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REPORT NO. 377

COMPARISON OF BUDD AND REVERE 4.5" ROCKETS

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U.S. ARMY ABERDEEN RESEARCH AND DEVELOPMENT CENTER BALLISTIC RESEARCH LABORATORIES ABERDEEN PROVING GROUND, MARYLAND

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Ballistic Research Laboratory Report No. 377

RJW/bvs Aberdeen Proving Ground, Md. July 9, 1943

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Abstract

Two types of 4.5" rocket have been fired statically and in flight to determine the differences in performance due to differences in design and methods of manufacture of the rocket motors. / The following conclusions can be drawn from the data obtained:

1. When fired at high temperatures the Budd motor is slightly less likely to fail than the Revere motor. The critical temperature range for both rockets with 4.81bs. propellant is from 110° to 120°F.

2. The low temperature limit for satisfactory operation is 25°F lower for the Budd than for the Revere.

3. The Budd outranges the Revere by 24%.

4. When fired from a 20 ft. launching tube the lateral dispersion of the Budd is about 40% less than that of the Revere. From a 10 ft. tube the dispersions of the two rockets are not significantly different.

An extended series of tests has been made to compare the behavior of two types of 4.5" rockets. These tests were planned and executed by the Ballistic Research Laboratory with the cooperation of members of Division 3 of the National Defense Research Committee. This report presents and discusses the complete data of the static tests and gives a summary of the flight test results. The flight test data are given in detail in Intra-office Memoranda E-46-6,7,8, and 9 of the Photographic Measurement Section, Exterior Ballistic Branch.

Characteristics of the Rockets.

The significant features of the two types of 4.5" rockets are illustrated in Figure 1. The fins are not shown in this diagram but can be seen in Figure 2. The rockets are manufactured respectively by the Revere Copper and Brass Co. and by the Budd Wheel Co. and the Budd Induction Heating Co. Their important differences lie in the construction of the motors and are listed below.

1. Method of manufacture. The Budd Motor is made from 1035 steel seamless tubing which has been hardened by induction heating. It is machined to size, and the threaded end is left considerably thicker than the rest of the wall of the motor.

The Revere motor is made from welded 1025 steel tubing, formed and strengthened by cold drawing. There is no extra thickness at the threads.

In each type of motor there is cut a safety groove slightly back of the threads. The purpose of this is to cause a clean break separating the motor from the HE head if excess pressures are developed in the chamber. Without such a groove the motor is in danger of shattering. The Budd safety groove is set to break at about 6000 lbs/sg.in., although it can safely be set at 6500 as the ungrooved Budd motor will hold pressures up to 8,000.

2. Throat diameter. On the Revere motor the diameter of the throat of the venturi varies from 1.820 to 1.835 inches. Under normal conditions (4.8 lbs. powder, 70°F) this gives a peak pressure of about 2500 lbs/sq.in. (see Table II). To take advantage of the greater strength of the Budd rocket the throat diameter was set at 1.750 inches. The corresponding peak pressure is about 3400 lb/in². This higher operating pressure gives shorter burning time and consequent lower dispersion in flight. Also, the higher pressure obtained in the Budd gives satisfactory powder burning at a temperature well below that at which the Revere ceases to function properly (Tables V and VI.)

3. Fin assembly. The fin assemblies of the two rockets are shown in Figure 2. The Revere assembly is somewhat more rugged than the Budd, but it exerts a large drag on the rocket in flight. The 300 yard shorter range of the Revere rockets (see Table VII) can presumably be accounted for mainly by the different fin assemblies.

Description of Tests.

Throughout these tests the loading of the rockets was kept as constant as possible. Each rocket was loaded with 4.80 lbs. of Radford Ordnance Works Lot 10015. This is one of the lots which is loaded into standard rounds, and it is assumed, for lack of any information to the contrary, that it is typical JPT powder. Its properties are given in Table I. The Revere rockets used in the flight tests were standard rounds, the igniter consisting of two 20 gm. bags of grade A-1 black powder and a plastic cup containing 45 gm. of the same powder. All Budd rockets and all Revere rockets tested statically were ignited by a <u>single</u> bag containing 35 gms of this same powder.

