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Passive Microwave Measurements of Sea Surface Temperature

by D.G. Shipley
K.J. Terek

Final Report
Contract No. N00014-69-C-0245
NR-387-043

Prepared for:

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SECTION I

ABSTRACT

RCA Astro Electronics Division under Contract Number N00014-69-C-0245, sponsored by the Geography Branch of the Office of Naval Research (ONR), conducted a field experiment to verify a theoretical approach toward remote sensing of sea surface temperature using passive microwave radiation.

There is a correspondence between the radiometric temperature of sea water and its thermometric temperature. This correspondence is influenced by the horizontal and vertical emissivity, the incidence angle at which the radiometric measurement is made, contaminants on the water surface, and by the sea surface roughness.

This experiment addressed itself to two questions.

- I Can one measure the vertically and/or horizontally polarized radiometric emissions from the sea water and obtain an accurate measure of the thermometric temperature
- II Can one also make a determination of the sea state from such measurements

Radiometric measurements of sea water temperatures were made from a site on the Chesapeake Bay during July and August 1969. The bulk of the measurements were made at a frequency of 16.5 GHz.

The following conclusions are drawn from an analysis of the data collected during these measurements.

- I There is a correlation between the thermometric temperature and the vertically polarized radiometric temperature. In this particular experiment a sea state invariant angle was observed to fall in the zenith angle range of 103° to 114° .
- II There was no observed correlation of thermometric temperature with the horizontally polarized radiometric temperatures.
- III While theoretical considerations strongly indicate that the horizontally polarized radiometric temperatures should have a strong dependency on sea state, no definitive trends were found in the measured data.

SECTION II

INTRODUCTION AND SUMMARY

A. Introduction

RCA Astro Electronics Division under Office of Naval Research Contract Number N00014-69-C-0245 conducted an experiment to verify a theoretical approach of remote sea surface temperature sensing. The passive radiometric radiation from the sea surface is partially dependent on the thermometric temperature. The vertically and horizontally polarized components of the radiation can be measured separately and from these measurements it should be possible to derive the thermometric temperature. Passive microwave measurements were made with a microwave radiometer from a site on the Chesapeake Bay. The analysis and results of these measurements are presented in this report.

Remote sensing of ocean surface and subsurface features is of interest to a large number of ocean and marine users. Scientists, meteorologists, engineers, fishermen and commercial shippers all have requirements which makes remote sensing by aircraft or satellite economically practical.

Measurement of ocean surface roughness, i.e. sea state, surface temperature, biological growth, current, floating objects and pollutants has been shown to be possible. Fish schools leave characteristic oily patches and other patterns which aid in their detection. Kelp beds and algae blooms have been detected by radar and infrared photographic techniques. Mapping of sea-ice distribution has been achieved by aircraft and satellite observations. Ocean currents, thermal distribution, mud and silt deposits and movements, saline and fresh water distribution in deltas and estuaries, and atmosphere-sea interaction are of interest. These also may be measured or inferred from remote observations.

These remote observations may be made by a number of methods. To date the bulk of aircraft and satellite observations have been made with photographic and infrared techniques. Other techniques are available including active and passive radar and microwave radiometry. Microwave radiometry has been shown theoretically capable of performing as a competent sensor for many of the aforementioned applications. Aircraft tests have proven feasibility with existing equipment. Microwave

radiometers have flown on earth orbiting and planetary exploration spacecraft. Microwave radiometry has the capability of seeing through cloud cover, and frequencies can be chosen where the atmospheric absorption is low. These advantages provide all weather day-and-night capability in remote sensing. This experiment used a radiometric receiver and the passive microwave radiation from the sea to determine sea surface temperature.

Environmental scientists and meteorologists have demonstrated that long range weather prediction and determination of the atmospheric and oceanic circulation must treat the total fluid envelope of the earth, air and water, as a continuous physical entity. The transfer of momentum, mass, and heat through the sea-air interface is the key process whereby the oceans, as storehouses of heat and moisture, influence longer term atmospheric circulation changes; the atmosphere, in turn, drives the ocean currents and mixes the upper layers of the sea.

An important parameter in the description of these vital dynamical and physical processes is the sea surface temperature. It delineates the heat sources and sinks at the ocean surface and hence, the regions of moisture and heat flux within the atmospheric boundary layer. This, in turn, influences low-level atmospheric stability and bears heavily on the occurrence of cloudiness and the development of weather systems over the oceans. To an oceanographer, knowledge of sea surface temperature, provides a means of locating and tracking ocean currents and regions of upwelling and, as such, is an additional input to the definition of the three-dimensional ocean circulation and its seasonal variation. In addition, sea surface temperatures mark surface water anomalies such as eddies, ocean fronts, estuary effluents, plankton blooms, and extensive areas of seaweed. The biological reflections of sea surface temperature seem to account for the importance of these data to the fishing industry. Sea surface thermal anomalies have also been found to be associated with underwater volcanic eruptions.

Currently, sea surface temperature data that are routinely available are concentrated along the heavily travelled shipping routes of the North Atlantic and North Pacific Oceans. Extensive areas of the Northern Hemisphere and essentially all of the Southern Hemisphere have very sparse, if not nonexistent, regular coverage. For many of the Navy's and ESSA's needs, full global sea surface temperature data are required from one to four times per day. The Navy's mission is clearly a global one. Sea surface temperature data are vitally needed to forecast the temperature structure of the thermocline and the many aspects of sound propagation throughout the oceans. Global sea surface temperature data are an integral requirement for the World Weather Watch, now being implemented by all the member nations of the World Meteorological Organization.

Earth orbiting satellites have proven themselves to be efficient platforms for frequent observations of all of the earth's surface. Indeed, each TIROS Operational Meteorological Satellite is capable of viewing all of the earth's surface twice each day. It would be most desirable to place a sensor for observation of sea surface temperature on these satellite platforms to provide vital data to environmental scientists. Some experimental sea surface data have been obtained from TIROS and Nimbus weather satellites using infrared sensors operating in the major atmospheric window at wavelengths from 8 to 12 microns. However, infrared sensors are severely limited in their capability to view the earth's surface from space in that almost all clouds are opaque in this part of the spectrum. Thus, the earth's surface can be seen only in cloud-free areas. The cloud cover pictures from TIROS have shown us that this would be a severe limitation over the oceans; the earth is indeed a cloudy planet. Some high-level cirrus clouds, being composed of ice crystals, are partly transparent to infrared radiation, but their effect at any given time or place could not be known, and, therefore the correction necessary to determine the actual radiance from the sea surface could not be known.

The problems of viewing the earth in the infrared spectrum has suggested the possible use of passive microwave radiometers. In much of the lower microwave region of the spectrum, only the relatively restricted areas of heavy precipitation would prevent a spaceborne radiometer from "seeing" the earth's surface. The complication that arises in using passive microwaves for remotely sensing the sea surface temperature is that the emissivity of the surface is a function of both the thermometric temperature and the roughness of the sea surface. The two effects must be separated without prior knowledge of the sea state. The purposes of this experiment was to verify experimentally a theoretical approach to remote radiometric sensing of sea surface temperatures.

The implementation of the experiment and the subsequent data analysis was directed toward two basic questions:

- A. Can the thermometric temperature of the surface of the sea be determined in a sufficiently accurate manner by radiometric measurements and would the method of measurement be applicable to aircraft or satellite systems?
- B. Can a sufficiently accurate measure of the surface roughness of the sea i.e., sea state, be determined by similar radiometric means?

To implement this experiment a mobile radiometric van was subleased from GCA Corporation, Bedford, Mass. This van had radiometric equipment designed for operation at 9.5, 16.5 and 94 GHz. This equipment, supported by additional ground truth observation instrumentation was set up on an island site in the Chesapeake Bay and a series of radiometric measurements were made. The operation of the equipment and subsequent data reduction and analysis was performed by personnel from RCA Astro Electronics Division.

In co-operation with RCA, personnel from the National Environmental Satellite Center (NESC) of the Environmental Science Services Administration (ESSA) supplied and operated an infrared radiometer in conjunction with the microwave radiometric measurements. The IR radiometer was a Barnes Engineering Company Model PRT-5 which has a spectral response from 8 to 16 micrometers. Its temperature range is 212°K to 338°K with a long term stability of $\pm 0.5^{\circ}\text{K}$.

B. Summary of Results

The bulk of the radiometric measurements were made at 16.5 GHz using both horizontal and vertical polarization. The radiometric temperature of the vertically polarized runs correlates with the thermometric temperature of the sea water and shows a sea state invariant zenith angle range from about 103° to 114° . At 109° , the median zenith angle of this range, the average radiometrically derived temperature of the vertical runs is 299°K with a standard deviation of about 5°K . The nominal average thermometric temperature of the sea water was 299°K .

The horizontally polarized radiometric measurements were used to derive apparent water temperature and horizontal emissivity. Neither of these shows any direct correlation with sea surface roughness (sea state). This is in contradiction with accepted theory and may be due to equipment sensitivity limitations and restrictions on the viewing angle at the site.

The horizontal runs do not show any direct correlation with sea water temperature.

SECTION III

BASIC THEORY

A. Radiometric Principles

Radiometric measurements of sea water are based on the principle that thermally emitted and reflected radiation from the sea are partially polarized. The amount of radiation received from the sea will be dependent upon the polarization, temperature of the sea, angle of observation and the temperature of any source reflected by the sea.

For a specular sea water surface the relationship between these parameters is expressed by:

$$T_b = \epsilon T_w + (1-\epsilon)T_r \quad (1)$$

where

- T_b = measured radiometric brightness temperature
 T_w = thermometric sea water temperature
 T_r = temperature of reflected source
 ϵ = emissivity

Equation (1) could be subscripted with either H or V to denote horizontally or vertically polarized conditions.

The relationship between emissivity, reflectivity, dielectric permittivity, (i.e. dielectric constant and loss factor) and observation angle is developed in Appendix A.

A non-specular surface would be expected to behave somewhat differently than indicated in equation (1). This would be inferred if one considers the surface of a rough sea. In this case, the observation angle of the sea surface is a function of the slope of the wave fronts and may best be described as a "cone" of angles about an average value. The size of the cone will be dependent upon the height and period of the wave and of the observation time. This indicates that the "apparent" emissivity of non-specular water should differ from that of specular sea water. It is also possible that there may be a range of observation angles

(or a specific angle) where the specular emissivity and the non-specular "apparent" emissivity coincide. If this condition existed one could define an invariant observation angle where the "sea state" has no effect on the observed temperature. As a corollary to this it would appear that the observed brightness temperature at other than an invariant angle should be dependent upon the roughness of the sea. Thus it should be possible to derive sea state from a series of radiometric measurements.

B. Emissivity of Sea Water

The equations for the vertical and horizontal emissivities of sea water are developed in Appendix A. These equations show the emissivity to be a function of the dielectric permittivity and the observation angle. The horizontal and vertical emissivities of sea water are shown in Figure III-1 for a frequency of 16.5 GHz.

The dielectric permittivity of sea water is a function of frequency, salinity, and temperature. The relationship of dielectric permittivity, frequency, salinity and temperature is developed in Appendix B.

C. Temperature Determination

Referring to equation (1), sky radiation is the dominant contributor to T_r in sea water radiometric measurements. Thus equation (1) can be rewritten:

$$T_b\phi = \epsilon_\phi T_w + (1-\epsilon_\phi)T_s\theta \quad (2)$$

where

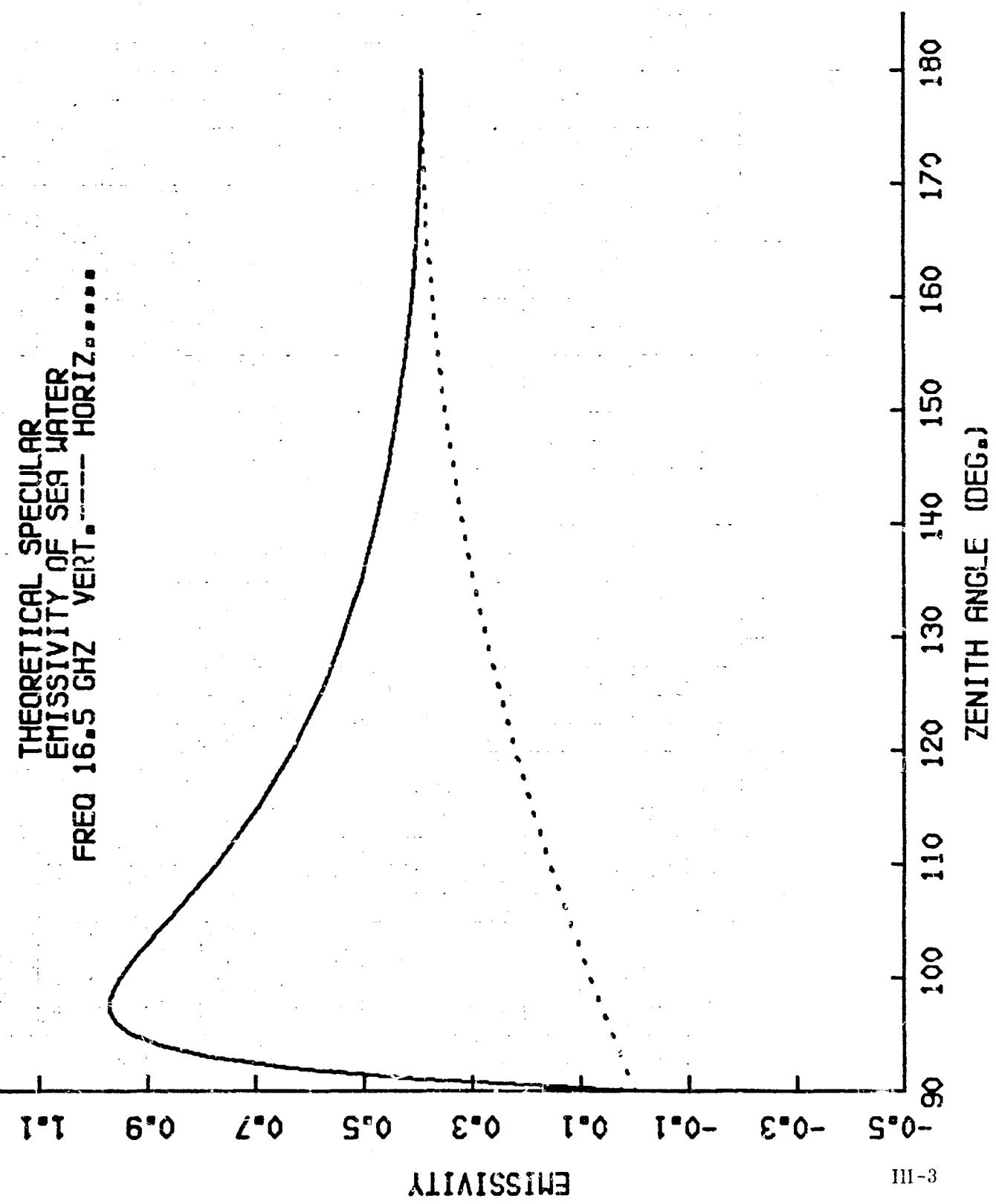
T_s = the sky temperature

ϕ = observation angle

θ = $180 - \phi$

For purposes of definition the angle ϕ will henceforth be referred to as the zenith angle, that is the angle measured from the upward pointing local vertical. This angle and definition will be used throughout this report.

At a given zenith angle, assuming the salinity to be constant, the emissivity becomes only a function of water temperature. If values of T_b and T_s were measured then there would be only one unique value of T_w which would satisfy equation (2). This type of calculation is easily accomplished with a computer by iterating values of T_w , calculating the value of ϵ and then using T_w , ϵ and T_s to calculate the value of T_b . This process is repeated until a value of T_b is calculated which is sufficiently close to the measured value of T_b . The final value of T_w is then the unique value which satisfies equation (2). This value of T_w would be equal to the thermometric temperature of the sea water only at the angle where there was an invariance



III-3

FIGURE III-1

with sea state. (This temperature determination method is described in detail in Appendix C, Paragraph C.) Other investigators (Stogryn Ref. 1) have developed curves showing the theoretical dependency of the horizontally and vertically polarized radiometric temperatures upon sea state. Stogryn's work also suggests a stronger dependency of the horizontally polarized temperature on sea state. Thus one would anticipate a correlation of sea water temperature with the vertically polarized radiometric measurements and a correlation of sea state with the horizontally polarized radiometric measurements.

Other methods for deriving water temperature from radiometric measurements have been suggested. Some of these are discussed in Appendix C.

SECTION IV

SITE AND EQUIPMENT DESCRIPTION

A. Field Site Location and Description

The measurements were taken from North Island of the Chesapeake Bay Bridge and Tunnel District. The Chesapeake Bay Bridge-Tunnel is the world's longest bridge and tunnel complex. It links the city of Norfolk and Cape Charles, Virginia, across 17.6 miles of water. North Island is at the northern end of the Thimble Shoal Channel Tunnel.

This is a man made island and is about 1,200 feet long with a maximum width of 220 feet at the channel end. It is approximately 30 feet above mean low water and is surrounded by large rip-rap boulders. The nominal water depth around the island is 30 feet. A large thirty foot high vent building is located above the tunnel entrance at the southern end of the island. This island is black-topped and has a concrete retaining wall around the periphery with the rip-rap boulders sloping outward toward sea level. A two foot high fence about eight feet from the edge of the concrete retaining wall, encircles the island.

The radiometric van was positioned against this fence on the west or bay side of North Island. The side of the van faced Chesapeake Bay. The vent building was on the opposite side of the van about eighty feet away. The azimuth of the radiometric measurements was 310° and the antenna had a zenith angle capability of 0° to 180° . Radiometric observations of the water were possible through zenith elevation angles of 90° to about 125° because the main beam of the antenna intercepted the boulders at about 125° . Figure IV-1, 2 and 3 show three views of the van at the site.

A marker buoy was placed on an azimuth of approximately 280° about a hundred feet from shore. The buoy was held in position with two Danforth anchors and two lines from shore. The shore lines were attached to the buoy through pulleys. One of the pulley lines was used to deploy a series of floating temperature thermistors while the other was used in obtaining surface water samples. Figure IV-4 shows the buoy and the floating temperature sensors in place.

The water depth at the field test site varies from about 20 feet at the near vicinity of the island to nearly 50 feet in the Thimble Shoal Channel. This depth of water permitted a wide range of wave height conditions.

Figure IV-5 shows the field site location and its relationship to other land areas. The prime measurement azimuth of 310° is marked on this figure. A plan view of the island lay-out is shown in Figure IV-6.

B. Equipment Description

The radiometric van was a WW-II model SCR-584 radar trailer that had been converted to a mobile radiometric station in 1964-65. It basically consisted of three r-f heads designed to operate at 9.5, 16.5 and 94 GHz working into a common i-f, video and data recording section. The van equipment included an elevator for raising and lowering the radiometer antenna pedestal. A gasoline-driven primary power generator provided line power. Air conditioning provided for interior temperature control. Two close-up views of the van are shown in Figure IV-7 and IV-8.

The remotely controlled radiometer antenna pedestal permitted positioning of the radiometer antenna beams to an accuracy of 0.2 degrees, over a total useful vertical angle of 180 degrees from zenith to nadir. The pedestal could be turned through 360° in azimuth. Two r-f heads are mounted back-to-back on the pedestal, at opposite ends of a horizontal shaft. A motor, located on the pedestal yoke, permits remote control of antenna polarization by turning the shaft through 90 degrees about the antenna axis. A third r-f head could be readily installed after removal of one of the previously installed heads. Figure IV-9 shows a view of the 16.5 GHz r-f head on the antenna pedestal.

Each r-f head consisted of an antenna, mixer, klystron local oscillator, ambient and hot loads, pre i-f amplifier, and switching networks. The i-f output and thermistor temperature information were coupled to the interior van electronics by cables. The interior electronics consisted of the required power supplies, an i-f amplifier and detector, a video amplifier, a synchronous video detector, output voltmeter and recorder, and the antenna positioning controls. The radiometric output signal was measured with an HP 3440A Digital Voltmeter and was recorded on an HP 562A Digital Printer.

The pertinent design parameters and performance characteristics of the radiometric equipment are summarized in Table IV-1.

TABLE IV-1 RADIOMETER CHARACTERISTICS

| | | | |
|-------------------------------------|--|-----------|---------------|
| Radiometer Type | Double-side band superhetrodyne, chopper stabilized, absolute type. | | |
| Antenna Type | Prime focus paraboloids | | |
| Antenna Polarization | Horizontal and Vertical (Polarization changed by mechanical rotation) | | |
| Antenna Diameter and 3dE Beamwidths | | | |
| | Frequency | Diameter | 3dB Beamwidth |
| | 9.5 GHz | 19 inches | 5.5° |
| | 18.5 GHz | 16 inches | 3.7° |
| | 94 GHz | 6 inches | 1.6° |
| IF 3dB Bandwidth | 100 MHz | | |
| Internal Calibration | Two waveguide terminations whose temperatures can be measured to within $\pm 0.2^{\circ}$ by internal thermistors. Nominal temperatures are: Hot Load 400°K, Cold Load 300°K | | |
| Video Amplifier and Detector | Locked video amplifier and synchronous detector | | |
| Integration Time | 1.0 second (other integration times were available) | | |
| Radiometric Sensitivity | 9.5 GHz | 16.5 GHz | 94 GHz |
| | 0.92°K | 1.13°K | Not measured |

