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PART I

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**CHARACTERIZATION OF VERY PAUCI-DISPERSE
SYSTEMS WITH STRONG INTERACTION BY
EQUILIBRIUM SEDIMENTATION**

**PART I. DETERMINATION OF MOLECULAR WEIGHTS AND
PARTIAL EVALUATION OF INTERACTION MATRIX**

MATATIAHU GEHATIA

DONALD R. WIFF

TECHNICAL REPORT AFML-TR-69-235, PART I

JANUARY 1970

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PART I

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FOREWORD

This report was prepared by the Polymer Branch of the Nonmetallic Materials Division. The work was initiated under Project 7342, "Fundamental Research on Macromolecular Materials and Lubrication Phenomena," Task No. 734203, "Fundamental Principles Determining the Behavior of Macromolecules." The work was administered under the direction of the Air Force Materials Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, with Dr. M. T. Gehatia acting as project scientist.

The report covers research conducted from January 1968 to April 1969. The manuscript was released by the author in May 1969 for publication as a technical report.

This technical report has been reviewed and is approved.

William E. Gibbs

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ABSTRACT

As part of a series of investigations of the fundamental properties of certain aromatic-heterocyclic polymers, a study has been done on the equilibrium sedimentation of samples of poly (2,2'-m-phenylene-5,5'-bibenzimidazole) in dimethylacetamide. Although these samples were obtained by fractional precipitation techniques from a whole polymer, it was found that their behavior was best described by assuming some samples to be composed of at least two major sub-fractions. In addition, this analysis required that each sub-fraction have a relatively strong interaction with itself and other sub-fractions. Because each sample consisted of a small number of major fractions a method was developed based upon considerations from pauci-disperse systems to characterize molecular weights and polymer-polymer interaction terms. This report details the development of this method. The concentration of these samples is represented by:

$$c \approx \sum_{n=1}^N g_n \exp [h_n \omega^2 x - R_{nk} c + (R_{nk} - R_{nn}) c_n],$$

where c is concentration; x = square of the distance from the center of rotation; h_n a constant proportional to molecular weight of fraction n ; R_{nk} , R_{nn} are interaction coefficients and ω is the angular velocity.

The distribution of this Abstract is unlimited.

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LIST OF SYMBOLS

- r = the distance from the center of rotation
- r_m = the distance from the center of rotation to the meniscus
- r_b = the distance from the center of rotation to the bottom of the cell
- $x = r^2$
- $m = r_m^2$
- $b = r_b^2$
- r_o = the distance from the center of rotation to the initial boundary in a velocity experiment
- s = sedimentation constant
- D = diffusion constant
- ω = angular velocity
- $\beta = h \omega^2$
- t = time
- T = absolute temperature in °K
- R = universal gas constant, or interaction parameter in general
- ρ = density of solution
- ρ_0 = density of solvent
- V = partial specific volume of polymer in solution
- c = concentration in g of polymer per g of solution
- c^* = initial concentration
- $H = 2RT/(1-V\rho)$
- M = molecular weight
- $h = M/H$
- g = a constant defined for θ -temperature where, $g = c e^{-h \omega^2 x}$

LIST OF SYMBOLS (CONT)

 c_n c^*_n M_n h_n g_n

$\left. \begin{array}{l} c_n \\ c^*_n \\ M_n \\ h_n \\ g_n \end{array} \right\}$ the above defined quantities corresponding to fraction n,
 R_{nk} = interaction parameter appearing in an expression for c_n , and
caused by c_k

SECTION I

INTRODUCTION

Aromatic-heterocyclic polymers are a class of interesting materials that are currently being developed due to their resistance to high temperature. Relatively little has been done toward determining many of the fundamental parameters that govern the physical behavior of these chains. This report covers one phase of an investigation of the dilute solution properties of one of the earlier, high molecular weight aromatic-heterocycles, poly(2,2'-m-phenylene-5,5'-bibenzimidazole) (PBI), dissolved in a good solvent dimethylacetamide (DMAC). Specifically this report concerns equilibrium sedimentation measurements on samples of this polymer in an effort to define molecular weight, and polymer-polymer interaction parameters.

Preliminary measurements on these samples suggested that each sample consists of a relatively small number of rather discrete molecular weight ranges. In addition, it was suspected that relatively strong interactions could exist between various species. Therefore, early consideration was given to describing this situation by applying a method developed from study of pauci-disperse systems.

This is discussed in the next section.

SECTION II

THEORY

A MONODISPERSE SYSTEM WITH INTERACTION

Consider a monodisperse polymer with significant concentration dependence. If higher than first order terms can be neglected, the concentration achieved in equilibrium-sedimentation can be expressed by the following equation:

$$c = g e^{\hbar \omega^2 c - R c} \quad (1)$$

The relationship expressed by Equation 1 and especially the interaction parameter R were discussed by Fujita (Reference 1), Casassa (Reference 2), Gehatia and Wiff (Reference 3), and others.

By differentiating Equation 1 with respect to x one obtains:

$$\frac{dc}{dx} = \left(\hbar \omega^2 - R \frac{dc}{dx} \right) c \quad (2)$$

which leads to the following working formulas:

$$c^{-1} \frac{dc}{dx} = \hbar \omega^2 - R \frac{dc}{dx} \quad (3)$$

$$c^{-1} = \hbar \omega^2 \left(\frac{dc}{dx} \right)^{-1} - R \quad (4)$$

A plot of $c^{-1} \frac{dc}{dx}$ vs. $\frac{dc}{dx}$, according to Equation 3, should give a straight line with a slope equal to $(-R)$. Similarly, according to Equation 4, a plot of c^{-1} vs. $\left(\frac{dc}{dx} \right)^{-1}$ gives a slope equal to $\hbar \omega^2$, which is a quantity proportional to the molecular weight (References 3 and 4).

By knowing $\hbar \omega^2$ and R one can evaluate the constant g from Equation 1 and thereby fully characterize the system under consideration.

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SYSTEM OF TWO DISTINCT INTERACTING FRACTIONS

Consider a solution of polymer comprised of two interacting fractions (1 and 2). The concentration can be expressed as:

$$c = c_1 + c_2 \quad (5)$$

where:

$$c_1 = g_1 e^{h_1 \omega^2 x} - R_{1,1} c_1 - R_{1,2} c_2 \quad (6)$$

and:

$$c_2 = g_2 e^{h_2 \omega^2 x} - R_{2,1} c_1 - R_{2,2} c_2 \quad (7)$$

It has been assumed that in a certain region ($m \leq x \leq x^*$) the fraction 1 prevails, e.g., that $c_1 \approx c$ and $c_2 \ll c_1$. Since $c_1 = c - c_2$ the exponent in Equation 6 can be modified:

$$-R_{1,1} c_1 - R_{1,2} c_2 = -R_{1,1} c - (R_{1,2} - R_{1,1}) c_2 \quad (8)$$

and Equation 5 can be approximated by the formula:

$$c \approx g_1 e^{h_1 \omega^2 x} - R_{1,1} c \left[1 - (R_{1,2} - R_{1,1}) c_2 \right] + c_2 \quad (9)$$

Denote:

$$g_1 e^{h_1 \omega^2 x} - R_{1,1} c = G_1 \quad (10)$$

and:

$$R_{1,2} - R_{1,1} = K_m \quad (11)$$

Equation 9 will now lead to the following expression for c_2 :

$$\frac{c - G_1}{1 - K_m G_1} \approx c_2 \quad (12)$$

The approximation is justified if the quantity $K_m c_2 \ll 1$, e.g., if, for a certain $x > x^*$, c_2 is not negligible in comparison to be c , but is still small enough to make the following transformation valid:

$$e^{-K_m c_2} \approx 1 - K_m c_2 \quad (13)$$

For a known value of K_m one can evaluate the c_2 curve in a region in which $K_m c_2 \ll 1$. According to Fujita (Reference 1),

$$R_{1,2} = M_1 f_{1,2} \quad (14)$$

and:

$$R_{2,1} = M_2 f_{2,1} \quad (15)$$

where f_{12} and f_{21} are the cross coefficients of interaction and:

$$f_{1,2} = f_{2,1} \quad (16)$$

Using this assumption of a symmetric interaction one obtains:

$$R_{2,1} = R_{1,2} \left(\frac{M_2}{M_1} \right) = R_{1,2} \left(\frac{h_2 \omega^2}{h_1 \omega^2} \right) \quad (17)$$

By inserting this expression for $R_{2,1}$ into Equation 7 one obtains the following formula:

$$\ln c_2 = \ln g_2 - \frac{h_2 \omega^2}{h_1 \omega^2} R_{1,2} c + \left[\frac{h_2 \omega^2}{h_1 \omega^2} R_{1,2} - R_{2,2} \right] c_2 \quad (18)$$

Equation 18 is an expression for c_2 with three unknown parameters; $\ln g_2$, $(h_1 \omega^2/h_2 \omega^2) R_{1,2} = a$, and $\left[(h_2 \omega^2/h_1 \omega^2) R_{1,2} - R_{2,2} \right] = b$

For a large number of c values one can determine the parameters in Equation 18 as well as the total error of the system. In this calculation a measure of the error was taken as:

$$\Delta_m^2 = \sum_i \delta_{m,i}^2 \quad , \quad (19)$$

where:

$$\delta_{m,i} = \ln(c_2)_{m,i} - \ln(g_2)_m + a_m(c)_i + b_m(c_2)_{m,i} \quad (20)$$

One must remember that such a treatment was originally suggested for the case when K_m is a known quantity. In a real case such a value is not known, a priori. However, the following procedure can be applied. A set of values can be assumed for K_m and accordingly Δ_m^2 can be evaluated. The "best fit," e.g.,

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the minimum of a plot Δ_m^2 vs. K_m , gives an acceptable value for K_m . In such a case the values of K_m as well as other parameters, are determined. These parameters finally lead to evaluation of the following constants: M_1 , M_2 , g_1 , g_2 , $R_{1,1}$, $R_{1,2}$, $R_{2,1}$, and $R_{2,2}$, which fully describe the system comprised of two interacting fractions (Figures 16 and 17).

The search for appropriate K_m values can be accomplished by use of a high speed computer. In case of a few fractions one can find more than one distinct K_m value, i.e., $\{K_{m,n}\}$; with the corresponding set M_n , g_n , R_{1n} , R_{ni} , and R_{nn} . If there are too many fractions in the system $K_{m,n}$ values cannot be distinguished by searching, and "noise" is created.

In case of two fractions, and if all parameters of the transcendental equation, Equation 7, are known, c_2 can be precisely evaluated for all values of x without need of an approximation.

SECTION III

EXPERIMENTAL

Bulk PBI was dissolved in DMAC and fractionated with hexane. The fractions were purified in the following manner. Each sample was redissolved in DMAC, precipitated and washed with methyl ethyl ketone (MEK), filtered and washed again with MEK. The process of washing was continued; however, MEK was replaced by mixtures of MEK-MEOH with successively decreasing amounts of MEK. The polymer was further washed with pure methanol and replaced by mixtures of MEOH-ether with successively decreasing amounts of MEOH. Finally, the remaining polymer was washed with ether and dried under vacuum (this method of purification and fractionation was suggested by T. E. Helminiak).

A set of sedimentation equilibrium experiments was carried out with four samples of PBI in DMAC at 40°C. An aluminum, 12mm, 4°, single sector cell containing the solution and another similar cell with DMAC were inserted into a J-rotor. The resulting Schlieren curves appeared, therefore, with a base line in addition to the sedimentation curve (Figures 2-8).

Each sample was measured at different rotor speeds. It required about 14-17 days to achieve the first equilibrium. If the speed was decreased the next equilibrium could be achieved within 7-10 days. However, it took only a few days to achieve equilibrium when the speed was increased rather than decreased. This surprising behavior, which contradicts theoretical considerations and expectations, has not yet been explained. In several cases no equilibrium was achieved as the speed was lowered and the Schlieren curve dissipated.

The quantity $\frac{dc}{dn}$ has been determined from auxiliary velocity runs carried out with a synthetic boundary cell.

Finally the plates were enlarged and the coordinates $\frac{dn}{dr}$ and Δr were measured.

SECTION IV

COMPUTATION

The experimental data was analyzed by applying Equations 3 and 4. (Figures 2-16 and Tables I-XI). As one can readily see no linear plots have been obtained. Therefore, the samples under consideration are not homogenous. On the other hand, one can also observe that these plots clearly show a straight line in a zone close to the meniscus ($m \leq x \leq x^*$, where x^* is a special value different for each sample and speed). Only sample three led to a straight line over all values of x .

Such a peculiarity of the plot can be explained by assuming the existence of a distinct low molecular weight fraction. This, as well as other considerations, suggests that there exists a very pauci-disperse system, i.e., that each sample is comprised of a few fractions (as a matter of fact, 2, 3, or 4 fractions). In addition, the low molecular weight fraction is very distinct in a certain zone near the meniscus, $c_{\text{total}} \approx c_1$ and $c_{n \neq 1} \ll c_1$.

The results of applying a method based upon these considerations to the four samples is summarized in Table XII. An equilibrium sedimentation experiment was made at each speed indicated. The first fraction parameters (g_1 , M_1 , and $R_{1,1}$) were evaluated by the procedure outlined above. The other parameters (g_m , M_m , R_{mm} , and R_{1m}) were determined by finding minima as indicated in Figure 22. All minima corresponding to fractions within a sample are indicated in Table XII.

SECTION V

DISCUSSION OF RESULTS

The computation just described cannot be considered as completed. In the case of four fractions:

$$c_n = g_n \exp(h_n \omega^2 - R_{n1} c_1 - R_{n2} c_2 - R_{n3} c_3 - R_{n4} c_4) \quad (21)$$

each curve can be evaluated within a zone, where $K_m c_m \ll 1$, and the corresponding parameters can be determined within such a zone.

However, an assumption has been made, according to Fujita (Reference 1), that:

$$\frac{R_{nk}}{M_n} = \frac{R_{kn}}{M_k} \quad (22)$$

which is not readily apparent (Reference 2). Without using the relationship described in Equation 22, the cross-coefficients R_{kn} ($k \neq 1$) cannot be easily evaluated.

The parameters $h_1 \omega^2$ and $R_{1,1}$ were determined from the linear portion of original plots. However, such an evaluation may introduce a numerical error which exceeds the tolerances required by the $K_{m,n}$, $\Delta_{m,n}$ analysis. Therefore, a variance in the values of $h_1 \omega^2$ and $R_{1,1}$ has to be taken into account to better fit the system.

Finally, the analysis has been performed by comparing the lowest fraction of a given sample with the other fractions in the sample. The results of applying this analysis to four samples is given in Table XII. Samples 1, 2, and 4 show that they are composed of about four sub-fractions. These sub-fractions have molecular weights of approximately 1,500; 30,000; 60,000; and 120,000. One sample, namely number 3, appears to have a very narrow distribution. Its weight average molecular weight is about 4,500.

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It is also significant that the diagonal elements (R_{mm}) of the "interaction" matrix were all found to be negative. Only values for R_{1m} are given in Table XII, since no proper method was applied to determine the off-diagonal elements R_{nk} for $n \neq 1$.

It has been suggested that some of the molecular weights indicated (Table XII) by this experimental analysis are higher than would be expected from condensation polymerization. Therefore, further investigations must be initiated for better examination of the system. Also, additional work will be required to more fully evaluate the validity of this method and to make necessary modifications to include in the calculation of all R_{nk} parameters.

SECTION VI

COMPUTER PROGRAM

COMPUTER SYMBOL IDENTIFICATION

Following is a list of symbols used in the computer program. Where possible the symbols are identified with the previously derived theory. One must remember that the computer program was written only for the case of two major distinct molecular weight components.

REC \varnothing RD - Used as "flag" for subroutine calling order.

PNAME1 and **PNAME2** - Identification of experiment.

NMAX - Number of data points read into machine.

CO - Initial concentration of experimental solution.

R1 - First radial value. The distance from the center of rotation in the meniscus.

DLR - Incremented value for radial distances. Radial distance to the bottom of cell is given by $R1 + (NMAX-1)*DLR$.

R(I) - Array of radial values

X(I) - Array $R(I)^{**2}$

CR(I) - Array containing experimentally measured ordinates from Schlieren Curves. Once these are read they are multiplied by **SCALE** to obtain the true $\frac{dc}{dr}$ values.

CX(I) - Array $(1/2r) \left(\frac{dc}{dr} \right)$

C(I) - Array of concentrations obtained from $\int_m^x \frac{dc}{dx} dx = c - c_m$. Then use is made of the equation $\int_m^b c dx = c^o(b-m)$ to calculate c_m , the concentration at the meniscus.

ZLC(I) - Array $\ln(C(I))$

CX \varnothing VX(I) - Array $(dc/dx)/C$

XCX(I) - Array $(dc/dx)^{-1}$

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 $XC(I) - \text{Array } (C^{-1})$ $NMAX1 - \text{First point at which } c_2 \text{ is small but must be considered.}$ $NMAX2 - \text{Highest point at which } c_2 \text{ is small but not zero.}$ $DLK = R_{1,1} + R_{1,2}$ $DKMAX - \text{Maximum value of DLK.}$ $XDLK - \text{Increment value for DLK.}$ $G(I) - \text{Array } \{ g_1 e^{h_1 \omega^2 x} - R_{11} c \}$ $H10MSQ = h_1 \omega^2$ $R11 = R_{1,1}$ $G1 = g_1$ $Y(I,J) - \text{Array containing three consecutive sets of values (three successive DLK values) for } YN(I).$ $YN(I) = (C(I) - G(I))/(1 - DLK * G(I))$ $U(I) - \text{Array } (X - (R_{12}/h_1 \omega^2) * c)$ $IY(I,J) - \text{Array containing the values of NMAX1 and NMAX2 corresponding to the array } Y(I,J).$ $Z(I) - \text{Array } \ln C_2(I)$ $R22 = R_{2,2}$ $R12 = R_{1,2} = DLK = R_{1,1}$ $G2 = g_2$ $H20MSQ = h_2 \omega^2$ $XLNG2 = \ln(g_2)$ $XN - \text{Number of data points sampled (NMAX2-NMAX1 + 1)}$

$$\begin{aligned} \text{DELTA} = & \frac{1}{XN} \sum_{i=NMAX1}^{NMAX2} \left\{ \ln c_2(x_i) - \left[\ln g_2 + h_2 \omega^2(x_i) - \frac{R_{1,2}}{h_1 \omega^2} c(x_i) \right] \right. \\ & \left. + \frac{R_{1,2}}{h_1 \omega^2} - R_{2,2} c_2(x_i) \right\}^2 \end{aligned}$$

The flow of computer data is shown in Figure 1.

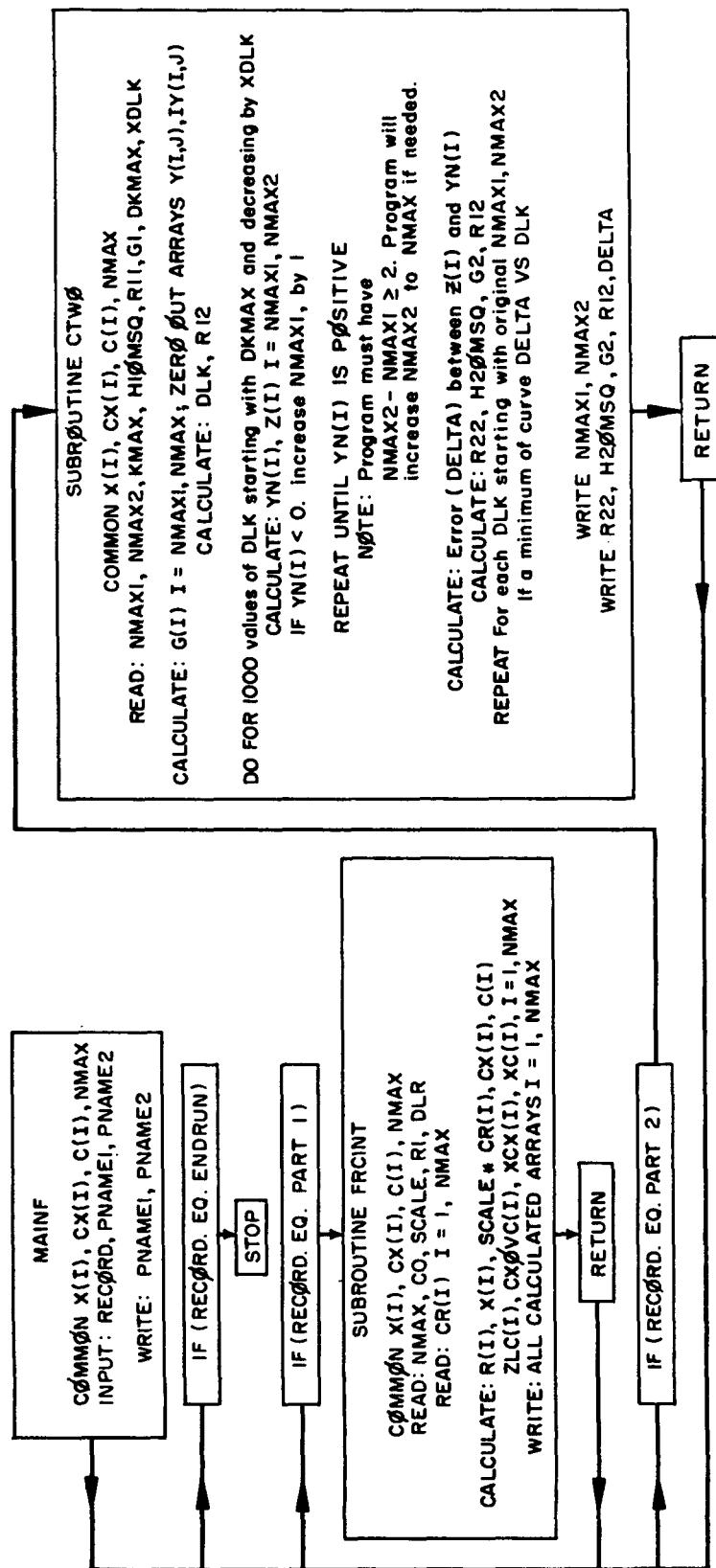


Figure 1. Computer Data Flow Diagram

COMPUTER PRINTOUT

```
$IBFTC MAINF DECK
COMMON X,CX,C,NMAX
C   DIMENSIONS FOR COMMON
DIMENSION X(100),CX(100),C(100)
DATA P1,P2,P3/6HPART 1,6HENDRUN,6H
DATA P4/6HPART 2/
1 READ(5,101) RECORD,PNAME1,PNAME2
101 FORMAT(A6,4X,2A6)
    IF(RECORD = P1) 2,10,2
    2 IF(RECORD = P2) 3,89,3
    3 IF(RECORD = P4) 4,11,4
    4 IF(RECORD = P3) 99,1,99
10 WRITE(6,1000)
1000 FORMAT(1H1/1HA)
    WRITE(6,2000) PNAME1,PNAME2
2000 FORMAT(1H ,50X,25HIDENTIFICATION NUMBER IS ,2A6)
    CALL FRCINT
    WRITE(6,1001)
1001 FORMAT(1HA/1HA)
    GO TO 1
11 WRITE(6,1000)
    WRITE(6,2000) PNAME1,PNAME2
    CALL CTWO
    WRITE(6,1001)
    GO TO 1
99 WRITE(6,3000) RECORD
3000 FORMAT(1H ,36HWWHAT DO WE DO WITH THE CARD LABELED ,A6)
    GO TO 1
89 WRITE(6,1000)
    WRITE(6,7000)
7000 FORMAT(8(1H END OF RUN,3X)/1H1)
    STOP
    END
```

COMPUTER PRINTOUT (CONT)

```

$IBFTC FRCIN DECK
    SUBROUTINE FRCINT
    COMMON X,CX,C,NMAX
C    DIMENSIONS FOR COMMON
    DIMENSION X(100),CX(100),C(100)
    DIMENSION CR(100),R(100),ZLC(100),CXOVC(100),XLX(100),XL(100)
    READ(5,101) NMAX,CO,SCALE,R1,DLR
101 FORMAT(13,1P2E11.4,0PF10.5,0PF10.6)
100 FORMAT(A6)
    READ(5,102) (CR(I),I = 1,NMAX)
102 FORMAT(16F5.0)
    DO 1 I = 1,NMAX
    R(I) = R1 + FLOAT(I-1)*DLR
    X(I) = R(I)**2
    CR(I) = SCALE*CR(I)
    CX(I) = CR(I)/(2.*R(I))
1 CONTINUE
    A = 0.
    COEF = 0.
    DO 2 I = 1,NMAX
    IF(I.EQ.1) GO TO 2
    DLX = X(I) - X(I-1)
    AVGCX = (CX(I)+CX(I-1))/2.
    COEF = COEF + DLX*AVGCX
    AC = (COEF + C(I-1))/2.
    A = A + DLX*AC
2 C(I) = COEF
    DIFBM = X(NMAX) - X(1)
    CM = (DIFBM*CO - A)/DIFBM
    WRITE(6,2000) CO,DIFBM,CM
2000 FORMAT(1H ,33HTHE CONCENTRATION FOR THIS RUN = ,E11.4/43H DIFFEREN
    1CF BTWN SQS OF BTM AND MENISCUS = ,E15.8/21H CONC. AT MENISCUS = ,
    2E11.4///)
    DO 3 I = 1,NMAX
    C(I) = C(I) + CM
    ZLC(I) = 0.
    IF(C(I).LE.0.) GO TO 3
    ZLC(I) = ALOG(C(I))
    CXOVC(I) = CX(I)/C(I)
    XCX(I) = 1./CX(I)
    XC(I) = 1./C(I)
3 CONTINUE
    WRITE(6,2001)
2001 FORMAT(1H ,1X,1HI,9X,1HR,11X,1HX,11X,2HCR,1CX,2HCX,10X,IHC,9X,5HLN
    1(C),7X,4HCX/C,8X,4H1/CX,8X,3H1/C//)
    DO 4 I = 1,NMAX
4 WRITE(6,2002) I,R(I),X(I),CR(I),CX(I),C(I),ZLC(I),CXOVC(I),XCX(I),
    1XC(I)
2002 FORMAT(1H ,I2,5X,9(1PE11.4,1X))
    RETURN
    END

