4.4671E-4 3.8295E-4 3.299E-4 1.091E-4 2.8451E-4 4 RD
55 5.4716E-4 2.8051E-5 5.6255E-4 1.3392E-4 1.732E-4 3.8516E-4 5 RD
56 2.0588E-4 1.3766E-4 2.792E-4 1.44E-4 2.8758E-4 3.9299E-4 5 RD
57 5.0546E-4 1.3766E-4 2.937E-4 3.647E-4 1.9484E-4 3.570E-4 5 RD
58 9.1168E-4 3.6452E-5 2.9645E-4 3.387E-4 4.4887E-4 3.8802E-4 5 RD
59 8.9131E-4 7.431E-4 9.0743E-5 8.695E-4 2.1001E-4 9.1818E-4 5 RD
60 1.3817E-3 1.0181E-4 8.978E-4 7.765E-4 8.978E-4 8.978E-4 5 RD
61 3.886E-4 3.482E-5 1.170E-3 1.622E-3 2.852E-3 3.697E-4 5 RD
62 8.693E-4 6.6591E-5 2.0384E-4 2.695E-4 1.954E-4 4.1387E-4 5 RD
63 1.0929E-3 8.2045E-5 1.1002E-3 8.2494E-5 1.2641E-3 9.8751E-4 5 RD
64 2.8671E-4 2.5420E-5 1.3612E-3 2.3612E-3 1.2054E-4 3.1331E-4 5 RD
DATA (RD(1))=3434567/
65 1.866E-4 5.031E-4 4.966E-4 4 RD
66 2.420E-4 1.793E-4 5 RD
67 1.838E-4 1.841E-4 4 RD
68 1.5668E-4 3.9991E-4 4 RD
69 2.7136E-4 5.2336E-4 4 RD
70 3.2054E-4 2.7136E-4 5 RD
71 1.091E-4 2.8451E-4 4 RD
72 5.6215E-4 1.3392E-4 5 RD
73 1.44E-4 2.8758E-4 5 RD
74 3.9299E-4 3.570E-4 5 RD
75 1.9484E-4 3.570E-4 5 RD
76 3.387E-4 4.4887E-4 5 RD
77 2.1001E-4 9.1818E-4 5 RD
78 8.978E-4 8.978E-4 5 RD
79 3.697E-4 3.697E-4 5 RD
80 2.852E-3 3.697E-4 5 RD
81 1.954E-4 4.1387E-4 5 RD
82 4.1387E-4 4.1387E-4 5 RD
83 1.2641E-3 9.8751E-4 5 RD
84 3.1331E-4 3.1331E-4 5 RD
85 9.0931E-4 6.6485E-4 5 RD
86 2.9480E-5 2.4980E-5 4 RD
87 7.6355E-4 1.5687E-4 7.9459E-5 7.4334E-6 4 RD
88 3.3446E-4 2.9377E-5 1.8080E-4 1.3518E-4 4 RD
89 3.5174E-4 3.3684E-4 3.3859E-4 3.6599E-4 4 RD
90 3.8752E-4 3.484E-4 3.1093E-4 2.8110E-4 4 RD
91 1.8494E-4 8.235E-4 1.0169E-4 4 RD
92 5.057E-4 1.6264E-4 9.5952E-5 2.9723E-4 7.4624E-4 4 RD
93 1.2054E-4 5.869E-5 4.857E-4 6.232E-4 4 RD
94 3.908E-5 1.814E-4 4.574E-4 3.792E-4 4 RD
95 2.243E-4 1.2786E-4 3.6923E-4 4 RD
96 1.268E-4 1.699E-4 1.7877E-4 4 RD
97 3.991E-5 1.268E-4 1.699E-4 1.7877E-4 4 RD
98 1.172E-4 1.672E-4 3.0975E-4 4 RD
99 5.028E-4 1.172E-4 1.672E-4 3.0975E-4 4 RD
100 1.0776E-4 2.4793E-4 1.450E-4 1.2933E-4 4 RD
101 1.1765E-2 1.0713E-2 1.284E-5 1.2228E-4 4 RD
102 4.6588E-4 1.1031E-4 1.7667E-3 1.2602E-3 6.7132E-4 4.1380E-4 4 RD
103 2.569E-2 9.2427E-3 1.2406E-2 4 RD
104 1.6211E-2 1.4457E-2 3.324E-8 4.7945E-8 4 RD
105 1.452E-4 1.6917E-3 1.0745E-4 1.1715E-4 4 RD
106 0.7773E-3 6.7855E-3 2.6593E-3 7.2347E-4 4.1935E-4 3.0361E-4 4 RD
107 3.4000E-5 5.9299E-6 3.1212E-3 2.4799E-4 7.0302E-3 5.6028E-4 4 RD
108 9.3363E-4 2.1428E-3 5.3912E-3 1.1641E-9 2.2394E-3 1.6019E-7 4 RD
109 7.8974E-4 1.2896E-8 3.7012E-3 1.8529E-4 5.3897E-3 4.8056E-7 4 RD
110 2.2871E-3 6.2543E-5 1.5555E-3 6.3336E-8 2.1540E-3 2.766E-6 4 RD
111 2.5913E-4 1.2666E-7 5.0039E-3 3.521E-8 2.576E-3 2.7940E-8 4 RD
112 1.0499E-2 4.2946E-9 6.1681E-2 3.5840E-3 2.958E-4 2.219E-8 4 RD
113 9.7907E-3 2.7946E-3 6.3162E-3 8.3815E-8 3.2700E-3 2.6077E-8 4 RD
114 2.6448E-2 7.8245E-3 1.4795E-2 1.487E-2 3.461E-2 6.4256E-3 4 RD
115 3.5912E-2 1.6868E-3 7.611E-2 1.958E-2 3.489E-2 3.0190E-3 4 RD
116 1.7105E-2 4.8290E-3 4.1028E-1 1.6885E-3 1.113E-3 4.6023E-3 4 RD
117 9.304E-3 1.6282E-3 1.424E-2 3.1987E-3 1.192E-2 3.1852E-3 4 RD
118 4.0598E-4 8.8853E-4 8.8418E-4 1.1652E-3 7.4406E-3 1.0431E-7 4 RD

