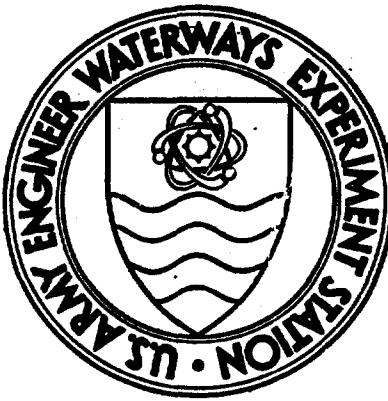


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TECHNICAL REPORT H-72-2

GRAYS HARBOR ESTUARY, WASHINGTON

Report I

VERIFICATION AND BASE TESTS

Hydraulic Model Investigation

by

N. J. Brogdon, Jr.



1

April 1972

Sponsored by U. S. Army Engineer District, Seattle

Conducted by U. S. Army Engineer Waterways Experiment Station, Vicksburg, Mississippi

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FOREWORD

The model study reported herein was requested by the U. S. Army Engineer Division, North Pacific, in a letter to the Office, Chief of Engineers, dated 20 April 1966 and was subsequently approved in a letter to the North Pacific Division dated 22 July 1966. Authority to initiate the investigation was granted by the U. S. Army Engineer District, Seattle, in a letter to the Director, U. S. Army Engineer Waterways Experiment Station (WES), dated 24 January 1968.

Design and construction of the model were accomplished during the period February 1968-June 1969; hydraulic and salinity verifications were carried out during the period June 1969-December 1969; and fixed-bed shoaling verification was carried out during the period August 1970-September 1970. Hydraulic, salinity, and dye dispersion base tests were performed during the period January 1970-July 1970. After completion of all fixed-bed model verifications and base tests, the general investigation program was initiated.

This report describes the problems that necessitated the model investigation, the model and its appurtenances, and the fixed-bed model verification and base tests. Subsequent reports will describe the various studies conducted in the model.

The study was conducted in the Hydraulics Division of the WES under the direction of Mr. E. P. Fortson, Jr., Chief of the Hydraulics Division, and Mr. H. B. Simmons, Chief of the Estuaries Branch. The design, construction, verification, and base tests were conducted by Mr. N. J. Brogdon, Jr., Project Engineer, and technicians of the Estuaries Branch, under the supervision of Mr. F. A. Herrmann, Jr., Chief

of the Harbor Entrance Section. This report was prepared by Mr. Brogdon with the assistance of Mr. Herrmann.

Personnel of the Seattle District who were principally responsible for planning the course of study included: Messrs. Dwain Hogan, John Norman, Bruce McCartney, Bill Peterson, and Harry Disbrow. These personnel and others participated in conferences on the model study and visited the model from time to time.

Directors of WES during the conduct of the study and the preparation and publication of this report were COL Levi A. Brown, CE, and COL Ernest D. Peixotto, CE. Technical Directors were Messrs. J. B. Tiffany and F. R. Brown.

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CONVERSION FACTORS, BRITISH TO METRIC UNITS OF MEASUREMENT

British units of measurement used in this report can be converted to metric units as follows:

<u>Multiply</u>	<u>By</u>	<u>To Obtain</u>
inches	2.54	centimeters
feet	0.3048	meters
miles (U. S. statute)	1.609344	kilometers
square feet	0.092903	square meters
square miles (U. S. statute)	2.58999	square kilometers
cubic yards	0.764555	cubic meters
feet per second	0.3048	meters per second
cubic feet per second	0.02831685	cubic meters per second

SUMMARY

Grays Harbor model, a fixed-bed model with provisions for future conversion to a movable-bed model, was constructed to scales of 1:500 horizontally and 1:100 vertically and reproduced all of Grays Harbor, the Chehalis River, to the head of tidal influence (South Montesano), and a portion of the Pacific Ocean adjacent to the harbor entrance. The primary purposes of the overall model study will be to determine the effects of rehabilitation of both the north and south jetties, investigate the stability of Point Chehalis, determine the effects of enlarging and realigning the navigation channel, and locate suitable dredge spoil disposal areas. The flushing rate and dispersion characteristics of waste materials discharged into the system will also be investigated.

The model verification tests described herein indicated that the model hydraulic and salinity regimens were in satisfactory agreement with those of the prototype for comparable conditions. It therefore can be assumed that the model will provide quantitative answers concerning the effects of the proposed improvement plans on the hydraulic and salinity regimens of the estuary.

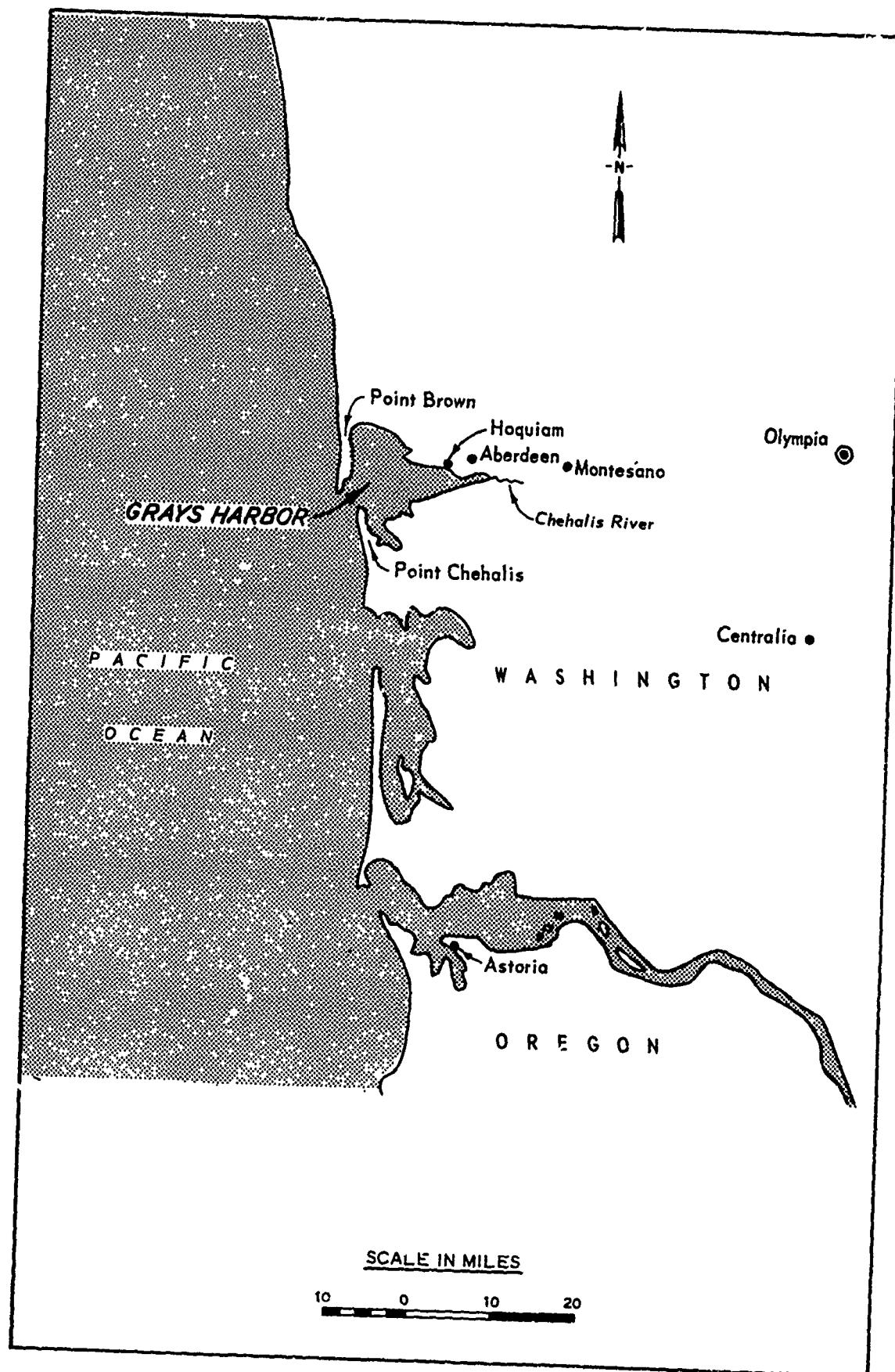


Fig. 1. Vicinity map

GRAYS HARBOR ESTUARY, WASHINGTON

VERIFICATION AND BASE TESTS

Hydraulic Model Investigation

PART I: INTRODUCTION

The Prototype

1. Grays Harbor, Wash. (fig. 1), located about 45 miles* north of the mouth of the Columbia River and 93 miles south of Cape Flattery, is a large bay at the head of which is the Chehalis River. The roughly pear-shaped harbor diverges from the Chehalis River at Aberdeen, Wash., 15 miles east of the entrance, to a maximum width of 13 miles, including North and South Bays (plate 1). The water-surface area of the harbor varies from about 94 square miles at mean higher high water (mhhw) to about 35 square miles at mean lower low water (mllw). The harbor is separated from the Pacific Ocean by two narrow sandy peninsulas. The northerly peninsula is 7 miles long and terminates at Point Brown, just north of the harbor entrance; Point Chehalis comprises the north end of the southerly peninsula, which is 4 miles long.

2. The entrance to Grays Harbor (between Point Brown and Point Chehalis) is about 2.5 miles wide and is protected by two converging rubble-mound jetties that are 6500 ft apart at their outer ends. The existing navigation project for Grays Harbor and Chehalis River was authorized by the Rivers and Harbors Acts of 3 June 1896, 2 March 1907, 25 June 1910, 8 August 1917, 21 January 1927, 3 July 1930, 30 August 1935, 2 March 1945, 30 June 1948, and 3 September 1954. The project provides for a 600-ft-wide by 30-ft-deep entrance channel from the Pacific Ocean across the bar to be secured by dredging, by a south jetty 13,700 ft long, and by a north jetty 16,000 ft long. The top elevation

* A table of factors for converting British units of measurement to metric units is presented on page vii.

of both jetties, as originally constructed, was +16 ft mllw. The entrance channel is actually self-maintaining for the authorized dimensions and thus requires no maintenance dredging. Maximum depths in the channel are about -70 ft mllw. Based on the recommendations of the U. S. Army Engineer Committee on Tidal Hydraulics and the results of a hydraulic model study conducted at the U. S. Army Engineer Waterways Experiment Station during the period 1950-1952, it was concluded that the outer 6000 ft of the south jetty should be allowed to deteriorate to about elevation 0.0 ft mllw to alleviate the very serious erosion problem at Point Chehalis which resulted from the reconstruction of this jetty during the period 1935-1939. The above-mentioned Rivers and Harbors Acts further provide for maintenance of a channel 30 ft deep and 350 ft wide from the entrance to Cow Point (immediately east of Rennie Island), a distance of 14 miles; thence 30 ft deep and 200 ft wide, for a distance of 4-1/8 miles; a turning basin 30 ft deep, 550 ft wide, and 1000 ft long at the upstream end of the 30-ft channel near Cosmopolis; thence a channel 16 ft deep and 150 ft wide for 10-3/4 miles to Montesano, with a turning basin at Montesano. The interior channel below Cow Point requires annual maintenance dredging of about 1,600,000 cu yd.

3. Tides occurring in Grays Harbor are of the mixed type and vary in mean diurnal range from 9.0 ft at Point Chehalis to 9.9 ft at Aberdeen. At Point Chehalis the elevation of mllw is -4.9 ft mean sea level (msl), while that of mhhw is +4.1 ft msl. The estuary is partially mixed, with a significant difference between surface and bottom salinity concentrations but no distinct saltwater wedge. Saltwater intrusion extends upstream from South Aberdeen (20 miles from the entrance) at normal freshwater flows with the salinity concentration at sta 18 (plate 1) varying from 0.0 ppt (total salt) at lower low water (llw) to about 10.0 to 12.0 ppt at higher high water (hhw). The horizontal density gradient from the entrance to the upstream limits is fairly uniform. Surface salinities in the entrance area average about 1.0 to 2.0 ppt lower than those at the bottom, while near the upstream limits of saltwater intrusion, the surface salinities average about 3.0 to 5.0 ppt lower than those at the bottom.

Purpose of Investigation

4. In general, the primary purposes of the overall model study are to: determine the need for and develop optimum plans for rehabilitation of existing jetties, in conjunction with erosion studies of Point Chehalis and scour adjacent to the south jetty; determine the effects of realignment of the entrance and Sand Island shoal navigation channels; determine the effects of enlarging the navigation channel; determine the location of suitable dredge spoil disposal areas; investigate ways of reducing maintenance dredging requirements in the navigation channel; determine the effects of enlarging existing small-boat basins; and determine the flushing rate and dispersion characteristics of waste materials that are discharged into the estuary.

5. Following the rehabilitation of the north and south jetties in 1942, the entrance channel migrated south to its present location adjacent to the south jetty. Scour adjacent to this jetty has caused fear that the structure may eventually be undermined unless the scour can be controlled or a new entrance can be developed in the northern portion of the entrance. The alignments of the entrance and the bar channels, and their close proximity to the south jetty, present a navigation problem for small and large craft alike when entering and leaving the harbor. This problem could also be resolved if a new entrance channel were developed. The erosion problem at Point Chehalis was also investigated in conjunction with the jetty and entrance channel studies.

6. Model studies will be conducted to develop plans to reduce the existing annual maintenance dredging requirements in the interior channel of the harbor. These studies will be conducted in conjunction with proposed changes in channel alignments and enlarged channel dimensions. Studies will be made for both existing and proposed channel changes to determine best locations of spoil disposal areas and to determine if turning basins along the channel might also serve as sediment traps. This report contains all important data related to the hydraulic, salinity, and fixed-bed shoaling (entrance area) verification of the model.

PART II: THE MODEL

Description

7. The Grays Harbor model reproduced approximately 230 square miles of the prototype area, including the Chehalis River to South Montesano, the Pacific coast from about 7.5 miles north of the north jetty to about 7.5 miles south of the south jetty, and offshore areas well beyond the -60 ft contours; Elk, Johns, Humptulips, Hoquiam, and Wishkah Rivers; North and South Bays; and the system of sloughs and creeks that affects tidal action throughout the model area. The limits of the area reproduced are shown in plate 1. A general view of the model is shown in fig. 2.

8. The model was constructed to linear scale ratios, model to prototype, of 1:500 horizontally and 1:100 vertically. From these basic ratios the following scale relations were computed by the Froudian relations: slope 5:1, velocity 1:10, time 1:50, discharge 1:500,000, and volume 1:25,000,000. The salinity and dye concentration ratios for the study were 1:1. One prototype cycle (diurnal tide) of 24 hr and 50 min was reproduced in the model in 29 min and 48.5 sec. Horizontal grid coordinates are based on Polyconic Projection 1927 North American Datum, and vertical control was based on USC&GS msl 1929 adjustment. The model was approximately 320 ft long and 180 ft wide at its widest point, and covered an area of about 30,000 sq ft. It was completely enclosed to protect it and its appurtenances from the weather and to permit uninterrupted operation.

9. The model was initially constructed as a fixed-bed model; however, provisions were made to convert the entrance area to a movable-bed model at a later date when such studies were deemed necessary. Limits of the movable-bed section are shown in plate 1. The model was molded to conform to the prototype hydrographic conditions that existed in 1967. The navigation channel was molded in removable blocks so that desired alterations could readily be made.

10. The permanent model roughness employed consisted of



Fig. 2. General view of model, looking upstream

H698-10

3/4-in.-wide metal strips placed in depths greater than 6 ft below msl and cut off below the low-water elevation. The use of these metal strips as roughness was necessary because proper adjustment of velocity and distribution of currents, both horizontally and vertically, in any given cross section could not be obtained by the use of ordinary boundary roughness alone in the deep areas of the model. The areas above -6 ft msl (shoal areas and tide flats) were roughened by raking the model surface during construction to provide the desired degree of roughness.

Appurtenances

11. The model was equipped with the necessary appurtenances to reproduce and measure all pertinent phenomena such as tidal elevations, saltwater intrusion, current velocities, freshwater inflow, waves, dispersion characteristics, and shoaling distribution. Apparatus used in connection with the reproduction and measurement of these phenomena include a tide generator and recorder, tide gages, salinity meters, salinity samplers, chemical titration equipment, current velocity meters, freshwater measuring weirs, wave generators, dye injection and measuring equipment, and shoaling injection and recovery apparatus. This equipment is described in detail in subsequent paragraphs.

Tide generator and recorder

12. The reproduction of tidal action in the model was accomplished by means of a tide generator (figs. 3 and 4), located in the model ocean, that maintained a differential between a pumped inflow of salt water to the model and a gravity return flow to the supply sump as required to reproduce all characteristics of the prototype tides at the control station (Westport). The tide generator was equipped with a continuous tide recorder so that the accuracy of the model tide reproduction could be checked visually at any time.

Tide gages

13. Permanently mounted point gages were installed in the model at the locations of the seven recording tide gages used for collection of field tide data (plate 1). Portable point gages were used to measure

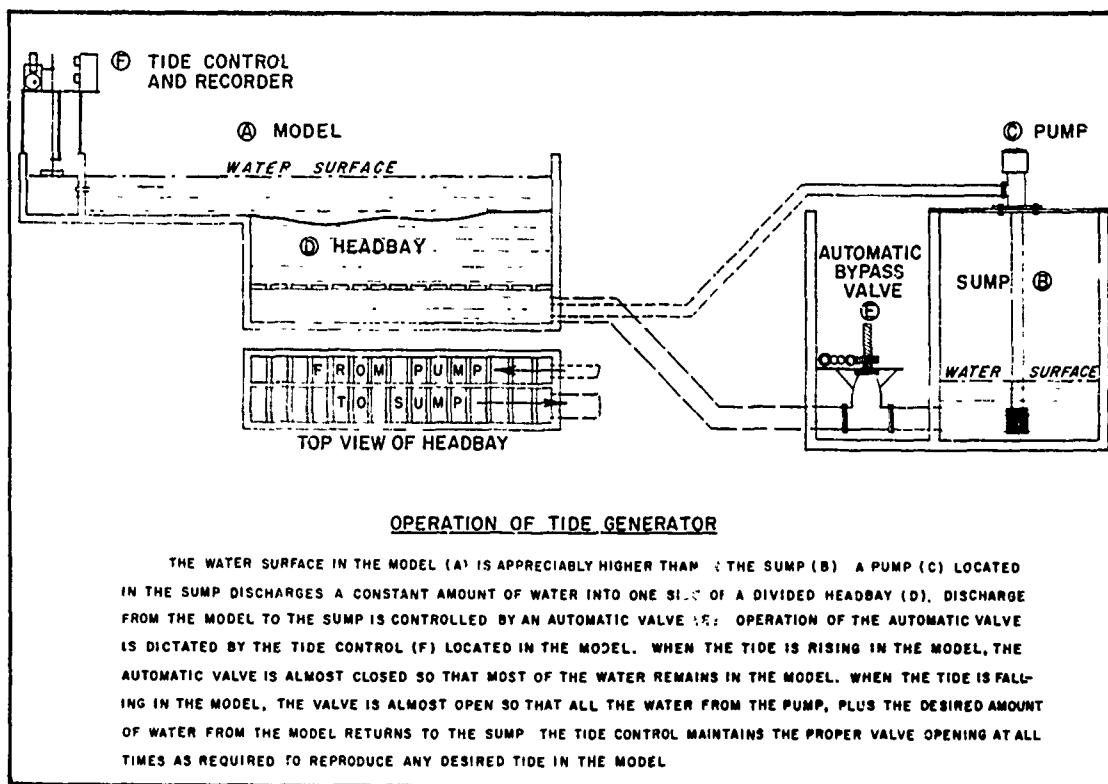


Fig. 3. Operation of tide generator



Fig. 4. Tide recorder

tidal elevation at other points as required. The model gages were graduated in 0.001 ft (0.1 ft prototype).

Salinity and dye samplers

14. Salinity and dye water samples were drawn into collection vials by negative pressure from a vacuum pump connected to a central manifold, which in turn was connected to tubes running to each sampling location. This device enabled simultaneous sampling at all desired depths at all sampling stations throughout the model. Details of the multidepth sampler are shown in fig. 5.

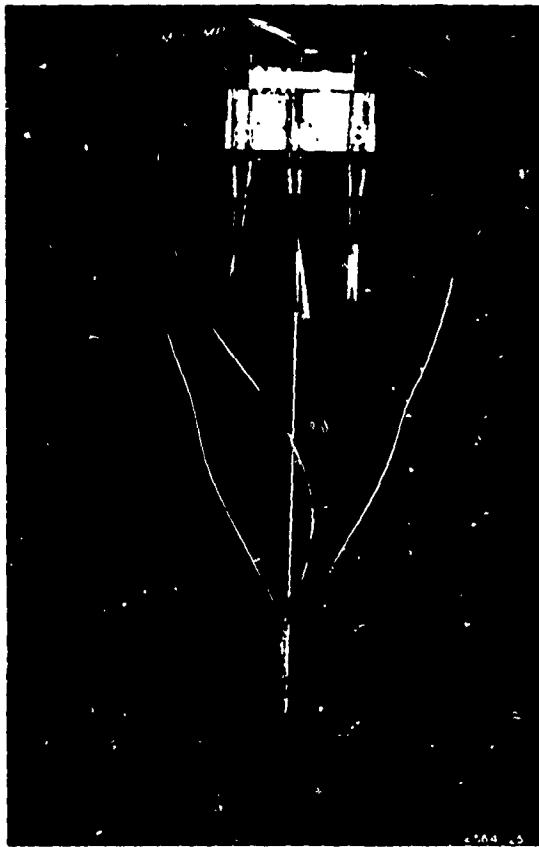


Fig. 5. Multidepth sampler

Chemical titration equipment

15. This method of determining salinity concentration was used primarily to determine the salinity concentration at the saltwater source (sump). The equipment consisted of a graduated burette for measuring the volume of silver nitrate, pipettes for measuring the volume of samples used, sample jars in which to perform the titration, a supply of silver

nitrate, and a quantity of potassium chromate for use as an end-point indicator in the titration process. The method consisted of adding a known concentration of silver nitrate solution to a known volume of the model salinity sample; the amount of silver nitrate required to precipitate the salt contained in the sample was then converted to salinity in parts per thousand of NaCl.

Salinity meters

16. All salinity concentrations for samples taken from the model were determined by use of conductivity cells especially built and calibrated for this purpose. The salinity meter assembly is shown in fig. 6.

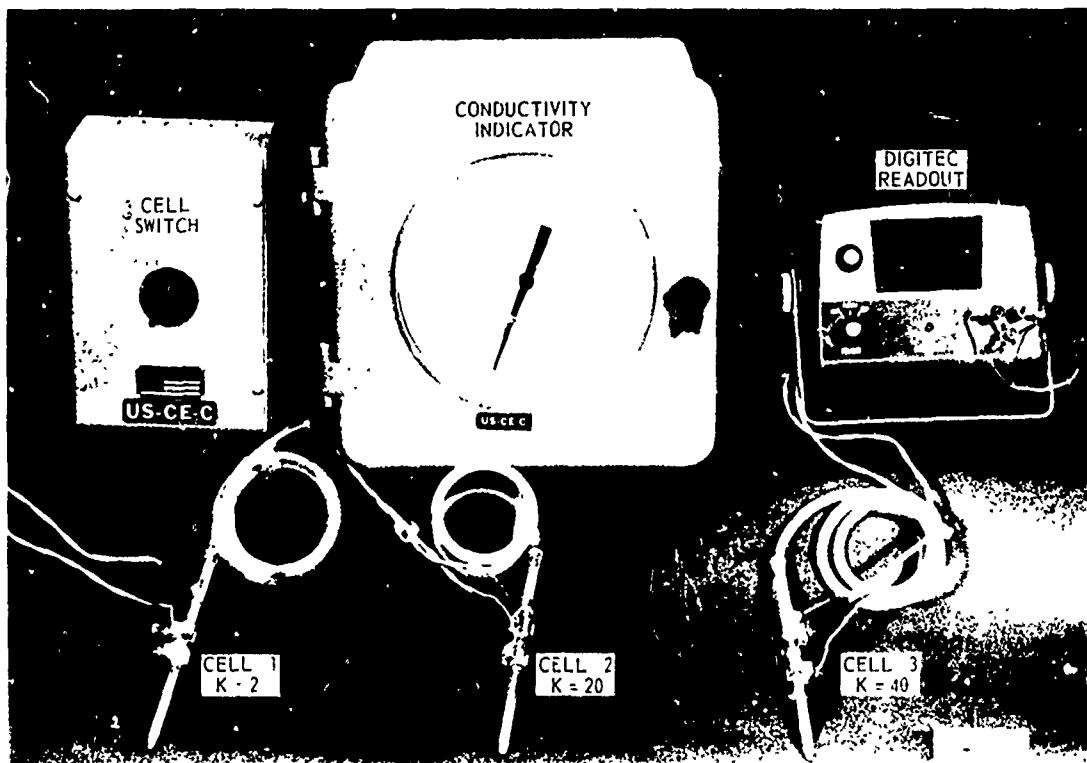


Fig. 6. Salinity meter assembly

Current velocity meters

17. Current velocity measurements were obtained with miniature Price-type current meters (fig. 7). The five meter cups, constructed of a light plastic or metal material, were approximately 0.04 ft (4 ft prototype) in diameter and were mounted on a horizontal wheel 0.09 ft in diameter; the center of the cups was 0.05 ft (5 ft prototype) from the

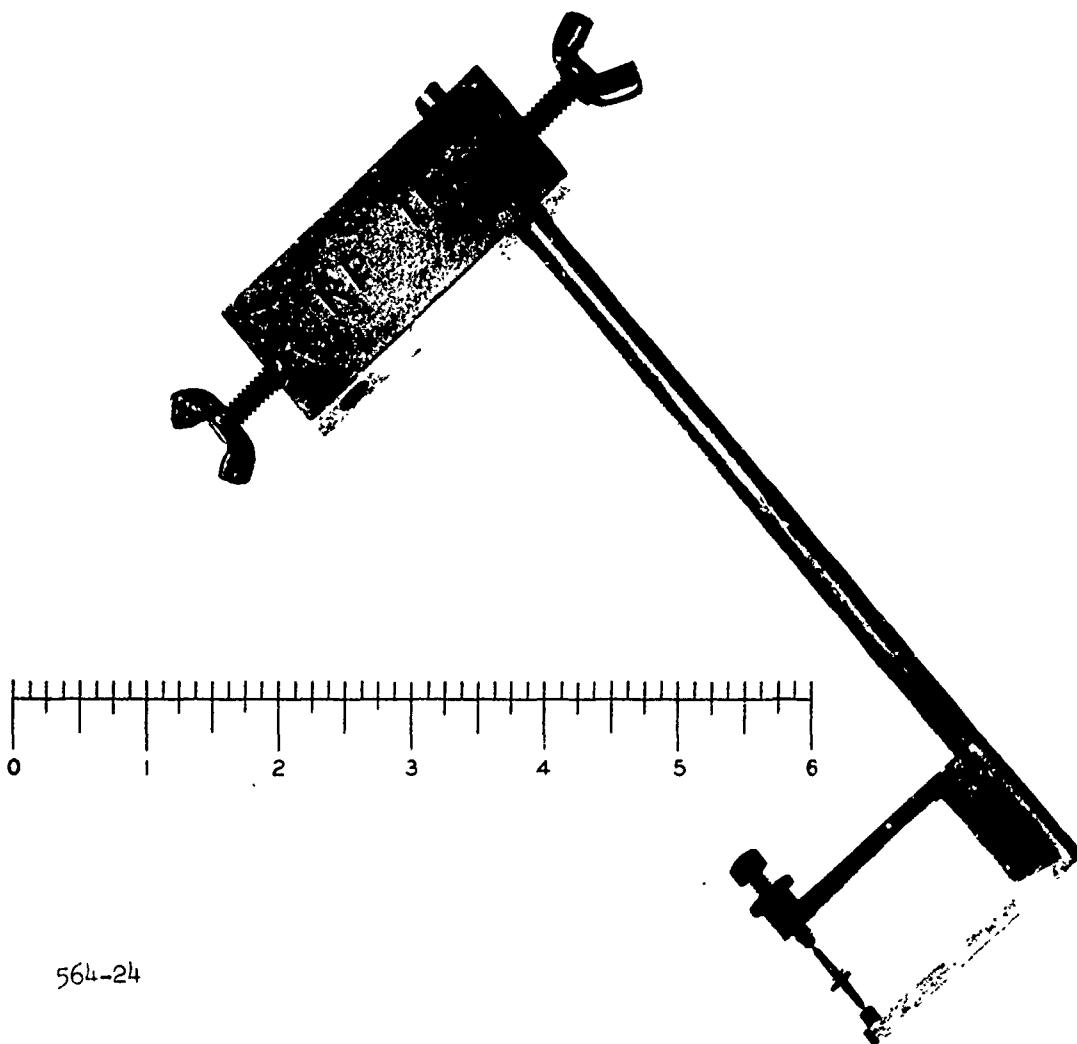


Fig. 7. Miniature Price-type current meter

bottom of the frame. The meters were calibrated frequently to ensure accurate operation and were capable of measuring actual velocities as low as 0.03 fps (0.3 fps prototype).

Freshwater inflow measuring devices

18. All rivers with significant mean freshwater inflows were equipped with a constant head tank and Van Leer weir for precise measurements of their respective flows. The inflows of streams with minor freshwater inflows were combined with those of nearby streams of significant inflow, and the combined inflow was introduced at a central point. Individual inflow points were located on the Chehalis, Hoquiam, and

Wishkah Rivers. Chenois Creek and Grass Creek inflows were combined with that of Humptulips River. Johns River, Newskah Creek, Charley Creek, Stafford Creek, Indian Creek, Campbell Creek, Chapin Creek, O'Leary Creek, and Andrews Creek inflows were combined with that of Elk River.

Skimming weir

19. The mixed salt water and fresh water that accumulated in the model ocean had to be removed in order to maintain a constant volume and a constant source salinity. This was accomplished by means of skimming weirs that removed a quantity of mixed water from the surface layer equal to the freshwater inflow to the estuary. Precise measurement of the combined discharge from the skimming weirs was made by use of a Van Leer weir.

Wave generators

20. The model ocean was equipped with two 20-ft-long wave generators to produce the effects of ocean waves on the transportation and deposition of sediments. The wave generators were of the plunger type and could be adjusted to produce the desired wave height and period.

Dye injection and measuring equipment

21. Model tests were made to determine the flushing rate and dispersion characteristics of the model. A given weight of powdered fluorescent dye was thoroughly mixed with a known volume of water and then stored in a glass-sided tank. The tanks were equipped with a system of valves and tubes to control the desired discharge at the injection locations. Injection was made at two locations simultaneously by utilizing two different types of dyes. Water samples were collected at locations throughout the model with a sampling device identical with the multidepth salinity sampler described in paragraph 14. Concentrations of the samples were measured by means of a Turner Model III fluorometer (fig. 8).

Shoaling injection
and recovery apparatus

22. Shoaling was reproduced in the model by injecting granulated (1/8 in. by 1/8 in.) nylon particles or polystyrene plastics. The specific weight of the model sediment to be used for a particular problem

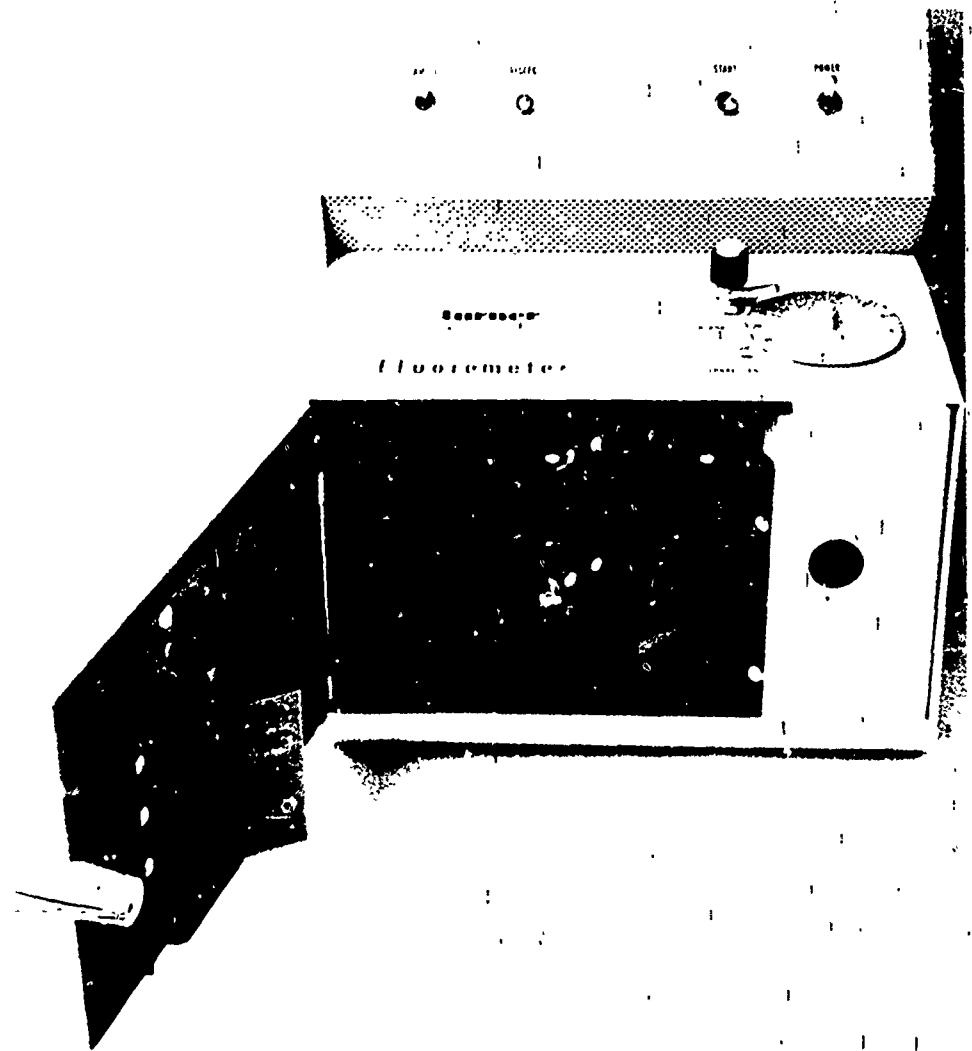


Fig. 8. Turner fluorometer

was determined by trial and error, and varied from about 1.03 to 1.20. The injection procedure for individual problem areas varied; however, the normal methods were to place the material by hand or allow a slurry of the material to flow into the model through a perforated trough. At the end of each model test, the shoaling material deposited within the limits of the navigation channel or prescribed problem area was recovered and measured volumetrically.

PART III: VERIFICATION OF THE MODEL

23. Verification of the Grays Harbor fixed-bed model was accomplished in three phases: (a) hydraulic verification, which ensured that tidal elevations and times, and current velocities and directions were in proper agreement with the prototype; (b) salinity verification, which ensured that salinity phenomena in the model correspond to those of the prototype for similar conditions of tide, ocean salinity, and freshwater inflow; and (c) fixed-bed shoaling verification, which ensured acceptable reproduction of prototype shoaling distribution.

Fixed-bed shoaling verification for the interior 30- by 350-ft navigation channel and movable-bed shoaling verification are beyond the scope of this report; however, the fixed-bed shoaling verification for the area between the jetties will be discussed. The need for movable-bed studies had not been determined at the time of preparation and publication of this report; therefore, the movable-bed verification had not been initiated.

24. The accurate reproduction of hydraulic and salinity phenomena in an estuary model is an important phase in the preparation of the model for its ultimate use in evaluating the effects of proposed improvement works. Every effort was made to obtain a comprehensive verification of all pertinent phenomena. Prototype data used for the model hydraulic and salinity verification were collected in the field by U. S. Army Engineer District, Seattle, personnel during the period 4 October to 17 October 1967. These data were furnished to Waterways Experiment Station engineers in the form of curves and tables. The entrance shoaling verification (fixed bed) was based on soundings taken in September 1965 and November 1969.

25. This report contains all important data related to the hydraulic, salinity, and fixed-bed shoaling (entrance area) verification of the model, in order to facilitate reference to these data in other phases of the overall investigation.

Hydraulic Verification

Prototype data

26. In 1967 the Seattle District undertook an extensive prototype metering program of the Grays Harbor estuary in order to obtain data with which to adjust and verify the Grays Harbor estuary model. The metering program was carried out in two consecutive 6-day periods that were selected as being generally representative of normal spring and neap tide conditions on the basis of predicted tides. Eighteen stations on eight ranges (plate 1) were established at which to collect current and salinity data. Because of insufficient personnel and equipment and prohibitive cost, it was impossible to obtain simultaneous observations at all stations.

Tidal adjustment

27. The objective of the model tidal adjustment was to obtain an accurate reproduction of prototype tidal elevations and tidal phases throughout the model. Prototype tidal data from seven recording tide gages (plate 1) were available to verify the accuracy of the model tidal adjustment. These gages recorded essentially continuously throughout the prototype data collection period discussed previously.

28. During each of the 6-day metering periods there were significant variations of tidal ranges and other tidal characteristics. In order to avoid the time-consuming and expensive procedures of adjusting the model to reproduce all of the tides observed during the metering program, it was decided to select one 24.84-hr (diurnal) tide for each of the 6-day periods that approximated the tidal condition for that particular period and to complete the adjustment of tides, currents, and salinities throughout the model for only the two tides thus selected. The two tides chosen were 6-7 October 1967 (spring tide) and 13-14 October 1967 (neap tide).

29. The procedure followed was to adjust the tide generator in such a manner that the tides generated in the model ocean would cause an accurate reproduction of prototype tides at Westport (control) tide gage, then to adjust the model roughness until prototype tidal

elevations and times were reproduced to scale throughout the model.

30. Comparisons of model and prototype tidal data for the two tides reproduced in the model are presented in plates 2-9. Plates 2-4 show tidal elevations for the spring tide condition at the Westport, Bay City, Goose Island, Crossover Channel, Aberdeen Port Dock, South Aberdeen, and Montesano tide gages. Low- and high-water lunar intervals; high-, low-, and mean-water levels; and range of tide profiles are presented in plate 5 for the spring tide condition. The maximum discrepancy in tidal range was in the order of 0.5 ft prototype (0.005 ft model). This maximum discrepancy occurred at the gage located at Montesano. This gage also reflected the greatest discrepancy for high- and low-water lunar intervals and high- and low-water levels. This gage was located very near the upstream model limits (plate 1) and the freshwater discharge point for the Chehalis River. Although tidal effects extend a considerable distance upstream from this gage location in the prototype, there was no supplemental provision for the passage of tidal flow at the upstream model limit. Since the tidal flow in this area is quite small, and since this area is a considerable distance upstream from any potential problem areas that might have been subject to model investigations, it was believed that provision for such tidal flow would have involved an unnecessary expense. The discrepancies between model and prototype tidal data at the Montesano gage are a direct result of the close proximity of this gage to the upstream model limit. Comparisons of model and prototype tidal data for the neap tide condition are presented in plates 6-9. The maximum discrepancy in tidal range was about 1.2 ft and was observed at the Montesano gage location.

Adjustment of currents

31. The objective of the model current adjustment was to obtain an accurate reproduction of prototype current velocities and distributions throughout the model. Prototype current velocity data were available at 18 stations, the locations of which are shown in plate 1. Prototype readings were made at the surface, quarter depth, middepth, three-quarter depth, and 2 ft above the bottom for a period of at least 25 hr at each station. As discussed above, no single simultaneous

survey of the entire estuary was made; and the model adjustment was made for only one tide from each of the 6-day metering periods. The neap and spring tides selected for reproduction in the model corresponded to the days on which current measurements were obtained on range 3 (sta 7, 8, 9, 10, 11, and 12). Since the tidal characteristics varied throughout each 6-day period it is obvious that current velocities observed on any particular day are not necessarily representative of those which would have been observed at the same station on any other day within the 6-day observation period. Thus, it was necessary to adjust at least the maximum prototype velocity observations in order that they would more nearly represent prototype conditions for the tides reproduced in the model. It was found that there was a reasonably good linear relation between tidal range and maximum velocity. The adjusted maximum prototype velocities are shown in the velocity verification plates (10-73) for those stations at which the prototype observations were made on a different tide than that reproduced in the model. Also shown for each current velocity station are the tide which was reproduced in the model and that which actually occurred during prototype data collection corresponding to the prototype current velocity data presented.

32. The procedure followed for adjustment of current velocities was to reproduce each of the two tidal and discharge conditions in turn and adjust the model roughness until the current velocities at each metering station were correctly reproduced in the model. The freshwater discharges used during the current velocity verification were obtained by averaging the inflows that occurred during each of the 6-day metering periods. Comparisons of model and prototype current velocities for all stations are presented in plates 10-73. Measurements obtained at half-hour intervals were plotted for both model and prototype, and smooth curves were drawn through the points. No attempt will be made to discuss each comparison of prototype and model measurements, but the agreement obtained throughout the model is considered to be very satisfactory.

Salinity Verification

33. The objective of the model salinity adjustment was to obtain an accurate reproduction of vertical and lateral distribution of prototype salinities throughout the model. Reproduction of prototype salinity phenomena in the model required the maintenance of the proper salinity in the ocean water-supply system and the establishment of the proper mixing environment. Because prototype salinity data obtained at stations near the mouth of the estuary were obviously in error, it was decided to use a model ocean salinity that was representative of salinities known to occur near the entrance to most west coast estuaries (33.0 ppt). The prototype salinity data at sta 1, 6, and 10 for the neap tide condition and those at sta 1 for the spring tide conditions are omitted from this report because they were obviously erroneous. Prototype observations at these locations were all made with the same meter. Salinity data at other times and stations obtained with the same meter were also obviously in error, but they were not used in the model verification. Salinity observations were made at hourly (prototype) intervals in both the model and prototype. These data were plotted and smooth curves were drawn through the points and are compared with corresponding prototype curves in plates 74-105.

34. The agreement demonstrated between model and prototype is considered excellent. It is pointed out that no additional adjustment of the model was necessary to obtain the agreement shown in plates 74-105. This substantiates the model adjustment of tides and currents and indicates that the upland fresh water was being properly mixed with salt water from the ocean supply.

Entrance Area Fixed-Bed Shoaling Verification

35. The entrance area fixed-bed verification involved the reproduction of the prototype shoaling pattern throughout the entrance area. The basic objective of the model shoaling verification was to identify a synthetic sediment that would move and deposit under the influence of

model forces in the same manner that the natural sediments move and deposit under the influence of natural forces. In the process of identifying a suitable model sediment, a great number of variables were involved and each had to be resolved by trial and error. The most significant variables included: (a) shape, size, gradation, and specific weight of the artificial sediment; (b) method, location, duration, and quantity of artificial sediment injection; (c) height and direction of waves; (d) magnitude of tide range; (e) length of model operation; and (f) readjustment of model roughness. The final adjustment was accomplished using a granulated nylon material with a specific weight of 1.13 to 1.15 and a grain size of about 1/8 in. by 1/8 in. (cylinders). A spring tide was reproduced in the model with a mean freshwater discharge, and waves were generated alternately from the west and southwest. Because of the distortion of the model scales, it was not possible to reproduce waves in the model that represented prototype conditions. At the start of the shoaling test, 100,000 cc of the above material was injected into the model over a period of five cycles beginning at hour 22 of cycle 1. During cycles 1 and 2, 5000 cc was placed in the model at hour 22 along a line represented by the east boundaries of shoaling sections 18, 19, C-7, and 20 (plate 2); 10,000 cc was placed in the model along this same line at hour 9.5; and 5000 cc was placed in the model along a line running north and south through the middle of section 19 at hour 14. During cycles 3, 4, and 5, 5000 cc was placed in the model at hour 22 along a line represented by the east boundaries of shoaling sections 18 and 19; 10,000 cc was placed in the model along this same line at hour 9.5; and 5000 cc was placed in the model at hour 14 along a north-south line represented by the center line of section 19. It was necessary to operate two wave machines in the model ocean to simulate the effects of wave energy on the resuspension and movement of the model sediment. Wave machine 1 was oriented so that waves were generated from the west; wave machine 2 was oriented so that waves were generated from the southwest. The wave heights and periods did not represent any particular prototype waves, but they were adjusted to simulate the degree of agitation required so the model shoal materials could

be moved and deposited by the tidal currents. Wave machine 1 was operated between hours 2 and 17; wave machine 2 was operated between hours 20 and 2. This wave machine operating procedure was repeated during each of the five injection cycles. At the end of the test, the material was recovered from individual sections (plate 106) and measured volumetrically.

36. Scour and fill patterns that developed in the prototype during the period 1965-1969 are shown in plate 107. Only the fill patterns indicated in this plate were used as a basis for the entrance shoaling verification since scour cannot be reproduced in a fixed-bed model. The relative shoaling pattern achieved in the model is shown in plate 108. The actual volumes of material retrieved from individual sections are shown in table 1 along with the respective percentages of the total amount injected and recovered.

Limitations of the Accuracy of Model Measurements

37. Measurements of tidal elevations in the model were made with point gages graduated to 0.001 ft, or 0.1 ft prototype. The limitations of the current velocity meters used in the model should be considered in making close comparisons between model and prototype velocity data. The center line of the meter cup was about 0.05 ft above the bottom of the frame; therefore, bottom velocity measurements in the model were actually obtained at a point 5.0 ft (prototype) above the bottom, instead of about 2.0 ft as in the prototype metering program. The model velocities were determined by counting the number of revolutions in a 10-sec interval (which represented a period of about 8 min in the prototype), as compared with about a 1-min observation in the prototype. The horizontal spread of the entire meter cup wheel was about 0.11 ft in the model, representing about 55 ft in the prototype, as compared with less than 1.0 ft for the prototype meter. Thus, the distortion of area (model to prototype) results in comparison of prototype point velocities with model mean velocities for a much larger area. The same is true for the vertical area, since the height of the meter cup was about 0.04 ft

(4.0 ft prototype) as compared with only a few inches for the prototype meter.

38. All model salinity measurements presented in this report were made with a salinity meter (conductivity type) and are considered to be accurate within 0.5 ppt in the higher ranges and 0.2 ppt in the lower ranges. The model samples were collected at the bottom, middepth, and surface elevations. The elevations of the bottom and middepth samplers were fixed in the model and were not allowed to vary with the tide as was the surface sampler. Simultaneous water samples were drawn into vials from the three elevations by means of a vacuum system, whereas the prototype salinities were measured in place at successive depths. Similar to the model velocity data, the model salinity data also represent an average over a much larger prototype area, since the vacuum sampling system used in the model drew the sample from a radius of about 1/2 to 1 in. (80 ft in the prototype). The accuracy with which the model could be expected to duplicate salinities from cycle to cycle for identical conditions appears to be about ± 3 percent.

Discussion of Results of Verification Tests

39. Agreement between model and prototype phenomena, as evidenced by the results of hydraulic and salinity verification data, appears to be excellent. The model was considered to be sufficiently similar to its prototype to be confidently utilized in quantitative studies of the effects of proposed improvement plans on hydraulic phenomena and salinity intrusion.

40. In fixed-bed shoaling tests it is not possible to reproduce bed scour. Should any significant scour areas develop in the prototype as the result of some new construction, they would create a source of new sediments that could cause significantly increased shoaling in other areas that would not be predicted from the model results. The accuracy of the model shoaling tests is considered to be about ± 10 percent, since that is about the limit of accuracy of repeating identical tests.

PART IV: BASE TEST RESULTS

41. In order to evaluate the effects of the proposed improvement plans, it was first necessary to establish hydraulic, salinity, shoaling, surface current pattern, and dye dispersion "base tests" that depicted, respectively, the characteristics of these conditions throughout the model for existing conditions. Thus, a test in which no improvement plan was installed in the model is referred to as a base test, since its results constitute a basis of comparison for determining the effects of improvement plans. The model base tests were conducted with model conditions of a mean tide, a source salinity concentration of 33.0 ppt, and a total freshwater discharge of 11,400 cfs. The discharges at individual inflow points were: Chehalis River, 6300 cfs; Hoquiam River, 970 cfs; Wishkah River, 420 cfs; Humptulips River, 2750 cfs; and Elk River, 960 cfs. Prior to data collection of any type, the model was operated for a sufficient period of time to achieve a condition of dynamic salinity stability. The procedure for starting operation of a tidal model utilizing salt water is developed during the verification phase of the study and thereafter is followed exactly. The initial salinity concentrations are artificial; and the model must be operated for a period of time to allow salinities to reach stable values with respect to time, depth, and location. It was found for the Grays Harbor model that the best procedure was to flood the entire model with ocean water to the elevation of mhhw, then to turn on the freshwater inflow weirs and allow the model to operate until salinity stability was achieved. It was necessary to operate the model for about five tidal cycles (about 2.5 hr) before relatively stable conditions existed, after which data collection could be initiated. To ensure a higher degree of salinity stability when obtaining salinity measurements, salinity samples were not taken until the model had operated for at least 10 cycles (about 4 hr).

42. The locations of all stations monitored during base test conditions are shown in plate 109. Tide gage locations are identical with those in the verification, except that two gages were added in the entrance area (Ocean and Westport "A") to more accurately define tidal

changes in this area resulting from any tests investigated. The verification of current velocities and salinities was based on the results of data obtained at 18 locations throughout the estuary (see plate 1). For obvious reasons, none of these stations could be located along the navigation channel center line. The coverage was not sufficient, particularly in the entrance area, to give a complete composite picture of the effects of future improvement plans to be tested; therefore, the station location and numbering scheme used during the verification phase of the model study was abandoned during the testing phase for a sampling scheme that would better define the effects of proposed plans. These sampling stations were numbered 19-58 in order to avoid confusion with the verification stations (1-18). Several stations were added after the above scheme was adopted and are postfixed with a letter to the number of the nearest station.

Tides

43. Base test tidal height data were obtained at nine locations throughout the model. The data, collected at half-hour intervals, were plotted and smooth curves were drawn through the points. The locations of tide stations are shown in plate 109 and data are presented in plates 110-112.

Current Velocities

44. Base test current velocity data were obtained at 44 locations throughout the model. Data were collected at the surface, middepth, and bottom elevations at half-hour intervals at all locations where the depth of water was sufficient. At the few stations that were located in shallow water, middepth measurements were not made. The half-hour measurements were plotted, and smooth curves were drawn through the points. The locations of current velocity stations are shown in plate 109, and the current velocity data are presented in plates 113-156.

Salinities

45. Base test salinity data were obtained at 41 locations throughout the model. Water samples were collected at the surface, mid-depth, and bottom elevations at hourly intervals. The salinity concentrations were determined with a salinity meter and were later plotted and smooth curves were drawn through the points. The locations of salinity stations are shown in plate 109, and the salinity data are presented in plates 157-197.

Entrance Shoaling

46. The final results for the verification of shoaling in the entrance area, discussed in paragraphs 35 and 36 of this report, also served as the shoaling base test, since there were no plans installed in the model during the verification tests. The location of the shoal sections, prototype data used as the basis for verification, and final model shoaling verification results are shown in plates 106, 107, and 108, respectively. The volumes of shoaling material retrieved from individual sections are presented in table 1. The shoaling test technique developed for this model provided only qualitative information concerning entrance area shoaling. It was possible to identify areas of heavy shoaling and to compare the merits of various plans on the basis of the relative quantities of shoaling in the entrance area; however, it was not possible to relate quantities of model shoaling to prototype quantities.

Dye Dispersion

47. Model tests were made to determine the flushing rate and dispersion characteristics of the estuary for two very generalized sources (one upstream and one at the entrance) of materials entering the estuary. Test procedures consisted of introducing one type of conservative fluorescent dye (Pontacyl Brilliant Pink) at a point near Cosmopolis and

another type (Uranine) near the outer end of the south jetty. Four liters of Pontacyl Brilliant Pink dye with an initial concentration of 10,000,000 ppb and the density of fresh water of 1.0 was injected into the model near Cosmopolis at the middepth elevation over a complete tidal cycle beginning at hour 0 of cycle 1. Four liters of Uranine dye with an initial concentration of 10,000,000 ppb and the density of sea water was injected into the model near the outer end of the south jetty at the bottom of the channel from hour 20 (llw) of cycle 1 until hour 2 (lhw) of cycle 2. Each dye mixture was contained in a glass standpipe and was introduced at a constant rate throughout the injection period through a 1/4-in. copper tube oriented at the proper elevation. Prior to initiating dye injection, the model was operated for four tidal cycles to establish salinity stability throughout the model.

48. The locations of the two dye release points are shown in plate 109. During the dye dispersion tests, water samples were withdrawn from the model for subsequent analysis for dye concentration. The samples were taken at 41 locations with the multidepth sampler described in paragraph 14. Samples were obtained at surface, middepth, and bottom elevations at the times of hhw slack current (hour 13) and llw slack current (hour 20) over a period of 16 tidal cycles. Concentrations of the samples were measured by means of a Turner Model III fluorometer.

49. Plots of dye concentration as a function of time at typical stations for the Cosmopolis dye release are shown in plates 198-202. Smooth curves have been drawn through the data points. Plots of dye concentration profiles along the navigation channel after 5 and 12 tidal cycles for the Cosmopolis dye release are shown in plates 203 and 204, respectively. Similar plots of concentration histories and profiles for the south jetty dye release are presented in plates 205-211. Table 2 presents the dye concentrations for high- and low-water slacks at surface, middepth, and bottom elevations at all stations for both the Cosmopolis and south jetty dye releases.

Current Pattern Mosaics

50. Surface current pattern mosaics were made of the entrance area for use in evaluating proposed channel realignments, effectiveness of dikes, groins, etc. The mosaic also provides a means for current velocity analysis in areas too shallow for measurements with the velocity meter. The mosaics included in this report cover only the entrance area and a portion of the inner harbor; however, it was anticipated that as the model study progressed this partial mosaic would be expanded to include the entire estuary.

51. The mosaics were prepared from time-exposure photographs of confetti floating on the water surface. A bright light was flashed immediately before the camera lens was closed, resulting in a bright spot at approximately the end of each confetti streak which indicates the direction of flow. Current velocities can be determined from the photographs by measuring the lengths of the confetti streaks and comparing the lengths with the velocity scale presented in each mosaic. Photographs were taken at hourly (prototype) intervals throughout a complete tidal cycle (24.84 hr). Surface current pattern mosaics for base test conditions are presented in photos 1-25.

Table 1
Entrance Shoaling
 Base Test Conditions

Section No.	Volume Retrieved cc*	Percent Retrieved	Percent of Total Injected	Section No.	Volume Retrieved cc*	Percent Retrieved	Percent of Total Injected
1	10	0.01	0.01	31	1,070	1.28	1.07
2	1,125	1.36	1.12	32	15	0.02	0.02
3	220	0.26	0.22	33	0	0.00	0.00
4	1,230	1.47	1.23	34	2,175	2.62	2.18
5	5,680	6.83	5.68	35	0	0.00	0.00
6	10	0.01	0.01	36	0	0.00	0.00
7	20	0.02	0.02	37	1,810	2.18	1.81
8	790	0.95	0.79	38	3,890	4.68	3.89
9	3,750	4.50	3.75	39	5	0.00	0.00
10	1,930	2.32	1.93	40	5	0.00	0.00
11	3,595	4.31	3.59	41	0	0.00	0.00
12	15	0.02	0.02	42	0	0.00	0.00
13	3,960	4.76	3.96	43	6,570	7.50	6.57
14	3,535	4.26	3.54	44	0	0.00	0.00
15	5,985	7.19	5.98	45	0	0.00	0.00
16	3,440	4.13	3.44	46	0	0.00	0.00
17	1,465	1.76	1.46	47	835	1.00	0.84
18	495	0.59	0.49	48	2,710	3.27	2.71
19	2,440	2.94	2.44	49	880	1.06	0.88
20	3,070	3.69	3.07	C-1	15	0.02	0.02
21	25	0.03	0.03	C-2	0	0.00	0.00
22	25	0.03	0.03	C-3	0	0.00	0.00
23	1,210	1.46	1.21	C-4	15	0.02	0.02
24	965	1.16	0.96	C-5	3,795	4.56	3.79
25	340	0.40	0.34	C-6	885	1.05	0.88
26	10	0.01	0.01	C-7	1,110	1.34	1.11
27	2,435	2.94	2.44	C-8	3,035	3.65	3.04
28	2,190	2.64	2.19	C-9	2,245	2.69	2.24
29	1,800	2.16	1.80	C-10	340	0.42	0.34
30	15	0.02	0.02	C-11	15	0.01	0.01
				Total	83,200	100.00	83.20

Note: Total volume injected was 100,000 cc.

* Average of two identical runs.

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 0

REFERENCE SCALE
100 FT.
100 M.



6

PHOTO 1

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 1

Y.E. SIGHT SCALE
1000 ft.
100 ft.



PHOTO 2

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 2



PHOTO 3

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 3

400' SWALE
LAWSON HILL



PHOTO 4

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 4

VERTICAL SCALE
1000 ft.
1000 ft.



PHOTO 5

SURFACE CURRENT DIRECTIONS
BASE TEST - HOU

VELOCITY SCALE
per 1/2 sec
f/s



PHOTO 6

SL. RENT DIRECTIONS
EST - HOUR 6

ALL DIRECTIONS
EST - HOUR 6



SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 7

Vel. 20 ft. scale
10 sec. interval

4"



PHOTO 8

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 8

SE: OGTY SCALE
1000' 1000'
100' 100'



PHOTO 9

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 9

FIGC - SCALE
100 ft.
1000 ft.



19

PHOTO 10

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 1C



SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 11



PHOTO 12

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 12



PHOTO 13

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 13



PHOTO 14

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 14



PHOTO 15

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 15



PHOTO 16



SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 16

TOUCHY SCALE
1 mm = 1' 10"

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 17



PHOTO 18

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 18

STUDY SITE
TEST SITE



PHOTO 19

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 19

Velocity Scale
1000 ft/min



SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 20

ELOCITY SCALE
100 ft/min

60

PHOTO 21



SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 21

Velocity Scale
1000 ft/min



PHOTO 22

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 22

VELOCITY SCALE
0.05
1.00
2.00



100

PHOTO 23

SURFACE CURRENT DIRECTIONS
BASE TEST - HOUR 23

VELOCITY SCALE
0.000 0.001 0.002
FPM



PHOTO 24

113

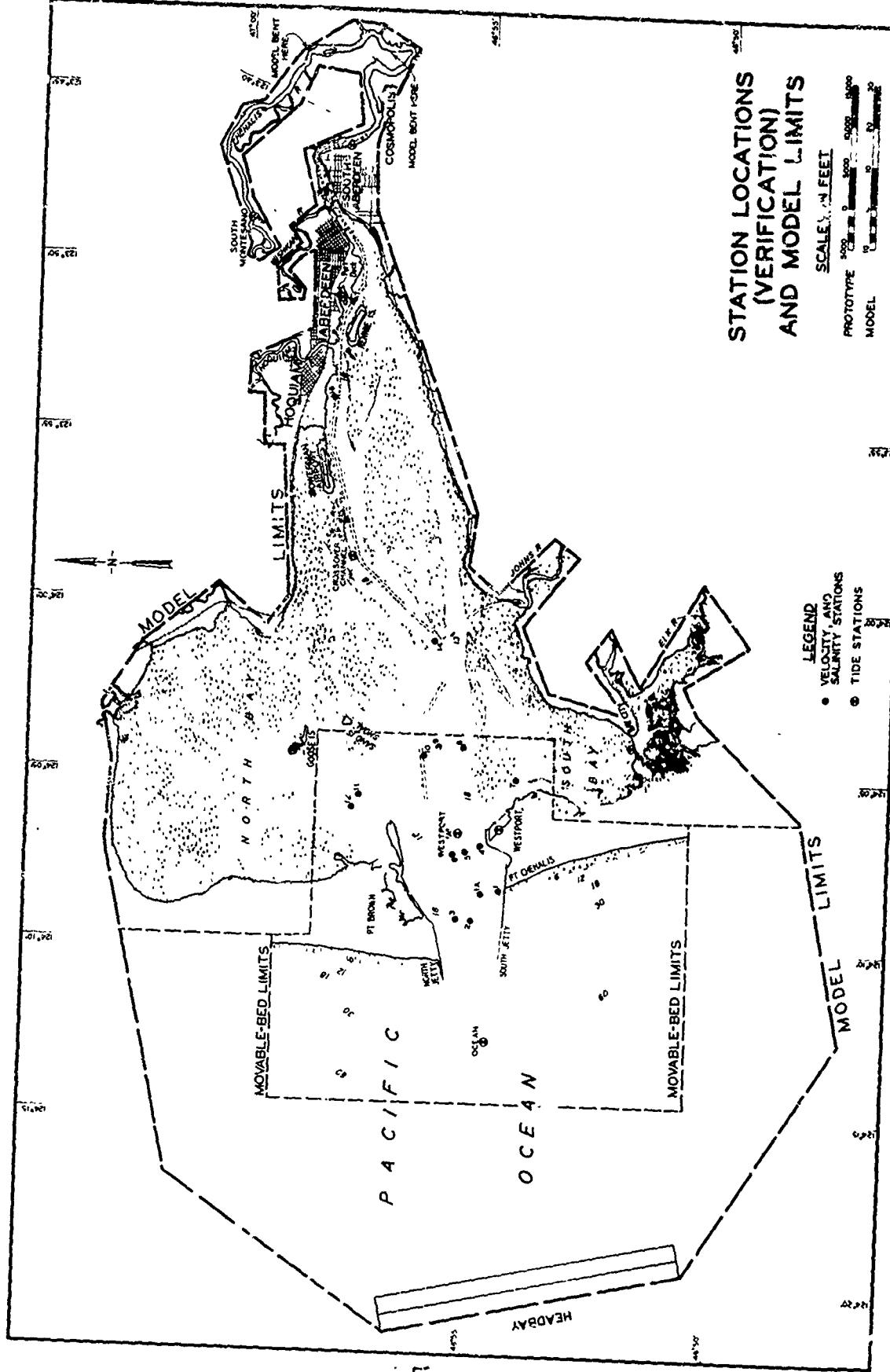
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BASE TEST - HOUR 24

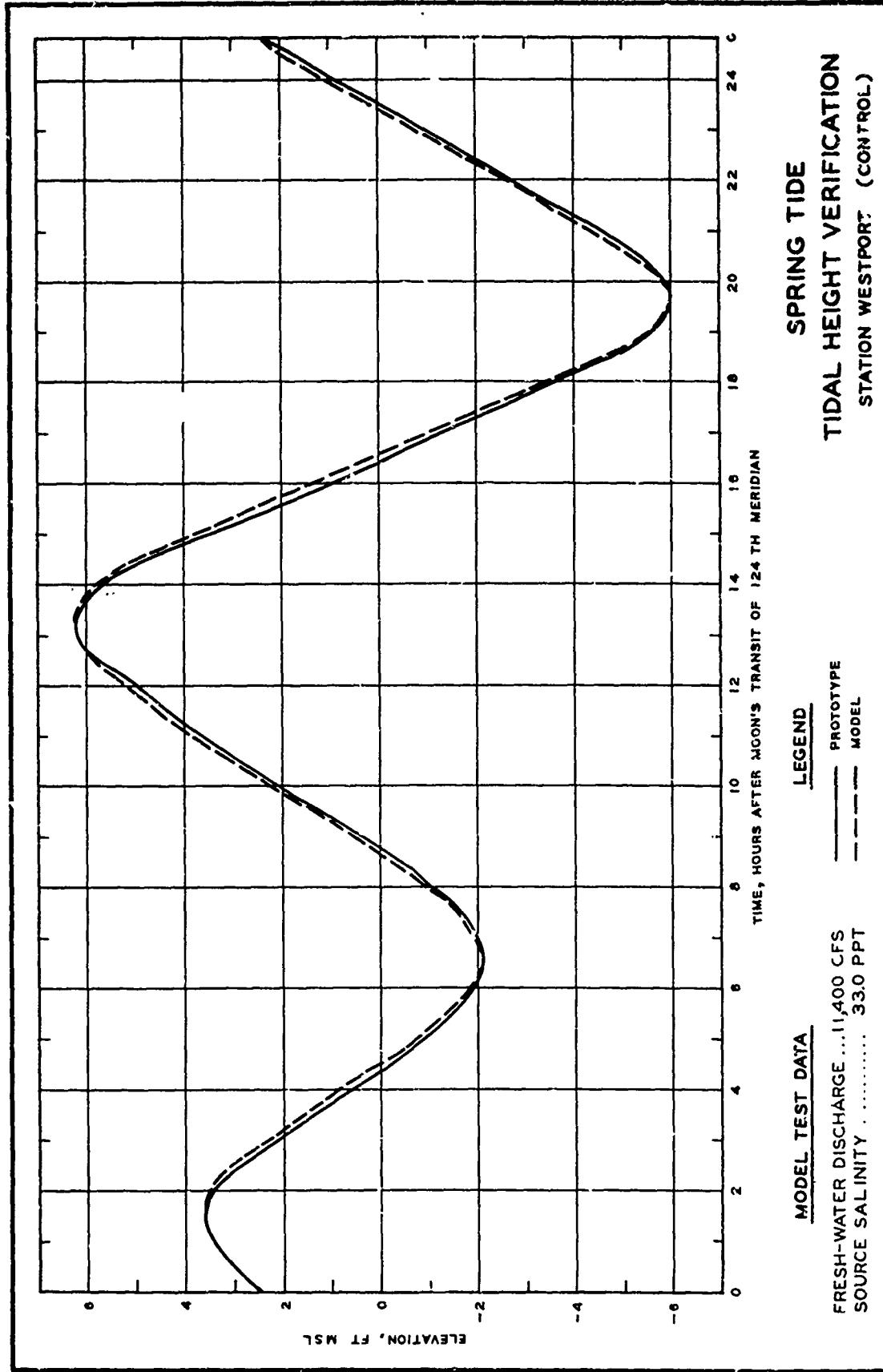


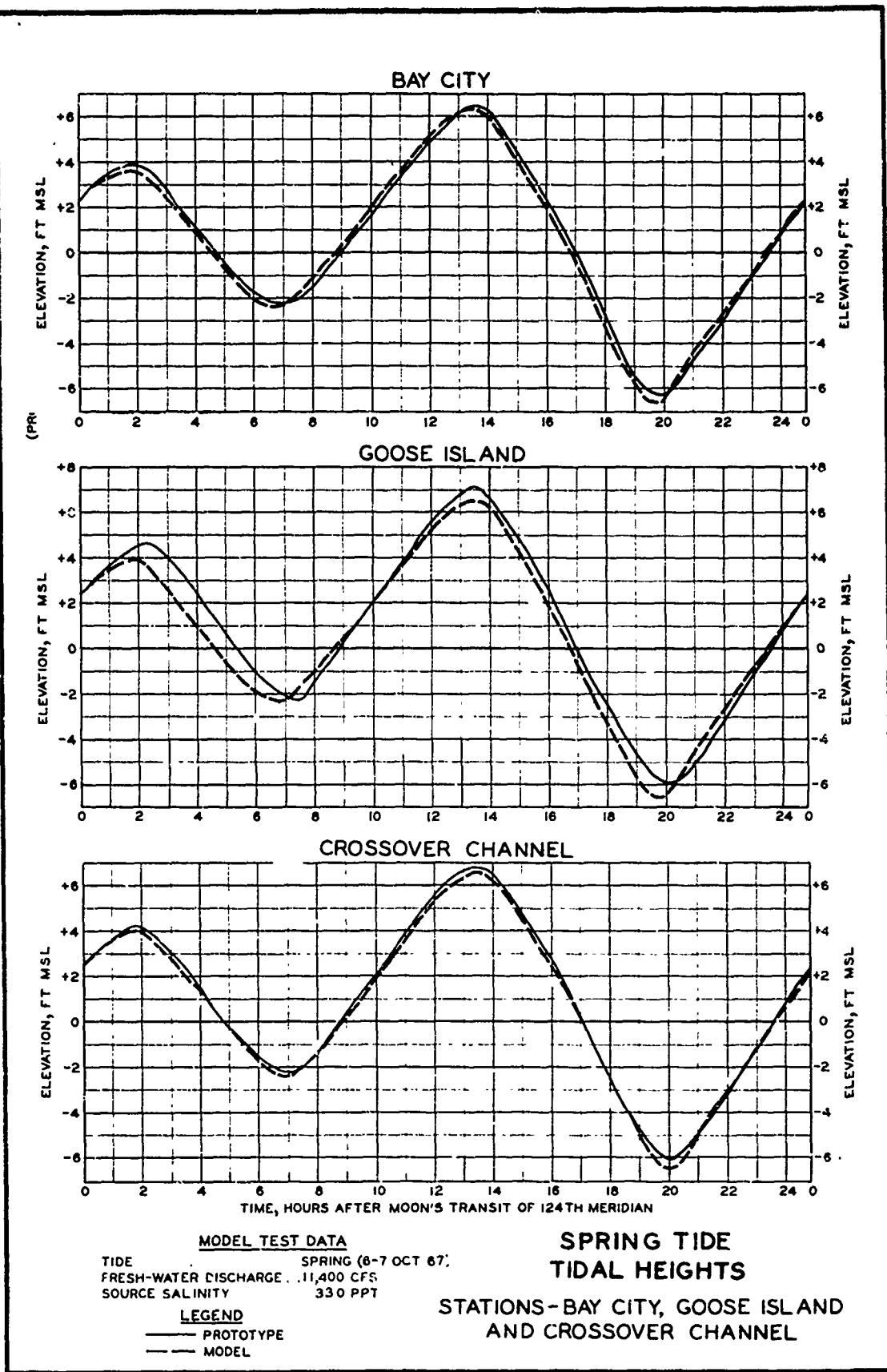
STATION LOCATIONS
(VERIFICATION)
AND MODEL LIMITS

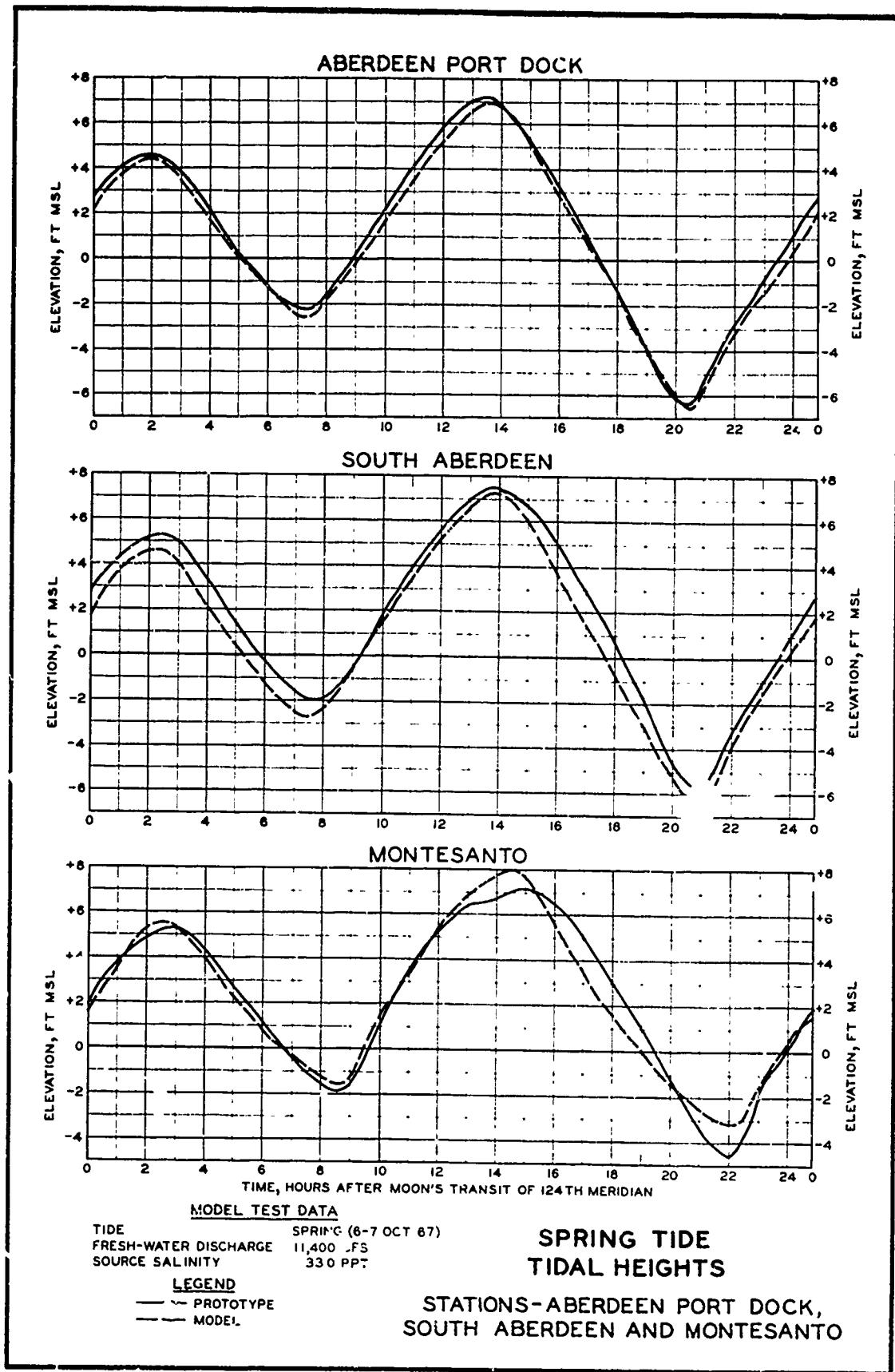
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PROTOTYPE 5000 5000 5000
MODEL 50 50 50

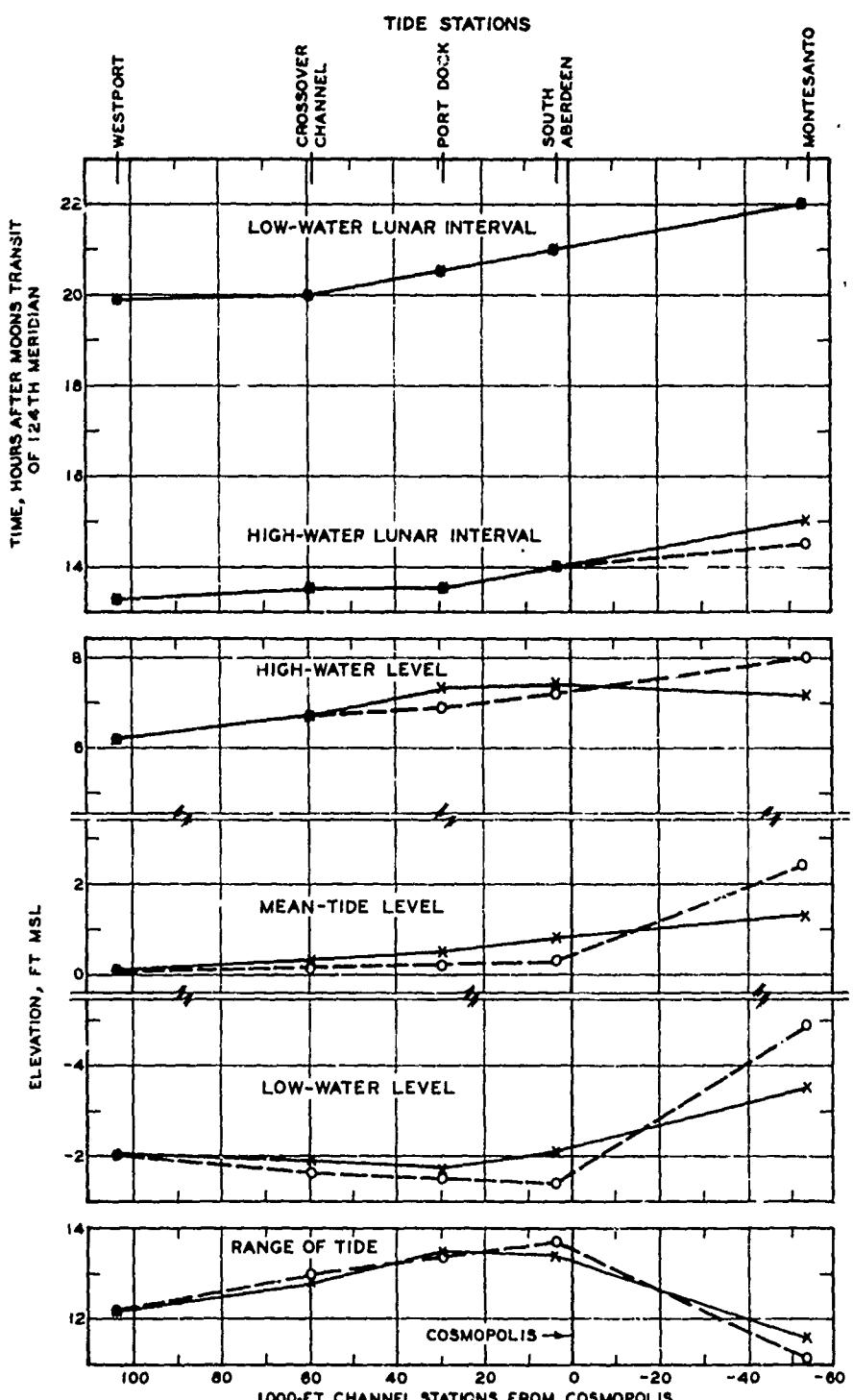
LEGEND
• VELOCITY AND
SALINITY STATIONS
◎ TIDE STATIONS











MODEL TEST DATA

FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 33.0 PPT

LEGEND
— PROTOTYPE
- - - MODEL

TIDAL OBSERVATIONS
SPRING TIDE (6-7 OCT '67)

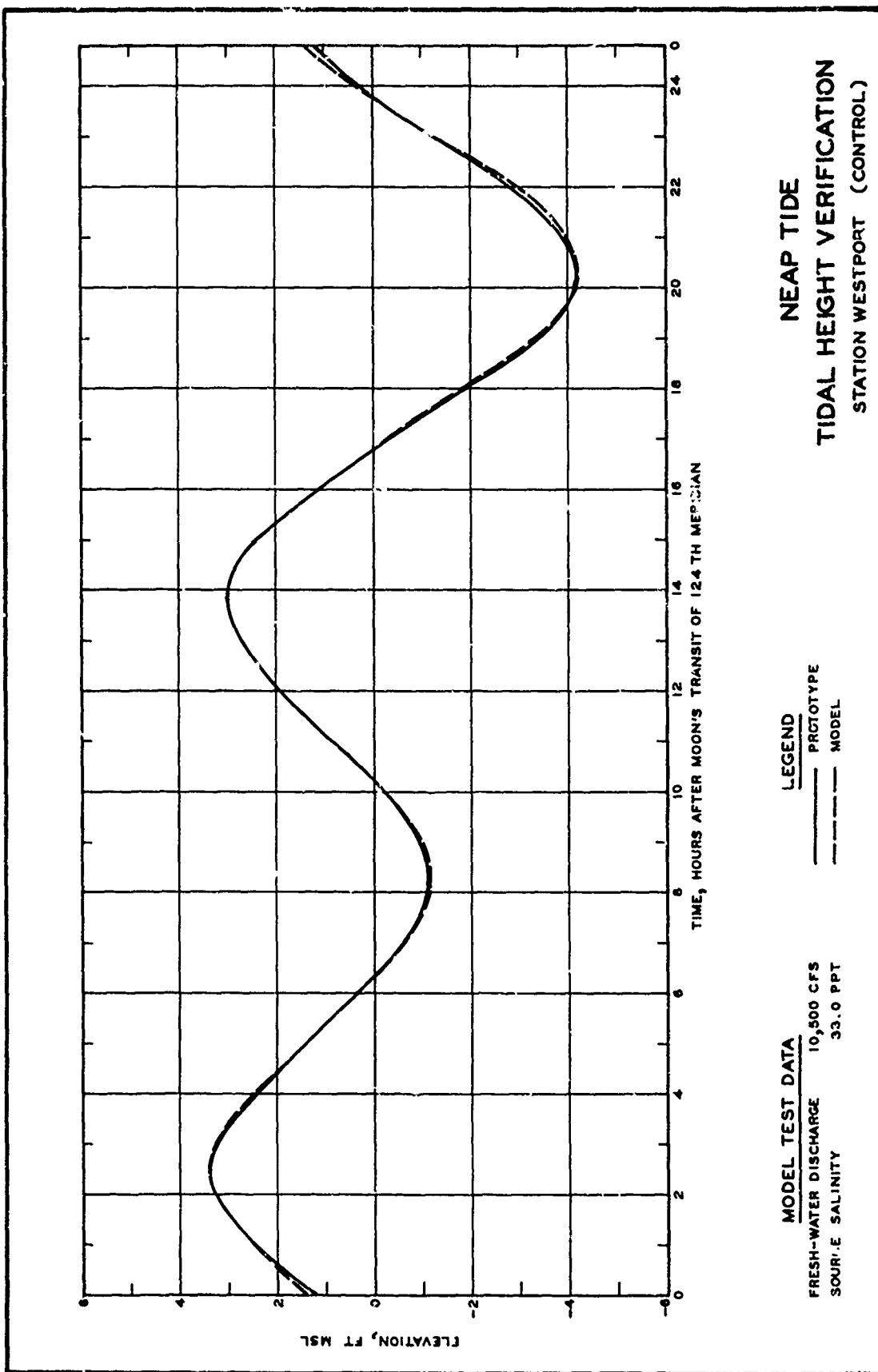
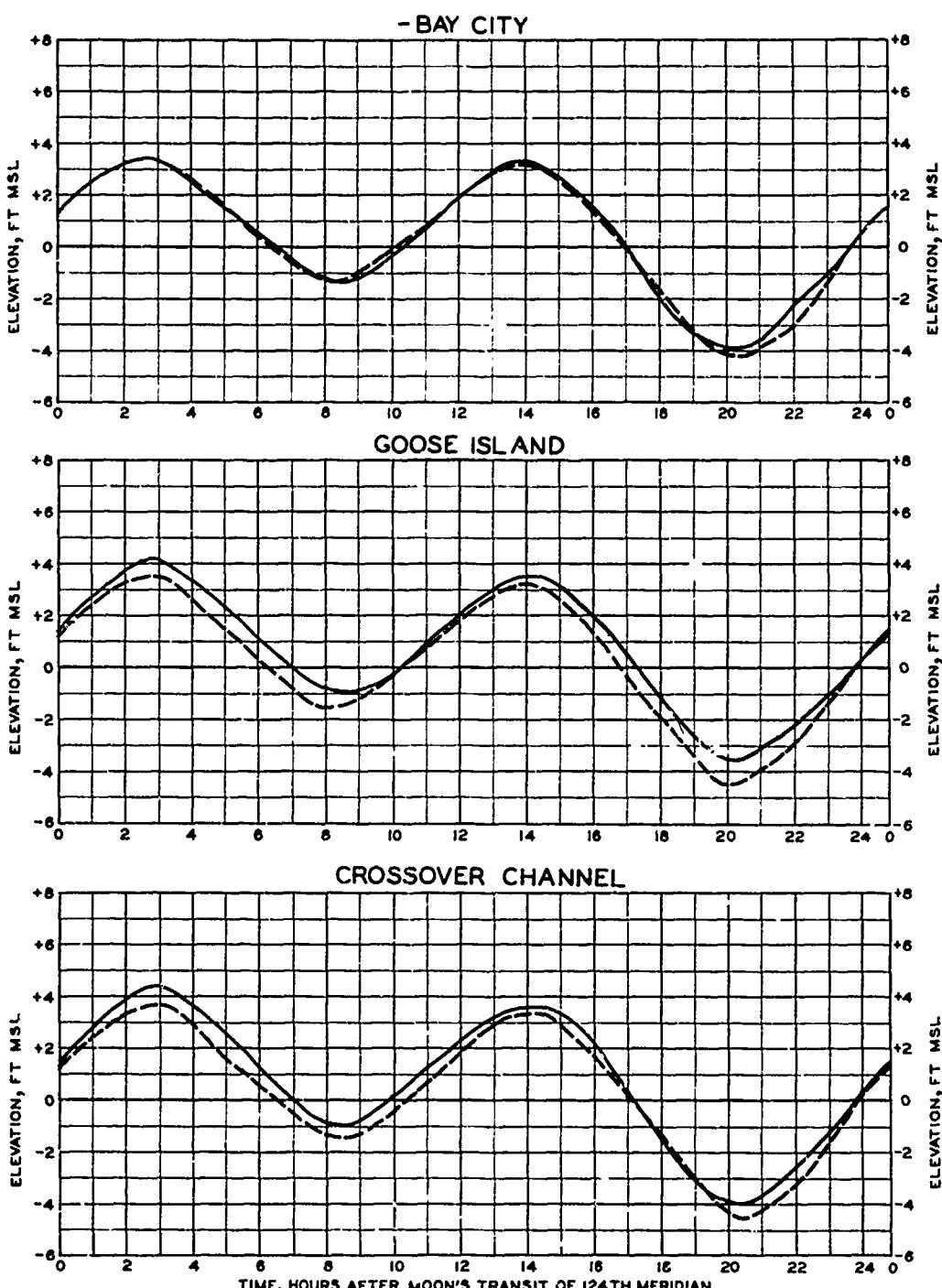


PLATE 6

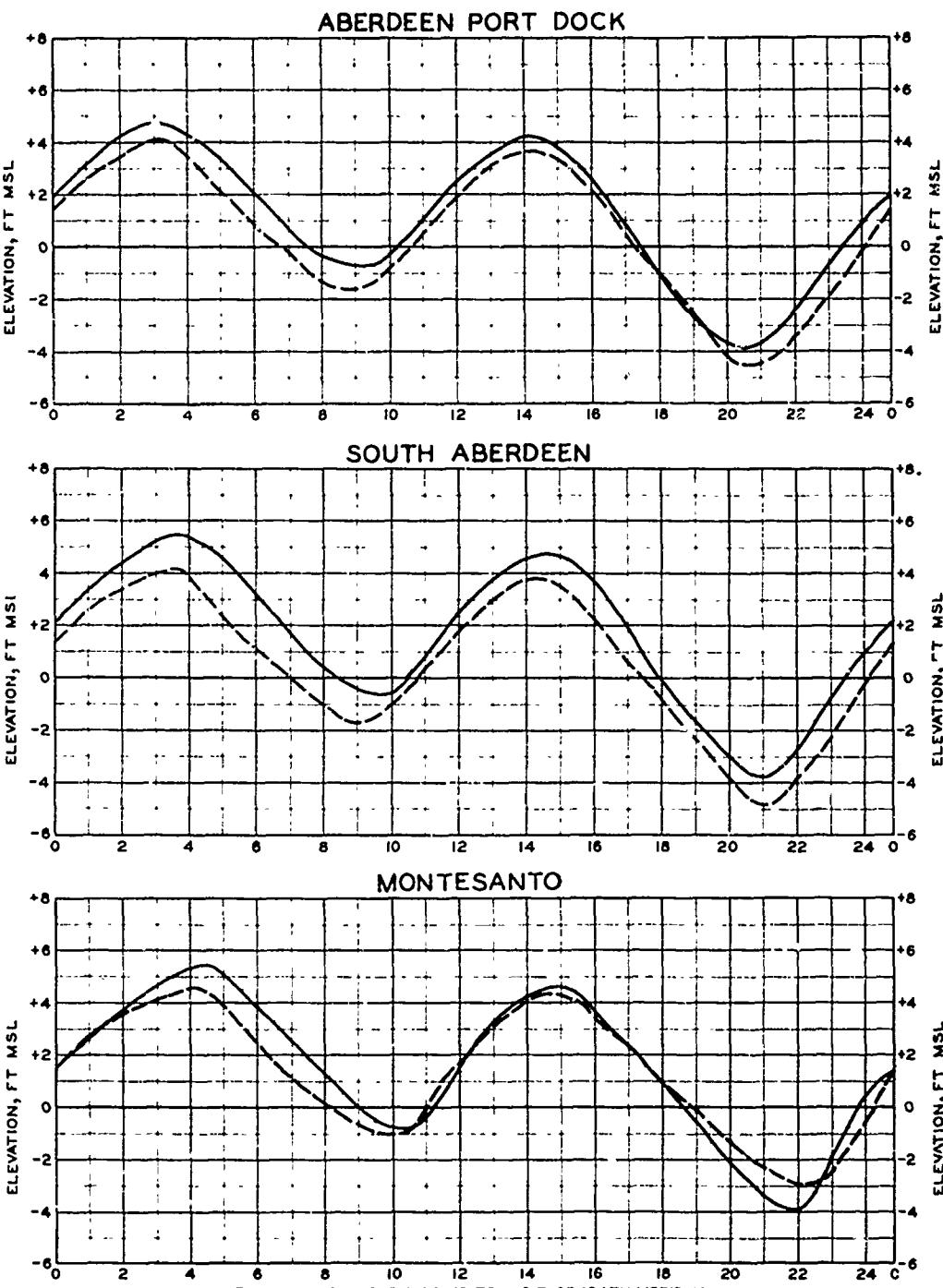


MODEL TEST DATA

TIDE NEAP
 FRESH-WATER DISCHARGE . 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND
 — PROTOTYPE
 - - - MODEL

**NEAP TIDE
 TIDAL HEIGHTS**
 STATIONS-BAY CITY, GOOSE ISI AND
 AND CROSSOVER CHANNEL



MODEL TEST DATA

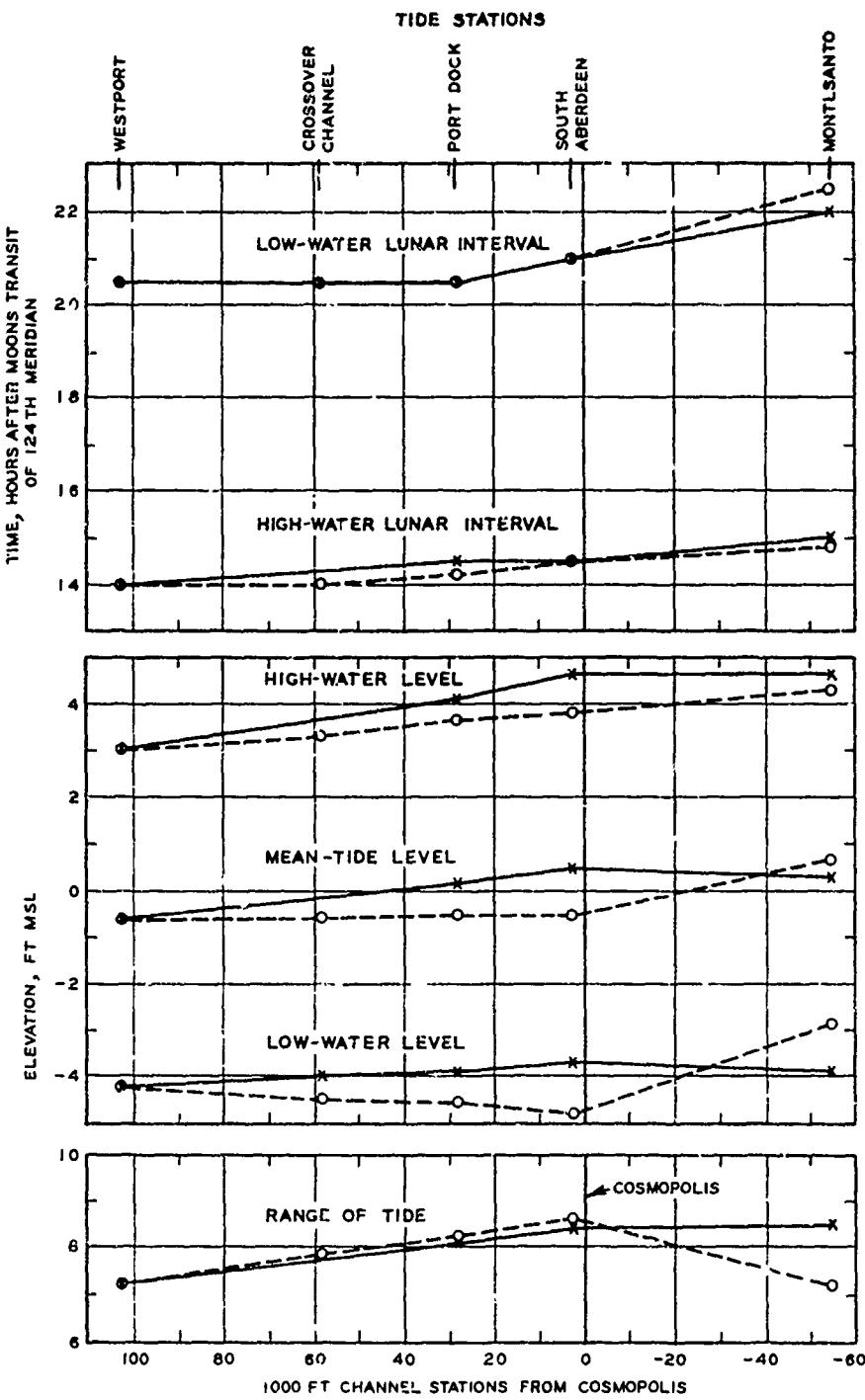
TIDE NEAP
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND

- PROTOTYPE
- MODEL

**NEAP TIDE
TIDAL HEIGHTS**

STATIONS - ABERDEEN PORT DOCK,
SOUTH ABERDEEN AND MONTE SANTO



MODEL TEST DATA
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY 330 P.T.

