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PRECISION OF THE DETERMINATION OF FOCAL DEPTH FROM THE SPECTRAL RATIO OF LOVE/RAYLEIGH SURFACE WAVES

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27 JANUARY 1972

Prepared for
AIR FORCE TECHNICAL APPLICATIONS CENTER
Washington, D.C.

Under
Project VELA UNIFORM

Sponsored by
ADVANCED RESEARCH PROJECTS AGENCY
Nuclear Monitoring Research Office
ARPA Order No.1714



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| REF ID: | AVAIL AND/ OR SPECIAL |
| A | |

Unclassified

Security Classification

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1 ORIGINATING ACTIVITY (Corporate author)

Teledyne Geotech
Alexandria, Virginia

2a REPORT SECURITY CLASSIFICATION

Unclassified

2b GROUP

3 REPORT TITLE

PRECISION OF THE DETERMINATION OF FOCAL DEPTH FROM THE SPECTRAL
RATIO OF LOVE/RAYLEIGH SURFACE WAVES

4 DESCRIPTIVE NOTES (Type of report and inclusive dates)

Scientific

5 AUTHOR(S) (Last name, first name, initials)

Massé, R.P.; Lambert, D.G.; Harkrider, D.G.

6 REPORT DATE

January 27, 1972

7a TOTAL NO OF PAGES

75

7b NO OF REPS

26

8a CONTRACT OR GRANT NO.

F33657-72-C-0009

8b ORIGINATOR'S REPORT NUMBER(S)

287

8c PROJECT NO.

VELA T/2706

9a ARPA Order No. 1714

9b ARPA Program Code No. 2F-10

9d OTHER REPORT NO(S) (Any other numbers that may be assigned
this report)

10 AVAILABILITY/LIMITATION NOTICES

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.

11 SUPPLEMENTARY NOTES

12 SPONSORING MILITARY ACTIVITY

Advanced Research Projects Agency
Nuclear Monitoring Research Office
Washington, D.C.

13 ABSTRACT

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14 KEY WORDS

Focal Depth
Love/Rayleigh Spectral Ratios
Surface Wave Spectra

Unclassified

Security Classification

PRECISION OF THE DETERMINATION OF FOCAL DEPTH FROM
THE SPECTRAL RATIO OF LOVE/RAYLEIGH SURFACE WAVES

SEISMIC DATA LABORATORY REPORT NO. 287

AFTAC Project No.: VELA T/2706
Project Title: Seismic Data Laboratory
ARPA Order No.: 1714
ARPA Program Code No.: 2F-10

Name of Contractor: TELEDYNE GEOTECH

Contract No.: F33657-72-C-0009
Date of Contract: 01 July 1971
Amount of Contract: \$ 1,314,000
Contract Expiration Date: 30 June 1972
Project Manager: Royal A. Hartenberger
(703) 836-7647

P. O. Box 334, Alexandria, Virginia

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INTRODUCTION

Accurate determination of focal depth from body wave information is usually not possible for shallow-focus earthquakes because of the difficulty in identifying depth phases such as pP. Recently the problem of determining the focal depth of an earthquake has been approached using surface wave information such as spectra and spectral ratios (Keilis-Borok and Yanovskaya, 1962; Tsai, 1969; Harkrider, 1970; Tsai and Aki, 1970a, 1970b, 1970c; and Canitez and Toksöz, 1971). Surface wave spectra are functions not only of the focal depth, but also of the earthquake source mechanism and the physical parameters of the earth. Therefore the source parameters and the Earth model must be derived from other information before the focal depth can be estimated using surface wave spectra. The purpose of the present study is to determine how sensitive the ratio of Love to Rayleigh wave spectral amplitudes is to changes in the source depth, in the shear velocity within the Earth near the source, and in the source orientation. The accuracy of the focal depth determined from surface wave spectral ratios may then be specified in terms of the accuracy of the source mechanism and of the Earth model.

The theory is now available for the calculation of the far-field displacement associated with the propagation of surface waves generated by mathematical representations of earthquake source models within realistic Earth structures. The theory for calculating surface

wave dispersion in a multilayered medium was developed initially by Haskell (1953), and was expanded by the work of Harkrider and Anderson (1962), Rosenbaum (1964), Thrower (1965), Dunkin (1965) and Saito (1967). Mathematical representations of source models for earthquakes were derived through the work of Yanovskaya (1958), Knopoff and Gilbert (1960), Ben-Menahem (1961), Maruyama (1963), Haskell (1963, 1964), Burridge and Knopoff (1964) and Haskell (1966). The relations yielding the far-field surface wave displacements due to source models located in specified realistic Earth structures were presented by Harkrider (1964) and Ben-Menahem and Harkrider (1964), and have been expanded upon in the work of Harkrider and Anderson (1966), Saito (1967), and Harkrider (1970). Using the theory developed in these studies, spectral ratios of surface waves are determined in the present study for a series of source mechanisms, focal depths, and Earth structures. An estimate is then made of the precision of focal depth determinations from surface wave spectral ratios.

THEORY

Using the notation of Harkrider (1970), the far-field expressions for Rayleigh and Love wave spectral amplitudes may be written

$$U_R = S k_R^m e^{-i(1+2m)\pi/4} \chi_R(\theta, h) E_R \frac{e^{-ik_R r}}{r^{1/2}} e^{-\gamma_R r} \quad (1)$$

$$U_L = S k_L^m e^{-i(1+2m)\pi/4} \chi_L(\theta, h) E_L \frac{e^{-ik_L r}}{r^{1/2}} e^{-\gamma_L r}$$

where S is the spectral source function, $m = 0$ for a point force source and $m = 1$ for a couple of double-couple source, $k_R = \omega/C_R$ for Rayleigh waves, where C_R is the Rayleigh wave phase velocity, $k_L = \omega/C_L$ for Love waves, where C_L is the Love wave phase velocity, h is the source depth, θ is the azimuth from source to station, r is the epicentral distance, and γ_R and γ_L are the Rayleigh and Love wave attenuation coefficients respectively. The terms E_R and E_L in equation (1) are given by

$$E_R = \epsilon_0 A_R k_R^{-1/2} \quad (2)$$

$$E_L = A_L k_L^{-1/2}$$

where ϵ_o is the Rayleigh wave ellipticity

$$\epsilon_o = - [\dot{U}_o^* / \dot{W}_o^*] \quad (3)$$

and A_R and A_L are the Rayleigh and Love amplitude response due to a vertical point force at the surface. The radiation pattern function $\chi(\theta, h)$ given in equation (1) is

$$\begin{aligned} \chi(\theta, h) = & d_0 + i(d_1 \sin \theta + d_2 \cos \theta) + d_3 \sin 2\theta \\ & + d_4 \cos 2\theta \end{aligned} \quad (4)$$

where the coefficients d_i are defined in Table I.

Using equations (1) and (2), the Love/Rayleigh amplitude ratio may be written:

$$J = \left| \frac{U_L}{U_R} \right| = \left| \frac{k_L^m}{k_R^m} \frac{\chi_L}{\chi_R} \frac{A_L k_L^{-1/2}}{\epsilon_o A_R k_R^{-1/2}} \frac{e^{-\gamma_L r}}{e^{-\gamma_R r}} \right| \quad (5)$$

assuming the spectral source function S to be approximately the same for Rayleigh and Love waves.

To determine the sensitivity of the ratio Love/Rayleigh to focal depth h as compared to its sensitivity

to changes in the shear velocity β of the Earth and in the dip angle δ and slip angle λ of the fault, the following ratios of partial derivatives may be computed:

$$DR(h, \beta) = \frac{\frac{\partial J}{\partial h}}{\frac{\partial J}{\partial \beta}}$$

$$DR(h, \delta) = \frac{\frac{\partial J}{\partial h}}{\frac{\partial J}{\partial \delta}}$$

(6)

$$DR(h, \lambda) = \frac{\frac{\partial J}{\partial h}}{\frac{\partial J}{\partial \lambda}}$$

From equations (5) and (6), we have:

$$DR(h, \beta) = \frac{\frac{k_L^{m-1/2}}{k_R^{m-1/2}} \frac{A_L}{\epsilon_0 A_R} \frac{\partial}{\partial h} \left| \begin{array}{c} x_L \\ x_R \end{array} \right|}{\frac{\partial \beta}{\partial \beta} \left| \begin{array}{c} \frac{k_L^{m-1/2}}{k_R^{m-1/2}} \frac{x_L}{x_R} \frac{A_L}{\epsilon_0 A_R} \\ \end{array} \right|},$$

$$DR(h, \delta) = \frac{\frac{\partial}{\partial h} \left| \frac{x_L}{x_R} \right|}{\frac{\partial}{\partial \delta} \left| \frac{x_L}{x_R} \right|}, \text{ and } DR(h, \lambda) = \frac{\frac{\partial}{\partial h} \left| \frac{x_L}{x_R} \right|}{\frac{\partial}{\partial \lambda} \left| \frac{x_L}{x_R} \right|}. \quad (7)$$

These ratios of partial derivatives are independent of the attenuation coefficients γ_R and γ_L and are dependent on frequency ω and azimuth θ .

CALCULATIONS FOR THE BASIN AND RANGE VELOCITY STRUCTURE

The Basin and Range province was chosen as a source model for study of Love/Rayleigh spectral ratios both because the earthquakes occurring within this province are typically shallow-focus and because of the availability of a large amount of seismic data for this region making possible the construction of a velocity model which may be more accurate than that obtainable for most seismically active areas. The P velocity structure chosen to represent the Basin and Range source region is based on an upper mantle model (CIT 111P) determined by Archambeau et al., (1969). The crustal model is similar to that determined by Warren (1969) for the southeastern part of the Basin and Range province. The P and S velocity structures as well as the density distribution for the Basin and Range source model are shown in Figure 1 for the crust and in Figure 2 for the upper mantle, and the parameters for the model are listed in Table II. The S velocity structure was computed from the P velocity structure by assuming a Poisson's ratio of 0.25.

Two source models were considered in the present study: left-lateral fault with dip angle of 90° and slip angle of 0° and a left lateral fault with dip angle of 90° and slip angle of 45° . Calculations were made for focal depths corresponding to a source successively positioned in the middle of each of the first six layers of the Basin and Range model. The

partial derivatives $\partial J / \partial \beta$ were computed for the first six layers for both source models. This was accomplished by successively incrementing the shear velocity β of the first, fourth and fifth layers by $\Delta\beta = 0.1$ km/sec, and, since the velocities of the second and third layers are nearly equal, incrementing the shear velocities of both these layers together by $\Delta\beta = 0.1$ km/sec. Spectral amplitudes U_L and U_R were then calculated. The partial derivatives of spectral ratio with respect to dip angle δ , $\partial J / \partial \delta$, were computed by varying δ by 10° and computing the spectral ratio for each source depth for slip angles λ of 0° and 45° . Partial derivatives of spectral ratio with respect to slip angle, $\partial J / \partial \lambda$, were calculated from the difference in the computed spectral ratios for slip angles 0° and 45° . Because of the large differential in slip angle, the calculated derivative is accurate enough only for rough estimates. Depth partials, $\partial J / \partial h$, were computed by taking differences in spectral ratios for sources within the i^{th} and $(i + 1)^{\text{th}}$ layers. It is possible by means of the depth derivatives given by Harkrider (1970) to determine analytically the partials $\partial J / \partial h$ for changes in source depth which occur completely within any given layer.

The fundamental mode phase and group velocity dispersion for Rayleigh and Love waves for the Basin and Range model are shown in Figures 3 and 4. The fundamental mode radiation pattern functions x_R and x_L for the two sources studied are presented in Figures 5 through 20 for periods of 20 to 40 seconds. These radiation patterns show that the amount of energy

propagating from a source decreases with increasing depth for periods of 20 to 40 seconds. For the source with a strike of 0° , a dip angle of 90° and a slip angle of 0° , both the Rayleigh and Love radiation patterns for periods of 20 and 40 seconds have four equal lobes for all depths. For the source with a strike of 0° , a dip angle of 90° and a slip angle of 45° , only the Love wave radiation patterns have four equal lobes over the depth range examined. Love/Rayleigh spectral ratios are given in Figures 21, 22 and 23 for a few selected source geometries. Figure 21 illustrates the variation in J as a function of θ . The dependence of J on the source parameters λ and δ is illustrated in Figure 22, and Figure 23 shows the change in J due to change in only focal depth. From Figures 21, 22 and 23, the orientation of the source can be seen to have as great an effect on the Love/Rayleigh spectral ratio as does the focal depth. The period at which a maximum occurs in the Love/Rayleigh ratios (corresponding to a minimum in the Rayleigh wave amplitude) can also be seen to vary with source parameters such as dip and slip angles as well as with focal depth.

The partial derivative ratios $DR(h,\beta)$, $DR(h,\delta)$ and $DR(h,\lambda)$ given in equation (6) may be interpreted as the changes $\Delta\beta$, $\Delta\delta$, and $\Delta\lambda$ respectively which would produce the same change in J as a change Δh in h of 1 km. Therefore the values of $DR(h,\beta)$, $DR(h,\delta)$ and $DR(h,\lambda)$ given in Tables III, IV and V respectively may be used to determine how accurately the shear velocity of the Earth and the dip and slip angles of the source must be

known in order to determine the focal depth to some desired accuracy. Consider, for example, that it is desired that the focal depth be determined correct to within \pm 5 km. Then the values of $\Delta\beta$, $\Delta\delta$, and $\Delta\lambda$ which would produce the same change in J as a change in h of 5 km are given by multiplying the values of $DR(h, \beta)$, $DR(h, \delta)$ and $DR(h, \lambda)$ in Tables III, IV and V by a factor of 5. The resulting $\Delta\beta$, $\Delta\delta$ and $\Delta\lambda$ are larger respectively than 0.2 km/sec, 10° and 10° for sources in certain layers but are smaller for sources in others. Moreover, $\Delta\beta$, $\Delta\delta$ and $\Delta\lambda$ are a function of azimuth and if a combination of changes in shear velocities, dip angle, and slip angle were made, the result could equal to a Δh of 5 km with $\Delta\beta < 0.2$ km/sec, $\Delta\delta < 10^\circ$ and $\Delta\lambda < 10^\circ$ for sources within several of the layers.

Therefore the conclusion must be that the accuracy of the focal depth determined from Love/Rayleigh spectral ratios is very much dependent not only on the velocity structure and source parameters but also on the layer in which the source is located and the azimuth of the recording station from the source. In some cases, the shear velocity of the model near the source would need to be known to better than ± 0.2 km/sec and the dip and slip angles to better than $\pm 10^\circ$ in order to attain an accuracy of ± 5 km in the focal depth.

If spectral ratios are available for several different values of period and several stations, the depth resolution could be better. However, consideration of the first or fifth column of Table III for a slip

angle of 0° shows that the error can be of the same sign at every station and frequency; and one would not, therefore, expect it to be minimized by any "least squares" procedure. With respect to determining depth by finding nulls in the spectra, column two of Table III shows that the errors can have the same pattern as a function of azimuth at every frequency, thus leading to a consistent shift of the null frequency.

DISCUSSION

The accuracy of the focal depth determined from the spectral ratio of Love wave to Rayleigh wave energy depends upon the accuracy of the mathematical models used for the Earth structure and for the source mechanism. Recent studies by Tsai and Aki (1970a, b, c) and Canitez and Toksöz (1971) have concluded that it is possible to determine the focal depth to an accuracy of a few kilometers if the source mechanism and the Earth structure are reasonably well known. However, in order to define the terms "reasonably well known", the partial derivative $DR(h,\beta)$, $DR(h,\delta)$ and $DR(h,\lambda)$ should be available for models of the Earth structure and for the source mechanism which are close to those being assumed in the calculation of the focal depth. In some cases it probably will not be possible to estimate the focal depth to within a few kilometers of the correct value from surface wave spectral information alone.

We see that it is not true, as often hypothesized, that error due to lack of knowledge of the velocity structure will be reduced to negligible proportions by using Love/ Rayleigh spectral ratios, instead of Love or Rayleigh spectra values alone, to determine source parameters. Also the difficulty in determining the dip and slip angles to better than 10° may in many cases preclude the determination of focal depth from surface wave spectral information to an accuracy of a few kilometers.

ACKNOWLEDGMENTS

We wish to thank Drs. S. Alexander and R. Blandford for their encouragement and their many helpful discussions. We also thank Dr. E.A. Flinn for critically reading this paper.

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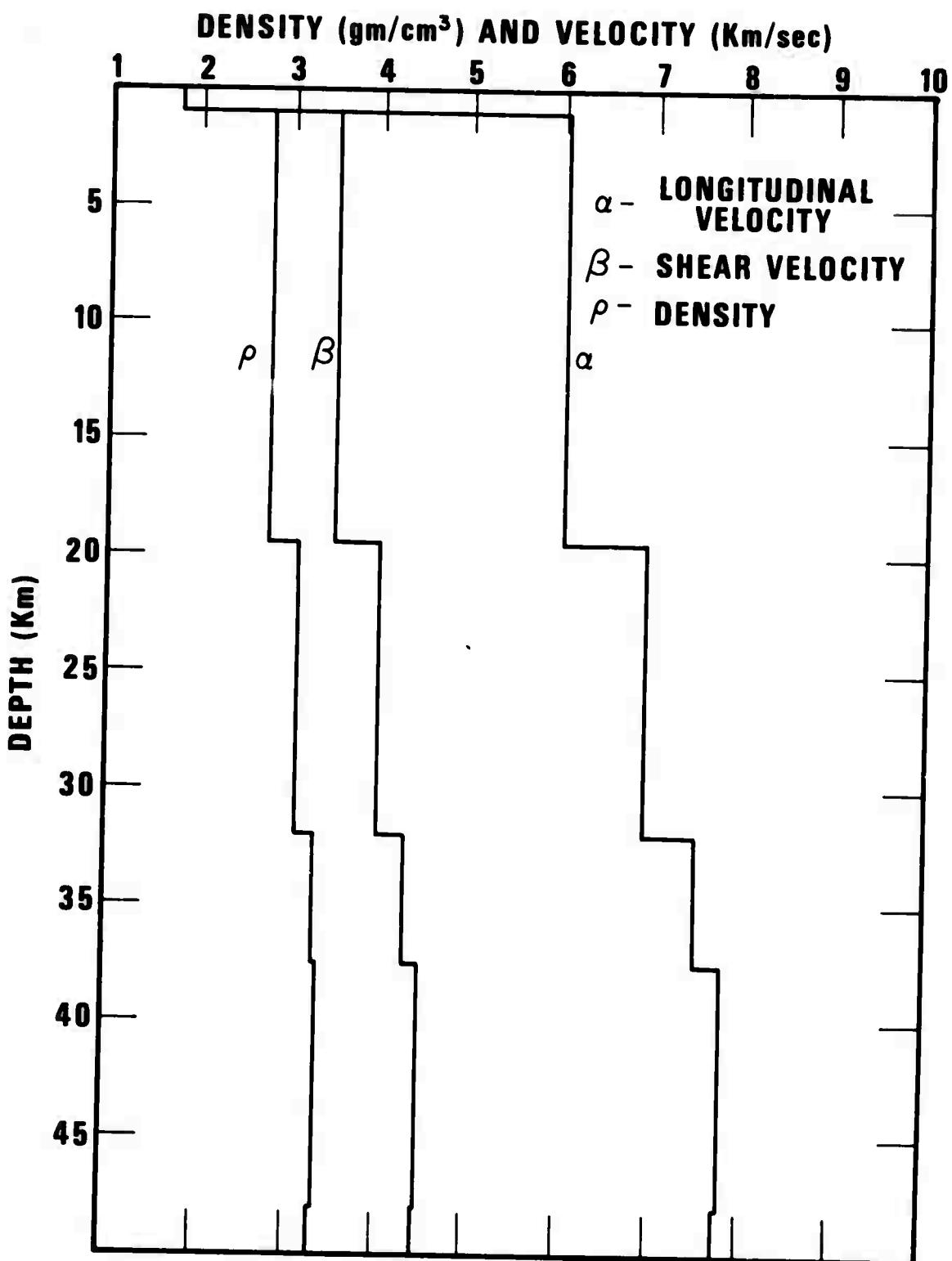


Figure 1. Basin and Range crustal model.

DENSITY (gm/cm³) AND VELOCITY (Km/sec)

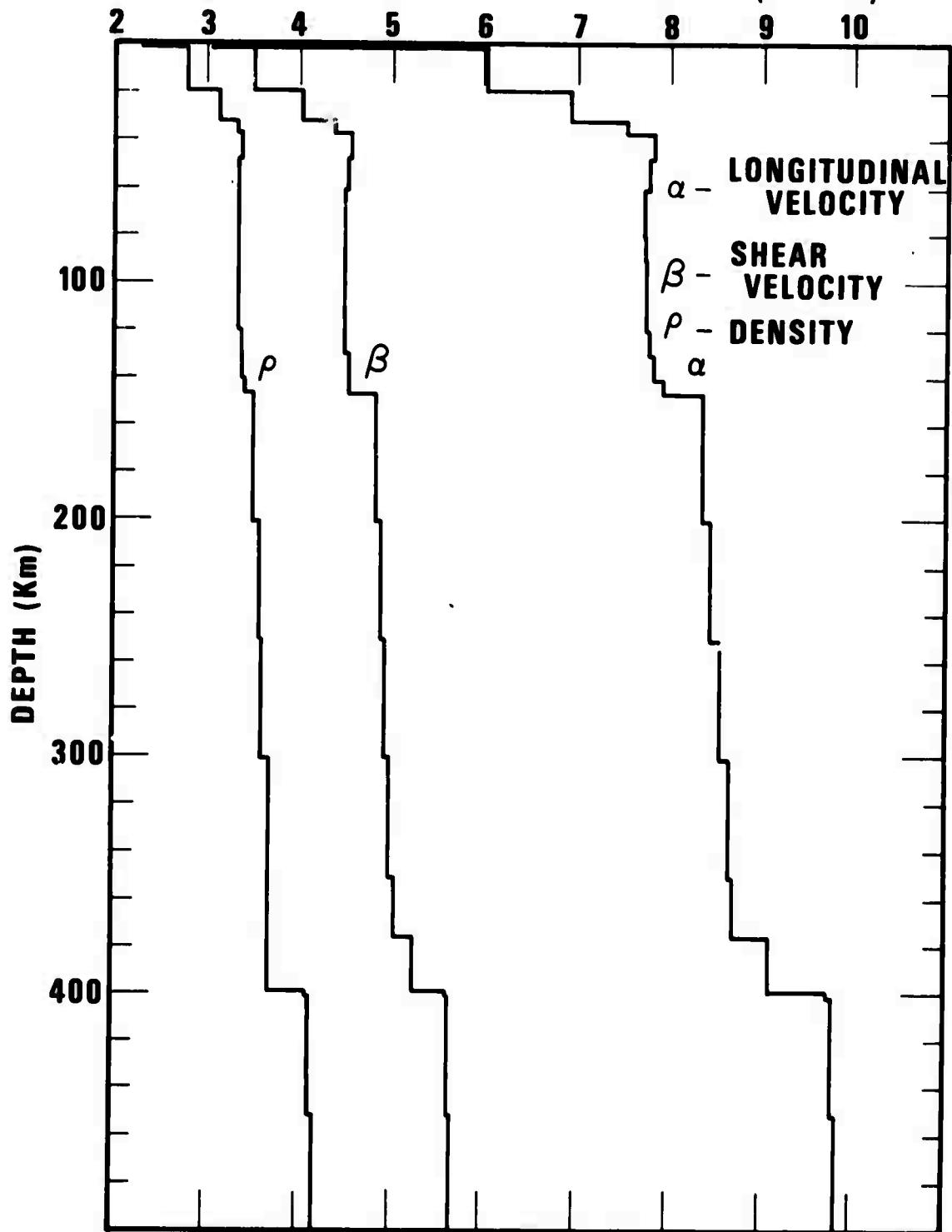


Figure 2. Basin and Range upper mantle model.

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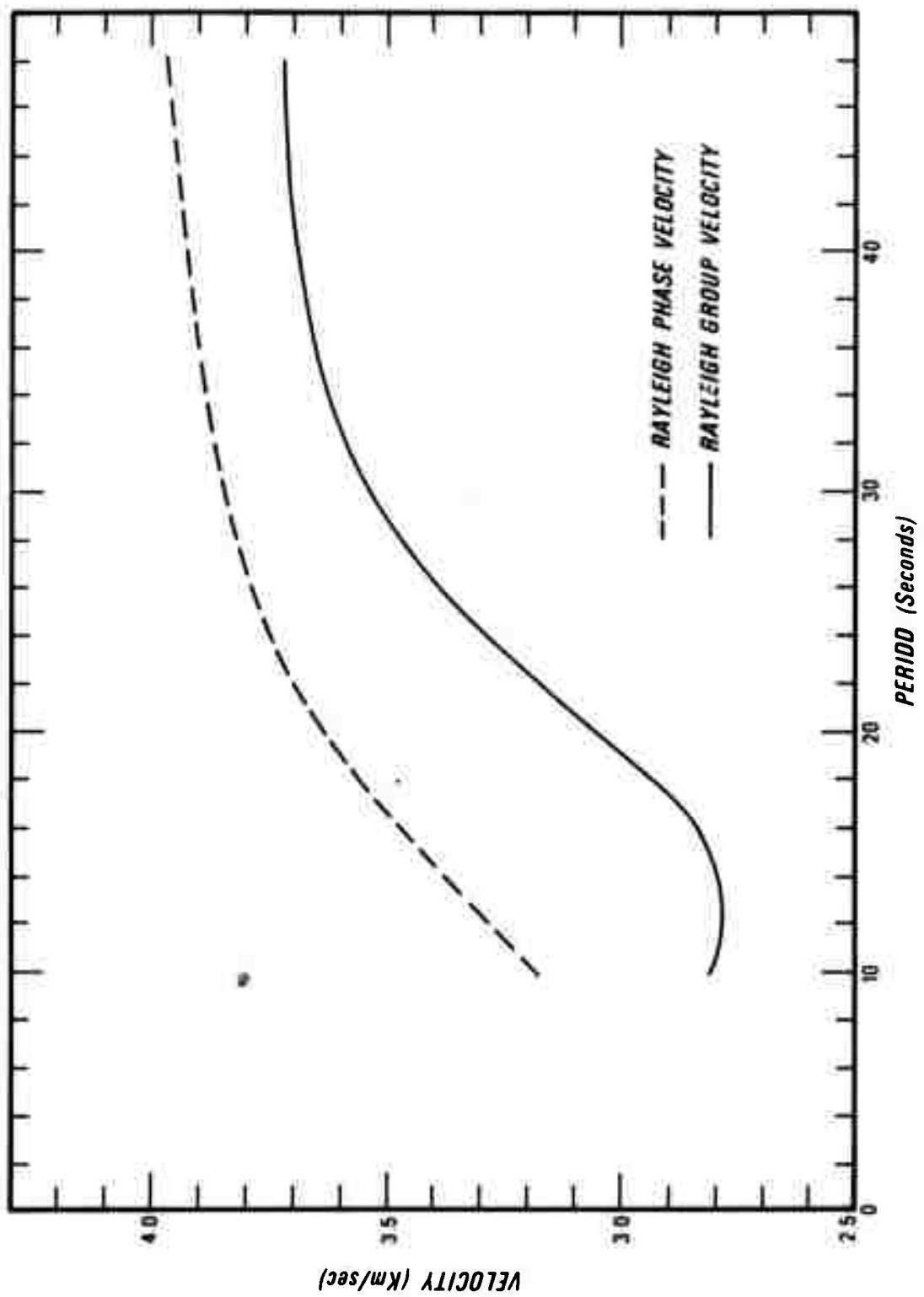


Figure 3. Fundamental mode Rayleigh wave dispersion for the Basin and Range model.

