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Technical Memorandum 1982

A METHOD OF CHOOSING PROJECTILE MANUFACTURING TOLERANCES SO AS TO MINIMIZE COSTS OF PRODUCTION WHILE SATISFYING FUNCTIONAL REQU'TREMENTS

by

Eugene Friedman Edward Lacher Chiu Ng

December 1970

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SUMMARY

A method has been devised which allows one to compute the tolerances of dimensions of a projectile or other manufactured item in such a manner as to minimize the costs of production. The method further allows the imposition of any number of inequality constraints (tolerances) on properties of the dimensions (weight, volume, center of mass position, etc.), which will be satisfied to a linear appro imation.

A particular form (hyperbolic) for the cost function has been chosen as the example here computed, but the method is not limited to this form. A computer program to facilitate numerical application of this technique has been written, and another program to compute the required sensitivity coefficients for three dimensional mass asymmetry limits is presently in development.

INTRODUCTION

Certain problems of dimensional irregularity encountered during the production of the 175mm, M437 Projectile were brought to the attention of this laboratory. The effects of these irregularities on the static and dynamic unbalances and the effect of these unbalances on the flight of these projectiles were not sufficiently well understood to justify acceptance or rejection of the projectiles in question. During the course of the investigation of the flight dynamic effects of these irregularities (which did not fall within manufacturing tolerances) it became clear that an opportunity existed for the introduction of more sophisticated engineering methods into the decision making process. These methods ought to be useful for evaluation of requests for waiver of tolerance.

The following analysis is an early result of a search for superior techniques for choosing projectile tolerances.

DISCUSSION

If the properties of an item one wishes to control in manufacture are called Z^{i} and these Z^{1} are functions of the dimensions of the item, X^{i} , and the minimum and maximum acceptable values of Z^{i} are C_{1}^{i} , and C_{2}^{i} , one may say

$$C_{1}^{i} \leq Z^{i}[X^{k}, k=1, n] \leq C_{2}^{i}$$
 (1)

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If we assume that any variation in any actual dimension of an item is small compared to the nominal dimension itself, then

$$\Delta z^{i} \simeq \sum_{k=1}^{n} \frac{\partial z^{i}}{\partial x^{k}} \qquad (2)$$

where the $\frac{\partial Z^{i}}{\partial \chi^{k}}$ are evaluated at the nominal dimensions of the item, and are called sensitivity coefficients.

Combining Equations 1 and 2 we obtain, approximately

$$\delta C_{1}^{i} \leq \sum_{k=1}^{n} \frac{\partial Z^{i}}{\partial x^{k}} \Delta x^{k} \leq \delta C_{2}^{i}$$
(3)

where $\delta C_{1}^{i} = C_{1}^{i} - Z_{nominal}^{i} \leq 0$, $\delta C_{2}^{i} = C_{2}^{i} - Z_{nominal}^{i} \geq 0$ and $\Delta Z^{i} = Z^{i} - Z_{nominal}^{i}$, $\Delta X^{k} = X^{k} - X^{k}_{nominal}$

In order to assure that

 $\sum_{k=1}^{n} \frac{\partial Z^{i}}{\partial x^{k}} \Delta x^{k} \leq \delta C_{2}^{i}$

One may require that

$$\frac{\partial z^{i}}{\partial x^{k}} \Delta x^{k} \leq f_{k} \delta C_{2}^{i}$$
(4)

where the f_k are not a priori known but obey

$$0 \le f_k \le 1 \tag{5}$$

$$\sum_{k=1}^{n} f_k = 1$$
 (6)

and, similarly, to assure that

$$\sum_{k=1}^{n} \frac{\partial z^{i}}{\partial x^{k}} \Delta x^{k} \geq \delta C_{1}^{i}$$

we require that

$$\frac{\partial z^{i}}{\partial x^{k}} \Delta x^{k} \geq f_{k} \delta C_{1}^{i}$$

with the f_k obeying Equations 5 and 6.

Assuming that the f_k be somehow determined for each control property, Z^{i} , the minimum and maximum excursion of the ΔX^k can be written

 $\Delta \mathbf{x}_{i\min}^{\mathbf{k}} \equiv \frac{\delta \mathbf{C}_{1}^{i} \mathbf{f}_{\mathbf{k}}}{\frac{\partial z^{i}}{\partial \mathbf{x}^{\mathbf{k}}}} \qquad \frac{\partial z^{i}}{\partial \mathbf{x}^{\mathbf{k}}} > 0. \quad (8)$ $\equiv \frac{\delta \mathbf{C}_{2}^{i} \mathbf{f}_{\mathbf{k}}}{\frac{\partial z^{i}}{\partial \mathbf{x}^{\mathbf{k}}}} \qquad \frac{\partial z^{i}}{\partial \mathbf{x}^{\mathbf{k}}} < 0.$

and

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$$\Delta x_{i_{max}}^{k} \equiv \frac{\delta C_{2}^{i} f_{k}}{\frac{\partial z^{i}}{\partial x^{k}}} \qquad \qquad \frac{\partial z^{i}}{\partial x^{k}} > 0.$$
(9)

$$= \frac{\frac{\delta c_{1}^{i} f_{k}}{\frac{\partial z^{i}}{\partial x^{k}}}}{\frac{\partial z^{i}}{\partial x^{k}}} < 0$$

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from Equations 4 and 7.