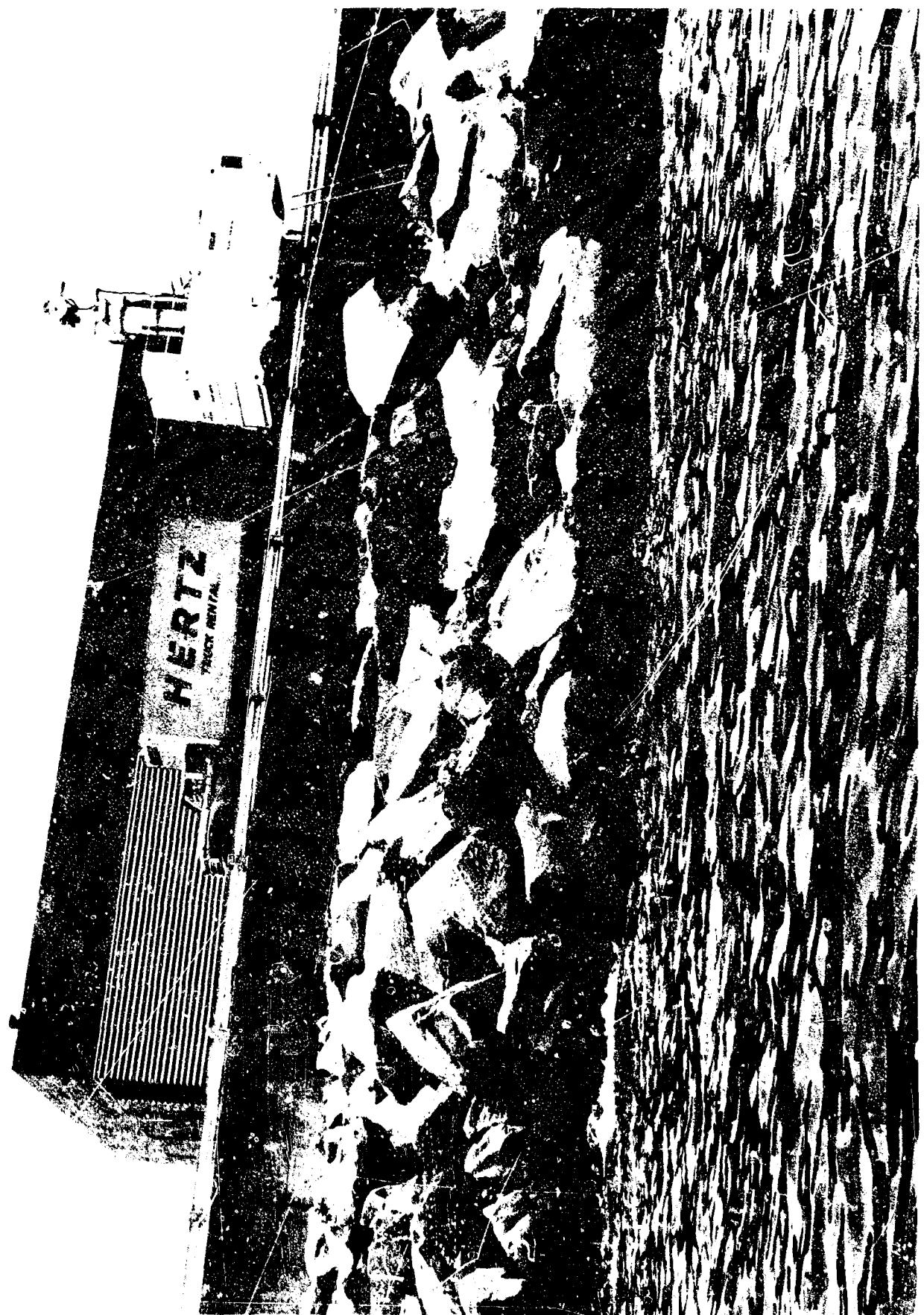


Figure IV-1. Experiment Site

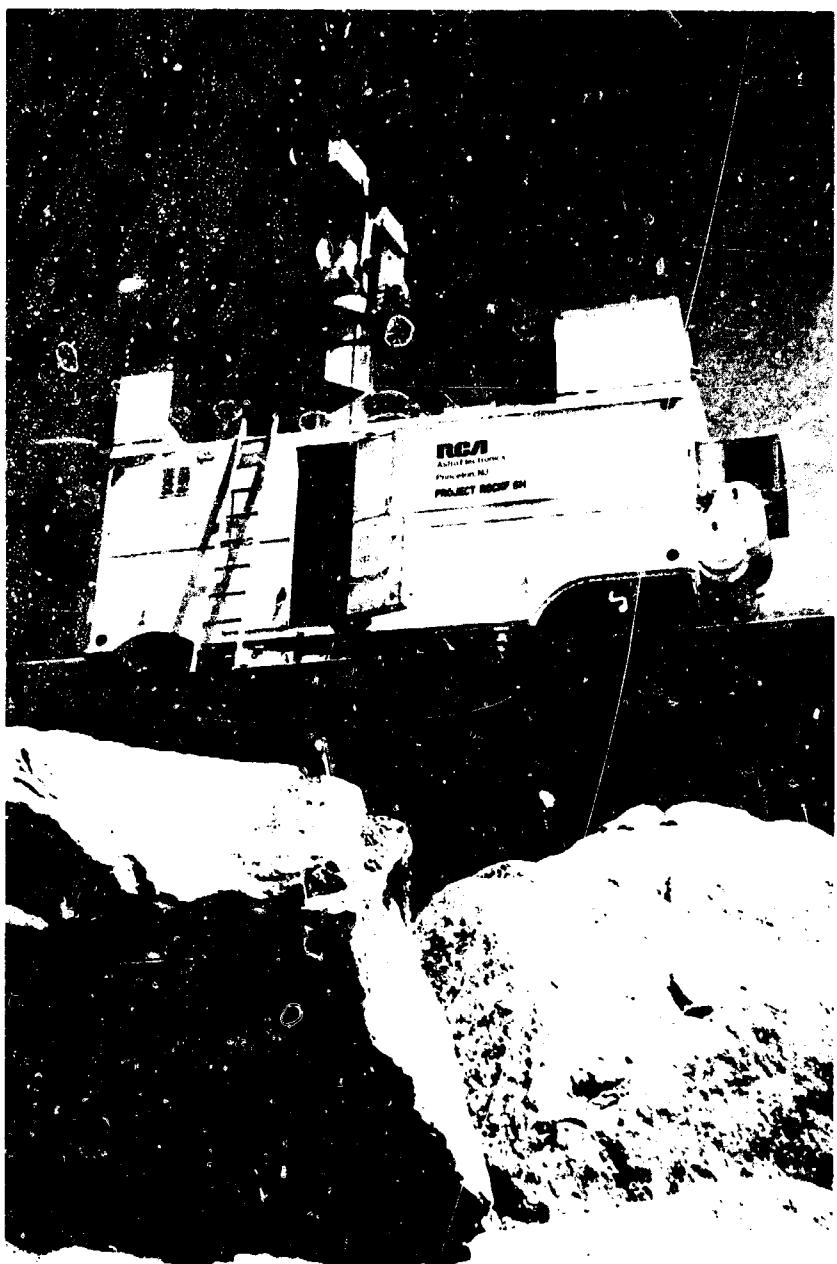


Figure IV-2. Radiometric Van at the Site

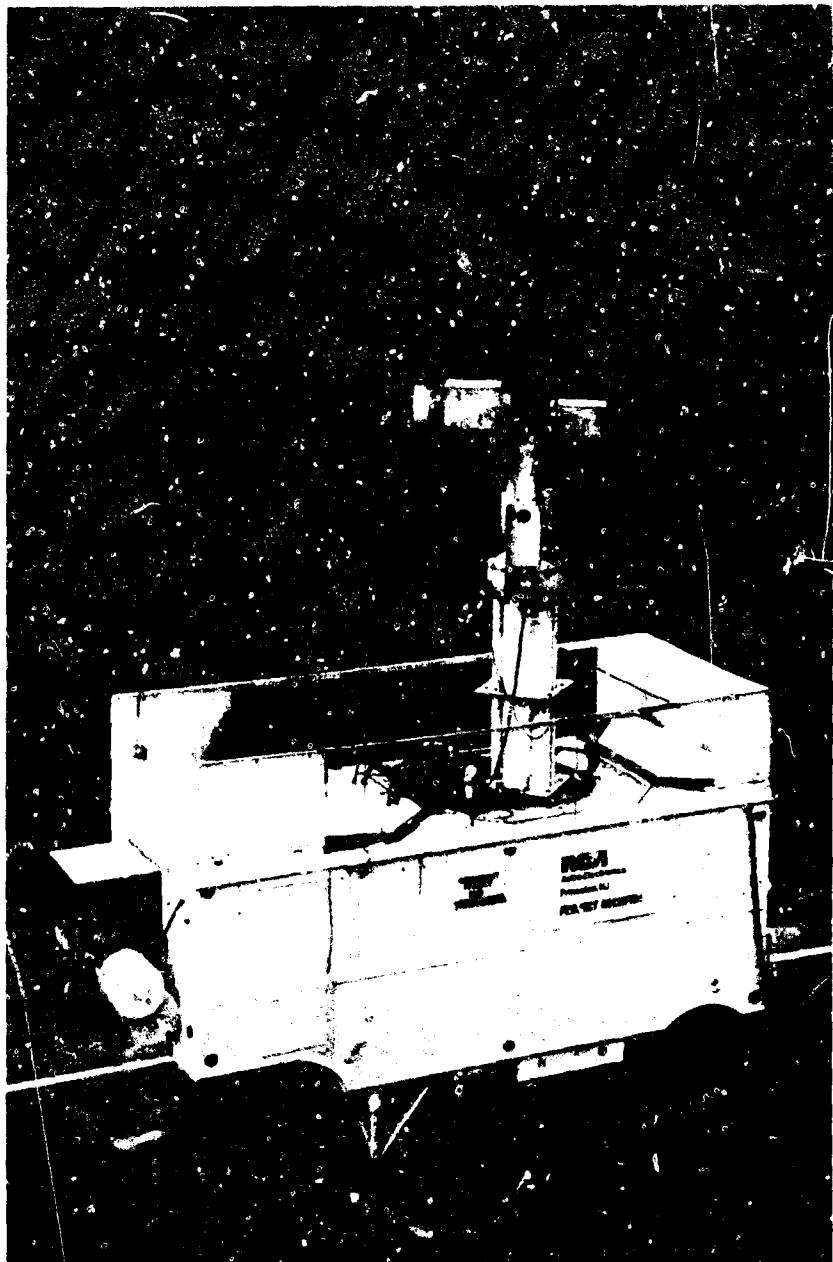


Figure IV-3. Radiometric Van

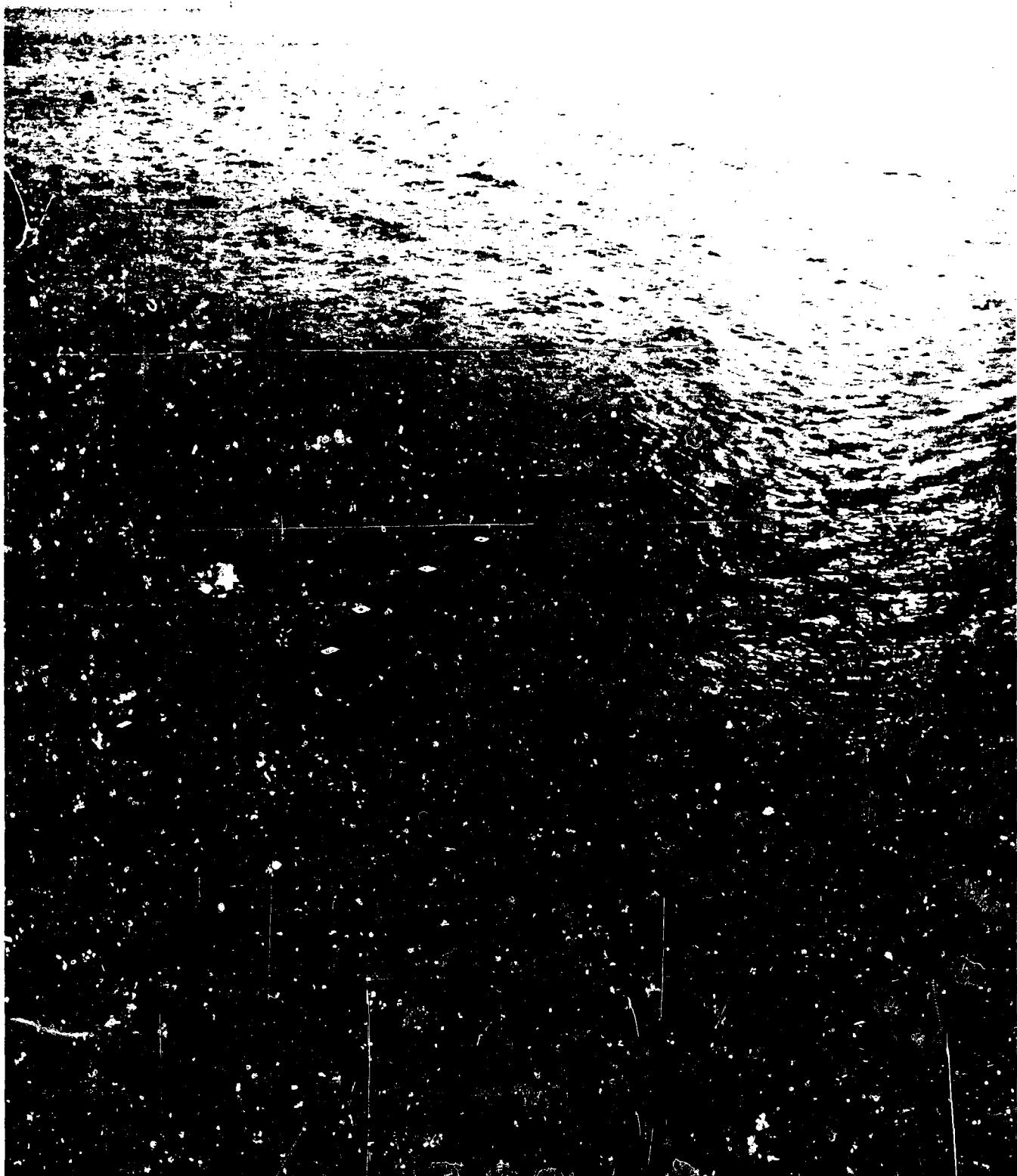


Figure IV-4. Marker Buoy and Floating
Temperature Sensors

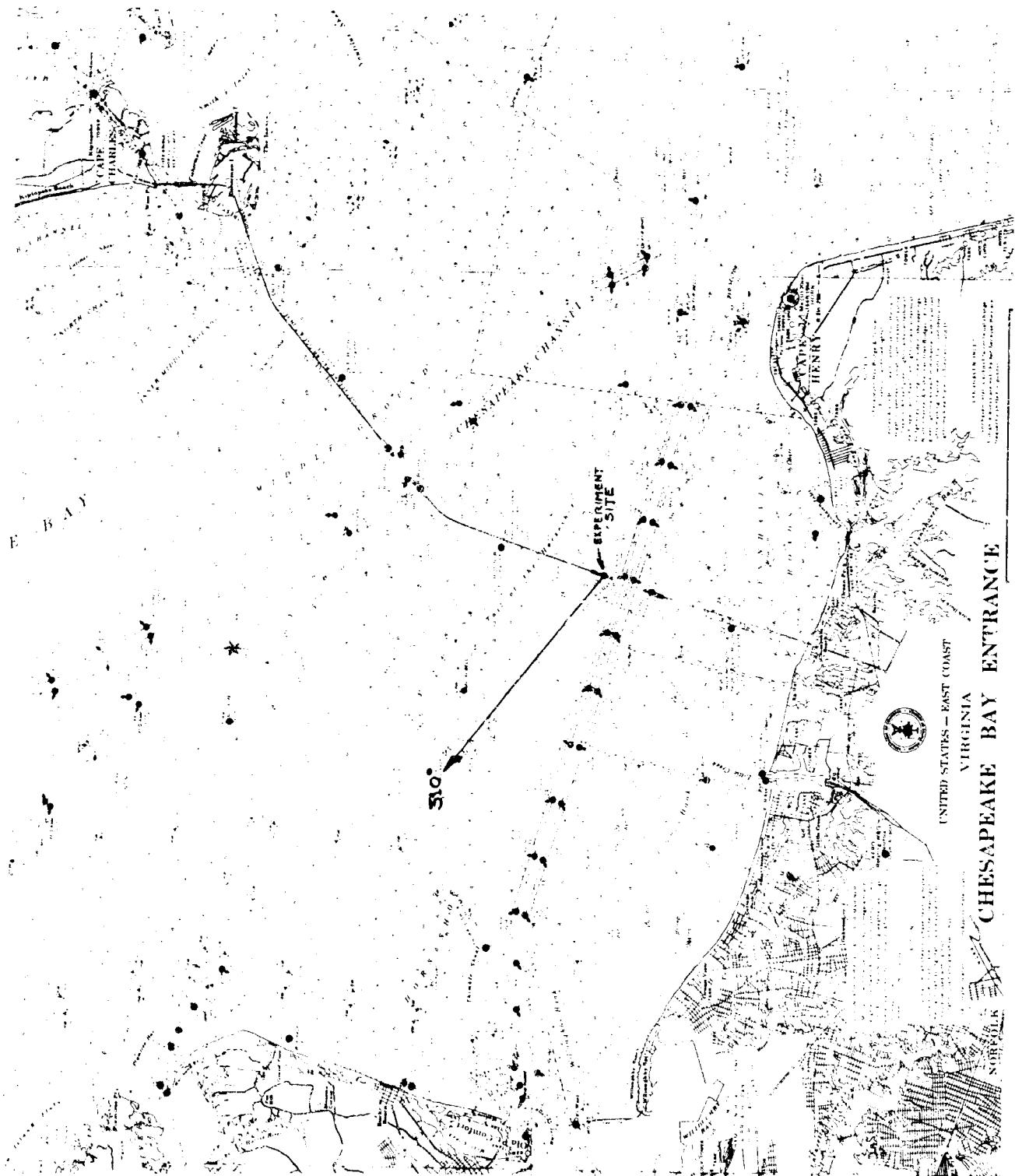


Figure IV-5. Field Test Site Location

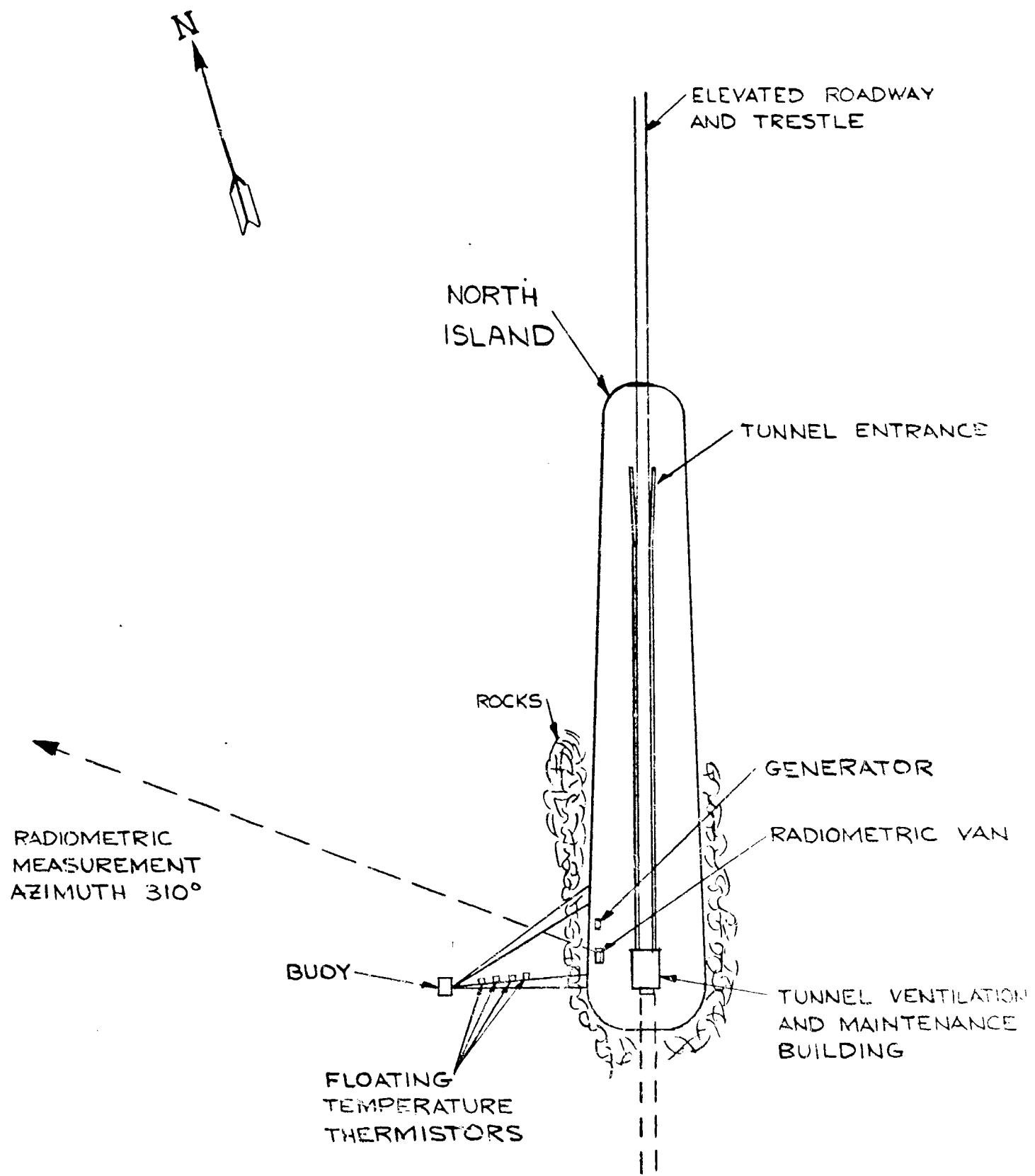


FIGURE IV-6. MEASUREMENT SITE PLAN VIEW

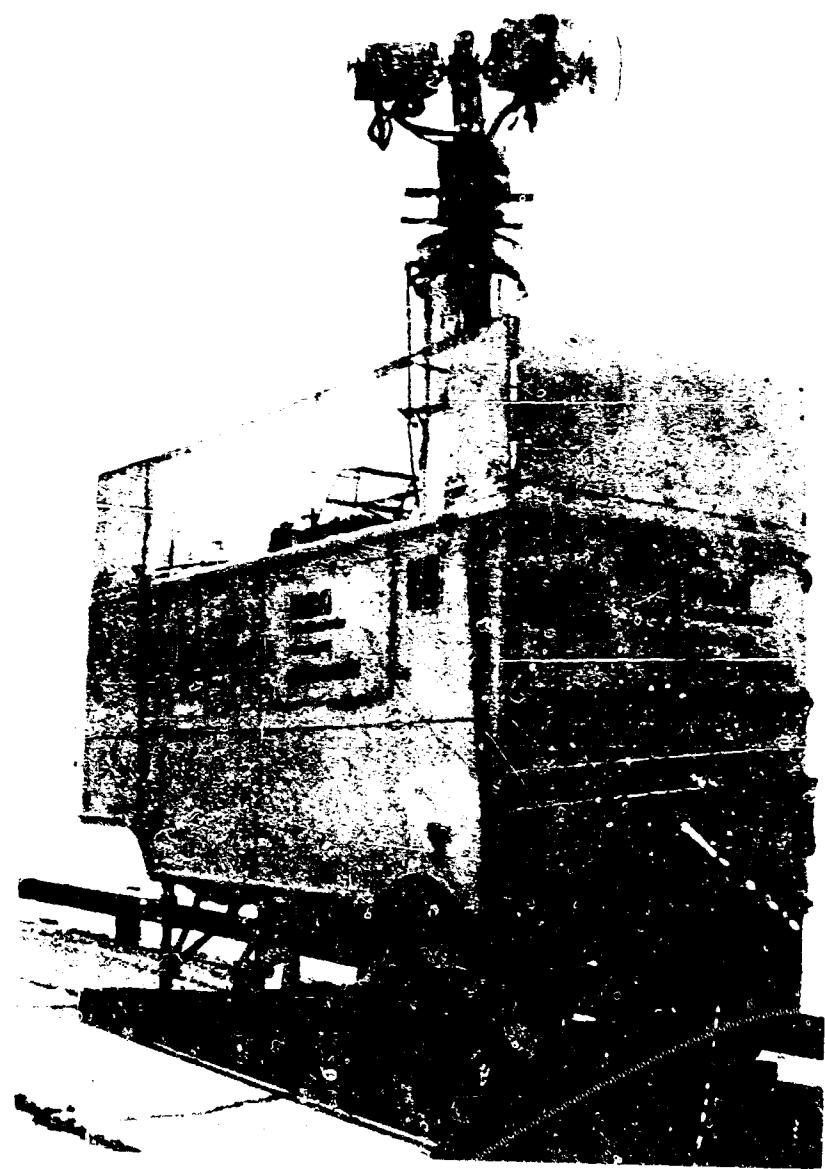


Figure IV-7. Close-up View of Radiometric Van

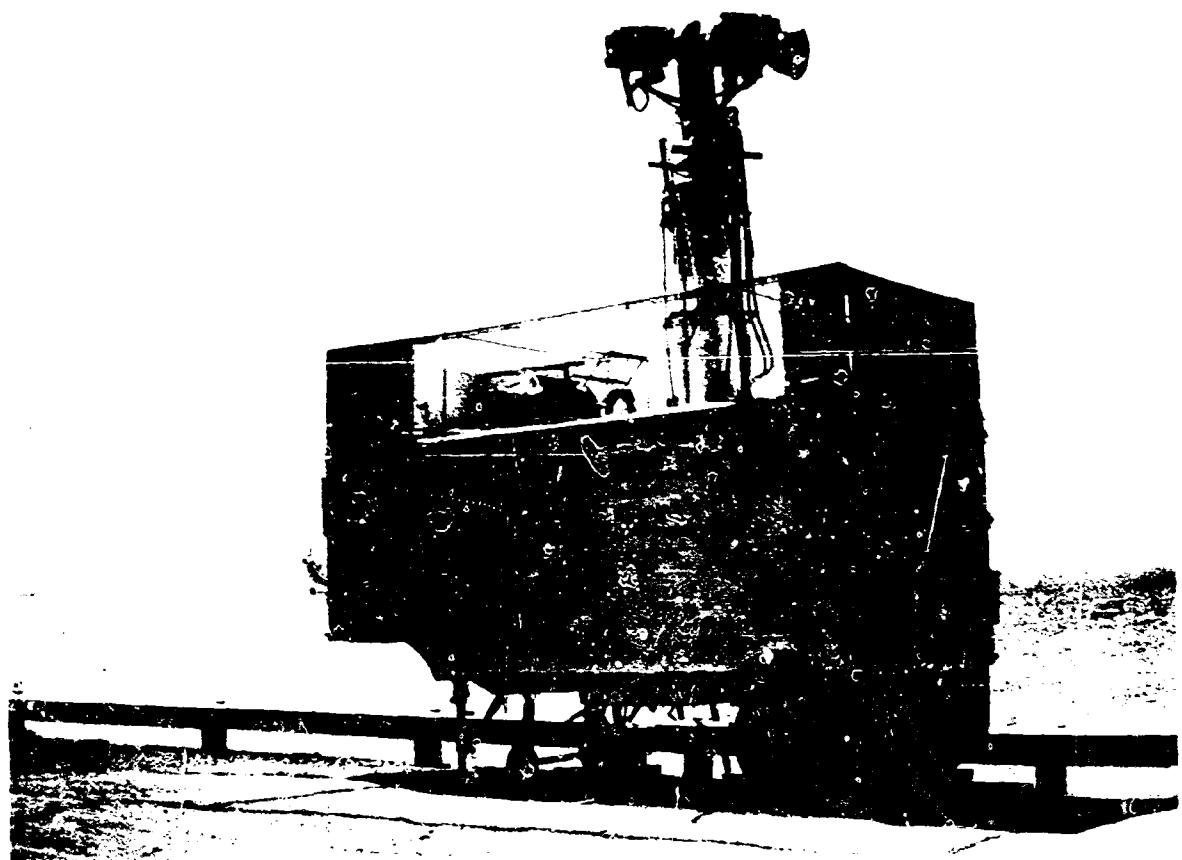


Figure IV-8. Antenna Pedestal and R. F. Heads



Figure IV-9. Close-up of 16.5 GHz R.F. Head and Infrared Sensor

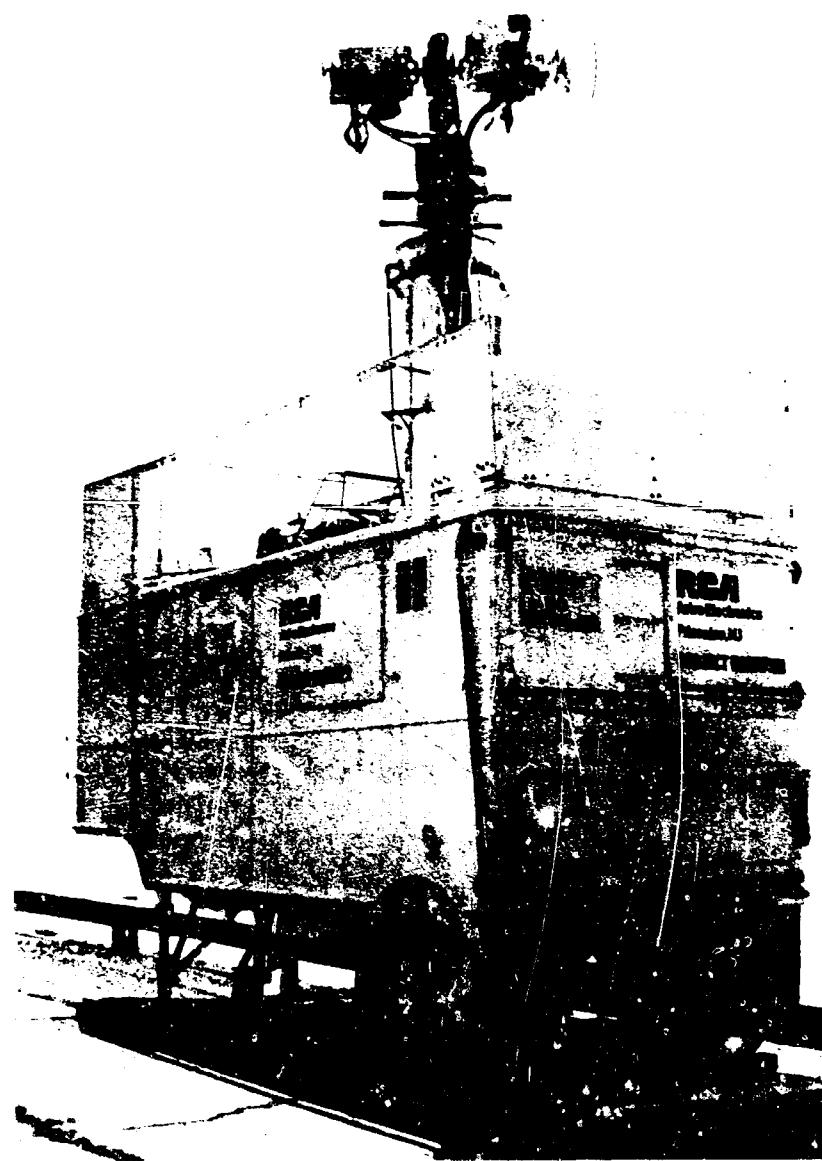


Figure IV-7. Close-up View of Radiometric Van

SECTION V

DATA MEASUREMENTS

A. Radiometric Measurements

Radiometric measurements were made at the site from July 17 through August 14, 1969. Both vertically and horizontally polarized measurements were made. Fifty-six data runs were made during the months of July and August, 1969. Of these, 46 were made at a frequency of 16.5 GHz and 10 were made at a frequency of 9.5 GHz. No measurements were made at 94 GHz because of equipment failure. There was observable interference at 9.5 GHz and therefore the data at this frequency is considered questionable.

The data runs can be divided into three types. The first type are designated standard data runs and consisted of measuring data at a sufficient number of zenith angles to adequately describe the elevation temperature profile along a fixed azimuth. The second type consisted of a series of measurements made with a fixed zenith angle and a fixed azimuth angle. These are further classified as stability runs, where the polarization was held constant for a long period of time and as switched polarization runs where the polarization was switched from vertical to horizontal every 50 to 100 seconds. The third type of run was a horizontal environment check where the zenith angle was held constant at 90° and the azimuth was slowly swept from 0° to 360° . These runs gave an indication of any possible interference and also a check on the temperature variation of the environment. The measured radiometric temperature is the resultant of the energy received by the main beam of the antenna and the side lobes. This measured temperature is called the apparent temperature (T_a). By providing an antenna pattern correction this apparent temperature is converted to brightness temperature (T_b). The brightness temperature is the radiated temperature of the observed source. The conversion from apparent temperature to brightness temperature requires a knowledge of the total radiometric environment. One of the prime reasons for taking sufficient data on a run was to describe a complete elevation profile. This in turn was used to define the total radiometric environment. In converting from apparent to brightness temperature, the elevation profile was assumed to be symmetrical around 360 degrees of azimuth.

B. Supplementary Observations

In addition to the radiometric measurements a large amount of supplementary and supporting data was obtained.

1. Sea Water Thermometric Temperature

The surface water temperature was measured using both mercury bulb thermometers and floating thermistors. The mercury bulb readings were taken at the waters edge by immersing the thermometer in the water. The thermistor measurements were accomplished by placing the thermistors on specially designed floats and deploying these floats on a pulley line between shore and the marker buoy. This enabled surface temperature measurements to be made at varying distances from the shore to a distance of about 100 feet. The floats were 12 x 12 inch squares of 1 inch thick styrofoam with a 3 or 4 inch diameter hole in the center. The thermistor was attached in the center of a doughnut shaped piece of styrofoam which was in turn confined to the hole in the square float. A second type placed the thermistor on the bottom of a ping-pong ball which was in turn confined to the hole in the square float. At the site the floats, when first placed, had a tendency to flip over in rough seas. This was eliminated by attaching short one foot pieces of nylon thread to each corner of the square float and suspending one or two B-B shots from each thread.

2. Sea Water Samples

Samples of the sea water were taken at various times during the course of the program. In general, samples were obtained near the time of the high and low tides and following any rainfall. The sea water samples were obtained by skimming a container along the water surface using the second shore-to-buoy pulley line. Care was exercised to obtain a representative sample of the water close to the surface. This was somewhat dependent on the roughness state of the sea, but most samples were obtained from water within 3 to 4 inches of the surface. The water samples were stored in special air-tight bottles, marked with the sample time, date and other pertinent information.

The salinity of the samples was measured at the Virginia Institute of Marine Science. The dielectric constant and loss tangent of representative samples was measured at the MIT Insulation Laboratory. These measurements were made at 8.5 and 14 GHz.

3. Weather Observations

Weather and meteorological observations were made at various times throughout each days operation. The observations included percent sky cover, cloud types,

air temperature - both dry and wet bulb, visibility, and weather comments. Additional weather observations were available from the Chesapeake Bay Bridge and Tunnel Authority which kept a regular weather log on an adjacent island.

4. Sea State Observations

Observations of the sea state were made with each data run and at other appropriate times. These observations included the swell and wind chop height and sometimes the wave period and wind speed and direction. These were visual observations made by inexperienced observers but the relative accuracy of the observations is considered good. Sea state conditions at the site, during the period of measurement varied from a smooth, calm sea to a sea with a three to three and one-half foot swell.

5. Photographs

Photographic records were made with each data run. The pictures generally were taken along the azimuth of the radiometric measurements and included pictures at zenith angles of 0° , 45° , 90° , 115° and 135° . This provided a fairly complete coverage of the elevation profile. Additional pictures were taken to record sea conditions. These in general included the marker buoy which had orange and white vertical sections alternating every six inches. Most of the pictures were taken with a 86 mm telephoto lens. A representative sample set of pictures taken in conjunction with run 7 and 8 are included as Figures V-1 thru V-6. The first five pictures are at the measurement azimuth of 310° with zenith elevation angles of 0° , 60° , 90° , 110° and 135° . The sixth picture is of the marker buoy and thermistor sensors.

6. Radiosonde Data

Radiosonde data was obtained from daily observations made at Wallops Island, Va. This is about 70 miles north of the experiment site and the atmospheric conditions were considered similar. This radiosonde data was used to determine radiometric zenith sky temperatures which were used for a third calibration point.

7. Wave Gage Recorder

The Army's Coastal Engineering Research Center (CERC) has a wave gage mounted on the adjacent South Island. This is about 1800 yards from the measurement site. It consists of a series of vertically spaced electrodes which when shorted by the conducting sea water provide an output signal proportional to the wave height. This wave gage is one of a network of similar gages along the Atlantic seaboard. It is automatically sequenced on for ten minutes out of each hour.

During this period a paper chart record is made at the wave gage location and data recordings are made at a central location in Washington, D. C. Facilitation was arranged to operate the local strip chart recorder on a continuous basis for eight hour periods. Several such recordings were made.

It was anticipated that the wave height and period at the test site and at the wave gage site would be representative of each other. However, visual observations showed that this was not true. There were wide variations in the surface conditions at the two sites most of the time. Apparently the water turbulence created by the island and the tidal currents, together with difference in local wind parameters degraded the correlation. As a result, the wave gage has not been used as an analysis tool.

8. Infra-red Radiometer Measurements

As previously mentioned, personnel from the National Environmental Satellite Center (NESC) supplied and operated an infra-red radiometer in conjunction with the microwave measurements. The results of the measurements and their analysis are treated in an internal NESC report (Ref 2). For a comparison to the microwave radiometric measurements a summary of the results of some of the infra-red radiometric data is contained in Appendix F of this report.

C. Site Operations and Data Measurements

The types of radiometric data runs have been described in Section V-A. The standard runs were numbered Run 1 thru Run 36.

Normally four calibrations were performed during a run. Each calibration consisted of measuring ten 1-second samples of the radiometer output voltage of first the zenith sky (nominally 10^0 K), second the ambient load (nominally 300^0 K), and last the hot load (nominally 400^0 K). A data measurement consisted of taking ten 1-second samples of the radiometer output voltage at the antenna zenith angle of interest. Each run had data points taken at zenith angles of 0^0 , 20^0 , 40^0 , 50^0 , 60^0 , 70^0 , 80^0 , 85^0 , 90^0 , 95^0 , 100^0 , 102^0 , 104^0 , . . . , 128^0 , 130^0 , 140^0 , 150^0 , 160^0 , 170^0 and 180^0 . The four calibrations were taken at the beginning of the run, before the 100^0 data point, after the 130^0 data point, and at the end of the run. The total time for a run was about 25 minutes. Comments pertinent to each run were written on the run log sheet. The calibration determination is described in Appendix E.

The 16.5 GHz stability runs and switched polarization runs were numbered Run 301 thru Run 313.

Runs 201 thru 206 consist of a preliminary 9.5 GHz data run, a 9.5 GHz zenith stability run and the horizon check runs.

Runs 101 and 102 are two preliminary 9.5 GHz standard runs.

Printouts of the comments accompanying or adjacent to each run are tabulated in Tables V-1 thru V-12. The first line on each of the run listings gives the month, date and year as a six digit number; the start time as a six digit number in hour, minutes, and seconds; the measurement azimuth angle in degrees; the polarization either H or V; the frequency in GHz times 10, as a 3 digit number; the integration time in seconds; and the apparent zenith sky temperature used as a third calibration point. The time is EDST expressed in a 24 hour format. The run comments sometimes include calibration data which is referenced only for programming use.

The thermometric water temperature was measured by a mercury bulb and by RCA and ESSA floating thermistors. The average daily temperature readings from the various devices is tabulated in Table V-13. It can be noted that the average temperature as measured by the various devices varied from a low of 297.5°K to a high 300.7°K , a variation of 3.2°K . Supplementary water temperature data was obtained from the United States Coast Guard from their Wolf Trap Light Station. Wolf Trap Light is located about 25 miles from the test site on an azimuth of about 351 degrees. This is representative of the water temperature further up the Chesapeake Bay and would indicate the temperature variations that might be expected as the horizon was approached. The Wolf Trap Light measurements were recorded every three hours. A tabulation of the daily temperature is in Table V-14. The readings were made in degrees Fahrenheit, but are presented in the table in degrees Kelvin for ease of comparison to other data. The temperature range of this data is from 297.6° to 299.8°K , and is in reasonable agreement with the site temperatures. This tends to support the basic contention that the water under observation had a relatively constant thermometric temperature along the line-of-sight.

Table V-15 tabulates the measured dry bulb air temperatures and the calculated relative humidity. The air temperatures varied about 11° during the course of the measurements.

Table V-16 tablates the salinity, in parts per thousand, of the sea water samples. The date and time of the sample plus the tide condition and other pertinent comments are also tabulated. The salinity variation was from a low of 21.41 to a high of 25.95 parts per thousand. Low salinity readings, after a rain, were obtained only if the sea was relatively calm. No explanation of the low readings on 8/7/69 and 8/8/69 is offered. The three samples which do not have salinity measurements were used for dielectric constant evaluation. In the computer programs the average salinity value of 24.17 parts per thousand was used in calculating the permittivity.

The permittivity is not strongly dependent on the salinity. The permittivity of salt water has been calculated for a water temperature of 300°K and for salinity values from 20 to 39 parts per thousand. The results are tabulated in Table V-17. These permittivity values have been used to calculate the vertical and horizontal emissivity. Representative values of the calculated emissivity are tabulated in Table V-18. The theoretical emissivity variation is quite small over the salinity range that was measured from the water samples.

Three of the sea water samples were sent to the MIT Insulation Laboratory for dielectric constant measurements. It was intended to have these measurements made at 8.5 and 14 GHz. The measurements at 8.5 GHz were completed, but because of instrumentation problems the 14 GHz measurements were not completed at the time this report is being written. The results of the 8.5 GHz measurements are tabulated in Table V-19, along with theoretical values computed for 8.5 GHz using a salinity value of 24.167 parts per thousand. The intent of the measurement was to verify the accuracy of the theoretical calculations of dielectric parameters. The agreement between the measured and theoretical data at 8.5 GHz supports the contention that the derived theoretical formulas for permittivity are adequate. (Reference Appendix B)

The values of the radiometric zenith sky temperatures as computed from the radiosonde data, is tabulated in Table V-20. These are brightness temperatures and were used to determine the third calibration point.

A rain gage was installed at the site. A tabulation of the rain gage measurements is in Table V-21. This data was not used in the data analysis, but may provide some correlation with the salinity variations. It is of interest to note that the low salinity readings of 8/7/69 and 8/8/69 were preceded by heavy rains on 8/5/69.

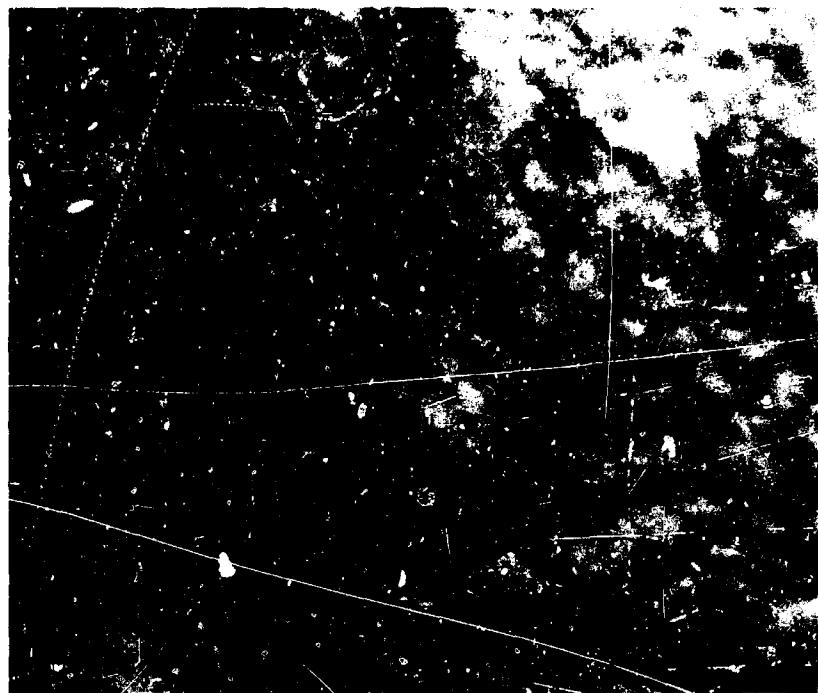


Figure V-1. Zenith Sky
Runs 7 and 8

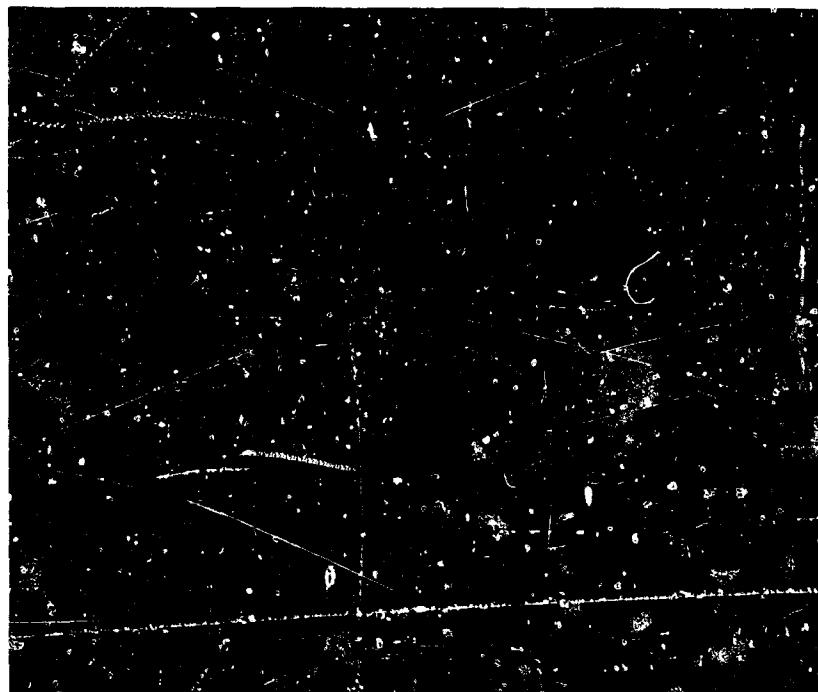


Figure V-2. Azimuth 310°, Zenith Angle 60°
Runs 7 and 8



Figure V-3. Horizon, Azimuth 310°
Runs 7 and 8

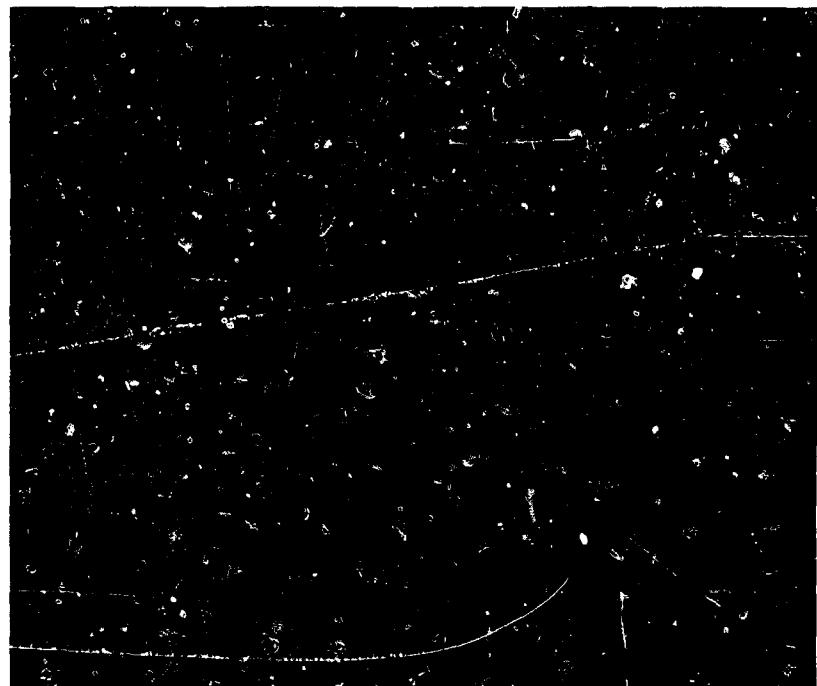


Figure V-4. Azimuth 310° , Zenith Angle 110°
Runs 7 and 8

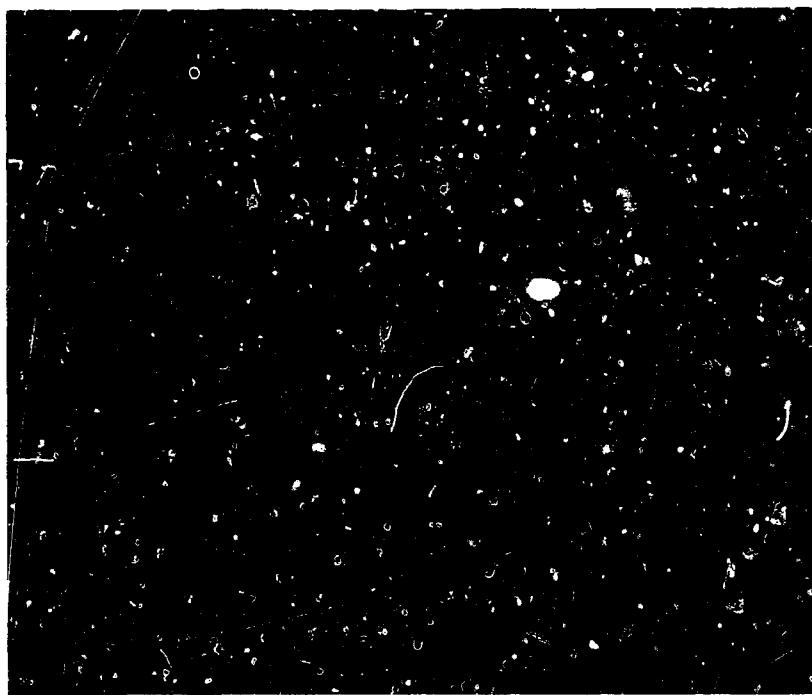


Figure V-5. Azimuth 310° , Zenith Angle 135°
Runs 7 and 8



Figure V-6. Buoy and Sensors
Runs 7 and 8

TABLE V-1. RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 1

072569 124800 310 H 095 01 10.1
XTAL I L25 R33.5 BV-300 I-29.5
INTERMEDIATE CAL AT MID POINT WITH ZENITH
THIS RUN SEQUENCE IS 90 TO 0 DEGREES, THEN 90 TO 178 DEGREES

RUN NO. 2

072569 134545 310 V 095 01 23.6
SEA CALM SLIGHT SWELL 77.5DEGREE WATER TEMP (BULB)
AT 1430 VISIBILITY 10+, CLOUDS 90%

RUN NO. 4

072969 200230 310 V 165 01 27.7
DIGITAL PRINTER WAS NOTED TO MISPRINT OCCASIONALLY

RUN NO. 5

080169 113200 310 V 165 01 18.9
XTAL L24.5 R32.5
INTERMEDIATE CAL POINTS DURING RUN
AT 1030 SLIGHT CHOP, LESS THAN 1FT SWELL, 10-12 VIS, 80-90% DIS CUM

RUN NO. 6

080169 120630 310 H 165 01 13.8
ISLAND CURRENT CHANGED SOUTH TO NORTH FROM RUN 05 TO 06
H2O SAMPLE AFTER RUN AT 1235 NO. 5
NOTE INT TA - SUN NEAR ZENITH
ADDL CAL AT INTERMEDIATE POINTS DURING RUN
AT 1230 LESS THAN 1FT SWELL, SLIGHT CHOP

RUN NO. 7

080169 134700 310 H 165 01 14.1
SLIGHT SWELL, 3 TO 6 INCHES - NO CHOP - GLASSY SURFACE
SCAT. CLOUDS AT ZENITH
INTERMEDIATE CAL POINTS DURING RUN
AT 1330 10-12MILE VIS, 60-70% SKY COVER

RUN NO. 8

080169 141700 310 V 165 01 15.0
SLIGHT SWELL 3 TO 6 INCHES - NO CHOP - GLASSY SURFACE
SCAT. CLOUDS AT ZENITH
INTERMEDIATE CAL POINTS DURING RUN

TABLE V-2. RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 9

080169 161000 310 V 165 01 18.1
XTAL I L26 R34
SEA WHITE CAPS - GOOD 3 FOOT SWELL PLUS 1 TO 2 FOOT CHOP
100 % CLOUD COVER WIND SW
INTERMEDIATE CAL POINTS DURING RUN

RUN NO. 10

080169 163700 310 H 165 01 23.6
SEA WHITE CAPS - GOOD 3 FOOT SWELL PLUS 1 TO 2 FOOT CHOP
100 % CLOUD COVER - WIND SW
XTAL I L26 R34
INTERMEDIATE CAL POINTS DURING RUN
AT 1700 10-12MILE VIS, CLOUDS 100%, CUM THUNDERHEADS

RUN NO. 11

080569 155500 310 V 165 01 120.
XTAL I L21 R33.5
HEAVY OVERCAST - DRIZZLE 3 FT SWELL SLIGHT WIND RIPPLE
INTERMEDIATE CAL POINTS

RUN NO. 12

080569 162830 310 H 165 01 104.
XTAL I L22 R33.5
HEAVY OVERCAST - DRIZZLE 2-3 FOOT SWELL 1-2 INCH WIND RIPPLE
INTERMEDIATE CAL POINTS
AT 1630 3FT HEAVE, SKY OVERCAST & RAIN

RUN NO. 13

080569 130900 310 V 165 01 13.5
CL-0-401.2 CL-0-308.0 INIT // HL-0-402.1 CAL2 //
HL-0-403.2 CL-0-307.5 CAL3 // HL-0-404.7 CL-0-307.2 FINI //
SEA 1-2 FOOT SWELL 2-12 INCH WIND CHOP

RUN NO. 14

080569 155000 310 H 165 01 18.2
XTAL I L25.5 R34.0 BEAM VOLTS 322 I=22.5
SEA 1-2 FOOT SWELL 5-10 INCH WIND CHOP
HL-0-402.1 CL-0-306.9 INIT // HL-0-401.9 CL-0-308.2 CAL2 //
ELEV HANGUP 1610 TO 1621 // HL-0-403.5 CL-0-309.8 CAL3 //
HL-0-400.8 CL-0-302.4 FINI //
WATER SAMPLE AT 1545- CLEAR SKY, 2-3FT WAVES

TABLE V-3

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 15

080769 121600 310 V 165 01 13.5
 CLEAR SKY EXCEPT 5-10 % CUM CLOUDS ON HORIZON
 APPROX ONE FOOT SWELL - LONG PERIOD - 20FT - 3-4 INCH WIND CHOP
 BRIGHT-SUNNY-HAZY WNW WIND 1-2 MPH VIS 6-8 MI.
 XTAL I L24.5 R32.5 BEAM V 321 I22 MA.
 HL-0-403.5 CL-0-309.4 INIT //
 HL-0-402.7 CL-0-310.5 CAL2 // HL-0-402.3 CL-0-310.7 CAL3 //
 HL-0-404.2 CL-0-311.1 FINI //
 WATER SAMPLE AT 1200- CLEAR SKY, APPROX 1FT SEA

RUN NO. 16

080769 125500 310 H 165 01 13.2
 CLEAR SKY EXCEPT 5-10% CUMULUS CLOUDS ON HORIZON
 APPROX ONE FOOT SWELL- LONG PERIOD-20FT- 3-4 INCH WIND CHOP
 BRIGHT-SUNNY-HAZY WNW WIND 1-2 MPH VIS 6-8 MI.
 XTAL I L24.5 R32.5 BEAM V 321 I=22 MA // HL-0-402.0 CL-0-311.6 INIT//
 HL-0-404.0 CL-0-311.7 CAL2 // HL-0-403.0 CL-0-312.5 CAL3 //
 HL-0-404.2 CL-0-313.0 FINI //
 SAME COMMENTS AS RUN NO 15
 AT 1330 10% HORIZIN CUM,1FT SWELL, LONG PERIOD 3-4IN WIND CHOP
 AT 1330 WNW WIND 1-2, 6-8MILE VIS

RUN NO. 17

080769 165500 310 H 165 01 18.0
 2-5 % CIRRUS CLOUDS DRIFTING OVERHEAD
 1 FOOT SWELL 6-8 INCH CHOP WIND SOUTH 5-10 MPH
 HL-0-401.5 CL-0-307.0 INIT // HL-0-400.0 CL-0-306.6 CAL2 //
 HL-0-403.5 CL-0-306.5 CAL3 // HL-0-402.0 CL-0-306.4 FINI //
 APPROX 1700 SKY CLEAR WITH HAZE,6MILE VIS,WIND S 5-10,1-1.5FT SWELLS

RUN NO. 18

080769 172900 310 V 165 01 13.0
 OVERHEAD CLEAR 1 FOOT SWELL 6-8 INCH CHOP VERY HAZY - SUNNY
 WIND S 5-10 MPH
 XTAL I L26.5 R34.5 BEAM V 323 I 22.2 MA
 HL-0-404.6 CL-0-307.0 INIT // HL-0-404.6 CL-0-307.2 CAL2 //
 HL-0-404.0 CL-0-307.3 CAL3 // HL-0-401.4 CL-0-307.1 FINI //
 AT 1725 10-15% CLOUDS