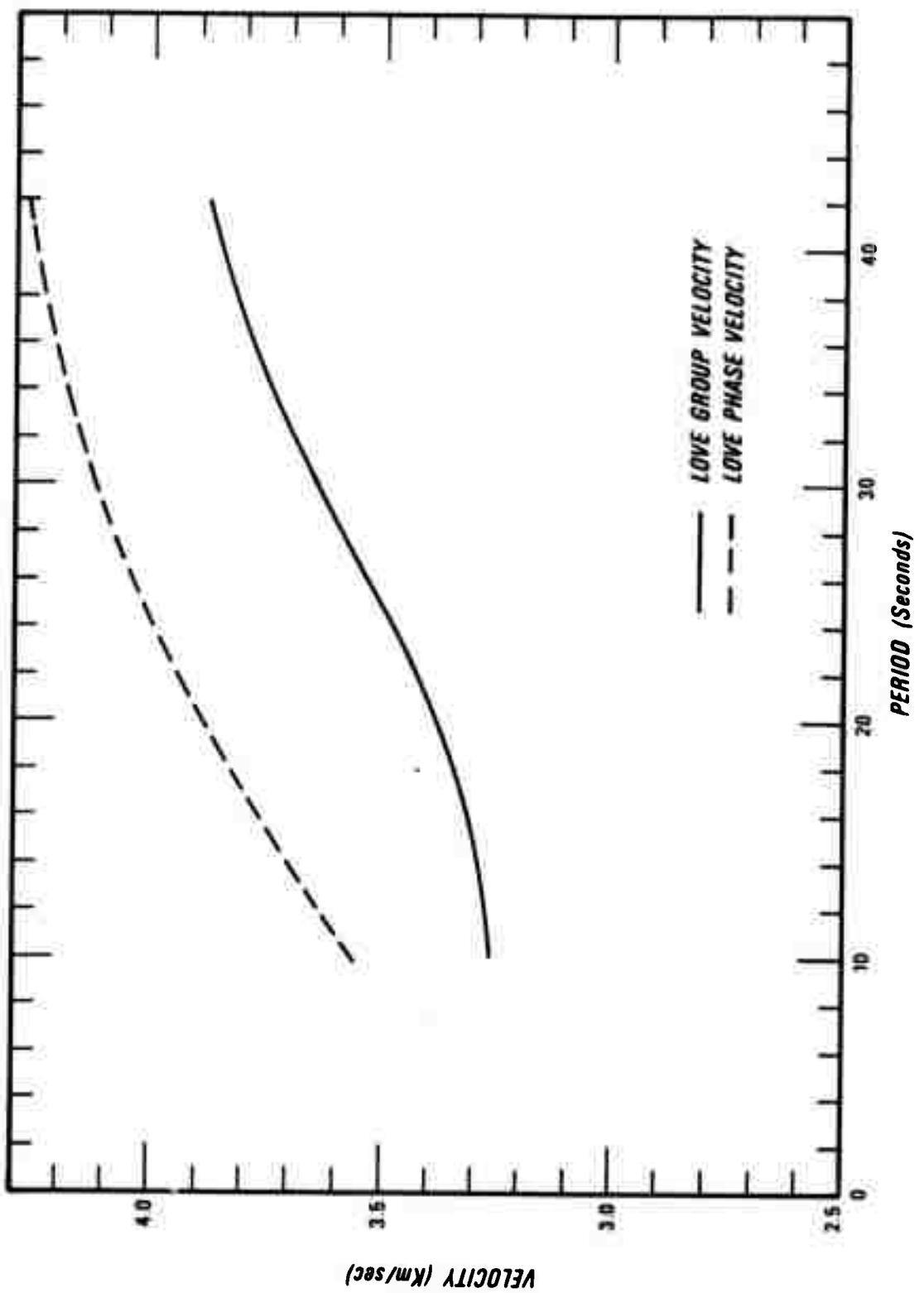


Figure 4. Fundamental mode Love wave dispersion for the Basin and Range model.

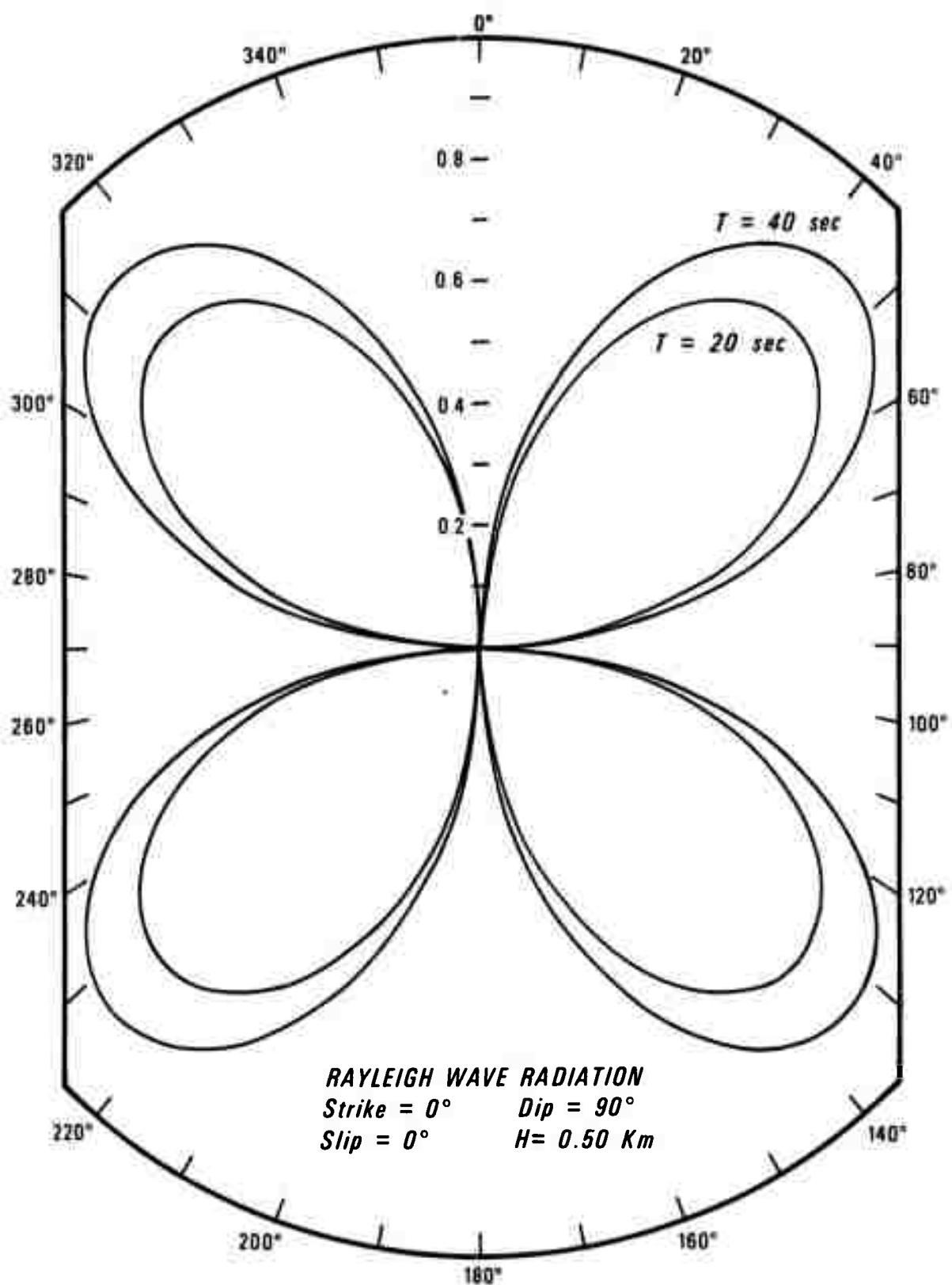


Figure 5. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 0.5 km and with a strike of 0° and a slip of 0° .

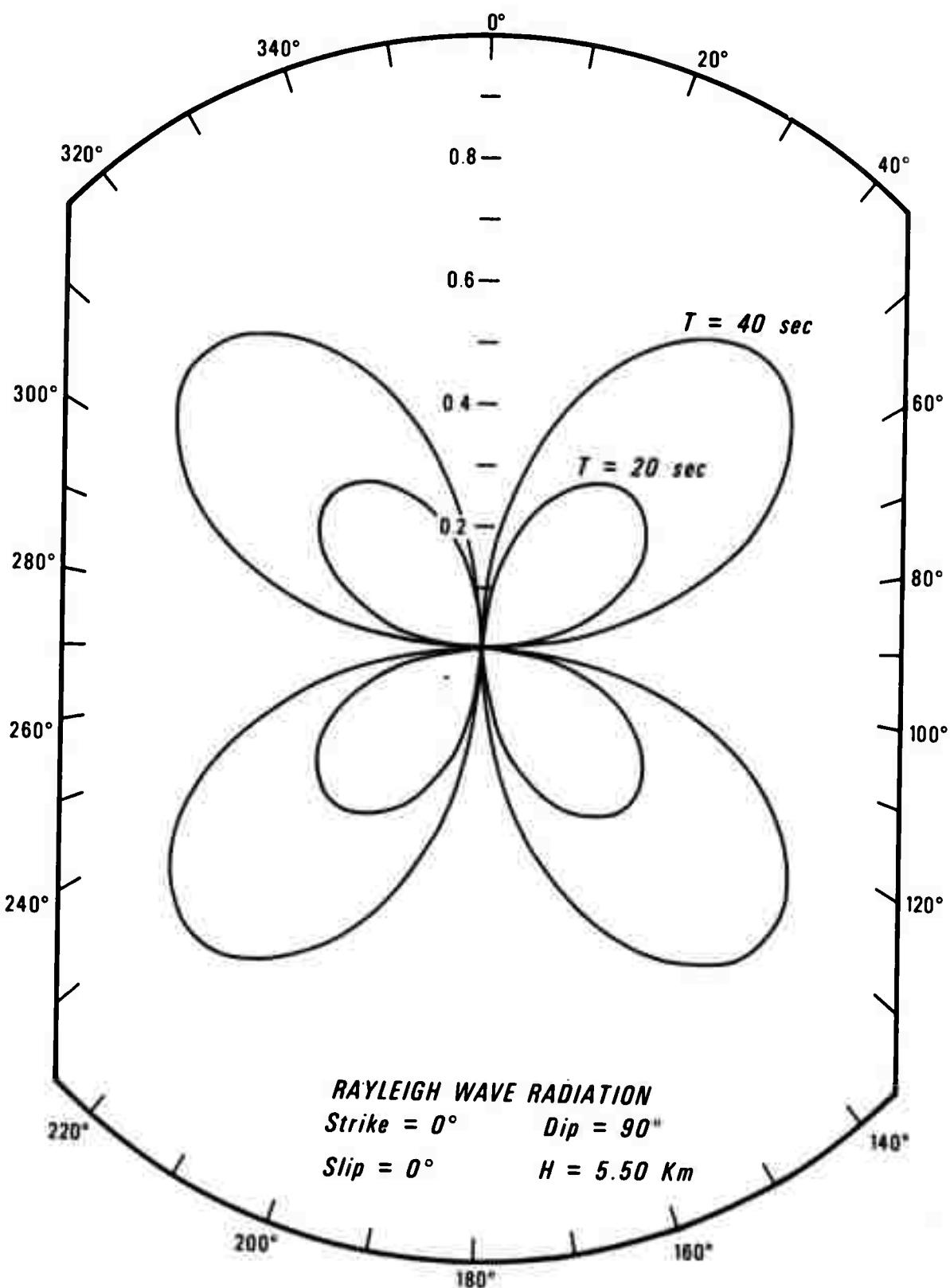


Figure 6. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 5.5 km and with a strike of 0° and a slip of 0° .

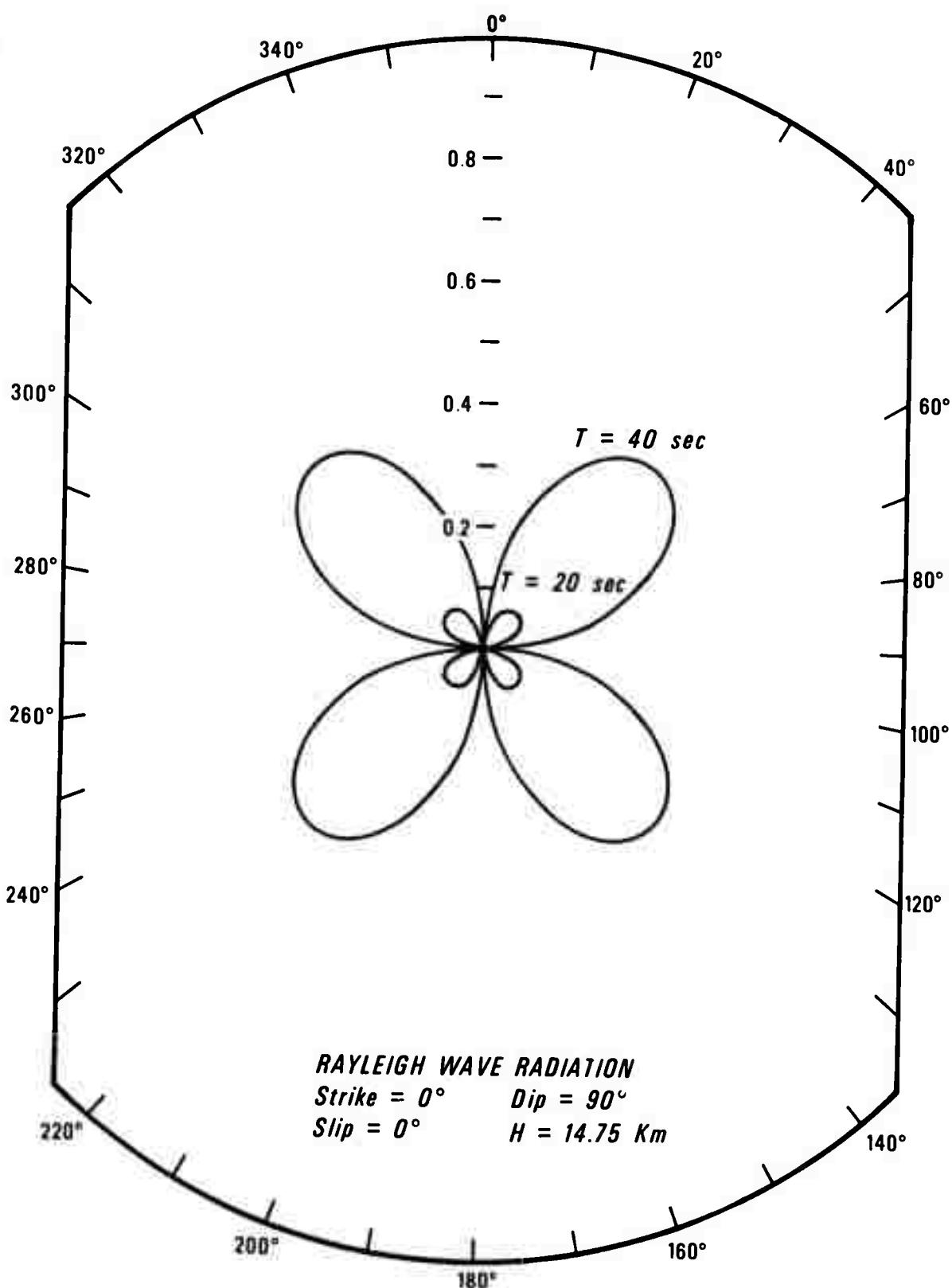


Figure 7. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 14.75 km and with a strike of 0° and a slip of 0° .

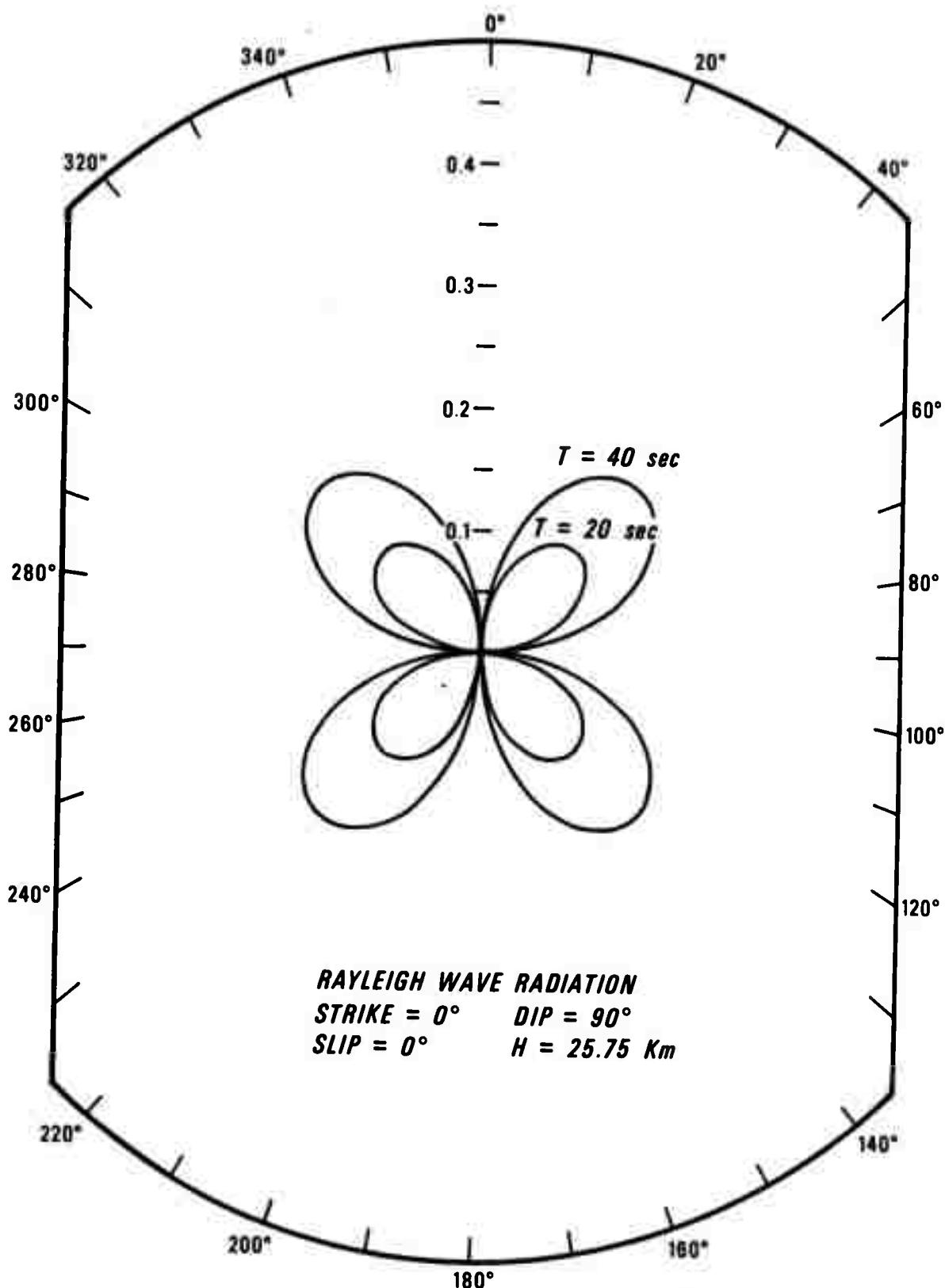


figure 8. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 25.75 km and with a strike of 0° and a slip of 0° .

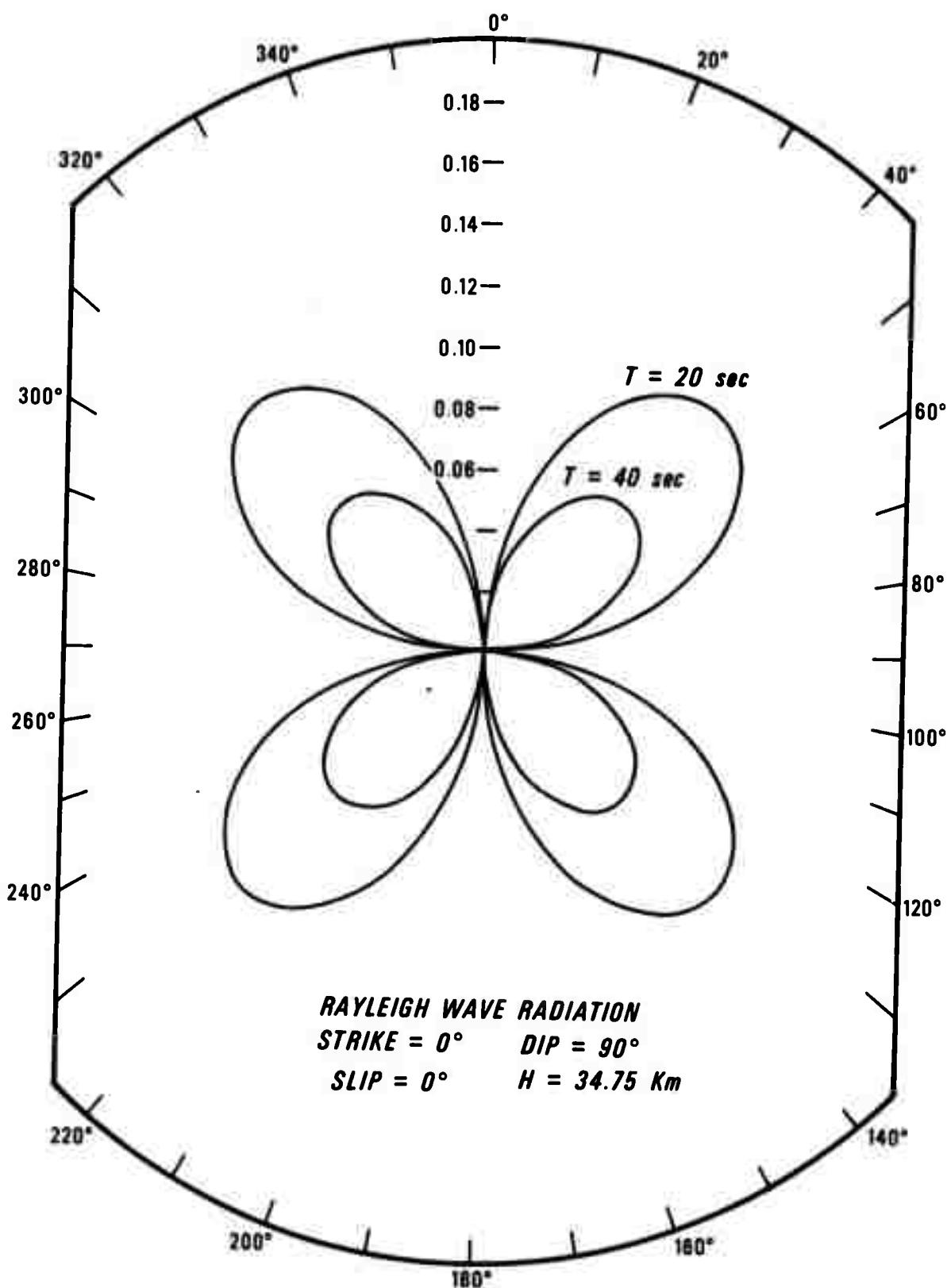


Figure 9. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 34.75 km and with a strike of 0° and a slip of 0°.

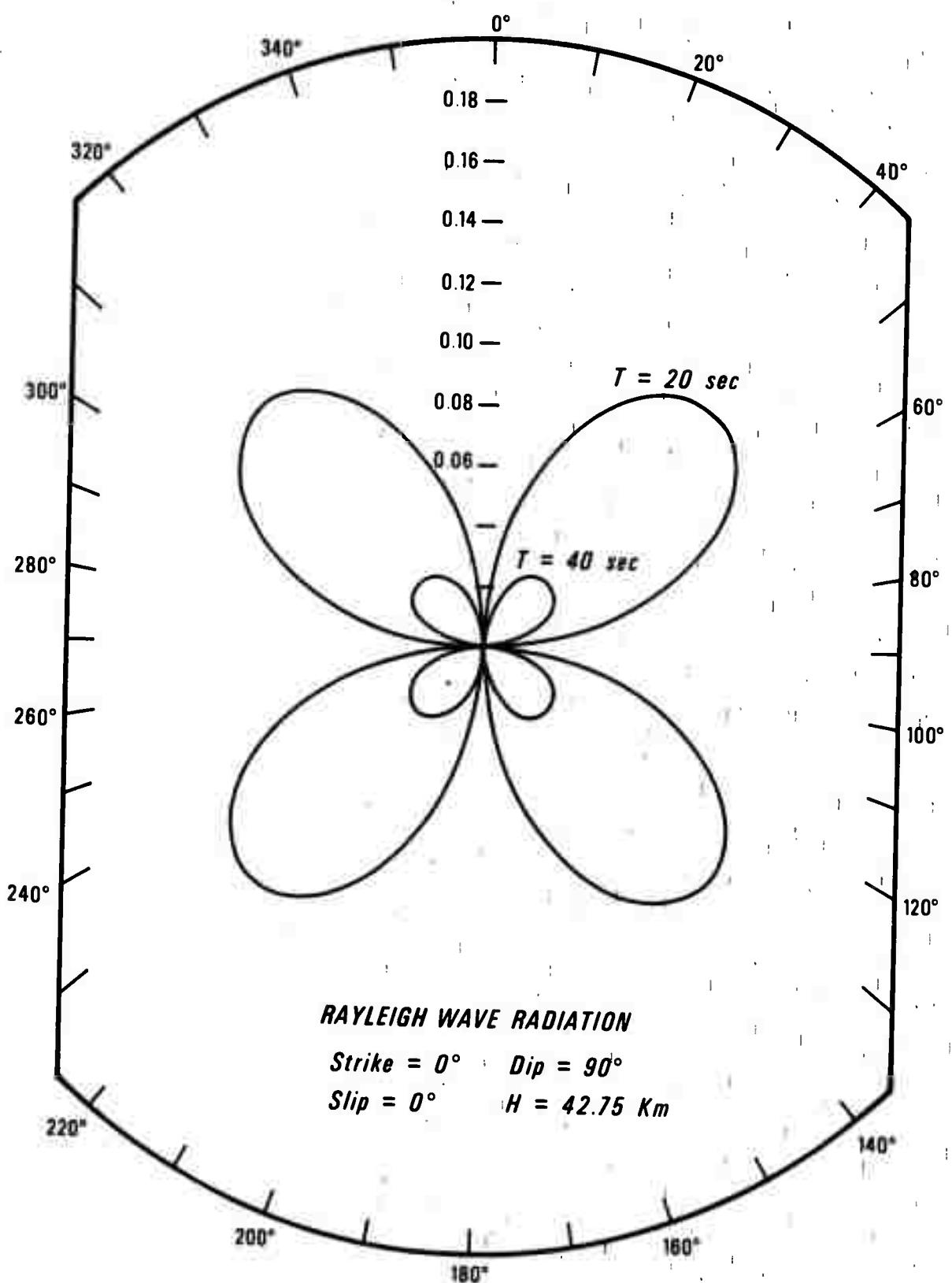


Figure 10. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 42.75 km and with a strike of 0° and a slip of 0° .