LEGEND
 — PROTOTYPE
 - - - MODEL

TIDAL OBSERVATIONS
 NEAP TIDE (13-14 OCT '67)

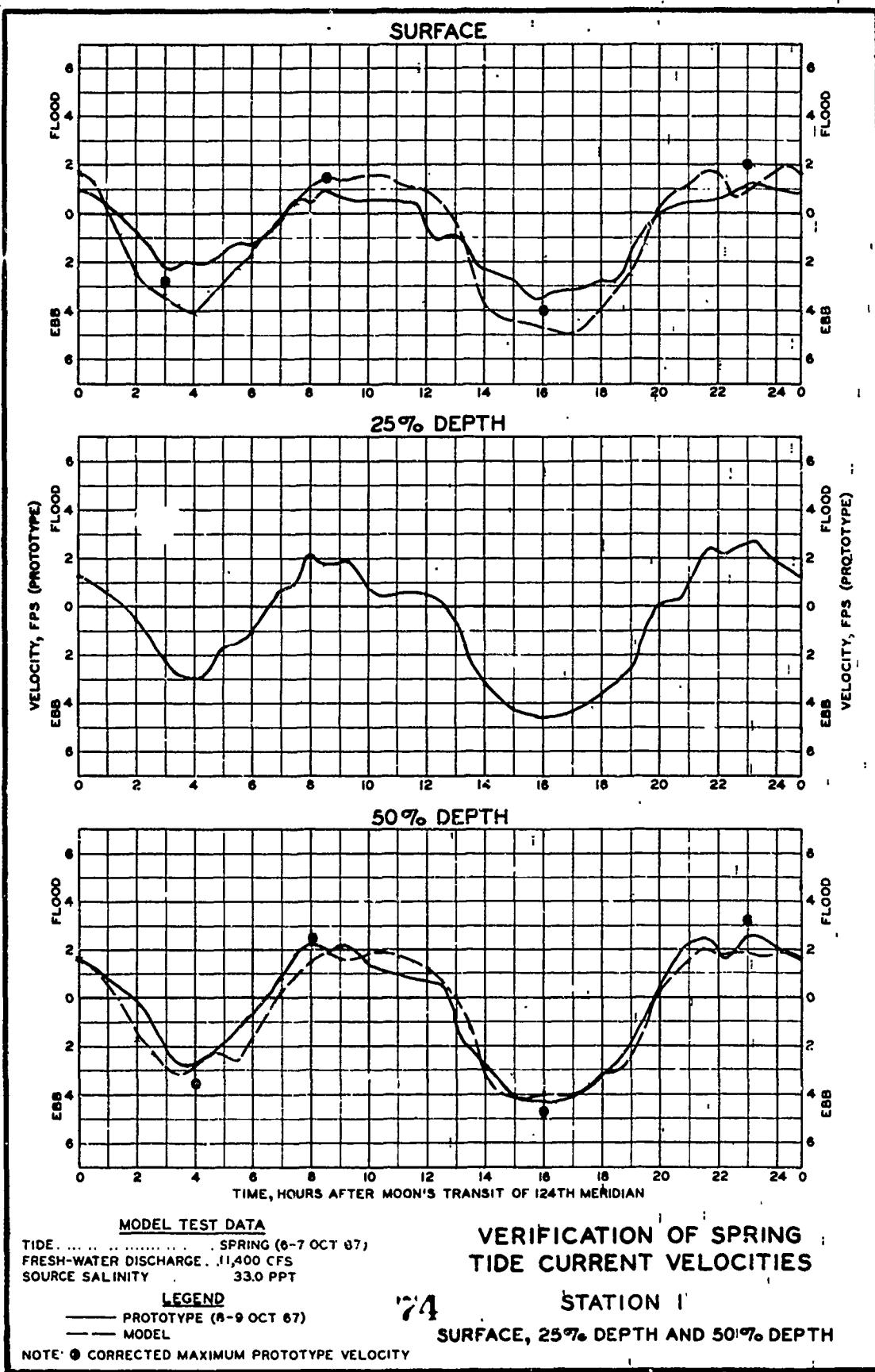
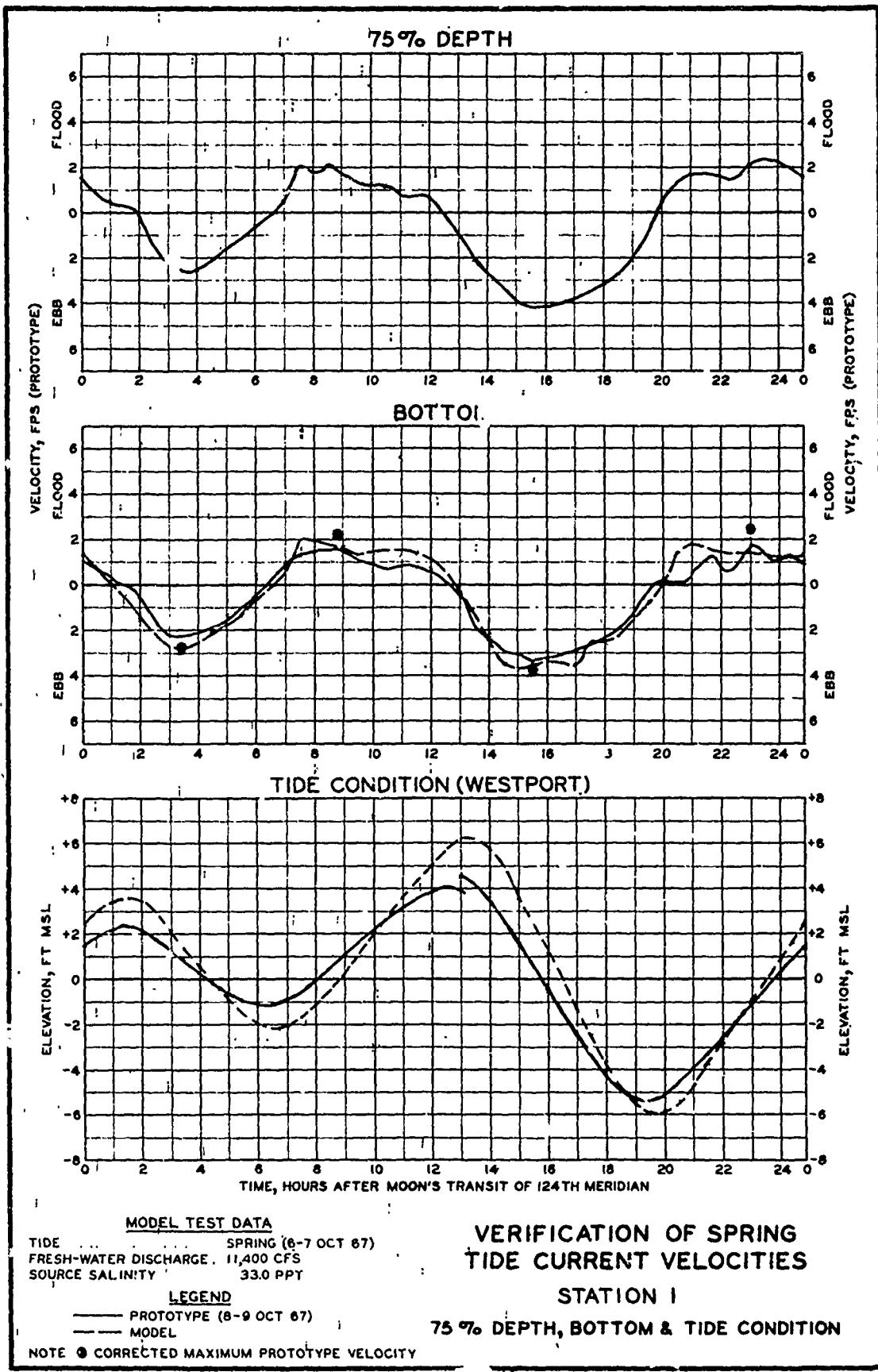
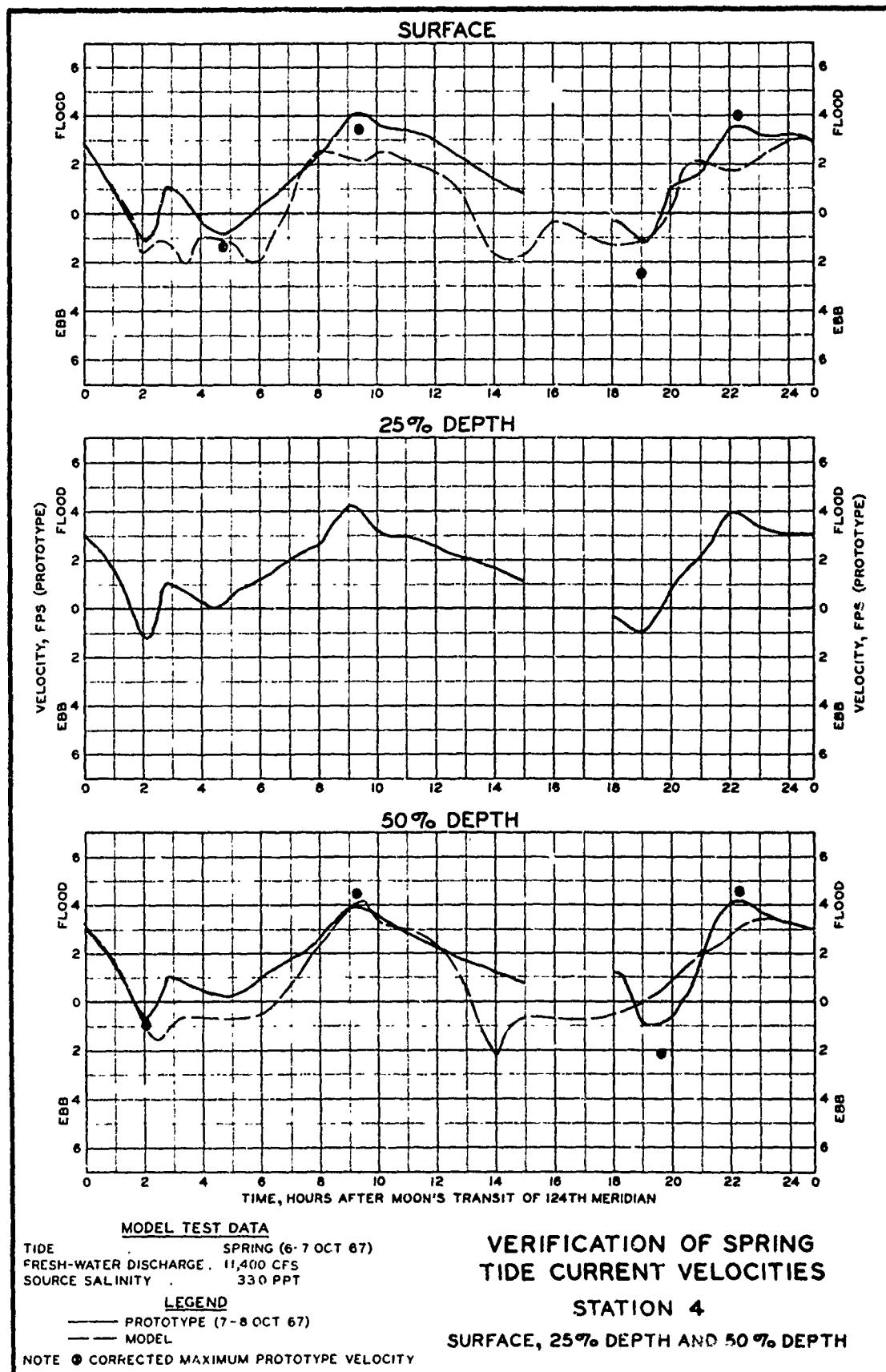
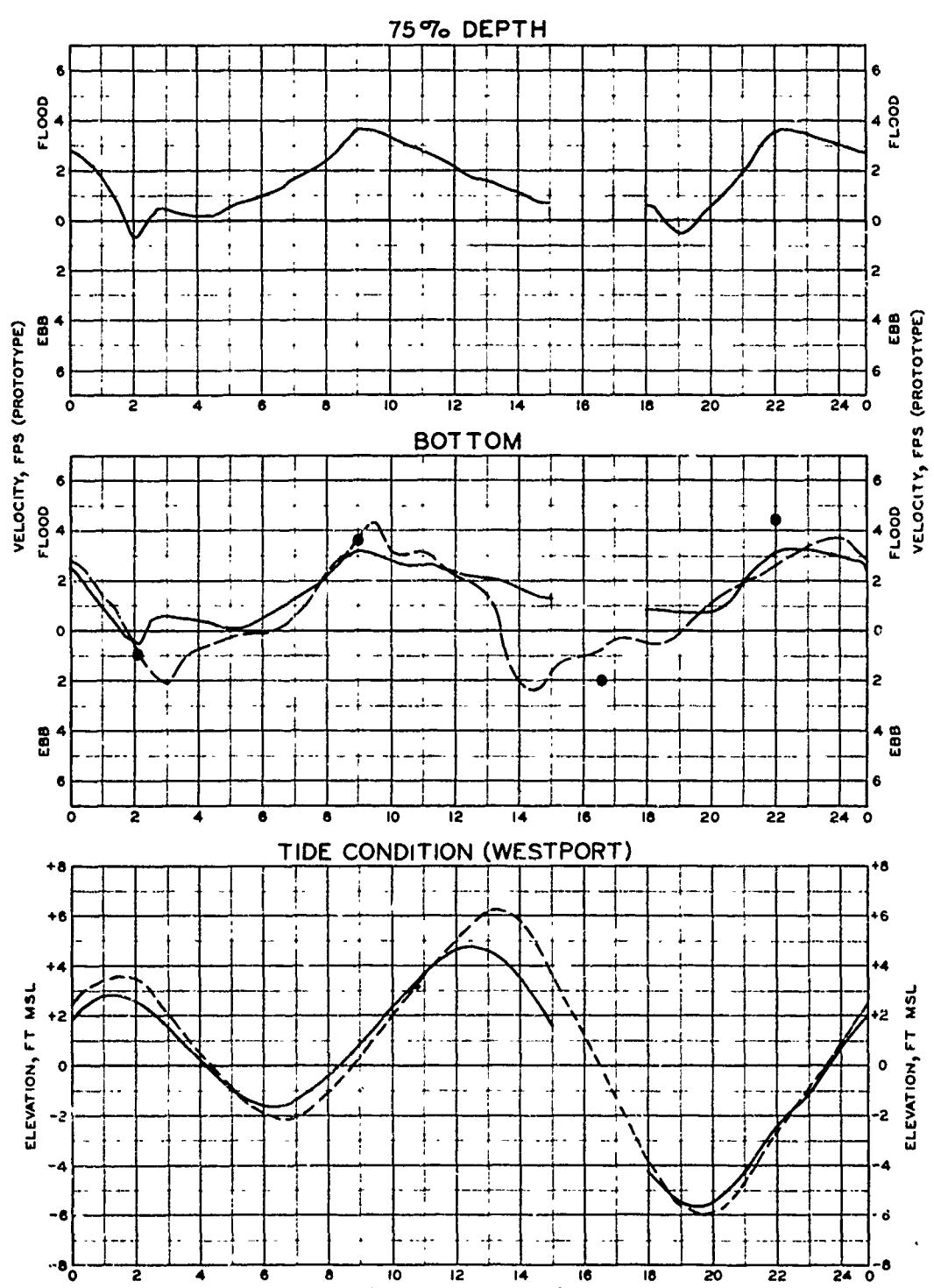


PLATE 10







MODEL TEST DATA

TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— PROTOTYPE (7-8 OCT 67)
 - - MODEL
 NOTE. • CORRECTED MAXIMUM PROTOTYPE VELOCITY

**VERIFICATION OF SPRING
TIDE CURRENT VELOCITIES**

STATION 4

75% DEPTH, BOTTOM & TIDE CONDITION

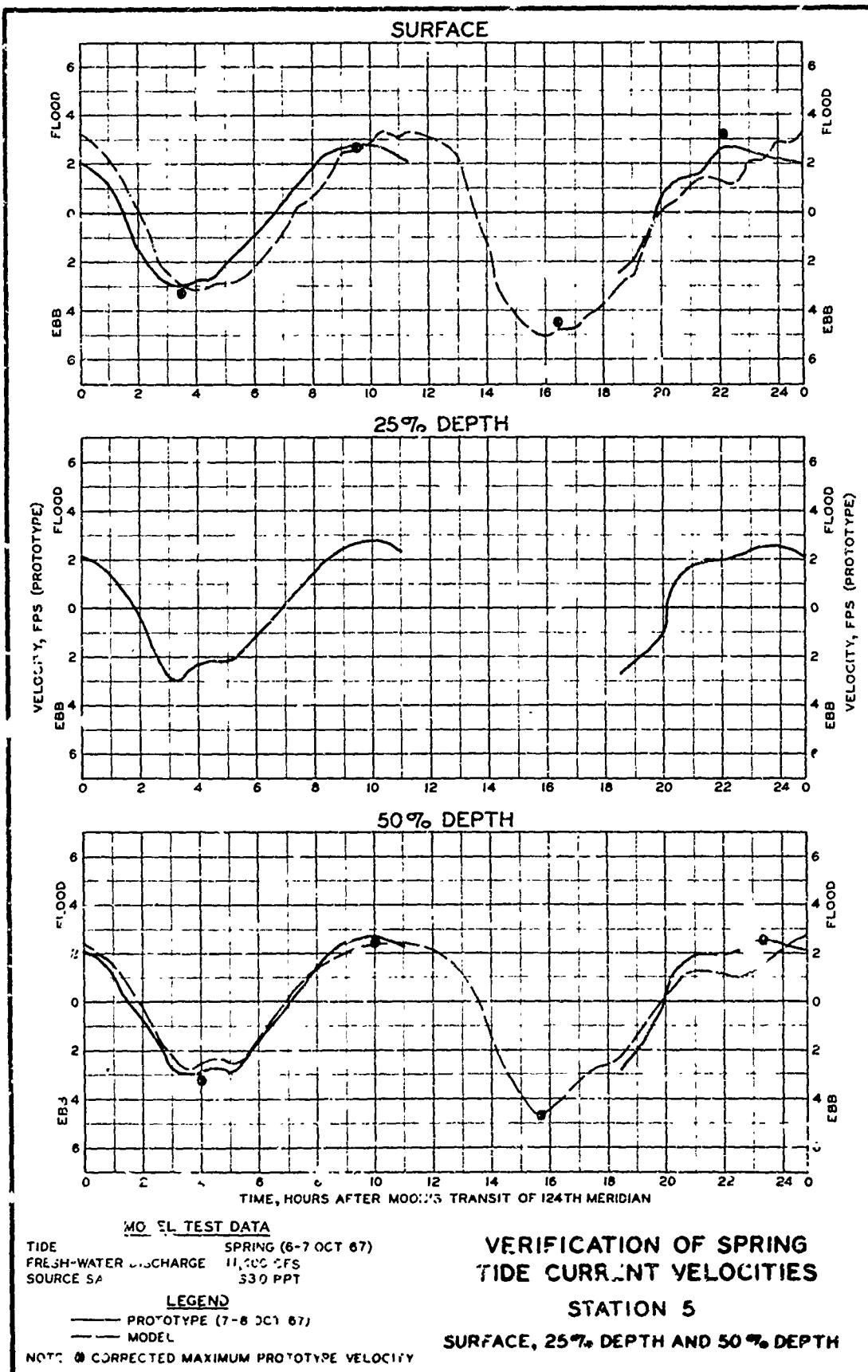
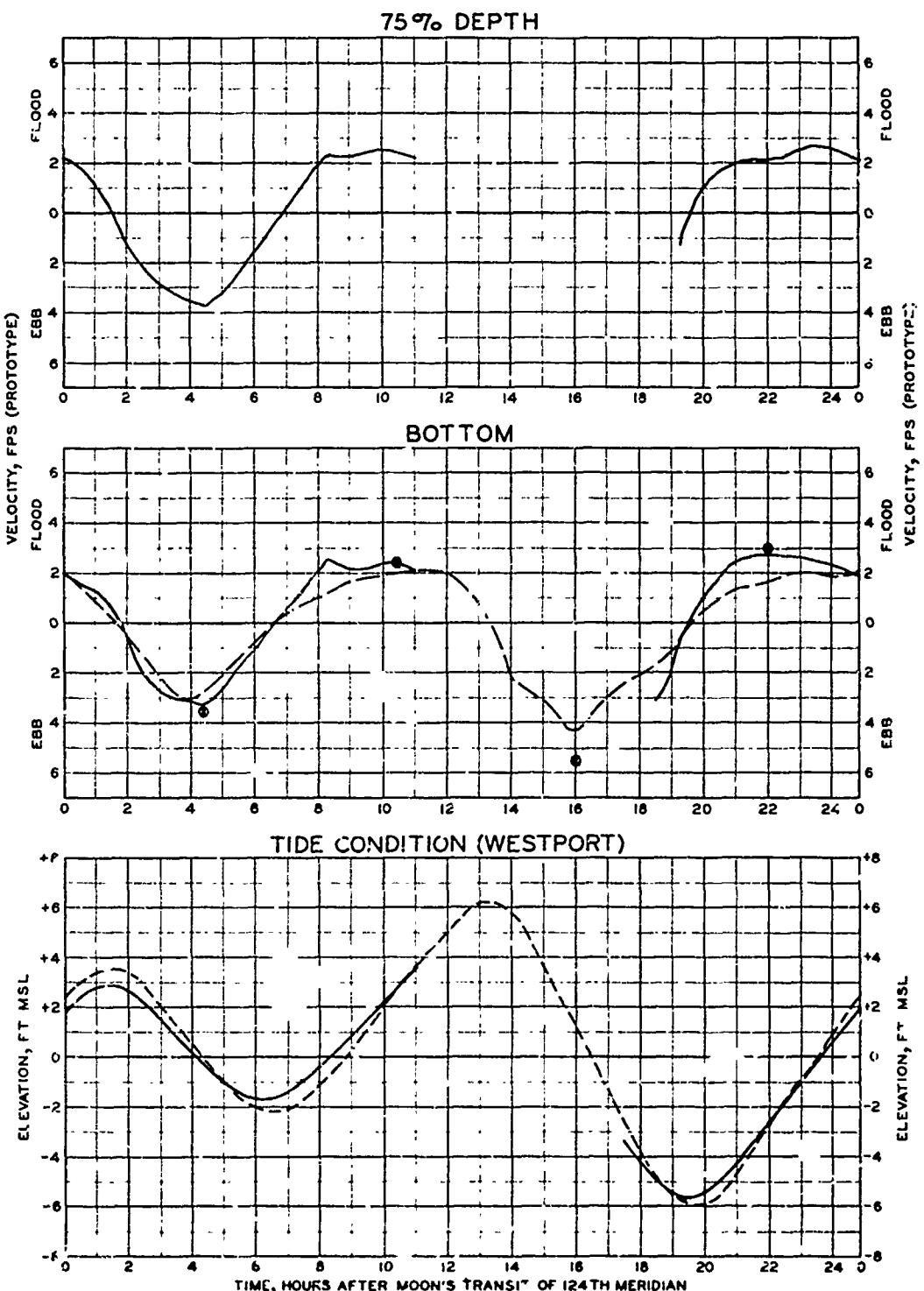


PLATE 14



MODEL TEST DATA
 TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE 1,400 CFS
 SOURCE SALINITY 13.0 PPT

LEGEND
 — PROTOTYPE 17 OCT 67
 - - MODEL

VERIFICATION OF SPRING TIDE CURRENT VELOCITIES
STATION 5
75% DEPTH, BOTTOM & TIDE CONDITION

NOTE: @ CORRECTED MAXIMUM PROTOTYPE VELOCITY

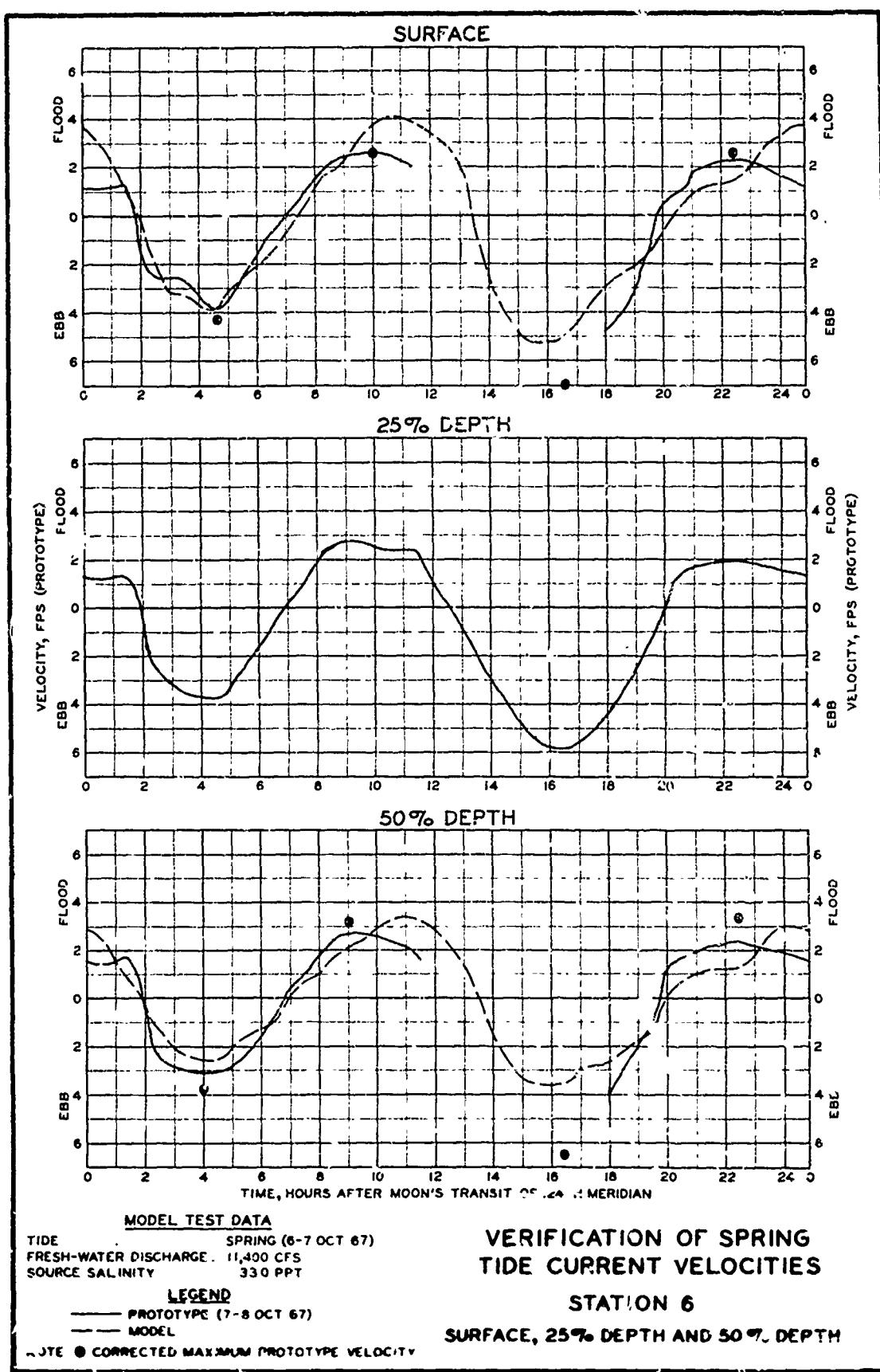
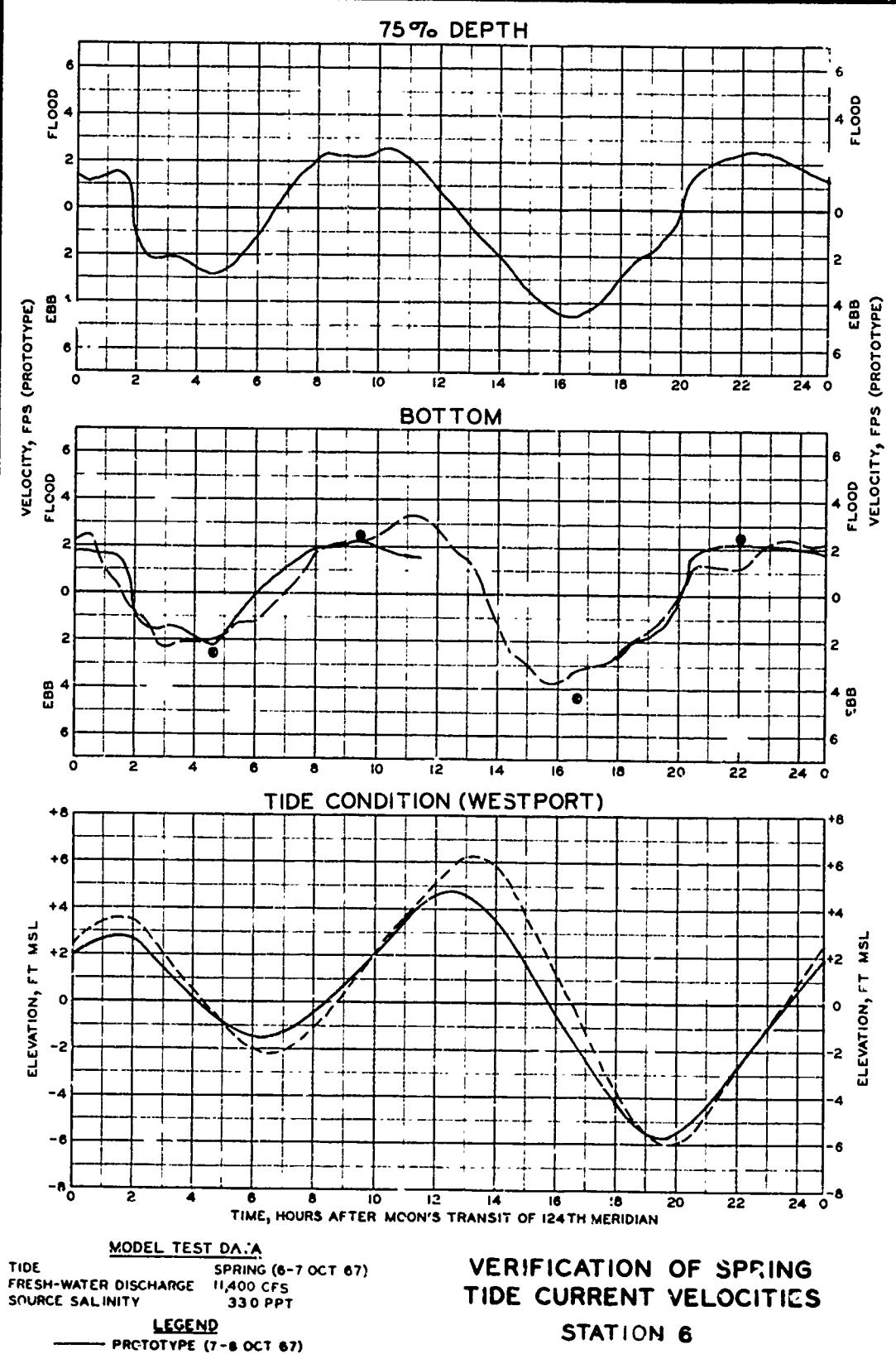


PLATE 16

60



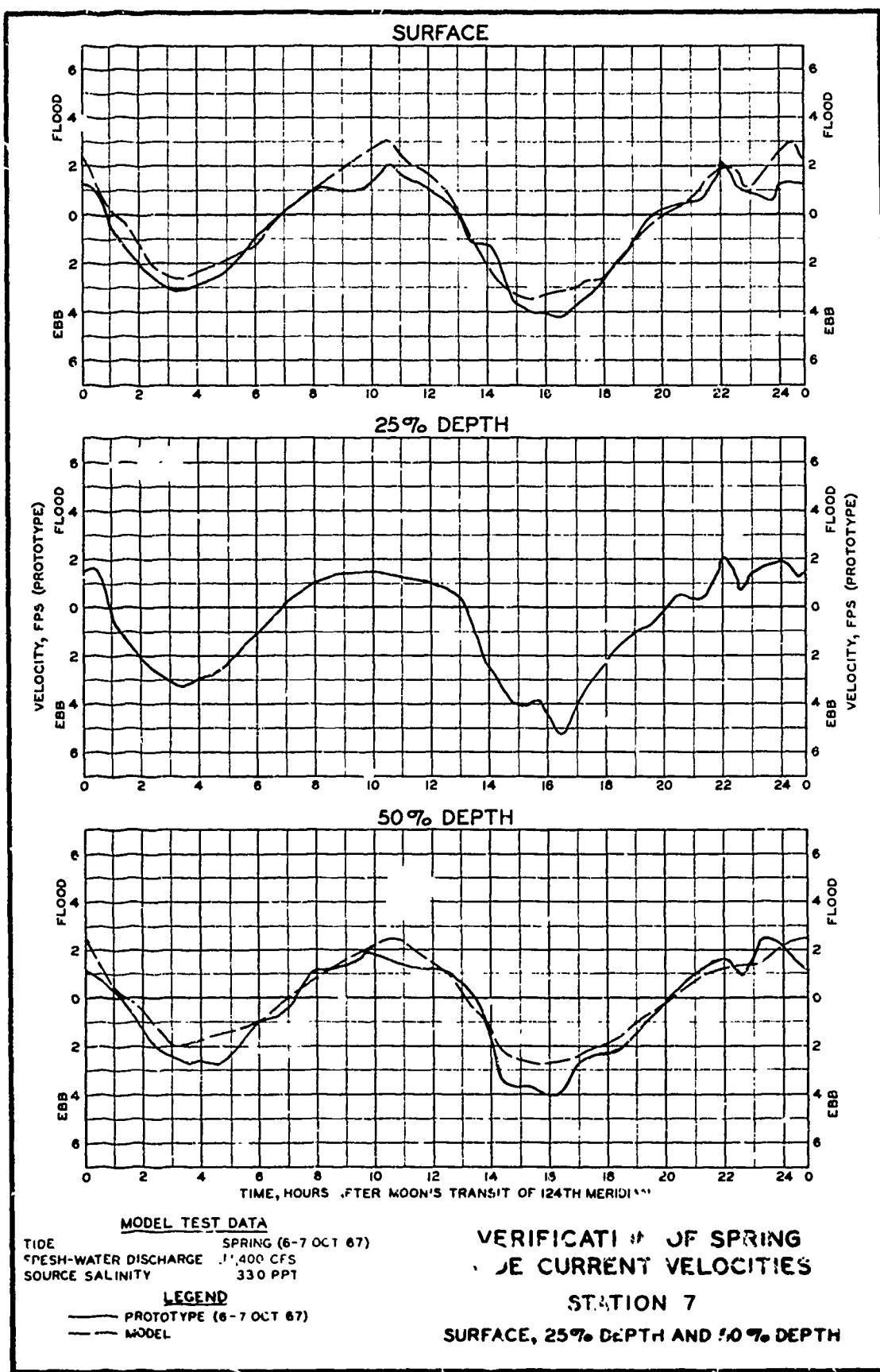
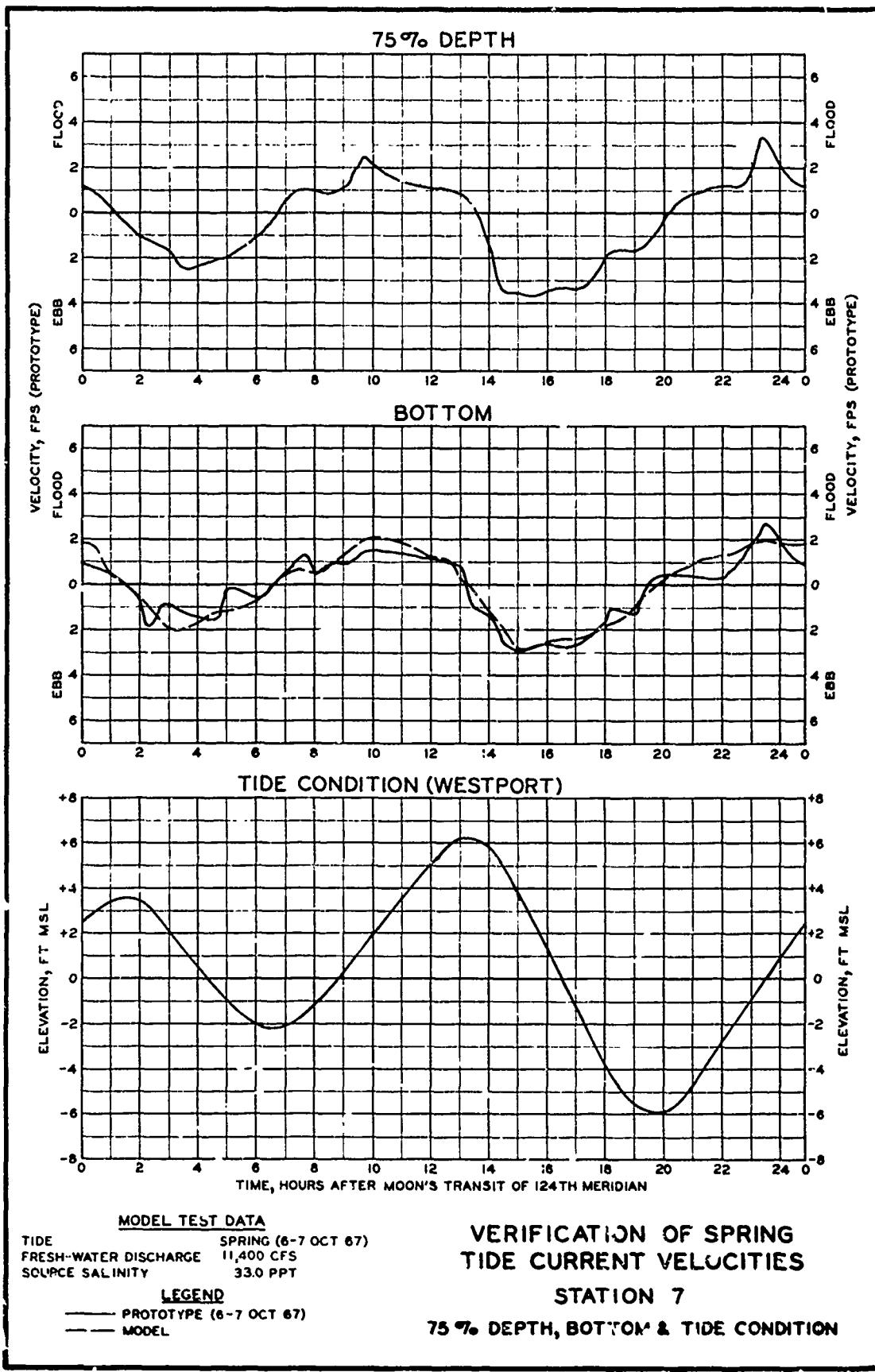


PLATE 18



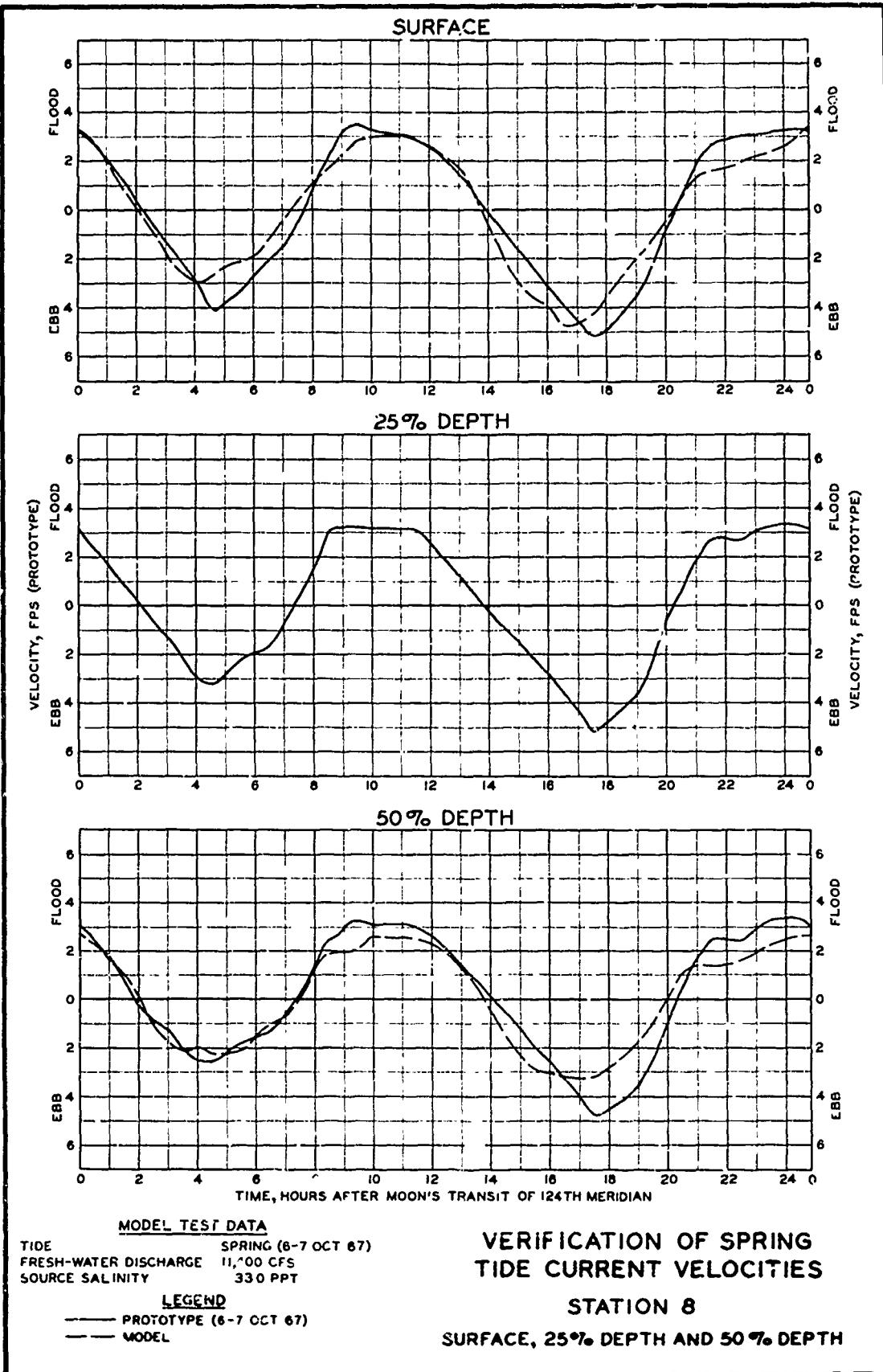


PLATE 20

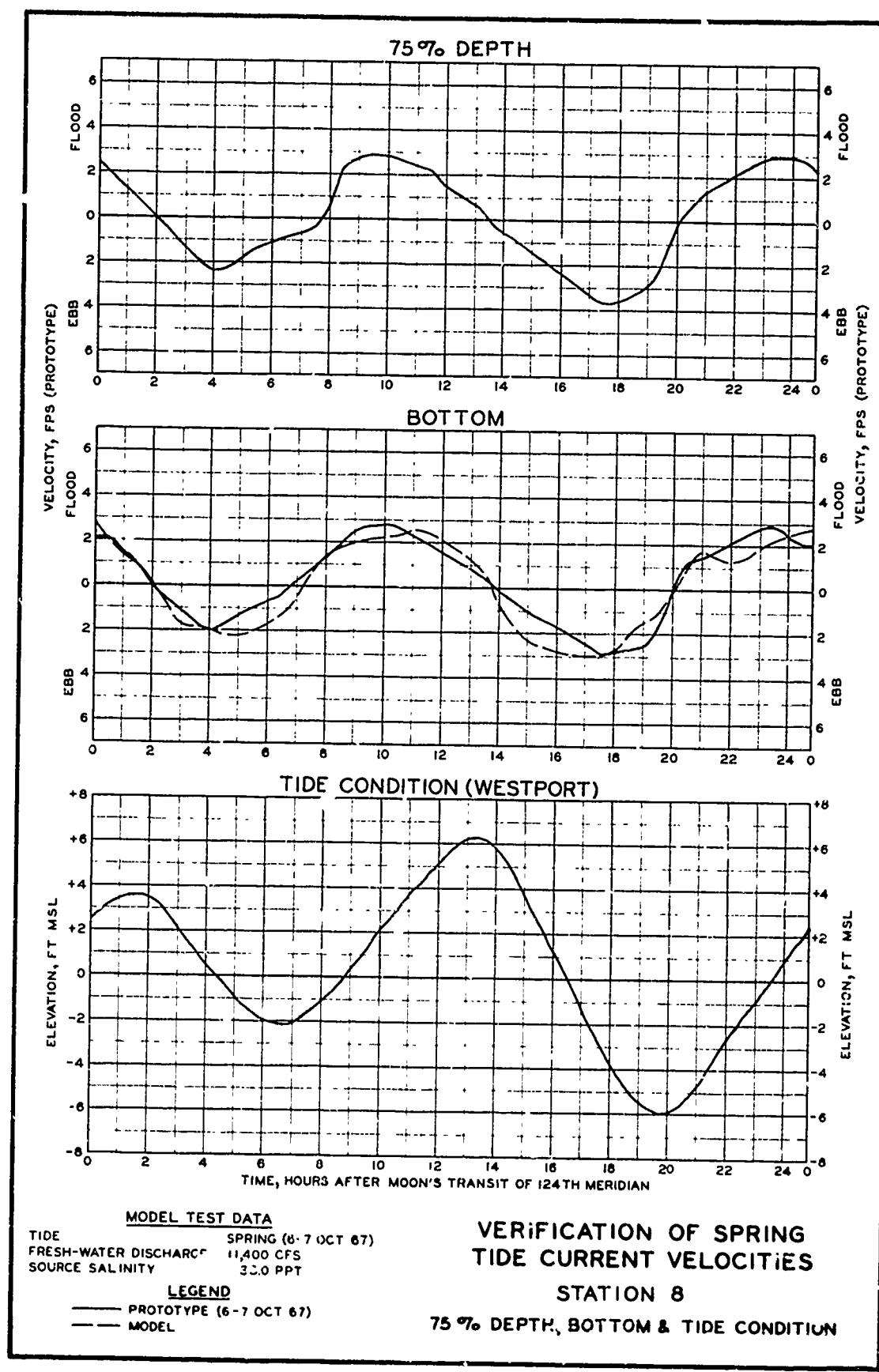
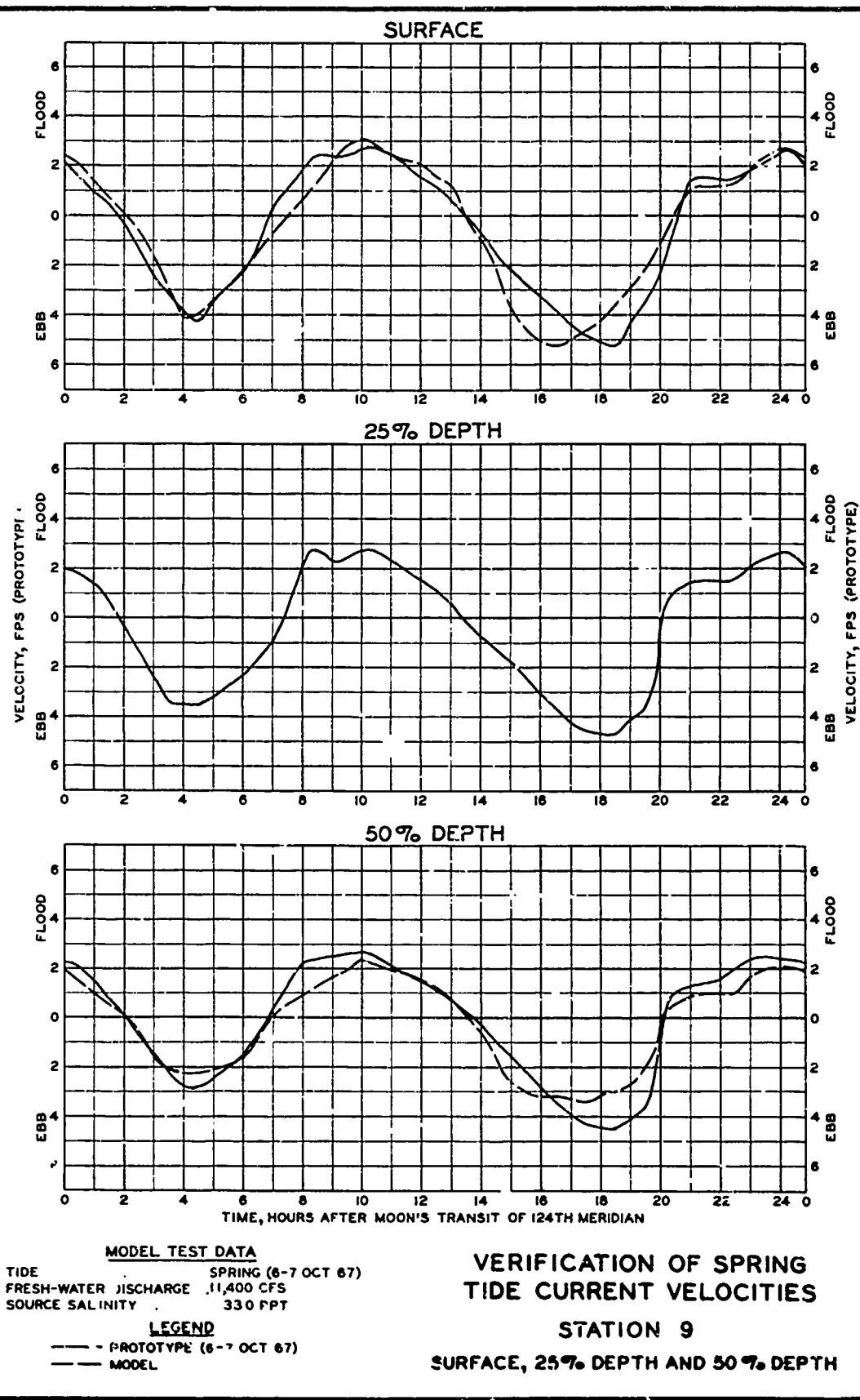
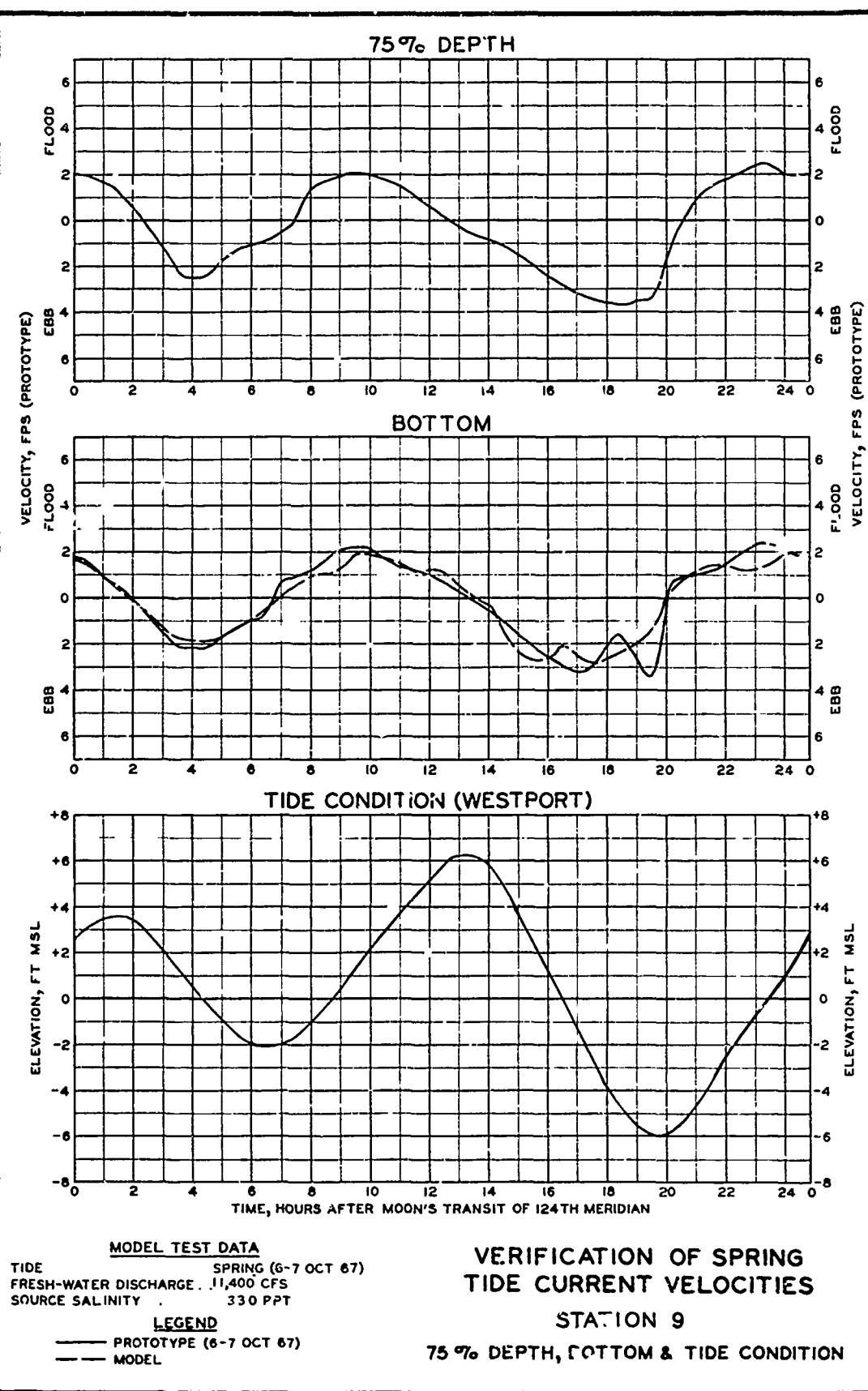


PLATE 21





87

PLATE 23

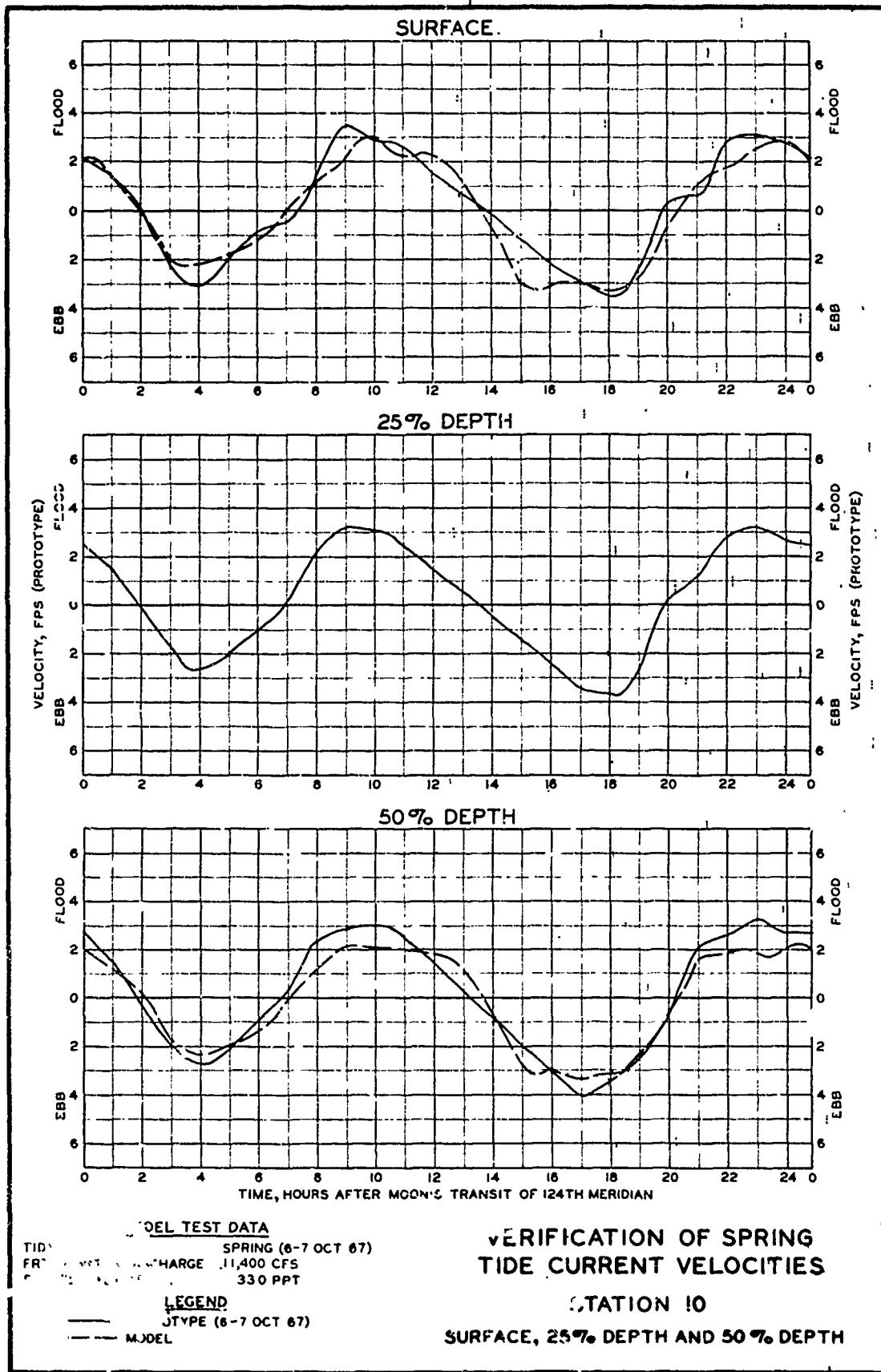
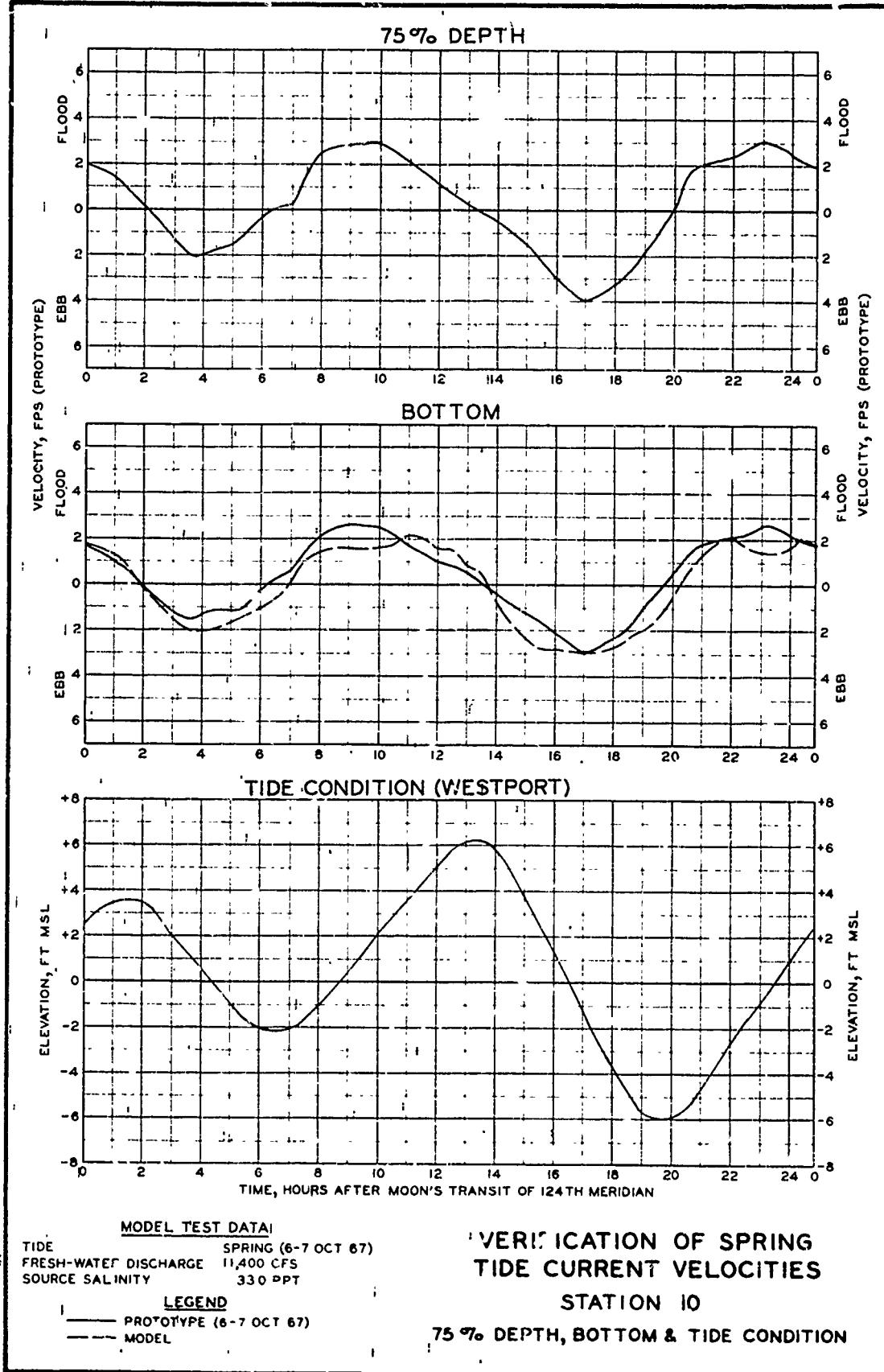


PLATE 24

08



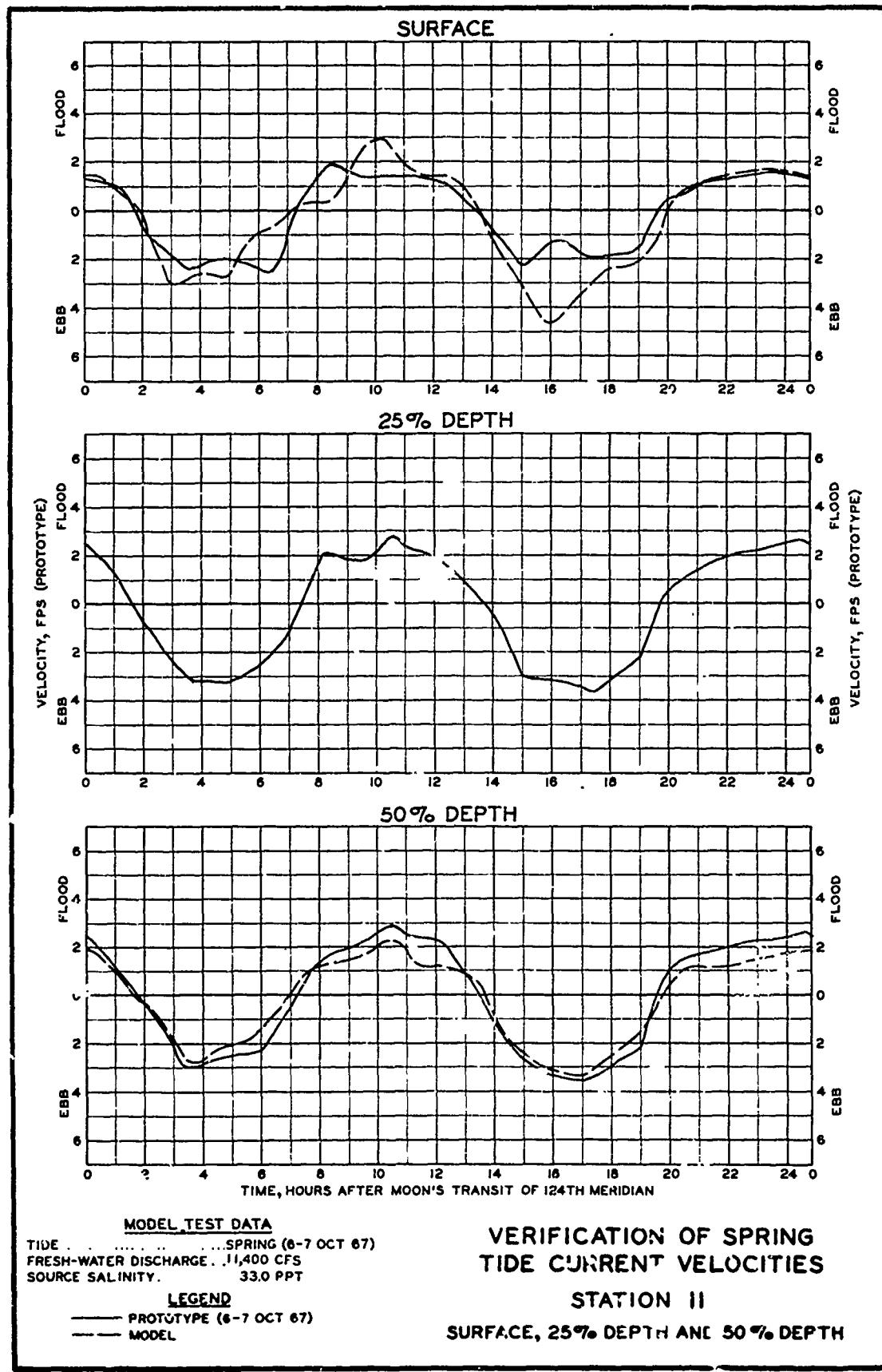
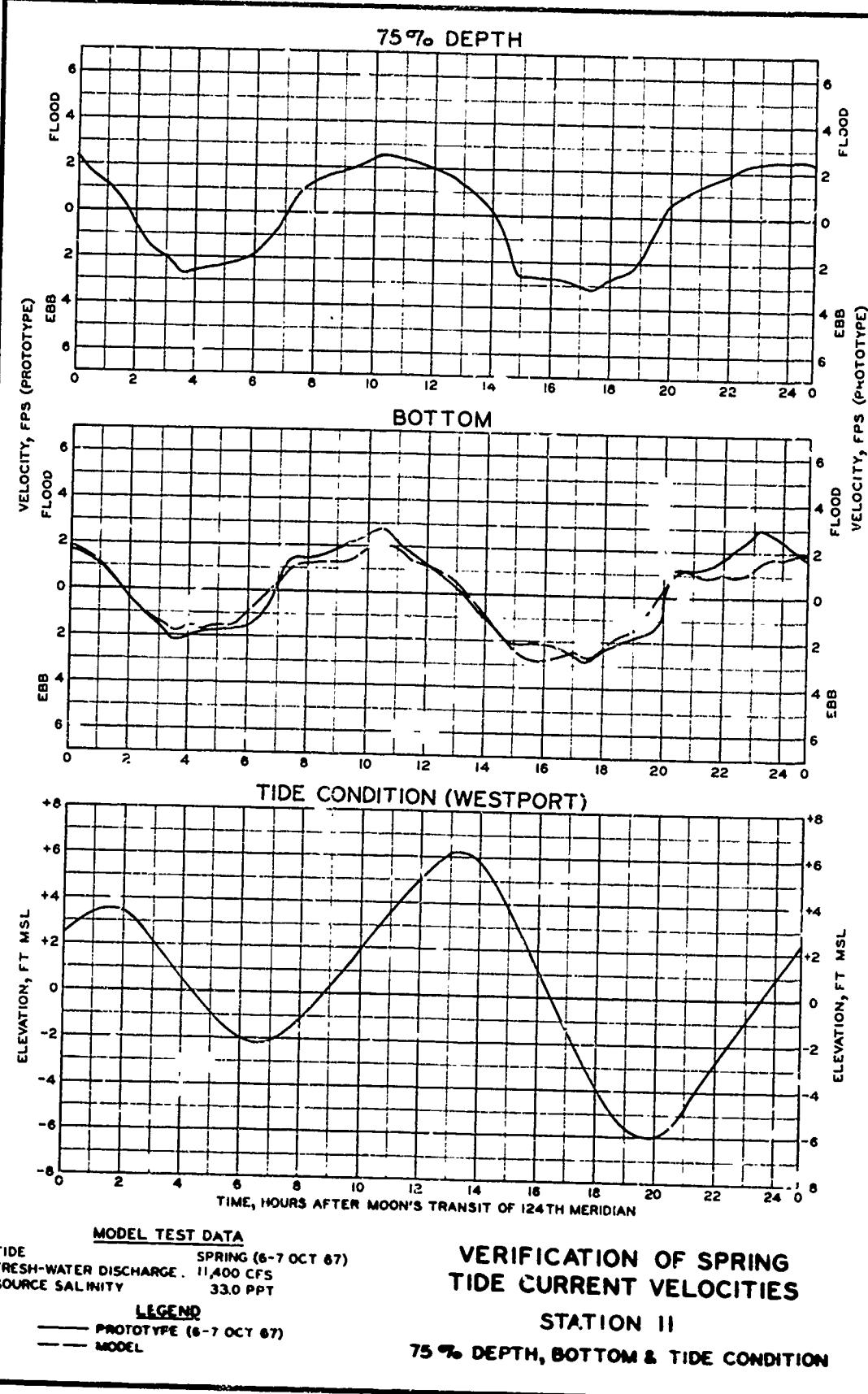
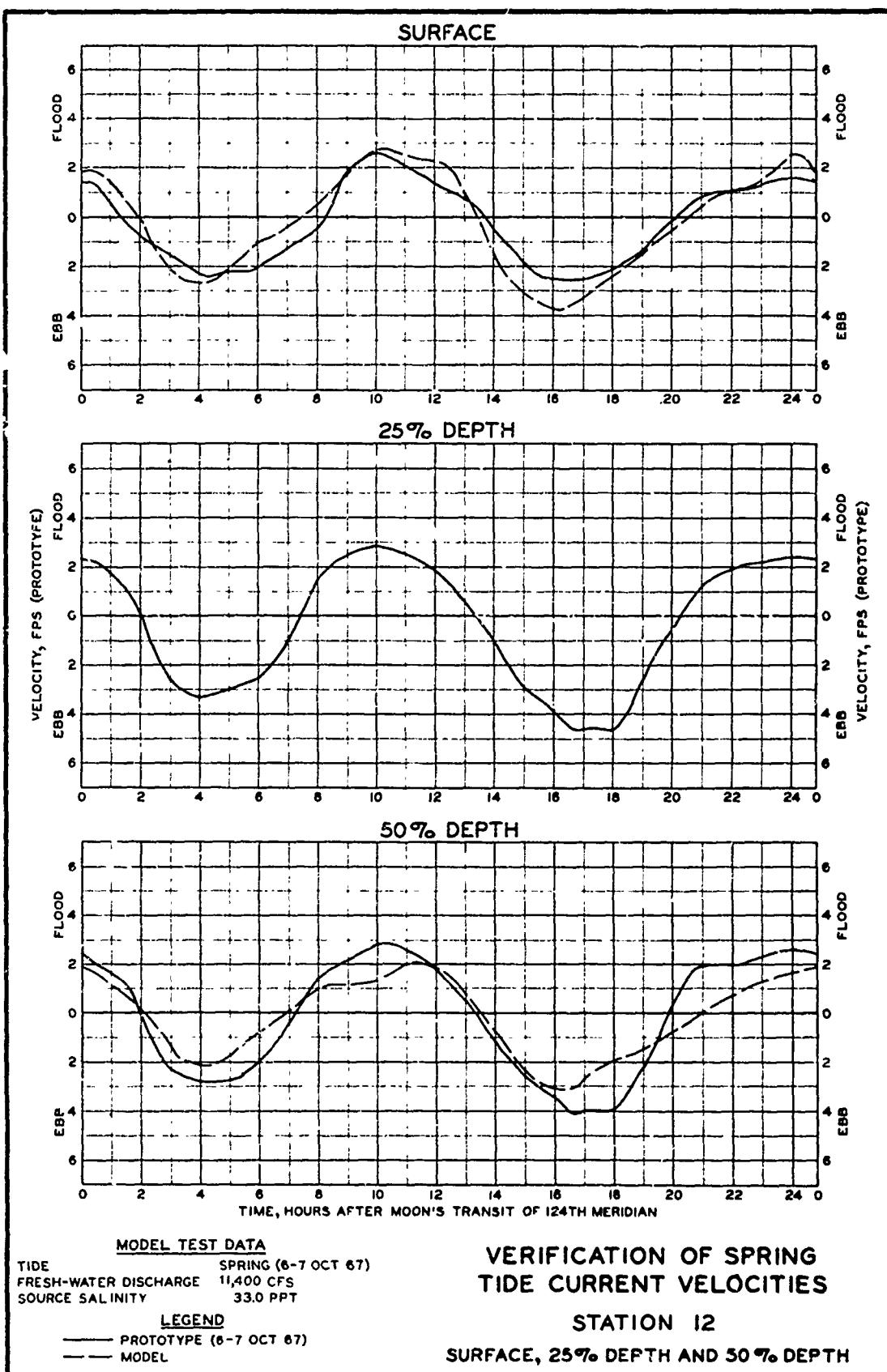
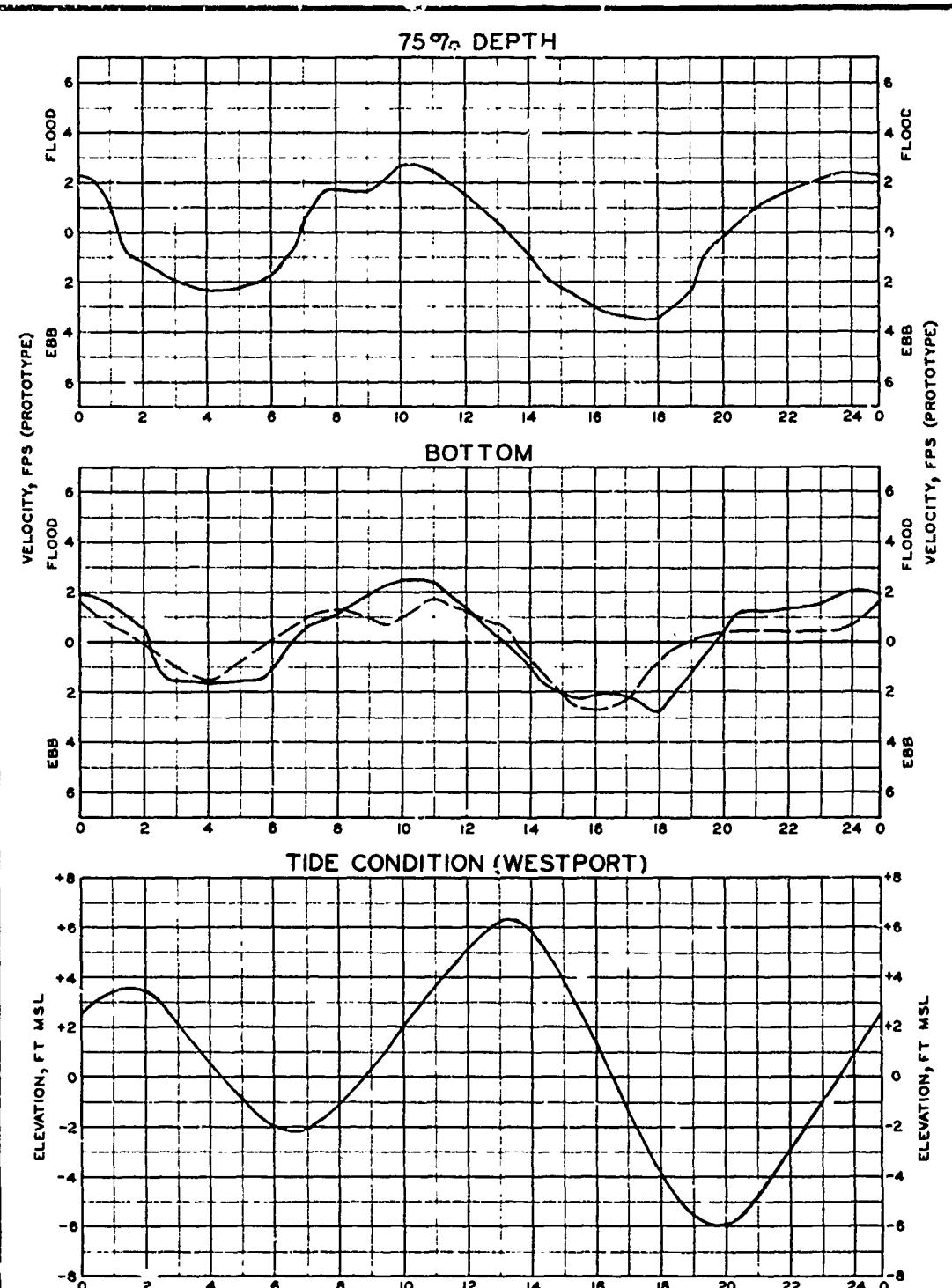


PLATE 2C

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MODEL TEST DATA
 TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — PROTOTYPE (6-7 OCT 67)
 - - MODEL

VERIFICATION OF SPRING TIDE CURRENT VELOCITIES

STATION 12.

75% DEPTH, BOTTOM & TIDE CONDITION

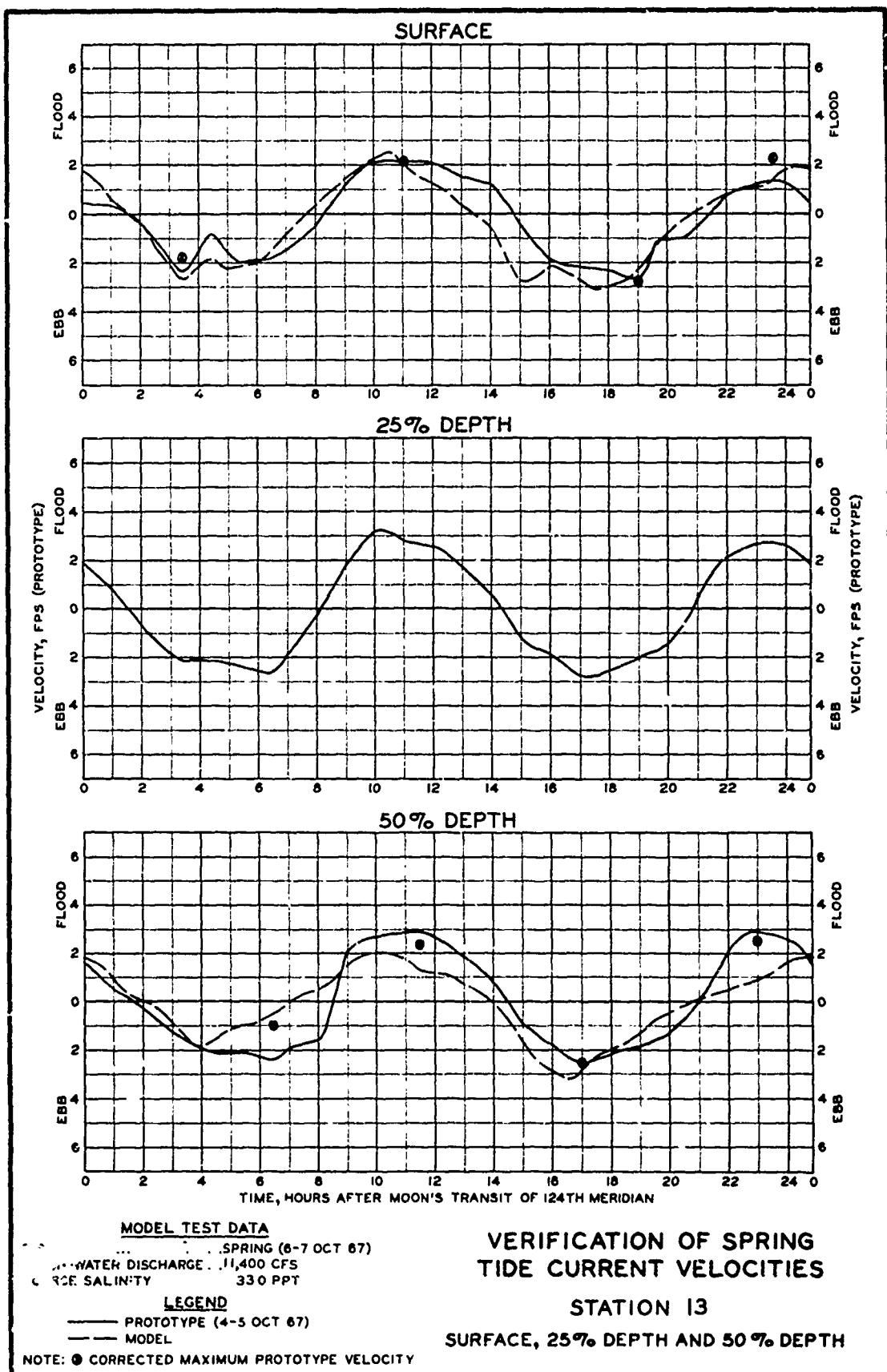
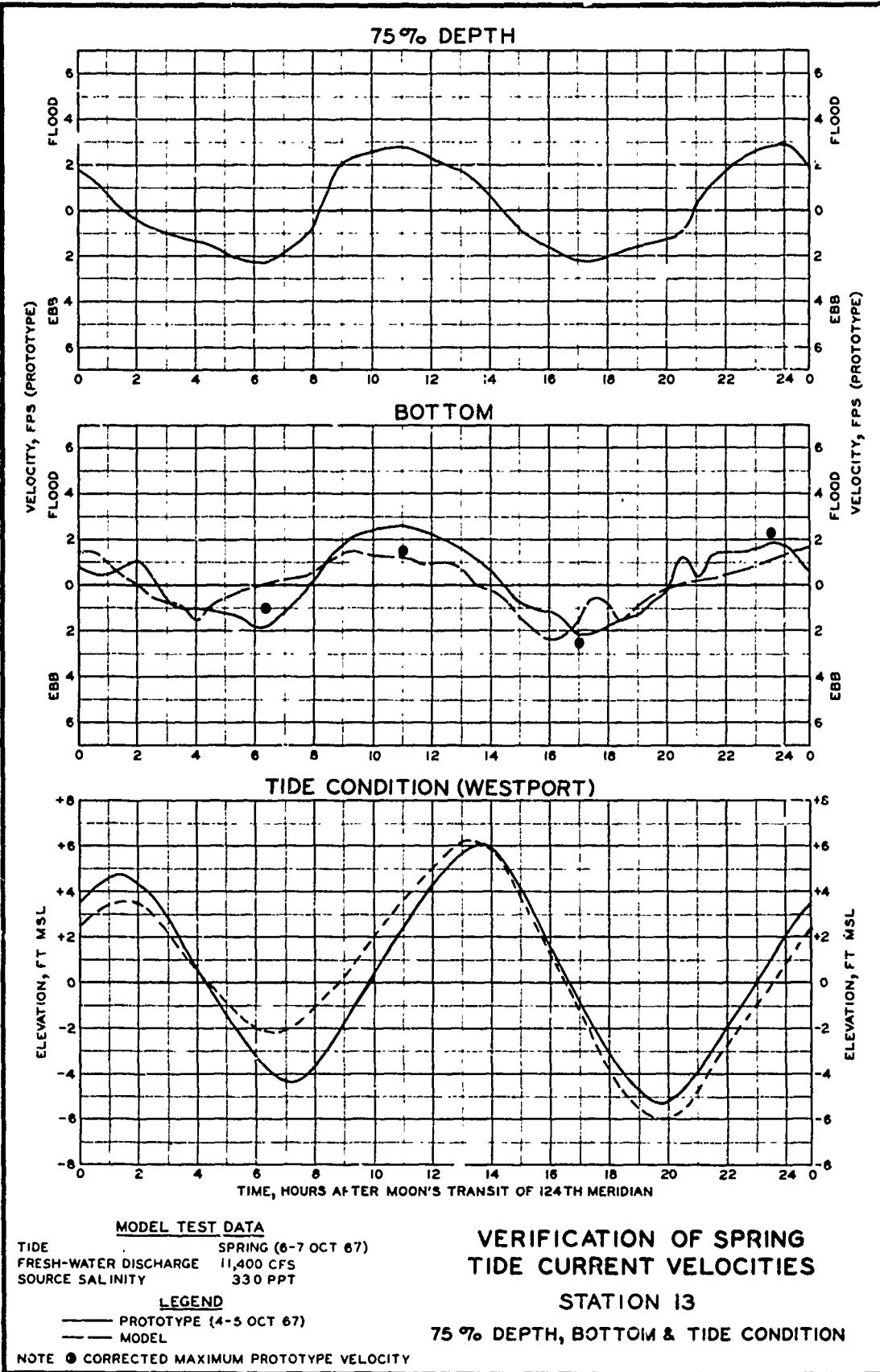
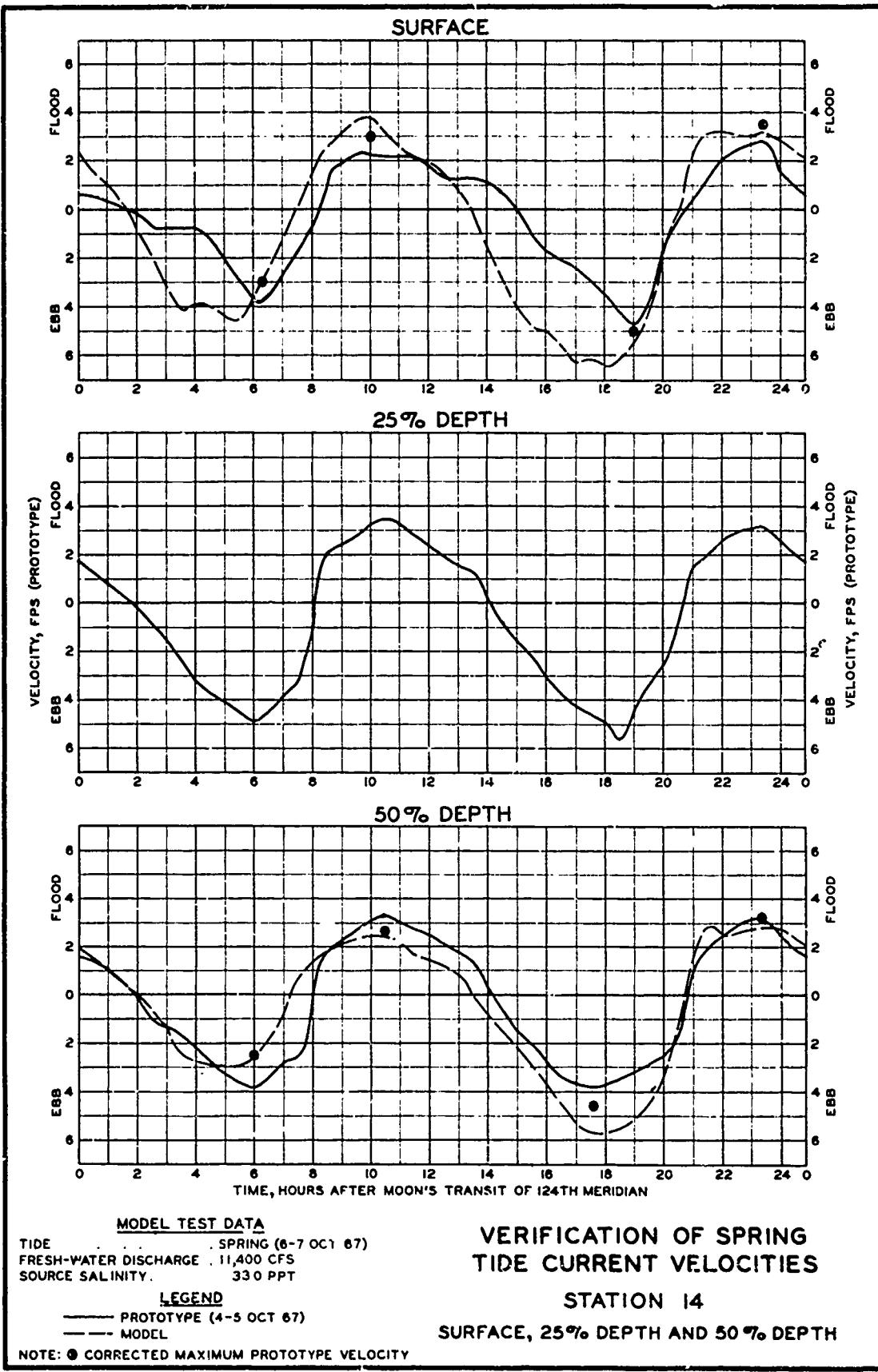
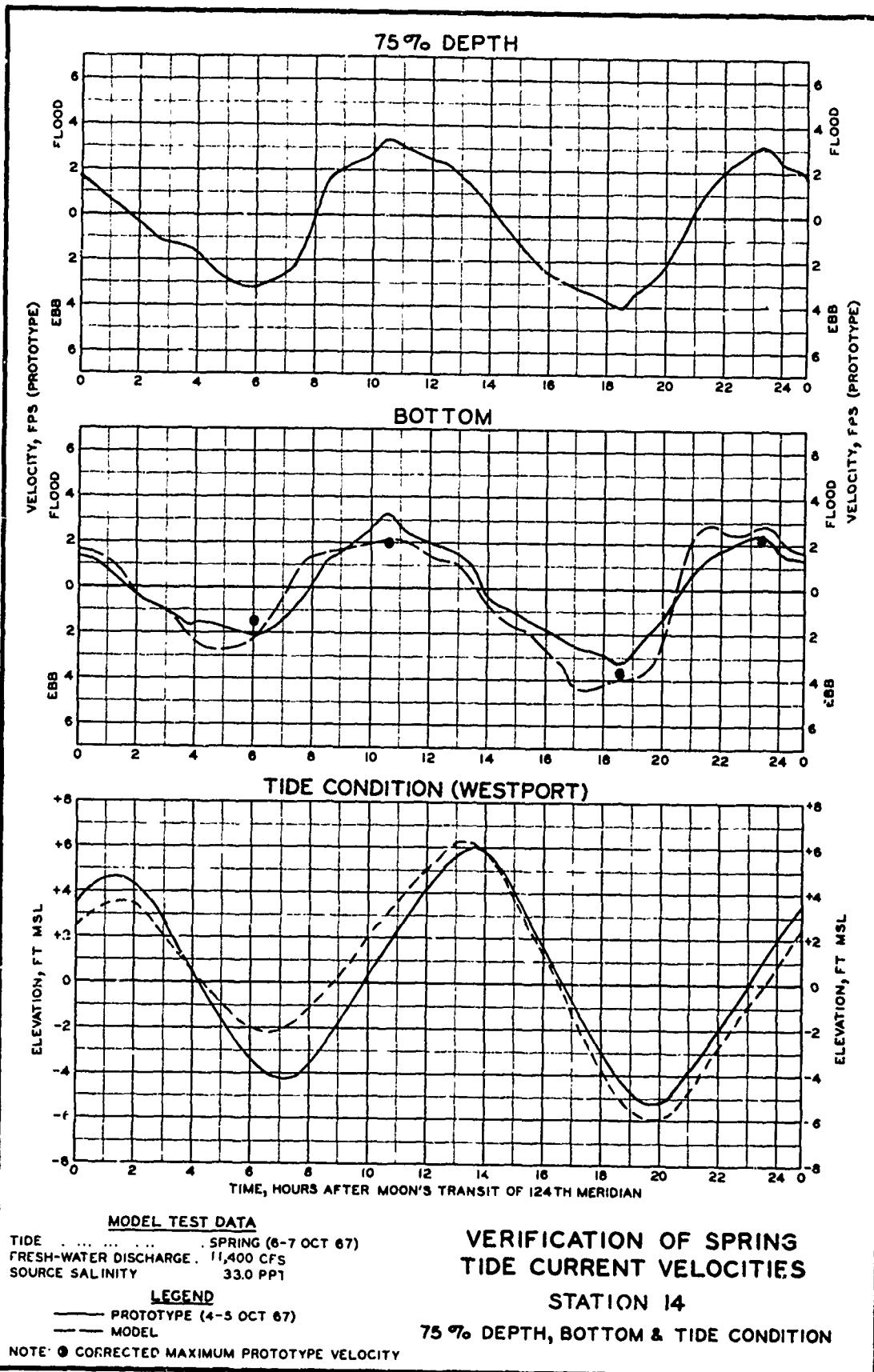


PLATE 30







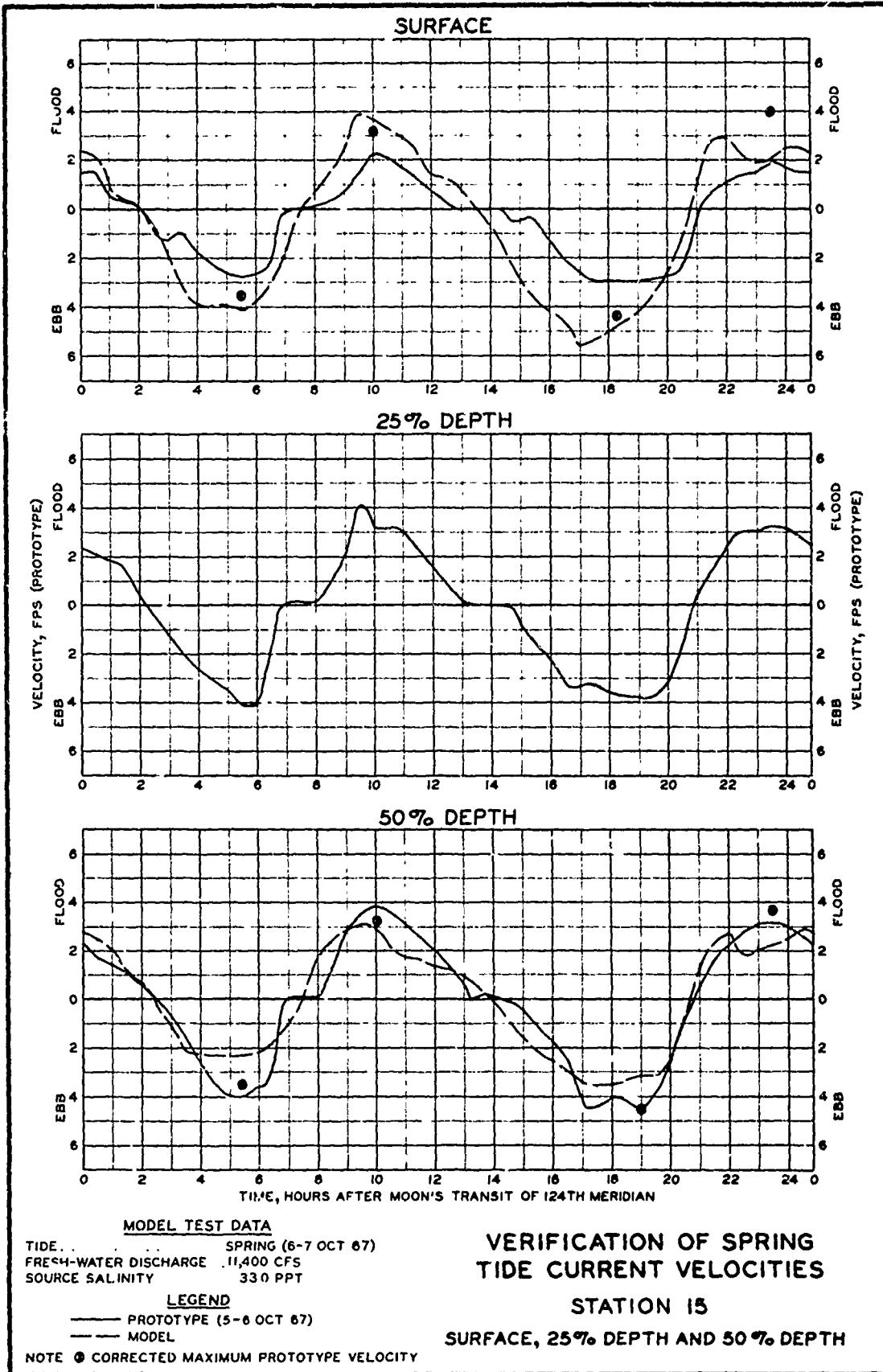
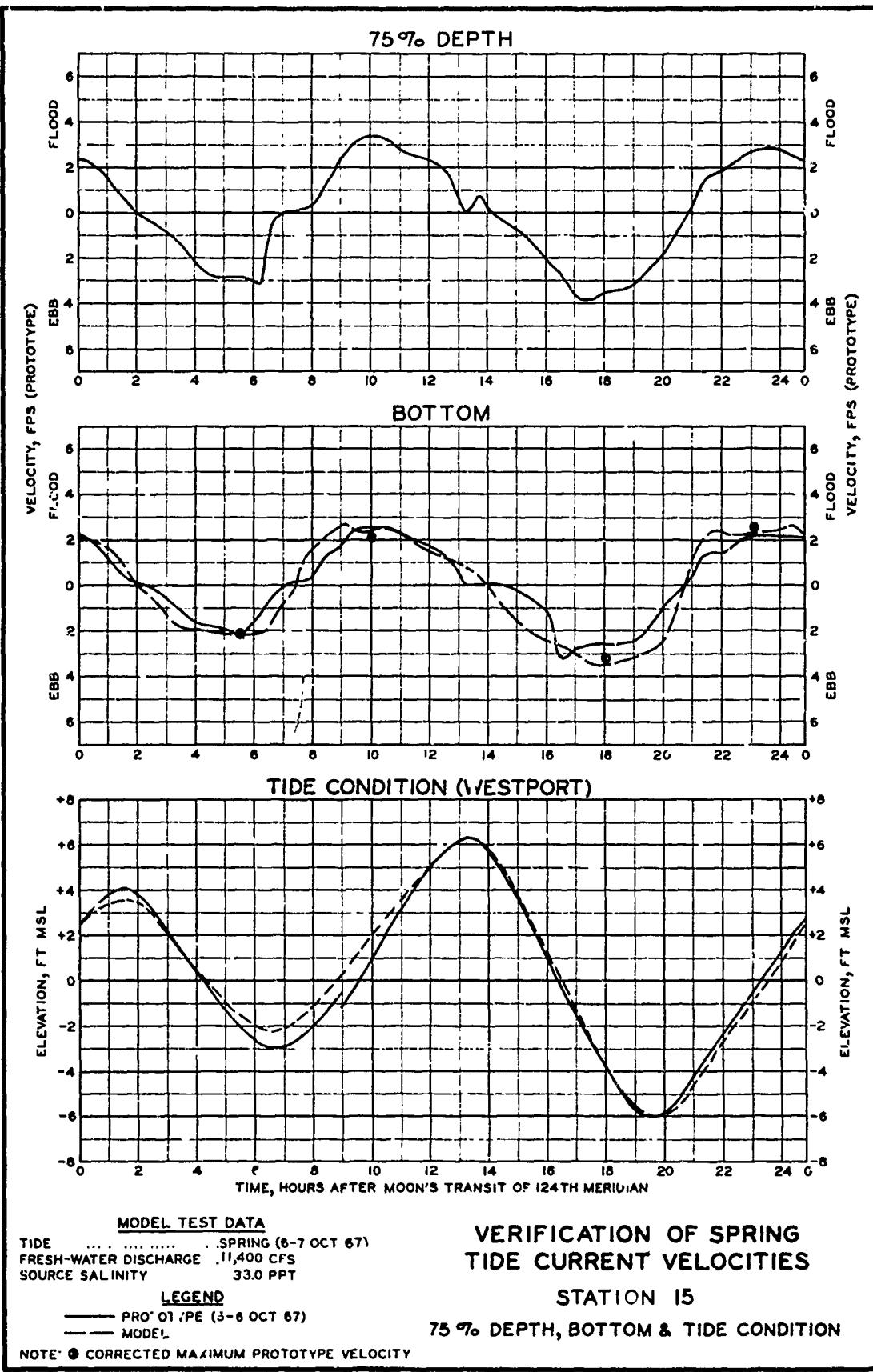
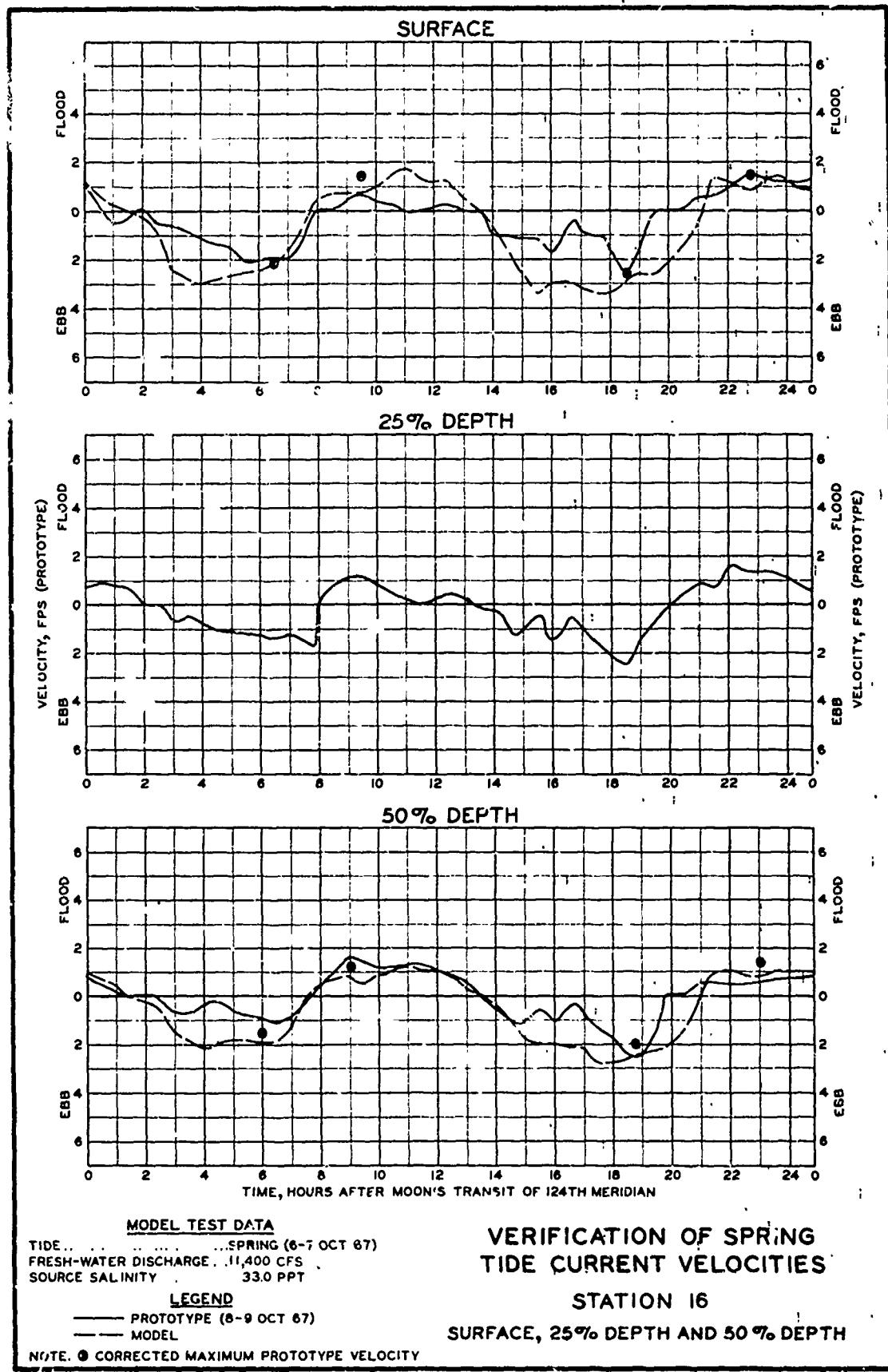


PLATE 34





PL TE 36

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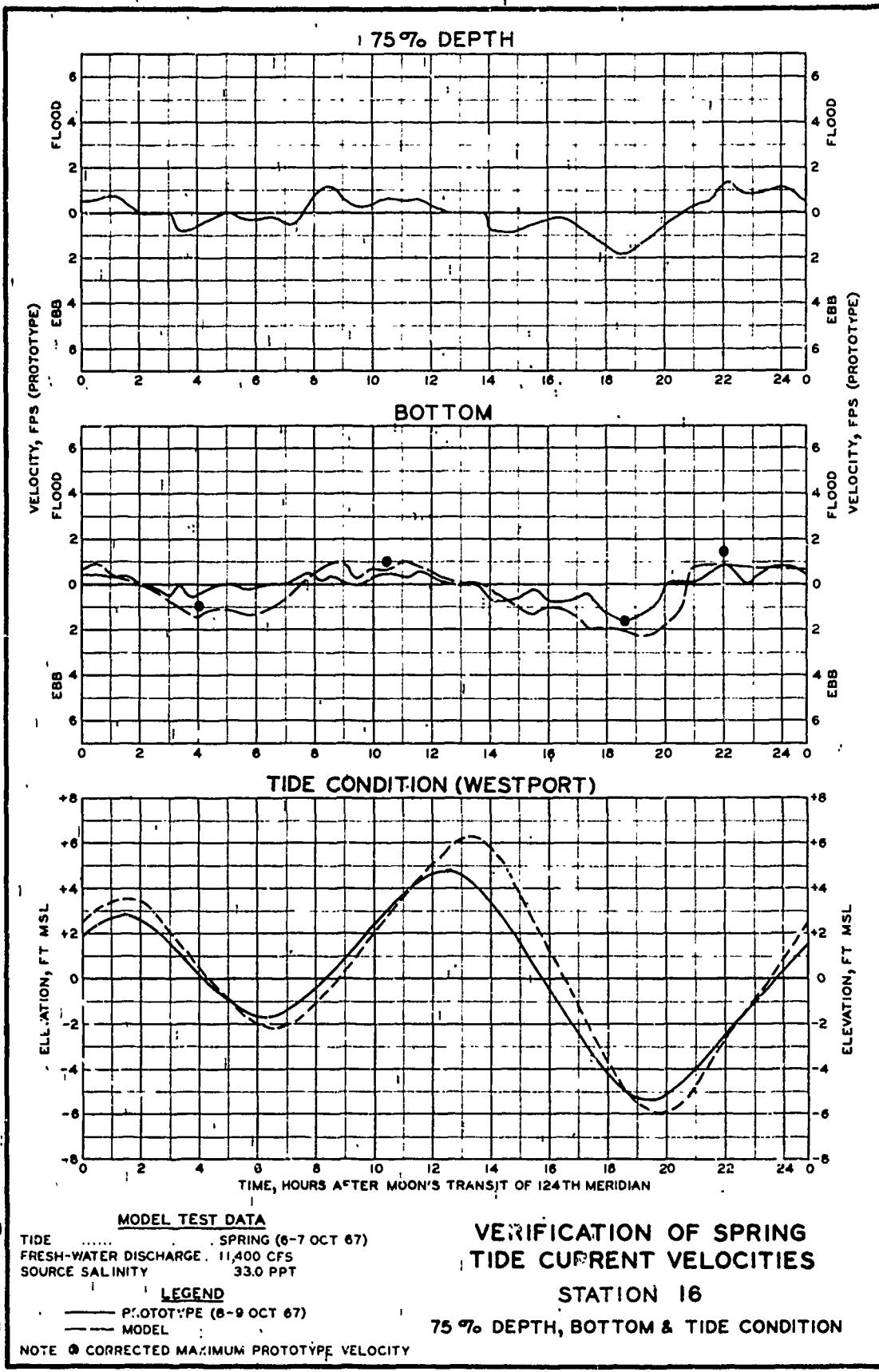


PLATE 37

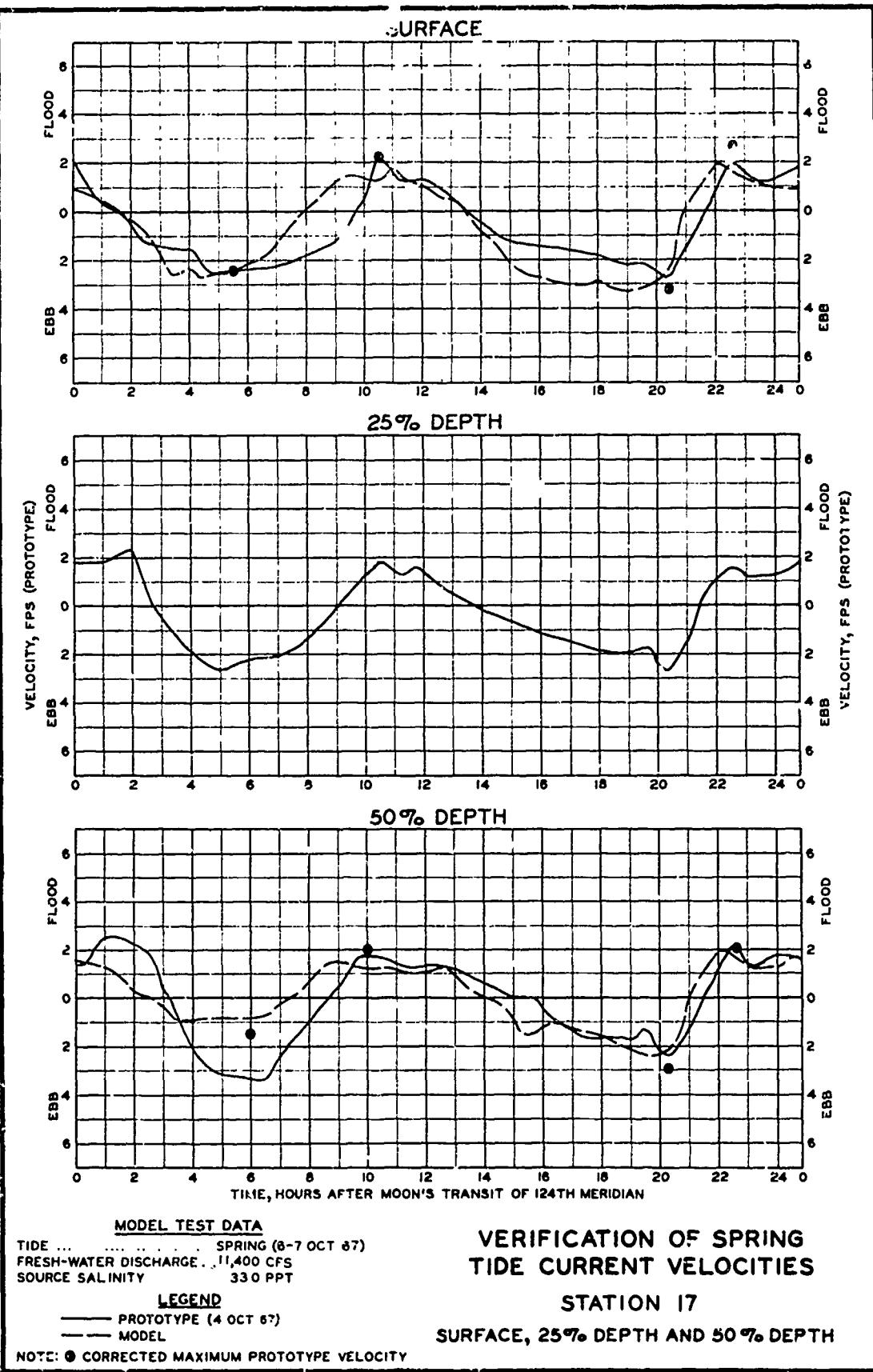
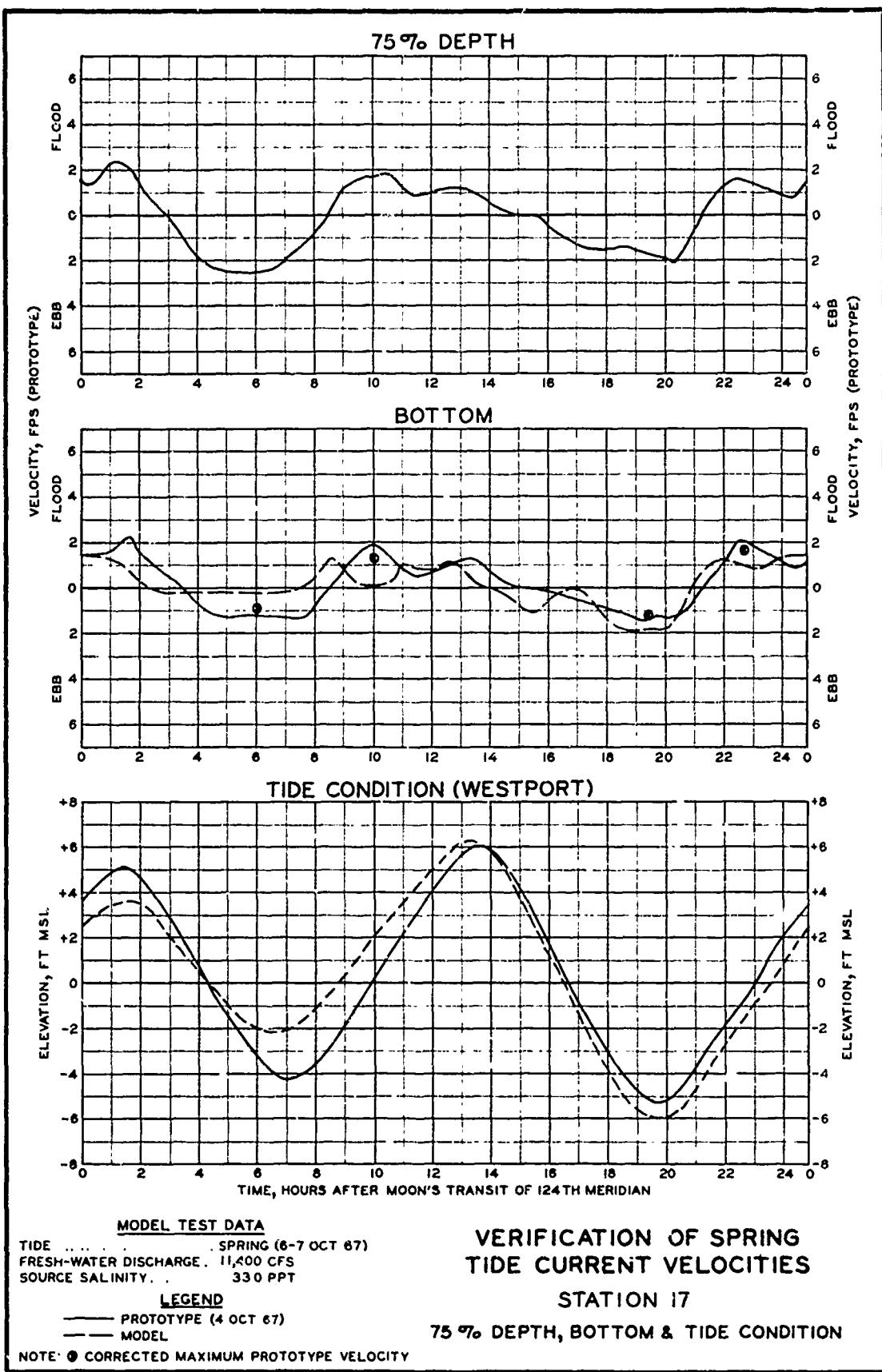