SECTION 5

LISTINGS OF THE DIFFUSION FACTOR DATA AND EQUILIBRIUM THERMOCHEMICAL DATA BUILT INTO THE GASKET PROGRAM

Diffusion factors are stored in the GASKET program for the fourteen selected species listed below. These factors are considered to be more accurate than the general correlation which is described in Section 4 of Volume I and which is used to compute the diffusion factors for the remaining species. The diffusion factors presented below were obtained from Reference 4.

The equilibrium thermochemical data listed below include all species tabulated in the JANAF Thermochemical Tables (Reference 5) which are comprised of the elements A, Al, B, Be, C, Cl, F, H, He, Li, N, O, and Si. These data, in addition to the diffusion factor data, are stored in the special data statement called DATX in the GASKET program. The order of the data and the formats of the cards used to generate the listing below are prescribed in Section 4 of Volume I.

DIFFUSION FACTORS

14	FIS FROM AERO 69-53						
CO2	1.2495	N2	1.0275	O2	0.9553	O	0.7063
CO	1.0172	H	.19396	C	.6895	CH	.7495
H2	0.28302	H2O	0.7704	N	0.7553	HCN	1.1173
CH4	0.9503	CA	1.0333				

EQUILIBRIUM THERMOCHEMICAL DATA, pp. 5-2 thru 5-9

1	1	1	3	1	8	0	0	C	0	0	0	0	0	-OJANAF TAPE 7/71 3/66	HL10*
-115230+6	41750+6	99256+6	1	106420+2	516700+2	500	744.2	-O.M10*							
-113202+6	56035+6	20740+2	2	605335+7	579999+4	601678+2	744	3500.3	-O.M110*						
2	1	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/64	HL120*					
-143	90+6	61989+6	17445+2	356485+2	605330+6	5011242+2	500	1957.2	-O.L120*						
-131230+6	623610+5	23998+2	363215+7	163999+3	626331+2	1937	4000.3	-O.L120*							
1	6	1	5	2	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 12/64	HL10*
-242890+6	89580+6	143733+2	116810-1	347280+6	72335+2	500	1116.2	-O.B10*							
-23861+6	684	145	34861+2	358559+7	159999+3	80892+2	116	4000.3	-O.B102*						
-119590+6	437119+6	226195+2	327	4-2-856638+6	569	42+2	699	679.2	8CL10*						
-117420+6	763180+6	280199+2	260770+7	239999+2	80448+2	879	2000.3	-O.BECL12*							
-245399+6	661769+5	114165+2	790	67-2-133382+5	606974+2	500	824.2	8PF2*							
-24272+6	676921+8	138453+2	708747-2	483265+6	631393+2	924	2000.3	-O.BE2*							
2	13	4	4	8	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 9/64	HL10*
-544999+6	126637+6	350310+2	792725+2	110319+7	111980+3	500	1700.2	-O.AL28E04*							
-544999+6	126470+6	395377+2	642652+2	675205+7	11191+3	1700	3000.2	-O.AL28E04*							
4	6	2	3	7	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 6/65	HL10*
-803598+6	240767+6	475582+2	26478-1	206819+7	208921+3	600	1190.2	9ALI807*							
-792780+6	286874+6	10141+3	752653+2	246932+7	248982+3	1190	3000.3	-O.BALI207*							
6	5	2	3	10	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/65	HL10*
-111373+7	286890+6	616137+2	167955-1	245753+7	267222+3	500	1200.2	-O.BALI201*							
-111373+7	280801+6	765302+2	160770-1	690757+7	263619+3	1200	2000.2	-O.BALI201*							
6	6	2	3	13	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/65	HL10*
-141385+7	362466+6	110861+3	144809-1	395675+7	337542+3	500	1200.2	-O.BALI201*							