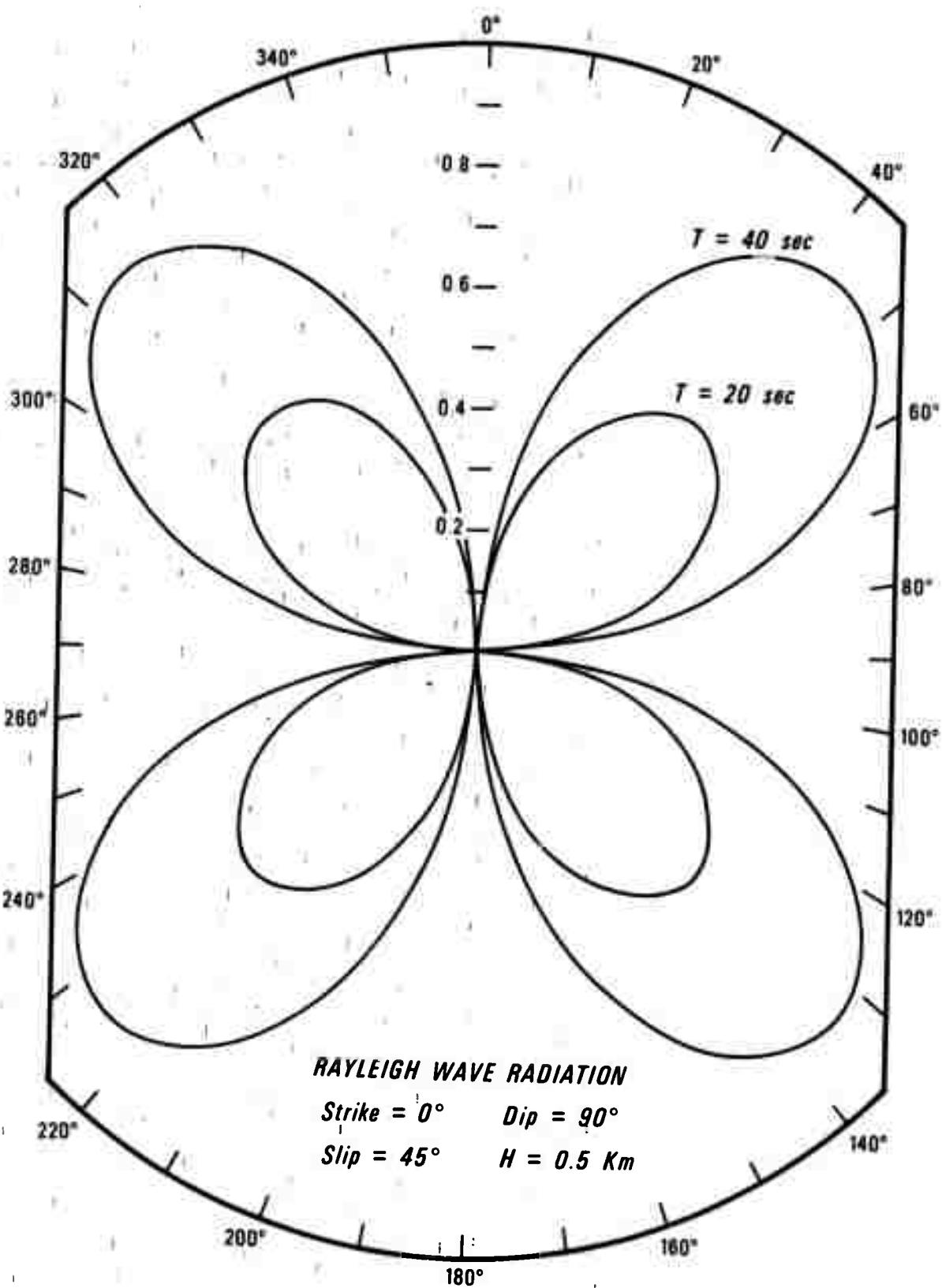


Figure 11. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 0.5 km and with a strike of 0° and a slip of 45° .

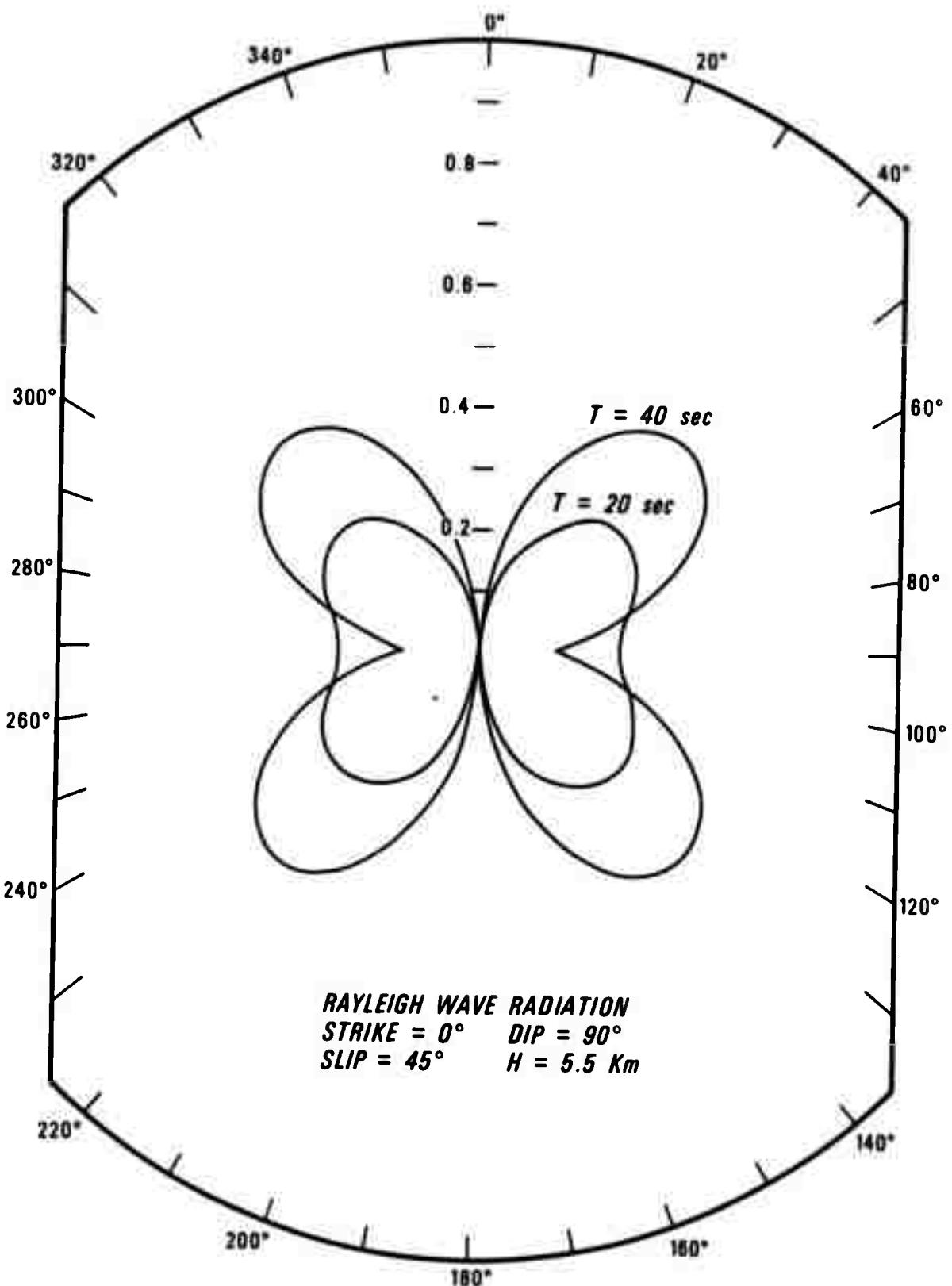


Figure 12. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 5.5 km and with a strike of 0° and a slip of 45°.

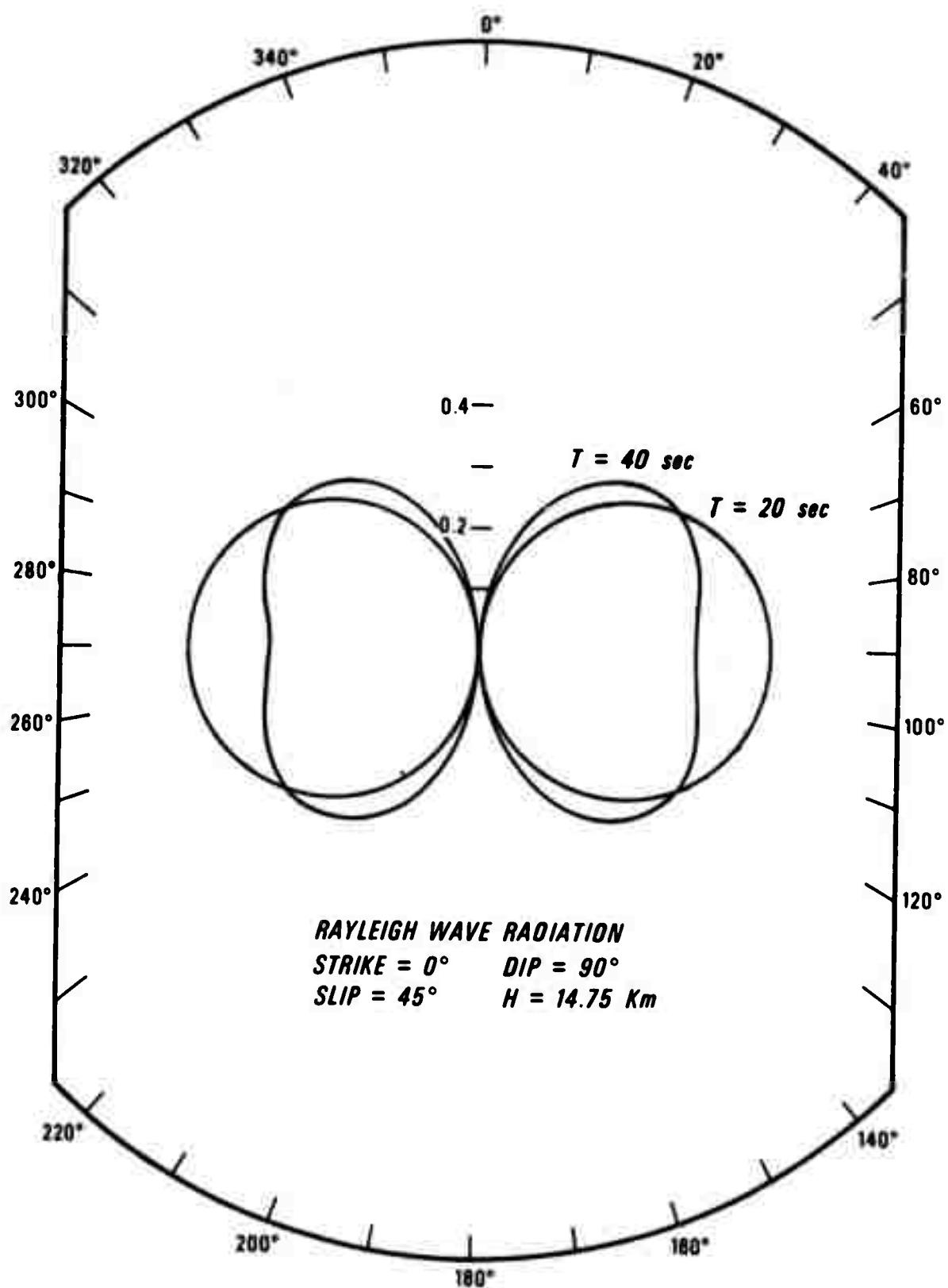


Figure 13. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 14.75 km and with a strike of 0° and a slip of 45° .

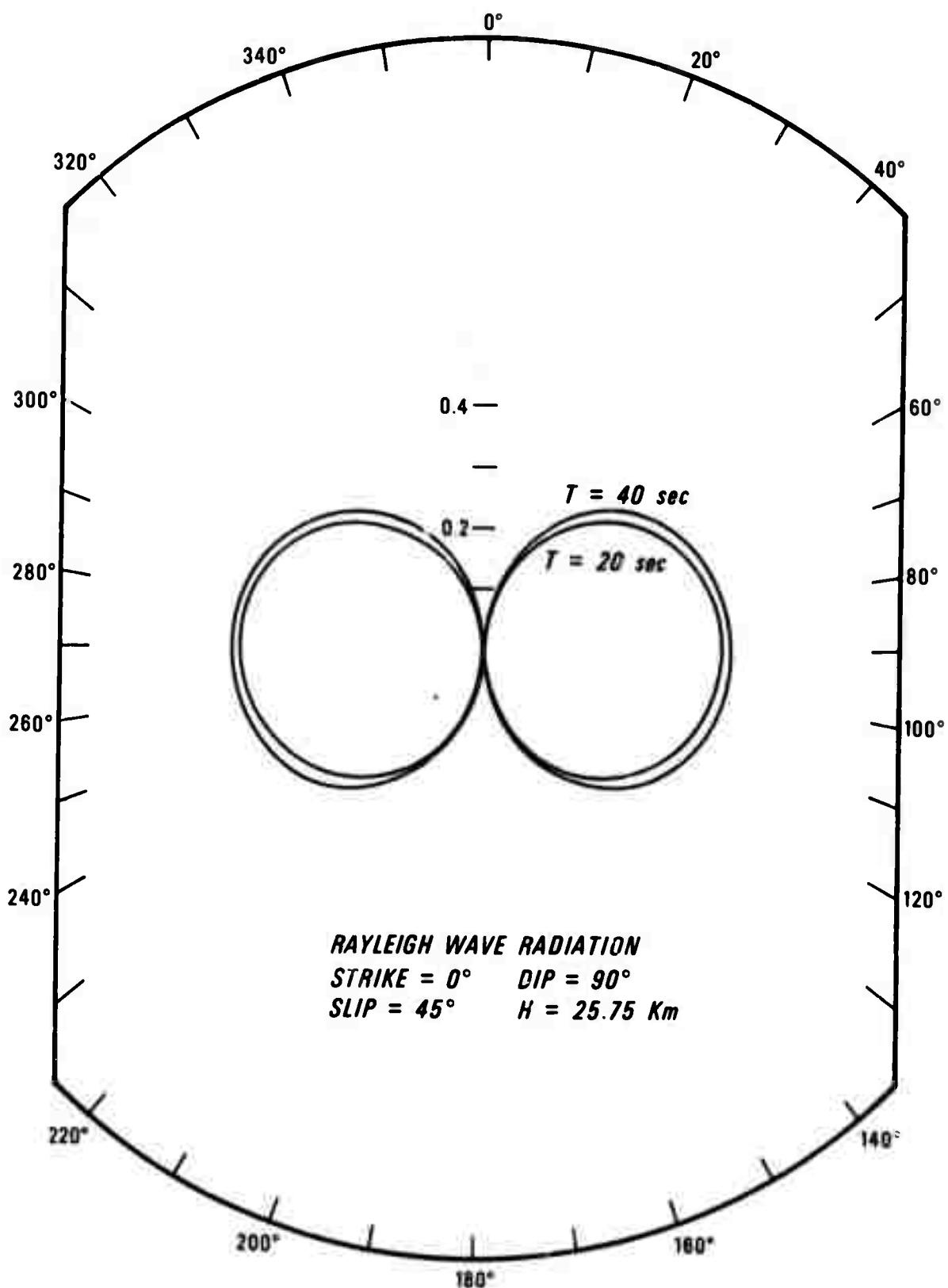


Figure 14. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 25.75 km and with a strike of 0° and a slip of 45° .

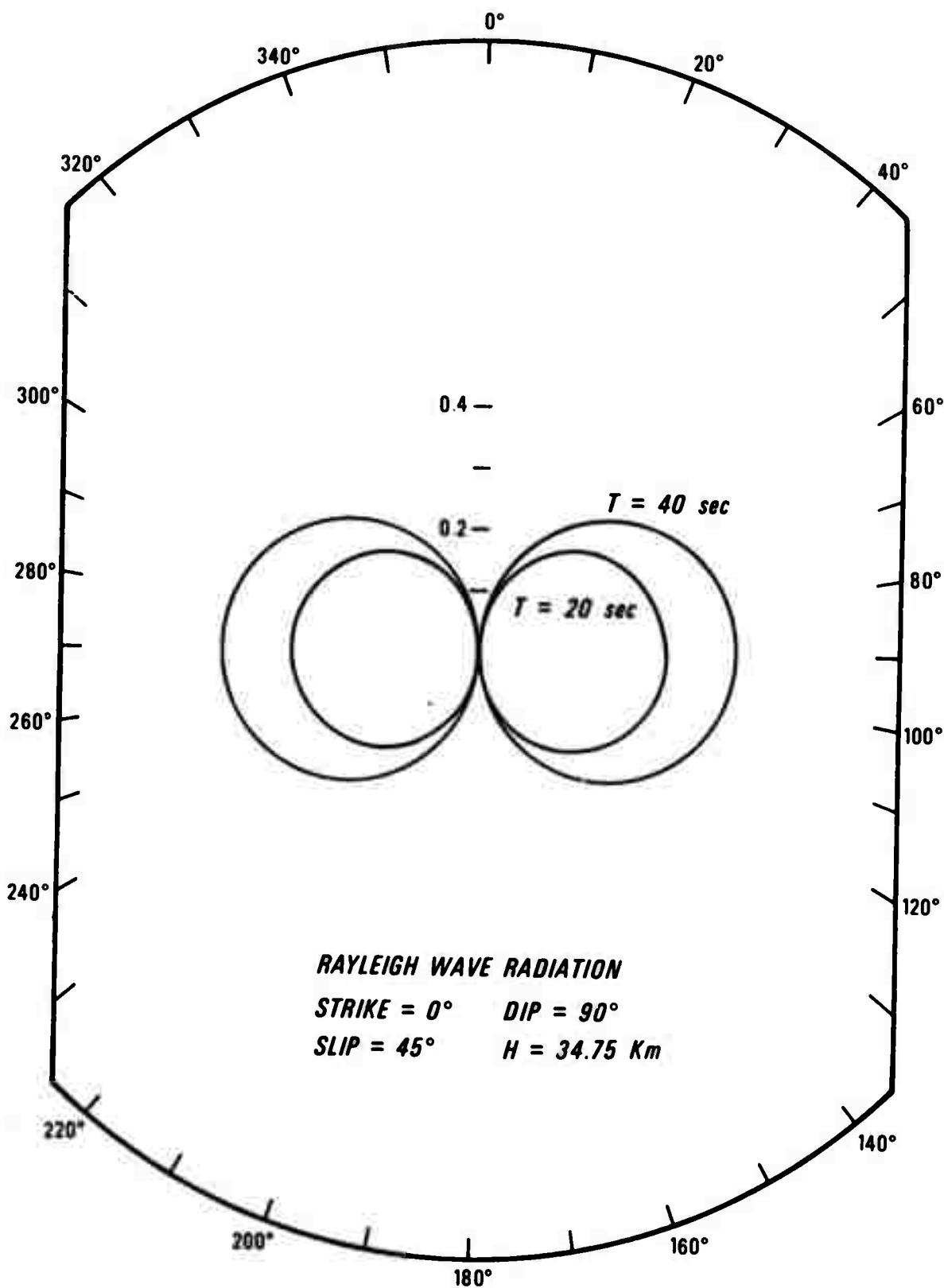


Figure 15. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 34.75 km and with a strike of 0° and a slip of 45° .

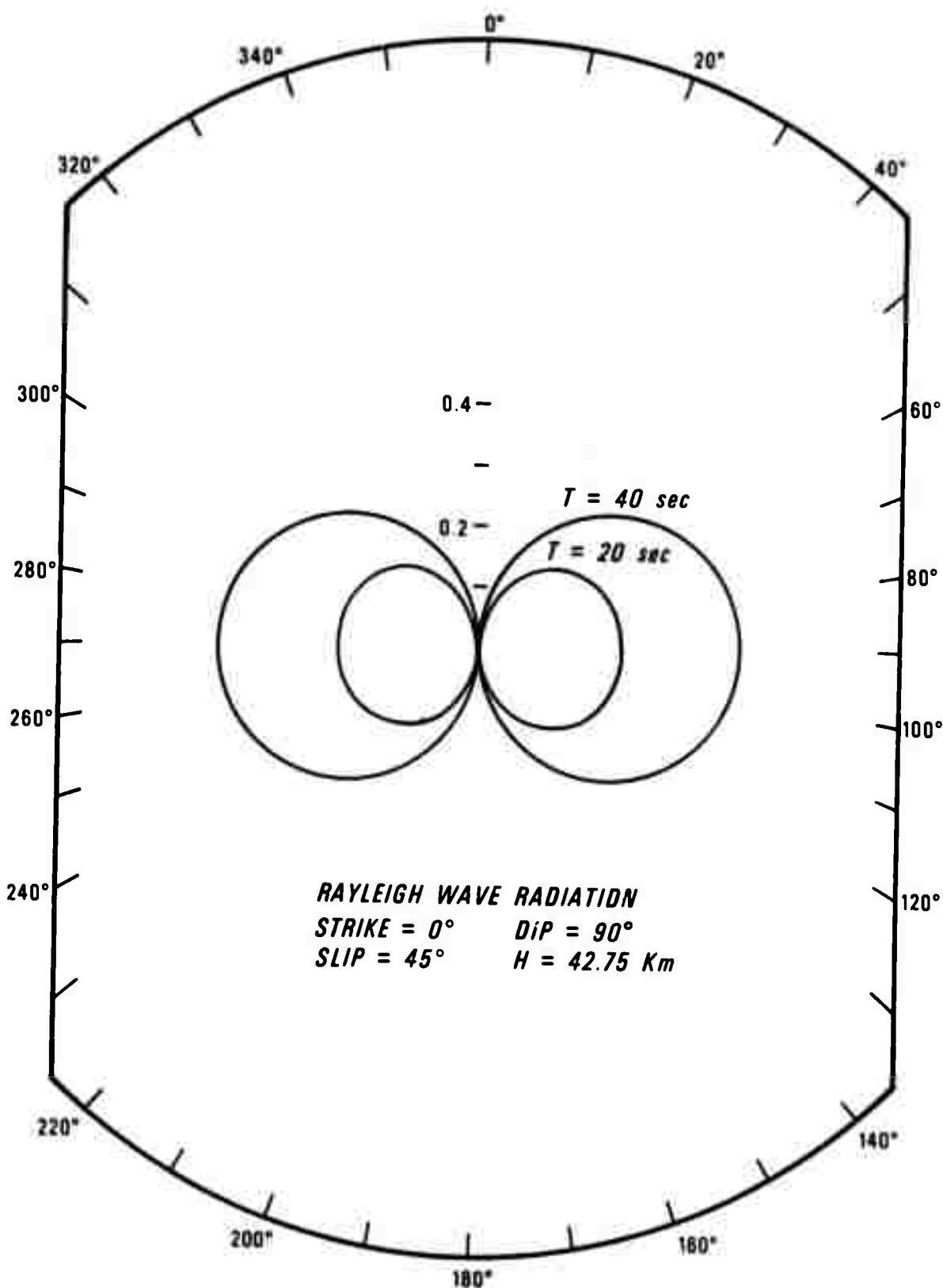


Figure 16. Rayleigh radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 42.75 km and with a strike of 0° and a slip of 45° .

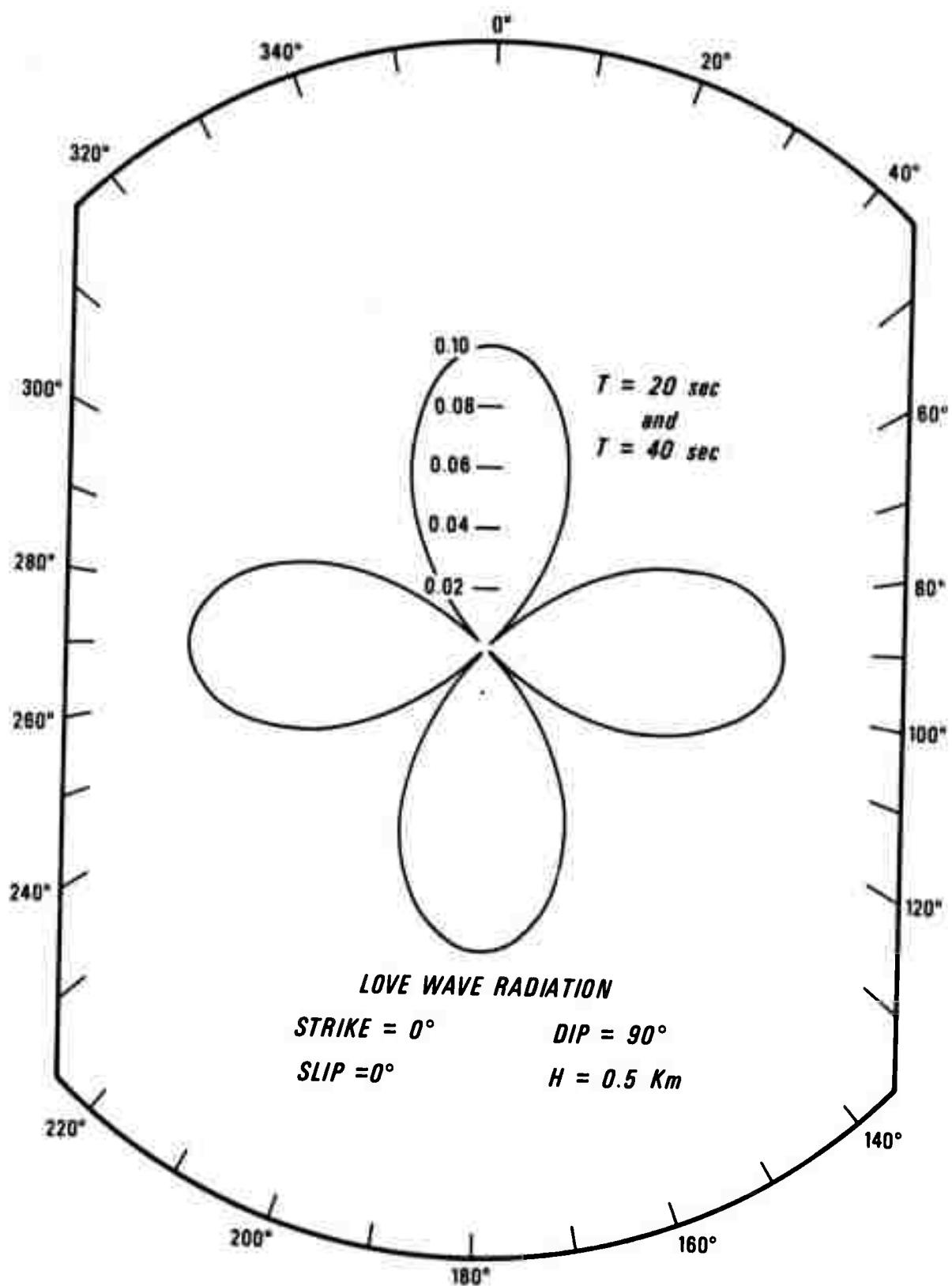


Figure 17. Love radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 0.5 km and with a strike of 0° and a slip of 0° .

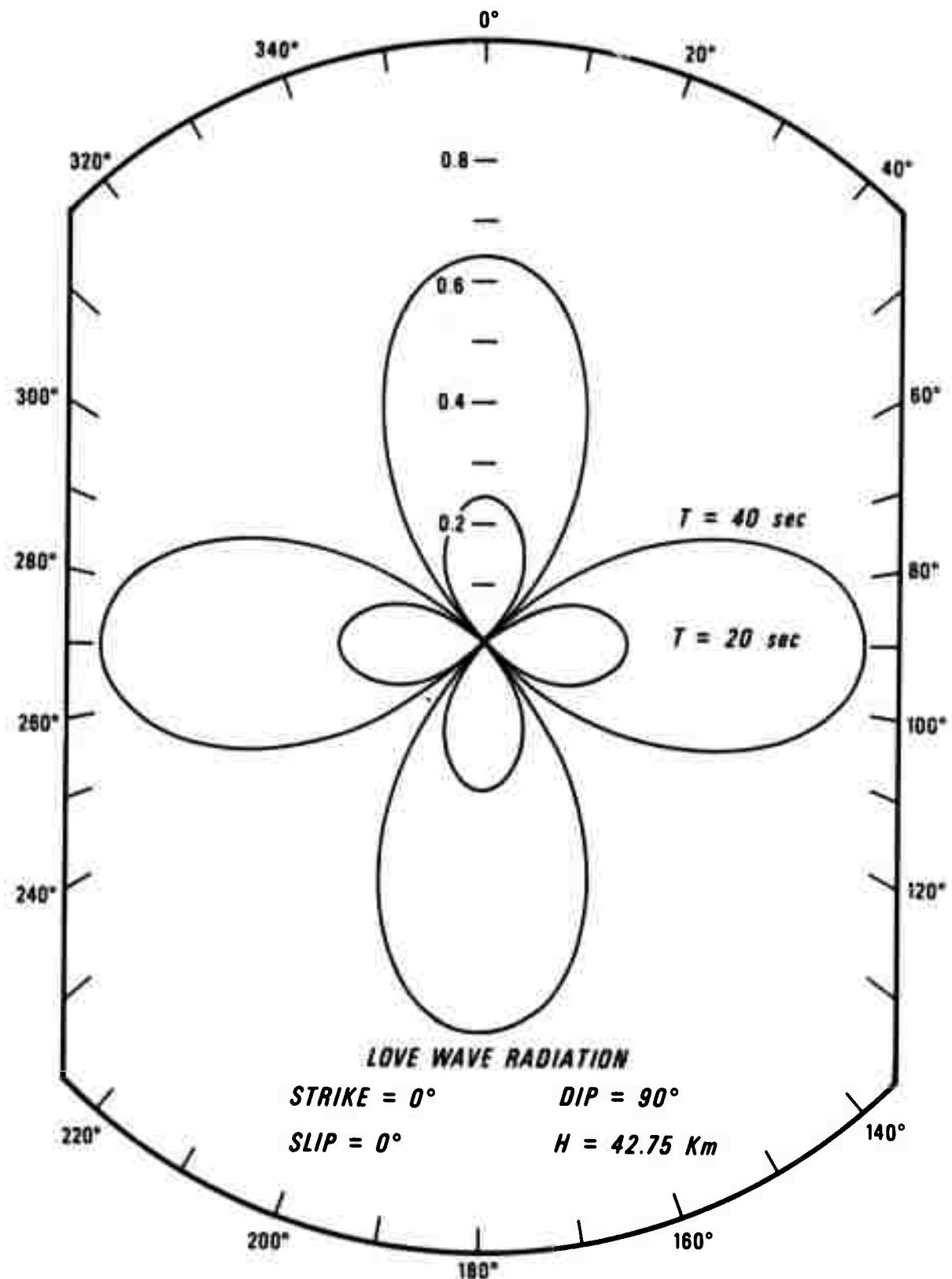


Figure 18. Love radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 42.75 km and with a strike of 0° and a slip of 0°.