TABLE V-4
RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 19

080769 191500 310 V 165 01 8.7
WATER SENSORS 1-298.2 2-298.6 3-298.6 4-298.6 AT 19145100
HL-0-401.6 CL-0-302.6 INIT // HL-0-401.5 CL-0-302.9 CAL2 //
HL-0-401.2 CL-0-303.0 CAL3 // HL-0-403.5 CL-0-302.9 FINI //
AT 1810 10% CLOUDS, OH CLEAR, WIND S 5-10, 1FT SWELL, 10FT PERIOD
AT 1810 6-8IN CHOP, 6-9MILE VIS

RUN NO. 20

080769 194930 310 H 165 01 10.5
HL-0-405.0 CL-0-302.8 INIT // HL-0-405.0 CL-0-302.5 CAL2 //
HL-0-403.5 CL-0-302.4 CAL3 // HL-0-401.5 CL-0-302.3 FINI //
WATER SENSORS #1-298.8 #2-298.1 #3-298.1 #4-298.1
AT 2025 WIND SE 10-15, 10MILE VIS, 10% CLOUDS, OH CLEAR

RUN NO. 21

080769 113200 310 V 165 01 14.2
HL-0-405.0 CL-0-303.0 INIT // HL-0-404.5 CL-0-306.0 CAL2 //
SENSORS #1-301.6 #2-301.7 #3-299.4 #4-298.5 ALL UPSIDE DOWN TIME 1155
HL-0-402.0 CL-0-304.5 CAL3 //
SENSORS #1-301.0 #2-301.0 #3-298.9 #4-298.4 TIME 1205
HL-0-402.5 CL-0-306.7 FINI //
SENSORS #1-302.6 #2-301.5 #3-302.5 #4-299.5 TIME 1225
AT 1100 1-1.5FT SEA, CLEAR SKY, 6MILE VIS

RUN NO. 22

080769 124000 310 H 165 01 16.0
HL-0-401.5 CL-0-307.0 INIT // HL-0-405.8 CL-0-307.2 CAL2 //
HL-0-404.7 CL-0-307.1 CAL3 // HL-0-401.0 CL-0-307.3 FINI //

RUN NO. 23

080769 145500 310 V 165 01 11.4
1-2 PERCENT CUMULUS SCATTERED AND DRIFTING OVERHEAD
HL-0-405.0 CL-0-309.0 INIT // HL-0-401.1 CL-0-309.2 CAL2 //
HL-0-402.1 CL-0-308.7 CAL3 // HL-0-403.5 CL-0-308.5 FINI //

TABLE V-5
RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 24

080869 153100 310 H 165 01 11.7
5-10 PERCENT SCATTERED CUMULUS CLOUDS OVERHEAD
1.5 - 2 FOOT SWELL 12-18 INCH CHOP QUITE RUGH, VERY FEW WHITE CAPS
HL-0-403.0 CL-0-308.8 INIT // HL-0-401.0 CL-0-309.0 CAL2 //
HL-0-403.5 CL-0-308.8 CAL3 // HL-0-401.5 CL-0-300.0 FINI //
AT 1600 10% OH CUM & HORIZON, 6-8MILE VIS

RUN NO. 25

081269 122500 310 V 165 01 10.5
XTAL I INIT L=26.5 R=35.0 KLY 315V 23MA // HL-0-404.0 CL-0-301.4 INIT
HL-0-405.0 CL-0-302.1 CAL2 // TIDE LINE BTW RUGH & CALM WATER FINI
HL-0-404.0 CL-0-302.0 CAL3 // HL-0-402.0 CL-0-302.0 FINI
2-3FT SWELL FROM NW 6-12IN WIND RIPPLE 80-90% OVERCAST VAR OVERHEAD
SENSORS 1-297.5 2-298.0 3-298.0
AT 0900 90% SKY COVER
AT 1030 MOD SEA, SUNNY

RUN NO. 26

081269 131300 310 H 165 01 6.9
HL-0-402.0 CL-0-302.2 INIT // HL-0-401.5 CL-0-302.5 CAL2
HL-0-404.3 CL-0-302.5 CAL3 // HL-0-401.1 CL-0-302.7 FINI
2-3FT SWELL FROM NW 8-12IN WIND RIPPLE 80-90% OVERCAST OVERHEAD
SENSORS 1-297.5 2-298.0 3-297.9
AT 1300 2-3FT SWELL

RUN NO. 27

081269 162100 310 V 165 01 11.5
HL-0-401.5 CL-0-302.6 INIT // HL-0-402.3 CL-0-303.2 CAL2
HL-0-401.5 CL-0-303.1 CAL3 // HL-0-404.5 CL-0-303.0 FINI
21/2-31/2FT SWELL 4-8IN CHOP NW SEA NE WIND 10-15
AT 1555 2-3FT SWELL FROM NW,WIND NE 10-15, 90% SKY COVER

RUN NO. 28

081269 165500 310 H 165 01 16.5
HL-0-404.5 CL-0-302.8 INIT // HL-0-403.1 CL-0-303.0 CAL2
HL-0-404.5 CL-0-303.0 CAL3 // HL-0-401.0 CL-0-303.4 FINI
2-3FT SWELL 4-8IN CHOP PARTLY CLOUDY HAZY BUT BLUE SKY WITH SUN & CLOUDS
SENSORS 1-298.4 2-298.5 3-298.3 @ 17125100

TABLE V-6
RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 29

081269 184500 310 H 165 01 14.3
HL-0-403.1 CL-0-302.1 INIT // HL-0-405.0 CL-0-301.8 CAL2
HL-0-405.0 CL-0-301.1 CAL3 // HL-0-401.1 CL-0-301.0 FINI
11/2-2FT SWELL 6-8IN CHOP
SENSORS 1-297.3 2-299.0 3-298.1

RUN NO. 30

081269 191500 310 V 165 01 11.7
HL-0-403.0 CL-0-301.0 INIT // HL-0-405.0 CL-0-301.0 CAL2
HL-0-401.3 CL-0-300.5 CAL3 // HL-0-404.0 CL-0-300.5 FINI
1-11/2FT SWELL 6-8IN CHOP

RUN NO. 31

081369 103800 310 H 165 01 12.4
1-2FT SWELL 15-20FT PERIOD 4-8IN CHOP WIND N 5-10
SENSORS 1-297.6 2-298.4 3-298.4
AT 1030 80-90% SKY COVER, HAZY LIGHT TRANSPARENT OH CLOUDS, VIS 6-8
AT 1030 SUNNY SLIGHT HAZE

RUN NO. 32

081369 111500 310 V 165 01 14.8
EL 116 SMALL BOAT PASSED BY // OVERHEAD PATCHY -50% SOME LARGE CLOUDS
SENSORS- TIME 11:38:00 1-297.1 2-298.4 3-298.4
AT 1110 1-2FT SWELL
AT 1340 99% SKY COVER, LOW BIG SCAT CLOUDS PLUS HIGH OH ALMOST COMPLETE
AT 1340 VIS 6-7MILES, NO SUN
AT 1630 HEAVY SWELL FROM NW 3-3.5FT, 15-20FT PERIOD

RUN NO. 33

081469 101000 310 V 095 01 21.1
HL & CL MV READINGS WERE TAKEN AT NUMEROUS ELEVATION ANGLES
SEA CALM PERCEPTABLE SWELL VERY SMALL WIND RIPPLE
DATA RUN BEGAN AT 10120100
AT 0830 60-70% SKY COVER VIS 10-15 STRATO CUM N, LOW STRATUS & CUM N
AT 0830 CIR & CIR-STRATUS SEE
AT 0840 SEA CALM 1-2IN WIND RIPPLE, 6IN SWELL

TABLE V-7

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 34

081469 104700 310 H 095 01 15.5
HL & CL MV READINGS TAKEN AT SEVERAL ELEVATION ANGLES
SEA CALM OVERHEAD CLEAR
DATA RUN BEGAN AT 10159100
AT 1005 SEA CALM, SLIGHT WIND RIPPLE, 6IN SWLW SWELL

RUN NO. 35

081469 132500 310 H 165 01 24.0
SCATTERED CUMULUS CLOUDS OVERHEAD VERY CLEAR WHEN WO CLOUDS
PICTURES TAKEN AT 13146100
AT 1130 SEA CALM
AT 1300 40-50% SKY COVER, CUM MOSTLY, SUNNY

RUN NO. 36

081469 141500 310 V 165 01 14.8
CLEAR DH AT START // XTAL I L-23.5 R-32.5
TIME-14145100 THUNDER SQUALLS IN VICINITY DH IS NOW OVERCAST
TO NORTH DH IS CLEAR
AT 1500 THUNDERHEADS & STORM TO SW, DARK CLOUDS W, SEA CALM
AT 1500 SLIGHT SWELL WITH WIND RIPPLE
AT 1510 HEAVY RAIN STARTED, VIS LESS THAN 1 MILE
AT 1532 100% CLOUDS HEAVY RAIN
AT 1715 SEA DEAD CALM, AFTER BIG RAIN SHOWER, STILL RAINING LIGHTLY
AT 1930 SEA CALM, AFTER RAIN STOPPED

TABLE V-8
RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 101
072169 144500 310 V 095 01 31.7
RUNS 101 AND 102 ARE THE FIRST CONSECUTIVE HORIZ & VERT POL RUNS
VENT BLDG L7G @ 1500; WIND NE 10-15, CLOUDY, SEA CALM
WEATHER BUREAU WATER TEMP- 298.5

RUN NO. 102
072169 151000 310 H 095 01 10.9
RUNS 101 AND 102 ARE THE FIRST CONSECUTIVE HORIZ & VERT POL RUNS
STARTED TO RAIN AS RUN BEGAN//CLOUD COVER NEAR 100%

TABLE V-9

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 201

071769 175000 310 V 095 01 19.4

AIRPLANES FLEW OVER AT ELEVATION ANGLES OF 90 AND 95 DEGREES //

THIS RUN WAS A VERY PRELIMINARY CHECK OF AZIMUTH 310 //

USE INIT CAL TEMPERATURES IF COMPUTER NEEDS THEM FOR THE FINI POSITIONS

RUN NO. 202

072269 140000 310 V 095 01 4.56

ZENITH STABILITY RUN // USE FINI CAL TEMPERATURES IF COMPUTER NEEDS THEM
FOR THE INIT POSITIONS//

RUN NO. 203

072269 181520 V 095 01 4.56

HORIZON (ELEV ANGLE 90 DEGREES) CHECK WITH 360 DEG AZIMUTH ROTATION

RUN NO. 204

072269 183130 H 095 01 4.56

HORIZON (ELEV ANGLE 90 DEGREES) CHECK WITH 360 DEG AZIMUTH ROTATION

RUN NO. 205

072969 203000 V 165 01 27.7

HORIZON(ELEVATION ANGLE 90 DEGREES)CHECK WITH 360 DEG AZIMUTH ROTATION

RUN NO. 206

080569 164930 310 H 165 01 104.

HIT LOAD CAL RUN AND ZENITH TEMP STABILITY

THIS WAS FIRST RUN WHERE WE NOTED THAT HL TEMP WAS VARYING

ZENITH TEMP STABILITY DATA TAKEN END OF RUN 12. DATA IS IN RUN 12 TAPE

TABLE V-10

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 301

080169 153200 310 V 165 01

SEA WATER TEMP STABILITY AT ELEV. OF 115 DEGREE ZENITH ANGLE
 1-1.5 FOOT SWELL AND CHOP//NO FINAL ZENITH READING, STARTED TO POUR RAIN
 RAINED FROM 1555 TO 1605 LESS THAN 0.02 ACCUMULATED

RUN NO. 302

080869 095000 310 V 165 01

VERTICAL STABILITY CHECK AT 120 DEGREES ELEVATION

XTAL I AT START APPROX L22 R31

XTAL I DROPPED OFF DURING RUN - AT END WAS L16 R23

HL-0-403.7 CL-0-299.4 INIT // HL-0-404.5 CL-0-301.6 FINI //
 AT 0900 1.5-2FT SWELL, ROUGH 12-18IN CHOP, 5-10% WHITECAPS

RUN NO. 303

080869 133200 310 165 01

RUN AT 122 DEGREES ELEV - SWITCHING BETWEEN HORIZ AND VERTICAL

SEA WATER SENSORS #3-299.4 #4-299.8

FIRST 8 DATA POINTS ARE HORIZONTAL, NEXT 6 VERTICAL, NEXT 6 H, NEXT 7 V
 NO CAL TAKEN FOR HLOCLO200

RUN NO. 304

080869 161500 310 165 01 11.7

THIS RUN HAS BOTH VERT AND HORIZ MEA, AT 115,120, AND 125 DEGREES ELEV//
 START AT 115 DEG HORIZ // TIME 1620 115 DEG VERT //

TIME 16122130 115 DEG HORIZ // TIME 1625 115 DEG VERT //

TIME 16126130 120 DEG VERT // TIME 1628 120 DEG HORIZ //

TIME 16129130 120 DEG VERT // TIME 1631 120 DEG HORIZ //

TIME 16132130 125 DEG HORIZ // TIME 1634 125 DEG VERT //

TIME 16135130 125 DEG HORIZ // TIME 1637 125 DEG VERT //

HL-0-402.5 CL-0-308.9 INIT // HL-0-403.9 CL-0-308.3 FINI //

RUN NO. 305

080869 163800 310 V 165 01

THIS RUN IS A ZENITH STABILITY CHECK

STARTED RIGHT AFTER RUN 304 THEREFORE USE 304 FINAL CAL AS 305 INT CAL
 HL-0-403.9 CL-0-308.3 INIT //

AT 1705 CHOPPY SEA-2FT, SUNNY, HUMID

TABLE V-11

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 306

081169 122200 310 165 01
 SPECIAL RUN ELEVATION ANGLE 105 DEG//CHANGE BTWN H & V POLARIZATION
 HL-180-403.0 CL-180-309.5 INIT // FIRST V RUN LG CG SHIP POSSIBLY IN
 FIELD OF VIEW HL-105-402.0 CL-105-308.0 // START TIME FIRST H RUN 1307
 HL-180-403.4 CL-180-305.5 CAL2 // SWELL INCREASING & CHOPPIER AFTER 1315
 SECOND V 1324 HL-180-402.0 CL-180-306.4 CAL3 // SECOND H COMPLETE 1356
 AT 1030 SLIGHT SWELL FROM NW, CLOUDS 90% CS AC
 AT 1200 WIND NW 5-10, CLOUDS 80% CS CC
 AT 1300 SWELL DEVELOPING, SLIGHT CHOP, CLOUDS 90% CI SCAT CU

RUN NO. 307

081169 140000 310 165 01
 SPECIAL RUN ELEVATION ANGLE 110 DEG//CHANGE BTWN H & V POLARIZATION
 HL-180-405.0 CL-180-311.6 INIT // HL-180-402.5 CL-180-306.7 CAL2
 TIME-1430 START SECOND VERTICAL POL // TIME 1436 START SECOND HORIZ POL
 GENTLE BUT DISTINCT CHOP IN WATER // HL-180-404.6 CL-180-307.0 FINI
 AT 1330 CHOP INCREASING SINCE NOON UNDER STEADY NW WIND 5TH WHITETAPS
 AT 1330 SWELL PERIOD 15-20FT
 AT 1400 CLOUDS 80% CI CS, VIS 6MILES
 AT 1433 DISTINCT TIDAL LINE BTWN WHITE & CALM WATER, (NEAR MEASUREMENTS)
 AT 1450 2FT SWELL
 AT 1500 CLOUDS 70% CI CS, CU MED, CU BUILDING TO WEST & NW

RUN NO. 308

081169 161700 310 165 01
 SPECIAL RUN ELEVATION ANGLE 115 DEG // CHANGE BTWN H & V POLARIZATION
 HL-180-402.2 CL-180-302.3 INIT // TIME 1626 START FIRST H POL RUN
 HL-180-405.0 CL-180-304.0 CAL2 // TIME 1640 END FIRST V POL RUN & BEGIN
 SECOND V POL RUN // TIME 1647 START SECOND H POL RUN //
 HL-180-404.7 CL-180-304.0 FINI //

RUN NO. 309

081169 165700 310 165 01
 SPECIAL RUN ELEVATION ANGLE 120 DEG // CHANGE BTWN H & V POLARIZATION
 HL-180-404.1 CL-180-304.5 INIT // TIME 1704 START FIRST H POL RUN
 HL-180-403.3 CL-180-303.6 CAL2 // TIME 1717 START SECOND V POL RUN
 WATER MUCH CALMER // TIME 1722 END SECOND H POL RUN
 HL-180-405.0 CL-180-303.6 FINI
 1700 CLOUDS 40% CI, NO CU EVIDENT

TABLE V-12

RADIOMETRIC RUN COMMENT PRINTOUT

RUN NO. 310

091169 175500 310 165 01
 SPECIAL RUN ELEVATION ANGLE 125 DEG // CHANGE BTWN H & V POLARIZATION
 HL-180-404.0 CL-180-304.0 INIT // TIME 1800 START FIRST H POL RUN
 TIME 1806 END FIRST V POL RUN // HL-180-404.0 CL-180-303.2 CAL2 //
 TIME 1815 START SECOND V POL RUN // TIME 1823 START SECOND H POL RUN //
 HL-180-405.0 CL-180-302.7 FINI //
 AT 1730 WIND HAS DIED DOWN, WATER BECOMING QUITE CALM
 AT 1800 CLOUDS 10% CI
 AT 1900 1FT SWELL

RUN NO. 311

091269 143200 310 165 01
 SPECIAL RUN 120 DEG ELEVATION STABILITY WITH FIRST H THEN V POLARIZ
 HL-0-401.0 CL-0-304.5 INIT // START TIME H POL 14:37:00 STOP AT 15:40:00
 HL-0-403.5 CL-0-301.9 CAL2 // XTAL I L26.5 R35 // START V POL 15:44:00
 SATELLITAT IN BEAM APPROX 15:48:00 // STOP V POL AT 15:51:00 //
 HL-0-404.0 CL-0-302.1 FINI //
 AT 1400 APPROX 3FT SWELL

RUN NO. 312

091269 194500 310 V 165 01
 ZENITH STABILITY RUN // INIT CAL DATA IS SAME AS FINI CAL DATA ON RUN30
 USE COMMENTS ON RUN 30 // HL-0-404.0 CL-0-300.5 INIT //
 2000 1-1.5FT SWELL, 6-8IN C IOP
 2015 40-60% SKY COVER, HIGH HAZY STRATUS

RUN NO. 313

091369 023000 310 165 01
 SPECIAL RUN V & H STABILITY AT 120 DEG ELEVATION ANGLE
 HL-0-404.5 CL-0-208.6 INIT // START V POL AT 09:36:00 STOP AT 10:20:30//
 START H POL AT 10:27:00 STOP AT 10:30:30 // XTAL I L24.5 R35
 AT 0915 60-70% SKY COVER, HORIZON COVERED, OH LIGHT WISPY CLOUDS, VIS 6-8
 AT 0915 1-2FT SWELL

TABLE V-13

BEST AVERAGE FAHR TEMPERATURE EACH DAY

| DATE | HG BULB | RCA THERM | ESSA THERM | WEATHER BUREAU |
|---------|---------|-----------|------------|----------------|
| 7-17-69 | 299.5 | | 300.7 | |
| 7-21-69 | | | | 298.5 |
| 7-22-69 | | | | |
| 7-25-69 | | | 298.3 | |
| 7-29-69 | | | | |
| 7-30-69 | 299.5 | | 299.7 | |
| 8-01-69 | 299.5 | 300.4 | | |
| 8-05-69 | | | | |
| 8-06-69 | 299.0 | | | |
| 8-07-69 | 300.4 | 298.8 | | |
| 8-08-69 | 299.6 | 299.0 | | |
| 8-11-69 | 298.5 | | | |
| 8-12-69 | | 298.2 | | |
| 8-13-69 | 297.5 | 298.4 | | |
| 8-14-69 | 298.3 | 298.6 | | |

TABLE V-14
SEA WATER TEMPERATURE DATA FROM WOLFTRAP LIGHT

TIME - EDST

| Date | 0200 | 0500 | 0800 | 1100 | 1400 | 1700 | 2000 | 2300 |
|----------|-------|------|-------|-------|-------|-------|------|------|
| July 14 | 297.6 | | | | | | | → |
| 15 | 297.6 | | | | | | | → |
| 16 | 297.6 | | | | | | | → |
| 17 | 297.6 | → | 298.7 | | | | | → |
| 18 | 298.7 | | | | | | | → |
| 19 | 298.7 | | | | | | | → |
| 20 | 298.7 | | | | | | | → |
| 21 | 298.7 | | | | | | | → |
| 22 | 298.7 | | | | → | 299.3 | → | |
| 23 | 299.3 | | | | | | | → |
| 24 | 299.3 | | | | | | | → |
| 25 | 299.3 | | → | 299.8 | | | | → |
| 26 | 299.8 | | | | | | | → |
| 27 | 299.8 | | | | | | | → |
| 28 | 299.8 | | | | | | | → |
| 29 | 299.8 | | | | | | | → |
| 30 | 299.8 | | | | | | | → |
| 31 | 299.8 | | | | | | | → |
| August 1 | 299.8 | | | | | | | → |
| 2 | 299.8 | | | | | | | → |
| 3 | 299.8 | | | | | | | → |
| 4 | 299.8 | | | | | | | → |
| 5 | 299.8 | | | | | | | → |
| 6 | 299.8 | | | | | | | → |
| 7 | 299.8 | | | | | | | → |
| 8 | 299.8 | | | | | | | → |
| 9 | 299.8 | | | | | | | → |
| 10 | 299.8 | | | | | | | → |
| 11 | 298.7 | | → | 299.8 | 298.7 | | | → |
| 12 | 298.7 | | | | | | | → |
| 13 | 298.7 | | | | | | | → |
| 14 | 298.7 | | | | | | | → |

TABLE V-15

AIR TEMPERATURE AND RELATIVE HUMIDITY

| DATE | TIME | AIR TEMP-F | R.H.% |
|---------|------|------------|-------|
| 7-16-69 | 1315 | 85 | 63 |
| 7-17-69 | 1130 | 81 | 75 |
| 7-21-69 | 1800 | 77 | 83 |
| 7-25-69 | 1430 | 79 | 71 |
| 8-01-69 | 1030 | 79 | 79 |
| 8-01-69 | 1330 | 82.5 | 60 |
| 8-01-69 | 1700 | 79 | 83 |
| 8-07-69 | 1130 | 85 | 59 |
| 8-07-69 | 1410 | 82 | 65 |
| 8-07-69 | 2025 | 78 | 77 |
| 8-08-69 | 1100 | 82 | 72 |
| 8-08-69 | 1600 | 85 | 63 |
| 8-11-69 | 1230 | 77 | 72 |
| 8-11-69 | 1200 | 79 | 71 |
| 8-11-69 | 1300 | 79 | 65 |
| 8-11-69 | 1400 | 83 | 69 |
| 8-11-69 | 1500 | 83 | 69 |
| 8-11-69 | 1700 | 81 | 72 |
| 8-11-69 | 1800 | 78 | 79 |
| 8-12-69 | 0900 | 75 | 82 |
| 8-12-69 | 1600 | 81 | 70 |
| 8-12-69 | 2015 | 75 | 84 |
| 8-13-69 | 0915 | 77 | 83 |
| 8-13-69 | 1030 | 78.5 | 81 |
| 8-13-69 | 1340 | 77 | 87 |
| 8-14-69 | 0930 | 77.2 | 91 |
| 8-14-69 | 1100 | 80.5 | 83 |
| 8-14-69 | 1500 | 77 | 91 |

TABLE V-16

WATER SAMPLE SALINITY

| DATE | TIME | TIDE | SALINITY | COMMENTS |
|---------|------|--------------|----------|------------------------------|
| 7-15-69 | 1530 | PLT | | LOW TIDE |
| 7-17-69 | 1730 | LT+42MIN | 24.05 | NONE |
| 7-21-69 | 1800 | LT-1HR | 25.03 | RIGHT AFTER 1.17IN RAIN |
| 7-25-69 | 1500 | HT-2HR42MIN | 25.95 | NONE |
| 8-01-69 | 1230 | HT+54MIN | 25.04 | NONE |
| 8-01-69 | 1400 | LT-1HR48MIN | | RIGHT AFTER LINE SQUALL |
| 8-05-69 | 1745 | HT+2HR33MIN | 25.45 | AFTER 11812 RAIN ALL DAY |
| 8-06-69 | 1545 | HT-21MIN | 25.42 | CLEAR SKY, 2-3FT WAVES |
| 8-07-69 | 1200 | LT+1HR35MIN | 21.41 | SKY CLEAR, APPROX 1FT SEA |
| 8-07-69 | 1815 | HT+1HR9MIN | 24.57 | WEATHER CLEAR |
| 8-08-69 | 1100 | LT-24MIN | 22.88 | 1-1.5FT SEA, CLEAR SKY |
| 8-08-69 | 1705 | HT-55MIN | 21.90 | SUNNY, HUMID, CLOUDY 2FT SEA |
| 8-11-69 | 1450 | LT+55MIN | 25.30 | 2FT SWELL, PARTLY CLOUDY |
| 8-11-69 | 1700 | HT-18MIN | 24.78 | 1FT SWELL, SCAT CIRRUS |
| 8-12-69 | 1030 | HT+1HR54MIN | 25.52 | SUNNY, MOD SEA |
| 8-12-69 | 1550 | LT+1 HR14MIN | 24.34 | 2-3FT SEA SWELL |
| 8-13-69 | 0910 | HT-24MIN | 24.59 | 1-2FT SEA SWELL |
| 8-13-69 | 1630 | LT+1HR18MIN | 25.04 | HEAVY FROM NW, 3-3.5FT |
| 8-14-69 | 0840 | HT-1HR8MIN | 23.90 | SEA CALM, RAIN EARLY AM |
| 8-14-69 | 1005 | HT+17MIN | | SEA CALM, SIN SLOW SWELL |
| 8-14-69 | 1715 | LT+1HR27MIN | 22.11 | SEA CALM AFTER HEAVY RAIN |
| 8-14-69 | 1930 | LT+3HR42MIN | 21.89 | CALM, AFTER RAIN STOPPED |

NOTE 1- SALINITY IS EXPRESSED IN PARTS PER THOUSAND

NOTE 2- SALINITY AVERAGE OF ALL MEASUREMENTS = 24.17

TABLE V-17
CALCULATED PERMITTIVITY VS SALINITY

Frequency = 16.5 GHz
Temperature = 300°K

| Salinity (Parts per Thousand) | Calculated Permittivity | |
|-------------------------------------|-------------------------|----------------|
| | Real Part | Imaginary Part |
| 20 | 45.384 | 36.480 |
| 22 | 45.076 | 36.532 |
| 24 | 44.761 | 36.583 |
| 26 | 44.439 | 36.631 |
| 28 | 44.110 | 36.677 |
| 30 | 43.775 | 36.720 |

TABLE V-18 EMISSIVITY VS SALINITY

FREQUENCY = 16.5 GHz

TEMPERATURE = 300°K

| Salinity (Parts per Thousand) | Zenith Angle | Emissivity | |
|-------------------------------------|--------------|------------|----------|
| | | Horizontal | Vertical |
| 20 | 95° | .0424 | .9326 |
| 24.167 | 95° | .0425 | .9312 |
| 30 | 95° | .0426 | .9290 |
| 20 | 100° | .0827 | .9513 |
| 24.167 | 100° | .0828 | .9511 |
| 30 | 100° | .0831 | .9508 |
| 20 | 105° | .1206 | .8629 |
| 24.167 | 105° | .1209 | .8633 |
| 30 | 105° | .1213 | .8638 |
| 20 | 110° | .1562 | .7719 |
| 24.167 | 110° | .1566 | .7726 |
| 30 | 110° | .1570 | .7736 |
| 20 | 115° | .1893 | .6946 |
| 24.167 | 115° | .1897 | .6953 |
| 30 | 115° | .1903 | .6965 |

TABLE V-19 MEASURED AND THEORETICAL PERMITTIVITY

| Sample No. | Measured Dielectric Constant (K') | Measured Loss Tangent (tan ζ) | Computed Loss Factor (K''=K' tan ζ) | Theoretical | |
|------------|--|-------------------------------------|---|------------------------------|-----------------------|
| | | | | Dielectric Constant K' | Loss Factor K'' |
| 1 | 57.0 | .505 | 28.79 | 60.50 | 32.77 |
| 6 | 57.2 | .517 | 29.57 | 60.50 | 32.77 |
| 20 | 58.9 | .503 | 29.63 | 60.50 | 32.77 |

TABLE V-20

ZENITH SKY TEMPERATURE AS CALCULATED FROM RADIOSONDE DATA

| DATE | 16.5 GHZ | | | 9.5 GHZ | | |
|---------|----------|-------|-------|---------|------|------|
| | 8AM | NOON | 8PM | 8AM | NOON | 8PM |
| 7-17-69 | | | 9.72 | | | 3.76 |
| 7-20-69 | | | 13.06 | | | 4.41 |
| 7-21-69 | | | 7.76 | | | 3.52 |
| 7-22-69 | 11.67 | | 13.81 | 4.16 | | 4.56 |
| 7-23-69 | | | 13.59 | | | 4.54 |
| 7-24-69 | | | 10.35 | | | 3.91 |
| 7-25-69 | | | 9.82 | | | 3.73 |
| 7-28-69 | | | 14.52 | | | 4.71 |
| 7-29-69 | | | 12.88 | | | 4.39 |
| 7-30-69 | | | 10.90 | | | 4.01 |
| 7-31-69 | | | 9.59 | | | 3.77 |
| 8-01-69 | 11.25 | | 12.49 | 4.09 | | 4.33 |
| 8-05-69 | | | 13.34 | | | 4.44 |
| 8-06-69 | 10.05 | 10.13 | 10.50 | 3.85 | 3.83 | 3.97 |
| 8-07-69 | 8.41 | 8.47 | 8.74 | 3.54 | 3.53 | 3.59 |
| 8-08-69 | 10.20 | | 11.37 | 3.89 | | 4.01 |
| 8-11-69 | 8.93 | | 8.35 | 3.64 | | 3.51 |
| 8-12-69 | 7.28 | | 6.87 | 3.32 | | 3.17 |
| 8-13-69 | 9.31 | | 12.53 | 3.72 | | 4.36 |
| 8-14-69 | 12.78 | 11.47 | 12.50 | 4.49 | 4.11 | 4.34 |

TABLE V-21

RAIN GAGE DATA

| DATE | TIME | GAGE READING |
|---------|------|---------------------------------|
| 7-21-69 | 1800 | 1.17 |
| 7-22-69 | 1300 | 1.35 |
| 7-23-69 | 0900 | 0.05 |
| 7-24-69 | 1030 | 0.125 |
| 7-25-69 | 0930 | 0.00 |
| 7-29-69 | 1300 | 4.25 |
| 8-01-69 | 0800 | 0.10 |
| 8-01-69 | 1605 | <0.02(TRACE)(AFTER SHOWER) |
| 8-05-69 | 1710 | 2.45 |
| 8-06-69 | 0900 | 0.42 |
| 8-07-69 | 0900 | 0.00 |
| 8-11-69 | 0900 | 0.30 |
| 8-12-69 | 0900 | 0.00 |
| 8-13-69 | 0900 | 0.00 |
| 8-14-69 | 0900 | (TRACE) RAINED LIGHTLY EARLY AM |
| 8-15-69 | 0815 | 1.35 |

NOTE - GAGE WAS EMPTIED AFTER EACH READING BUT NOT IN BETWEEN.

SECTION VI

DATA FLOW AND RESULTS

A. Data Analysis Flow

The data flow is shown on Figure VI-1A. The raw radiometric voltages were recorded, as previously described, on a HP562 Digital Recorder. This unit provided one printout per second of the integrated radiometric output voltage. Ten, 1-second samples were recorded for each data observation point. The printout was on HP folded paper tape. The data on these tapes was later key punched onto IBM cards which were run through a computer program that converted the radiometric voltages to apparent temperatures. This program, named MODROD, also processed the calibration data and required a zenith temperature for a third calibration point. By utilizing radiosonde data and a computer program called SKYTEM, the zenith radiometric temperature was calculated. The calculated temperature was a brightness temperature and the calibration point at this data level required an apparent temperature. An iteration was performed to provide a correction to accommodate this difference.

The apparent temperature data from MODROD was processed through a program called APCOR4 which provided the required pattern corrections to correct the apparent temperatures to brightness temperatures. APCOR4 required an antenna correction matrix which was obtained from ANTPT2, a program which converted actual antenna patterns to a matrix format.

The output from APCOR4 consisted of brightness temperatures at 69 angles, whose angular value was dependent on the mesh size of the antenna matrix. The calculated brightness temperature at zenith (i.e. at an angle of 0°) was then compared to the zenith temperature as calculated by the SKYTEM program. If the agreement was not sufficiently close (generally 0.5° was considered to be adequate), the apparent temperature used as a calibration point was adjusted and the program MODROD and APCOR4 were re-run. These iterations were continued until agreement was reached.

The outputs of APCOR4 for all of the standard runs were plotted for the complete elevation profile and expanded plots were made for those zenith angles which included the sea water observations. The brightness temperatures calculated from APCOR4 were used to obtain the radiometric sea water temperature for the vertically polarized runs. This was done by the method described in Section III-C using a computer program named ROCK 3.

This program iterates on water temperature until a value is found which gives a calculated brightness temperature in agreement with the measured brightness temperature. The criteria for "agreement" was a brightness temperature within $\pm 1^{\circ}$ of the measured brightness temperature. The "error" that this allows in the computed value of water temperature is $\pm (1/\text{emissivity})$. Thus over the zenith angles of interest (i.e. 91.69° to 130.32°) the error that will be allowed by this agreement criteria varies from a high of $\pm 2^{\circ}$ maximum to a low of about $\pm 1^{\circ}$. ROCK 3 was used only to obtain the water temperatures of the vertical runs. It was not used for the horizontal runs since the error due to the agreement criteria would be excessive at angles near the horizon and since the apparent emissivity varied too much from the true emissivity. Those few horizontal runs which were tried in this computer program would not finalize in a reasonable number of iterations.

ROCK 3 determines a value of water temperature which satisfies the basic radiometric equation

$$T_b = \epsilon T_w + (1-\epsilon) T_s$$

Since it calculates a corresponding value of emissivity for each water temperature, the value of the emissivity will change each time the water temperature value is changed. The printout for ROCK 3 includes the computed emissivity and the real and imaginary parts of the computed permittivity. Since it was felt that the horizontally polarized measurements would contain sea state information these runs were processed in a slightly different fashion. The iteration process was not feasible because of limitations previously described, therefore a method was required which would restrain the horizontal emissivity within reasonable bounds. This was accomplished by using the permittivity values, computed in ROCK 3 for the adjacent vertical runs, to calculate the horizontal emissivity. Using this value of emissivity, the horizontal radiometric water temperature was calculated using a computer program named ROCKFN. These computed, restrained emissivity, values of water temperature were not expected to be representative of the thermometric water temperature, but the shape or displacement of the curves might be expected to correlate with the observed sea state.

In order to get a set of "reference" curves, ROCKEN was also used to compute the radiometric water temperature based on the theoretical values of permittivity and emissivity for sea water at 299 K.

A more direct approach to determine the sea state dependency of the horizontally polarized measurements would be to calculate the emissivity directly from the measured data. The basic radiometric equation can be used to solve for the emissivity as follows:

$$T_b = \epsilon T_w + (1 - \epsilon) T_s \quad (3)$$

$$T = \epsilon T_w + T_s - \epsilon T_s$$

$$T_b = \epsilon(T_w - T_s) + T_s$$

$$\epsilon = \frac{T_b - T_s}{T_w - T_s} \quad (4)$$

The derived emissivity for both the horizontal and vertical runs was calculated using equation (4) in computer program EMISS. The brightness temperatures and sky temperatures are obtained from the APCOR4 output. An arbitrary value of water temperature (T_w) of 299°K was used.

In order to allow for the non-specular surface of the actual sea water, the value of sky temperature (T_s) was actually an average over a cone of angles about the nominal angle. In order to easily accomodate the input data format this angular cone was defined in terms of a constant cosine differential. This cosine difference was in turn defined in terms of the antenna mesh size (m).

Thus

$$\begin{aligned} \Delta\theta &= \theta_{\max} - \theta_{\min} \\ \cos\theta_{\min} - \cos\theta &\approx 2(\frac{1}{m}) \\ \cos\theta - \cos\theta_{\max} &\approx 2(\frac{1}{m}) \\ \cos\theta_{\min} - \cos\theta_{\max} &\approx 4(\frac{1}{m}) \\ \cos\theta_{\min} - \cos\theta_{\max} &\approx 4(\frac{1}{34}) = 0.11765 \end{aligned}$$

where

$$\begin{aligned} \theta &= \text{nominal angle of reflected source} \\ \Delta\theta &= \text{cone of angles} \\ \theta_{\max} &= \text{upper limit of angular cone} \\ m &= \text{mesh size} = 34 \\ \theta_{\min} &= \text{lower limit of angular cone} \end{aligned}$$

The cosine differential used was this value of 0.11765 which defined the cone size.

The stability runs and the switched polarization runs, do not contain measurements at angles other than that of the particular observation. Thus the elevation profile for these runs is not defined. Therefore they were only processed to determine the apparent temperatures corresponding to the measured data. This processing was accomplished in a modification of the MODROD program, called RODMOD.

B. Data Tables and Plots

A typical computer printout of the MODROD program is shown in Tables VI-1A and 1B. Page 1 of this output lists the run information and the calibration parameters. The minimum and maximum calibration temperature are the cold and hot load temperatures referred to the antenna input. The k factor is the slope of the best fit straight line between the three calibration points. The calculated maximum, minimum and zenith temperatures are the temperatures represented by the calibration data points for the hot load, cold load and zenith sky. The amount by which these values differ from the maximum and minimum calibration temperatures and the zenith sky temperature is indicative of the fit of the best straight line calibration curve. The comments for the run are also printed out on this page.

Page 2 of this output tabulates the radiometric voltage, and the computed apparent temperature for each of the zenith angle measurements. Each radiometric voltage is the average of ten one second readings. The tabulated tolerances represent the maximum and minimum of these ten readings converted to a temperature difference. This tolerance was used for a variety of purposes. First it highlights any key punching errors, second it identifies points of possible interference and third it is a gross representation of the sensitivity of the equipment.

Tables VI-2 through VI-41 are the computer printouts from the APCOR4 program. These provide a tabulation of the apparent and brightness temperatures as a function of zenith angle. Figures VI-2 through VI-39 are standard plots of the apparent and brightness temperature and Figures VI-40 through VI-77 are expanded plots showing the temperature variation over the water. These plots may be analyzed more readily if the environment profile is known. Figure VI-13 describes the profile and shows the observation zenith angles. The sea water observations were limited to a zenith angle range between 90° and approximately 126° . Near the zenith angle of 126° the antenna beam intercepted the large riprap boulders which surrounded the island.

The 9.5 GHz curves are included in the standard plots (Figures VI-33 thru VI-39), but as previously discussed their value is questioned as there was interference present at this frequency. Three other curves merit special mention at this point. Runs 11 and 12 (Figures VI-9 and VI-10) were taken while it was raining. The general shape of the curves and the high sky temperatures cast doubt on their validity. The second set of curves in these figures represent a two point calibration (the first set uses a three point calibration). Run 35 (Figure VI-31) was taken when there were heavy thunder squall clouds on the observation azimuth and probably some heavy rain 3 to 5 miles from the observation site. This accounts for the relatively high temperature just above the horizon.