```

COMPUTER PRINTOUT (CONT)

```

$IBFTC CTAU DECK
SUBROUTINE CTWO
COMMON X,CX,C,NMAX
C DIMENSIONS FOR COMMON
DIMENSION X(100),CX(100),C(100)
DIMENSION G(100),YN(100),U(100),Z(100)
READ(5,100) NMAX1,NMAX2,KMAX,H1OMSQ,R11,G1,DKMAX,XDLK
100 FORMAT(3I3,3F10.3,F15.8,F10.6)
DO 1 I = NMAX1,NMAX
A1 = H1OMSQ*X(I) - R11*C(I)
A2 = EXP(A1)
1 G(I) = G1*A2
DO 2 K = 1,KMAX
K1 = NMAX1
K2 = NMAX2
DLK = DKMAX + XDLK*FLOAT(K-1)
WRITE(6,1001) DLK
1001 FORMAT(1H ,8HX,5HKN = ,F10.5)
R12 = R11 - DLK
98 CONTINUE
WRITE(6,2000) NMAX1,NMAX2
2000 FORMAT(1H ,8HNMAX1 = ,I2,9H NMAX2 = ,I2)
DO 3 I = NMAX1,NMAX2
A1 = C(I) - G(I)
A2 = 1. + DLK*G(I)
YN(I) = A1/A2
IF(I.EQ.NMAX1) GO TO 20
GO TO 21
20 A3 = X(I) - R12*C(I)/H1OMSQ
XN1 = A3 - 1.
21 CONTINUE
U(I) = X(I) - (R12*C(I)/H1OMSQ) - XN1
XXN = 1.
IF(YN(I).LT.0.1E-05) GO TO 99
IF(I.EQ.NMAX1) GO TO 22
GO TO 23
22 A3 = ALOG(YN(I))
XN2 = ABS(A3) - 1.
23 CONTINUE
Z(I) = ALOG(YN(I)) + XN2
3 CONTINUE
A1 = 0.
A2 = 0.
A3 = 0.
A4 = 0.
A5 = 0.
A6 = 0.
A7 = 0.
A8 = 0.
XN = FLOAT(NMAX2 - NMAX1 + 1)
DO 4 I = NMAX1,NMAX2
A1 = A1 + 0.1*U(I)
A2 = A2 + (0.1*U(I))**2
A3 = A3 + 100.*YN(I)

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COMPUTER PRINTOUT (CONT)

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A4 = A4 + (100.*YN(I))**2
A5 = A5 + Z(I)
A6 = A6 + 10.*U(I)*YN(I)
A7 = A7 + 0.1*U(I)*Z(I)
4 A8 = A8 + 100.*YN(I)*Z(I)
B1 = A2*A4 - A6*A6
B2 = A1*A4 - A3*A6
B3 = A2*A3 - A1*A6
DENOM = XN*B1 - A1*B2 - A3*B3
ANUM = A5*B1 - A7*B2 - A8*B3
B1 = A7*A4 - A8*A6
B2 = A5*A4 - A3*A8
B3 = A3*A7 - A5*A6
BNUM = XN*B1 - A1*B2 - A3*B3
P1 = A7*A6 - A2*A8
B2 = A5*A6 - A1*A8
B3 = A1*A7 - A5*A2
CNUM = XN*B1 - A1*B2 - A3*B3
H2OMSQ = 0.1*(BNUM/DENOM)
B = 100.*(CNUM/DENOM)
R22 = B + R12*H2OMSQ/H10MSQ
XK = CNUM/DENOM
XLNG2 = XK - XN1*H2OMSQ - XN2
WRITE(6,3001) DENOM,ANUM,BNUM,CNUM,R22,H2OMSQ,XLNG2
3001 FORMAT(1H ,7(1X,E15.8,1X))
IF(ABS(XLNG2).GT.88.) GO TO 40
G2 = EXP(XLNG2)
GO TO 41
40 G2 = 0.
41 CONTINUE
COEF = 0.
DO 5 I = NMAX1,NMAX2
B1 = XK
B2 = H2OMSQ*U(I)
B3 = B*YN(I)
5 COEF = COEF + (Z(I)-B1-B2+B3)**2
DELTA = COEF/XN
IF(H2OMSQ.LT.0.) GO TO 32
WRITE(6,1000) K,R12,G2,H2OMSQ,R22,DELTA
1000 FORMAT(1H ,5X,I2,7H R12 = ,1PE10.3,6H G2 = ,1PE10.3,10H H2OMSQ = ,
11PE10.3,7H R22 = ,1PE10.3,9H DELTA = ,1PE10.3/)
32 CONTINUE
NMAX1 = K1
NMAX2 = K2
GO TO 2
92 CONTINUE
NMAX1 = NMAX1 + 1
IF((NMAX2-NMAX1).GT.2) GO TO 97
NMAX2 = NMAX2 + 1
IF(NMAX2.EQ.NMAX) GO TO 88
97 GO TO 98
2 CONTINUE
88 RETURN
END

```

SECTION VII

REFERENCES

1. H. Fujita, "Mathematical Theory of Sedimentation Analysis," Academic Press, New York, 1962.
2. E. F. Casassa, "Sedimentation Equilibrium in Multicomponent Solutions," (Private Communication).
3. M. Gehatia and D. R. Wiff, AFML-TR-67-121, Part II.
4. M. Gehatia, AFML-TR-67-121, Part I.

TABLE I

EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 10,589 RPM
(See Figure 2a)

THE CONCENTRATION FOR THIS RUN = 1.1394×10^{-6}
DIFFERENCE BTWN SOS OF BTW AND MENSCUS = $0.93875737 \times 10^{-6}$
CONE. AT MENISCUS = 1.10846×10^{-6}

Identification Number is Sample 1 10,589 RPM

T	R	X	C _R	CX	C	C _{N(C)}	CX/C	1/CX	1/C
1	6.5295E-00	4.2634E-01	3.9547E-02	2.9519E-03	1.0837E-01	-2.2222E-00	2.7237E-02	3.3878E-02	9.2272E-00
2	6.5413E-00	4.2798E-01	3.9548E-02	2.9519E-03	1.0838E-01	-2.2179E-00	2.7785E-02	3.3069E-02	9.1882E-00
3	6.5531E-00	4.2964E-01	4.0575E-02	3.0960E-03	1.0931E-01	-2.2136E-00	2.8324E-02	3.2309E-02	9.1486E-00
4	6.5649E-00	4.3170E-01	4.1692E-02	3.1754E-03	1.0979E-01	-2.2092E-00	2.8922E-02	3.1492E-02	9.1082E-00
5	6.5766E-00	4.3252E-01	4.2809E-02	3.2345E-03	1.1229E-01	-2.2047E-00	2.9509E-02	3.0766E-02	9.0671E-00
6	6.5884E-00	4.3427E-01	4.3924E-02	3.3334E-03	1.1080E-01	-2.2000E-00	3.0085E-02	2.9999E-02	9.0253E-00
7	6.6002E-00	4.3552E-01	4.5454E-02	3.4427E-03	1.1133E-01	-2.1953E-00	3.0925E-02	2.9047E-02	8.9826E-00
8	6.6119E-00	4.3719E-01	4.6865E-02	3.5440E-03	1.1187E-01	-2.1904E-00	3.1680E-02	2.8217E-02	8.9390E-00
9	6.6237E-00	4.3874E-01	4.8614E-02	3.6854E-03	1.2434E-01	-2.1854E-00	3.2691E-02	2.7207E-02	8.8942E-00
10	6.6355E-00	4.4033E-01	5.0213E-02	3.7836E-03	1.3101E-01	-2.1802E-00	3.3479E-02	2.6430E-02	8.8484E-00
11	6.6473E-00	4.4186E-01	5.1937E-02	3.9677E-03	1.3626E-01	-2.1749E-00	3.4385E-02	2.5559E-02	8.8016E-00
12	6.6591E-00	4.4343E-01	6.0445E-02	4.0445E-03	1.4695E-01	-2.1244E-01	3.4030E-02	2.4725E-02	8.7536E-00
13	6.6709E-00	4.4501E-01	5.5935E-02	4.1894E-03	1.4898E-01	-2.1638E-01	3.6466E-02	2.3879E-02	8.7043E-00
14	6.6926E-00	4.4655E-01	5.9124E-02	4.3141E-03	1.1556E-01	-2.1580E-01	3.7569E-02	2.3034E-02	8.6538E-00
15	6.6944E-00	4.4815E-01	6.3357E-02	4.5080E-03	1.1625E-01	-2.1520E-01	3.8777E-02	2.2183E-02	8.6019E-00
16	6.7162E-00	4.4973E-01	6.6597E-02	4.6740E-03	1.1698E-01	-2.1458E-01	3.9157E-02	2.1395E-02	8.5486E-00
17	6.7179E-00	4.5131E-01	6.5023E-02	4.8395E-03	1.1773E-01	-2.1394E-01	4.1107E-02	2.0663E-02	8.4940E-00
18	6.7297E-00	4.5289E-01	6.7557E-02	5.0277E-03	1.1851E-01	-2.1327E-01	4.2418E-02	1.9893E-02	8.4380E-00
19	6.7415E-00	4.5454E-01	7.3399E-02	5.2213E-03	1.1932E-01	-2.1259E-01	4.3757E-02	1.9152E-02	8.3805E-00
20	6.7533E-00	4.5627E-01	7.6137E-02	5.4207E-03	1.2017E-01	-2.1189E-01	4.4999E-02	1.8493E-02	8.3216E-00
21	6.7551E-00	4.5795E-01	7.6292E-02	5.6230E-03	1.2105E-01	-2.1116E-01	4.6453E-02	1.7784E-02	8.2612E-00
22	6.7769E-00	4.5955E-01	7.9322E-02	5.8303E-03	1.2196E-01	-2.1041E-01	4.7805E-02	1.7152E-02	8.1993E-00
23	6.7936E-00	4.6158E-01	8.2165E-02	6.0518E-03	1.2291E-01	-2.0963E-01	4.9237E-02	1.6552E-02	8.1360E-00
24	6.8044E-00	4.6245E-01	8.2500E-02	6.2550E-03	1.2390E-01	-2.0883E-01	5.0567E-02	1.5962E-02	8.0713E-00
25	6.8122E-00	4.6417E-01	9.8861E-02	6.5223E-03	1.2492E-01	-2.0801E-01	5.2211E-02	1.5332E-02	8.0051E-00
26	6.8230E-00	4.6556E-01	9.2112E-02	6.7537E-03	1.2599E-01	-2.0716E-01	5.3685E-02	1.4785E-02	7.9373E-00
27	6.8357E-00	4.6727E-01	9.6267E-02	7.0414E-03	1.2626E-01	-2.0716E-01	5.5201E-02	1.4202E-02	7.8679E-00
28	6.8475E-00	4.6885E-01	1.0.0122E-01	7.3182E-03	1.2826E-01	-2.0537E-01	5.7060E-02	1.36665E-02	7.7969E-00
29	6.8593E-00	4.7052E-01	1.0.2946E-01	7.5866E-03	1.2946E-01	-2.0444E-01	5.8603E-02	1.3181E-02	7.7455E-00
30	6.8711E-00	4.7211E-01	1.0.5915E-01	7.8936E-03	1.3071E-01	-2.0348E-01	6.0314E-02	1.2685E-02	7.6506E-00
31	6.8929E-00	4.8193E-01	1.0.3613E-01	9.8054E-03	1.3201E-01	-2.0242E-01	6.2520E-02	1.2225E-02	7.5752E-00
32	6.9146E-00	4.7536E-01	1.0.1695E-01	8.4744E-03	1.3316E-01	-2.0147E-01	6.3546E-02	1.1800E-02	7.4984E-00
33	6.9354E-00	4.7698E-01	1.0.2142E-01	8.7937E-03	1.3476E-01	-2.0042E-01	6.5230E-02	1.1376E-02	7.4203E-00
34	6.9187E-00	4.7861E-01	1.0.2599E-01	9.1256E-03	1.3622E-01	-1.9935E-01	6.6844E-02	1.0982E-02	7.3410E-00
35	6.9330E-00	4.8074E-01	1.0.3946E-01	1.0.3735E-01	1.3735E-01	-1.9924E-01	6.8044E-02	1.0592E-02	7.2603E-00
36	6.9417E-00	4.8243E-01	1.0.4154E-01	1.0.3934E-01	1.3915E-01	-1.9911E-01	6.9387E-02	1.0198E-02	7.1784E-00
37	6.9555E-00	4.8351E-01	1.0.4254E-01	1.0.4254E-01	1.4254E-01	-1.9901E-01	7.0453E-02	1.0571E-02	7.0950E-00
38	6.9664E-00	4.8515E-01	1.0.4745E-01	1.0.6175E-01	1.4745E-01	-1.9473E-01	7.4253E-02	9.7926E-01	6.6651E-00
39	6.9771E-00	4.8679E-01	1.0.5499E-01	1.0.7129E-01	1.4443E-01	-1.9350E-01	7.4425E-02	9.4189E-01	7.0101E-00
40	6.9880E-00	4.8844E-01	1.0.5354E-01	1.0.4161E-01	1.4028E-01	-1.9223E-01	7.9043E-02	9.0625E-02	6.9238E-00
41	7.0007E-00	4.9074E-01	1.0.5465E-01	1.0.4154E-01	1.4028E-01	-1.9223E-01	8.0592E-02	8.3664E-02	6.8364E-00
42	7.0124E-00	4.7174E-01	1.0.498E-01	1.0.3613E-01	1.3915E-01	-1.9111E-01	8.0198E-02	8.0198E-02	6.6571E-00
43	7.0142E-00	4.9339E-01	1.0.4224E-01	1.0.2121E-01	1.3250E-01	-1.8818E-01	8.5329E-02	7.6938E-01	6.6651E-00
44	7.0364E-00	4.9555E-01	1.0.911E-01	1.0.3567E-01	1.5432E-01	-1.8674E-01	8.7799E-02	7.3713E-01	6.4716E-00
45	7.0477E-00	4.9671E-01	1.0.934E-01	1.0.4177E-01	1.5622E-01	-1.8526E-01	9.0650E-02	8.0353E-01	6.3167E-00
46	7.0555E-00	4.9874E-01	1.0.9745E-01	1.0.4719E-01	1.4825E-01	-1.8092E-01	8.6664E-02	8.3661E-01	6.7476E-00
47	7.0713E-00	5.0033E-01	1.0.9874E-01	1.0.4259E-01	1.5022E-01	-1.8011E-01	8.3011E-02	8.0198E-02	6.6571E-00
48	7.0831E-00	5.0171E-01	2.0.2975E-01	1.0.6175E-01	1.6175E-01	-1.8217E-01	9.5783E-02	6.4545E-01	6.8824E-00
49	7.0945E-00	5.0337E-01	2.0.1717E-01	1.0.6439E-01	1.6439E-01	-1.8055E-01	9.8666E-02	6.1656E-01	6.0830E-00
50	7.1044E-00	2.0.4143E-01	1.0.7014E-01	1.0.6717E-01	1.6717E-01	-1.7888E-01	1.0178E-01	5.8774E-01	5.9820E-00

TABLE I (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1266E-00	5.0534E-01	2.5363E-01	1.7843E-C2	1.7008E-01	-1.7715E-00	1.0490E-01	5.6046E-01	5.8795E-00
51	7.1184E-00	5.2672E-01	2.6374E-01	1.8526E-C2	1.7313E-01	-1.7537E-00	1.0700E-01	5.3980E-01	5.7760E-00
52	7.11302E-00	5.0839E-01	2.7997E-01	1.9633E-C2	1.7633E-01	-1.7354E-00	1.1134E-01	5.0934E-01	5.6711E-00
53	7.1420E-00	5.1018E-01	2.9615E-01	2.06666E-02	1.7972E-01	-1.7164E-00	1.1499E-01	4.8389E-01	5.5642E-00
54	7.1537E-00	5.1176E-01	3.1955E-01	2.2334E-02	1.8334E-01	-1.664E-00	1.2182E-01	4.4776E-01	5.4544E-00
55	7.1655E-00	5.1345E-01	3.4997E-01	2.4420E-02	1.8728E-01	-1.6751E-00	1.3039E-01	4.0950E-01	5.3396E-00
56	7.1773E-00	5.1513E-01	3.8547E-01	2.6854E-02	1.9161E-01	-1.623E-00	1.4015E-01	3.7239E-01	5.2189E-00
57	7.1891E-00	5.1683E-01	4.5644E-01	3.1748E-02	1.9657E-01	-1.6267E-00	1.6151E-01	3.1498E-01	5.0372E-00
58	7.2020E-00	5.1852E-01	5.4270E-01	3.7683E-02	2.0245E-01	-1.572E-00	1.8613E-01	2.6537E-01	4.9394E-00
59	7.2126E-00	5.2022E-01	8.3691E-01	5.8156E-02	2.1059E-01	-1.5578E-00	2.7616E-01	1.7195E-01	4.7486E-00

TABLE II
EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 8,766 RPM
(See Figure 2b)

THE CONCENTRATION FOR THIS RUN = 3.1394×10^{-6}
DIFFERENCE Q_{TW} SOS OF RT4 AND MENISCUS = $0.93875737 \times 10^{-1}$
CONC. AT MENISCUS = 2.1152×10^{-6}

Ratification Number is Sample 1 8,766 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.5295E-10	4.2634E-01	3.2461E-02	2.4857E-03	1.1523E-01	-2.1608E-00	2.1572E-02	4.0230E-02	8.6783E-00
2	6.5413E-10	3.3475E-01	2.5590E-02	1.1562E-03	1.1562E-01	-2.1575E-00	2.2131E-02	3.9081E-02	8.6492E-00
3	6.5531E-10	4.2933E-01	3.4492E-02	2.6316E-03	1.1602E-01	-2.1540E-00	2.2682E-02	3.8000E-02	8.6193E-00
4	6.5548E-10	4.3277E-01	3.5524E-02	7.7441E-03	1.1643E-01	-2.1505E-00	2.3225E-02	3.6981E-02	8.5888E-00
5	6.5766E-10	4.3277E-01	3.6519E-02	1.1685E-03	1.1685E-01	-2.1468E-00	2.3759E-02	3.6018E-02	8.5576E-00
6	6.5944E-10	4.3477E-01	3.7533E-02	2.8484E-03	1.1729E-01	-2.1431E-00	2.4285E-02	3.5107E-02	8.5258E-00
7	6.6122E-10	4.3562E-01	3.8547E-02	2.9202E-03	1.1774E-01	-2.1393E-00	2.4802E-02	3.4245E-02	8.4934E-00
8	6.6119E-10	4.3718E-01	3.9066E-02	3.0147E-03	1.1820E-01	-2.1354E-00	2.5505E-02	3.3171E-02	8.6022E-00
9	6.5237E-10	4.3744E-01	3.1083E-02	3.1012E-03	1.1868E-01	-2.1313E-00	2.6132E-02	3.2245E-02	8.4262E-00
10	6.61355E-10	4.4032E-01	4.2625E-02	3.2104E-03	1.1917E-01	-2.1272E-00	2.6939E-02	3.1149E-02	8.3914E-00
11	6.64473E-10	4.4186E-01	4.3924E-02	3.3039E-03	1.1968E-01	-2.1229E-00	2.7606E-02	3.0288E-02	8.3556E-00
12	6.6591E-10	4.4434E-01	4.5649E-02	3.4275E-03	1.2021E-01	-2.1185E-00	2.9173E-02	2.9173E-02	8.390E-00
13	6.5778E-10	4.4575E-01	4.7372E-02	3.5507E-03	1.2075E-01	-2.1140E-00	2.9404E-02	2.8163E-02	8.2812E-00
14	6.5326E-10	4.4657E-01	4.8793E-02	3.6507E-03	1.2132E-01	-2.1093E-00	3.0091E-02	2.7392E-02	8.2426E-00
15	6.6944E-10	4.4815E-01	5.5729E-02	3.7882E-03	1.2191E-01	-2.1045E-00	3.1075E-02	2.6397E-02	8.2030E-00
16	6.7052E-10	4.4937E-01	5.2343E-02	3.9726E-03	1.2251E-01	-2.0995E-00	3.2251E-02	2.5624E-02	8.1623E-00
17	6.7179E-10	4.5111E-01	5.4372E-02	4.0468E-03	1.2314E-01	-2.0944E-00	3.2862E-02	2.4711E-02	8.1207E-00
18	6.7207E-10	4.5294E-01	5.6502E-02	4.1979E-03	1.2380E-01	-2.0891E-00	3.3910E-02	2.3821E-02	8.0778E-00
19	6.7415E-10	4.5448E-01	5.8632E-02	4.3486E-03	1.2447E-01	-2.0837E-00	3.4936E-02	2.2995E-02	8.0338E-00
20	6.7533E-10	4.5675E-01	6.6661E-02	4.4912E-03	1.2518E-01	-2.0780E-00	3.5879E-02	2.2266E-02	7.9888E-00
21	6.7551E-10	6.2791E-01	6.7791E-02	4.6409E-03	1.2590E-01	-2.0722E-00	3.6861E-02	2.1548E-02	7.9426E-00
22	6.7768E-10	4.5252E-01	6.4922E-02	4.7900E-03	1.2666E-01	-2.0663E-00	3.7819E-02	2.0877E-02	7.8955E-00
23	6.7896E-10	4.6085E-01	6.6950E-02	4.9311E-03	1.2743E-01	-2.0602E-00	3.8696E-02	2.0289E-02	7.8473E-00
24	6.8244E-10	4.5448E-01	5.9182E-02	5.3666E-03	1.2823E-01	-2.0539E-00	3.9667E-02	1.9659E-02	7.7983E-00
25	6.8122E-10	4.6464E-01	7.1207E-02	5.2714E-03	1.2906E-01	-2.0474E-00	4.0843E-02	1.8970E-02	7.7481E-00
26	6.8219E-10	4.6566E-01	7.4511E-02	5.4258E-03	1.2992E-01	-2.0408E-00	4.1762E-02	1.8430E-02	7.6969E-00
27	6.8357E-10	4.5727E-01	7.6597E-02	5.6202E-03	1.3034E-01	-2.0340E-00	4.2856E-02	1.7815E-02	7.6447E-00
28	6.8475E-10	4.6884E-01	7.9123E-02	5.7775E-03	1.3173E-01	-2.0279E-00	4.3860E-02	1.7368E-02	7.5915E-00
29	6.8593E-10	4.7050E-01	8.1964E-02	5.9746E-03	1.3268E-01	-2.0198E-00	4.5032E-02	1.6737E-02	7.5372E-00
30	6.8711E-10	4.7211E-01	8.4702E-02	6.1637E-03	1.3366E-01	-2.0125E-00	4.6116E-02	1.6224E-02	7.4818E-00
31	5.8378E-10	4.7373E-01	8.5433E-02	6.3595E-03	1.3467E-01	-2.0049E-00	4.7455E-02	1.5724E-02	7.4255E-00
32	5.8946E-10	4.7536E-01	9.3938E-02	6.5546E-03	1.3572E-01	-1.9972E-00	4.8295E-02	1.5256E-02	7.3682E-00
33	5.9554E-10	4.7639E-01	9.3932E-02	6.7931E-03	1.3680E-01	-1.9992E-00	4.9656E-02	1.4721E-02	7.3097E-00
34	6.0192E-10	4.7861E-01	9.6977E-02	7.0388E-03	1.3793E-01	-1.981CE-01	5.0815E-02	1.4268E-02	7.2536E-00
35	6.9378E-10	4.8244E-01	1.0434E-01	8.5273E-03	1.4554E-01	-1.9273E-00	5.2094E-02	1.3801E-02	7.1899E-00
36	5.9417E-10	4.8198E-01	1.0387E-01	8.1917E-03	1.4919E-01	-1.9175E-00	5.3333E-02	1.3361E-02	7.1279E-00
37	6.9515E-10	4.9313E-01	1.0753F-01	7.7319E-03	1.4154E-01	-1.9552E-00	5.4627E-02	1.2934E-02	7.0652E-00
38	6.9553E-10	4.9515E-01	1.1139E-01	7.9954E-03	1.4283E-01	-1.9461E-00	5.5982E-02	1.2507E-02	7.0015E-00
39	6.9771F-01	4.8617E-01	1.1534E-01	8.2655E-03	1.4416E-01	-1.9368E-00	5.7334E-02	1.2099E-02	6.9366E-00
40	6.9388E-10	4.8844E-01	1.1919E-01	8.5273E-03	1.4554E-01	-1.9273E-00	5.8589E-02	1.1777E-02	6.8708E-00
41	7.0176E-10	4.9047E-01	1.2345E-01	8.9173E-03	1.4697E-01	-1.9175E-00	5.9993E-02	1.1361E-02	6.8040E-00
42	7.0124E-10	4.9174E-01	1.2387E-01	9.1062E-03	1.4729E-01	-1.9075E-00	6.1341E-02	1.0981E-02	6.7362E-00
43	7.0242E-10	4.9313E-01	1.3197F-01	9.3942E-03	1.4998E-01	-1.8972E-00	6.2636E-02	1.0645E-02	6.6675E-00
44	7.0366E-10	4.9515E-01	1.3694E-01	9.7311E-03	1.5156E-01	-1.8867E-00	6.4209E-02	1.0276E-02	6.5979E-00
45	7.04477E-10	4.9671E-01	1.4202F-01	1.0075F-02	1.5321E-01	-1.8760E-00	6.5763E-02	9.5933E-02	6.5271E-00
46	7.0505E-10	4.9817E-01	1.4739E-01	1.0418E-02	1.5485E-01	-1.8649E-00	6.7250E-02	9.5544E-02	6.4554E-00
47	7.0712E-10	5.0226E-01	1.5226E-01	1.0760E-02	1.5667E-01	-1.8536E-00	6.8711E-02	9.2884E-02	6.3827E-00
48	7.0931E-10	5.1767E-01	1.5825E-01	1.1171E-02	1.5850E-01	-1.8420E-00	7.0478E-02	8.9519E-02	6.3091E-00
49	7.0949E-10	5.2337E-01	1.6427E-01	1.1581E-02	1.6040E-01	-1.8301E-00	7.2201E-02	8.6347E-02	6.2344E-00