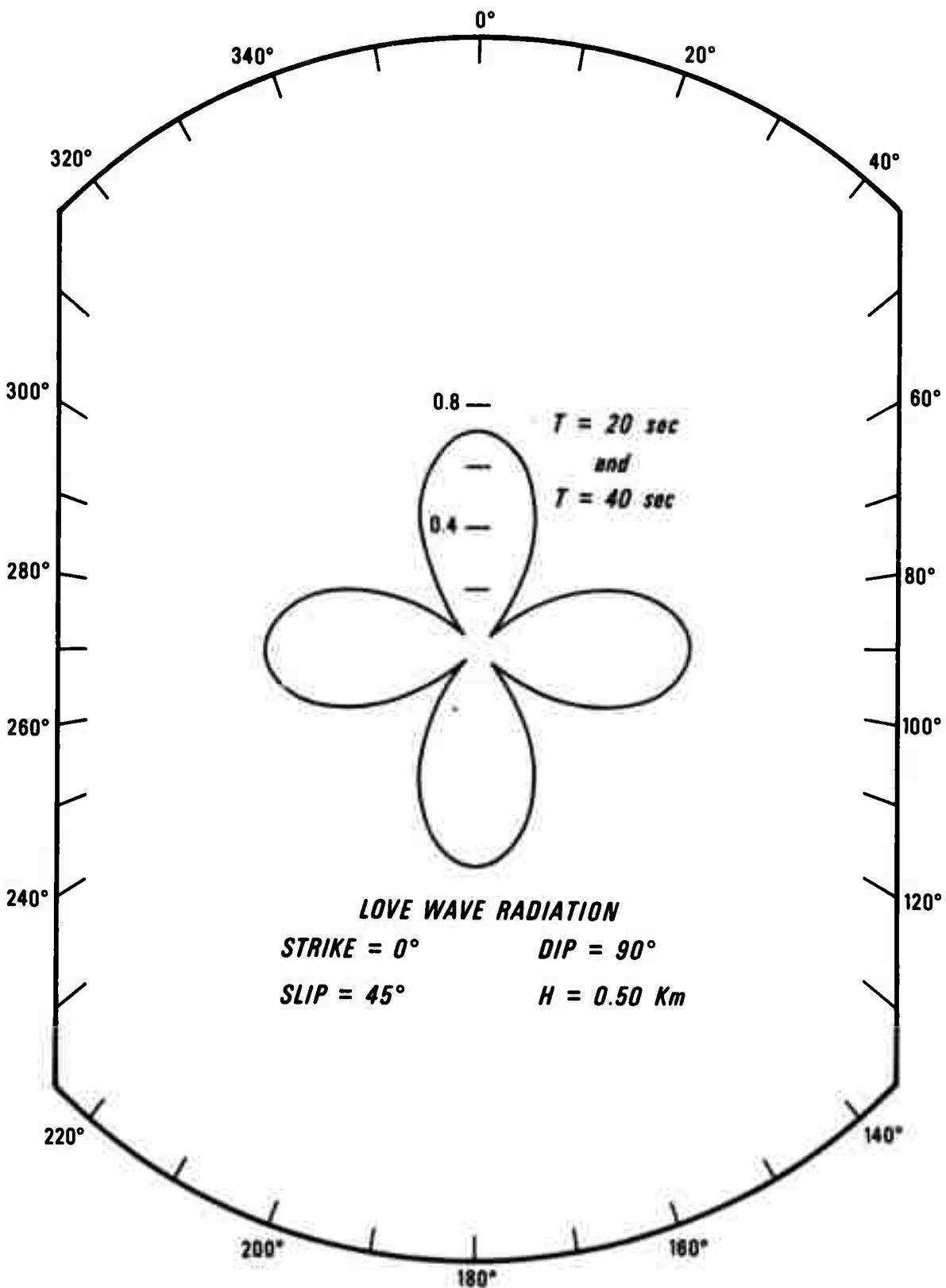


Figure 19. Love radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 0.5 km and with a strike of 0° and a slip of 45° .

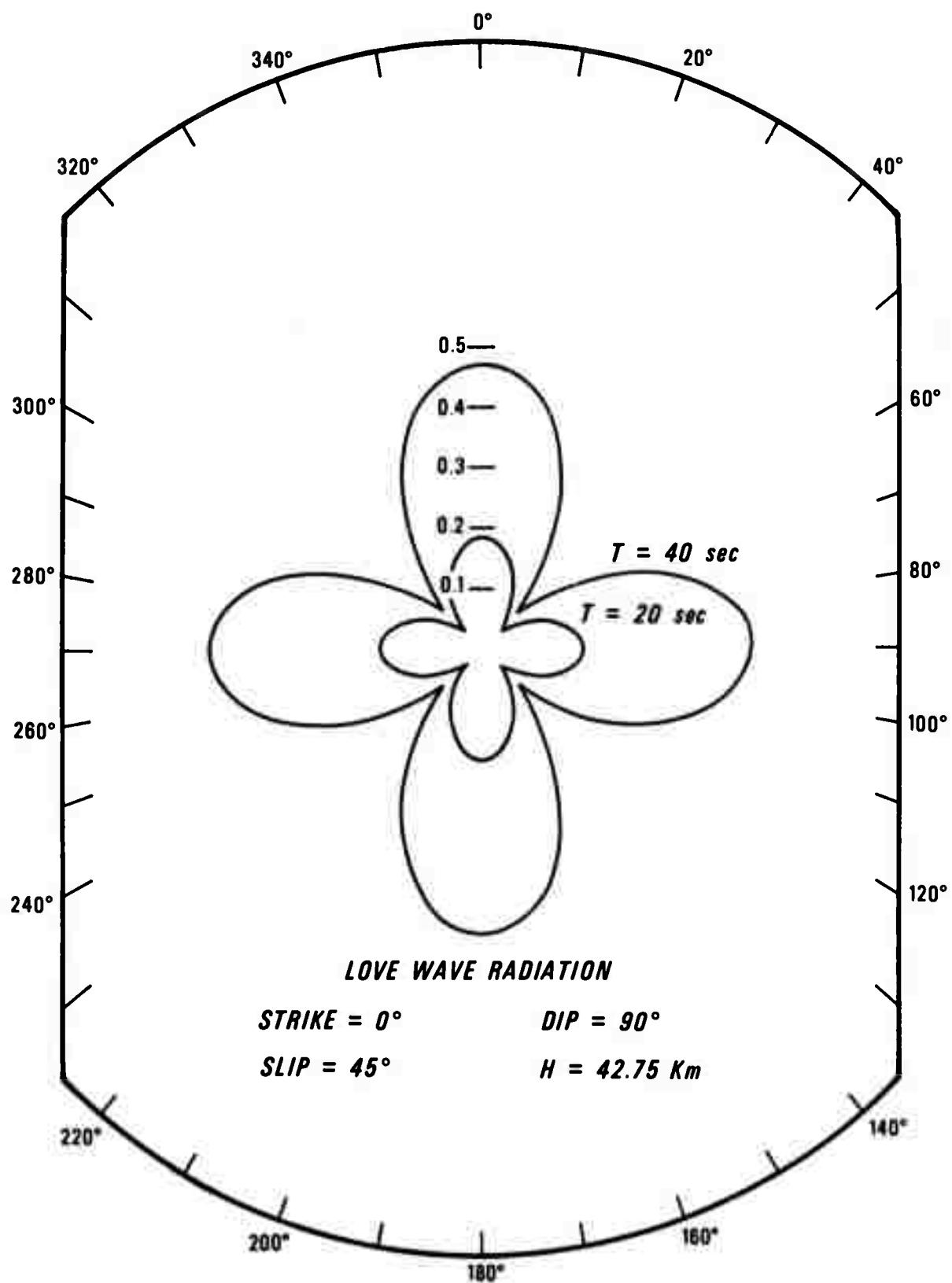


Figure 20. Love radiation pattern for a double couple representation of a left lateral vertical fault source at a depth of 42.75 km and with a strike of 0° and a slip of 45° .

LOVE/RAYLEIGH AMPLITUDE RATIO

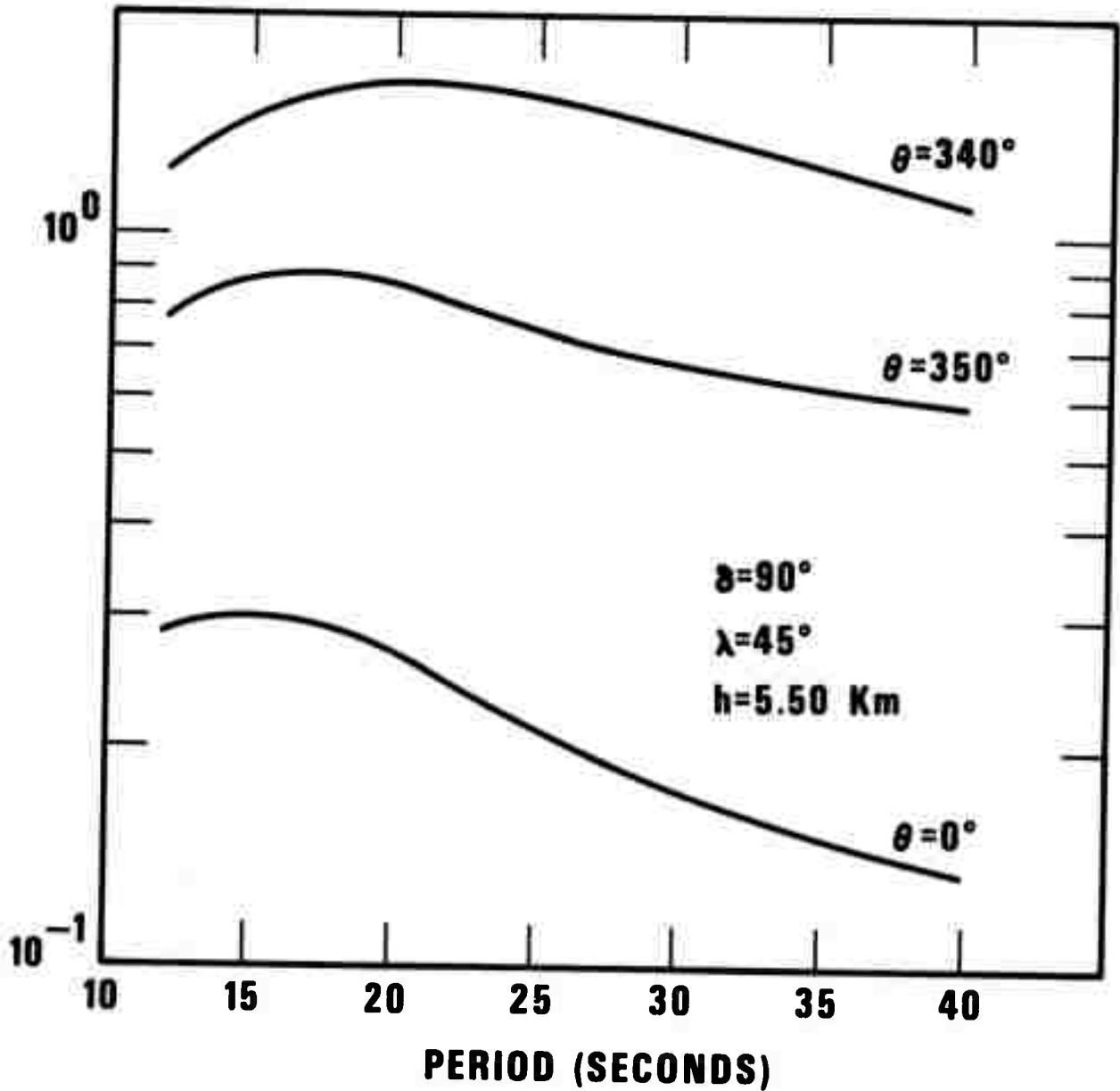


Figure 21. Love/Rayleigh amplitude ratio as a function of period and azimuth.

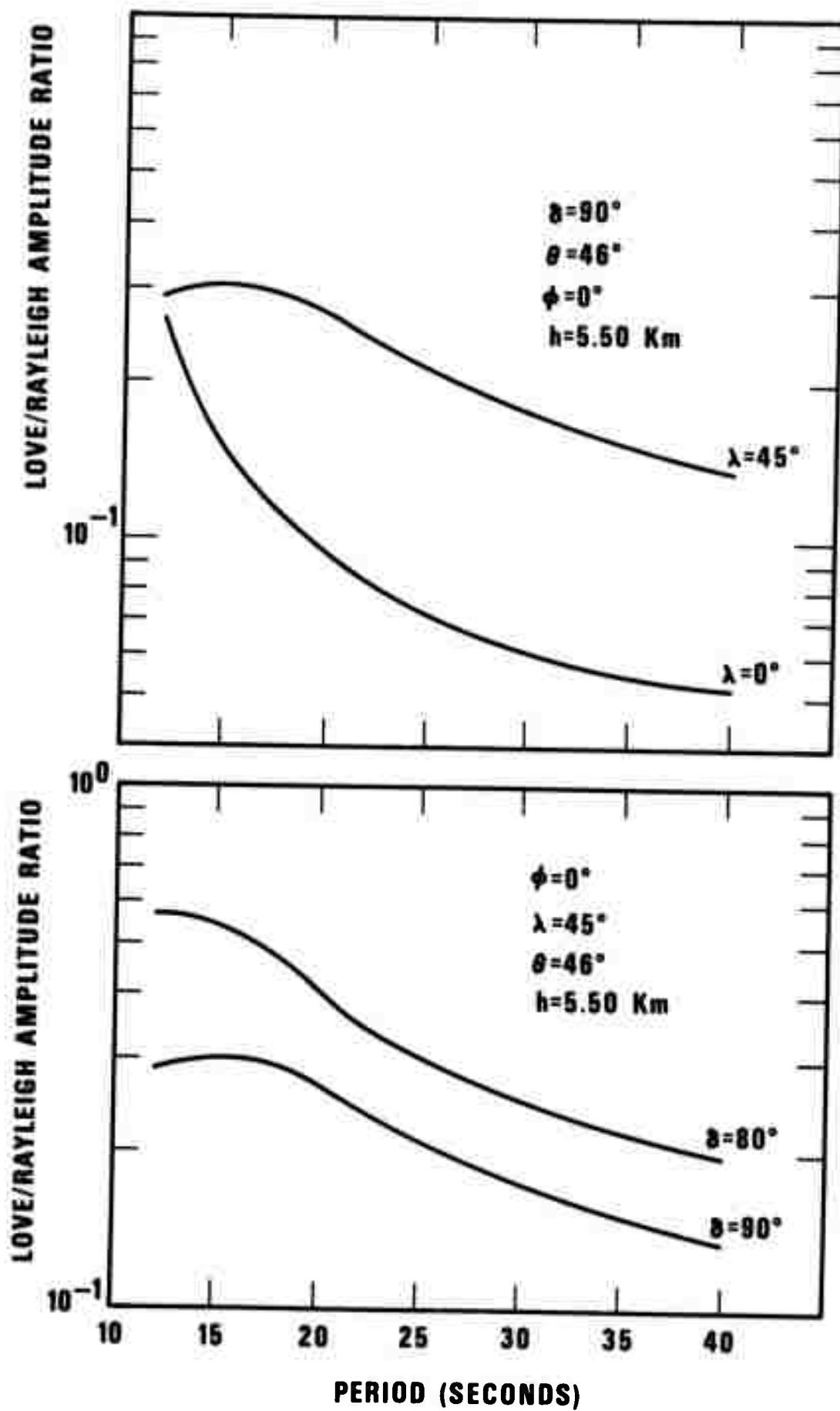


Figure 22. Love/Rayleigh amplitude ratio as a function of period, slip angle and dip angle.

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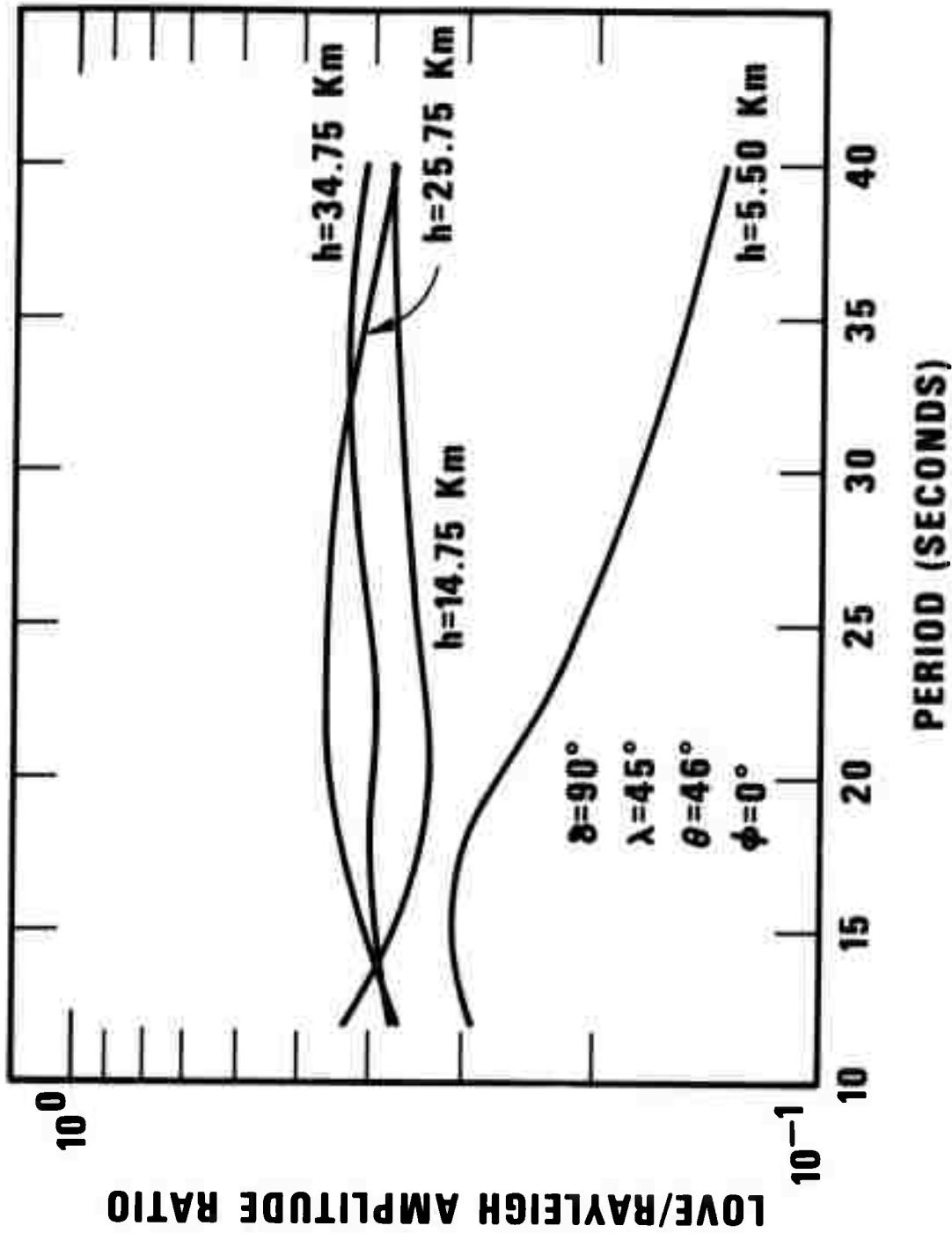


Figure 23. Love/Rayleigh amplitude ratio as a function of period and depth.

TABLE I
Radiation Pattern Coefficients

| Coefficient | Point Force | |
|-------------|--|---|
| | Love | Rayleigh |
| d_0 | 0 | $\sin \lambda \sin \delta W(h)$ |
| d_1 | $\cos \lambda V(h)$ | $-\sin \lambda \cos \delta A(h)$ |
| d_2 | $-\sin \lambda \cos \delta V(h)$ | $-\cos \lambda A(h)$ |
| d_3 | 0 | 0 |
| d_4 | 0 | 0 |
| | | |
| d_0 | $\frac{1}{2} \cos \lambda \sin \delta V(h)$ | $\frac{1}{2} \sin \lambda \sin 2\delta B(h)$ |
| d_1 | $\cos \lambda \cos \delta G(h)$ | $\sin \lambda (W(h) - \cos^2 \delta C(h))$ |
| d_2 | $-\sin \lambda \cos^2 \delta G(h)$ | $\cos \lambda \cos \delta (W(h) - C(h))$ |
| d_3 | $\frac{1}{2} \sin \lambda \sin 2\delta V(h)$ | $\frac{1}{2} \cos \lambda \sin \delta A(h)$ |
| d_4 | $\frac{1}{2} \cos \lambda \sin \delta V(h)$ | $-\frac{1}{2} \sin \lambda \sin 2\delta A(h)$ |
| | | |
| d_0 | 0 | $\frac{1}{2} \sin \lambda \sin 2\delta B(h)$ |
| d_1 | $\cos \lambda \cos \delta G(h)$ | $-\sin \lambda \cos 2\delta C(h)$ |
| d_2 | $-\sin \lambda \cos 2\delta G(h)$ | $-\cos \lambda \cos \delta C(h)$ |
| d_3 | $\frac{1}{2} \sin \lambda \sin 2\delta V(h)$ | $\cos \lambda \sin \delta A(h)$ |
| d_4 | $\cos \lambda \sin \delta V(h)$ | $-\frac{1}{2} \sin \lambda \sin 2\delta A(h)$ |
| | | |
| d_0 | 0 | $\frac{1}{2} \sin \lambda \sin 2\delta B(h)$ |
| d_1 | $\cos \lambda \cos \delta G(h)$ | $-\sin \lambda \cos 2\delta C(h)$ |
| d_2 | $-\sin \lambda \cos 2\delta G(h)$ | $-\cos \lambda \cos \delta C(h)$ |
| d_3 | $\frac{1}{2} \sin \lambda \sin 2\delta V(h)$ | $\cos \lambda \sin \delta A(h)$ |
| d_4 | $\cos \lambda \sin \delta V(h)$ | $-\frac{1}{2} \sin \lambda \sin 2\delta A(h)$ |

The factors $W(h)$, $A(h)$, $C(h)$, $B(h)$, $V(h)$ and $G(h)$ in terms of the Thomson-Haskell displacement-stress vector elements (Haskell, 1953) are:

$$\begin{aligned}
 W(h) &= [\dot{w}_S(h)/\dot{w}_0] \\
 A(h) &= -[\dot{u}_S^*(h)/\dot{w}_0] \\
 C(h) &= -\frac{1}{\omega_S} [\tau_{RS}(h)/(\dot{w}_0/C_R)] \\
 B(h) &= -(3 - 4 \frac{\beta_S^2}{\alpha_S}) (\dot{u}_S^*(h)/\dot{w}_0) + \frac{2}{\rho_S \alpha_S} [\sigma_{RS}^*(h)/(w_0/\bar{C}_R)]
 \end{aligned}$$

TABLE II
BASIN AND RANGE MODEL

| <u>Layer Thickness</u> | P <u>Velocity</u> | S <u>Velocity</u> | <u>Density</u> |
|----------------------------|----------------------|----------------------|----------------|
| 1.0 | 3.000 | 1.732 | 2.250 |
| 9.0 | 6.010 | 3.470 | 2.750 |
| 9.5 | 6.011 | 3.471 | 2.751 |
| 12.5 | 6.910 | 3.980 | 3.100 |
| 5.5 | 7.490 | 4.320 | 3.300 |
| 10.5 | 7.800 | 4.500 | 3.350 |
| 13.0 | 7.750 | 4.470 | 3.320 |
| 20.0 | 7.715 | 4.451 | 3.321 |
| 10.0 | 7.719 | 4.450 | 3.322 |
| 30.0 | 7.725 | 4.460 | 3.323 |
| 10.0 | 7.740 | 4.470 | 3.350 |
| 10.0 | 7.800 | 4.500 | 3.370 |
| 6.0 | 7.900 | 4.510 | 3.390 |
| 2.0 | 8.325 | 4.810 | 3.500 |
| 22.0 | 8.335 | 4.811 | 3.501 |
| 10.0 | 8.340 | 4.820 | 3.510 |
| 20.0 | 8.360 | 4.825 | 3.511 |
| 50.0 | 8.435 | 4.870 | 3.575 |
| 50.0 | 8.530 | 4.920 | 3.600 |
| 50.0 | 8.630 | 4.980 | 3.700 |
| 25.0 | 8.730 | 5.040 | 3.710 |
| 23.0 | 9.100 | 5.250 | 3.720 |
| 2.0 | 9.750 | 5.630 | 4.130 |
| 50.0 | 9.800 | 5.650 | 4.150 |
| 50.0 | 9.850 | 5.680 | 4.200 |
| 50.0 | 9.900 | 5.710 | 4.250 |
| 50.0 | 9.950 | 5.740 | 4.260 |
| 30.0 | 10.000 | 5.770 | 4.270 |
| 15.0 | 10.430 | 6.025 | 4.350 |
| 15.0 | 10.930 | 6.310 | 4.550 |
| 20.0 | 10.940 | 6.320 | 4.600 |
| 20.0 | 10.960 | 6.321 | 4.610 |
| 20.0 | 10.970 | 6.330 | 4.620 |
| 20.0 | 11.000 | 6.350 | 4.630 |
| 20.0 | 11.030 | 6.365 | 4.640 |
| 20.0 | 11.055 | 6.375 | 4.650 |
| 20.0 | 11.085 | 6.390 | 4.690 |
| 40.0 | 11.130 | 6.425 | 4.700 |
| 20.0 | 11.145 | 6.430 | 4.710 |
| 20.0 | 11.160 | 6.435 | 4.720 |
| 20.0 | 11.170 | 6.440 | 4.730 |
| | 11.200 | 6.460 | 4.750 |

TABLE III
DR(h,θ)