PLATE 38



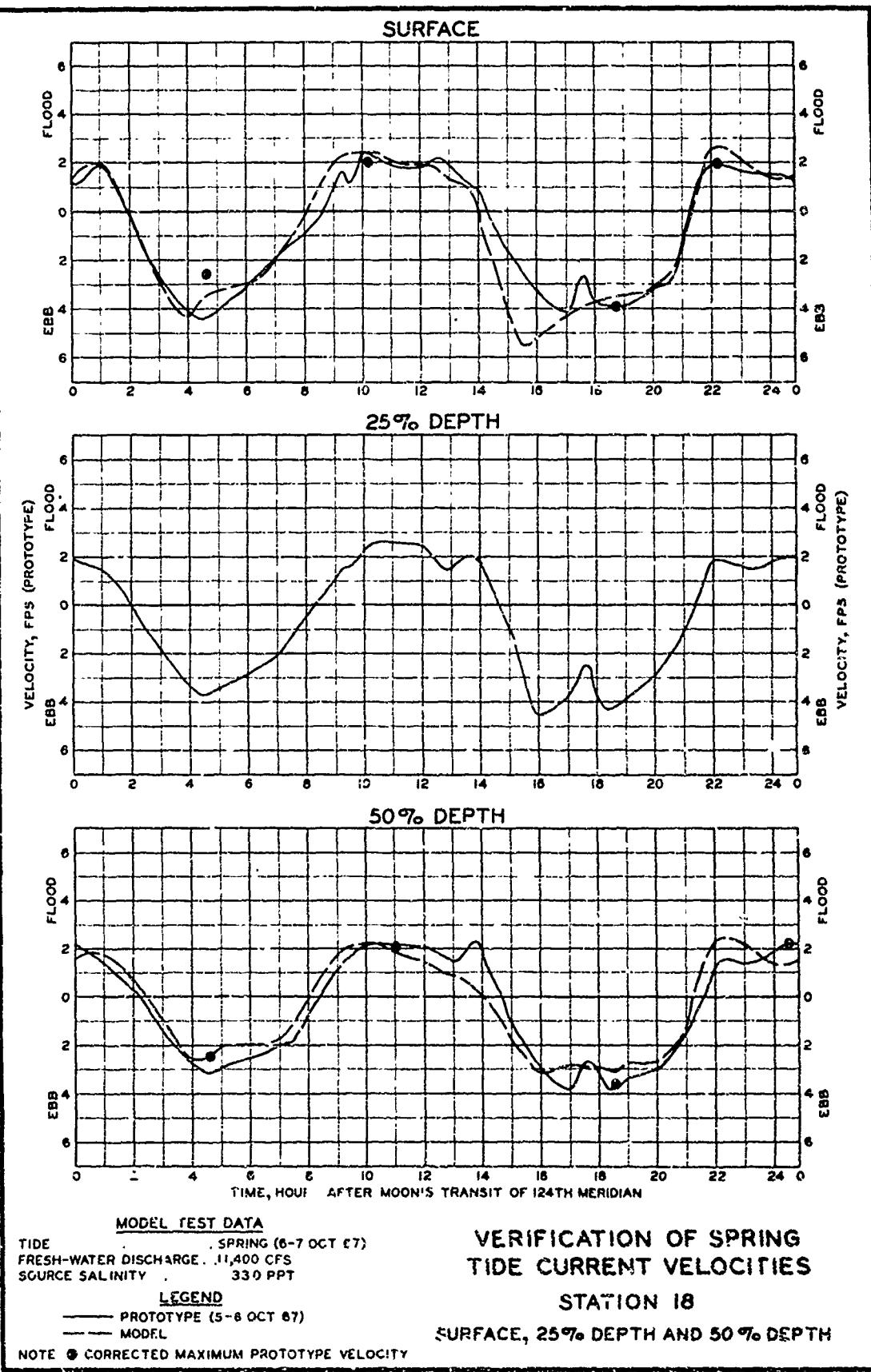


PLATE 40

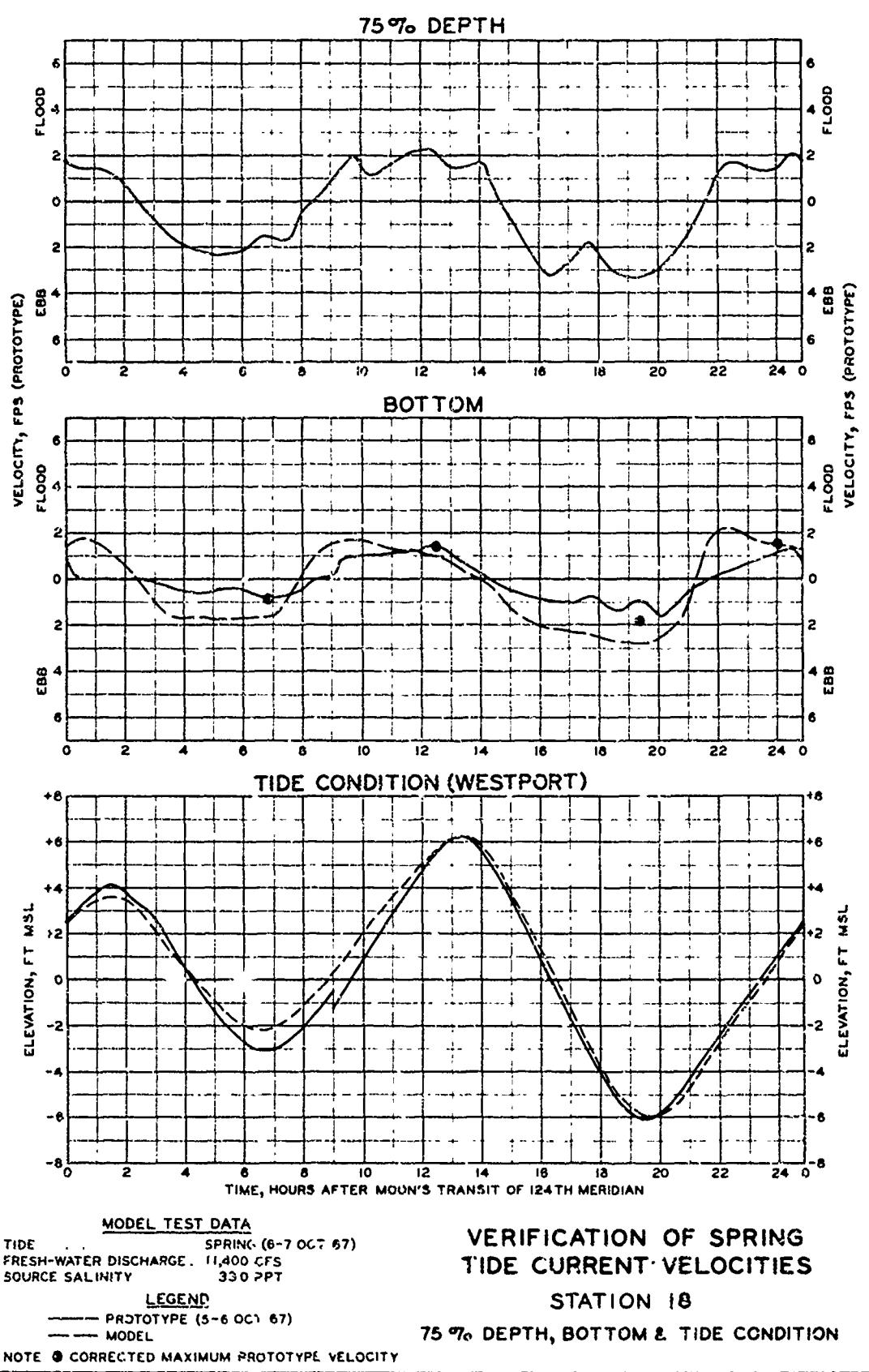
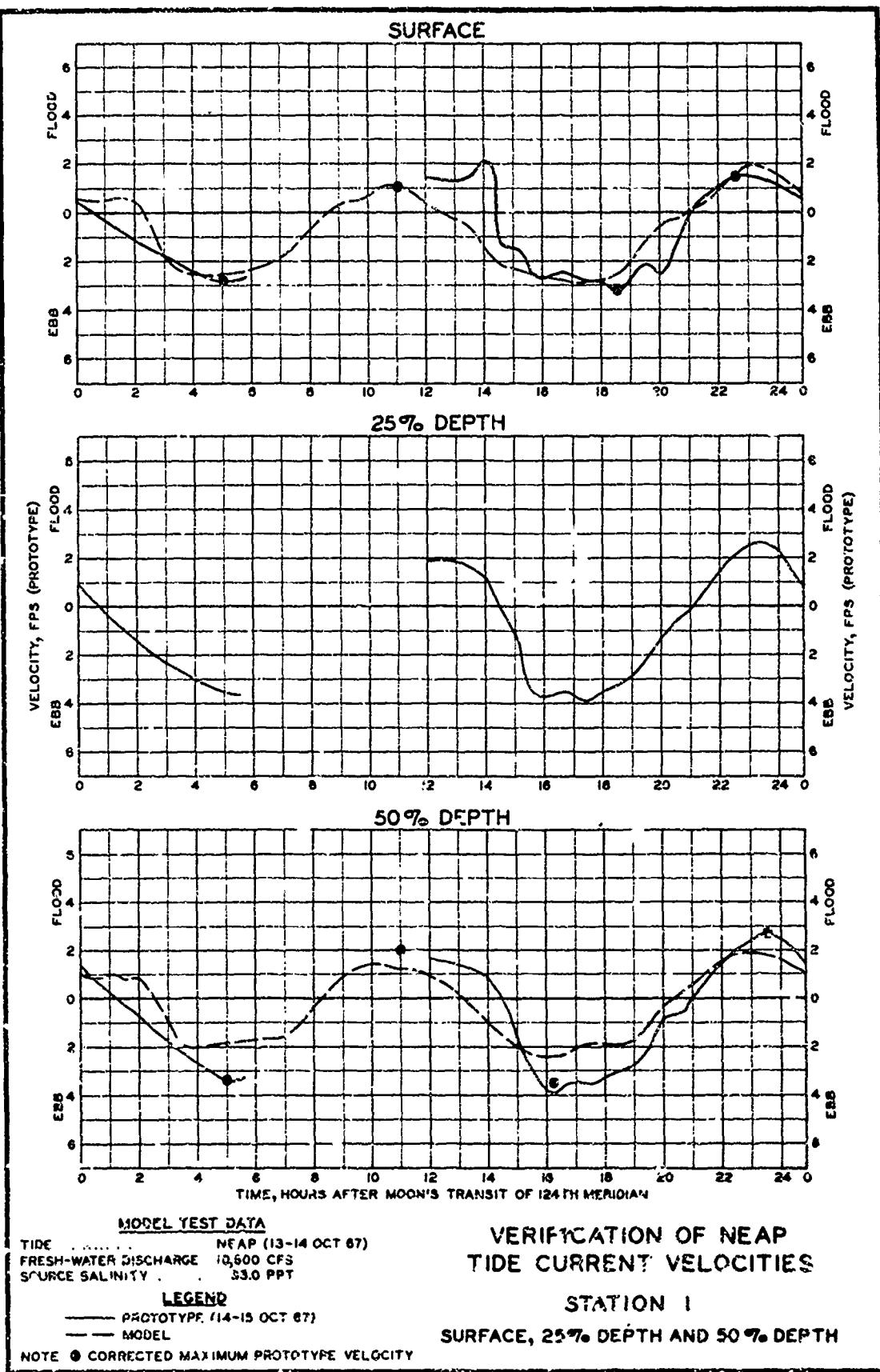
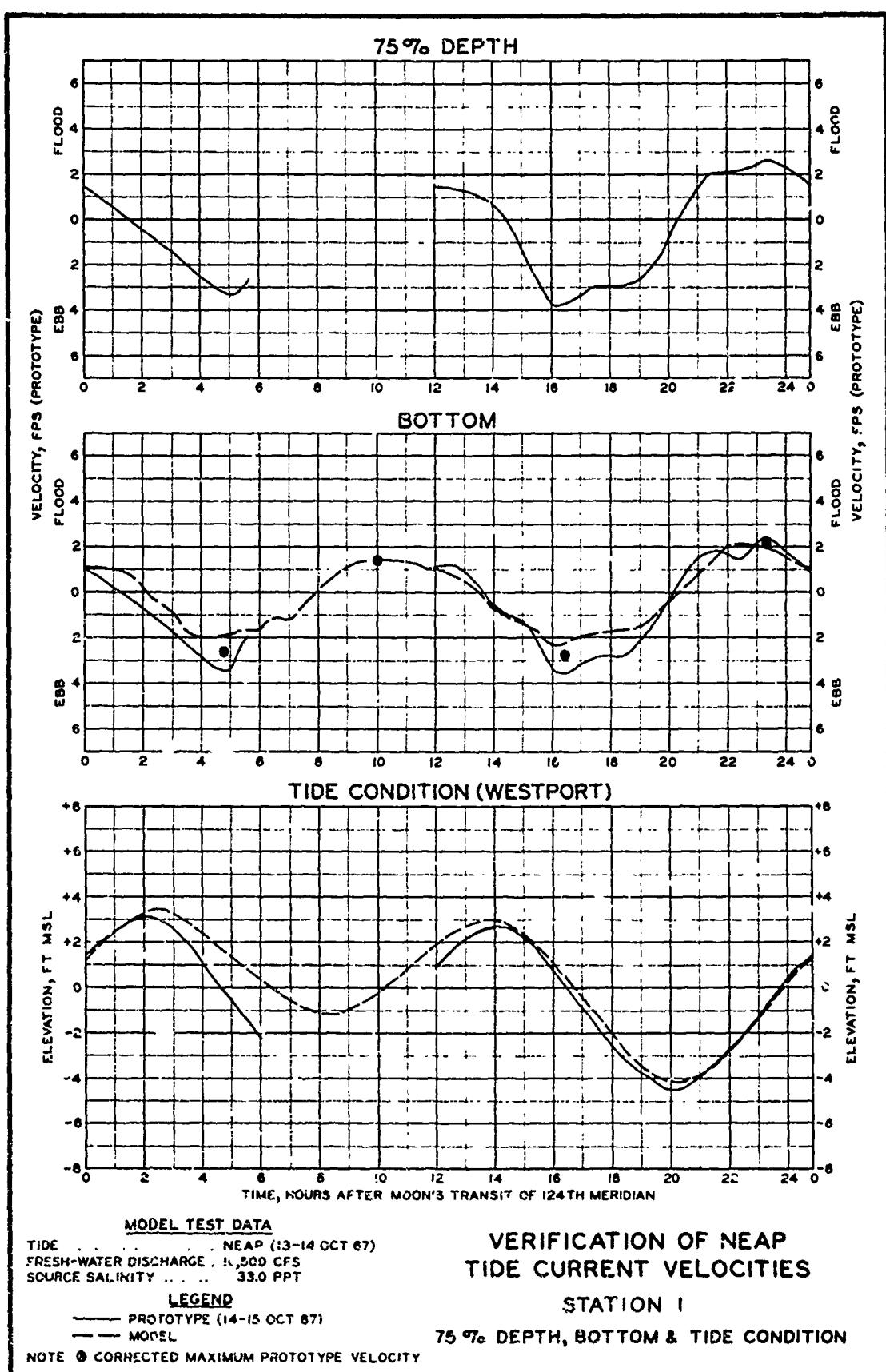
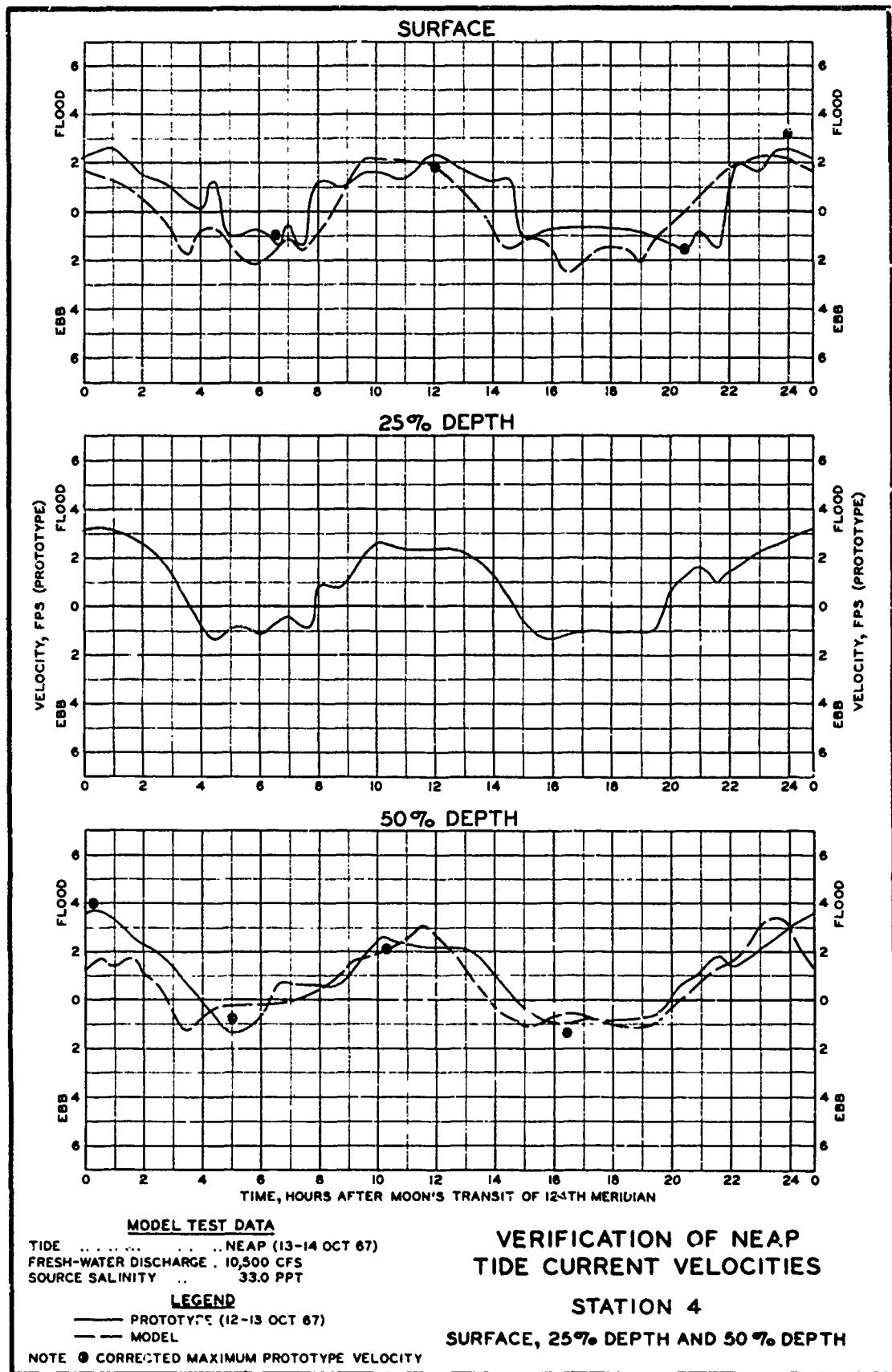
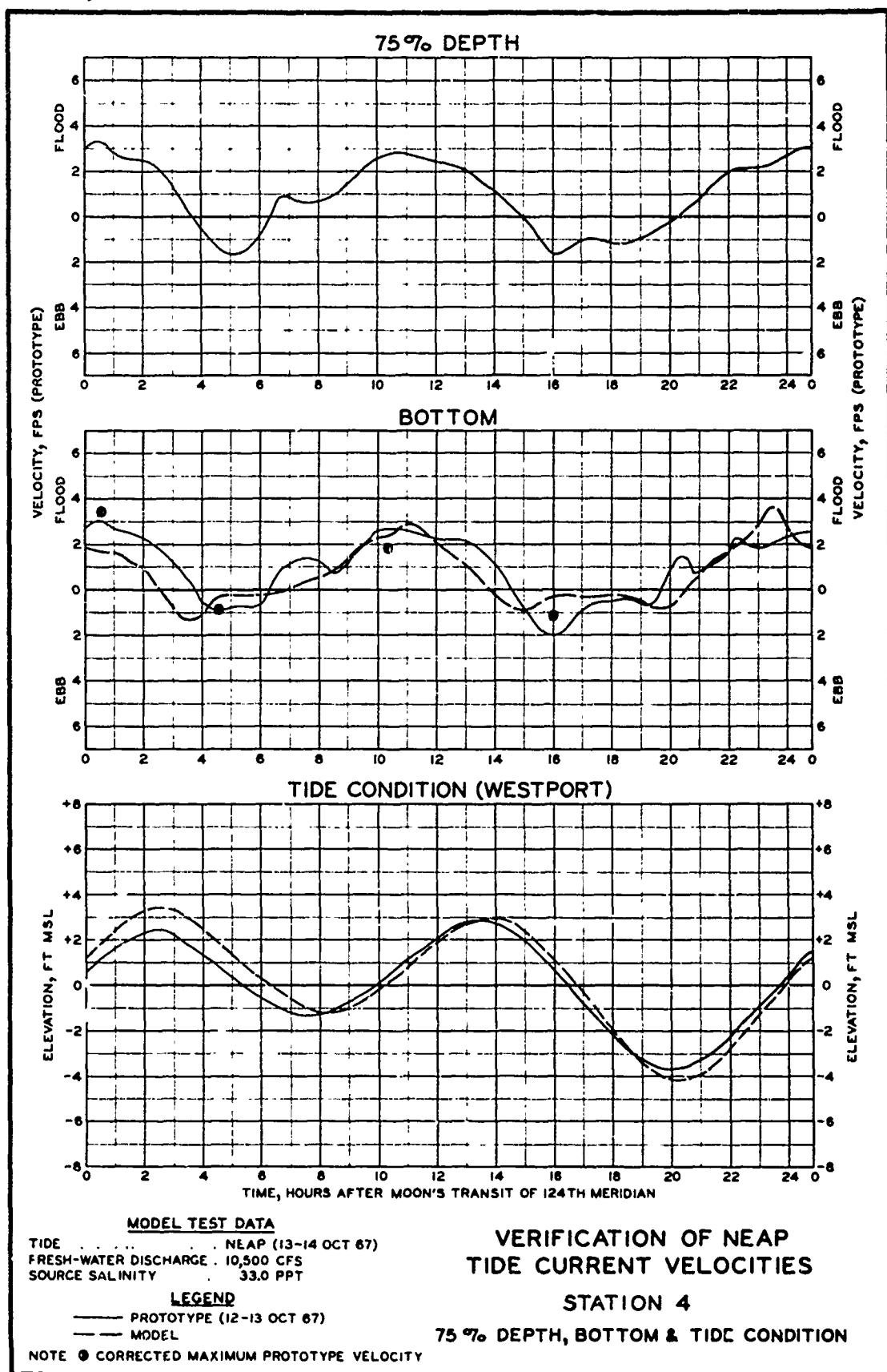


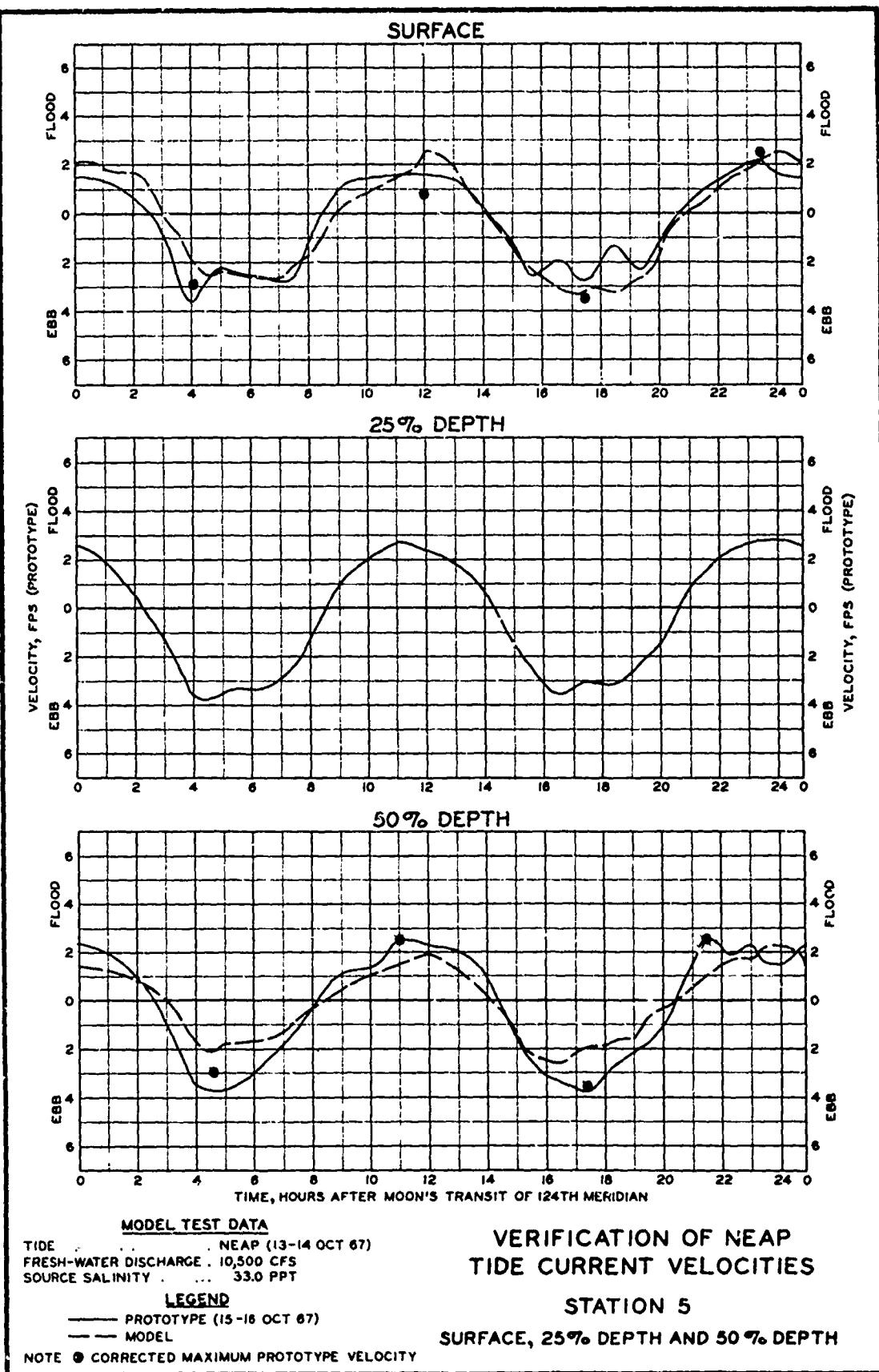
PLATE 41

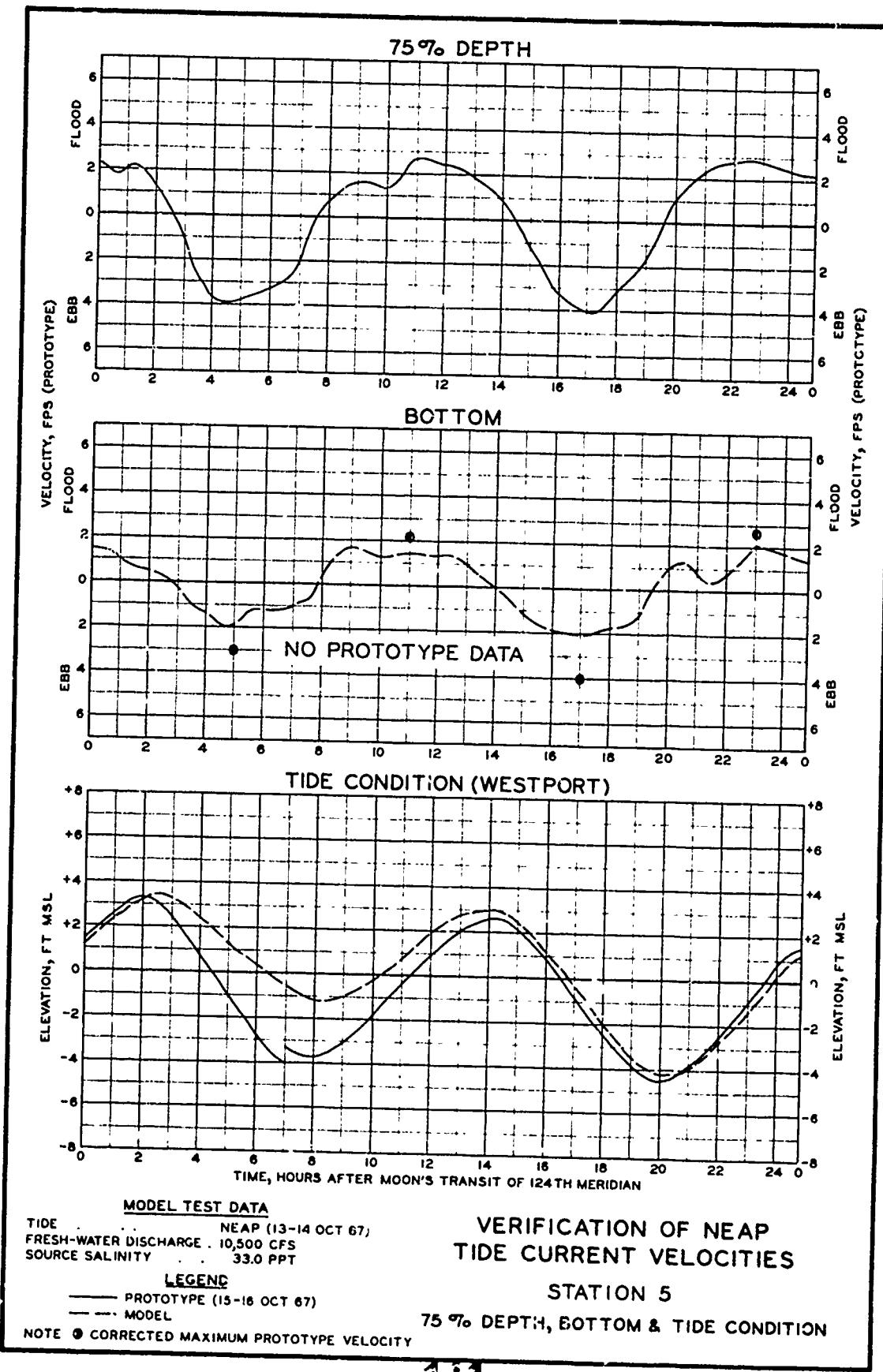












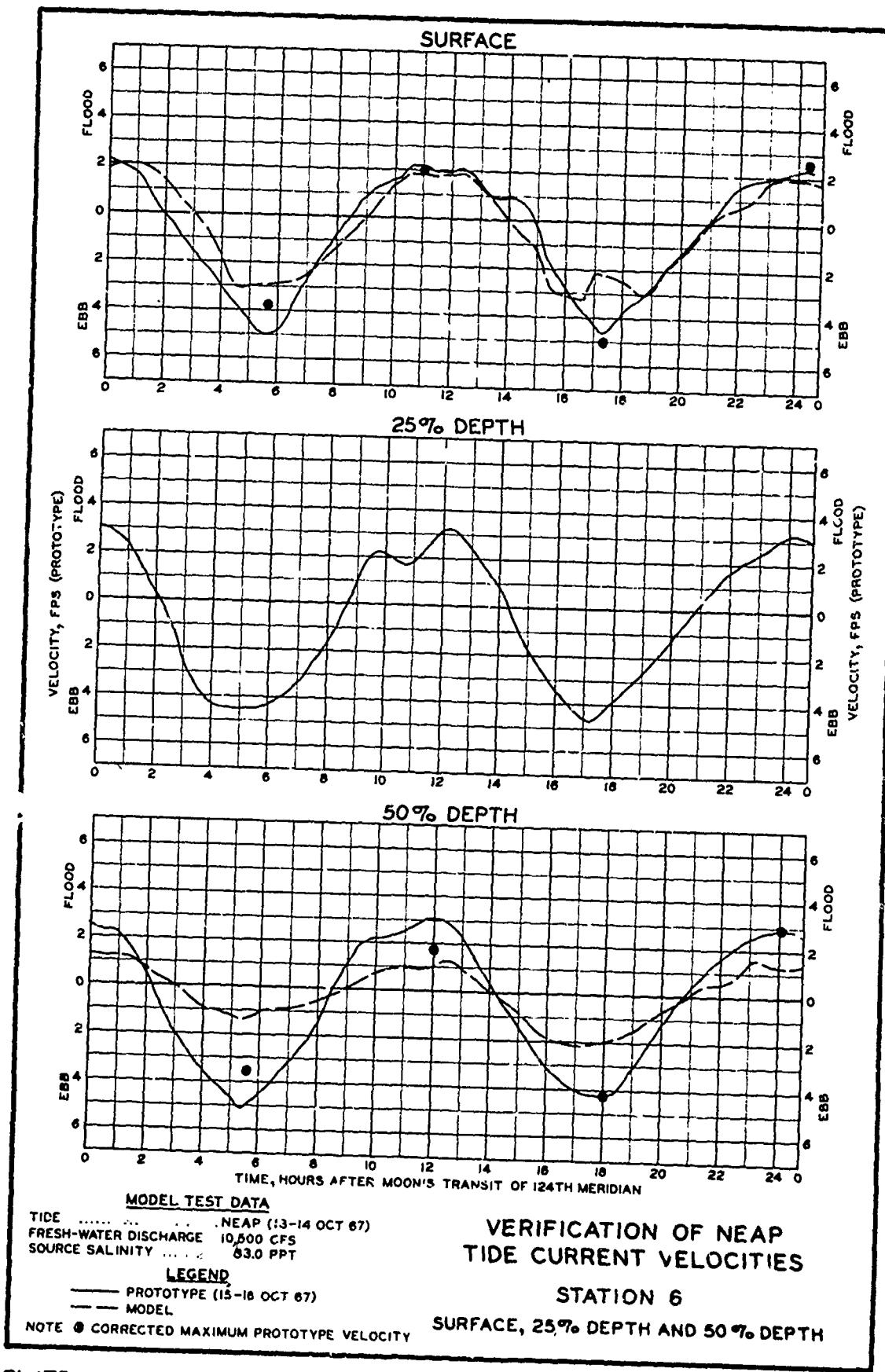
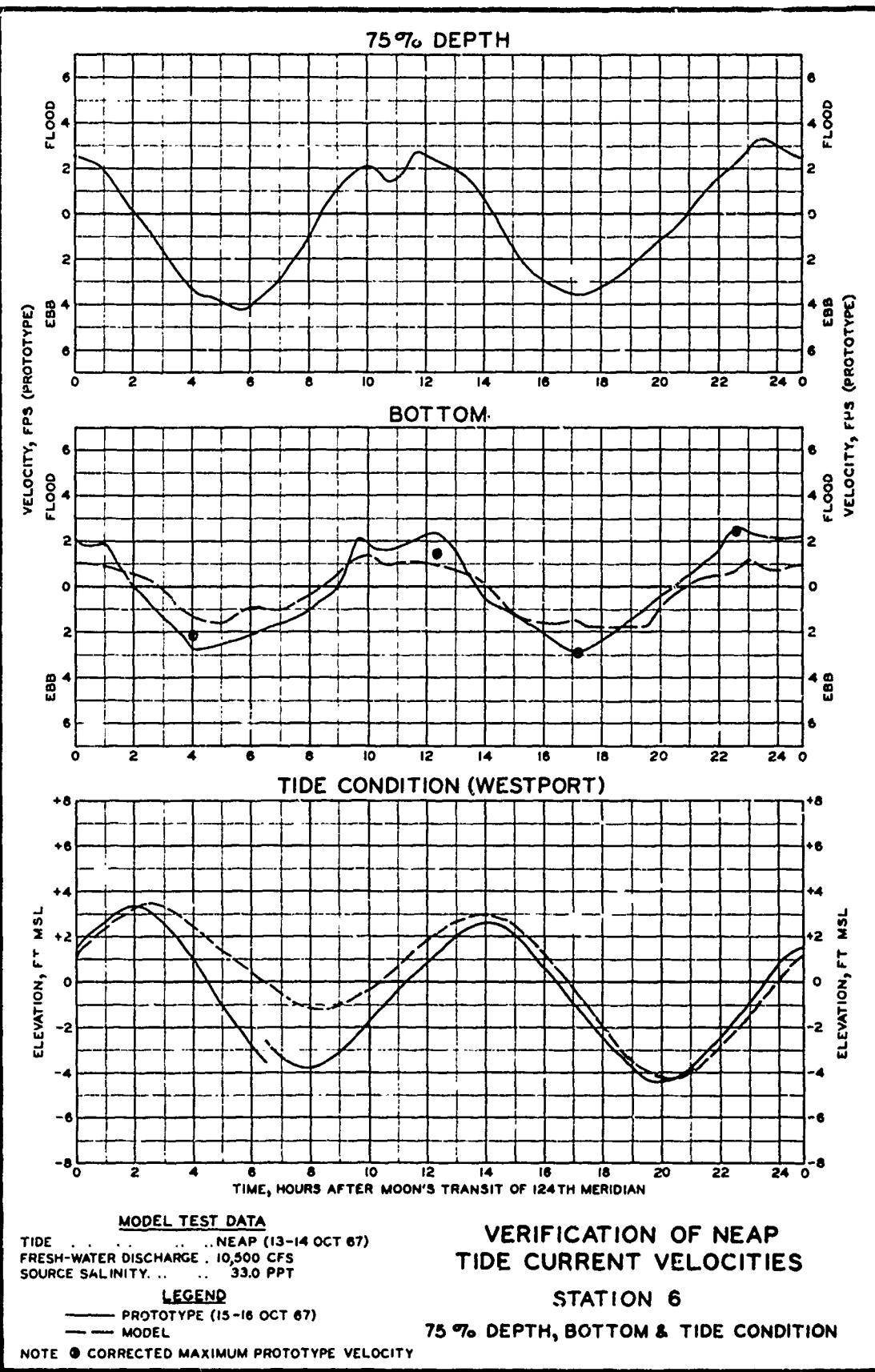


PLATE 48



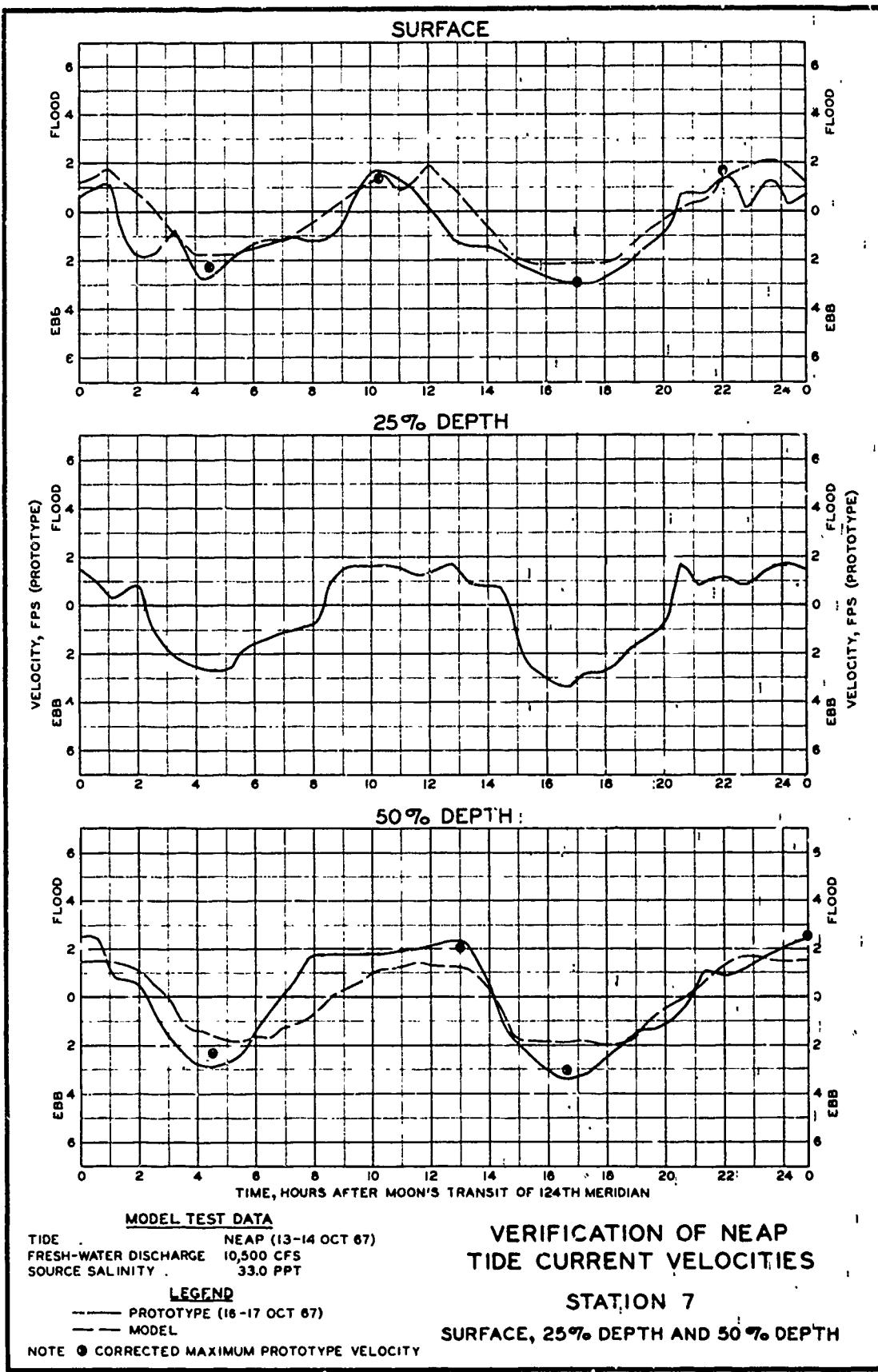
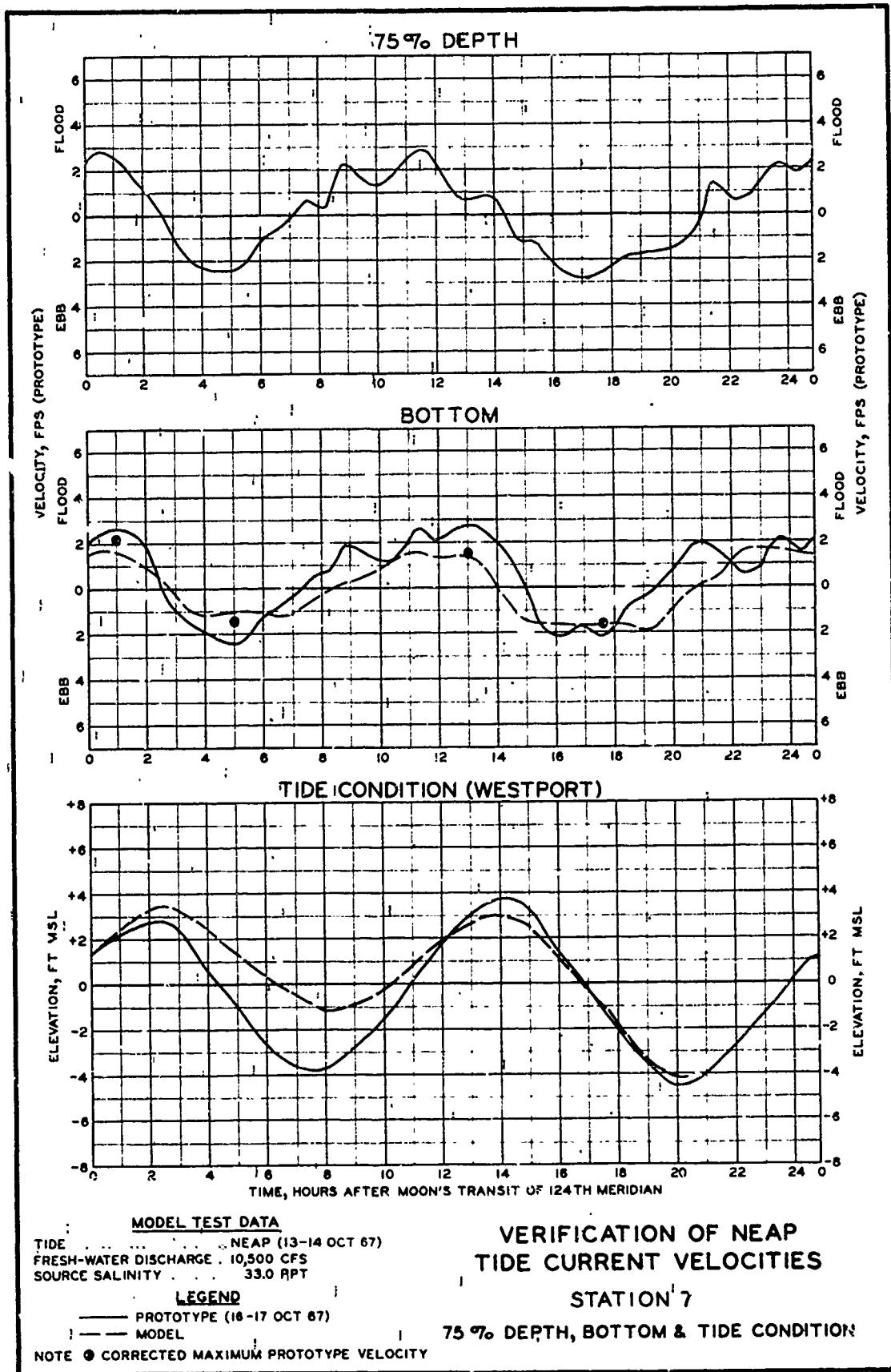
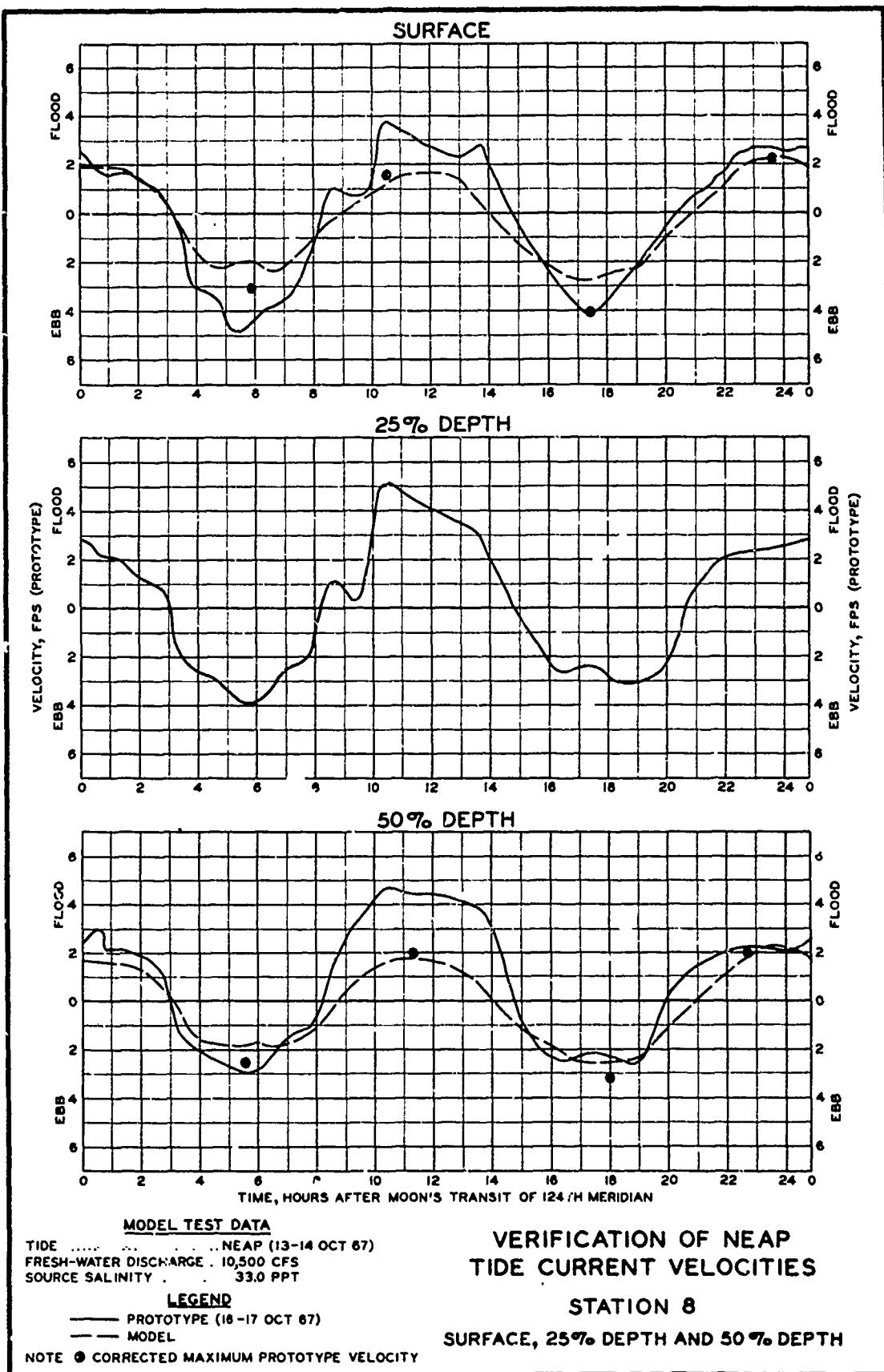
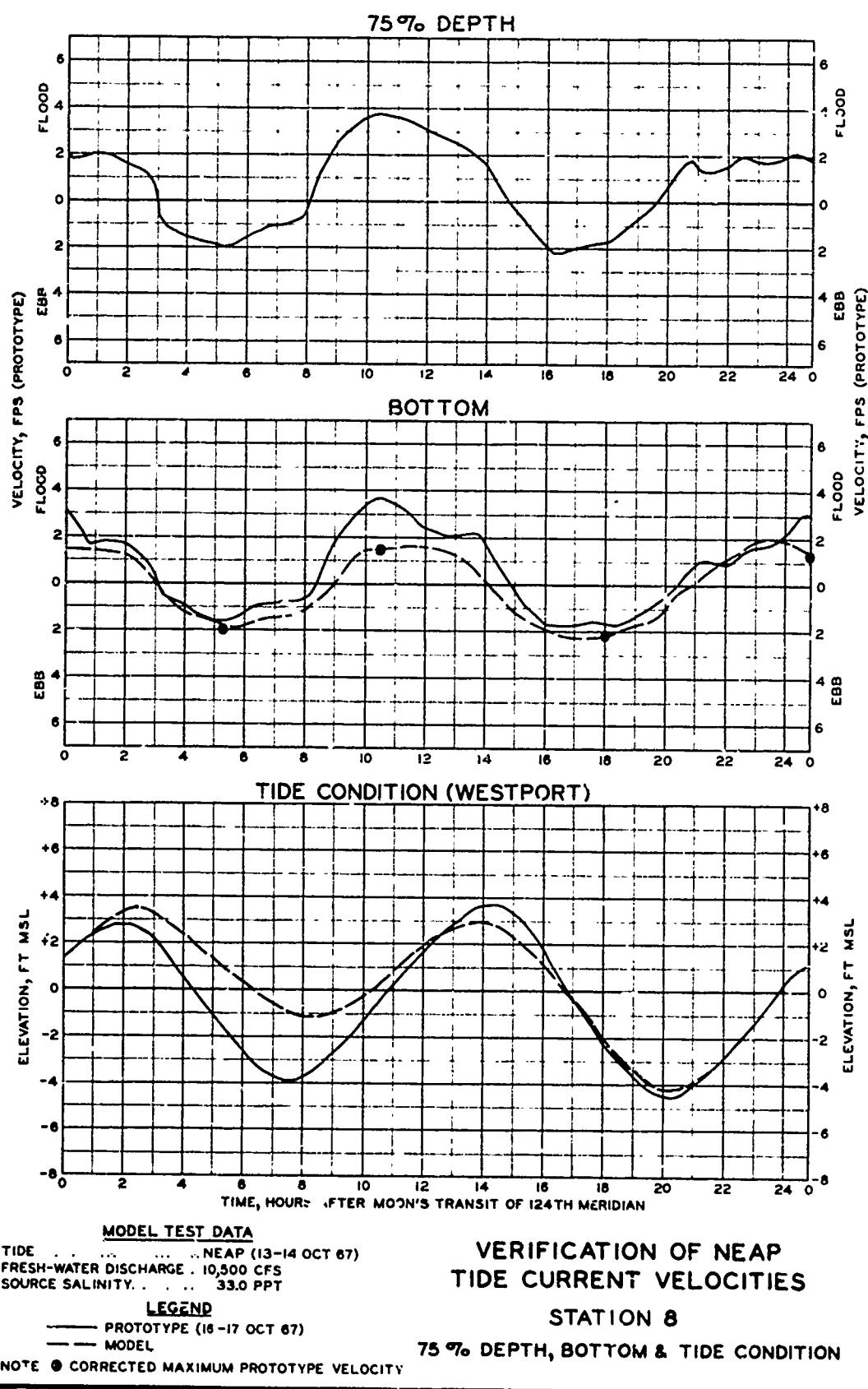


PLATE 50

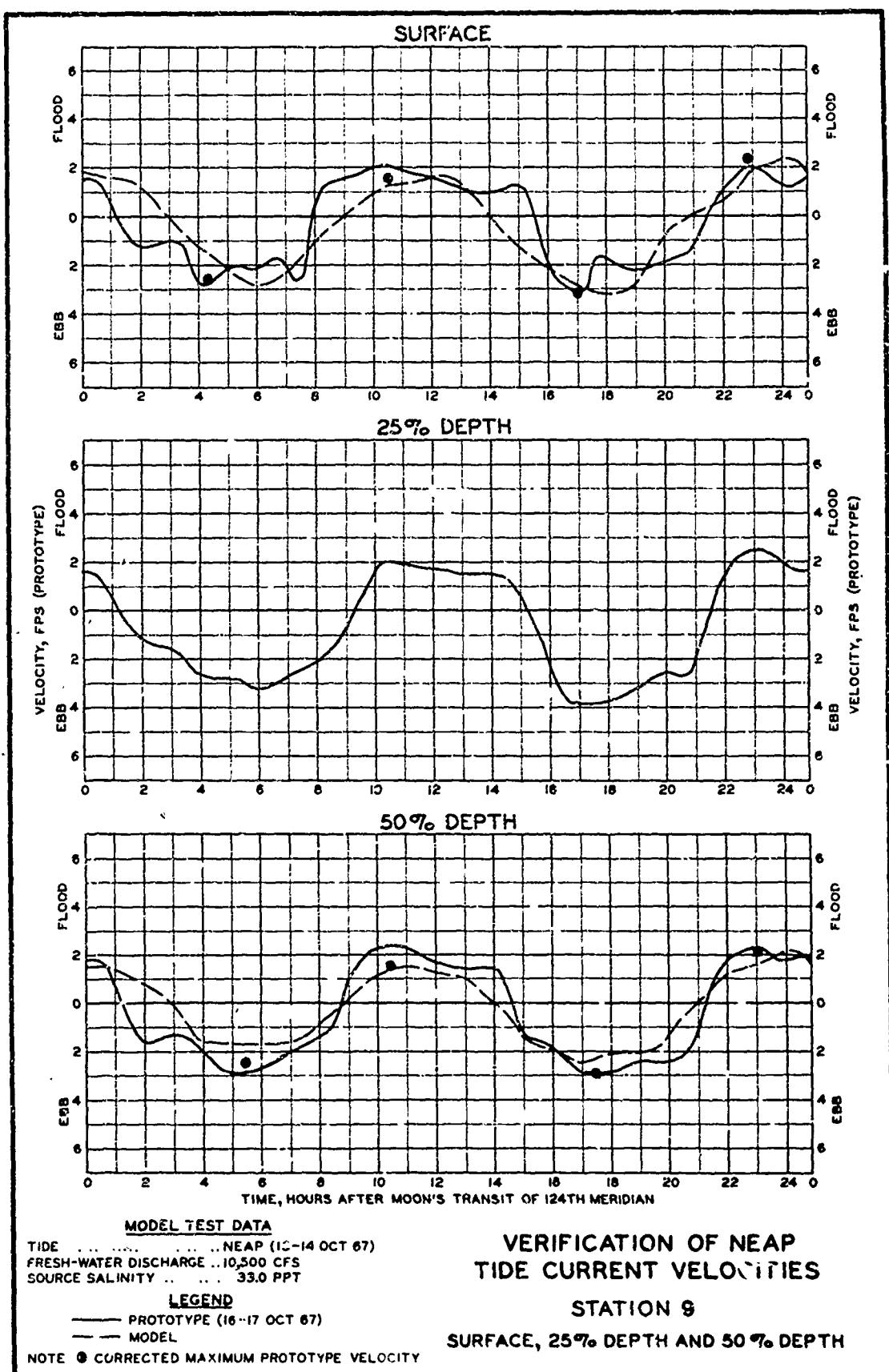


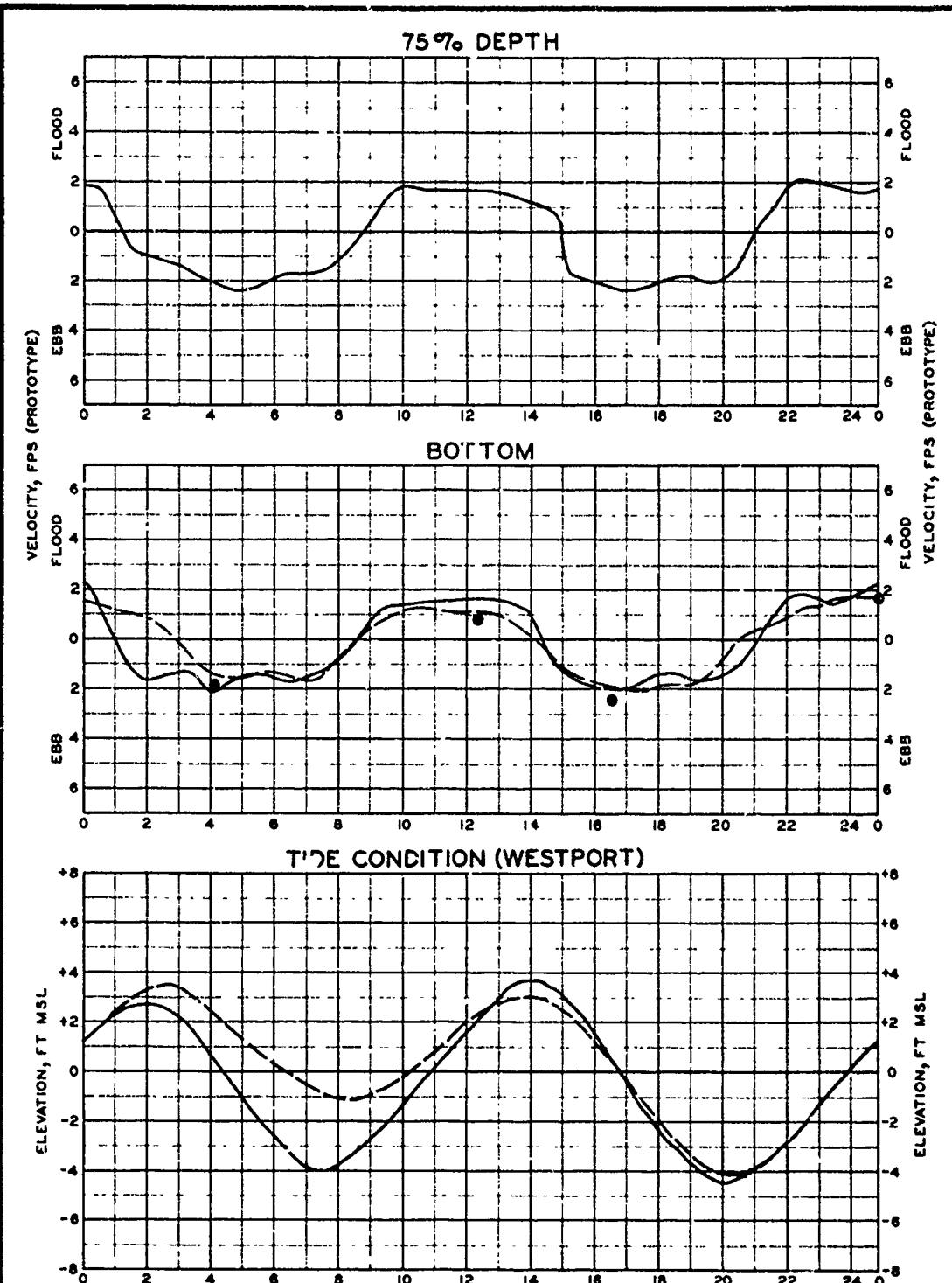




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PLATE 53





MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND

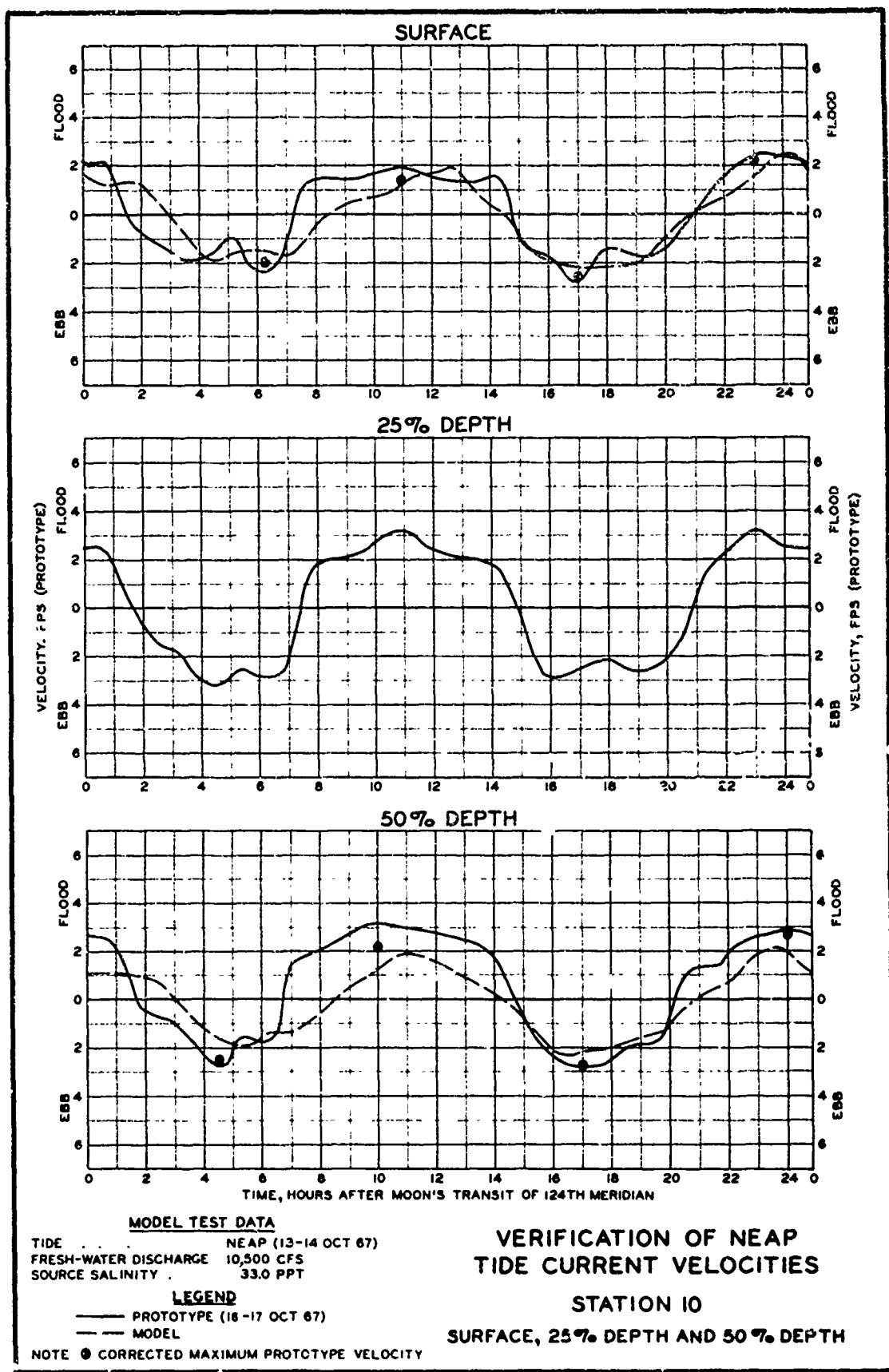
— PROTOTYPE (16-17 OCT 67)
 - - - MODEL

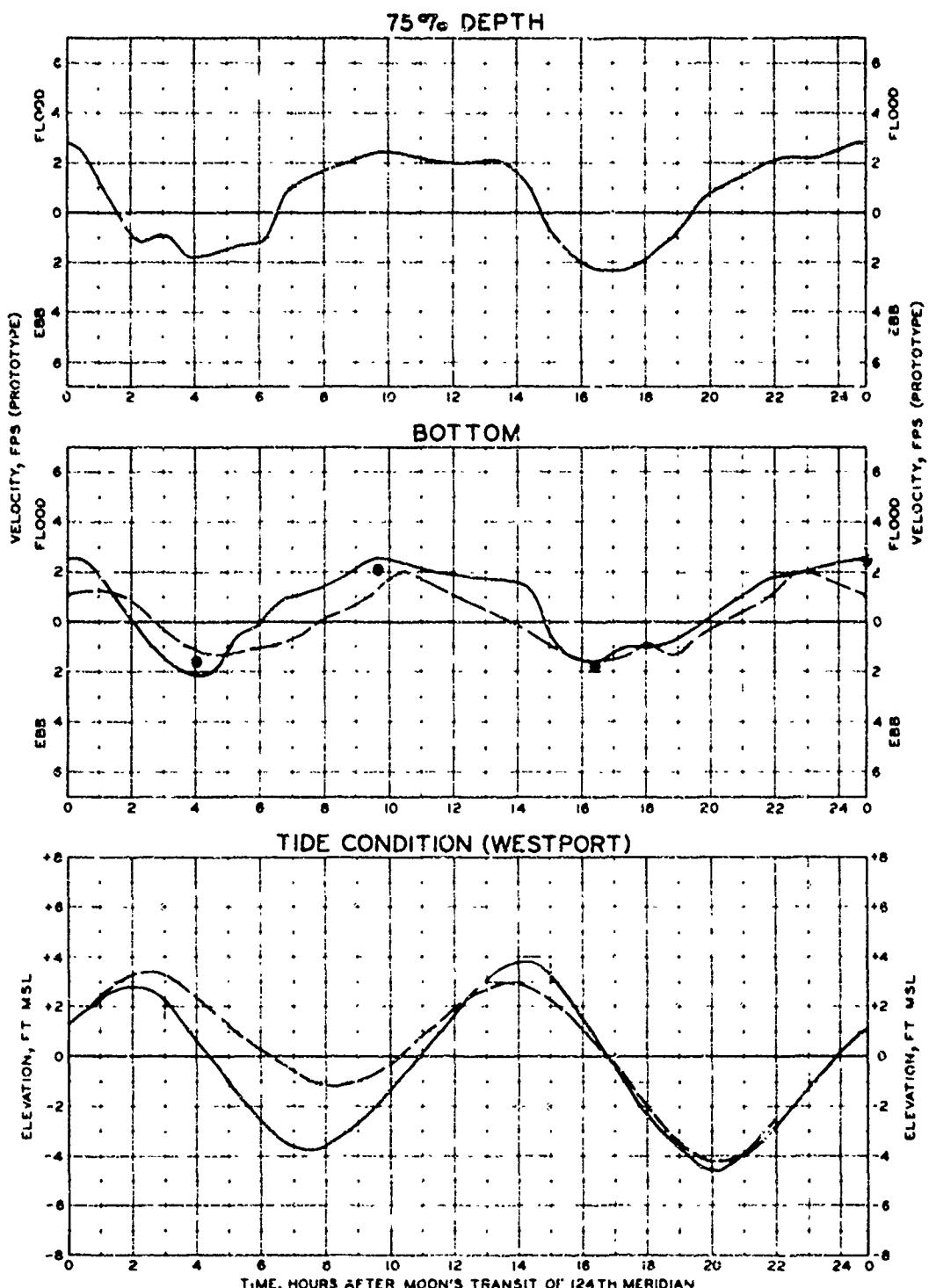
NOTE • CORRECTED MAXIMUM PROTOTYPE VELOCITY

**VERIFICATION OF NEAP
TIDE CURRENT VELOCITIES**

STATION 9

75% DEPTH, BOTTOM & TIDE CONDITION





MODEL TEST DATA

TIDE NEAP (13-14 OCT 87)
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY 330 PPT

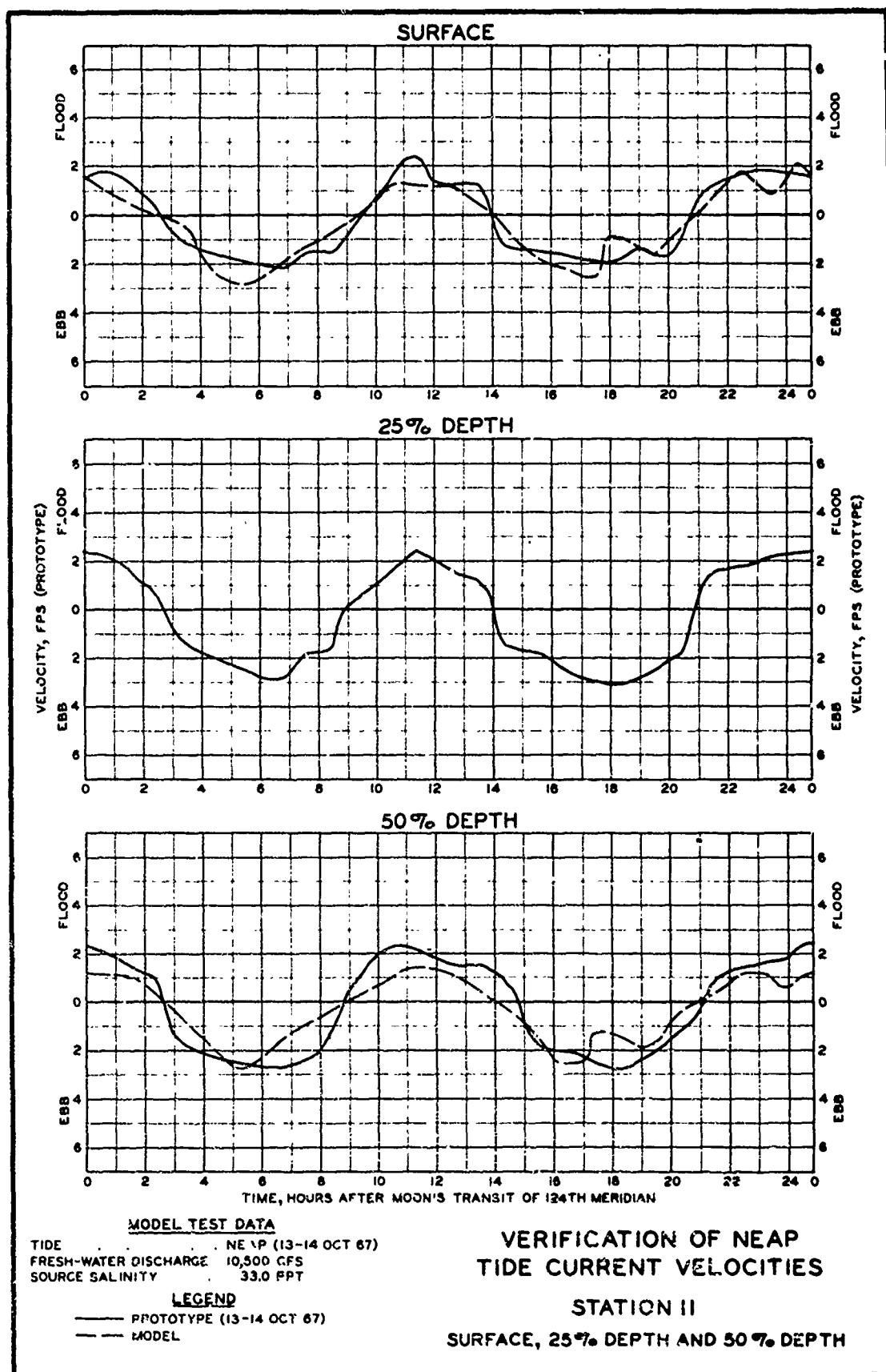
**VERIFICATION OF NEAP
TIDE CURRENT VELOCITIES**

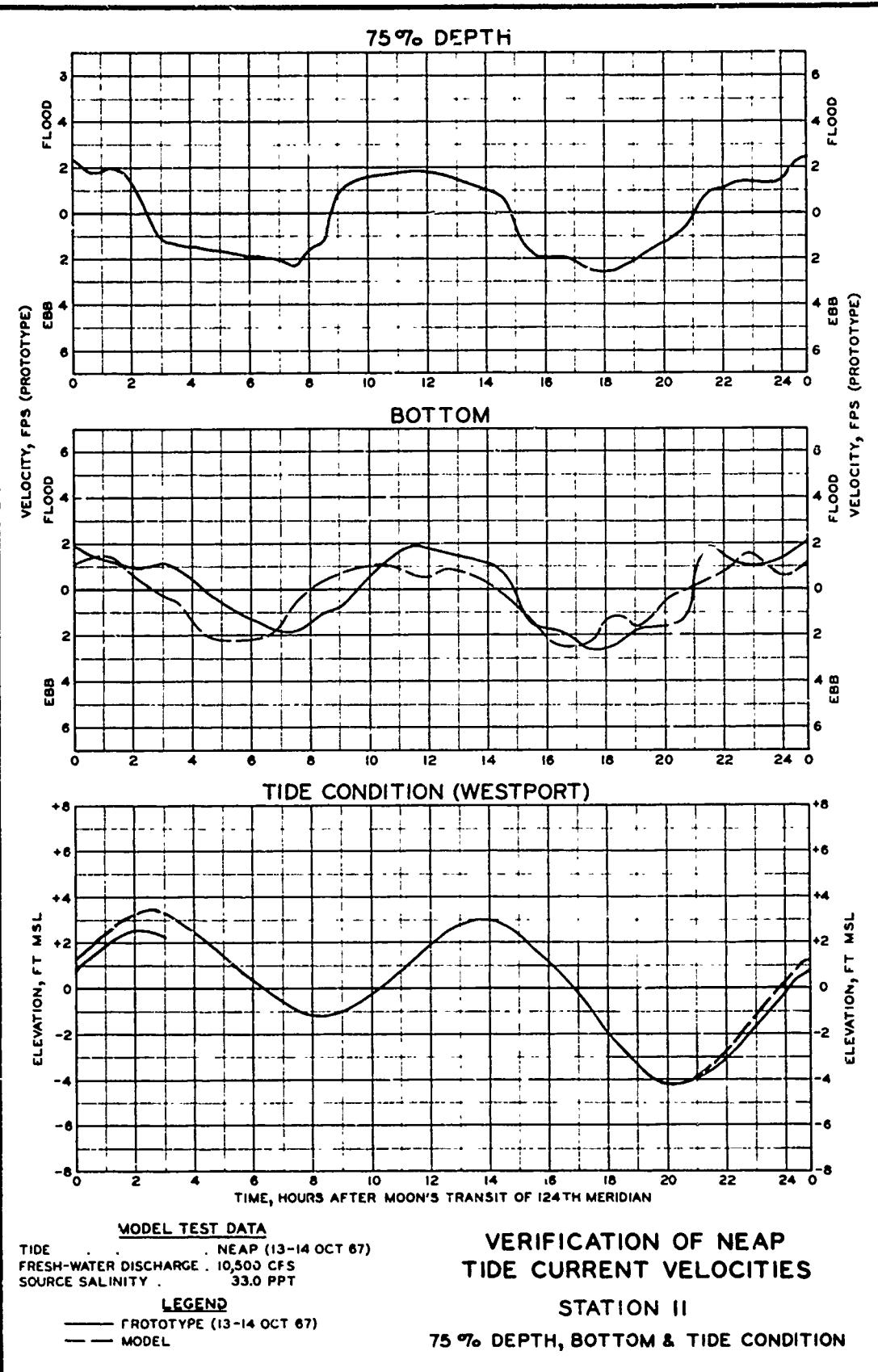
STATION 10

75% DEPTH, BOTTOM & TIDE CONDITION

LEGEND

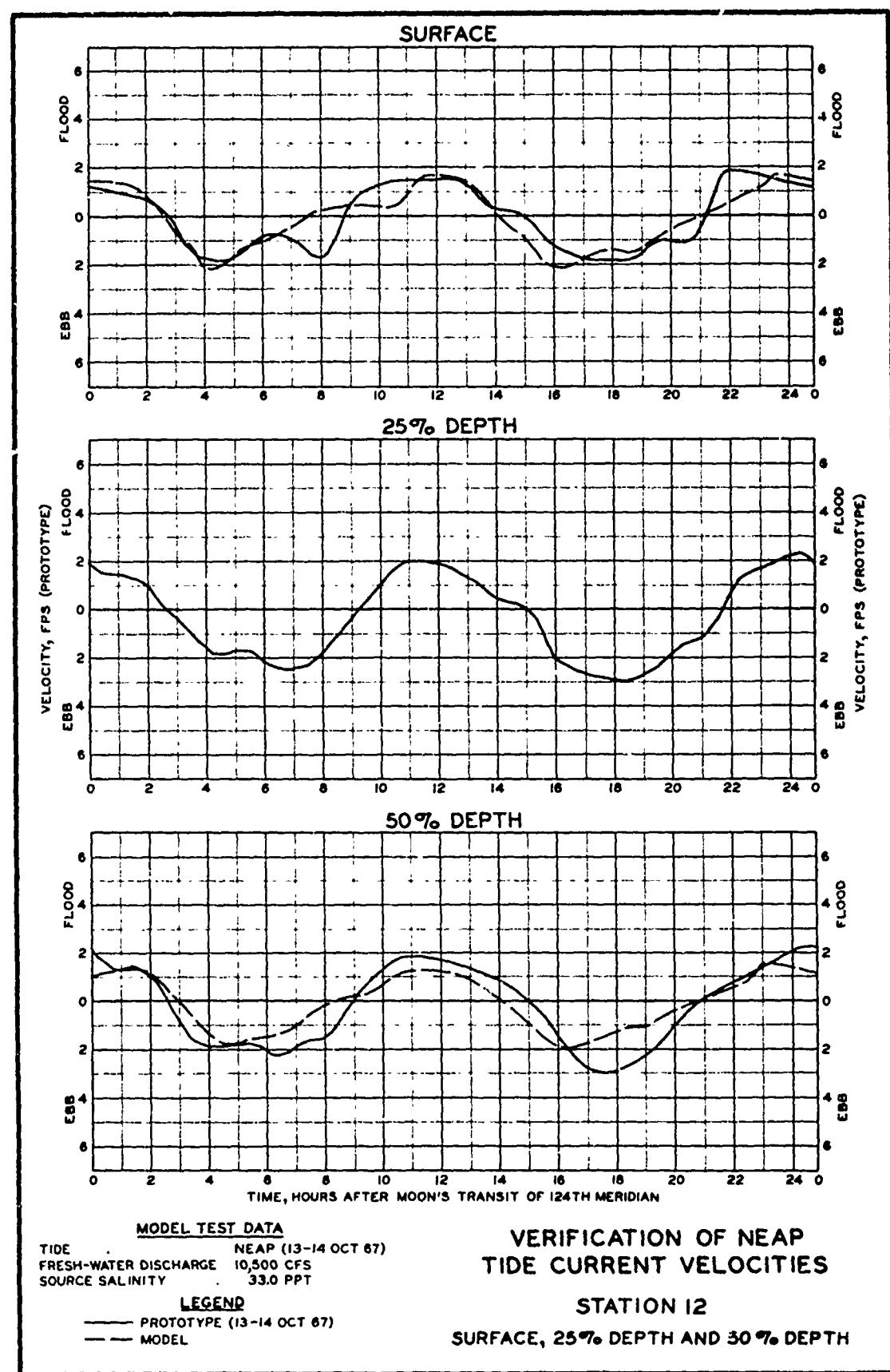
- PROTOTYPE (16-17 OCT 87)
- MODEL
- CORRECTED MAXIMUM PROTOTYPE VELOCITY

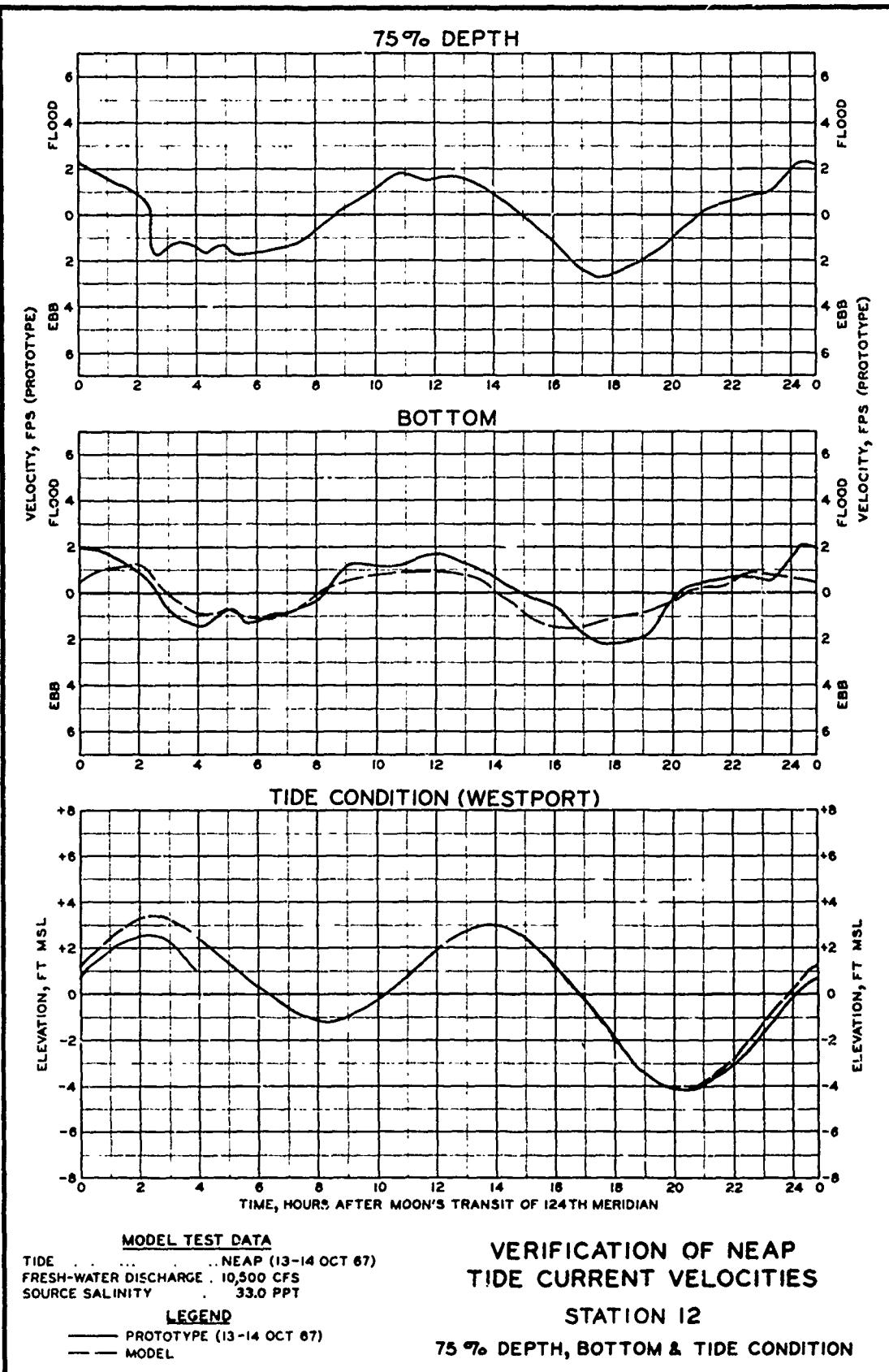




243

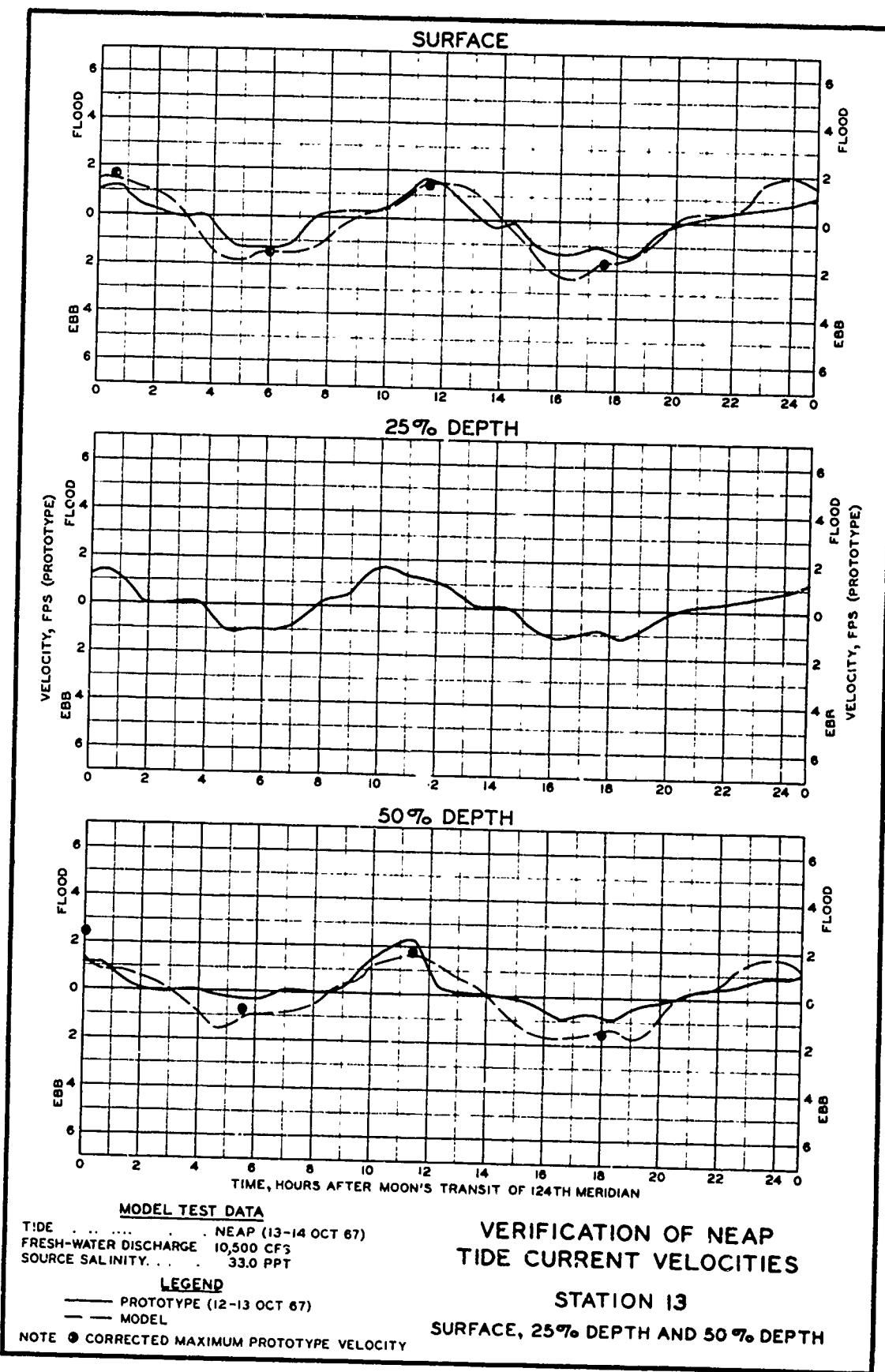
PLATE 59

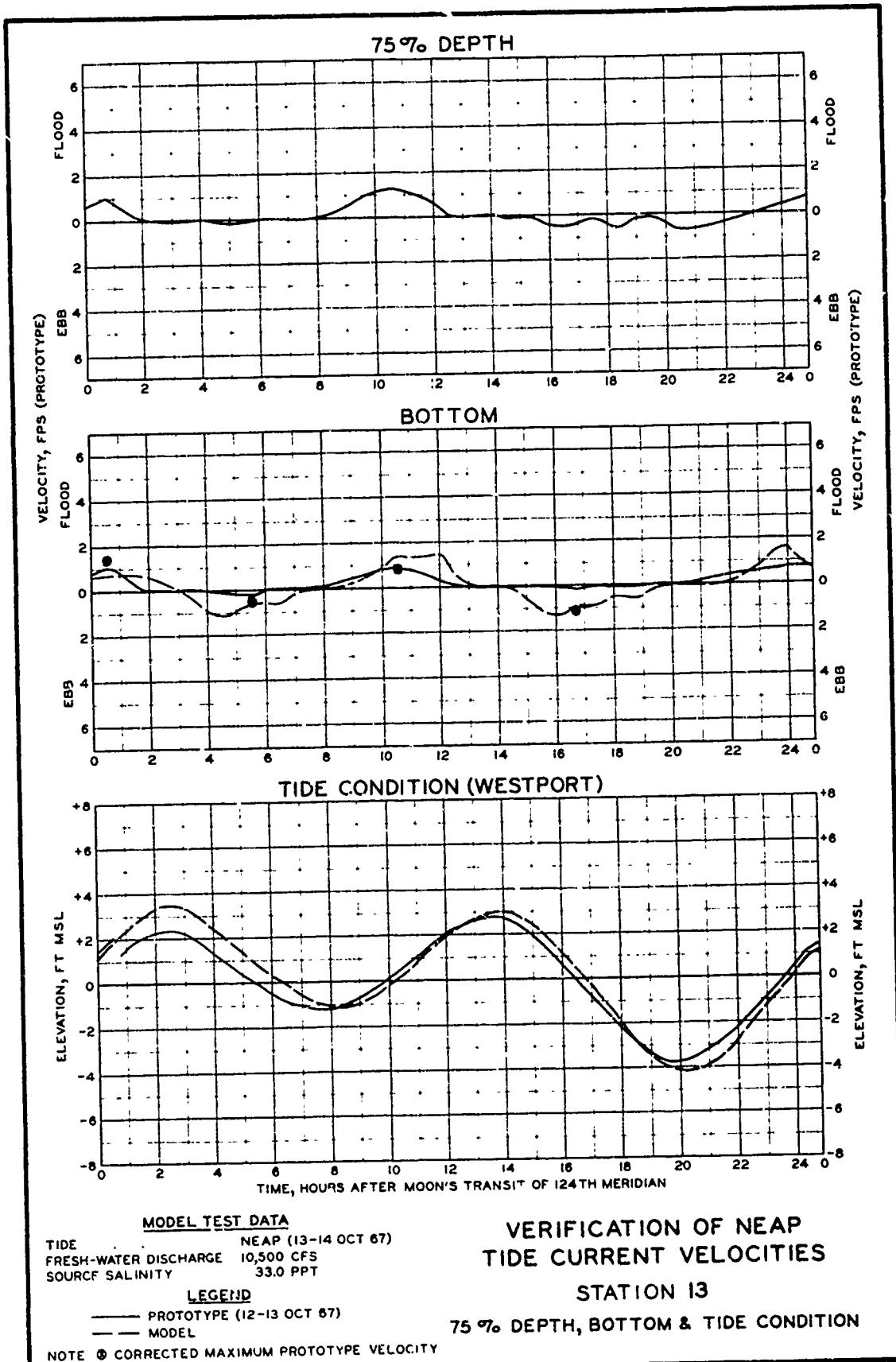


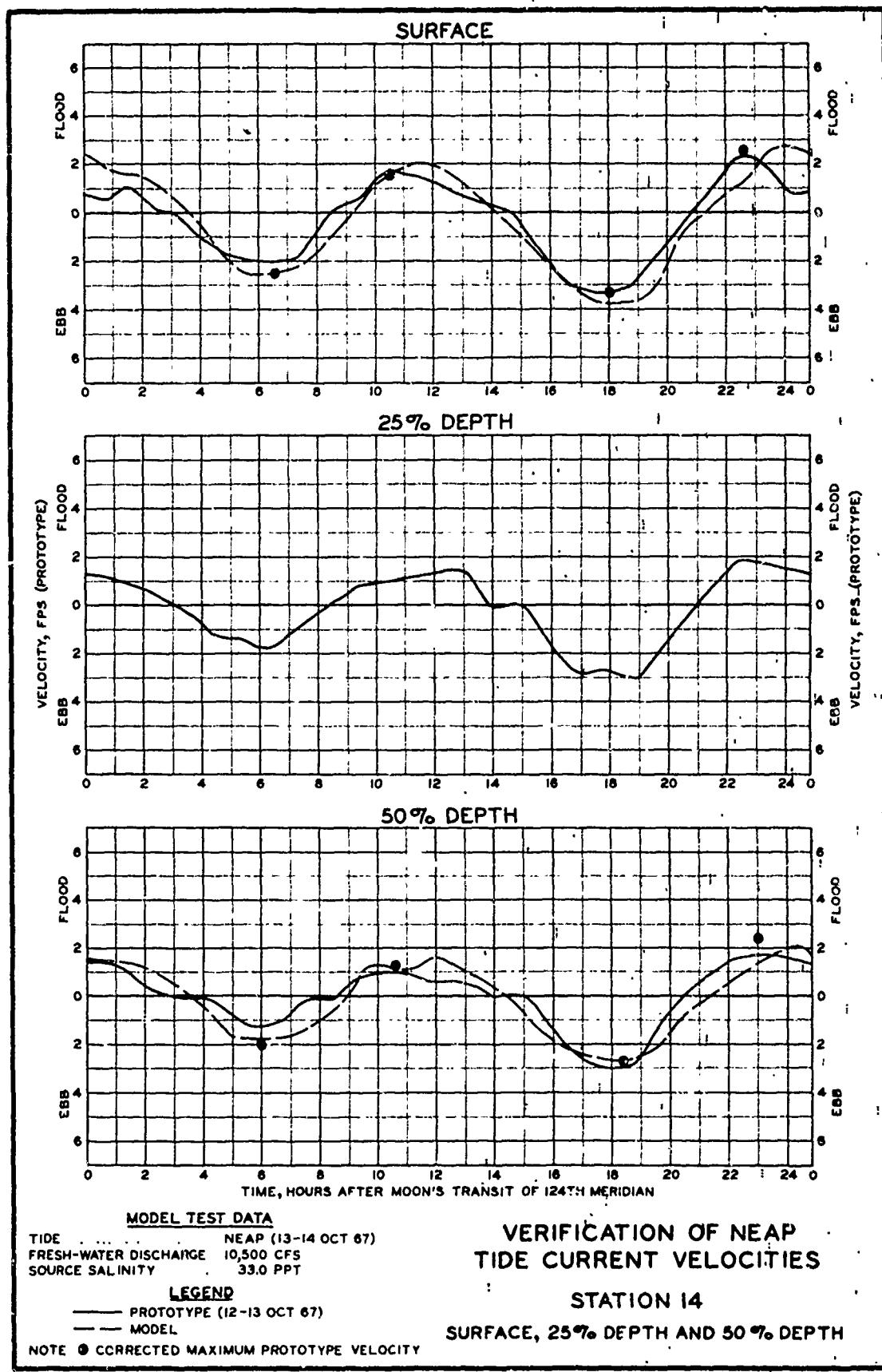


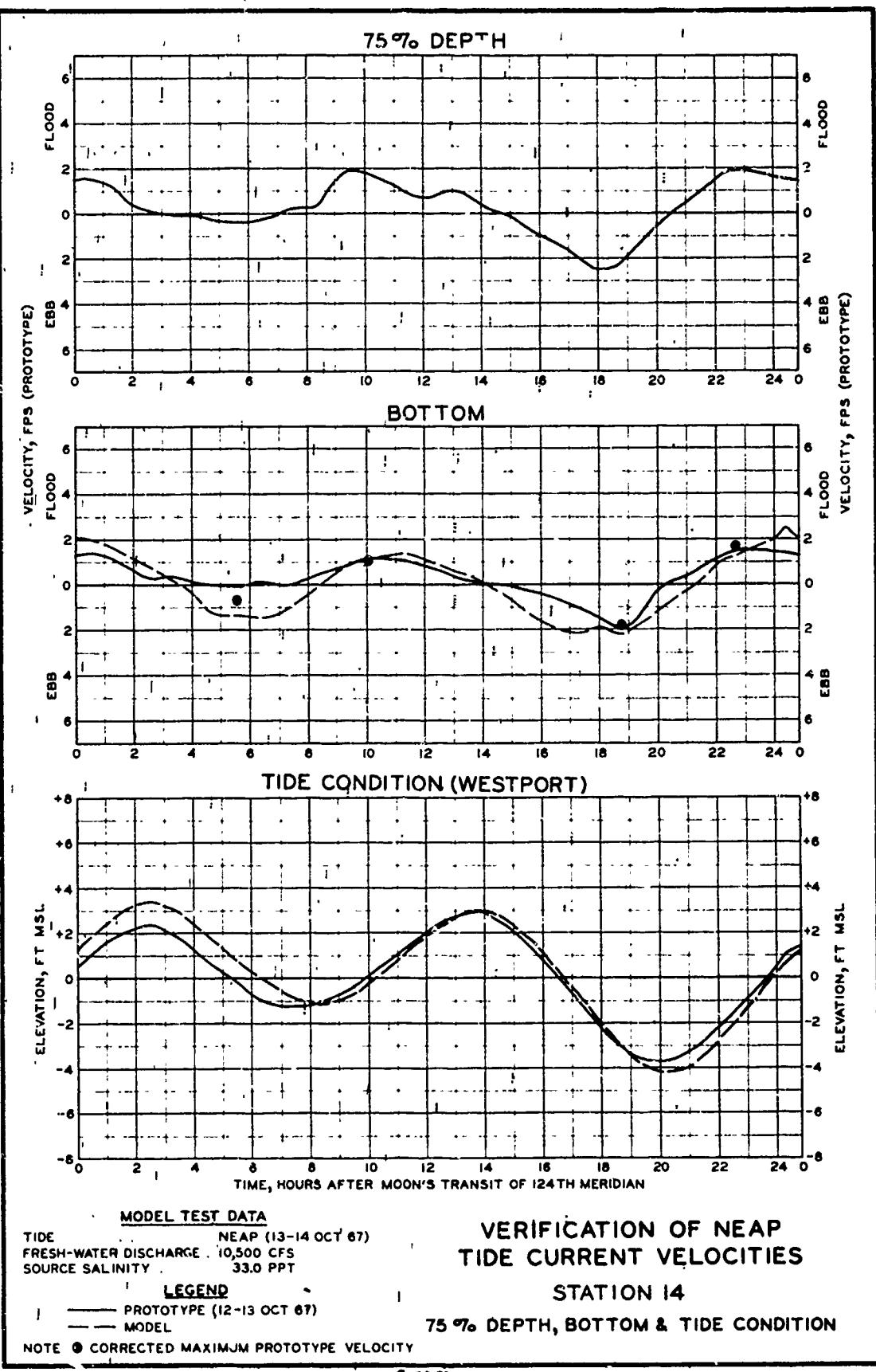
2405

PLATE 61



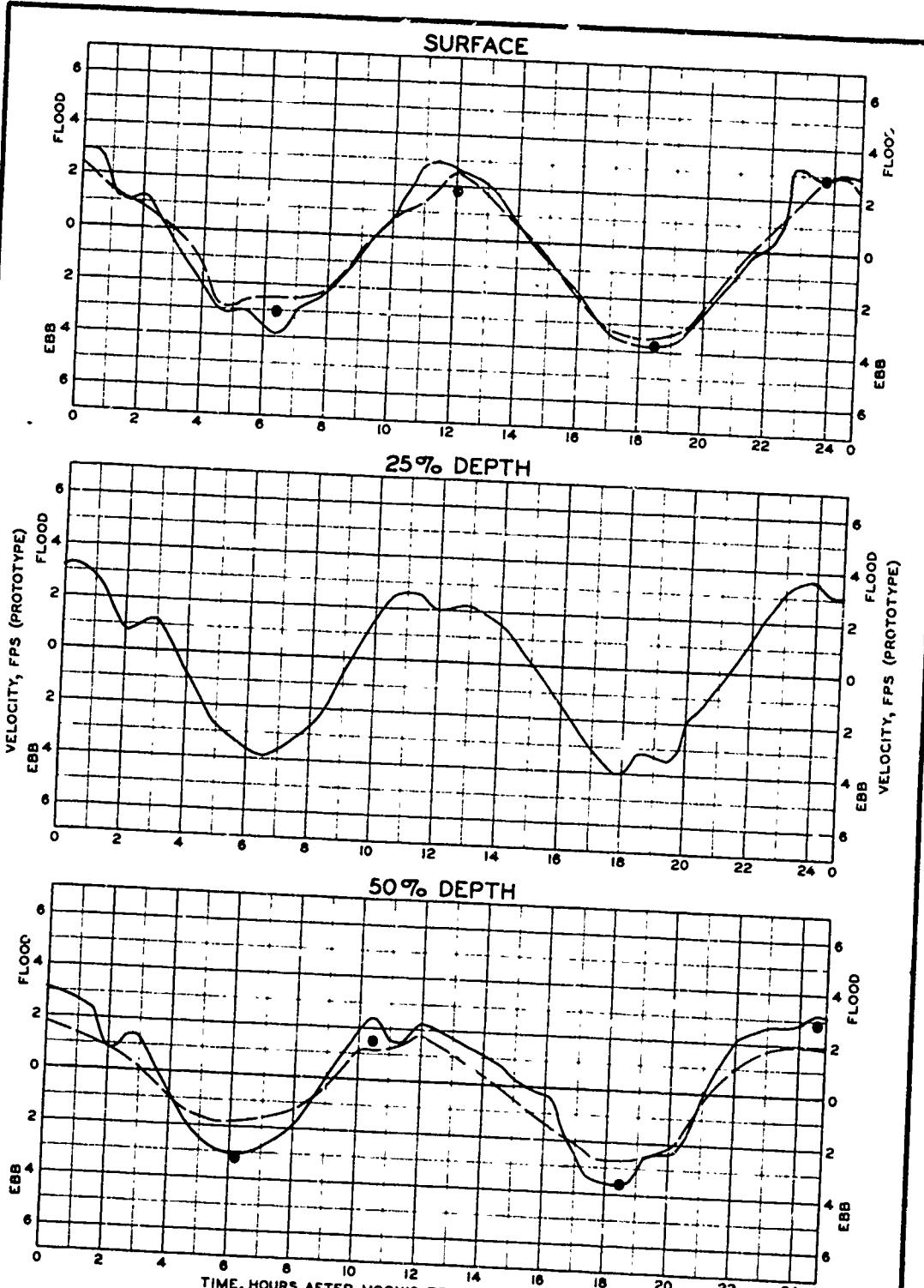






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PLATE 65

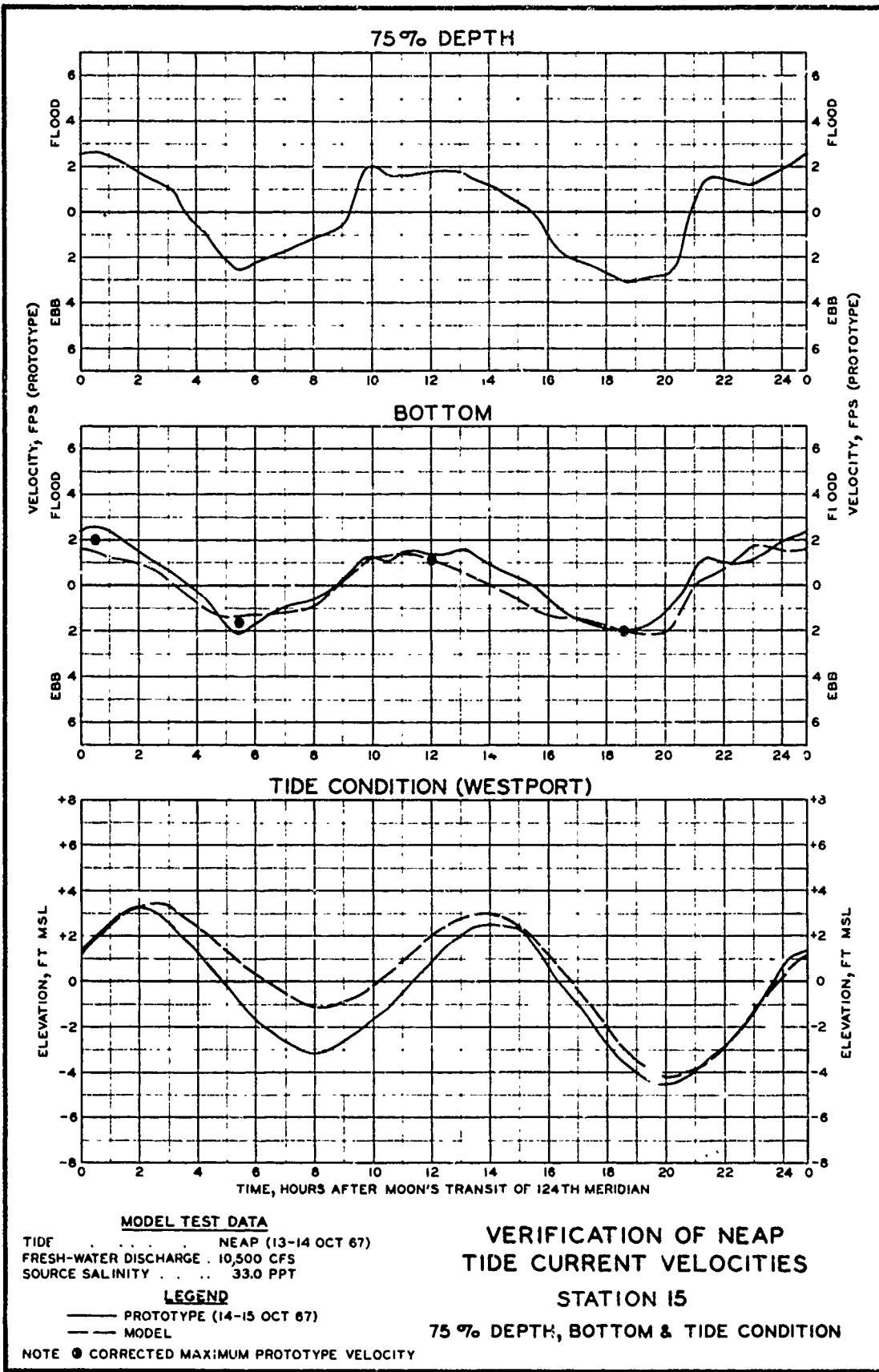


VERIFICATION OF NEAP TIDE CURRENT VELOCITIES

STATION 15

SURFACE, 25% DEPTH AND 50% DEPTH

LEGEND
 — PROTOTYPE (14-15 OCT 67)
 - - MODEL
 NOTE • CORRECTED MAXIMUM PROTOTYPE VELOCITY



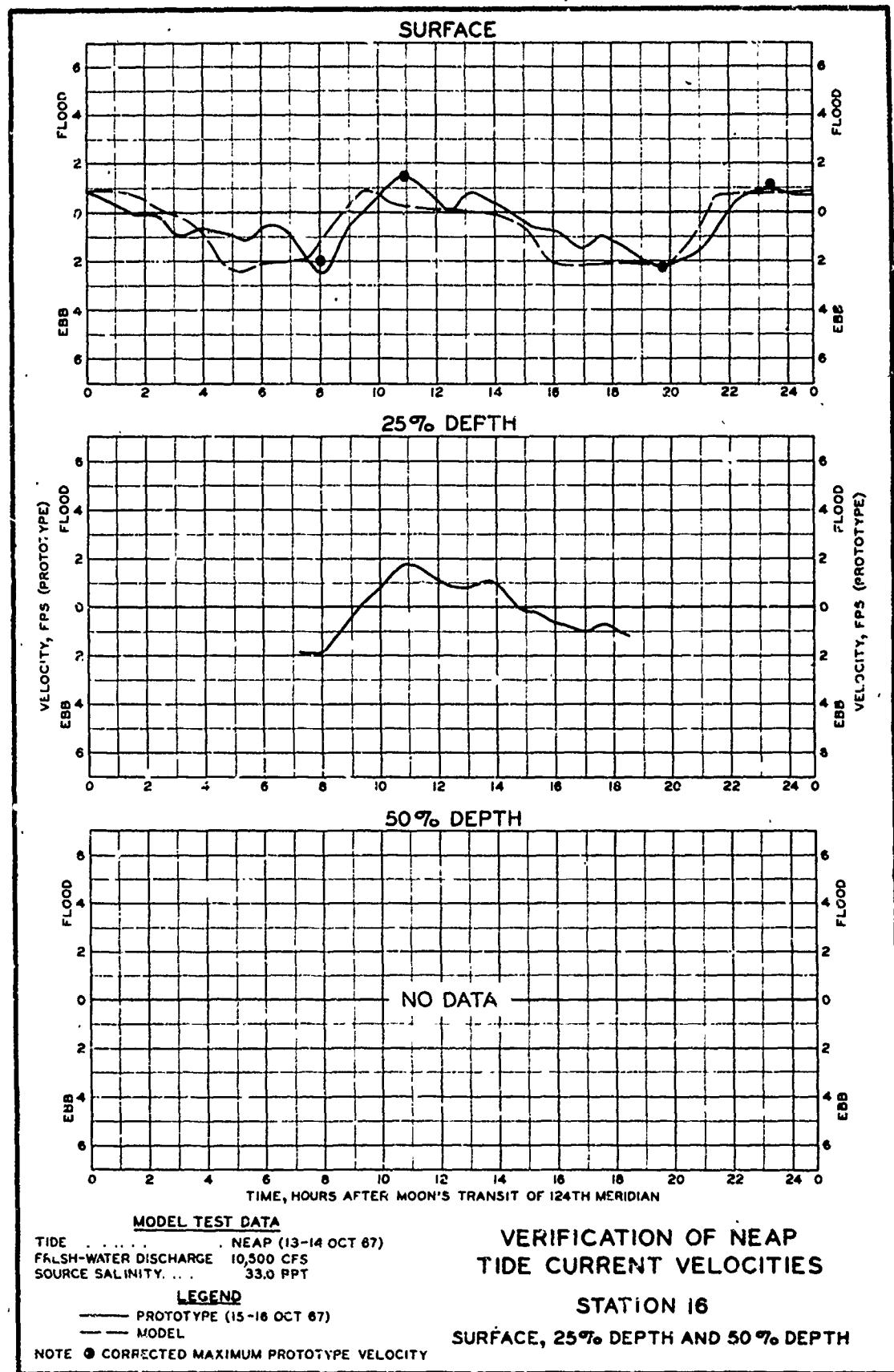
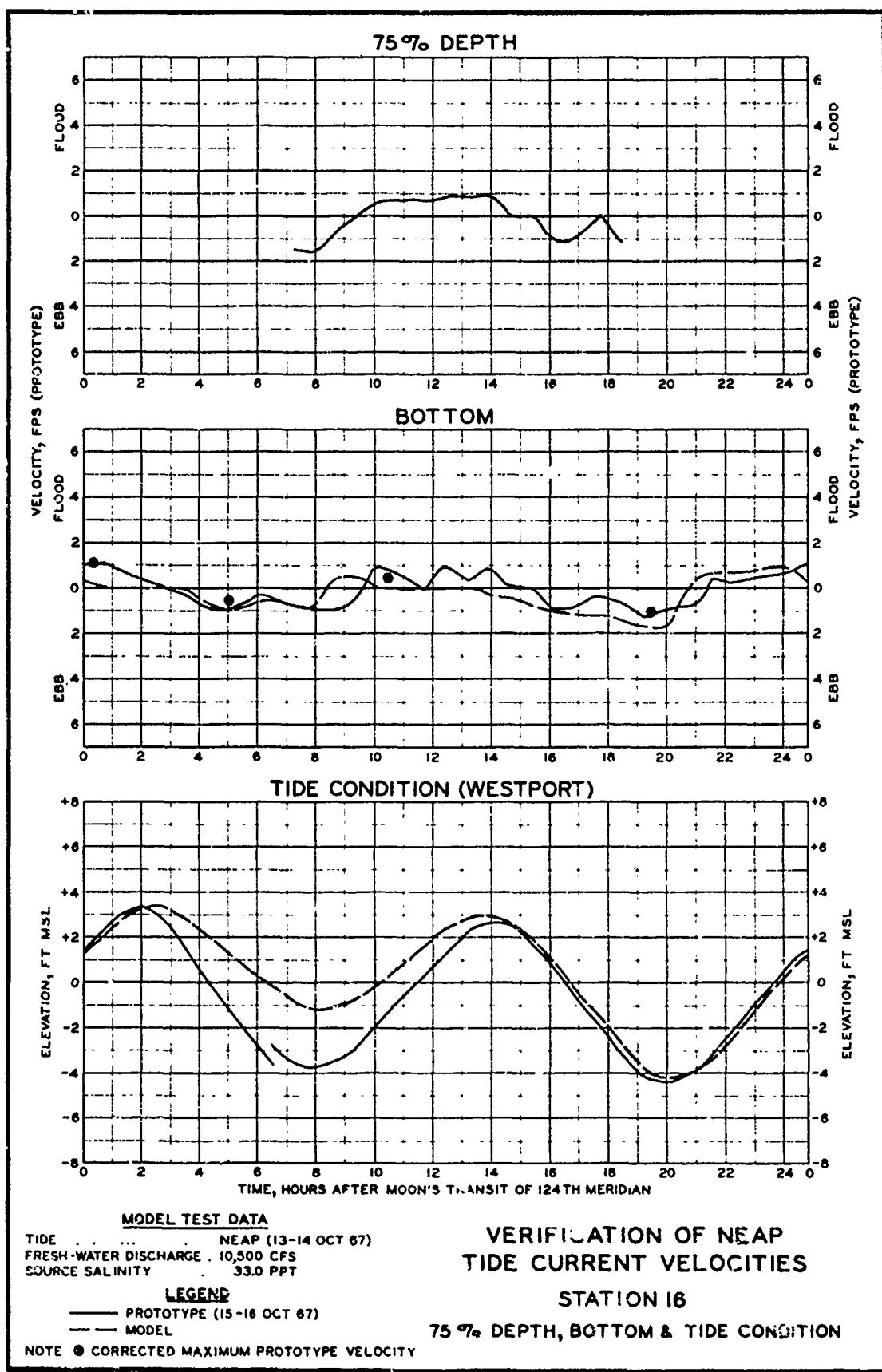