The expanded plots of the 9.5 GHz runs are shown in Figures VI-71 thru VI-77. The 16.5 GHz expanded plots are shown in Figures VI-40 thru VI-70. The temperature rise as the antenna beam intercepts the large boulders at the island edge is observable on all these plots at a zenith angle of about 126° . The computer printouts from ROCK 3 are reproduced in Tables VI-42 thru VI-61. The computed sea water temperatures from ROCK 3 are plotted on Figures VI-78 thru VI-96. The thermometric water temperature over the total period of measurements was within about $\pm 1.5^{\circ}$ of 299.5°K . The computed water temperatures are in agreement with this thermometric temperature on all of the 16.5 GHz plots (with the exception of Run 11) at a zenith angle that falls in the range of 103° to 114° . Thus a possible range of the invariant angle is suggested. The average value of this invariant angle is 109° .

ROCKFN computed the apparent sea water temperature for the horizontal runs using the permittivity values calculated in the adjacent vertical runs by ROCK 3. This restrained the allowable horizontal emissivity values and hence the output plots are referred to as restrained emissivity curves. The output data for the 16.5 GHz horizontal runs is plotted in Figure VI-97 thru VI-111. The apparent sea water temperature is quite different than the thermometric temperature. Examinations of these curves has shown no correlation with sea state.

ROCKFN also computed the apparent sea water temperature for both the horizontal and vertical runs using the theoretical value of permittivity for sea water at 29°K . This set of reference curves is plotted in Figure VI-112 thru VI-126.

The derived emissivities from the computer program EMISS are plotted in Figures VI-127 thru VI-163. The computer printouts for the derived emissivity are reproduced in Tables VI-62 thru VI-99. No direct correlation with sea state has been found in either the horizontal or vertical emissivity plots.

The radiometric measurements from the stability runs and the switched polarization runs have only been converted to apparent radiometric temperatures. These are plotted on Figures VI-164 thru VI-182 for the stability runs and on Figures VI-183 thru VI-191 for the switched polarization runs. Figures VI-192 and VI-193 are plots of a 9.5 GHz zenith stability run. These 9.5 GHz curves show severe interference toward the end of the run. These runs are plotted as a function of time, each plot presenting a total time interval of 1000 seconds or about 16-2/3 minutes. Those stability runs which took longer than that were plotted on successive plots.

The horizon check runs were made at both 16.5 and 9.5 GHz. These runs were made at a zenith angle of 90° and through a full 360° rotation in azimuth. These runs were plotted on the computer but are not included in this report since they are quite long.

The 9.5 GHz run showed severe interference at many points. Some of these were concentrated near the Norfolk Navy Yard and the Norfolk Municipal Airport, others were in areas where no specific local source could be identified. The apparent radiometric temperatures over the 360° azimuth rotation varied from a high of 498.9°K to a low of 178.8°K for vertical polarization and from 456.4K to 123.6°K for horizontal polarization.

The 16.5 GHz horizon check produced a much smoother curve, indicating much less interference. The apparent radiometric temperature ranges from 239.3°K to 166.7°K with the highest consistent temperatures being observed when the antenna was viewing the brick ventilation building on the island. The nominal building temperature was about 220°K, about 50°K above the nominal horizon temperature of 170°K.

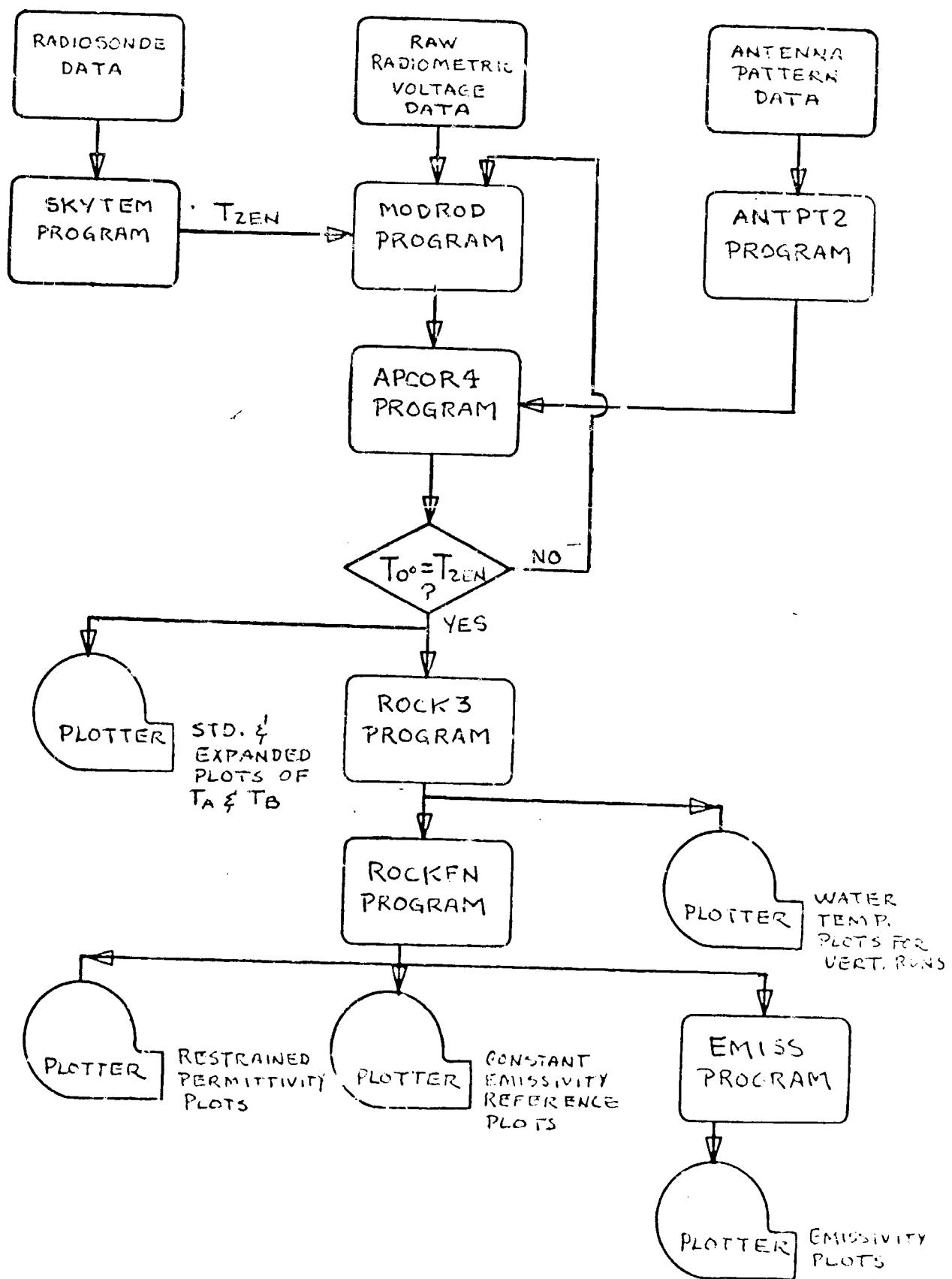


FIGURE VI-1A - DATA ANALYSIS FLOW

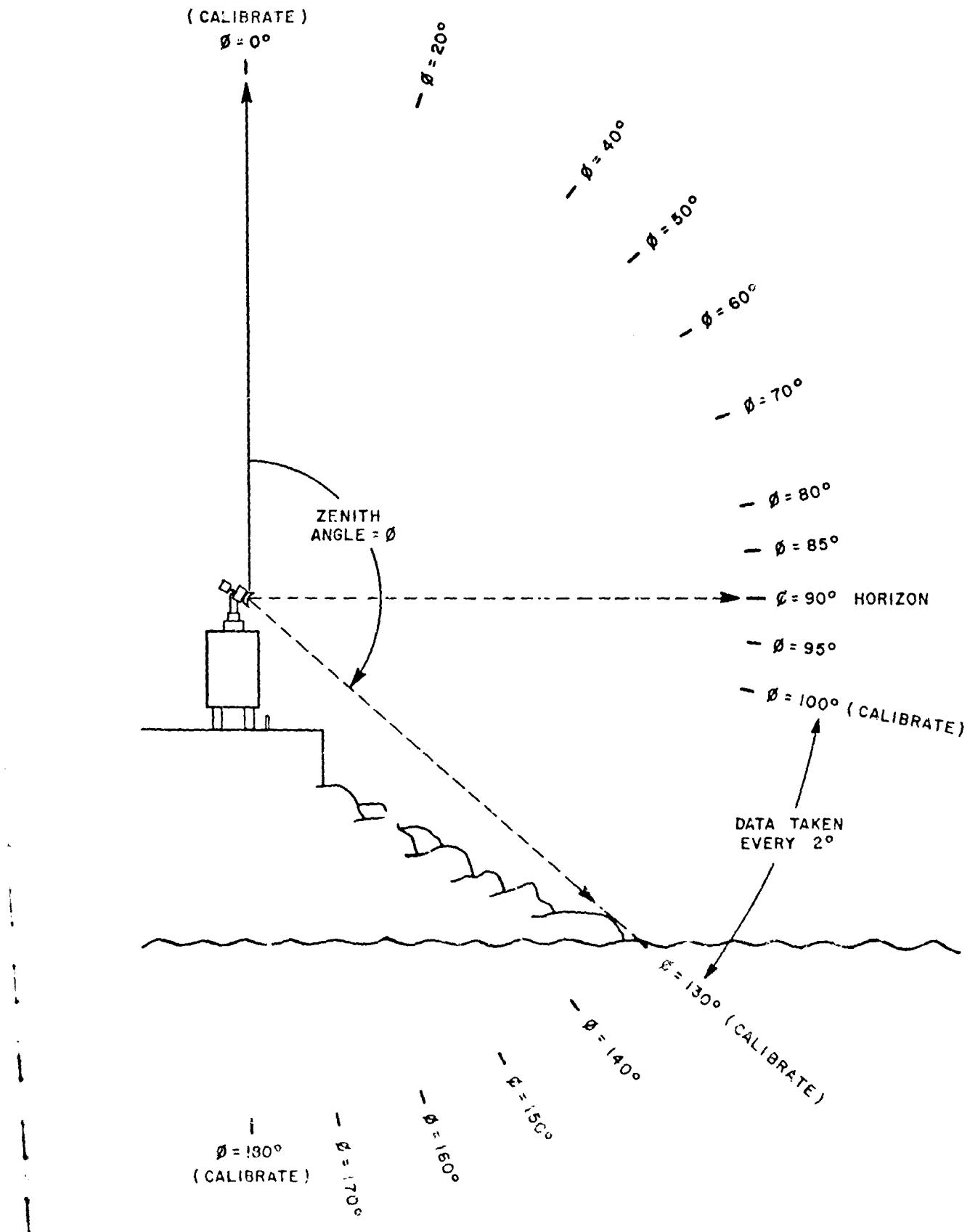


FIGURE VI-1B. MEASUREMENT SITE ENVIRONMENTAL PROFILE

PAGE 1 RUN 17

| | |
|-----------------------|----------|
| DATA DATE | 08/07/69 |
| START TIME | 165500 |
| FREQUENCY, GHZ | 16.3 |
| POLARIZATION | H |
| ANTENNA AZIMUTH, DEG | 310 |
| INTEGRATION TIME, SEC | 01 |
| ZENITH SKYTEMP | 18.0 |

| CALIBRATION DATA | INITIAL | CAL2 | CAL3 | FINAL |
|------------------------|----------|----------|----------|----------|
| MIN. CAL. TEMP, DEG, K | 307.91 | 307.35 | 307.19 | 307.09 |
| MAX. CAL. TEMP, DEG, K | 408.81 | 408.04 | 410.75 | 409.15 |
| K-FAC., # DEG, K/MV, | 0.2498 | 0.2494 | 0.2491 | 0.2487 |
| Y-INTERCEPT, DEG, K | -1372.22 | -1370.22 | -1369.19 | -1363.43 |

| CALIBRATION CONSTANTS | INITIAL | CAL2 | CAL3 | FINAL |
|------------------------|---------|---------|---------|---------|
| HOT LOAD | 401.50 | 400.90 | 403.50 | 402.00 |
| CAL WGS - MIN | 317.40 | 317.30 | 317.00 | 317.00 |
| CAL WGS - MAX | 317.80 | 317.70 | 317.50 | 317.50 |
| WAVE GUIDE SWITCH | 313.00 | 314.00 | 314.50 | 315.10 |
| ANTENNA | 300.90 | 301.50 | 301.50 | 301.00 |
| COLD LOAD | 307.00 | 306.60 | 306.50 | 306.40 |
| AVERAGE CAL. DATA-MAX, | 7130.90 | 7127.20 | 7146.50 | 7128.80 |
| -MIN. | 6726.00 | 6729.70 | 6728.50 | 6717.70 |
| -ZENITH | 5566.00 | 5565.10 | 5569.20 | 5555.60 |
| CALC. MAX TEMP. | 408.91 | 407.38 | 410.99 | 409.22 |
| CALC. MIN TEMP. | 307.78 | 308.24 | 306.87 | 306.99 |
| CALC. ZENITH TEMP. | 18.04 | 17.77 | 18.09 | 18.02 |

COMMENTS

2-5 % CIRRUS CLOUDS DRIFTING OVERHEAD
 1 FOOT SWELL 6-8 INCH CHOP WIND SOUTH 5-10 MPH
 HL-0-401.5 CL-0-307.0 INIT // HL-0-400.9 CL-0-306.6 CAL2 //
 HL-0-403.5 CL-0-306.5 CAL3 // HL-0-402.0 CL-0-306.4 FINI //

TABLE VI-1A SAMPLE MODROD OUTPUT

PAGE 2 RUN 17

| | |
|----------------|----------|
| DATA DATE | 08/07/69 |
| START TIME | 1655 |
| FREQUENCY, GHZ | 16.5 |
| POLARIZATION | H |

| ZENITH ANGLE DEG | APPARENT TEMP DEG K | READINGS MV | TOLERANCE +DEG | -DEG |
|------------------------|---------------------------|----------------|-------------------|------|
| 0.0 | 13.8 | 5549. | 1.9 | 2.5 |
| 20.0 | 20.7 | 5577. | 2.6 | 1.6 |
| 40.0 | 27.7 | 5605. | 1.3 | 1.5 |
| 50.0 | 32.8 | 5625. | 1.2 | 2.0 |
| 60.0 | 42.9 | 5666. | 1.5 | 1.9 |
| 70.0 | 56.5 | 5720. | 1.7 | 3.1 |
| 80.0 | 83.0 | 5826. | 3.1 | 2.3 |
| 85.0 | 120.2 | 5976. | 2.8 | 2.4 |
| 90.0 | 162.9 | 6147. | 1.6 | 1.9 |
| 95.0 | 116.3 | 5960. | 2.7 | 3.5 |
| 100.0 | 112.6 | 5945. | 2.0 | 2.3 |
| 102.0 | 113.8 | 5950. | 2.4 | 2.3 |
| 104.0 | 115.5 | 5957. | 3.9 | 2.3 |
| 106.0 | 115.8 | 5959. | 2.8 | 4.2 |
| 108.0 | 120.2 | 5977. | 1.6 | 1.6 |
| 110.0 | 123.5 | 5990. | 0.9 | 1.6 |
| 112.0 | 126.8 | 6004. | 3.1 | 3.1 |
| 114.0 | 129.1 | 6013. | 1.0 | 1.7 |
| 116.0 | 134.3 | 6034. | 3.7 | 2.1 |
| 118.0 | 137.3 | 6046. | 1.9 | 1.1 |
| 120.0 | 141.7 | 6064. | 1.9 | 3.1 |
| 122.0 | 144.4 | 6076. | 2.1 | 2.1 |
| 124.0 | 150.5 | 6100. | 2.9 | 2.3 |
| 126.0 | 161.2 | 6143. | 2.9 | 1.8 |
| 128.0 | 201.8 | 6306. | 3.4 | 5.3 |
| 130.0 | 249.9 | 6500. | 0.0 | 0.0 |
| 140.0 | 283.7 | 6633. | 0.9 | 0.8 |
| 150.0 | 287.8 | 6647. | 1.7 | 2.0 |
| 160.0 | 279.7 | 6613. | 1.8 | 1.4 |
| 170.0 | 213.6 | 6344. | 3.4 | 2.3 |
| 180.0 | 196.4 | 6273. | 2.5 | 1.5 |

TABLE VI-1B SAMPLE MOPROD C-TPUT

RUN NO. 1 07/25/69 4 POLAR, 9.5 GHZ SEA WATER
ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 3.91 | 10.68 | -6.8690 |
| 13.93 | 10.35 | 14.85 | -4.5023 |
| 19.75 | 13.08 | 17.55 | -4.4724 |
| 24.25 | 15.69 | 20.03 | -4.3377 |
| 28.07 | 18.74 | 22.39 | -3.6482 |
| 31.47 | 15.81 | 21.58 | -5.7704 |
| 34.56 | 19.38 | 24.44 | -5.0592 |
| 37.43 | 29.05 | 27.78 | -4.7283 |
| 40.12 | 27.09 | 31.52 | -4.4310 |
| 42.67 | 31.12 | 35.59 | -4.4696 |
| 45.10 | 41.23 | 42.91 | -1.6549 |
| 47.43 | 45.29 | 46.85 | -1.5631 |
| 49.68 | 48.54 | 49.85 | -1.3280 |
| 51.85 | 50.94 | 52.03 | -1.0907 |
| 53.97 | 52.75 | 53.44 | -0.6851 |
| 56.03 | 47.15 | 50.99 | -3.7462 |
| 58.03 | 48.58 | 52.06 | -3.4792 |
| 60.00 | 30.19 | 53.64 | -3.4510 |
| 61.93 | 52.03 | 55.63 | -3.5961 |
| 63.82 | 54.54 | 58.00 | -3.9569 |
| 65.68 | 62.31 | 63.65 | -1.3536 |
| 67.52 | 64.34 | 56.05 | -1.7158 |
| 69.33 | 63.78 | 58.00 | -2.0212 |
| 71.12 | 67.25 | 59.53 | -2.2801 |
| 72.90 | 68.50 | 70.64 | -2.1644 |
| 74.65 | 70.03 | 71.40 | -1.3671 |
| 76.39 | 52.59 | 62.55 | -9.9820 |
| 78.12 | 57.35 | 55.65 | -8.3155 |
| 79.84 | 63.43 | 70.72 | -7.2916 |
| 81.54 | 71.24 | 77.72 | -6.4796 |
| 83.24 | 92.07 | 91.54 | 0.5339 |
| 84.94 | 99.00 | 97.73 | 1.2711 |
| 86.63 | 102.30 | 100.91 | 1.3862 |
| 88.31 | 93.97 | 97.42 | -3.4540 |
| 90.00 | 94.77 | 98.34 | -3.5708 |
| 91.69 | 95.57 | 100.04 | -3.4757 |
| 93.37 | 95.76 | 100.97 | -5.2082 |
| 95.06 | 101.31 | 105.89 | -6.5830 |
| 96.76 | 109.75 | 113.24 | -3.4935 |
| 98.45 | 126.45 | 125.51 | 1.1380 |
| 100.16 | 138.16 | 134.95 | 3.2127 |
| 101.83 | 133.16 | 144.44 | 8.7216 |
| 103.61 | 165.41 | 149.49 | 15.9222 |
| 103.35 | 96.89 | 112.23 | -15.3364 |
| 107.10 | 96.31 | 110.49 | -14.1748 |
| 108.38 | 116.24 | 122.38 | -6.1421 |
| 110.67 | 131.32 | 135.41 | -1.0924 |
| 112.48 | 147.23 | 145.33 | 1.7022 |
| 114.32 | 171.57 | 158.75 | 12.8056 |
| 116.18 | 126.28 | 138.71 | -2.6347 |
| 118.07 | 102.14 | 118.44 | -16.3042 |
| 120.00 | 93.07 | 114.10 | -21.0265 |
| 121.97 | 127.31 | 136.57 | -9.0567 |
| 123.97 | 140.81 | 152.62 | -12.0120 |
| 126.03 | 208.00 | 198.57 | 9.4207 |
| 128.14 | 235.37 | 225.17 | 10.1994 |
| 130.32 | 286.08 | 262.39 | 23.6906 |
| 132.37 | 315.16 | 285.89 | 30.2666 |
| 134.90 | 330.34 | 294.99 | 33.3470 |
| 137.33 | 264.90 | 259.03 | 3.9412 |
| 139.88 | 272.27 | 250.59 | 11.6778 |
| 142.37 | 274.64 | 242.88 | 11.7609 |
| 145.44 | 285.13 | 270.69 | 15.4431 |
| 148.53 | 287.34 | 272.65 | 14.6833 |
| 151.93 | 284.13 | 271.71 | 12.4115 |
| 155.75 | 294.58 | 275.81 | 18.7650 |
| 159.28 | 275.37 | 254.69 | 20.6805 |
| 166.07 | 140.06 | 157.62 | -27.5621 |
| 180.00 | 146.89 | 160.50 | -13.6076 |

ABS. CORRECTION = 7.90E 00 DEC. K

RUN NO. 2 07/25/69 V POLAR, 9.3 MHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 3.67 | 21.64 | -17.9661 |
| 13.93 | 42.50 | 44.55 | -2.0475 |
| 19.75 | 49.19 | 52.26 | -3.0736 |
| 24.25 | 54.65 | 57.49 | -2.8286 |
| 28.07 | 58.71 | 61.40 | -2.6941 |
| 31.47 | 60.07 | 63.61 | -3.5199 |
| 34.56 | 62.59 | 66.27 | -3.5866 |
| 37.43 | 64.63 | 68.61 | -3.9830 |
| 40.12 | 66.43 | 70.70 | -4.2732 |
| 42.67 | 67.94 | 72.58 | -4.6450 |
| 45.10 | 71.30 | 75.30 | -4.0072 |
| 47.43 | 72.32 | 76.62 | -4.2995 |
| 49.68 | 72.86 | 77.41 | -4.5465 |
| 51.86 | 72.92 | 77.71 | -4.7891 |
| 53.97 | 72.61 | 77.57 | -4.9532 |
| 56.03 | 68.21 | 75.25 | -7.0368 |
| 58.03 | 67.59 | 74.93 | -7.3431 |
| 60.00 | 66.99 | 74.83 | -7.6430 |
| 61.93 | 66.50 | 74.93 | -8.4334 |
| 63.82 | 66.21 | 75.22 | -9.0133 |
| 65.68 | 66.21 | 75.74 | -9.5261 |
| 67.52 | 66.30 | 76.37 | -10.0769 |
| 69.33 | 66.32 | 77.17 | -10.6504 |
| 71.12 | 67.01 | 78.11 | -11.1066 |
| 72.90 | 68.36 | 79.20 | -10.8467 |
| 74.65 | 70.98 | 80.44 | -9.4623 |
| 76.39 | 45.15 | 57.69 | -2.5469 |
| 78.12 | 54.27 | 73.98 | -19.7135 |
| 79.84 | 86.65 | 84.00 | -17.3588 |
| 81.56 | 82.81 | 97.70 | -14.2933 |
| 83.24 | 100.40 | 113.74 | -13.3384 |
| 84.94 | 126.33 | 135.89 | -9.5660 |
| 86.63 | 158.10 | 152.93 | -4.8300 |
| 88.31 | 220.41 | 205.97 | 14.4371 |
| 90.00 | 250.48 | 231.65 | 14.9318 |
| 91.69 | 273.04 | 250.93 | 22.1133 |
| 93.37 | 286.04 | 252.87 | 23.1667 |
| 95.06 | 294.82 | 270.35 | 24.4756 |
| 96.76 | 296.92 | 272.36 | 24.5462 |
| 98.46 | 275.20 | 253.07 | 16.1249 |
| 100.16 | 276.50 | 250.76 | 15.7188 |
| 101.86 | 276.14 | 259.48 | 16.6554 |
| 103.61 | 267.29 | 233.50 | 13.7873 |
| 105.35 | 260.00 | 247.72 | 12.2813 |
| 107.10 | 245.70 | 238.23 | 7.4730 |
| 108.88 | 237.62 | 232.17 | 5.4536 |
| 110.67 | 235.79 | 230.12 | 6.5684 |
| 112.48 | 232.44 | 223.09 | 6.3539 |
| 114.32 | 227.18 | 220.65 | 6.5241 |
| 116.18 | 198.79 | 201.95 | -3.1634 |
| 118.07 | 190.25 | 195.75 | -3.5025 |
| 120.00 | 186.39 | 192.15 | -3.7562 |
| 121.97 | 176.91 | 187.41 | -10.4979 |
| 123.97 | 178.26 | 190.99 | -12.7512 |
| 126.03 | 208.66 | 212.88 | -4.2201 |
| 128.14 | 253.71 | 244.07 | 9.0440 |
| 130.22 | 273.36 | 262.66 | 12.7007 |
| 132.57 | 290.70 | 275.38 | 15.3172 |
| 134.90 | 299.12 | 281.37 | 17.7572 |
| 137.33 | 273.10 | 257.65 | 5.4466 |
| 139.88 | 276.51 | 258.83 | 7.6772 |
| 142.57 | 276.86 | 259.31 | 7.4914 |
| 145.44 | 277.17 | 259.68 | 7.4860 |
| 148.33 | 274.53 | 257.91 | 5.6177 |
| 151.93 | 268.00 | 254.09 | 3.9049 |
| 155.75 | 280.85 | 258.39 | 12.2628 |
| 160.23 | 259.91 | 245.30 | 16.6043 |
| 166.07 | 116.73 | 132.17 | -35.4363 |
| 180.00 | 117.76 | 140.56 | -22.7780 |

ABS CORRECTION = 1.06E 01 DEG. K

TABLE VI-3. APCOR4 OUTPUT

RUN NO. 4 07/29/69 V POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.85 | 27.13 | -14.2759 |
| 13.93 | 31.37 | 38.50 | -7.1222 |
| 19.75 | 34.73 | 42.61 | -7.8792 |
| 24.23 | 37.18 | 45.54 | -8.3570 |
| 28.07 | 37.35 | 47.25 | -9.6990 |
| 31.47 | 40.42 | 50.41 | -9.9024 |
| 34.56 | 43.59 | 53.94 | -10.2431 |
| 37.43 | 45.40 | 56.86 | -11.4539 |
| 40.12 | 50.62 | 51.91 | -11.2844 |
| 42.67 | 56.29 | 57.76 | -11.6677 |
| 45.10 | 70.22 | 78.09 | -7.8713 |
| 47.43 | 76.71 | 84.38 | -7.6677 |
| 49.68 | 82.35 | 89.71 | -7.3579 |
| 51.86 | 86.89 | 94.18 | -7.2961 |
| 53.97 | 90.82 | 97.88 | -7.0650 |
| 56.03 | 86.91 | 97.37 | -10.4590 |
| 58.03 | 90.68 | 100.91 | -10.2322 |
| 60.00 | 94.78 | 104.96 | -10.1805 |
| 61.93 | 99.51 | 109.50 | -9.9916 |
| 63.82 | 105.04 | 114.50 | -9.4656 |
| 65.68 | 108.13 | 118.43 | -10.3052 |
| 67.52 | 113.24 | 124.68 | -9.4440 |
| 69.33 | 123.26 | 131.76 | -8.4927 |
| 71.12 | 132.33 | 139.63 | -7.3052 |
| 72.90 | 142.39 | 148.30 | -5.9952 |
| 74.65 | 153.25 | 157.72 | -6.4776 |
| 76.35 | 169.97 | 170.36 | -0.3808 |
| 78.12 | 181.66 | 180.46 | 1.1945 |
| 79.84 | 193.75 | 190.69 | 3.0624 |
| 81.54 | 206.13 | 201.03 | 5.07 |
| 83.24 | 218.83 | 211.58 | 7.2690 |
| 84.94 | 251.60 | 242.16 | 9.4490 |
| 86.63 | 244.46 | 232.69 | 11.5705 |
| 88.31 | 264.15 | 246.84 | 17.3019 |
| 90.00 | 273.27 | 254.69 | 18.3851 |
| 91.69 | 276.64 | 259.51 | 19.1308 |
| 93.37 | 274.91 | 258.91 | 15.9997 |
| 95.06 | 275.72 | 260.21 | 15.5166 |
| 96.75 | 275.75 | 250.57 | 16.7839 |
| 98.46 | 273.90 | 251.56 | 14.3445 |
| 100.16 | 271.05 | 250.79 | 13.2575 |
| 101.88 | 270.99 | 259.08 | 11.9090 |
| 103.61 | 264.11 | 251.34 | 8.7683 |
| 105.33 | 264.94 | 255.31 | 9.4384 |
| 107.10 | 261.51 | 253.42 | 8.0816 |
| 108.88 | 257.02 | 250.58 | 6.4490 |
| 110.67 | 252.38 | 247.56 | 5.0189 |
| 112.46 | 247.21 | 243.91 | 3.2995 |
| 114.32 | 241.74 | 240.03 | 1.8036 |
| 116.18 | 231.25 | 233.46 | -2.2066 |
| 118.07 | 228.55 | 231.05 | -2.5064 |
| 120.00 | 223.09 | 227.42 | -4.3284 |
| 121.97 | 216.69 | 223.36 | -6.6704 |
| 123.97 | 208.58 | 218.83 | -10.2448 |
| 126.03 | 207.17 | 218.74 | -11.5692 |
| 128.14 | 211.19 | 223.50 | -12.3135 |
| 130.32 | 245.90 | 245.86 | 0.0407 |
| 132.57 | 260.16 | 253.71 | 6.4097 |
| 134.80 | 285.14 | 274.20 | 10.8623 |
| 137.33 | 277.25 | 272.14 | 5.10 |
| 139.88 | 203.32 | 278.30 | 8.0215 |
| 142.37 | 291.93 | 282.59 | 9.3375 |
| 145.44 | 292.29 | 283.44 | 8.8444 |
| 148.53 | 292.15 | 283.35 | 8.7917 |
| 151.93 | 288.83 | 280.85 | 7.9813 |
| 155.75 | 281.16 | 274.88 | 6.2741 |
| 160.25 | 268.45 | 264.10 | 4.3352 |
| 166.07 | 236.16 | 239.94 | -3.7821 |
| 180.00 | 170.04 | 200.98 | -30.9427 |

ABS. CORRECTION = 8.95E 00 DEG. K

TABLE VI-4. APCOM4 OUTPUT

RUN NO. 3 08/01/69 V POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.50 | 19.37 | -6.7699 |
| 13.93 | 20.94 | 24.62 | -3.6812 |
| 19.75 | 23.38 | 27.22 | -3.8381 |
| 24.25 | 25.41 | 29.40 | -3.9864 |
| 28.07 | 27.13 | 31.35 | -4.2315 |
| 31.47 | 28.10 | 32.90 | -4.8015 |
| 34.56 | 29.55 | 34.69 | -5.1381 |
| 37.43 | 30.91 | 36.45 | -5.5518 |
| 40.12 | 32.10 | 38.22 | -6.1162 |
| 42.67 | 33.11 | 39.97 | -6.8631 |
| 45.10 | 34.16 | 41.78 | -7.6212 |
| 47.43 | 35.08 | 43.52 | -8.4370 |
| 49.68 | 35.01 | 45.25 | -9.2204 |
| 51.86 | 36.97 | 46.97 | -9.9618 |
| 53.97 | 38.10 | 48.62 | -10.5241 |
| 56.03 | 37.10 | 49.23 | -12.1279 |
| 58.03 | 38.66 | 51.26 | -12.6043 |
| 60.00 | 40.51 | 53.64 | -13.1345 |
| 61.93 | 42.78 | 56.34 | -13.5582 |
| 63.82 | 45.58 | 59.34 | -13.7568 |
| 65.68 | 47.17 | 61.82 | -14.6473 |
| 67.52 | 50.98 | 65.39 | -14.6107 |
| 69.33 | 55.32 | 69.86 | -14.5419 |
| 71.12 | 60.25 | 74.61 | -14.3559 |
| 72.90 | 65.89 | 79.83 | -13.9384 |
| 74.65 | 72.39 | 85.50 | -13.1137 |
| 76.39 | 72.69 | 88.28 | -15.5947 |
| 78.12 | 81.59 | 95.99 | -14.3951 |
| 79.84 | 91.80 | 104.99 | -3.1931 |
| 81.54 | 103.84 | 115.27 | -11.4261 |
| 83.24 | 107.20 | 121.85 | -14.6592 |
| 84.94 | 128.99 | 139.37 | -10.4736 |
| 86.63 | 158.19 | 163.10 | -4.9073 |
| 88.31 | 223.55 | 236.03 | 17.5220 |
| 90.00 | 252.22 | 229.18 | 23.0359 |
| 91.69 | 272.73 | 245.35 | 26.8799 |
| 93.37 | 274.81 | 250.74 | 24.0733 |
| 95.06 | 281.53 | 256.96 | 24.5663 |
| 96.76 | 284.15 | 250.14 | 24.0048 |
| 98.46 | 276.65 | 257.42 | 19.2329 |
| 100.16 | 275.80 | 257.70 | 18.1059 |
| 101.85 | 275.00 | 257.93 | 17.0623 |
| 103.61 | 276.97 | 259.21 | 17.7612 |
| 105.33 | 267.36 | 251.17 | 13.1947 |
| 107.10 | 262.27 | 251.25 | 11.5174 |
| 108.88 | 260.35 | 250.10 | 10.2526 |
| 110.67 | 258.46 | 248.95 | 9.7084 |
| 112.48 | 250.87 | 244.44 | 6.4260 |
| 114.32 | 244.04 | 240.31 | 3.7256 |
| 116.18 | 241.26 | 238.24 | 3.0221 |
| 118.07 | 232.55 | 233.25 | -0.6983 |
| 120.00 | 228.12 | 230.70 | -2.5754 |
| 121.97 | 227.53 | 230.41 | -2.8801 |
| 123.97 | 220.47 | 226.99 | -6.5235 |
| 126.03 | 211.59 | 223.59 | -11.9900 |
| 128.14 | 219.19 | 231.36 | -12.1682 |
| 130.32 | 267.96 | 252.90 | 5.0577 |
| 132.57 | 298.82 | 285.50 | 13.3198 |
| 134.90 | 318.24 | 299.30 | 18.7345 |
| 137.33 | 293.57 | 288.21 | 5.4572 |
| 139.68 | 304.44 | 295.03 | 9.4367 |
| 142.57 | 311.13 | 300.35 | 10.7726 |
| 145.44 | 313.79 | 303.02 | 10.7714 |
| 148.53 | 315.73 | 304.82 | 10.9077 |
| 151.93 | 314.65 | 304.64 | 10.0126 |
| 155.75 | 316.15 | 304.56 | 11.5952 |
| 160.25 | 304.67 | 294.35 | 10.3254 |
| 166.07 | 256.12 | 250.21 | -4.0872 |
| 180.00 | 180.40 | 215.09 | -34.6918 |

ABS. CORRECTION = 1.15E 01 DEG. K

RUN NO. 6 08/01/69 H : POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.51 | 16.35 | -3.8527 |
| 13.93 | 13.64 | 17.51 | -3.8755 |
| 19.75 | 14.74 | 18.89 | -4.1514 |
| 24.25 | 15.92 | 20.31 | -4.3945 |
| 28.07 | 17.34 | 21.77 | -4.4382 |
| 31.47 | 16.62 | 22.14 | -5.5177 |
| 34.56 | 18.22 | 23.86 | -5.6361 |
| 37.43 | 19.88 | 25.79 | -5.9106 |
| 40.12 | 21.73 | 27.89 | -6.1626 |
| 42.67 | 23.78 | 30.13 | -6.3511 |
| 45.10 | 25.60 | 32.26 | -6.6581 |
| 47.43 | 28.21 | 34.81 | -6.6046 |
| 49.68 | 31.15 | 37.57 | -6.4221 |
| 51.86 | 34.31 | 40.52 | -6.2101 |
| 53.97 | 37.63 | 43.65 | -6.0232 |
| 56.03 | 42.60 | 47.74 | -5.0597 |
| 58.03 | 45.99 | 50.93 | -4.9384 |
| 60.00 | 49.23 | 54.02 | -4.7921 |
| 61.93 | 52.42 | 57.02 | -4.5952 |
| 63.82 | 55.73 | 59.93 | -4.2012 |
| 65.68 | 58.28 | 60.43 | -6.1514 |
| 67.52 | 58.04 | 63.75 | -5.7204 |
| 69.33 | 62.29 | 67.66 | -5.3749 |
| 71.12 | 67.18 | 72.11 | -6.9237 |
| 72.90 | 73.02 | 77.08 | -4.0678 |
| 74.65 | 80.15 | 82.58 | -2.4341 |
| 76.39 | 73.40 | 81.34 | -7.9340 |
| 78.12 | 85.07 | 90.30 | -5.2318 |
| 79.84 | 98.79 | 101.61 | -2.8255 |
| 81.54 | 114.91 | 115.24 | -0.3273 |
| 83.24 | 143.24 | 135.51 | 7.7278 |
| 84.94 | 159.66 | 149.58 | 10.0728 |
| 86.63 | 173.29 | 161.57 | 11.7230 |
| 88.31 | 198.37 | 177.87 | 20.4968 |
| 90.00 | 199.39 | 179.36 | 20.0301 |
| 91.69 | 190.29 | 172.32 | 17.9678 |
| 93.37 | 143.26 | 144.22 | -0.9588 |
| 95.06 | 129.48 | 133.28 | -3.7958 |
| 96.76 | 120.79 | 126.77 | -5.9826 |
| 98.46 | 124.88 | 128.14 | -3.2583 |
| 100.16 | 122.10 | 126.69 | -4.5902 |
| 101.88 | 120.59 | 126.07 | -5.4815 |
| 103.61 | 120.07 | 126.17 | -6.0944 |
| 105.35 | 119.93 | 126.57 | -7.0362 |
| 107.10 | 122.74 | 129.19 | -6.4518 |
| 108.88 | 126.04 | 132.04 | -6.0055 |
| 110.67 | 127.90 | 134.15 | -6.2663 |
| 112.48 | 127.91 | 135.37 | -7.4584 |
| 114.32 | 131.39 | 138.43 | -7.0410 |
| 116.18 | 135.24 | 141.72 | -6.4796 |
| 118.07 | 133.00 | 141.98 | -8.9804 |
| 120.00 | 135.87 | 145.07 | -9.1950 |
| 121.97 | 140.54 | 149.60 | -9.0637 |
| 123.97 | 140.65 | 153.12 | -12.4676 |
| 126.03 | 147.99 | 153.76 | -15.7683 |
| 128.14 | 195.61 | 199.95 | -4.3334 |
| 130.32 | 277.09 | 256.46 | 20.6377 |
| 132.57 | 325.36 | 293.96 | 32.3997 |
| 134.90 | 353.17 | 311.73 | 41.4346 |
| 137.33 | 273.45 | 269.10 | 6.3439 |
| 139.88 | 285.49 | 275.35 | 13.1316 |
| 142.57 | 294.11 | 281.46 | 14.4698 |
| 145.44 | 308.43 | 291.81 | 17.6229 |
| 148.53 | 313.55 | 296.03 | 17.5165 |
| 151.93 | 314.42 | 297.97 | 16.4576 |
| 155.75 | 319.29 | 300.20 | 19.0922 |
| 160.25 | 306.14 | 287.37 | 18.7743 |
| 166.07 | 239.65 | 237.39 | -2.7318 |
| 180.00 | 158.20 | 189.42 | -34.1447 |