TABLE II (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1266E-20	5.2574E-01	1.7793E-01	1.2026E-02	1.6237E-01	-1.8178E-00	7.4062E-02	8.3154E-01	6.1586E-00
51	7.1194E-00	5.1672E-01	1.7853E-01	1.2547E-02	1.6443E-01	-1.8051E-00	7.6264E-02	7.9743E-01	6.0815E-00
52	7.1352E-00	5.0839E-01	1.8746E-01	1.3146E-02	1.6659E-01	-1.7922E-00	7.8911E-02	7.6071E-01	6.0028E-00
53	7.1427E-00	5.1098E-01	1.9791E-01	1.3855E-02	1.6886E-01	-1.7787E-00	8.2054E-02	7.2174E-01	5.9222E-00
54	7.1537E-00	5.1117E-01	2.1211E-01	1.4825E-02	1.7127E-01	-1.7645E-00	8.6559E-02	6.7453E-01	5.8387E-00
55	7.1555E-00	5.1345E-01	2.2824E-01	1.5926E-02	1.7387E-01	-1.7493E-00	9.1601E-02	6.2789E-01	5.7516E-00
56	7.1773E-00	5.1513E-01	2.4854E-01	1.7313E-02	1.7667E-01	-1.7335E-00	9.7997E-02	5.7758E-01	5.6602E-00
57	7.1991E-00	5.1683E-01	2.8719E-01	1.9966E-02	1.7983E-01	-1.7158E-00	1.1103E-01	5.0085E-01	5.5609E-00
58	7.2078E-00	5.1852E-01	3.7229E-01	2.5850E-02	1.9371E-01	-1.6944E-00	1.4071E-01	3.8685E-01	5.4434E-00
59	7.2126E-00	5.2022E-01	5.3255E-01	3.6919E-02	1.8904E-01	-1.6658E-00	1.9530E-01	2.7087E-01	5.2900E-00

TABLE III
EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 7,447 RPM
(See Figure 2e)

THE CONCENTRATION FOR THIS RUN = 0.1394E-00
DIFFERENCE BTWN SQS OF RTM AND MENSUS = C.93875737E-01
CNC. AT MENISCUS = C.1200E-07

Identification Number is Sample 1 7,447 RPM

I	R	X	CR	CX	C	L(N(C))	CX/C	1/CX
1	6.5205E-00	4.2634E-01	3.6518E-02	2.7964E-03	1.2000E-01	-2.1203E-00	2.3304E-02	3.5760E-02
2	6.5413E-00	3.6924E-02	2.8224E-03	1.2043E-01	-2.1167E-00	2.3436E-02	3.5431E-02	8.3336E-00
3	6.5531E-00	4.2943E-01	3.7431E-02	2.8560E-03	1.2087E-01	-2.1131E-00	2.3630E-02	3.5014E-02
4	6.5644E-00	4.3097E-01	3.7937E-02	2.8818E-03	1.2131E-01	-2.1094E-00	2.3756E-02	3.4700E-02
5	6.5766E-00	4.3252E-01	3.8547E-02	2.9306E-03	1.2176E-01	-2.1057E-00	2.4069E-02	3.4122E-02
6	6.5884E-00	4.3407E-01	3.9554E-02	2.9639E-03	1.2222E-01	-2.1020E-00	2.4251E-02	3.3740E-02
7	6.6007E-00	4.3552E-01	3.9562E-02	2.9970E-03	1.2268E-01	-2.0982E-00	2.4430E-02	3.3367E-02
8	6.6119E-00	4.3718E-01	4.0373E-02	3.0530E-03	1.2315E-01	-2.0943E-00	2.4791E-02	3.2754E-02
9	6.6231E-00	4.3874E-01	4.0383E-02	3.1012E-03	1.2363E-01	-2.0905E-00	2.5085E-02	3.2245E-02
10	6.6355E-00	4.4032E-01	4.1692E-02	3.1416E-03	1.2412E-01	-2.0865E-00	2.5311E-02	3.1831E-02
11	6.6473E-00	4.4186E-01	4.2675E-02	3.2047E-03	1.2461E-01	-2.0825E-00	2.5717E-02	3.1204E-02
12	6.6591E-00	4.4343E-01	4.3518E-02	3.2676E-03	1.2512E-01	-2.0785E-00	2.6115E-02	3.0644E-02
13	6.6710E-00	4.4509E-01	4.4431E-02	3.3302E-03	1.2564E-01	-2.0743E-00	2.6506E-02	3.0298E-02
14	6.6826E-00	4.4657E-01	4.5141E-02	3.3775E-03	1.2617E-01	-2.0702E-00	2.6770E-02	2.9608E-02
15	6.6944E-00	4.4815E-01	4.5952E-02	3.4322E-03	1.2670E-01	-2.0659E-00	2.7088E-02	2.9250E-02
16	6.7052E-00	4.4973E-01	4.6764E-02	3.4866E-03	1.2725E-01	-2.0616E-00	2.7400E-02	2.8886E-02
17	6.7170E-00	4.5131E-01	4.7779E-02	3.5580E-03	1.2781E-01	-2.0572E-00	2.7824E-02	2.8211E-02
18	6.7297E-00	4.5289E-01	4.8691E-02	3.6176E-03	1.2837E-01	-2.0528E-00	2.8180E-02	2.7642E-02
19	6.7415E-00	4.5449E-01	4.9706E-02	3.6865E-03	1.2895E-01	-2.0483E-00	2.8588E-02	2.7126E-02
20	6.7533E-00	4.5607E-01	5.0520E-02	3.7552E-03	1.2954E-01	-2.0437E-00	2.8988E-02	2.6630E-02
21	6.7651E-00	4.5766E-01	5.1734E-02	3.8236E-03	1.3015E-01	-2.0391E-00	2.9379E-02	2.6153E-02
22	6.7769E-00	4.5926E-01	5.2749E-02	3.8919E-03	1.3076E-01	-2.0344E-00	2.9763E-02	2.5695E-02
23	6.7885E-00	4.6085E-01	5.3763E-02	3.9598E-03	1.3139E-01	-2.0296E-00	3.0138E-02	2.5154E-02
24	6.8004E-00	4.6245E-01	5.4879E-02	4.0350E-03	1.3203E-01	-2.0247E-00	3.0561E-02	2.4783E-02
25	6.8122E-00	4.6406E-01	5.5995E-02	4.1099E-03	1.3268E-01	-2.0198E-00	3.0975E-02	2.4331E-02
26	6.8240E-00	4.6565E-01	5.7111E-02	4.1846E-03	1.3335E-01	-2.0148E-00	3.1381E-02	2.3897E-02
27	6.8357E-00	4.6727E-01	5.8429E-02	4.2738E-03	1.3407E-01	-2.0097E-00	3.1881E-02	2.3410E-02
28	6.8475E-00	4.6888E-01	5.9748E-02	4.3628E-03	1.3473E-01	-2.0045E-00	3.2383E-02	2.2921E-02
29	6.8593E-00	4.7052E-01	6.0864E-02	4.4366E-03	1.3544E-01	-2.0004E-00	3.2758E-02	2.2540E-02
30	6.8711E-00	4.7211E-01	6.2396E-02	4.5397E-03	1.3616E-01	-1.9939E-00	3.3341E-02	2.2028E-02
31	6.8828E-00	4.7373E-01	6.4124E-02	4.6425E-03	1.3691E-01	-1.9850E-00	3.3910E-02	2.1540E-02
32	6.8946E-00	4.7536E-01	6.5124E-02	4.7228E-03	1.3767E-01	-1.9829E-00	3.4307E-02	2.1174E-02
33	6.9064E-00	4.7698E-01	6.6950E-02	4.8470E-03	1.3847E-01	-1.9793E-00	3.4788E-02	2.0741E-02
34	6.9182E-00	4.7861E-01	6.8675E-02	4.9634E-03	1.3924E-01	-1.9715E-00	3.5264E-02	2.0348E-02
35	6.9300E-00	4.9024E-01	7.0502E-02	5.0940E-03	1.4005E-01	-1.9657E-00	3.6370E-02	1.9631E-02
36	6.9417E-00	4.9189E-01	7.2532E-02	5.2242E-03	1.4090E-01	-1.9597E-00	3.7076E-02	1.9142E-02
37	6.9535E-00	4.9351E-01	7.4650E-02	5.3685E-03	1.4177E-01	-1.9535E-00	3.7867E-02	1.8627E-02
38	6.9653E-00	4.9515E-01	7.6794E-02	5.5372E-03	1.4267E-01	-1.9473E-00	3.8501E-02	1.8131E-02
39	6.9771E-00	4.9679E-01	7.9225E-02	5.6775E-03	1.4353E-01	-1.9408E-00	3.9541E-02	1.7613E-02
40	6.9889E-00	4.9844E-01	8.1852E-02	5.8566E-03	1.4453E-01	-1.9342E-00	4.0521E-02	1.7075E-02
41	7.0007E-00	4.9929E-01	8.4507E-02	6.0351E-03	1.4551E-01	-1.9275E-00	4.1475E-02	1.6570E-02
42	7.0124E-00	4.0174E-01	6.2203E-02	6.2203E-03	1.4653E-01	-1.9206E-00	4.2452E-02	1.6076E-02
43	7.0242E-00	4.9339E-01	8.9774E-02	6.39n6E-03	1.4757E-01	-1.9135E-00	4.3305E-02	1.5649E-02
44	7.0360E-00	4.9505E-01	9.2513E-02	6.5743E-03	1.4864E-01	-1.9062E-00	4.4229E-02	1.5211E-02
45	7.0477E-00	4.9671E-01	9.5354E-02	6.7648E-03	1.4959E-01	-1.8988E-00	4.5175E-02	1.4782E-02
46	7.0595E-00	4.9837E-01	9.8917E-02	6.9691E-03	1.5089E-01	-1.8912E-00	4.6187E-02	1.4349E-02
47	7.0713E-00	5.0033E-01	1.0185E-01	7.2027E-03	1.5207E-01	-1.8834E-00	4.7356E-02	1.3886E-02
48	7.0831E-00	5.1172E-01	7.4472E-03	1.5329E-01	-1.8754E-01	4.8583E-02	1.3428E-02	6.5236E-00
49	7.0942E-00	5.3377E-01	1.0755E-01	7.7209E-03	1.5556E-01	-1.8572E-01	4.9955E-02	1.2952E-02

TABLE III (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1184E-00	5.2554E-01	1.11361E-01	7.9934E-03	1.5587E-01	-1.8587E-00	5.1283E-02	1.2510E-02	6.4156E-00
51	7.1184E-00	5.2672E-01	1.11952E-01	8.3935E-03	1.5724E-01	-1.8500E-00	5.3379E-02	1.1914E-02	6.3596E-00
52	7.1302E-00	5.2839E-01	1.2529E-01	8.7851E-03	1.5868E-01	-1.8408E-00	5.5362E-02	1.1383E-02	6.3018E-00
53	7.1420E-00	5.1023E-01	1.37338E-01	9.2677E-03	1.6020E-01	-1.8313E-00	5.7850E-02	1.0790E-02	6.2421E-00
54	7.1537E-00	5.1176E-01	1.41107E-01	9.9551E-03	1.6181E-01	-1.8213E-00	6.0905E-02	1.0147E-02	6.1800E-00
55	7.1655E-00	5.1345E-01	1.5216E-01	1.0618E-02	1.6354E-01	-1.8107E-00	6.4924E-02	9.4184E-01	6.1148E-00
56	7.1773E-00	5.1513E-01	1.6738E-01	1.1564E-02	1.6542E-01	-1.7993E-00	7.0488E-02	8.5762E-01	6.0452E-00
57	7.1891E-00	5.1693E-01	1.9071E-01	1.3264E-02	1.6153E-01	-1.7866E-00	7.9173E-02	7.5394E-01	5.9692E-00
58	7.2008E-00	5.1862E-01	2.2317E-01	1.5496E-02	1.6997E-01	-1.7722E-00	9.1171E-02	6.4533E-01	5.8836E-00
59	7.2126E-00	5.2022E-01	2.8403E-01	1.9690E-02	1.7295E-01	-1.7547E-00	1.1385E-01	5.0787E-01	5.7820E-00

BEST AVAILABLE COPY

TABLE IV

EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 17,250 RPM

(See Figure 3a)

Identification Number is Sample 2 17,250 RPM

THE CONCENTRATION FOR THIS RUN = 0.673E-01
DIFFERENCE B/W SQS CF B/TM AND MENISCUS = 0.12556299E 02
CONC. AT MENISCUS = 0.2446E-01

I	R	X	CR	CX	C	LN(C)	Cx/C	1/CX	1/C
1	6.2624E 00	3.9218E 01	9.9452E-04	7.9404E-05	2.4463E-02	-3.7106E 00	3.2459E-03	1.2594E 04	4.0879E 01
2	6.2804E 00	3.9438E 01	2.9836E-03	2.3754E-04	2.4498E-02	-3.7092E 00	4.6966E-03	4.2997E 03	4.0820E 01
3	6.2974E 00	3.9660E 01	4.9726E-03	3.5480E-04	2.4568E-02	-3.7063E 00	1.6070E-02	2.2340E-02	4.0704E 01
4	6.3124E 00	3.9882E 01	6.9816E-03	5.4673E-04	2.4673E-02	-3.7021E 00	2.8481E-02	1.8413E 03	4.0531E 01
5	6.3324E 00	4.0105E 01	8.9507E-03	7.0669E-04	2.4813E-02	-3.6964E 00	2.8481E-02	1.4505E 03	4.0302E 01
6	6.3504E 00	4.0328E 01	1.0940E-02	8.6134E-04	2.4988E-02	-3.6894E 00	3.4471E-02	1.1610E 03	4.0020E 01
7	6.3688E 00	4.0552E 01	1.2929E-02	1.0151E-03	2.5198E-02	-3.6810E 00	4.0287E-02	9.8090E 02	3.6686E 01
8	6.3856E 00	4.0776E 01	1.4918E-02	1.1681E-03	2.5443E-02	-3.6713E 00	4.5910E-02	8.5011E 02	3.9304E 01
9	6.4031E 00	4.1001E 01	1.6907E-02	1.3202E-03	2.5723E-02	-3.6604E 00	5.1323E-02	7.547E 02	3.8876E 01
10	6.4208E 00	4.1227E 01	1.9890E-02	1.5489E-03	2.6047E-02	-3.6479E 00	5.9466E-02	6.4562E 02	3.8392E 01
11	6.4388E 00	4.1454E 01	2.1875E-02	1.6995E-03	2.6414E-02	-3.6338E 00	6.4326E-02	6.8931E-02	3.7858E 01
12	6.4566E 00	4.1681E 01	2.3668E-02	1.8485E-03	2.6817E-02	-3.6187E 00	7.0356E-02	5.0977E 02	3.7290E 01
13	6.4734E 00	4.1908E 01	2.5858E-02	1.9971E-03	2.7255E-02	-3.6025E 00	7.3277E-02	5.0072E 02	3.6691E 01
14	6.4912E 00	4.2136E 01	2.7847E-02	2.1449E-03	2.7727E-02	-3.5853E 00	7.7358E-02	4.6622E 02	3.6065E 01
15	6.5088E 00	4.2566E 01	2.9836E-02	2.2919E-03	2.8235E-02	-3.5672E 00	8.1138E-02	4.3311E 02	3.5417E 01
16	6.5265E 00	4.2959E 01	3.1825E-02	2.4381E-03	2.8778E-02	-3.5482E 00	8.4726E-02	4.1015E 02	3.4749E 01
17	6.5441E 00	4.2825E 01	3.3814E-02	2.5835E-03	2.9356E-02	-3.5283E 00	8.8009E-02	3.8077E 02	3.4065E 01
18	6.5617E 00	4.3055E 01	3.5803E-02	2.7282E-03	2.9968E-02	-3.5076E 00	9.0356E-02	3.6635E 02	3.3369E 01
19	6.5794E 00	4.3775E 01	3.7752E-02	2.8720E-03	3.0616E-02	-3.4862E 00	9.3808E-02	3.4819E 02	3.2663E 01
20	6.5969E 00	4.3519E 01	3.9781E-02	3.0151E-03	3.1299E-02	-3.4662E 00	9.6333E-02	3.3166E 02	3.1950E 01
21	6.6145E 00	4.3751E 01	4.2764E-02	3.2326E-03	3.2025E-02	-3.4412E 00	1.0099E-01	3.0355E 02	3.1225E 01
22	6.6321E 00	4.3985E 01	4.5748E-02	3.4490E-03	3.2804E-02	-3.4172E 00	1.0414E-01	2.8944E 02	3.0484E 01
23	6.6491E 00	4.4281E 01	4.9726E-02	3.7390E-03	3.3645E-02	-3.3919E 00	1.1113E-01	2.6742E 01	2.9722E 01
24	6.6667E 00	4.4453E 01	5.4699E-02	4.1020E-03	3.4564E-02	-3.3649E 00	1.1868E-01	2.4378E 02	2.8932E 01
25	6.6845E 00	4.4688E 01	6.1660E-02	4.6119E-03	3.5598E-02	-3.3357E 00	1.2959E-01	2.1833E 02	2.8099E 01
26	6.7022E 00	4.4924E 01	6.8622E-02	5.1191E-03	3.6735E-02	-3.3040E 00	1.3935E-01	1.9555E 02	2.7222E 01
27	6.7201E 00	4.5160E 01	7.4589E-02	5.5497E-03	3.7795E-02	-3.2703E 00	1.4606E-01	1.8019E 02	2.6319E 01
28	6.7377E 00	4.5397E 01	8.1551E-02	6.0518E-03	3.9365E-02	-3.2348E 00	1.5372E-01	1.6524E 02	2.5400E 01
29	6.7553E 00	4.5634E 01	8.8512E-02	6.5513E-03	4.0866E-02	-3.1975E 00	1.6031E-01	1.4526E-02	2.4470E 01
30	6.7729E 00	4.5972E 01	9.8457E-02	7.0205E-03	4.2512E-02	-3.1580E 00	1.7098E-01	1.3158E 02	2.3523E 01
31	6.7905E 00	4.6111E 01	1.0940E-01	8.0551E-03	4.4341E-02	-3.1158E 00	1.8166E-01	1.2444E 02	2.3552E 01
32	6.8081E 00	4.6351E 01	1.2034E-01	8.8377E-03	4.6335E-02	-3.0713E 00	1.9002E-01	1.1315E 02	2.1569E 01
33	6.8257E 00	4.6591E 01	1.3327E-01	9.7620E-03	4.8595E-02	-3.0242E 00	2.0088E-01	1.0460E 02	2.0577E 01
34	6.8433E 00	4.6818E 01	1.4818E-01	1.0827E-02	5.1072E-02	-2.9745E 00	2.1195E-01	9.2636E 01	1.9580E 01
35	6.8608E 00	4.7072E 01	1.6410E-01	1.1959E-02	5.3821E-02	-2.9221E 00	2.2219E-01	8.3621E 01	1.8580E 01
36	6.8785E 00	4.7314E 01	1.8399E-01	1.3377E-02	5.6884E-02	-2.8667E 00	2.3511E-01	7.4772E 01	1.7579E 01
37	6.8961E 00	4.7557E 01	2.0288E-01	1.4710E-02	6.0278E-02	-2.8086E 00	2.4399E-01	6.7822E 01	1.6597E 01
38	6.9137E 00	4.7800E 01	2.2675E-01	1.6399E-02	6.4071E-02	-2.7478E 00	2.5594E-01	6.0811E 01	1.5608E 01
39	6.9311E 00	4.8044E 01	2.5460E-01	1.8366E-02	6.8307E-02	-2.6837E 00	2.6887E-01	5.4450E 01	1.4640E 01
40	6.9499E 00	4.8288E 01	2.7946E-01	2.0100E-02	7.3008E-02	-2.6172E 00	2.7552E-01	4.9731E 01	1.3697E 01
41	6.9666E 00	4.8533E 01	3.1228E-01	2.2413E-02	7.8216E-02	-2.5483E 00	2.8655E-01	4.4617E 01	1.2785E 01
42	6.9842E 00	4.8779E 01	3.5305E-01	2.5275E-02	8.4072E-02	-2.4761E 00	3.0064E-01	3.9544E 01	1.1895E 01
43	7.0018E 00	4.9025E 01	3.9880E-01	2.8479E-02	9.0689E-02	-2.4003E 00	3.1403E-01	3.5141E 01	1.1027E 01
44	7.0194E 00	4.9222E 01	4.5350E-01	3.2304E-02	9.1911E-02	-2.3208E 00	3.2899E-01	3.0562E 01	1.0184E 01
45	7.0370E 00	4.9519E 01	5.1616E-01	3.6675E-02	1.0672E-01	-2.2375E 00	3.4366E-01	2.7667E 01	9.3699E 00
46	7.0544E 00	4.9767E 01	5.9971E-01	4.2504E-02	1.1655E-01	-2.1495E 00	3.6470E-01	2.3521E 01	8.5803E 00
47	7.0722E 00	5.0016E 01	6.9716E-01	4.9289E-02	1.2796E-01	-2.0560E 00	3.8519E-01	2.0150E 01	7.8150E 00
48	7.0892E 00	5.0265E 01	8.0059E-01	5.6461E-02	1.4114E-01	-1.9580E 00	4.0003E-01	1.7711E 01	7.0851E 00
49	7.1074E 00	5.0515E 01	9.6270E-01	6.7725E-02	1.5666E-01	-1.8537E 00	4.3230E-01	1.4766E 01	6.3832E 00

TABLE IV (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1250E 00	5.0768E 01	1.1517E 00	8.0818E-02	1.7527E-01	-1.7414E 00	4.6111E-01	1.2373E 01	5.7055E 00
51	7.1426E 00	5.1017E 01	1.4649E 00	1.0255E-01	1.9830E-01	-1.6180E 00	5.1715E-01	9.7555E 00	5.0430E 00
52	7.1602E 00	5.1269E 01	1.7931E 00	1.2521E-01	2.2697E-01	-1.4829E 00	5.5168E-01	7.9863E 00	4.4059E 00
53	7.1778E 00	5.1521E 01	2.1114E 00	1.4708E-01	2.6133E-01	-1.3420E 00	5.6279E-01	6.7992E 00	3.8265E 00
54	7.1954E 00	5.1774E 01	2.4336E 00	1.6911E-01	3.0134E-01	-1.1995E 00	5.6119E-01	5.9134E 00	3.3186E 00

TABLE V

EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 10,589 RPM
(See Figure 4)

THE CONCENTRATION FOR THIS RUN = 0.6737×10^{-1}
DIFFERENCE BTWN SQS OF RTW AND MENISCUS = $0.12693140 \times 10^{-1}$
CONE. AT MENISCUS = 0.3554×10^{-1}