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For the high temperature tests the rockets were left in an oven for from 36 to 44 hours. The oven had no forced air circulation, but at the times the rockets were removed there was a difference of at most 4°F between the top and the bottom The rockets were carried from the oven to the of the oven. firing position in individual insulated boxes. No more than four minutes elapsed between removal of a round from the oven and firing, and about three minutes of this time were spent in the insulated box. A test round fitted with a thermometer in contact with the powder showed a drop of 2°F under this treat-The two types of motors were distributed evenly on the ment. shelves of the oven, except in the case of the eight Budds at 140°F, and were fired alternately. During the time of firing of 8 rounds (the capacity of the oven), the temperature at the top of the oven fell about 4°F and that at the bottom rose between 4° and 14°F, this rise being due to the activation of the heating element. In each round, maximum pressure was measured by two ball crusher gages firmly fastened inside the motor.

In the low temperature tests the rounds were left in a refrigerator for from 18 to 24 hours. Since the refrigerator was cuite near the firing position no insulated boxes were used. From 1 to 4 minutes elapsed between removal from the refrigerator and firing, the longer period being due to the delay involved in connecting pressure strain gages.

The rockets used in the flight tests were stored together overnight, transported together to the firing position, and kept, throughout the firing, as much as possible under the same conditions. All the Budds were inert-loaded to 38.5 lbs. with a mixture of parafin and red lead and a dummy fuze. The Reveres were H. E. loaded. Those used on 27 April had a dummy fuze and were brought up to 38.5 lbs. with sand and metal slugs. The rest of the Reveres were standard M8 rounds, their weights varying between 38.0 and 39.0 lbs. Before firing, the safety pin was not withdrawn, but was cut off flush with the outside of the head.

Survey of the Data.

1. High temperature tests. The results obtained from tests at high temperatures are given in Tables III and IV. By taking rough averages we obtain the following table of pressures and behaviors.

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110°F

Budd5000 p.s.i; 8 held out of 85800 p.s.i; 4 held out of 8Revere4200 p.s.i; 7 held out of 84600 p.s.i; 1 held out of 7

It seems that the step from 110° to 120°F is rather critical for both types of rockets. The superior strength of the Budd is evident, as its maximum safe pressure is about 1000 p.s.i. higher than that of the Revere. Moreover, as has been pointed out earlier, the safety groove in the Budd can safely be set to 6500 p.s.i. instead of 6000, and at this setting a temperature of 120°F should be relatively safe. (If one accepts the pressure records on the individual rounds, two of the Budds would have failed at 120° even with the safety groove set at 6500 p.s.i. On the same basis, only two of the eight should have failed in the actual test. Since neither the pressure readings nor the setting of the safety grooves are particularly accurate such discrepancies are to be expected).

In addition to the difference in strength of the motors shown by these data there is a significant difference in the types of failure. All the Budds broke off cleanly at the safety groove, the motors being otherwise intact. In all but two of the Reveres, however, the safety groove did not break at all. The motors merely spread apart at the threads and slipped off the heads. The difference in behavior is undoubtedly due mainly to the different thickness of the two types of motors at the threads. The behavior of the Reveres makes it impossible to strengthen them by changing the depth of the safety groove.

2. Low temperature tests. The behavior of the rockets at low temperatures is shown in Tables V and VI. The significant point to be noted here is that the critical temperature dividing continuous from interrupted burning ("chuffing") is around -15°F for the Budd rockets and 10°F for the Reveres. Since interrupted burning is a relatively useless, and at times a dangerous, performance, the useful lower temperature limit for the Budd is about 25°F lower than for the Revere.

It should be noted that even with continuous burning at low temperatures the performance of the rocket will not be particularly good. The long burning times which are obtained at these temperatures will lead to a very large dispersion in the flight of the rocket, with a consequent lowering of its efficiency as a weapon.