PLATE 68

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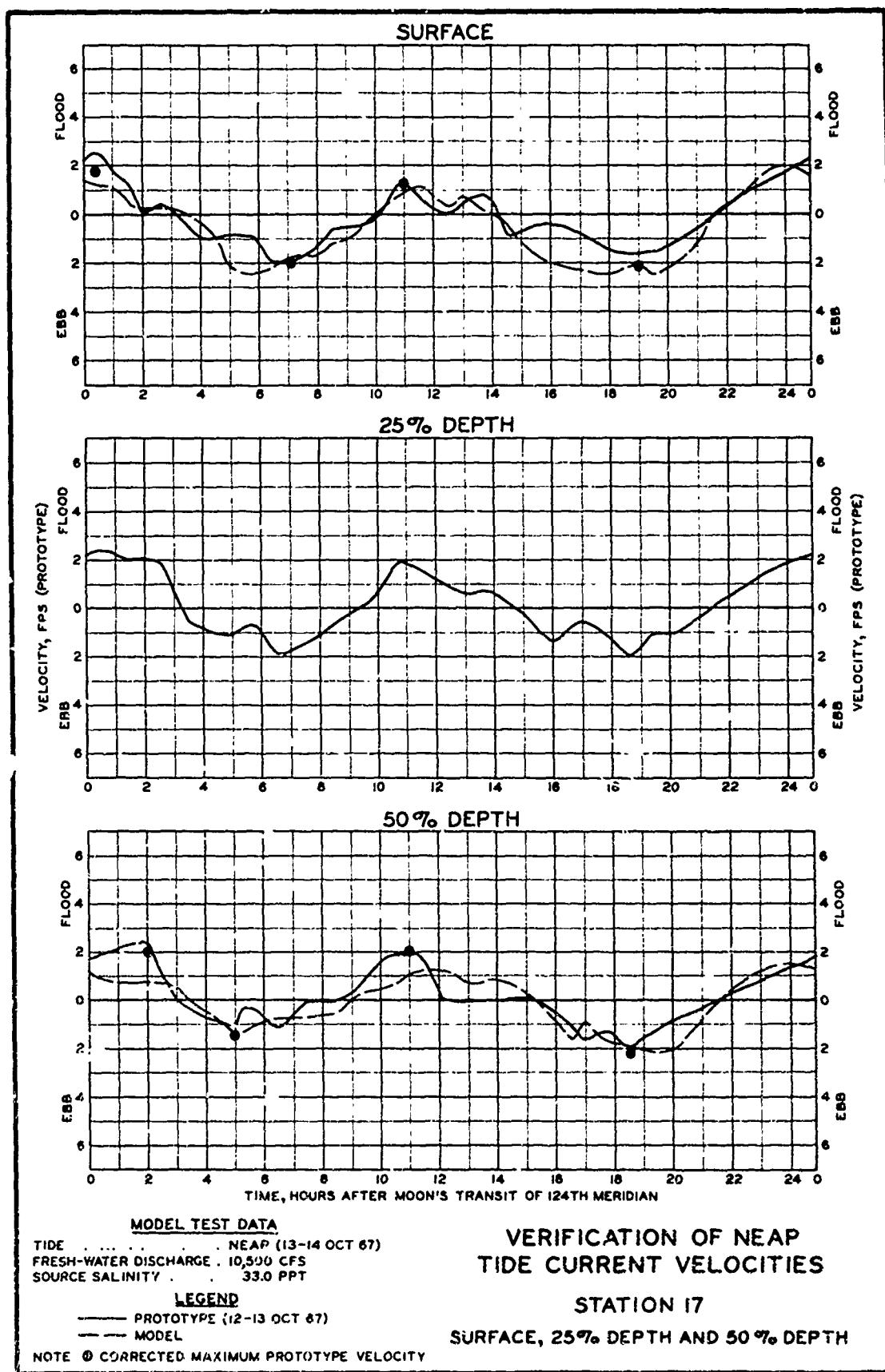
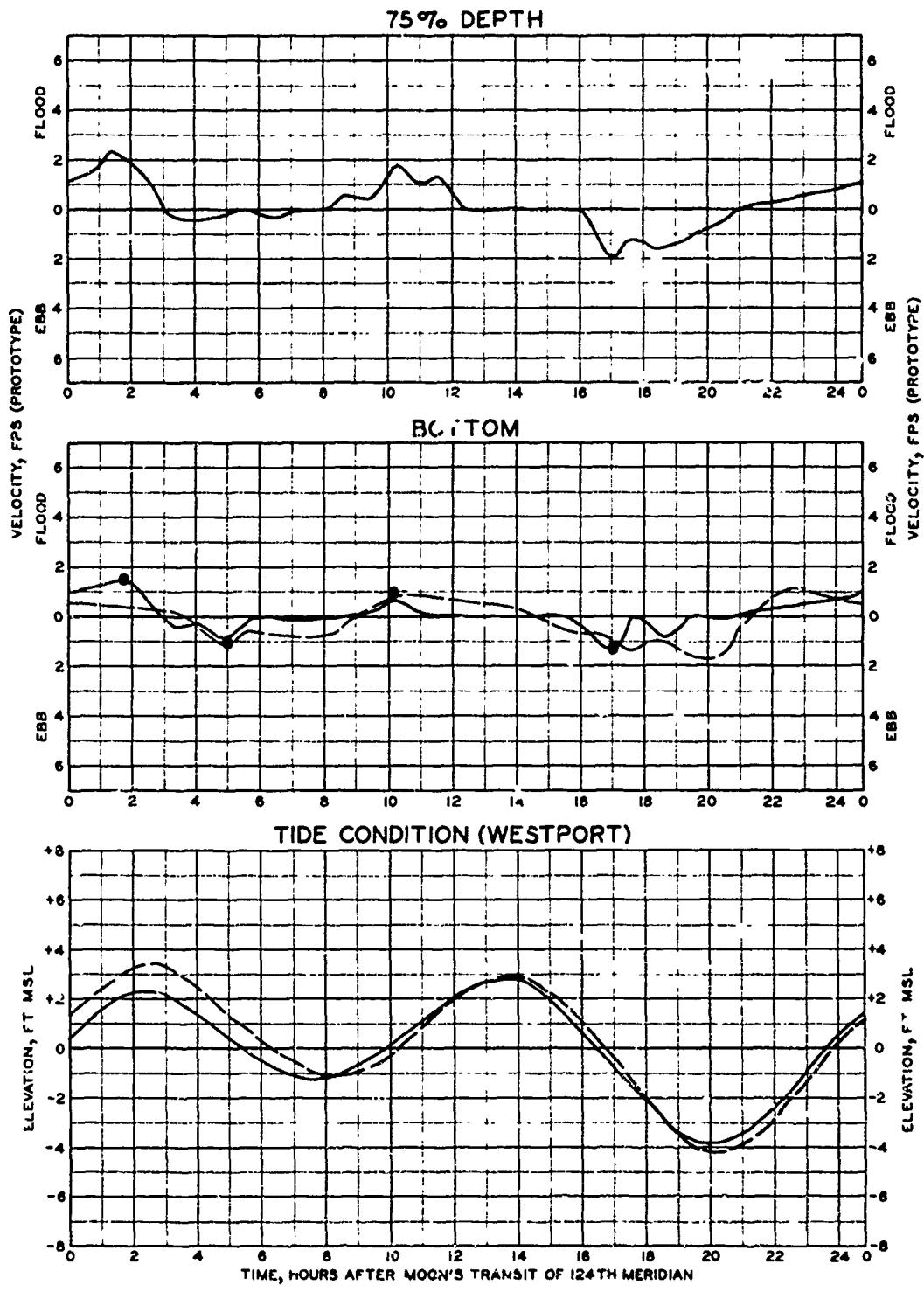


PLATE 70

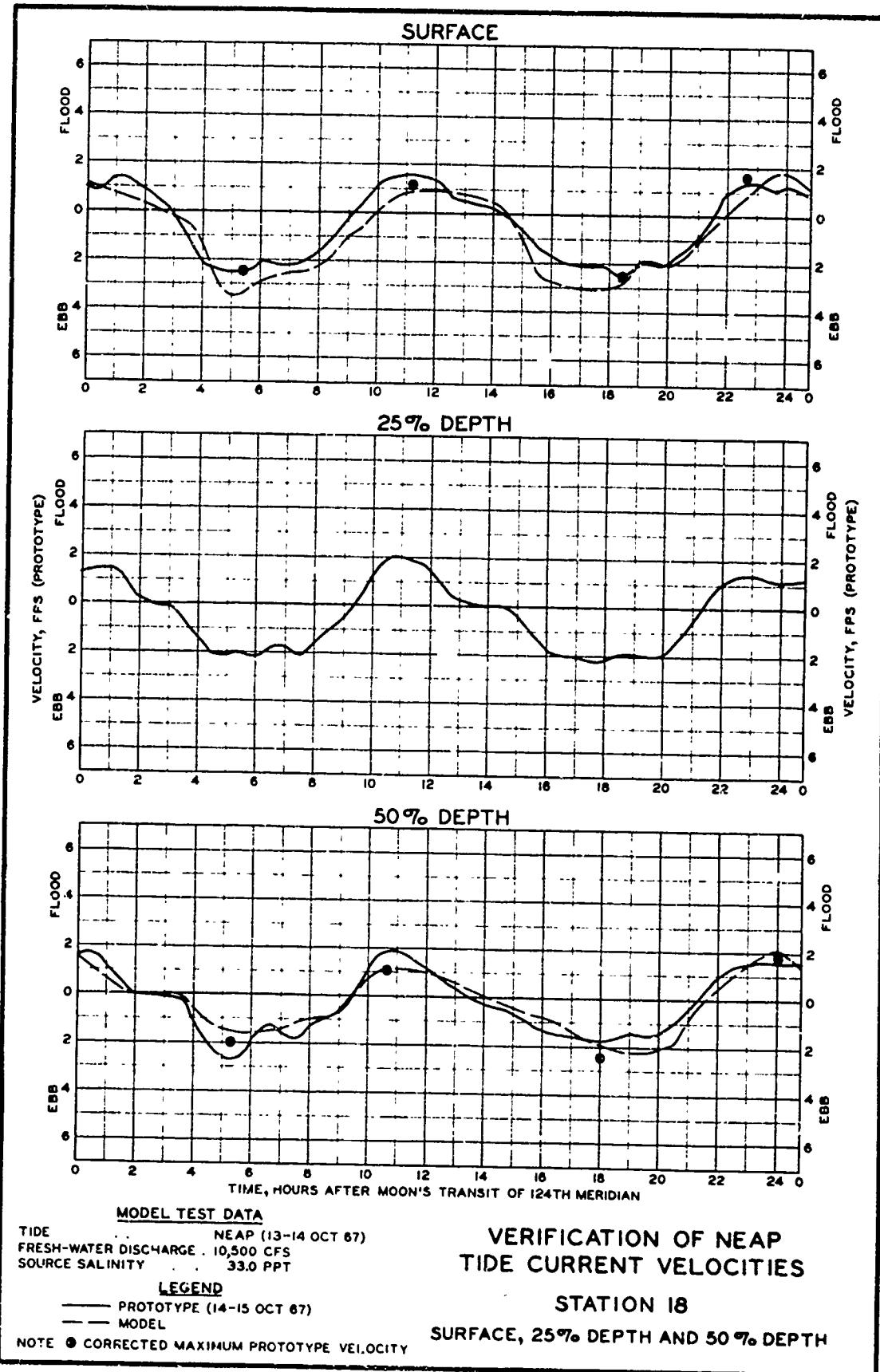


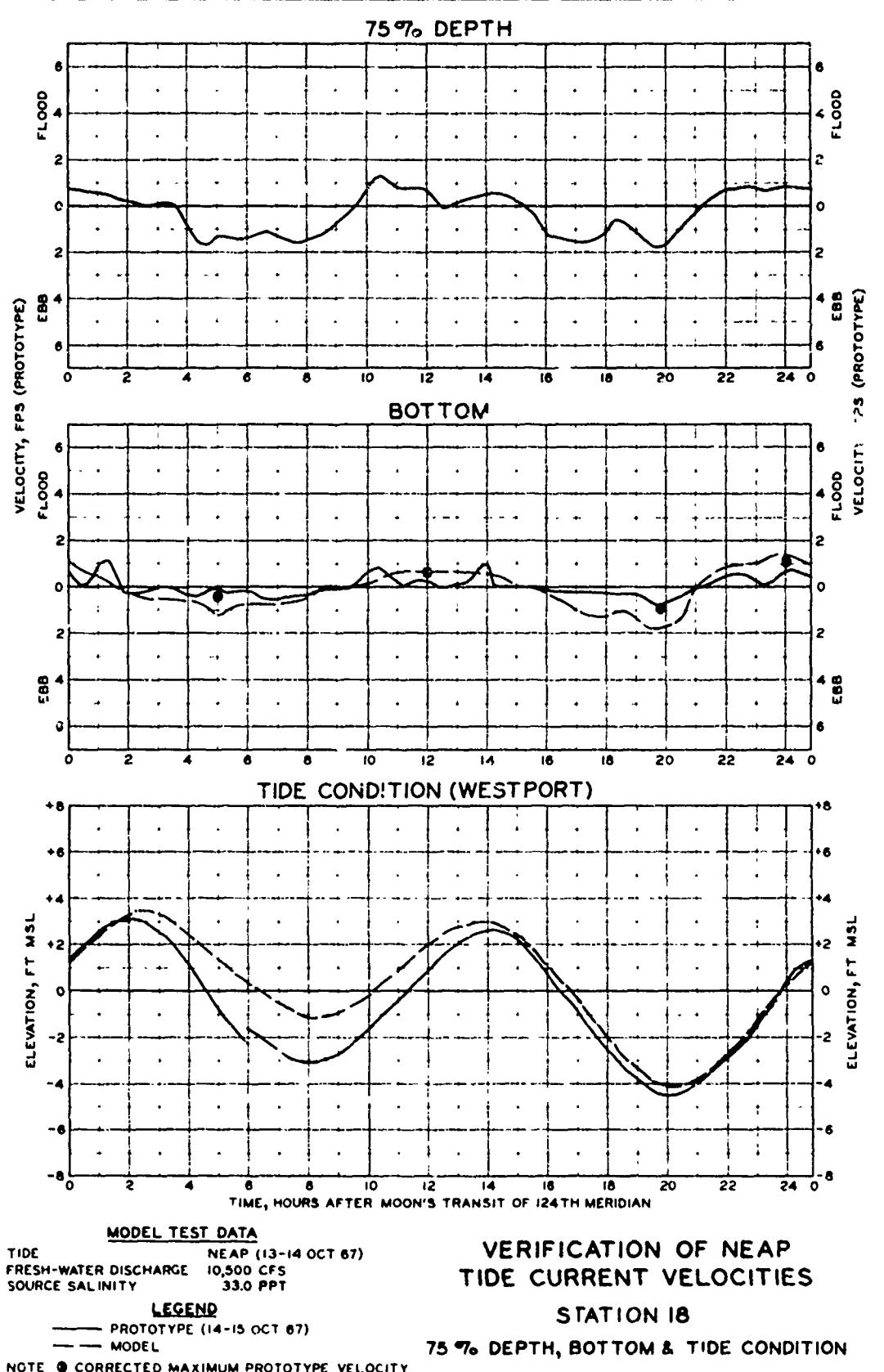
VERIFICATION OF NEAP TIDE CURRENT VELOCITIES

STATION 17

75% DEPTH, BOTTOM & TIDE CONDITION

PLATE 71





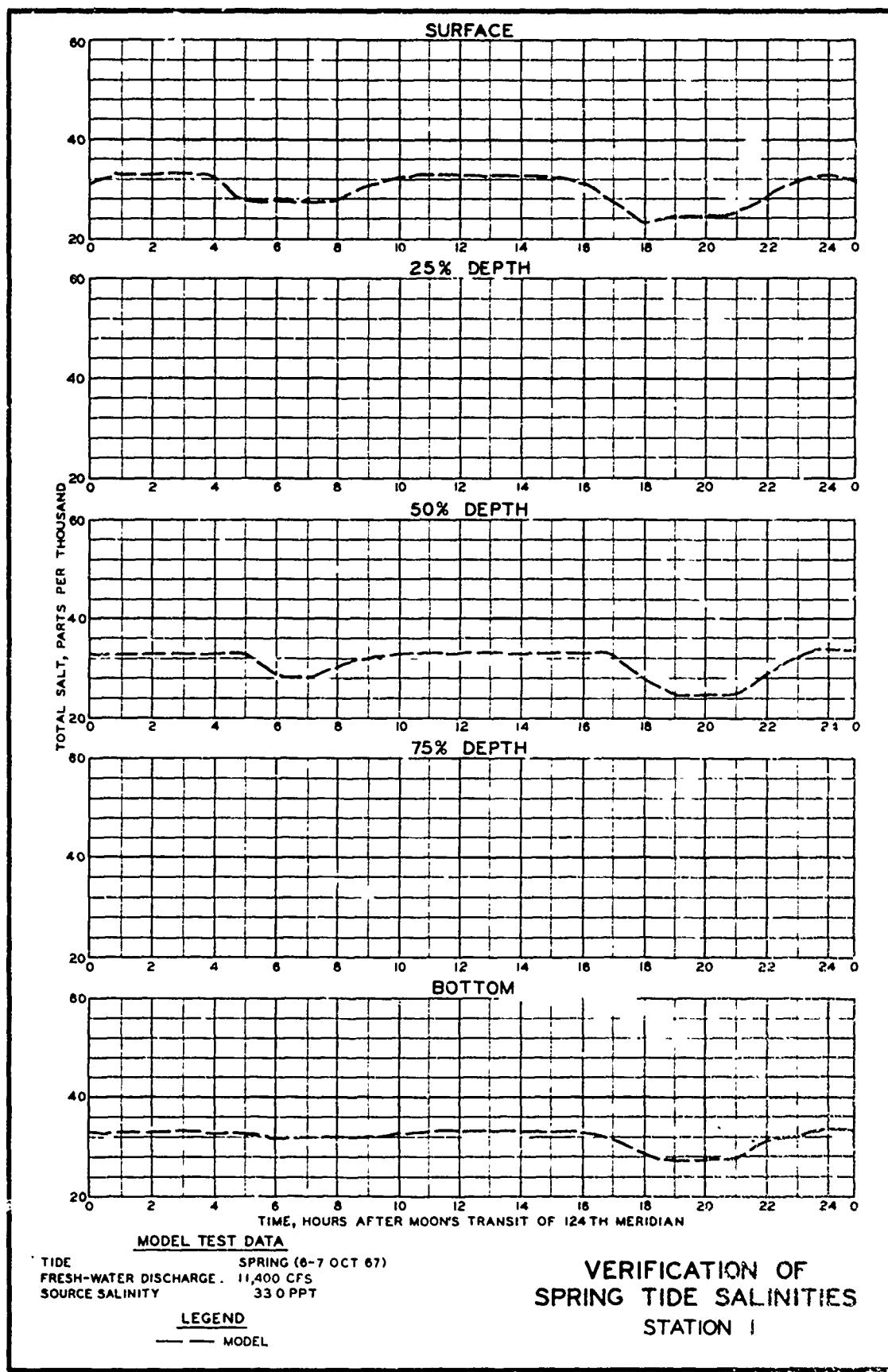
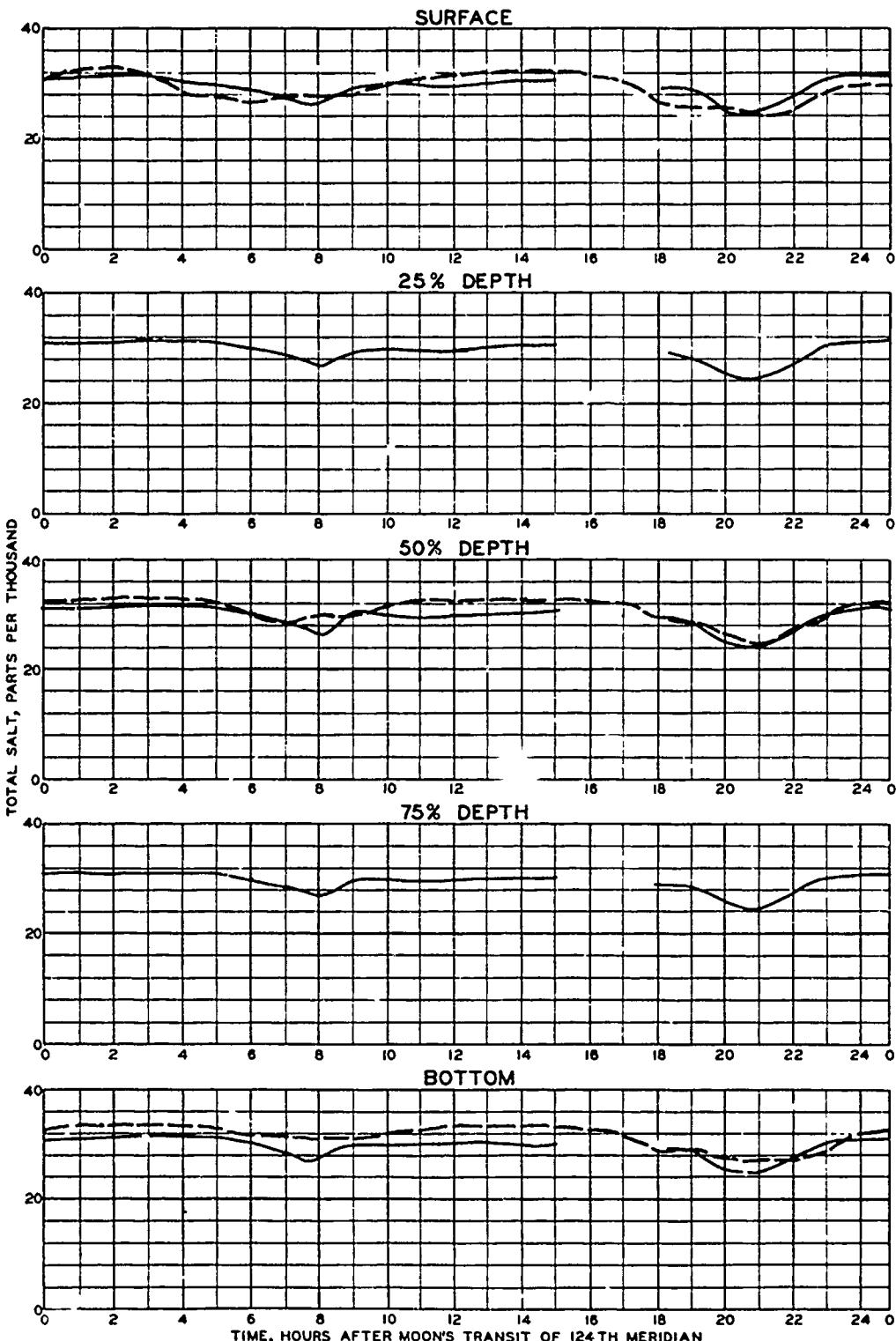


PLATE 74

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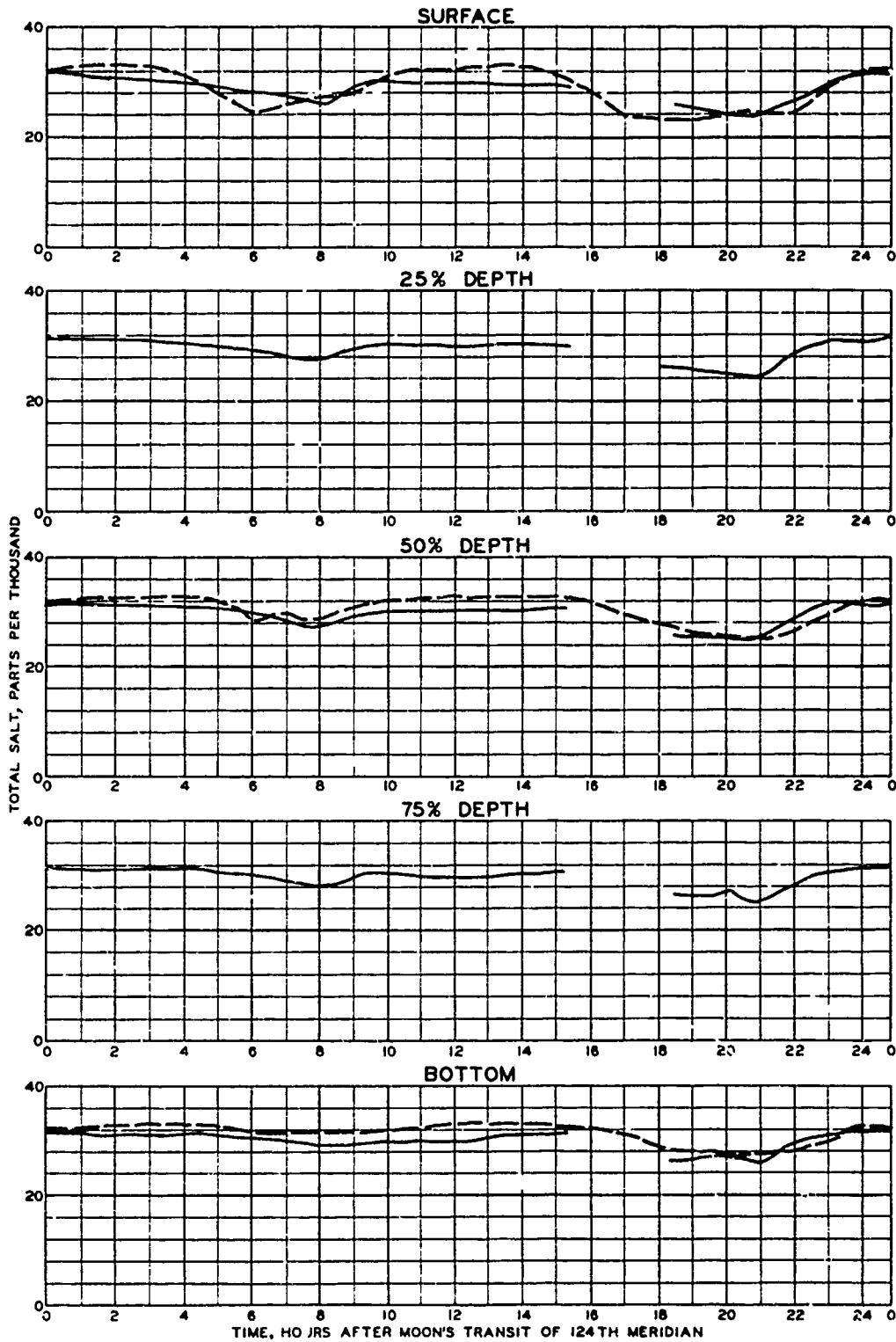
MODEL TEST DATA

TIDE SPRING (6-7 OCT 87)
 FRESH-WATER DISCHARGE . . 11,400 CFS
 SOURCE SALINITY 33.0 PPT

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 4

LEGEND
 — PROTOTYPE (7-8 OCT 87)
 - - MODEL

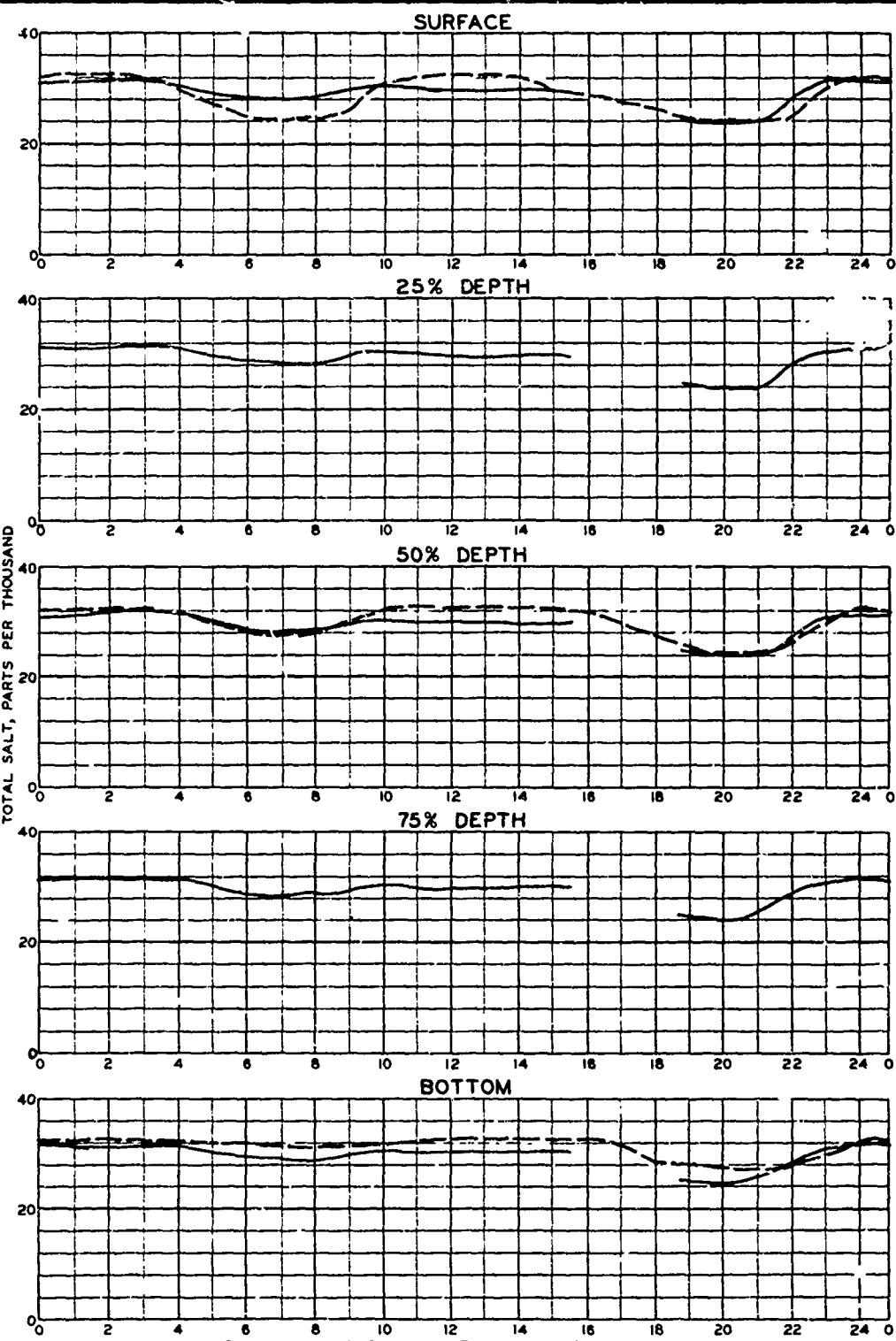


MODEL TEST DATA
 TIDE . SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE . 11,400 CFS
 SOURCE SALINITY . 330 PPT

LEGEND
 — PROTOTYPE (7-8 OCT 67)
 - - MODEL

VERIFICATION OF
SPRING TIDE SALINITIES

STATION 5



MODEL TEST DATA

TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

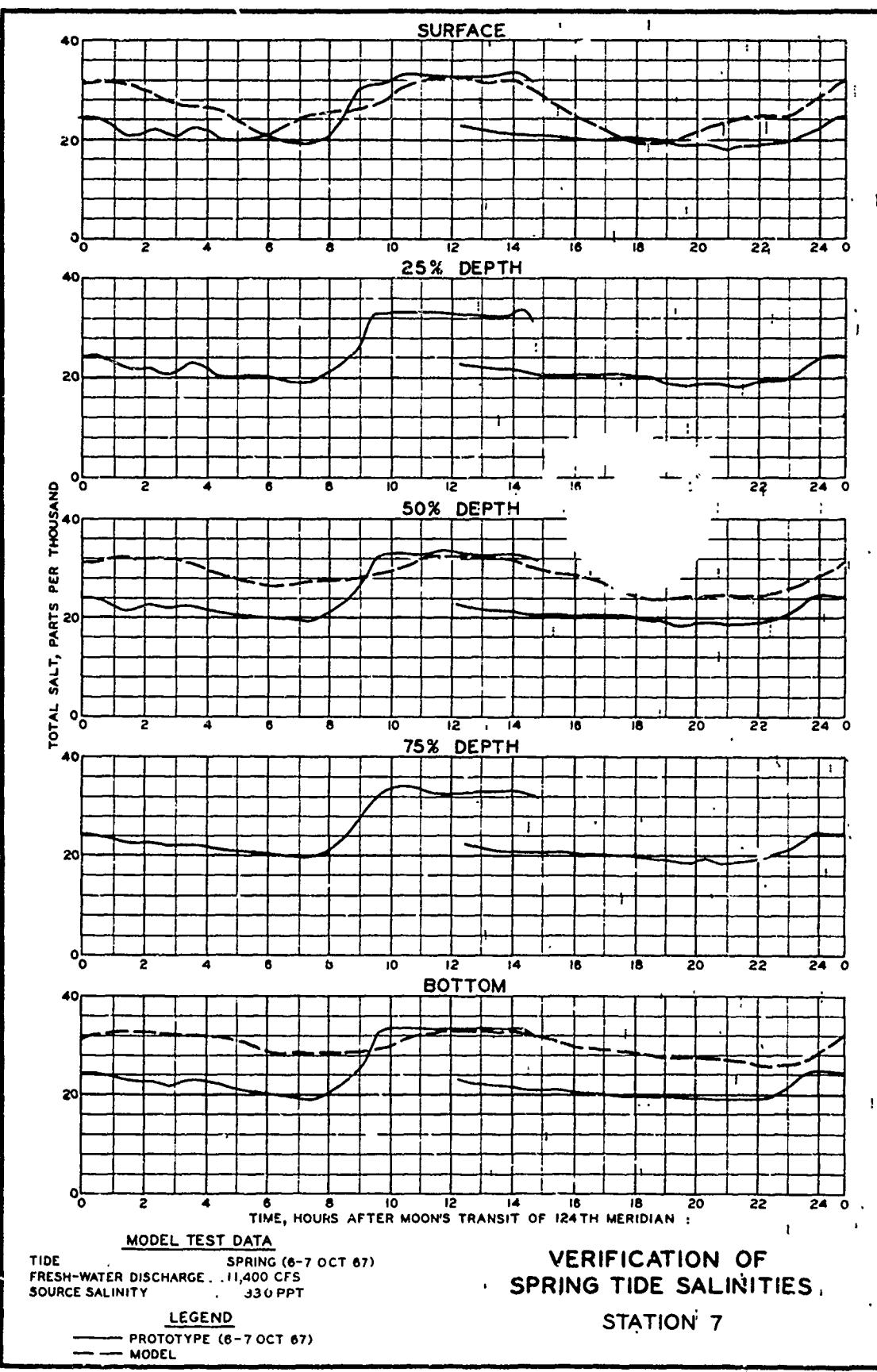
— PROTOTYPE (7-8 OCT 67)
 - - - MODEL

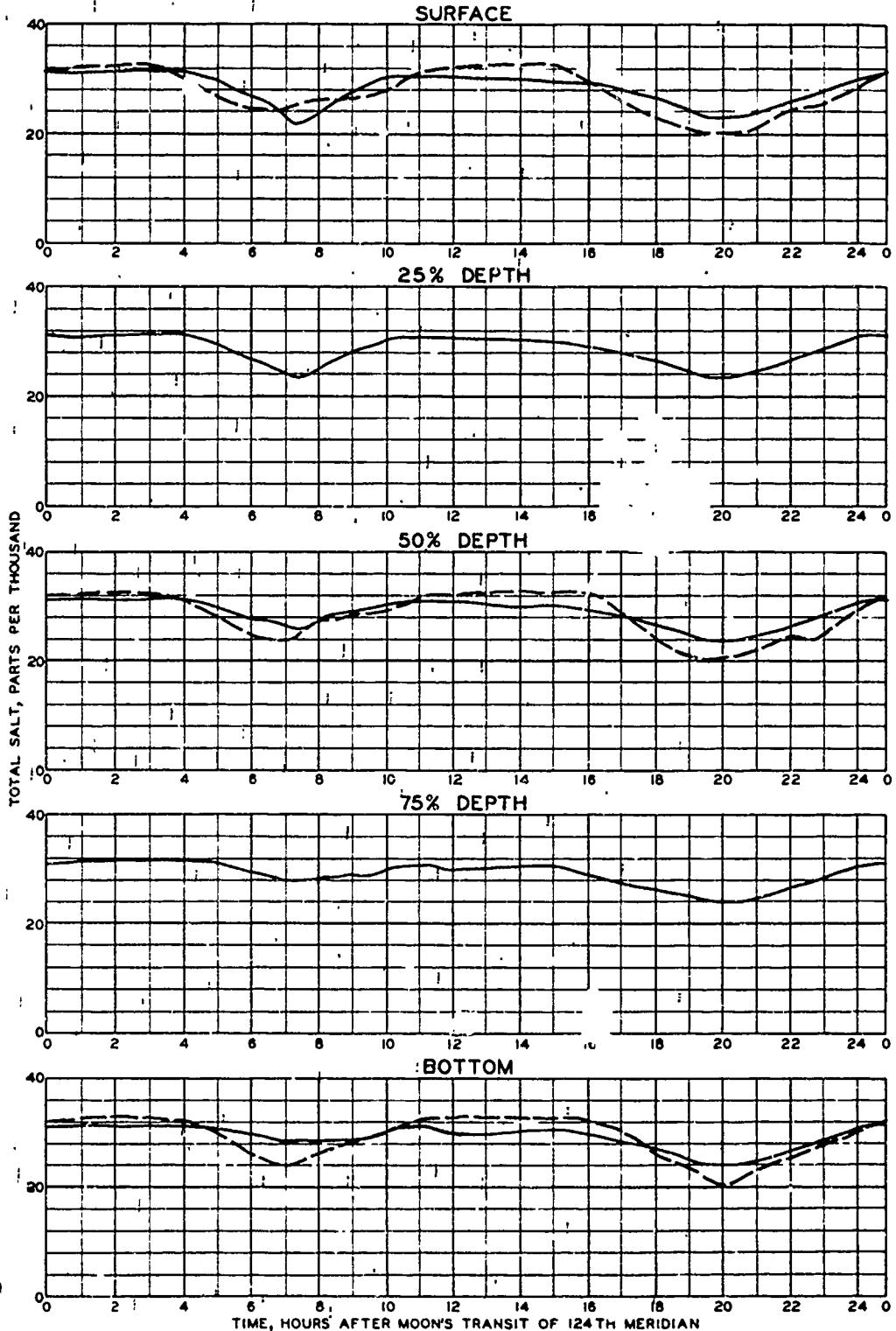
VERIFICATION OF
SPRING TIDE SALINITIES

STATION 6

1.11

PLATE 77





MODEL TEST DATA

TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— PROTOTYPE (6-7 OCT 67)
 - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 8

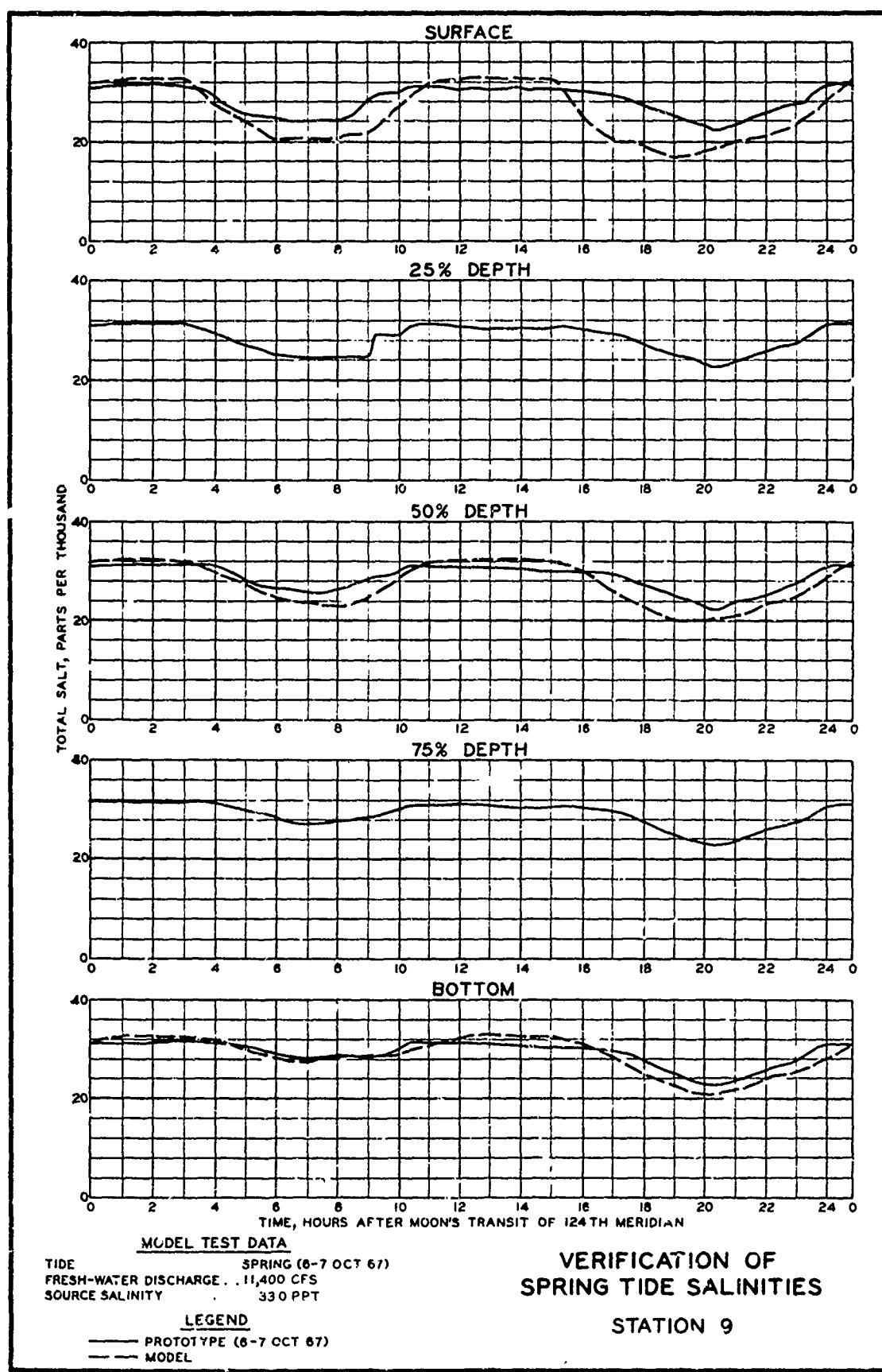
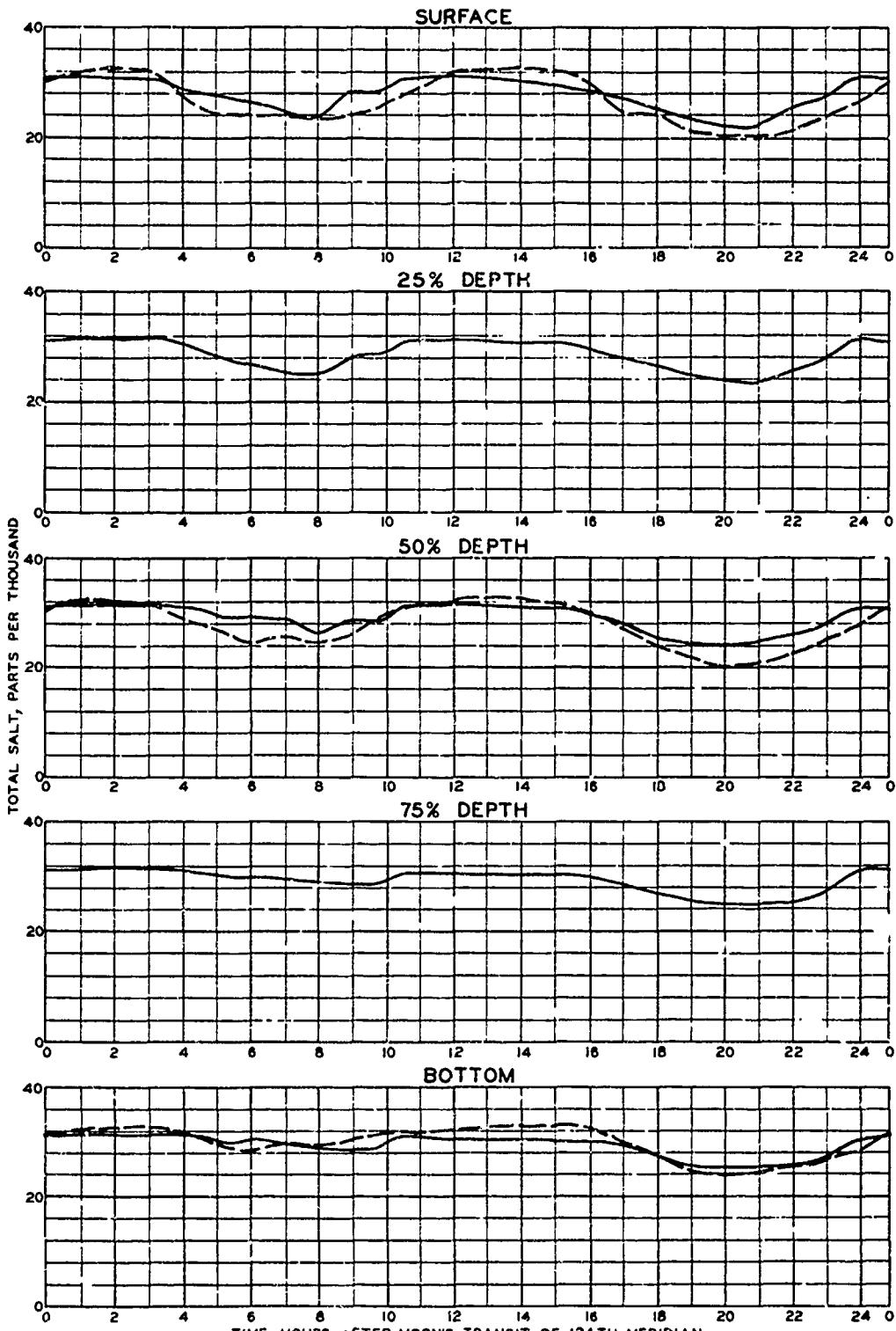


PLATE 80

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MODEL TEST DATA

TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE . . . 11,400 CFS
 SOURCE SALINITY . . . 330 PPT

LEGEND

— — PROTOTYPE (6-7 OCT 67)
 - - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 10

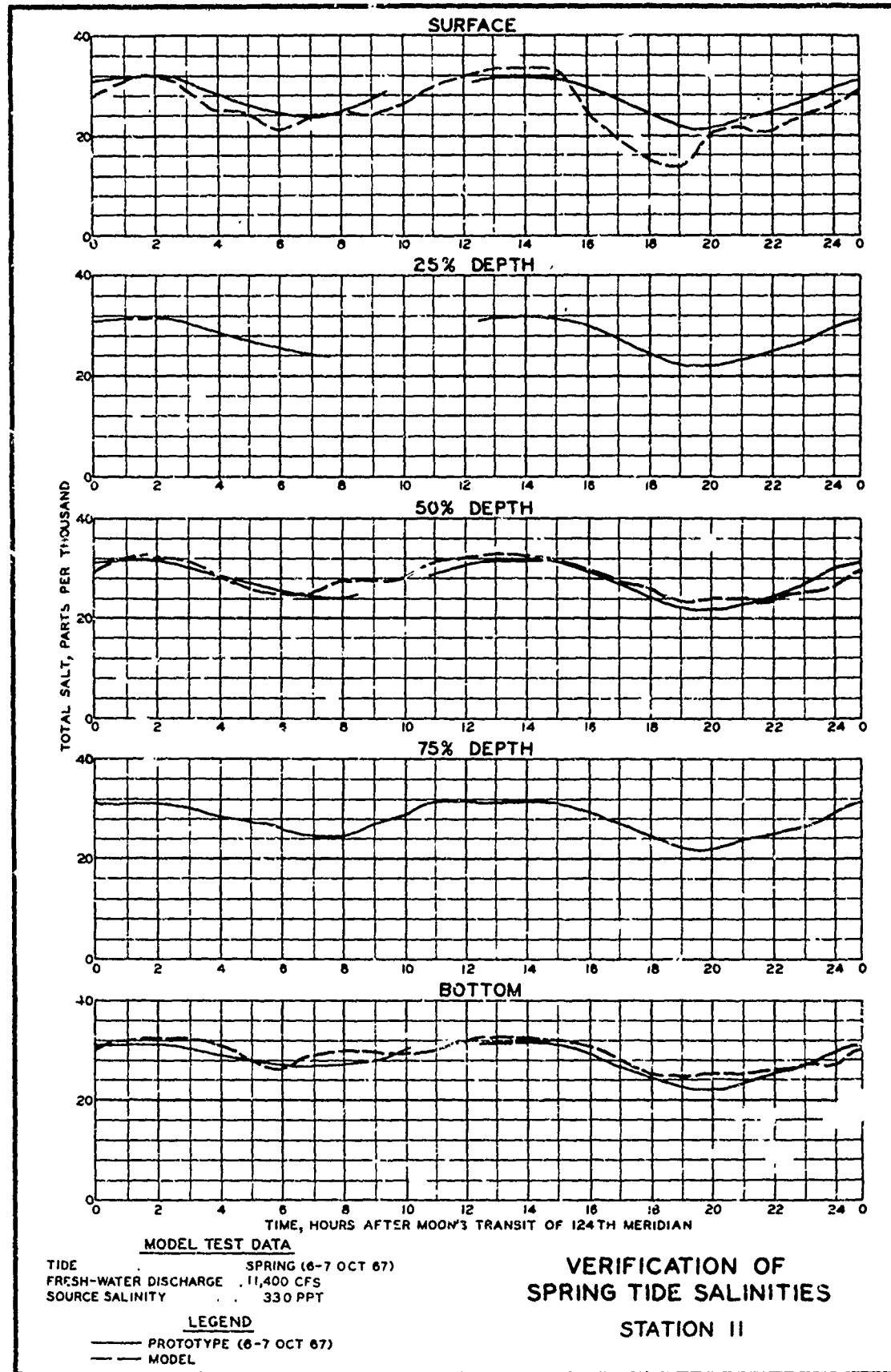
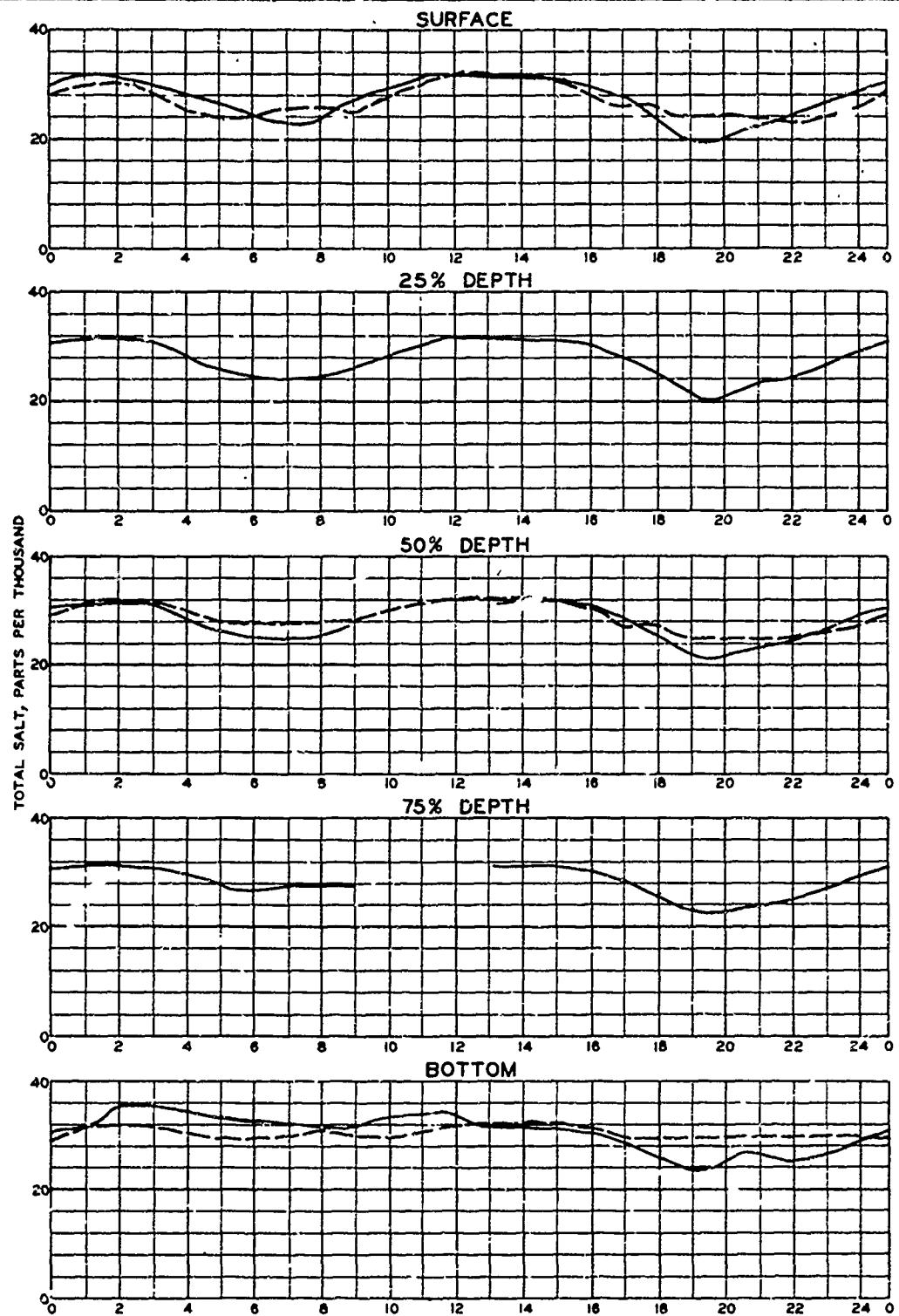


PLATE 82



TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE . . . 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — PROTOTYPE (6-7 OCT 67)
 - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 12

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PLATE 83

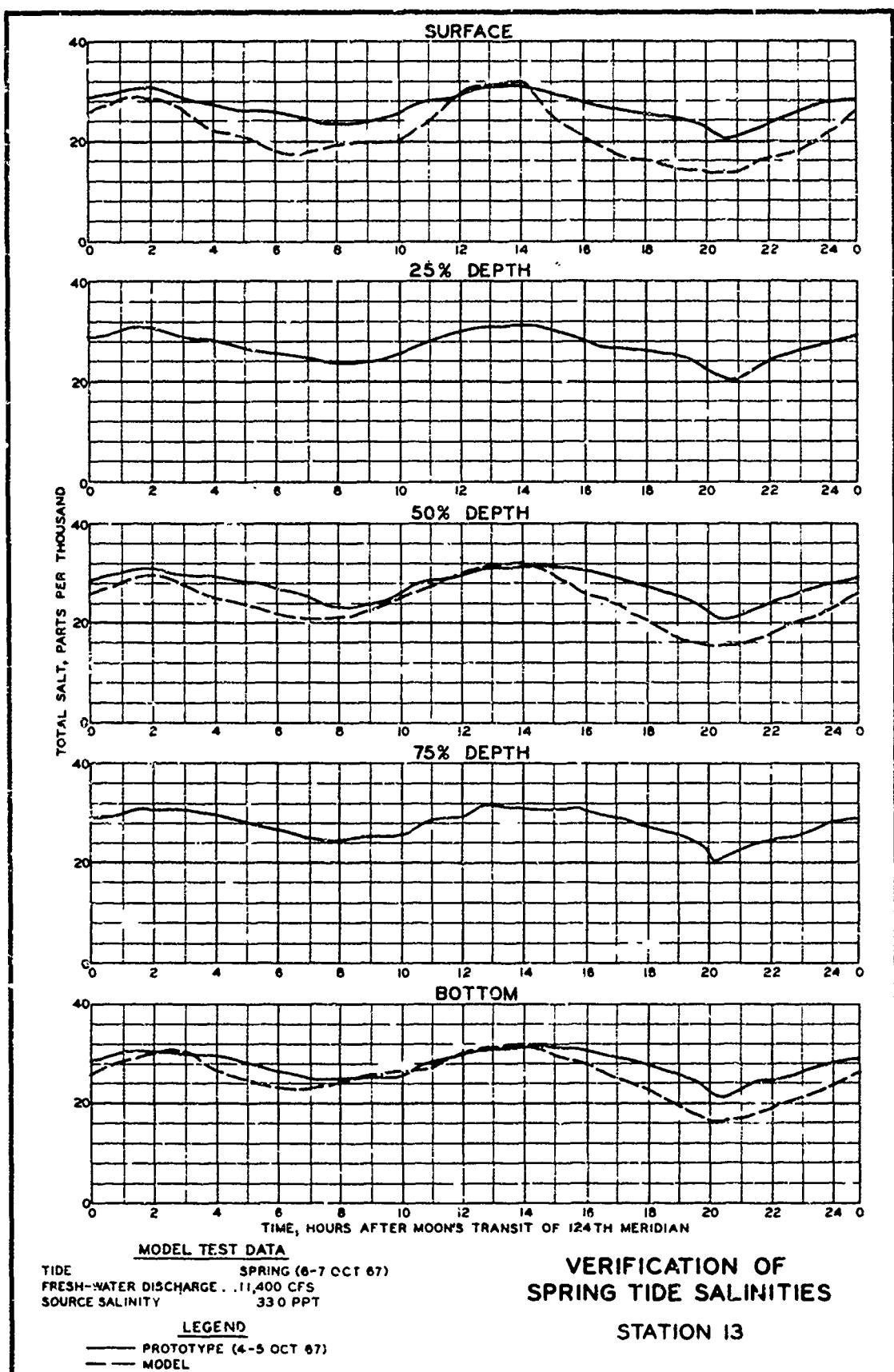
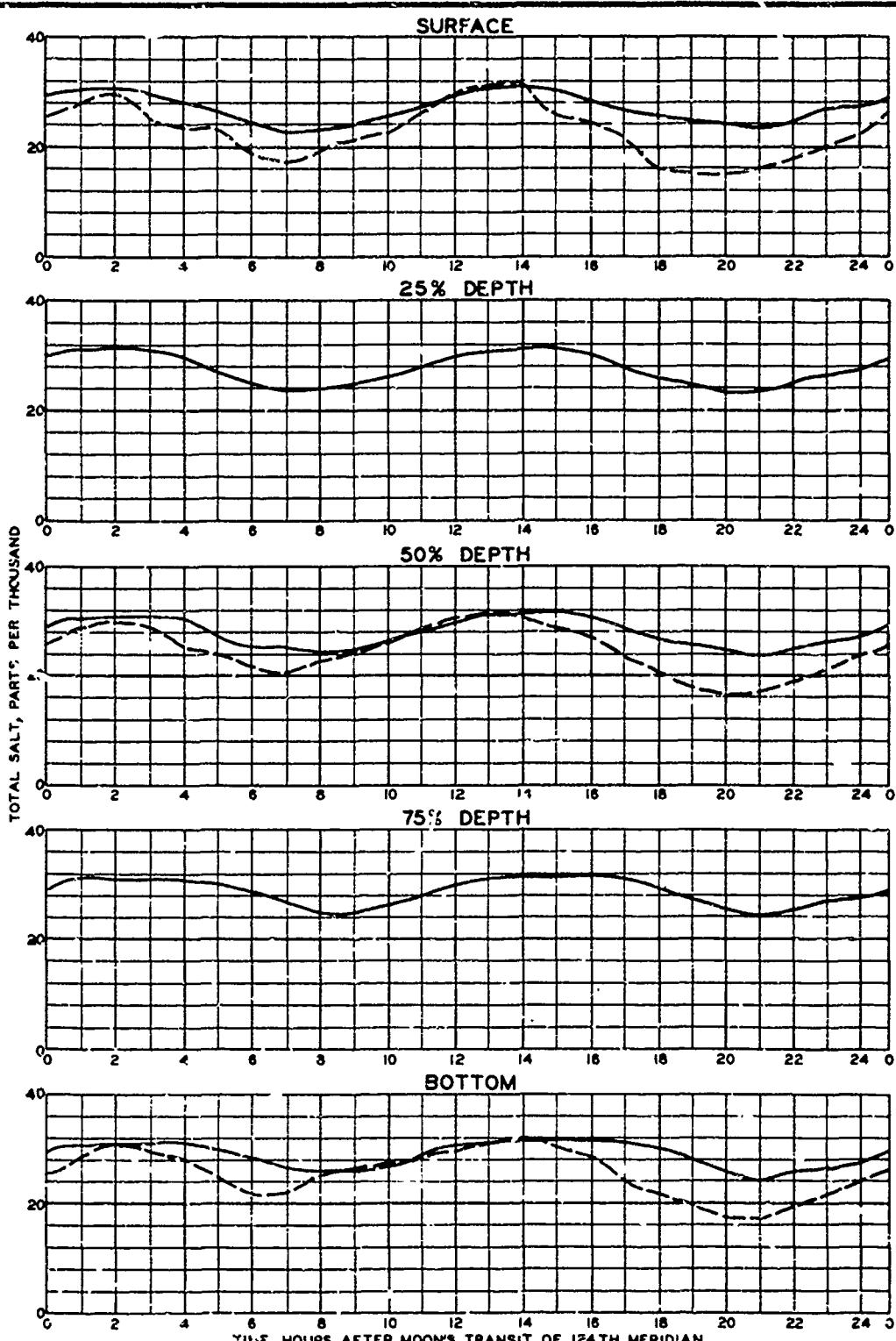


PLATE 84

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MODEL TEST DATA

TIDE SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE . . . 11,400 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND

— PROTOTYPE (4-5 OCT 67)
 - - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 14

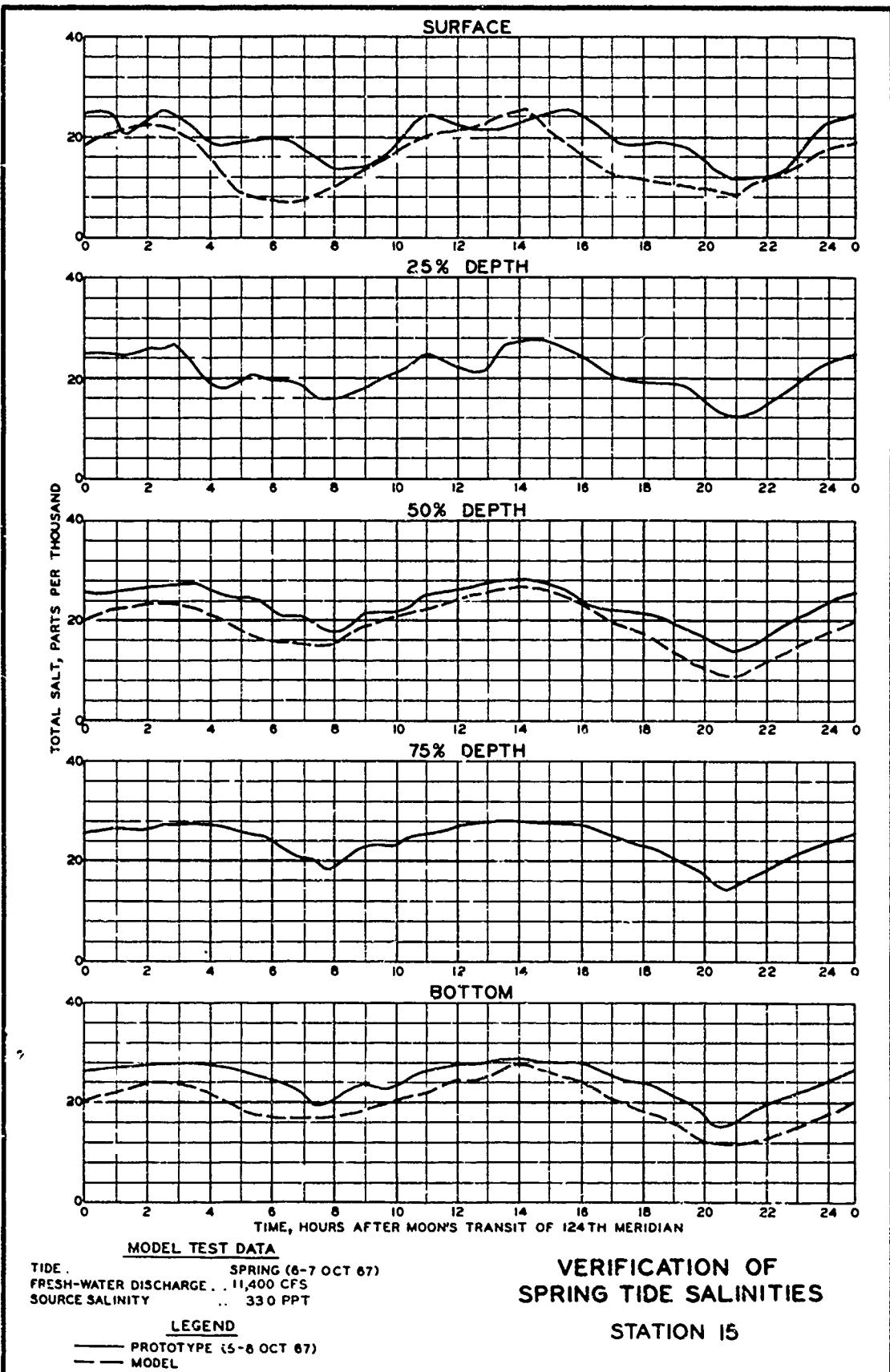
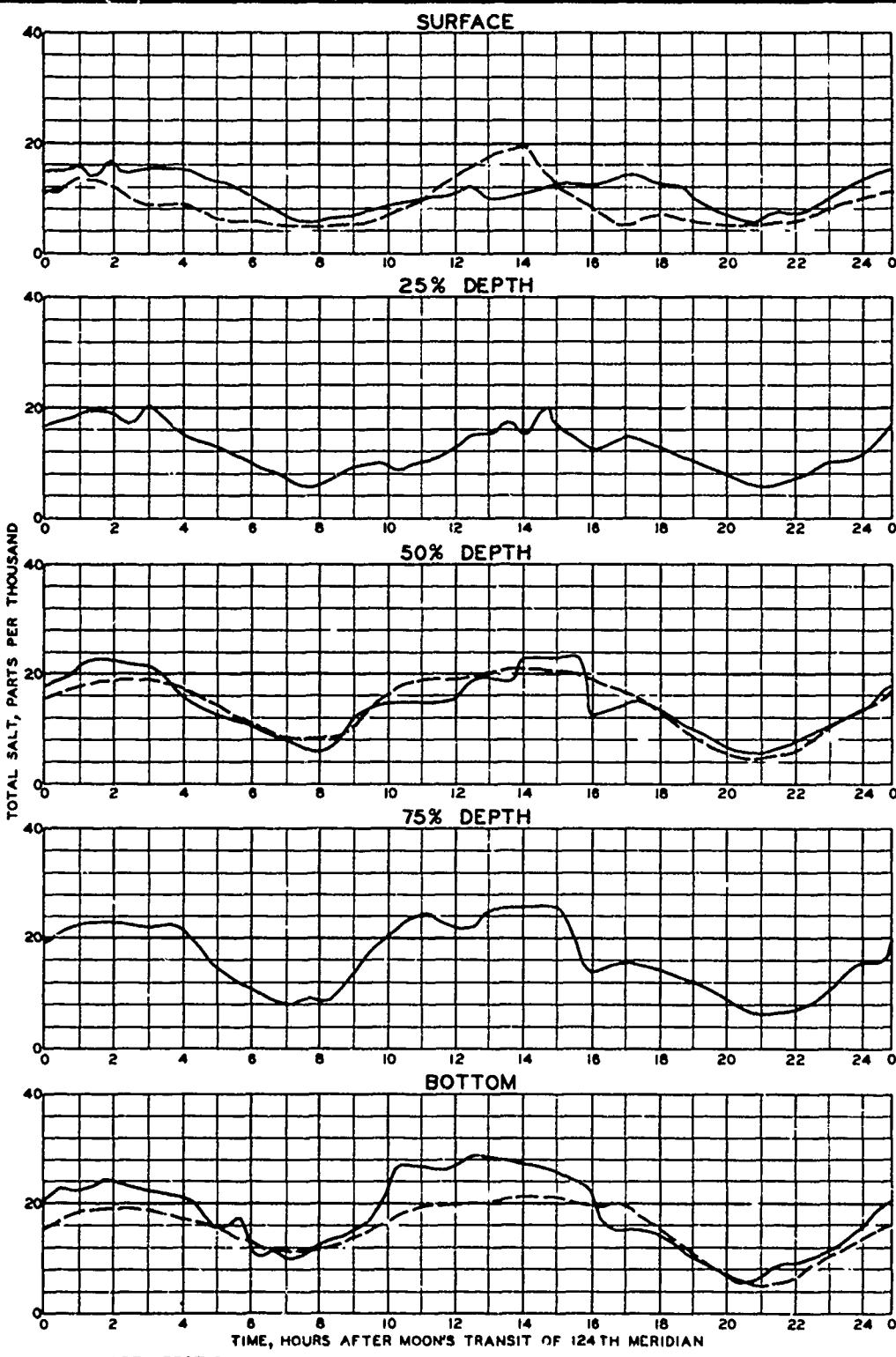


PLATE 86

100



MODEL TEST DATA

TIDE . . . SPRING (6-7 OCT 67)
 FRESH-WATER DISCHARGE . . . 11,400 CFS
 SOURCE SALINITY . . . 33.0 PPT

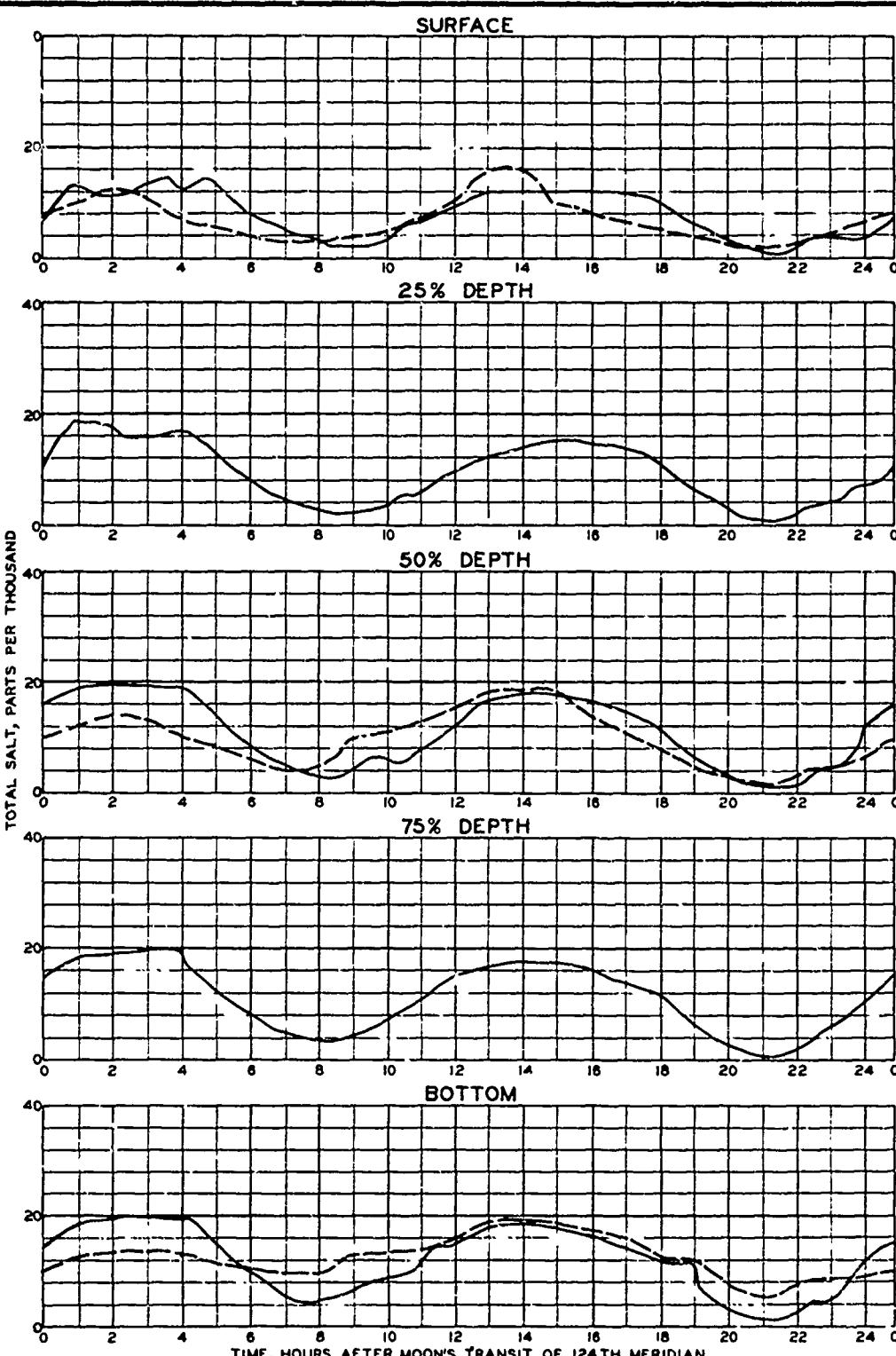
LEGEND

— PROTOTYPE (6-9 OCT 67)
 - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 16

PLATE 87

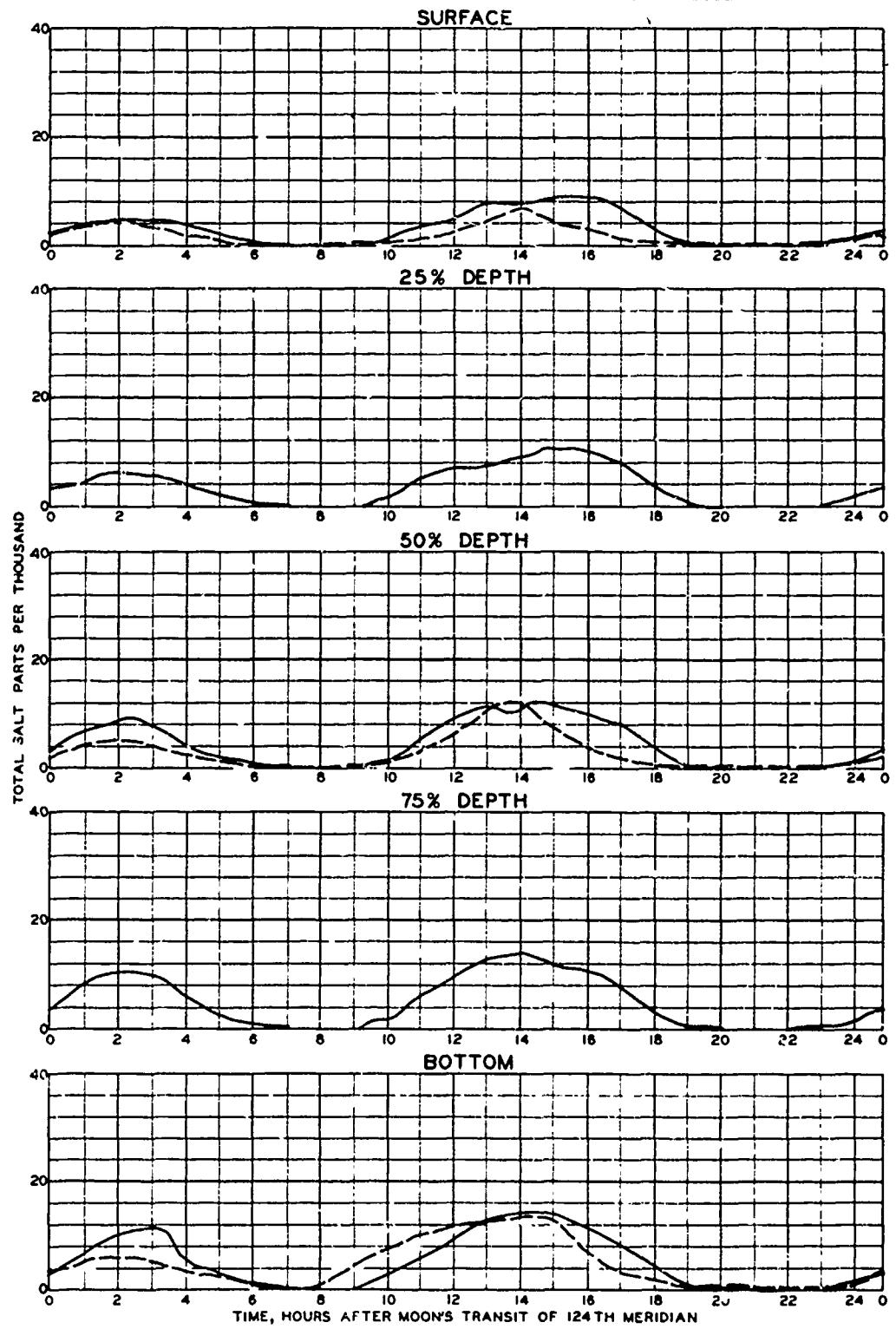


MODEL TEST DATA
 TIDE .. SPRINC (6-7 OCT 67)
 FRESH-WATER DISCHARGE .. 11400 CFS
 SOURCE SALINITY .. 33.0 PPT

LEGEND
 — PROTOTYPE (4-5 OCT 67)
 - - MODEL

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 17



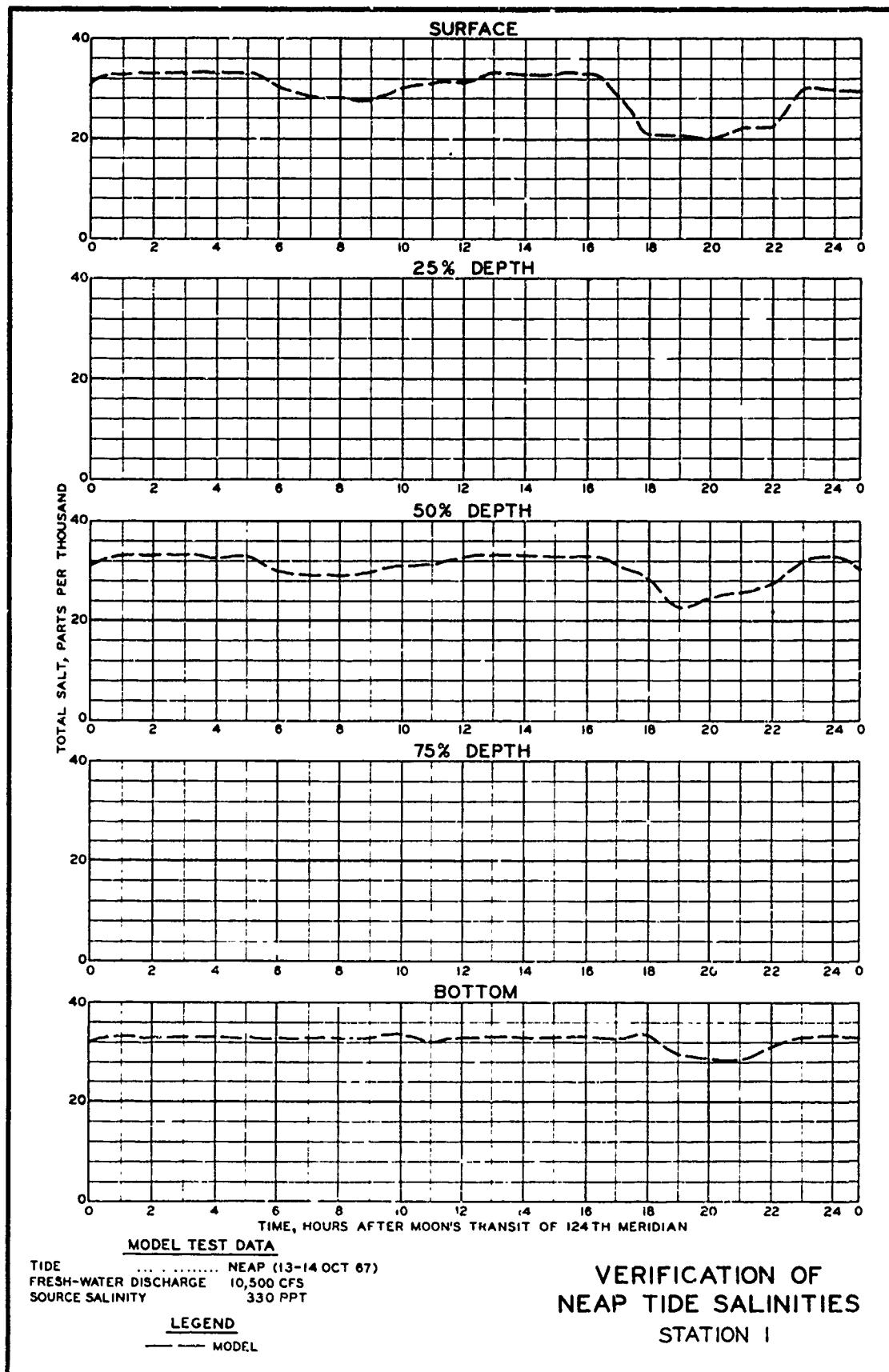
MODEL TEST DATA

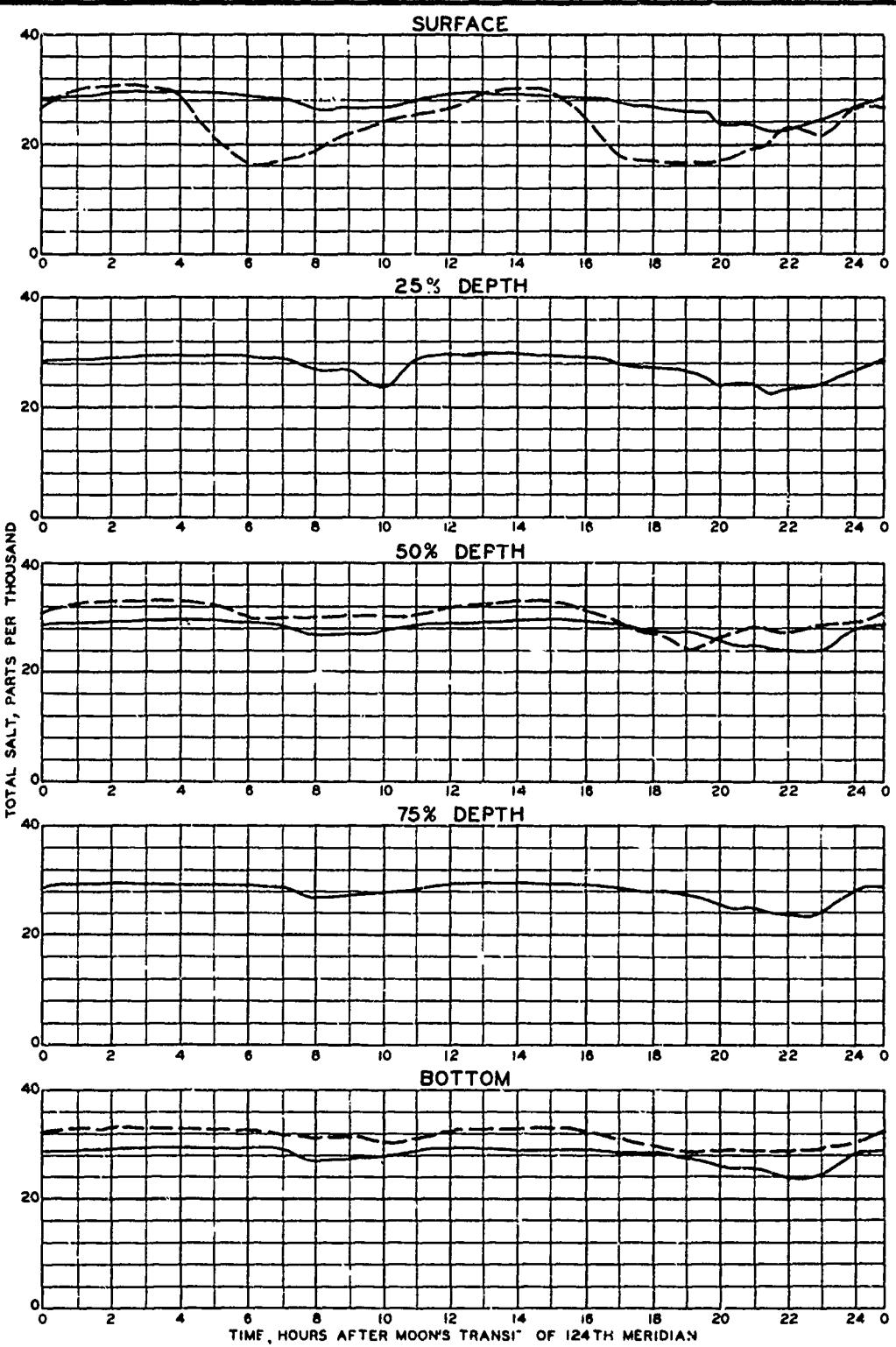
TIDE SPRING (6-7 OCT 67)
FRESH-WATER DISCHARGE . 11,400 CFS
SOURCE SALINITY 330 PPT

**VERIFICATION OF
SPRING TIDE SALINITIES**

STATION 18

LEGEND
— PROTOTYPE (5-6 OCT 67)
— MODEL





MODEL TEST DATA

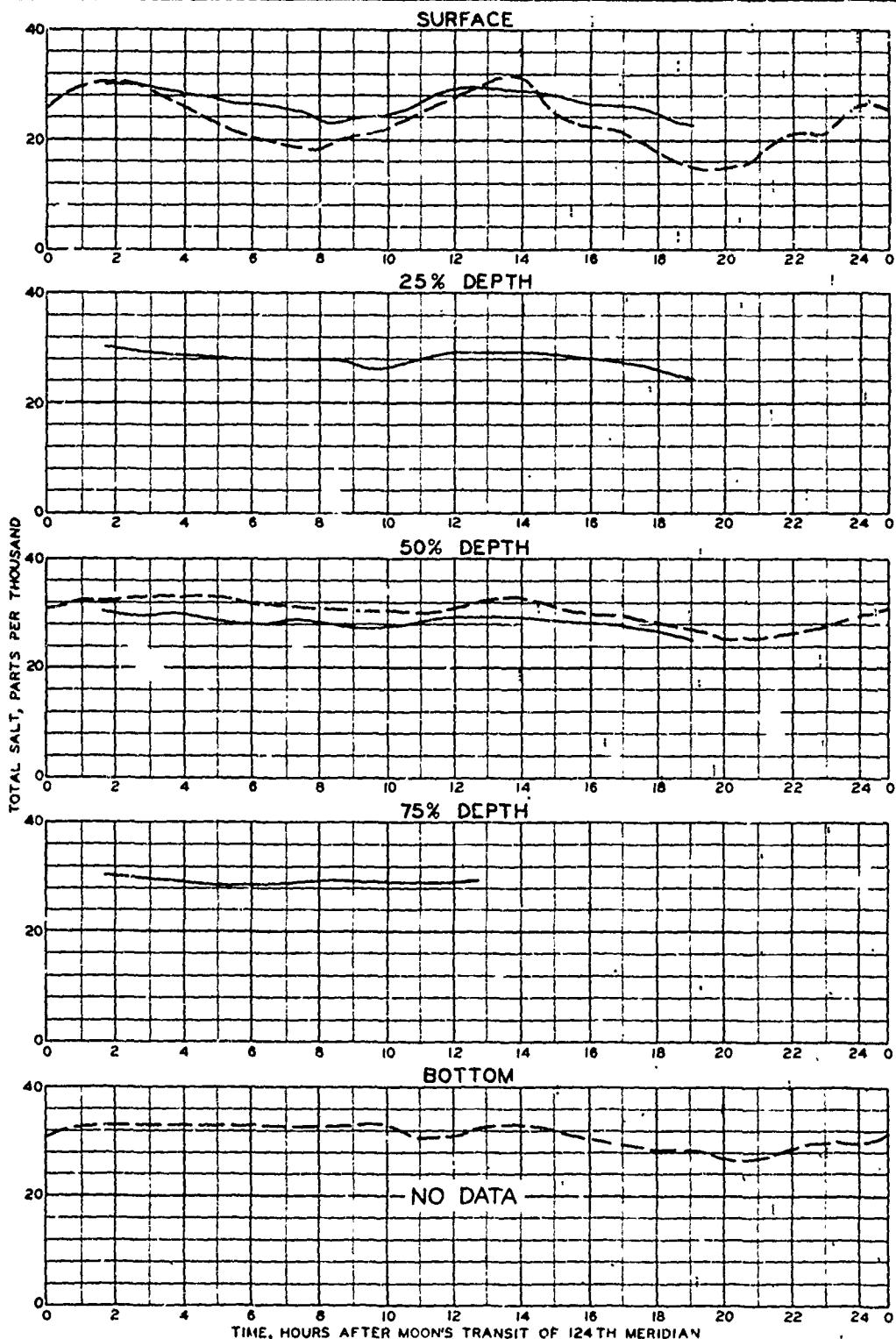
TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE .. 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND

— PROTOTYPE (12-13 OCT 67)
 - - MODEL

**VERIFICATION OF
NEAP TIDE SALINITIES**

STATION 4



MODEL TEST DATA

TIDE

FRESH-WATER DISCHARGE

SOURCE SALINITY

NEAP (13-14 OCT 87)

10,500 CFS

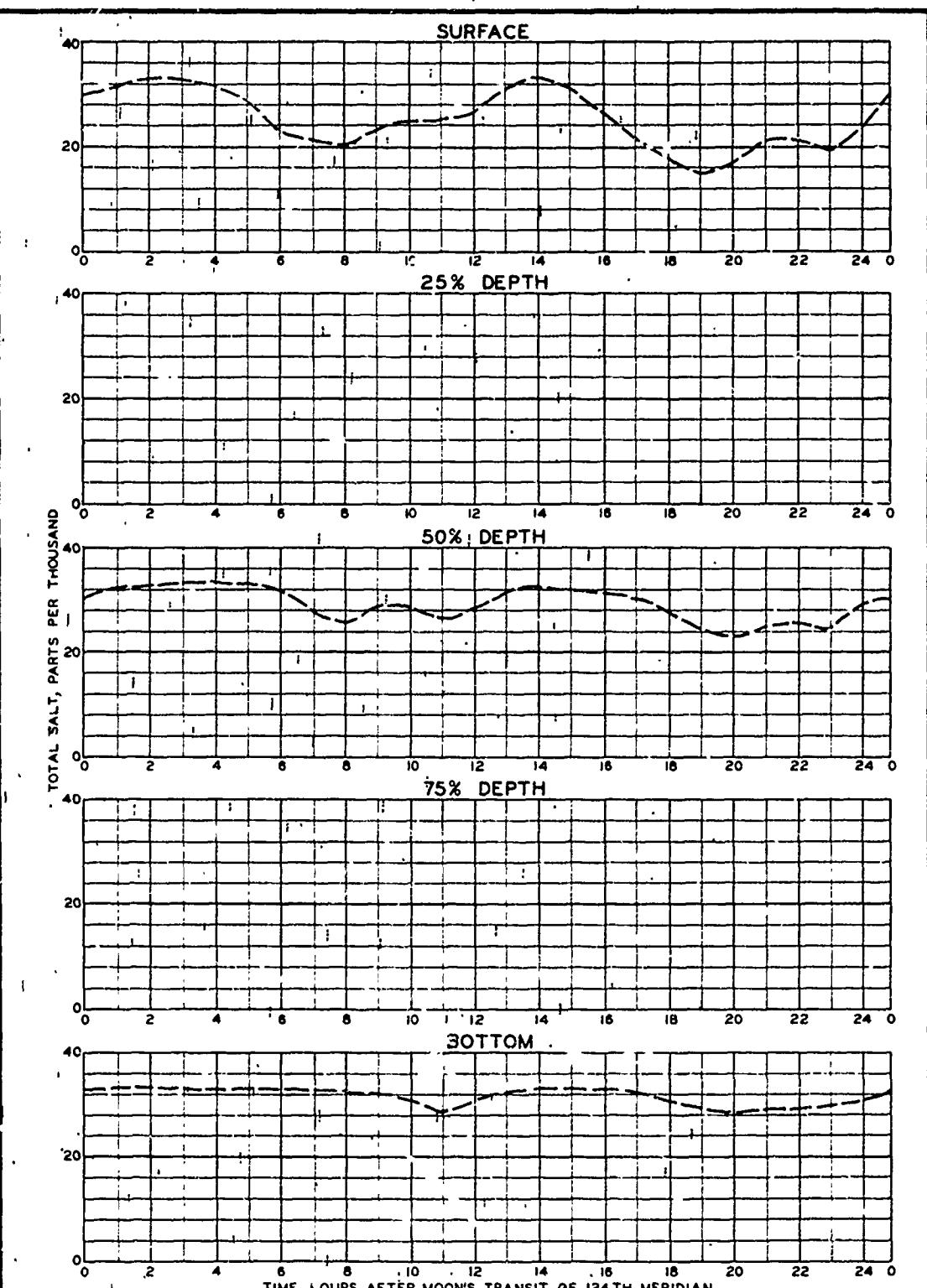
33.0 PPT

LEGEND

— PROTOTYPE (12-13 OCT 87)
— MODEL

**VERIFICATION OF
NEAP TIDE SALINITIES**

STATION 5

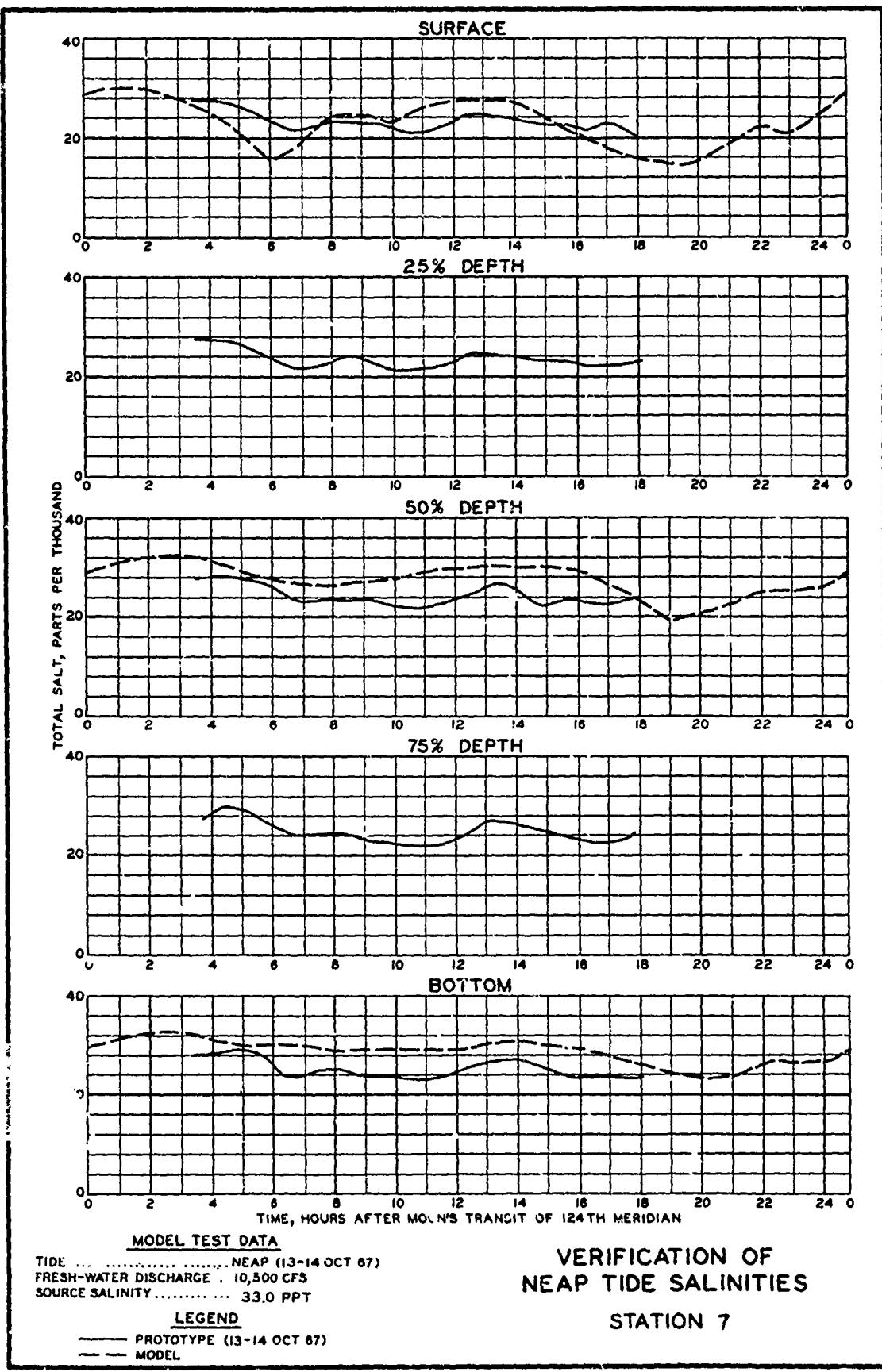


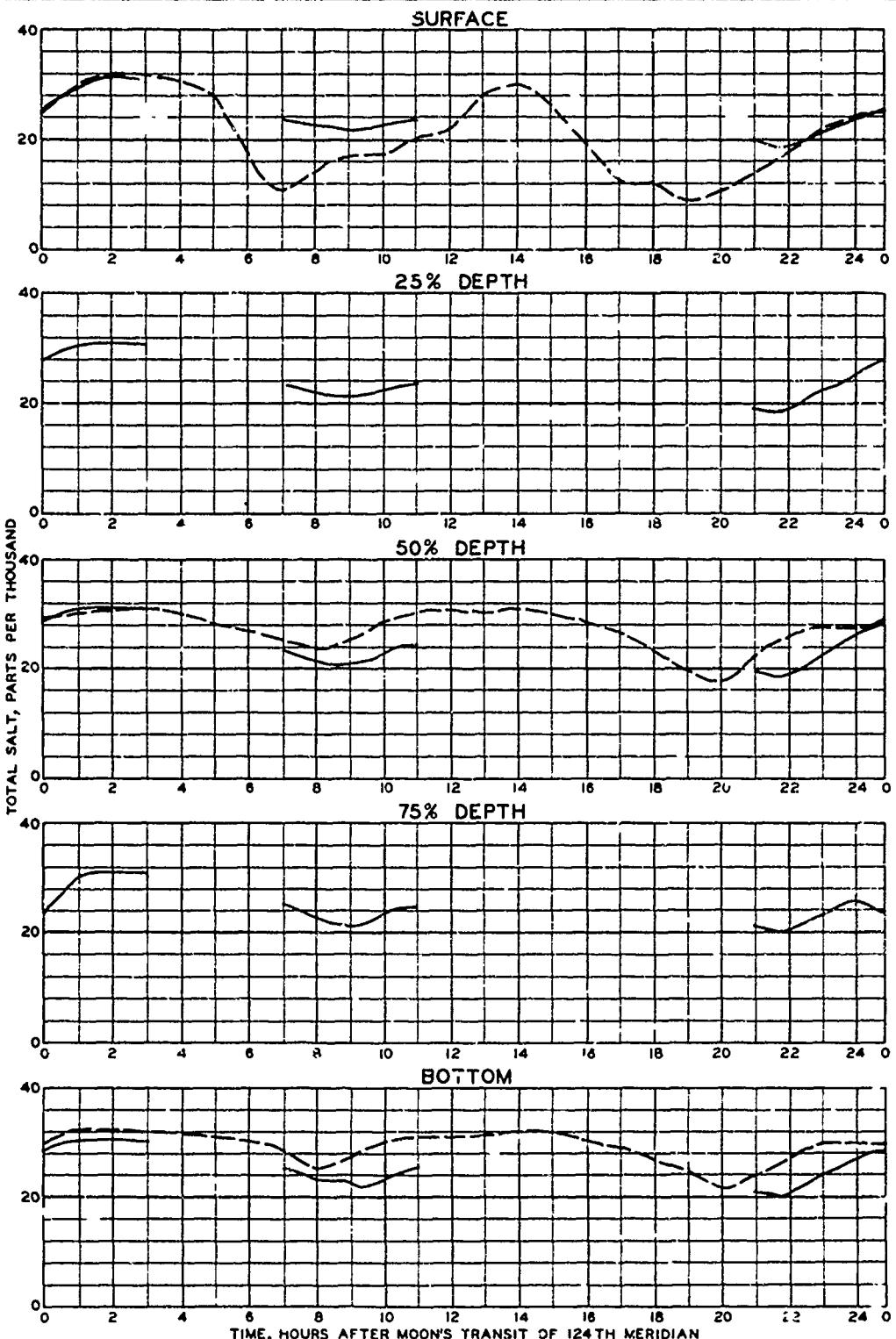
MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE : 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND
 — MODEL

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 VERIFICATION OF
 NEAP TIDE SALINITIES
 STATION 6





MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE . 10,500 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — PROTOTYPE (13-14 OCT 67)
 - - - MODEL

**VERIFICATION OF
NEAP TIDE SALINITIES**

STATION 8

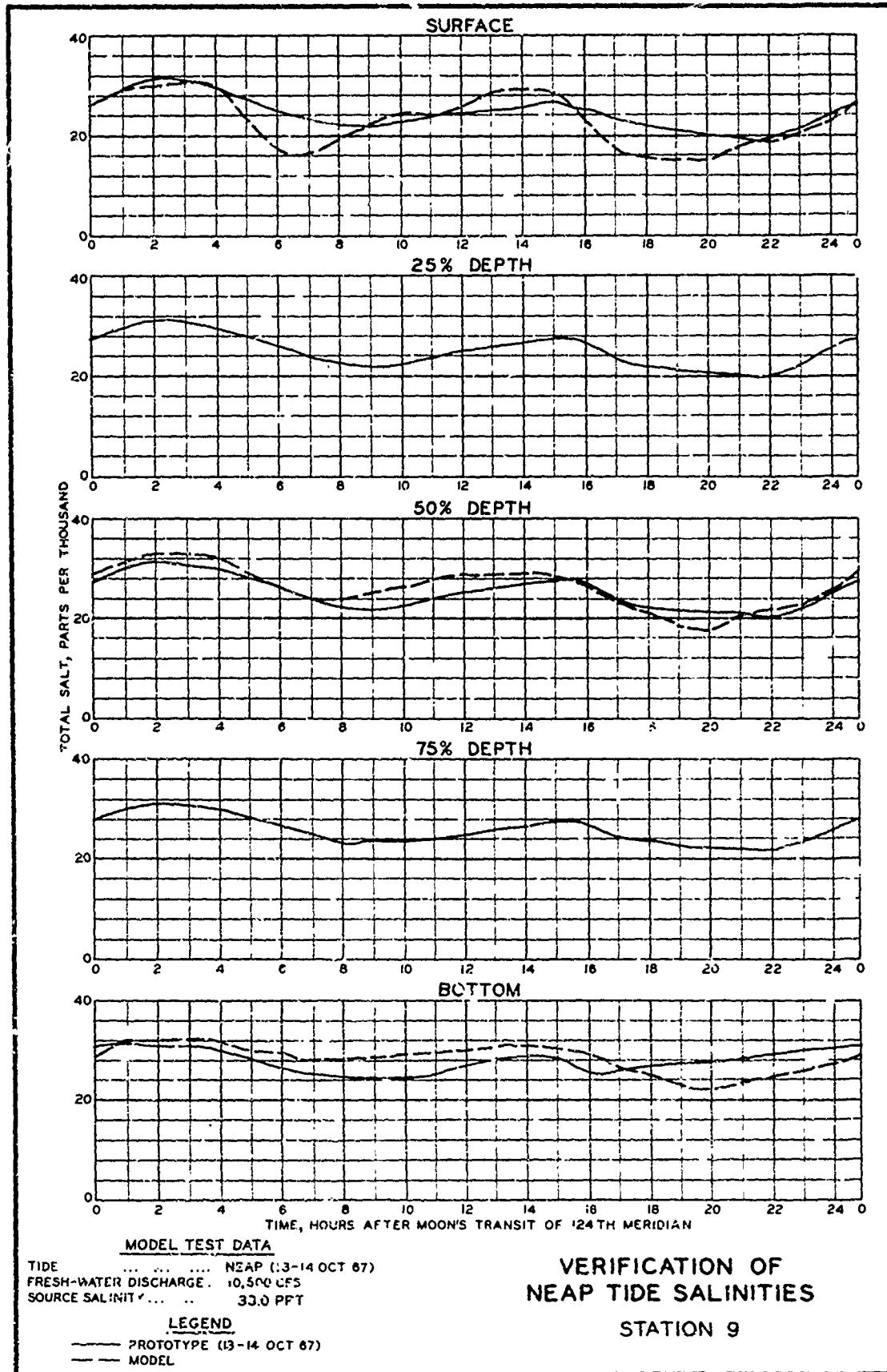
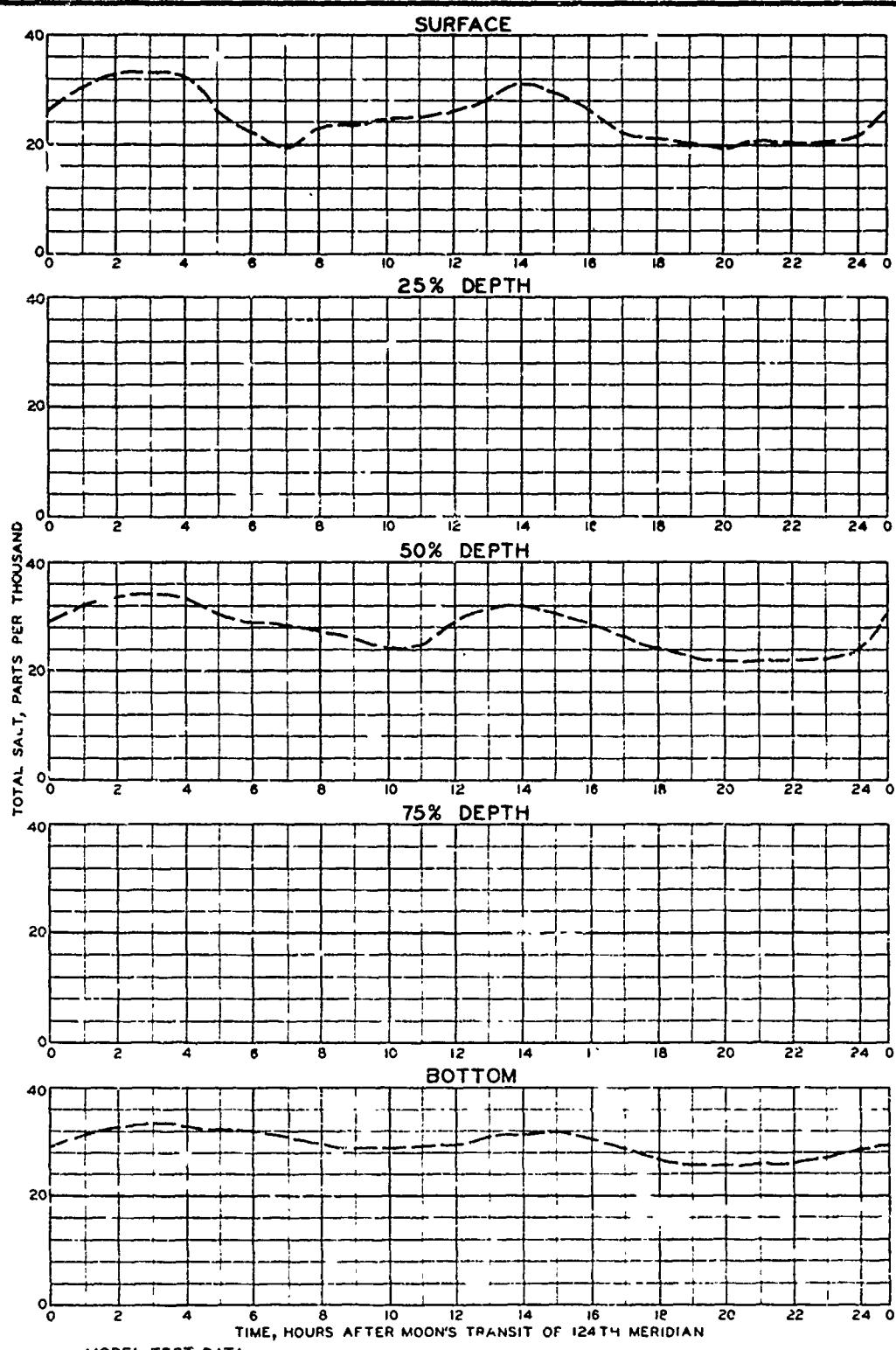