Identification Number is Sample 2 10,589 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.2645E-00	3.9244E-00	1.7955E-00	1.4331E-03	3.5236E-002	-3.3457E-00	4.0671E-002	6.9780E-002	2.8380E-001
2	6.2881E-00	3.9836E-00	1.9172E-00	1.5245E-03	3.5671E-002	-3.3334E-00	4.2735E-002	6.5596E-002	2.8032E-001
3	6.3116E-00	3.9836E-00	2.0592E-00	1.6313E-03	3.6141E-002	-3.3203E-00	4.5137E-002	6.1301E-002	2.7669E-001
4	6.2352E-00	4.0134E-00	2.2114E-00	1.7453E-03	3.6664E-002	-3.3065E-00	4.7629E-002	5.7296E-002	2.7289E-001
5	6.3587E-00	4.0423E-00	2.3713E-00	1.6655E-03	3.7184E-002	-3.2919E-00	5.0195E-002	5.3577E-002	2.6893E-001
6	6.3823E-00	4.0733E-00	2.5553E-00	2.0226E-03	3.7766E-002	-3.2776E-00	5.3029E-002	4.9934E-002	2.6480E-001
7	6.4258E-00	4.1035E-00	2.7490E-00	2.1457E-03	3.8390E-002	-3.2600E-00	5.5893E-002	4.6604E-002	2.6049E-001
8	6.4294E-00	4.1317E-00	2.9620E-00	3.0355E-03	3.9062E-002	-3.2422E-00	4.8970E-002	4.3412E-002	2.5600E-001
9	6.4529E-00	4.1641E-00	3.1954E-00	2.4759E-03	3.9788E-002	-3.2224E-00	6.2228E-002	4.0389E-002	2.5133E-001
10	6.4765E-00	4.1945E-00	3.4490E-00	2.6627E-03	4.0570E-002	-3.2047E-00	6.5631E-002	3.7556E-002	2.4464E-001
11	6.5001E-00	4.2251E-00	3.7127E-00	2.8559E-03	4.1414E-002	-3.1841E-00	6.8960E-002	3.5015E-002	2.4147E-001
12	6.5236E-00	4.2558E-00	3.9967E-00	3.0373E-03	4.2322E-002	-3.1625E-00	7.2381E-002	3.3629E-002	2.3629E-001
13	6.5472E-00	4.2865E-00	4.3711E-00	3.2847E-03	4.3299E-002	-3.1396E-00	7.5860E-002	3.0444E-002	2.3095E-001
14	6.5707E-00	4.3174E-00	4.6575E-00	3.5199E-03	4.4350E-002	-3.1156E-00	7.9366E-002	2.8410E-002	2.2548E-001
15	6.5243E-00	4.3488E-00	4.9765E-00	3.7688E-03	4.5480E-002	-3.0905E-00	8.2867E-002	2.6533E-002	2.1988E-001
16	6.6178E-00	4.3796E-00	5.3213E-00	4.0750E-03	4.6755E-002	-3.0667E-00	7.1000E-002	3.6298E-002	2.1471E-001
17	6.6414E-00	4.4108E-00	5.7314E-00	4.3149E-03	4.7759E-002	-3.0416E-00	9.0348E-002	2.3176E-002	2.0939E-001
18	6.6655E-00	4.4422E-00	6.1379E-00	4.6421E-03	4.9162E-002	-3.0126E-00	9.4423E-002	2.1542E-002	2.0341E-001
19	6.6885E-00	4.4736E-00	6.6749E-00	4.9897E-03	4.0677E-002	-2.9823E-00	9.8461E-002	1.9733E-002	1.9733E-001
20	6.7115E-00	4.5052E-00	7.2225E-00	5.3803E-03	5.2314E-002	-2.9505E-00	1.0285E-001	1.8586E-002	1.9115E-001
21	6.7354E-00	4.5369E-00	7.8312E-00	5.8132E-03	5.4087E-002	-2.9172E-00	1.0748E-001	1.7202E-002	1.8489E-001
22	6.7592E-00	4.5686E-00	8.4395E-00	6.2907E-03	5.6009E-002	-2.8822E-00	1.1214E-001	1.5922E-002	1.7854E-001
23	6.7927E-00	4.6005E-00	9.2205E-00	6.7973E-03	5.8039E-002	-2.8457E-00	1.1700E-001	1.4712E-002	1.7121E-001
24	6.8063E-00	4.6328E-00	1.0032E-00	7.3700E-03	6.0362E-002	-2.8074E-00	1.2210E-001	1.3569E-002	1.6567E-001
25	6.8208E-00	4.6644E-00	1.3915E-00	7.9976E-03	6.2829E-002	-2.7673E-00	1.2718E-001	1.2515E-002	1.5916E-001
26	6.8534E-00	4.6999E-00	1.1968E-00	8.6588E-03	6.5513E-002	-2.7250E-00	1.3217E-001	1.1549E-002	1.5264E-001
27	6.8771E-00	4.7294E-00	9.2913E-00	9.2920E-03	6.8431E-002	-2.6819E-00	1.3720E-001	1.0651E-002	1.4613E-001
28	6.9015E-00	4.7617E-00	1.4260E-00	1.0187E-02	7.1609E-002	-2.6336E-00	1.4227E-001	9.8161E-002	1.3965E-001
29	6.9241E-00	4.7943E-00	1.5379E-00	1.1105E-02	7.5075E-002	-2.5893E-00	1.4792E-001	9.0050E-001	1.3326E-001
30	6.9476E-00	4.8269E-00	1.6769E-00	1.2767E-02	7.8866E-002	-2.5401E-00	1.5302E-001	8.2867E-001	1.2681E-001
31	6.9712E-00	4.9597E-00	1.8235E-00	1.3118E-02	8.299CE-002	-2.4890E-00	1.5807E-001	7.6231E-001	1.2050E-001
32	6.9947E-00	4.9926E-00	1.9963E-00	1.427CE-02	8.7495E-002	-2.4362E-00	1.6310E-001	7.0076E-001	1.1429E-001
33	7.0183E-00	4.9256E-00	2.1779E-00	1.5465E-02	9.2405E-002	-2.3816E-00	1.6737E-001	6.4660E-001	1.0822E-001
34	7.0418E-00	4.9589E-00	2.3137E-00	1.6454E-02	9.7759E-002	-2.3253E-00	1.7241E-001	5.9332E-001	1.0230E-001
35	7.0654E-00	4.9979E-00	2.6079E-00	1.9444E-02	1.0362E-002	-2.2670E-00	1.7805E-001	5.4203E-001	9.6506E-001
36	7.0990E-00	5.0253E-00	2.8798E-00	2.1079E-02	1.1070E-002	-2.2066E-00	1.8395E-001	4.9387E-001	9.0850E-001
37	7.1125E-00	5.0599E-00	3.1751E-00	2.2320E-02	1.1719E-002	-2.1439E-00	1.9046E-001	4.4802E-001	8.5330E-001
38	7.1361E-00	5.0924E-00	3.5193E-00	2.519E-02	1.2514E-002	-2.0784E-00	1.9993E-001	3.9970E-001	7.9913E-001
39	7.1596E-00	5.1269E-00	4.1298E-00	2.8691E-02	1.3418E-002	-2.0366E-00	2.1382E-001	3.4854E-001	7.4527E-001
40	7.1822E-00	5.1591E-00	4.9775E-00	3.4599E-02	1.4448E-002	-1.9319E-00	2.38882E-001	2.8903E-001	6.9027E-001
41	7.2167E-00	5.1937E-00	7.2222E-01	4.9969E-02	1.5920E-002	-1.8376E-00	3.1387E-001	2.0012E-001	6.2833E-001

TABLE VI

EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 7,447 RPM
(See Figure 3b)

THE CONCENTRATION FOR THIS RUN = 0.6737×10^{-3}
DIFFERENCE BTW SGS OF STM AND MENISCUS = $0.12556299 \times 10^{-3}$
CONC. AT MENISCUS = 0.4797×10^{-3}

Identification Number is Sample 2 7,447 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.2624E 00	3.9218E 01	2.0995E-02	1.6675E-C3	4.7967E-02	-3.0373E 00	3.4763E-02	5.9971E 02	2.0048E 01
2	6.282CE 00	3.9438E 01	2.1879E-02	1.7422E-C3	4.8343E-02	-3.0294E 00	3.6034E-02	5.7406E 02	2.0686E 01
3	6.2976E 00	3.966CE 01	2.1879E-02	1.7371E-C3	4.8728E-02	-3.0215E 00	3.5649E-02	5.7566E 02	2.0222E 01
4	6.3152E 00	3.9882E 01	2.2874E-02	1.8110E-C3	4.9122E-02	-3.0134E 00	3.6868E-02	5.5217E 02	2.0357E 01
5	6.3328E 00	4.0105E 01	2.3868E-02	1.8845E 03	4.9533E-02	-3.0051E 00	3.0455E-02	5.3064E 02	2.0188E 01
6	6.3504E 00	4.0328E 01	2.4863E-02	1.9628E-C3	4.9962E-02	-2.9965E 00	5.1081E-02	5.1083E 02	2.0015E 01
7	6.3688E 00	4.0552E 01	2.5858E-02	2.0303E-C3	5.0409E-02	-2.9816E 00	4.0276E-02	4.9255E 02	1.9938E 01
8	6.3856E 00	4.0776E 01	2.6852E-02	2.0325E-C3	5.0873E-02	-2.9784E 00	4.1329E-02	4.7562E 02	1.9637E 01
9	6.4022E 00	4.1001E 01	2.7847E-02	2.1744E-03	5.1354E-02	-2.9690E 00	4.2341E-02	4.5989E 02	1.9473E 01
10	6.4208E 00	4.1227E 01	2.8841E-02	2.2159E-03	5.1853E-02	-2.9533E 00	4.3313E-02	4.4526E 02	1.9255E 01
11	6.4384E 00	4.1454E 01	2.9839E-02	2.3170E-03	5.2370E-02	-2.9494E 00	4.4243E-02	4.3159E 02	1.9095E 01
12	6.4560E 00	4.1681E 01	3.0839E-02	2.3877E-C3	5.2904E-02	-2.9333E 00	4.5133E-02	4.1881E 02	1.8902E 01
13	6.4736E 00	4.1928E 01	3.1825E-02	2.4580E-C3	5.3455E-02	-2.9289E 00	4.5983E-02	4.0683E 02	1.8707E 01
14	6.4913E 00	4.2136E 01	2.819E-02	2.5285E-C3	5.4024E-02	-2.9183E 00	4.6793E-02	3.8510E 02	1.8510E 01
15	6.5089E 00	4.2356E 01	3.3814E-02	2.5575E-C3	5.4611E-02	-2.9015E 00	4.7564E-02	3.8498E 02	1.8311E 01
16	6.5265E 00	4.2595E 01	3.4808E-02	2.6667E-C3	5.5215E-02	-2.8865E 00	4.8297E-02	3.7500E 02	1.8111E 01
17	6.5441E 00	4.2825E 01	3.5803E-02	2.7355E-C3	5.5836E-02	-2.8833E 00	4.8992E-02	3.6566E 02	1.7910E 01
18	6.5617E 00	4.3055E 01	3.6791E-02	2.8040E-C3	5.6475E-02	-2.8740E 00	4.9649E-02	3.5664E 02	1.7770E 01
19	6.5793E 00	4.3287E 01	3.7779E-02	2.8720E-C3	5.7132E-02	-2.8624E 00	5.0270E-02	3.4819E 02	1.7503E 01
20	6.5969E 00	4.3519E 01	3.8786E-02	2.9397E-03	5.7805E-02	-2.8507E 00	5.0856E-02	3.4017E 02	1.7299E 01
21	6.6145E 00	4.3751E 01	3.9781E-02	3.0071E-03	5.8497E-02	-2.8388E 00	5.1406E-02	3.3253E 02	1.7095E 01
22	6.6321E 00	4.3958E 01	4.0775E-02	3.0741E-03	5.9206E-02	-2.8287E 00	5.1922E-02	3.2530E 02	1.6890E 01
23	6.6497E 00	4.4218E 01	4.1770E-02	3.1407E-03	5.9933E-02	-2.8155E 00	5.2404E-02	3.1840E 02	1.6665E 01
24	6.6673E 00	4.4453E 01	4.3759E-02	3.2816E-C3	6.0686E-02	-2.8020E 00	5.4076E-02	3.0473E 02	1.6418E 01
25	6.6849E 00	4.4688E 01	4.4753E-02	3.4474E-03	6.1456E-02	-2.7893E 00	5.4640E-02	2.9874E 02	1.6270E 01
26	6.7025E 00	4.4924E 01	4.5748E-02	3.4128E-03	6.2261E-02	-2.7764E 00	5.4813E-02	2.9302E 02	1.6061E 01
27	6.7201E 00	4.5160E 01	4.6742E-02	3.4778E-03	6.3075E-02	-2.7634E 00	5.5137E-02	2.8754E 02	1.5854E 01
28	6.7377E 00	4.5397E 01	4.8731E-02	3.6163E-C3	6.5391E-02	-2.7502E 00	5.6122E-02	2.7652E 02	1.5664E 01
29	6.7553E 00	4.5634E 01	4.9766E-02	3.8045E-03	6.4782E-02	-2.7376E 00	5.6814E-02	2.7170E 02	1.5456E 01
30	6.7729E 00	4.5872E 01	5.1715E-02	3.8178E-03	6.5675E-02	-2.7330E 00	5.8131E-02	2.6193E 02	1.5226E 01
31	6.7905E 00	4.6111E 01	5.3704E-02	3.9543E-03	6.6603E-02	-2.7090E 00	5.9372E-02	2.5289E 02	1.5044E 01
32	6.8081E 00	4.6351E 01	5.4699E-02	4.0172E-03	6.7765E-02	-2.6948E 00	5.9463E-02	2.4892E 02	1.4892E 01
33	6.8257E 00	4.6591E 01	5.6688E-02	4.1525E-03	6.8538E-02	-2.6804E 00	6.0587E-02	2.4082E 02	1.4691E 01
34	6.8433E 00	4.6831E 01	5.8677E-02	4.2871E-03	6.9553E-02	-2.6657E 00	6.1639E-02	2.3326E 02	1.4318E 01
35	6.8609E 00	4.7072E 01	5.9671E-02	4.3486E-03	7.0595E-02	-2.6508E 00	6.1600E-02	2.2996E 02	1.4165E 01
36	6.8785E 00	4.7314E 01	6.1660E-02	4.4182E-03	7.1663E-02	-2.6338E 00	6.2311E 02	2.2311E 02	1.3934E 01
37	6.8961E 00	4.7557E 01	6.3649E-02	4.6148E-03	7.2766E-02	-2.6205E 00	6.3442E-02	2.1666E 02	1.3743E 01
38	6.9137E 00	4.780CE 01	6.5638E-02	4.7469E-03	7.3904E-02	-2.6050E 00	6.4232E-02	2.1066E 02	1.3531E 01
39	6.9314E 00	4.8044E 01	6.8622E-02	4.9501E-03	7.5085E-02	-2.5891E 00	6.5926E-02	2.0202E 02	1.2922E 01
40	6.9490E 00	4.8288E 01	7.1605E-02	5.1522E-03	7.6320E-02	-2.5728E 00	6.7509E-02	1.9490E 02	1.2103E 01
41	6.9666E 00	4.8533E 01	7.4589E-02	5.3134E-03	7.7606E-02	-2.5561E 00	6.8981E-02	1.8680E 02	1.2886E 01
42	6.9842E 00	4.8877E 01	7.7575E-02	5.5535E-03	7.8946E-02	-2.5390E 00	7.0345E-02	1.8007E 02	1.2667E 01
43	7.0018E 00	4.9025E 01	8.0555E-02	5.7553E-03	8.0337E-02	-2.5215E 00	7.1605E-02	1.7384E 02	1.2448E 01
44	7.0194E 00	4.9272E 01	8.3545E-02	5.9507E-03	8.1782E-02	-2.5037E 00	7.2773E-02	1.6805E 02	1.2228E 01
45	7.0370E 00	4.9519E 01	8.6523E-02	6.1478E-03	8.3279E-02	-2.4836E 00	7.3822E-02	1.6266E 02	1.2008E 01
46	7.0546E 00	4.9767E 01	8.9507E-02	6.3439E-03	8.4828E-02	-2.4671E 00	7.4785E-02	1.5763E 02	1.1789E 01
47	7.0722E 00	5.0016E 01	9.2490E-02	6.6390E-03	8.6430E-02	-2.4484E 00	7.5297E-02	1.5293E 02	1.1570E 01
48	7.0898E 00	5.0256E 01	9.5457E-02	6.9436E-03	8.8111E-02	-2.4292E 00	7.8806E-02	1.4402E 02	1.1349E 01
49	7.1074E 00	5.0515E 01	1.0741E-01	7.5561E-C3	8.992E-02	-2.4088E 00	8.4029E-02	1.3234E 02	1.1121E 01

TABLE VI (CONT)

I	R	X	CR	CX	C	LNC	CX/C	1/CX	1/C
50	7.1250E 20	5.02766E C1	1.01730E-01	8.2353E-C3	9.1901E-02	-2.3870E 00	8.9611E-02	1.2143E C2	1.0881E 01
51	7.1426E 20	5.1017E C1	1.2730E-01	8.9112F-C3	9.4054E-02	-2.3639E 00	9.4746E-02	1.1222E C2	1.0632E 01
52	7.1502E 20	5.1269E C1	1.4520E-01	9.6452E-C2	9.6452E-02	-2.3387E 00	1.0512E-01	9.8625E C1	1.0368E 01
53	7.1778E 20	5.1521E C1	1.7867E-C1	1.2401E-C2	9.9297E-02	-2.3096E 00	1.2488E-01	8.0641E 01	1.0071E 01
54	7.1954E 20	5.1774E C1	2.5559E-01	1.7761E-C2	1.0311E-01	-2.2719E 00	1.7225E-01	5.6304E 01	9.6981E 00

TABLE VII

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 10,589 RPM
(See Figure 5)

THE CONCENTRATION FOR THIS RUN = 5.1146×10^{-6}
DIFFERENCE BTWN SQS OF BTW AND MENISCUS = $0.12987963 \times 10^{-6}$
CONC. AT MENISCUS = 5.6796×10^{-6}

Identification Number Is Sample 3 10,589 RPM

I	R	X	CR	CX	C	LNC(C)	CX/C	1/CX	1/C
1	6.2486E-00	3.9045E-01	4.9353E-02	3.9491E-C3	6.7960E-02	-2.6888E-00	5.8109E-02	2.5322E-02	1.4715E-01
2	6.2778E-00	3.9411E-01	5.0305E-02	4.0100E-03	6.9418E-02	-2.6676E-00	5.7708E-02	2.4932E-02	1.4406E-01
3	6.3371E-00	3.9779E-01	5.2374E-02	4.1520E-03	7.0919E-02	-2.6622E-00	5.8546E-02	2.4085E-02	1.401E-01
4	6.3363E-00	4.0149E-01	5.3382E-02	4.2124E-03	7.2465E-02	-2.6246E-00	5.8129E-02	2.3740E-02	1.3800E-01
5	6.3965E-00	4.0520E-01	5.5396E-02	4.3512E-03	7.4051E-02	-2.5929E-00	5.8782E-02	2.2953E-02	1.3503E-01
6	6.3948E-00	4.0893E-01	5.7410E-02	4.4888E-03	7.5704E-02	-2.5809E-00	5.9294E-02	2.2277E-02	1.3209E-01
7	6.3948E-00	4.1268E-01	5.8418E-02	4.5468E-03	7.7398E-02	-2.5588E-00	5.8746E-02	2.1993E-02	1.2920E-01
8	6.4523E-00	4.1644E-01	6.0432E-02	4.6823E-03	7.9135E-02	-2.5366E-00	5.9169E-02	2.1357E-02	1.2637E-01
9	6.4425E-00	4.2023E-01	6.1434E-02	4.7389E-03	8.0916E-02	-2.5143E-00	5.8656E-02	2.1102E-02	1.2358E-01
10	6.5117E-00	4.2403E-01	6.3424E-02	4.8723E-03	8.2742E-02	-2.4920E-00	5.8885E-02	2.0524E-02	1.2086E-01
11	6.5412E-00	4.2794E-01	6.7494E-02	5.1584E-03	8.4656E-02	-2.4652E-00	6.0934E-02	1.9386E-02	1.1813E-01
12	6.5702E-00	4.3167E-01	7.2518E-02	5.5187E-03	8.6702E-02	-2.4453E-00	6.3652E-02	1.8120E-02	1.1534E-01
13	6.5504E-00	4.3553E-01	7.7554E-02	5.8758E-03	8.8796E-02	-2.4203E-00	6.6098E-02	1.7019E-02	1.1249E-01
14	6.5687E-00	4.3839E-01	8.2592E-02	6.2298E-03	9.1237E-02	-2.3943E-00	6.8282E-02	1.6052E-02	1.0961E-01
15	6.6577E-00	4.4329E-01	9.0648E-02	6.9075E-03	9.3769E-02	-2.3669E-00	7.2599E-02	1.4690E-02	1.0665E-01
16	6.6671E-00	4.4718E-01	9.7694E-02	7.3049E-03	9.6522E-02	-2.3380E-00	7.5682E-02	1.3689E-02	1.0360E-01
17	6.7164E-00	4.5110E-01	1.0374E-01	1.07230E-03	9.9466E-02	-2.3019E-00	7.7645E-02	1.2948E-02	1.0054E-01
18	6.4546E-00	4.5533E-01	1.17179E-01	8.2122E-03	1.0450E-01	-2.2169E-00	8.0039E-02	1.2177E-02	9.4644E-01
19	6.7744E-00	4.5893E-01	1.1988E-01	8.8457E-03	1.0597E-01	-2.2446E-00	8.3471E-02	1.1305E-02	9.4363E-00
20	6.8041E-00	4.6296E-01	2.8932E-01	9.4738E-03	1.0984E-01	-2.208E-00	8.6435E-02	1.0555E-02	9.1233E-00
21	6.8337E-00	4.6634E-01	1.3799E-01	1.0397E-02	1.1351E-01	-2.1759E-00	8.8948E-02	9.9043E-02	8.8697E-00
22	6.6526E-00	4.7095E-01	1.4906E-01	1.0787E-02	1.1769E-01	-2.1397E-00	9.1658E-02	9.2701E-01	8.4967E-00
23	6.8918E-00	4.7497E-01	1.5813E-01	1.1472E-02	1.2217E-01	-2.1024E-00	9.3907E-02	8.7169E-01	8.1855E-00
24	6.9214E-00	4.7911E-01	1.7212E-01	1.2297E-02	1.2697E-01	-2.0638E-00	9.6852E-02	8.1322E-01	7.8760E-00
25	6.6583E-00	4.8317E-01	1.8313E-01	1.3187E-02	1.3213E-01	-2.0239E-00	9.9802E-02	7.5831E-01	7.568CE-00
26	6.0795E-00	4.8713E-01	2.0313E-01	1.4359E-02	1.3774E-01	-1.924E-00	1.0424E-01	6.9644E-01	7.2598E-00
27	7.0397E-00	4.9122E-01	2.2158E-01	1.5908E-02	1.4391E-01	-1.9386E-00	1.0984E-01	6.3220E-01	6.9487E-00
28	7.3397E-00	4.9533E-01	2.4475E-01	1.7388E-02	1.5073E-01	-1.8923E-00	1.1536E-01	5.7512E-01	6.6344E-00
29	7.5757E-00	4.9945E-01	2.7492E-01	1.9454E-02	1.5832E-01	-1.8431E-00	1.2287E-01	5.1404E-01	6.3161E-00
30	7.2064E-00	5.0362E-01	3.1425E-01	2.2141E-02	1.6694E-01	-1.7901E-00	1.3263E-01	4.5165E-01	5.9903E-00
31	7.1257E-00	5.0775E-01	3.6635E-01	2.5725F-02	1.7689E-01	-1.7322E-00	1.4543E-01	3.8872E-01	5.5333E-00
32	7.1549E-00	5.1193E-01	4.6925E-01	3.1321E-02	1.9882E-01	-1.6671E-00	1.6590E-01	3.1927E-01	5.2967E-00
33	7.3142E-00	5.1612E-01	6.7482E-01	2.0521E-02	2.0521E-01	-1.5537E-00	2.2887E-01	2.1292E-01	4.8731E-00
34	7.2134E-00	5.2033E-01	1.0012E-00	2.2978E-01	1.4706E-00	3.0383E-01	4.3519E-01	4.3519E-01	4.3519E-01

TABLE VIII

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 8,766 RPM
(See Figure 6a)

THE CONCENTRATION FOR THIS RUN = $0.11146E-9C$
DIFFERENCE BTWN SQS OF BT4 AND MENISCUS = $0.12829269E-02$
C_{MNC} AT MFNTSCUS = $0.8063E-01$