3. Flight tests. The flight data have been tabulated and exhaustively analyzed in a separate report. (Intra-office Memoranda E 46-9). Hence we give here only a summary of the more important data (Table VII). The following conclusions can be drawn from these figures: a. The burnt velocity of the Budd rocket averages 27 ft./sec., or about 3% higher than that of the Revere. This is presumably due to the higher working pressure in the Budd, which gives a higher gas velocity and hence greater efficiency of the motor.

b. The Budd outranges the Revere by 775 yds. (24%). The difference in velocities can account for at most 6% out of the 24\%, the remaining difference is obviously due to the different fin assemblies. The flange which supports the Revere fins clearly causes a considerable drag on the rocket in flight.*

c. The burning distance of the Budd rocket is considerably less (about 20 ft.) than that of the Revere. (Since very short burning distances did not record on the films the statistic given for this quantity is the mode rather than the mean. Even the mode could not be determined for the extremely short burning distances of the Budd on the second day's firing.) This is another effect of the higher pressure in the Budd.

d. The lateral dispersions of the two types of rockets, as measured by the standard deviations of their lateral deflections from the assumed line of fire, are very nearly the same for the firings from the 10 ft. launching tube, about 15 mils. From the 20 ft. tube, however, their values, 9.0 mils for the Budd and 15.2 mils for the Revere, are consider-ably different. The reason for this behavior becomes apparent if we consider the burning distances outside the tubes. For the 20 ft. tube these are 40 and 59 for the Budd and Revere rockets respectively, while the corresponding figures for the 10 ft. tube on the third day are 59 and 76. The ratio of the first two figures is 1.47, and of the second pair 1.29. Since dispersion depends considerably on burning distance outside the . tube, it is easy to see why different results are obtained in The fact that with the 10 ft. tube the Revere the two cases. shows about the same dispersion as the Budd, in spite of the difference in burning distances, leads one to conclude that the Revere has probably less malalignment than the Budd - and would have somewhat less dispersion if the burning distances were equal.

Summary of Conclusions.

1. The Budd 4.5" rocket motor, with 1.75" throat and safety groove set at 6000 lbs./sc.in. is slightly less likely to fail at elevated temperatures than the Revere motor (1.83" throat). The critical region for both is from 110° to 120°F. The Budd can be made stronger by setting the safety groove at 6500 lbs./ sq. in., but even then failure would be likely to occur at 120°F in some cases.

*Cf. R. T. Knapp, Memorandum on water tunnel tests of the 4.5" rocket projectile with three different fin tails and with one ring type tail. NDRC, Div. 6, Sec. 6.1; C.I T. Hydraulic Machinery Laboratory Report No. ND-12.1. 2. At low temperatures the smaller throat of the Budd motor gives it a distinct advantage over the Revere. The lower limit of satisfactory burning for the Revere is about 10°F, whereas for the Budd the corresponding temperature is about -15°F.

3. The higher operating pressure of the Budd gives it a 3% greater burnt velocity than the Revere. This gives some increase in range to the Budd, but much more (to a total of 24%) is provided by the more streamlined fin assembly. The two rockets do not differ much in lateral dispersion when fired from a 10 ft. launching tube, but for a 20 ft. tube the shorter burning distance of the Budd, again due to the higher pressure, gives it a dispersion of 9.0 mills standard deviation as against 15.2 mills for the Revere.