-141365+7	351143+6	116663+3	140148-1	319404+7	336953+3	1200	2000.2	-O.BALI201*							
2	8	4	4	8	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/65	HL10*
-337	99+6	184720+6	372	62+2	201810-1	205638+7	160378+3	500	1000.2	-O.B2404*					
-337	99+6	183461+6	603721+2	453600+2	6956	07	151107+3	1000	1500.2	-O.B2404*					
1	2	3	3	8	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/66	HL10*
-260539+6	184751+6	08607+1	361152-1	180813+7	142813+3	500	593.2	-O.CLI203*							
-261628+6	14771+6	44320+2	435856-6	671999+3	126879+3	993	2000.3	-O.CLI203*							
1	4	3	9	1	3	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 6/66	HL10*
-390239+6	96273+6	32371+2	356191-2	159677+7	979550+2	800	1000.2	8EP3LI*							
-390239+6	964780+6	33346+2	303956-2	204379+7	977860+2	1000	1500.2	-O.BEP3LI*							
1	4	9	2	3	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 6/66	HL10*
-389999+6	216191+6	221889+2	166264-7	199999+2	157173+3	748	2000.3	8EP4LI2*							
2	5	3	4	6	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 9/66	HL10*
0741599+6	188899+6	709707+2	311327-2	628850+7	167660+3	500	1700.2	-O.B28E306*							
-741959+6	188872+6	66164+2	460229-2	285754+6	167658+3	1700	3000.2	-O.B28E306*							
3	5	3	3	4	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/65	HL10*
-885499+6	173715+6	375800+2	171859-1	189271+7	176618+3	500	1000.2	-O.B3P303*							
-886499+6	14218+6	65117+2	492905-2	114144+8	163112+3	1000	1500.2	-O.B3P303*							
10	5	14	1	0	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 0/64	HL10*
-169999+6	59491+6	64637+2	410265-1	559736+7	336853+3	500	1000.3	-O.B10M14*							
-169999+6	316150+6	17118+3	18855-1	352138+8	301924+3	1000	1500.3	-O.B10M14*							
1	1	3	1	3	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 9/67	HL10*
-216599+6	661595+6	372	97+1	126	91-1	724601+8	470483+2	500	942.2	-O.M11*					
-169729+6	402579+6	145	162-605359-7	749999+2	397139+3	982	2000.3	-O.M11*							
1	5	1	1	2	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 12/64	HL10*
-191669+6	766830+6	13830+2	930341-2	633	116	656373+2	500	1000.2	-O.B102*						
-191669+6	528514+6	236362+2	162828-4	131683+7	576682+2	1000	1500.2	-O.B102*							
1	5	3	1	3	8	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 12/64	HL10*
-261469+6	142828+6	260431+2	141236-1	143978+7	112468+3	500	1000.2	-O.BM303*							
-261469+6	114403+6	422911+2	315866-2	672256+7	106	40+3	1000	1500.2	-O.BM303*						
5	5	9	1	0	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/65	HL10*
102399+6	16184+6	59685+2	114916-1	515761+7	191461+3	500	1000.3	-O.BPM30*							
102399+6	16184+6	67237+2	318617-2	44040+7	183422+3	1000	1500.3	-O.BPM30*							
1	5	4	1	3	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 12/64	HL10*
-455219+5	739491+5	295147+2	405981-3	146142+7	762840+2	500	1200.2	-O.BM4LI*							
-455219+5	756743+5	276172+2	688526-3	965963+6	790200+2	1200	2000.2	-O.BM4LI*							
1	13	4	1	3	0	0	0	0	0	0	0	0	0	-OJANAF TAPE 7/71 3/64	HL10*
-279999+6	776450+6	28418+2	884184-3	117868+7	835879+2	500	1200.2	-O.ALM4LI*							
-279999+6	773164+6	274381+2	116524-2	2465	12+6	834700+2	1200	2000.2	-O.ALM4LI*						

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