I	q	x	CR	CX	C	LN(C)	CX/C	CX/CX	1/C
1	6.2468E-20	3.9523E-01	4.1592E-02	3.3289E-03	8.0627E-02	-2.5179E-00	4.1288E-02	3.0040E-02	1.2403E-01
2	6.2645E-00	3.9244E-01	4.2300E-02	3.3762E-03	8.1368E-02	-2.5088E-00	4.14493E-02	2.9619E-02	1.2290E-01
3	6.2821E-10	3.9555E-01	4.3213E-02	3.4344E-03	8.2123E-02	-2.44995E-00	4.1881E-02	2.9075E-02	1.2177E-01
4	6.2998E-00	3.9697E-01	4.4126E-02	3.5022E-03	8.2895E-02	-2.4902E-00	4.22494E-02	2.9553E-02	1.2063E-01
5	6.3175E-01	3.9910E-01	4.5039E-02	3.5647E-02	8.3683E-02	-2.4807E-00	4.2597E-02	2.8053E-02	1.1950E-01
6	6.3351E-00	4.0134E-01	4.6054E-02	3.6348E-02	8.4487E-02	-2.4712E-00	4.3022E-02	2.7512E-02	1.1836E-01
7	6.3528E-00	4.0158E-01	4.7064E-02	3.7045E-02	8.5310E-02	-2.4615E-00	4.3424E-02	2.6994E-02	1.1722E-01
8	6.3705E-10	4.0583E-01	4.8083E-02	3.7739E-02	8.6150E-02	-2.4517E-00	4.3806E-02	2.6498E-02	1.1608E-01
9	6.3891E-00	4.0894E-01	4.9198E-02	3.8508E-02	8.7010E-02	-2.4417E-00	4.4257E-02	2.5969E-02	1.1493E-01
10	6.4058E-20	4.1034E-01	5.0314E-02	3.9212E-02	8.7889E-02	-2.4317E-00	4.4684E-02	2.5463E-02	1.1378E-01
11	6.4235E-01	4.1261E-01	5.1532E-02	4.0112E-03	8.8788E-02	-2.4215E-00	4.5177E-02	2.4930E-02	1.1263E-01
12	6.4411E-20	4.1498E-01	5.2494E-02	4.1177E-03	8.9709E-02	-2.4112E-00	4.5644E-02	2.4422E-02	1.1147E-01
13	6.4588E-00	4.1716E-01	5.3966E-02	4.1777E-03	9.0652E-02	-2.4007E-00	4.6085E-02	2.3937E-02	1.1031E-01
14	6.4765E-02	4.1945E-01	5.5285E-02	4.2661E-03	9.1617E-02	-2.3901E-00	4.6587E-02	2.3429E-02	1.0915E-01
15	6.4941E-20	4.2174E-01	5.6604E-02	4.3580E-03	9.2606E-02	-2.3794E-00	4.7060E-02	2.2946E-02	1.0798E-01
16	6.5118E-20	4.2404E-01	5.8024E-02	4.5533E-03	9.3618E-02	-2.3685E-00	4.7590E-02	2.2464E-02	1.0682E-01
17	6.5295E-20	4.2634E-01	5.9444E-02	4.5522CE-03	9.4665E-02	-2.3575E-00	4.8090E-02	2.1969E-02	1.0565E-01
18	6.5471E-00	4.2865E-01	6.0864E-02	4.6461E-03	9.5718E-02	-2.4007E-00	4.8561E-02	2.1514E-02	1.0447E-01
19	6.5549E-02	4.3097E-01	6.2388E-02	4.7515E-03	9.6807E-02	-2.335CE-00	4.9082E-02	2.046E-02	1.0330E-01
20	6.5925E-02	4.3229E-01	6.3927E-02	4.8543E-03	9.7923E-02	-2.3236E-00	4.9573E-02	2.0606E-02	1.0212E-01
21	6.6561E-00	4.3562E-01	6.5530E-02	4.9643E-03	9.9066E-02	-2.3120E-00	5.0111E-02	2.0144E-02	1.0094E-01
22	6.6738E-02	4.3795E-01	6.7153E-02	5.0737E-03	1.0024E-01	-2.3002E-00	5.0616E-02	1.9710E-02	9.9762E-00
23	6.6355E-20	4.4030E-01	6.8978E-02	5.1301E-03	1.0444E-01	-2.2838E-00	5.1626E-02	1.9581E-02	9.8581E-00
24	6.6531E-00	4.4264E-01	7.0602E-02	5.1595E-03	1.0267E-01	-2.2762E-00	5.1679E-02	1.8847E-02	9.7398E-00
25	6.6709E-20	4.4500E-01	7.2428E-02	5.4487E-03	1.0394E-01	-2.2640E-00	5.2232E-02	1.8420E-02	9.6214E-00
26	6.6845E-02	4.4736E-01	7.4254E-02	5.5509E-03	1.0523E-01	-2.2516E-00	5.2750E-02	1.8015E-02	9.5029E-00
27	6.7761E-02	4.6872E-01	7.6181E-02	5.6156E-03	1.0792E-01	-2.2236E-00	5.3300E-02	1.7606E-02	9.3844E-00
28	6.7234E-20	4.5210E-01	7.8210E-02	5.8159E-03	1.0792E-01	-2.1736E-00	5.3889E-02	1.7194E-02	9.2658E-00
29	6.7415E-02	4.5447E-01	8.0342E-02	5.9581E-03	1.0932E-01	-2.134E-00	5.4505E-02	1.6782E-02	9.1471E-00
30	6.7591E-02	4.5686E-01	8.2572E-02	6.1282E-03	1.1076E-01	-2.104E-00	5.5146E-02	1.6371E-02	9.0283E-00
31	6.7758E-10	4.5925E-01	8.4517E-02	6.2711E-03	1.1244E-01	-2.0817E-00	5.5877E-02	1.5944E-02	8.9092E-00
32	6.7945E-02	4.6165E-01	9.7543E-02	6.4422F-03	1.1377E-01	-2.0736E-00	5.6626E-02	1.5523E-02	8.7898E-00
33	6.8111E-20	4.6405E-01	9.9322E-02	6.6265E-03	1.1534E-01	-2.0562E-00	5.7453E-02	1.5091E-02	8.6701E-00
34	6.8298E-00	4.6666E-01	9.3122E-02	6.8173E-03	1.1696E-01	-2.0354E-00	6.3354E-02	1.2537E-02	7.9425E-00
35	6.8475E-00	4.6919E-01	9.6165E-02	6.9219E-03	1.1863E-01	-2.1317E-00	5.9192E-02	1.4241E-02	8.4295E-00
36	6.8651E-00	4.7130E-01	9.9317E-02	7.2229E-03	1.2036E-01	-2.1173E-00	6.0095E-02	1.3826E-02	8.3086E-00
37	6.8828E-02	4.7273E-01	1.0275E-01	7.4649E-03	1.2214E-01	-2.1026E-00	6.1116E-02	1.3396E-02	8.1872E-00
38	6.9015E-02	4.7417E-01	1.0641E-01	7.7174E-03	1.2399E-01	-2.0876E-00	6.286E-02	1.2970E-02	8.0652E-00
39	6.9181E-00	4.7611E-01	1.1373E-01	7.9766E-03	1.2590E-01	-2.0722E-00	6.4354E-02	1.2537E-02	7.9425E-00
40	6.9358E-02	4.8115E-01	1.1463E-01	8.2534E-03	1.2789E-01	-2.0566E-00	6.6612E-02	1.2102E-02	7.8191E-00
41	6.9535E-02	4.8351E-01	1.1929E-01	8.51ACF-03	1.2996E-01	-2.0405E-00	6.6005E-02	1.1658E-02	7.6948E-00
42	6.9711E-02	4.8597E-01	1.2437E-01	8.900E-03	1.3211E-01	-2.0241E-00	6.7519E-02	1.1211E-02	7.5694E-00
43	6.9888E-02	4.8844E-01	1.2994E-01	9.2666E-03	1.3436E-01	-2.0073E-00	6.9193E-02	1.0757E-02	7.4428E-00
44	7.0074E-02	4.9171E-01	1.3603E-01	9.775E-03	1.3671E-01	-1.9899E-00	7.1010E-02	1.0301E-02	7.3145E-00
45	7.0274E-02	4.9339E-01	1.4293E-01	1.0174E-02	1.3917E-01	-1.9721E-00	9.8289E-02	9.8289E-02	7.1854E-00
46	7.0474E-02	4.9554E-01	1.1699E-01	1.4176E-01	1.4176E-01	-1.9536E-00	7.5399E-02	9.3556E-01	7.0540E-00
47	7.0674E-02	4.9836E-01	1.5926E-01	1.280E-02	1.4450E-01	-1.9345E-00	7.062E-02	8.8653E-01	6.9204E-00
48	7.0877E-02	5.0146E-01	1.694E-01	1.4740E-02	1.4740E-01	-1.9146E-00	8.1196E-02	8.3553E-01	6.7841E-00
49	7.1074E-02	5.0366E-01	1.9361E-01	1.2399E-02	1.5052E-01	-1.8937E-00	8.5965E-02	7.7283E-01	6.6436E-00

TABLE VIII (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1125E 00	5.0587E 01	2.0095E -01	1.4120E -01	1.5392E -02	1.8713E 00	9.1735E -02	7.0823E 01	6.4970E 00
51	7.1311E 00	5.0839E 01	2.2114E -01	1.5507E -02	1.5764E -01	-1.8474E 00	9.8369E -02	6.4486E 01	6.3434E 00
52	7.1478E 00	5.1091E 01	2.4356E -01	1.7030E -02	1.6175E -01	-1.8217E 00	1.0529E -01	5.8720E 01	6.1823E 00
53	7.1655E 00	5.1344E 01	2.8423E -01	1.9819E -02	1.6641E -01	-1.7933E 00	1.1910E -01	5.0455E 01	6.0094E 00
54	7.1832E 00	5.1598E 01	3.3475E -01	2.3301E -02	1.7187E -01	-1.7610E 00	1.2557E -01	4.2916E 01	5.8183E 00
55	7.2008E 00	5.1852E 01	4.3619E -01	3.0288E -02	1.7868E -01	-1.7221E 00	1.6951E -01	3.3017E 01	5.5963E 00

TABLE IX

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 7,447 RPM
(See Figure 6b)

THE CONCENTRATION FOR THIS RUN = 0.1146E-00
DIFFERENCE BTWN SQS OF BTM AND MENISCUS = 0.12629269E-02
CNC. AT MENISCUS = 0.8673E-01

Identification Number is Sample 3 7,447 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	LCX	1/C
1	6.2468F 00	3.9023E 01	3.8547E-02	3.05654E-03	6.6728E-02	-2.4450E 00	3.5575E-02	3.2411E 02	1.1530E 01
2	6.2645E 00	3.9244E 01	3.8750E-02	3.0978E-03	8.7410E-02	-2.4371E 00	3.2333E-02	1.1440E 01	1.1351E 01
3	6.2221F 00	3.9465E 01	3.9054E-02	3.1384E-03	8.8078E-02	-2.4293E 00	3.5235E-02	3.2171E 02	1.1351E 01
4	6.2998F 00	3.9687E 01	3.9460E-02	3.1319E-03	8.8791E-02	-2.4215E 00	3.5222E-02	3.1930E 02	1.1262E 01
5	6.3115E 00	3.9910E 01	3.9866E-02	3.1522E-03	8.9492E-02	-2.4136E 00	3.5257E-02	3.1694E 02	1.1174E 01
6	6.3351E 00	4.0134E 01	4.0373E-02	3.1864E-03	9.0201E-02	-2.4057E 00	3.5326E-02	3.1383E 02	1.1086E 01
7	6.3528E 00	4.0583E 01	4.0891E-02	3.2175E-03	9.0919E-02	-2.3978E 00	3.5389E-02	3.1080E 02	1.0999E 01
8	6.3775E 00	4.0831E 00	4.1383E-02	3.2484E-03	9.1645E-02	-2.3898E 00	3.5443E-02	3.0784E 02	1.0912E 01
9	6.3881E 00	4.0808E 01	4.1996E-02	3.2870E-03	9.2382E-02	-2.3818E 00	3.5581E-02	3.0422E 02	1.0825E 01
10	6.4258F 00	4.1034E 01	4.2605E-02	3.3255E-03	9.3129E-02	-2.3738E 00	3.5708E-02	3.0171E 02	1.0738E 01
11	6.4225F 00	4.1261E 01	4.3315E-02	3.3716E-03	9.3888E-02	-2.3657E 00	3.5911E-02	2.9659E 02	1.0651E 01
12	6.4411E 00	4.1488E 01	4.4025E-02	3.4117E-03	9.4660E-02	-2.3575E 00	3.6103E-02	2.9261E 02	1.0564E 01
13	6.4584E 00	4.1716E 01	4.4836E-02	3.4710E-03	9.5445E-02	-2.3492E 00	3.6366E-02	2.8810E 02	1.0477E 01
14	6.4765E 00	4.1945E 01	4.5643E-02	3.5244E-03	9.6244E-02	-2.3405E 00	3.6617E-02	2.8377E 02	1.0396E 01
15	6.4941F 00	4.2174E 01	4.6460E-02	3.5710E-03	9.7057E-02	-2.3325E 00	3.6853E-02	2.7956E 02	1.0303E 01
16	6.5118E 00	4.2494E 01	4.7372E-02	3.6314E-03	9.7886E-02	-2.3239E 00	3.7160E-02	2.7479E 02	1.0216E 01
17	6.5295E 00	4.2634E 01	4.8285E-02	3.6975E-03	9.8731E-02	-2.3154E 00	3.7450E-02	2.7045E 02	1.0129E 01
18	6.5471F 00	4.2865E 01	4.9300E-02	3.7550E-03	9.9593E-02	-2.3071E 00	3.7804E-02	2.6565E 02	1.0041E 01
19	6.5648E 00	4.3097E 01	5.0416E-02	3.8339E-03	1.0047E-01	-2.2979E 00	3.8217E-02	2.6043E 02	9.9528E 00
20	6.5825E 00	4.3329E 01	5.1633E-02	3.9220E-03	1.0138E-01	-2.2889E 00	3.8688E-02	2.5497E 02	9.8643E 00
21	6.6021F 00	4.3562E 01	5.2850E-02	4.0037E-03	1.0250E-01	-2.2797E 00	3.9138E-02	2.4977E 02	9.7753E 00
22	6.6178E 00	4.3795E 01	5.4069E-02	4.0505E-03	1.0324E-01	-2.2707E 00	3.9566E-02	2.4480E 02	9.6859E 00
23	6.6355E 00	4.4030E 01	5.5386E-02	4.1135E-03	1.0421E-01	-2.2613E 00	4.0049E-02	2.3981E 02	9.5960E 00
24	6.6531E 00	4.4264E 01	5.6808E-02	4.2691E-03	1.0520E-01	-2.2519E 00	4.0542E-02	2.3424E 02	9.5056E 00
25	6.6709E 00	4.4500E 01	5.8372E-02	4.3633E-03	1.0622E-01	-2.2423E 00	4.1088E-02	2.2913E 02	9.4147E 00
26	6.6885E 00	4.4736E 01	5.9748E-02	4.4665E-03	1.0726E-01	-2.2325E 00	4.1642E-02	2.2389E 02	9.3232E 00
27	6.7061E 00	4.4972E 01	6.1371E-02	4.5577E-03	1.0833E-01	-2.2226E 00	4.2239E-02	2.1854E 02	9.2311E 00
28	6.7238E 00	4.5210E 01	6.3096E-02	4.6692E-03	1.0943E-01	-2.2125E 00	4.2877E-02	2.1313E 02	9.1384E 00
29	6.7415E 00	4.5447E 01	6.4820E-02	4.8076E-03	1.1056E-01	-2.2022E 00	4.3484E-02	2.0801E 02	9.0450E 00
30	6.7591E 00	4.5686E 01	6.6646E-02	4.9301E-03	1.1172E-01	-2.1918E 00	4.4129E-02	2.0284E 02	8.9510E 00
31	6.7768E 00	4.5925E 01	6.8573E-02	5.0594E-03	1.1291E-01	-2.1811E 00	4.4808E-02	1.9765E 02	8.8563E 00
32	6.7945E 00	4.6155E 01	7.0602E-02	5.1966E-03	1.1454E-01	-2.1730E 00	4.5518E-02	1.9247E 02	8.7690E 00
33	6.8121E 00	7.2723E 01	5.3384E-02	5.3384E-03	1.1593E-01	-2.1593E 00	4.6256E-02	1.8132E 02	8.6648E 00
34	6.8298E 00	4.6646E 01	7.4964E-02	5.4880E-03	1.1671E-01	-2.1480E 00	4.7021E-02	1.8222E 02	8.5679E 00
35	6.8475E 00	4.6888E 01	7.7297E-02	5.6644E-03	1.1806E-01	-2.1366E 00	4.7717E-02	1.7771E 02	8.4703E 00
36	6.8651E 00	4.8351E 01	9.5759E-02	5.8144E-03	1.1945E-01	-2.1249E 00	4.8676E-02	1.7197E 02	8.3719E 00
37	6.8828E 00	4.7373E 01	8.2577E-02	5.9984E-03	1.2088E-01	-2.1129E 00	4.9622E-02	1.6671E 02	8.2725E 00
38	6.9005E 00	4.7671E 01	8.5514E-02	6.1962E-03	1.2237E-01	-2.1007E 00	5.0633E-02	1.6139E 02	8.1722E 00
39	6.9181E 00	4.7861E 01	8.8659E-02	6.4077E-03	1.2391E-01	-2.0882E 00	5.1714E-02	1.5606E 02	8.0707E 00
40	6.9358E 00	4.8105E 01	9.2108E-02	6.6400E-03	1.2550E-01	-2.0754E 00	5.2290E-02	1.5060E 02	7.9680E 00
41	6.9535E 00	4.8351E 01	9.5759E-02	6.8857E-03	1.2716E-01	-2.0623E 00	5.4149E-02	1.4523E 02	7.8646E 00
42	6.9711E 00	4.9579E 01	9.9716E-02	7.1320E-03	1.2889E-01	-2.0488E 00	5.5490E-02	1.3982E 02	7.7587E 00
43	6.9888E 00	4.8844E 01	1.0398E-01	7.4487E-03	1.3069E-01	-2.0349E 00	5.6920E-02	1.3443E 02	7.6519E 00
44	7.0065E 00	4.9091E 01	1.0854E-01	7.7457E-03	1.3256E-01	-2.0207E 00	5.8430E-02	1.2910E 02	7.5435E 00
45	7.0241F 00	4.9339E 01	1.1366E-01	8.0973E-03	1.3453E-01	-2.0060E 00	6.0117E-02	1.2365E 02	7.4335E 00
46	7.0418E 00	4.9587E 01	1.1909E-01	8.4660E-03	1.3658E-01	-1.9908E 00	6.1911E-02	1.1862E 02	7.3216E 00
47	7.0555E 00	4.9836E 01	1.2518E-01	8.8659E-03	1.3874E-01	-1.9752E 00	6.3874E-02	1.1279E 02	7.2077E 00
48	7.0711E 00	5.0086E 01	1.3207E-01	9.3315E-03	1.4101E-01	-1.9589E 00	6.6172E-02	1.0717E 02	7.0916E 00
49	7.0944E 00	5.0336E 01	1.4019E-01	9.8798E-03	1.4342E-01	-1.9420E 00	6.8888E-02	1.0122E 02	6.9727E 00

TABLE IX (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1125E 00	5.0587E 01	1.5013E-01	1.0554E-02	1.4598E-02	1.9243E 00	7.2297E-02	9.4750E 01	6.8502E 00
51	7.1501E 00	5.0839E 01	1.6322E-01	1.1453E-02	1.4875E-02	1.9055E 00	7.6992E-02	8.7316E 01	6.7227E 00
52	7.1478E 00	5.1091E 01	1.8259E-01	1.2773E-02	1.5181E-02	1.8852E 00	8.4138E-02	7.8293E 01	6.5874E 00
53	7.1655E 00	5.1344E 01	2.1322E-01	1.4865E-02	1.5530E-02	1.8624E 00	9.5715E-02	6.7274E 01	6.4391E 00
54	7.1832E 00	5.1598E 01	2.5369E-01	1.7652E-02	1.5940E-02	1.8362E 00	1.1013E-01	5.6649E 01	6.2727E 00
55	7.2008E 00	5.1852E 01	3.6518E-01	2.5357E-02	1.6489E-02	1.8025E 00	1.5319E-01	3.9437E 01	6.0648E 00

TABLE X
EXPERIMENTAL DATA FOR SAMPLE 4 AT ROTOR SPEED 13,410 RPM
(See Figure 7)

THE CONCENTRATION FOR THIS RUN = $0.1098E-0^0$
DIFFERENCE BTWN SQS OF BTM AND MENISCUS = $0.14738286E-0^2$
CONC. AT MENISCUS = $0.7052E-0^1$

Identification Number is Sample 4 13,410 RPM

I	R	X	CR	CX	C	LNC	CX/C	1/CX	1/C
1	6.1025E 00	3.7241E 01	1.0245E-02	8.3945E-04	7.0518E-02	-2.6519E 00	1.1904E-02	1.1913E 03	1.4181E 01
2	6.1261F 00	3.7529E 01	1.2984E-02	7.0598E-03	7.0792E-02	-2.6480E 00	1.4970E-02	1.4126E 02	1.4126E 01
3	6.1496F 00	3.7818E 01	1.5013E-02	1.2207E-03	7.1121E-02	-2.6434E 00	1.7163E-02	8.1923E 02	1.4050E 01
4	6.1732E 00	3.8128E 01	1.7245E-02	1.3968E-03	7.1501E-02	-2.6380E 00	1.9535E-02	7.1595E 02	1.3986E 01
5	6.1967E 00	3.8399E 01	1.9375E-02	1.5633E-03	7.1933E-02	-2.6320E 00	2.1733E-02	6.3966E 02	1.3902E 01
6	6.2213E 00	3.8692E 01	2.1607E-02	1.7368E-03	7.2415E-02	-2.6253E 00	2.3984E-02	5.7577E 02	1.3809E 01
7	6.2438F 00	3.9985E 01	3.7241E 00	1.9171E-02	7.2952E-02	-2.6180E 00	2.6279E-02	5.2163E 02	1.3708E 01
8	6.2674E 00	3.9280E 01	6.3740E-02	2.1044E-03	7.3544E-02	-2.6099E 00	2.8610E-02	4.7526E 02	1.3597E 01
9	6.2919E 00	3.9576E 01	2.4030E-02	2.2575E-03	7.4189E-02	-2.6011E 00	3.0428E-02	4.4297E 02	1.3479E 01
10	6.3145E 00	3.9873E 01	3.0838E-02	2.4418E-03	7.4887E-02	-2.5918E 00	4.2607E-02	4.0953E 02	1.3353E 01
11	6.3381E 00	4.0171E 01	3.3475E-02	2.6404E-03	7.5644E-02	-2.5817E 00	3.4911E-02	3.7867E 02	1.3220E 01
12	6.3616E 00	4.0470E 01	3.6911E-02	2.8303E-03	7.6463E-02	-2.5710E 00	3.7016E-02	3.5331E 02	1.3078E 01
13	6.3852E 00	4.0770E 01	3.8547E-02	3.0185E-03	7.7334E-02	-2.5595E 00	3.9028E-02	3.3129E 02	1.2930E 01
14	6.4087F 00	4.1072E 01	4.0880E-02	4.2587E-03	7.8189E-03	-2.5475E 00	4.0746E-02	3.1354E 02	1.2775E 01
15	6.4323E 00	4.1374E 01	4.3721E-02	3.3985E-03	7.9273E-03	-2.5349E 00	4.2871E-02	2.9424E 02	1.2615E 01
16	6.4559E 00	4.1678E 01	4.6662E-02	3.6140E-03	8.0337E-03	-2.5215E 00	4.4985E-02	2.7670E 02	1.2448E 01
17	6.4794E 00	4.1983E 01	4.9198E-02	3.7965E-03	8.1466E-03	-2.5076E 00	4.6603E-02	2.6634E 02	1.2225E 01
18	6.5030E 00	4.2288E 01	5.2242E-02	4.0168E-03	8.2661E-03	-2.4930E 00	4.8593E-02	2.4896E 02	1.2098E 01
19	6.5265E 00	4.2595E 01	5.5589E-02	4.2587E-03	8.3931E-03	-2.4778E 00	5.0741E-02	2.3481E 02	1.1915E 01
20	6.5501E 00	4.2903E 01	5.8835E-02	4.4912E-03	8.5278E-03	-2.4618E 00	5.2665E-02	2.2266E 02	1.1726E 01
21	6.5736E 00	4.3212E 01	6.1980E-02	4.7143E-03	8.6701E-03	-2.4453E 00	5.4374E-02	2.1212E 02	1.1534E 01
22	6.5972E 00	4.5523E 01	5.5429E-02	4.9588E-03	8.8202E-03	-2.4281E 00	5.6222E-02	2.0166E 02	1.1338E 01
23	6.6207E 00	4.3834E 01	6.9182E-02	5.2247E-03	8.9787E-03	-2.4103E 00	5.8189E-02	1.9140E 02	1.1137E 01
24	6.6443F 00	4.4147E 01	7.3240E-02	5.5115E-03	9.1465E-03	-2.3918E 00	6.0258E-02	1.8144E 02	1.0933E 01
25	6.6679E 00	4.4466E 01	7.7602E-02	5.8191E-03	9.3241E-03	-2.3726E 00	6.2409E-02	1.7185E 02	1.0725E 01
26	6.6914E 00	4.4775E 01	8.2166E-02	6.1397E-03	9.5123E-03	-2.3526E 00	6.4545E-02	1.6287E 02	1.0513E 01
27	6.7150E 00	4.5091E 01	8.7238E-02	6.4958E-03	9.7118E-03	-2.3318E 00	6.6886E-02	1.5394E 02	1.0291E 01
28	6.7385E 00	4.5408E 01	9.2412E-02	6.9570E-03	9.9234E-03	-2.3103E 00	6.9099E-02	1.4584E 02	1.0077E 01
29	6.7621E 00	4.5726E 01	9.8397E-02	7.2755E-03	1.0148E-03	-2.2879E 00	7.1695E-02	1.3744E 02	9.8541E 00
30	6.7856E 00	4.6045E 01	1.0479E-02	7.7213E-03	1.0387E-03	-2.2646E 00	7.4333E-02	1.2956E 02	9.6277E 00
31	6.8092E 00	4.6365E 01	1.1158E-02	8.1936E-03	1.0642E-03	-2.2403E 00	7.6992E-02	1.2205E 02	9.3955E 00
32	6.8327E 00	4.6686E 01	1.1970E-02	8.7592E-03	1.0915E-03	-2.2151E 00	8.0252E-02	1.1417E 02	9.1626E 00
33	6.8563E 00	4.7038E 01	1.2728E-02	9.3205E-03	1.1261E-03	-2.1887E 00	8.3308E-02	1.0712E 02	8.9235E 00
34	6.8879E 00	4.7323E 01	1.3777E-02	1.0012E-02	1.1519E-03	-2.1611E 00	8.6910E-02	9.9835E 01	8.6810E 00
35	6.9212E 00	4.7657E 01	1.4810E-02	1.0727E-02	1.1856E-03	-2.1323E 00	9.0475E-02	9.3225E 01	8.4345E 00
36	6.9570E 00	4.7983E 01	1.5957E-02	1.1518E-02	1.2218E-03	-2.1022E 00	9.4265E-02	8.6833E 01	8.1844E 00
37	6.9919E 00	4.8310E 01	1.7296E-02	1.2442E-02	1.2610E-03	-2.0707E 00	9.8667E-02	8.0374E 01	7.9302E 00
38	6.9974E 00	4.8638E 01	1.8844E-02	1.3513E-02	1.3036E-03	-2.0375E 00	1.03666E-01	7.4005E 01	7.6713E 00
39	6.9976E 00	4.8967E 01	2.0846E-02	1.4895E-02	1.3503E-03	-2.0022E 00	1.1031E-01	6.7137E 01	7.4057E 00
40	7.0212E 00	4.9297E 01	2.3433E-02	1.6687E-02	1.4025E-03	-1.9644E 00	1.1898E-01	5.9927E 01	7.1303E 00
41	7.0447E 00	4.9628E 01	2.8910E-02	1.4641E-02	1.9213E 00	-1.9213E 00	1.4015E-01	4.8735E 01	6.8301E 00
42	7.0683E 00	4.9961F 01	3.3780E-02	2.3895E-02	1.3379E-01	-1.8722E 00	1.5537E-01	4.1850E 01	6.5023E 00
43	7.0919E 00	5.0294E 01	4.2909E-02	3.0252E-02	1.6282E-01	-1.8151E 00	1.8580E-01	3.3055E 01	6.1466E 00
44	7.1154E 00	5.0629E 01	5.2749E-02	1.3513E-02	1.7067E-02	-1.7482E 00	2.1292E-01	5.7442E 01	5.7442E 00
45	7.1396E 00	5.0955E 01	6.8942E-02	1.8842E-02	1.8842E-01	-1.6669E 00	2.5640E-01	2.0699E 01	5.3072E 00
46	7.1625E 00	5.1302E 01	1.0651E 00	7.4354E-02	2.0908E-01	-1.5650E 00	3.5562E-01	1.3449E 01	4.7828E 00
47	7.1961F 00	5.1640E 01	1.2724E 00	1.3410E-01	1.4939E-01	-1.4939E 00	5.4890E-01	7.4569E 00	4.0931E 00
48	7.2096E 00	5.1979E 01	1.9065E-01	2.7490E-01	2.9938E-01	-1.2061E 00	5.3688E-01	5.2452E 00	3.3403E 00