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	Data on ROW Powder Lot 1001	5
<u></u>	Composition (percent)	
	Nitrocellulose (13.23%N)	58.73
	Nitroglycerin	40.07
	Ethyl Centralite	1.04
	Diphenylamine	0.16
Normal control (Science and a Science)		100.00
	Total Volatiles	1.71
	Heat of explosion (cal./gm.)	12.02
	Length (in.)	5.138
	Outside diameter (in.)	0.368
	Inside diameter (in.)	0.284
	Web (in.)	0.292
	Specific gravity (25°C)	1.62

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Motor Type		Reve	ere			Bude	1	
Motor Number	61C	1210	78D	172B	2947	2952	2979	3003
Throat Diameter (in.)		1.825	+ .0	10	1.746	1.746	1.754	1.750
Powder Lot				ROW	10015			
Powder Wt. (1b.)				4.	80			
No. Grains	35	35	34	30	36	37	30	30
Powder Temp. (°F)	70	70	70	73	70	70	73	73
ĸ	232	232	232	228	253	253	246	246
Burning Time (sec.)	.174	.182	.186	.180	.130	.140	158	
Max. Press.(1b./sq.in.)								1
Strain Gage	2750	2550	2430	2240	4230	3650	3040	2880
Ball Gage 1	2700	2600	2600	2400	4300	3500	3000	2900
Ball Gage 2	2700	2600	2600	2400	4100	3400	3100	2900
Ave. Pressure	1610	1380	1380	1500	2250	2210	1780	-
<pre>Impulse (lb.sec.)</pre>	960	960	890	1090	960	1060	1000	-
Eff.Gas Vel.(ft/sec.)	6400	6400	5900	7300	6400	7100	6700	-

			T	ABLE	II		
Static	Test	of	Budd	and	Revere	4.5"	Rockets

Ignition by a single bag containing 35 gm. of A-1 black powder.

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Powder Temp. (°F)	No. of Grains of Powder	Throat Diam. (in.)	Pres	r Ball ssures sq.in.)	Behavior
140 140 140 140 140 140 140 140	30 30 30 30 30 30 30 30	1.746 1.745 1.745 1.742 1.745 1.750 1.746 1.742	7300 3300 5900 4100 5900 5100 6300 5900	7500 7000 7300 6600 6700 7900 7300	Failed at groove n n n n n n n n
120 120 120 120 120 120 120 120	37 36 35 38 38 35 35 35 36	1.745 1.747 1.754 1.748 1.750 1.748 1.757 1.749	4700 6200 6800 5700 5700 7500	4650 5750 5600 5100 5900 7500	Held Failed at Groove Held Failed at Groove Held Failed at Groove Held Failed at Groove
110 110 110 110 110 110 110 110	35 36 41 40 40 35 43 40	1.745 1.745 1.748 1.764 1.747 1.754 1.748 1.762	4700 4800 4800 5900 3700 4800	2800 4900 4900 5600 5100 5200 2500	Held II II II II II II II

High Temperature Test of Budd 4.5" Rockets

Rockets loaded with 4.80 lbs. of ROW Lot 10015. Ignition by a single bag containing 35 gm. of A-1 black powder. Thickness of wall at safety groove was from .047 to .056 inches

TABLE IV

Powder Temp. (°F)	No. of Grains of Powder	Copper Ball Fressures (lb./sq.in.)	Behavior
120 120 120 120 120 120 120 120 120	33 34 35 34 34 35 34 35 34 34	4800 4300 4500 4600 5000 5100 3700 3800 4400 4500 4500 4600 4600 4900	Failed at threads Misfire Failed at threads Failed at threads and groove Failed at groove Held Failed at threads
110 110 110 110 110 110 110 110	35 35 34 35 35 35 35 36	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Held "" "" " Failed at threads

High Temperature Test of Revere 4.5" Rockets

Rockets loaded with 4.80 lbs. of ROW Lot 10015.

Ignition by a single bag containing 35 gm. of A-1 black powder.

Throat diameters: 1.825 ± .010. (Total Range)

TABLE V

Low T	emperature	Test of Bud	ld 4.5" Rocket	S
Powder T'emp.	No. of Blasts	Eurning Time	Maximum Fressure	Comments
(°F)	an ann an an an tach ann an	(sec.)	(1b./sq.in.)	
-8 -8 -8 -8	1 1 2 2	.320 .304 _ _	2320 1600 - -	
-13 -13 -13 -13		•334 •298 -		
-13 -13 -13 -13	1 1 1 1	- - -	- - -	
-22 -22 -22 -22	N N N N N N	- - -		About 1 sec. between blasts " "
-26 -26 -26	2 1 2	. 326*	-	About 1 sec. between blasts
-26	2	.306* .058**	1710* 1120**	2.4 sec. between blas *First blast. **Second blast

Rockets loaded with 4.80 lbs. of ROW Lot 10015.