If these be interpreted as limits on the range of x^k due to the limits imposed on Z^1 , the intersection over all i of the regions

$$\Delta x_{i_{\min}}^{k} \leq \Delta x^{k} \leq \Delta x_{i_{\max}}^{k}$$

will have bounds δX_{\min}^k and δX_{\max}^k and still obey all requirements within the approximation (Eq 2). These are the intersections of all the sets of restrictions:

$$\delta x_{\min}^{\mathbf{k}} = \max_{\mathbf{i}} (\Delta x_{\min}^{\mathbf{k}})$$
(10)

 $\delta \mathbf{x}_{\max}^{\mathbf{k}} = \frac{\min}{\mathbf{i}} (\Delta \mathbf{x}_{\max}^{\mathbf{k}})$ (11)

The absolute minimum and maximum may be chosen at this point although the f_k are not known. Since for a given k all the ΔX^k contributing to δX^k_{max} have the same f_k (and different C's and $\frac{\partial Z^i}{\partial X^k}$'s), the minimum ΔX^k_{max} is the one with minimum $\frac{\delta C}{\frac{\partial Z^i}{\partial X^k}}$. The same argument holds for δX^k_{min} .

So for a given projectile and specifications [Z, X, C], δx_{\min}^k and δx_{\max}^k are constants times f_k .

It is now necessary to introduce the notion of a cost function, which reflects the unit cost of production with a given process or sequence of processes, and depends on the tolerances required. Given the equipment and size of the lot, the fixed costs are determined. Call this $\xi_{\rm o}$.

It is apparent that there exists some tolerance which is not quite possible to obtain using the ℓ th process; call it n_{ℓ} . The production cost grows very large as the tolerance.

on this process, $\delta X_{\max}^{\ell} - \delta X_{\min}^{\ell}$, approaches this η_{ℓ} and the cost function must reflect this tendency. Further, each process is different and each has its own constant, ξ_{ℓ} , multiplying its contribution to the total cost. Therefore we define a cost function ξ_{ℓ} .

$$\$ = \xi_0 + \Sigma \frac{\xi_\ell}{\delta x_{\max}^\ell - \delta x_{\min}^\ell - \eta_\ell}$$
(12)

where the ξ_{ℓ} are provided; they reflect the cost of reducing the tolerance on a given process; they need not be given in absolute terms, but relative to each other: i.e., $\xi_j=2.3 \ \xi_{j-1}$; and the η_{ℓ} are the lowest practical value of the tolerance of the ℓ th operation. So the problem proposed is to minimize \$ by a suitable choice of the f_k subject to the conditions $\Sigma f_{j}=1$, $f_{j}\geq 0$. Note that the δX^{j} are linear in f_j and are functions only of f_j and the constants of the minimization problem. C_1^i , C_2^i , $\frac{\partial Z^i}{\partial X_j}$ are all fixed for a given projectile. Therefore we propose to minimize

$$s = \xi_0 + \ell_{z=1}^{\Pi} \frac{\xi_\ell}{k_\ell f_\ell - \eta_\ell}$$
(13)

where η_{ℓ} is the tightest tolerance possible by the ℓ th manufacturing operation, and ξ_{ℓ} is the rate of change of cost with respect to tolerance level for the ℓ th operation, subject to the condition

$$\sum_{\ell=1}^{n} f_{\ell} = 1 \xrightarrow{\ell} \sum_{\ell=1}^{n} (f_{\ell} - \frac{1}{n}) = 0$$
 (6a)

Equations 5,6a, and 13 can be combined into

$$\$ = \xi_0 + \Sigma \left[\frac{\xi_{\ell}}{\kappa_{\ell} f_{\ell} - \eta_{\ell}} + \Pi \left(f_{\ell} - \frac{1}{n} \right) \right]$$
(14)

where Π is a Lagrange multiplier (\neq 0) and the usual condition for an extremum with respect to f_i is applied:

$$\frac{\partial \xi}{\partial f_{j}} = \frac{-\xi_{j}k_{j}}{[k_{j}f_{j} - n_{j}]^{2}} + \Pi = 0,$$

which is n equations in the n f's and one II and

$$\sum_{\ell=1}^{n} f = 1$$
 is the n+1th equation.

Solving for f_i and Π yields:

$$f_{j} = \frac{\frac{\xi_{j}k_{j}}{\Pi} + \eta_{j}}{k_{j}} = \frac{\xi_{j}}{k_{j}} + \frac{\eta_{j}}{k_{j}}$$
(15)

and

$$\Pi = \left\{ \begin{array}{c} \frac{n}{\sum_{j=1}^{n} \sqrt{\xi_{j/k_{j}}}} \\ \frac{j=1}{1 - \sum_{j=1}^{n} \eta_{j/k_{j}}} \end{array} \right\}^{2}$$
(16)

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Therefore, the actual tolerances can be calculated from these closed form solutions by substituting actual values into Equations 8, 9, 15, and 16, and the results into Equations 10 and 11.

CONCLUSIONS

It has been demonstrated that it is possible to optimize the cost of production of a projectile in a manner which guarantees approximate satisfaction of any number of inequality constraints on any property of the dimensions (the functional requirements).

This is, of course, in some sense a "worst case" solution since an item with maximum error in all its dimensions still satisfies all the inequality constraints. This may lead to impractically tight tolerances. It is then clear that some small but finite failure rate (fail-

ure to meet the functional requirements) is acceptable in a lot, if all of the items in it satisfy the tolerances imposed on the dimensions.

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We believe that the above computed distribution of tolerance (that is, the relative sizes of the tolerance) is still useful. Further, it is felt that a suitable constant for each tolerance can be developed which will involve the probability of each half-distribution of dimension exceeding tolerance, normalized in such a way that each half distribution will contribute an equal amount toward the probability of not satisfying the functional requirements.

Further effort in this direction is necessary for a more complete understanding of the probabilistic effects and this effort will be pursued.