ABS. CORRECTION = 9.11E 00 DEG. K

TABLE VI-6. APCOR4 OUTPUT

RUN NO. 7 08/01/69 + POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP., (DEG K) | APPARENT TEMP., (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|------------------------------|----------------------------|-----------------------------|
| 0.00 | 12.98 | 15.70 | -3.1248 |
| 13.93 | 12.08 | 15.97 | -3.8947 |
| 19.75 | 13.29 | 17.35 | -4.0758 |
| 24.25 | 14.68 | 18.95 | -4.2674 |
| 28.07 | 16.00 | 20.65 | -4.6545 |
| 31.47 | 19.28 | 23.44 | -4.1659 |
| 34.56 | 20.41 | 25.10 | -4.6848 |
| 37.43 | 21.47 | 26.65 | -5.1771 |
| 40.12 | 22.46 | 28.12 | -5.6562 |
| 42.67 | 23.55 | 29.51 | -5.9687 |
| 45.10 | 22.70 | 29.84 | -7.1392 |
| 47.43 | 24.16 | 31.38 | -7.2174 |
| 49.68 | 26.10 | 33.29 | -7.1918 |
| 51.85 | 28.43 | 35.55 | -7.1201 |
| 53.97 | 31.07 | 38.12 | -7.0513 |
| 56.03 | 35.65 | 41.80 | -6.1558 |
| 58.03 | 38.53 | 44.66 | -6.1256 |
| 60.00 | 41.46 | 47.51 | -6.0535 |
| 61.93 | 44.46 | 50.35 | -5.8977 |
| 63.82 | 47.70 | 53.22 | -5.5173 |
| 65.68 | 49.90 | 53.55 | -7.6495 |
| 67.52 | 49.83 | 57.03 | -7.2031 |
| 69.33 | 54.36 | 61.19 | -6.8295 |
| 71.12 | 59.74 | 66.02 | -6.2875 |
| 72.90 | 64.49 | 71.50 | -5.0146 |
| 74.65 | 75.38 | 77.61 | -2.2272 |
| 76.39 | 53.74 | 59.67 | +13.9392 |
| 78.12 | 72.79 | 81.98 | -9.1881 |
| 79.84 | 93.18 | 98.62 | -5.2396 |
| 81.54 | 118.22 | 119.53 | -1.3132 |
| 83.24 | 173.19 | 156.30 | 17.0928 |
| 84.94 | 193.07 | 174.67 | 20.3956 |
| 86.63 | 207.64 | 185.60 | 22.0434 |
| 88.31 | 210.16 | 188.64 | 21.5195 |
| 90.00 | 205.54 | 185.35 | 20.1869 |
| 91.69 | 192.65 | 175.23 | 17.4216 |
| 93.37 | 146.91 | 147.17 | -0.2629 |
| 95.06 | 131.47 | 135.03 | -3.5511 |
| 96.76 | 121.45 | 127.52 | -6.0710 |
| 98.44 | 124.93 | 128.28 | -3.3505 |
| 100.16 | 121.20 | 126.05 | -4.8565 |
| 101.88 | 118.79 | 124.70 | -3.9143 |
| 103.61 | 115.13 | 123.12 | -7.9915 |
| 105.35 | 117.25 | 125.05 | -7.8021 |
| 107.10 | 125.45 | 130.42 | -4.9714 |
| 108.84 | 126.38 | 132.08 | -5.7007 |
| 110.67 | 122.02 | 131.13 | -9.1109 |
| 112.42 | 131.98 | 137.58 | -5.6983 |
| 114.32 | 139.07 | 142.48 | -3.4098 |
| 116.18 | 126.04 | 136.07 | -12.0347 |
| 118.07 | 137.28 | 144.46 | -7.1772 |
| 120.00 | 142.80 | 149.40 | -6.6044 |
| 121.97 | 142.56 | 151.48 | -8.9145 |
| 123.97 | 144.46 | 155.58 | -11.1347 |
| 126.03 | 145.85 | 152.88 | -17.0250 |
| 128.14 | 200.13 | 201.72 | -1.5883 |
| 130.32 | 268.70 | 250.46 | 10.2392 |
| 132.57 | 311.85 | 283.69 | 28.1645 |
| 134.90 | 336.57 | 300.59 | 35.9844 |
| 137.33 | 273.97 | 257.89 | 6.0769 |
| 139.88 | 288.46 | 274.08 | 13.5820 |
| 142.57 | 296.52 | 281.59 | 14.9384 |
| 143.64 | 308.23 | 290.60 | 17.6303 |
| 148.53 | 312.88 | 295.33 | 17.5527 |
| 151.93 | 313.65 | 297.15 | 16.4954 |
| 155.75 | 317.96 | 298.99 | 18.8658 |
| 160.25 | 304.87 | 286.29 | 18.5824 |
| 166.07 | 232.46 | 236.69 | -6.2282 |
| 180.00 | 169.11 | 197.45 | -28.3368 |

APJ. CORRECTION = 9.66E 00 DEG, K

TABLE VI-7. APCOR4 OUTPUT

RUN NO. 8 08/01/69 V POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 16.52 | 16.85 | -2.3305 |
| 13.93 | 10.01 | 14.88 | -4.863 |
| 19.75 | 10.93 | 15.92 | -4.9910 |
| 24.25 | 12.05 | 17.47 | -5.4262 |
| 28.07 | 13.34 | 19.31 | -5.7722 |
| 31.47 | 15.97 | 21.90 | -5.9320 |
| 34.56 | 17.50 | 23.97 | -6.4624 |
| 37.43 | 19.01 | 26.05 | -7.0464 |
| 40.12 | 20.39 | 28.17 | -7.7780 |
| 42.67 | 21.71 | 30.31 | -8.5944 |
| 45.10 | 22.62 | 32.24 | -9.6231 |
| 47.43 | 24.14 | 34.49 | -10.3441 |
| 49.68 | 25.89 | 36.85 | -10.9633 |
| 51.85 | 27.79 | 39.34 | -11.5516 |
| 53.97 | 29.90 | 41.93 | -12.0293 |
| 56.03 | 31.22 | 44.15 | -12.9359 |
| 58.03 | 33.79 | 47.10 | -13.3129 |
| 60.00 | 36.60 | 50.29 | -13.6932 |
| 61.93 | 39.73 | 53.71 | -13.9762 |
| 63.82 | 43.36 | 57.35 | -13.9938 |
| 65.68 | 44.69 | 59.87 | -15.1857 |
| 67.52 | 49.37 | 54.26 | -14.8941 |
| 69.33 | 54.59 | 59.20 | -14.6147 |
| 71.12 | 60.38 | 74.69 | -14.3137 |
| 72.90 | 67.09 | 80.71 | -13.6210 |
| 74.65 | 75.31 | 87.25 | -11.7422 |
| 76.39 | 60.28 | 82.18 | -21.7934 |
| 78.12 | 75.76 | 93.84 | -18.0816 |
| 79.84 | 94.57 | 109.09 | -14.5210 |
| 81.54 | 117.67 | 127.88 | -10.2123 |
| 83.24 | 151.67 | 153.00 | -1.3333 |
| 84.94 | 180.71 | 176.11 | 4.6017 |
| 86.63 | 210.29 | 199.87 | 10.4236 |
| 88.31 | 258.25 | 232.51 | 25.7471 |
| 90.00 | 278.61 | 249.39 | 29.2207 |
| 91.69 | 289.33 | 258.61 | 30.7178 |
| 93.37 | 274.68 | 253.08 | 21.6011 |
| 95.05 | 275.18 | 254.47 | 20.7157 |
| 96.74 | 275.20 | 255.54 | 19.6518 |
| 98.46 | 271.67 | 254.79 | 16.8861 |
| 100.16 | 274.01 | 257.01 | 17.0014 |
| 101.88 | 279.86 | 250.84 | 19.0136 |
| 103.61 | 275.59 | 259.05 | 16.5320 |
| 105.35 | 272.54 | 257.23 | 15.3094 |
| 107.10 | 264.45 | 252.35 | 12.1053 |
| 108.88 | 254.18 | 246.11 | 8.0701 |
| 110.61 | 245.39 | 240.81 | 4.5816 |
| 112.48 | 245.42 | 240.22 | 5.2049 |
| 114.32 | 238.35 | 236.07 | 2.2852 |
| 116.12 | 233.17 | 232.77 | 0.3927 |
| 118.07 | 229.50 | 230.24 | -0.7421 |
| 120.00 | 219.27 | 224.57 | -5.2987 |
| 121.97 | 217.16 | 223.46 | -6.3044 |
| 123.97 | 215.73 | 223.19 | -7.4698 |
| 126.03 | 205.25 | 219.54 | -14.2892 |
| 128.14 | 222.46 | 232.54 | -10.0825 |
| 130.32 | 261.02 | 250.83 | 4.1955 |
| 132.57 | 293.18 | 281.62 | 11.5657 |
| 134.90 | 311.61 | 294.89 | 16.7213 |
| 137.33 | 292.41 | 287.05 | 5.7655 |
| 139.88 | 303.61 | 294.15 | 9.4475 |
| 142.57 | 310.73 | 299.84 | 10.6836 |
| 145.44 | 313.49 | 302.76 | 10.7347 |
| 148.53 | 316.28 | 305.22 | 11.0560 |
| 151.93 | 316.31 | 306.04 | 10.2716 |
| 155.75 | 322.99 | 309.13 | 13.8629 |
| 160.25 | 312.30 | 299.22 | 13.0746 |
| 166.07 | 256.00 | 250.12 | -4.1186 |
| 180.00 | 172.47 | 210.06 | -37.5930 |

C ABS. CORRECTION = 1.19E 01 DEG. K

TABLE VI-8. APCOR4 OUTPUT

RUN NO. 9 08/01/69 V POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0.

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.93 | 17.63 | -5.0966 |
| 13.93 | 13.46 | 18.97 | -4.5134 |
| 19.75 | 14.94 | 20.95 | -6.3108 |
| 24.25 | 16.46 | 23.05 | -6.5215 |
| 28.07 | 17.83 | 25.23 | -7.3950 |
| 31.47 | 19.86 | 27.89 | -8.0274 |
| 34.56 | 21.01 | 30.09 | -9.0837 |
| 37.43 | 22.22 | 32.27 | -10.0453 |
| 40.12 | 23.47 | 34.44 | -10.9609 |
| 42.67 | 24.84 | 36.60 | -11.7528 |
| 45.10 | 24.64 | 37.92 | -13.2765 |
| 47.43 | 26.24 | 40.27 | -14.0335 |
| 49.68 | 28.25 | 42.96 | -14.7101 |
| 51.86 | 30.72 | 45.97 | -15.2431 |
| 53.97 | 33.72 | 49.26 | -15.5375 |
| 56.03 | 35.42 | 51.98 | -16.5656 |
| 58.03 | 39.50 | 56.08 | -16.5731 |
| 60.00 | 44.15 | 60.68 | -16.9287 |
| 61.93 | 49.53 | 65.76 | -16.2322 |
| 63.82 | 56.36 | 71.31 | -14.9536 |
| 65.68 | 64.64 | 88.67 | -22.0278 |
| 67.52 | 56.97 | 77.16 | -20.1875 |
| 69.37 | 70.07 | 88.36 | -18.2906 |
| 71.12 | 86.58 | 102.20 | -19.6188 |
| 72.90 | 106.09 | 118.59 | -12.5003 |
| 74.65 | 127.30 | 137.48 | -10.1834 |
| 76.39 | 187.72 | 176.89 | 10.8364 |
| 78.12 | 206.86 | 194.52 | 12.3345 |
| 79.84 | 224.95 | 209.94 | 15.0102 |
| 81.54 | 240.72 | 223.20 | 17.5187 |
| 83.24 | 253.80 | 234.41 | 19.3868 |
| 84.94 | 263.94 | 243.40 | 20.5406 |
| 86.63 | 271.43 | 250.27 | 21.1635 |
| 88.31 | 274.86 | 254.38 | 20.4830 |
| 90.00 | 277.89 | 257.69 | 20.1998 |
| 91.69 | 279.14 | 259.57 | 19.5690 |
| 93.37 | 275.98 | 258.82 | 17.1572 |
| 95.06 | 273.29 | 259.12 | 16.1729 |
| 96.76 | 274.38 | 259.23 | 15.1480 |
| 98.46 | 273.93 | 259.46 | 14.4675 |
| 100.16 | 272.14 | 248.86 | 13.2822 |
| 101.88 | 269.66 | 257.73 | 11.9328 |
| 103.61 | 267.60 | 256.58 | 11.0206 |
| 105.35 | 260.33 | 252.66 | 7.6638 |
| 107.10 | 259.68 | 252.00 | 7.6719 |
| 108.88 | 255.61 | 249.51 | 6.1045 |
| 110.67 | 248.18 | 245.22 | 2.9503 |
| 112.48 | 247.61 | 244.34 | 3.2674 |
| 114.32 | 239.89 | 239.77 | 0.1135 |
| 116.18 | 234.75 | 236.40 | -1.6524 |
| 118.07 | 227.94 | 232.43 | -4.4966 |
| 120.00 | 227.07 | 231.84 | -4.7696 |
| 121.97 | 223.32 | 230.12 | -6.8015 |
| 123.97 | 221.90 | 229.82 | -7.9213 |
| 126.03 | 216.08 | 228.28 | -12.2052 |
| 128.14 | 229.36 | 233.63 | -9.2757 |
| 130.32 | 267.68 | 253.73 | 3.9467 |
| 132.57 | 292.67 | 291.92 | 10.7468 |
| 134.90 | 300.63 | 293.19 | 15.4443 |
| 137.33 | 290.47 | 285.13 | 5.3361 |
| 139.88 | 299.17 | 290.65 | 8.5197 |
| 142.57 | 304.22 | 294.78 | 9.4369 |
| 145.44 | 310.45 | 298.30 | 11.5414 |
| 148.53 | 309.82 | 298.56 | 11.2659 |
| 151.93 | 304.57 | 294.08 | 10.4883 |
| 155.75 | 282.04 | 273.97 | 3.0656 |
| 160.29 | 265.09 | 255.46 | -0.3689 |
| 166.07 | 237.50 | 246.31 | -8.8159 |
| 180.00 | 220.03 | 235.06 | -15.0316 |

ABS. CORRECTION = 1.16E-01 EG. K

TABLE VI-9. APCOR4 OUTPUT

RUN NO. 10 08/01/69 4 POL/R. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.70 | 19.70 | -7.0501 |
| 13.93 | 18.86 | 24.18 | -5.3225 |
| 19.75 | 21.01 | 26.81 | -5.8012 |
| 24.25 | 23.12 | 29.16 | -6.0405 |
| 28.07 | 25.11 | 31.37 | -6.2612 |
| 31.47 | 25.03 | 32.55 | -7.5267 |
| 34.56 | 26.88 | 34.82 | -7.9413 |
| 37.43 | 28.71 | 37.21 | -8.4987 |
| 40.12 | 30.82 | 39.70 | -8.8727 |
| 42.67 | 33.43 | 42.27 | -9.8416 |
| 45.10 | 32.95 | 43.22 | -10.2675 |
| 47.43 | 36.40 | 46.35 | -9.9565 |
| 49.68 | 40.76 | 50.27 | -9.5111 |
| 51.86 | 45.77 | 54.88 | -9.1102 |
| 53.97 | 51.08 | 50.13 | -9.0483 |
| 56.03 | 65.57 | 70.25 | -4.6886 |
| 58.03 | 70.39 | 75.20 | -4.8098 |
| 60.00 | 74.62 | 79.31 | -4.6902 |
| 61.93 | 78.46 | 82.64 | -4.1997 |
| 63.82 | 82.59 | 85.24 | -2.5496 |
| 65.68 | 61.28 | 74.61 | -13.3231 |
| 67.52 | 67.38 | 78.85 | -11.4764 |
| 69.33 | 75.70 | 85.80 | -10.0982 |
| 71.12 | 86.84 | 93.35 | -8.5239 |
| 72.90 | 100.88 | 107.45 | -6.5777 |
| 74.65 | 117.53 | 122.02 | -4.4891 |
| 76.39 | 148.99 | 144.86 | 4.1318 |
| 78.12 | 169.06 | 152.24 | 6.8240 |
| 79.84 | 190.51 | 180.47 | 10.0384 |
| 81.54 | 212.86 | 190.57 | 13.2870 |
| 83.24 | 260.30 | 230.59 | 29.7165 |
| 84.94 | 272.17 | 240.93 | 31.2169 |
| 86.63 | 271.75 | 241.13 | 30.6242 |
| 88.31 | 241.39 | 223.13 | 18.2681 |
| 90.00 | 226.19 | 211.14 | 15.0517 |
| 91.69 | 208.57 | 197.25 | 11.3186 |
| 93.37 | 175.57 | 175.39 | -0.0217 |
| 95.05 | 160.68 | 154.02 | -3.3423 |
| 96.76 | 150.82 | 154.70 | -5.7808 |
| 98.45 | 151.76 | 153.72 | -4.1519 |
| 100.16 | 148.66 | 153.87 | -5.2905 |
| 101.88 | 147.67 | 153.68 | -5.8098 |
| 103.61 | 147.85 | 152.16 | -6.1179 |
| 105.35 | 152.97 | 157.08 | -6.1075 |
| 107.10 | 150.74 | 156.37 | -6.5349 |
| 108.88 | 149.42 | 156.00 | -6.5704 |
| 110.67 | 149.84 | 156.54 | -6.7016 |
| 112.48 | 146.66 | 155.47 | -8.8064 |
| 114.32 | 150.30 | 158.12 | -7.8235 |
| 116.18 | 150.98 | 159.55 | -8.5703 |
| 118.07 | 153.13 | 151.87 | -8.7328 |
| 120.08 | 151.18 | 152.49 | -11.3071 |
| 121.97 | 158.03 | 168.41 | -10.3595 |
| 123.97 | 164.52 | 175.70 | -11.1781 |
| 126.09 | 173.74 | 187.47 | -13.7273 |
| 128.14 | 231.32 | 226.94 | 4.3804 |
| 130.32 | 277.56 | 251.59 | 15.9680 |
| 132.57 | 307.89 | 285.27 | 22.6265 |
| 134.90 | 325.19 | 296.99 | 26.1922 |
| 137.33 | 278.44 | 272.37 | 6.0561 |
| 139.88 | 288.28 | 276.90 | 11.3785 |
| 142.57 | 293.40 | 281.27 | 12.1311 |
| 145.49 | 302.31 | 287.91 | 14.3969 |
| 148.53 | 304.73 | 290.68 | 14.1051 |
| 151. | 304.05 | 290.89 | 13.1630 |
| 155. | 304.31 | 270.11 | 14.2002 |
| 160. | 292.39 | 270.65 | 13.7401 |
| 166.07 | 232.60 | 238.65 | -5.8313 |
| 180.00 | 194.35 | 213.07 | -19.3889 |

ABS. CORRECTION = 1.01E-01 DEG. K

TABLE VI-10. APCOR4 OUTPUT

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | | | |
| 13.93 | 133.52 | 134.00 | -0.4751 |
| 19.75 | 158.92 | 157.07 | 1.0501 |
| 24.25 | 157.47 | 156.53 | 0.9396 |
| 28.07 | 153.60 | 155.37 | 0.2335 |
| 31.47 | 154.01 | 153.88 | 0.1287 |
| 34.36 | 142.80 | 147.29 | -4.4848 |
| 37.43 | 141.70 | 146.34 | -4.6363 |
| 40.12 | 140.69 | 146.04 | -5.3557 |
| 42.67 | 140.21 | 146.27 | -6.0568 |
| 45.10 | 140.10 | 143.96 | -6.8267 |
| 47.43 | 142.37 | 148.97 | -7.6065 |
| 49.68 | 142.95 | 150.13 | -7.1754 |
| 51.46 | 143.42 | 151.18 | -7.6654 |
| 53.97 | 143.55 | 152.16 | -8.1955 |
| 56.03 | 144.38 | 153.05 | -8.6680 |
| 58.03 | 143.12 | 153.06 | -9.9399 |
| 60.00 | 143.79 | 154.11 | -10.3124 |
| 61.93 | 144.44 | 155.35 | -10.7078 |
| 63.82 | 145.76 | 156.79 | -11.0294 |
| 65.68 | 147.33 | 158.40 | -11.0781 |
| 67.52 | 146.95 | 158.07 | -12.1128 |
| 69.33 | 147.58 | 172.26 | -12.8643 |
| 71.12 | 151.14 | 177.54 | -12.8445 |
| 72.90 | 155.38 | 174.47 | -11.5967 |
| 74.65 | 160.67 | 184.09 | -9.9455 |
| 76.39 | 167.59 | 196.65 | -17.0266 |
| 78.12 | 157.44 | 212.10 | -13.7198 |
| 79.84 | 170.37 | 235.30 | -10.4428 |
| 81.54 | 186.21 | 251.84 | -6.7015 |
| 83.24 | 205.40 | 256.34 | 3.5579 |
| 84.94 | 238.86 | 279.12 | 7.7611 |
| 86.63 | 259.60 | 289.28 | 11.3943 |
| 88.31 | 277.73 | 297.14 | 14.7132 |
| 90.00 | 293.83 | 302.27 | 16.8661 |
| 91.69 | 306.15 | 305.98 | 18.2939 |
| 93.37 | 315.43 | 307.83 | 18.5386 |
| 95.06 | 320.81 | 306.31 | 18.8067 |
| 96.74 | 324.79 | 305.56 | 18.3613 |
| 98.46 | 326.42 | 301.24 | 19.0989 |
| 100.16 | 322.41 | 301.26 | 19.5031 |
| 101.84 | 321.59 | 294.34 | 15.2872 |
| 103.61 | 320.97 | 290.35 | 11.6417 |
| 105.35 | 312.88 | 289.88 | 13.1022 |
| 107.10 | 314.36 | 280.21 | 8.2033 |
| 108.88 | 302.35 | 285.41 | 6.0666 |
| 110.67 | 295.41 | 281.02 | 7.4320 |
| 112.44 | 297.64 | 279.95 | 4.4647 |
| 114.32 | 289.88 | 276.28 | 2.0077 |
| 116.18 | 283.03 | 271.08 | 2.5733 |
| 118.07 | 282.54 | 267.71 | 0.6562 |
| 120.00 | 276.93 | 265.29 | -2.3133 |
| 121.97 | 269.07 | 256.65 | -4.8026 |
| 123.97 | 262.90 | 270.59 | -4.1003 |
| 126.03 | 264.19 | 238.30 | -6.8667 |
| 128.14 | 259.90 | 248.30 | -6.9085 |
| 130.32 | 253.68 | 288.30 | 4.9445 |
| 132.37 | 293.76 | 280.30 | 1.2072 |
| 134.90 | 289.51 | 301.03 | -1.9149 |
| 137.33 | 286.39 | 306.16 | 5.9154 |
| 139.88 | 304.99 | 307.35 | 4.8541 |
| 142.57 | 309.01 | 318.04 | 4.5310 |
| 143.44 | 311.88 | 317.92 | 1.5730 |
| 148.53 | 320.63 | 311.17 | 1.1350 |
| 151.13 | 329.05 | 282.13 | 1.1079 |
| 153.73 | 322.27 | 256.67 | -5.2532 |
| 150.23 | 276.87 | 253.95 | -10.2610 |
| 166.07 | 250.41 | 286.88 | -11.9194 |
| 180.00 | 252.03 | | 7.0972 |

ABS. CORRECTION = 8.56E 00 DEG. K

TABLE VI-11. APCOR 4 OUTPUT
TWO POINTS

RUN NO. 11 08/09/89 V POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 123.53 | 124.22 | -0.6895 |
| 13.93 | 129.99 | 127.84 | 2.0418 |
| 19.75 | 128.29 | 127.28 | 1.0072 |
| 24.25 | 126.22 | 126.01 | 0.2097 |
| 28.07 | 124.45 | 124.35 | 0.0995 |
| 31.47 | 111.70 | 116.86 | -5.1611 |
| 34.56 | 110.50 | 115.82 | -5.3245 |
| 37.43 | 109.38 | 115.52 | -6.1355 |
| 40.12 | 108.89 | 115.82 | -6.9249 |
| 42.67 | 108.81 | 116.62 | -7.8043 |
| 45.10 | 111.45 | 118.98 | -7.5268 |
| 47.43 | 112.16 | 120.33 | -8.1658 |
| 49.68 | 112.85 | 121.57 | -8.7145 |
| 51.86 | 113.40 | 122.71 | -9.3098 |
| 53.97 | 113.92 | 123.76 | -9.8398 |
| 56.03 | 112.53 | 123.81 | -11.2792 |
| 58.03 | 113.33 | 125.03 | -11.6966 |
| 60.00 | 114.33 | 126.47 | -12.1404 |
| 61.93 | 115.63 | 128.13 | -12.3009 |
| 63.82 | 117.45 | 130.00 | -12.5528 |
| 65.68 | 114.81 | 129.66 | -14.8479 |
| 67.52 | 117.93 | 132.49 | -14.5635 |
| 69.33 | 121.88 | 136.16 | -14.2757 |
| 71.12 | 126.72 | 140.62 | -13.9013 |
| 72.90 | 132.74 | 145.86 | -13.1204 |
| 74.65 | 140.61 | 151.86 | -11.2486 |
| 76.39 | 129.14 | 148.40 | -19.2659 |
| 78.12 | 143.81 | 159.33 | -15.5200 |
| 79.64 | 161.76 | 173.57 | -11.8082 |
| 81.54 | 183.52 | 191.09 | -7.5708 |
| 83.24 | 221.43 | 217.38 | 4.0512 |
| 84.94 | 244.94 | 236.13 | 8.8101 |
| 86.63 | 265.47 | 252.55 | 12.9225 |
| 88.31 | 283.70 | 257.02 | 16.6736 |
| 90.00 | 297.45 | 278.54 | 19.1082 |
| 91.69 | 308.17 | 287.45 | 20.7220 |
| 93.37 | 314.24 | 293.26 | 20.9832 |
| 95.04 | 318.76 | 297.47 | 21.2918 |
| 96.76 | 320.62 | 299.57 | 21.0476 |
| 98.46 | 316.11 | 297.88 | 18.2345 |
| 100.16 | 315.20 | 297.64 | 17.5602 |
| 101.88 | 314.52 | 297.20 | 17.3138 |
| 103.61 | 305.38 | 292.19 | 13.1937 |
| 105.35 | 307.06 | 292.23 | 14.8352 |
| 107.10 | 293.76 | 284.45 | 9.3124 |
| 108.88 | 286.86 | 279.95 | 6.9042 |
| 110.67 | 288.23 | 279.81 | 8.4410 |
| 112.48 | 279.30 | 274.42 | 5.0852 |
| 114.32 | 271.81 | 269.49 | 2.3192 |
| 116.18 | 271.29 | 268.33 | 2.9662 |
| 118.07 | 264.92 | 254.19 | 0.7993 |
| 120.00 | 256.15 | 250.69 | -2.5440 |
| 121.97 | 249.24 | 254.58 | -5.3401 |
| 123.97 | 250.69 | 255.25 | -4.5555 |
| 126.03 | 245.80 | 255.45 | -7.6547 |
| 128.14 | 250.20 | 257.90 | -7.6998 |
| 130.32 | 283.48 | 277.84 | 5.6435 |
| 132.57 | 279.27 | 277.84 | 1.4339 |
| 134.90 | 275.75 | 277.84 | -2.0622 |
| 137.33 | 298.74 | 292.09 | 6.6532 |
| 139.89 | 301.01 | 295.56 | 3.4717 |
| 142.57 | 304.23 | 299.12 | 5.1030 |
| 145.44 | 324.26 | 311.18 | 13.0812 |
| 148.53 | 323.59 | 311.03 | 12.5395 |
| 151.93 | 313.90 | 303.38 | 12.5214 |
| 155.75 | 264.59 | 270.56 | -5.9640 |
| 160.25 | 241.45 | 253.06 | -11.6251 |
| 166.07 | 236.39 | 249.92 | -13.5242 |
| 180.00 | 283.63 | 275.73 | 7.9021 |

ABS. CORRECTION = 9.70E 00 DEG. K

TABLE VI-12. APCOR4 OUTPUT
THREE POINT CALIBRATION

RUN NO. 12 08/05/69 + POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 147.04 | 137.92 | 9.1173 |
| 13.93 | 123.58 | 124.73 | -1.1492 |
| 19.75 | 119.39 | 120.73 | -1.3385 |
| 24.25 | 115.95 | 118.25 | -2.2960 |
| 28.07 | 113.56 | 116.56 | -2.9930 |
| 31.47 | 109.32 | 114.11 | -4.7917 |
| 34.56 | 108.14 | 113.54 | -5.3937 |
| 37.43 | 107.37 | 113.45 | -6.0809 |
| 40.12 | 107.12 | 113.76 | -6.6419 |
| 42.67 | 107.35 | 114.40 | -7.0500 |
| 45.10 | 107.72 | 115.18 | -7.4554 |
| 47.43 | 108.41 | 116.39 | -7.5794 |
| 49.68 | 110.31 | 117.90 | -7.5909 |
| 51.88 | 112.13 | 119.67 | -7.5347 |
| 53.97 | 114.27 | 121.68 | -7.4065 |
| 56.03 | 116.41 | 123.89 | -7.2014 |
| 58.03 | 119.22 | 126.34 | -7.1175 |
| 60.00 | 122.08 | 129.00 | -6.9204 |
| 61.93 | 123.29 | 131.85 | -6.5663 |
| 63.82 | 129.13 | 134.90 | -5.7725 |
| 65.68 | 125.15 | 134.07 | -8.9229 |
| 67.52 | 130.58 | 138.45 | -7.8744 |
| 69.23 | 137.19 | 144.09 | -8.8473 |
| 71.12 | 145.16 | 150.94 | -5.7742 |
| 72.90 | 154.56 | 158.97 | -4.4069 |
| 74.65 | 161.35 | 158.15 | -2.7998 |
| 76.39 | 179.18 | 179.26 | -0.0769 |
| 78.12 | 192.46 | 190.42 | 2.0462 |
| 79.84 | 206.81 | 202.48 | 4.3349 |
| 81.54 | 222.10 | 215.43 | 6.6767 |
| 83.24 | 249.88 | 234.51 | 13.3656 |
| 84.94 | 261.32 | 244.29 | 17.0294 |
| 86.63 | 267.46 | 249.72 | 17.7330 |
| 88.31 | 266.76 | 250.12 | 16.6382 |
| 90.00 | 263.28 | 247.65 | 13.6343 |
| 91.69 | 255.48 | 241.61 | 13.8614 |
| 93.37 | 232.37 | 227.05 | 5.3111 |
| 95.06 | 222.11 | 219.07 | 3.0391 |
| 96.74 | 213.60 | 212.63 | 0.9763 |
| 98.46 | 210.12 | 209.19 | 0.9355 |
| 100.16 | 203.07 | 204.16 | -1.0891 |
| 101.84 | 195.29 | 199.01 | -3.7246 |
| 103.61 | 190.08 | 195.75 | -5.6652 |
| 105.35 | 196.21 | 198.70 | -2.4935 |
| 107.10 | 191.96 | 196.65 | -6.6886 |
| 108.88 | 191.01 | 196.38 | -5.3674 |
| 110.67 | 194.76 | 198.64 | -3.8799 |
| 112.48 | 192.15 | 197.84 | -5.6945 |
| 114.32 | 183.96 | 199.48 | -5.5167 |
| 116.18 | 197.78 | 202.35 | -6.5741 |
| 118.07 | 198.57 | 203.73 | -5.1635 |
| 120.00 | 201.43 | 206.03 | -4.5957 |
| 121.97 | 195.93 | 204.34 | -8.4096 |
| 123.97 | 200.14 | 208.74 | -8.6036 |
| 126.03 | 205.70 | 216.65 | -10.7515 |
| 128.14 | 251.49 | 247.04 | 4.4495 |
| 130.32 | 288.33 | 272.40 | 13.9263 |
| 132.57 | 281.45 | 272.40 | 9.0539 |
| 134.90 | 278.40 | 272.40 | 5.9961 |
| 137.33 | 287.83 | 278.86 | 8.9769 |
| 139.88 | 291.09 | 282.48 | 8.6072 |
| 142.57 | 294.50 | 286.76 | 7.7473 |
| 145.44 | 316.41 | 300.70 | 13.7121 |
| 148.53 | 317.30 | 302.35 | 14.9350 |
| 151.93 | 312.41 | 297.01 | 13.3999 |
| 155.73 | 265.78 | 268.64 | 0.1384 |
| 160.25 | 249.88 | 253.50 | -3.6183 |
| 166.07 | 238.84 | 248.50 | -9.6581 |
| 180.00 | 298.63 | 281.23 | 17.4046 |

ABS. CORRECTION = 7.13E 00 DEG. K

TABLE VI-13. APCOR4 OUTPUT
TWO POINT CALIBRATION

RUN NO. 12 08/05/69 4 POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 117.49 | 107.67 | 9.8243 |
| 13.93 | 91.71 | 93.20 | -1.4842 |
| 19.75 | 87.16 | 88.86 | -1.7031 |
| 24.25 | 83.43 | 86.20 | -2.7685 |
| 28.07 | 80.89 | 84.41 | -3.5249 |
| 31.47 | 78.06 | 81.67 | -3.6084 |
| 34.54 | 74.49 | 81.14 | -6.2572 |
| 37.47 | 74.16 | 81.18 | -7.0135 |
| 40.12 | 74.03 | 81.65 | -7.6281 |
| 42.67 | 74.43 | 82.53 | -8.0741 |
| 45.10 | 75.09 | 83.58 | -8.4856 |
| 47.43 | 76.48 | 85.10 | -8.6122 |
| 49.68 | 78.32 | 86.93 | -8.6095 |
| 51.84 | 82.52 | 89.05 | -8.5337 |
| 53.97 | 83.06 | 91.44 | -8.3785 |
| 56.03 | 85.84 | 94.05 | -8.2193 |
| 58.03 | 88.91 | 96.93 | -8.0252 |
| 60.00 | 92.24 | 100.03 | -7.7938 |
| 61.93 | 94.95 | 102.34 | -7.3878 |
| 63.82 | 100.37 | 106.85 | -6.4924 |
| 65.68 | 96.07 | 106.05 | -9.9917 |
| 67.52 | 102.25 | 111.06 | -8.8129 |
| 69.33 | 109.75 | 117.46 | -7.7143 |
| 71.12 | 118.75 | 125.20 | -6.4533 |
| 72.90 | 129.34 | 134.25 | -6.9199 |
| 74.65 | 141.48 | 144.60 | -3.1182 |
| 76.39 | 156.98 | 157.07 | -0.0906 |
| 78.12 | 171.70 | 159.61 | 2.2871 |
| 79.84 | 184.01 | 183.15 | 4.8481 |
| 81.54 | 203.17 | 197.70 | 7.4683 |
| 83.24 | 238.27 | 219.09 | 17.1730 |
| 84.94 | 249.14 | 230.10 | 19.0385 |
| 86.61 | 256.08 | 226.25 | 19.8342 |
| 88.31 | 255.34 | 236.75 | 18.5807 |
| 90.00 | 251.61 | 234.12 | 17.4870 |
| 91.69 | 243.07 | 227.56 | 19.5340 |
| 93.37 | 217.58 | 211.51 | 6.0636 |
| 95.04 | 204.34 | 202.78 | 3.5594 |
| 96.76 | 197.05 | 195.76 | 1.2876 |
| 98.46 | 193.48 | 192.15 | 1.3339 |
| 100.16 | 185.73 | 186.65 | -0.9140 |
| 101.82 | 177.09 | 180.96 | -3.8667 |
| 103.61 | 171.33 | 177.35 | -6.0294 |
| 105.35 | 178.10 | 190.63 | -2.5335 |
| 107.10 | 173.39 | 178.35 | -4.9724 |
| 108.88 | 172.33 | 178.07 | -5.7334 |
| 110.67 | 176.48 | 180.58 | -6.0943 |
| 112.44 | 173.61 | 179.71 | -6.0988 |
| 114.32 | 175.59 | 181.51 | -5.9198 |
| 116.18 | 179.80 | 184.69 | -6.8860 |
| 118.07 | 180.68 | 186.22 | -5.9367 |
| 120.00 | 183.86 | 186.77 | -6.9101 |
| 121.97 | 177.78 | 186.90 | -9.1274 |
| 123.97 | 182.41 | 191.77 | -9.3585 |
| 126.03 | 188.40 | 200.52 | -11.7164 |
| 128.14 | 239.16 | 234.09 | 5.0699 |
| 130.32 | 279.86 | 252.11 | 17.7514 |
| 132.57 | 272.29 | 252.11 | 10.1789 |
| 134.90 | 269.03 | 252.11 | 6.9174 |
| 137.33 | 278.38 | 258.60 | 9.7759 |
| 139.88 | 282.00 | 272.54 | 9.4553 |
| 142.57 | 285.71 | 277.22 | 8.4923 |
| 145.44 | 310.18 | 292.75 | 17.4193 |
| 148.53 | 311.03 | 294.50 | 16.5327 |
| 151.93 | 305.40 | 298.36 | 17.0362 |
| 155.75 | 256.35 | 256.43 | -0.0791 |
| 160.25 | 234.96 | 239.27 | -4.3070 |
| 166.07 | 222.13 | 233.52 | -11.1831 |
| 180.00 | 288.70 | 269.70 | 18.9994 |