TABLE XI
EXPERIMENTAL DATA FOR SAMPLE 4 AT ROTOR SPEED 10,659 RPM
(See Figure 8)

I	R	X	CR	CX	C	LN(C)	C/X/C	1/CX	1/C
1	6.1057E 00	3.7280E 01	2.4082E-02	1.9721E-03	7.3156E-02	-2.6152E 00	2.6957E-02	5.0708E 02	1.3669E 01
2	6.1349E 00	3.7637E 01	2.5742E-02	2.0980E-03	7.3884E-02	-2.6053E 00	2.8396E-02	4.7664E 02	1.3555E 01
3	6.1642E 00	3.7997E 01	2.7403E-02	2.2228E-03	7.4661E-02	-2.5948E 00	4.4989E-02	1.3344E 01	
4	6.1934E 00	3.8358E 01	3.0725E-02	2.4804E-03	7.5510E-02	-2.5835E 00	3.2849E-02	4.0315E 02	1.3232E 01
5	6.2226E 00	3.8721E 01	3.2386E-02	2.6022E-03	7.6433E-02	-2.5713E 00	3.4046E-02	3.8428E 02	1.3033E 01
6	6.2519E 00	3.9086E 01	3.4046E-02	2.7299E-03	7.7404E-02	-2.5587E 00	3.5178E-02	3.6726E 02	1.2919E 01
7	6.2811E 00	3.9456E 01	3.6584E-02	2.9083E-03	7.8436E-02	-2.5455E 00	3.7082E-02	3.4382E 02	1.2779E 01
8	6.3104E 00	3.9821E 01	3.9859E-02	3.1582E-03	7.9552E-02	-2.5313E 00	3.9700E-02	3.1663E 02	1.2570E 01
9	6.3396E 00	4.0190E 01	4.1520E-02	3.2747E-03	8.0742E-02	-2.5165E 00	4.0557E-02	3.0538E 02	1.2309E 01
10	6.3688E 00	4.0562E 01	4.2350E-02	3.3248E-03	8.1968E-02	-2.5014E 00	4.0562E-02	3.0077E 02	1.2200E 01
11	6.3981E 00	4.0935E 01	4.4011E-02	3.4394E-03	8.3230E-02	-2.4861E 00	4.1324E-02	2.9075E 02	1.2015E 01
12	6.4223E 00	4.1310E 01	4.6502E-02	3.6176E-03	8.4553E-02	-2.4704E 00	4.2784E-02	2.7643E 02	1.1827E 01
13	6.4555E 00	4.1687E 01	4.8994E-02	3.7941E-03	8.5949E-02	-2.4540E 00	4.4144E-02	2.6357E 02	1.1639E 01
14	6.4885E 00	4.2065E 01	5.0654E-02	3.9050E-03	8.7406E-02	-2.4332E 00	4.4677E-02	2.5608E 02	1.1441E 01
15	6.5157E 00	4.2445E 01	5.3146E-02	4.0787E-03	8.8923E-02	-2.4220E 00	4.5868E-02	2.4513E 02	1.1248E 01
16	6.5442E 00	4.2827E 01	5.6467E-02	4.3143E-03	9.0525E-02	-2.4021E 00	4.7658E-02	2.3179E 02	1.1047E 01
17	6.5735E 00	4.3211E 01	5.8128E-02	4.4214E-03	9.2200E-02	-2.3838E 00	4.7954E-02	2.2617E 02	1.0846E 01
18	6.6027E 00	4.3596E 01	5.9789E-02	4.5276E-03	9.3924E-02	-2.3653E 00	4.8205E-02	2.2087E 02	1.0647E 01
19	6.6319E 00	4.3983E 01	6.2280E-02	4.6955E-03	9.5708E-02	-2.3464E 00	4.9060E-02	2.1297E 02	1.0448E 01
20	6.6612E 00	4.4371E 01	6.4771E-02	4.8618E-03	9.7566E-02	-2.3272E 00	4.9831E-02	2.0568E 02	1.0250E 01
21	6.6904E 00	4.4762E 01	6.7262E-02	5.0268E-03	9.9496E-02	-2.3076E 00	5.0523E-02	1.9893E 02	1.0051E 01
22	6.7197E 00	4.5154E 01	6.8923E-02	5.1255E-03	1.0149E-01	-2.4021E 00	5.1534E-02	1.9499E 02	9.8535E 00
23	6.7489E 00	4.5548E 01	7.3075E-02	5.4339E-03	1.0356E-01	-2.2676E 00	5.2277E-02	1.8471E 02	9.6561E 00
24	6.7781E 00	4.5943E 01	7.7227E-02	5.6968E-03	1.0576E-01	-2.2466E 00	5.3866E-02	1.7554E 02	9.4555E 00
25	6.8074E 00	4.6340E 01	8.3010E-02	6.0933E-03	1.0810E-01	-2.2247E 00	5.4622E-02	1.6395E 02	9.2506E 00
26	6.8366E 00	4.6739E 01	8.9633E-02	6.5590E-03	1.1063E-01	-2.2016E 00	5.5290E-02	1.5246E 02	9.0394E 00
27	6.8658E 00	4.7140E 01	9.7987E-02	7.1359E-03	1.1337E-01	-2.1771E 00	6.22943E-02	1.4014E 02	8.8207E 00
28	6.8951E 00	4.7542E 01	1.0878E-01	7.8884E-03	1.1639E-01	-2.1508E 00	6.7775E-02	1.2677E 02	8.5917E 00
29	6.9243E 00	4.7946E 01	1.2207E-01	8.8145E-03	1.1977E-01	-2.1222E 00	7.3598E-02	1.1345E 02	8.3496E 00
30	6.9535E 00	4.8352E 01	1.3702E-01	9.8522E-03	1.2355E-01	-2.0911E 00	7.9741E-02	1.0150E 02	8.0937E 00
31	6.9828E 00	4.8759E 01	1.5612E-01	1.1179E-02	1.2784E-01	-2.0570E 00	8.7444E-02	8.9457E 01	7.8225E 00
32	7.0120E 00	4.9168E 01	1.8186E-01	1.2968E-02	1.3278E-01	-2.0191E 00	9.7664E-02	7.7115E 01	7.5314E 00
33	7.0413E 00	4.9579E 01	2.1593E-01	1.5321E-02	1.3859E-01	-1.9762E 00	1.1062E-01	6.5226E 01	7.2155E 00
34	7.0705E 00	4.9992E 01	2.7403E-01	1.9319E-02	1.4575E-01	-1.9259E 00	1.3296E-01	5.1603E 01	6.8610E 00
35	7.0997E 00	5.0406E 01	3.2801E-01	2.3100E-02	1.5455E-01	-1.8672E 00	1.4947E-01	4.3290E 01	6.4704E 00
36	7.1290E 00	5.0822E 01	4.3181E-01	3.0255E-02	1.6565E-01	-1.7979E 00	1.8228E-01	3.3019E 01	6.0367E 00
37	7.1582E 00	5.1240E 01	6.9754E-01	4.8123E-02	1.8215E-01	-1.7029E 00	2.6748E-01	5.4899E 01	5.4899E 00
38	7.1874E 00	5.1659E 01	1.1460E 00	7.9719E-02	2.0909E-01	-1.5650E 00	3.8127E-01	1.2544E 01	4.7827E 00
39	7.2167E 00	5.2080E 01	1.5030E 00	1.0414E-01	2.4780E-01	-1.3951E 00	4.2024E-01	9.6029E 00	4.0355E 00

TABLE XII
FINAL RESULTS OF THE ELEVEN EXPERIMENTS REPORTED

SAMPLE	ROTOR SPEED (RPM)	$M_1 \times 10^{-3}$	g_1	$-R_{11}$	$M_m \times 10^{-3}$	g_m	$-R_{mm}$	$+R_{1m}$
1	10,589	1.4	3.393×10^{-2}	6.16	28.9	2.135×10^{-7}	134	0.83
					50.2	1.715×10^{-10}	165	0.79
					97.7	9.757×10^{-17}	89	0.78
1	8,766	1.4	4.015×10^{-2}	6.24	30.1	1.022×10^{-5}	386	2.04
					38.6	8.520×10^{-6}	325	1.97
					67.4	1.427×10^{-6}	208	1.86
					82.6	4.047×10^{-7}	166	1.81
					105.5	5.114×10^{-8}	110	1.77
					112.9	2.545×10^{-8}	95	1.76
1	7,477	1.7	4.430×10^{-2}	5.90	29.6	1.413×10^{-4}	241	1.43
					59.3	1.301×10^{-5}	217	1.40
					131.3	6.394×10^{-8}	127	1.36
2	17,250	1.6	3.520×10^{-3}	20.0	5.2	8.288×10^{-5}	75	1.87
					43.8	1.187×10^{-20}	186	4.37
					116.3	6.127×10^{-48}	255	1.29
2	10,589	1.6	1.050×10^{-2}	20.0	44.5	1.381×10^{-7}	122	6.04
					58.6	1.222×10^{-8}	45	5.89
					62.1	6.474×10^{-9}	27	5.86
					66.6	2.874×10^{-9}	6	5.82
2	7,447	3.3	1.503×10^{-2}	13.2	32.7	5.616×10^{-5}	215	4.66
					114.3	2.545×10^{-8}	86	4.49
3	10,589	4.4	1.125×10^{-2}	5.3				
3	8,766	4.7	1.966×10^{-2}	4.7		No other significant components found for this fraction.		
3	7,447	4.2	2.740×10^{-2}	5.5				
4	13,410	1.6	1.901×10^{-2}	7.0	6.2	1.729×10^{-4}	164	2.11
					10.7	2.003×10^{-5}	160	2.12
					139.3	1.580×10^{-31}	117	2.32
4	10,589	1.6	2.422×10^{-2}	8.3	3.2	3.352×10^{-3}	136	6.02
					9.8	2.337×10^{-3}	38	0.92
					44.6	1.525×10^{-6}	373	3.85
					123.1	1.190×10^{-10}	1,558	5.41

The subscript m ($m = 2, 3, \dots$) indicates other fractions found.

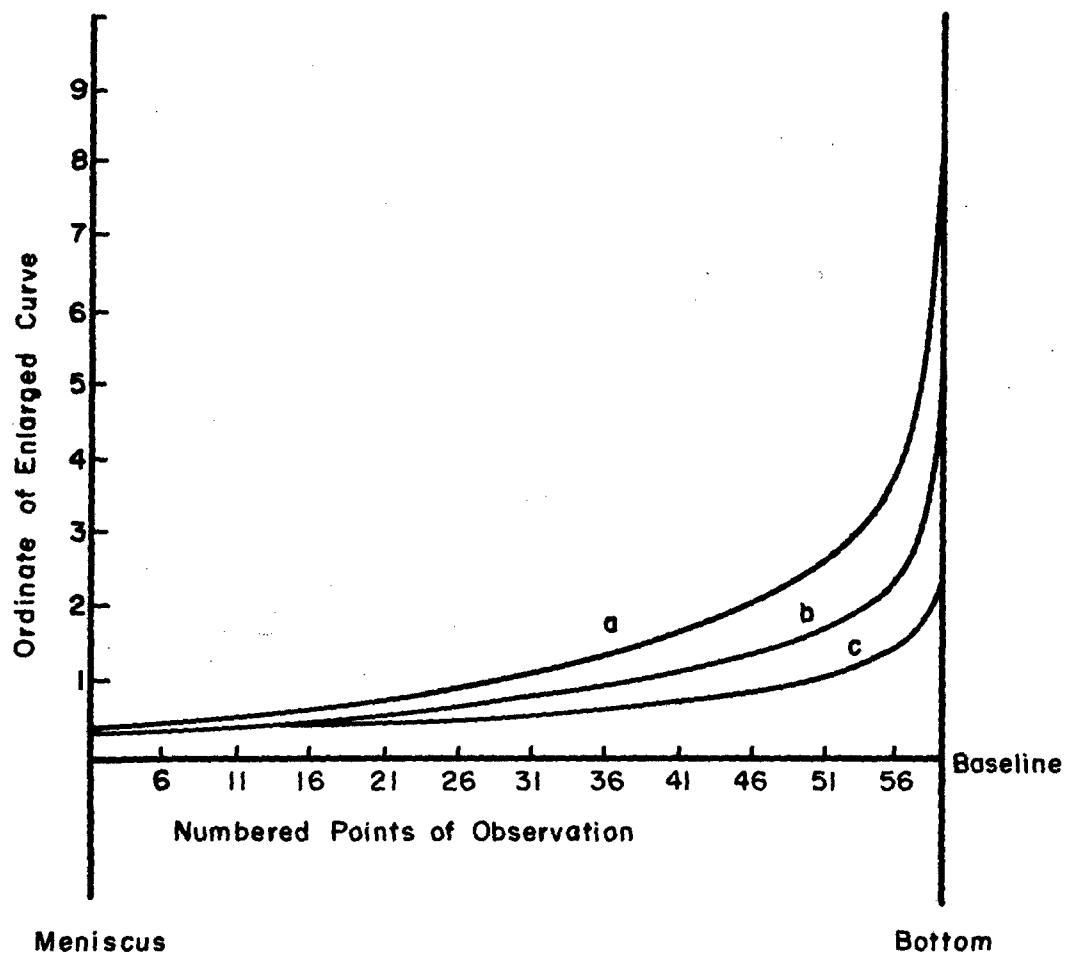


Figure 2. Schlieren Curves for Sample 1 at Rotor Speeds: a) 10,589 RPM; b) 8,766 RPM; and c) 7,447 RPM

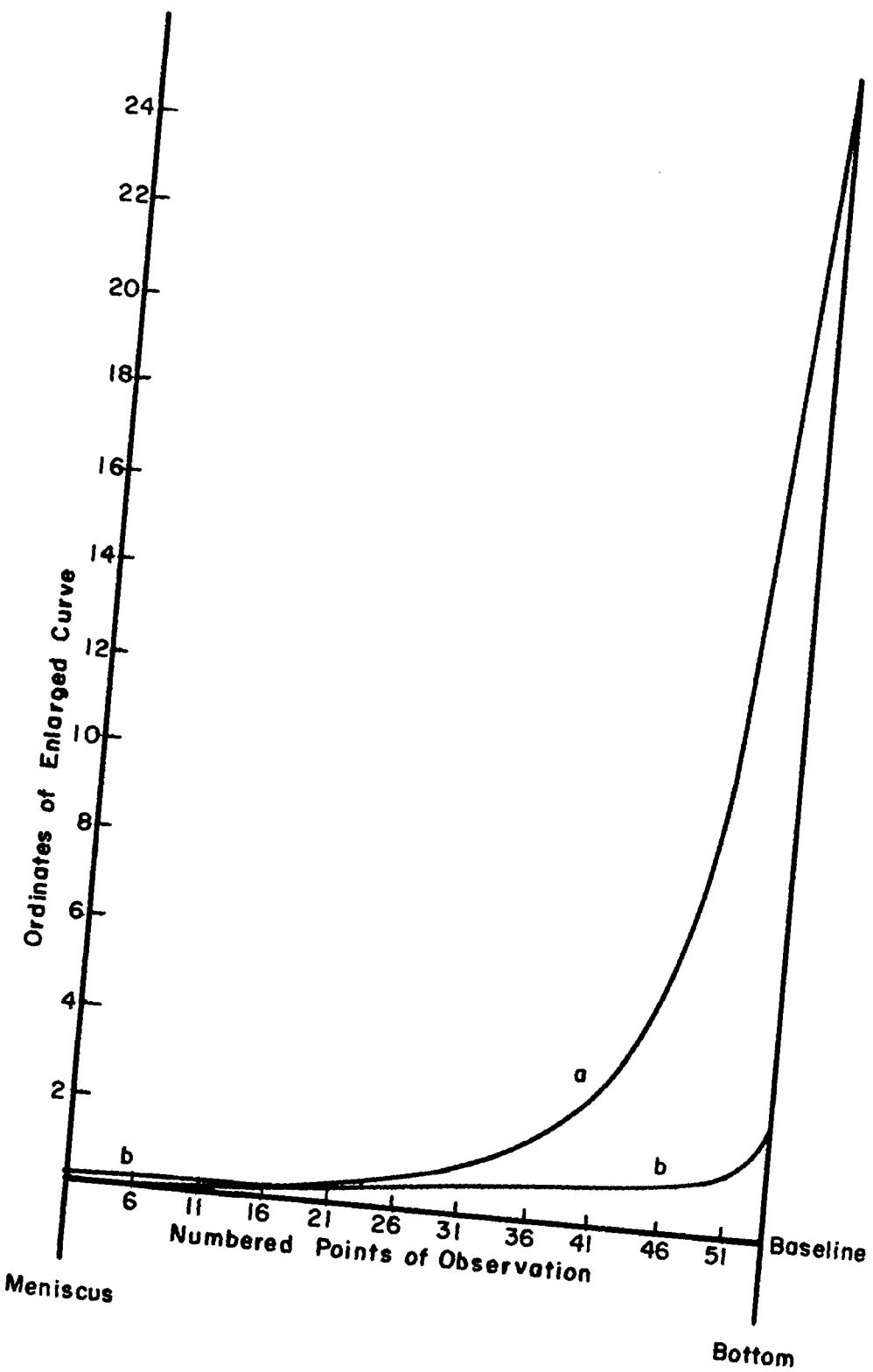


Figure 3. Schlieren Curve for Sample 2 at Rotor Speeds: a) 17,250 RPM; and
b) 7,447 RPM

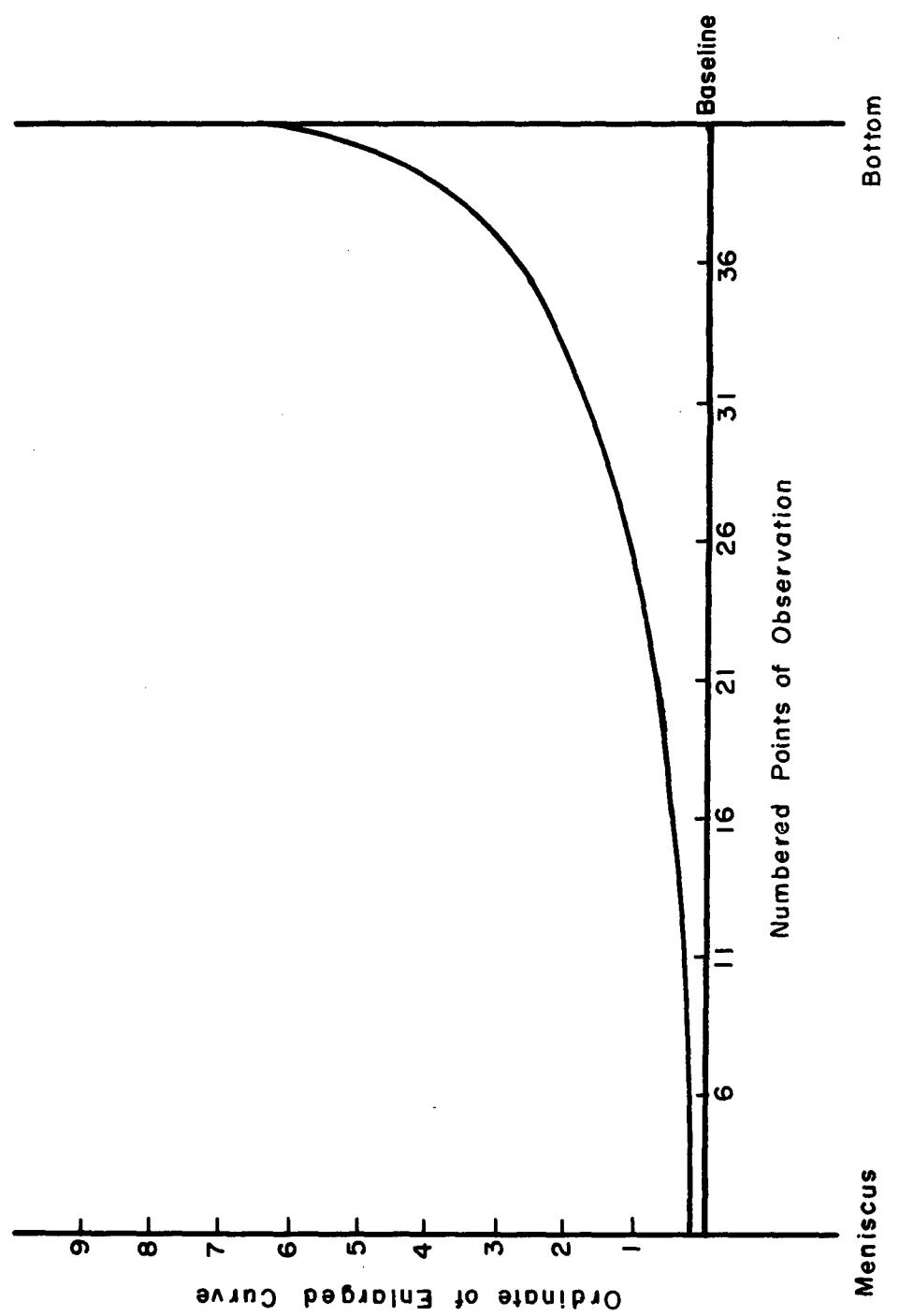


Figure 4. Schlieren Curve for Sample 2 at Rotor Speed 10,589 RPM

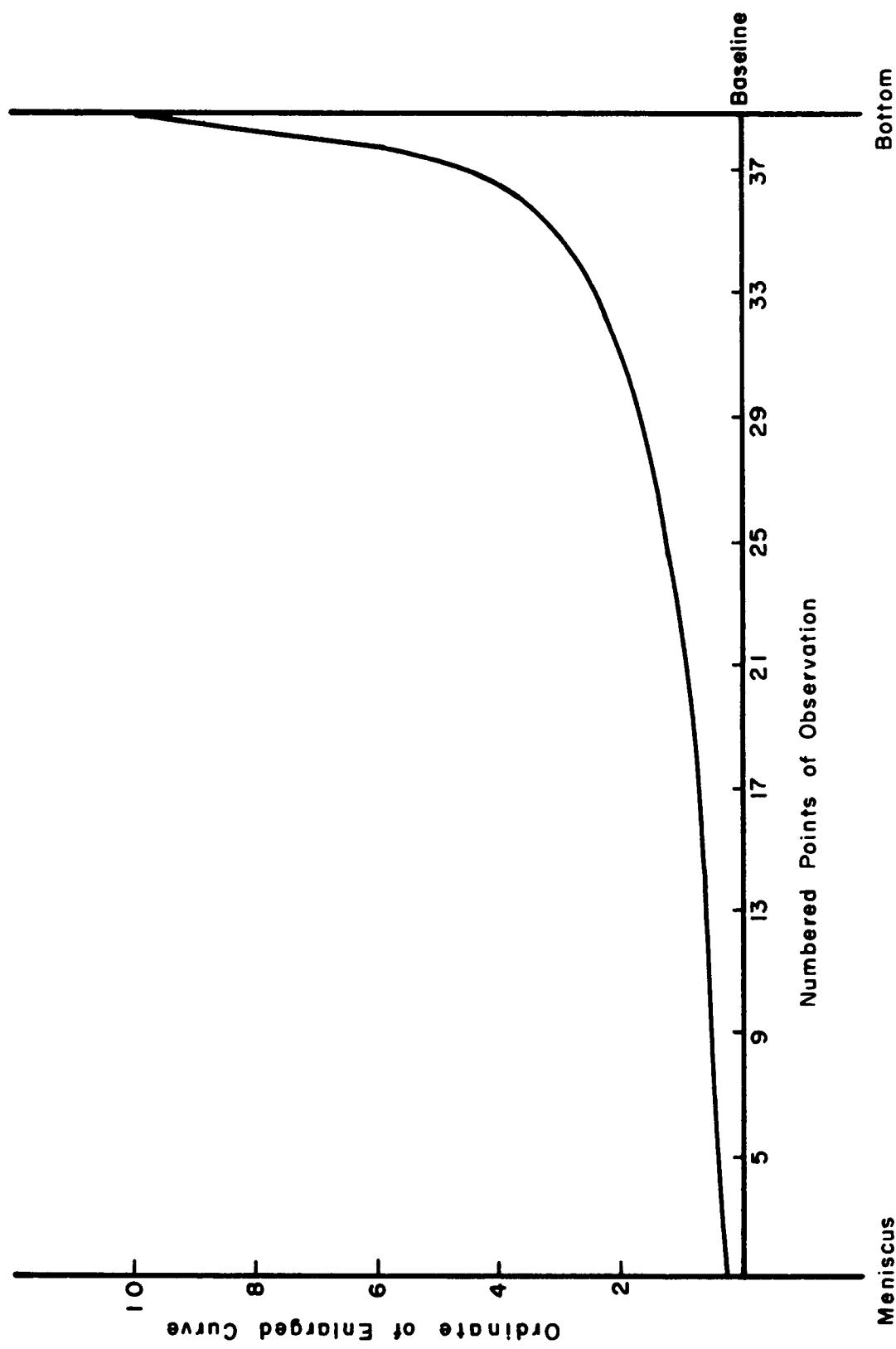


Figure 5. Schlieren Curve for Sample 3 at Rotor Speed 10,589 RPM

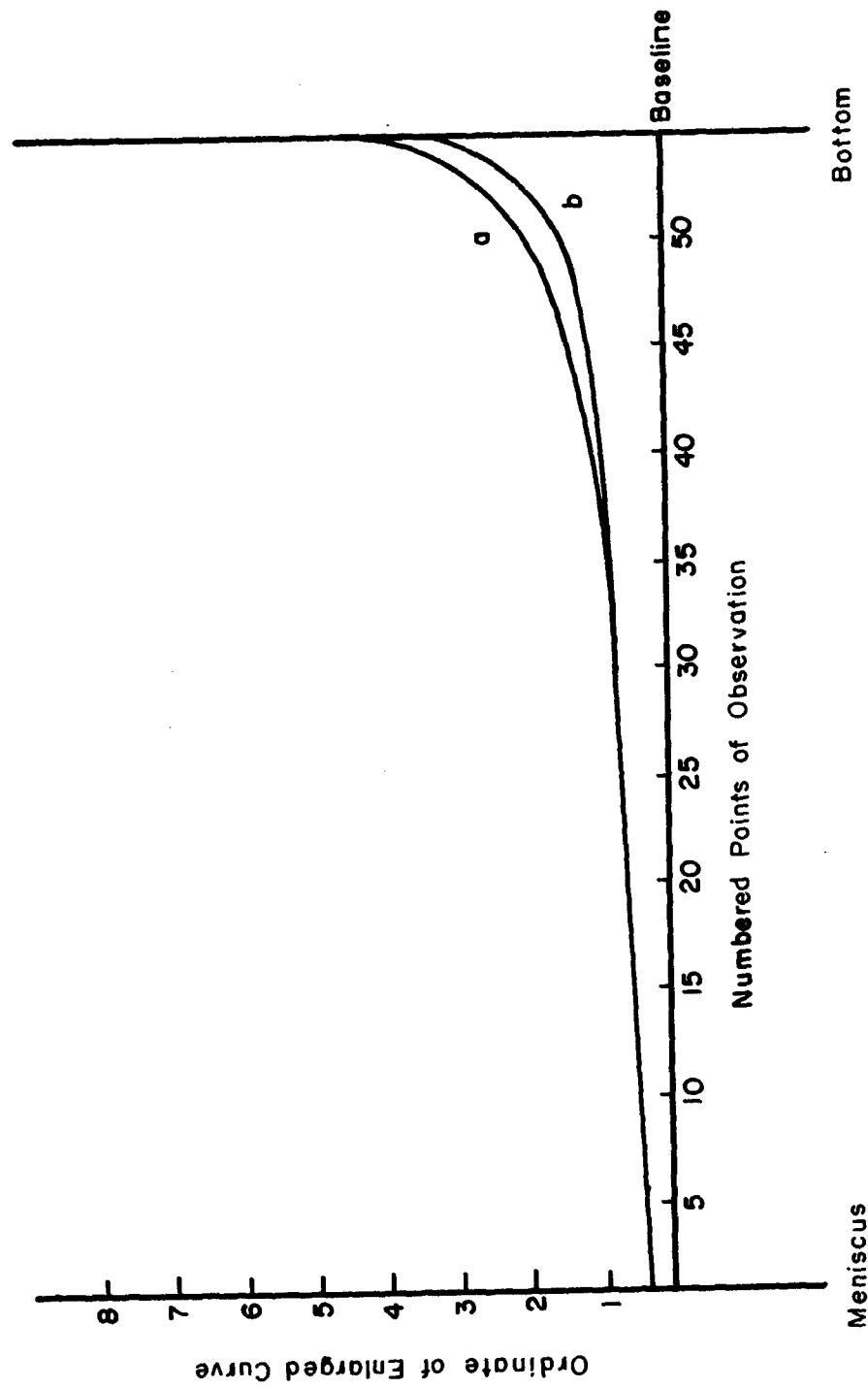


Figure 6. Schlieren Curve for Sample 3 at Rotor Speeds: a) 8,766 RPM; and
b) 7,447 RPM