PLATE 96

100

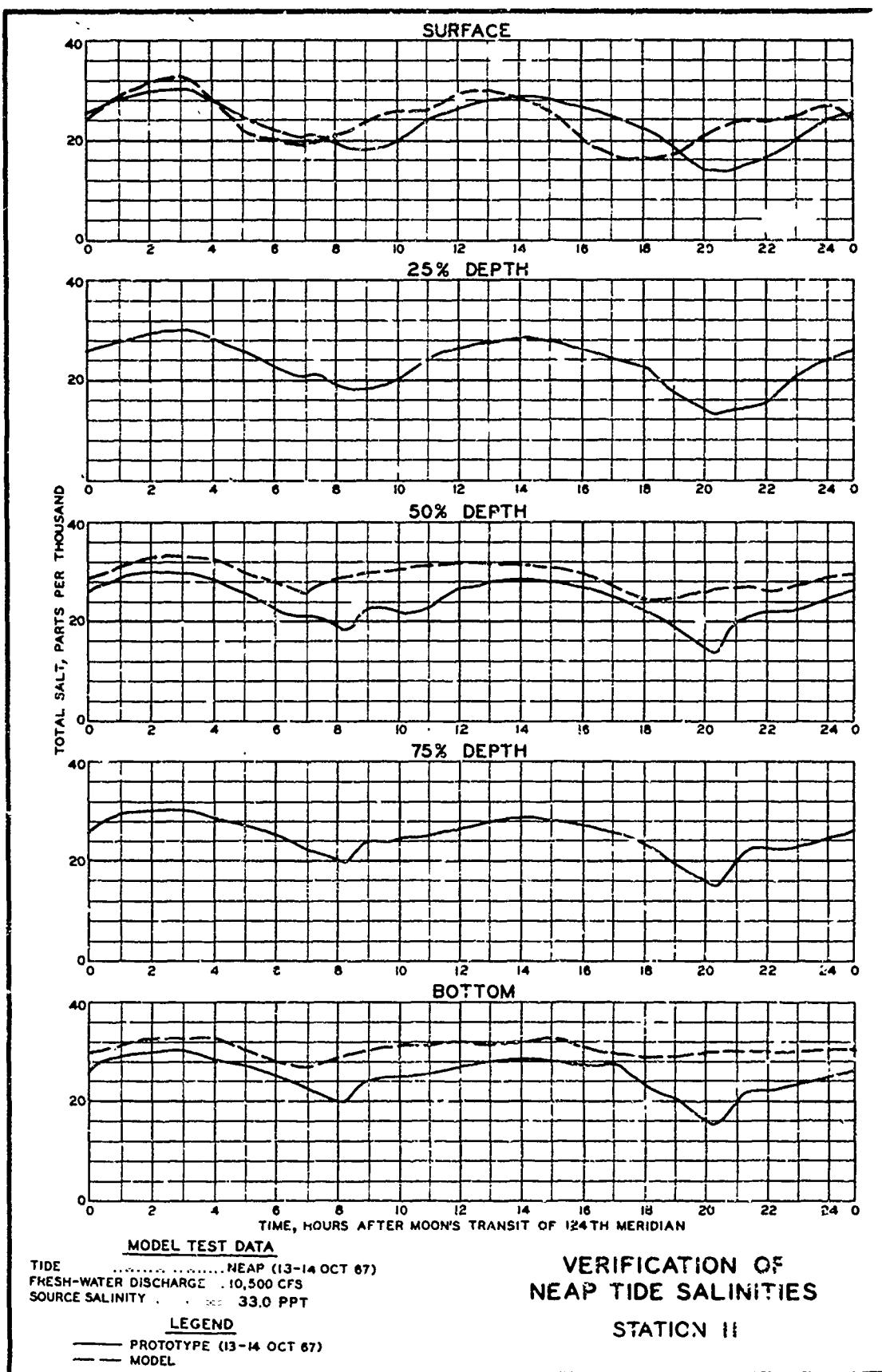


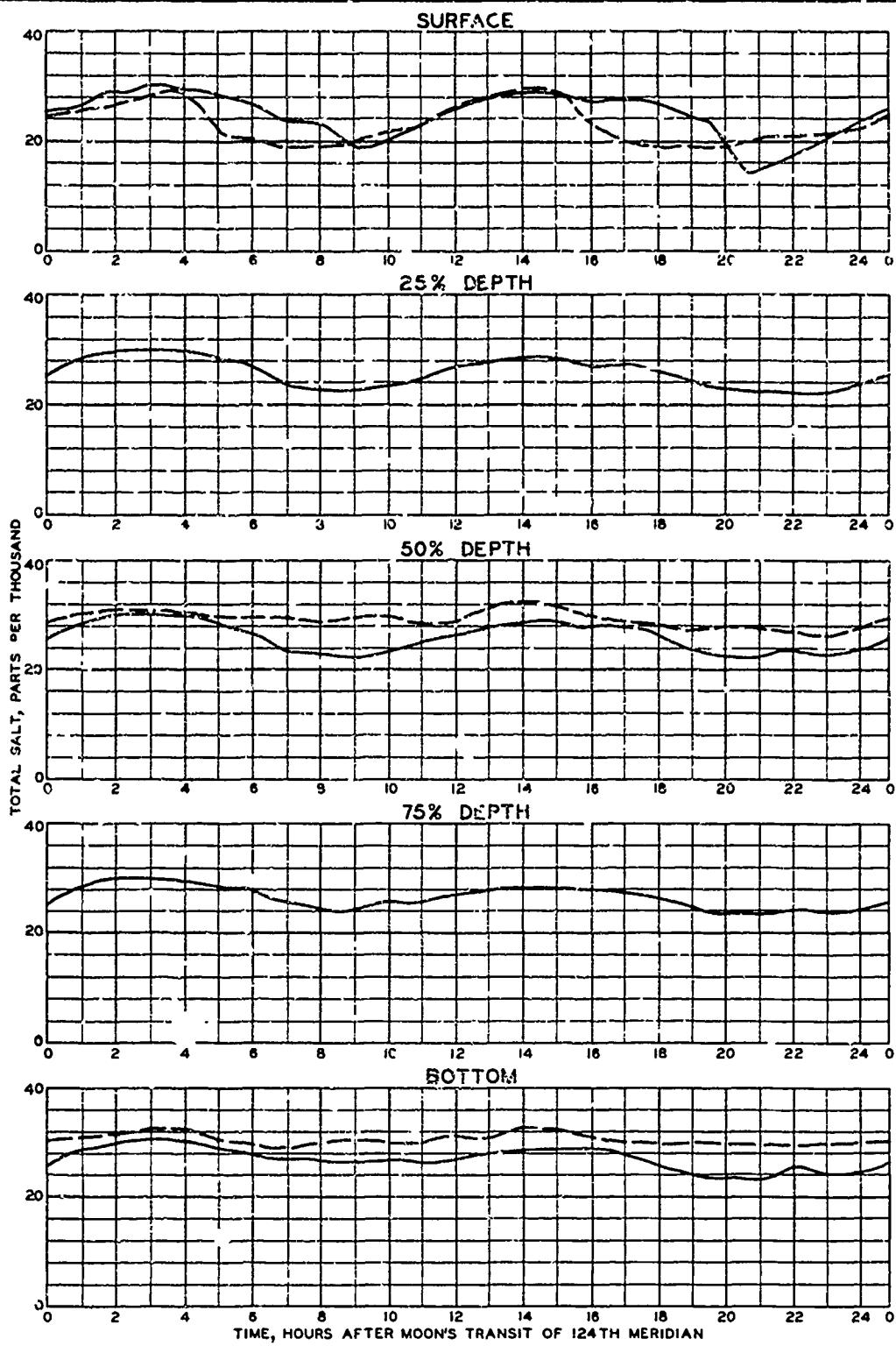
MODEL TEST DATA

TIDE .. NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY . 33.0 PPT

LEGEND
 — MODEL

VERIFICATION OF
 NEAP TIDE SALINITIES
 STATION 10





MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE ... 10,500 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND
 —— PROTOTYPE (13-14 OCT 67)
 - - - MODEL

**VERIFICATION OF
NEAP TIDE SALINITIES**

STATION 12

PLATE 99

103

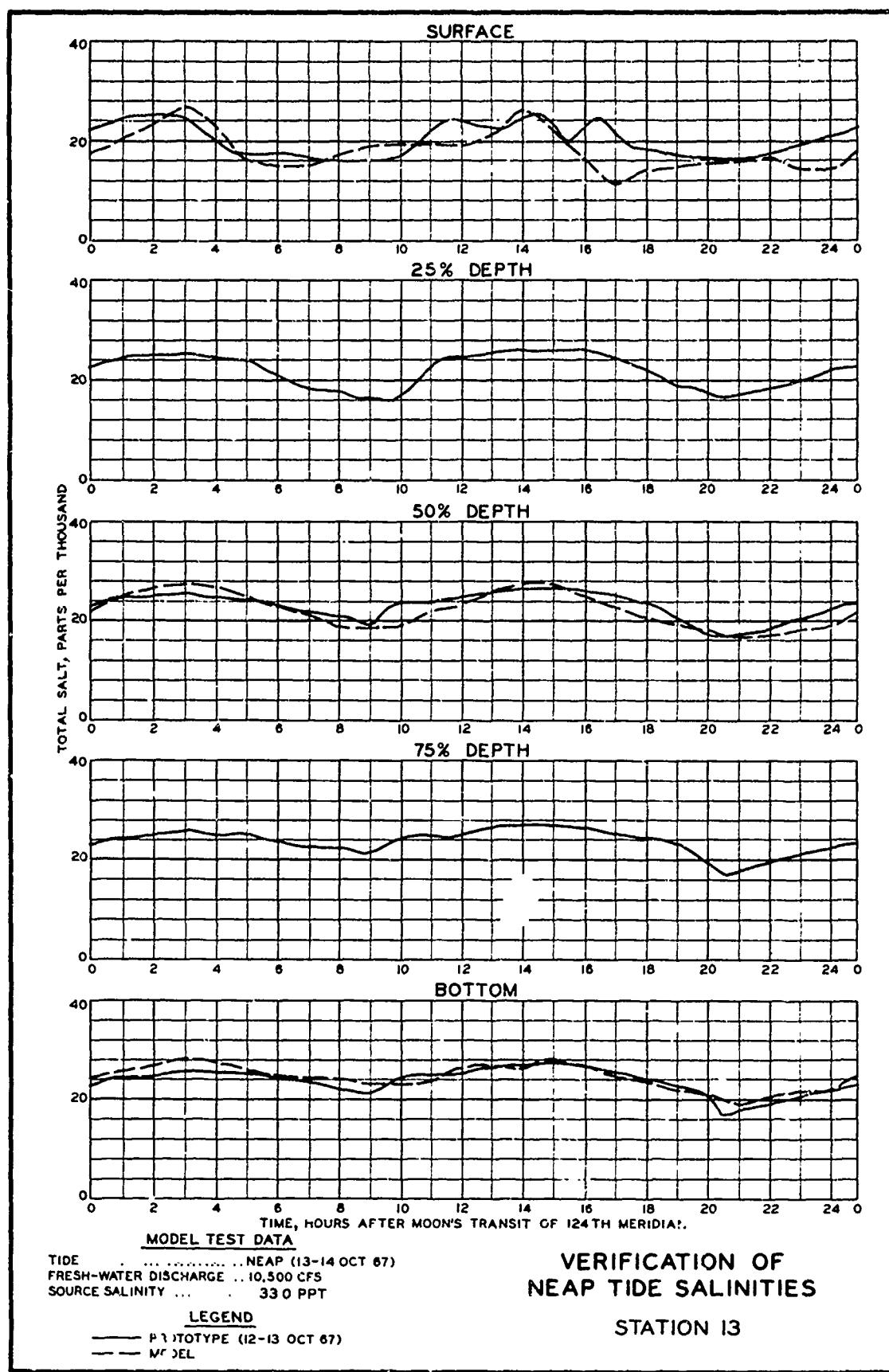
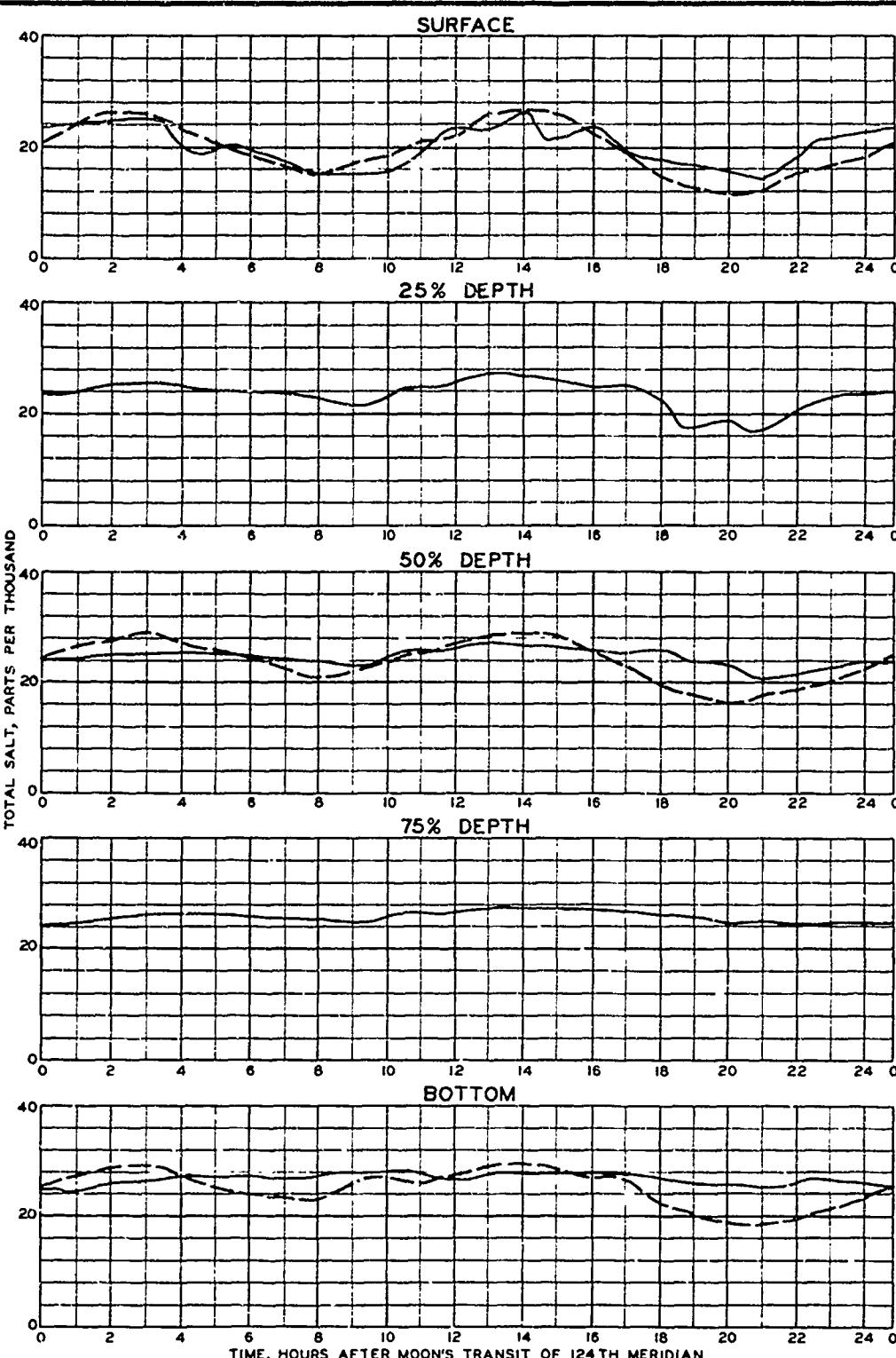


PLATE 100

164



MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY ... 33.0 PPT

LEGEND

— PROTOTYPE (12-13 OCT 67)
 - - MODEL

VERIFICATION OF
NEAP TIDE SALINITIES

STATION 14

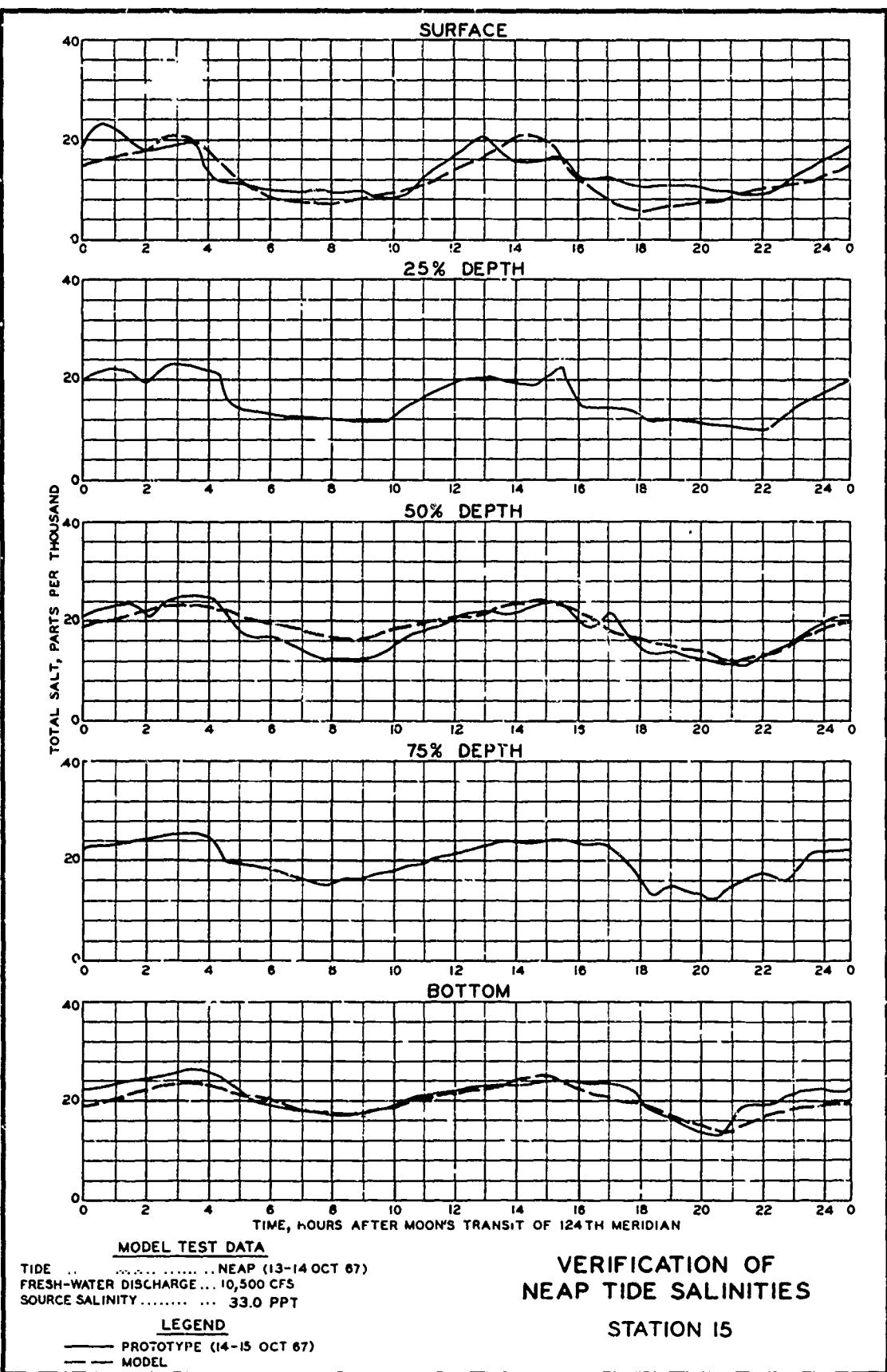
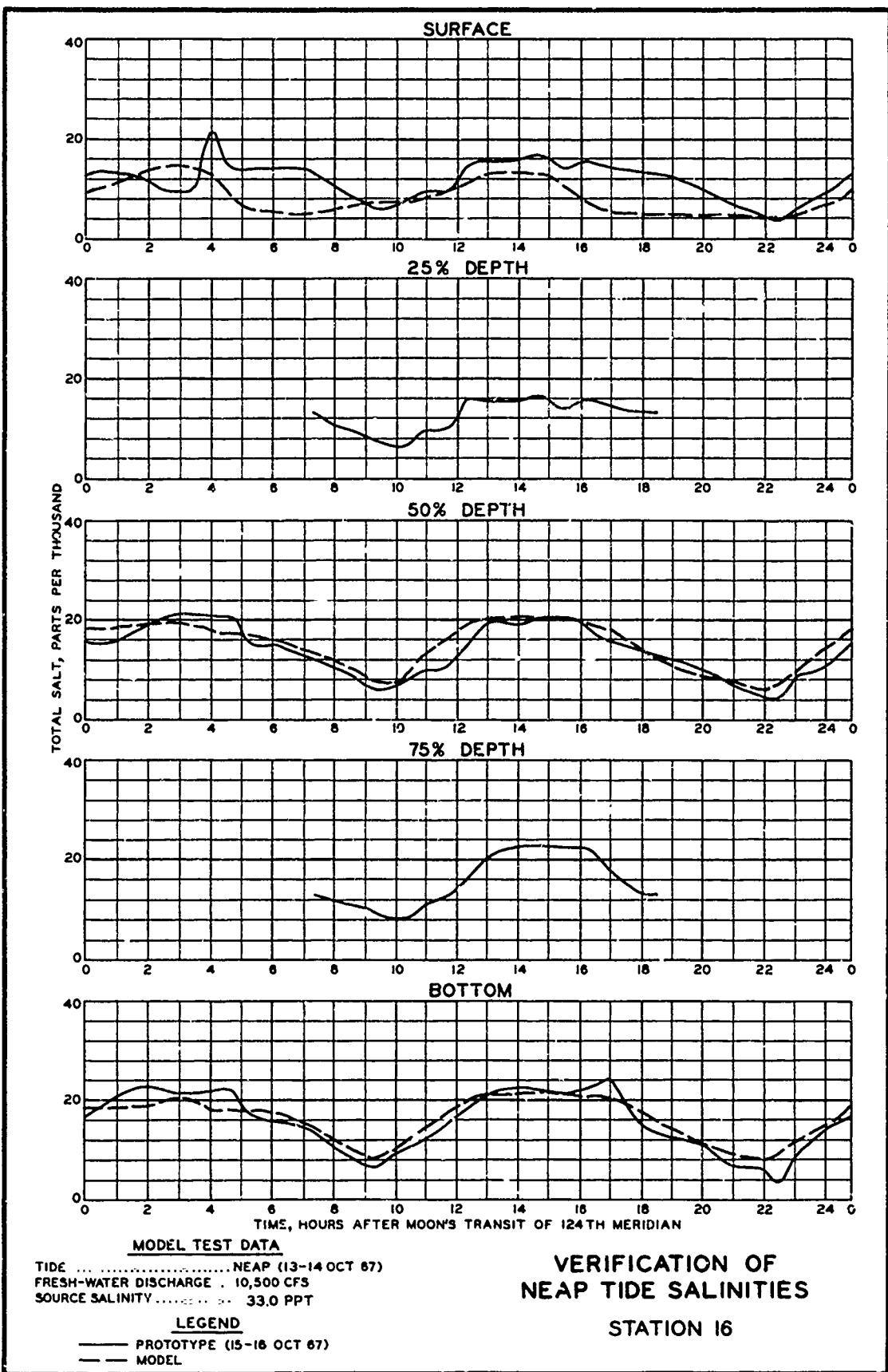
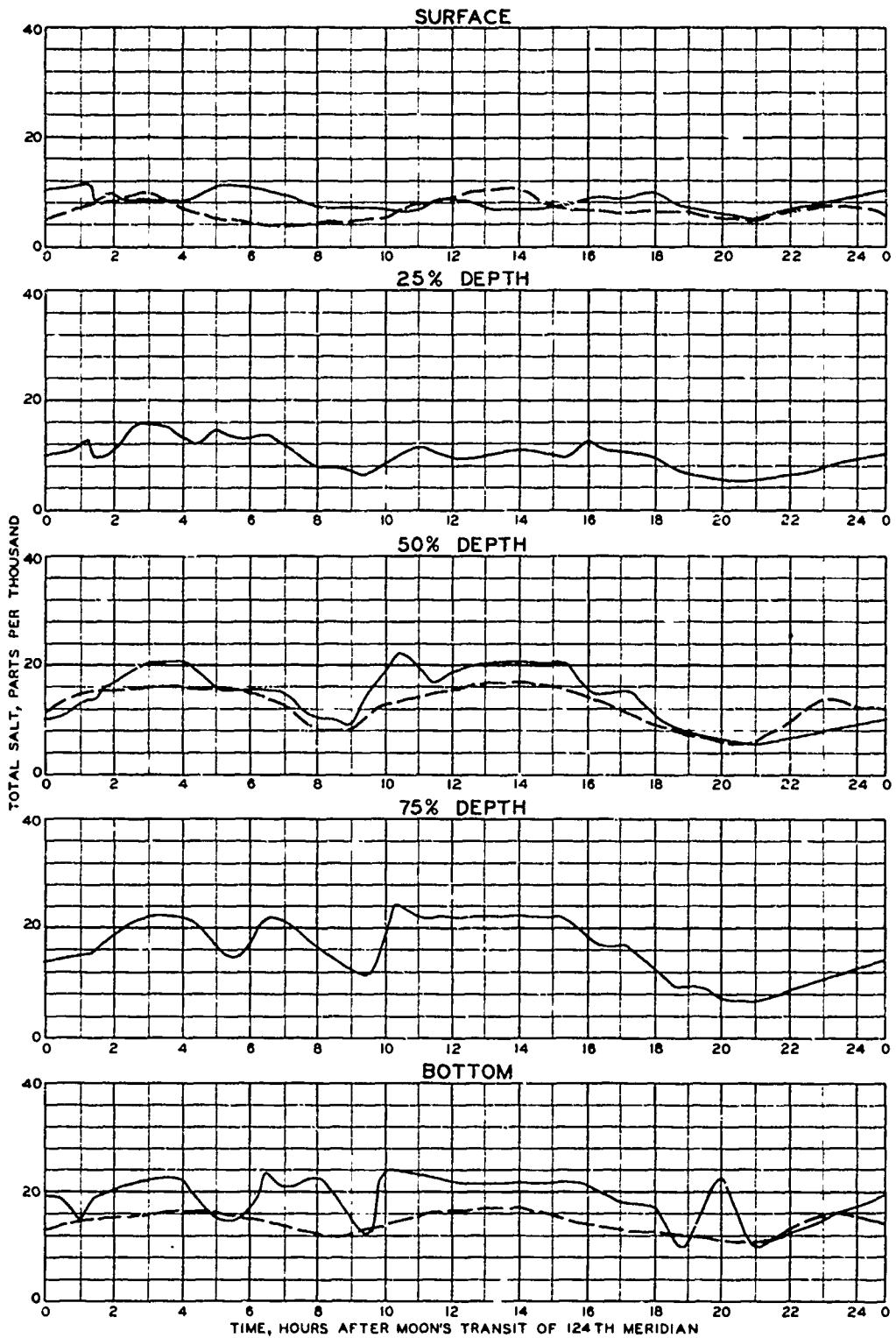


PLATE 102

106





MODEL TEST DATA

TIDE NEAP (13-14 OCT 67)
 FRESH-WATER DISCHARGE.. 10,500 CFS
 SOURCE SALINITY .. 33.0 PPT

**VERIFICATION OF
NEAP TIDE SALINITIES**

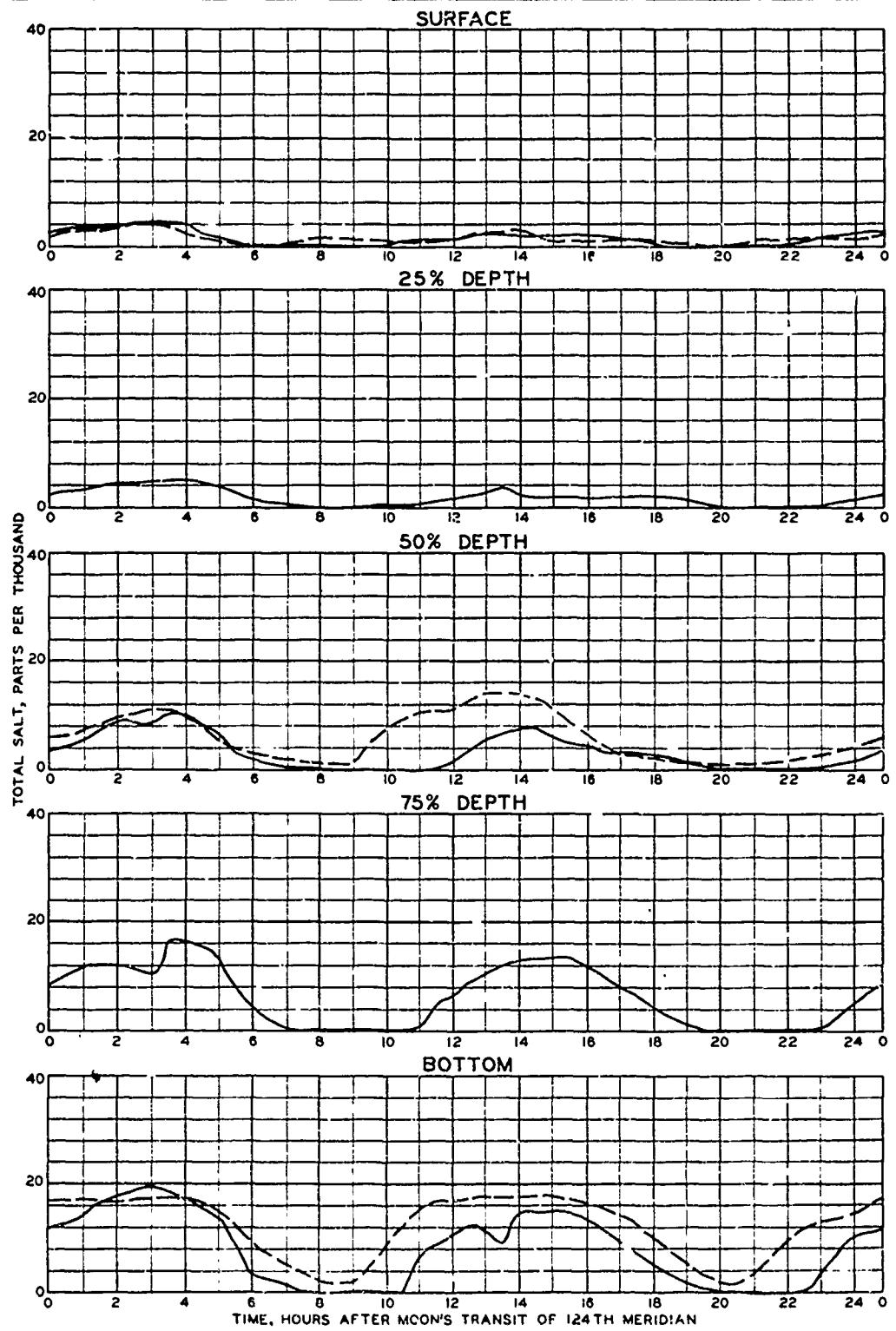
STATION 17

LEGEND

— PROTOTYPE (12-13 OCT 67)
 - - MODEL

PLATE 104

18



MODEL TEST DATA

TIDE ... NEAP (3-14 OCT 67)
 FRESH-WATER DISCHARGE 10,500 CFS
 SOURCE SALINITY ... 330 PPT

VERIFICATION OF
NEAP TIDE SALINITIES

STATION 18

LEGEND
 — PROTOTYPE (14-15 OCT 67)
 - - MODEL

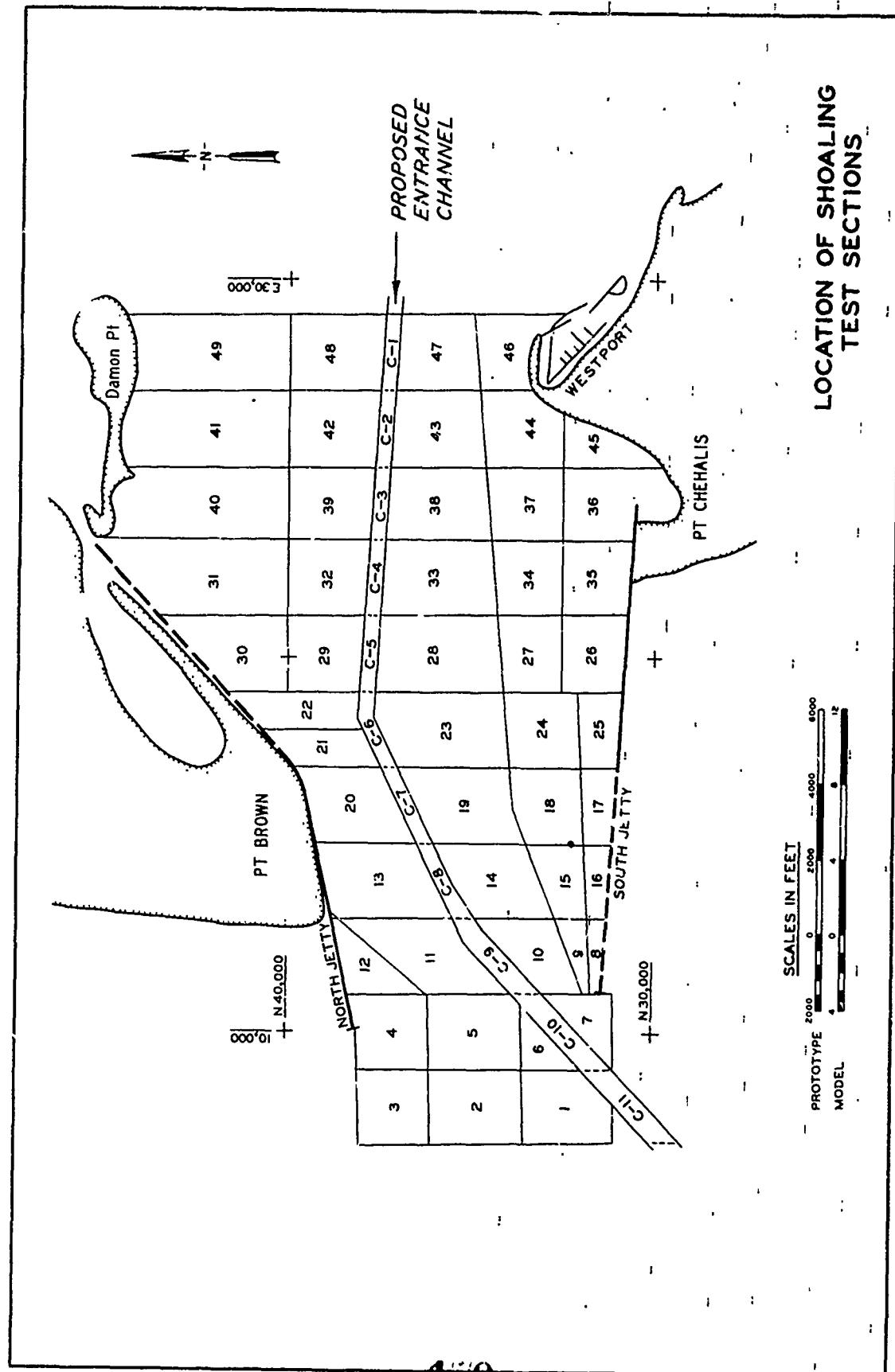
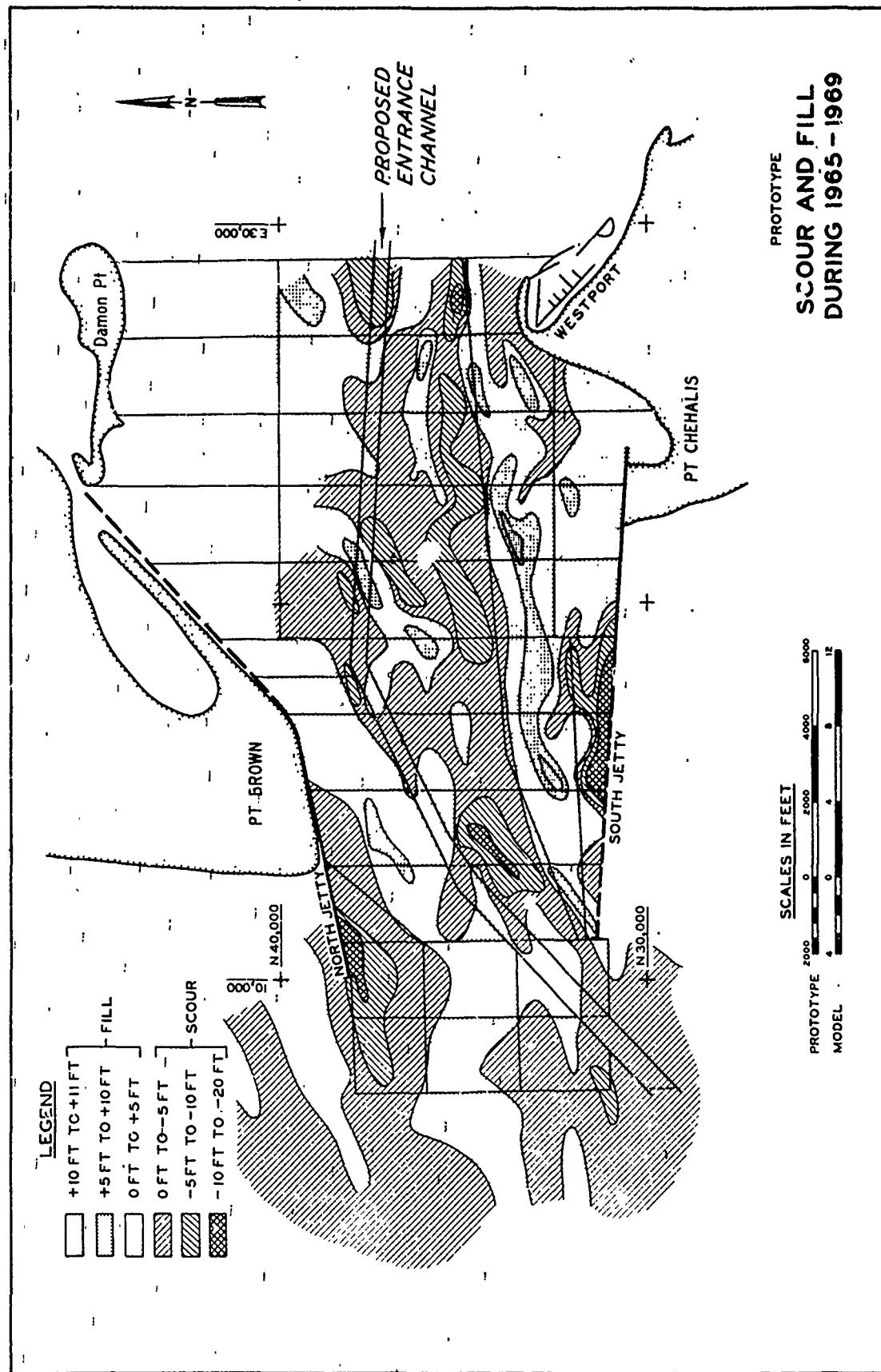
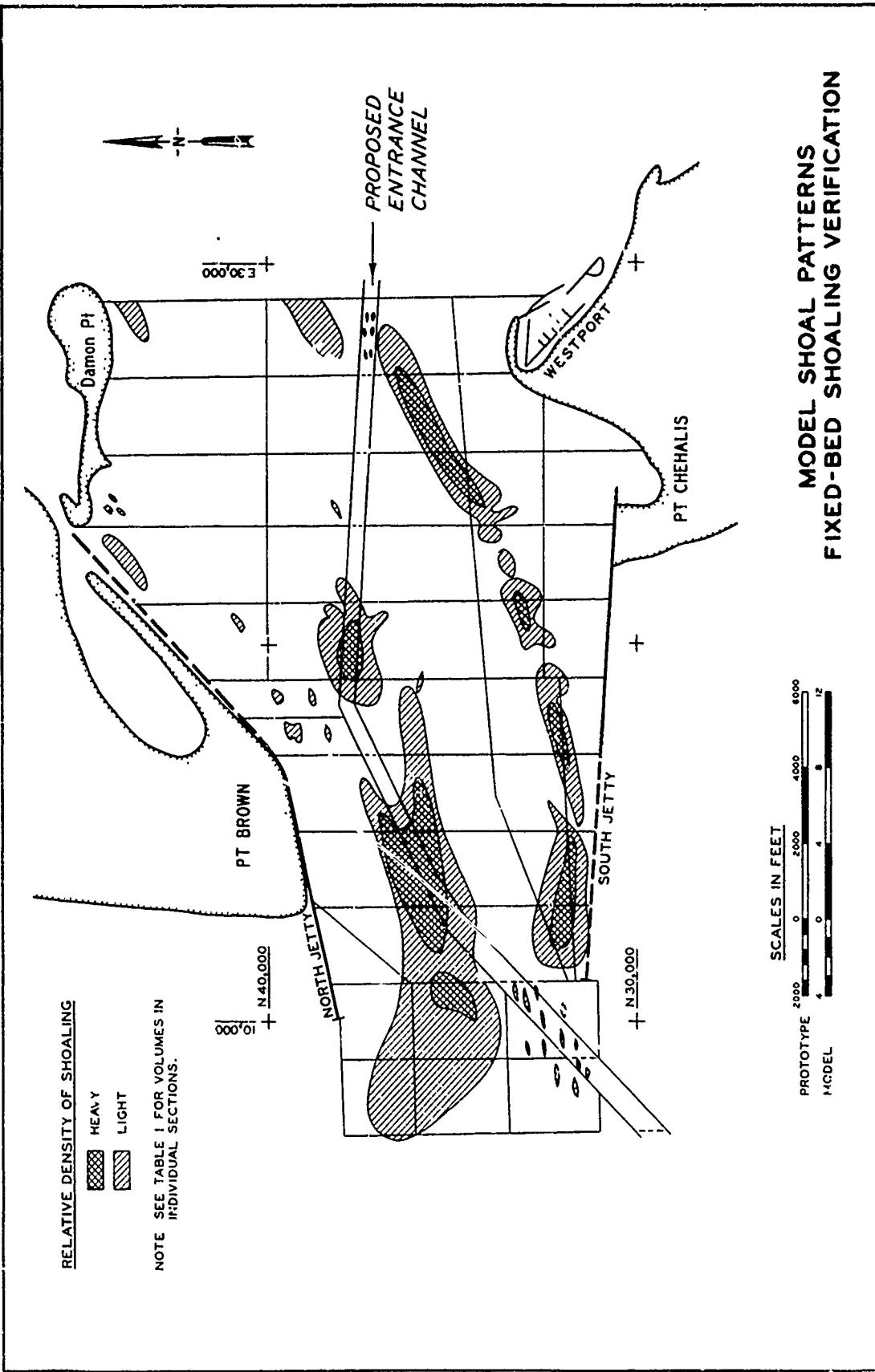


PLATE 106



**MODEL SHOAL PATTERNS
FIXED-BED SHOALING VERIFICATION**



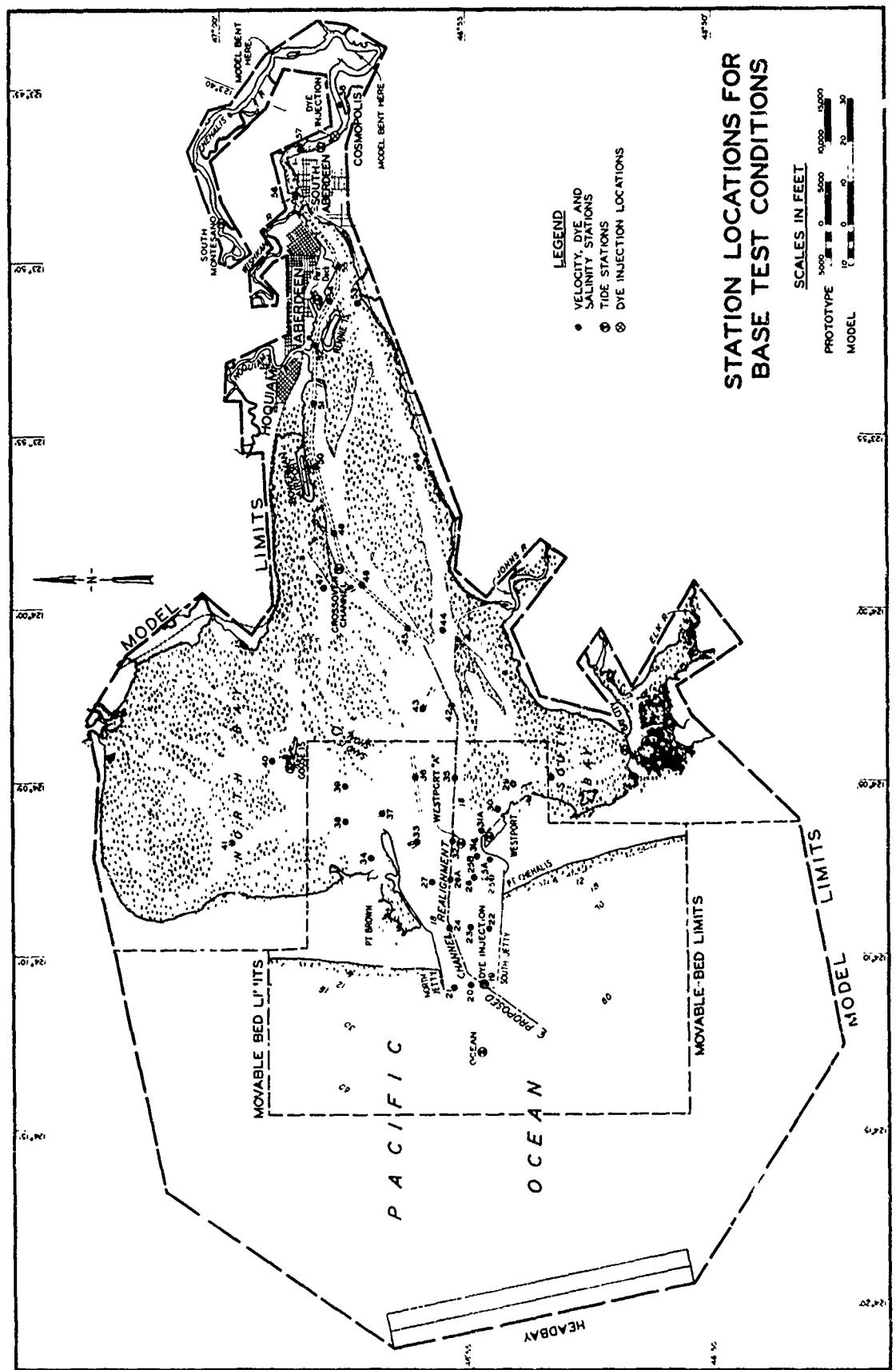
**STATION LOCATIONS FOR
BASE TEST CONDITIONS**

LEGEND

- VELOCITY, DYE AND SALINITY STATIONS
- TIDE STATIONS
- ◎ DYE INJECTION LOCATIONS

SCALES IN FEET

PROTOTYPE	5000	0	5000	10,000
MODEL	10	0	10	20



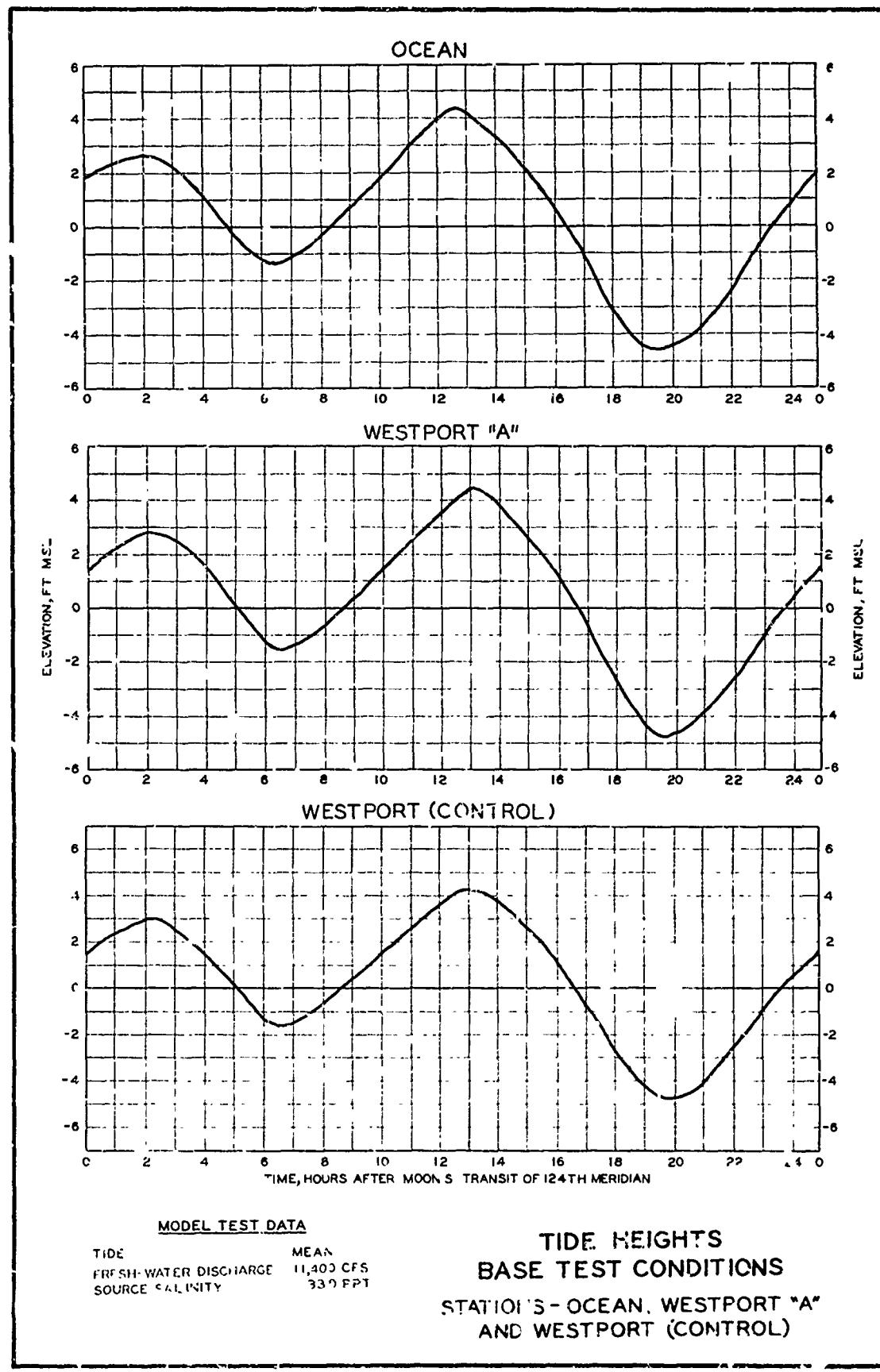
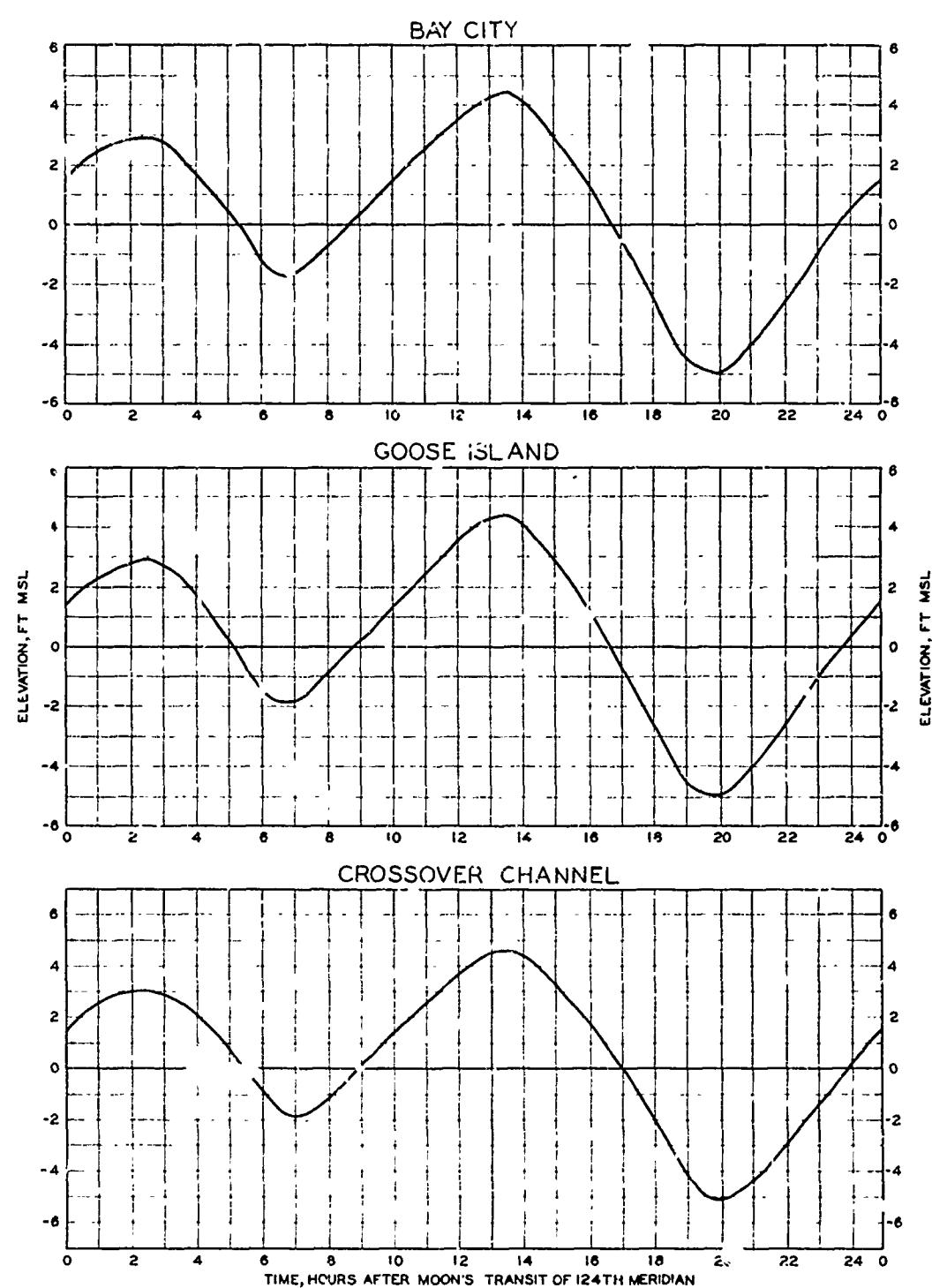


PLATE 110



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	330 PPT

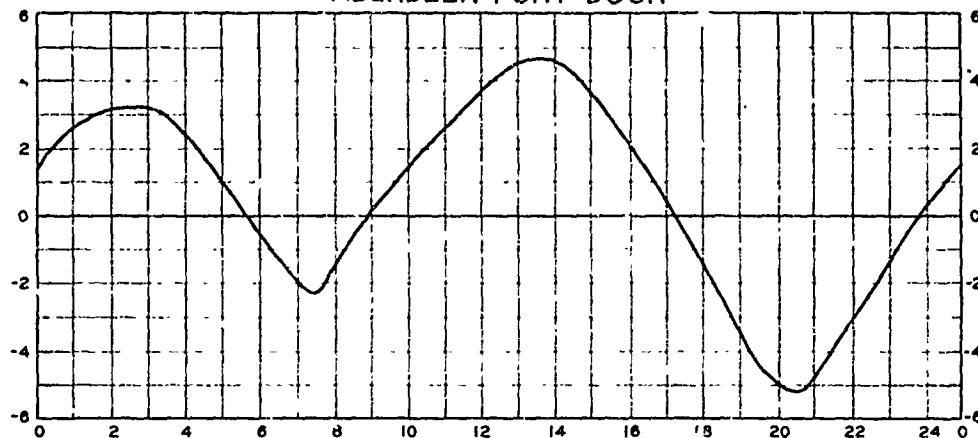
TIDE HEIGHTS

BASE TEST CONDITIONS

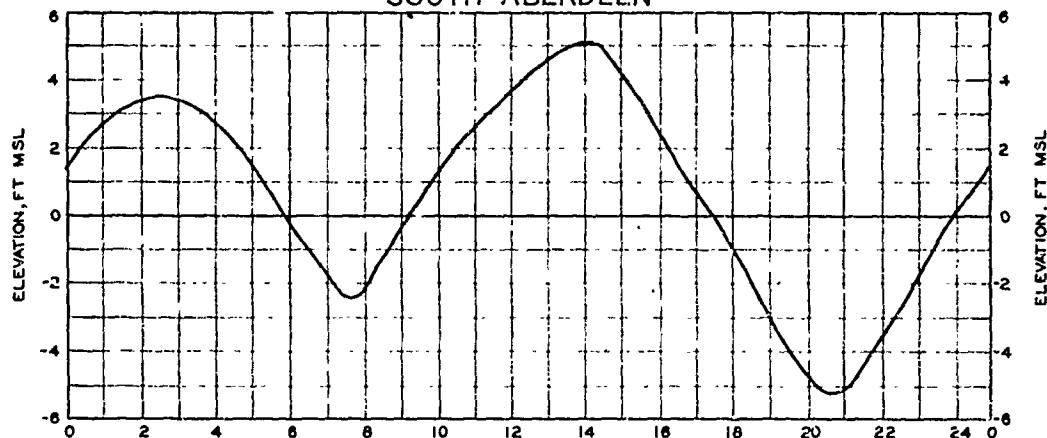
STATIONS-BAY CITY, GOOSE ISLAND
AND CROSSOVER CHANNEL

PLATE III

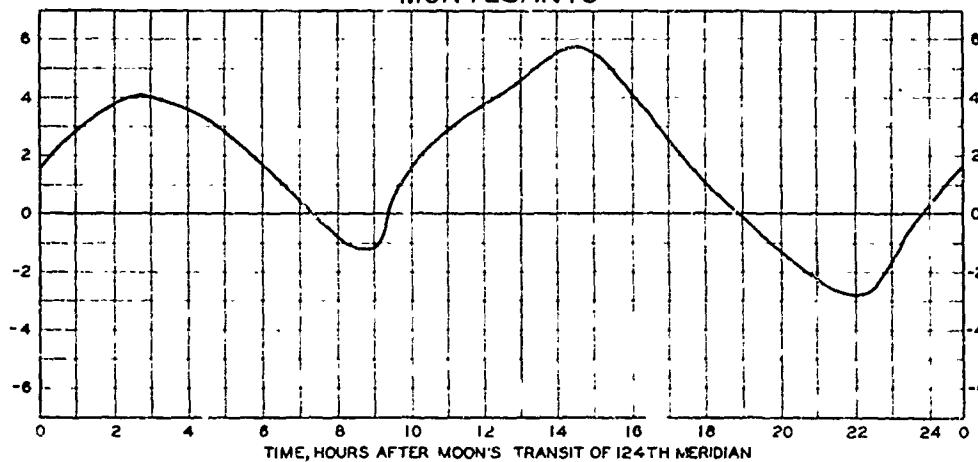
ABERDEEN PORT DOCK



SOUTH ABERDEEN



MONTESANTO



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 330 PPT

TIDE HEIGHTS BASE TEST CONDITIONS

STATIONS--ABERDEEN PORT DOCK,
SOUTH ABERDEEN AND MONTESANTO

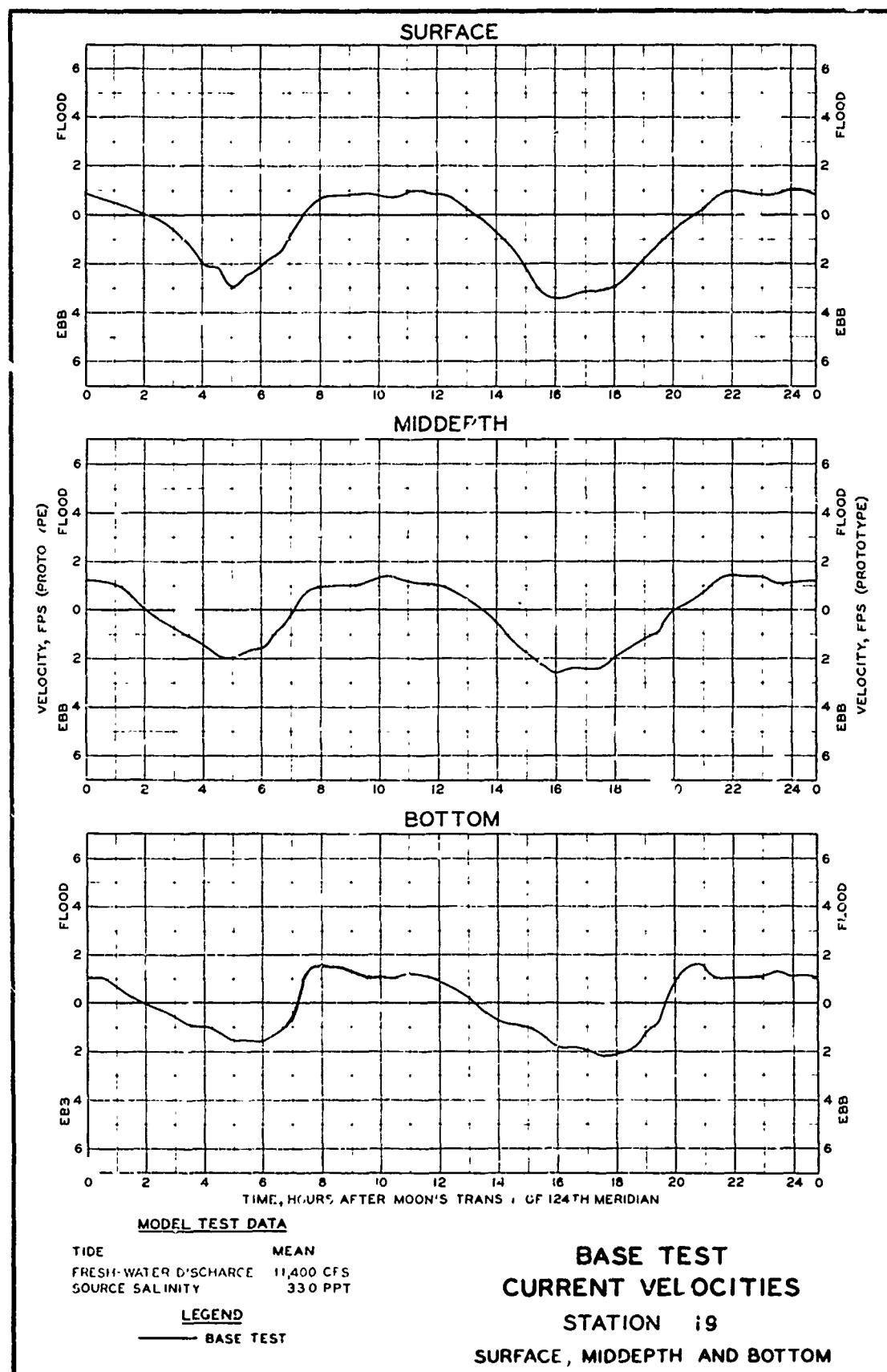


PLATE 113

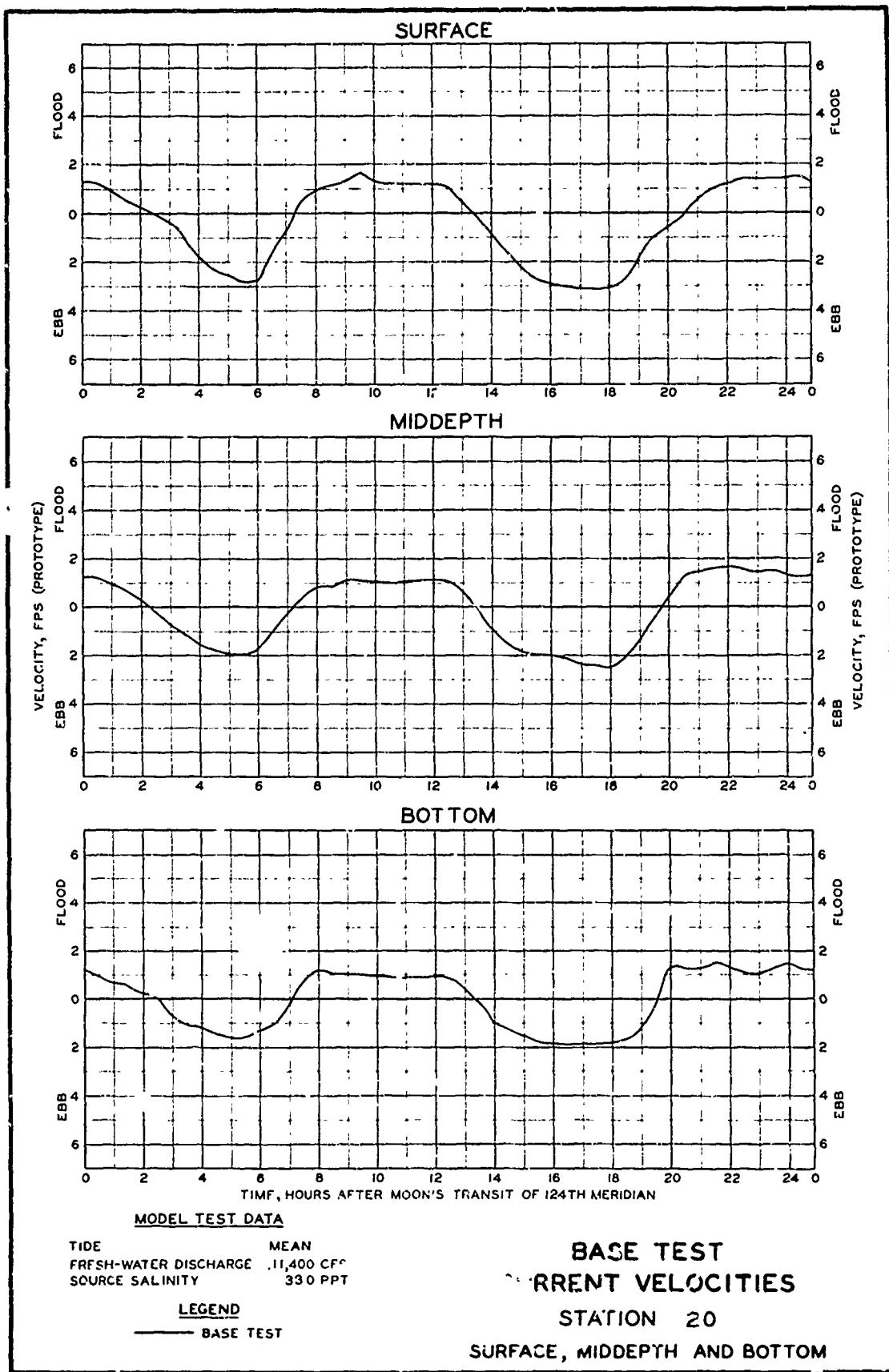


PLATE 114

1.83

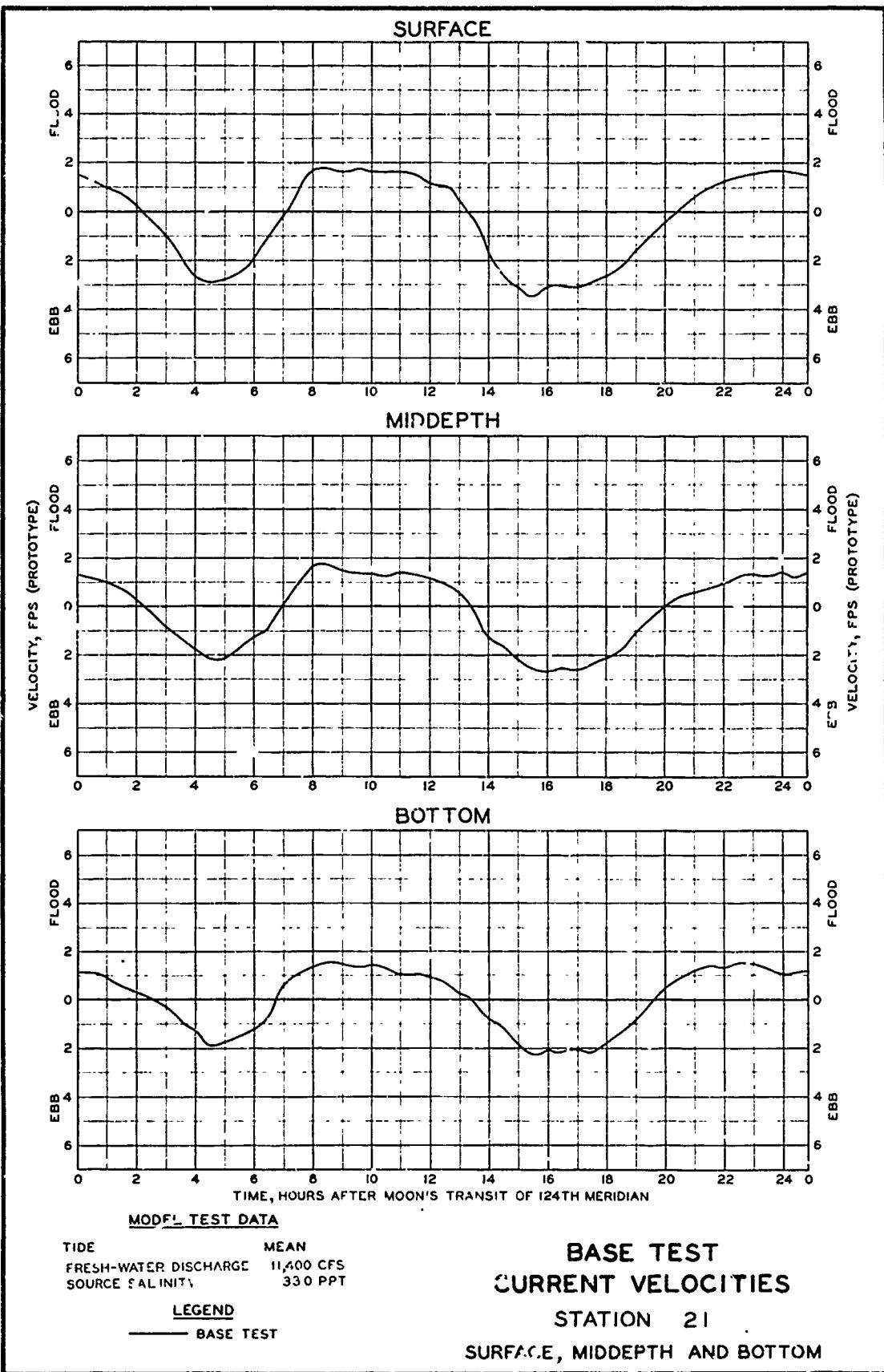


PLATE 115

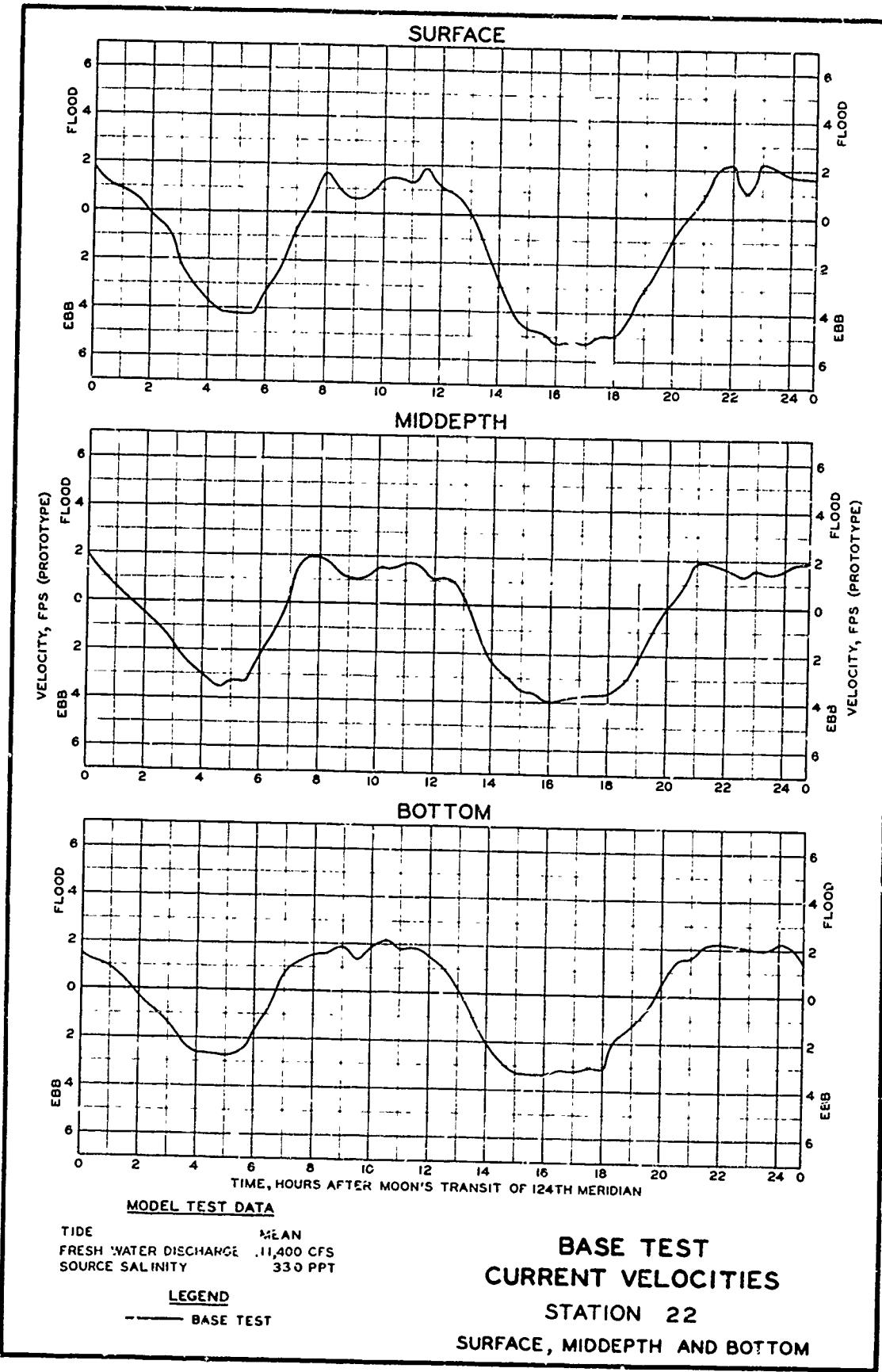
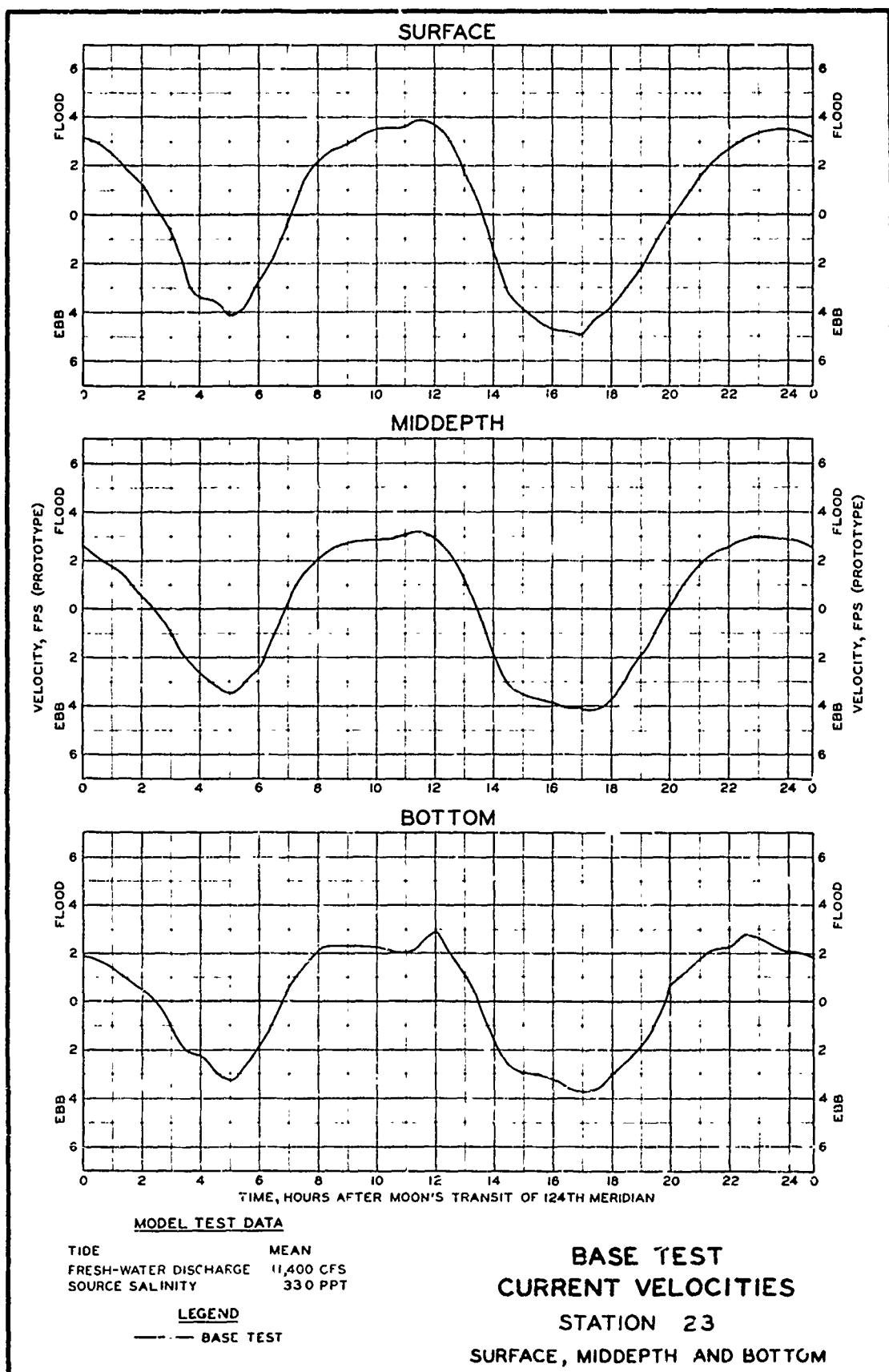


PLATE 116



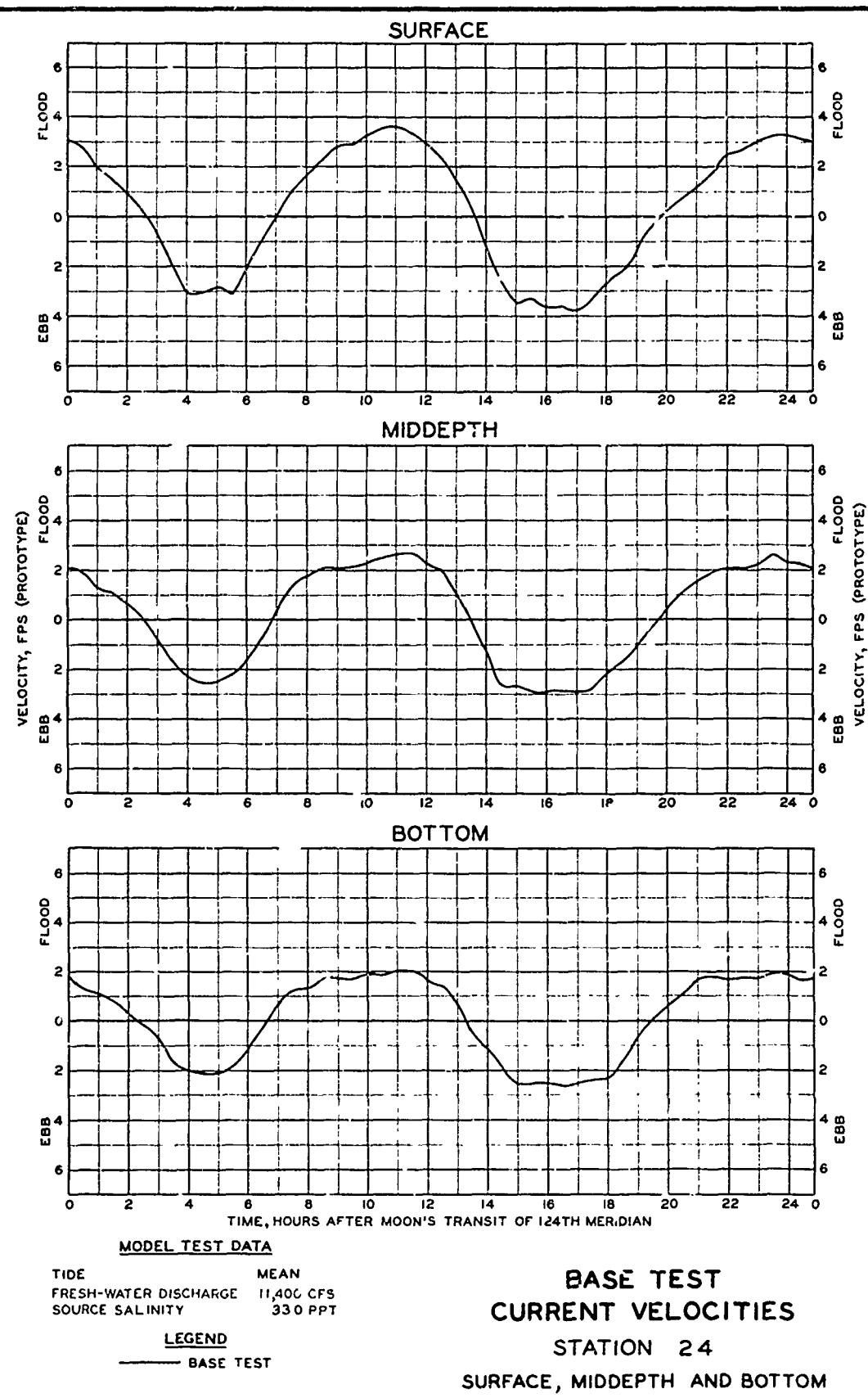
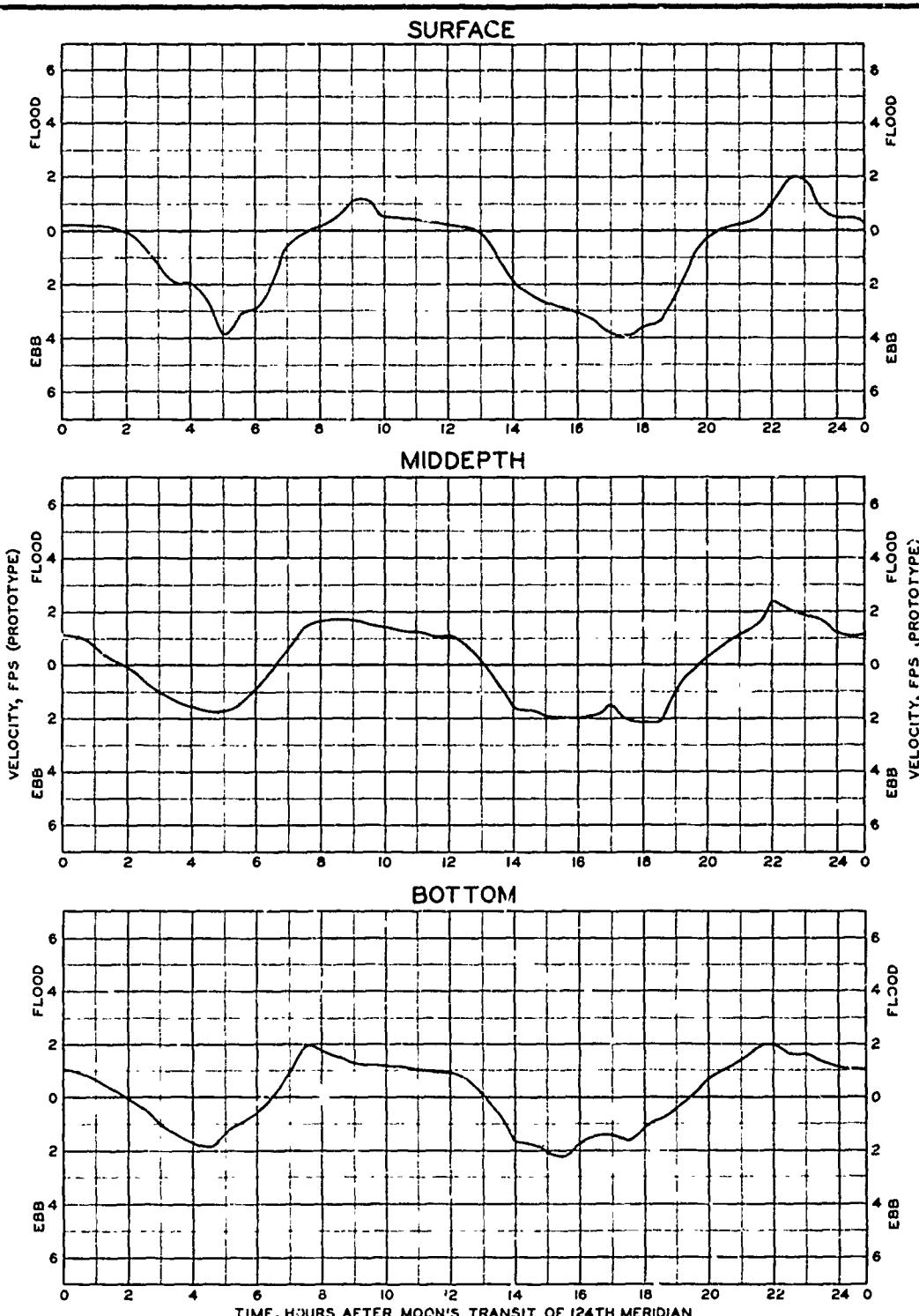


PLATE 118



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE .11,400 CFS
SOURCE SALINITY 33.0 PPT

LEGEND

— BASE TEST

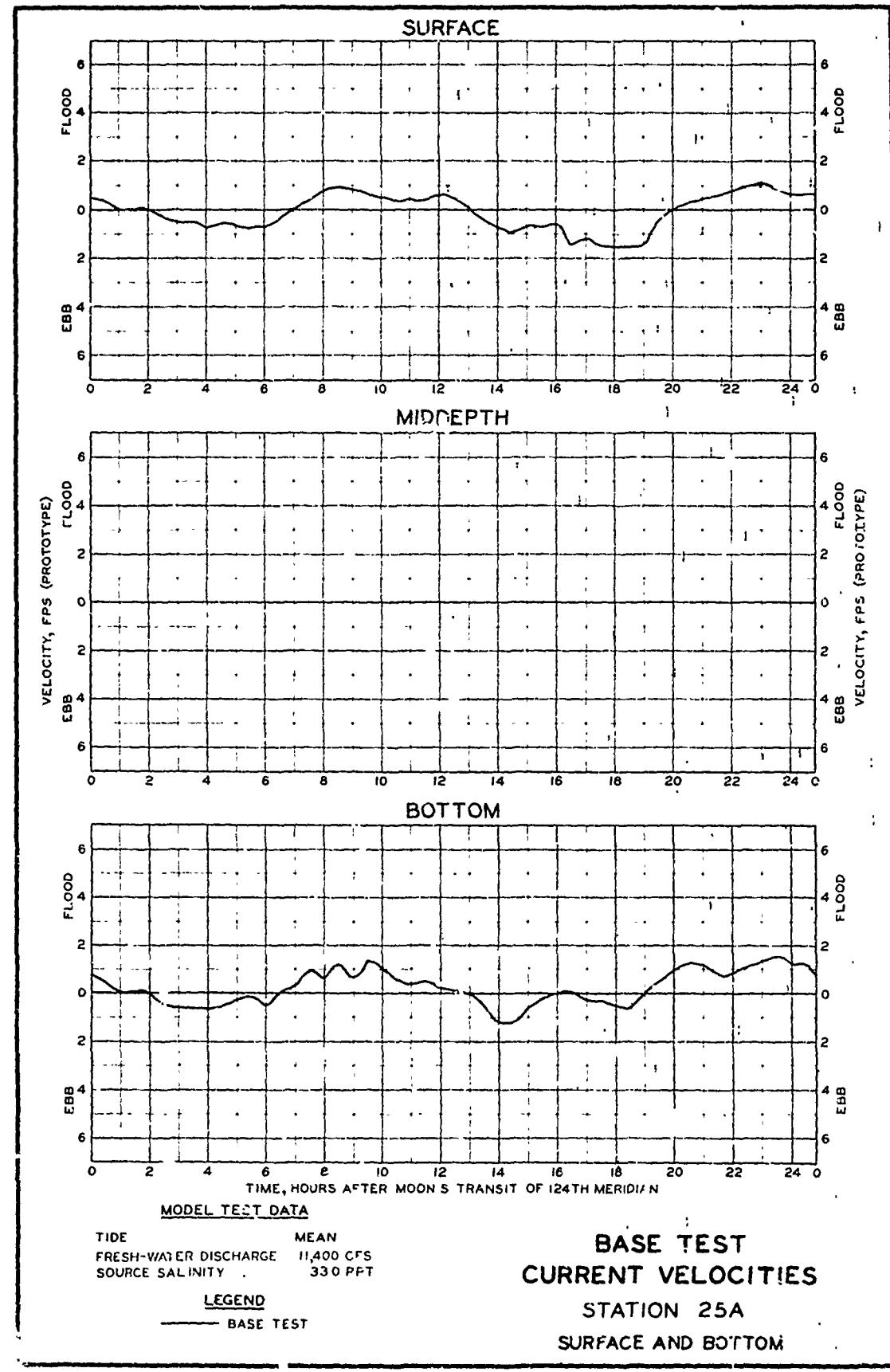
**BASE TEST
CURRENT VELOCITIES**

STATION 25

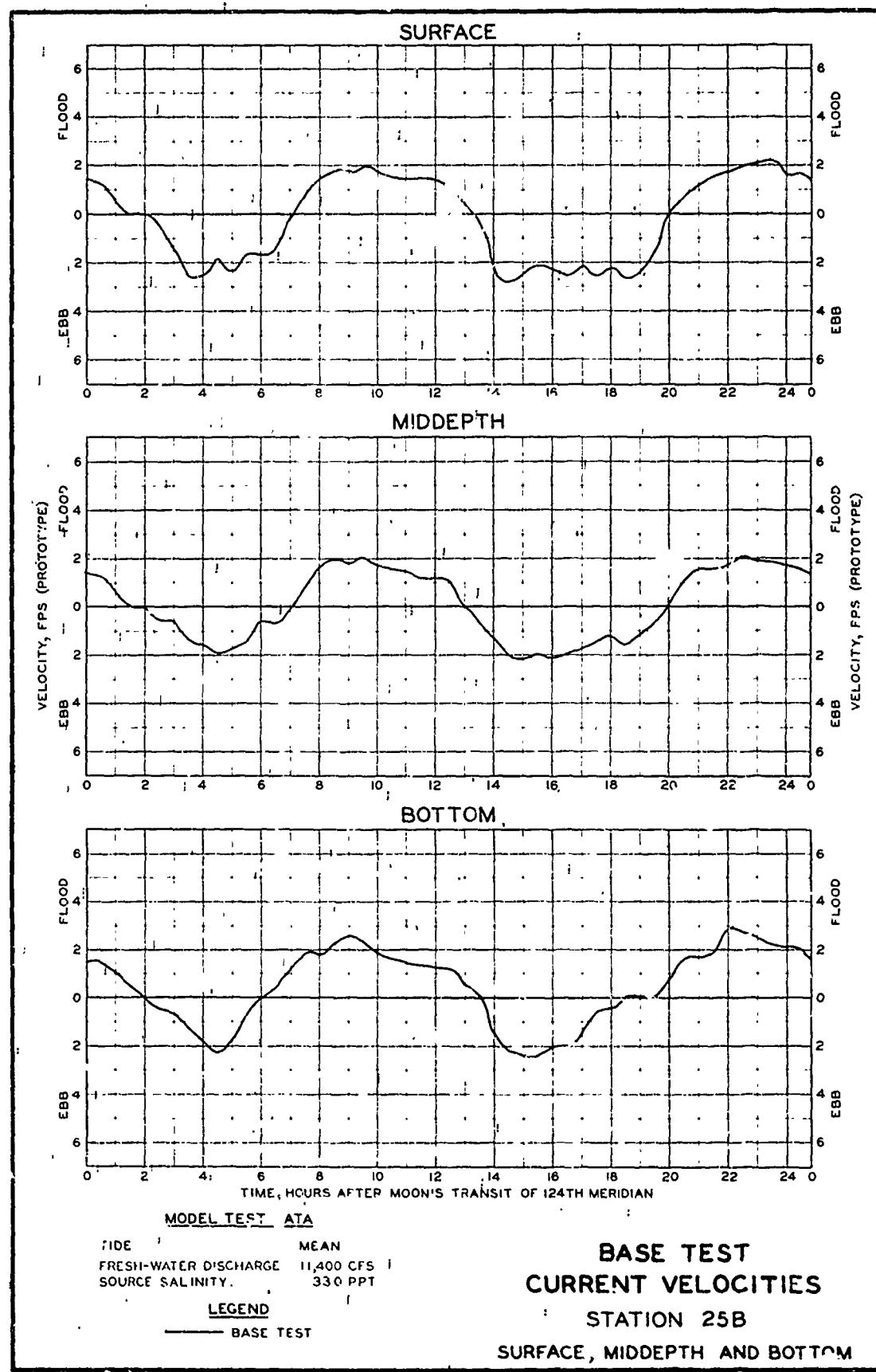
SURFACE, MIDDEPTH AND BOTTOM

1003

PLATE 119



LATE 120



2005

PLATE 121

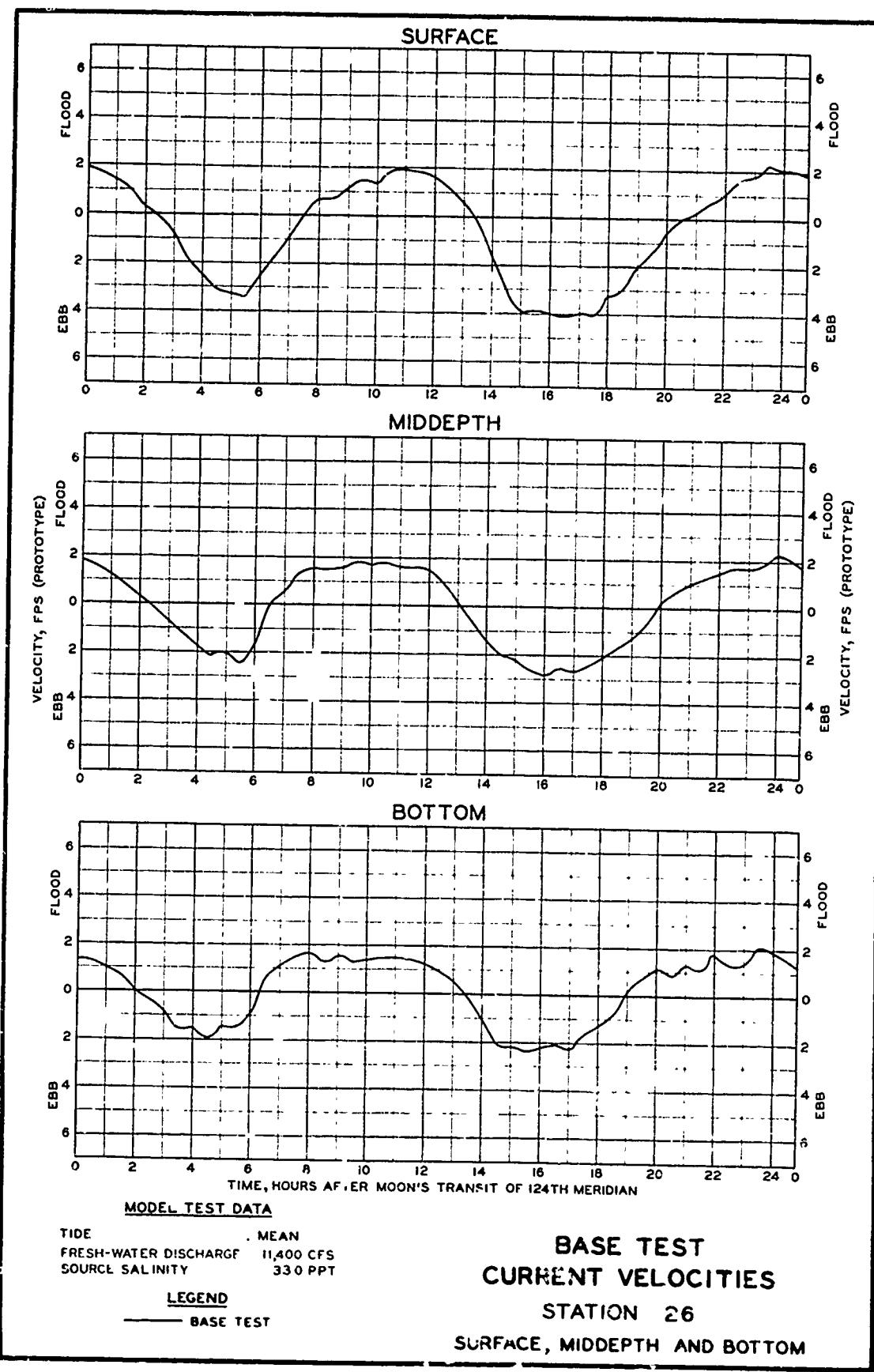
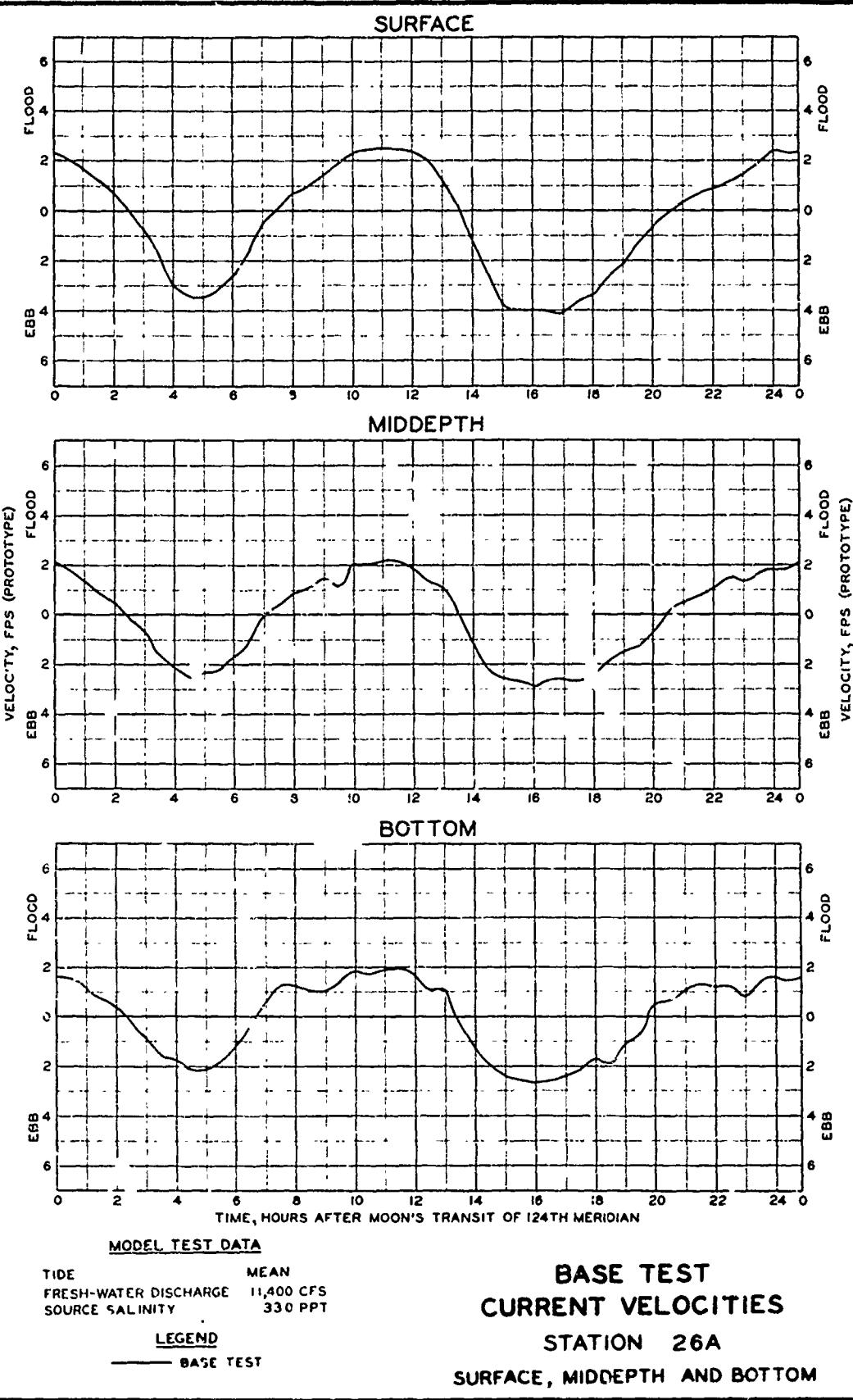


PLATE 122



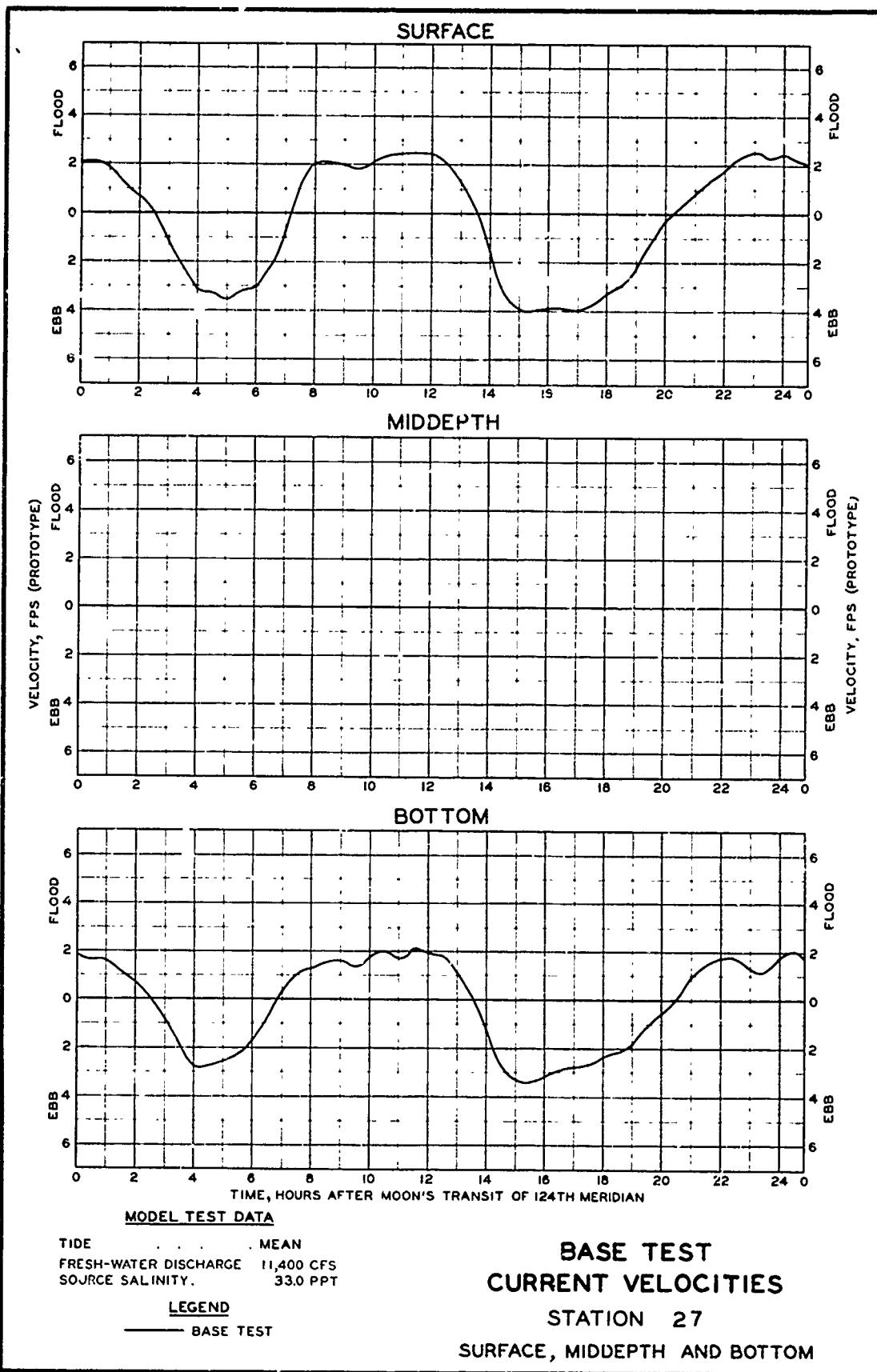
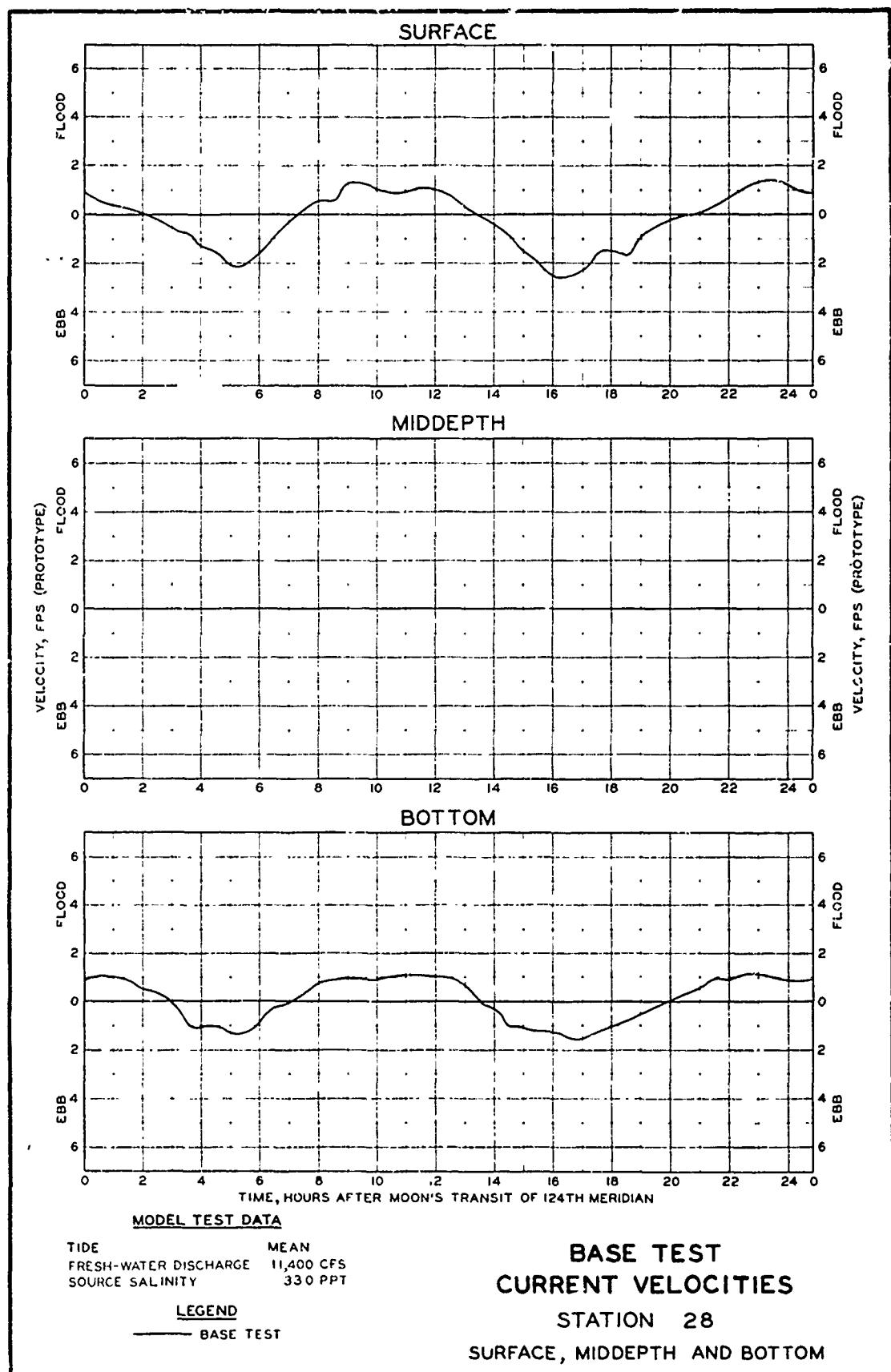
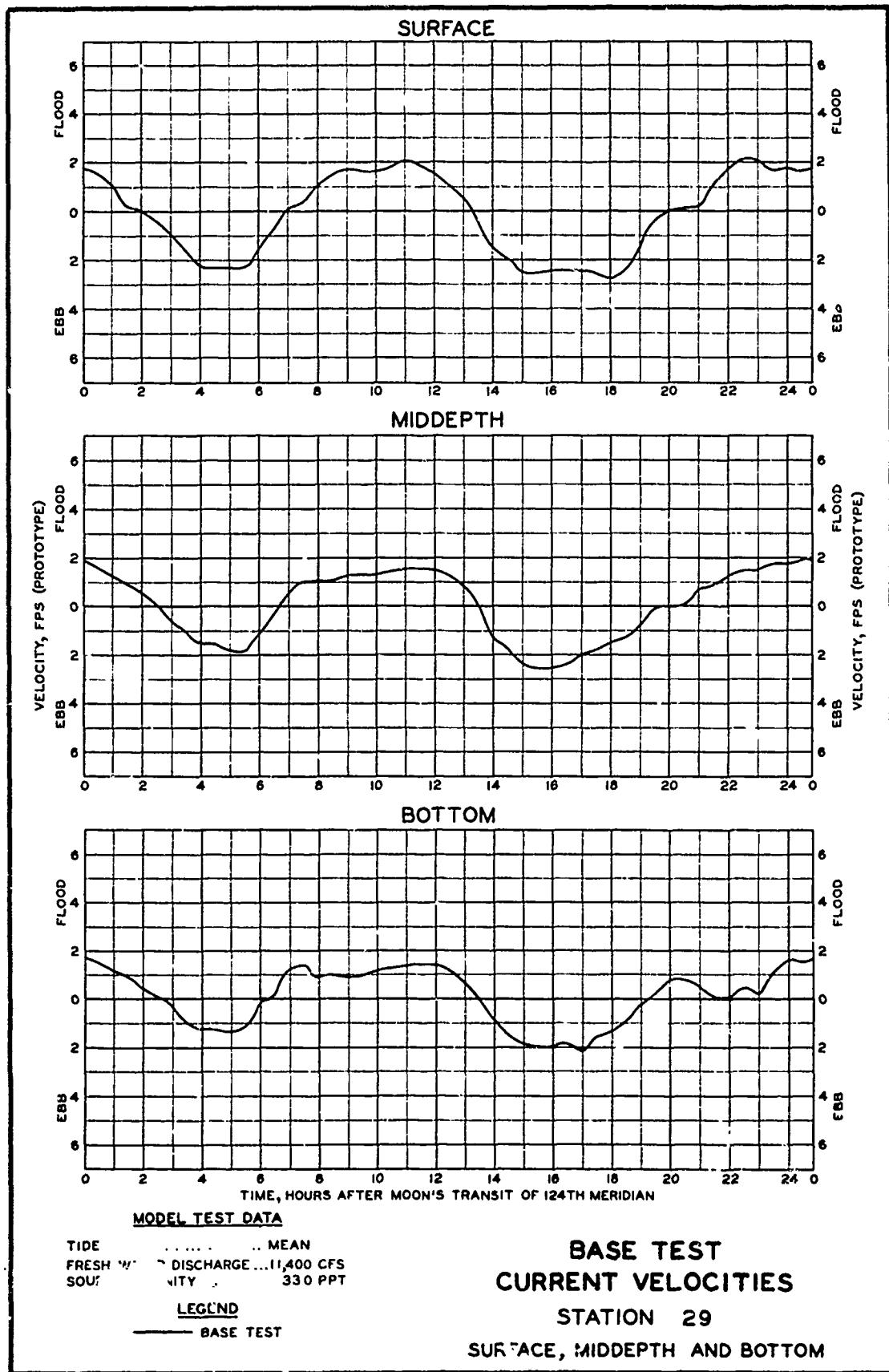
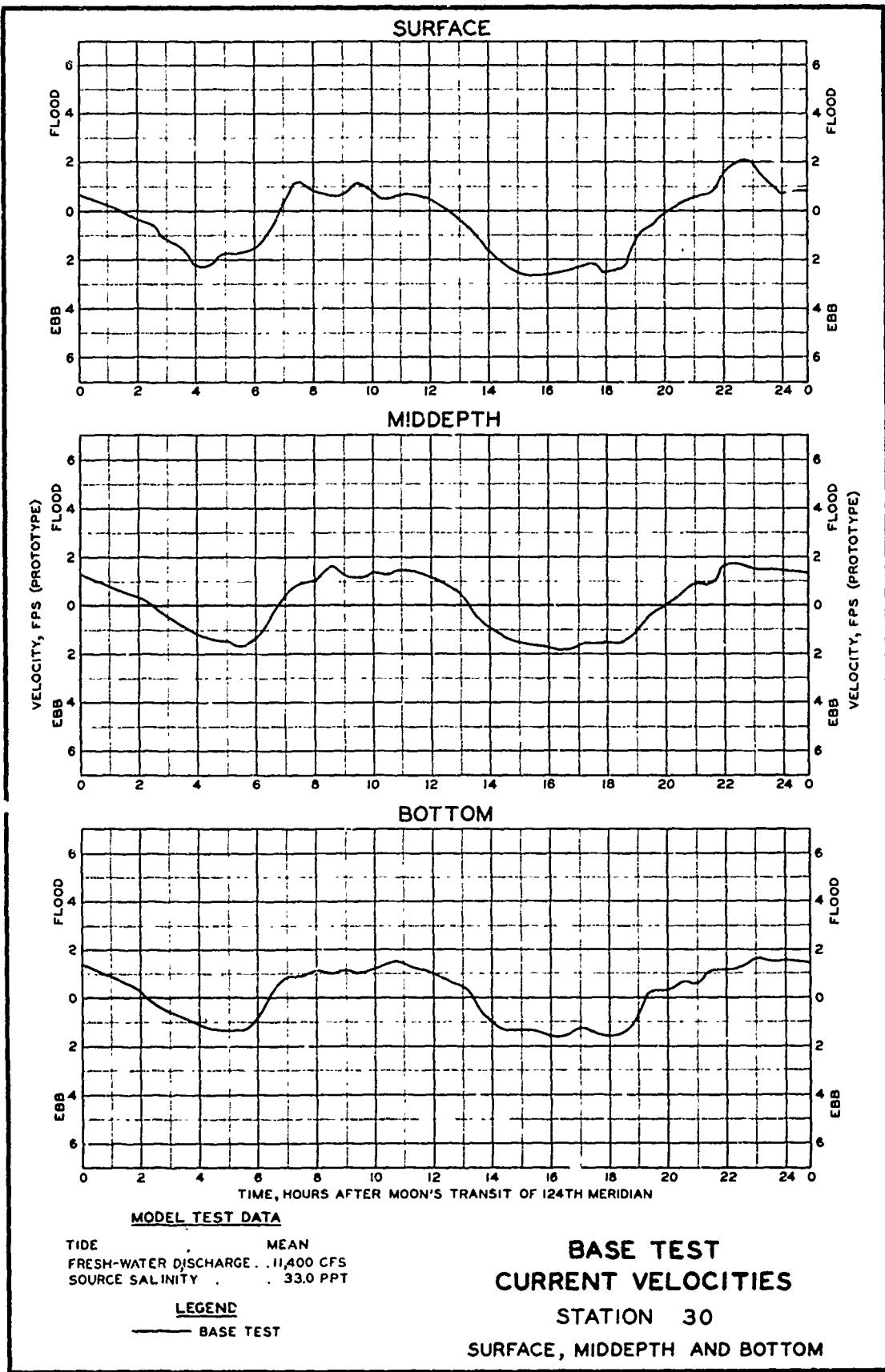