ABS. CORRECTION = 7.98E 00 DEG. K

TABLE VI-14. APCOR4 OUTPUT
THREE POINT CALIBRATION

RUN NO. 13 DR/05/69 V POLAR, 16.5 GHZ SEA. WATER
ITERATION NUMBER 3

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 10.55 | 15.52 | -4.9578 |
| 13.93 | 16.17 | 19.13 | -2.2602 |
| 19.75 | 17.37 | 20.83 | -3.2623 |
| 24.25 | 18.71 | 22.23 | -3.5195 |
| 28.07 | 19.85 | 23.47 | -3.6206 |
| 31.47 | 17.98 | 22.65 | -3.5810 |
| 34.55 | 18.39 | 24.11 | -5.7198 |
| 37.43 | 19.76 | 25.83 | -6.0659 |
| 40.12 | 21.27 | 27.75 | -6.4928 |
| 42.67 | 22.76 | 29.89 | -7.1309 |
| 45.10 | 25.74 | 32.83 | -7.1503 |
| 47.43 | 27.11 | 35.15 | -7.8454 |
| 49.68 | 28.77 | 37.27 | -8.5069 |
| 51.84 | 30.09 | 39.25 | -9.1700 |
| 53.97 | 31.42 | 41.12 | -9.6968 |
| 56.03 | 30.64 | 41.85 | -11.2205 |
| 58.03 | 32.16 | 43.85 | -11.6922 |
| 60.00 | 33.96 | 46.07 | -12.2323 |
| 61.93 | 35.85 | 48.54 | -12.6988 |
| 63.82 | 38.21 | 51.21 | -13.0068 |
| 65.68 | 39.70 | 53.51 | -13.6076 |
| 67.52 | 42.76 | 56.72 | -13.9537 |
| 69.33 | 46.19 | 50.27 | -14.0843 |
| 71.12 | 50.03 | 54.17 | -14.1375 |
| 72.90 | 54.39 | 58.39 | -14.0033 |
| 74.65 | 59.46 | 72.94 | -13.4787 |
| 76.39 | 57.59 | 76.18 | -14.5853 |
| 78.12 | 64.45 | 80.59 | -14.7365 |
| 79.84 | 73.10 | 88.24 | -14.9406 |
| 81.54 | 83.48 | 97.12 | -13.6323 |
| 83.24 | 84.13 | 101.92 | -17.7936 |
| 84.96 | 104.10 | 118.22 | -14.1205 |
| 86.63 | 132.10 | 141.01 | -8.9113 |
| 88.31 | 192.70 | 191.45 | 11.2451 |
| 90.03 | 223.73 | 206.01 | 17.2243 |
| 91.69 | 247.73 | 225.68 | 27.0452 |
| 93.37 | 265.47 | 260.35 | 25.1283 |
| 95.05 | 277.08 | 250.42 | 24.6671 |
| 96.75 | 282.45 | 255.73 | 26.7239 |
| 98.46 | 274.04 | 252.79 | 21.2478 |
| 100.16 | 272.18 | 252.45 | 19.7162 |
| 101.88 | 268.59 | 251.05 | 17.5949 |
| 103.51 | 264.21 | 249.24 | 15.6654 |
| 105.35 | 261.08 | 247.15 | 13.9196 |
| 107.10 | 255.46 | 243.95 | 11.4970 |
| 108.89 | 250.22 | 240.78 | 9.4350 |
| 110.67 | 246.21 | 237.12 | 7.0863 |
| 112.48 | 234.51 | 231.89 | 2.7256 |
| 114.32 | 230.50 | 233.75 | 4.7381 |
| 116.18 | 232.30 | 230.65 | 1.6337 |
| 118.07 | 230.20 | 229.59 | 0.6162 |
| 120.00 | 228.16 | 228.51 | -0.3454 |
| 121.97 | 215.76 | 222.51 | -6.7470 |
| 123.97 | 222.97 | 226.85 | -3.8819 |
| 126.03 | 208.59 | 221.47 | -12.8783 |
| 128.14 | 222.99 | 233.54 | -10.5485 |
| 130.32 | 277.20 | 258.88 | 8.3222 |
| 132.57 | 311.13 | 293.81 | 17.3205 |
| 134.90 | 331.69 | 308.35 | 23.3340 |
| 137.33 | 300.10 | 293.39 | 6.7152 |
| 139.88 | 310.45 | 299.72 | 10.8665 |
| 142.57 | 318.46 | 314.50 | 12.0634 |
| 145.44 | 316.89 | 309.65 | 11.2365 |
| 148.53 | 317.82 | 306.65 | 11.1559 |
| 151.93 | 316.05 | 305.95 | 10.0967 |
| 155.75 | 315.44 | 304.81 | 10.6335 |
| 159.25 | 305.01 | 295.92 | 9.0896 |
| 166.07 | 266.06 | 268.48 | -2.4227 |
| 180.00 | 202.74 | 231.26 | -28.5305 |

ABS. CORRECTION = 1.14E 01 DEG. K

TABLE VI-15. APCOR4 OUTPUT

RUN NO. 14 08/06/69 POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 10.51 | 16.01 | -5.4971 |
| 13.93 | 15.37 | 19.81 | -3.4399 |
| 19.75 | 18.41 | 22.05 | -3.6402 |
| 24.25 | 20.13 | 24.05 | -3.7199 |
| 28.07 | 22.12 | 25.93 | -3.8101 |
| 31.47 | 23.70 | 27.80 | -3.8927 |
| 34.55 | 25.45 | 29.55 | -4.0979 |
| 37.43 | 25.75 | 31.25 | -4.3107 |
| 40.12 | 28.40 | 32.95 | -4.5430 |
| 42.67 | 29.83 | 34.61 | -4.7804 |
| 45.10 | 30.82 | 36.02 | -5.1926 |
| 47.43 | 32.41 | 37.71 | -5.3020 |
| 49.65 | 34.17 | 39.55 | -5.3371 |
| 51.86 | 36.06 | 41.38 | -5.3190 |
| 53.97 | 38.09 | 43.33 | -5.2442 |
| 56.03 | 39.93 | 45.25 | -5.3120 |
| 58.03 | 42.12 | 47.39 | -5.2689 |
| 60.00 | 44.40 | 49.65 | -5.2671 |
| 61.93 | 45.93 | 52.01 | -5.1853 |
| 63.82 | 47.91 | 54.48 | -4.9670 |
| 65.68 | 49.15 | 55.45 | -4.3121 |
| 67.52 | 52.49 | 58.51 | -4.0196 |
| 69.33 | 56.32 | 52.07 | -5.7460 |
| 71.12 | 60.74 | 56.13 | -5.3943 |
| 72.90 | 65.84 | 70.69 | -4.8466 |
| 74.65 | 71.75 | 75.72 | -3.9787 |
| 76.39 | 73.15 | 78.70 | -5.5500 |
| 78.12 | 81.35 | 85.53 | -4.1758 |
| 79.84 | 90.69 | 93.45 | -2.7670 |
| 81.54 | 101.31 | 102.49 | -1.1786 |
| 83.24 | 112.44 | 112.24 | 0.1914 |
| 84.94 | 125.75 | 123.77 | 1.9808 |
| 86.63 | 140.47 | 136.73 | 3.7385 |
| 88.31 | 172.64 | 151.52 | 18.1219 |
| 90.00 | 185.35 | 156.95 | 18.3945 |
| 91.69 | 180.30 | 153.28 | 17.0212 |
| 93.37 | 137.90 | 138.50 | -0.6005 |
| 95.06 | 125.09 | 129.15 | -3.0600 |
| 96.76 | 117.93 | 123.07 | -5.1436 |
| 98.46 | 118.47 | 122.52 | -4.0444 |
| 100.16 | 114.91 | 120.47 | -5.6629 |
| 101.85 | 111.97 | 119.25 | -7.3872 |
| 103.61 | 114.27 | 121.28 | -7.0095 |
| 105.35 | 119.68 | 125.18 | -5.4967 |
| 107.10 | 120.93 | 127.05 | -6.1263 |
| 108.88 | 121.98 | 128.85 | -6.8632 |
| 110.67 | 124.47 | 131.52 | -7.0473 |
| 112.48 | 128.68 | 135.23 | -6.5519 |
| 114.32 | 131.35 | 138.27 | -6.9235 |
| 116.18 | 135.17 | 141.97 | -6.8012 |
| 118.07 | 137.86 | 145.22 | -7.3641 |
| 120.00 | 137.56 | 147.41 | -9.8475 |
| 121.97 | 150.06 | 156.79 | -6.7267 |
| 123.97 | 153.74 | 152.92 | -9.1789 |
| 126.03 | 163.48 | 174.90 | -11.4182 |
| 128.14 | 203.97 | 206.87 | -9.9026 |
| 130.32 | 280.18 | 259.91 | 20.2733 |
| 132.57 | 327.56 | 296.25 | 31.3005 |
| 134.90 | 354.92 | 315.43 | 39.4859 |
| 137.33 | 295.22 | 284.75 | 10.4702 |
| 139.88 | 309.08 | 291.30 | 17.7005 |
| 142.57 | 315.08 | 295.75 | 19.3216 |
| 145.44 | 311.24 | 294.82 | 16.4174 |
| 148.33 | 311.00 | 295.20 | 19.6030 |
| 151.93 | 305.19 | 294.38 | 13.8123 |
| 155.75 | 314.39 | 297.29 | 17.0928 |
| 160.27 | 303.00 | 286.33 | 16.6685 |
| 166.07 | 235.32 | 242.17 | -5.8433 |
| 180.00 | 198.13 | 217.77 | -19.6363 |

ABS. CORRECTION = 8.23E 00 DEG. K

TABLE VI-16. APCOR1 OUTPUT

RUN NO. 15 DR/07/69 V POLAR. 16.5 MHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 8.45 | 12.93 | -4.4793 |
| 13.92 | 12.50 | 15.64 | -3.1450 |
| 19.79 | 14.09 | 17.35 | -3.2635 |
| 24.25 | 15.50 | 18.92 | -3.4227 |
| 28.07 | 15.77 | 20.41 | -3.5462 |
| 31.47 | 17.14 | 21.44 | -4.2963 |
| 36.56 | 18.37 | 22.94 | -4.5706 |
| 37.43 | 19.58 | 24.50 | -4.9189 |
| 40.12 | 20.69 | 26.09 | -5.4038 |
| 42.67 | 21.65 | 27.73 | -6.0818 |
| 45.10 | 22.88 | 29.58 | -6.6916 |
| 47.43 | 23.77 | 31.25 | -7.4828 |
| 49.58 | 24.54 | 32.82 | -8.2562 |
| 51.84 | 25.50 | 34.51 | -9.0078 |
| 53.97 | 26.46 | 36.11 | -9.6420 |
| 56.03 | 26.42 | 37.18 | -10.7528 |
| 58.03 | 27.58 | 38.91 | -11.3362 |
| 60.09 | 28.43 | 40.85 | -11.9704 |
| 61.93 | 30.29 | 42.83 | -12.5386 |
| 63.82 | 32.75 | 45.03 | -12.9456 |
| 65.65 | 32.56 | 46.57 | -14.0045 |
| 67.52 | 34.91 | 49.17 | -14.2690 |
| 69.33 | 37.57 | 52.10 | -14.5367 |
| 71.12 | 40.60 | 55.34 | -14.7401 |
| 72.93 | 44.15 | 58.89 | -14.7439 |
| 74.65 | 48.43 | 52.73 | -14.3020 |
| 76.39 | 44.28 | 52.51 | -18.2370 |
| 78.12 | 50.99 | 58.42 | -17.4335 |
| 79.84 | 59.01 | 75.73 | -16.7188 |
| 81.54 | 68.98 | 84.41 | -19.4347 |
| 83.24 | 68.59 | 88.69 | -20.0979 |
| 84.94 | 89.42 | 135.57 | -18.1544 |
| 86.63 | 119.00 | 129.60 | -10.5428 |
| 88.31 | 185.91 | 173.29 | 11.7185 |
| 90.00 | 217.06 | 199.13 | 18.0303 |
| 91.69 | 242.70 | 219.17 | 23.0330 |
| 93.37 | 250.55 | 232.13 | 24.4121 |
| 95.05 | 265.27 | 242.75 | 26.2085 |
| 96.76 | 275.15 | 249.42 | 26.7289 |
| 98.45 | 271.71 | 269.12 | 27.5894 |
| 100.15 | 275.28 | 251.16 | 22.1245 |
| 101.88 | 274.48 | 252.53 | 22.4691 |
| 103.61 | 265.91 | 248.13 | 17.7720 |
| 105.35 | 262.70 | 245.80 | 16.3971 |
| 107.10 | 254.31 | 261.13 | 11.1714 |
| 108.84 | 247.18 | 236.75 | 10.4184 |
| 110.7 | 242.06 | 233.42 | 8.6460 |
| 112.48 | 236.50 | 229.82 | 6.6795 |
| 114.32 | 229.44 | 225.45 | 4.0392 |
| 116.18 | 222.24 | 220.95 | 1.2907 |
| 118.07 | 217.46 | 217.93 | -0.4752 |
| 120.00 | 210.97 | 214.38 | -3.4089 |
| 121.97 | 209.05 | 213.48 | -4.4245 |
| 123.97 | 203.94 | 211.39 | -7.4495 |
| 126.03 | 196.44 | 209.57 | -13.1252 |
| 128.14 | 217.39 | 225.85 | -6.4630 |
| 130.32 | 256.66 | 251.47 | 5.1903 |
| 132.57 | 282.76 | 271.15 | 11.6088 |
| 134.90 | 300.82 | 294.76 | 16.0535 |
| 137.33 | 291.25 | 282.51 | 8.7344 |
| 139.84 | 301.48 | 290.13 | 11.7550 |
| 142.57 | 308.82 | 295.75 | 13.0727 |
| 145.44 | 310.06 | 297.64 | 12.4233 |
| 148.53 | 310.94 | 298.65 | 12.2904 |
| 151.93 | 308.42 | 297.17 | 11.2501 |
| 155.75 | 303.91 | 293.34 | 10.5779 |
| 160.25 | 290.59 | 282.01 | 8.6759 |
| 166.07 | 264.62 | 250.35 | -5.7236 |
| 180.00 | 189.79 | 217.06 | -27.2675 |

ABS. CORRECTION = 1.17E 01 DEG. K

TABLE VI-17. APCOR4 OUTPUT

RUN NO. 16 08/07/69 4 POLAR, 16.9 GHZ SEA WATER
ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.07 | 8.47 | 12.15 | -3.4872 |
| 13.91 | 10.02 | 13.84 | -2.9236 |
| 19.75 | 12.20 | 15.30 | -3.0935 |
| 24.24 | 13.48 | 16.73 | -3.2475 |
| 28.07 | 14.72 | 18.15 | -3.4323 |
| 31.47 | 16.40 | 19.83 | -3.6254 |
| 34.54 | 17.47 | 21.21 | -3.7420 |
| 37.41 | 18.51 | 22.55 | -4.0495 |
| 40.12 | 19.51 | 23.89 | -4.3779 |
| 42.67 | 20.49 | 25.20 | -4.7136 |
| 45.10 | 21.00 | 26.23 | -5.2324 |
| 47.43 | 22.20 | 27.59 | -5.3898 |
| 49.69 | 23.59 | 29.05 | -5.6607 |
| 51.85 | 25.14 | 30.61 | -5.4700 |
| 53.97 | 26.82 | 32.25 | -5.4345 |
| 56.03 | 28.46 | 33.94 | -5.4819 |
| 58.03 | 30.27 | 35.77 | -5.4993 |
| 60.00 | 32.16 | 37.70 | -5.5429 |
| 61.93 | 34.17 | 39.72 | -5.5457 |
| 63.82 | 35.45 | 41.82 | -5.3742 |
| 65.69 | 35.20 | 42.20 | -6.9937 |
| 67.52 | 38.16 | 44.91 | -6.7408 |
| 69.33 | 41.65 | 48.18 | -6.5329 |
| 71.17 | 45.78 | 52.01 | -6.2303 |
| 72.90 | 50.76 | 56.37 | -5.5088 |
| 74.65 | 55.86 | 51.25 | -4.3901 |
| 76.39 | 52.76 | 51.24 | -8.4778 |
| 78.12 | 62.56 | 58.97 | -6.4128 |
| 79.84 | 74.11 | 78.58 | -4.4676 |
| 81.54 | 87.72 | 90.04 | -2.3167 |
| 83.24 | 105.22 | 104.12 | 1.1023 |
| 84.94 | 122.00 | 118.50 | 3.4970 |
| 86.63 | 139.64 | 133.93 | 5.7028 |
| 88.31 | 185.54 | 152.75 | 22.7892 |
| 90.00 | 190.92 | 157.93 | 22.9936 |
| 91.69 | 182.75 | 151.62 | 21.1261 |
| 93.37 | 125.49 | 127.81 | -2.3257 |
| 95.05 | 110.02 | 115.34 | -5.3178 |
| 96.75 | 100.35 | 107.95 | -7.6026 |
| 98.46 | 102.65 | 108.38 | -5.7271 |
| 100.16 | 101.80 | 108.19 | -6.3943 |
| 101.88 | 105.18 | 110.45 | -5.2788 |
| 103.61 | 102.29 | 109.72 | -7.4336 |
| 105.33 | 104.18 | 112.52 | -6.3393 |
| 107.10 | 105.02 | 113.45 | -7.4279 |
| 108.88 | 107.23 | 115.30 | -8.0676 |
| 110.67 | 111.71 | 119.06 | -7.3522 |
| 112.49 | 116.59 | 125.24 | -6.3538 |
| 114.32 | 114.43 | 123.79 | -4.9583 |
| 116.14 | 122.17 | 129.18 | -7.0138 |
| 118.07 | 121.34 | 130.67 | -9.3238 |
| 120.00 | 127.21 | 135.78 | -8.5717 |
| 121.97 | 126.18 | 138.38 | -12.2034 |
| 123.97 | 137.40 | 149.45 | -12.0510 |
| 125.03 | 158.99 | 159.90 | -10.9004 |
| 126.14 | 223.74 | 215.88 | 7.4596 |
| 130.37 | 285.05 | 251.65 | 23.4064 |
| 132.57 | 325.05 | 292.99 | 32.0615 |
| 134.90 | 347.75 | 338.83 | 38.9136 |
| 137.33 | 290.85 | 279.15 | 11.6865 |
| 139.88 | 307.12 | 294.14 | 17.9811 |
| 142.57 | 305.57 | 287.65 | 18.9152 |
| 145.44 | 305.14 | 288.11 | 17.2296 |
| 148.31 | 304.81 | 288.40 | 16.4081 |
| 151.93 | 301.47 | 297.17 | 16.2968 |
| 155.75 | 306.95 | 289.40 | 17.5605 |
| 150.25 | 293.68 | 276.67 | 16.9975 |
| 166.07 | 221.28 | 228.15 | -4.8633 |
| 180.00 | 172.11 | 197.21 | -25.0979 |

ABS. CORRECTION = 9.21E 00 DEG. K

TABLE VI-18. APCOM4 OUTPUT

RUN NO. 17 08/07/69 4 POLAR. 16'S GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 8.54 | 13.84 | -5.2998 |
| 13.93 | 16.16 | 18.59 | -2.4167 |
| 19.75 | 17.78 | 20.59 | -2.8170 |
| 24.25 | 19.20 | 22.15 | -2.9546 |
| 28.07 | 20.46 | 23.50 | -3.0414 |
| 31.47 | 20.66 | 24.24 | -3.3797 |
| 34.55 | 21.53 | 25.42 | -3.7961 |
| 37.43 | 22.50 | 26.61 | -4.1033 |
| 40.12 | 23.36 | 27.79 | -4.4312 |
| 42.67 | 24.26 | 28.99 | -4.7259 |
| 45.10 | 24.74 | 29.67 | -5.4353 |
| 47.63 | 25.43 | 31.00 | -5.5658 |
| 49.69 | 26.93 | 32.54 | -5.6139 |
| 51.85 | 28.68 | 34.18 | -5.6020 |
| 53.97 | 30.65 | 36.20 | -5.5503 |
| 56.03 | 33.17 | 38.48 | -5.3125 |
| 58.03 | 35.38 | 40.65 | -5.2836 |
| 60.00 | 37.58 | 42.93 | -5.2533 |
| 61.93 | 40.08 | 45.29 | -5.1979 |
| 63.82 | 42.58 | 47.72 | -5.0362 |
| 65.68 | 43.76 | 49.08 | -6.0177 |
| 67.52 | 46.16 | 51.95 | -5.7993 |
| 69.33 | 49.52 | 55.22 | -5.6055 |
| 71.12 | 53.54 | 58.85 | -5.3266 |
| 72.90 | 58.13 | 52.87 | -4.7451 |
| 74.67 | 63.58 | 57.24 | -3.5529 |
| 76.39 | 57.85 | 56.05 | -8.2139 |
| 78.12 | 65.93 | 73.13 | -6.2014 |
| 79.84 | 77.57 | 82.05 | -4.3773 |
| 81.54 | 90.39 | 92.79 | -2.4020 |
| 83.24 | 107.48 | 106.55 | 1.3312 |
| 84.94 | 123.23 | 119.74 | 3.4834 |
| 86.63 | 138.92 | 133.52 | 5.6012 |
| 88.31 | 178.41 | 158.45 | 19.9613 |
| 90.00 | 182.90 | 152.85 | 20.0395 |
| 91.02 | 175.43 | 157.14 | 18.2935 |
| 93.37 | 123.85 | 126.79 | -2.9424 |
| 95.05 | 110.41 | 116.03 | -5.6251 |
| 96.75 | 102.51 | 110.14 | -7.5287 |
| 98.45 | 108.16 | 112.69 | -4.5217 |
| 100.15 | 107.10 | 112.59 | -5.4895 |
| 101.88 | 109.00 | 113.68 | -5.6864 |
| 103.61 | 109.63 | 115.24 | -5.5112 |
| 105.35 | 107.82 | 115.23 | -7.4124 |
| 107.10 | 111.61 | 118.36 | -6.7259 |
| 108.83 | 115.59 | 121.78 | -6.1925 |
| 110.67 | 115.28 | 124.64 | -6.3592 |
| 112.48 | 120.30 | 127.41 | -6.6195 |
| 114.32 | 122.10 | 129.70 | -7.6051 |
| 116.18 | 124.39 | 134.70 | -6.3054 |
| 118.07 | 129.91 | 137.61 | -7.5003 |
| 120.00 | 134.51 | 141.73 | -7.2203 |
| 121.97 | 134.94 | 144.35 | -9.4200 |
| 123.97 | 139.24 | 150.42 | -11.1845 |
| 126.03 | 146.09 | 161.65 | -15.5584 |
| 128.14 | 205.68 | 204.98 | 1.6935 |
| 130.32 | 278.77 | 256.38 | 21.9076 |
| 132.57 | 323.76 | 291.58 | 32.1752 |
| 134.90 | 349.74 | 309.65 | 40.0882 |
| 137.33 | 288.16 | 277.65 | 10.5151 |
| 139.98 | 301.20 | 293.52 | 17.6761 |
| 142.57 | 306.62 | 287.63 | 18.9955 |
| 145.64 | 304.07 | 287.42 | 16.6500 |
| 148.53 | 303.88 | 287.91 | 15.9690 |
| 151.93 | 301.10 | 287.16 | 13.9558 |
| 155.75 | 307.71 | 290.25 | 17.4573 |
| 160.25 | 295.73 | 278.79 | 16.9350 |
| 166.07 | 229.98 | 233.73 | -3.7529 |
| 180.00 | 168.60 | 176.41 | -27.8072 |

ABS. CORRECTION = 8.74E-09 DEG. K

TABLE VI-19. APCOR4 OUTPUT

RUN NO. 18 08/07/69 V POLAR. 16.5 GHz

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 8.97 | 11.86 | -2.8804 |
| 13.93 | 8.70 | 12.13 | -3.4358 |
| 19.75 | 9.85 | 13.35 | -3.5028 |
| 24.25 | 11.03 | 14.74 | -3.7184 |
| 28.07 | 12.11 | 16.23 | -4.1203 |
| 31.47 | 14.28 | 18.34 | -4.0518 |
| 34.56 | 15.35 | 19.85 | -4.4949 |
| 37.43 | 15.41 | 21.31 | -4.9065 |
| 40.12 | 17.29 | 22.75 | -5.4601 |
| 42.67 | 18.01 | 24.17 | -6.1631 |
| 45.10 | 18.09 | 25.31 | -7.2174 |
| 47.43 | 18.70 | 26.75 | -8.0617 |
| 49.68 | 19.43 | 28.32 | -8.8855 |
| 51.85 | 20.31 | 29.95 | -9.6505 |
| 53.97 | 21.40 | 31.69 | -10.2899 |
| 56.03 | 22.19 | 33.28 | -11.0990 |
| 58.03 | 23.58 | 35.25 | -11.6563 |
| 60.00 | 25.10 | 37.36 | -12.2576 |
| 61.93 | 25.93 | 39.61 | -12.7761 |
| 63.82 | 28.88 | 41.99 | -13.1147 |
| 65.68 | 29.17 | 43.52 | -14.3529 |
| 67.52 | 31.85 | 46.40 | -14.5451 |
| 69.33 | 34.91 | 49.65 | -14.7473 |
| 71.12 | 38.42 | 53.29 | -14.8647 |
| 72.90 | 42.51 | 57.28 | -14.7762 |
| 74.65 | 47.34 | 51.63 | -14.2975 |
| 76.39 | 45.46 | 52.81 | -17.3533 |
| 78.12 | 52.48 | 59.05 | -16.5786 |
| 79.84 | 60.70 | 76.55 | -15.8436 |
| 81.54 | 70.70 | 85.25 | -14.5623 |
| 83.24 | 70.20 | 89.45 | -19.2551 |
| 84.94 | 90.59 | 106.04 | -15.4498 |
| 86.63 | 119.57 | 129.59 | -10.0177 |
| 88.31 | 183.71 | 172.18 | 11.5304 |
| 90.00 | 215.70 | 197.50 | 17.7017 |
| 91.69 | 240.10 | 217.47 | 22.6346 |
| 93.37 | 255.16 | 230.80 | 24.3563 |
| 95.05 | 267.54 | 241.45 | 24.0929 |
| 96.76 | 274.54 | 248.08 | 26.4671 |
| 98.45 | 272.09 | 248.74 | 23.3548 |
| 100.15 | 271.39 | 249.43 | 21.9583 |
| 101.88 | 267.33 | 247.98 | 19.3476 |
| 103.61 | 265.47 | 247.41 | 18.2548 |
| 105.35 | 262.91 | 245.83 | 17.0623 |
| 107.10 | 253.49 | 240.45 | 13.0405 |
| 108.84 | 245.06 | 235.90 | 10.1588 |
| 110.67 | 241.61 | 232.89 | 8.7219 |
| 112.48 | 234.55 | 228.58 | 15.9750 |
| 114.32 | 227.90 | 224.51 | 3.2861 |
| 116.18 | 224.47 | 222.35 | 2.1150 |
| 118.07 | 221.72 | 220.51 | 1.2133 |
| 120.00 | 211.34 | 214.63 | 3.4911 |
| 121.97 | 208.59 | 213.37 | 4.7799 |
| 123.7 | 203.99 | 211.55 | 7.5776 |
| 126.03 | 200.37 | 211.34 | 10.9748 |
| 128.14 | 205.55 | 218.33 | 12.5863 |
| 130.32 | 255.28 | 251.21 | 5.0715 |
| 132.57 | 288.23 | 275.29 | 13.6427 |
| 134.90 | 310.29 | 290.83 | 19.4582 |
| 137.33 | 290.61 | 263.00 | 7.6102 |
| 139.08 | 302.53 | 270.97 | 11.5533 |
| 142.57 | 309.71 | 296.85 | 13.0489 |
| 145.44 | 310.50 | 298.42 | 12.0794 |
| 148.53 | 311.90 | 299.71 | 12.0898 |
| 151.93 | 309.96 | 298.82 | 11.1436 |
| 155.75 | 304.60 | 295.94 | 10.6635 |
| 160.25 | 295.73 | 296.33 | 8.8797 |
| 166.07 | 267.02 | 250.28 | -0.2589 |
| 180.00 | 182.50 | 215.23 | -32.7277 |

ABS. CORRECTION = 1.1E 01 DEG. K

TABLE VI-20. APCOR4 OUTPUT

RUN NO. 19 08/07/69 V POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP., (DEG K) | APPARENT TEMP., (DEG K) | CORRECTION TEMP., (DEG K) |
|-----------------------|------------------------------|----------------------------|------------------------------|
| 0.00 | 8.72 | 11.75 | -3.0391 |
| 13.93 | 9.23 | 12.85 | -2.9169 |
| 19.75 | 10.81 | 13.95 | -3.1445 |
| 24.25 | 11.63 | 15.07 | -3.4375 |
| 28.07 | 12.45 | 16.20 | -3.7501 |
| 31.47 | 11.85 | 16.61 | -4.7626 |
| 34.56 | 12.80 | 17.90 | -5.0989 |
| 37.43 | 13.80 | 19.32 | -5.5207 |
| 40.12 | 14.80 | 20.85 | -6.0530 |
| 42.67 | 15.73 | 22.47 | -6.7488 |
| 45.10 | 16.84 | 24.27 | -7.4327 |
| 47.43 | 17.81 | 26.03 | -8.2217 |
| 49.68 | 18.85 | 27.83 | -8.9748 |
| 51.86 | 19.97 | 29.65 | -9.6853 |
| 53.97 | 21.24 | 31.51 | -10.2719 |
| 56.03 | 21.86 | 33.04 | -11.1777 |
| 58.03 | 23.39 | 35.09 | -11.6985 |
| 60.00 | 25.02 | 37.28 | -12.2586 |
| 61.93 | 25.87 | 39.61 | -12.7490 |
| 63.82 | 29.04 | 42.09 | -13.0458 |
| 65.68 | 29.24 | 43.60 | -14.3512 |
| 67.52 | 32.10 | 46.59 | -14.4935 |
| 69.33 | 35.36 | 50.00 | -14.6408 |
| 71.12 | 39.12 | 53.82 | -14.5941 |
| 72.90 | 43.49 | 58.03 | -14.5422 |
| 74.65 | 48.61 | 62.63 | -14.0122 |
| 76.39 | 47.58 | 54.33 | -16.7516 |
| 78.12 | 54.86 | 70.80 | -15.9360 |
| 79.84 | 53.32 | 78.47 | -15.1495 |
| 81.54 | 73.52 | 97.34 | -13.8185 |
| 83.24 | 73.29 | 91.69 | -18.4042 |
| 84.94 | 93.75 | 108.31 | -14.5605 |
| 86.63 | 122.70 | 131.81 | -9.1111 |
| 88.31 | 185.84 | 174.33 | 12.5013 |
| 90.00 | 218.00 | 199.38 | 18.6156 |
| 91.69 | 242.37 | 218.93 | 23.4399 |
| 93.37 | 255.48 | 231.60 | 24.8895 |
| 95.05 | 268.13 | 241.64 | 26.4966 |
| 96.75 | 274.40 | 247.62 | 26.7860 |
| 98.46 | 269.19 | 246.67 | 22.5187 |
| 100.15 | 269.79 | 247.69 | 21.5973 |
| 101.84 | 268.41 | 247.72 | 20.6912 |
| 103.61 | 261.21 | 244.07 | 17.1368 |
| 105.35 | 255.95 | 241.53 | 15.3227 |
| 107.10 | 251.71 | 238.42 | 13.2899 |
| 108.88 | 245.40 | 234.55 | 10.8523 |
| 110.67 | 238.45 | 230.26 | 8.1834 |
| 112.48 | 232.65 | 226.58 | 6.0679 |
| 114.32 | 227.32 | 223.25 | 4.2681 |
| 116.18 | 222.24 | 218.87 | 1.3710 |
| 118.07 | 214.24 | 215.41 | -1.1689 |
| 120.00 | 214.12 | 215.23 | -1.1069 |
| 121.97 | 208.53 | 212.42 | -3.8902 |
| 123.97 | 201.63 | 209.30 | -7.4729 |
| 126.03 | 198.10 | 208.84 | -10.7329 |
| 128.14 | 205.20 | 216.45 | -11.2608 |
| 130.32 | 249.66 | 245.61 | 4.0504 |
| 132.57 | 277.10 | 257.42 | 11.6758 |
| 134.90 | 294.98 | 282.11 | 16.6758 |
| 137.33 | 286.15 | 278.03 | 8.1193 |
| 139.84 | 297.26 | 285.72 | 11.5373 |
| 142.57 | 304.14 | 291.11 | 13.0367 |
| 145.44 | 301.36 | 290.72 | 10.8363 |
| 148.53 | 302.28 | 291.51 | 10.7643 |
| 151.93 | 300.54 | 290.81 | 9.7323 |
| 155.75 | 301.22 | 290.39 | 10.8302 |
| 158.25 | 291.33 | 281.85 | 9.4718 |
| 166.07 | 256.55 | 255.77 | 0.7847 |
| 180.00 | 170.83 | 206.08 | -15.2306 |

ABS. CORRECTION = 1.16E 01 DEG. K

TABLE VI-21. APCOR4 OUTPUT

RUN NO. 20 08/07/69 4 POLAR. 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 9.34 | 11.65 | -2.3070 |
| 13.93 | 8.34 | 11.53 | -3.1611 |
| 19.75 | 9.21 | 12.48 | -3.2783 |
| 24.25 | 10.17 | 13.66 | -3.4925 |
| 28.07 | 11.20 | 14.95 | -3.7497 |
| 31.47 | 13.01 | 16.69 | -3.6875 |
| 34.34 | 14.01 | 18.05 | -3.0384 |
| 37.43 | 15.03 | 19.39 | -4.3454 |
| 40.12 | 16.08 | 20.73 | -4.6460 |
| 42.67 | 17.16 | 22.07 | -4.9071 |
| 45.10 | 17.29 | 22.88 | -5.5951 |
| 47.43 | 18.65 | 24.35 | -5.7030 |
| 49.68 | 20.30 | 26.03 | -5.7320 |
| 51.85 | 22.19 | 27.91 | -5.7128 |
| 53.97 | 24.29 | 29.95 | -5.6777 |
| 56.03 | 27.22 | 32.53 | -5.3136 |
| 58.03 | 29.50 | 34.80 | -5.3065 |
| 60.00 | 31.83 | 37.12 | -5.2887 |
| 61.93 | 34.26 | 39.48 | -5.2207 |
| 63.82 | 35.92 | 41.88 | -4.9633 |
| 65.68 | 35.67 | 42.34 | -6.6708 |
| 67.52 | 38.98 | 45.31 | -6.3316 |
| 69.33 | 42.81 | 48.65 | -6.0450 |
| 71.12 | 47.29 | 52.97 | -5.6770 |
| 72.90 | 52.51 | 57.61 | -5.0750 |
| 74.65 | 58.72 | 62.79 | -4.0728 |
| 76.39 | 59.18 | 65.32 | -6.1417 |
| 78.12 | 68.08 | 72.61 | -4.5329 |
| 79.84 | 78.28 | 81.22 | -2.9434 |
| 81.54 | 89.25 | 91.14 | -1.1902 |
| 83.24 | 104.30 | 102.98 | 1.5292 |
| 84.94 | 118.27 | 114.89 | 3.5766 |
| 86.63 | 132.49 | 127.47 | 5.0211 |
| 88.31 | 169.42 | 150.74 | 18.6812 |
| 90.00 | 173.30 | 154.55 | 18.6437 |
| 91.69 | 166.00 | 149.09 | 16.9184 |
| 93.37 | 116.59 | 120.08 | -3.4855 |
| 95.05 | 104.17 | 110.15 | -3.9839 |
| 96.76 | 97.40 | 105.15 | -7.7666 |
| 98.46 | 104.41 | 108.73 | -4.1179 |
| 100.16 | 104.73 | 109.62 | -4.3881 |
| 101.88 | 107.49 | 111.78 | -4.2376 |
| 103.61 | 105.90 | 111.67 | -5.6704 |
| 105.35 | 105.63 | 112.53 | -6.8656 |
| 107.10 | 104.29 | 115.62 | -6.3255 |
| 108.88 | 113.06 | 119.45 | -5.5871 |
| 110.67 | 117.72 | 122.90 | -5.1772 |
| 112.48 | 118.29 | 124.55 | -6.2776 |
| 114.32 | 117.26 | 126.47 | -7.2260 |
| 116.18 | 122.85 | 130.00 | -7.1467 |
| 118.07 | 127.40 | 134.25 | -5.8638 |
| 120.00 | 130.40 | 137.91 | -7.5087 |
| 121.97 | 132.38 | 141.60 | -9.2146 |
| 123.97 | 137.04 | 148.42 | -11.3741 |
| 124.03 | 153.46 | 154.55 | -12.0922 |
| 126.14 | 212.90 | 207.73 | 5.0982 |
| 130.32 | 276.78 | 254.35 | 27.4212 |
| 132.57 | 317.70 | 286.22 | 31.4802 |
| 134.90 | 340.81 | 302.29 | 38.5179 |
| 137.33 | 283.45 | 272.31 | 11.1368 |
| 139.88 | 294.50 | 277.02 | 17.4710 |
| 142.57 | 298.50 | 280.00 | 18.4944 |
| 145.44 | 294.07 | 278.41 | 15.6609 |
| 148.33 | 292.87 | 278.04 | 14.8273 |
| 151.93 | 289.46 | 276.75 | 12.8945 |
| 155.75 | 294.47 | 280.07 | 13.3968 |
| 160.25 | 285.00 | 259.13 | 15.8791 |
| 166.07 | 221.48 | 225.81 | -4.3273 |
| 160.00 | 164.77 | 191.25 | -26.4806 |

ABS. CORRECTION = 8.47E 00 DEG. K

TABLE VI-22. APCOR4 OUTPUT

RUN NO. 21 CP/08/69 V POLAR, 16.5 GHZ SEA WATER
ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP., (DEG K) | APPARENT TEMP., (DEG K) | CORRECTION TEMP., (DEG K) |
|-----------------------|------------------------------|----------------------------|------------------------------|
| 0.00 | 11.53 | 14.33 | -2.8000 |
| 13.93 | 11.28 | 14.61 | -3.3300 |
| 19.75 | 12.40 | 15.80 | -1.4040 |
| 24.25 | 13.53 | 17.15 | -3.6204 |
| 28.07 | 14.56 | 18.61 | -6.0512 |
| 31.47 | 16.92 | 20.80 | -3.8746 |
| 34.55 | 17.90 | 22.24 | -5.3336 |
| 37.42 | 18.46 | 23.61 | -6.7518 |
| 40.12 | 19.62 | 24.94 | -5.3180 |
| 42.57 | 20.21 | 26.23 | -6.0158 |
| 45.10 | 19.85 | 27.05 | -7.2104 |
| 47.43 | 20.35 | 28.40 | -8.0442 |
| 49.68 | 21.04 | 29.88 | -8.8461 |
| 51.86 | 21.96 | 31.51 | -9.5608 |
| 53.97 | 23.09 | 33.25 | -10.1679 |
| 55.03 | 24.24 | 35.04 | -10.8013 |
| 58.03 | 23.74 | 37.03 | -11.2154 |
| 60.00 | 27.36 | 39.21 | -11.8445 |
| 61.93 | 29.18 | 41.50 | -12.3230 |
| 63.82 | 31.20 | 43.91 | -12.6358 |
| 65.68 | 31.85 | 45.59 | -13.7362 |
| 67.52 | 34.55 | 46.45 | -13.9081 |
| 69.33 | 37.58 | 51.67 | -14.0852 |
| 71.12 | 41.03 | 55.22 | -14.1931 |
| 72.90 | 45.01 | 59.11 | -14.0992 |
| 74.65 | 49.75 | 53.32 | -13.5672 |
| 76.39 | 46.49 | 53.69 | -17.1983 |
| 78.12 | 53.65 | 59.94 | -16.2941 |
| 79.84 | 62.10 | 77.57 | -15.6695 |
| 81.54 | 72.45 | 86.55 | -14.1005 |
| 83.24 | 73.50 | 91.61 | -18.1078 |
| 84.94 | 94.00 | 108.25 | -14.2503 |
| 86.63 | 122.65 | 131.50 | -8.8553 |
| 88.31 | 185.73 | 173.32 | 12.4147 |
| 90.00 | 216.12 | 197.75 | 18.3674 |
| 91.69 | 239.59 | 216.60 | 22.9900 |
| 93.37 | 252.91 | 228.58 | 24.3249 |
| 95.06 | 263.27 | 237.33 | 25.6473 |
| 96.76 | 268.06 | 242.40 | 25.6537 |
| 98.46 | 258.31 | 238.76 | 19.5482 |
| 100.16 | 258.51 | 239.65 | 18.8570 |
| 101.88 | 259.94 | 240.85 | 19.0885 |
| 103.61 | 252.08 | 236.87 | 13.2122 |
| 105.33 | 246.36 | 233.62 | 12.7474 |
| 107.10 | 241.78 | 230.93 | 10.8438 |
| 108.88 | 233.16 | 228.76 | 9.3926 |
| 110.67 | 234.46 | 226.44 | 8.0136 |
| 112.48 | 227.37 | 222.33 | 5.0453 |
| 114.32 | 222.91 | 219.60 | 1.3173 |
| 116.16 | 219.57 | 217.53 | 2.0412 |
| 118.07 | 212.97 | 213.93 | -0.9511 |
| 120.00 | 210.38 | 212.51 | -2.1346 |
| 121.97 | 201.39 | 208.70 | -6.8137 |
| 123.97 | 206.32 | 212.34 | -5.0262 |
| 126.03 | 207.54 | 215.87 | -8.3321 |
| 128.14 | 223.79 | 229.42 | -5.6348 |
| 130.32 | 271.86 | 251.27 | 10.5849 |
| 132.57 | 302.27 | 293.78 | 18.4871 |
| 134.90 | 320.58 | 276.88 | 21.7026 |
| 137.33 | 292.07 | 203.78 | 9.0905 |
| 139.88 | 201.96 | 288.97 | 12.5895 |
| 142.57 | 305.42 | 292.19 | 13.2342 |
| 143.44 | 307.04 | 293.42 | 13.6239 |
| 146.53 | 303.95 | 291.25 | 17.6992 |
| 151.93 | 296.14 | 285.05 | 21.0780 |
| 155.75 | 272.98 | 259.15 | 3.7239 |
| 160.25 | 253.06 | 253.39 | -0.3313 |
| 166.07 | 212.88 | 229.74 | -9.8538 |
| 180.00 | 183.06 | 207.53 | -24.4670 |