T = 12 sec STRIKE = 0° DIP = 90° SLIP = 0°

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \theta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \theta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \theta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \theta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \theta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \theta}$ of Layer 3 |
|----------|---|---|---|---|---|---|
| 10.00 | -9.6514 | -0.07110 | .02670 | -2520 | -0.03618 | |
| 20.00 | -9.3757 | -0.07134 | .02676 | -2570 | -0.03690 | |
| 30.00 | -9.3119 | -0.07123 | .02672 | -2573 | -0.03709 | |
| 40.00 | -9.4139 | -0.07130 | .02675 | -2558 | -0.03687 | |
| 44.00 | -8.2707 | -0.07076 | .02654 | -2598 | -0.03792 | |
| 50.00 | -9.4139 | -0.07130 | .02675 | -2558 | -0.03687 | |
| 60.00 | -9.3145 | -0.07124 | .02672 | -2559 | -0.03677 | |
| 70.00 | -9.3757 | -0.07134 | .02676 | -2570 | -0.03677 | |
| 80.00 | -9.6514 | -0.07110 | .02670 | -2520 | -0.03690 | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | |
| 100.00 | -9.6514 | -0.07110 | .02670 | -2520 | -0.03618 | |
| 110.00 | -9.3757 | -0.07134 | .02676 | -2570 | -0.03618 | |
| 120.00 | -9.3119 | -0.07123 | .02672 | -2573 | -0.03690 | |
| 130.00 | -9.4139 | -0.07130 | .02675 | -2558 | -0.03709 | |
| 134.00 | -8.2707 | -0.07076 | .02654 | -2598 | -0.03687 | |
| 140.00 | -9.4139 | -0.07130 | .02675 | -2558 | -0.03687 | |
| 150.00 | -9.3145 | -0.07124 | .02672 | -2672 | -0.03677 | |
| 160.00 | -9.3757 | -0.07134 | .02676 | -2570 | -0.03690 | |
| 170.00 | -9.6514 | -0.07110 | .02670 | -2520 | -0.03618 | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | |

| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \theta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \theta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \theta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \theta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \theta}$ of Layer 6 |
|----------|---|---|---|---|---|
| 10.00 | -2057 | .005975 | .006652 | .002853 | .01845 |
| 20.00 | -2513 | .009433 | .008718 | .005852 | -.00714 |
| 30.00 | -2343 | .009325 | .011283 | -.007362 | -.00961 |
| 40.00 | -2212 | .008848 | .010059 | -.001836 | -.00236 |
| 44.00 | -1404 | .001230 | .001204 | -.005220 | -.01537 |
| 50.00 | -2212 | .008848 | .010059 | -.001836 | -.00236 |
| 60.00 | -2502 | .009190 | .008773 | -.002499 | -.00716 |
| 70.00 | -2533 | .009433 | .008718 | -.002852 | -.00714 |
| 80.00 | -2057 | .005975 | .006652 | -.002853 | -.01845 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -2057 | .005975 | .006652 | -.002853 | -.01845 |
| 110.00 | -2513 | .009433 | .008718 | -.005852 | -.00714 |
| 120.00 | -2343 | .009325 | .011283 | -.007362 | -.00961 |
| 130.00 | -2212 | .008848 | .010059 | -.001836 | -.00236 |
| 134.00 | -1404 | .001230 | .001204 | -.005220 | -.01537 |
| 140.00 | -2212 | .008848 | .010059 | -.001836 | -.00236 |
| 150.00 | -2502 | .009190 | .008773 | -.002499 | -.00716 |
| 160.00 | -2513 | .009433 | .008718 | -.002852 | -.00714 |
| 170.00 | -2057 | .005975 | .006652 | -.002853 | -.01845 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

DR(h, β)
 T = 16 sec STRIKE = 0° DIP = 90° SLIP = 0°

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 |
|----------|--|--|--|--|--|
| 10.00 | -7.3806 | -.07652 | -.03591 | .03539 | -.04372 |
| 20.00 | -7.4046 | -.07648 | -.03592 | .03509 | -.04331 |
| 30.00 | -7.2791 | -.07638 | -.03583 | .03498 | -.04320 |
| 40.00 | -7.1097 | -.07623 | -.03574 | .03502 | -.04329 |
| 44.00 | -6.3600 | -.07732 | -.03634 | .03469 | -.04261 |
| 50.00 | -7.1097 | -.07623 | -.03574 | .03502 | -.04329 |
| 60.00 | -6.9903 | -.07637 | -.03583 | .03498 | -.04318 |
| 70.00 | -7.4046 | -.07648 | -.03592 | .03509 | -.04351 |
| 80.00 | -7.3806 | -.07652 | -.03591 | .03539 | -.04372 |
| 90.00 | .0 | .0 | .0 | .0 | .0 |
| 100.00 | -7.3806 | -.07652 | -.03591 | .03539 | -.04372 |
| 110.00 | -7.4046 | -.07648 | -.03592 | .03509 | -.04351 |
| 120.00 | -7.2791 | -.07638 | -.03583 | .03498 | -.04320 |
| 130.00 | -7.1097 | -.07623 | -.03574 | .03502 | -.04329 |
| 134.00 | -6.3600 | -.07732 | -.03634 | .03469 | -.04261 |
| 140.00 | -7.1097 | -.07623 | -.03574 | .03502 | -.04329 |
| 150.00 | -6.9903 | -.07637 | -.03583 | .03498 | -.04318 |
| 160.00 | -7.4046 | -.07648 | -.03592 | .03509 | -.04351 |
| 170.00 | -7.3806 | -.07652 | -.03591 | .03539 | -.04372 |
| 180.00 | .0 | .0 | .0 | .0 | .0 |
| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 6 |
| 10.00 | -1920 | -.03007 | -.1069 | -.1046 | -.3439 |
| 20.00 | -1913 | -.02992 | -.1056 | -.1030 | -.3940 |
| 30.00 | -1910 | -.02983 | -.1111 | -.1092 | -.3475 |
| 40.00 | -1916 | -.02984 | -.1091 | -.1065 | -.5092 |
| 44.00 | -1944 | -.03027 | -.1301 | -.1380 | -.4614 |
| 50.00 | -1916 | -.02984 | -.1091 | -.1065 | -.5092 |
| 60.00 | -1928 | -.03023 | -.1115 | -.1092 | -.2798 |
| 70.00 | -1913 | -.02992 | -.1056 | -.1030 | -.3940 |
| 80.00 | -1920 | -.93007 | -.1069 | -.1046 | -.3439 |
| 90.00 | .0 | .0 | .0 | .0 | .0 |
| 100.00 | -1920 | -.03007 | -.1069 | -.1046 | -.3439 |
| 110.00 | -1913 | -.02992 | -.1056 | -.1030 | -.3940 |
| 120.00 | -1910 | -.02983 | -.1111 | -.1092 | -.3475 |
| 130.00 | -1916 | -.02984 | -.1091 | -.1065 | -.5092 |
| 134.00 | -1944 | -.03027 | -.1301 | -.1380 | -.4614 |
| 140.00 | -1916 | -.02984 | -.1091 | -.1065 | -.5092 |
| 150.00 | -1928 | -.03023 | -.1115 | -.1092 | -.2798 |
| 160.00 | -1913 | -.02992 | -.1056 | -.1030 | -.3940 |
| 170.00 | -1920 | -.93007 | -.1069 | -.1046 | -.3439 |
| 180.00 | .0 | .0 | .0 | .0 | .0 |

DR(h,θ)

T = 20 sec STRIKE = 0° DIP = 90°

SLIP = 0°

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \theta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \theta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \theta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \theta}$ of Layer 3 |
|----------|---|---|---|---|
| 10.00 | -5.9840 | -0.06504 | -2.4824 | .02374 |
| 20.00 | -5.6680 | -0.06495 | -2.4678 | .02604 |
| 30.00 | -5.9070 | -0.06495 | -2.4934 | .02602 |
| 40.00 | -5.1638 | -0.06504 | -2.4769 | .02525 |
| 44.00 | -5.0104 | -0.06478 | -2.4740 | .02575 |
| 50.00 | -5.1638 | -0.06504 | -2.4769 | .02525 |
| 60.00 | -5.9070 | -0.06495 | -2.4935 | .02605 |
| 70.00 | -5.6680 | -0.06495 | -2.4678 | .02604 |
| 80.00 | -5.9840 | -0.06504 | -2.4824 | .02374 |
| 90.00 | 0 | 0 | 0 | 0 |
| 100.00 | -5.9840 | -0.06504 | -2.4824 | .02374 |
| 110.00 | -5.6680 | -0.06495 | -2.4678 | .02604 |
| 120.00 | -5.9070 | -0.06495 | -2.4934 | .02602 |
| 130.00 | -5.1638 | -0.06504 | -2.4769 | .02525 |
| 134.00 | -5.0104 | -0.06478 | -2.4740 | .02575 |
| 140.00 | -5.1638 | -0.06504 | -2.4769 | .02525 |
| 150.00 | -5.9070 | -0.06495 | -2.4935 | .02605 |
| 160.00 | -5.6680 | -0.06495 | -2.4678 | .02604 |
| 170.00 | -5.9840 | -0.06504 | -2.4824 | .02374 |
| 180.00 | 0 | 0 | 0 | 0 |

| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \theta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \theta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \theta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \theta}$ of Layer 5 |
|----------|---|---|---|---|
| 10.00 | -1.4430 | -0.02531 | -0.1445 | -.09747 |
| 20.00 | -1.4335 | -0.02518 | -.1471 | -.10007 |
| 30.00 | -1.4505 | -0.02529 | -.1464 | -.09960 |
| 40.00 | -1.4231 | -0.02489 | -.1514 | -.10407 |
| 44.00 | -1.4213 | -0.02485 | -.1227 | -.08207 |
| 50.00 | -1.4231 | -0.02489 | -.1514 | -.10407 |
| 60.00 | -1.4552 | -0.02537 | -.1463 | -.09951 |
| 70.00 | -1.4335 | -0.02518 | -.1471 | -.10007 |
| 80.00 | -1.4430 | -0.02531 | -.1445 | -.09747 |
| 90.00 | 0 | 0 | 0 | 0 |
| 100.00 | -1.4430 | -0.02531 | -.1445 | -.09747 |
| 110.00 | -1.4335 | -0.02518 | -.1471 | -.10007 |
| 120.00 | -1.4505 | -0.02529 | -.1464 | -.09660 |
| 130.00 | -1.4231 | -0.02489 | -.1514 | -.10407 |
| 134.00 | -1.4213 | -0.02485 | -.1227 | -.08207 |
| 140.00 | -1.4231 | -0.02489 | -.1514 | -.10407 |
| 150.00 | -1.4552 | -0.02537 | -.1463 | -.09951 |
| 160.00 | -1.4335 | -0.02518 | -.1471 | -.10007 |
| 170.00 | -1.4430 | -0.02531 | -.1445 | -.09747 |
| 180.00 | 0 | 0 | 0 | 0 |

DR(h,β)

T = 50 sec STRIKE = 0° DIP = 90°

SLIP = 0°

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 3 |
|----------|--|--|--|--|--|
| 10.00 | -3.9039 | -0.04671 | -0.08441 | -0.05052 | -0.2609 |
| 20.00 | -4.3396 | -0.04673 | -0.08450 | -0.05045 | -0.2605 |
| 30.00 | -4.4932 | -0.04676 | -0.08449 | -0.05066 | -0.2616 |
| 40.00 | -3.8748 | -0.04667 | -0.08434 | -0.05050 | -0.2601 |
| 44.00 | 11.3437 | -0.9704 | -0.08501 | -0.05154 | -0.2655 |
| 50.00 | -3.8748 | -0.04667 | -0.08434 | -0.05050 | -0.2601 |
| 60.00 | -4.4901 | -0.04674 | -0.08449 | -0.05066 | -0.2617 |
| 70.00 | -4.3396 | -0.04673 | -0.08450 | -0.05045 | -0.2605 |
| 80.00 | -3.9039 | -0.04671 | -0.08441 | -0.05052 | -0.2609 |
| 90.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 100.00 | -3.9039 | -0.04671 | -0.08441 | -0.05052 | -0.2609 |
| 110.00 | -4.3396 | -0.04673 | -0.08450 | -0.05045 | -0.2605 |
| 120.00 | -4.4932 | -0.04676 | -0.08449 | -0.05066 | -0.2616 |
| 130.00 | -3.8748 | -0.04667 | -0.08434 | -0.05050 | -0.2601 |
| 134.00 | 11.3437 | -0.04704 | -0.08501 | -0.05154 | -0.2655 |
| 140.00 | -3.8748 | -0.04667 | -0.08434 | -0.05050 | -0.2601 |
| 150.00 | -4.4901 | -0.04674 | -0.08449 | -0.05066 | -0.2617 |
| 160.00 | -4.3396 | -0.04673 | -0.08450 | -0.05052 | -0.2605 |
| 170.00 | -3.9039 | -0.04671 | -0.08441 | -0.05052 | -0.2609 |
| 180.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 6 |
|----------|--|--|--|--|--|
| 10.00 | -0.03752 | -0.004499 | 0.006206 | -0.07020 | -0.4621 |
| 20.00 | -0.03711 | -0.004390 | -0.005953 | -0.06813 | -0.4694 |
| 30.00 | -0.03741 | -0.004419 | .006010 | *.6885 | -0.4742 |
| 40.00 | -0.03751 | -0.004548 | .006129 | -0.06857 | -0.4735 |
| 44.00 | -0.03776 | -0.004505 | .006041 | -0.06851 | -0.4801 |
| 50.00 | -0.03751 | -0.004548 | .006129 | -0.06857 | -0.4735 |
| 60.00 | -0.03736 | -0.004418 | .006035 | -0.06908 | -0.4708 |
| 70.00 | -0.03711 | -0.004390 | .005953 | -0.06813 | -0.4694 |
| 80.00 | -0.03752 | -0.004499 | .006206 | -0.07020 | -0.4621 |
| 90.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 100.00 | -0.03752 | -0.004499 | .006206 | -0.07020 | -0.4621 |
| 110.00 | -0.03711 | -0.004390 | -0.005953 | -0.06813 | -0.4694 |
| 120.00 | -0.03741 | -0.004419 | .006010 | -0.06885 | -0.4742 |
| 130.00 | -0.03751 | -0.004548 | .006129 | -0.06857 | -0.4735 |
| 134.00 | -0.03776 | -0.004505 | .006041 | -0.06851 | -0.4801 |
| 140.00 | -0.03751 | -0.004548 | .006129 | -0.06857 | -0.4735 |
| 150.00 | -0.03736 | -0.004418 | .006035 | -0.06908 | -0.4708 |
| 160.00 | -0.03711 | -0.004390 | .005953 | -0.06813 | -0.4694 |
| 170.00 | -0.03752 | -0.004499 | .006206 | -0.07020 | -0.4621 |
| 180.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

DR(h, β)

T = 40 sec STRIKE = 0° DIP = 90°

SLIP = 0°

$$\frac{\partial J}{\partial h} \text{Layer 1 to 2}$$

$$\frac{\partial J}{\partial \beta} \text{of Layer 1}$$

| $\frac{\partial J}{\partial h} \text{Layer 1 to 2}$ | $\frac{\partial J}{\partial \beta} \text{Layer 1 to 2}$ | $\frac{\partial J}{\partial h} \text{Layer 1 to 2}$ | $\frac{\partial J}{\partial \beta} \text{Layer 1 to 2}$ | $\frac{\partial J}{\partial h} \text{Layer 2 to 3}$ | $\frac{\partial J}{\partial \beta} \text{Layer 2 to 3}$ | $\frac{\partial J}{\partial h} \text{Layer 2 to 3}$ | $\frac{\partial J}{\partial \beta} \text{Layer 2 to 3}$ | $\frac{\partial J}{\partial h} \text{Layer 3 to 4}$ | $\frac{\partial J}{\partial \beta} \text{Layer 3 to 4}$ |
|---|---|---|---|---|---|---|---|---|---|
| 10.00 | -5.4639 | -0.04658 | -0.04639 | -0.06326 | -0.05074 | -0.05074 | -0.1059 | -0.1059 | -0.1059 |
| 20.00 | -4.5210 | -0.04639 | -0.06294 | -0.05114 | -0.05114 | -0.05114 | -0.1069 | -0.1069 | -0.1069 |
| 30.00 | -4.8319 | -0.04659 | -0.06330 | -0.05104 | -0.05104 | -0.05104 | -0.1064 | -0.1064 | -0.1064 |
| 40.00 | -4.2014 | -0.04664 | -0.06343 | -0.05103 | -0.05103 | -0.05103 | -0.1066 | -0.1066 | -0.1066 |
| 44.00 | -4.0110 | -0.04698 | -0.06433 | -0.05024 | -0.05024 | -0.05024 | -0.1045 | -0.1045 | -0.1045 |
| 50.00 | -4.2014 | -0.04664 | -0.06343 | -0.05103 | -0.05103 | -0.05103 | -0.1066 | -0.1066 | -0.1066 |
| 60.00 | -4.8318 | -0.04649 | -0.06313 | -0.05102 | -0.05102 | -0.05102 | -0.1064 | -0.1064 | -0.1064 |
| 70.00 | -4.5210 | -0.04639 | -0.06294 | -0.05114 | -0.05114 | -0.05114 | -0.1069 | -0.1069 | -0.1069 |
| 80.00 | -5.4639 | -0.04658 | -0.06326 | -0.05074 | -0.05074 | -0.05074 | -0.1059 | -0.1059 | -0.1059 |
| 90.00 | .0. | .0. | .0. | .0. | .0. | .0. | .0. | .0. | .0. |
| 100.00 | -5.4639 | -0.04658 | -0.06326 | -0.05074 | -0.05074 | -0.05074 | -0.1059 | -0.1059 | -0.1059 |
| 110.00 | -4.5210 | -0.04639 | -0.06294 | -0.05114 | -0.05114 | -0.05114 | -0.1069 | -0.1069 | -0.1069 |
| 120.00 | -4.8319 | -0.04659 | -0.06330 | -0.05104 | -0.05104 | -0.05104 | -0.1064 | -0.1064 | -0.1064 |
| 130.00 | -4.2014 | -0.04664 | -0.06343 | -0.05103 | -0.05103 | -0.05103 | -0.1066 | -0.1066 | -0.1066 |
| 134.00 | -4.0110 | -0.04698 | -0.06433 | -0.05024 | -0.05024 | -0.05024 | -0.1045 | -0.1045 | -0.1045 |
| 140.00 | -4.2014 | -0.04664 | -0.06343 | -0.05103 | -0.05103 | -0.05103 | -0.1066 | -0.1066 | -0.1066 |
| 150.00 | -4.831 | -0.04649 | -0.06313 | -0.05102 | -0.05102 | -0.05102 | -0.1064 | -0.1064 | -0.1064 |
| 160.00 | -4.5210 | -0.04639 | -0.06294 | -0.05114 | -0.05114 | -0.05114 | -0.1069 | -0.1069 | -0.1069 |
| 170.00 | -5.4639 | -0.04658 | -0.06326 | -0.05074 | -0.05074 | -0.05074 | -0.1059 | -0.1059 | -0.1059 |
| 180.00 | .0. | .0. | .0. | .0. | .0. | .0. | .0. | .0. | .0. |

$$\frac{\partial J}{\partial h} \text{Layer 3 to 4}$$

$$\frac{\partial J}{\partial \beta} \text{of Layer 4}$$

| $\frac{\partial J}{\partial h} \text{Layer 3 to 4}$ | $\frac{\partial J}{\partial \beta} \text{of Layer 4}$ | $\frac{\partial J}{\partial h} \text{Layer 4 to 5}$ | $\frac{\partial J}{\partial \beta} \text{of Layer 4}$ | $\frac{\partial J}{\partial h} \text{Layer 5 to 6}$ | $\frac{\partial J}{\partial \beta} \text{of Layer 5}$ | $\frac{\partial J}{\partial h} \text{Layer 5 to 6}$ | $\frac{\partial J}{\partial \beta} \text{of Layer 6}$ |
|---|---|---|---|---|---|---|---|
| 10.00 | -0.06865 | -0.2748 | -0.1464 | -0.2716 | -0.3832 | -0.3832 | -0.3832 |
| 20.00 | -0.06877 | -0.2748 | -0.1528 | -0.2828 | -0.3557 | -0.3557 | -0.3557 |
| 30.00 | -0.06902 | -0.2761 | -0.1559 | -0.2887 | -0.3599 | -0.3599 | -0.3599 |
| 40.00 | -0.06794 | -0.2716 | -0.1563 | -0.2897 | -0.3641 | -0.3641 | -0.3641 |
| 44.00 | -0.06751 | -0.2692 | -0.1558 | -0.2889 | -0.3638 | -0.3638 | -0.3638 |
| 50.00 | -0.06794 | -0.2716 | -0.1563 | -0.2897 | -0.3641 | -0.3641 | -0.3641 |
| 60.00 | -0.06902 | -0.2762 | -0.1559 | -0.2887 | -0.3607 | -0.3607 | -0.3607 |
| 70.00 | -0.06877 | -0.2748 | -0.1528 | -0.2828 | -0.3557 | -0.3557 | -0.3557 |
| 80.00 | -0.06865 | -0.2748 | -0.1464 | -0.2716 | -0.3832 | -0.3832 | -0.3832 |
| 90.00 | .0. | .0. | .0. | .0. | .0. | .0. | .0. |
| 100.00 | -0.06865 | -0.2748 | -0.1464 | -0.2716 | -0.3557 | -0.3557 | -0.3557 |
| 110.00 | -0.06877 | -0.2748 | -0.1428 | -0.2828 | -0.3599 | -0.3599 | -0.3599 |
| 120.00 | -0.06902 | -0.2761 | -0.1559 | -0.2887 | -0.3641 | -0.3641 | -0.3641 |
| 130.00 | -0.06794 | -0.2716 | -0.1563 | -0.2897 | -0.3641 | -0.3641 | -0.3641 |
| 134.00 | -0.06751 | -0.2692 | -0.1558 | -0.2889 | -0.3638 | -0.3638 | -0.3638 |
| 140.00 | -0.06794 | -0.2716 | -0.1563 | -0.2897 | -0.3641 | -0.3641 | -0.3641 |
| 150.00 | -0.06902 | -0.2762 | -0.1559 | -0.2887 | -0.3607 | -0.3607 | -0.3607 |
| 160.00 | -0.06877 | -0.2748 | -0.1528 | -0.2828 | -0.3557 | -0.3557 | -0.3557 |
| 170.00 | -0.06865 | -0.2748 | -0.1464 | -0.2716 | -0.3832 | -0.3832 | -0.3832 |
| 180.00 | .0. | .0. | .0. | .0. | .0. | .0. | .0. |

| T = 12 sec | | STRIKE = 0° | | DIP = 45° | | SLIP = 45° | |
|--|----------|--|---------|--|---------|--|--|
| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 1 | | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | |
| θ | | | | | | | |
| 10.00 | -1.4247 | --1.254 | .05167 | .3409 | .02594 | | |
| 20.00 | -1.1554 | --1.231 | .05064 | .2484 | .01754 | | |
| 30.00 | -.6552 | --1.177 | .04626 | .1371 | .00836 | | |
| 40.00 | -.1420 | -.0806 | .01047 | .0119 | .00028 | | |
| 44.00 | -.0383 | -.0375 | -.02583 | -.0211 | -.00125 | | |
| 50.00 | -.1101 | -.0678 | .01884 | .0212 | -.00074 | | |
| 60.00 | -.2700 | -.0579 | -.07102 | .2020 | | | |
| 70.00 | .3284 | .0643 | .08568 | .2739 | .00338 | | |
| 80.00 | 6.7215 | .5097 | .09427 | .2819 | .00236 | | |
| 90.00 | -.0614 | 4.2732 | .09746 | .2779 | -.00011 | | |
| 100.00 | 6.7215 | .5097 | .09427 | .2819 | -.00116 | | |
| 110.00 | .3284 | .0643 | .08568 | .2739 | -.00011 | | |
| 120.00 | -.2700 | -.0579 | .07102 | .2020 | .00236 | | |
| 130.00 | -.1101 | -.0678 | .01884 | .0212 | -.00074 | | |
| 134.00 | -.0328 | -.0337 | -.02650 | -.0212 | -.00154 | | |
| 140.00 | -.1420 | -.0806 | .01047 | .0119 | .00028 | | |
| 150.00 | -.6552 | -.0579 | .04626 | .1371 | .00836 | | |
| 160.00 | -.1.1554 | -.1.231 | .05064 | .2484 | .01754 | | |
| 170.00 | -1.4247 | -.1.254 | .05167 | .3409 | .02594 | | |
| 180.00 | .0 | .0 | .0 | .0 | .0 | | |

| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | |
|--|---------|--|--------|--|---------|--|--|
| θ | | | | | | | |
| 10.00 | .04561 | -.03085 | .1533 | -.04328 | -.05126 | | |
| 20.00 | .03376 | -.03266 | -.6900 | .33353 | .03831 | | |
| 30.00 | .01704 | -.03458 | -.1165 | .0991 | .06774 | | |
| 40.00 | -.00068 | -.04103 | -.0672 | .08912 | .09471 | | |
| 44.00 | -.00318 | -.04308 | -.0522 | .07238 | .07532 | | |
| 50.00 | -.00170 | -.03837 | -.0616 | .07511 | .07657 | | |
| 60.00 | .00589 | -.02106 | .2973 | .09251 | .01767 | | |
| 70.00 | .00378 | -.01109 | .0265 | .08211 | .01804 | | |
| 80.00 | -.00017 | -.00787 | .0167 | .08780 | .08820 | | |
| 90.00 | -.00170 | -.00704 | .0149 | .08780 | .08820 | | |
| 100.00 | -.00017 | -.00787 | .0167 | .08780 | .08820 | | |
| 110.00 | .00378 | -.01109 | .0265 | .08211 | .01767 | | |
| 120.00 | -.00589 | -.02106 | .2973 | .09251 | .01804 | | |
| 130.00 | -.00017 | -.00787 | .0167 | .08780 | .08820 | | |
| 134.00 | -.00318 | -.04155 | -.0539 | -.07713 | -.07657 | | |
| 140.00 | -.00068 | -.04103 | -.0672 | .08912 | .08940 | | |
| 150.00 | -.01704 | -.03458 | -.1165 | .0991 | .09471 | | |
| 160.00 | .03376 | -.03266 | -.6900 | .33353 | .06774 | | |
| 170.00 | -.04561 | -.04308 | -.0522 | .07238 | .07532 | | |
| 180.00 | .0 | .0 | .0 | .0 | .0 | | |

DR(h, g)

T = 16 Sec STRIKE = 0° DIP = 90°

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 1 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 2 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 3 |
|--|--|--|--|--|
| 10.00 | -2.2671 | -0.07832 | .02395 | .04386 |
| 20.00 | -1.8846 | -0.07769 | .02415 | .04111 |
| 30.00 | -1.1101 | -0.07554 | .02213 | .06153 |
| 40.00 | - .2766 | -0.06226 | .00065 | .00094 |
| 44.00 | - .0942 | -0.04399 | -.02350 | -.02210 |
| 50.00 | - .2637 | -0.06012 | .01137 | .01605 |
| 60.00 | -1.0270 | -0.05779 | .04725 | .17731 |
| 70.00 | - .3196 | -0.01272 | .06168 | .28262 |
| 80.00 | -2.5393 | .18228 | .07459 | .33182 |
| 90.00 | - .0755 | 1.83957 | .08074 | .34588 |
| 100.00 | -2.5393 | .18228 | .07459 | .33182 |
| 110.00 | - .3196 | -0.01272 | .06168 | .28262 |
| 120.00 | -1.0270 | -0.05779 | .04725 | .17731 |
| 130.00 | - .2637 | -0.06012 | .01137 | .01605 |
| 140.00 | - .0895 | -0.04319 | -.02246 | -.02113 |
| 150.00 | - .2680 | -0.06226 | .00065 | .00084 |
| 160.00 | -1.1101 | -0.07554 | .02213 | .06153 |
| 170.00 | -1.8846 | -0.07769 | .02415 | .09411 |
| 180.00 | -2.2671 | -0.07832 | .02395 | .04386 |
| | 0 | 0 | 0 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 6 |
|--|--|--|--|--|
| 10.00 | -1.18322 | -.07707 | -.1623 | -.1761 |
| 20.00 | - .22694 | -.09800 | -.1876 | -.2296 |
| 30.00 | - .65401 | -.28764 | 1.3365 | 2.3063 |
| 40.00 | - .07914 | .03409 | .0354 | .1432 |
| 44.00 | - .04029 | .01728 | .0190 | .1225 |
| 50.00 | - .07578 | .03684 | .0432 | .1640 |
| 60.00 | - .26568 | -.15052 | -.1097 | -.0923 |
| 70.00 | -1.5722 | -.09654 | -.0715 | -.0283 |
| 80.00 | -1.4630 | -.09460 | -.0662 | -.0174 |
| 90.00 | -1.4216 | -.09391 | -.0648 | -.0139 |
| 100.00 | -1.4630 | -.09460 | -.0662 | -.0174 |
| 110.00 | -1.5722 | -.09654 | -.0715 | -.0283 |
| 120.00 | - .26568 | -.15052 | -.1097 | -.0923 |
| 130.00 | -1.4630 | -.09460 | -.0662 | -.0174 |
| 134.00 | .03949 | .03684 | .0432 | .1640 |
| 140.00 | .07914 | .01721 | .0185 | .1211 |
| 150.00 | - .65401 | -.28764 | 1.3365 | .1432 |
| 160.00 | - .22694 | -.09800 | -.1876 | 2.3063 |
| 170.00 | -1.8846 | -.07707 | -.1623 | -.2296 |
| 180.00 | 0 | 0 | 0 | 0 |