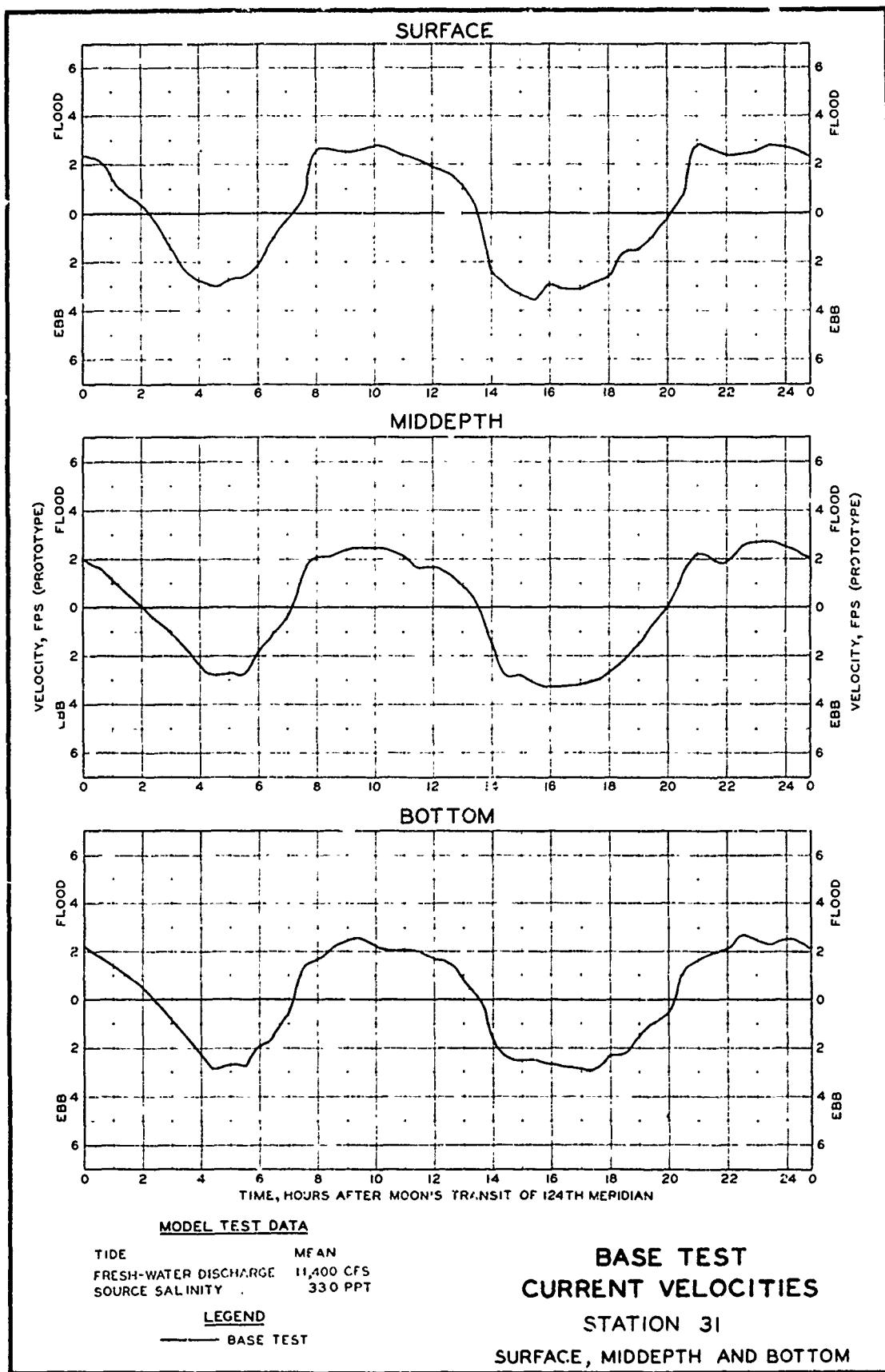
PLATE 124

208









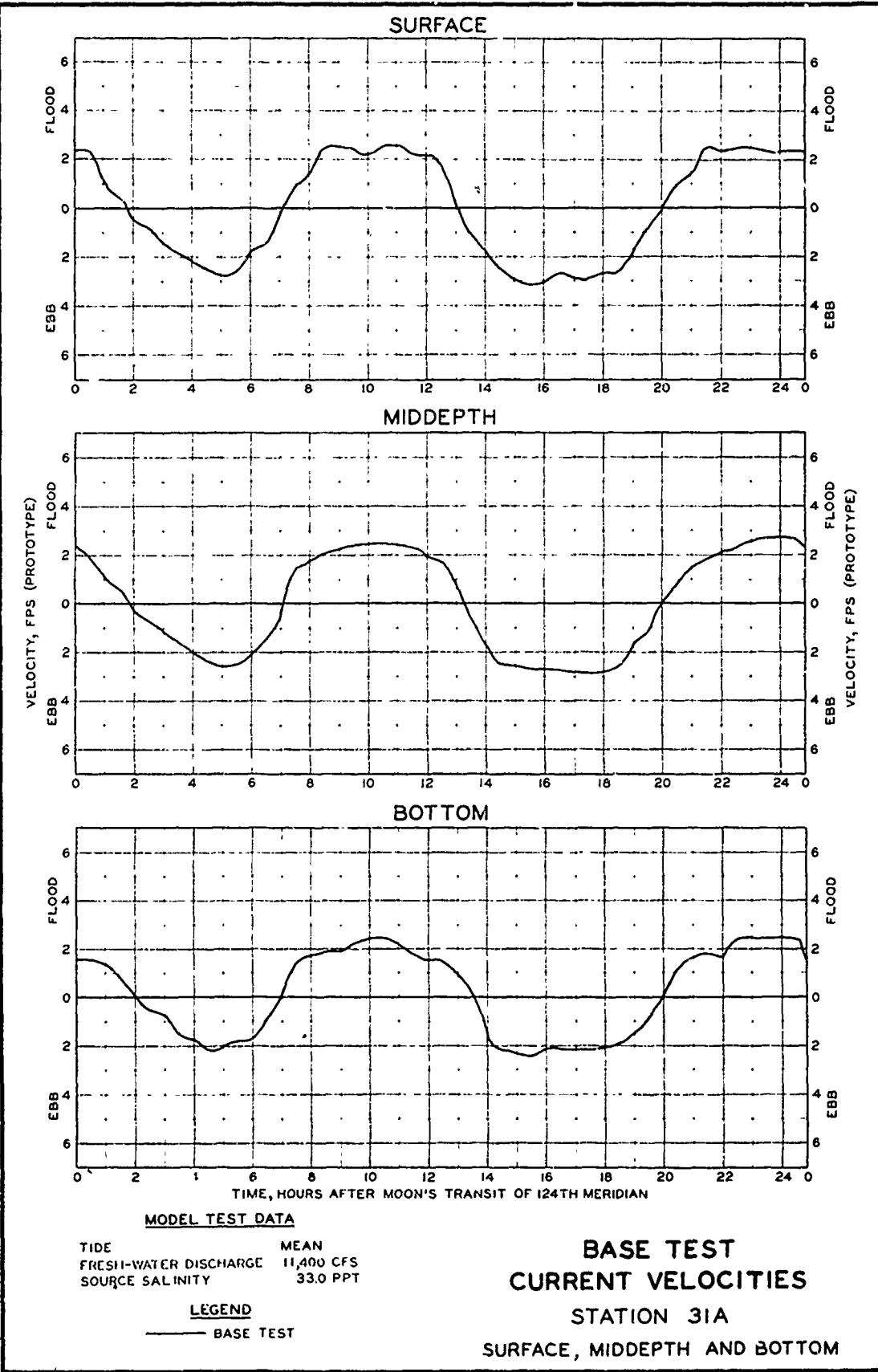


PLATE 129

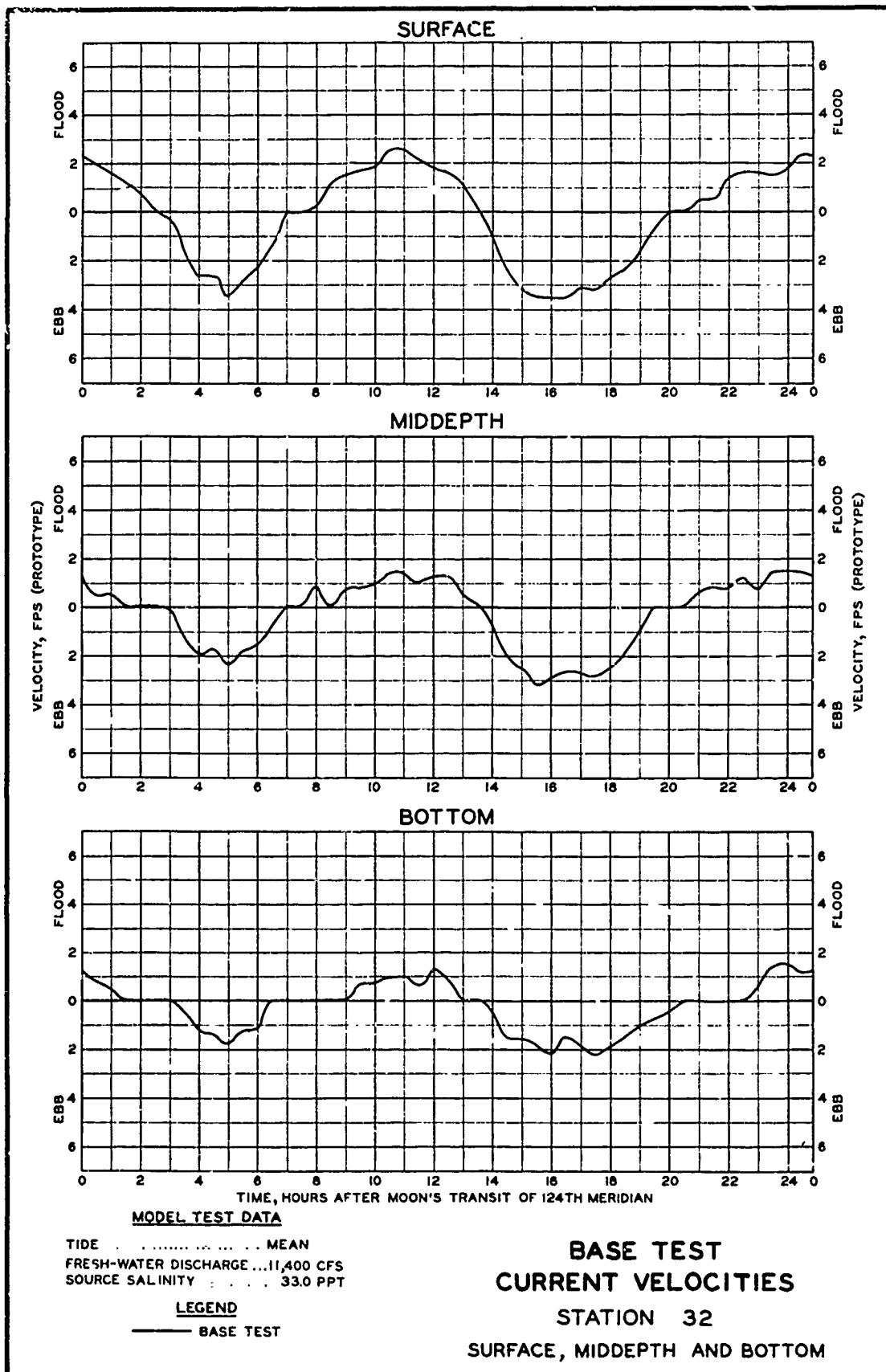


PLATE 130

184

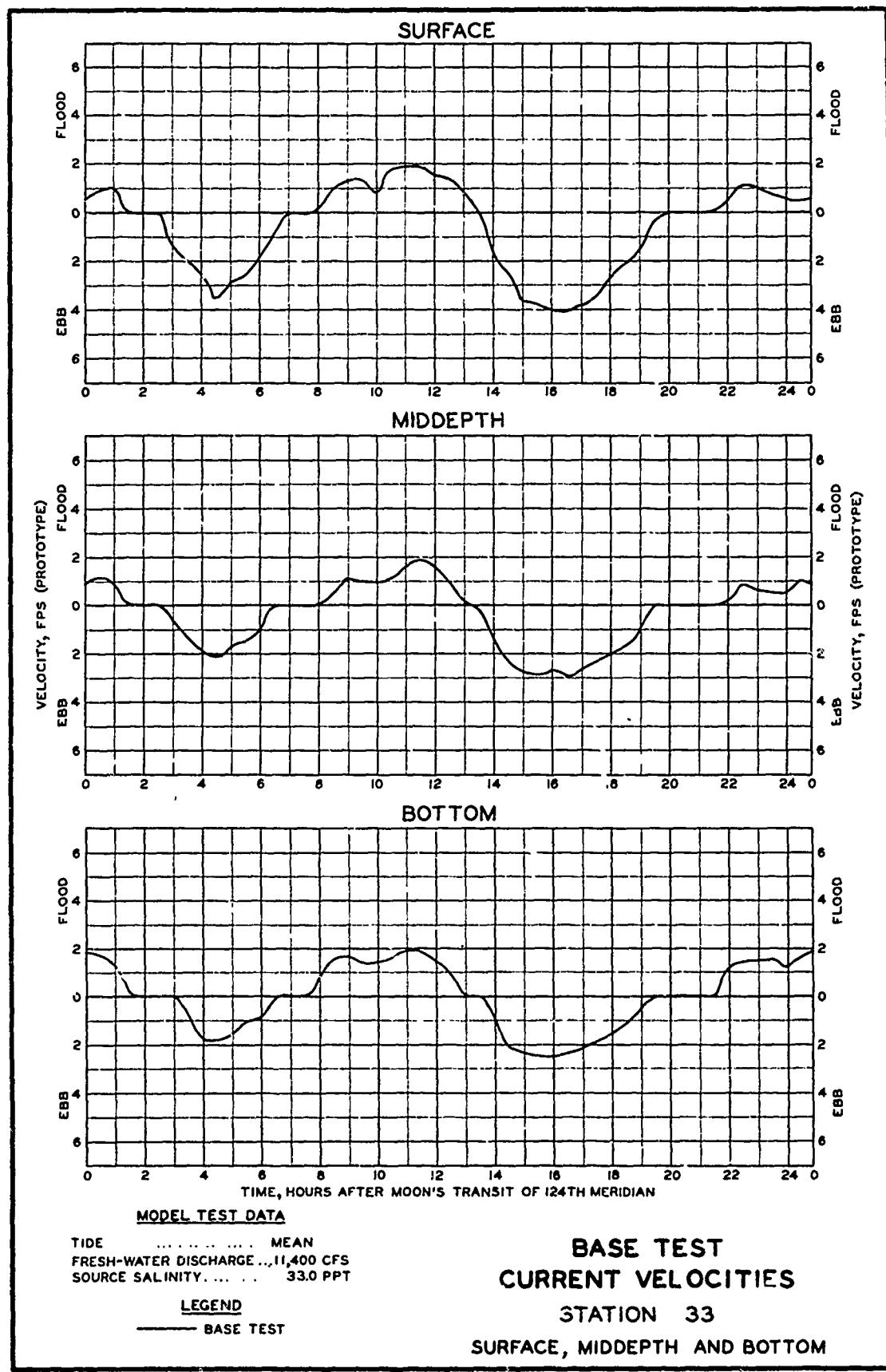
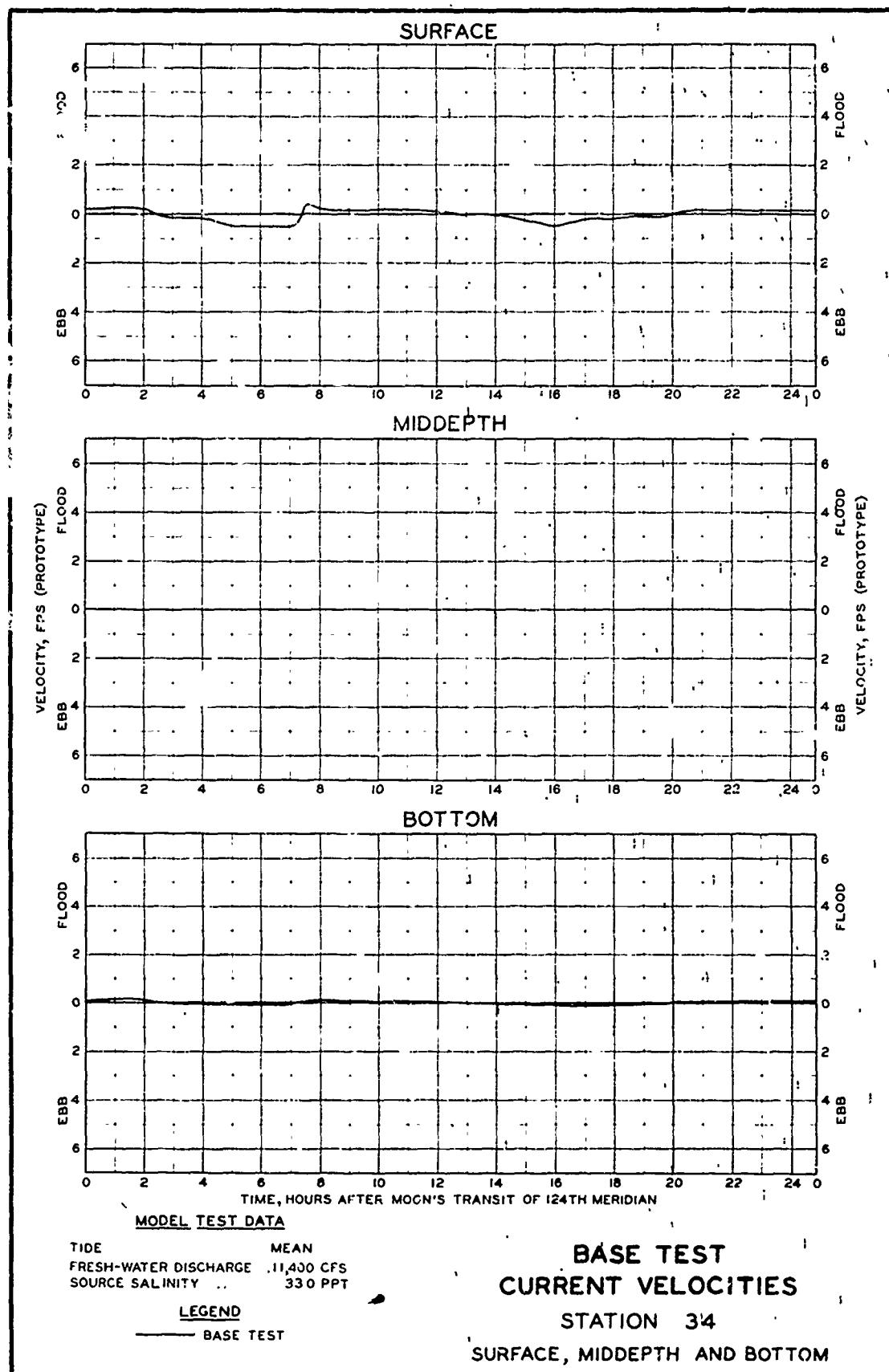
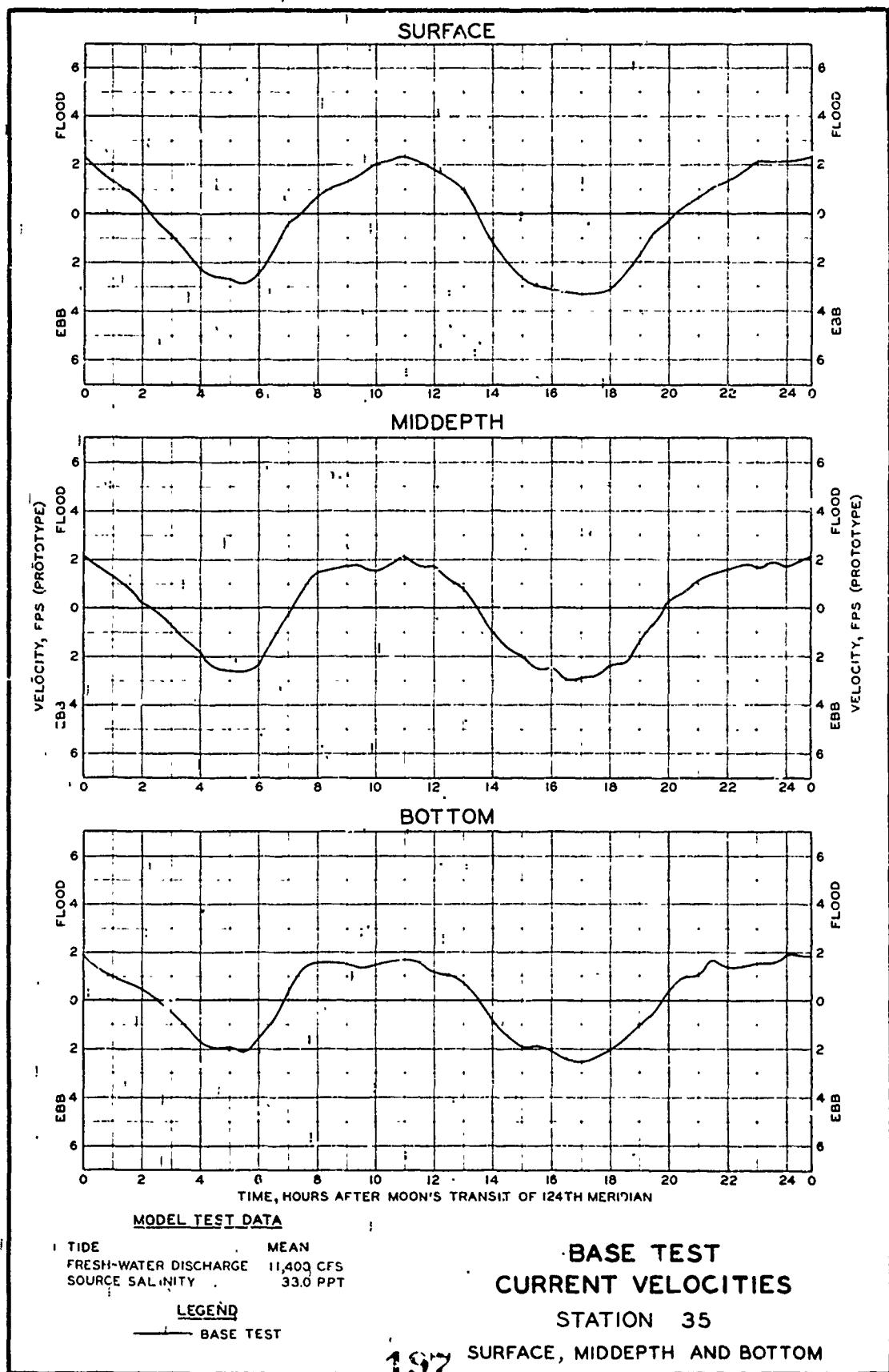
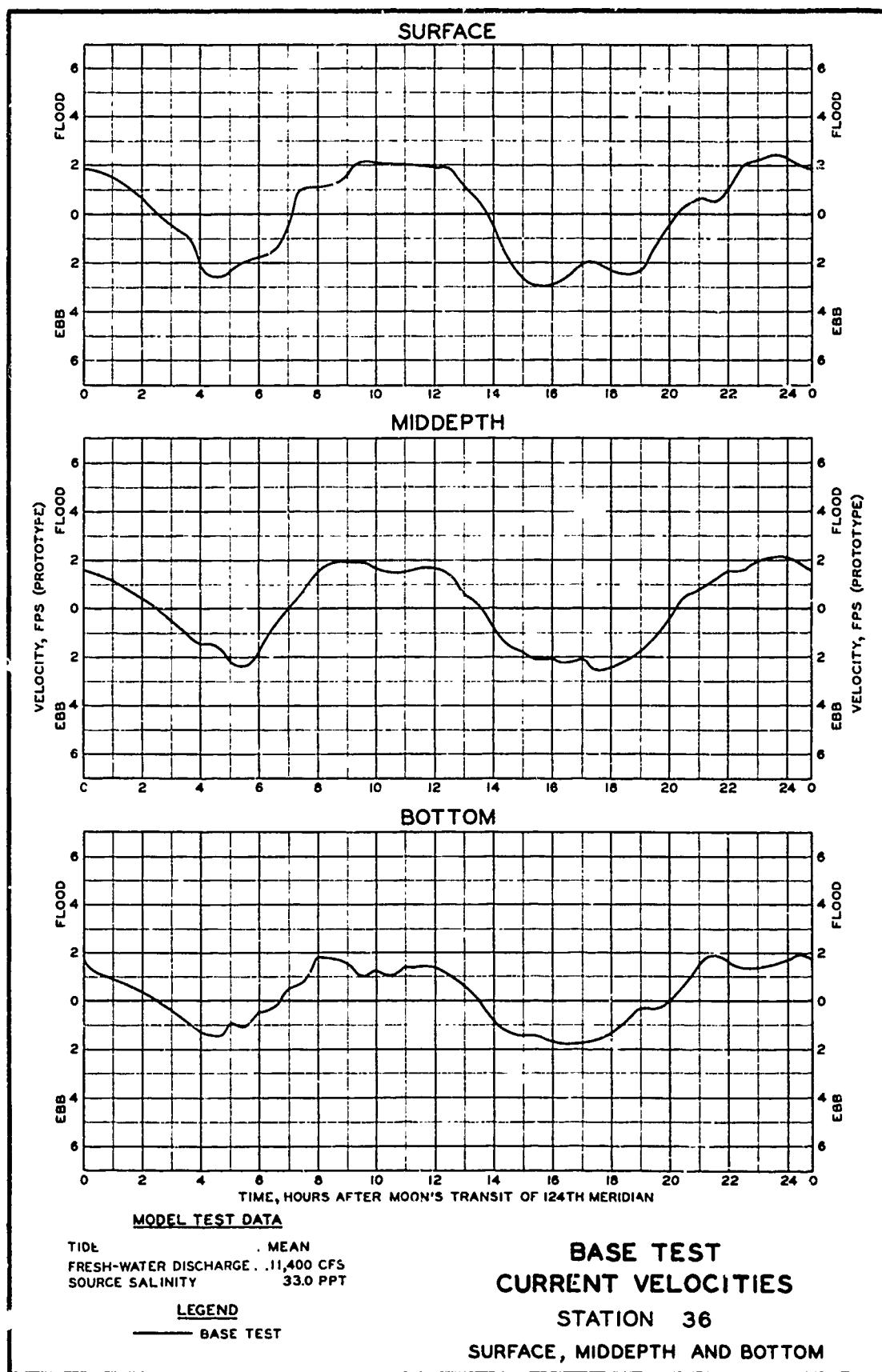
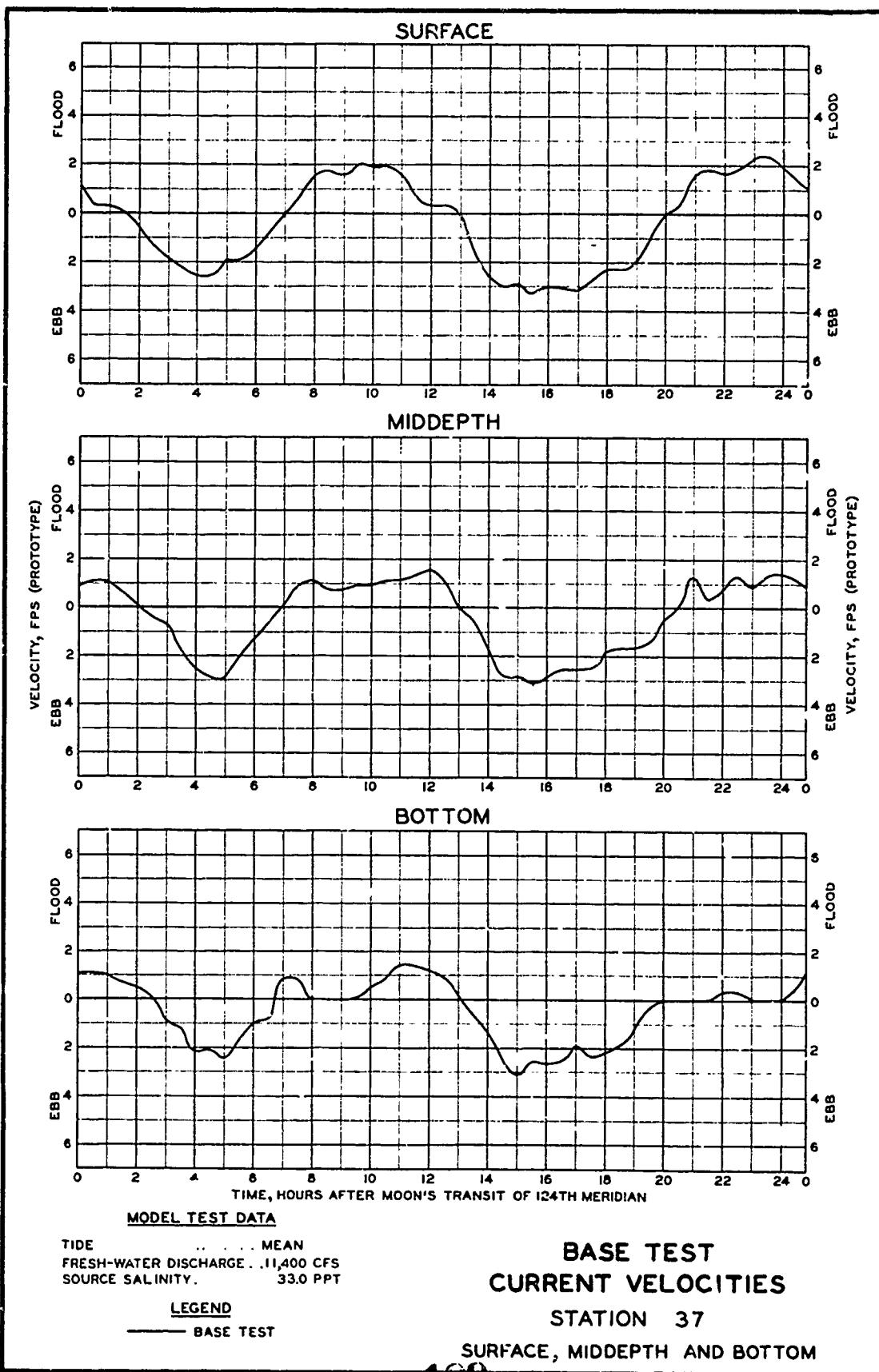


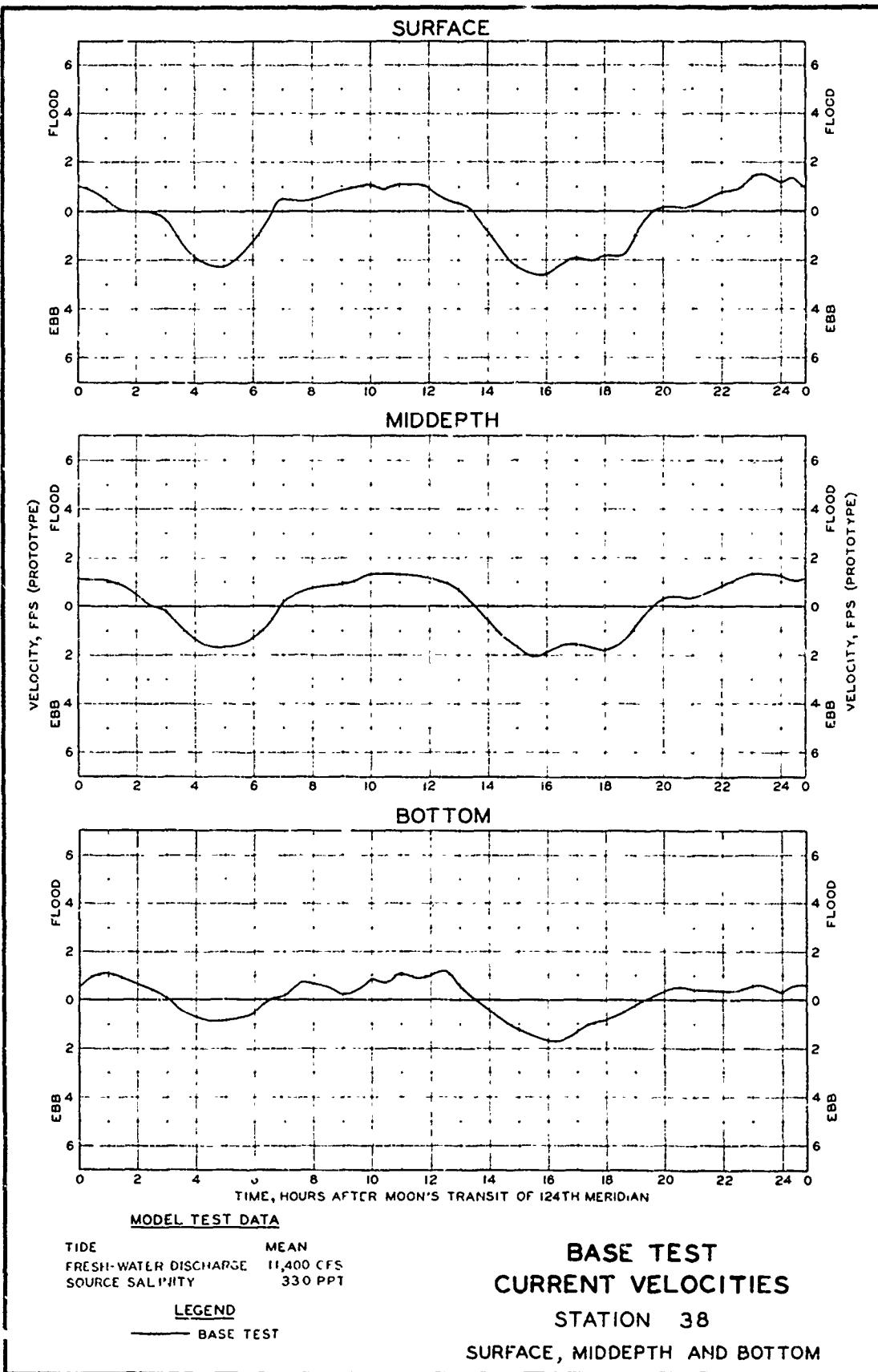
PLATE 131

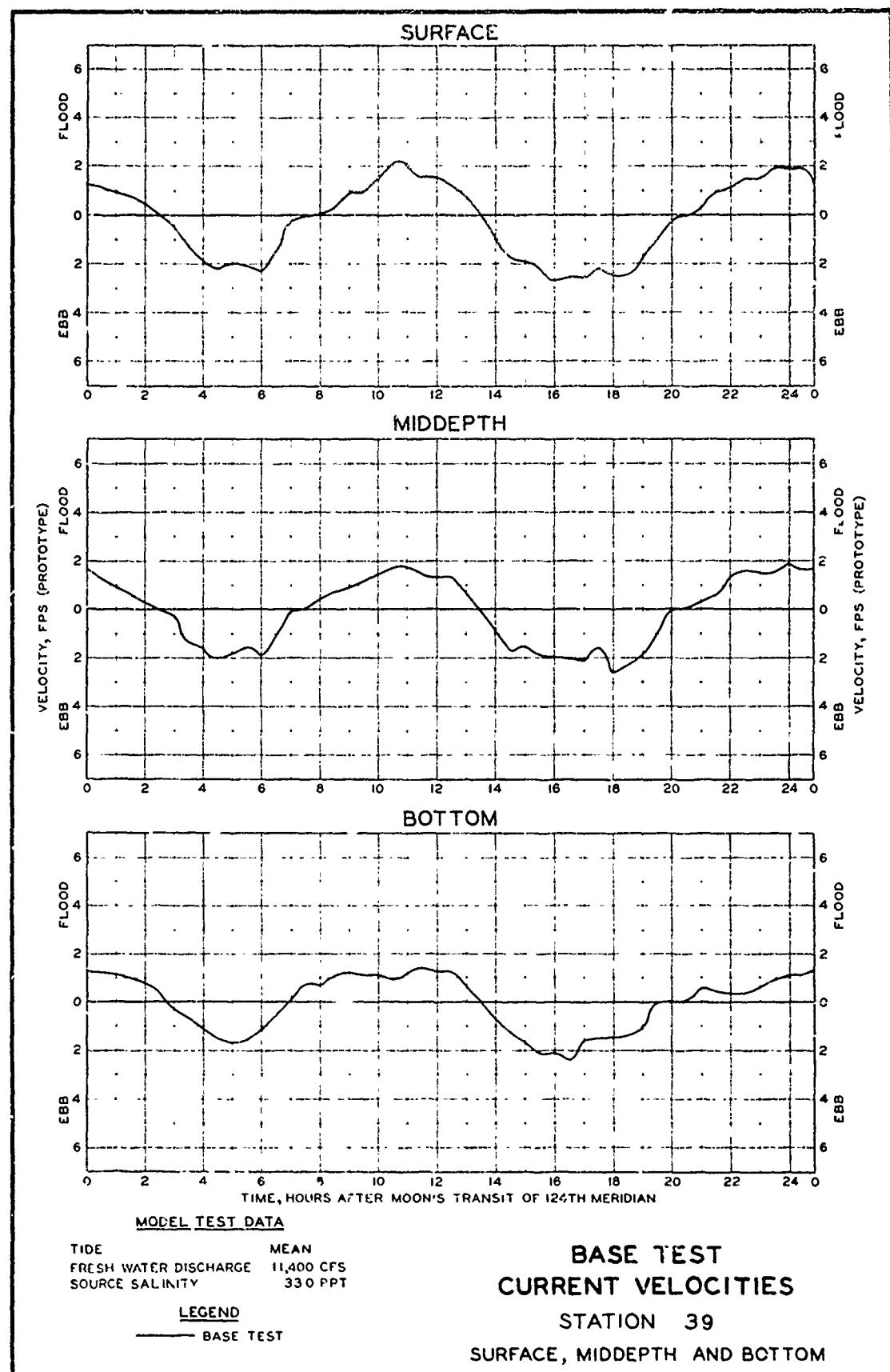


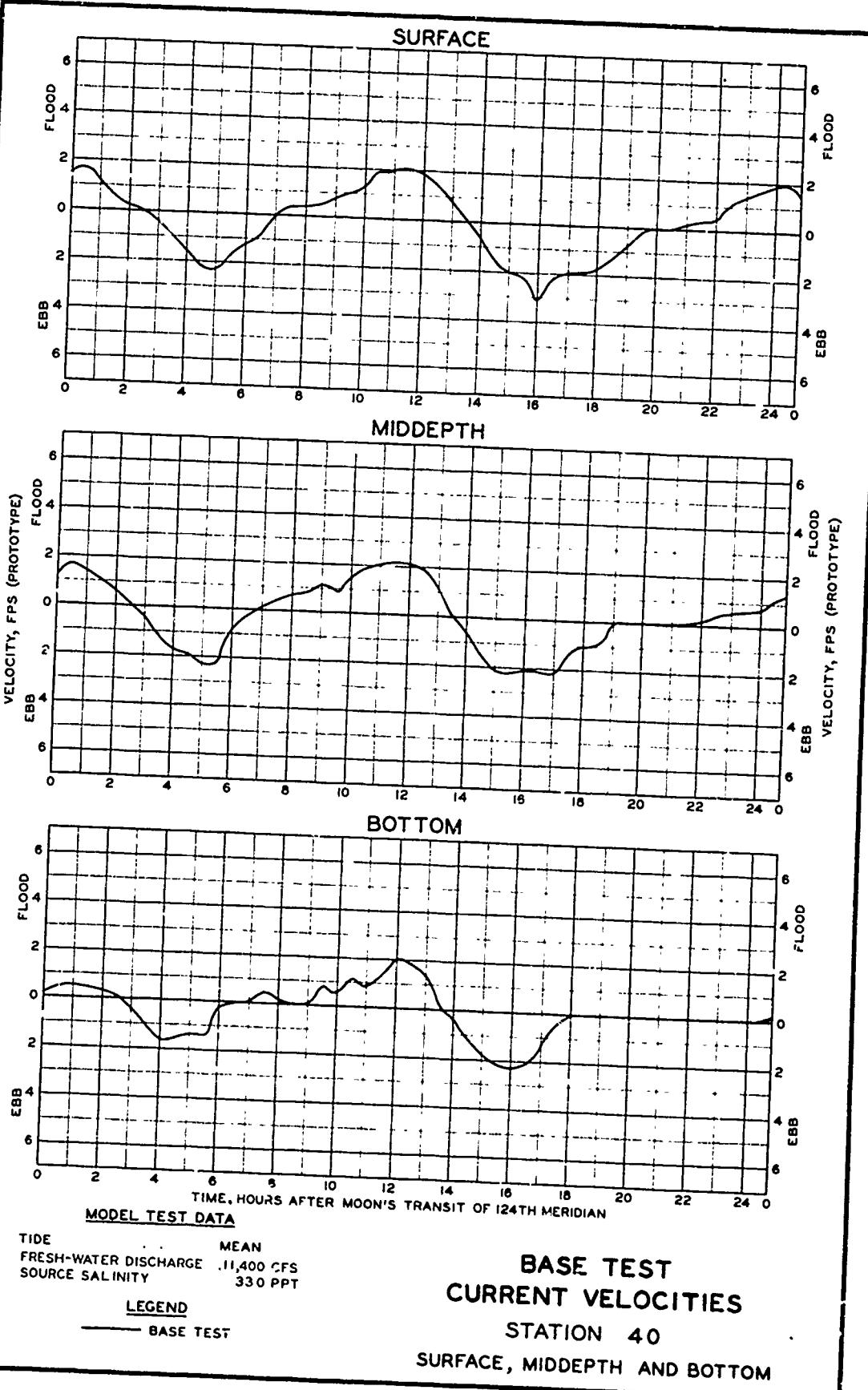


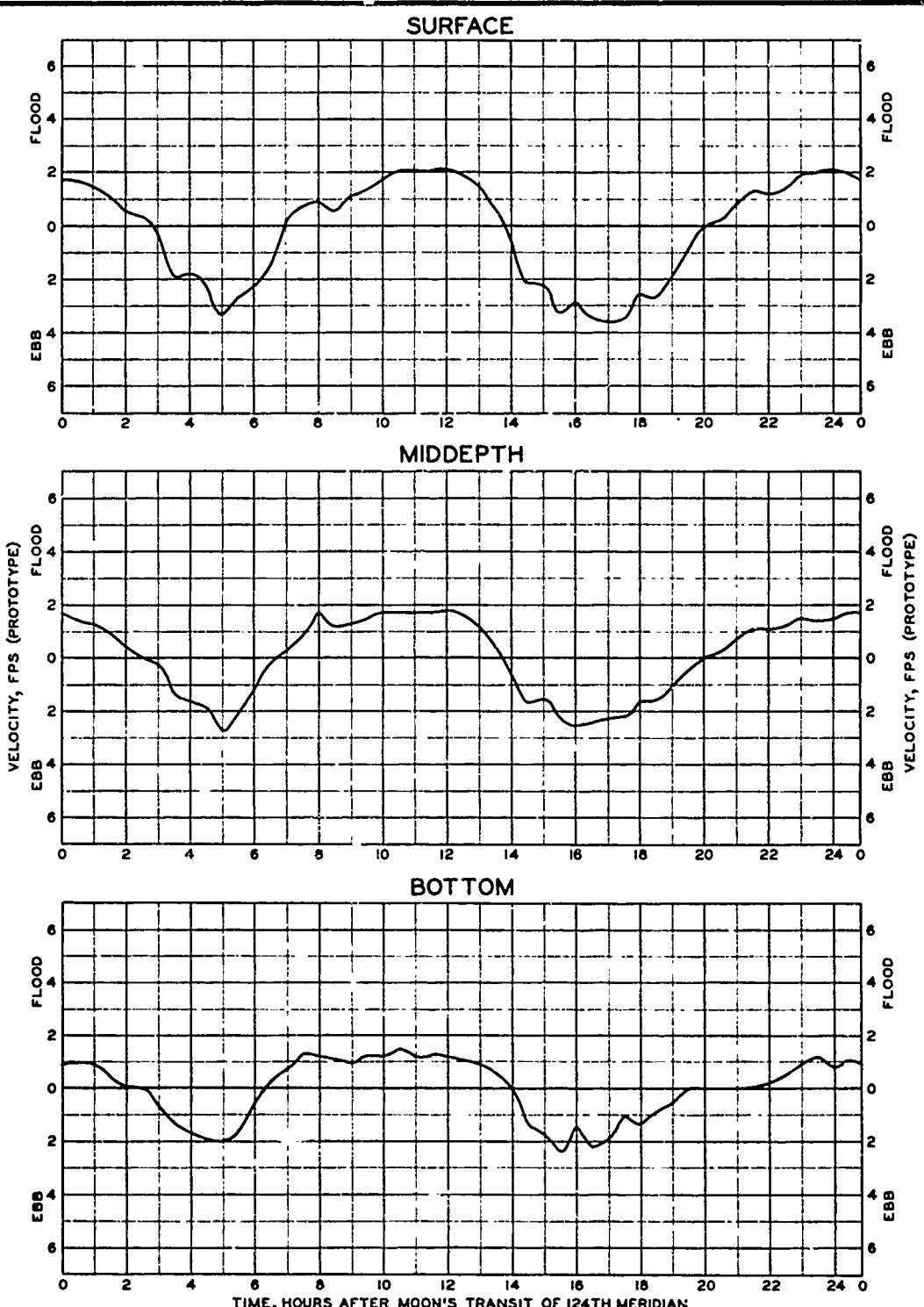












MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE . . 11,400 CFS
 SOURCE SALINITY . . 330 PPT

BASE TEST
CURRENT VELOCITIES

STATION 41

2/17/63 SURFACE, MIDDEPTH AND BOTTOM

LEGEND
 — BASE TEST

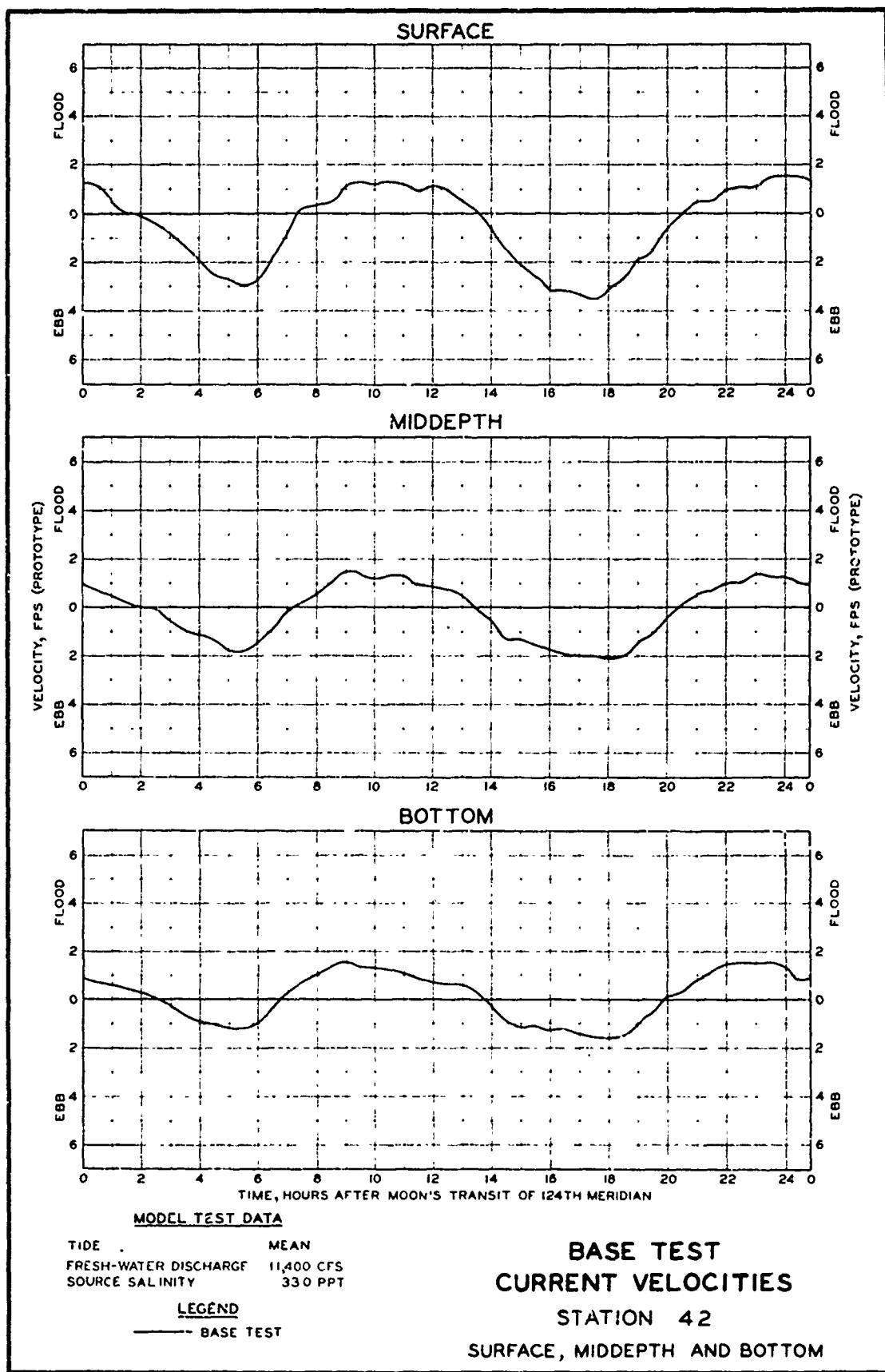
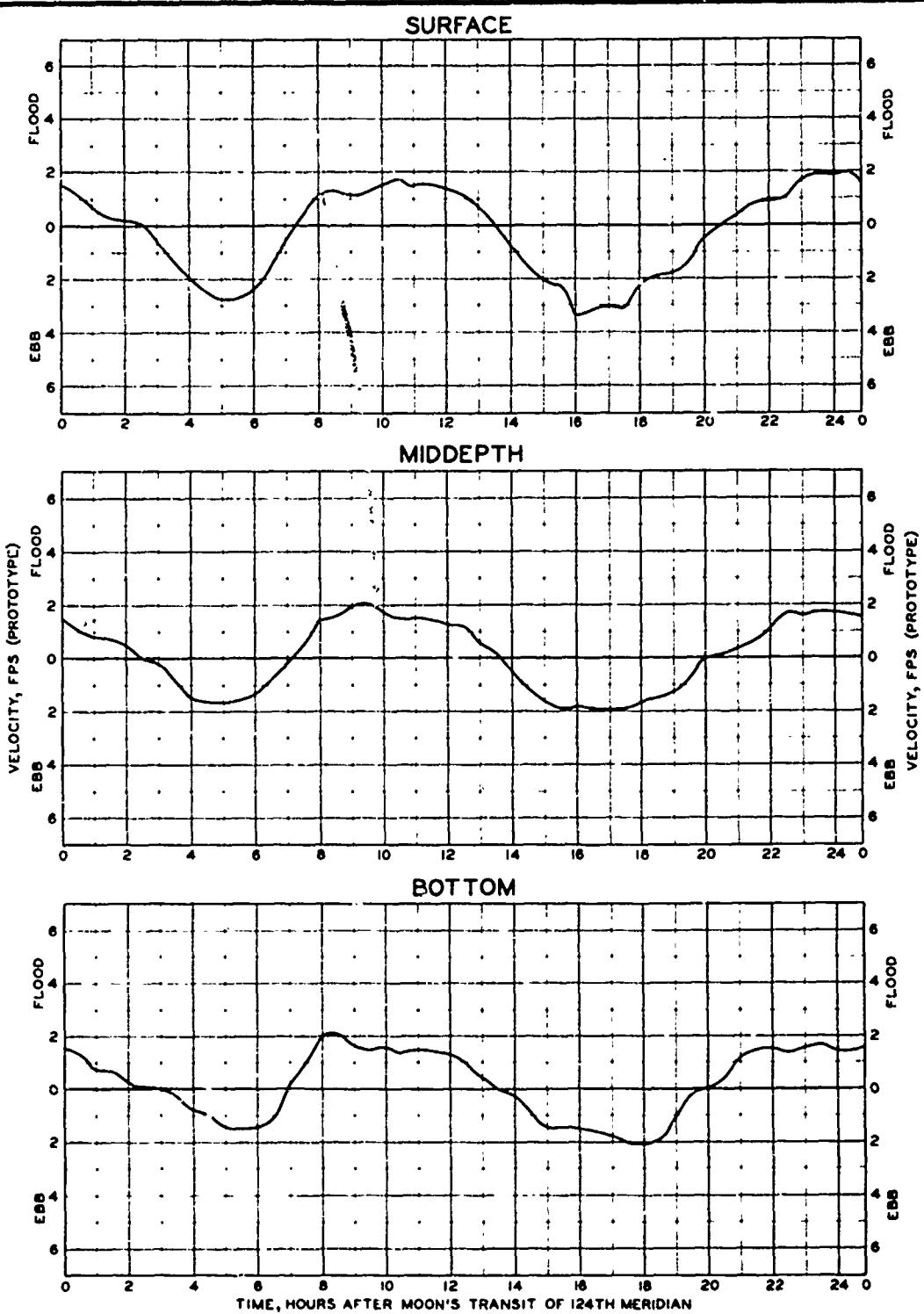


PLATE 140

204



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 33.0 PPT

LEGEND

— BASE TEST

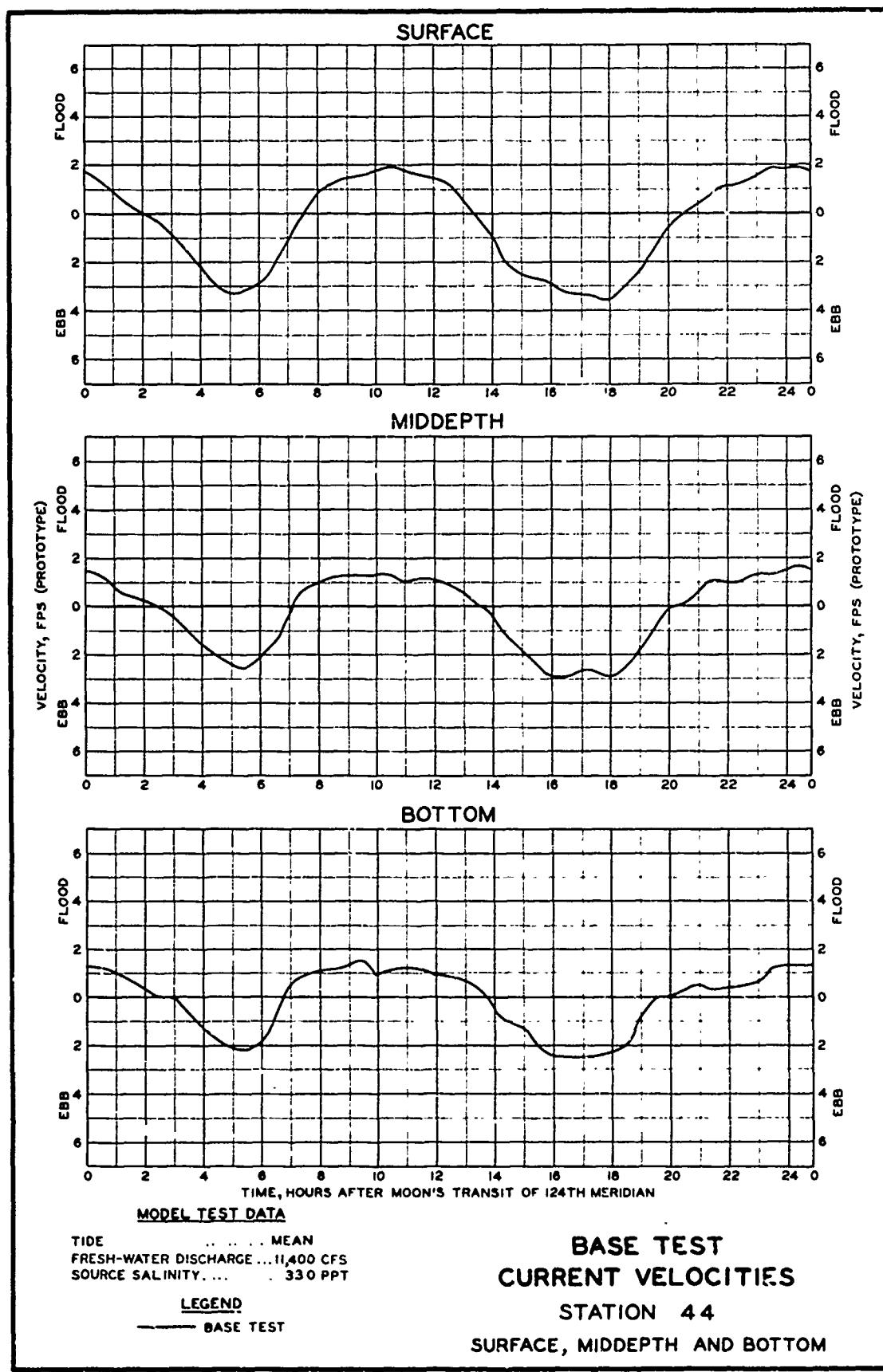
**BASE TEST
CURRENT VELOCITIES**

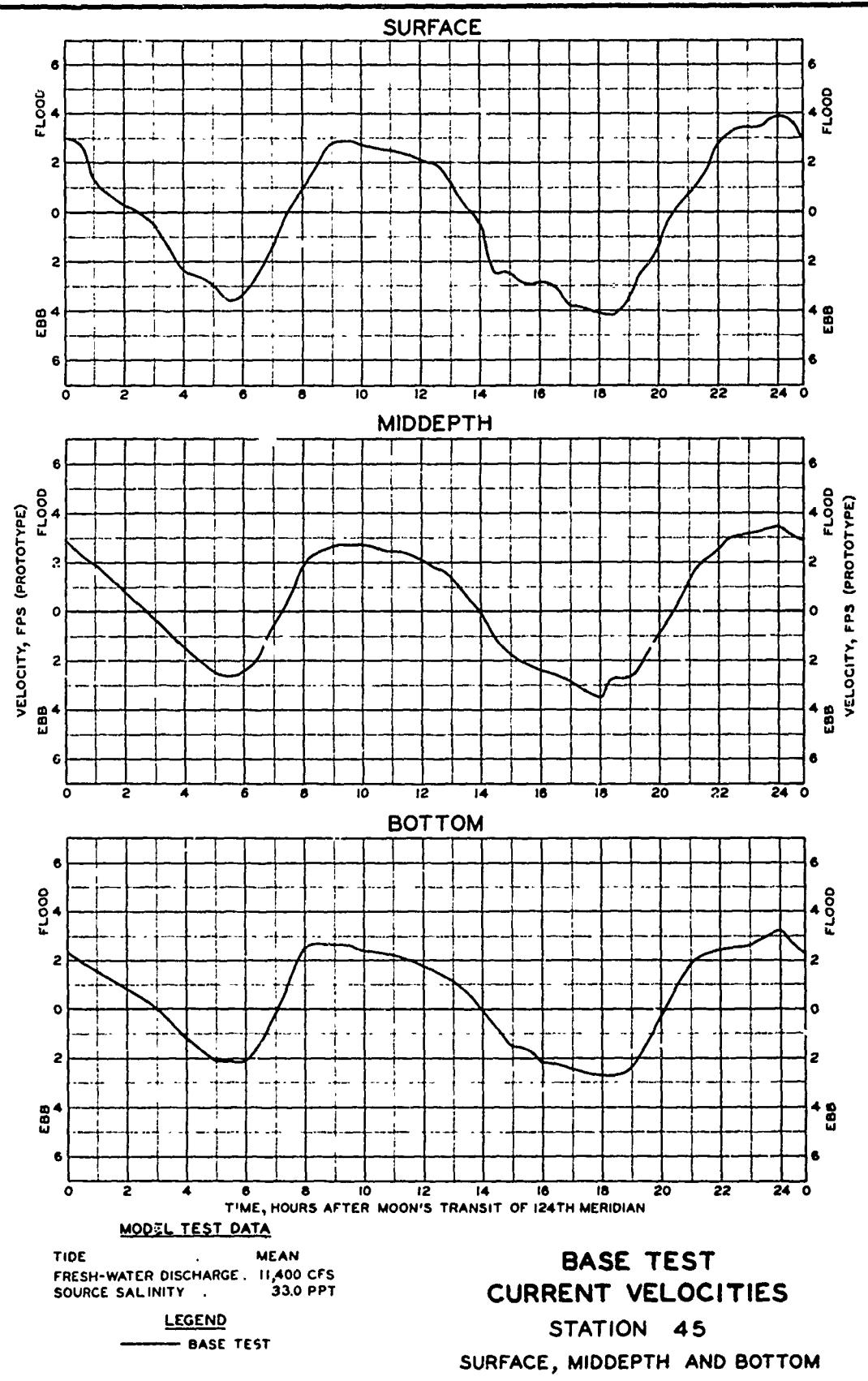
STATION 43

SURFACE, MIDDEPTH AND BOTTOM

205

PLATE 141





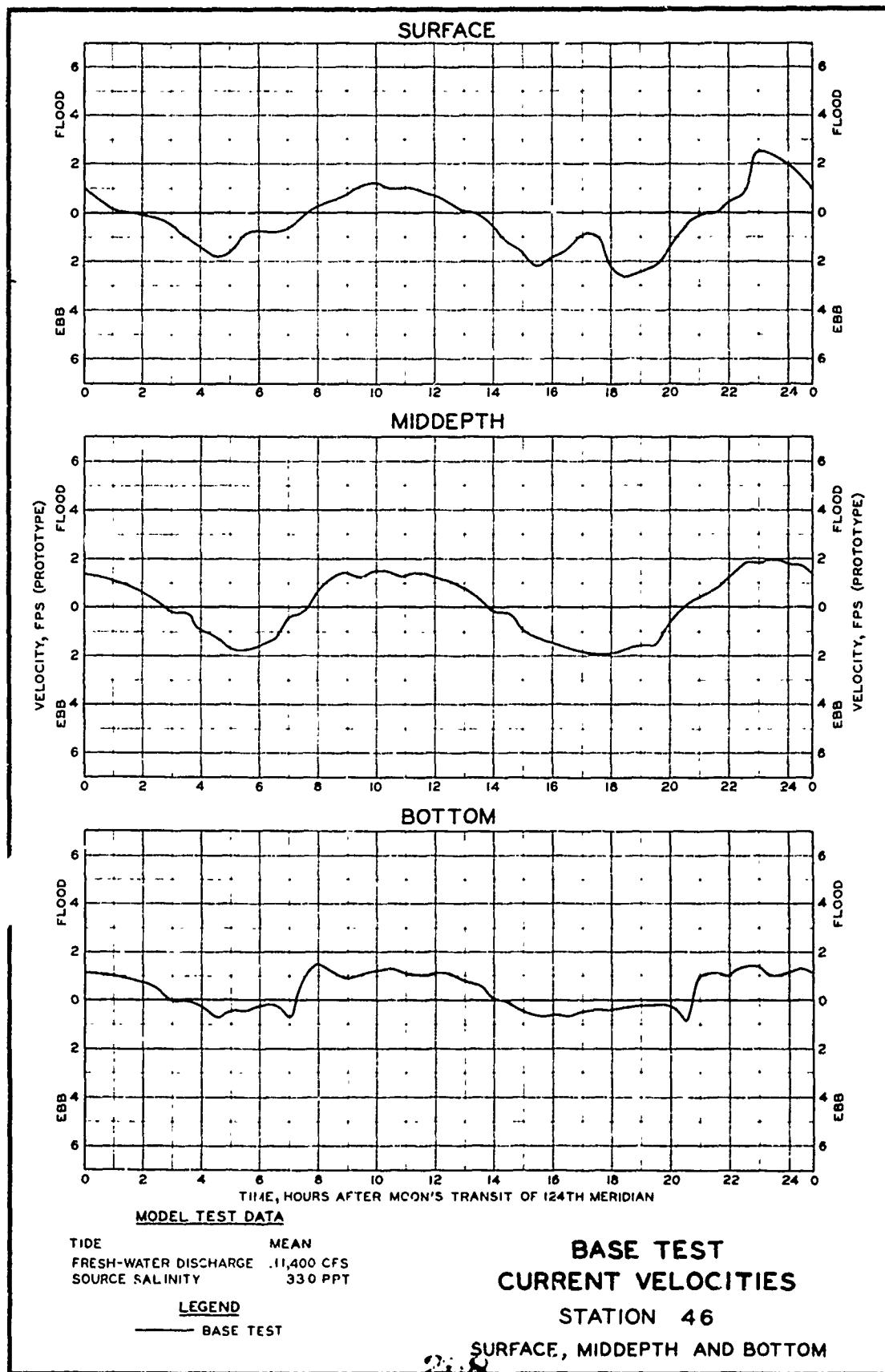
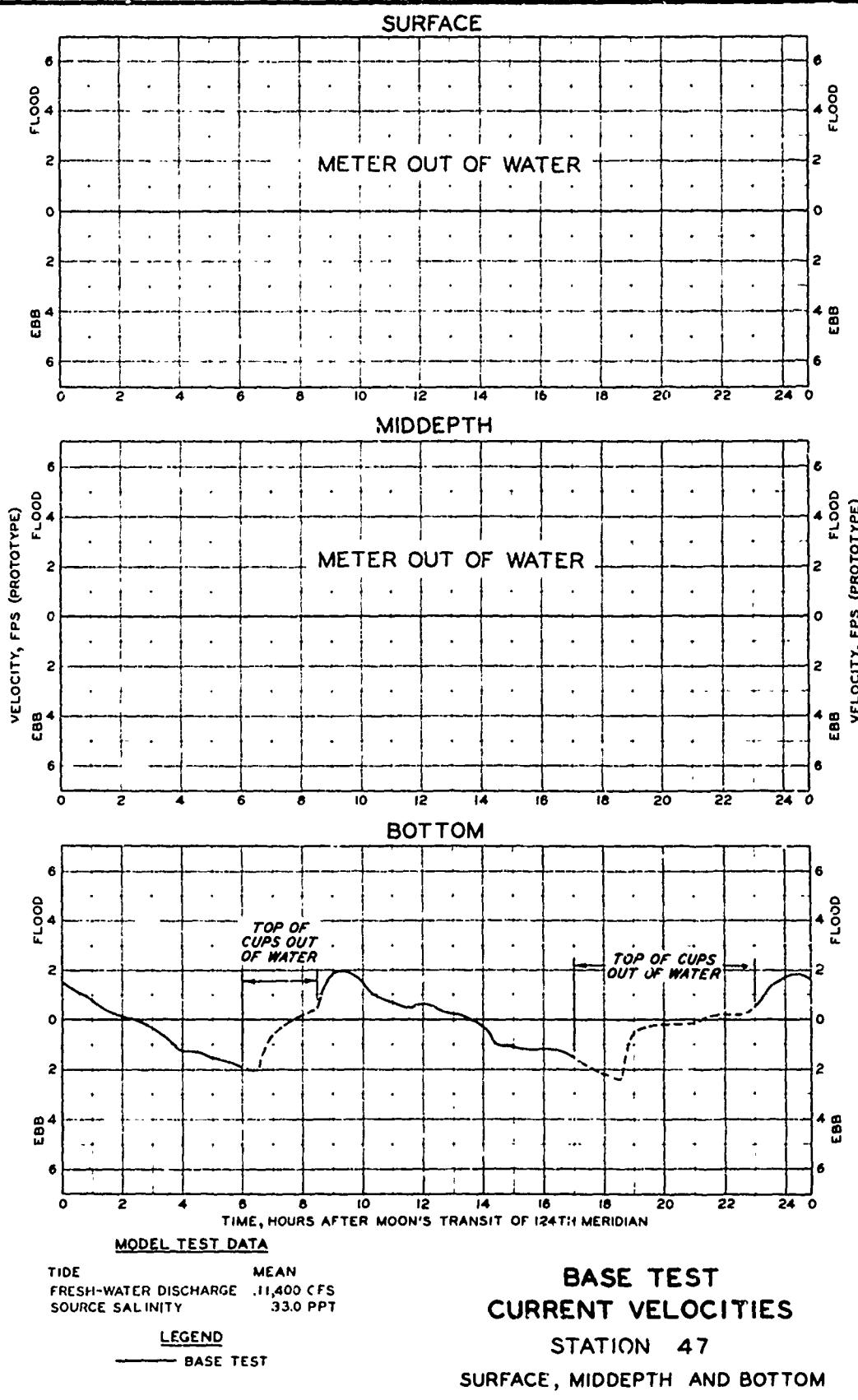
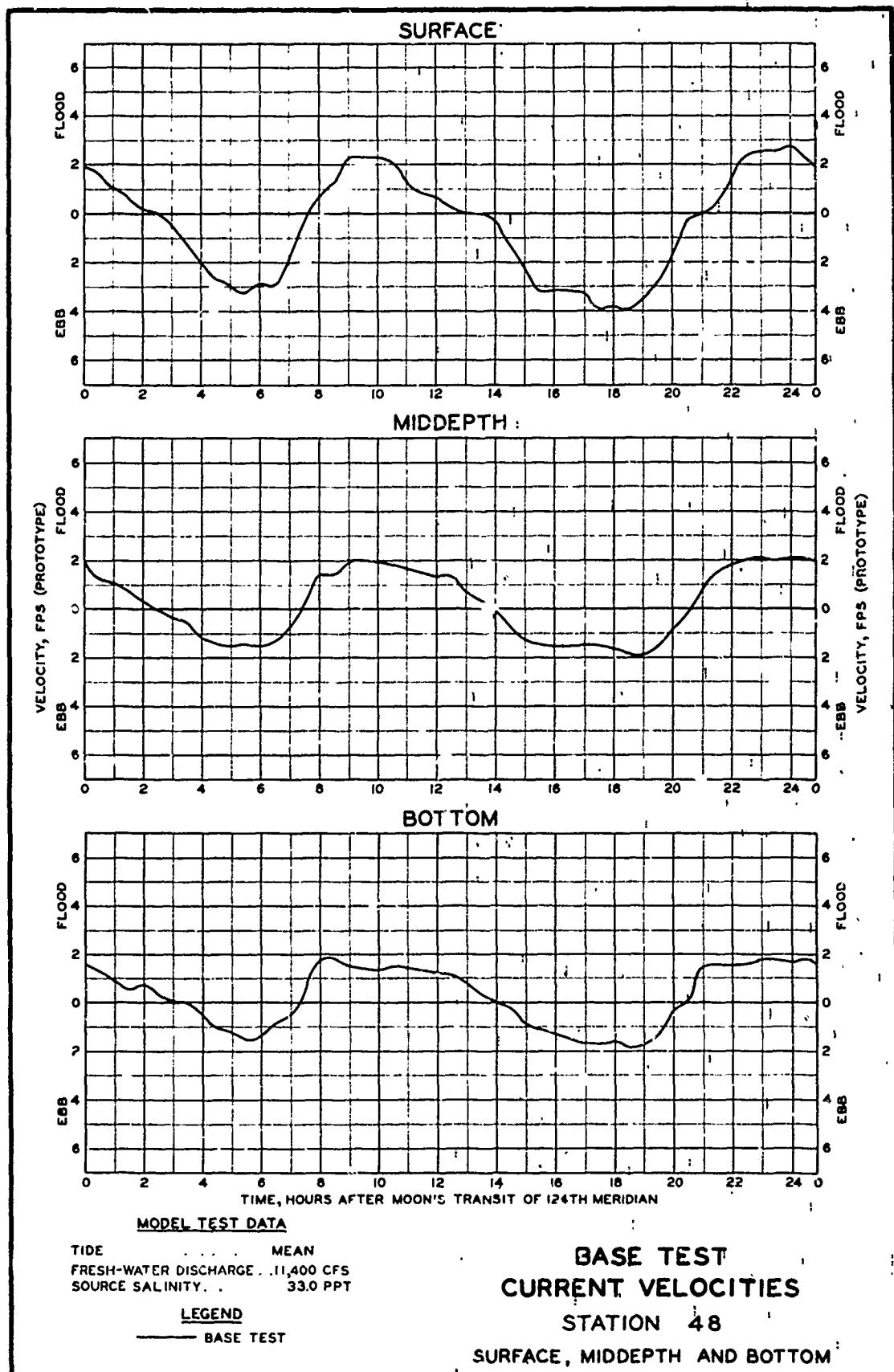
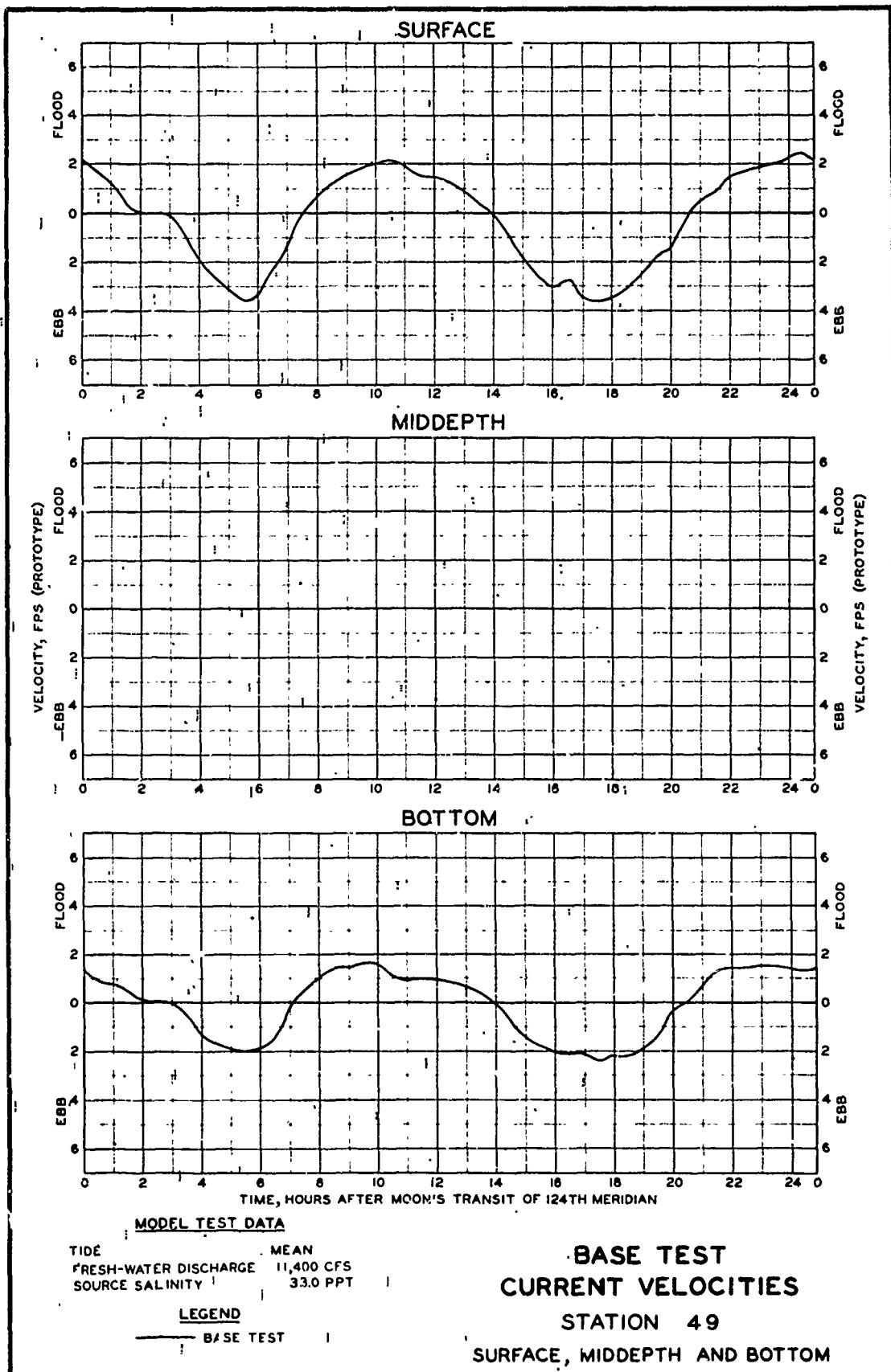


PLATE 144







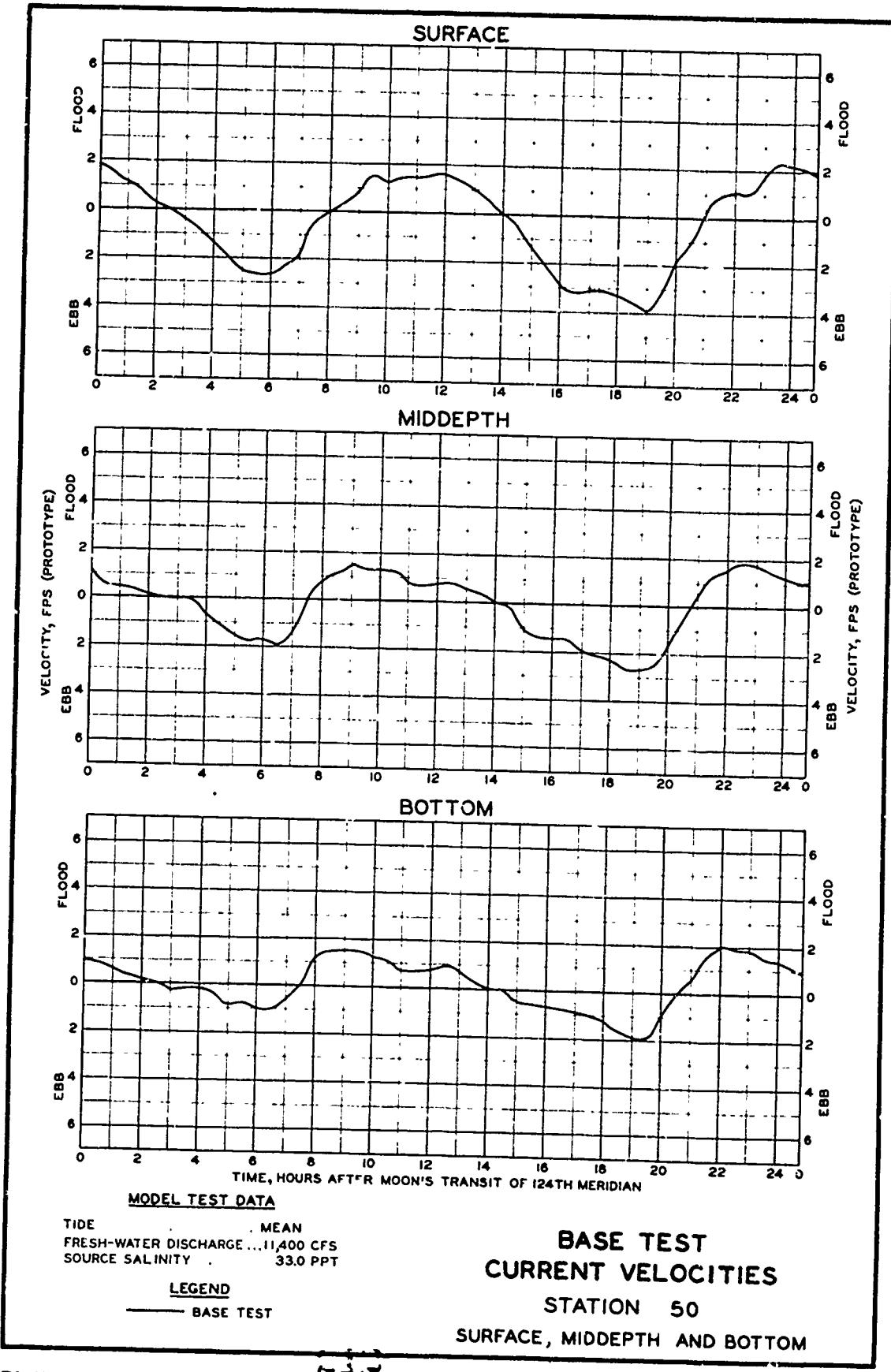
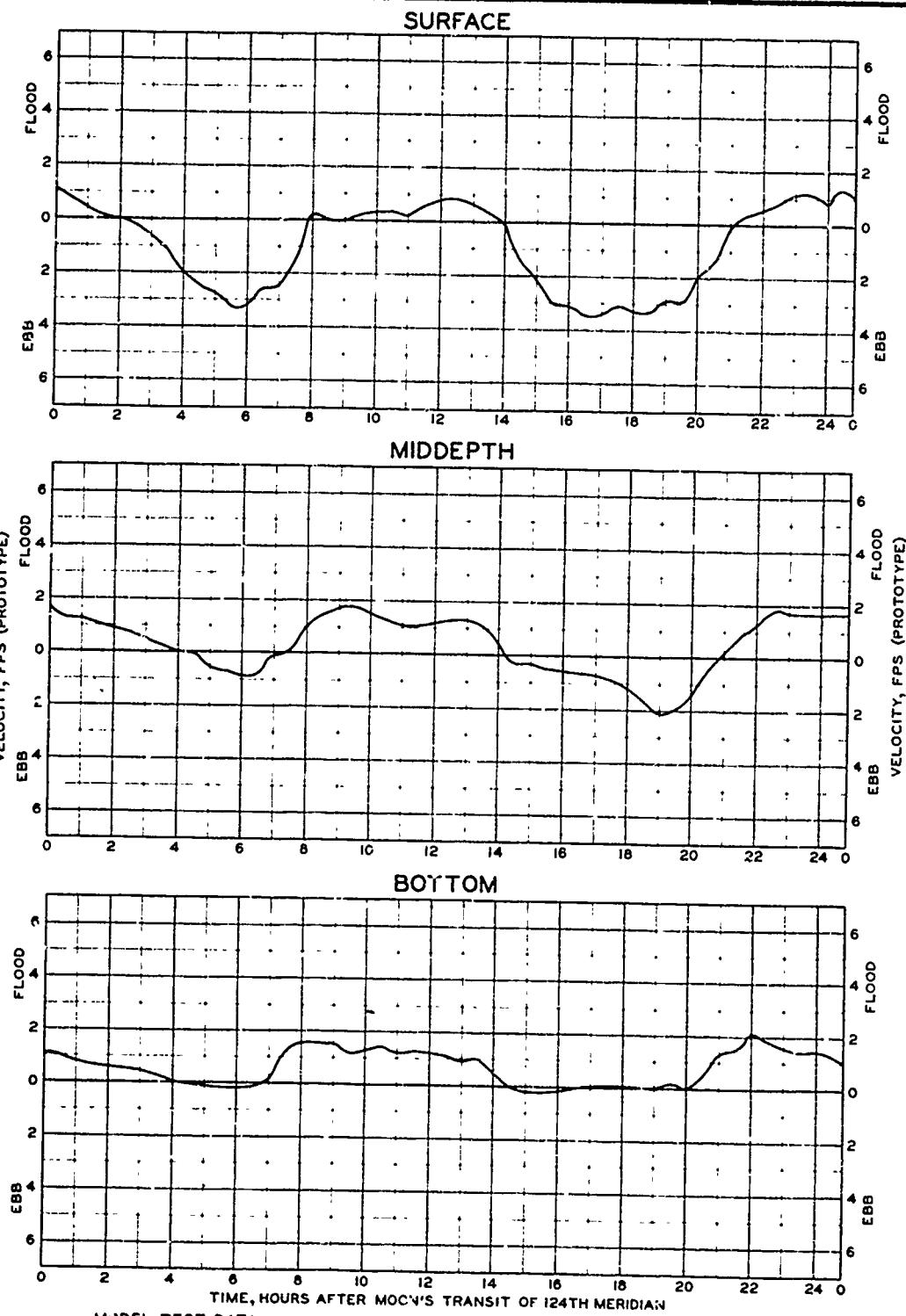


PLATE 148



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE .11,400 CFS
SOURCE SALINITY . 33.0 PPT

LEGEND
— BASE TEST

BASE TEST
CURRENT VELOCITIES

STATION 51

SURFACE, MIDDEPTH AND BOTTOM

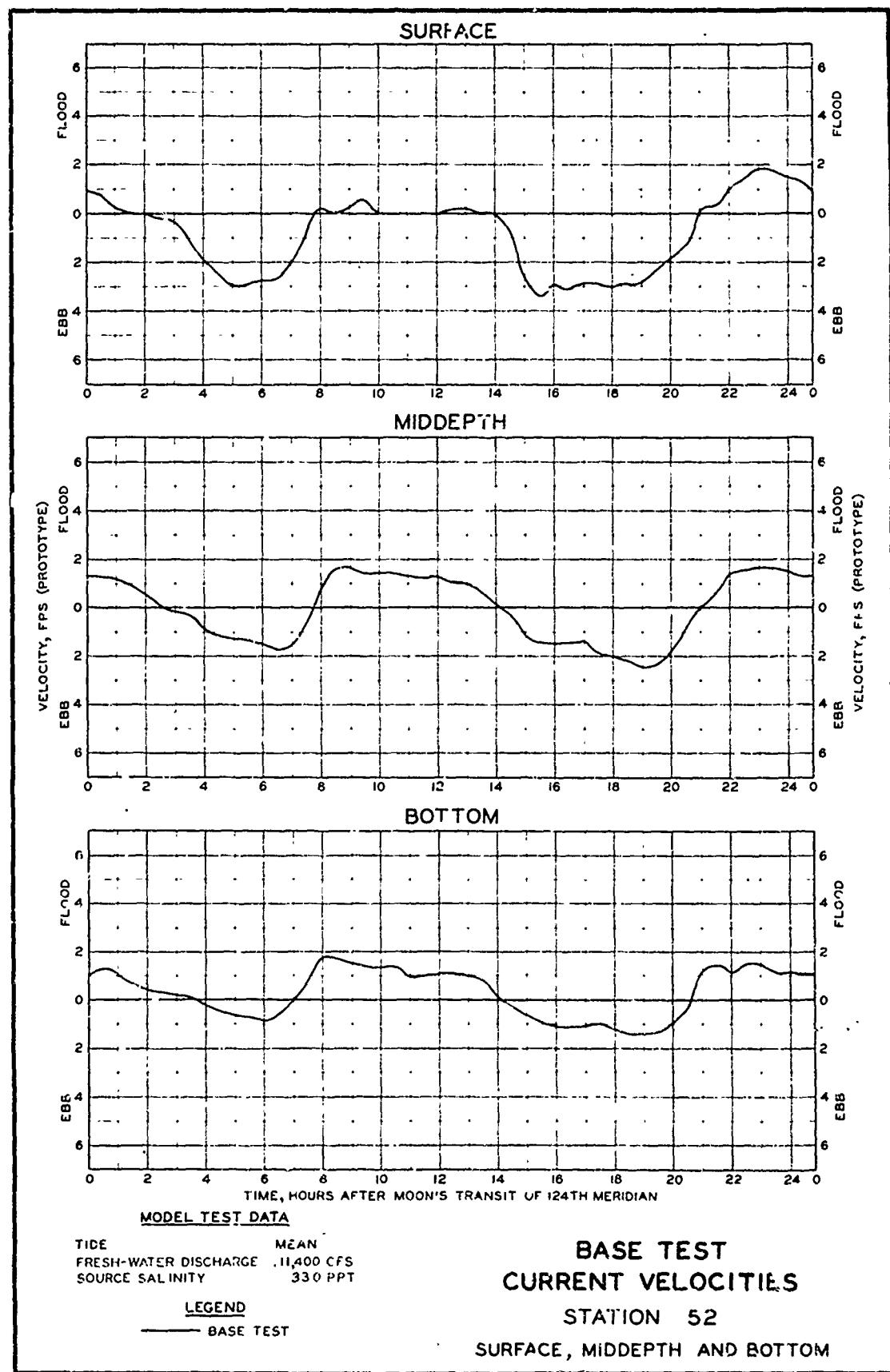
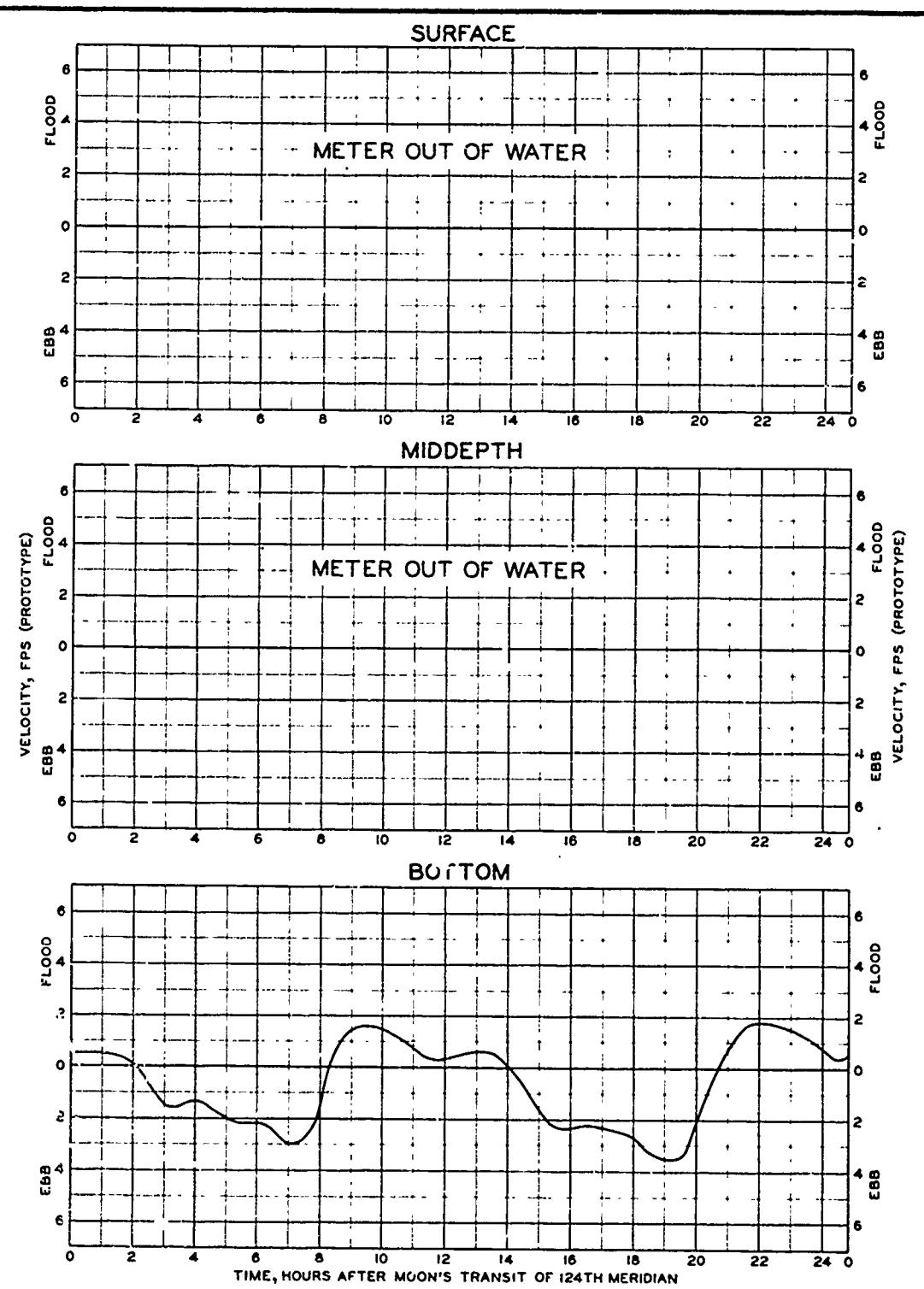
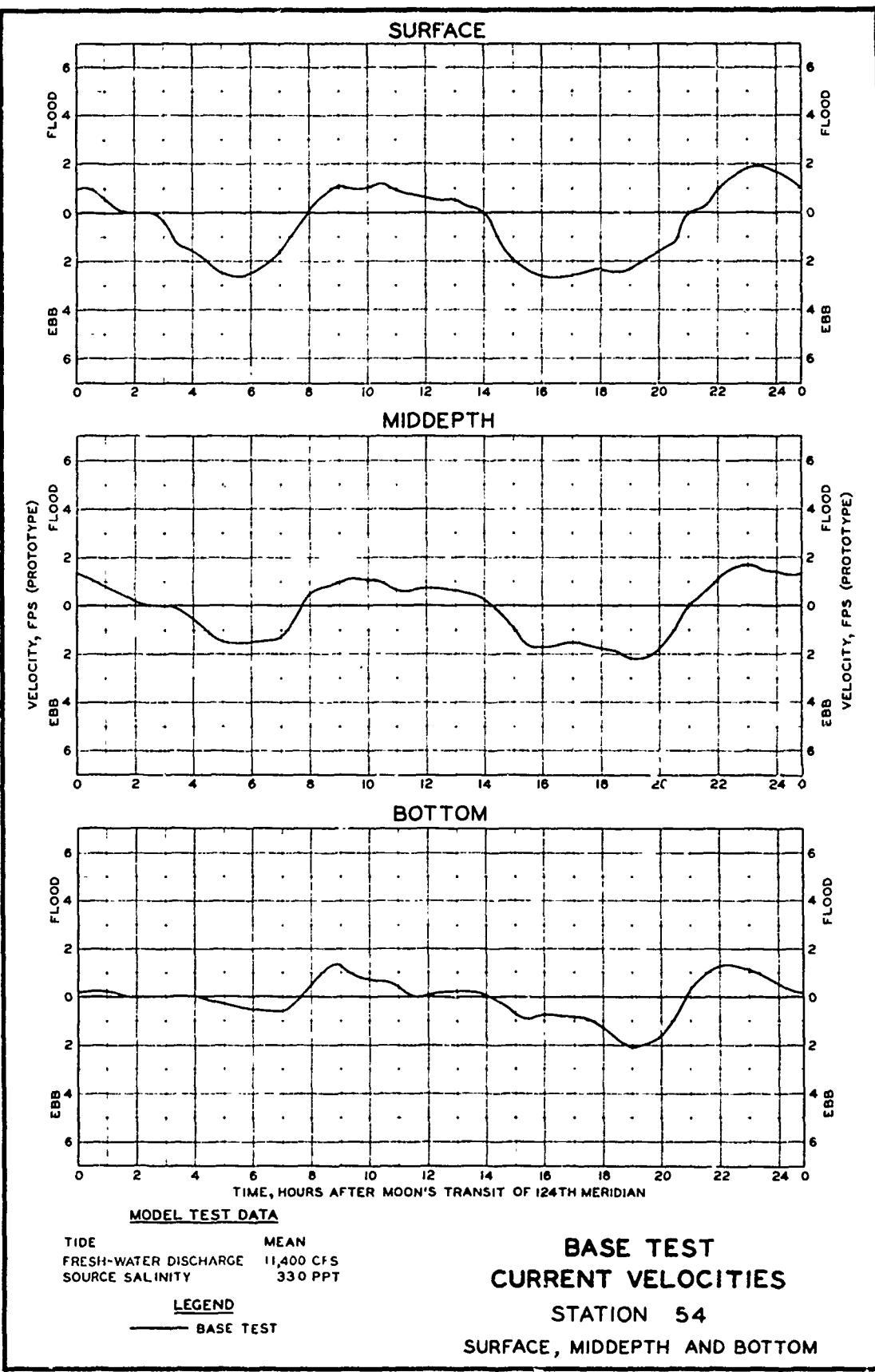
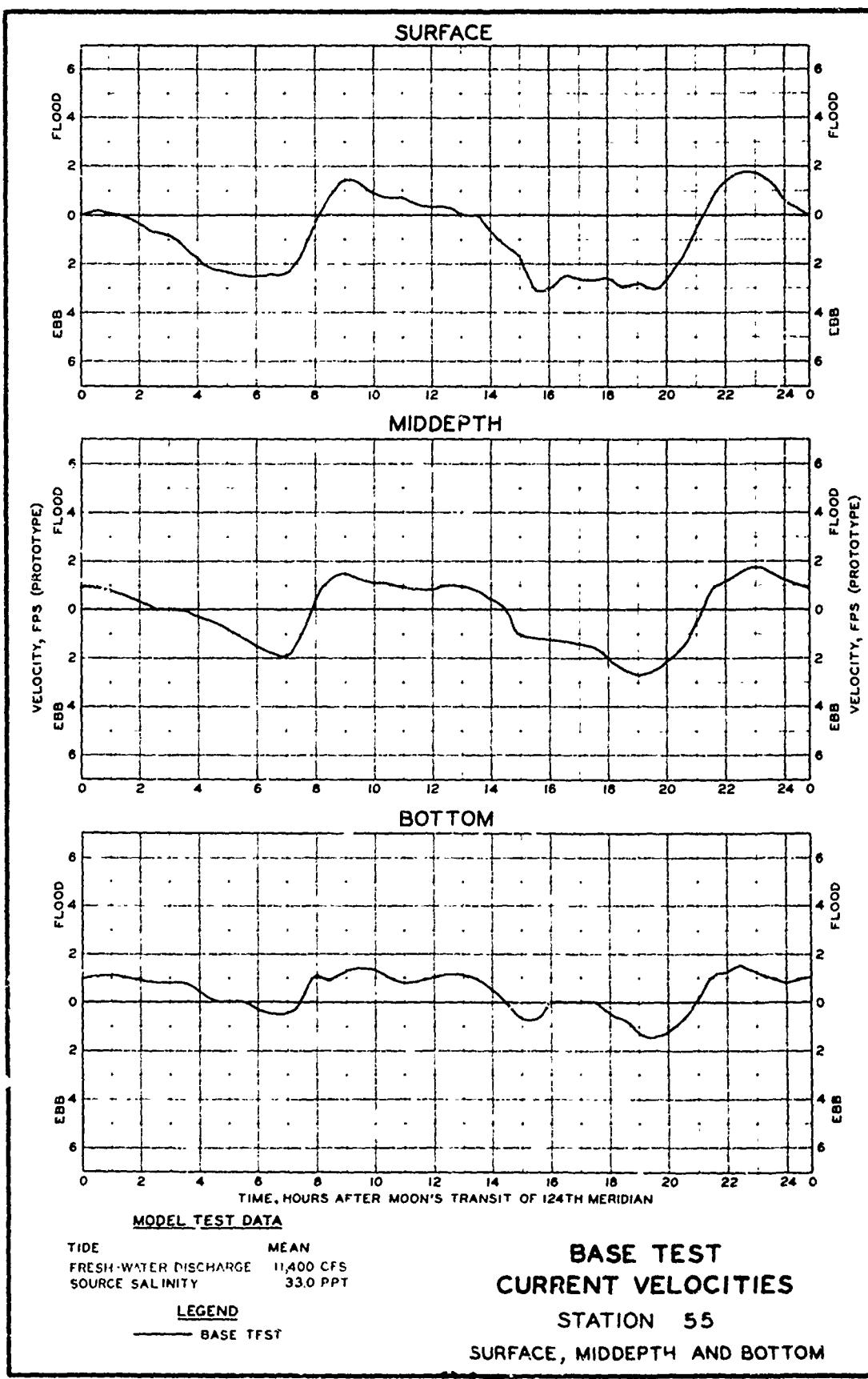
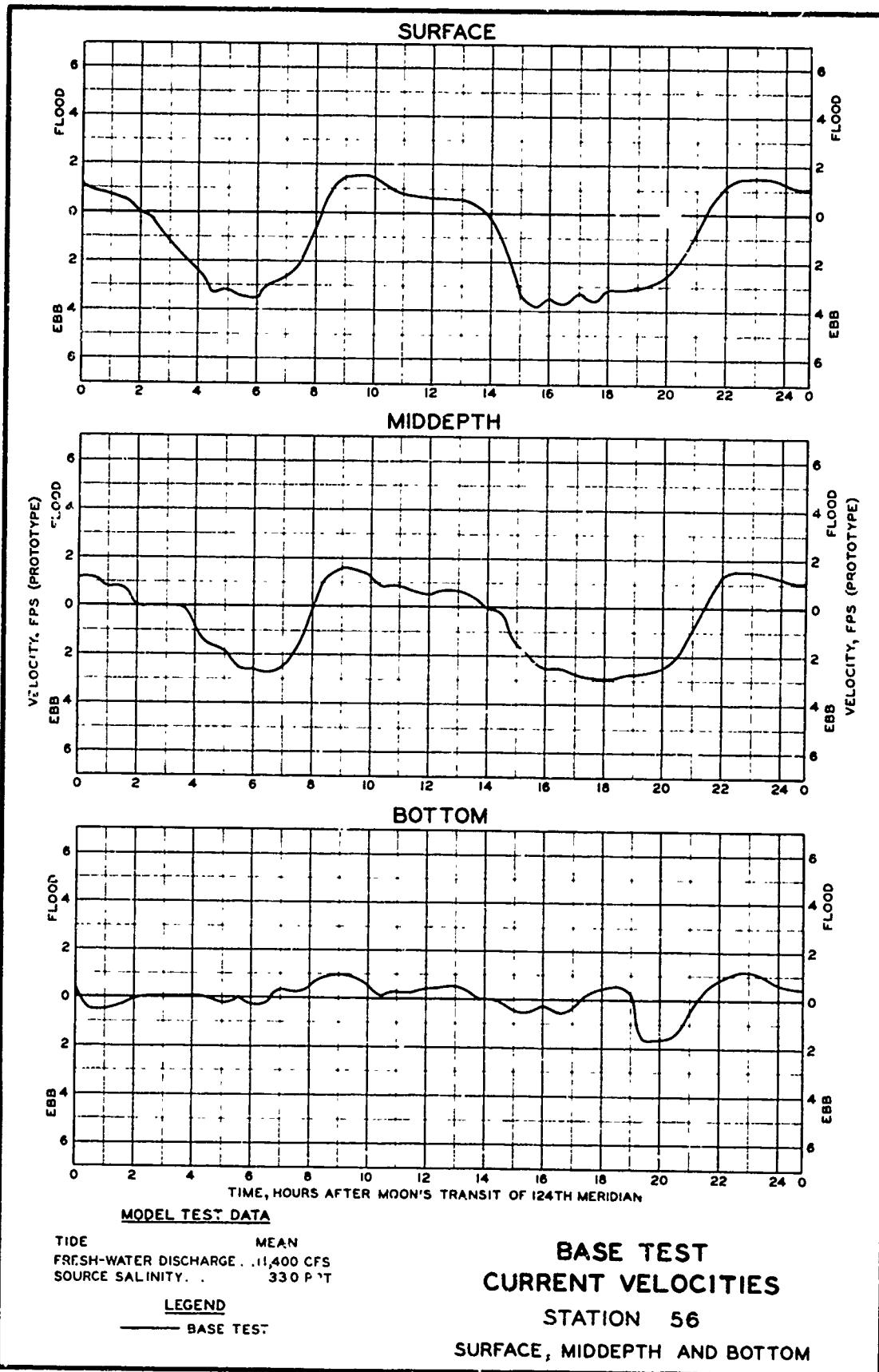