A85, CORRECTION = 1.13E 01 DEG. K

TABLE VI-23. APCOR4 OUTPUT

RUN NO. 22 08/08/09 4 POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP., (DEG K) | APPARENT TEMP., (DEG K) | CORRECTION TEMP., (DEG K) |
|-----------------------|------------------------------|----------------------------|------------------------------|
| 0.00 | 11.31 | 15.35 | -4.0499 |
| 25.92 | 16.28 | 18.55 | -2.2731 |
| 19.75 | 17.31 | 19.99 | -2.6779 |
| 24.25 | 18.22 | 21.14 | -2.9130 |
| 28.07 | 19.15 | 22.14 | -2.9848 |
| 31.67 | 19.04 | 22.05 | -4.0051 |
| 34.56 | 18.99 | 23.09 | -4.1964 |
| 37.43 | 19.72 | 24.24 | -4.5242 |
| 40.12 | 20.64 | 25.49 | -4.8517 |
| 42.67 | 21.56 | 26.82 | -5.1608 |
| 45.10 | 22.45 | 28.02 | -5.5732 |
| 47.43 | 23.85 | 29.54 | -5.6870 |
| 49.68 | 25.48 | 31.20 | -5.7158 |
| 51.84 | 27.29 | 32.99 | -5.7004 |
| 53.97 | 29.26 | 34.90 | -5.8476 |
| 56.03 | 31.32 | 36.94 | -5.6181 |
| 58.03 | 33.46 | 39.07 | -5.6119 |
| 60.00 | 35.59 | 41.31 | -5.6189 |
| 61.93 | 38.07 | 43.65 | -5.5776 |
| 63.82 | 40.72 | 45.08 | -5.3608 |
| 65.69 | 40.01 | 46.85 | -5.8550 |
| 67.52 | 43.36 | 49.90 | -6.5372 |
| 69.33 | 47.24 | 53.50 | -6.2553 |
| 71.12 | 51.75 | 57.63 | -5.8833 |
| 72.90 | 57.06 | 62.29 | -5.2343 |
| 74.65 | 53.38 | 57.45 | -4.0838 |
| 76.39 | 61.69 | 58.83 | -7.1412 |
| 78.12 | 71.19 | 76.47 | -5.2806 |
| 79.84 | 82.17 | 85.69 | -3.5201 |
| 81.54 | 94.88 | 96.49 | -1.6099 |
| 83.24 | 112.66 | 110.32 | -2.3371 |
| 84.94 | 127.11 | 122.82 | -4.2934 |
| 86.63 | 141.31 | 135.37 | -5.9350 |
| 88.31 | 178.27 | 157.45 | 18.8096 |
| 90.00 | 179.33 | 150.70 | 18.6350 |
| 91.69 | 171.16 | 156.61 | 18.7525 |
| 93.37 | 119.99 | 124.27 | -4.2820 |
| 95.06 | 107.05 | 113.95 | -6.9008 |
| 96.76 | 107.17 | 108.92 | -3.7512 |
| 98.46 | 109.12 | 113.54 | -4.4211 |
| 100.16 | 108.39 | 114.24 | -5.2482 |
| 101.88 | 103.71 | 115.63 | -5.9176 |
| 103.61 | 111.31 | 117.65 | -6.3364 |
| 105.35 | 117.16 | 122.00 | -4.8406 |
| 107.10 | 119.01 | 124.42 | -5.4158 |
| 108.88 | 122.21 | 127.51 | -5.2955 |
| 110.67 | 123.34 | 130.96 | -4.6233 |
| 112.46 | 124.95 | 131.54 | -6.5891 |
| 114.32 | 120.48 | 135.05 | -5.5732 |
| 116.18 | 125.40 | 134.50 | -9.0997 |
| 118.07 | 134.15 | 140.85 | -6.7034 |
| 120.00 | 136.00 | 144.26 | -8.2384 |
| 121.97 | 139.94 | 149.63 | -9.6948 |
| 123.97 | 150.19 | 150.44 | -10.2328 |
| 126.03 | 177.12 | 183.29 | -6.1724 |
| 128.14 | 231.65 | 223.38 | -8.2707 |
| 130.32 | 289.92 | 255.64 | 21.2748 |
| 132.57 | 225.69 | 294.42 | 31.2718 |
| 134.90 | 346.29 | 308.77 | 37.5215 |
| 137.33 | 293.21 | 280.96 | 12.2482 |
| 138.88 | 302.93 | 285.04 | 17.8947 |
| 142.57 | 306.04 | 287.62 | 18.4175 |
| 145.44 | 305.79 | 288.28 | 17.5086 |
| 148.32 | 303.23 | 286.95 | 16.2780 |
| 151.93 | 295.97 | 292.92 | 14.0446 |
| 155.75 | 291.76 | 277.85 | 13.8928 |
| 160.25 | 273.91 | 261.37 | 12.5399 |
| 166.07 | 197.06 | 211.85 | -14.7634 |
| 180.00 | 186.64 | 202.05 | -15.6088 |

ABS. CORRECTION = 8.56E 00 DEG. K

TABLE VI-24. APCOR4 OUTPUT

RUN NO. 23 08/08/69 V POLAR.

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 11.39 | 12.15 | -1.2522 |
| 13.93 | 3.41 | 9.49 | -4.0579 |
| 19.75 | 5.28 | 10.21 | -3.9324 |
| 24.25 | 7.45 | 11.57 | -4.1235 |
| 28.07 | 8.64 | 13.27 | -4.5580 |
| 31.47 | 13.48 | 17.00 | -3.5154 |
| 34.56 | 16.72 | 18.75 | -4.0394 |
| 37.43 | 15.95 | 20.37 | -4.4121 |
| 40.12 | 16.90 | 21.87 | -4.7675 |
| 42.67 | 17.55 | 23.25 | -5.7077 |
| 45.17 | 17.59 | 24.95 | -6.7554 |
| 47.43 | 18.02 | 25.65 | -7.5372 |
| 49.68 | 18.31 | 27.00 | -8.4933 |
| 51.85 | 19.78 | 28.29 | -9.2965 |
| 53.97 | 19.83 | 29.78 | -9.9474 |
| 56.03 | 19.43 | 30.61 | -11.1774 |
| 58.03 | 21.50 | 32.24 | -11.7815 |
| 60.00 | 21.75 | 34.18 | -12.4319 |
| 61.93 | 23.29 | 35.29 | -13.0038 |
| 63.82 | 25.18 | 38.81 | -13.4774 |
| 65.68 | 26.57 | 40.77 | -14.1029 |
| 67.52 | 29.19 | 43.56 | -14.3117 |
| 69.33 | 31.99 | 46.82 | -14.4213 |
| 71.12 | 35.11 | 49.94 | -14.5515 |
| 72.90 | 38.70 | 53.53 | -14.9339 |
| 74.65 | 63.05 | 57.35 | -14.3254 |
| 76.39 | 36.89 | 58.11 | -14.2192 |
| 78.12 | 44.03 | 52.23 | -14.2560 |
| 79.84 | 52.67 | 70.08 | -17.4113 |
| 81.54 | 63.55 | 79.47 | -15.9179 |
| 83.24 | 64.09 | 84.51 | -20.4232 |
| 84.94 | 85.65 | 102.68 | -14.3294 |
| 86.63 | 110.42 | 128.37 | -7.9463 |
| 88.31 | 191.51 | 176.20 | 15.3010 |
| 90.00 | 223.83 | 202.21 | 21.6157 |
| 91.69 | 245.99 | 220.82 | 26.1556 |
| 93.37 | 252.08 | 228.20 | 23.8740 |
| 95.04 | 260.84 | 236.09 | 24.7539 |
| 96.76 | 264.38 | 240.55 | 24.4435 |
| 98.46 | 257.77 | 238.45 | 19.3361 |
| 100.16 | 254.10 | 239.57 | 18.5279 |
| 101.88 | 258.01 | 240.53 | 17.4735 |
| 103.61 | 252.06 | 243.24 | 18.8269 |
| 105.35 | 255.99 | 240.15 | 15.7853 |
| 107.10 | 245.78 | 234.54 | 11.2471 |
| 108.88 | 241.47 | 231.97 | 8.4989 |
| 110.67 | 240.90 | 231.37 | 9.5339 |
| 112.48 | 230.87 | 225.94 | 4.9205 |
| 114.32 | 230.55 | 225.41 | 5.1629 |
| 116.18 | 223.61 | 221.61 | 2.0017 |
| 118.07 | 220.81 | 219.83 | 0.7847 |
| 120.00 | 215.08 | 217.25 | -1.1809 |
| 121.97 | 205.50 | 212.35 | -3.8878 |
| 123.97 | 204.83 | 212.14 | -7.3597 |
| 126.03 | 202.48 | 212.95 | -10.4767 |
| 128.14 | 212.55 | 222.62 | -10.3699 |
| 130.32 | 258.25 | 252.87 | 5.3845 |
| 132.57 | 288.59 | 275.55 | 13.1671 |
| 134.90 | 309.26 | 290.82 | 18.4331 |
| 137.33 | 296.43 | 286.88 | 9.5452 |
| 139.88 | 307.62 | 294.65 | 12.9523 |
| 142.57 | 314.33 | 299.84 | 14.4971 |
| 145.44 | 307.91 | 297.29 | 10.6258 |
| 148.52 | 308.37 | 297.91 | 10.4562 |
| 151.93 | 307.24 | 298.01 | 9.2342 |
| 155.75 | 314.49 | 301.80 | 12.6915 |
| 160.25 | 307.08 | 295.18 | 11.8952 |
| 166.07 | 271.62 | 258.63 | 3.1820 |
| 180.00 | 175.62 | 213.23 | -37.6035 |

ABS. CORRECTION = 1.19E-01 DEG, K

TABLE VI-25. APCOR4 OUTPUT

RUN NO. 24 OR/08/69 4 POLAR. 16.5 GHz SEA WATER

ITERATION NUMBER 3

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 11.38 | 15.39 | -4.0121 |
| 13.93 | 14.21 | 17.42 | -3.2077 |
| 19.75 | 13.85 | 19.18 | -3.3299 |
| 24.57 | 17.48 | 20.92 | -3.4330 |
| 28.39 | 18.98 | 22.65 | -3.5702 |
| 31.21 | 22.09 | 25.23 | -3.1415 |
| 34.03 | 23.34 | 26.81 | -3.4726 |
| 37.85 | 24.51 | 28.25 | -3.7431 |
| 40.67 | 25.56 | 29.69 | -4.0442 |
| 42.49 | 26.51 | 30.85 | -4.3561 |
| 45.31 | 26.99 | 31.83 | -4.8346 |
| 47.13 | 28.00 | 33.02 | -5.0171 |
| 49.95 | 29.11 | 34.25 | -5.1437 |
| 51.86 | 30.33 | 35.54 | -5.2084 |
| 53.67 | 31.73 | 36.85 | -5.1256 |
| 56.03 | 30.89 | 37.09 | -6.1928 |
| 58.03 | 32.77 | 38.85 | -6.0922 |
| 60.00 | 34.97 | 41.03 | -6.0594 |
| 61.93 | 37.94 | 43.97 | -6.0346 |
| 63.82 | 40.44 | 46.47 | -6.0327 |
| 65.68 | 45.05 | 50.39 | -5.3268 |
| 67.52 | 48.97 | 53.79 | -5.2177 |
| 69.33 | 52.31 | 57.34 | -5.0316 |
| 71.17 | 55.28 | 61.02 | -4.7434 |
| 72.90 | 60.76 | 64.85 | -4.0961 |
| 74.65 | 66.16 | 68.81 | -2.6523 |
| 76.39 | 54.58 | 54.35 | -9.7665 |
| 78.12 | 64.17 | 71.48 | -7.3122 |
| 79.84 | 75.65 | 80.93 | -5.2862 |
| 81.54 | 89.47 | 92.67 | -3.1936 |
| 83.24 | 113.22 | 139.99 | -3.2302 |
| 84.94 | 128.46 | 123.10 | -5.3603 |
| 86.63 | 142.12 | 135.12 | -7.0016 |
| 88.31 | 170.09 | 153.21 | 16.8824 |
| 90.00 | 172.69 | 155.97 | 16.6821 |
| 91.69 | 165.37 | 150.43 | 14.9490 |
| 93.37 | 120.81 | 124.20 | -3.3943 |
| 95.06 | 109.21 | 115.04 | -5.8333 |
| 96.74 | 102.77 | 110.39 | -7.6168 |
| 98.46 | 109.71 | 113.91 | -6.1931 |
| 100.15 | 109.95 | 114.17 | -5.2217 |
| 101.88 | 109.04 | 115.04 | -5.9997 |
| 103.61 | 112.33 | 117.69 | -3.3596 |
| 105.35 | 111.66 | 118.38 | -6.9217 |
| 107.10 | 118.19 | 123.25 | -2.1102 |
| 108.88 | 121.17 | 126.16 | -4.9925 |
| 110.67 | 119.50 | 126.63 | -4.9947 |
| 112.48 | 123.09 | 129.93 | -6.8385 |
| 114.32 | 127.08 | 133.65 | -6.5792 |
| 116.18 | 137.21 | 138.08 | -5.8668 |
| 118.07 | 132.01 | 139.93 | -7.9180 |
| 120.00 | 135.99 | 144.30 | -8.3120 |
| 121.97 | 144.96 | 151.98 | -7.0263 |
| 123.97 | 145.57 | 157.65 | -11.0888 |
| 126.03 | 169.67 | 177.43 | -7.7872 |
| 128.14 | 218.78 | 213.93 | -4.8456 |
| 130.32 | 275.73 | 255.68 | 20.0527 |
| 132.57 | 313.25 | 295.08 | 28.1681 |
| 134.90 | 335.22 | 351.41 | 34.4079 |
| 137.33 | 293.43 | 290.42 | 19.0132 |
| 139.68 | 305.06 | 296.57 | 18.4378 |
| 142.37 | 310.36 | 290.73 | 19.6309 |
| 145.44 | 306.01 | 289.45 | 18.5623 |
| 148.53 | 305.50 | 289.65 | 19.8432 |
| 151.93 | 302.44 | 288.81 | 19.6259 |
| 155.75 | 311.46 | 293.23 | 18.1737 |
| 160.25 | 299.06 | 281.29 | 17.7766 |
| 166.07 | 227.03 | 232.02 | -6.9813 |
| 180.00 | 161.28 | 191.60 | -30.3265 |

ABS. CORRECTION = 8.52E-00 DEG; K

TABLE VI-26. APCOR4 OUTPUT

RUN NO. 25 08/12/69 V POLAR. 16.5 GHZ SEA WATER
ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 6.52 | 9.79 | -3.2749 |
| 13.93 | 7.97 | 10.98 | -3.1123 |
| 19.75 | 9.07 | 12.29 | -3.2254 |
| 24.25 | 10.22 | 13.64 | -3.4230 |
| 28.07 | 11.23 | 15.01 | -3.7829 |
| 31.47 | 12.93 | 16.77 | -3.8440 |
| 34.56 | 13.44 | 18.11 | -4.2744 |
| 37.43 | 14.71 | 19.41 | -4.7003 |
| 40.12 | 15.41 | 20.68 | -5.2639 |
| 42.67 | 16.00 | 21.92 | -5.9185 |
| 45.10 | 15.19 | 22.48 | -7.2980 |
| 47.43 | 15.75 | 23.88 | -8.1035 |
| 49.68 | 16.61 | 25.48 | -8.8730 |
| 51.86 | 17.79 | 27.35 | -9.5612 |
| 53.97 | 19.22 | 29.43 | -10.2105 |
| 56.03 | 22.73 | 32.62 | -9.8826 |
| 58.03 | 24.30 | 34.78 | -10.4768 |
| 60.00 | 25.77 | 36.89 | -11.0595 |
| 61.93 | 27.17 | 38.78 | -11.6137 |
| 63.82 | 28.69 | 40.64 | -11.9502 |
| 65.69 | 25.90 | 40.27 | -14.3720 |
| 67.52 | 27.96 | 42.47 | -14.6129 |
| 69.33 | 30.75 | 45.17 | -14.9708 |
| 71.12 | 33.21 | 48.35 | -15.1401 |
| 72.90 | 35.88 | 52.00 | -15.1231 |
| 74.65 | 41.46 | 58.11 | -14.6498 |
| 76.39 | 38.64 | 56.71 | -18.0700 |
| 78.12 | 45.91 | 63.04 | -17.1277 |
| 79.84 | 54.59 | 70.81 | -18.2162 |
| 81.54 | 65.21 | 80.00 | -14.7895 |
| 83.24 | 64.38 | 86.19 | -17.8047 |
| 84.94 | 88.21 | 102.35 | -14.1530 |
| 86.63 | 115.24 | 124.36 | -9.1237 |
| 88.31 | 171.03 | 161.99 | 9.0455 |
| 90.00 | 200.56 | 185.77 | 14.7866 |
| 91.69 | 224.93 | 205.39 | 19.5405 |
| 93.37 | 243.34 | 220.63 | 22.7084 |
| 95.06 | 256.92 | 232.15 | 24.7608 |
| 96.75 | 265.39 | 239.75 | 25.6399 |
| 98.46 | 261.97 | 240.25 | 21.7135 |
| 100.16 | 265.08 | 243.43 | 21.6522 |
| 101.86 | 268.36 | 266.11 | 22.2364 |
| 103.61 | 262.61 | 243.41 | 19.2076 |
| 105.35 | 252.76 | 238.05 | 14.7002 |
| 107.10 | 249.84 | 236.02 | 13.8221 |
| 108.88 | 243.53 | 232.14 | 11.4887 |
| 110.67 | 233.11 | 225.95 | 7.1467 |
| 112.48 | 227.74 | 222.58 | 5.1617 |
| 114.32 | 227.52 | 221.94 | 5.5749 |
| 116.18 | 217.32 | 216.41 | 1.4139 |
| 118.07 | 212.73 | 213.18 | -0.4467 |
| 120.00 | 203.08 | 239.01 | -3.9278 |
| 121.97 | 203.83 | 208.51 | -4.6724 |
| 123.97 | 197.36 | 205.92 | -8.5567 |
| 126.03 | 194.95 | 206.78 | -11.8298 |
| 128.14 | 210.62 | 219.51 | -8.8957 |
| 130.32 | 254.80 | 249.05 | 5.7529 |
| 132.57 | 284.14 | 270.55 | 13.1918 |
| 134.90 | 303.48 | 285.24 | 18.2423 |
| 137.33 | 286.47 | 278.80 | 7.6758 |
| 139.88 | 297.39 | 286.27 | 11.1203 |
| 142.57 | 304.36 | 291.83 | 12.5284 |
| 145.44 | 302.99 | 292.35 | 10.6481 |
| 148.53 | 304.98 | 294.20 | 10.7778 |
| 151.93 | 305.07 | 295.05 | 10.0219 |
| 155.75 | 309.19 | 297.24 | 11.9561 |
| 160.25 | 302.64 | 291.55 | 11.0945 |
| 166.07 | 275.39 | 270.29 | 5.0995 |
| 180.00 | 186.73 | 219.68 | -32.9531 |

ABS. CORRECTION = 1.15E 01 DEG. K

TABLE VI-27. APCOR4 OUTPUT

RUN NO. 27 08/12/69 V .POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 5.70 | 10.05 | -3.3628 |
| 13.93 | 7.32 | 10.58 | -3.5591 |
| 19.75 | 8.72 | 12.33 | -3.6104 |
| 24.25 | 10.10 | 13.91 | -3.6053 |
| 28.07 | 11.27 | 15.55 | -4.2812 |
| 31.47 | 14.79 | 18.45 | -3.6743 |
| 34.55 | 15.76 | 19.97 | -4.2123 |
| 37.43 | 16.56 | 21.32 | -4.6624 |
| 40.12 | 17.26 | 22.54 | -5.2800 |
| 42.67 | 17.58 | 23.67 | -5.9895 |
| 45.10 | 16.08 | 23.77 | -7.6955 |
| 47.43 | 16.38 | 24.95 | -8.5745 |
| 49.65 | 17.04 | 26.46 | -9.4161 |
| 51.86 | 18.10 | 28.24 | -10.1429 |
| 53.97 | 19.52 | 30.29 | -10.7716 |
| 56.03 | 22.50 | 33.20 | -10.7015 |
| 58.03 | 24.26 | 35.51 | -11.2649 |
| 60.00 | 26.06 | 37.84 | -11.7766 |
| 61.93 | 27.93 | 40.19 | -12.2572 |
| 63.82 | 30.02 | 42.57 | -12.5470 |
| 65.69 | 29.31 | 43.52 | -14.2133 |
| 67.52 | 31.71 | 46.23 | -14.3876 |
| 69.33 | 34.48 | 49.48 | -14.5972 |
| 71.12 | 38.34 | 53.05 | -14.7210 |
| 72.90 | 42.40 | 57.03 | -14.6256 |
| 74.65 | 47.28 | 61.38 | -14.1042 |
| 76.39 | 44.84 | 52.25 | -17.4264 |
| 78.12 | 52.11 | 58.66 | -16.5486 |
| 79.84 | 60.69 | 76.41 | -15.7209 |
| 81.54 | 71.15 | 85.48 | -14.3338 |
| 83.24 | 71.95 | 90.45 | -18.5081 |
| 84.94 | 92.69 | 107.29 | -14.5999 |
| 86.63 | 121.74 | 130.87 | -9.1294 |
| 88.31 | 185.40 | 173.34 | 12.4572 |
| 90.00 | 216.57 | 198.18 | 18.4911 |
| 91.69 | 240.58 | 217.38 | 22.2034 |
| 93.37 | 253.38 | 229.24 | 24.1420 |
| 95.06 | 264.59 | 238.95 | 25.6321 |
| 96.76 | 270.50 | 244.79 | 25.8180 |
| 98.46 | 266.19 | 244.25 | 21.9384 |
| 100.16 | 265.77 | 245.02 | 20.7573 |
| 101.88 | 263.61 | 244.45 | 19.1525 |
| 103.61 | 259.72 | 242.60 | 17.1255 |
| 105.35 | 253.28 | 239.15 | 14.1214 |
| 107.10 | 250.26 | 237.28 | 12.9777 |
| 108.85 | 244.74 | 233.99 | 10.7491 |
| 110.67 | 236.98 | 229.46 | 7.5013 |
| 112.48 | 233.97 | 227.31 | 6.5584 |
| 114.32 | 227.68 | 223.64 | 4.0373 |
| 116.18 | 222.33 | 220.49 | 1.9335 |
| 118.07 | 217.22 | 217.39 | -0.1734 |
| 120.00 | 212.61 | 214.78 | -2.1655 |
| 121.97 | 205.03 | 211.02 | -5.9859 |
| 123.97 | 205.24 | 211.78 | -6.5368 |
| 126.03 | 197.30 | 209.97 | -12.6670 |
| 128.14 | 220.45 | 226.51 | -6.0640 |
| 130.32 | 259.90 | 253.43 | 6.4758 |
| 132.57 | 286.48 | 273.55 | 13.1325 |
| 134.90 | 304.41 | 286.74 | 17.6730 |
| 137.33 | 289.38 | 291.20 | 8.1834 |
| 139.68 | 299.38 | 288.06 | 11.3196 |
| 142.57 | 305.62 | 293.05 | 12.5536 |
| 145.44 | 309.06 | 293.85 | 11.2112 |
| 148.33 | 306.06 | 294.95 | 11.1163 |
| 151.93 | 304.56 | 294.45 | 10.1159 |
| 155.75 | 304.90 | 293.91 | 10.9884 |
| 158.25 | 295.02 | 285.44 | 9.5764 |
| 166.07 | 262.28 | 250.14 | 2.1426 |
| 180.00 | 167.19 | 205.39 | -38.1984 |

ABS. CORRECTION = 1.16E 01 DEG. K

TABLE VI-29. APCOR4 OUTPUT

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 6.85 | 12.10 | -5.3323 |
| 13.93 | 14.24 | 16.75 | -2.5232 |
| 19.75 | 15.05 | 18.81 | -2.8579 |
| 24.25 | 17.47 | 20.45 | -2.9757 |
| 28.07 | 18.87 | 21.88 | -3.0144 |
| 31.47 | 19.01 | 22.61 | -3.6060 |
| 34.56 | 20.18 | 23.93 | -3.7495 |
| 37.43 | 21.28 | 25.27 | -3.9907 |
| 40.12 | 22.38 | 26.63 | -4.2480 |
| 42.67 | 23.40 | 28.02 | -4.5174 |
| 45.10 | 24.63 | 29.39 | -4.7617 |
| 47.41 | 25.93 | 30.82 | -4.8986 |
| 49.68 | 27.32 | 32.29 | -4.9708 |
| 51.86 | 28.80 | 33.80 | -4.9997 |
| 53.97 | 30.39 | 35.33 | -4.9400 |
| 56.09 | 30.69 | 36.25 | -5.5622 |
| 58.03 | 32.56 | 39.07 | -5.5128 |
| 60.00 | 34.62 | 40.13 | -5.5070 |
| 61.93 | 34.76 | 42.42 | -5.4799 |
| 63.82 | 39.55 | 44.92 | -5.3700 |
| 65.68 | 41.17 | 47.02 | -5.0463 |
| 67.52 | 44.45 | 50.08 | -5.6314 |
| 69.33 | 48.12 | 53.51 | -5.3922 |
| 71.12 | 52.72 | 57.29 | -5.0642 |
| 72.90 | 56.71 | 51.41 | -4.4960 |
| 74.64 | 62.40 | 55.87 | -3.4624 |
| 76.39 | 59.42 | 56.22 | -6.8061 |
| 78.12 | 67.71 | 72.84 | -5.1296 |
| 79.84 | 71.31 | 80.92 | -3.6053 |
| 81.54 | 84.45 | 90.43 | -1.9850 |
| 83.24 | 104.71 | 102.95 | 1.7513 |
| 84.94 | 117.21 | 113.81 | 3.3956 |
| 86.63 | 129.26 | 124.50 | 4.7525 |
| 88.31 | 156.34 | 142.05 | 14.3914 |
| 90.00 | 159.72 | 145.42 | 14.3042 |
| 91.69 | 154.41 | 141.51 | 12.9029 |
| 93.37 | 116.93 | 119.72 | -2.7405 |
| 95.06 | 107.62 | 112.40 | -4.7764 |
| 96.76 | 102.49 | 108.77 | -6.2841 |
| 98.46 | 108.21 | 111.81 | -3.5972 |
| 100.16 | 107.86 | 112.30 | -4.4464 |
| 101.88 | 108.39 | 113.39 | -4.9947 |
| 103.61 | 110.23 | 115.28 | -5.0624 |
| 105.35 | 111.98 | 117.29 | -5.3034 |
| 107.10 | 114.40 | 119.81 | -5.4139 |
| 108.88 | 117.45 | 123.00 | -5.1486 |
| 110.67 | 121.57 | 126.34 | -4.7693 |
| 112.48 | 123.00 | 128.43 | -5.4376 |
| 114.32 | 125.76 | 131.07 | -5.3138 |
| 116.18 | 124.03 | 131.52 | -7.4929 |
| 118.07 | 125.98 | 134.25 | -5.2737 |
| 120.00 | 134.29 | 140.64 | -6.3932 |
| 121.97 | 136.50 | 144.44 | -7.9411 |
| 123.97 | 140.03 | 150.07 | -10.0368 |
| 126.03 | 149.53 | 151.97 | -12.4421 |
| 128.14 | 196.54 | 197.38 | -0.8468 |
| 130.32 | 268.40 | 248.14 | 20.4653 |
| 132.57 | 313.71 | 292.36 | 30.8486 |
| 134.90 | 339.53 | 300.87 | 38.6610 |
| 137.33 | 280.22 | 270.18 | 10.0346 |
| 139.88 | 293.20 | 276.17 | 17.0313 |
| 142.57 | 298.72 | 280.32 | 18.4065 |
| 145.44 | 295.35 | 279.64 | 15.7084 |
| 148.33 | 295.33 | 290.23 | 15.0980 |
| 151.93 | 293.04 | 279.83 | 13.2069 |
| 155.75 | 300.38 | 283.58 | 16.7989 |
| 160.25 | 290.01 | 273.64 | 16.3757 |
| 166.07 | 230.34 | 232.67 | -2.3380 |
| 180.00 | 171.53 | 197.19 | -25.6571 |

ABS. CORRECTION = 7.90E 00 DEG. K

TABLE VI-31. APCOR4 OUTPUT

RUN NO. 30 08/12/57 V POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 6.65 | 10.93 | -6.2843 |
| 13.93 | 10.39 | 13.50 | -3.1129 |
| 19.75 | 11.60 | 15.11 | -3.3178 |
| 24.25 | 13.04 | 16.58 | -3.5430 |
| 28.07 | 14.12 | 17.97 | -3.8506 |
| 31.47 | 14.55 | 19.03 | -4.4872 |
| 34.38 | 15.35 | 20.42 | -6.8612 |
| 37.43 | 16.36 | 21.83 | -9.2724 |
| 40.12 | 17.48 | 23.28 | -5.7945 |
| 42.67 | 18.31 | 24.75 | -6.4360 |
| 45.10 | 18.39 | 25.90 | -7.5017 |
| 47.43 | 19.20 | 27.50 | -8.2975 |
| 49.65 | 20.20 | 29.25 | -9.0605 |
| 51.35 | 21.43 | 31.17 | -9.7461 |
| 53.97 | 22.91 | 33.23 | -10.3154 |
| 56.03 | 24.72 | 35.48 | -10.7518 |
| 58.03 | 26.53 | 37.75 | -11.2311 |
| 60.00 | 23.42 | 40.14 | -11.7203 |
| 61.93 | 30.46 | 42.81 | -12.1519 |
| 63.82 | 32.77 | 45.18 | -12.4077 |
| 65.69 | 32.96 | 46.65 | -13.7841 |
| 67.52 | 35.76 | 49.67 | -13.9112 |
| 69.33 | 39.06 | 53.11 | -14.0425 |
| 71.12 | 42.86 | 56.93 | -14.0684 |
| 72.90 | 47.22 | 51.14 | -13.9168 |
| 74.65 | 52.21 | 55.72 | -13.5073 |
| 76.39 | 53.71 | 58.74 | -15.0297 |
| 78.12 | 60.20 | 74.71 | -14.5105 |
| 79.86 | 67.54 | 81.53 | -13.9898 |
| 81.54 | 75.18 | 99.20 | -13.0129 |
| 83.24 | 73.53 | 91.84 | -18.3083 |
| 84.94 | 91.58 | 105.73 | -15.0479 |
| 86.63 | 115.10 | 128.32 | -10.1590 |
| 88.31 | 176.07 | 157.10 | 8.4676 |
| 90.00 | 205.57 | 191.57 | 15.0053 |
| 91.69 | 232.20 | 212.07 | 20.1752 |
| 93.37 | 254.57 | 229.54 | 25.0283 |
| 95.06 | 268.24 | 261.15 | 27.0880 |
| 96.76 | 275.42 | 247.82 | 27.6010 |
| 98.46 | 260.45 | 246.47 | 22.9817 |
| 100.16 | 269.26 | 246.65 | 21.6110 |
| 101.84 | 264.48 | 245.11 | 19.5691 |
| 103.61 | 255.18 | 240.80 | 15.3793 |
| 105.35 | 255.50 | 240.41 | 15.1945 |
| 107.10 | 252.42 | 238.55 | 13.8612 |
| 108.83 | 246.49 | 234.97 | 11.5162 |
| 110.67 | 238.71 | 230.15 | 8.5492 |
| 112.46 | 231.20 | 225.45 | 5.7431 |
| 114.32 | 224.53 | 221.35 | 3.1686 |
| 116.19 | 221.70 | 219.35 | 2.3449 |
| 118.07 | 214.74 | 215.38 | -0.6360 |
| 120.00 | 210.45 | 212.95 | -2.5033 |
| 121.97 | 206.26 | 211.02 | -4.7670 |
| 123.97 | 206.03 | 211.53 | -5.4983 |
| 126.03 | 198.91 | 209.55 | -10.6553 |
| 128.14 | 209.83 | 219.10 | -9.2763 |
| 130.32 | 251.28 | 246.53 | 4.7451 |
| 132.57 | 278.74 | 256.97 | 11.7519 |
| 134.90 | 297.11 | 250.59 | 16.5199 |
| 137.33 | 283.39 | 275.83 | 7.5557 |
| 139.88 | 293.78 | 293.00 | 10.7803 |
| 142.57 | 300.31 | 298.19 | 12.1244 |
| 145.44 | 299.43 | 288.78 | 10.6464 |
| 148.33 | 300.50 | 289.87 | 10.6265 |
| 151.93 | 299.09 | 299.36 | 9.7266 |
| 155.73 | 294.36 | 298.25 | 10.1165 |
| 160.25 | 289.14 | 280.41 | 8.7266 |
| 166.07 | 260.98 | 258.23 | 2.7516 |
| 180.00 | 172.12 | 207.23 | -35.1141 |

ABS. CORRECTION = 1.13E 01 DEG. K

TABLE VI-32. APCOR4 OUTPUT

RUN NO. 31 08/13/69 H POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 10.40 | 13.32 | -2.7186 |
| 13.93 | 9.67 | 13.27 | -3.5977 |
| 19.75 | 10.69 | 14.42 | -3.7298 |
| 24.25 | 11.83 | 15.77 | -3.9416 |
| 28.07 | 13.04 | 17.25 | -4.2105 |
| 31.47 | 13.02 | 19.18 | -4.1637 |
| 34.36 | 16.22 | 20.73 | -4.5140 |
| 37.43 | 17.44 | 22.28 | -4.8443 |
| 40.12 | 18.67 | 23.83 | -5.1616 |
| 42.67 | 19.98 | 25.38 | -5.3989 |
| 43.10 | 20.24 | 26.35 | -6.1126 |
| 47.43 | 21.87 | 28.05 | -6.1870 |
| 49.68 | 23.82 | 30.00 | -6.1767 |
| 51.86 | 24.05 | 32.17 | -6.1193 |
| 53.97 | 24.50 | 34.34 | -6.0412 |
| 56.03 | 32.02 | 37.35 | -5.5303 |
| 58.03 | 34.68 | 40.19 | -5.4762 |
| 60.00 | 37.39 | 42.79 | -5.3994 |
| 61.93 | 40.20 | 45.46 | -5.2589 |
| 63.82 | 43.25 | 48.17 | -4.9191 |
| 65.68 | 42.16 | 48.82 | -4.6531 |
| 67.52 | 45.98 | 52.11 | -6.2244 |
| 69.33 | 50.14 | 56.00 | -5.8571 |
| 71.12 | 53.07 | 60.47 | -5.4000 |
| 72.90 | 60.90 | 65.51 | -4.6060 |
| 74.65 | 67.73 | 71.10 | -3.1684 |
| 76.39 | 64.70 | 71.66 | -7.1614 |
| 78.12 | 75.42 | 80.22 | -4.8053 |
| 79.84 | 85.07 | 90.73 | -2.6591 |
| 81.54 | 102.73 | 103.16 | -0.4359 |
| 83.24 | 127.72 | 121.21 | 6.5065 |
| 84.96 | 142.57 | 133.95 | 8.6204 |
| 86.63 | 135.03 | 144.87 | 10.1545 |
| 88.31 | 177.25 | 159.48 | 17.7749 |
| 90.00 | 178.79 | 151.36 | 17.4284 |
| 91.69 | 171.59 | 155.91 | 15.6829 |
| 93.37 | 132.44 | 132.65 | -0.2083 |
| 95.06 | 120.77 | 123.32 | -2.7469 |
| 96.76 | 113.03 | 117.89 | -4.8624 |
| 98.46 | 116.50 | 119.07 | -2.5709 |
| 100.16 | 112.28 | 116.96 | -4.6770 |
| 101.88 | 111.67 | 117.00 | -5.3256 |
| 103.61 | 113.35 | 118.53 | -5.1942 |
| 105.35 | 116.44 | 121.04 | -4.5023 |
| 107.00 | 117.50 | 122.41 | -4.9167 |
| 108.88 | 117.31 | 123.20 | -5.8889 |
| 110.67 | 117.58 | 124.40 | -6.8197 |
| 112.48 | 121.94 | 127.93 | -5.9871 |
| 114.32 | 123.20 | 131.08 | -5.8796 |
| 116.18 | 126.67 | 133.46 | -6.7950 |
| 118.07 | 132.35 | 138.03 | -5.6793 |
| 120.00 | 131.14 | 140.15 | -7.0143 |
| 121.97 | 132.82 | 142.22 | -9.3992 |
| 123.97 | 139.12 | 149.36 | -10.2248 |
| 126.03 | 150.99 | 192.83 | -11.8373 |
| 128.14 | 209.11 | 233.00 | 6.1109 |
| 130.32 | 269.27 | 243.33 | 23.7449 |
| 132.57 | 257.94 | 243.53 | 14.4086 |
| 134.90 | 249.84 | 243.53 | 6.3121 |
| 137.33 | 294.76 | 271.61 | 23.3431 |
| 139.88 | 296.29 | 276.38 | 19.9317 |
| 142.37 | 298.87 | 279.40 | 19.4660 |
| 145.44 | 293.26 | 277.15 | 16.1135 |
| 148.53 | 291.87 | 276.65 | 15.2249 |
| 151.93 | 288.43 | 275.30 | 13.0498 |
| 155.73 | 295.49 | 278.79 | 16.7087 |
| 160.25 | 284.82 | 258.33 | 16.2983 |
| 166.07 | 222.22 | 226.73 | -6.5090 |
| 180.00 | 192.42 | 200.94 | -18.5159 |