DR(h, ϵ)
T = 20 sec STRIKE = 0° DIP = 90° SLIP = 45°

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \epsilon}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \epsilon}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 1 to 3 $\frac{\partial J}{\partial \epsilon}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \epsilon}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \epsilon}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \epsilon}$ of Layer 3 |
|---|---|---|---|---|---|
| 10.00 | -2.2591 | -0.06083 | .002448 | .004394 | .02932 |
| 20.00 | -2.0036 | -0.06027 | .003297 | .006181 | .02661 |
| 30.00 | -1.2126 | -0.05845 | .002532 | .004033 | .02051 |
| 40.00 | - .3073 | -0.05085 | -.017174 | -.015659 | -.01022 |
| 44.00 | - .1120 | -0.04039 | -.039425 | -.027573 | -.00728 |
| 50.00 | - .3377 | -0.04957 | -.002342 | -.002599 | .01057 |
| 60.00 | -1.6385 | -0.04795 | -.032428 | .094583 | .02541 |
| 70.00 | -1.9351 | -0.02633 | .046145 | .181735 | .03089 |
| 80.00 | -1.4660 | .07367 | .058907 | .255328 | .03199 |
| 90.00 | - .0815 | 1.01349 | .065675 | .288873 | .03211 |
| 100.00 | -1.4660 | .07367 | .058907 | .255328 | .03199 |
| 110.00 | -1.9351 | .02633 | .046145 | .181735 | .03089 |
| 120.00 | -1.6385 | .04795 | .032428 | .094583 | .02541 |
| 130.00 | - .3377 | .04957 | -.002342 | -.002599 | .01057 |
| 134.00 | - .1086 | -.03998 | -.037162 | -.026595 | -.00717 |
| 140.00 | - .3073 | -.05085 | -.017174 | -.015659 | .01022 |
| 150.00 | -1.2126 | -.05845 | -.002532 | .004033 | .02051 |
| 160.00 | -2.0036 | -.06027 | -.002597 | .006181 | .02661 |
| 170.00 | -2.2591 | -.06083 | .002248 | .004394 | .02932 |
| 180.00 | .0 | .0 | .0 | .0 | .0 |

| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \epsilon}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \epsilon}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \epsilon}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \epsilon}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \epsilon}$ of Layer 6 |
|---|---|---|---|---|
| 10.00 | .0975 | -.05790 | -.009257 | -.007838 |
| 20.00 | .1032 | -.06372 | -.008969 | -.008012 |
| 30.00 | -.1404 | -.09501 | -.008667 | -.009027 |
| 40.00 | .2972 | .27784 | -.008591 | -.012865 |
| 44.00 | .0896 | .10141 | -.308569 | -.014587 |
| 50.00 | .3590 | .33212 | -.007740 | -.011058 |
| 60.00 | -.1001 | -.06363 | -.006361 | -.004858 |
| 70.00 | -.0861 | .05156 | -.005750 | -.003241 |
| 80.00 | -.0828 | .04905 | -.005418 | -.004858 |
| 90.00 | -.0828 | -.04895 | -.005312 | -.002649 |
| 100.00 | -.0828 | -.04905 | -.005418 | -.002498 |
| 110.00 | -.0861 | -.05156 | -.005750 | -.002649 |
| 120.00 | -.1001 | -.06363 | -.006361 | -.003241 |
| 130.00 | .3590 | .33212 | -.007740 | -.3547 |
| 134.00 | .0861 | .09843 | -.008397 | -.011058 |
| 140.00 | .2972 | .27784 | -.008391 | -.014400 |
| 150.00 | -.1404 | -.09501 | -.008667 | -.012865 |
| 160.00 | -.1032 | -.06372 | -.009569 | -.009027 |
| 170.00 | -.0975 | -.05790 | -.009257 | -.5373 |
| 180.00 | .0 | .0 | .0 | .0 |

DR(h,β)

T = 30 sec STRIKE = 0° DIP = 90° SLIP = 45°

| θ | $\frac{\partial J}{\partial h}$ Layers 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 3 |
|----------|---|--|--|--|--|
| 10.00 | -2.1967 | -0.04443 | -0.02999 | -0.02764 | 0.0298 |
| 20.00 | -1.8462 | -0.04414 | -0.02892 | -0.02617 | 0.0382 |
| 30.00 | -1.2135 | -0.04335 | -0.02989 | -0.02444 | 0.0430 |
| 40.00 | -3.1110 | -0.04099 | -0.05118 | -0.02832 | 0.0224 |
| 44.00 | -1.1114 | -0.93778 | -0.08307 | -0.03368 | 0.0136 |
| 50.00 | -3.8005 | -0.04018 | -0.03411 | -0.02177 | 0.0512 |
| 60.00 | -2.1024 | -0.03840 | -0.01192 | -0.01879 | 0.1769 |
| 70.00 | -4.2831 | -0.02951 | -0.03224 | -0.07698 | 0.2492 |
| 80.00 | -6.6953 | -0.01381 | -0.05211 | -0.18122 | 0.2892 |
| 90.00 | -0.0845 | -0.60231 | -0.06544 | -0.28016 | 0.3035 |
| 100.00 | -6.6953 | -0.01381 | -0.05211 | -0.18122 | 0.2892 |
| 110.00 | -4.2831 | -0.02951 | -0.03224 | -0.07698 | 0.2492 |
| 120.00 | -2.1024 | -0.03840 | -0.01192 | -0.01879 | 0.1769 |
| 130.00 | -3.8005 | -0.04018 | -0.03411 | -0.02177 | 0.0512 |
| 134.00 | -1.1116 | -0.03779 | -0.07995 | -0.03326 | 0.0170 |
| 140.00 | -3.1110 | -0.04099 | -0.05518 | -0.02332 | 0.0224 |
| 150.00 | -1.2135 | -0.04335 | -0.02989 | -0.02444 | 0.0430 |
| 160.00 | -1.8462 | -0.04414 | -0.02892 | -0.02617 | 0.0383 |
| 170.00 | -2.1967 | -0.04443 | -0.02999 | -0.02764 | 0.0298 |
| 180.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 6 |
|----------|--|--|--|--|--|
| 10.00 | .08442 | -0.4172 | -0.06157 | -0.06667 | 0.08626 |
| 20.00 | .0877 | -0.3269 | -0.06731 | -0.07292 | 0.09366 |
| 30.00 | .0499 | .1510 | -0.09395 | -0.10468 | -0.13630 |
| 40.00 | .0125 | .0573 | .56006 | .72887 | .69736 |
| 44.00 | .0067 | .0447 | .13454 | .18745 | .18903 |
| 50.00 | .0334 | .0674 | 28.57270 | 34.53836 | 2.31319 |
| 60.00 | -1.4489 | -1.1442 | -0.06226 | -0.05239 | -0.06765 |
| 70.00 | -3.272 | -1.1964 | -0.05093 | -0.03706 | -0.04882 |
| 80.00 | -3041 | -1.1601 | -0.04923 | -0.03347 | -0.04384 |
| 90.00 | -3064 | -1.1549 | -0.04864 | -0.03140 | -0.04553 |
| 100.00 | -3041 | -1.1601 | -0.04923 | -0.03347 | -0.04384 |
| 110.00 | -3272 | -1.1964 | -0.05093 | -0.03706 | -0.04882 |
| 120.00 | -1.4489 | -1.1442 | -0.06226 | -0.05239 | -0.06765 |
| 130.00 | -0.0334 | .0674 | 28.57270 | 34.53836 | 2.31319 |
| 134.00 | .0083 | .0445 | .13377 | .18437 | .17975 |
| 140.00 | .0125 | .0573 | .56006 | .72887 | .69736 |
| 150.00 | .0499 | .1510 | .09195 | .10468 | -0.13630 |
| 160.00 | .0877 | .3269 | -0.06731 | -0.07292 | -0.09366 |
| 170.00 | .0842 | .4172 | -0.06157 | -0.06667 | -0.08626 |
| 180.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

DR(h, β)

T = 40 sec STRIKE = 0° DIP = 90° SLIP = 45°

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \beta}$ of Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 3 |
|----------|--|--|--|--|--|
| 10.00 | -2.6321 | -0.04493 | -0.04220 | -0.03629 | -0.02188 |
| 20.00 | -1.9842 | -0.04462 | -0.04220 | -0.03504 | -0.01871 |
| 30.00 | -1.2874 | -0.04423 | -0.04528 | -0.03314 | -0.01377 |
| 40.00 | -0.3546 | -0.04307 | -0.07790 | -0.03406 | -0.00826 |
| 44.00 | -0.1147 | -0.04236 | -0.11333 | -0.03877 | -0.00666 |
| 50.00 | -0.4102 | -0.04225 | -0.05684 | -0.02987 | -0.00322 |
| 60.00 | -2.55610 | -0.04068 | -0.00331 | -0.00411 | -0.01024 |
| 70.00 | -6.1954 | -0.03456 | -0.02477 | -0.04522 | -0.02453 |
| 80.00 | -0.1574 | -0.00256 | -0.06022 | -0.17678 | -0.92453 |
| 90.00 | -0.0812 | -0.82196 | -0.09073 | -0.39952 | -0.03664 |
| 100.00 | -0.1574 | -0.00256 | -0.06022 | -0.17678 | -0.04168 |
| 110.00 | -6.1954 | -0.03456 | -0.02477 | -0.04522 | -0.03664 |
| 120.00 | -2.55610 | -0.04068 | -0.00331 | -0.00411 | -0.01024 |
| 130.00 | -0.4102 | -0.04225 | -0.05684 | -0.02987 | -0.00322 |
| 134.00 | -0.1144 | -0.04239 | -0.11131 | -0.03845 | -0.00591 |
| 140.00 | -0.3546 | -0.04307 | -0.07790 | -0.03406 | -0.00826 |
| 150.00 | -1.2874 | -0.04423 | -0.04528 | -0.03314 | -0.01377 |
| 160.00 | -11.9842 | -0.04462 | -0.04220 | -0.03504 | -0.01871 |
| 170.00 | -2.6321 | -0.04493 | -0.04220 | -0.03629 | -0.02188 |
| 180.00 | .0 | .0 | .0 | .0 | .0 |

| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \beta}$ of Layer 6 |
|----------|--|--|--|--|--|
| 10.00 | -0.05783 | .001706 | -0.01942 | -0.05887 | -0.06245 |
| 20.00 | -0.05078 | .006647 | -0.008420 | -0.06590 | -0.07269 |
| 30.00 | -0.03670 | .012988 | -0.028026 | -0.10486 | -0.11476 |
| 40.00 | -0.01964 | .014801 | -0.080908 | -0.20738 | -0.22030 |
| 44.00 | -0.01536 | .014181 | -0.038993 | -0.09426 | -0.09642 |
| 50.00 | -0.00891 | .022542 | -0.235278 | -0.43751 | -0.41349 |
| 60.00 | .06652 | .091824 | -0.048090 | -0.05663 | -0.07220 |
| 70.00 | .38681 | .277720 | -0.047927 | -0.04461 | -0.05774 |
| 80.00 | 3.16454 | 1.689635 | -0.048090 | -0.05663 | -0.07220 |
| 90.00 | -19.07733 | -9.273250 | -0.051917 | -0.43751 | -0.41349 |
| 100.00 | 3.16454 | 1.689635 | -0.053346 | -0.04253 | -0.05556 |
| 110.00 | .38681 | .277720 | -0.047927 | -0.04302 | -0.05686 |
| 120.00 | .06652 | .091824 | -0.047927 | -0.04461 | -0.05774 |
| 130.00 | -0.00891 | .022542 | -0.048090 | -0.05663 | -0.07220 |
| 134.00 | -0.01394 | .015185 | -0.235278 | -0.43751 | -0.41349 |
| 140.00 | -0.01964 | .014801 | -0.041670 | -0.09431 | -0.09352 |
| 150.00 | -0.03670 | .012988 | -0.080908 | -0.20738 | -0.22030 |
| 160.00 | -0.05078 | .006647 | -0.028026 | -0.10486 | -0.11476 |
| 170.00 | -0.05783 | .001706 | -0.06590 | -0.08420 | -0.07269 |
| 180.00 | .0 | .0 | .0 | .0 | .0 |

TABLE IV
DR(h, δ)

T = 12 Seconds $\lambda = 0^\circ$

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 |
|----------|---|---|---|---|---|
| 10.00 | 14589.1200 | 2.7674 | -1.0384 | -2.9176 | -4193 |
| 20.00 | -486487.9236 | 4.8239 | -1.8101 | -5.9563 | -8560 |
| 30.00 | -10542.1116 | 7.7863 | -2.9217 | -10.6092 | -1.5247 |
| 40.00 | -711.5536 | 11.8042 | -4.4294 | -25.4075 | -3.6514 |
| 44.00 | -28.2917 | -57.3203 | 21.5089 | 2.2194 | .3190 |
| 50.00 | -501.3786 | 16.3930 | -6.1513 | -83.5137 | -12.0021 |
| 56.00 | -3252.0278 | 18.9374 | -7.1061 | -31.8388 | -4.5757 |
| 60.00 | -6521.5246 | 21.7255 | -8.1523 | -34.5805 | -4.9697 |
| 70.00 | -8968.6165 | 23.5805 | -8.8484 | -37.0468 | -5.3242 |
| 80.00 | 0 | 0 | 0 | 0 | 0 |
| 90.00 | -8968.6166 | 23.5805 | -8.8484 | -37.0468 | -5.3242 |
| 100.00 | -6521.5245 | 21.7255 | -8.1523 | -34.5805 | -4.9697 |
| 110.00 | -3252.0279 | 18.9374 | -7.1061 | -31.8388 | -4.5757 |
| 120.00 | -501.3785 | 16.3930 | -6.1513 | -83.5137 | -12.0021 |
| 130.00 | -26.6139 | -34.5384 | 12.9602 | 2.0627 | .2964 |
| 134.00 | -711.5536 | 11.8042 | -4.4294 | -25.4075 | -3.6514 |
| 140.00 | -10542.1117 | 7.7863 | -2.9217 | -10.6092 | -1.5247 |
| 150.00 | -486488.3973 | 4.8239 | -1.8101 | -5.9563 | -8560 |
| 160.00 | -14589.1201 | 2.7674 | -1.0384 | -2.9176 | -4193 |
| 170.00 | 0 | 0 | 0 | 0 | 0 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |
| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 |
| 10.00 | -6797 | 0.0249 | .0248 | -0.138 | -0.170 |
| 20.00 | -1.6082 | .0589 | .0588 | -0.0376 | -0.0419 |
| 30.00 | -3.0921 | .1133 | .1143 | -0.0731 | -0.0816 |
| 40.00 | -15.6617 | .5737 | 2.3444 | -1.4990 | -3.6779 |
| 44.00 | -3430 | -0.0126 | -0.0100 | .0064 | .0093 |
| 50.00 | 16.7034 | -6.6118 | -2.8552 | .1823 | .5539 |
| 60.00 | -11.3750 | .4167 | .4772 | -0.3051 | -2.2975 |
| 70.00 | -11.4750 | .4203 | .4492 | -0.2872 | -3.3207 |
| 80.00 | -12.0826 | .4426 | .4656 | -0.2977 | -3.3037 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -12.0826 | .4426 | .4656 | -0.2977 | -3.3037 |
| 110.00 | -11.4750 | .4203 | .4492 | -0.3051 | -2.2975 |
| 120.00 | -11.3750 | .4167 | .4772 | -0.2872 | -3.3207 |
| 130.00 | 16.7034 | -6.6118 | -2.8552 | .1823 | .5539 |
| 134.00 | -5218 | -0.0118 | .0094 | .0060 | .0087 |
| 140.00 | -15.6617 | .5737 | 2.3444 | -1.4990 | -3.6779 |
| 150.00 | -3.0921 | .1133 | .1143 | -0.0731 | -0.0816 |
| 160.00 | -1.6082 | .0589 | .0588 | -0.0376 | -0.0419 |
| 170.00 | -6797 | .0249 | .0248 | -0.138 | -0.170 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

J4

T = 12 Seconds $\lambda = 45^\circ$ DR(h, δ)

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 |
|----------|---|---|---|---|---|---|---|---|---|---|
| 10.00 | 17.2177 | - .1360 | .0560 | - .2890 | - .2474 | | | | | |
| 20.00 | 73.3978 | - .7091 | .2916 | 10.2811 | .7274 | | | | | |
| 30.00 | -26.4127 | - .9781 | .3841 | 2.6445 | .1641 | | | | | |
| 40.00 | -3.9267 | - .5567 | .0721 | .2818 | .0074 | | | | | |
| 44.00 | -1.8361 | - .2827 | - .1955 | - .7093 | .0430 | | | | | |
| 50.00 | 1.9555 | 2.7186 | - .7521 | - .8527 | .5601 | | | | | |
| 60.00 | .9271 | 2.3682 | -2.9008 | -3.8755 | .0676 | | | | | |
| 70.00 | - .6474 | -10.7102 | -14.2720 | -6.9867 | .0621 | | | | | |
| 80.00 | -1.9708 | 138.1522 | 25.5577 | -16.8289 | .0054 | | | | | |
| 90.00 | -2.1904 | 419.3027 | 9.5734 | 87.2187 | .3492 | | | | | |
| 100.00 | .3829 | 32.8830 | 6.0814 | 12.3435 | .0040 | | | | | |
| 110.00 | .1744 | 2.9510 | 3.9325 | 6.1700 | .0548 | | | | | |
| 120.00 | - .4080 | -1.6930 | 2.0737 | 3.4003 | .0593 | | | | | |
| 130.00 | - .6595 | -1.0277 | .2843 | .8610 | .0304 | | | | | |
| 134.00 | - .5191 | - .6548 | - .5125 | -185.6569 | -13.2884 | | | | | |
| 140.00 | 4.6950 | 1.2565 | - .1628 | - .3099 | .0082 | | | | | |
| 150.00 | 16.5548 | 2.2071 | - .8667 | - 1.8221 | .1131 | | | | | |
| 160.00 | -65.6186 | 2.5470 | -1.0475 | -2.3548 | .1666 | | | | | |
| 170.00 | -11.1622 | 2.0672 | - .8513 | -1.7192 | .1293 | | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | | | | | |
| | | | | | | | | | | |
| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 | | | | | |
| 10.00 | - .2379 | .1688 | .1726 | - .0440 | - .0467 | | | | | |
| 20.00 | 6.8817 | -6.7287 | -3.0352 | 1.4599 | 1.0565 | | | | | |
| 30.00 | .2525 | - .5174 | - .4969 | .4311 | .4040 | | | | | |
| 40.00 | - .0098 | - .5354 | - .5352 | .7049 | .6450 | | | | | |
| 44.00 | - .0567 | - .7445 | - .7274 | 1.0282 | .9745 | | | | | |
| 50.00 | .1621 | 3.6437 | -957.6124 | 1179.0552 | -2.5558 | | | | | |
| 60.00 | - .0617 | - .2109 | - .2385 | .0804 | .0618 | | | | | |
| 70.00 | - .0513 | - .1500 | - .1609 | .4831 | .3991 | | | | | |
| 80.00 | - .0038 | .2267 | .2455 | 1.2414 | 1.0135 | | | | | |
| 90.00 | 8.4032 | 37.0932 | -4.9960 | -28.7174 | 427.9968 | | | | | |
| 100.00 | - .0038 | - .2246 | - .204 | - 1.1146 | .9906 | | | | | |
| 110.00 | - .0494 | - 1444 | - .1469 | - .4410 | .6604 | | | | | |
| 120.00 | .0545 | - .1862 | - .1987 | - .0670 | .2303 | | | | | |
| 130.00 | - .0294 | - .6608 | - .9114 | 1.1221 | .1008 | | | | | |
| 134.00 | -1.5160 | -16.8721 | 3.5790 | 5.0351 | .6243 | | | | | |
| 140.00 | - .0092 | - .5051 | - 4730 | .6231 | .0182 | | | | | |
| 150.00 | - .1345 | - 2757 | - .2655 | - .2303 | .2364 | | | | | |
| 160.00 | - .2105 | - 2058 | - 1970 | - .0948 | .1008 | | | | | |
| 170.00 | - .1568 | .1113 | .1076 | - .0275 | .0291 | | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | | | | | |

DR(h, δ) $T = 16$ Seconds $\lambda = 0^\circ$

| θ | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 1 | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 3 | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 3 |
|----------|---|---|---|---|---|
| 10.00 | 4866.1606 | 5.4202 | 2.5454 | .5677 | -.7007 |
| 20.00 | 46914.3226 | 15.8211 | 7.4299 | .8656 | -1.0683 |
| 30.00 | -7099.1588 | 31.9851 | 15.0208 | 1.2822 | -1.5825 |
| 40.00 | -443.3283 | 67.3625 | 31.6346 | 2.0361 | -2.5129 |
| 44.00 | -16.7768 | -9.0434 | -4.2469 | -.8645 | 1.0670 |
| 50.00 | -311.5883 | 139.5038 | 65.5134 | 3.0794 | -5.8005 |
| 60.00 | -2039.5212 | 100.7815 | 47.3287 | 2.9023 | -3.5819 |
| 70.00 | -4113.7526 | 113.3522 | 53.2321 | 3.2401 | -3.9988 |
| 80.00 | -5676.9895 | 122.8341 | 57.6850 | 3.4802 | -4.2952 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -5676.9896 | 122.8341 | 57.6850 | 3.4802 | -4.2952 |
| 110.00 | -4113.7529 | 113.3522 | 53.2321 | 3.2401 | -3.9988 |
| 120.00 | -2039.5212 | 100.7815 | 47.3287 | 2.9023 | -3.5819 |
| 130.00 | -311.5883 | 139.5038 | 65.5134 | 3.0794 | -3.8005 |
| 134.00 | -15.7431 | -8.3060 | -3.9006 | -.7716 | .9523 |
| 140.00 | -443.3283 | 67.3625 | 31.6346 | 2.0361 | -2.5129 |
| 150.00 | -7099.1580 | 31.9851 | 15.0208 | 1.2822 | -1.5825 |
| 160.00 | -46914.3337 | 15.8211 | 7.4299 | .8656 | -1.0683 |
| 170.00 | -4866.1607 | 5.4202 | 2.5454 | .5677 | -.7007 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |
| θ | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 |
| 10.00 | -2.0860 | -3264 | -3984 | -.3917 | -.5159 |
| 20.00 | -1.3220 | -6763 | -.8536 | -.8393 | -1.1924 |
| 30.00 | -7.7929 | -1.2194 | -1.5716 | -1.5452 | -2.2570 |
| 40.00 | -23.3584 | -3.6550 | -6.4659 | -6.3574 | -7.5179 |
| 44.00 | -1.2479 | -1.953 | 2010 | 1.1977 | -3.3173 |
| 50.00 | -1604.2055 | -251.0144 | -12.5638 | 12.3529 | 61.5763 |
| 60.00 | -24.8746 | -3.8922 | -5.4182 | -5.3272 | -7.6338 |
| 70.00 | -26.2789 | -4.1119 | -5.5427 | -5.4496 | -8.0146 |
| 80.00 | -27.9562 | -4.3744 | -5.8512 | -5.7529 | -8.5204 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -27.9562 | -4.3744 | -5.8512 | -5.7529 | -8.5204 |
| 110.00 | -26.2789 | -4.1119 | -5.5427 | -5.4496 | -8.0146 |
| 120.00 | -24.8746 | -3.8922 | -5.4182 | -5.3272 | -7.6338 |
| 130.00 | -1604.2074 | -251.0147 | 12.5638 | 12.3529 | 61.5762 |
| 134.00 | -1.1659 | -1.1659 | -1.1659 | -1.1659 | -1.1659 |
| 140.00 | -23.3584 | -1.1659 | -1.1659 | -1.1659 | -1.1659 |
| 150.00 | -7.7929 | -1.2194 | -1.5716 | -1.5452 | -1.5179 |
| 160.00 | -4.5220 | -6763 | -.8536 | -.8536 | -2.2570 |
| 170.00 | -2.0860 | -3264 | -.3917 | -.3917 | -1.1924 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

| θ | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 1 | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 3 | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 3 |
|----------|---|---|---|---|---|
| 10.00 | 13.9951 | - .9288 | - .2841 | - .2467 | - .1031 |
| 20.00 | 54.9232 | - 1.7383 | - .5399 | - .3042 | - .1216 |
| 30.00 | - 26.7593 | - 1.7500 | - .5130 | - .4179 | - .1700 |
| 40.00 | - 4.3653 | - .9222 | - .0096 | - .0108 | - .1325 |
| 44.00 | - 2.7013 | - .6399 | - .3408 | - .4046 | - .1243 |
| 48.00 | - 2.4261 | - .4604 | - .7090 | - .4341 | - |
| 50.00 | - 2.6905 | - 2.1018 | - .23.4021 | - .3.6318 | - |
| 60.00 | 1.7971 | - 2.5701 | - .5.3365 | - .29.5397 | - .35.5383 |
| 70.00 | .2659 | 1.1427 | - 24.8630 | .48.2231 | .4.8923 |
| 80.00 | - 1.4766 | - 60.7686 | .15.4958 | .28.0732 | .2.6847 |
| 90.00 | - 2.1197 | 35.2.9567 | .6.0342 | .19.0607 | .1.9337 |
| 100.00 | - 3.2277 | 14.7483 | .3.3947 | .12.0528 | .1.4396 |
| 110.00 | - .0694 | - 7.007 | 1.7818 | .6.4337 | .1.9984 |
| 120.00 | - .7802 | - 2.1421 | .2235 | .1.7851 | .1.0928 |
| 130.00 | - .9484 | - 1.1781 | - .5163 | .2.8179 | -.8732 |
| 134.00 | - .9302 | - .9921 | - .0165 | - .0227 | - .2789 |
| 140.00 | 4.9031 | 1.5958 | - .7577 | - .9427 | - .3834 |
| 150.00 | 17.0217 | 2.5844 | - .9683 | - 1.0606 | - .4239 |
| 160.00 | - 42.5440 | 3.1178 | - .7575 | - .8249 | - .3449 |
| 170.00 | - 8.4866 | 2.4766 | 0 | 0 | 0 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

| θ | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 |
|----------|---|---|---|---|---|
| 10.00 | - 1.0281 | - 4.3330 | - .5308 | - .5788 | -.6389 |
| 20.00 | 3.4652 | 1.4840 | 1.4229 | 1.7641 | 2.4905 |
| 30.00 | .9393 | .4099 | .4502 | .7875 | .9254 |
| 40.00 | .4026 | .1740 | .1946 | .8245 | .9081 |
| 44.00 | .3558 | .1537 | .1701 | .1.0789 | .1.2315 |
| 50.00 | 5.8414 | 2.8190 | 1.7057 | 6.5132 | .6.8177 |
| 60.00 | - 1.0044 | -.5636 | -.6660 | -.5733 | -.4502 |
| 70.00 | - 1.5026 | -.9173 | - 1.0430 | -.4193 | -.3494 |
| 80.00 | - 3.3569 | - 2.1670 | - 2.4743 | -.6467 | -.5022 |
| 90.00 | 15.2517 | 10.0485 | 9.3603 | 2.0840 | .3.9039 |
| 100.00 | 2.3751 | 1.5332 | 1.6305 | .4261 | .4102 |
| 110.00 | 1.2891 | .7870 | .8549 | .3437 | .3134 |
| 120.00 | .8393 | .4709 | .5277 | .4543 | .3903 |
| 130.00 | .8328 | .4019 | .5233 | 1.9983 | .1.1237 |
| 134.00 | - 2.0667 | -.9140 | -.6914 | -.4.4213 | .9.1991 |
| 140.00 | -.4128 | -.1785 | -.1956 | -.8288 | -.9844 |
| 150.00 | -.6218 | -.2714 | -.3038 | -.5313 | -.6169 |
| 160.00 | -.7439 | -.3186 | -.3607 | -.4472 | -.5403 |
| 170.00 | -.5389 | -.2269 | -.2578 | -.2811 | -.3343 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