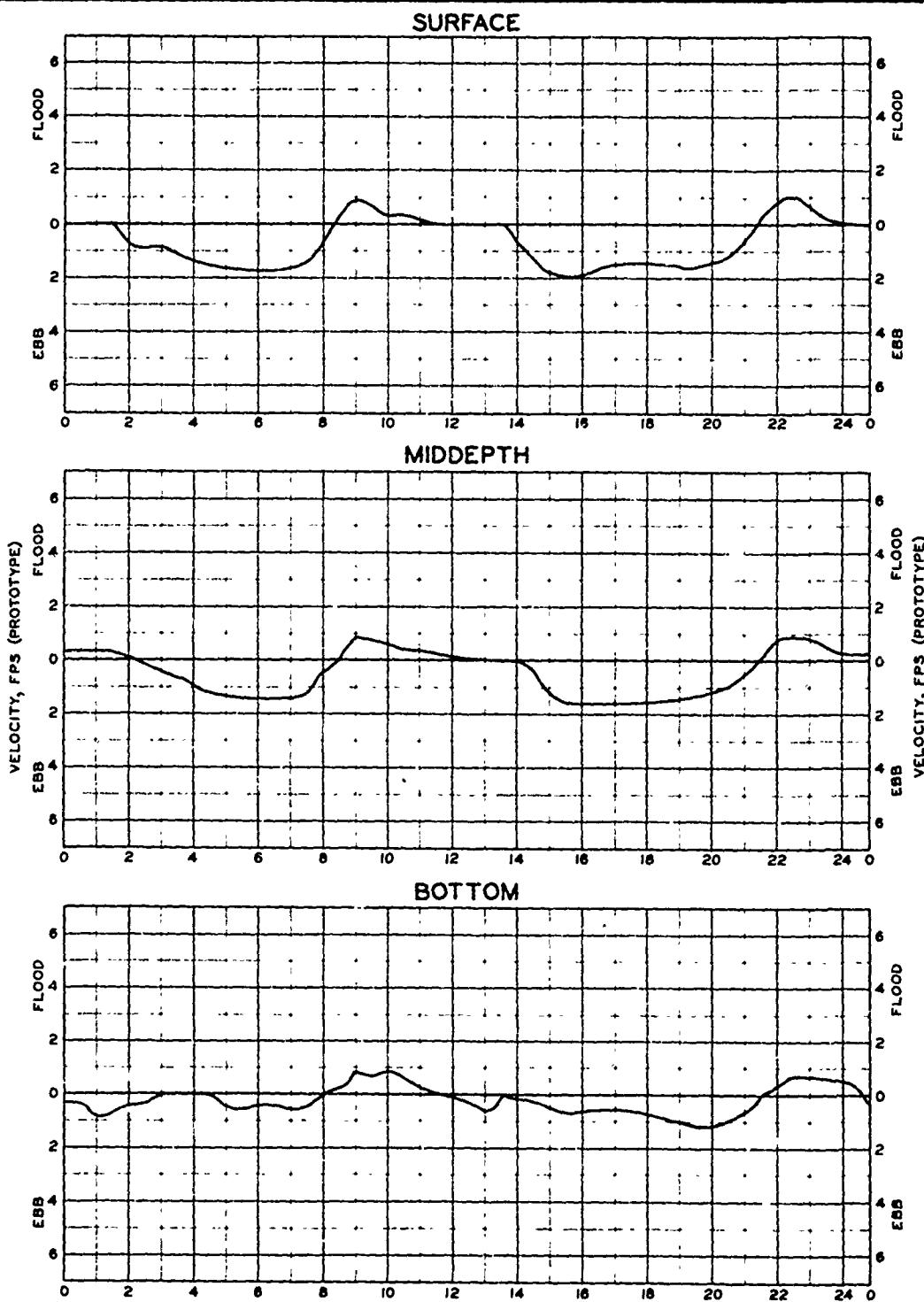
PLATE 150











MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE . . . 11,400 CFS
SOURCE SALINITY . . . 330 PPT

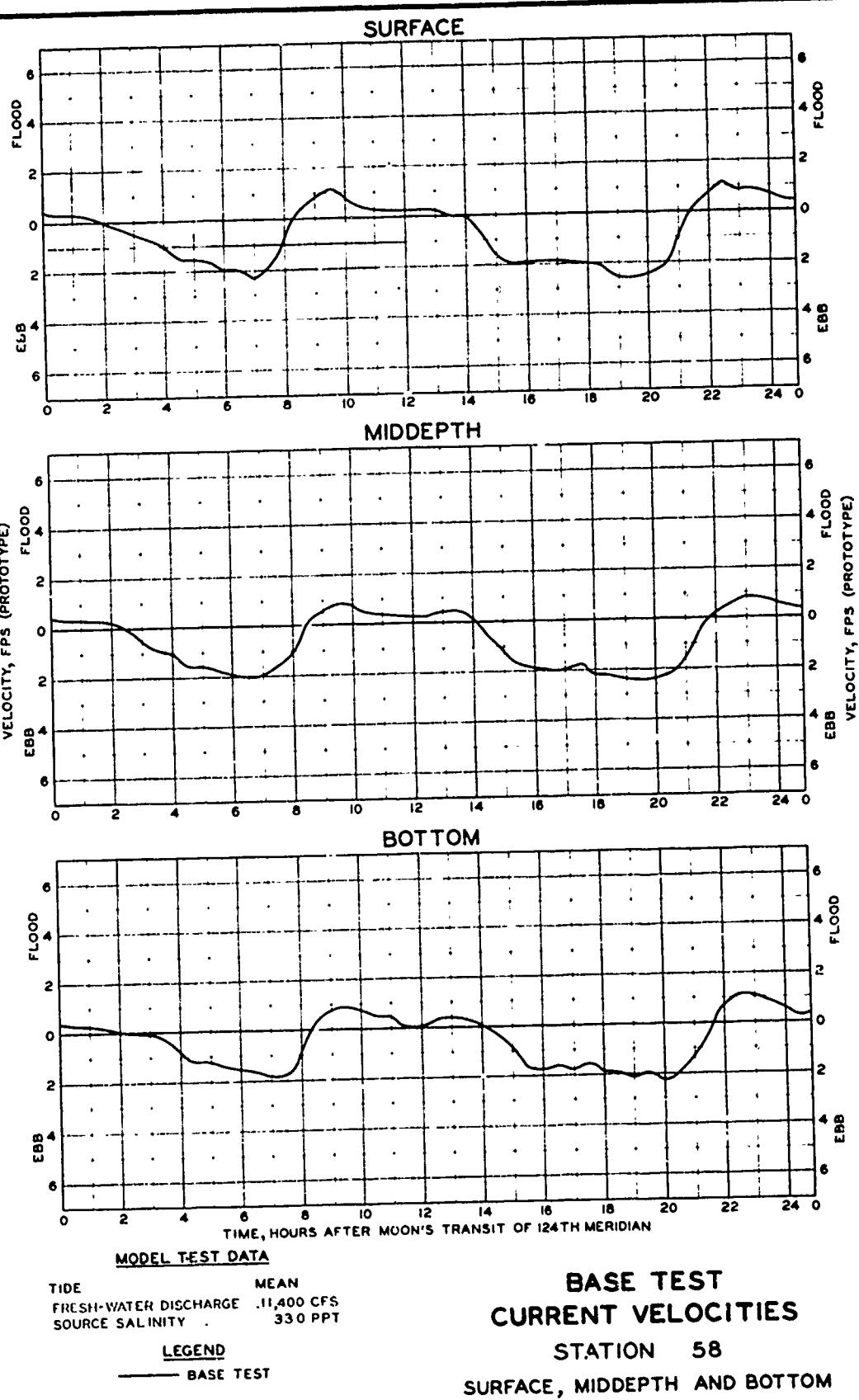
LEGEND

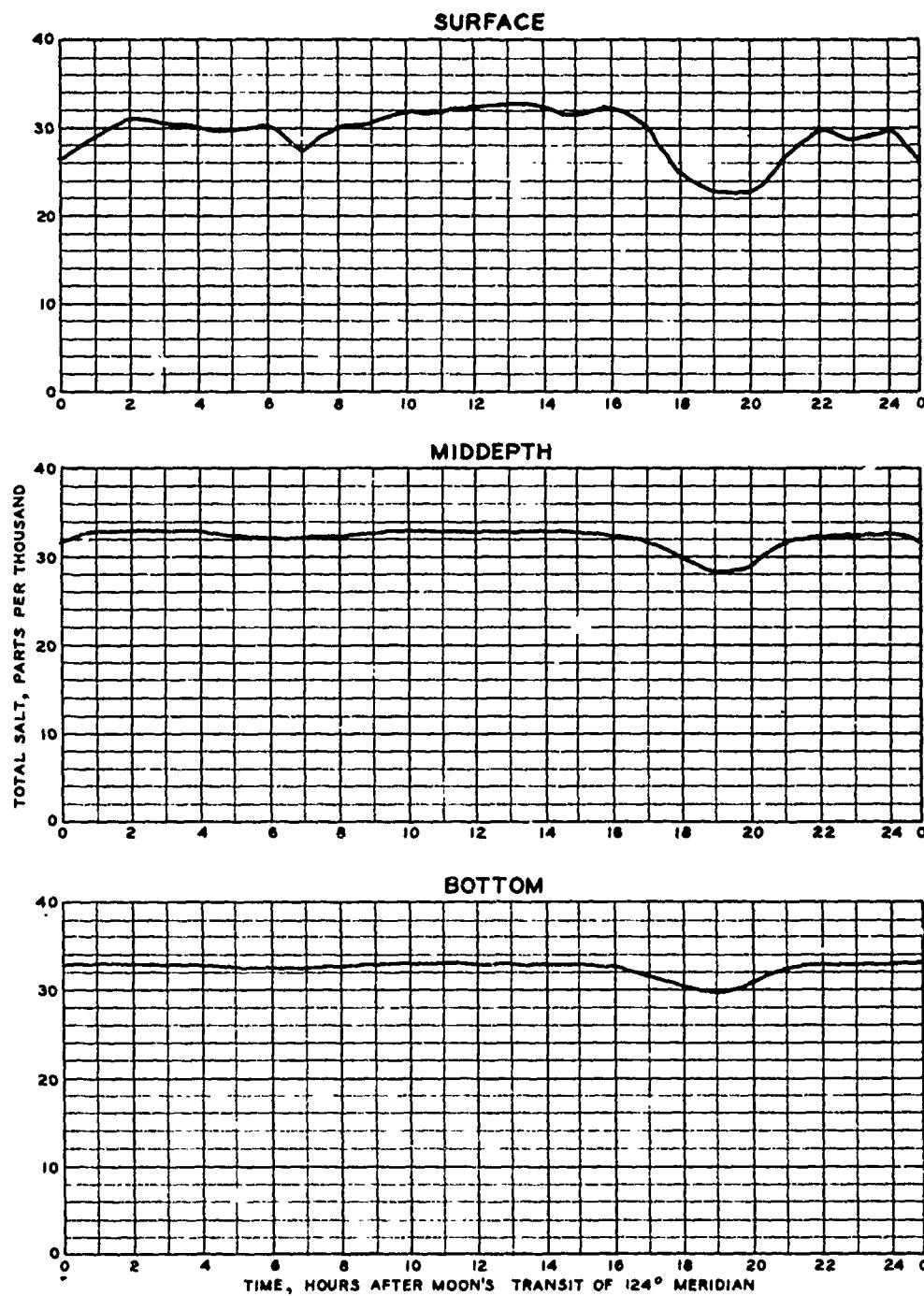
— BASE TEST

**BASE TEST
CURRENT VELOCITIES**

STATION 57

SURFACE, MIDDEPTH AND BOTTOM





MODEL TEST DATA

TIDE

FRESH-WATER DISCHARGE. 11,400 CFS

SOURCE SALINITY. .. 33.0 PPT

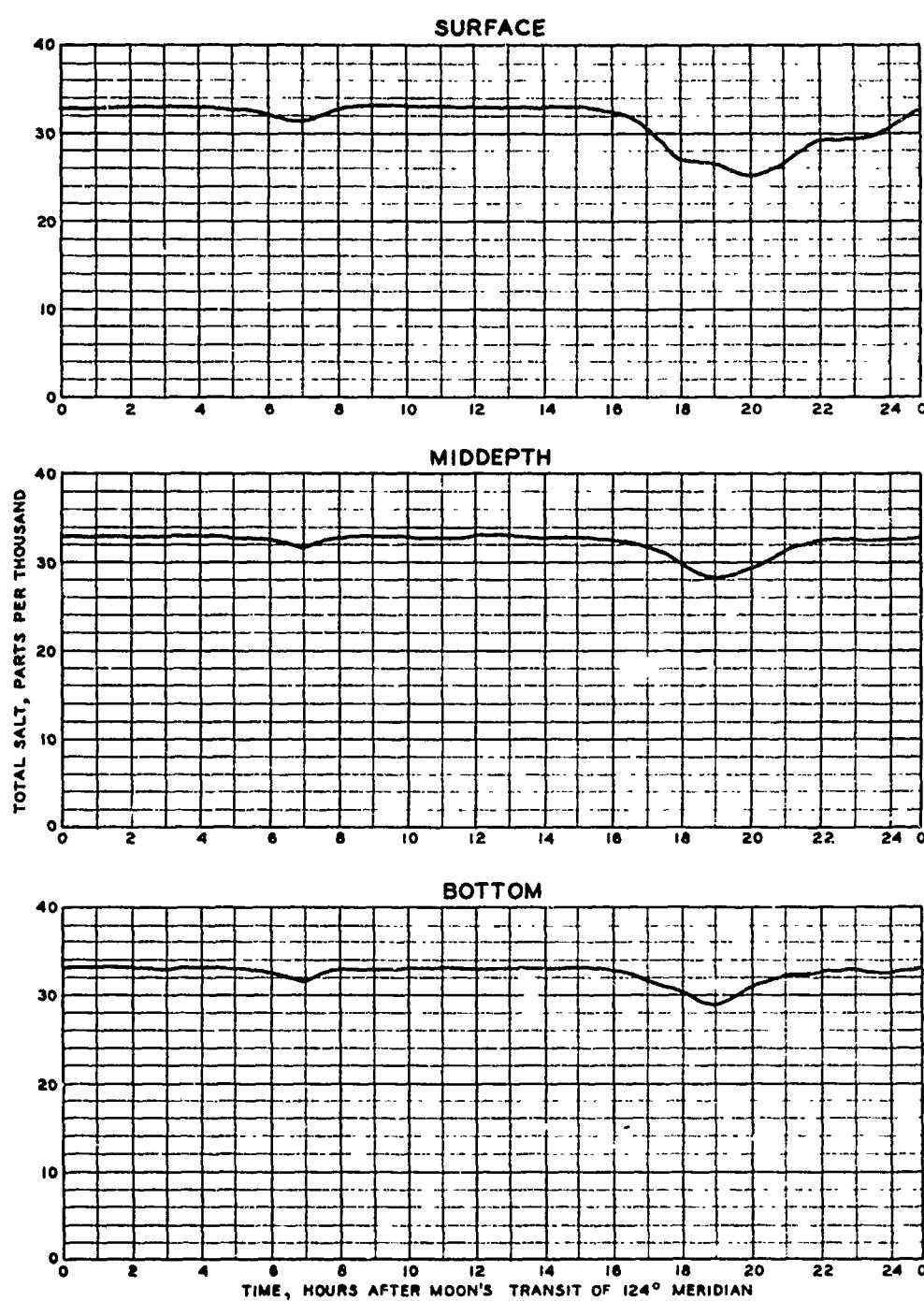
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 19

SURFACE, MIDDEPTH AND BOTTOM



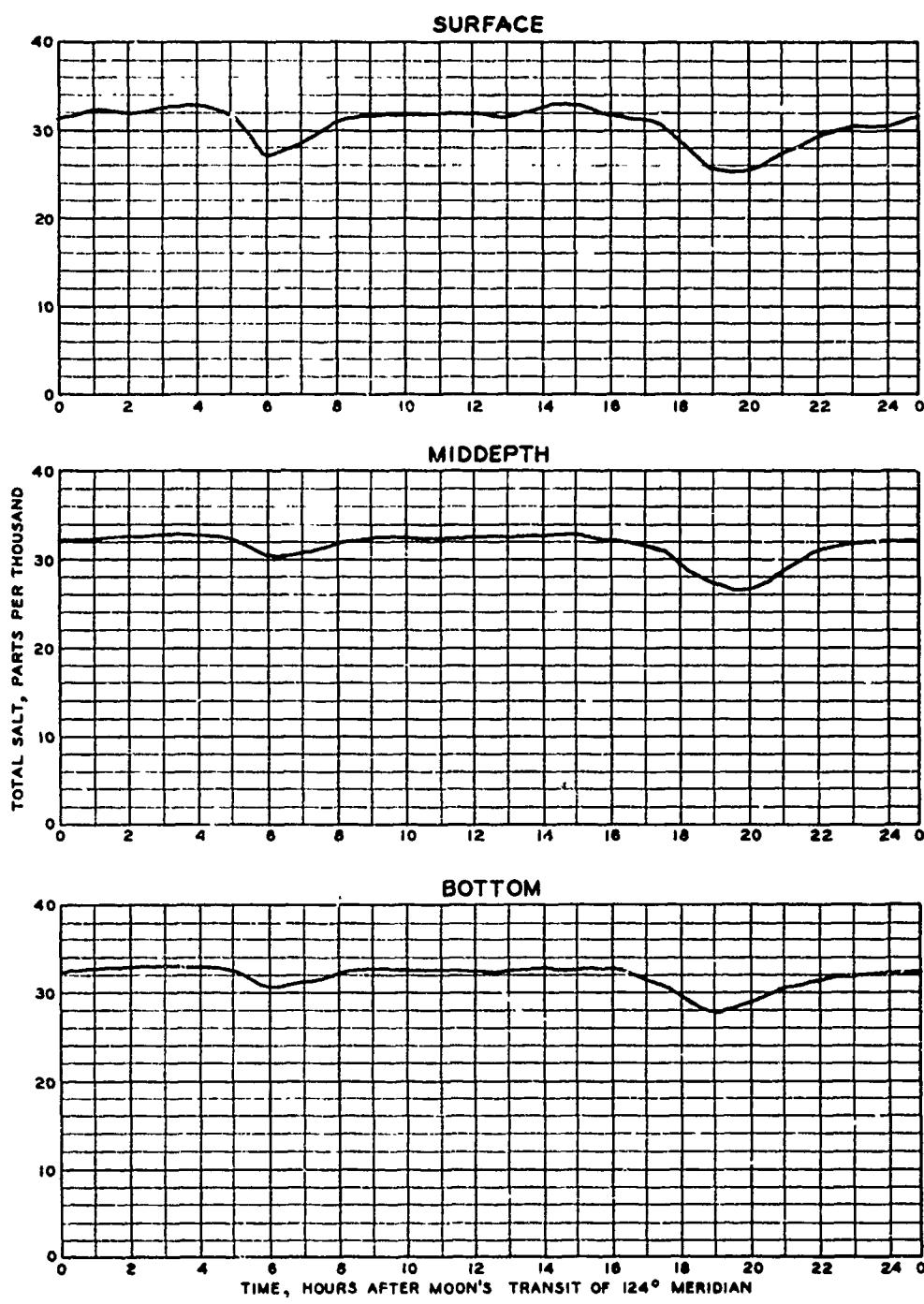
MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE....11,400 CFS
SOURCE SALINITY. 33.0 PPT

LEGEND
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 20
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE .. MEAN
FRESH-WATER DISCHARGE ... 11,400 CFS
SOURCE SALINITY ... 33.0 PPT

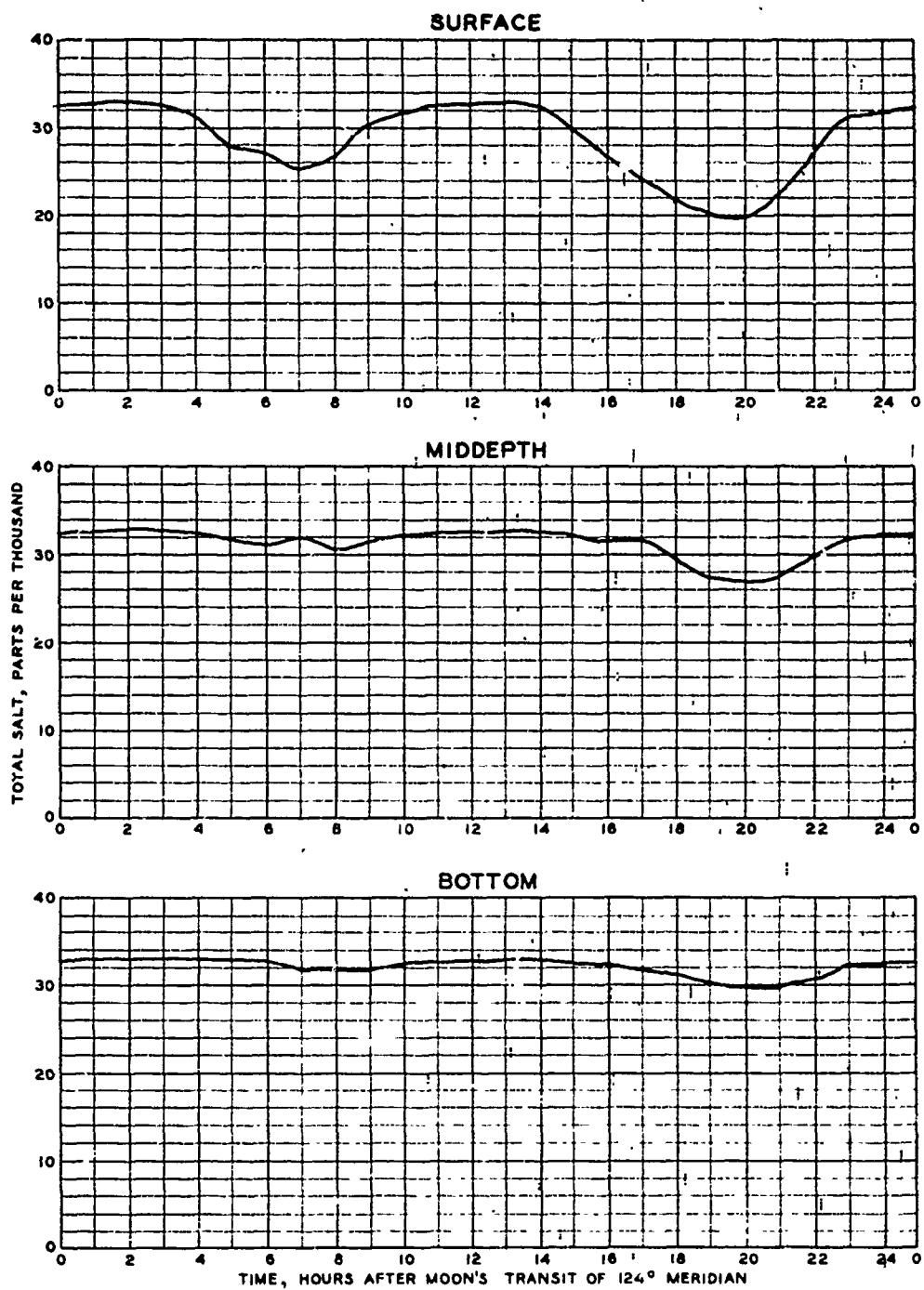
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 21
SURFACE, MIDDEPTH AND BOTTOM

223

PLATE 159



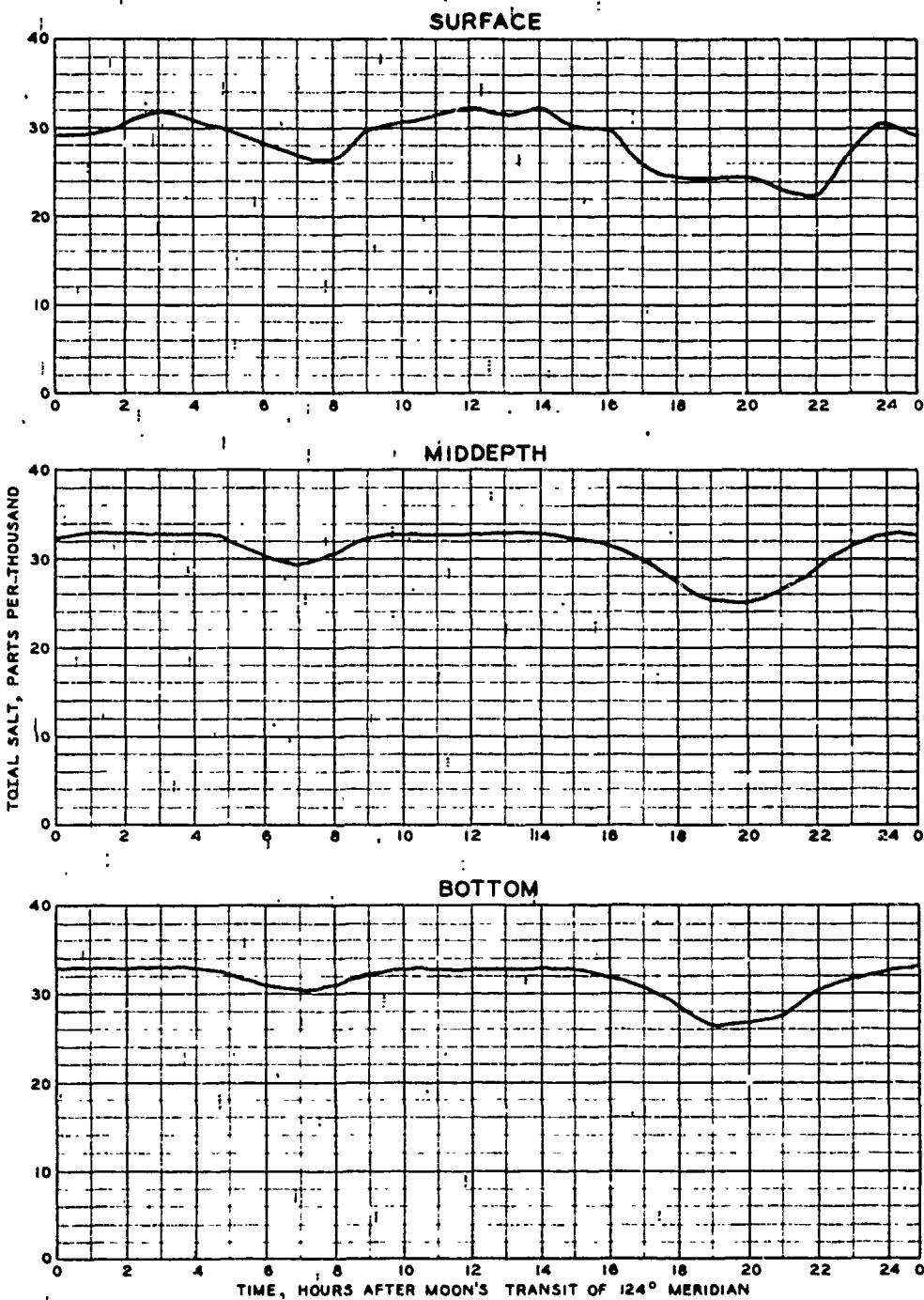
MODEL TEST DATA

TIDE .. MEAN
FRESH-WATER DISCHARGE . . 11,400 CFS
SOURCE SALINITY... 330 PPT

LEGEND
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 22
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	330 PPT

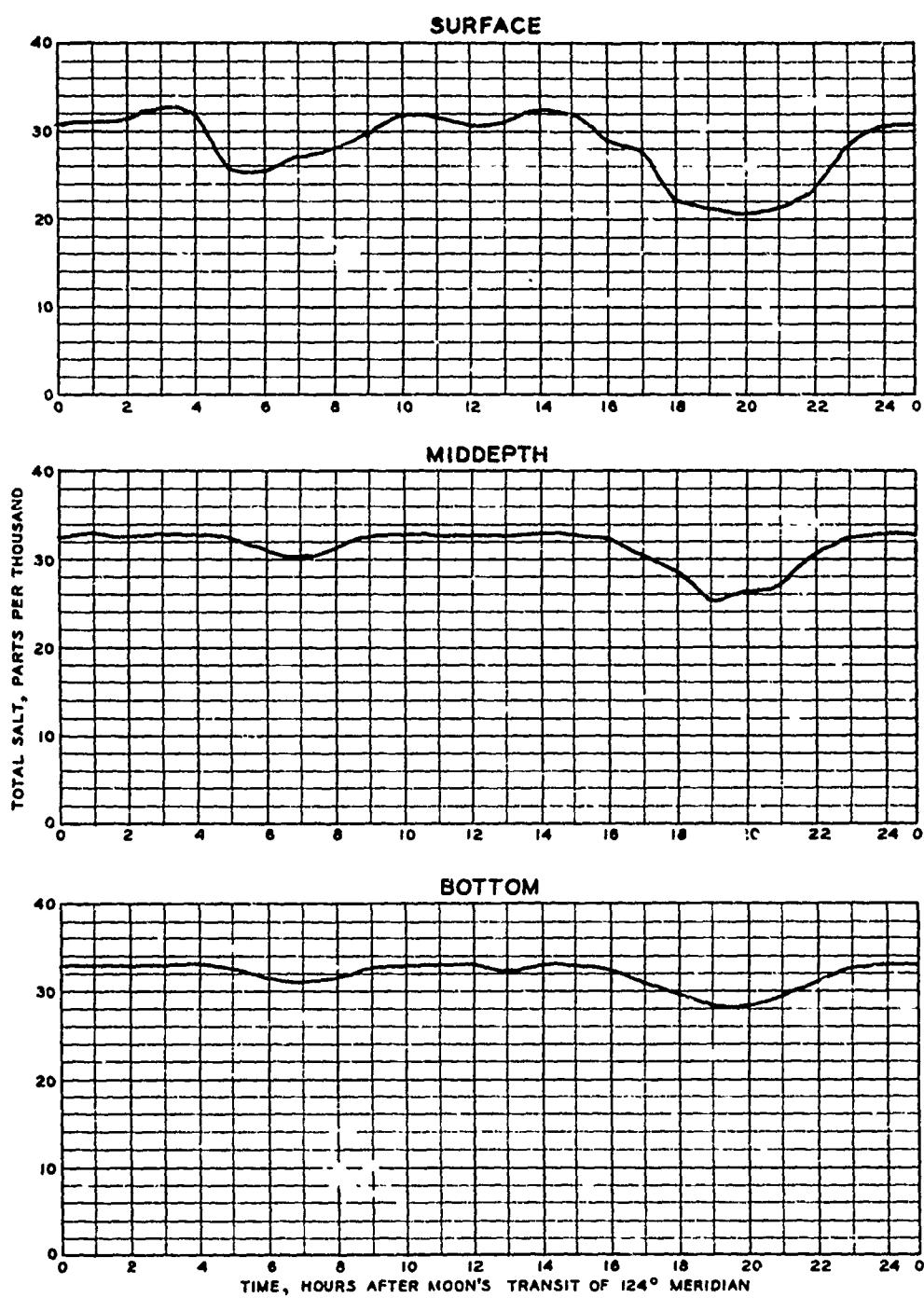
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 23

SURFACE, MIDDEPTH AND BOTTOM

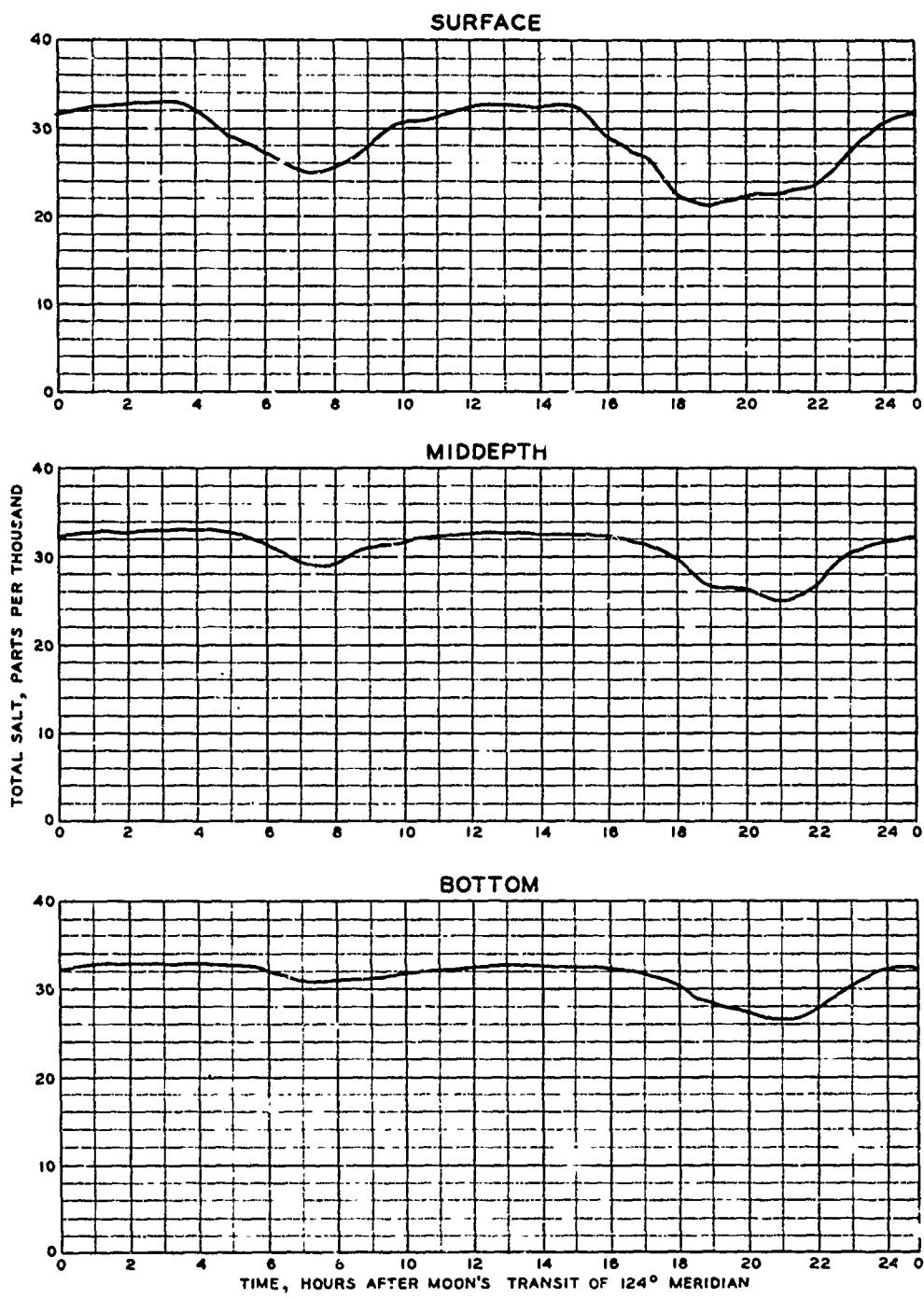


MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE ... 11,400 CFS
 SOURCE SALINITY . 330 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
 STATION 24
 SURFACE, MIDDEPTH AND BOTTOM



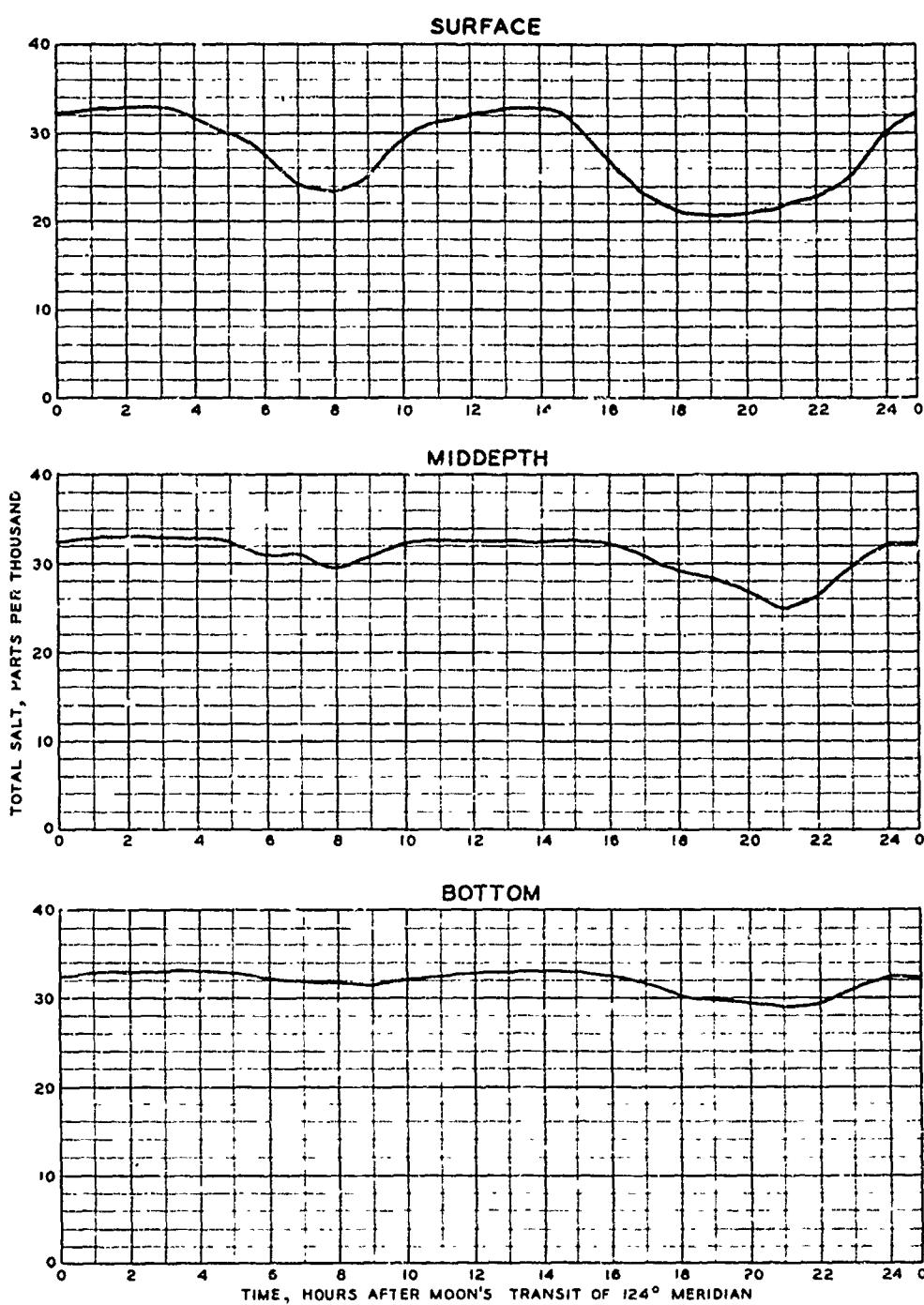
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 25
SURFACE, MIDDEPTH AND BOTTOM

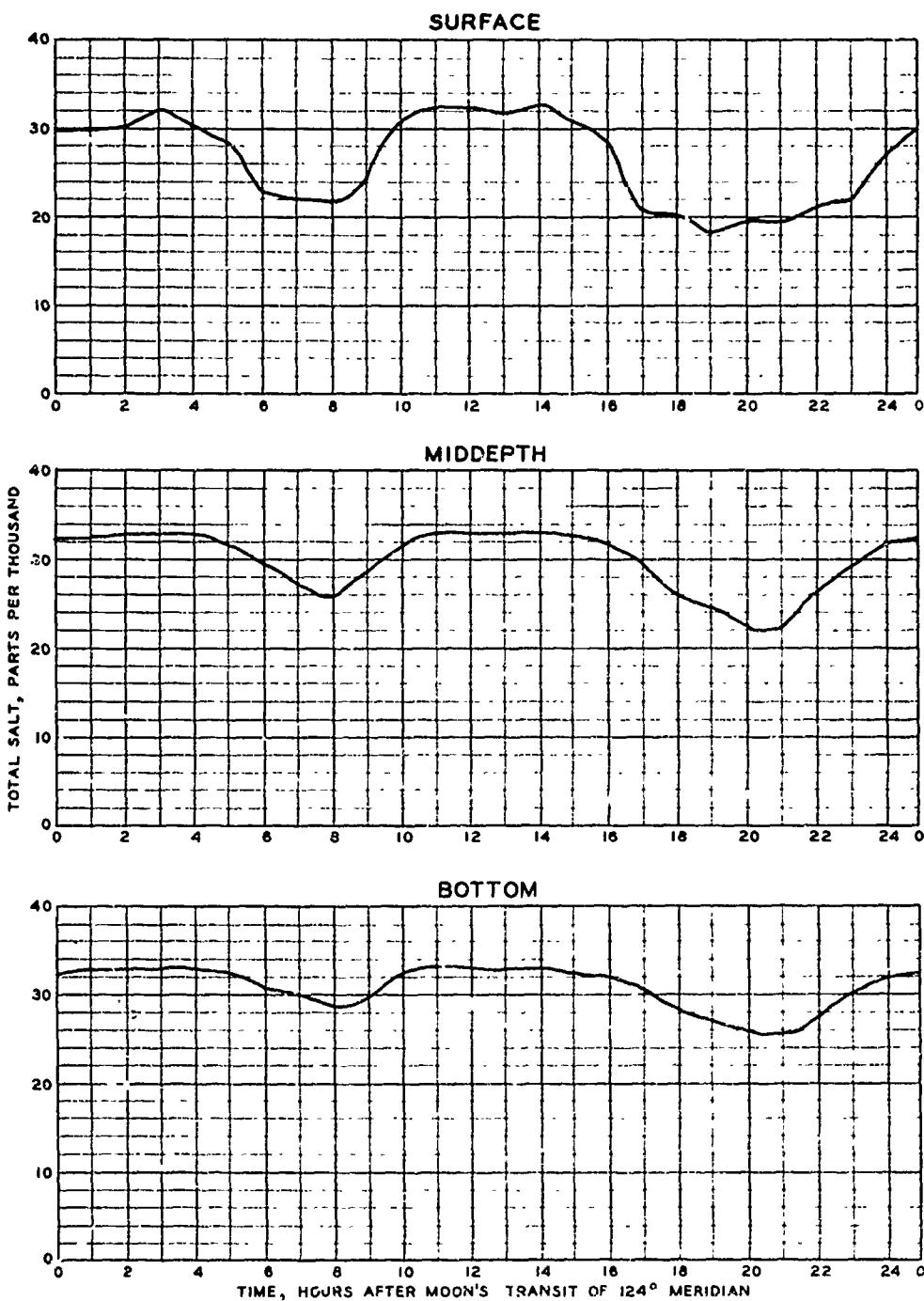


MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 330 PPT

LEGEND
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 26
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 330 PPT

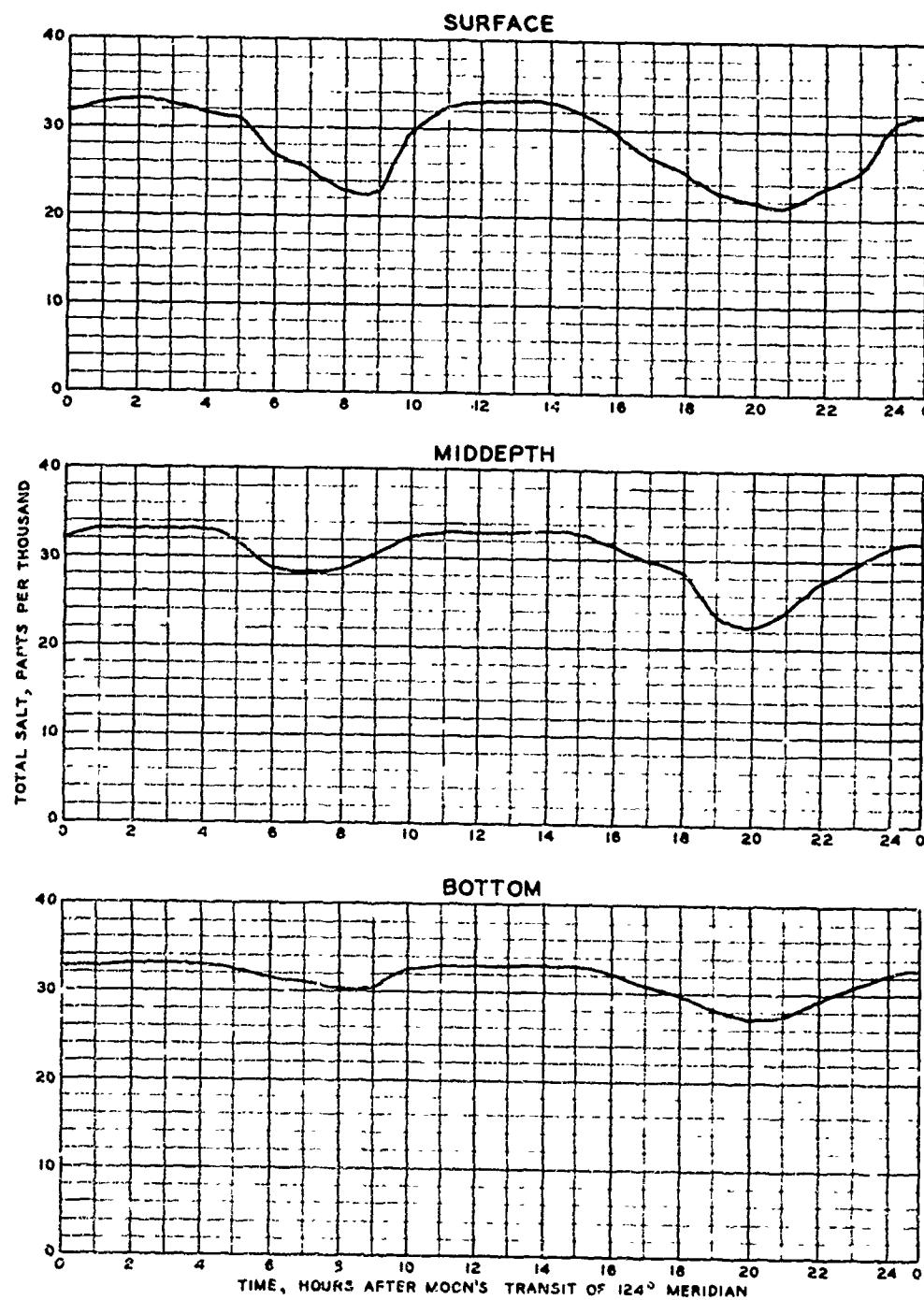
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 26A

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

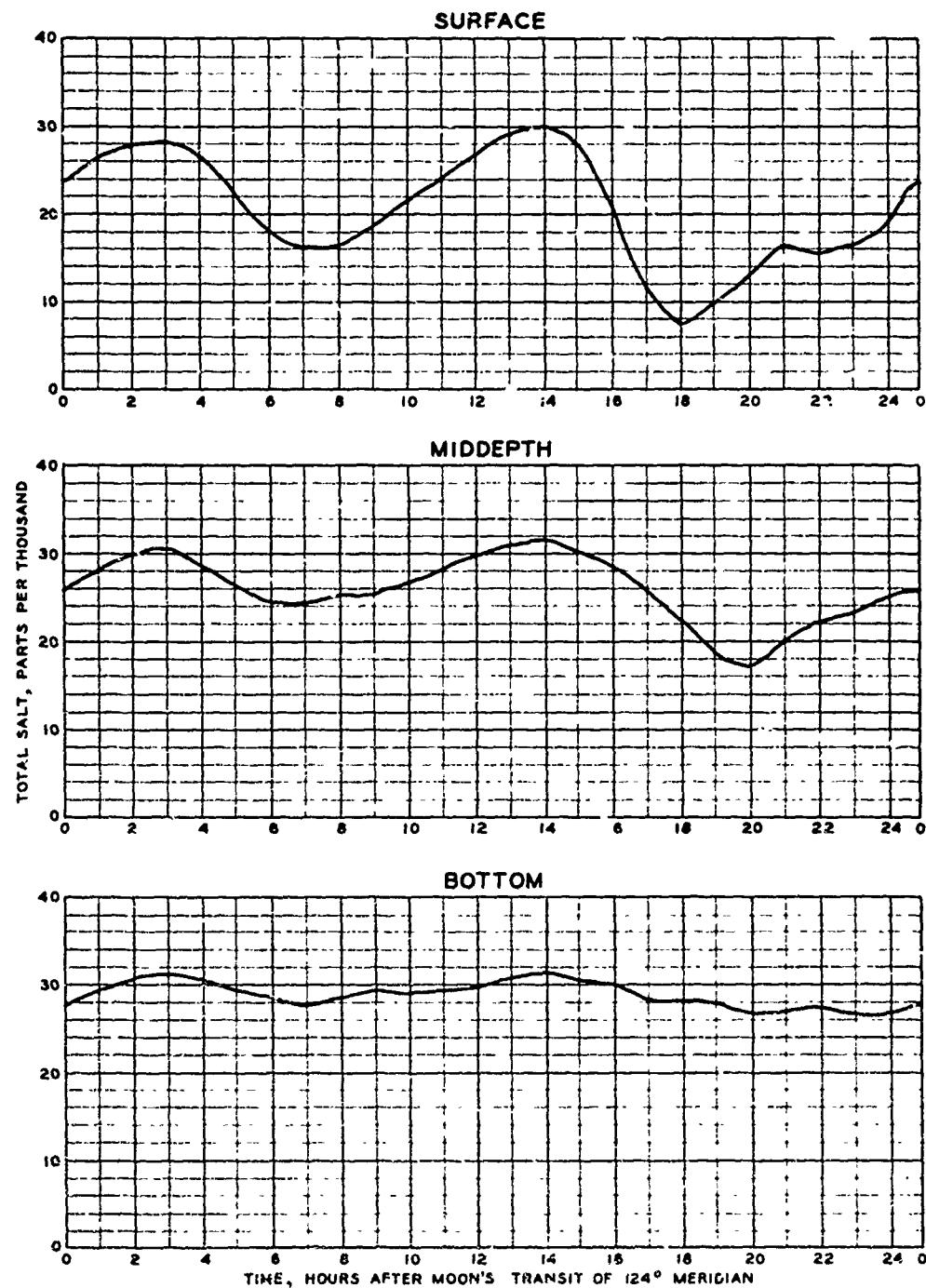
TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 27

SURFACE, MIDDEPTH AND BOTTOM



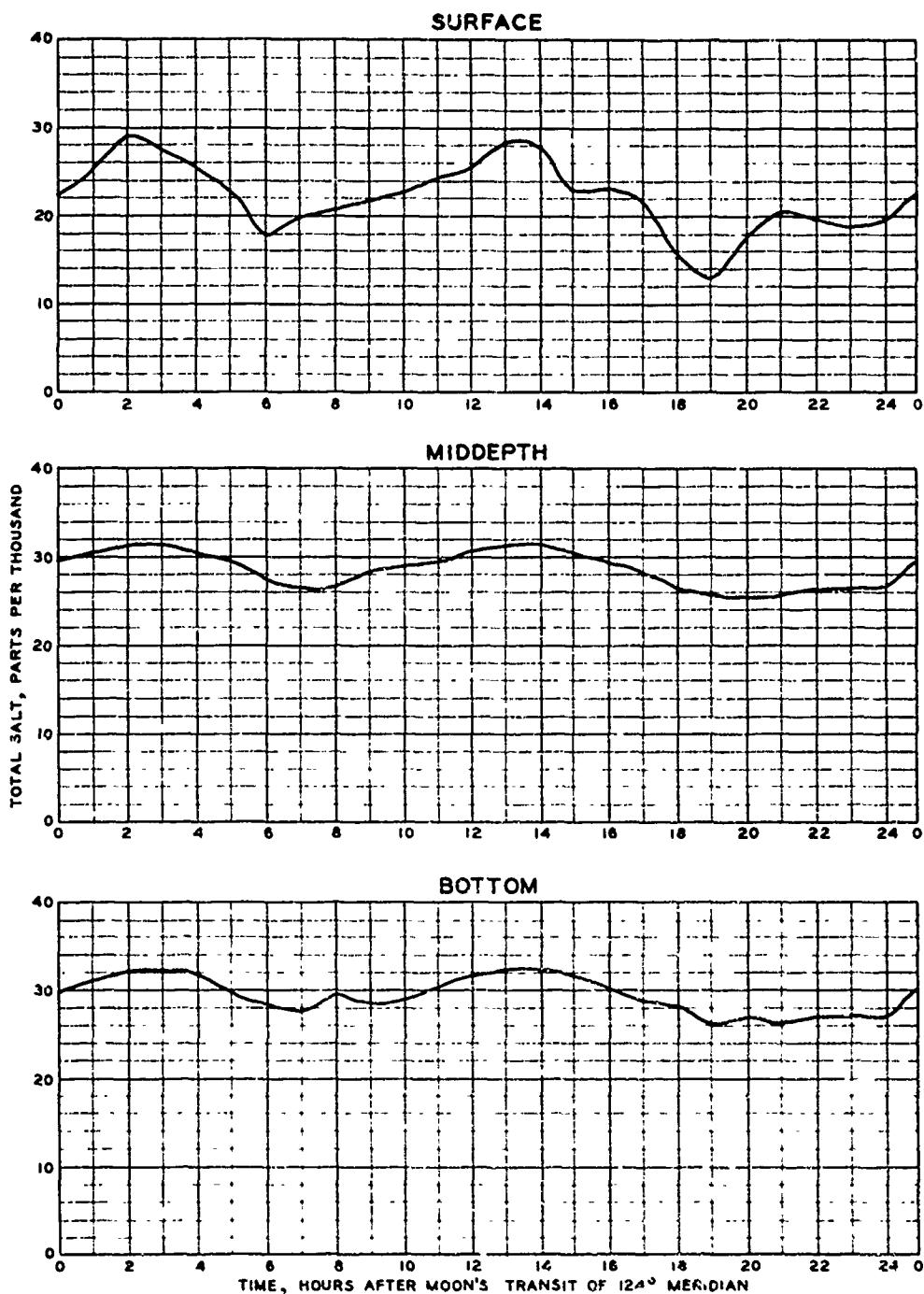
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE . 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 28
 SURFACE, MIDDEPTH AND BOTTOM

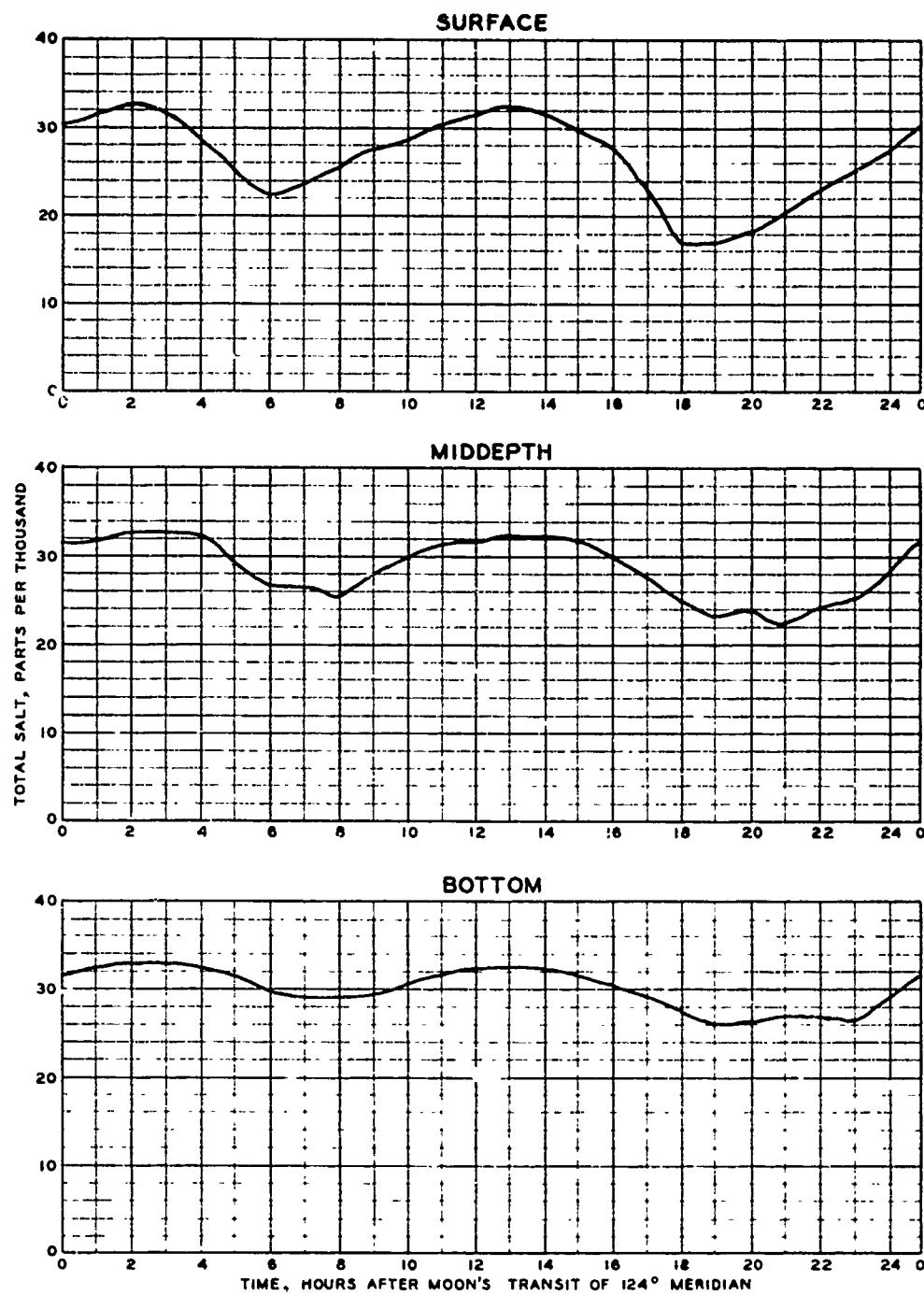


MODEL TEST DATA

TIDE MEAN
 FRESH-WATER D'SCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
 STATION 29
 SURFACE, MIDDEPTH AND BOTTOM



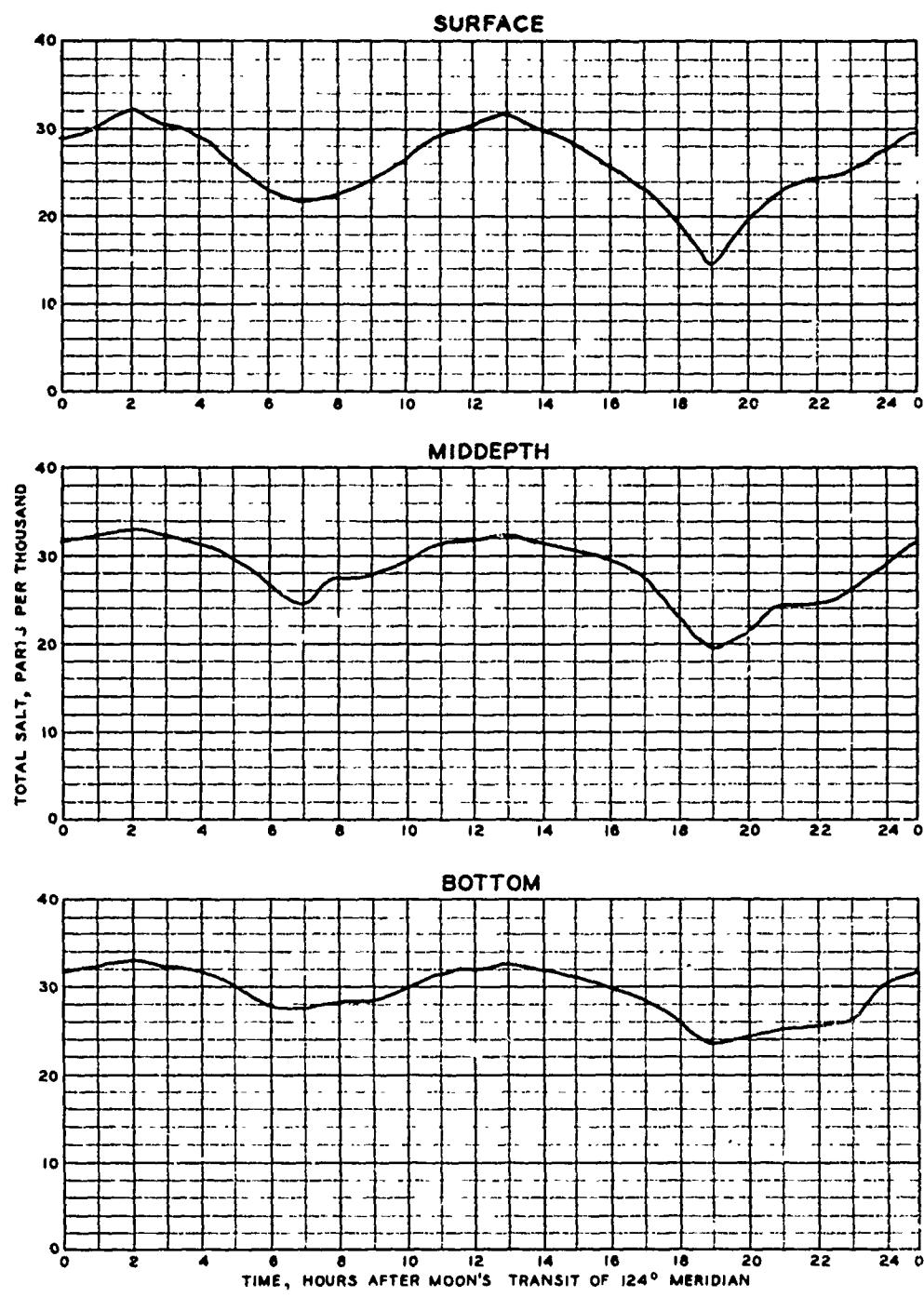
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY. 33.0 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 30
SURFACE, MIDDEPTH AND BOTTOM



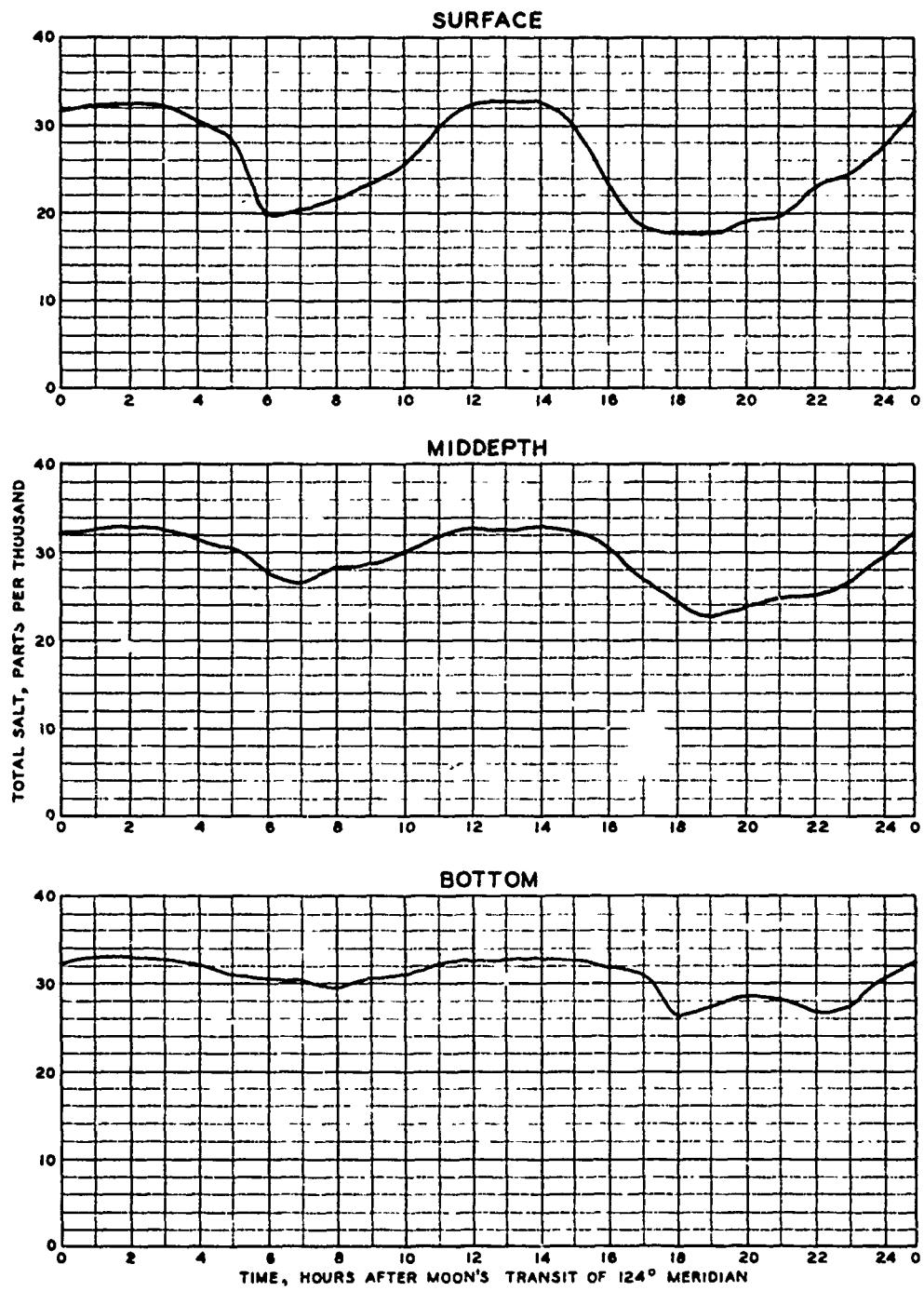
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY. 33.0 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 31
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 33.0 PPT

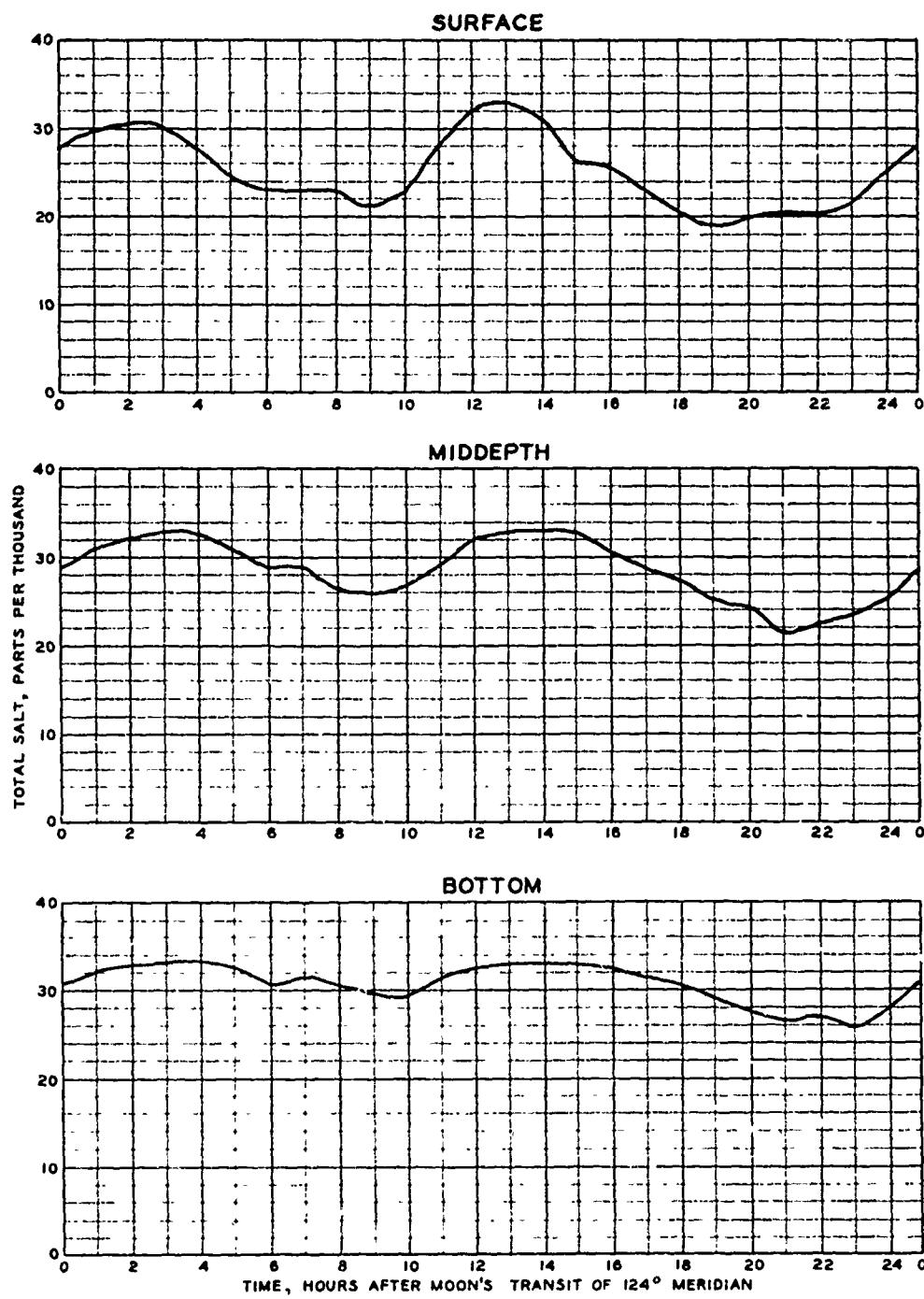
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 32

SURFACE, MIDDEPTH AND BOTTOM



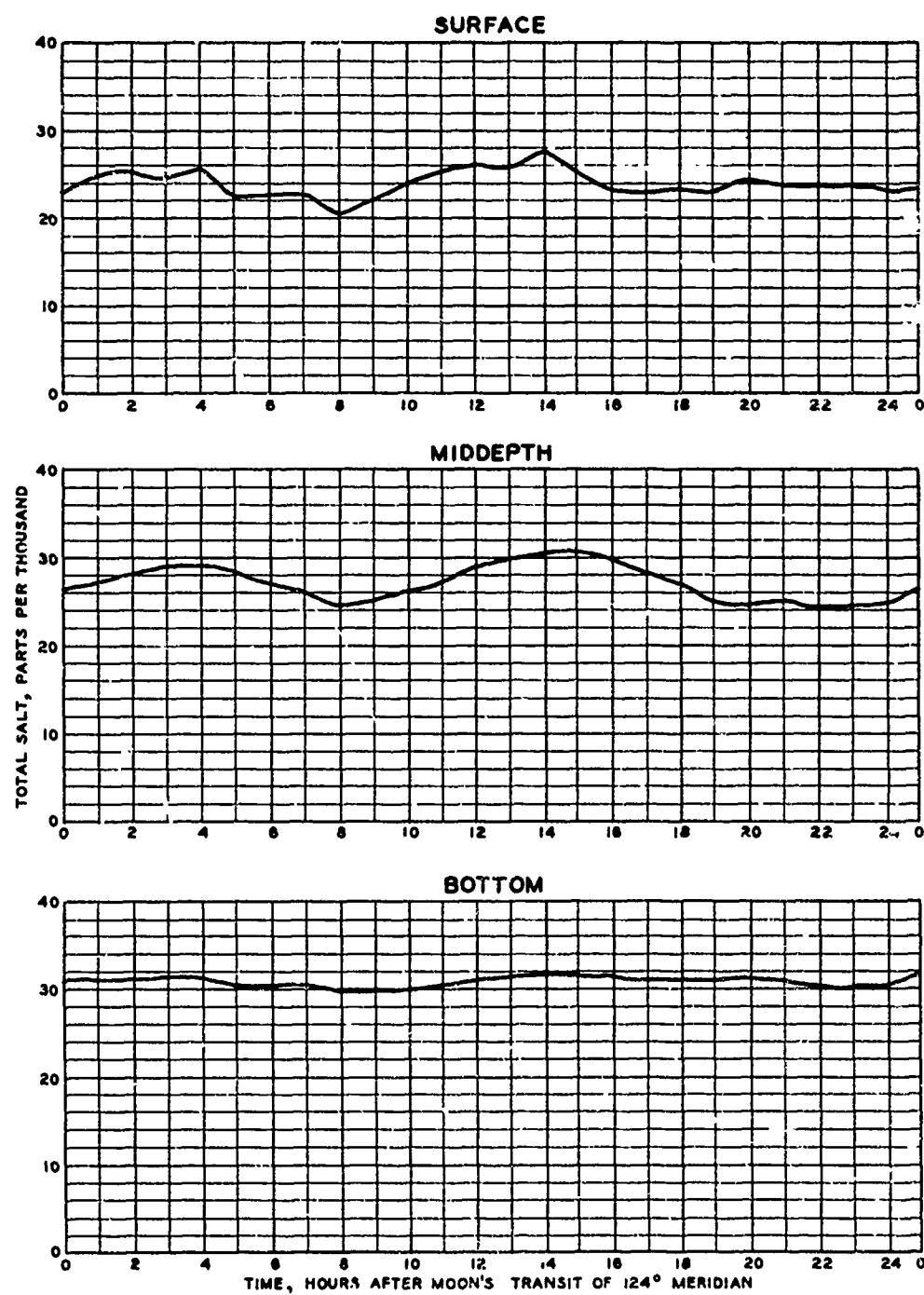
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 33.0 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 33
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE . . 11,400 CFS
 SOURCE SALINITY 33.0 PPT

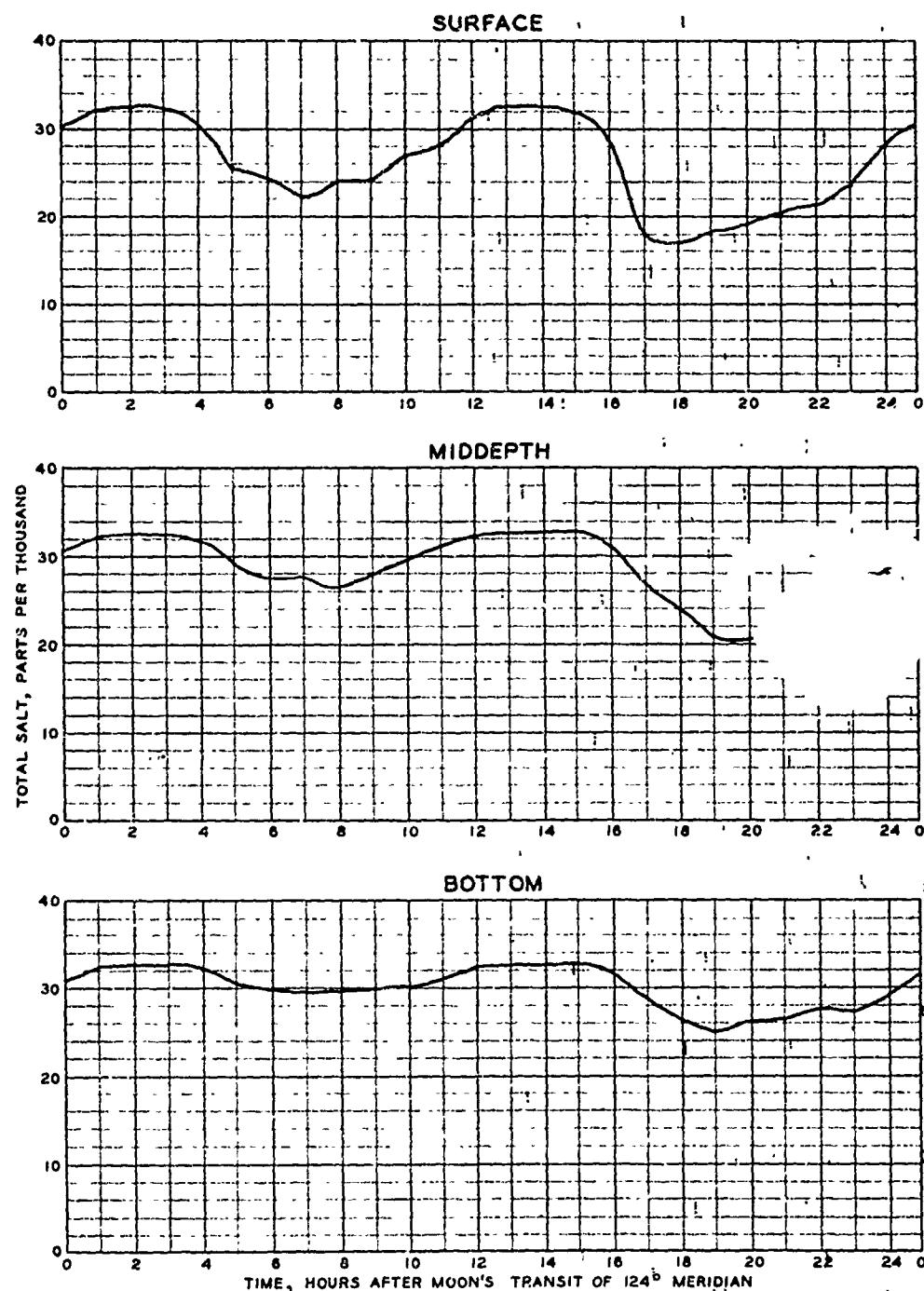
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 34
SURFACE, MIDDEPTH AND BOTTOM

22.37

PLATE 173



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE . . 11,400 CFS
SOURCE SALINITY 330 PPT

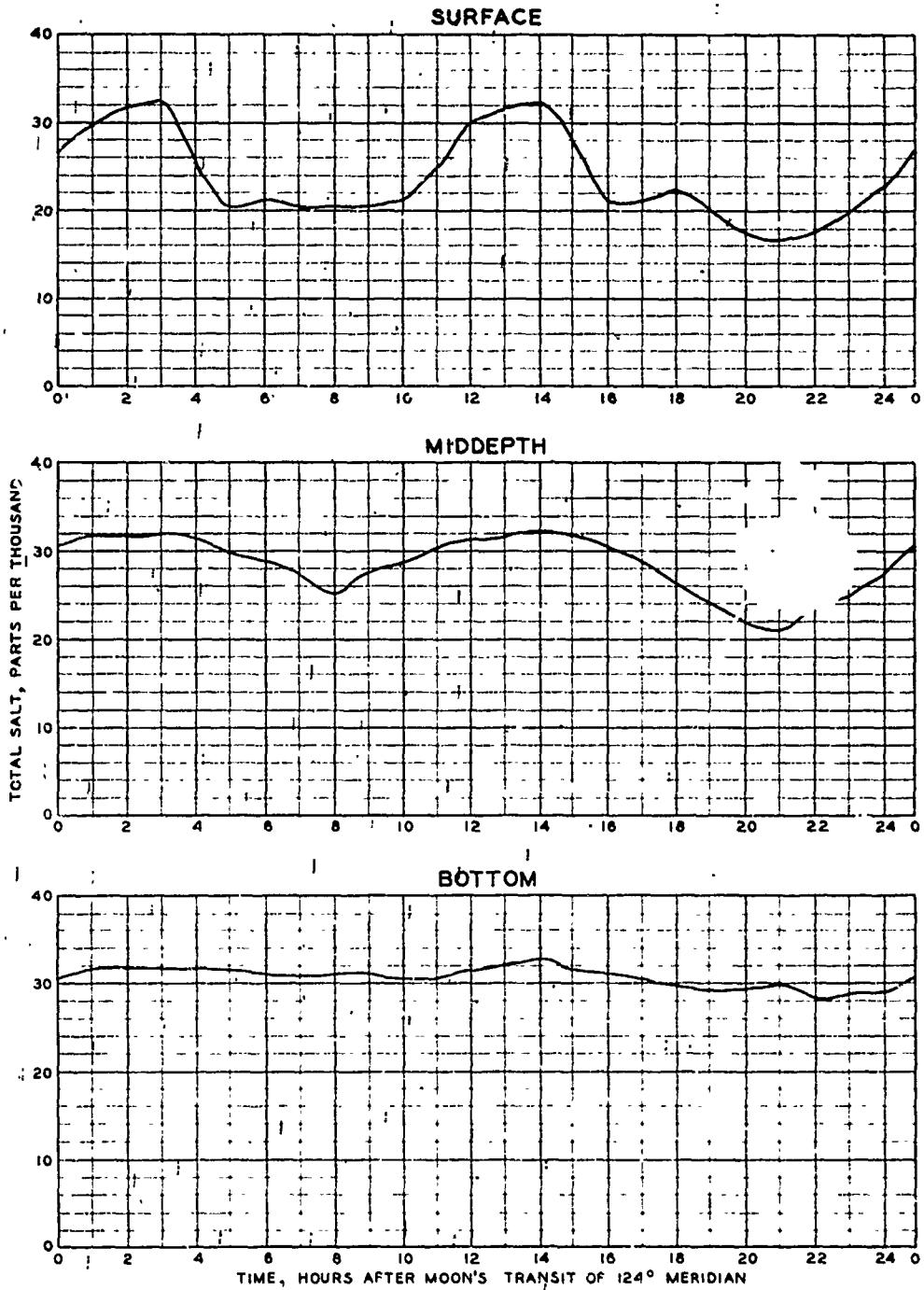
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 35.

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	33.0 PPT

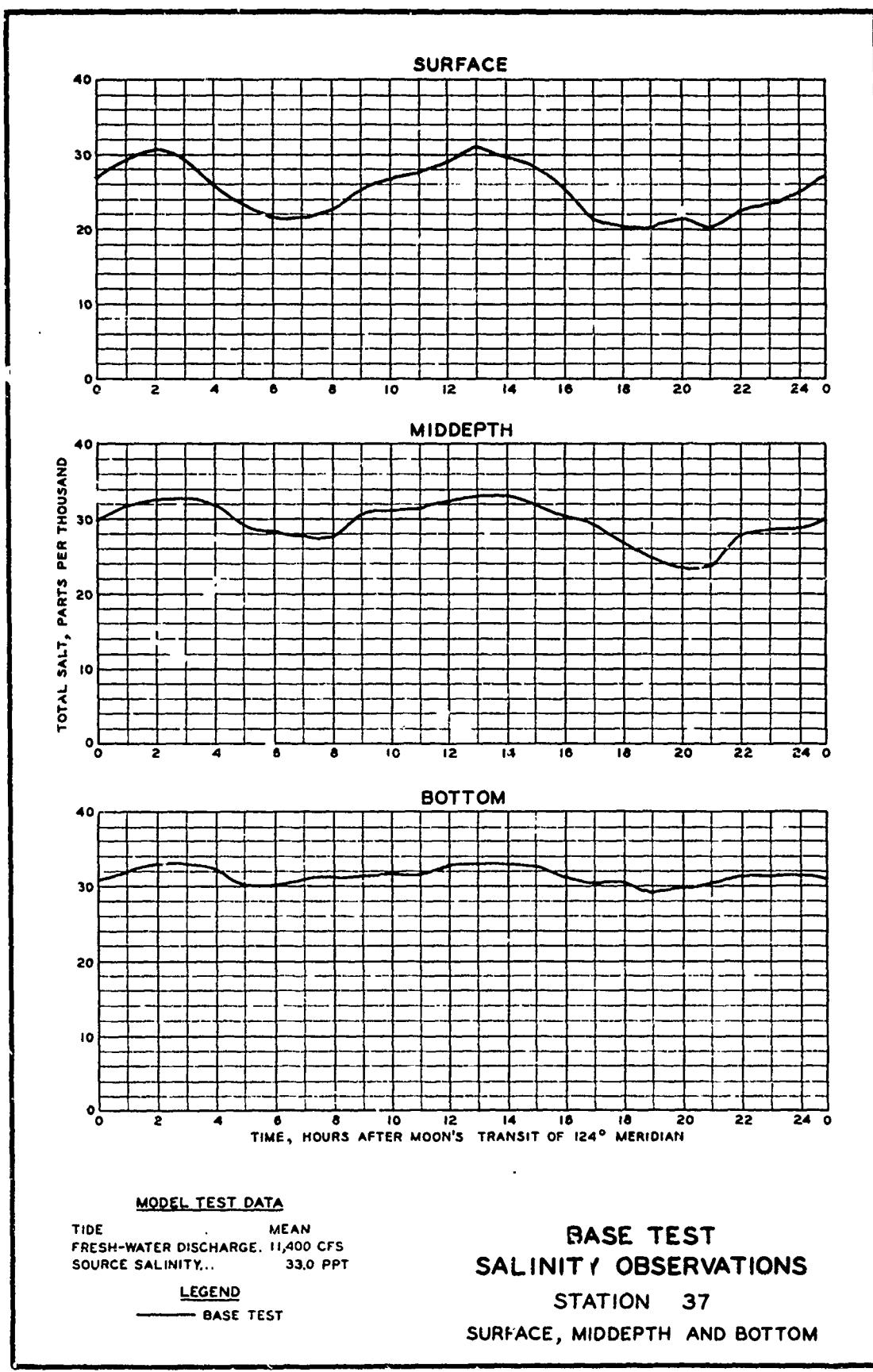
LEGEND

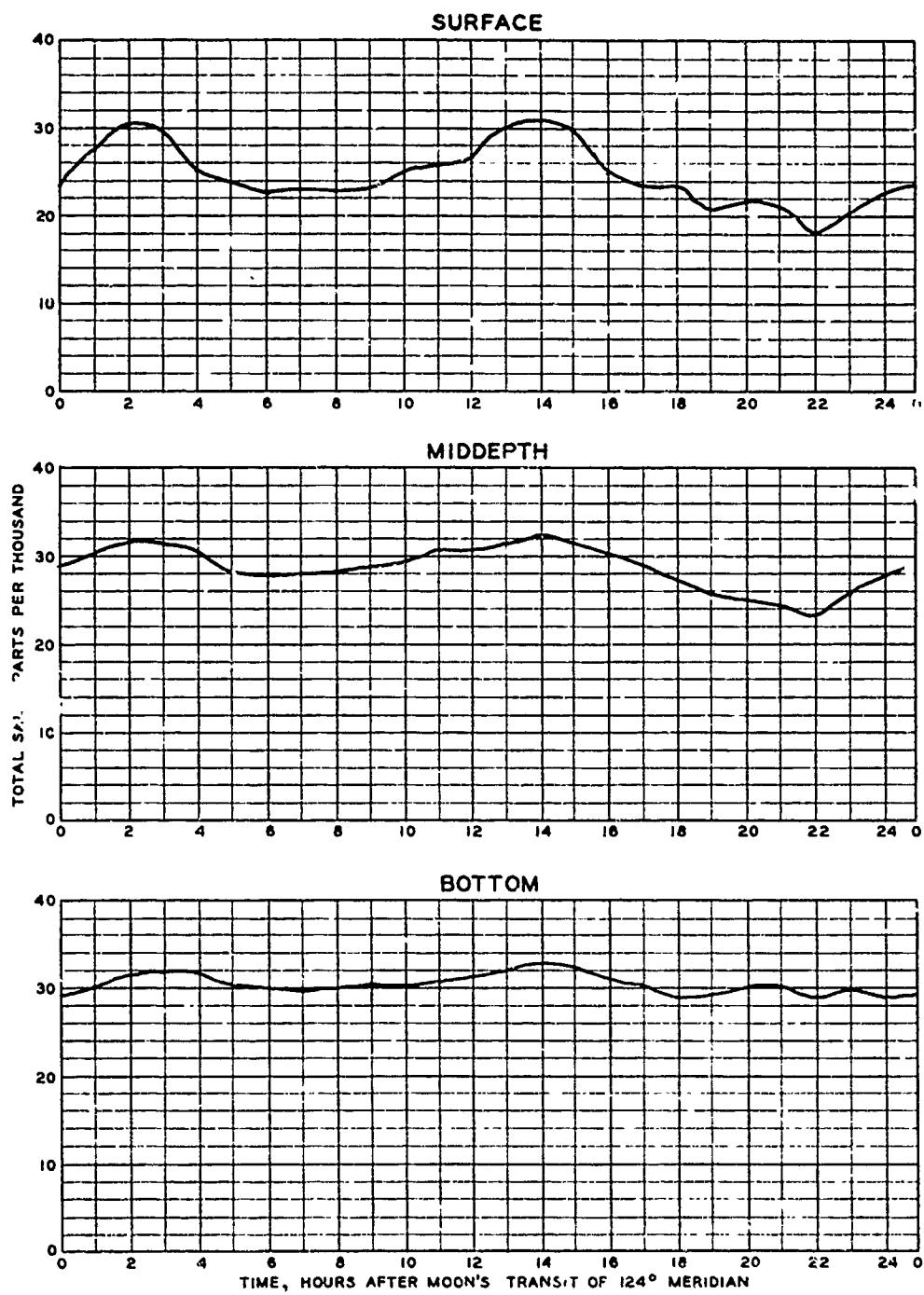
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 36

SURFACE, MIDDEPTH AND BOTTOM





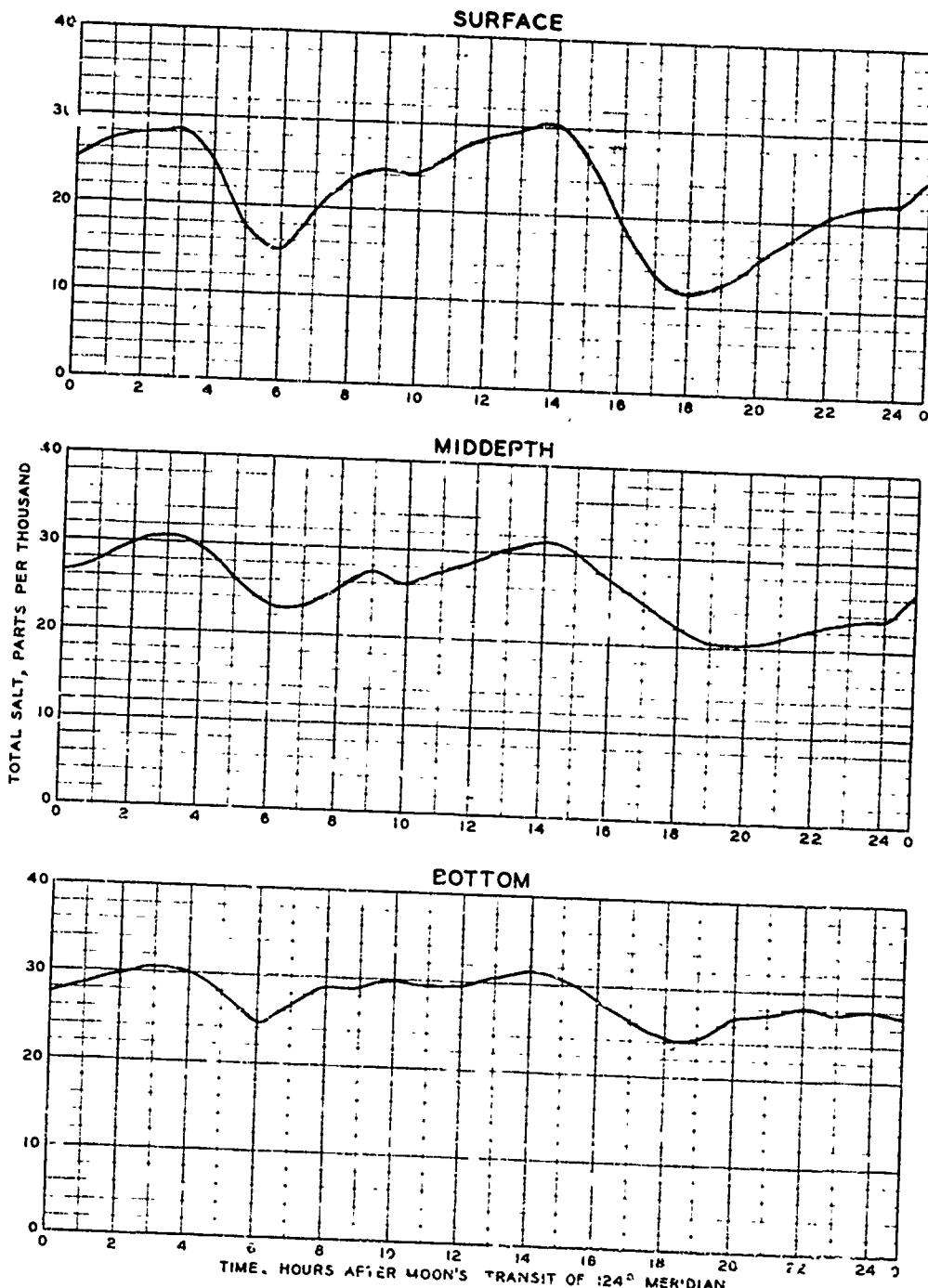
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
 STATION 38
 SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

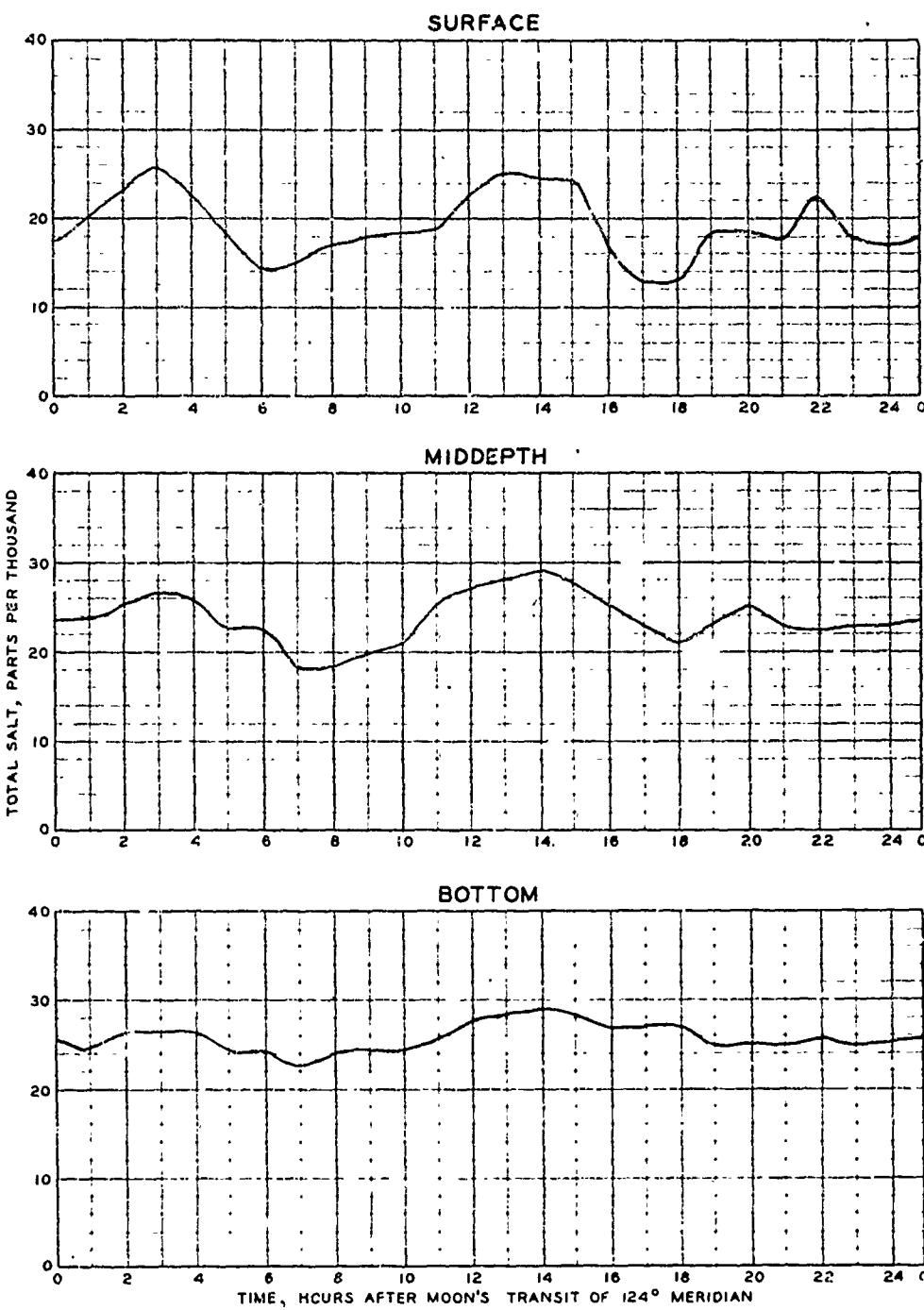
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 39
SURFACE, MIDDEPTH AND BOTTOM

PLATE 178

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MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE 11,400 CFS
SOURCE SALINITY 33.0 PPT

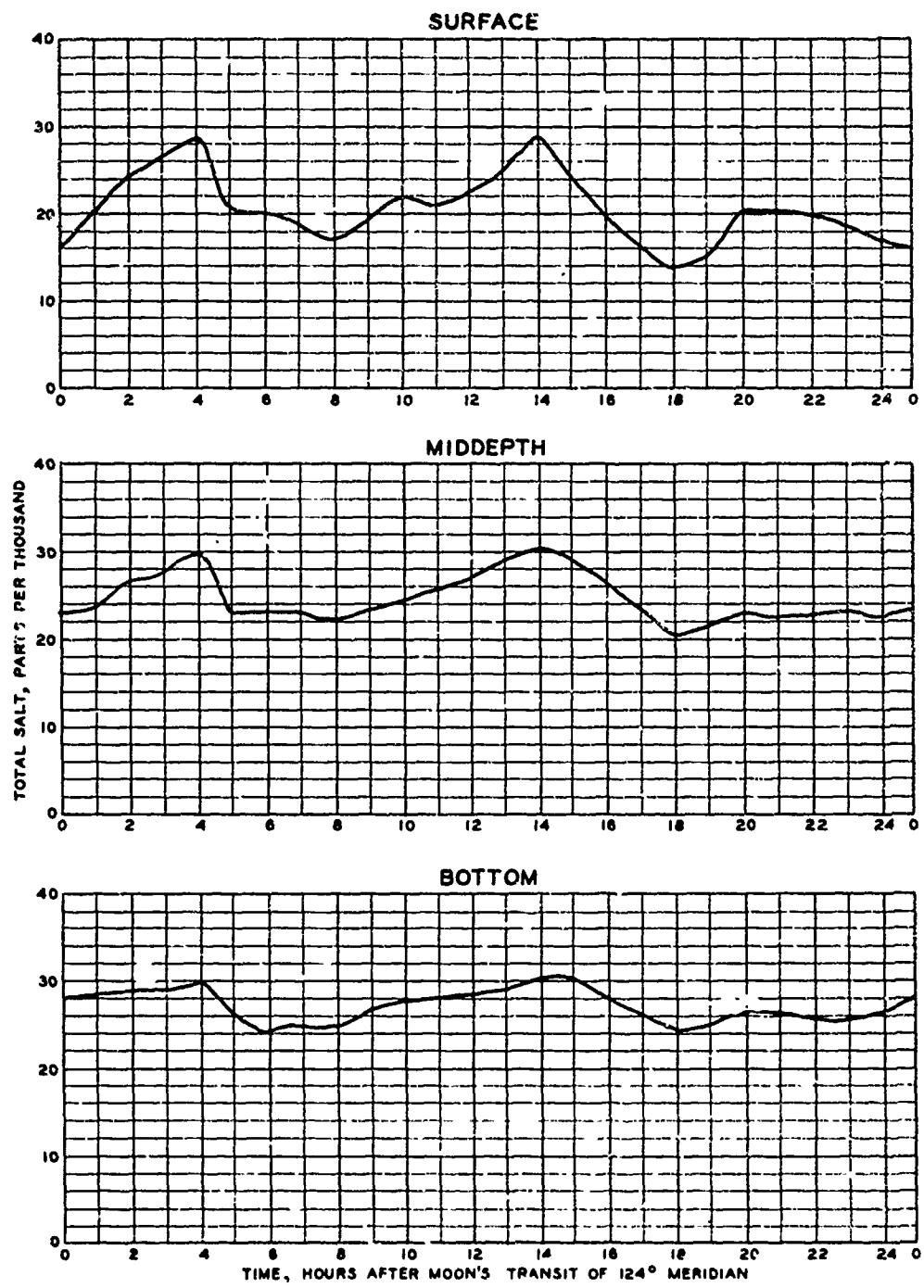
LEGEND
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 40

SURFACE, MIDDEPTH AND BOTTOM

PLATE 178



MODEL TEST DATA

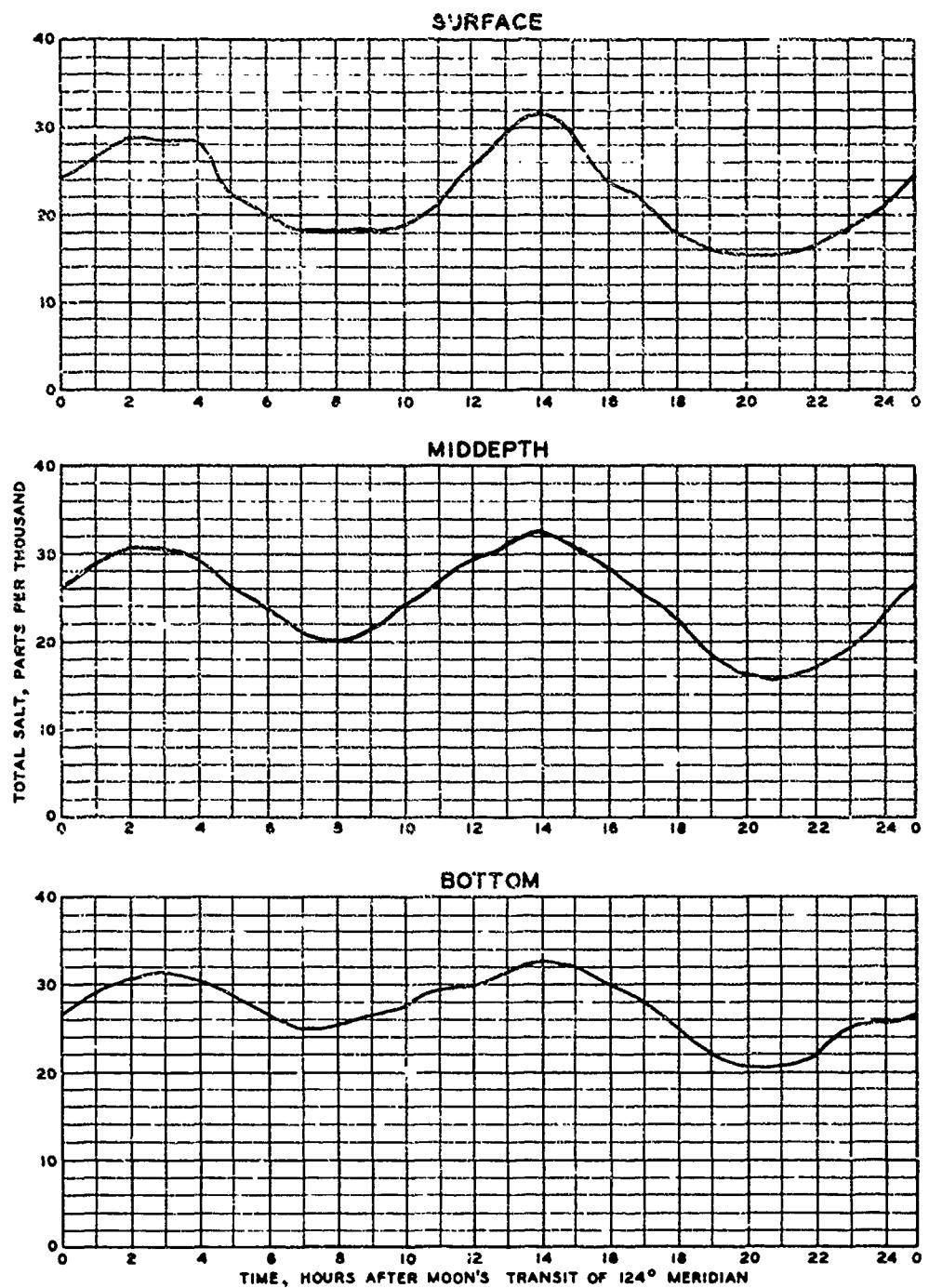
TIDE : MEAN
FRESH-WATER DISCHARGE, 11,400 CFS
SOURCE SALINITY . . . 33.0 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 41
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE, 11,400 CFS
SOURCE SALINITY... ... 33.0 PPT

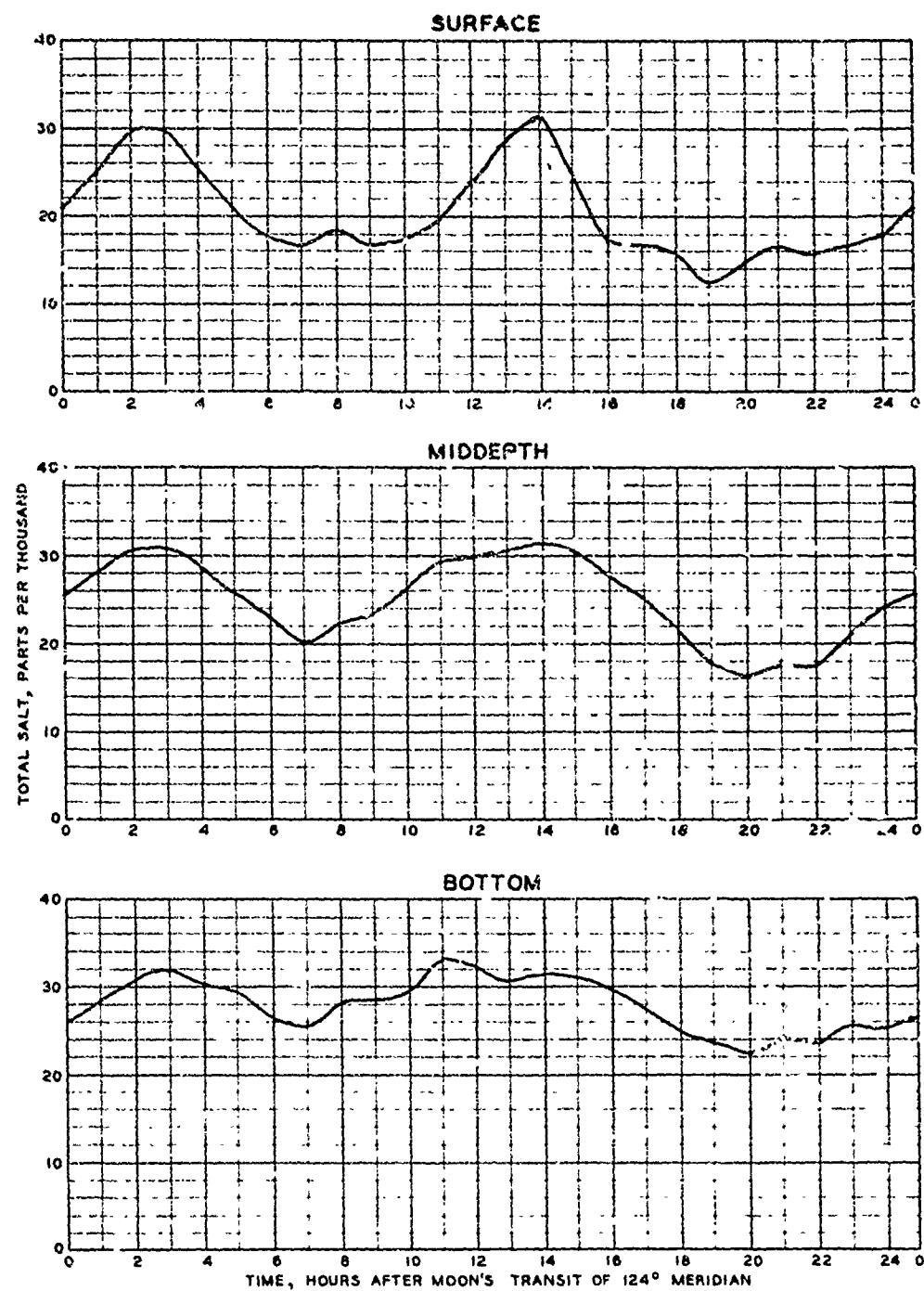
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 42

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

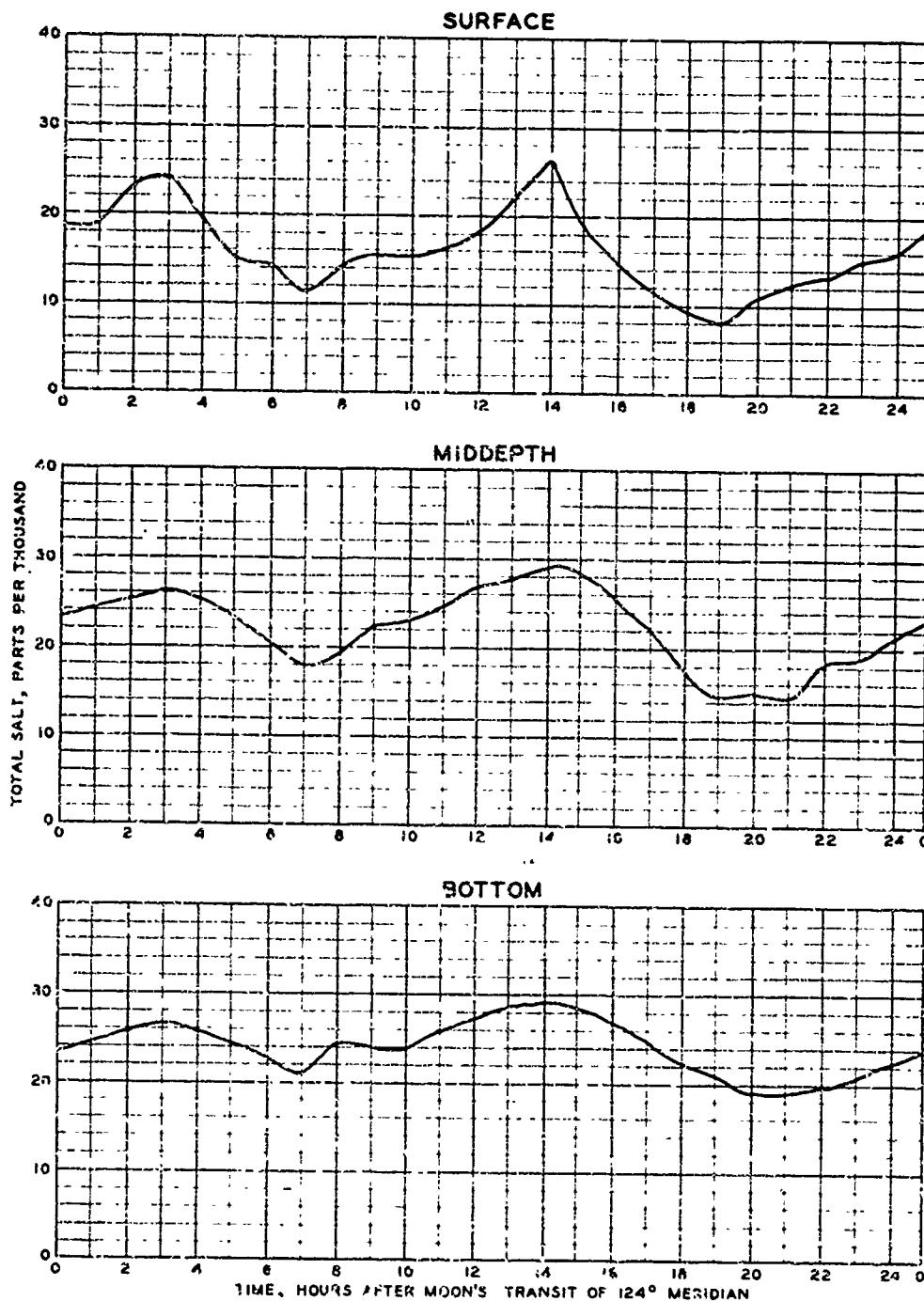
TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 43
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