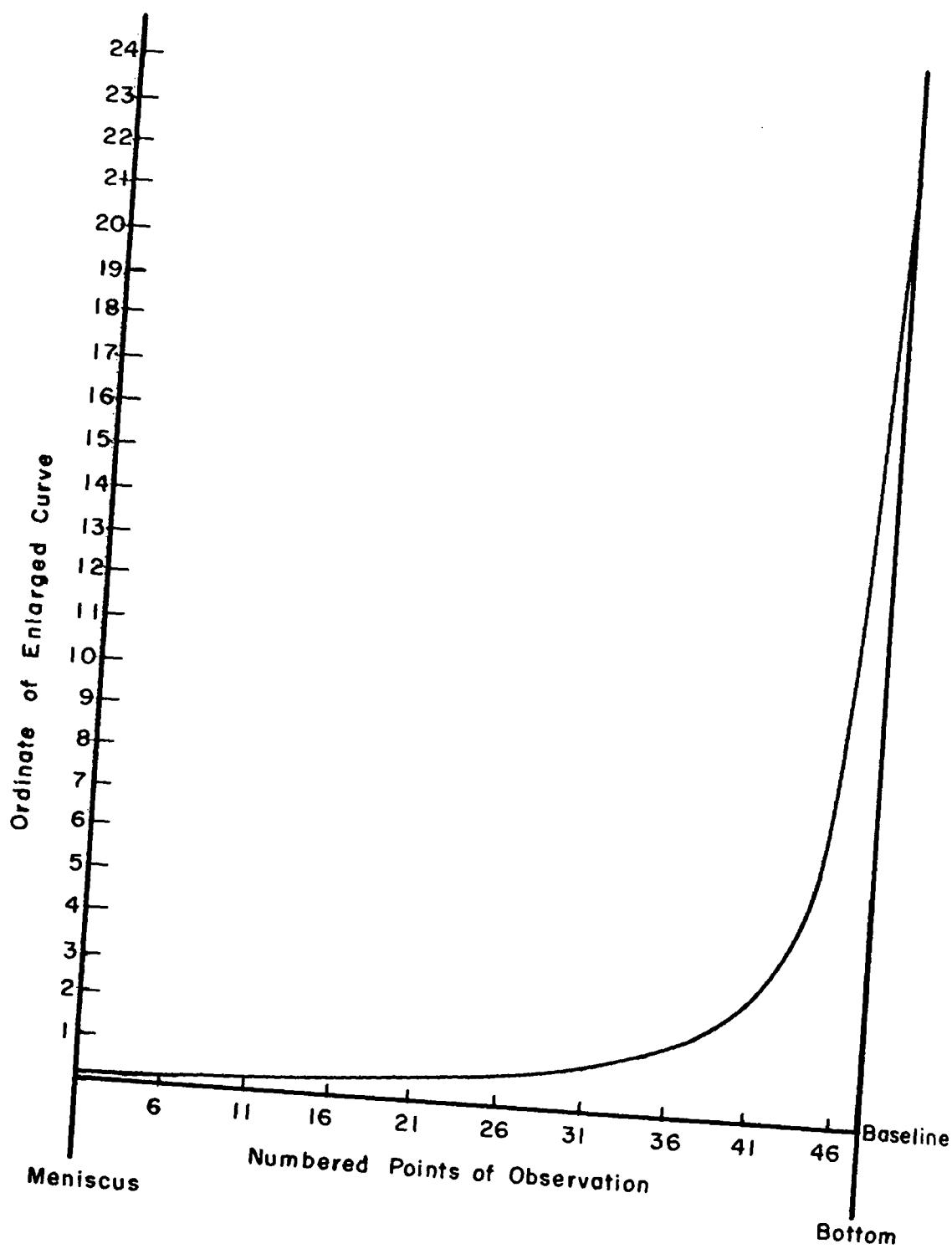


Figure 7. Schlieren Curve for Sample 4 at Rotor Speed 13,410 RPM

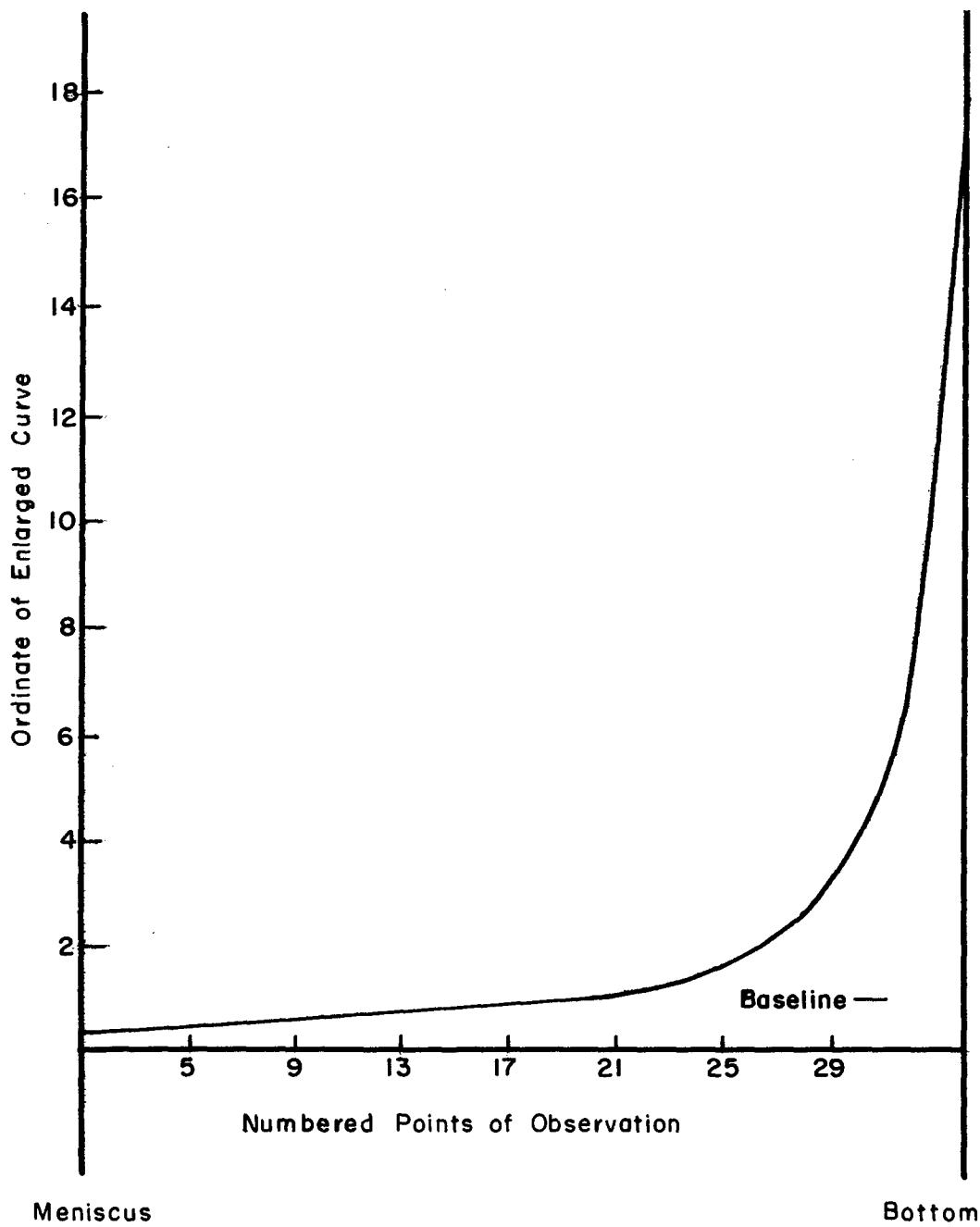


Figure 8. Schlieren Curve for Sample 4 at Rotor Speed 10,589 RPM

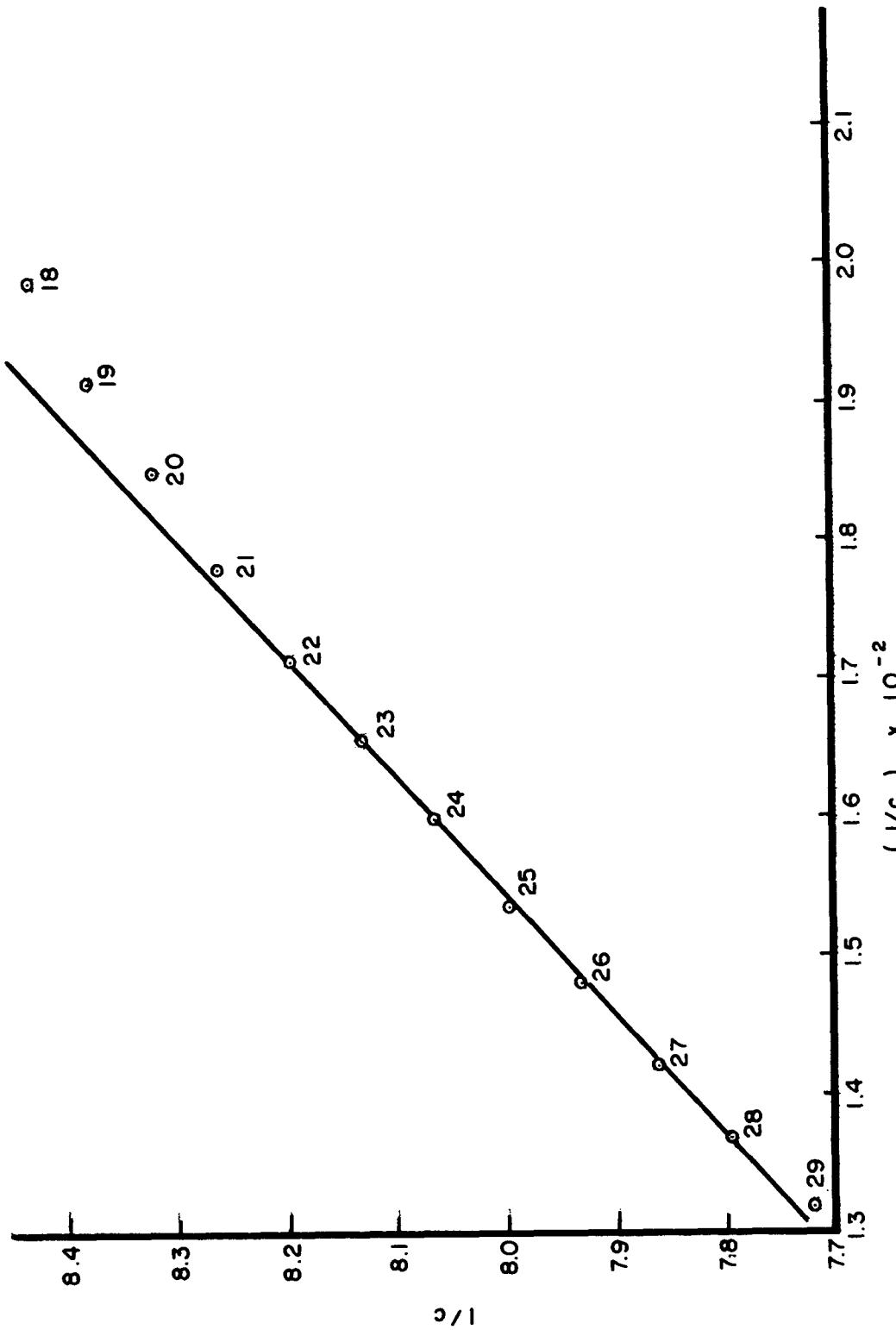


Figure 9. Equilibrium Sedimentation for Sample 1 at 10,589 RPM Showing Slope Equal to $h; \omega_2$

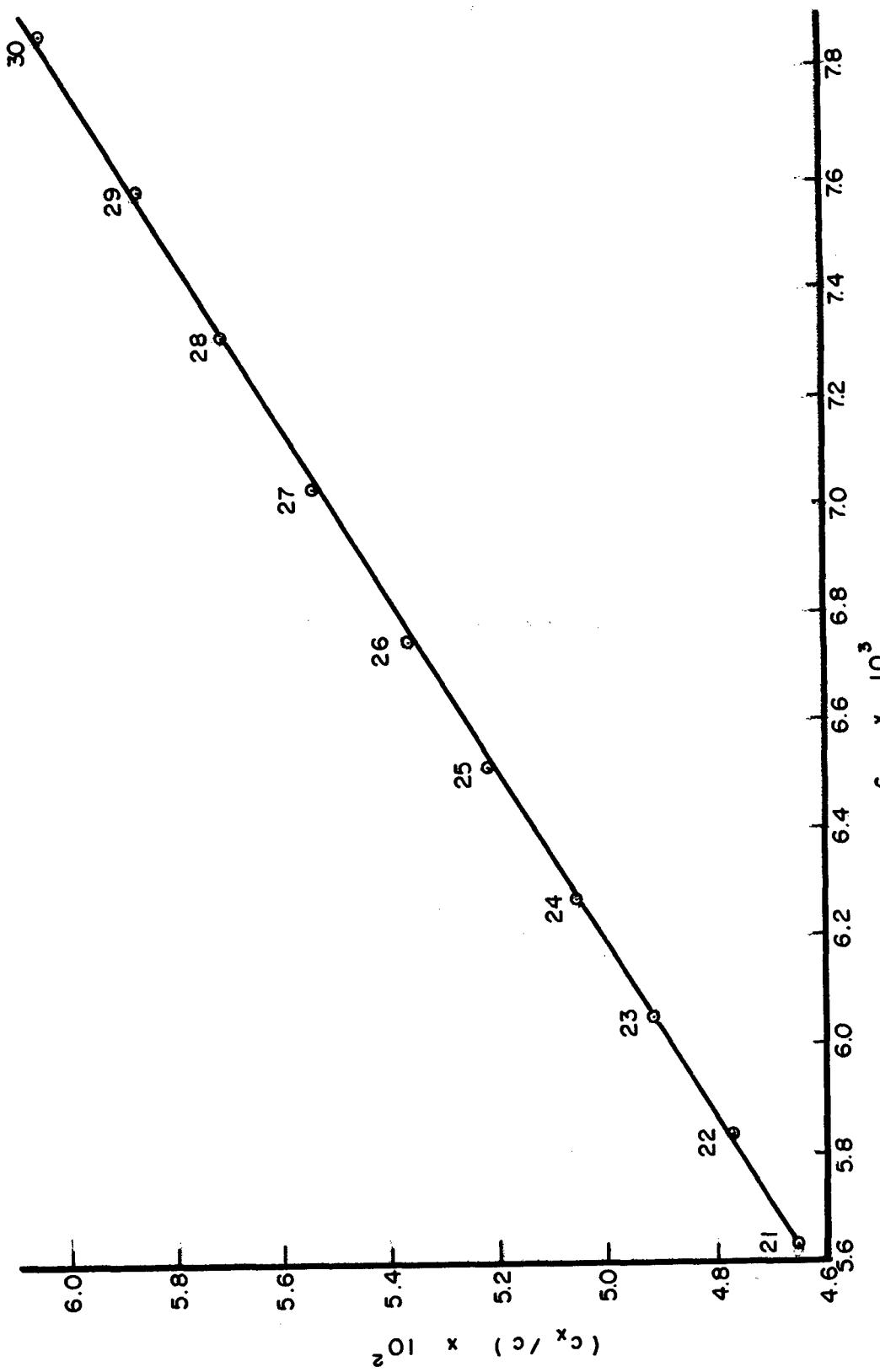


Figure 10. Equilibrium Sedimentation for Sample 1 at 10,589 RPM Showing Slope Equal to $-R_{1,1}$

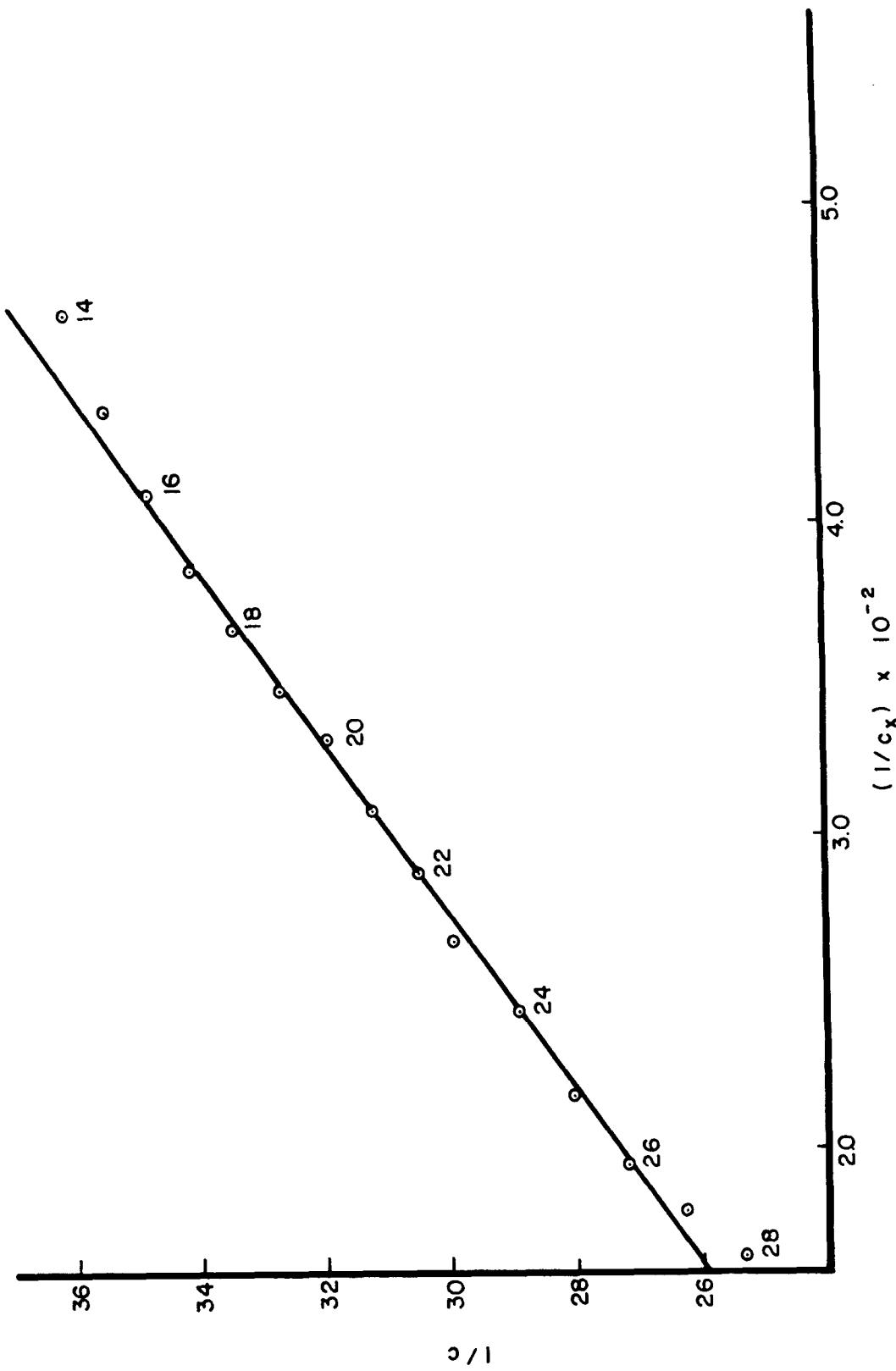


Figure 11. Equilibrium Sedimentation for Sample 2 at 17,250 RPM Showing Slope Equal to h, ω_2^2

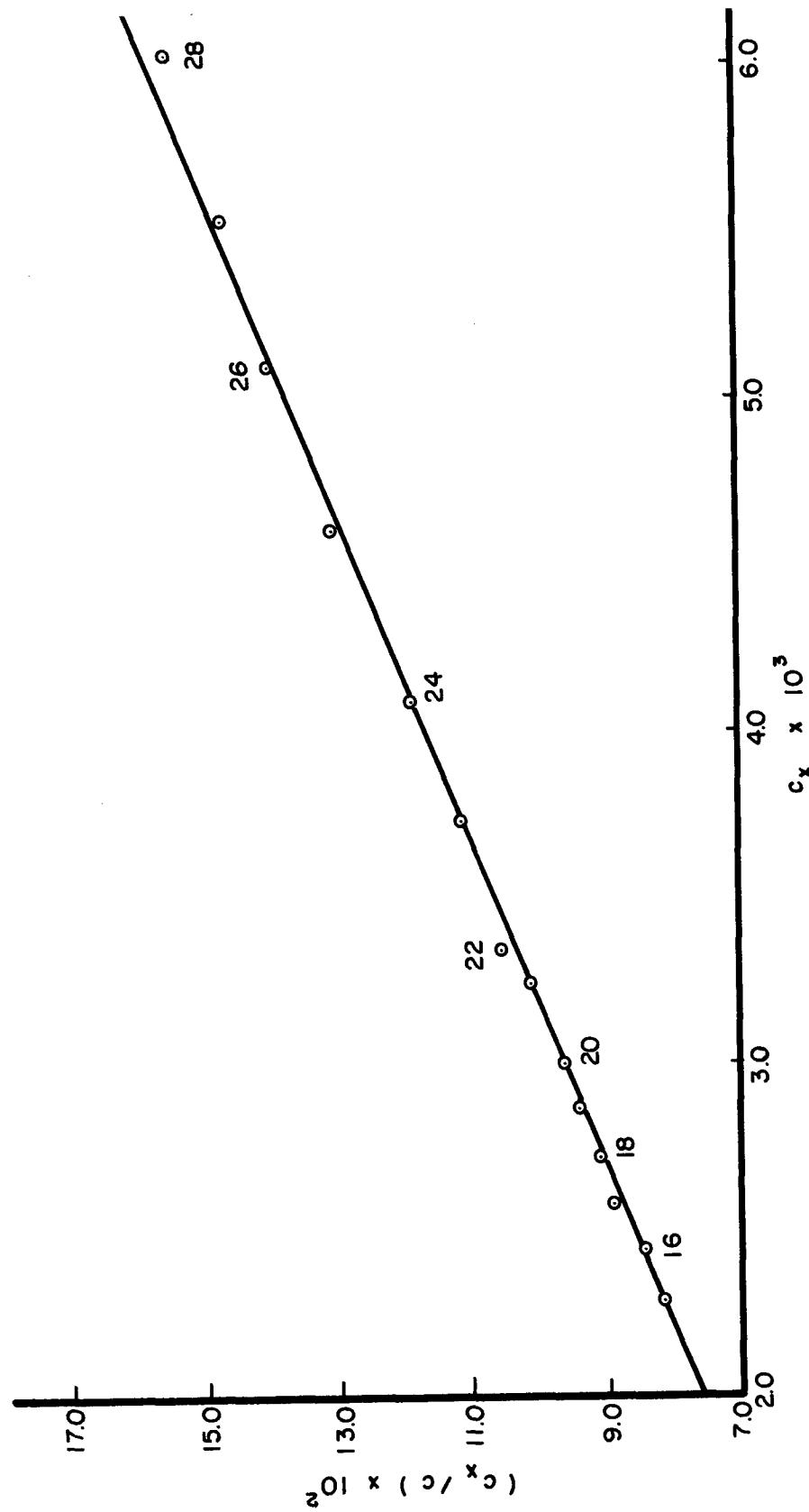


Figure 12. Equilibrium Sedimentation for Sample 2 at 17,250 RPM Showing
Equal to $-R_{1,1}$