$\text{DR}(\hbar, \delta)$
 $T = 20$ Seconds $\lambda = 0^\circ$

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 | | $\frac{\partial J}{\partial \delta}$ Layer 1 to 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 | | $\frac{\partial J}{\partial \delta}$ Layer 2 to 3 | | $\frac{\partial J}{\partial h}$ Layer 3 to 4 | | $\frac{\partial J}{\partial \delta}$ Layer 3 to 4 | |
|----------|---|--|---|--|---|--|---|--|---|--|---|--|
| | $\frac{\partial J}{\partial h}$ for Source in Layer 1 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ for Source in Layer 1 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ for Source in Layer 2 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ for Source in Layer 3 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ for Source in Layer 4 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ for Source in Layer 5 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 |
| 10.00 | 2733.2571 | 10.4671 | 399.4511 | 1.0754 | - | - | - | - | - | - | - | .8882 |
| 20.00 | 18385.0593 | 36.5017 | 1392.9949 | 1.1000 | - | - | - | - | - | - | - | .9085 |
| 30.00 | -6065.7369 | 78.5989 | 2999.5249 | 1.1242 | - | - | - | - | - | - | - | .9285 |
| 40.00 | -351.9419 | 444.0968 | 16947.8129 | 1.1504 | - | - | - | - | - | - | - | .9502 |
| 44.00 | -12.9458 | -6.7414 | -257.2682 | 1.2512 | - | - | - | - | - | - | - | .0334 |
| 50.00 | -246.8953 | -395.1418 | -15079.5700 | 1.1734 | - | - | - | - | - | - | - | .9691 |
| 60.00 | -1627.4623 | 315.4869 | 12039.7443 | 1.1847 | - | - | - | - | - | - | - | .9785 |
| 70.00 | -5299.4888 | 318.8119 | 12166.6357 | 1.1968 | - | - | - | - | - | - | - | .9885 |
| 80.00 | -4567.5540 | 336.4264 | 12838.8478 | 1.2045 | - | - | - | - | - | - | - | .9948 |
| 90.00 | 0 | 0 | 0 | 0 | - | - | - | - | - | - | - | 0 |
| 100.00 | 4567.5537 | 336.4264 | 12838.8478 | 1.2045 | - | - | - | - | - | - | - | .9948 |
| 110.00 | -3299.4888 | 318.8119 | 12166.6358 | 1.1968 | - | - | - | - | - | - | - | .9885 |
| 120.00 | -1627.4623 | 315.4869 | 12039.7445 | 1.1847 | - | - | - | - | - | - | - | .9785 |
| 130.00 | -246.8953 | -395.1418 | -15079.5693 | 1.1734 | - | - | - | - | - | - | - | .9691 |
| 134.00 | -12.9458 | -6.2776 | -239.5702 | 1.2658 | - | - | - | - | - | - | - | .0455 |
| 140.00 | -351.9419 | 444.0968 | 16947.8123 | 1.1504 | - | - | - | - | - | - | - | .9502 |
| 150.00 | -6065.7369 | 78.5989 | 2999.5249 | 1.1242 | - | - | - | - | - | - | - | .9285 |
| 160.00 | 18385.0655 | 36.5017 | 1392.9949 | 1.1000 | - | - | - | - | - | - | - | .9085 |
| 170.00 | 2733.2571 | 10.4671 | 399.4511 | 1.0754 | - | - | - | - | - | - | - | .8882 |
| 180.00 | 0 | 0 | 0 | 0 | - | - | - | - | - | - | - | 0 |
| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 | | $\frac{\partial J}{\partial \delta}$ Layer 4 to 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 | | $\frac{\partial J}{\partial \delta}$ Layer 5 to 6 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 | | $\frac{\partial J}{\partial \delta}$ Layer 5 to 6 | |
| | $\frac{\partial J}{\partial h}$ for Source in Layer 4 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ for Source in Layer 4 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ for Source in Layer 5 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ for Source in Layer 5 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 | $\frac{\partial J}{\partial h}$ for Source in Layer 6 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 | $\frac{\partial J}{\partial h}$ for Source in Layer 6 | $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 |
| 10.00 | -30.4772 | - | -5336 | - | - | - | - | - | - | - | - | - |
| 20.00 | -49.9811 | - | .8751 | - | - | - | - | - | - | - | - | - |
| 30.00 | -78.1996 | - | -1.3692 | - | -2.7013 | - | - | - | - | - | - | - |
| 40.00 | -142.7543 | - | -2.4995 | - | -6.0463 | - | - | - | - | - | - | - |
| 44.00 | -29.3076 | - | .5131 | - | -6.381 | - | - | - | - | - | - | - |
| 50.00 | -26.1585 | - | -4.5551 | - | -16.7154 | - | - | - | - | - | - | - |
| 60.00 | -194.9684 | - | -3.4137 | - | -7.6240 | - | - | - | - | - | - | - |
| 70.00 | -215.4981 | - | -3.7731 | - | -8.2890 | - | - | - | - | - | - | - |
| 80.00 | -231.2344 | - | -4.0487 | - | -8.8720 | - | - | - | - | - | - | - |
| 90.00 | 0 | - | 0 | - | 0 | - | - | - | - | - | - | - |
| 100.00 | -231.2344 | - | -4.0487 | - | -8.8720 | - | - | - | - | - | - | - |
| 110.00 | -215.4981 | - | -3.7731 | - | -8.2890 | - | - | - | - | - | - | - |
| 120.00 | -194.9684 | - | -3.4137 | - | -7.6240 | - | - | - | - | - | - | - |
| 130.00 | -260.1585 | - | -4.5551 | - | -16.7154 | - | - | - | - | - | - | - |
| 134.00 | -26.8403 | - | -4.699 | - | .5919 | - | - | - | - | - | - | - |
| 140.00 | -142.7543 | - | -2.4995 | - | -6.0463 | - | - | - | - | - | - | - |
| 150.00 | -78.1996 | - | -1.3692 | - | -7.6240 | - | - | - | - | - | - | - |
| 160.00 | -49.9811 | - | -8.7751 | - | -8.2890 | - | - | - | - | - | - | - |
| 170.00 | -30.4772 | - | -5.3336 | - | -8.8720 | - | - | - | - | - | - | - |
| 180.00 | 0 | - | 0 | - | - | - | - | - | - | - | - | - |

| | | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1 | | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | |
|--------|-----------|---|--|---|--|---|--|---|--|---|--|
| θ | | | | | | | | | | | |
| 10.00 | 9.38882 | -3.4044 | | -3.4044 | | .1277 | | .2036 | | 1.3369 | |
| 20.00 | 34.5391 | -3.8550 | | -3.8550 | | .2114 | | .0731 | | .3442 | |
| 30.00 | -21.1372 | -2.8247 | | -2.8247 | | .1219 | | .0564 | | .2879 | |
| 40.00 | -5.4828 | -1.2068 | | -1.2068 | | .4071 | | -.3092 | | .2020 | |
| 44.00 | -2.2716 | -.8832 | | -.8832 | | .8632 | | -.7353 | | .1937 | |
| 50.00 | 2.3294 | 1.7906 | | 1.7906 | | .0832 | | -.1996 | | .8231 | |
| 60.00 | 1.9153 | 1.8631 | | 1.8631 | | -1.2593 | | -.9.5150 | | -2.5572 | |
| 70.00 | .8158 | 1.4159 | | 1.4159 | | -2.4816 | | -.39.9150 | | -6.7848 | |
| 80.00 | -.9960 | -.57.7816 | | -.57.7816 | | -4.6253 | | 163.5769 | | 20.4946 | |
| 90.00 | -2.0240 | -.891.3881 | | -.891.3881 | | -.57.7599 | | 46.8524 | | 5.2138 | |
| 100.00 | .2359 | 5.2848 | | 5.2848 | | 4.2278 | | 24.6768 | | 3.0918 | |
| 110.00 | -.2066 | -1.1090 | | -1.1090 | | 1.9437 | | 12.0225 | | 2.0436 | |
| 120.00 | -.8204 | -1.4698 | | -1.4698 | | .9934 | | 4.8556 | | 1.3050 | |
| 130.00 | -.8513 | -.8843 | | -.8843 | | -.0411 | | -.3055 | | 1.2602 | |
| 134.00 | -.8472 | -.8051 | | -.8051 | | -.7492 | | 5.2207 | | -1.4052 | |
| 140.00 | 3.6793 | 1.6249 | | 1.6249 | | .5481 | | .5542 | | -.3622 | |
| 150.00 | 13.4610 | 2.8570 | | 2.8570 | | -.1233 | | -.0929 | | -.4744 | |
| 160.00 | -25.0354 | 4.0598 | | 4.0598 | | -.2226 | | -.1189 | | -.5113 | |
| 170.00 | -5.4227 | 3.3390 | | 3.3390 | | -.1253 | | -.0614 | | -.4032 | |
| 180.00 | 0 | 0 | | 0 | | 0 | | 0 | | 0 | |
| | | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 | |
| θ | | | | | | | | | | | |
| 10.00 | -2.1640 | -1.2797 | | -1.2797 | | -1.5264 | | -1.3017 | | -1.2467 | |
| 20.00 | 1.3155 | .8073 | | .8073 | | 1.1514 | | 1.0356 | | 1.8141 | |
| 30.00 | .7317 | .4955 | | .4955 | | .6617 | | .6894 | | .9626 | |
| 40.00 | .3975 | .3717 | | .3717 | | .4765 | | .7110 | | .8984 | |
| 44.00 | .3635 | .4123 | | .4123 | | .5273 | | .9016 | | 1.1716 | |
| 50.00 | 1.7582 | 1.6288 | | 1.6288 | | 2.4040 | | 3.4504 | | -20.8513 | |
| 60.00 | -2.1213 | -1.3526 | | -1.3526 | | -1.4146 | | -1.0692 | | -.8084 | |
| 70.00 | -.3.6055 | -2.1577 | | -2.1577 | | -2.1747 | | -1.2207 | | -.9527 | |
| 80.00 | -.13.0675 | -7.7320 | | -7.7320 | | -6.6410 | | -3.2600 | | -2.0422 | |
| 90.00 | 10.4930 | 6.1983 | | 6.1983 | | 7.7643 | | 3.6528 | | 5.9191 | |
| 100.00 | 3.8766 | 2.2938 | | 2.2938 | | 2.5254 | | 1.2397 | | 1.2545 | |
| 110.00 | 2.2832 | 1.3664 | | 1.3664 | | 1.4747 | | .8278 | | .7778 | |
| 120.00 | 1.4807 | .9442 | | .9442 | | 1.0204 | | .7712 | | .6814 | |
| 130.00 | 1.7826 | 1.6515 | | 1.6515 | | 1.6850 | | 2.4184 | | 1.3875 | |
| 134.00 | -1.5332 | -1.7585 | | -1.7585 | | -2.4008 | | -4.1159 | | 14.4884 | |
| 140.00 | -.5020 | -.4694 | | -.4694 | | -.5730 | | -.8551 | | -.0798 | |
| 150.00 | -.7046 | -.4772 | | -.4772 | | -.5928 | | -.6176 | | -.7701 | |
| 160.00 | -.7931 | -.4867 | | -.4867 | | -.6186 | | -.5564 | | -.7223 | |
| 170.00 | -.5990 | -.3542 | | -.3542 | | -.4457 | | -.3801 | | -.4820 | |
| 180.00 | 0 | 0 | | 0 | | 0 | | 0 | | 0 | |

DR(h,δ)

T = 30 Seconds λ = 0°

| <u>$\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3</u> | |
|--|------------|--|-------------|--|------------|--|--|--|--|
| 9 | | | | | | | | | |
| 10.00 | 1737.6040 | 27.4973 | 49.7058 | 1.4441 | 7.4478 | | | | |
| 20.00 | 10099.8645 | 105.2587 | 190.2221 | 3.5020 | 18.0606 | | | | |
| 30.00 | -5295.5271 | 251.8420 | 455.2453 | 6.7455 | 34.7882 | | | | |
| 40.00 | -285.1913 | -211.1868 | -381.7543 | 21.6674 | 111.7445 | | | | |
| 44.00 | -10.1385 | -4.9538 | -8.9549 | - | -4.9397 | | | | |
| 50.00 | -199.6986 | -115.2148 | -208.2694 | -381.5060 | -1967.5298 | | | | |
| 60.00 | -1325.4683 | -7665.7989 | -13857.1734 | 22.9177 | 118.1928 | | | | |
| 70.00 | -2700.4580 | 2176.2153 | 3933.8978 | 24.2122 | 124.8687 | | | | |
| 80.00 | -3749.5689 | 1763.6521 | 3188.0868 | 25.7891 | 133.0014 | | | | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | | | | |
| 100.00 | -3749.5689 | 1763.6523 | 3188.0873 | 25.7891 | 133.0014 | | | | |
| 110.00 | -2700.4578 | 2176.2350 | 3933.8974 | 24.2122 | 124.8687 | | | | |
| 120.00 | -1325.4682 | -7665.8017 | -13857.1785 | 22.9177 | 118.1928 | | | | |
| 130.00 | -199.6986 | -115.2148 | -208.2694 | -381.5059 | -1967.5291 | | | | |
| 134.00 | -9.4804 | -4.6305 | -8.3703 | - | -4.6136 | | | | |
| 140.00 | -285.1913 | -211.1868 | -381.7543 | -21.6674 | 111.7445 | | | | |
| 150.00 | -5295.5264 | 251.8420 | 455.2453 | 6.7455 | 34.7832 | | | | |
| 160.00 | 10099.8717 | 105.2587 | 190.2721 | 3.5020 | 18.0606 | | | | |
| 170.00 | 1737.6041 | 27.4973 | 49.7058 | 1.4441 | 7.4478 | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | | | | |
| <u>$\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5</u> | | <u>$\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6</u> | |
| 6 | | | | | | | | | |
| 10.00 | . | .8029 | .0958 | .0864 | .9799 | - 4.1725 | | | |
| 20.00 | . | .9528 | .1157 | .0987 | -1.1202 | - 6.4584 | | | |
| 30.00 | 1.1314 | *1.1350 | *1.1350 | *1.129 | -1.2810 | - 9.6573 | | | |
| 40.00 | 1.3688 | *1.634 | *1.634 | *1.307 | -1.4831 | -14.7675 | | | |
| 44.00 | 7.1450 | *8529 | *8529 | *2976 | -3.3768 | 10.2330 | | | |
| 50.00 | 1.6170 | *1.930 | *1.930 | *1.487 | -1.6867 | -21.2219 | | | |
| 60.00 | 1.7142 | *2046 | *2046 | *1570 | -1.7814 | -21.8498 | | | |
| 70.00 | 1.8483 | *2206 | *2206 | *1671 | -1.8959 | -24.6066 | | | |
| 80.00 | 1.9379 | *2313 | *2313 | *1738 | -1.9715 | -26.5057 | | | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| 100.00 | 1.9379 | *2313 | *2313 | *1671 | -1.8959 | -24.6066 | | | |
| 110.00 | 1.8483 | *2206 | *2206 | *1570 | -1.7814 | -21.8498 | | | |
| 120.00 | 1.7142 | *2046 | *2046 | *1487 | -1.6867 | -21.2219 | | | |
| 130.00 | 1.6170 | *1930 | *1930 | *1307 | -1.4831 | -14.7675 | | | |
| 134.00 | 13.7224 | 1.6380 | 1.6380 | *3520 | -3.9958 | 8.8673 | | | |
| 140.00 | 1.3688 | *1634 | *1634 | *1129 | -1.2810 | - 9.6573 | | | |
| 150.00 | 1.1314 | *1350 | *1350 | *987 | -1.1202 | - 6.4584 | | | |
| 160.00 | 0 | *9528 | *9528 | *864 | *9799 | - 4.1725 | | | |
| 170.00 | 0 | *8029 | *8029 | 0 | 0 | 0 | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | 0 | | | |

UU DR(h, δ)

T = 30 Seconds $\lambda = 45^\circ$

| θ | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 1 | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 3 | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 3 |
|----------|---|---|---|---|---|
| 10.00 | 4.1595 | 8.4845 | 5.7059 | - | .0685 |
| 20.00 | 13.7818 | -20.5255 | -13.4317 | - | .2738 |
| 30.00 | -11.9140 | -4.0925 | -2.8244 | - | .0399 |
| 40.00 | -1.8699 | -1.1749 | -1.5812 | - | .0687 |
| 44.00 | -1.2899 | - | 2.0141 | - | .0478 |
| 50.00 | 1.2665 | 1.0520 | .8923 | - | .0391 |
| 60.00 | 1.2858 | 1.0846 | - | 2.9257 | .6901 |
| 70.00 | .9330 | .9309 | - | 1.6836 | -1.5871 |
| 80.00 | -2.565 | - | 1.0118 | - | -17.5069 |
| 90.00 | -1.8302 | -29.3124 | -1.5697 | - | -102.5145 |
| 100.00 | - | -0.0626 | -2.8078 | - | 42.9505 |
| 110.00 | - | -2211 | - | 1.5253 | 17.0327 |
| 120.00 | - | - | - | - | 2.7192 |
| 130.00 | - | - | - | 5.1111 | 1.6533 |
| 134.00 | - | - | - | - | .9317 |
| 140.00 | - | - | - | - | .8782 |
| 150.00 | - | - | - | - | .3780 |
| 160.00 | - | - | - | - | 23.5145 |
| 170.00 | - | - | - | - | - |
| 180.00 | - | - | - | - | - |
| | | | 0 | 0 | 0 |
| θ | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 |
| 10.00 | .0302 | .1519 | .6018 | .6538 | .1832 |
| 20.00 | .0343 | .1282 | .2636 | .2856 | .6284 |
| 30.00 | .0608 | .1841 | .2852 | .3176 | *.5317 |
| 40.00 | .0462 | .2130 | .2927 | .3787 | .5410 |
| 44.00 | .0380 | .2593 | .3529 | .4909 | .7012 |
| 50.00 | .4047 | .8147 | .4088 | .7037 | 14.5590 |
| 60.00 | -3.8618 | -3.0439 | -2.0989 | - | -1.7711 |
| 70.00 | -22.6394 | -13.5988 | -5.3477 | -3.8940 | -1.1649 |
| 80.00 | 13.0839 | 6.8948 | 20.7287 | 14.0845 | -2.1221 |
| 90.00 | 6.6365 | 3.3538 | 4.5566 | 3.0285 | -11.0757 |
| 100.00 | 4.2840 | 2.2575 | 2.6281 | 4.3780 | - |
| 110.00 | 2.6160 | 1.5714 | 1.7103 | 1.7857 | 1.9296 |
| 120.00 | 1.3662 | 1.0769 | 1.1307 | 1.2454 | 1.2251 |
| 130.00 | .7620 | 1.5341 | 1.3888 | .9540 | .8879 |
| 134.00 | - | -4.161 | -2.1927 | 1.6794 | 1.1900 |
| 140.00 | - | .0948 | -4.2205 | -5.8312 | 7.1752 |
| 150.00 | - | -1.284 | - | .6861 | - |
| 160.00 | - | - | - | .5257 | -6653 |
| 170.00 | - | - | - | .4906 | -6390 |
| 180.00 | - | .0559 | - | .3661 | -4648 |
| | | | 0 | 0 | 0 |

DR(h, δ) $T = 40$ Seconds $\lambda = 0^\circ$
 $\frac{\partial J}{\partial h}$ Layer 1 to 2
 $\frac{\partial J}{\partial \delta}$ for Source in
Layer 1
 θ

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 1 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 |
|---|---|---|---|---|---|
| 10.00 | 1716.7772 | 45.7247 | 62.0835 | 2.3983 | 5.0076 |
| 20.00 | 9784.7640 | 178.9135 | 242.9230 | 7.7860 | 16.2570 |
| 30.00 | -5536.8907 | 473.5531 | 642.9752 | 16.9845 | 35.4630 |
| 40.00 | -293.6014 | -165.0005 | -224.0324 | -62.6176 | -130.7435 |
| 44.00 | -10.2829 | -4.7293 | -6.4213 | -7.7996 | -1.6694 |
| 50.00 | -205.4875 | -102.4471 | -139.0994 | -19.9476 | -41.6500 |
| 60.00 | -1366.2445 | -1262.7014 | -1714.4554 | 107.0624 | 223.5429 |
| 70.00 | -2786.3273 | -11470.1806 | -15573.8428 | 82.1997 | 171.6303 |
| 80.00 | -3871.1413 | 13670.9366 | 18561.9586 | 82.0518 | 171.3214 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -3871.1403 | 13670.9365 | 18561.9585 | 82.0518 | 171.3214 |
| 110.00 | -2786.3263 | -11470.1909 | -15573.8568 | 82.1997 | 171.6303 |
| 120.00 | -1366.2443 | -1262.7013 | -1714.4552 | 107.0624 | 223.5429 |
| 130.00 | -205.4875 | -102.4471 | -139.0994 | -19.9476 | -41.6500 |
| 134.00 | -9.6060 | -4.4196 | -6.0008 | -7.514 | -1.5688 |
| 140.00 | -293.6014 | -165.0005 | -224.0324 | -62.6176 | -130.7435 |
| 150.00 | -5536.8907 | 473.5531 | 642.9752 | 16.9845 | 35.4630 |
| 160.00 | 9784.7640 | 178.9135 | 242.9230 | 7.7860 | 16.2570 |
| 170.00 | 1716.7774 | 45.7247 | 62.0835 | 2.3983 | 5.0076 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

 $\frac{\partial J}{\partial h}$ Layer 3 to 4
 $\frac{\partial J}{\partial \delta}$ for Source in
Layer 4
 θ

| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \delta}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 4 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \delta}$ for Source in Layer 6 |
|---|---|---|---|
| 10.00 | .9021 | 3.6106 | .8496 |
| 20.00 | 1.9072 | 7.6335 | 1.1034 |
| 30.00 | 3.4400 | 13.7685 | 1.4275 |
| 40.00 | 7.2840 | 29.1539 | 1.8655 |
| 44.00 | -.9177 | -3.6729 | -70.6474 |
| 50.00 | 16.3731 | 65.5330 | 2.3460 |
| 60.00 | 10.0901 | 40.3855 | 2.5599 |
| 70.00 | 11.1768 | 44.7351 | 2.8312 |
| 80.00 | 12.0406 | 48.1924 | 3.0125 |
| 90.00 | 0 | 0 | 0 |
| 100.00 | 12.0406 | 48.1924 | 3.0125 |
| 110.00 | 11.1768 | 44.7351 | 2.8312 |
| 120.00 | 10.0901 | 40.3855 | 2.5599 |
| 130.00 | 16.3731 | 65.5330 | 2.3460 |
| 134.00 | -.8477 | -3.3928 | -13.1901 |
| 140.00 | 7.2840 | 29.1539 | 1.8655 |
| 150.00 | 3.4400 | 13.7685 | 1.4275 |
| 160.00 | 1.9072 | 7.6335 | 1.1034 |
| 170.00 | .9021 | 3.6106 | .8496 |
| 180.00 | 0 | 0 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \delta}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \delta}$ for Source in Layer 3 |
|---|---|---|---|---|
| 10.00 | 1716.7772 | 45.7247 | 62.0835 | 2.3983 |
| 20.00 | 9784.7640 | 178.9135 | 242.9230 | 7.7860 |
| 30.00 | -5536.8907 | 473.5531 | 642.9752 | 16.9845 |
| 40.00 | -293.6014 | -165.0005 | -224.0324 | -62.6176 |
| 44.00 | -10.2829 | -4.7293 | -6.4213 | -7.7996 |
| 50.00 | -205.4875 | -102.4471 | -139.0994 | -19.9476 |
| 60.00 | -1366.2445 | -1262.7014 | -1714.4554 | 107.0624 |
| 70.00 | -2786.3273 | -11470.1806 | -15573.8428 | 82.1997 |
| 80.00 | -3871.1413 | 13670.9366 | 18561.9586 | 82.0518 |
| 90.00 | 0 | 0 | 0 | 0 |
| 100.00 | -3871.1403 | 13670.9365 | 18561.9585 | 82.0518 |
| 110.00 | -2786.3263 | -11470.1909 | -15573.8568 | 82.1997 |
| 120.00 | -1366.2443 | -1262.7013 | -1714.4552 | 107.0624 |
| 130.00 | -205.4875 | -102.4471 | -139.0994 | -19.9476 |
| 134.00 | -9.6060 | -4.4196 | -6.0008 | -7.514 |
| 140.00 | -293.6014 | -165.0005 | -224.0324 | -62.6176 |
| 150.00 | -5536.8907 | 473.5531 | 642.9752 | 16.9845 |
| 160.00 | 9784.7640 | 178.9135 | 242.9230 | 7.7860 |
| 170.00 | 1716.7774 | 45.7247 | 62.0835 | 2.3983 |
| 180.00 | 0 | 0 | 0 | 0 |