Ignition by a single bag containing 35 gm. of A-1 black powder. Throat diameters: $1.748 \pm .007$ in. (Total Range)

Low	Temperat	ure Test of	f Revere 4.5" R	ockets
Powder Temp. (°F)	No. of Blasts '	Burning Time (sec.)	Maximum Pressure (1b./sq.in.)	Comments
23 23 23 23 23 23 23 6 6 6 6 6 6 6 6 6 6	1 1 1 1 1 2 1 2 1 2 1 2 2 2 2 2 2 2 2 2	- .248 .274 - - - - - - - - - - - - - - - - - - -	- 1980 1840 - - - - - - - - - - - - - - - - - - -	<pre>About 1/2 sec. between blasts 1.6 sec. between blasts About 2 sec.between blasts l.5 " " " About 2 sec. between blasts l.5 " " " 3.7 sec. between first and second blasts.</pre>

TABLE VI

* First blast. ** Second blast.

Rockets loaded with 4.80 lbs. of ROW Lot 10015.

Ignition by a single bag containing 35 gms. of A-1 black powder.

Throat diameters: 1.825 ± .010 in. (Total Range)

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•	i	÷.	:	n S ^{al}	Flight	Test of	of budd	and hev	Revere 4.5"	5" Rockets	S		1	i	, ,
i	Date Fired	red	Type	No. of Rds.	Length of Launcher (ft.)	Range (yds. M	ls: (Lateral Deflection M o	l tion s) o	Burning Dist. (ft.) Mode	Velocity* (ft./sec.) M o	ity* sec.) o	Eff. Gas Vel. (ft./sec.)	Pdr. Temp. (°F)	Air Temp. (°F)
1	4/5	4/27/43	Budd	33	20	3944	78	-2.0	0.6	60	016	30	6850	1	55 _
	4/2	4/27/43	Revere.	30	. 20	3139	57	-5.9	15.2	- 64	878	32	6600	1	55
ł	: 4/2	4/23/43	Budd	- 29.	10	4056	146	0.8	15.6	I	920	-23	6920	.78	74
,	. 4/2	4/28/43-	Revere	30	I.O	3311	-109	-1.6-	17.5-	85	886	27	6600	- 82	- 74
****	. 4/2	4/29/43	Budd	45	10	3917	- 96	-1.4	15.2	69	899	28	. 6760	. 65	- 22 -
1	4/5	4/29/43	Revere	39		3141	611	- 3.2	17.4	- 86	885	30	6650	65	57
ł	13-	L rock	sts load	ed with /	All rockets loaded with 4.80 lbs.	of ROW Lot		10015.	La R	11	-	1	۰ ۱	-d -	1
í	Tot	tal we:	Total weight of Reveres	Reveres (on 4/27/43	and of all		Budds: 3	38.50 ±	.05 lbs.	. (Total	al hange	3e)		ł
1	Tot	tal we.	Total weight of Reveres	Reveres (on 4/28/43 and 4/29/4	and 4/	29/43:	: 38.5 ±	5	lbs.(Total	Range)				
	H M	= mean	mean value = $\sum x_1/N$	2 x1/N											
	11 15		lard dev:	Standard deviation =	\Σ (x ₁ -M) ² /(N-1)	(T-N)/2		Probable	error	= .674 σ	•				
	> *	/eloci1	ty 135 ft	t. horize	* Velocity 135 ft. horizontally from breech	om bree	of	launcher	. 4						
	* *	Effective		gas velocity	y = (Rocket wt.	t wt	- I N	Powder wt.)		Velocity/Powder	ler wt.				
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