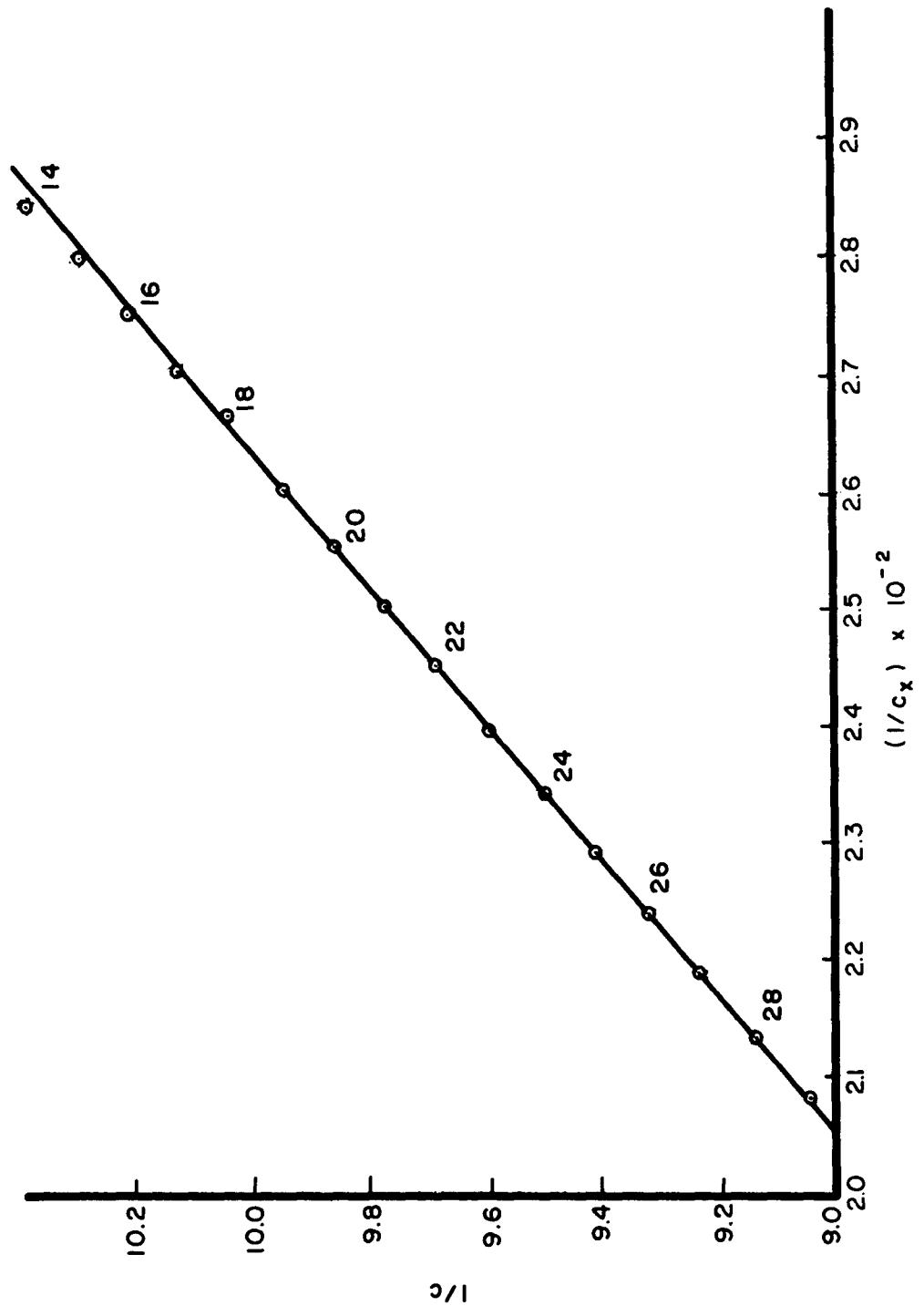


Figure 13. Equilibrium Sedimentation for Sample 3 at 7,447 RPM Showing Slope Equal to $h\omega^2$

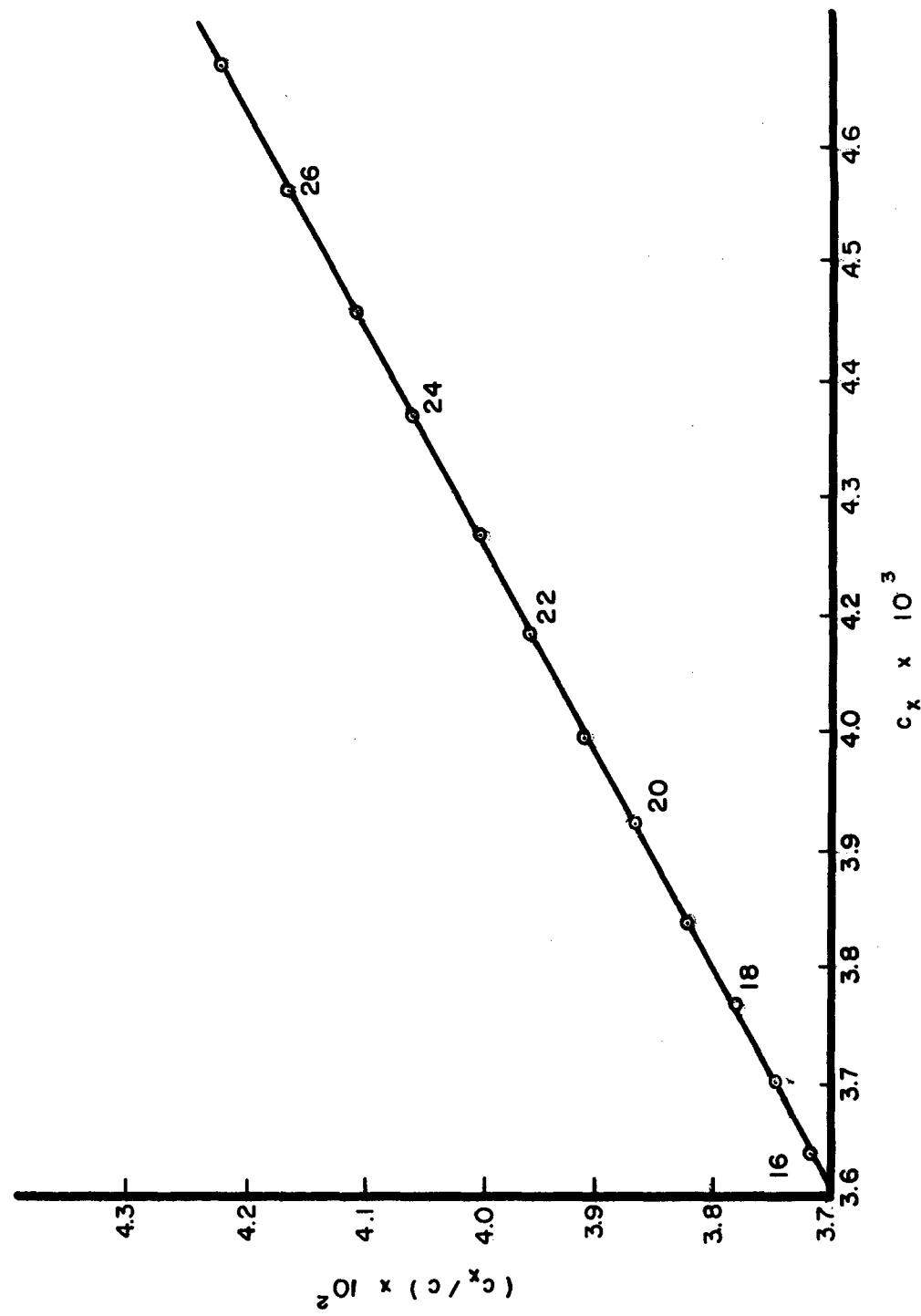


Figure 14* Equilibrium Sedimentation for Sample 3 at 7,447 RPM Showing
Slope Equal to $-R_{L1}$

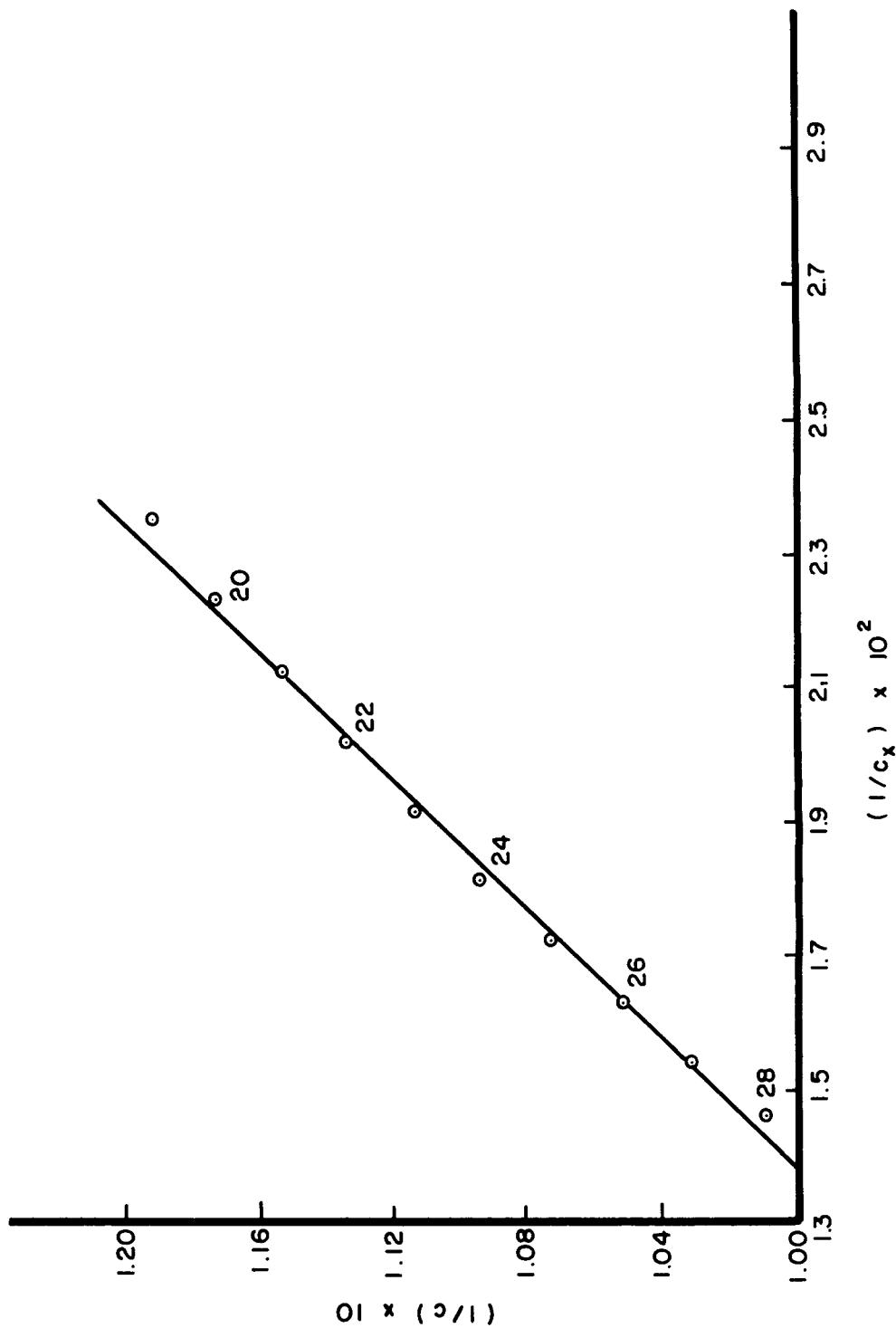


Figure 15. Equilibrium Sedimentation for Sample 4 at 13,410 RPM Showing
Slope Equal to h, ω_2

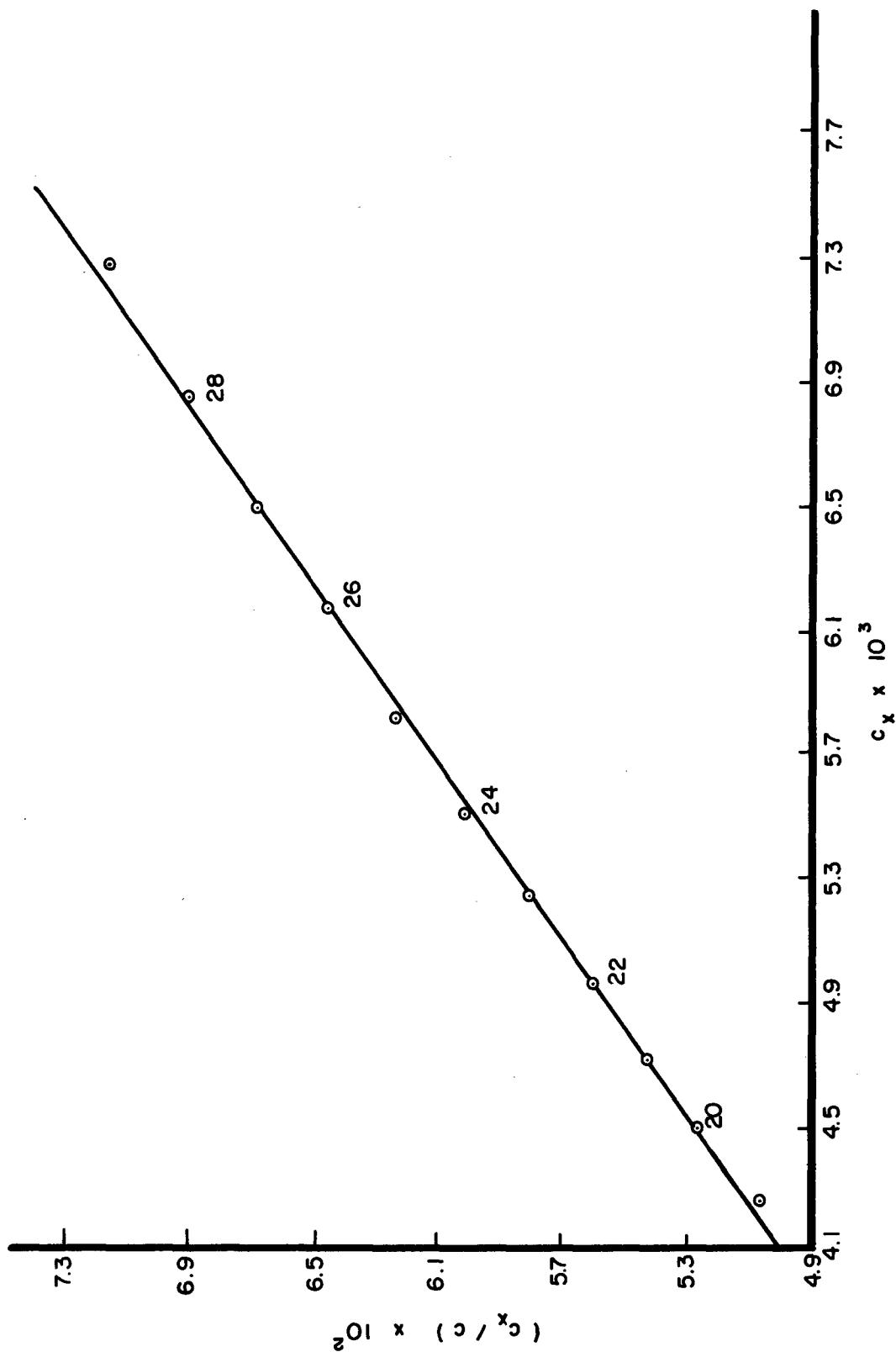


Figure 16. Equilibrium Sedimentation for Sample 4 at 13,410 RPM Showing Slope Equal to $-R_{1,1}$

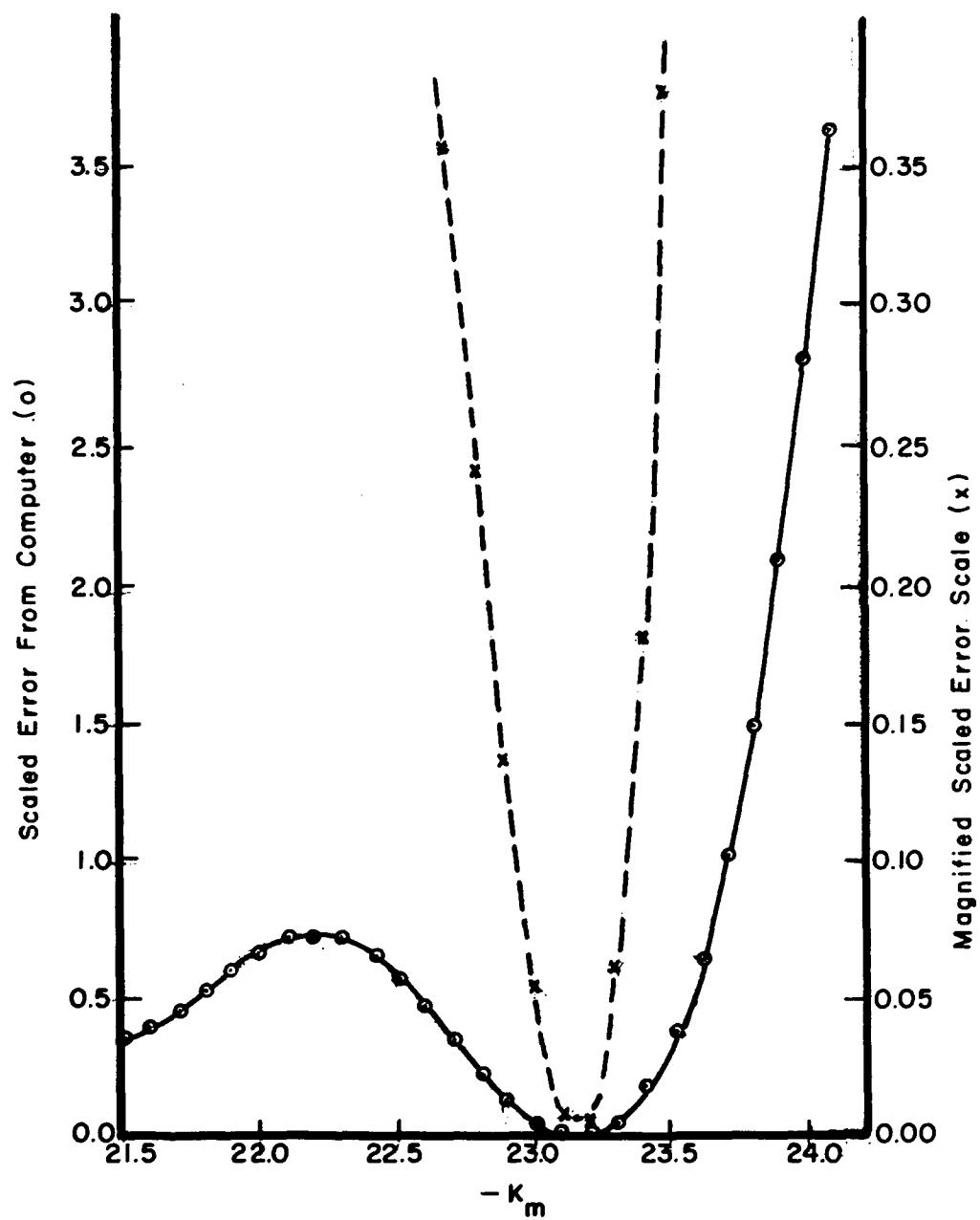


Figure 17. Error Δ_m^2 Vs. $(-K_m)$ for Sample 2 at 17,250 RPM, Indicating a Minimum at $K_m = 23.16$

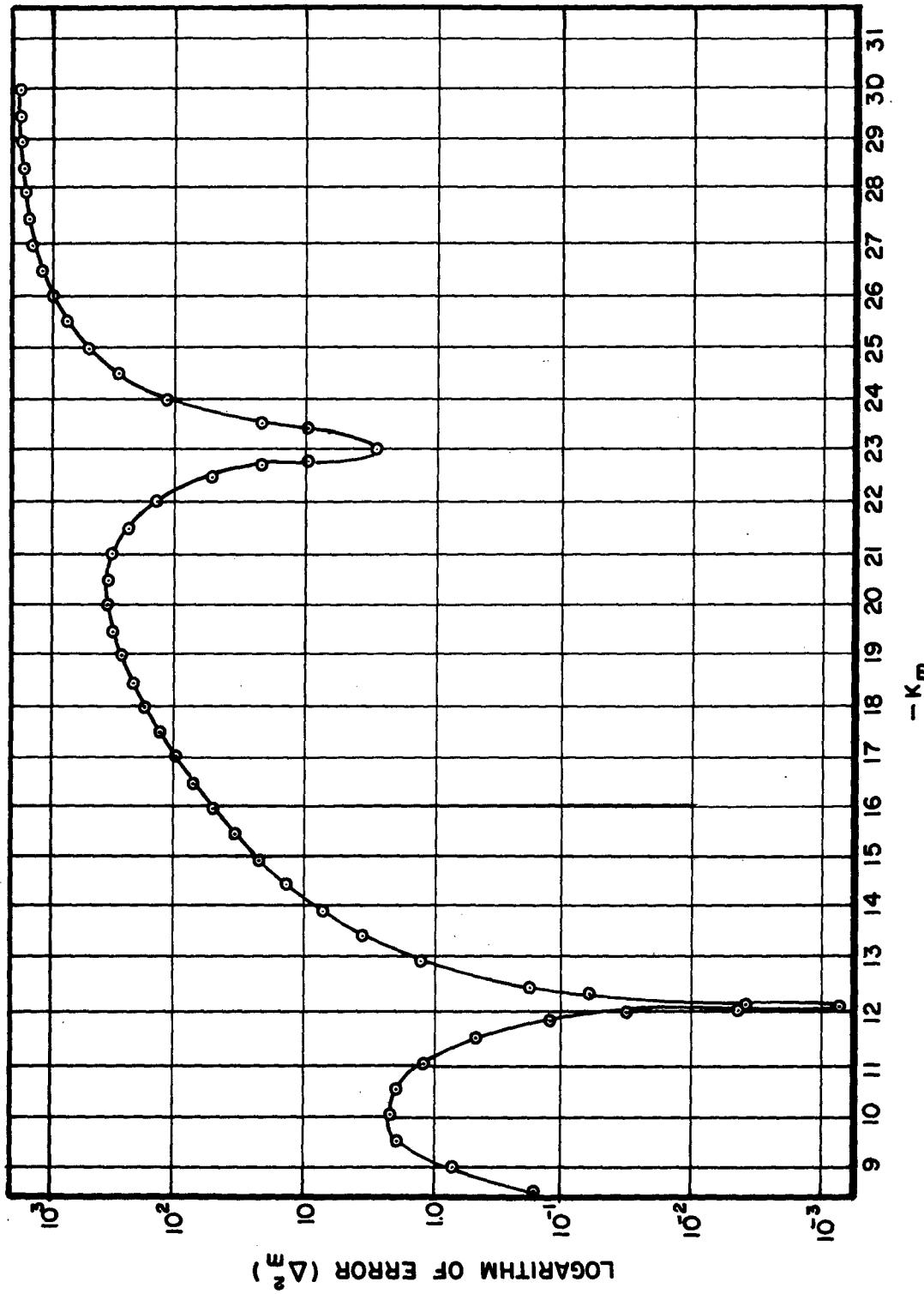


Figure 18. Example of How More Than One Fraction is Predicted (Each Minimum Corresponds to a Value K_m , and, Therefore, a Definite Fraction)

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Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author)

Air Force Materials Laboratory
Wright-Patterson AFB, Ohio 45433

2a. REPORT SECURITY CLASSIFICATION

Unclassified

2b. GROUP

3. REPORT TITLE

Characterization of Very Pauci-Disperse Systems with Strong Interaction by Equilibrium
Sedimentation
Part I. Determination of Molecular Weights and Partial Evaluation of Interaction Matrix

4. DESCRIPTIVE NOTES (Type of report and inclusive dates)

Summary Report (January 1968 to April 1969)

5. AUTHOR(S) (First name, middle initial, last name)

Matatiahu T. Gehatia
Donald R. Wiff

6. REPORT DATE

January 1970

7a. TOTAL NO. OF PAGES

64

7b. NO. OF REFS

4

8a. CONTRACT OR GRANT NO.

9a. ORIGINATOR'S REPORT NUMBER(S)

b. PROJECT NO.

AFML-TR-69-235

c.

Part I

d.

9b. OTHER REPORT NO(S) (Any other numbers that may be assigned
this report).

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11. SUPPLEMENTARY NOTES

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13. ABSTRACT

Samples of dilute solutions of poly-2,2' (m-phenylene -5,5' bibenzimidazole) (PBI) in DMAC have been subjected to equilibrium sedimentation at 40°C. Each sample was composed of a very few distinct fractions, between 1 and 4. Since sedimentation of PBI in DMAC is characterized by strong concentration dependence, an appropriate computational method has been developed based on the formula:

$$c \approx \sum_{n=1}^N g_n \exp \left[h_n \omega^2 x - R_{nk} c + (R_{nk} - R_{nn}) c_n \right],$$

This method led to determination of molecular weights and other parameters characterizing fractions which appeared in each sample.

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14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Ultracentrifugation Equilibrium Sedimentation Polydispersity PBI Concentration Dependence Theory						

UNCLASSIFIED

Security Classification