DR(h, δ) $T = 40$ Seconds $\lambda = 45^\circ$

| θ | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 1 | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \delta$ for Source in Layer 2 | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \delta$ for Source in Layer 3 | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 |
|----------|---|---|---|---|---|---|
| 10.00 | 2.6122 | 3.1439 | 2.9614 | - | .5792 | - .3472 |
| 20.00 | 8.2886 | 25.7988 | 24.1096 | - | .8342 | - .4455 |
| 30.00 | -8.3177 | - 4.0892 | - 4.1818 | - | .8317 | - .3459 |
| 40.00 | -1.2442 | - .9397 | - 1.6993 | - | .9091 | - .2208 |
| 44.00 | - .8780 | - .7478 | - 2.0003 | - | 1.4552 | - .2508 |
| 50.00 | - .8194 | - .7317 | .9840 | 3.5321 | - .3850 | - |
| 60.00 | .9150 | .7877 | .0649 | 1.2228 | - .3026 | - |
| 70.00 | .7706 | .7157 | - | .5125 | - 1.8726 | - 1.0160 |
| 80.00 | .0395 | .0472 | - 1.0748 | - 1.6131 | 100.9842 | - 3.0937 |
| 90.00 | -1.7232 | -14.6484 | - | .7360 | 8.6653 | 10.5388 |
| 100.00 | - .0096 | - .0323 | - | .1961 | 1.3595 | 1.7948 |
| 110.00 | - .1757 | - .2739 | - | .0318 | - .0956 | - .3776 |
| 120.00 | - .3756 | - .3864 | - | .4130 | - .8964 | - .2356 |
| 130.00 | - .3343 | - .3071 | - | .9149 | - 3.2319 | - .0977 |
| 134.00 | - .3728 | - .3494 | - | 1.6832 | 1.3268 | - 4.9669 |
| 140.00 | 1.0683 | .909 | - | 2.8386 | 1.9626 | - .3222 |
| 150.00 | 5.2464 | 2.7758 | - | -32.9440 | 1.0650 | - 4.004 |
| 160.00 | -5.3834 | -34.8188 | - | 1.8386 | .5688 | - |
| 170.00 | -1.3345 | -2.5001 | - | -2.3550 | .4925 | - |
| 180.00 | 0 | 0 | 0 | 0 | 0 | 0 |
| θ | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \delta$ for Source in Layer 4 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 5 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \delta$ for Source in Layer 6 |
| 10.00 | - .0197 | .0005 | .0020 | .0656 | .3545 | - |
| 20.00 | - .1121 | .0147 | .0123 | .0963 | .1955 | - |
| 30.00 | - .1368 | .0487 | .0434 | .1614 | .2366 | - |
| 40.00 | - .1210 | .0913 | .0874 | .2238 | .2889 | - |
| 44.00 | - .1410 | .1303 | .1274 | .3061 | .3927 | - |
| 50.00 | - .3661 | .9193 | .8472 | 1.5733 | 9.6561 | - |
| 60.00 | - .7949 | -1.0977 | -1.4123 | -1.6596 | -1.2495 | - |
| 70.00 | -6.3518 | -4.5519 | -7.9975 | -7.4573 | -3.6682 | - |
| 80.00 | 15.2153 | 8.1458 | 7.6972 | 6.3591 | 22.0710 | - |
| 90.00 | 6.1899 | 3.0140 | 3.6346 | 2.8887 | 3.8787 | - |
| 100.00 | 3.4189 | 1.8304 | 2.3073 | 1.9062 | 2.1872 | - |
| 110.00 | 1.5475 | 1.1090 | 1.3846 | 1.2911 | 1.3788 | - |
| 120.00 | -4.4322 | .5968 | .7148 | .8400 | .8562 | - |
| 130.00 | - .1708 | .4290 | .4822 | .8955 | .7914 | - |
| 134.00 | -3.3147 | 3.5998 | 4.3072 | 9.8033 | 2.6910 | - |
| 140.00 | - .2475 | - .1867 | - .1921 | - .4916 | - .5739 | - |
| 150.00 | - .2758 | - .0981 | - .0969 | - .3605 | - .4174 | - |
| 160.00 | .3335 | - .0437 | - .0415 | - .3244 | - .3762 | - |
| 170.00 | .2839 | - .0078 | - .0073 | - .2395 | - .2718 | - |
| 180.00 | 0 | 0 | 0 | 0 | 0 | 0 |

TABLE V

 $\partial R(h, \lambda)$ $T = 12 \text{ Seconds}$ $\delta = 90^\circ$

| | | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \lambda$ for Source in Layer 1 | | $\partial J/\partial h$ Layer 1 to 2 $\partial J/\partial \lambda$ for Source in Layer 2 | | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \lambda$ for Source in Layer 2 | | $\partial J/\partial h$ Layer 2 to 3 $\partial J/\partial \lambda$ for Source in Layer 3 | | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \lambda$ for Source in Layer 3 | | | |
|--------|------------|--|----------|--|---------|--|--|--|--|--|--|--|--|
| 9 | | | | | | | | | | | | | |
| 10.00 | 1.2775 | 9.9627 | -12.6025 | 4.7290 | 14.5351 | 2.0889 | | | | | | | |
| 20.00 | 9.935 | 1.1501 | -12.3178 | 4.6221 | 14.4292 | 2.0737 | | | | | | | |
| 30.00 | 4.74 | .7773 | -11.9447 | 4.4822 | 15.0362 | 2.1609 | | | | | | | |
| 40.00 | 86.2402 | -12.6551 | -12.6551 | 4.7487 | 55.1954 | 7.9324 | | | | | | | |
| 41.00 | 9.8354 | 41.4490 | -11.0949 | -15.5534 | -2.6023 | -3740 | | | | | | | |
| 50.00 | 1.16 | .6688 | -11.0949 | 4.1635 | 19.3920 | 2.7870 | | | | | | | |
| 60.00 | 1501.8526 | -9.5157 | -9.5157 | 3.5707 | 9.3594 | 1.3451 | | | | | | | |
| 70.00 | 6380.5 | .575 | -8.7202 | 3.2722 | 8.0929 | 1.1631 | | | | | | | |
| 80.00 | -2104.7251 | 0 | -8.0097 | 5.0056 | 7.1809 | 1.0320 | | | | | | | |
| 90.00 | 100.00 | -2104.7246 | -8.0097 | 0 | 0 | 0 | | | | | | | |
| 100.00 | 6380.4 | .0735 | -8.7202 | 3.0050 | 7.1809 | 1.0320 | | | | | | | |
| 110.00 | 110.00 | 1501.8528 | -9.5157 | 3.2722 | 8.0929 | 1.1631 | | | | | | | |
| 120.00 | 130.00 | 116.6688 | -11.0949 | 5.5707 | 9.3594 | 1.3451 | | | | | | | |
| 130.00 | 154.00 | 10.2562 | 70.3324 | 4.1633 | 19.3929 | 2.7870 | | | | | | | |
| 140.00 | 140.00 | 86.2402 | -12.6551 | -26.3916 | -2.8505 | -4097 | | | | | | | |
| 150.00 | 150.00 | 474.7773 | -11.9447 | 4.7487 | 55.1954 | 7.9324 | | | | | | | |
| 160.00 | 160.00 | 933.1501 | -12.3178 | 4.4822 | 15.0362 | 2.1609 | | | | | | | |
| 170.00 | 170.00 | 1275.9627 | -12.6025 | 4.6221 | 14.4292 | 2.0737 | | | | | | | |
| 180.00 | 180.00 | 0 | 0 | 4.7290 | 14.5351 | 2.0889 | | | | | | | |
| | | $\partial J/\partial h$ Layer 3 to 4 $\partial J/\partial \lambda$ for Source in Layer 4 | | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \lambda$ for Source in Layer 4 | | $\partial J/\partial h$ Layer 4 to 5 $\partial J/\partial \lambda$ for Source in Layer 5 | | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \lambda$ for Source in Layer 5 | | $\partial J/\partial h$ Layer 5 to 6 $\partial J/\partial \lambda$ for Source in Layer 6 | | | |
| 9 | | | | | | | | | | | | | |
| 10.00 | 3.6575 | -1.1340 | -1.1420 | -1.1420 | .0908 | .0904 | | | | | | | |
| 20.00 | 3.6759 | -1.1346 | -1.1454 | -1.1454 | .0929 | .0902 | | | | | | | |
| 30.00 | 4.1075 | -.1505 | -.1756 | -.1756 | .0988 | .0988 | | | | | | | |
| 40.00 | -8.6560 | .3171 | .1553 | .1553 | -.0993 | -.2586 | | | | | | | |
| 44.00 | -.3361 | .0123 | .0102 | .0102 | -.0065 | -.0083 | | | | | | | |
| 50.00 | 9.1398 | -.3348 | -.4244 | -.4244 | .9107 | .1933 | | | | | | | |
| 60.00 | 1.9854 | -.0727 | -.0736 | -.0736 | .0470 | .0478 | | | | | | | |
| 70.00 | 1.6205 | -.0594 | -.0591 | -.0591 | .0378 | .0387 | | | | | | | |
| 80.00 | 1.3802 | -.0506 | -.0502 | -.0502 | .0321 | .0326 | | | | | | | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| 100.00 | 1.3802 | -.0506 | -.0502 | -.0502 | .0321 | .0326 | | | | | | | |
| 110.00 | 1.6205 | -.0594 | -.0591 | -.0591 | .0378 | .0387 | | | | | | | |
| 120.00 | 1.9854 | -.0727 | -.0756 | -.0756 | .0470 | .0478 | | | | | | | |
| 130.00 | 9.1398 | -.3348 | -.4244 | -.4244 | .9107 | .1933 | | | | | | | |
| 134.00 | -.3638 | .0135 | .0110 | .0110 | -.0071 | -.0090 | | | | | | | |
| 140.00 | 8.6560 | .3171 | .1553 | .1553 | -.0993 | -.2586 | | | | | | | |
| 150.00 | 4.1075 | -.1505 | -.1756 | -.1756 | .0929 | .0988 | | | | | | | |
| 160.00 | 3.6759 | -.1346 | -.1454 | -.1454 | .0902 | .0904 | | | | | | | |
| 170.00 | 3.6575 | -.1340 | -.1420 | -.1420 | 0 | 0 | | | | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |

$\Delta R(h, \lambda)$

T = 16 Seconds $\delta = 90^\circ$

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 1 | | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 | | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 3 | | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 3 | |
|--|------------|--|----------|--|----------|--|--|--|--|
| 10.00 | 803.0896 | -25.7187 | -12.0779 | -2.6746 | 3.3010 | | | | |
| 20.00 | 584.1114 | -24.5101 | -11.5103 | -2.6570 | 3.2792 | | | | |
| 30.00 | 293.4180 | -23.2374 | -10.9127 | -2.6891 | 3.3188 | | | | |
| 40.00 | 50.3484 | -38.1060 | -17.8952 | -3.7866 | 4.6733 | | | | |
| 44.00 | 5.0967 | 4.1152 | 1.9326 | 1.5549 | -1.9190 | | | | |
| 50.00 | 69.1533 | -20.8523 | -9.7926 | -2.9064 | 3.5870 | | | | |
| 60.00 | 1006.5306 | -12.0619 | -5.645 | -2.1287 | 2.6272 | | | | |
| 70.00 | -6635.2122 | -9.3072 | -4.3708 | -1.9716 | 2.4332 | | | | |
| 80.00 | -704.8194 | -7.2374 | -3.3988 | -1.8481 | 2.2808 | | | | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | | | | |
| 100.00 | -704.8193 | -7.2374 | -3.3988 | -1.8481 | 2.2808 | | | | |
| 110.00 | -6635.2040 | -9.3072 | -4.3708 | -1.9716 | 2.4332 | | | | |
| 120.00 | 1006.5307 | -12.0619 | -5.645 | -2.1287 | 2.6272 | | | | |
| 130.00 | 69.1533 | -20.8523 | -9.7926 | -2.9064 | 3.5870 | | | | |
| 134.00 | 5.3241 | 4.5109 | 1.9184 | 1.7740 | -2.1895 | | | | |
| 140.00 | 50.3484 | -38.1060 | -17.8952 | -3.7866 | 4.6733 | | | | |
| 150.00 | 293.4180 | -23.2374 | -10.9127 | -2.6891 | 3.3188 | | | | |
| 160.00 | 584.1114 | -24.5101 | -11.5103 | -2.6570 | 3.2792 | | | | |
| 170.00 | 803.0896 | -25.7187 | -12.0779 | -2.6746 | 3.3010 | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | | | | |
| | | | | | | | | | |
| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 | | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 | |
| 10.00 | 10.7571 | 1.6832 | 2.1276 | 2.0919 | 2.6662 | | | | |
| 20.00 | 10.7720 | 1.6855 | 2.1474 | 2.1114 | 2.6527 | | | | |
| 30.00 | 11.6085 | 1.8164 | 2.3962 | 2.3559 | 2.8385 | | | | |
| 40.00 | 1075.9354 | 168.5542 | -8.1241 | -7.9877 | -32.1829 | | | | |
| 44.00 | -1.4982 | - | -23356 | -2317 | - | 3102 | | | |
| 50.00 | 17.9164 | 2.8034 | 4.7419 | 4.6623 | 4.4693 | | | | |
| 60.00 | 6.6983 | 1.0481 | 1.2617 | 1.2405 | 1.2615 | | | | |
| 70.00 | 5.7170 | .8946 | 1.0586 | 1.0408 | 1.0833 | | | | |
| 80.00 | 5.0497 | .7901 | .9266 | .9110 | 0 | | | | |
| 90.00 | 0 | 0 | 0 | 0 | 0 | | | | |
| 100.00 | 5.0497 | .7901 | .9266 | .9110 | 1.0833 | | | | |
| 110.00 | 5.7170 | .8946 | 1.0586 | 1.0408 | 1.2615 | | | | |
| 120.00 | 6.6983 | 1.0481 | 1.2617 | 1.2405 | 1.5191 | | | | |
| 130.00 | 17.9164 | 2.8034 | 4.7419 | 4.6623 | 4.4693 | | | | |
| 134.00 | -1.6328 | .2555 | -2558 | -2515 | -3370 | | | | |
| 140.00 | 1075.9324 | 168.3541 | -8.1241 | -7.9877 | -32.1829 | | | | |
| 150.00 | 11.6085 | 1.8164 | 2.3962 | 2.3559 | 2.8385 | | | | |
| 160.00 | 10.7720 | 1.6855 | 2.1474 | 2.1114 | 2.6527 | | | | |
| 170.00 | 10.7571 | 1.6832 | 2.1276 | 2.0919 | 2.6662 | | | | |
| 180.00 | 0 | 0 | 0 | 0 | 0 | | | | |

DR(h, λ) $T = 40$ Seconds $\delta = 90^\circ$

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 3 | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 3 |
|----------|--|--|--|--|--|
| 10.00 | 543.1106 | -1946.5281 | -2642.9334 | -15.0710 | -31.4678 |
| 20.00 | 391.2632 | 1637.7327 | 2223.6609 | -15.5345 | -32.4355 |
| 30.00 | 192.4640 | 181.7297 | 246.7467 | -21.6188 | -45.1393 |
| 40.00 | 29.9003 | 15.6294 | 21.2211 | 5.2478 | 10.9571 |
| 44.00 | 2.0710 | 1.1256 | 1.5283 | .4289 | .8955 |
| 50.00 | 42.2716 | 24.9539 | 33.8816 | 17.3521 | 36.2307 |
| 60.00 | 777.6790 | 69.9839 | -95.0218 | -4.8697 | -10.1678 |
| 70.00 | -1374.7909 | -27.8354 | -37.7940 | -3.2671 | -6.8216 |
| 80.00 | -243.7620 | -9.0527 | -12.2915 | -2.3026 | -4.8077 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -243.7618 | -9.0527 | -12.2915 | -2.3026 | -4.8077 |
| 110.00 | -1374.7885 | -27.8354 | -37.7940 | -3.2671 | -6.8216 |
| 120.00 | 777.6797 | -69.9839 | -95.0218 | -4.8697 | -10.1678 |
| 130.00 | 42.2716 | 24.9539 | 33.8816 | 17.3521 | 36.2307 |
| 134.00 | 2.1801 | 1.1838 | 1.6073 | .4565 | .9532 |
| 140.00 | 29.9003 | 15.6294 | 21.2211 | 5.2478 | 10.9571 |
| 150.00 | 192.4640 | 181.7297 | 246.7467 | -21.6188 | -45.1393 |
| 160.00 | 391.2632 | 1637.7327 | 2223.6609 | -15.5345 | -32.4355 |
| 170.00 | 543.1107 | -1946.5269 | -2642.9318 | -15.0710 | -31.4678 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |
| θ | $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 |
| 10.00 | -4.3751 | -17.5114 | -3.8854 | -7.1741 | -3.1114 |
| 20.00 | -4.3017 | -17.2174 | -3.8576 | -7.1228 | -3.1008 |
| 30.00 | -4.3511 | -17.4153 | -3.8448 | -7.0991 | -3.0919 |
| 40.00 | -9.53318 | -38.1509 | -4.2798 | -7.9024 | -3.1899 |
| 44.00 | 4.9460 | 3.7863 | 34.2394 | 63.2208 | 4.9420 |
| 50.00 | -4.9423 | -19.7813 | -3.8760 | -7.1567 | -3.0849 |
| 60.00 | -2.7944 | -11.1847 | -3.4053 | -6.2877 | -2.9479 |
| 70.00 | -2.4159 | -9.6696 | -3.2598 | -6.0190 | -2.8950 |
| 80.00 | -2.1284 | -8.5190 | -3.1320 | -5.7830 | -2.8453 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -2.1284 | -8.5190 | -3.1320 | -5.7830 | -2.8453 |
| 110.00 | -2.4159 | -9.6696 | -3.2598 | -6.0190 | -2.8950 |
| 120.00 | -2.7944 | -11.1847 | -3.4053 | -6.2877 | -2.9479 |
| 130.00 | -4.9423 | -19.7813 | -3.8760 | -7.1567 | -3.0849 |
| 134.00 | 1.0416 | 4.1691 | 186.0357 | 343.5027 | 4.7025 |
| 140.00 | -9.5318 | -38.1509 | -4.2798 | -7.9024 | -3.1899 |
| 150.00 | -4.3511 | -17.4153 | -3.8448 | -7.0991 | -3.0919 |
| 160.00 | -4.3017 | -17.2174 | -3.8576 | -7.1228 | -3.1008 |
| 170.00 | -4.3751 | -17.5114 | -3.8854 | -7.1741 | -3.1114 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

$T = 30$ Seconds $\delta = 90^\circ$

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 1 | $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 |
|--|--|
| 10.00 | 526.9347 |
| 20.00 | 380.0459 |
| 30.00 | 187.4937 |
| 40.00 | 29.7072 |
| 44.00 | 2.3144 |
| 50.00 | 41.7452 |
| 60.00 | 745.4753 |
| 70.00 | -1422.4226 |
| 80.00 | -248.7182 |
| 90.00 | 0 |
| 100.00 | -248.7181 |
| 110.00 | -1422.4210 |
| 120.00 | 745.4757 |
| 130.00 | 41.7452 |
| 134.00 | 2.4294 |
| 140.00 | 29.7072 |
| 150.00 | 187.4937 |
| 160.00 | 380.0459 |
| 170.00 | 526.9348 |
| 180.00 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 1 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 1 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 |
|--|--|
| 10.00 | -3.6705 |
| 20.00 | -3.6585 |
| 30.00 | -3.6676 |
| 40.00 | -4.0546 |
| 44.00 | -44.8523 |
| 50.00 | -3.7455 |
| 60.00 | -3.3551 |
| 70.00 | -3.2522 |
| 80.00 | -3.1648 |
| 90.00 | 0 |
| 100.00 | -3.1648 |
| 110.00 | -3.2522 |
| 120.00 | -3.3551 |
| 130.00 | -3.7455 |
| 134.00 | -23.5681 |
| 140.00 | -4.0546 |
| 150.00 | -3.6676 |
| 160.00 | -3.6585 |
| 170.00 | -3.6705 |
| 180.00 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 1 to 2 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 2 | $\frac{\partial J}{\partial h}$ Layer 2 to 3 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 3 |
|--|--|
| -256.0989 | -462.9403 |
| -317.6043 | -574.1213 |
| 1133.6420 | 204.1874 |
| 18.4676 | 33.3831 |
| 1.3220 | 2.3897 |
| 33.7708 | 61.0462 |
| -39.7761 | -71.9018 |
| -18.5598 | -33.5498 |
| -7.4359 | -13.4415 |
| 0 | 0 |
| -7.4359 | -13.4415 |
| -18.5598 | -33.5498 |
| -39.7761 | -71.9018 |
| 33.7708 | 61.0462 |
| 1.3917 | 2.5157 |
| 18.4676 | 33.3831 |
| 1133.6117 | 2049.1869 |
| -317.6043 | -574.1213 |
| -256.0989 | -462.9403 |
| 0 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 2 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 2 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 |
|--|--|
| -4381 | -3932 |
| -4367 | -3921 |
| -4378 | -3925 |
| -4840 | -4219 |
| -5.3540 | -1.2397 |
| -4471 | -3980 |
| -4005 | -3665 |
| -3882 | -3577 |
| -3778 | -3500 |
| 0 | 0 |
| -3778 | -3500 |
| -3882 | -3577 |
| -4005 | -3665 |
| -4471 | -3980 |
| -2.8133 | -1.0553 |
| -4840 | -4219 |
| -4378 | -3925 |
| -4367 | -3921 |
| -4381 | -3932 |
| 0 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 3 to 4 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 4 | $\frac{\partial J}{\partial h}$ Layer 3 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 |
|--|--|
| 9 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 4 to 5 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 5 | $\frac{\partial J}{\partial h}$ Layer 4 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 |
|--|--|
| -3.6705 | -3.9711 |
| -3.6585 | 4.0580 |
| -3.6676 | 4.1583 |
| -4.0546 | 4.5153 |
| -44.8523 | 11.9732 |
| -3.7455 | 4.7870 |
| -3.3551 | 14.0647 |
| -3.2522 | 14.5153 |
| -3.1648 | 15.158 |
| 0 | 0 |
| -3.1648 | 15.4338 |
| -3.2522 | 16.3304 |
| -3.3551 | 17.4106 |
| -3.6676 | 18.3304 |
| -4.0546 | 19.1138 |
| -44.8523 | 24.0081 |
| -3.7455 | -16.4158 |
| -3.3551 | 19.6458 |
| -3.2522 | 20.0081 |
| -3.1648 | -19.3004 |
| 0 | -19.3004 |
| -3.1648 | 24.0081 |
| -3.2522 | 24.4481 |
| -3.3551 | 24.4606 |

| $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 | $\frac{\partial J}{\partial h}$ Layer 5 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 |
|--|--|
| 0 | 0 |

| $\frac{\partial J}{\partial h}$ Layer 6 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 | $\frac{\partial J}{\partial h}$ Layer 6 to 6 $\frac{\partial J}{\partial \lambda}$ for Source in Layer 6 |
|--|--|
| 0 | 0 |

DR(h,λ)

T = 20 Seconds δ = 90°

 $\frac{\partial}{\partial h} \text{Layer 1 to 2}$
 $\frac{\partial J}{\partial h} \text{for Source in}$
 Layer 1
 $\frac{\partial}{\partial h} \text{Layer 1 to 3}$
 $\frac{\partial J}{\partial h} \text{for Source in}$
 Layer 2

| θ | $\frac{\partial J}{\partial h}$ Layer 1 to 2 for Source in Layer 1 | $\frac{\partial}{\partial h} \text{Layer 1 to 3}$ $\frac{\partial J}{\partial h}$ for Source in Layer 2 | $\frac{\partial}{\partial h} \text{Layer 2 to 3}$ $\frac{\partial J}{\partial h}$ for Source in Layer 2 | $\frac{\partial}{\partial h} \text{Layer 2 to 3}$ $\frac{\partial J}{\partial h}$ for Source in Layer 3 | $\frac{\partial}{\partial h} \text{Layer 3 to 4}$ $\frac{\partial J}{\partial h}$ for Source in Layer 3 |
|--------|--|---|---|---|---|
| 10.00 | 644.2503 | -54.8378 | -2092.7418 | -4.8497 | 4.0055 |
| 20.00 | 466.6341 | -52.7728 | -2013.9379 | -4.8475 | 4.0037 |
| 30.00 | 232.3539 | -54.0168 | -2061.4138 | -4.8491 | 4.0050 |
| 40.00 | 38.4799 | 76.7256 | 2928.0350 | -4.9114 | 4.0564 |
| 44.00 | 3.5486 | 2.2616 | 86.3079 | -5.5216 | 4.5604 |
| 50.00 | 53.3796 | -90.6998 | -3461.3253 | -4.8624 | 4.0160 |
| 60.00 | 857.6700 | -17.4598 | -666.3088 | -4.7897 | 3.9559 |
| 70.00 | -2598.4890 | -11.0740 | -422.6120 | -4.7682 | 3.9382 |
| 80.00 | -395.6496 | -6.9018 | -263.3899 | -4.7491 | 3.9224 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | -395.6495 | -6.9018 | -263.3899 | -4.7491 | 3.9224 |
| 110.00 | -2598.4868 | -11.0740 | -422.6120 | -4.7682 | 3.9382 |
| 120.00 | 857.6702 | -17.4598 | -666.3088 | -4.7897 | 3.9559 |
| 130.00 | 53.3796 | -90.6998 | -3461.3253 | -4.8624 | 4.0160 |
| 134.00 | 3.7125 | 2.4128 | 92.0783 | -5.4604 | 4.5099 |
| 140.00 | 38.4799 | 76.7256 | 2928.0350 | -4.9114 | 4.0564 |
| 150.00 | 232.3539 | -54.0168 | -2061.4138 | -4.8491 | 4.0050 |
| 160.00 | 466.6341 | -52.7728 | -2013.9379 | -4.8475 | 4.0037 |
| 170.00 | 644.2504 | -54.8378 | -2092.7418 | -4.8497 | 4.0055 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

 $\frac{\partial}{\partial h} \text{Layer 3 to 4}$
 $\frac{\partial J}{\partial h}$ for Source in
 Layer 4
 $\frac{\partial}{\partial h} \text{Layer 4 to 5}$
 $\frac{\partial J}{\partial h}$ for Source in
 Layer 4

| θ | $\frac{\partial}{\partial h} \text{Layer 3 to 4}$ $\frac{\partial J}{\partial h}$ for Source in Layer 4 | $\frac{\partial}{\partial h} \text{Layer 4 to 5}$ $\frac{\partial J}{\partial h}$ for Source in Layer 4 | $\frac{\partial}{\partial h} \text{Layer 4 to 5}$ $\frac{\partial J}{\partial h}$ for Source in Layer 5 | $\frac{\partial}{\partial h} \text{Layer 5 to 6}$ $\frac{\partial J}{\partial h}$ for Source in Layer 5 | $\frac{\partial}{\partial h} \text{Layer 5 to 6}$ $\frac{\partial J}{\partial h}$ for Source in Layer 6 |
|--------|---|---|---|---|---|
| 10.00 | 147.3938 | 2.5807 | 4.3311 | 2.9513 | 4.7770 |
| 20.00 | 146.9187 | 2.5724 | 4.3249 | 2.9471 | 4.7308 |
| 30.00 | 151.4278 | 2.6513 | 4.5422 | 3.0952 | 4.9084 |
| 40.00 | 278.7405 | 4.8805 | 14.1075 | 9.6132 | 18.2860 |
| 44.00 | -49.2925 | -8631 | -9091 | -6195 | -8230 |
| 50.00 | 176.9778 | 3.0987 | 5.8884 | 4.0125 | 6.2642 |
| 60.00 | 111.0030 | 1.9435 | 2.9902 | 2.0376 | 3.0065 |
| 70.00 | 100.8038 | 1.7650 | 2.6392 | 1.7984 | 2.5820 |
| 80.00 | 93.3080 | 1.6337 | 2.3915 | 1.6296 | 2.2741 |
| 90.00 | 0 | 0 | 0 | 0 | 0 |
| 100.00 | 93.3080 | 1.6337 | 2.3915 | 1.6296 | 2.2741 |
| 110.00 | 100.8038 | 1.7650 | 2.6392 | 1.7984 | 2.5820 |
| 120.00 | 111.0030 | 1.9435 | 2.9902 | 2.0376 | 3.0065 |
| 130.00 | 176.9778 | 3.0987 | 5.8884 | 4.0125 | 6.2642 |
| 134.00 | -54.8557 | -3605 | -9989 | -6807 | -9008 |
| 140.00 | 278.7405 | 4.8805 | 14.1075 | 9.6132 | 18.2860 |
| 150.00 | 151.4278 | 2.6513 | 4.5422 | 3.0952 | 4.9084 |
| 160.00 | 146.9187 | 2.5724 | 4.3249 | 2.9471 | 4.7308 |
| 170.00 | 147.3938 | 2.5807 | 4.3311 | 2.9513 | 4.7770 |
| 180.00 | 0 | 0 | 0 | 0 | 0 |

 $\frac{\partial}{\partial h} \text{Layer 5 to 6}$
 $\frac{\partial J}{\partial h}$ for Source in
 Layer 6
 $\frac{\partial}{\partial h} \text{Layer 5 to 6}$
 $\frac{\partial J}{\partial h}$ for Source in
 Layer 6

| θ | $\frac{\partial}{\partial h} \text{Layer 5 to 6}$ $\frac{\partial J}{\partial h}$ for Source in Layer 6 |
|--------|---|
| 10.00 | 0 |
| 20.00 | 0 |
| 30.00 | 0 |
| 40.00 | 0 |
| 44.00 | 0 |
| 50.00 | 0 |
| 60.00 | 0 |
| 70.00 | 0 |
| 80.00 | 0 |
| 90.00 | 0 |
| 100.00 | 0 |
| 110.00 | 0 |
| 120.00 | 0 |
| 130.00 | 0 |
| 134.00 | 0 |
| 140.00 | 0 |
| 150.00 | 0 |
| 160.00 | 0 |
| 170.00 | 0 |
| 180.00 | 0 |