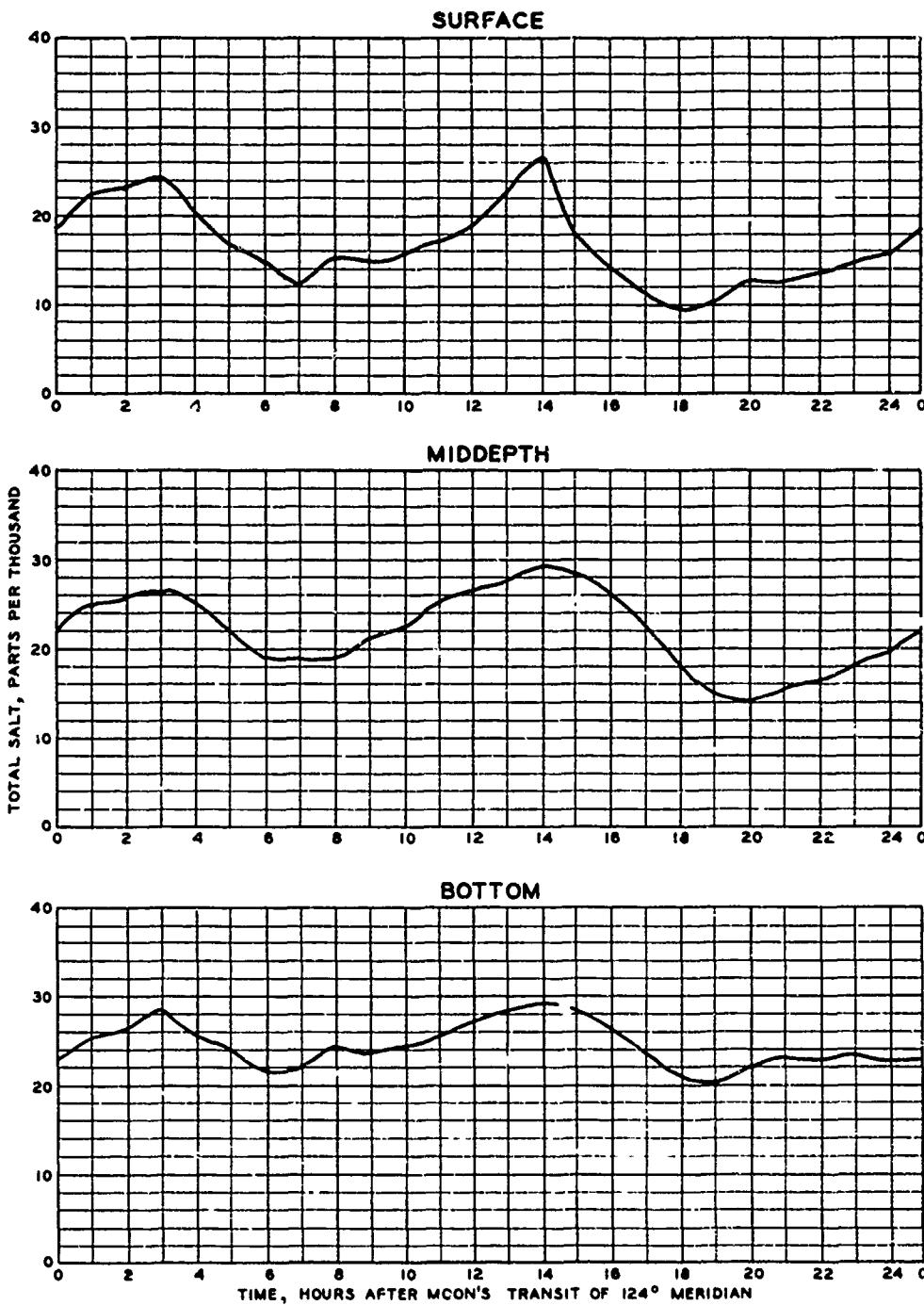
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 44

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE ... 11,400 CFS
 SOURCE SALINITY... 33.0 PPT

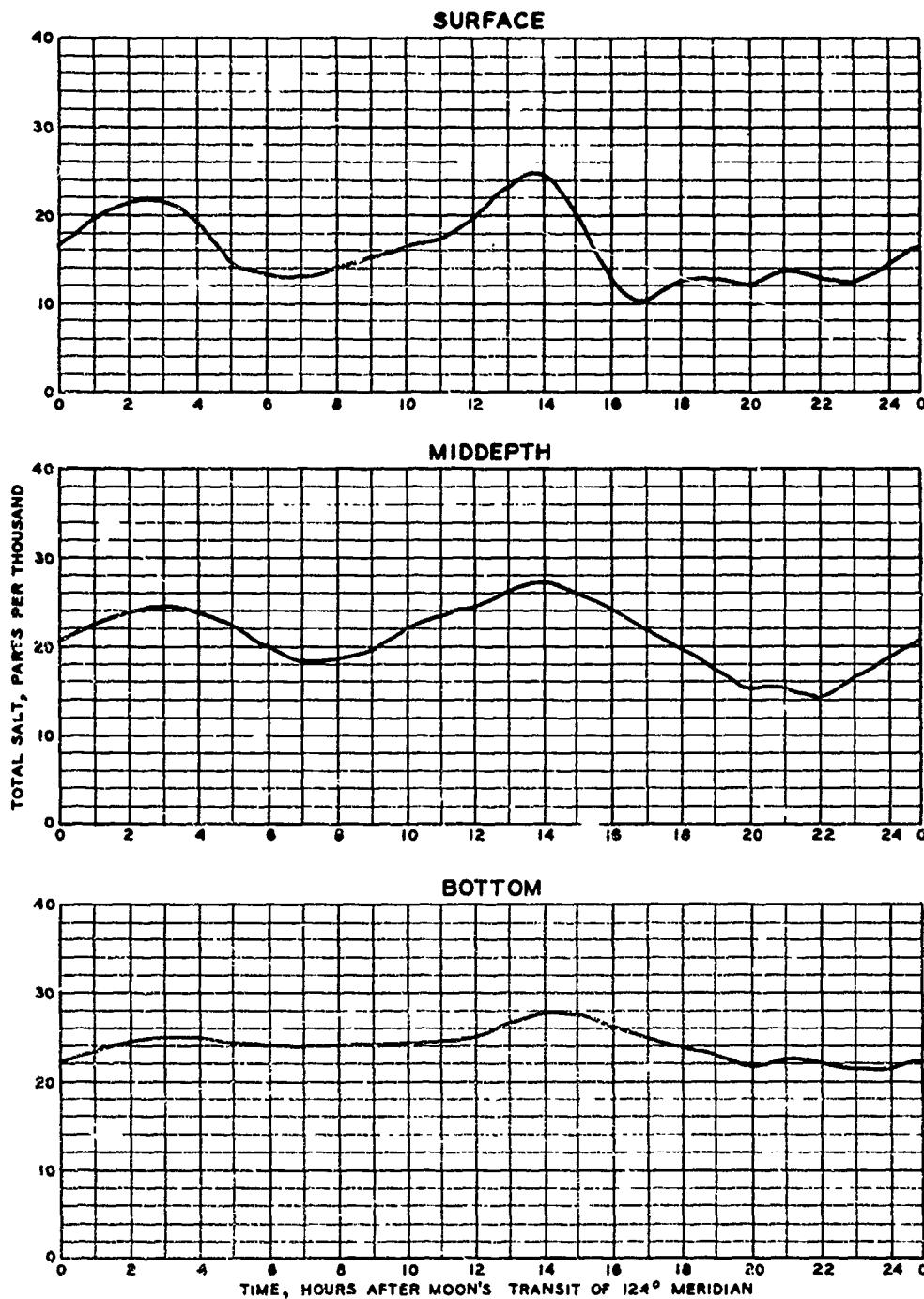
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 45

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

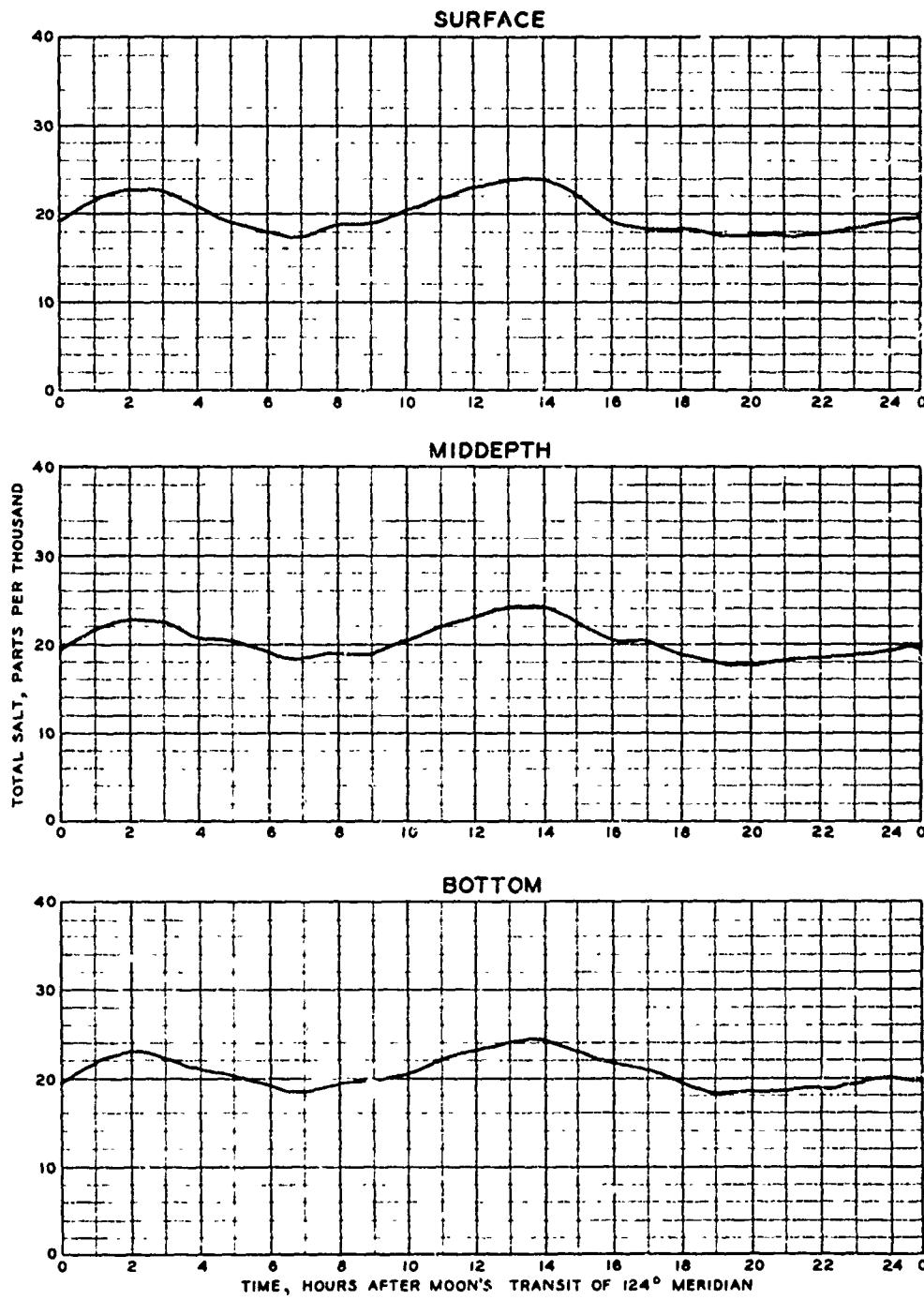
TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 —— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 46

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

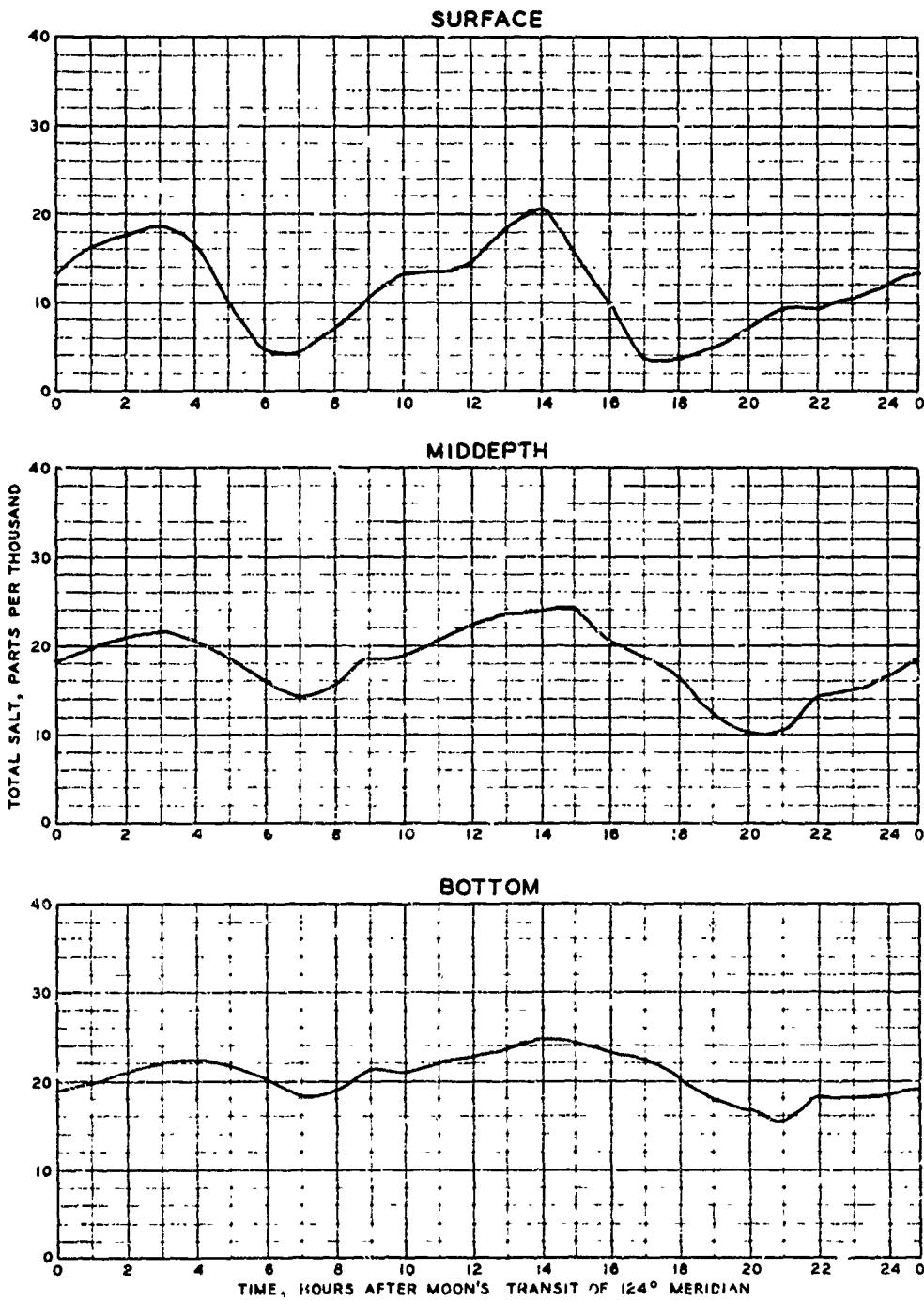
TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	330 PPT

LEGEND
— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 47

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

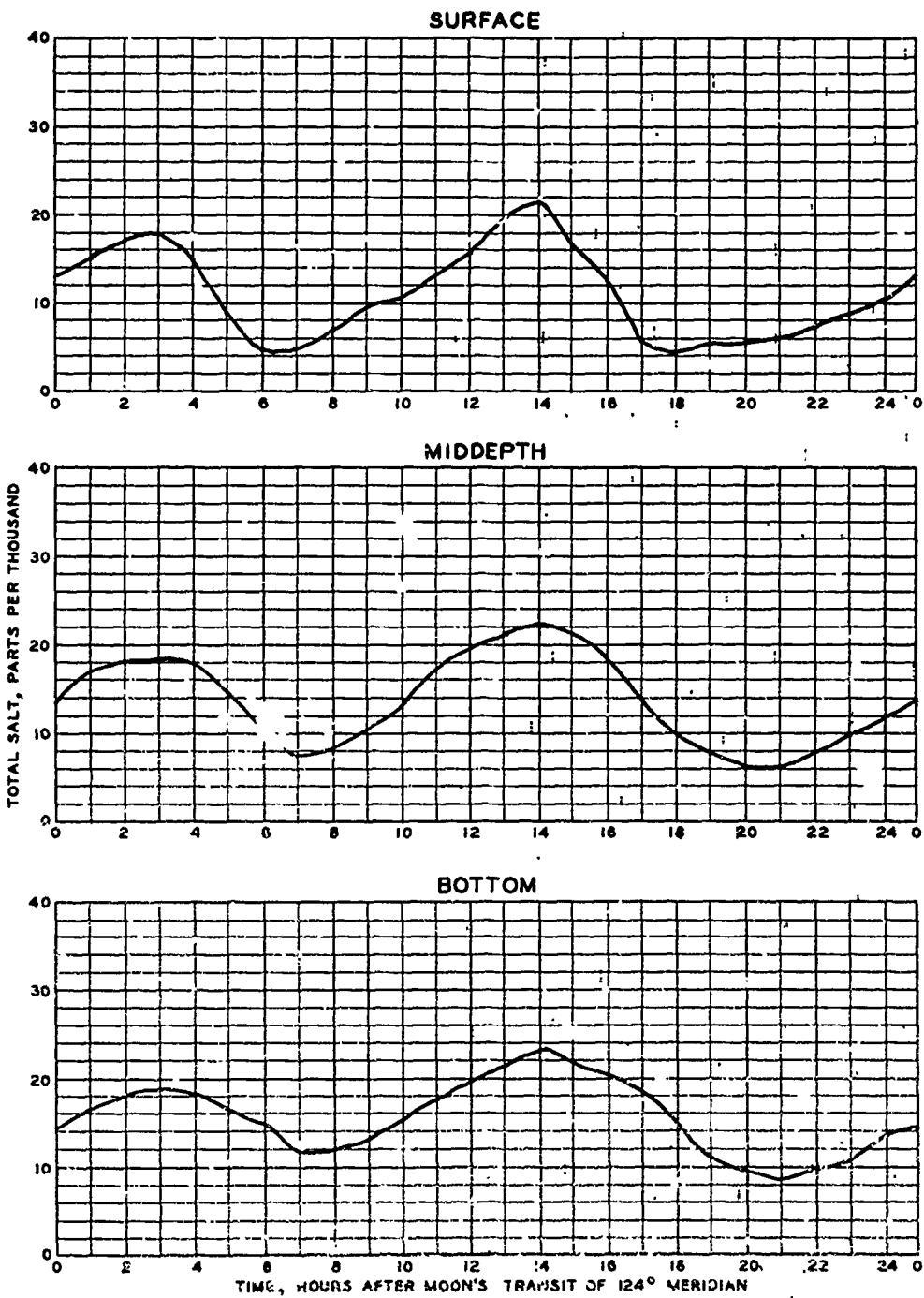
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 48

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 33.0 PPT

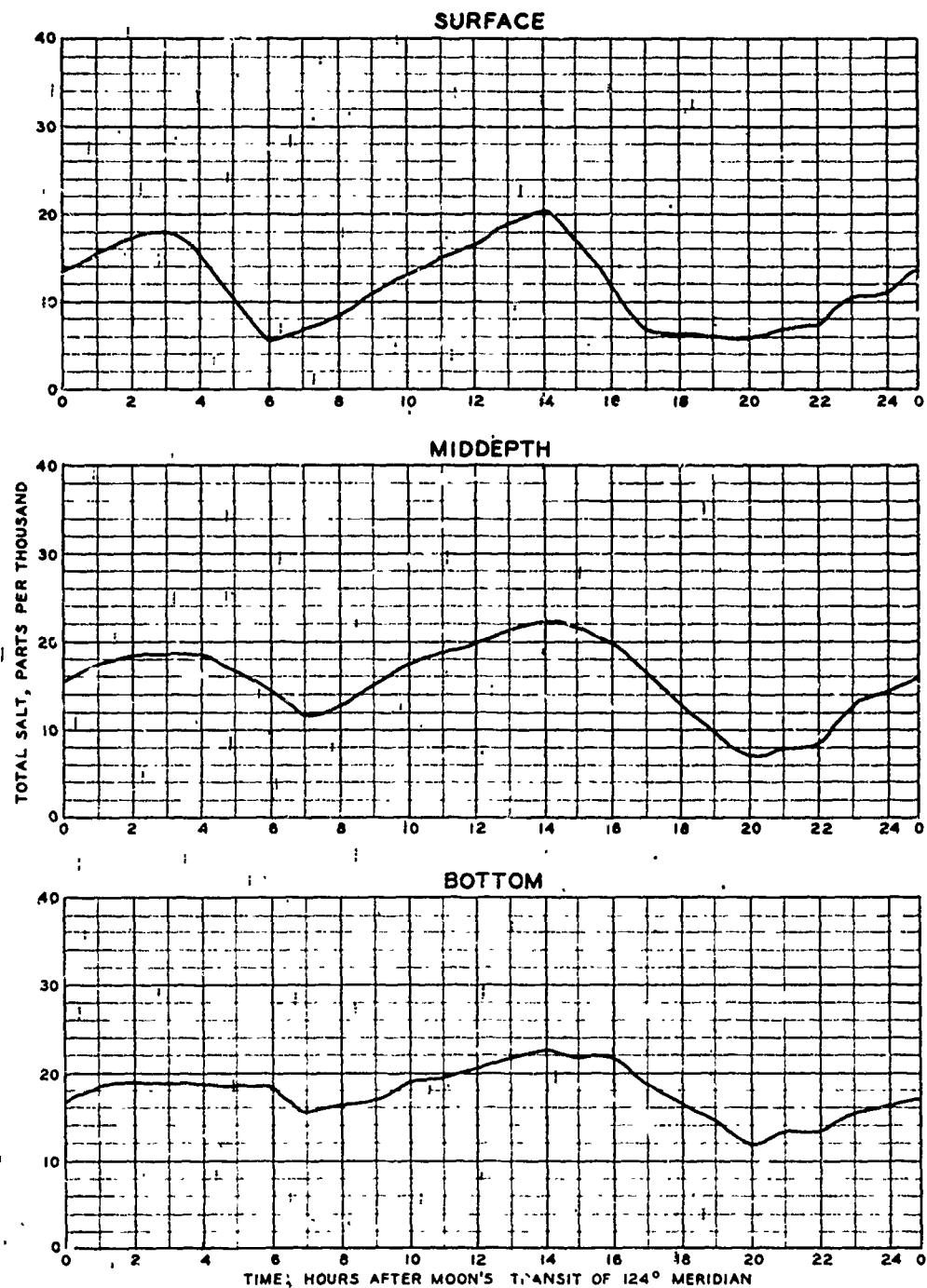
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 49

SURFACE, MIDDEPTH AND BOTTOM.



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

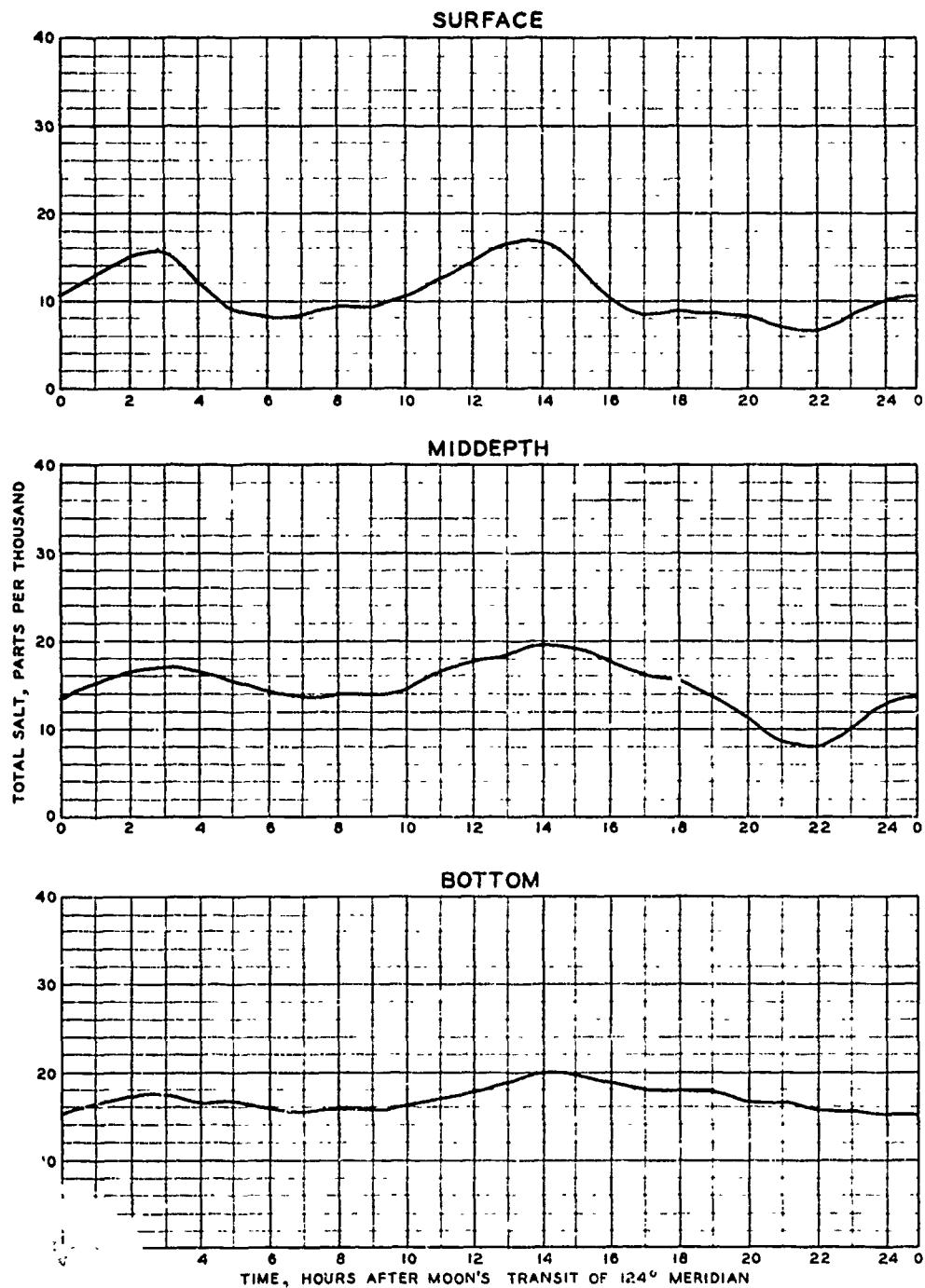
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 50

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	330 PPT

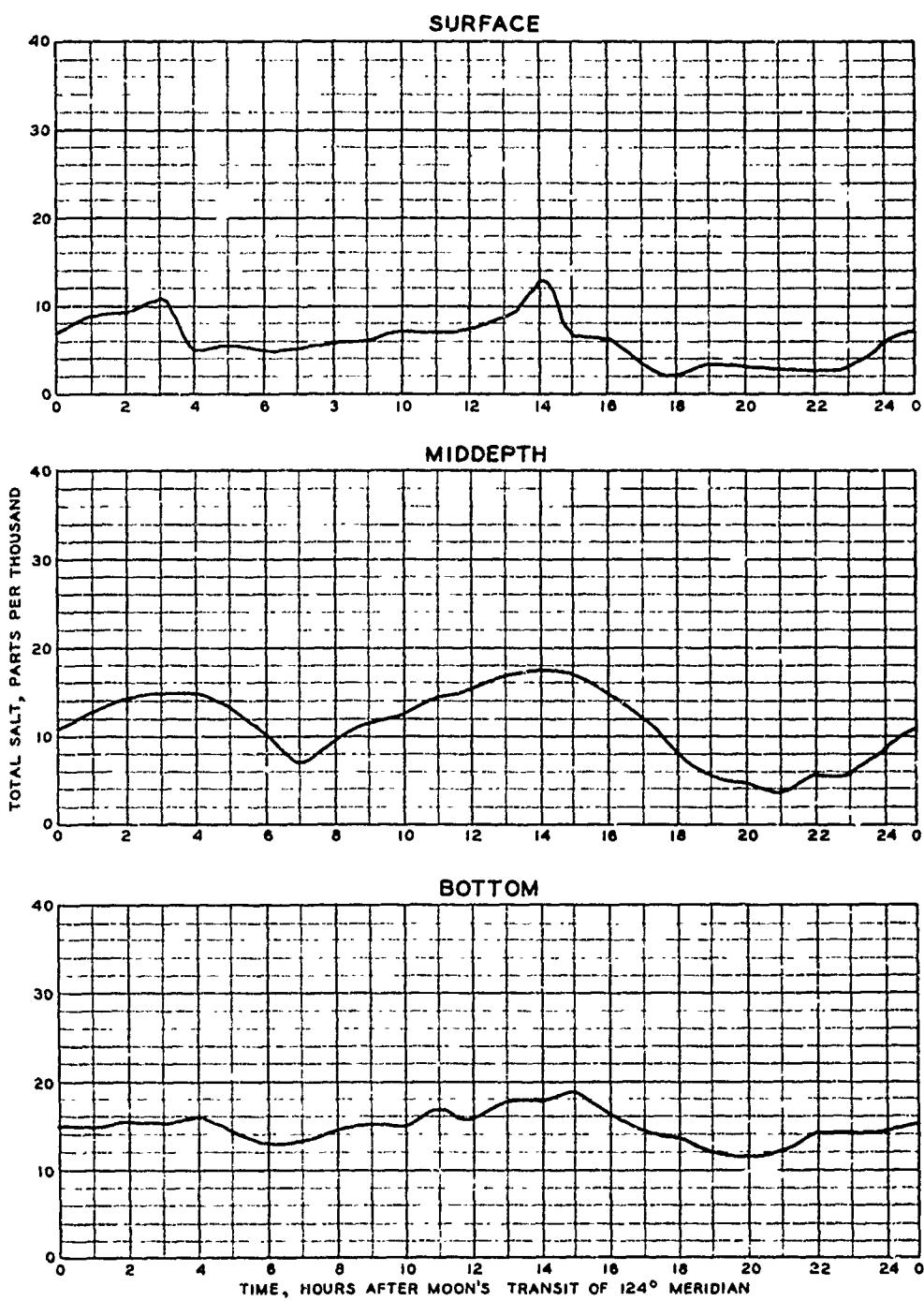
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 51

SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE MEAN
FRESH-WATER DISCHARGE .11,400 CFS
SOURCE SALINITY 330 PPT

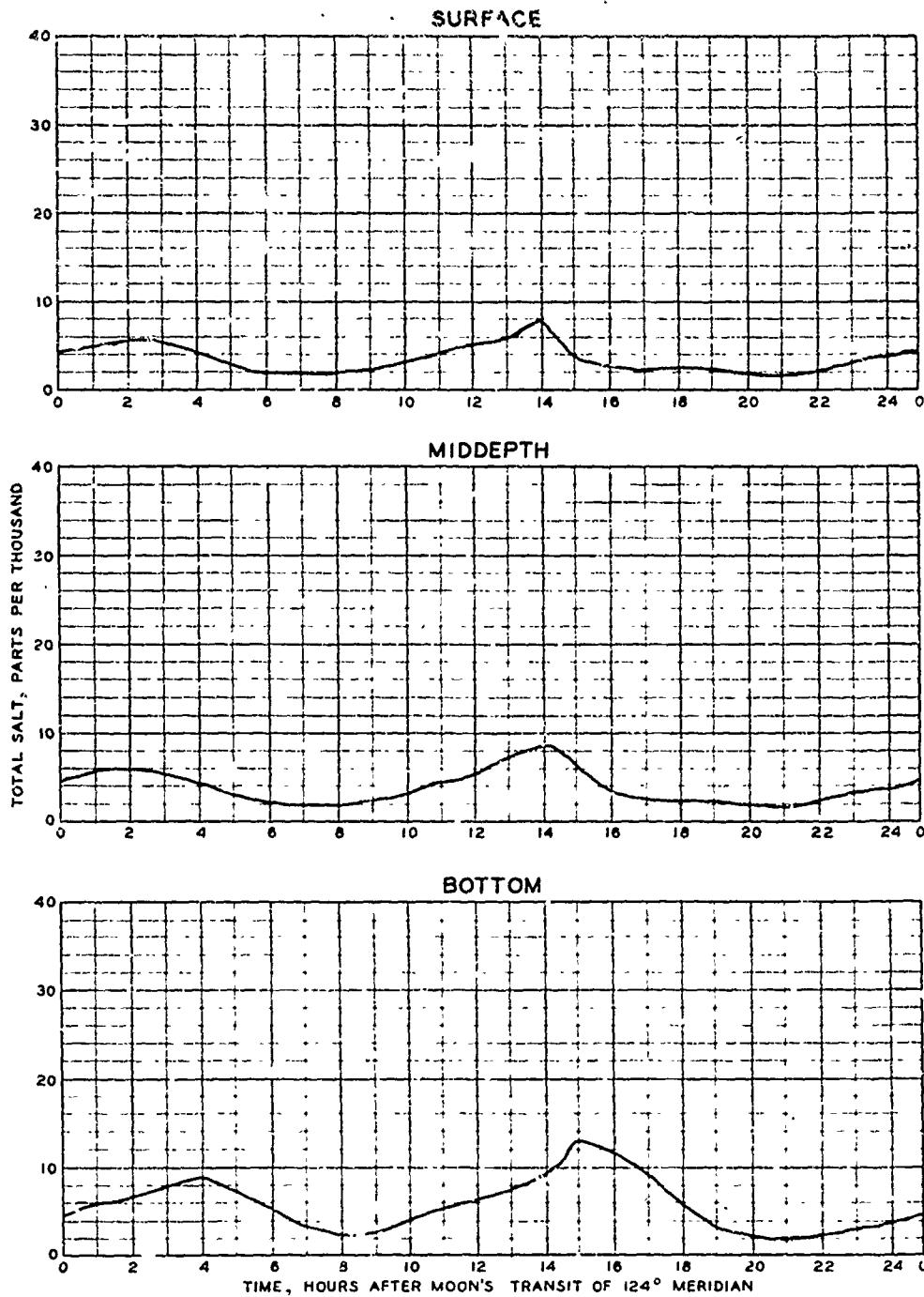
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 52
SURFACE, MIDDEPTH AND BOTTOM

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PLATE 191



MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

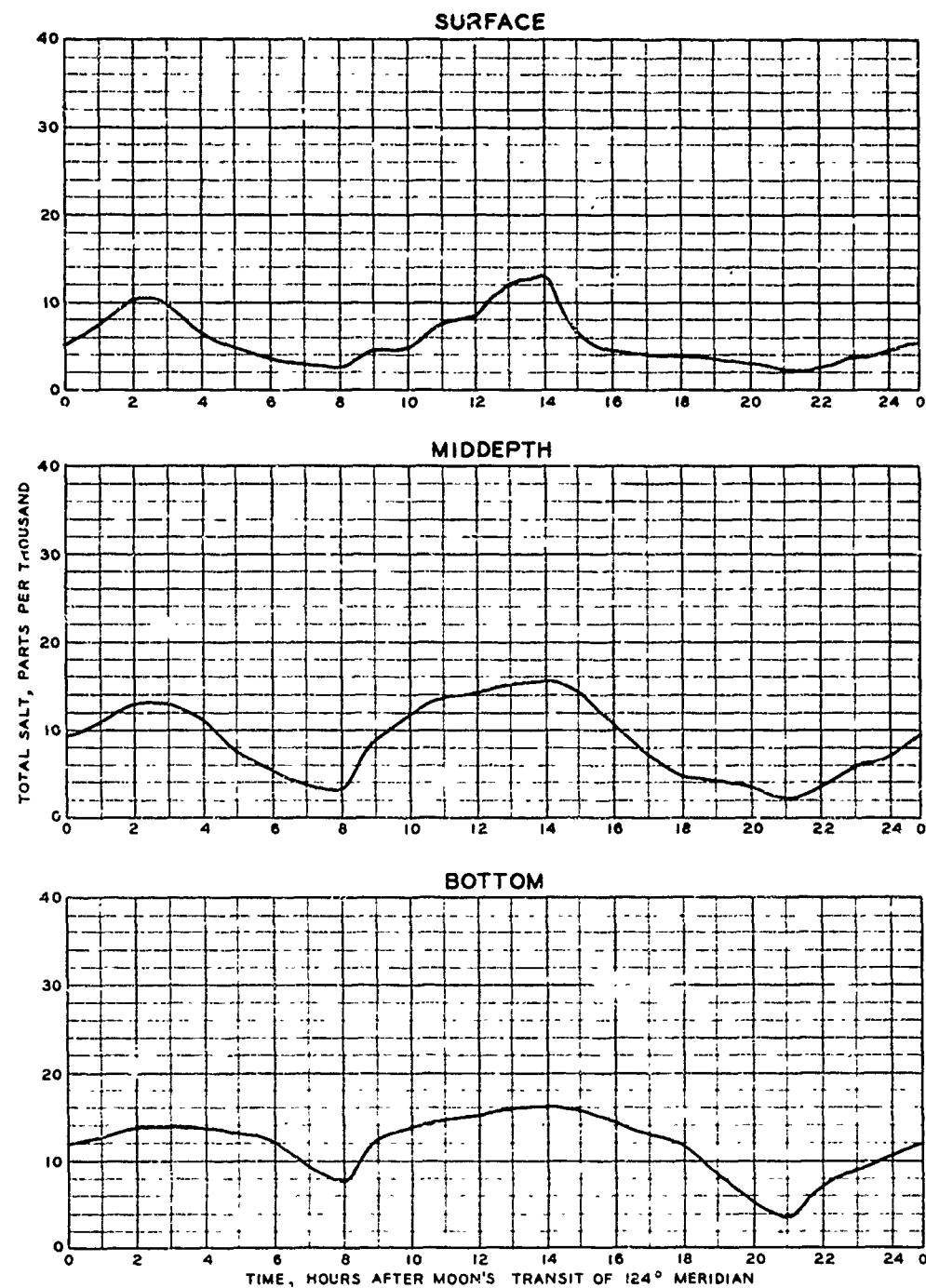
LEGEND

— BASE TEST

BASE TEST
 SALINITY OBSERVATIONS

STATION 53

SURFACE, MIDDEPTH AND BOTTOM



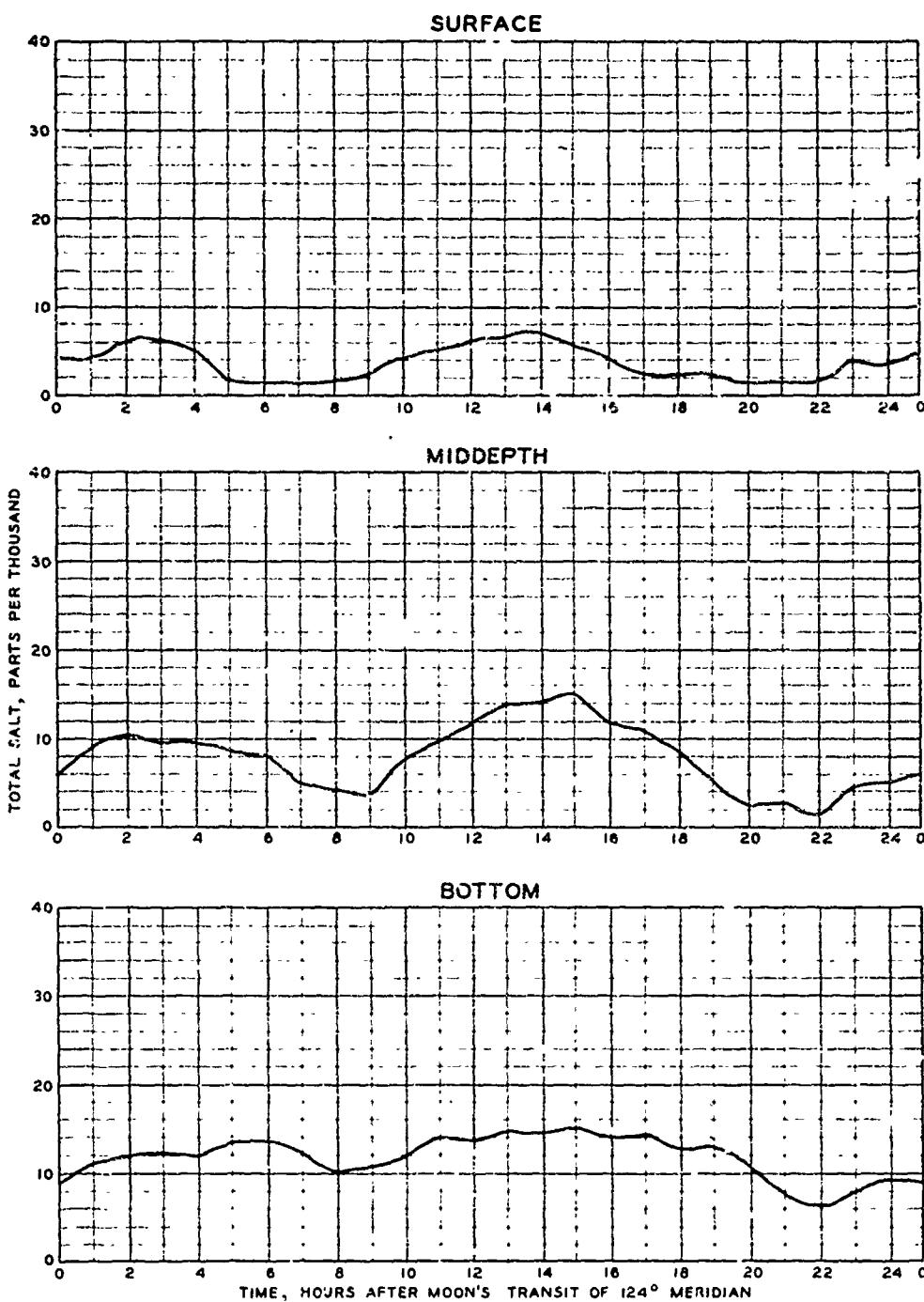
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**
STATION 54
SURFACE, MIDDEPTH AND BOTTOM



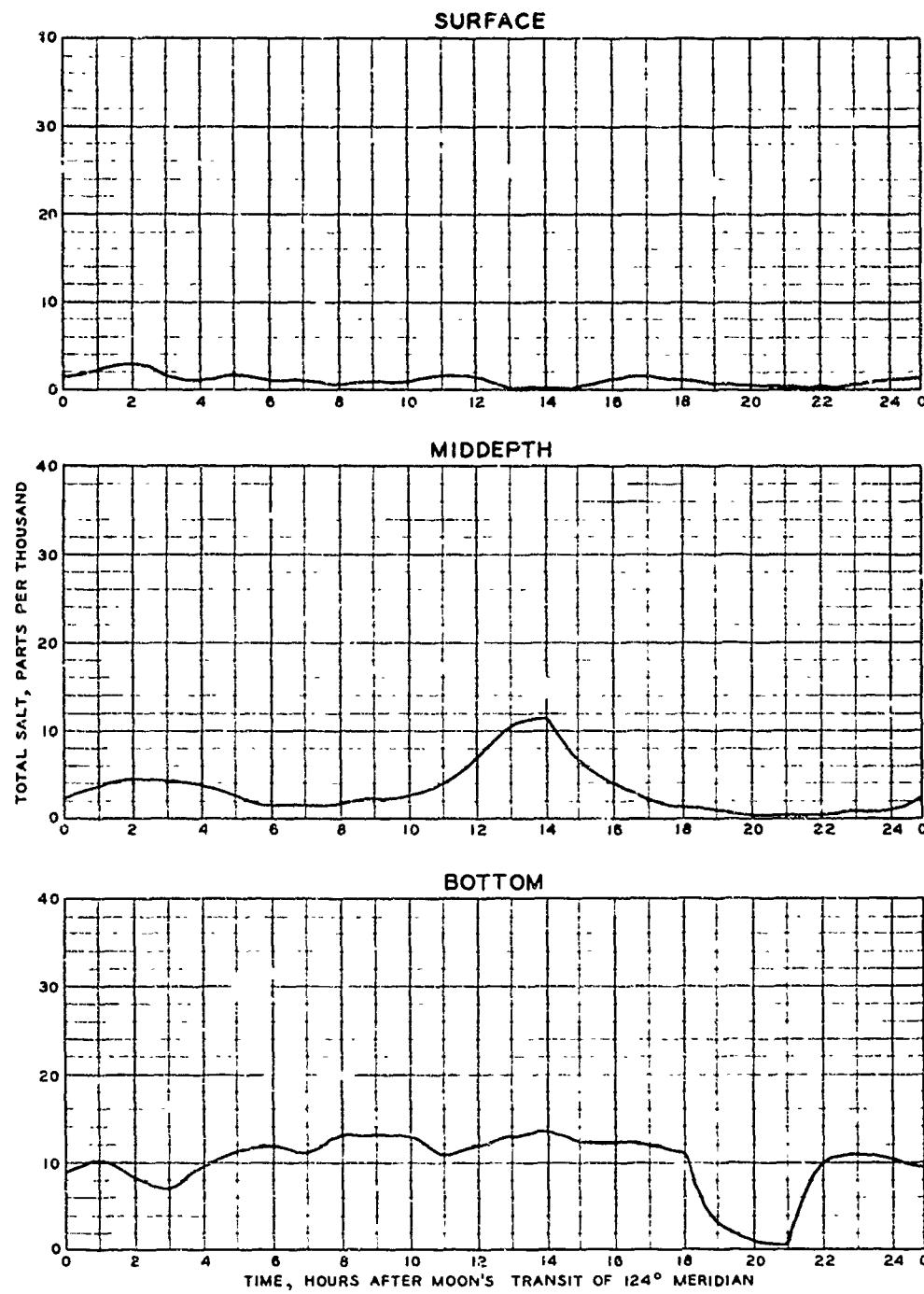
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE 11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 55
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	11,400 CFS
SOURCE SALINITY	33.0 PPT

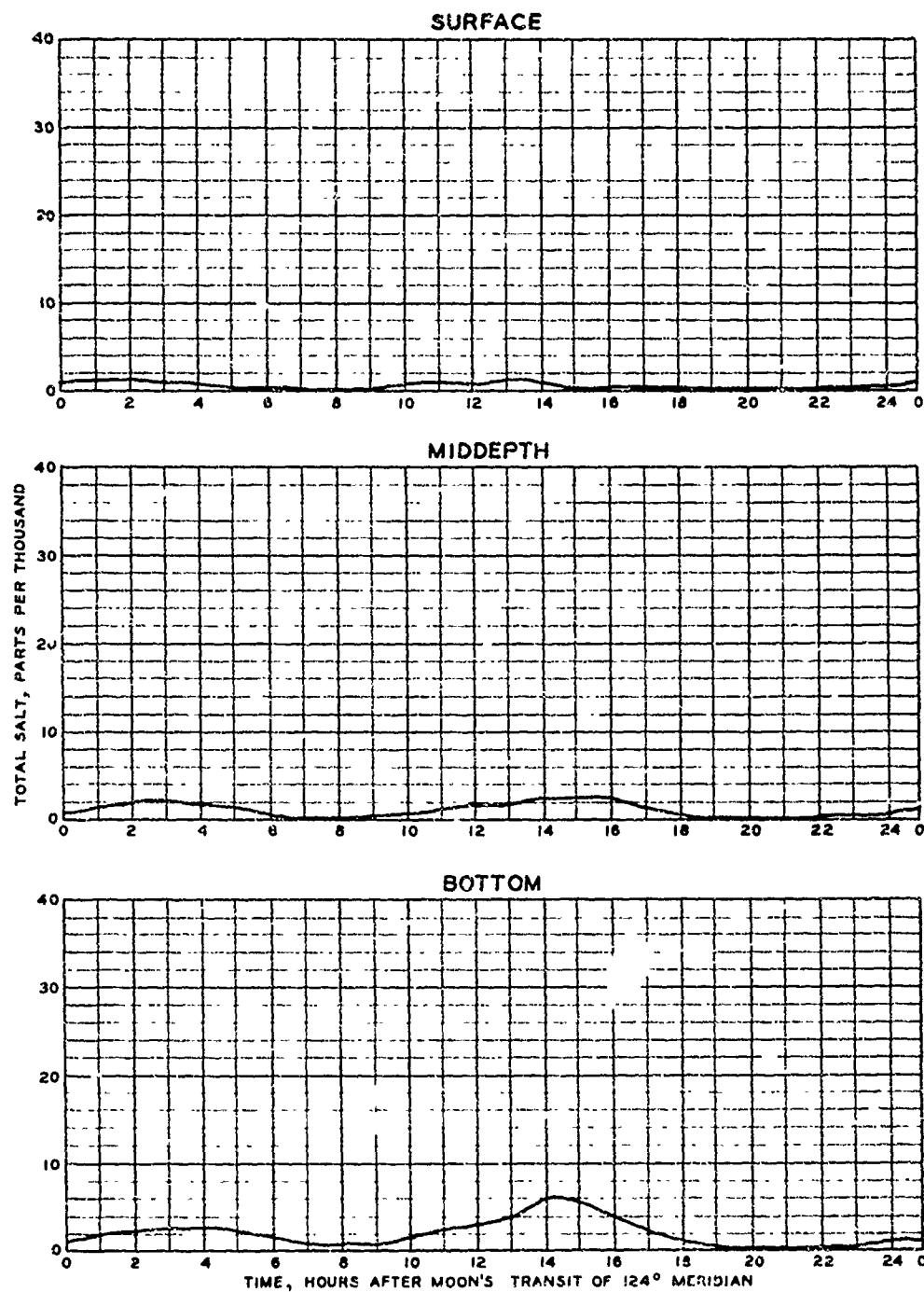
LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 56

SURFACE, MIDDEPTH AND BOTTOM



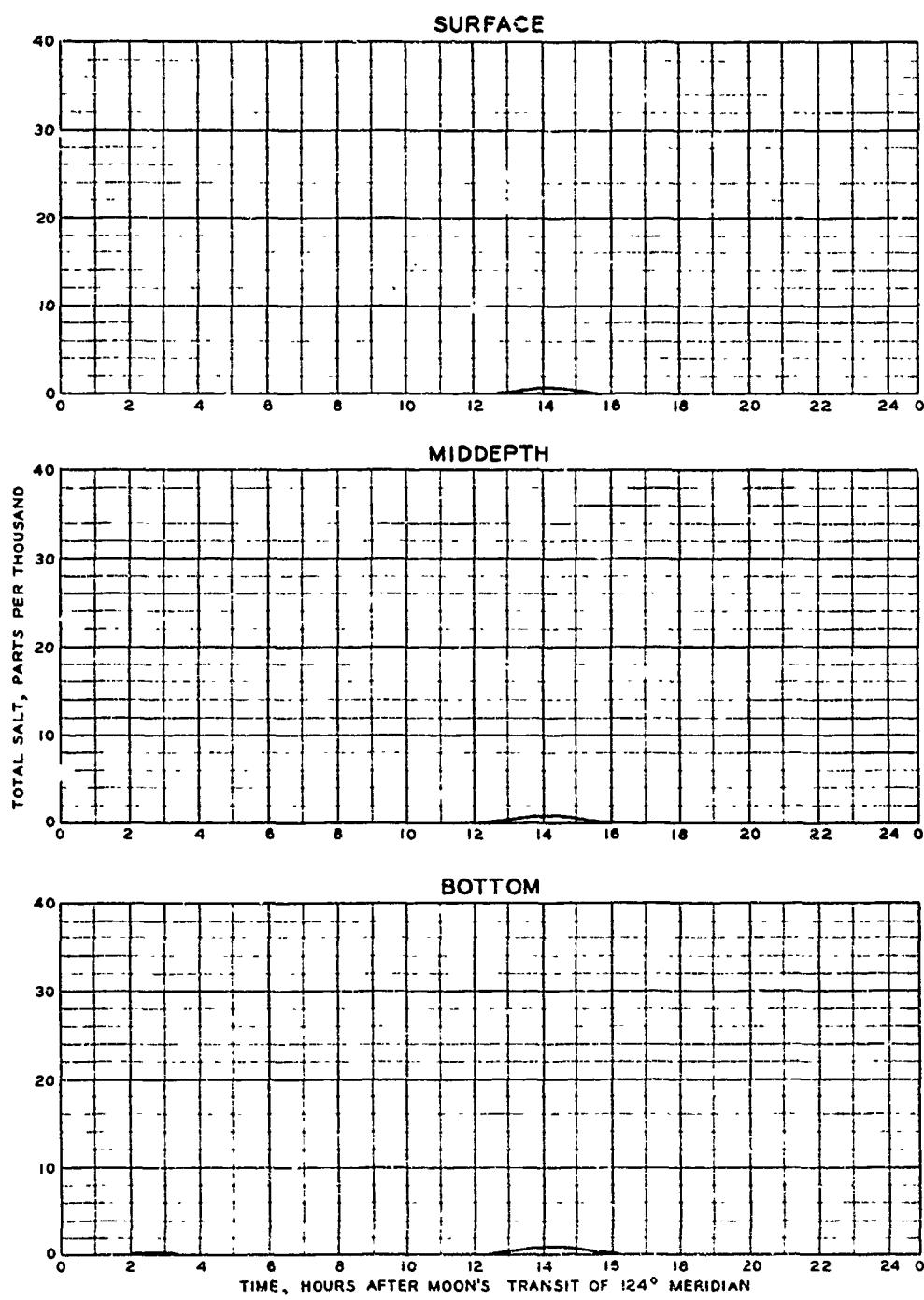
MODEL TEST DATA

TIDE MEAN
 FRESH-WATER DISCHARGE .11,400 CFS
 SOURCE SALINITY 330 PPT

LEGEND
 — BAS' TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 57
SURFACE, MIDDEPTH AND BOTTOM



MODEL TEST DATA

TIDE	MEAN
FRESH-WATER DISCHARGE	.11,400 CFS
SOURCE SALINITY	330 PPT

LEGEND

— BASE TEST

**BASE TEST
SALINITY OBSERVATIONS**

STATION 58

SURFACE, MIDDEPTH AND BOTTOM

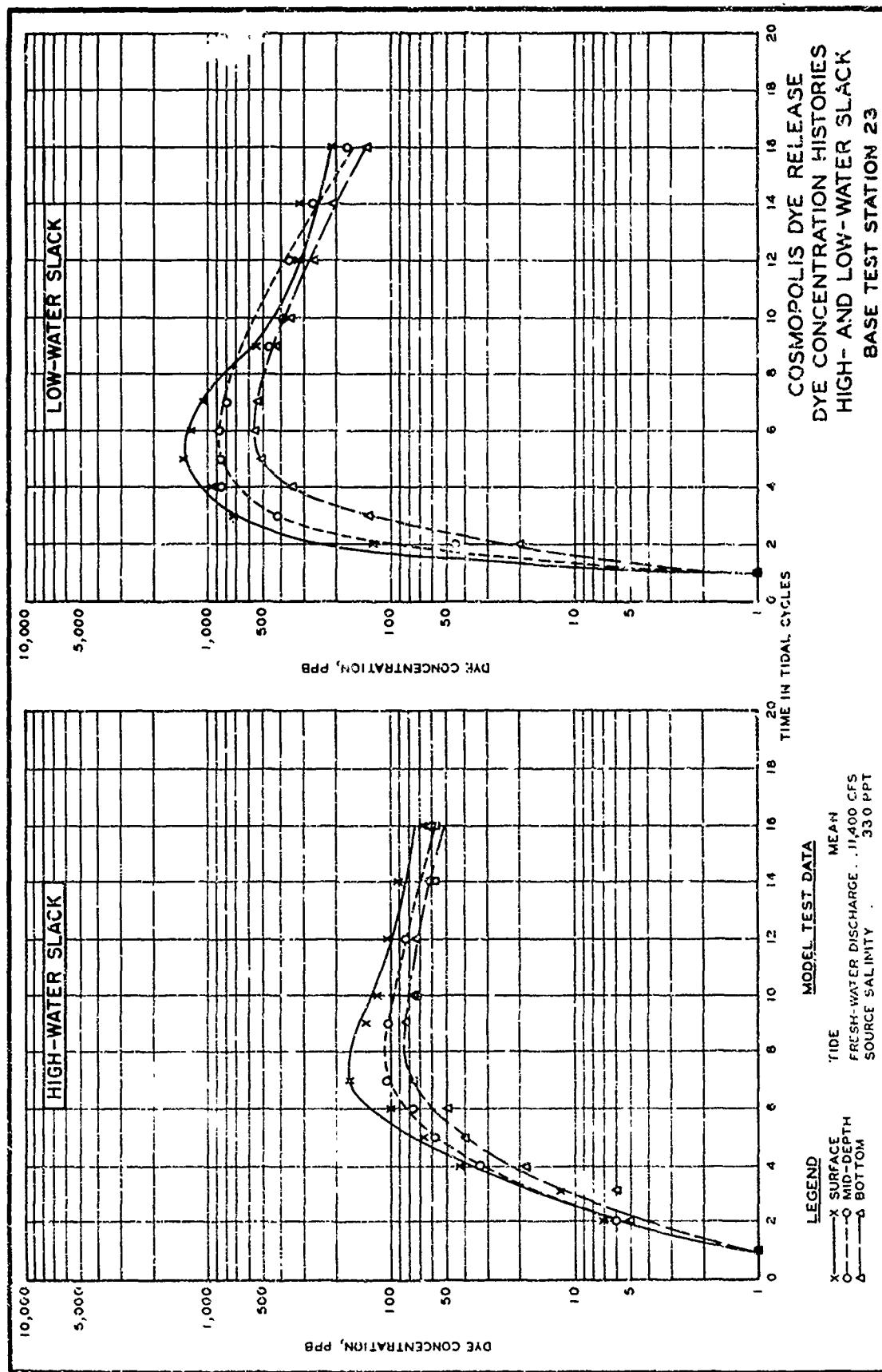
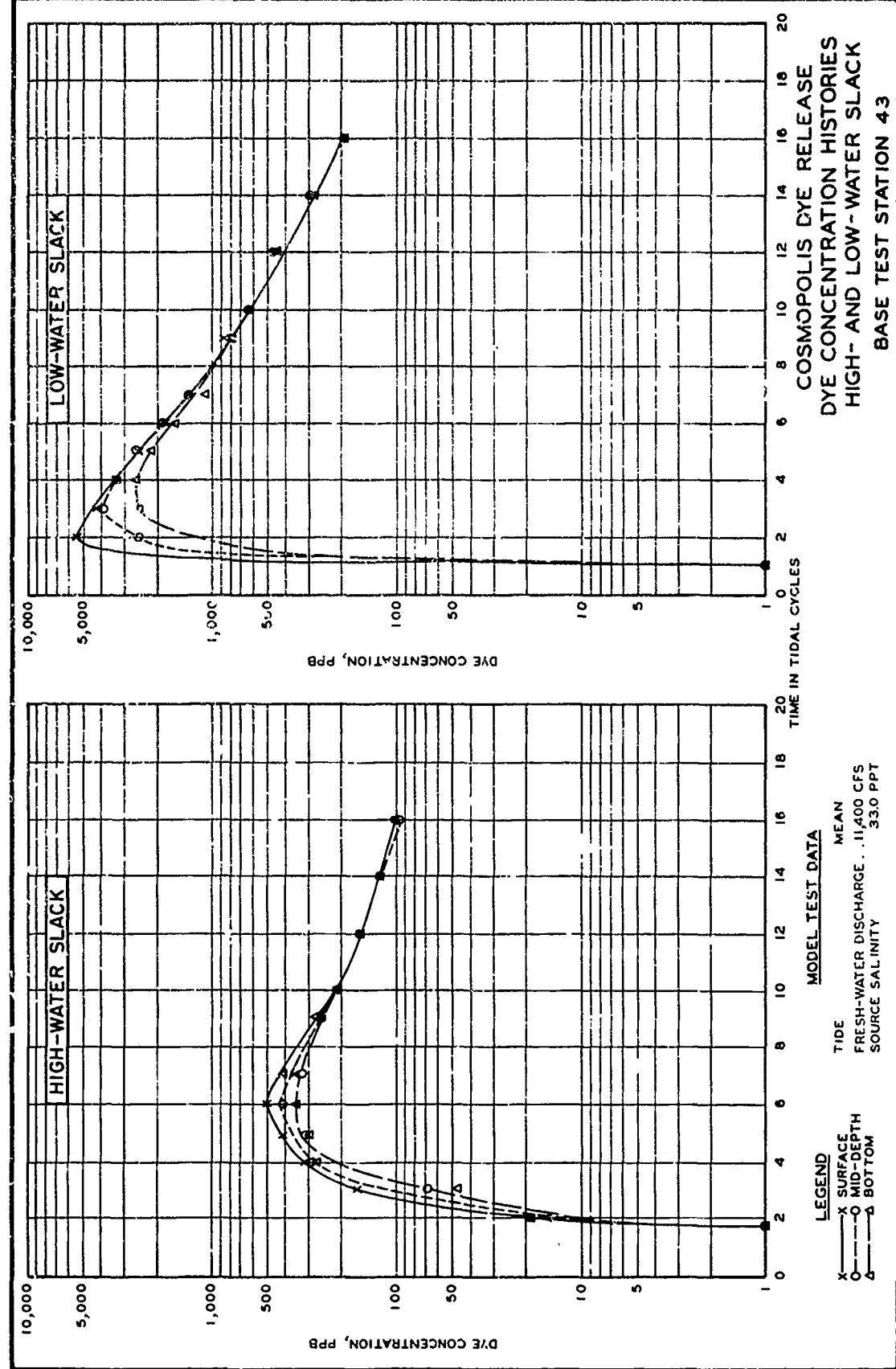


PLATE 198

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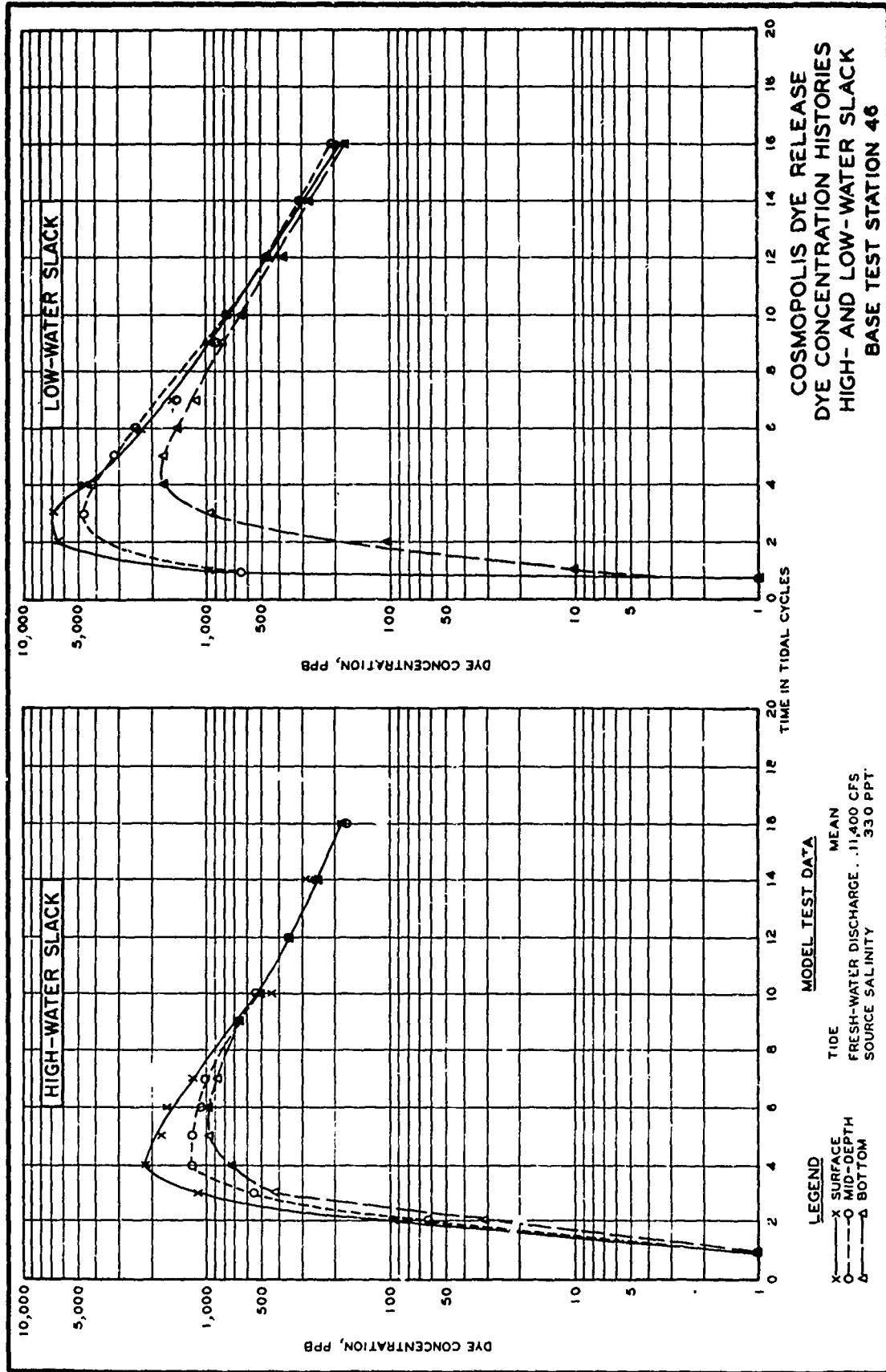


PLATE 200

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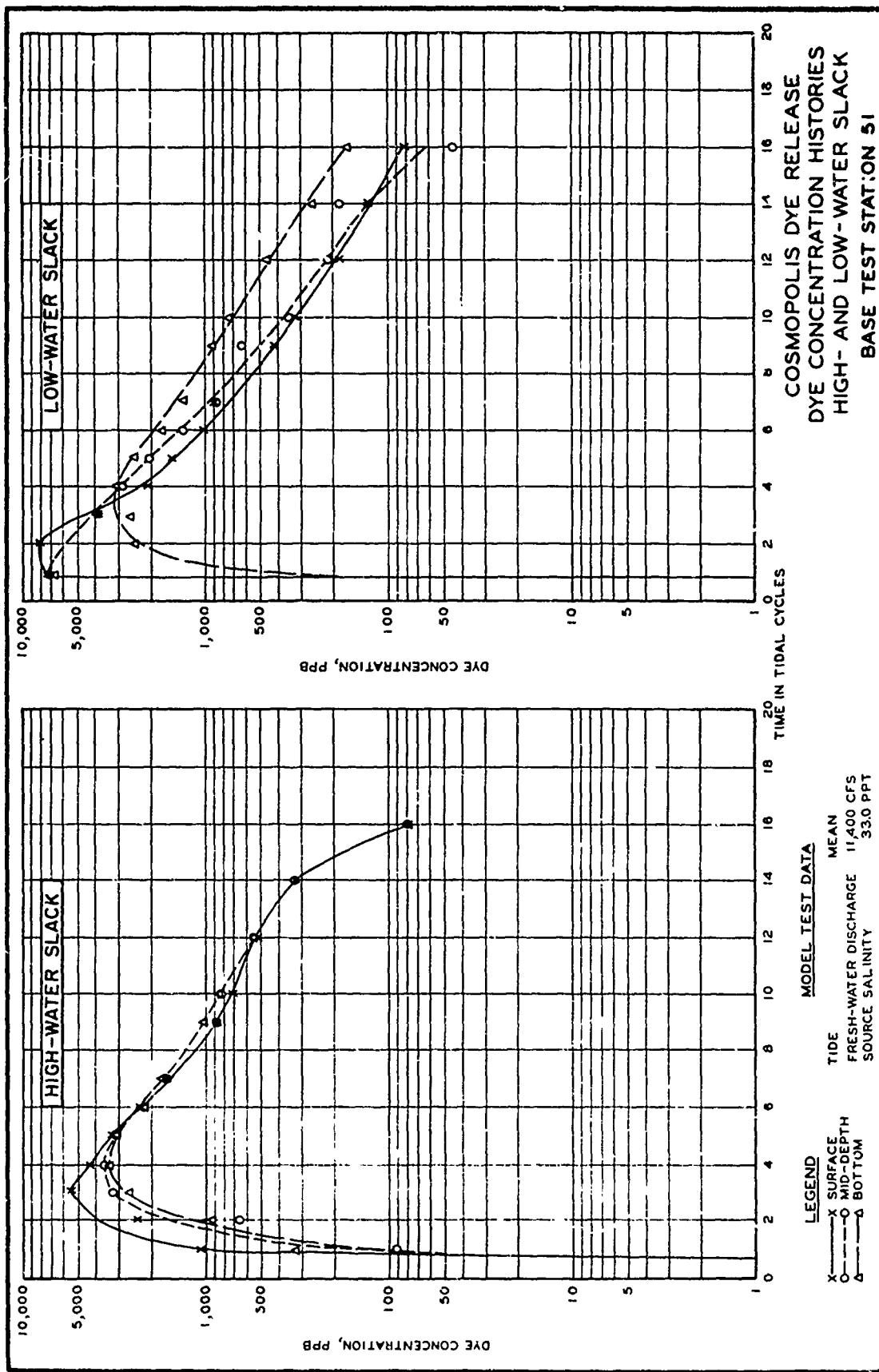
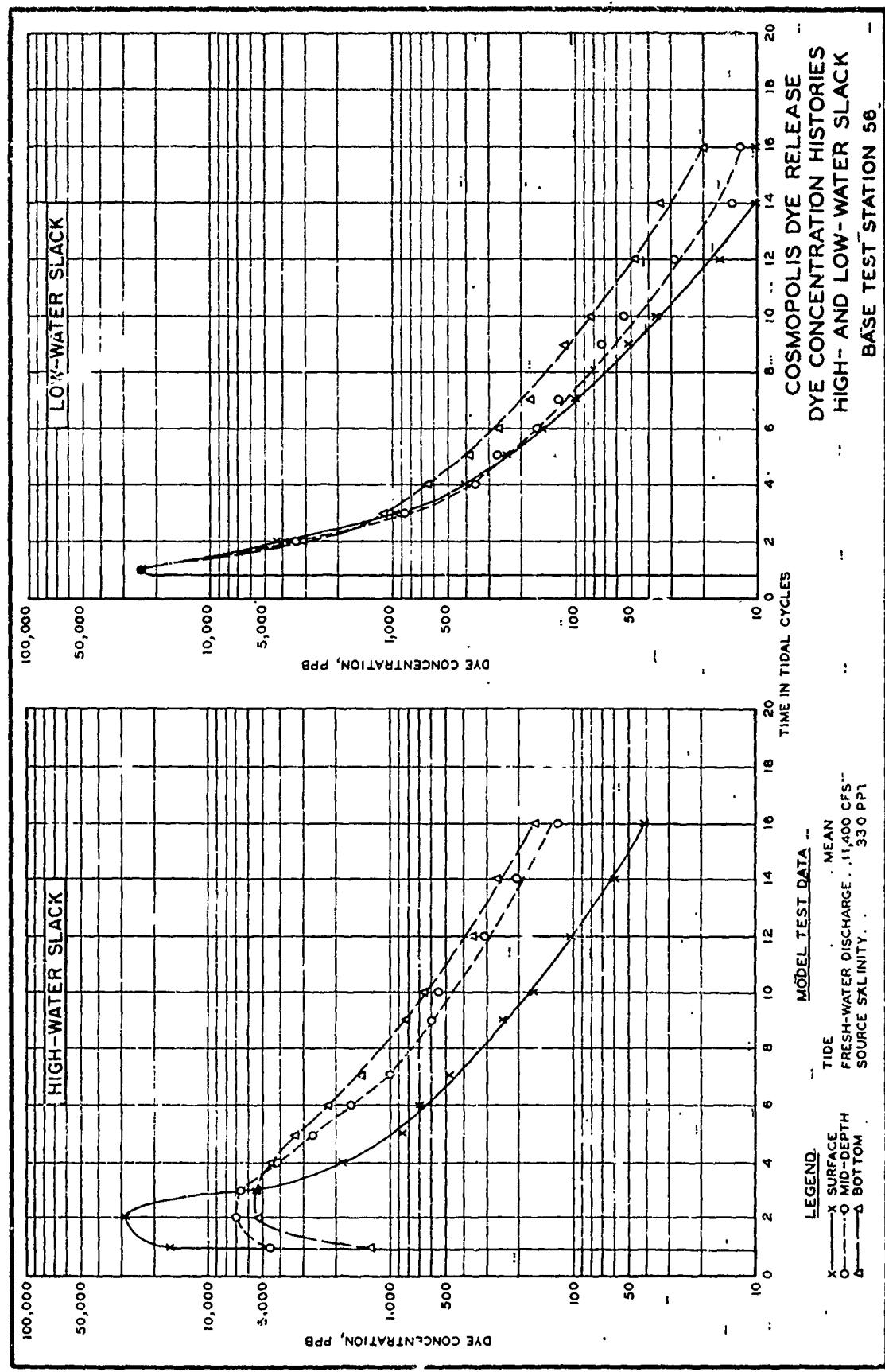
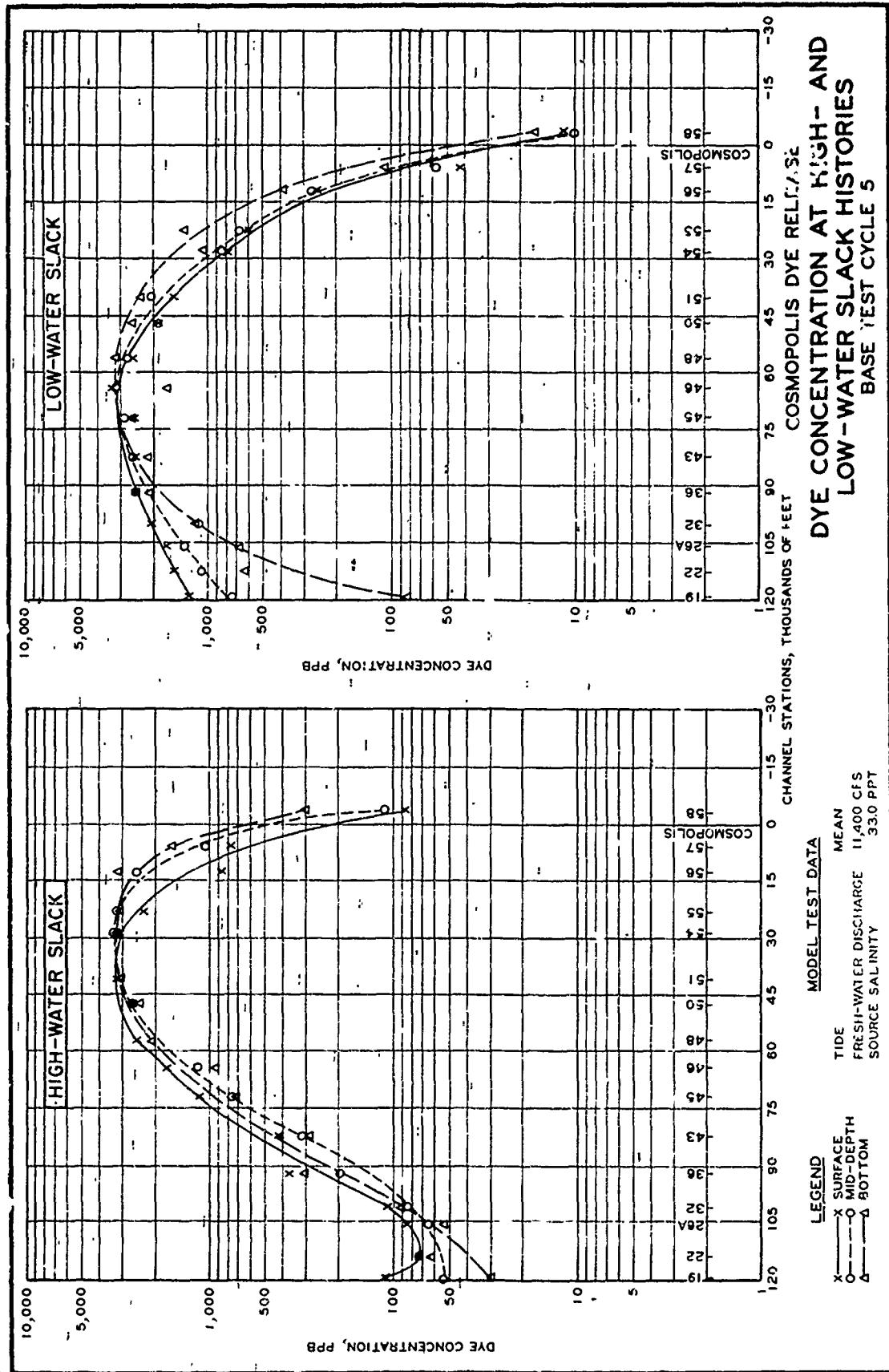


PLATE 201

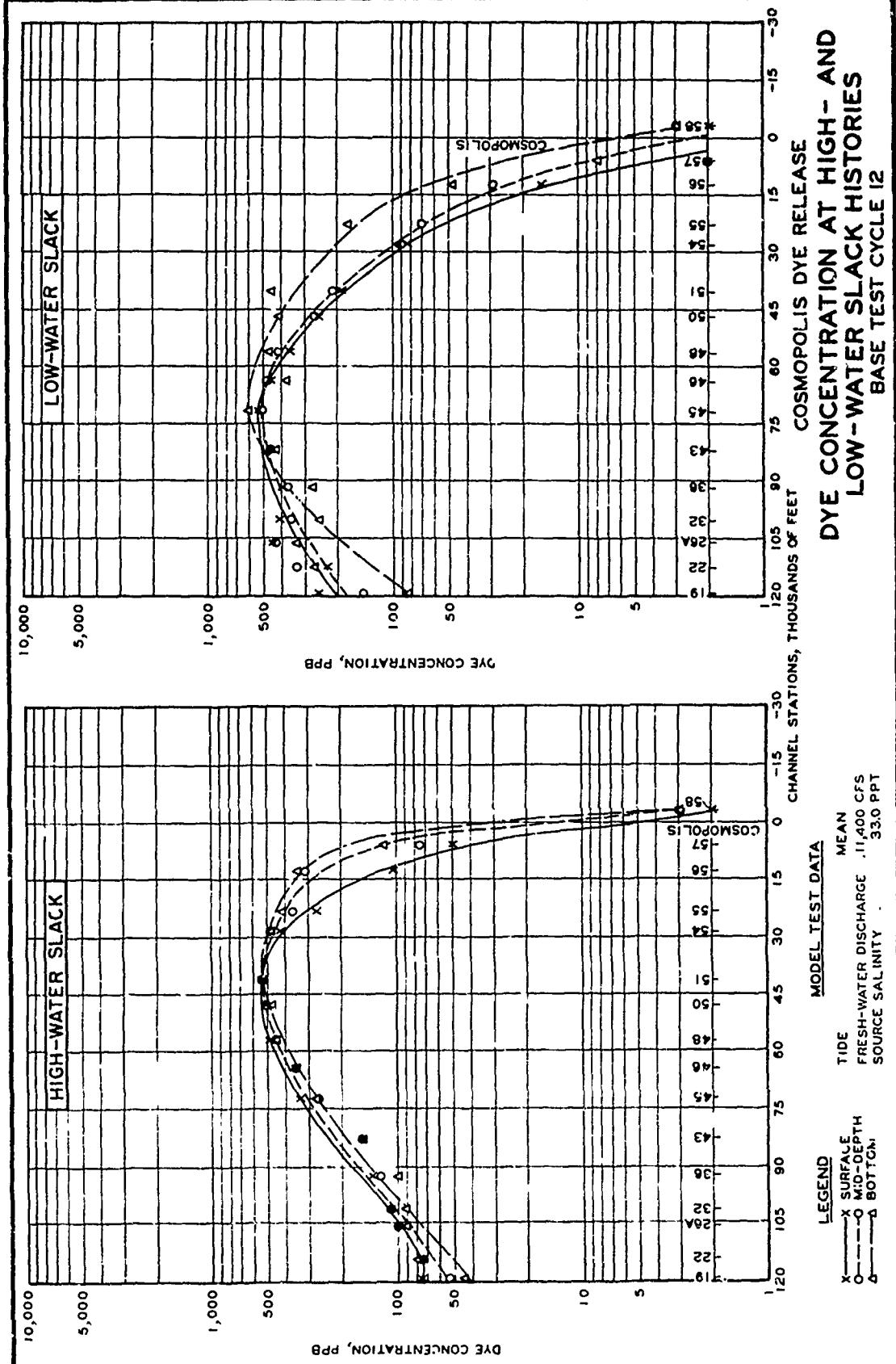


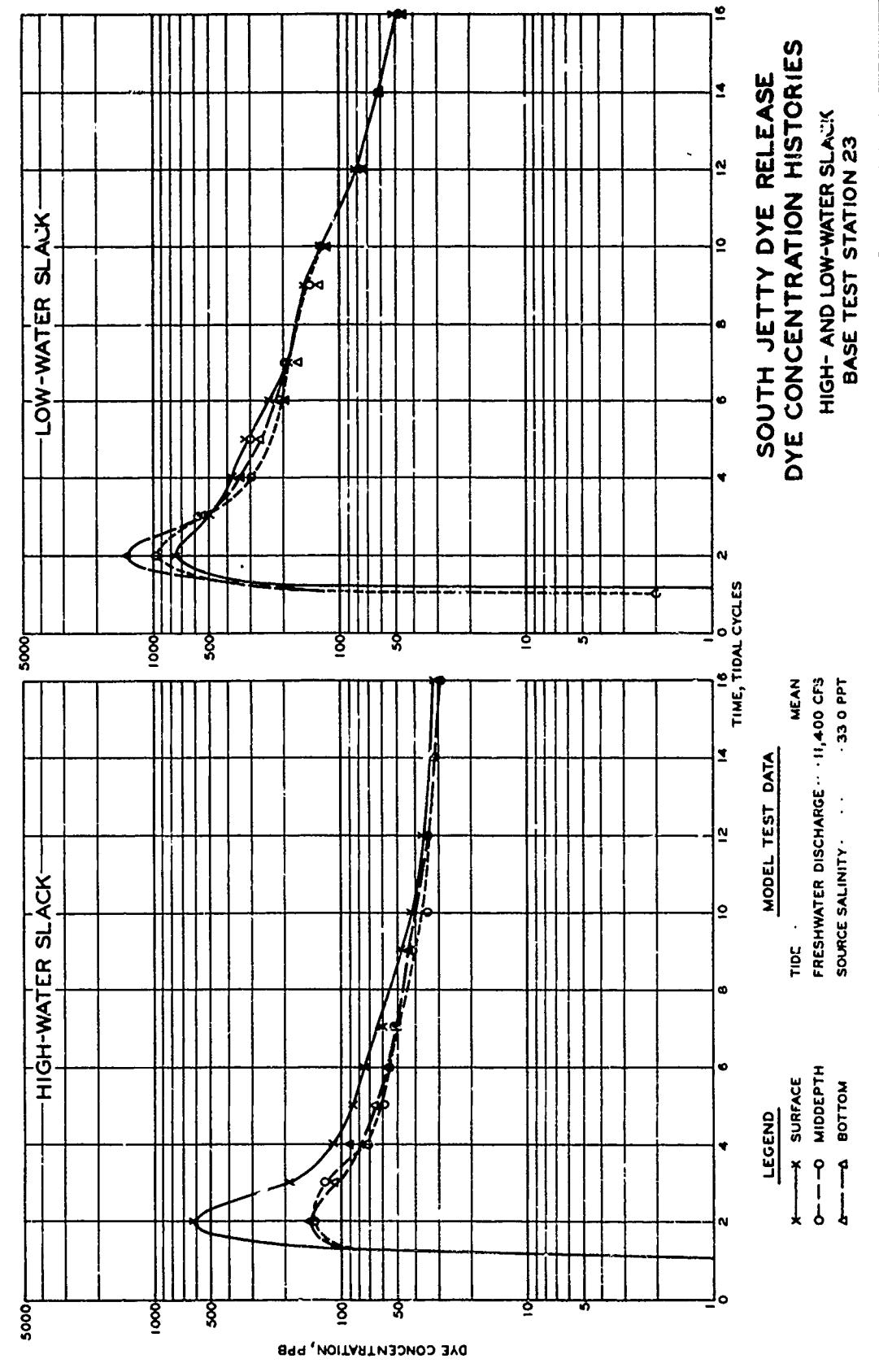


COSMOPOLIS DYE RELEASE
DYE CONCENTRATION AT HIGH - AND
LOW-WATER SLACK HISTORIES
BASE TEST CYCLE 12

MODEL TEST DATA

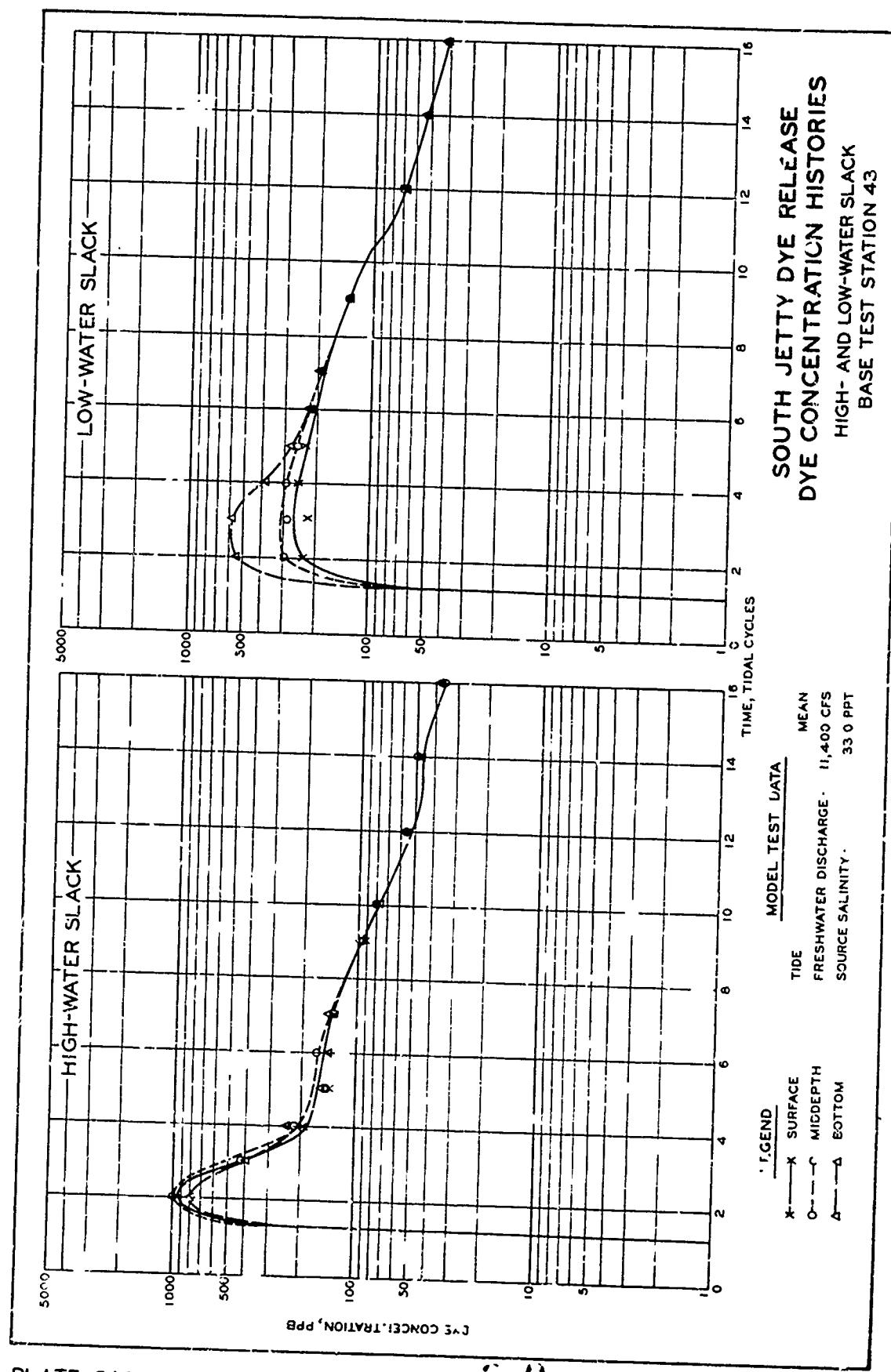
LEGEND	TIDE
X SURFACE	FRESH-WATER DISCHARGE .11,400 CFS
O MID-DEPTH	SOURCE SALINITY 33.0 PPT
A BOTTOM	





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PLATE 205



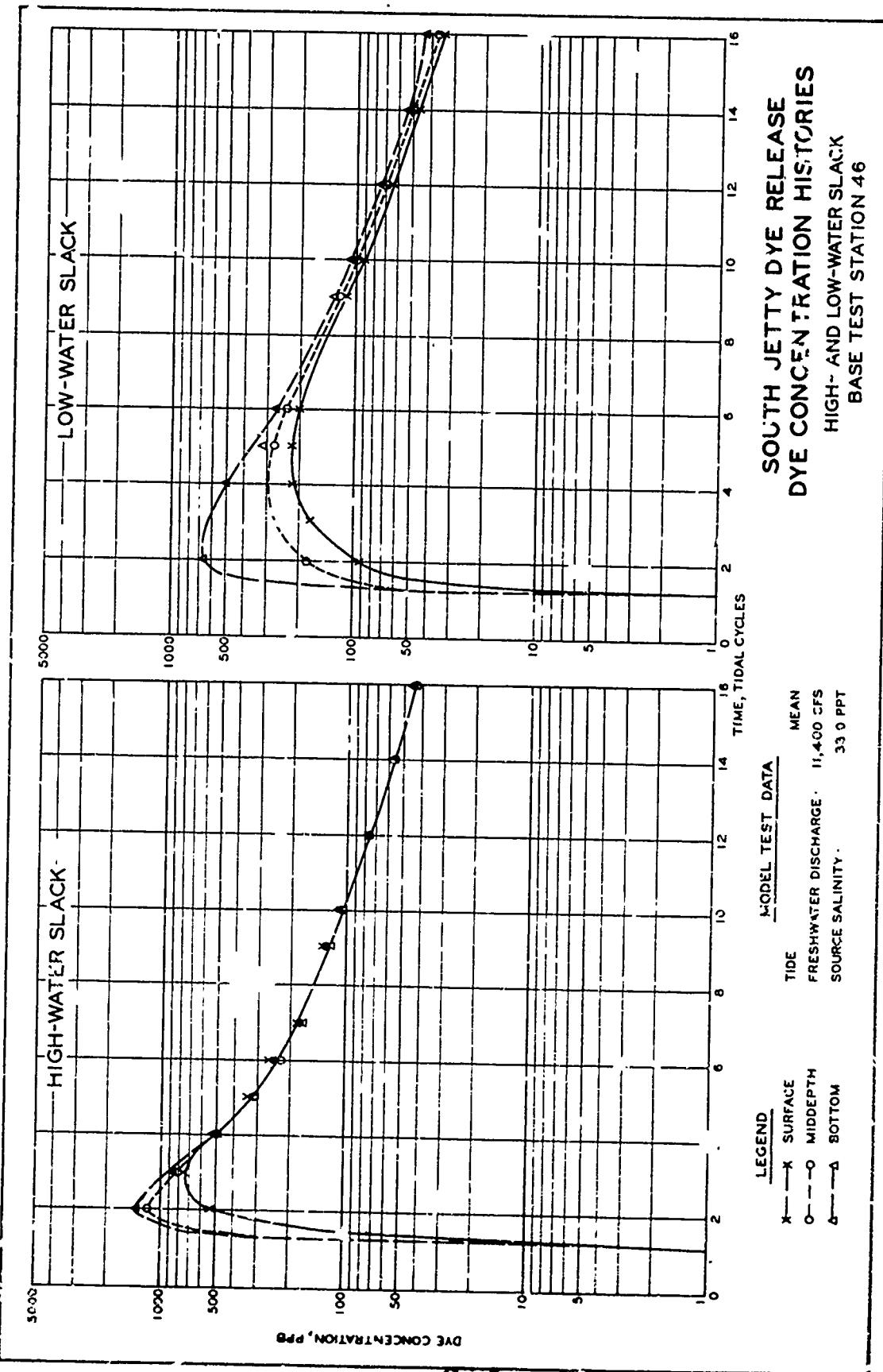


PLATE 267

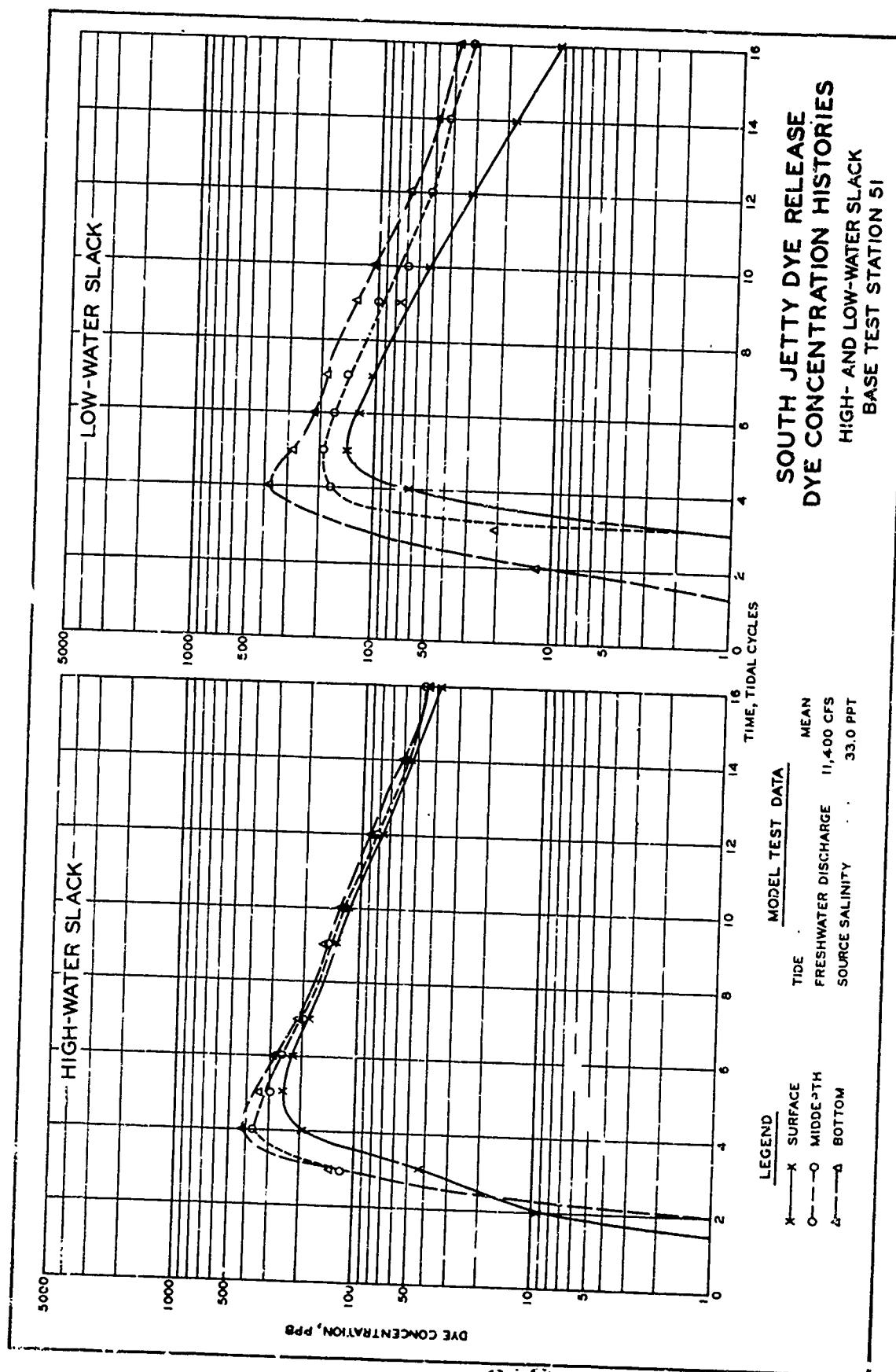
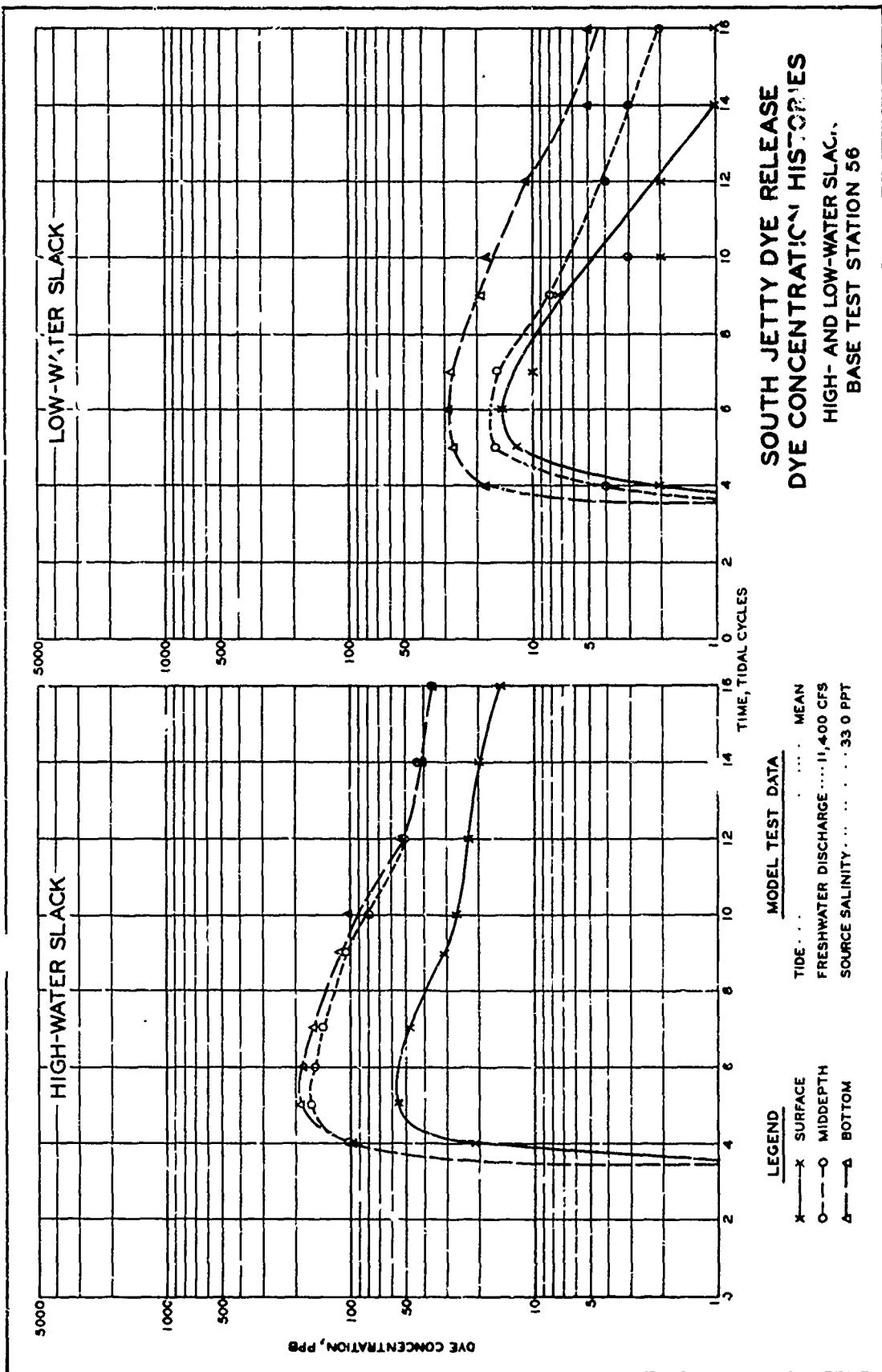
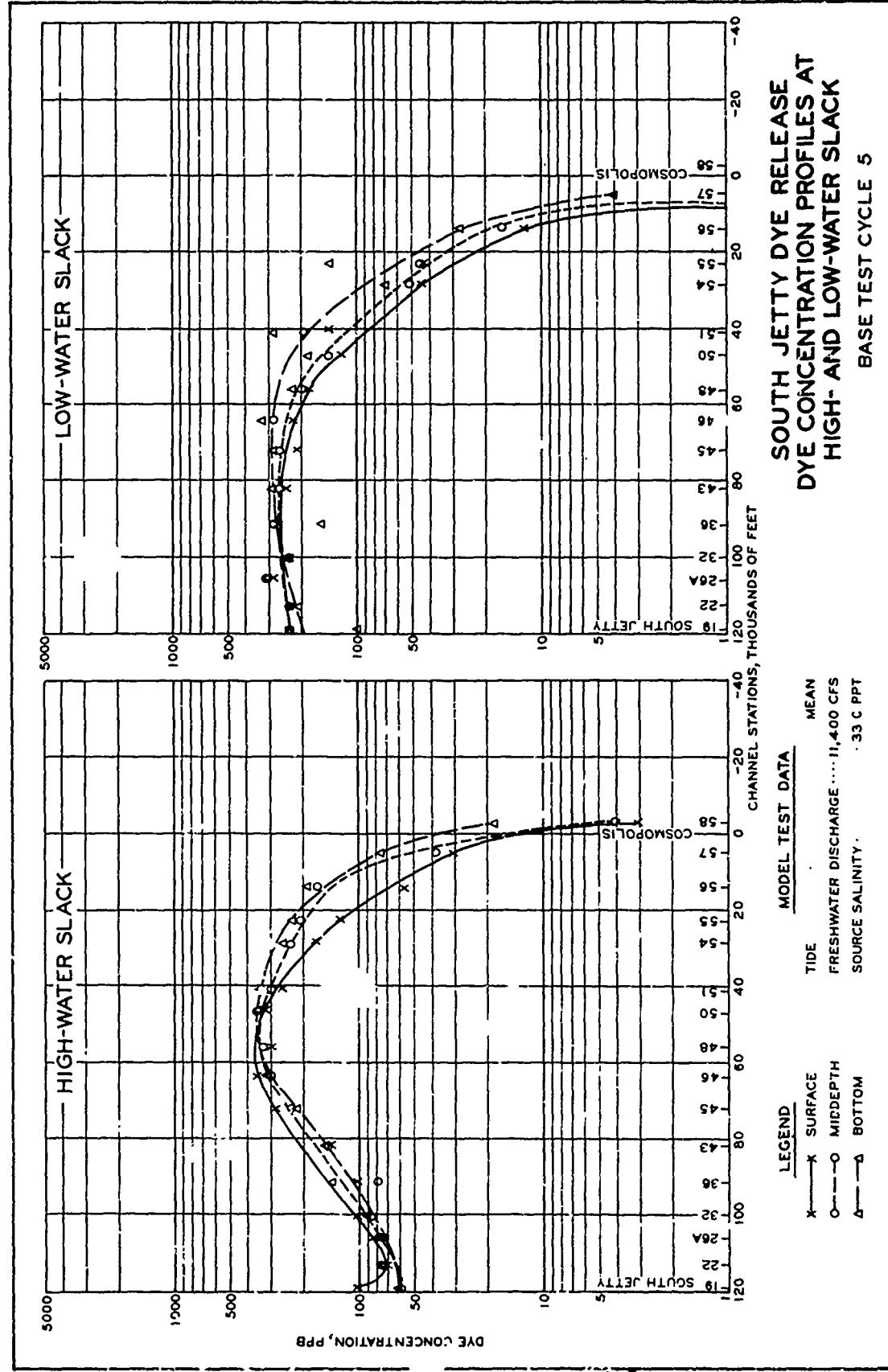


PLATE 208



SOUTH JETTY DYE RELEASE
DYE CONCENTRATION PROFILES AT
HIGH- AND LOW-WATER SLACK
BASE TEST CYCLE 5



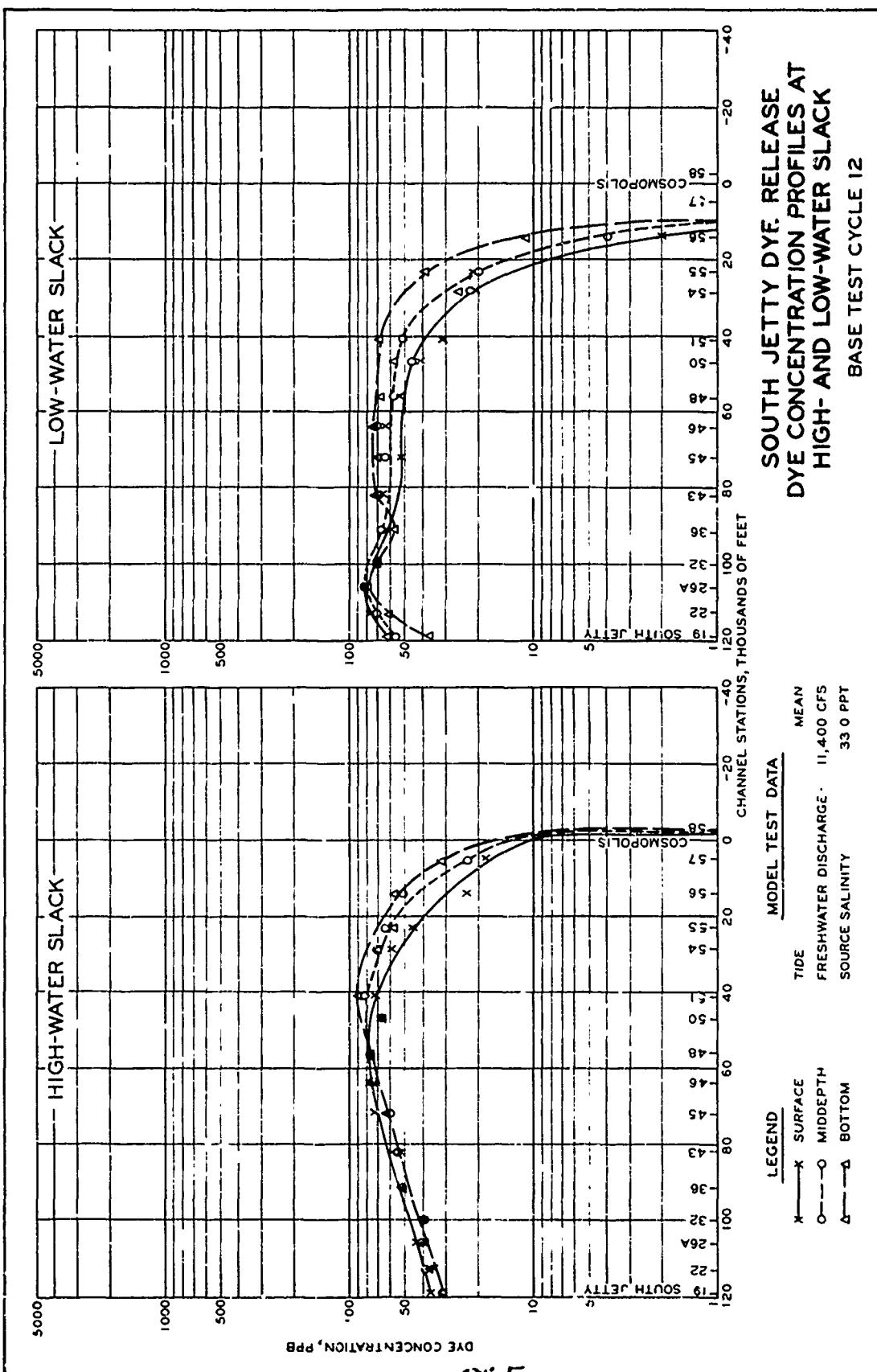


PLATE 2II