ABS. CORRECTION = 7.96E 00 DEG. K

TABLE VI-33. APCOR4 OUTPUT

RUN NO. 32 08/19/69 V PULS. 16.5 GHz SEA MATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 10.68 | 14.70 | -4.0192 |
| 13.93 | 13.56 | 16.84 | -1.1846 |
| 19.75 | 14.73 | 18.22 | -3.4917 |
| 24.25 | 15.67 | 19.49 | -3.8146 |
| 28.07 | 16.56 | 20.70 | -4.0320 |
| 31.47 | 16.58 | 20.30 | -5.7197 |
| 34.55 | 15.81 | 21.75 | -5.9468 |
| 37.41 | 17.09 | 23.45 | -6.3599 |
| 40.12 | 18.48 | 25.35 | -6.8695 |
| 42.67 | 19.88 | 27.42 | -7.5355 |
| 45.10 | 22.11 | 30.00 | -7.8964 |
| 47.43 | 21.70 | 32.28 | -8.5737 |
| 49.68 | 23.14 | 34.52 | -9.1890 |
| 51.84 | 20.97 | 36.75 | -9.7055 |
| 53.97 | 24.70 | 38.98 | -10.2764 |
| 56.03 | 29.49 | 40.81 | -11.1197 |
| 58.03 | 31.59 | 43.15 | -11.5598 |
| 60.00 | 33.96 | 45.61 | -12.0467 |
| 61.93 | 35.72 | 48.19 | -12.4680 |
| 63.82 | 38.21 | 50.87 | -12.6660 |
| 65.68 | 37.98 | 52.21 | -14.2264 |
| 67.52 | 41.22 | 55.46 | -14.2416 |
| 69.33 | 44.94 | 59.21 | -14.2703 |
| 71.12 | 49.25 | 63.45 | -14.1992 |
| 72.90 | 54.28 | 58.15 | -13.8714 |
| 74.65 | 60.28 | 73.31 | -13.0241 |
| 76.39 | 57.37 | 74.21 | -16.8405 |
| 78.12 | 64.43 | 91.85 | -15.4259 |
| 79.84 | 77.10 | 91.15 | -14.0495 |
| 81.54 | 89.98 | 102.07 | -12.0863 |
| 83.24 | 94.73 | 110.73 | -13.7699 |
| 84.94 | 119.03 | 128.50 | -9.4695 |
| 86.63 | 147.78 | 151.73 | -3.9525 |
| 88.31 | 208.48 | 191.95 | 16.5279 |
| 90.00 | 256.42 | 214.51 | 21.9109 |
| 91.69 | 256.56 | 230.78 | 25.7795 |
| 93.37 | 261.22 | 237.43 | 23.7906 |
| 95.05 | 269.32 | 244.64 | 24.6735 |
| 96.76 | 273.62 | 249.03 | 24.5955 |
| 98.46 | 268.58 | 247.89 | 20.6926 |
| 100.16 | 269.96 | 249.43 | 20.5254 |
| 101.88 | 267.50 | 248.62 | 18.0735 |
| 103.61 | 264.42 | 246.98 | 17.4351 |
| 105.35 | 258.89 | 242.75 | 14.1971 |
| 107.10 | 250.23 | 238.75 | 11.4760 |
| 108.84 | 246.42 | 236.31 | 10.1019 |
| 110.67 | 243.09 | 234.04 | 9.0474 |
| 112.49 | 233.25 | 228.44 | 4.8143 |
| 114.32 | 233.66 | 228.01 | 3.6444 |
| 116.14 | 225.23 | 223.12 | 2.1130 |
| 118.07 | 216.91 | 219.28 | -0.4650 |
| 120.00 | 214.69 | 216.84 | -2.1477 |
| 121.97 | 211.67 | 215.12 | -3.4494 |
| 123.97 | 201.60 | 210.48 | -8.8861 |
| 126.03 | 208.78 | 216.25 | -7.4758 |
| 128.14 | 229.98 | 230.88 | -0.9045 |
| 130.32 | 252.16 | 245.95 | 6.2103 |
| 132.57 | 247.29 | 243.95 | 1.3419 |
| 134.90 | 240.39 | 243.95 | -3.5579 |
| 137.33 | 292.54 | 277.76 | 14.7768 |
| 139.88 | 297.61 | 234.65 | 12.9599 |
| 142.57 | 303.03 | 289.31 | 13.7135 |
| 145.44 | 302.95 | 289.26 | 11.6922 |
| 148.33 | 300.19 | 289.09 | 11.0960 |
| 151.93 | 296.79 | 286.70 | 10.0921 |
| 155.75 | 288.75 | 280.03 | 7.9230 |
| 160.25 | 276.97 | 271.10 | 5.8697 |
| 166.07 | 253.80 | 251.81 | 1.9921 |
| 180.00 | 169.08 | 202.83 | -33.7542 |

ABS. CORRECTION = 1.10E 01 DEG. K

TABLE VI-34. APCOR4 OUTPUT

DATE 23 NOV/14/89 V POLAR, 9.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 4.64 | 20.94 | -16.4982 |
| 15.93 | 33.97 | 38.51 | -6.5358 |
| 19.75 | 39.65 | 44.98 | -5.3355 |
| 24.25 | 44.37 | 49.64 | -5.2652 |
| 28.07 | 48.53 | 53.36 | -4.8237 |
| 31.47 | 45.71 | 53.19 | -7.4804 |
| 34.56 | 49.30 | 56.50 | -7.1982 |
| 37.43 | 52.71 | 50.02 | -7.3117 |
| 40.12 | 36.35 | 53.71 | -7.3541 |
| 42.67 | 60.10 | 57.56 | -7.4533 |
| 45.10 | 68.16 | 72.61 | -6.4657 |
| 47.43 | 70.07 | 76.47 | -6.3959 |
| 49.58 | 73.82 | 80.01 | -6.1892 |
| 51.84 | 77.22 | 83.28 | -6.0515 |
| 53.97 | 80.28 | 96.30 | -6.0165 |
| 56.03 | 83.60 | 89.41 | -5.7556 |
| 58.03 | 85.98 | 91.90 | -5.9155 |
| 60.00 | 87.94 | 94.09 | -6.1493 |
| 61.93 | 89.62 | 96.01 | -6.3931 |
| 63.82 | 91.15 | 97.69 | -6.5335 |
| 65.68 | 89.21 | 97.52 | -8.3127 |
| 67.52 | 92.59 | 99.11 | -8.5216 |
| 69.33 | 92.01 | 100.90 | -8.8880 |
| 71.12 | 93.68 | 102.90 | -9.2194 |
| 72.90 | 93.24 | 105.09 | -9.8503 |
| 74.65 | 100.14 | 107.48 | -7.3438 |
| 76.39 | 75.37 | 96.27 | -19.9026 |
| 78.12 | 86.80 | 103.69 | -16.8957 |
| 79.84 | 100.42 | 114.81 | -14.3937 |
| 81.54 | 117.76 | 129.57 | -11.8037 |
| 83.24 | 140.14 | 148.28 | -8.1445 |
| 84.94 | 165.31 | 159.87 | -4.5576 |
| 86.63 | 194.26 | 194.65 | -0.3861 |
| 88.31 | 269.56 | 232.74 | 16.8135 |
| 90.00 | 274.34 | 253.82 | 20.5155 |
| 91.69 | 250.68 | 257.85 | 22.8304 |
| 93.37 | 284.96 | 269.51 | 17.4507 |
| 95.05 | 293.30 | 275.04 | 18.2615 |
| 96.73 | 297.57 | 279.00 | 18.5686 |
| 98.43 | 303.54 | 283.14 | 20.4010 |
| 100.15 | 301.08 | 281.95 | 19.1230 |
| 101.4* | 294.22 | 277.17 | 17.0499 |
| 103.61 | 287.81 | 271.38 | 16.4325 |
| 105.35 | 255.32 | 252.73 | 3.5887 |
| 107.10 | 257.00 | 250.97 | 6.0307 |
| 108.88 | 258.43 | 250.45 | 7.9911 |
| 110.67 | 257.73 | 246.37 | 6.3671 |
| 112.48 | 249.45 | 242.77 | 6.5925 |
| 114.32 | 235.18 | 232.83 | 2.3486 |
| 116.15 | 217.41 | 220.93 | -3.5172. |
| 118.07 | 207.69 | 213.87 | -6.1765 |
| 120.00 | 210.44 | 214.28 | -6.5406 |
| 121.97 | 200.33 | 209.41 | -9.0874 |
| 123.97 | 198.91 | 211.59 | -12.6739 |
| 126.03 | 233.24 | 235.28 | -2.0484 |
| 128.14 | 265.92 | 250.68 | 5.2428 |
| 130.32 | 305.46 | 289.67 | 15.7953 |
| 132.57 | 329.09 | 308.05 | 21.0297 |
| 134.90 | 340.13 | 315.17 | 24.9595 |
| 137.33 | 295.12 | 290.04 | 5.0820 |
| 139.88 | 297.01 | 288.39 | 8.6241 |
| 142.57 | 293.54 | 284.95 | 8.5927 |
| 145.44 | 280.89 | 276.32 | 6.5506 |
| 148.53 | 272.81 | 259.61 | 3.1930 |
| 151.93 | 262.26 | 262.31 | -0.0529 |
| 155.75 | 271.85 | 254.58 | 7.2661 |
| 160.25 | 252.25 | 243.63 | 8.6206 |
| 166.07 | 135.17 | 156.71 | -31.5391 |
| 180.00 | 131.34 | 134.21 | -22.8746 |

ABS. CORRECTION = 9.96E 00 DEG. K

TABLE VI-35. APCCOR4 OUTPUT

RUN NO. 34 08/14/69 14 POLAR, 9.5 GHz SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 4.36 | 13.65 | -9.1045 |
| 13.93 | 14.96 | 20.33 | -5.3690 |
| 19.75 | 19.13 | 24.63 | -5.4974 |
| 24.25 | 23.12 | 28.53 | -5.4086 |
| 28.07 | 26.45 | 32.24 | -5.7836 |
| 31.47 | 34.92 | 38.52 | -3.6648 |
| 34.56 | 37.68 | 41.60 | -3.9200 |
| 37.43 | 40.30 | 44.12 | -3.8189 |
| 40.12 | 42.58 | 46.25 | -3.5836 |
| 42.87 | 44.60 | 48.08 | -3.4757 |
| 45.10 | 44.48 | 48.69 | -4.2150 |
| 47.43 | 46.05 | 50.22 | -4.1619 |
| 49.68 | 47.78 | 51.92 | -4.1380 |
| 51.85 | 49.64 | 53.77 | -4.1303 |
| 53.97 | 51.68 | 55.77 | -4.0914 |
| 56.03 | 53.54 | 57.75 | -4.2134 |
| 58.03 | 55.88 | 59.05 | -4.1707 |
| 60.00 | 58.42 | 52.53 | -4.1086 |
| 61.93 | 61.24 | 55.17 | -3.9245 |
| 63.87 | 64.45 | 57.95 | -3.5061 |
| 65.68 | 63.75 | 58.86 | -3.1097 |
| 67.52 | 67.84 | 72.43 | -4.5990 |
| 69.33 | 72.53 | 76.70 | -4.1364 |
| 71.12 | 77.92 | 81.62 | -3.7027 |
| 72.90 | 84.25 | 87.20 | -2.9495 |
| 74.65 | 91.57 | 93.41 | -1.7395 |
| 76.39 | 92.99 | 96.78 | -3.8901 |
| 77.12 | 103.28 | 105.40 | -2.0146 |
| 79.84 | 115.13 | 115.50 | -0.3745 |
| 81.54 | 128.39 | 127.08 | 1.3121 |
| 83.24 | 157.32 | 146.41 | 10.9082 |
| 84.94 | 167.17 | 154.95 | 12.2122 |
| 86.63 | 171.16 | 158.65 | 12.5008 |
| 88.31 | 163.29 | 154.74 | 8.5496 |
| 90.00 | 159.30 | 151.64 | 7.6586 |
| 91.69 | 152.69 | 146.60 | 6.2875 |
| 93.37 | 137.56 | 136.78 | 0.8889 |
| 95.06 | 130.02 | 130.82 | -0.7995 |
| 96.75 | 123.59 | 125.85 | -2.2591 |
| 98.46 | 118.82 | 122.15 | -3.3307 |
| 100.16 | 113.46 | 118.83 | -5.3924 |
| 101.85 | 106.61 | 115.82 | -9.2100 |
| 103.51 | 124.84 | 126.08 | -1.2478 |
| 103.35 | 130.57 | 129.60 | 0.9789 |
| 107.10 | 122.87 | 124.85 | -1.9859 |
| 108.88 | 107.23 | 114.99 | -7.7625 |
| 110.67 | 90.56 | 104.88 | -14.3158 |
| 112.48 | 94.28 | 106.20 | -11.9225 |
| 114.32 | 101.54 | 110.38 | -8.5467 |
| 116.18 | 93.43 | 106.93 | -13.4980 |
| 118.07 | 92.91 | 108.01 | -15.1003 |
| 120.00 | 105.82 | 116.89 | -11.0637 |
| 121.97 | 101.00 | 118.95 | -17.9532 |
| 123.97 | 114.05 | 134.26 | -20.2125 |
| 126.03 | 105.63 | 103.97 | 1.6579 |
| 128.14 | 245.08 | 230.74 | 17.3386 |
| 130.32 | 284.69 | 262.17 | 22.5270 |
| 132.57 | 310.82 | 283.85 | 26.9697 |
| 134.90 | 325.35 | 294.54 | 31.0118 |
| 137.33 | 285.16 | 273.53 | 11.6289 |
| 139.88 | 291.46 | 275.93 | 15.5577 |
| 142.57 | 293.17 | 276.80 | 16.3718 |
| 145.44 | 282.74 | 271.10 | 11.6312 |
| 148.53 | 281.61 | 270.30 | 11.3100 |
| 151.93 | 279.11 | 271.07 | 8.0458 |
| 155.75 | 315.03 | 291.73 | 23.3080 |
| 160.25 | 305.78 | 278.41 | 27.3679 |
| 166.07 | 160.32 | 187.85 | -27.5314 |
| 180.00 | 195.57 | 196.07 | -0.4956 |

ABS. CORRECTION = 8.37E 00 DEG. K

TABLE VI-36. APCOR4 OUTPUT

RUN NO. 35 08/14/69 H POLAR, 16.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP., (DEG K) | APPARENT TEMP., (DEG K) | CORRECTION TEMP., (DEG K) |
|-----------------------|------------------------------|----------------------------|------------------------------|
| 0.00 | 12.31 | 24.20 | -11.8880 |
| 13.93 | 21.37 | 30.74 | -9.3637 |
| 19.75 | 22.97 | 34.00 | -11.0300 |
| 26.25 | 24.59 | 36.74 | -12.1542 |
| 30.07 | 27.08 | 39.22 | -12.1362 |
| 31.47 | 19.11 | 36.00 | -16.8898 |
| 34.36 | 22.79 | 39.26 | -18.4872 |
| 37.47 | 26.66 | 43.32 | -16.6561 |
| 40.12 | 31.38 | 48.05 | -16.6708 |
| 42.67 | 37.36 | 53.34 | -15.9780 |
| 45.10 | 36.19 | 55.14 | -18.9451 |
| 47.43 | 44.20 | 52.32 | -18.1108 |
| 49.68 | 54.49 | 71.51 | -17.0189 |
| 51.86 | 66.83 | 82.53 | -15.7016 |
| 53.97 | 81.05 | 95.24 | -14.1858 |
| 56.03 | 102.03 | 111.94 | -9.9113 |
| 58.03 | 119.07 | 126.85 | -7.7795 |
| 60.00 | 137.11 | 142.37 | -5.2593 |
| 61.93 | 155.52 | 158.49 | -2.9672 |
| 63.82 | 173.37 | 175.18 | -1.8152 |
| 65.69 | 215.12 | 204.68 | 11.4349 |
| 67.32 | 232.14 | 219.57 | 12.5647 |
| 69.33 | 245.90 | 231.75 | 14.1426 |
| 71.12 | 256.93 | 241.35 | 15.5737 |
| 72.90 | 265.32 | 248.45 | 16.0693 |
| 74.65 | 271.51 | 253.14 | 18.4745 |
| 76.39 | 255.31 | 245.64 | 9.6708 |
| 78.12 | 260.73 | 249.01 | 11.2556 |
| 79.84 | 264.42 | 252.63 | 11.7894 |
| 81.54 | 268.34 | 256.50 | 11.8338 |
| 83.24 | 278.24 | 253.27 | 14.9720 |
| 84.94 | 279.79 | 255.16 | 16.6357 |
| 85.63 | 278.55 | 254.65 | 13.8917 |
| 88.31 | 269.09 | 259.89 | 9.1982 |
| 90.00 | 264.66 | 256.58 | 8.0790 |
| 91.69 | 261.92 | 254.87 | 7.0668 |
| 93.37 | 261.33 | 254.42 | 6.9108 |
| 95.06 | 259.17 | 253.20 | 5.9636 |
| 96.76 | 256.71 | 251.89 | 5.0179 |
| 98.46 | 254.17 | 250.39 | 3.7850 |
| 100.16 | 251.27 | 249.11 | 2.1625 |
| 101.88 | 254.28 | 251.22 | 3.0590 |
| 103.61 | 259.28 | 254.44 | 4.8368 |
| 105.35 | 262.19 | 256.15 | 6.2379 |
| 107.10 | 253.90 | 251.16 | 2.7624 |
| 108.86 | 247.04 | 246.22 | 0.8165 |
| 110.57 | 242.37 | 241.31 | 3.5668 |
| 112.48 | 227.24 | 231.65 | -4.4167 |
| 114.32 | 207.67 | 219.72 | -12.0490 |
| 116.18 | 217.28 | 223.48 | -6.2021 |
| 118.07 | 212.76 | 220.57 | -7.8115 |
| 120.00 | 205.77 | 216.05 | -10.9820 |
| 121.97 | 196.32 | 212.09 | -15.7695 |
| 123.97 | 214.24 | 223.66 | -9.4124 |
| 126.03 | 212.91 | 228.67 | -15.7576 |
| 128.14 | 274.98 | 257.88 | 7.1068 |
| 130.32 | 303.47 | 289.10 | 14.3695 |
| 132.57 | 297.03 | 289.10 | 7.9519 |
| 134.90 | 293.45 | 289.10 | 4.3513 |
| 137.33 | 311.96 | 300.53 | 11.3304 |
| 139.88 | 312.40 | 302.62 | 9.7772 |
| 142.57 | 313.03 | 303.91 | 9.1144 |
| 145.44 | 316.90 | 306.40 | 10.4962 |
| 148.33 | 314.42 | 304.80 | 9.6222 |
| 151.93 | 308.67 | 299.95 | 5.7186 |
| 155.75 | 293.09 | 298.35 | 4.7436 |
| 160.25 | 277.32 | 274.58 | 2.7345 |
| 166.07 | 246.61 | 230.57 | -4.1606 |
| 180.00 | 193.85 | 211.05 | -25.2022 |

ABS. CORRECTION = 1.02E 01 DEG. K

TABLE VI-37. APCOR4 OUTPUT

ITERATION NUMBER 0

| EMISSION ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-------------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 12.57 | 17.13 | -4.5757 |
| 13.93 | 11.62 | 17.44 | -5.8220 |
| 19.75 | 12.65 | 19.04 | -6.3945 |
| 24.23 | 13.78 | 20.87 | -7.0986 |
| 28.07 | 15.15 | 22.54 | -7.6956 |
| 31.47 | 14.48 | 23.80 | -9.3148 |
| 36.56 | 16.26 | 26.14 | -9.8802 |
| 37.43 | 16.18 | 26.73 | -10.3467 |
| 40.12 | 20.32 | 31.52 | -11.1980 |
| 42.67 | 22.70 | 34.48 | -11.7886 |
| 45.10 | 24.43 | 37.17 | -12.7410 |
| 47.43 | 27.30 | 40.53 | -13.2345 |
| 49.68 | 30.60 | 44.20 | -13.5997 |
| 51.86 | 34.28 | 48.15 | -13.8730 |
| 53.97 | 38.49 | 52.37 | -13.8771 |
| 56.03 | 40.18 | 55.41 | -15.2220 |
| 58.03 | 45.63 | 58.58 | -14.9505 |
| 60.00 | 31.82 | 58.43 | -14.6066 |
| 61.93 | 58.84 | 72.92 | -14.0761 |
| 63.82 | 66.73 | 80.03 | -13.2906 |
| 63.68 | 74.79 | 87.43 | -12.6383 |
| 67.32 | 84.29 | 95.77 | -11.4816 |
| 69.32 | 94.55 | 104.74 | -10.1920 |
| 71.12 | 105.63 | 114.33 | -8.7031 |
| 72.90 | 117.49 | 124.53 | -7.0411 |
| 74.65 | 130.03 | 135.34 | -5.3054 |
| 76.39 | 145.96 | 148.06 | -2.0919 |
| 78.12 | 159.40 | 159.60 | -0.1975 |
| 79.84 | 173.30 | 171.39 | 1.9107 |
| 81.54 | 187.64 | 183.45 | 4.1944 |
| 83.24 | 201.89 | 195.52 | 6.3703 |
| 84.94 | 217.37 | 208.36 | 9.0110 |
| 86.63 | 233.43 | 221.74 | 11.6859 |
| 88.31 | 259.00 | 239.77 | 19.2270 |
| 90.00 | 271.15 | 250.16 | 20.9948 |
| 91.69 | 278.95 | 256.95 | 21.9053 |
| 93.37 | 274.60 | 258.75 | 17.8445 |
| 95.06 | 277.66 | 259.90 | 17.7571 |
| 96.76 | 280.57 | 262.96 | 17.6150 |
| 98.46 | 293.45 | 253.82 | 17.6211 |
| 100.15 | 286.85 | 258.52 | 18.3327 |
| 101.88 | 284.30 | 267.60 | 16.7001 |
| 103.61 | 278.35 | 254.49 | 13.8662 |
| 105.35 | 276.73 | 253.22 | 13.5181 |
| 107.10 | 270.09 | 259.02 | 11.0745 |
| 108.88 | 260.42 | 252.90 | 7.5210 |
| 110.67 | 250.46 | 246.57 | 3.8885 |
| 112.48 | 245.24 | 243.30 | 2.9453 |
| 114.32 | 240.10 | 239.13 | 0.9682 |
| 116.18 | 232.44 | 234.22 | -1.7816 |
| 118.07 | 227.54 | 230.92 | -3.2787 |
| 120.00 | 220.75 | 226.84 | -6.0848 |
| 121.97 | 217.51 | 224.94 | -7.4244 |
| 123.97 | 211.77 | 222.43 | -10.6583 |
| 126.03 | 214.18 | 225.37 | -11.3922 |
| 128.14 | 229.98 | 238.02 | -8.0479 |
| 130.32 | 280.06 | 258.64 | 11.4220 |
| 132.57 | 273.60 | 258.64 | 4.7646 |
| 134.90 | 267.91 | 268.64 | -0.7295 |
| 137.33 | 304.90 | 291.31 | 13.5951 |
| 139.88 | 306.93 | 295.38 | 11.6036 |
| 142.57 | 309.61 | 298.02 | 11.5841 |
| 145.44 | 311.35 | 299.67 | 11.8918 |
| 148.53 | 309.24 | 298.19 | 11.0454 |
| 151.93 | 303.42 | 293.37 | 10.0489 |
| 155.75 | 283.42 | 279.85 | 3.5726 |
| 160.25 | 268.04 | 267.81 | 0.2235 |
| 166.07 | 259.60 | 256.35 | 3.2458 |
| 180.00 | 163.34 | 202.07 | -38.7272 |

ABS. CORRECTION = 1.04E 01 DEG. K

TABLE VI-33. APCOR4 OUTPUT

RUN NO. 501 07/21/69 V POLAR, 9.5 GHz SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP (DEG K) |
|-----------------------|-----------------------------|---------------------------|----------------------------|
| 0.00 | 3.86 | 26.70 | +24.8396 |
| 13.93 | 60.44 | 51.88 | -1.4332 |
| 19.75 | 68.57 | 72.02 | -3.1578 |
| 24.25 | 75.41 | 78.37 | -2.9550 |
| 28.07 | 80.09 | 82.73 | -2.3430 |
| 31.47 | 79.09 | 81.59 | -6.5032 |
| 34.56 | 81.73 | 86.17 | -6.4197 |
| 37.43 | 63.73 | 68.40 | -5.5723 |
| 40.12 | 85.63 | 90.35 | -4.9198 |
| 42.67 | 86.98 | 92.07 | -2.0875 |
| 45.10 | 88.42 | 93.59 | -5.1705 |
| 47.43 | 89.84 | 94.94 | -5.1067 |
| 49.68 | 91.67 | 96.15 | -6.4744 |
| 51.86 | 84.61 | 92.73 | -8.1427 |
| 53.97 | 86.74 | 94.27 | -7.5289 |
| 56.03 | 88.60 | 95.07 | -7.4738 |
| 58.03 | 90.59 | 98.19 | -7.5359 |
| 60.00 | 92.92 | 100.43 | -7.5143 |
| 61.93 | 95.47 | 102.96 | -7.6904 |
| 63.82 | 98.20 | 105.71 | -7.5163 |
| 65.68 | 101.46 | 108.68 | -7.2190 |
| 67.32 | 107.30 | 111.85 | -4.5513 |
| 69.33 | 117.96 | 115.22 | 2.7386 |
| 71.12 | 45.92 | 76.35 | -30.4267 |
| 72.90 | 60.75 | 83.17 | -22.4242 |
| 74.65 | 74.46 | 92.82 | -18.3595 |
| 76.39 | 89.24 | 105.23 | -13.9876 |
| 78.12 | 106.91 | 120.34 | -13.4310 |
| 79.84 | 127.68 | 138.12 | -10.4302 |
| 81.54 | 131.63 | 138.52 | -6.8926 |
| 83.24 | 189.25 | 186.31 | 2.9359 |
| 84.94 | 214.07 | 207.43 | 6.6427 |
| 86.63 | 236.24 | 226.37 | 9.8689 |
| 88.31 | 258.40 | 244.28 | 14.1222 |
| 90.00 | 273.24 | 257.87 | 16.3671 |
| 91.69 | 286.15 | 258.25 | 17.8992 |
| 93.37 | 294.90 | 275.73 | 19.1667 |
| 95.06 | 298.75 | 279.34 | 19.4070 |
| 96.75 | 298.28 | 279.38 | 18.8967 |
| 98.46 | 286.76 | 272.86 | 13.6960 |
| 100.16 | 281.71 | 269.09 | 12.6251 |
| 101.88 | 276.27 | 264.90 | 11.3723 |
| 103.61 | 270.46 | 260.28 | 10.1873 |
| 105.35 | 239.09 | 252.66 | 6.4364 |
| 107.10 | 252.74 | 247.57 | 5.1742 |
| 108.88 | 246.62 | 242.64 | 3.7735 |
| 110.67 | 240.26 | 237.88 | 2.3735 |
| 112.48 | 234.77 | 233.29 | 1.4781 |
| 114.32 | 230.39 | 228.86 | 1.5326 |
| 116.18 | 205.49 | 214.24 | -8.7506 |
| 118.07 | 206.10 | 213.69 | -7.3960 |
| 120.00 | 209.77 | 216.67 | -6.8475 |
| 121.97 | 216.59 | 223.23 | -6.6432 |
| 123.97 | 226.19 | 233.76 | -7.5764 |
| 126.03 | 279.20 | 287.62 | 11.5246 |
| 128.14 | 290.63 | 279.92 | 10.7003 |
| 130.32 | 300.78 | 289.48 | 11.2972 |
| 132.57 | 308.35 | 296.10 | 12.2527 |
| 134.90 | 312.46 | 299.46 | 12.9973 |
| 137.33 | 300.61 | 293.62 | 6.9897 |
| 139.88 | 302.11 | 294.39 | 7.7217 |
| 142.57 | 301.95 | 294.59 | 7.3608 |
| 145.44 | 301.91 | 294.67 | 7.2425 |
| 148.53 | 299.51 | 293.09 | 6.4233 |
| 151.93 | 294.08 | 289.89 | 4.1912 |
| 155.75 | 304.33 | 293.35 | 10.9804 |
| 160.23 | 286.79 | 274.72 | 12.0672 |
| 166.07 | 189.29 | 205.53 | -16.2461 |
| 180.00 | 105.29 | 149.63 | -44.3806 |

ABS. CORRECTION = 9.75E 00 DEG. K

TABLE VI-39. APCOR1 OUTPUT

RUN NO. 102 07/21/69 4 POLAR. 9.5 GHZ SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 3.56 | 12.50 | -8.9446 |
| 13.93 | -1.83 | 11.81 | -13.6605 |
| 19.75 | 9.11 | 20.87 | -11.7559 |
| 24.25 | 21.03 | 31.65 | -10.6110 |
| 28.07 | 30.62 | 43.39 | -12.7723 |
| 31.47 | 80.26 | 76.54 | 3.7205 |
| 34.56 | 87.26 | 85.94 | 1.7198 |
| 37.43 | 94.01 | 91.65 | 2.3565 |
| 40.12 | 98.45 | 95.43 | 3.0254 |
| 42.67 | 100.34 | 97.26 | 3.2803 |
| 45.10 | 100.60 | 97.43 | 3.1712 |
| 47.43 | 100.09 | 96.14 | 3.0522 |
| 49.68 | 101.73 | 93.55 | 8.1739 |
| 51.86 | 48.31 | 62.28 | -13.7735 |
| 53.97 | 51.56 | 50.93 | -9.3908 |
| 56.03 | 52.56 | 50.98 | -8.3984 |
| 58.03 | 53.81 | 62.27 | -8.4553 |
| 60.00 | 56.41 | 64.73 | -8.3213 |
| 61.93 | 60.37 | 68.30 | -7.9367 |
| 63.82 | 65.58 | 72.93 | -7.3538 |
| 65.68 | 71.95 | 78.56 | -6.6162 |
| 67.52 | 79.58 | 85.16 | -5.5816 |
| 69.33 | 88.43 | 92.69 | -4.2564 |
| 71.12 | 95.78 | 99.82 | -4.0422 |
| 72.90 | 106.85 | 109.24 | -2.3884 |
| 74.65 | 118.99 | 119.61 | -0.6159 |
| 76.39 | 137.27 | 130.90 | 1.3624 |
| 78.12 | 146.68 | 143.12 | 3.5637 |
| 79.84 | 162.01 | 156.25 | 5.7554 |
| 81.54 | 178.37 | 170.29 | 8.0780 |
| 83.24 | 210.06 | 191.69 | 18.3683 |
| 84.94 | 221.27 | 201.45 | 19.8235 |
| 86.63 | 225.67 | 205.66 | 20.0121 |
| 88.31 | 226.25 | 205.55 | 20.7012 |
| 90.00 | 216.56 | 197.60 | 18.9639 |
| 91.69 | 198.84 | 192.98 | 15.8649 |
| 93.37 | 148.63 | 150.71 | -2.0879 |
| 95.06 | 128.57 | 134.22 | -5.6471 |
| 96.75 | 114.00 | 122.37 | -8.3625 |
| 98.46 | 113.05 | 118.90 | -5.8476 |
| 100.16 | 104.18 | 112.16 | -7.9838 |
| 101.88 | 96.43 | 106.11 | -9.6822 |
| 103.61 | 69.96 | 100.75 | -10.8123 |
| 105.35 | 80.31 | 94.06 | -13.7509 |
| 107.10 | 75.89 | 90.47 | -14.5828 |
| 108.88 | 72.74 | 98.13 | -15.3878 |
| 110.67 | 71.08 | 87.07 | -15.9863 |
| 112.48 | 71.49 | 87.33 | -15.8353 |
| 114.37 | 74.92 | 88.96 | -14.4424 |
| 116.18 | 57.02 | 80.95 | -23.9304 |
| 118.07 | 68.40 | 89.31 | -20.9116 |
| 120.00 | 84.64 | 102.78 | -18.1363 |
| 121.97 | 105.92 | 121.68 | -16.1562 |
| 123.97 | 130.19 | 146.37 | -16.1761 |
| 126.03 | 223.92 | 208.11 | 15.8040 |
| 128.14 | 250.12 | 234.65 | 15.6770 |
| 130.37 | 273.57 | 255.84 | 17.7296 |
| 132.57 | 292.72 | 271.85 | 20.3721 |
| 134.90 | 304.52 | 281.90 | 22.6186 |
| 137.33 | 288.10 | 275.33 | 12.8557 |
| 139.88 | 295.71 | 280.42 | 15.2941 |
| 142.57 | 301.04 | 294.30 | 16.7393 |
| 145.44 | 291.18 | 280.06 | 11.1220 |
| 148.53 | 295.99 | 284.09 | 11.9033 |
| 151.93 | 300.68 | 292.16 | 8.5289 |
| 155.75 | 368.99 | 333.85 | 35.1343 |
| 160.25 | 367.10 | 325.08 | 42.0208 |
| 166.07 | 190.43 | 211.45 | -21.0242 |
| 180.00 | 154.61 | 177.62 | -23.0060 |

ABS. CORRECTION = 1.21E OF DEG. K

TABLE VI-40. APCOR4 OUTPUT

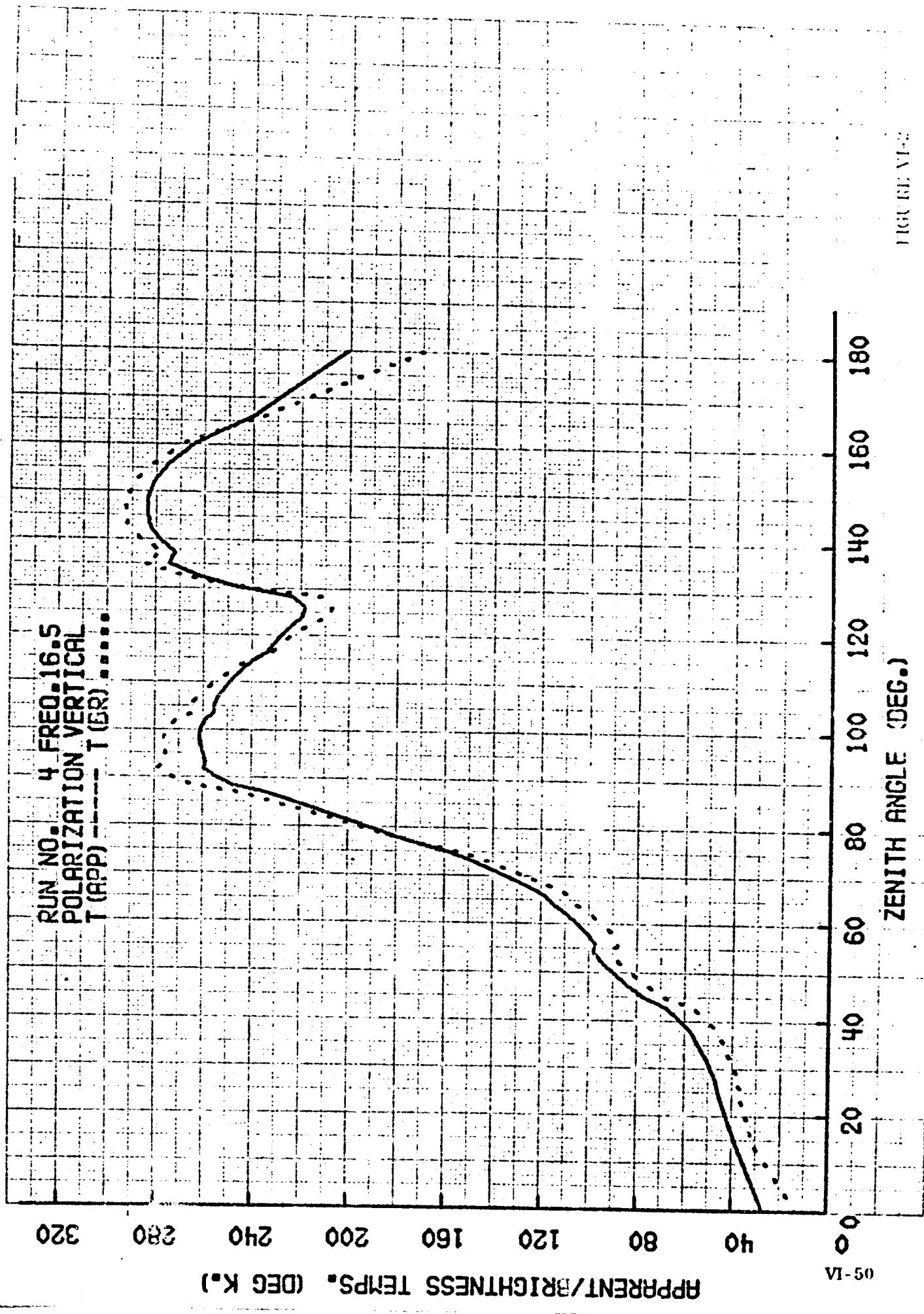
RUN NO. 201 07/17/59 V POLAR, 9.5 GHz SEA WATER

ITERATION NUMBER 0

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMP. (DEG K) | APPARENT TEMP. (DEG K) | CORRECTION TEMP. (DEG K) |
|-----------------------|-----------------------------|---------------------------|-----------------------------|
| 0.00 | 3.71 | 23.12 | -19.6062 |
| 13.93 | 33.12 | 61.17 | -8.0476 |
| 19.75 | 42.69 | 50.68 | -7.9865 |
| 24.25 | 51.42 | 58.82 | -7.4063 |
| 28.07 | 59.49 | 66.29 | -7.7977 |
| 31.47 | 73.35 | 77.84 | -4.2936 |
| 34.55 | 78.70 | 83.75 | -4.0534 |
| 37.43 | 83.88 | 88.74 | -4.0534 |
| 40.12 | 88.21 | 92.98 | -4.7737 |
| 42.67 | 91.73 | 96.61 | -4.6779 |
| 45.10 | 95.16 | 99.73 | -4.5697 |
| 47.43 | 98.00 | 102.39 | -4.3908 |
| 49.58 | 100.90 | 104.65 | -3.7628 |
| 51.85 | 98.16 | 102.89 | -6.7379 |
| 53.97 | 98.76 | 104.97 | -6.2107 |
| 56.03 | 100.90 | 107.05 | -6.1667 |
| 58.03 | 102.92 | 109.19 | -6.2667 |
| 60.00 | 104.95 | 111.34 | -6.3912 |
| 61.93 | 106.20 | 113.52 | -6.6165 |
| 63.82 | 108.80 | 115.73 | -6.9239 |
| 65.68 | 111.00 | 117.95 | -6.9625 |
| 67.52 | 115.09 | 120.23 | -5.1422 |
| 69.23 | 122.77 | 122.53 | 0.2426 |
| 71.12 | 66.75 | 92.24 | -25.4842 |
| 72.90 | 77.33 | 96.95 | -19.6286 |
| 74.65 | 86.91 | 103.73 | -16.9266 |
| 76.39 | 94.95 | 112.52 | -15.6731 |
| 78.12 | 109.02 | 123.28 | -14.2644 |
| 79.84 | 123.51 | 135.98 | -12.0665 |
| 81.54 | 141.45 | 150.60 | -9.1473 |
| 83.24 | 148.35 | 151.25 | -12.9115 |
| 84.94 | 175.29 | 185.22 | -8.9352 |
| 86.63 | 213.36 | 216.94 | -3.5782 |
| 88.31 | 304.69 | 276.75 | 27.9865 |
| 90.00 | 336.16 | 303.57 | 32.5925 |
| 91.69 | 352.18 | 317.54 | 34.6466 |
| 93.37 | 333.26 | 309.53 | 23.5296 |
| 95.06 | 330.32 | 307.23 | 23.0925 |
| 96.76 | 323.03 | 301.38 | 21.6523 |
| 98.46 | 300.50 | 287.30 | 13.2056 |
| 100.16 | 290.47 | 279.58 | 10.8915 |
| 101.85 | 281.01 | 273.29 | 8.5181 |
| 103.61 | 274.13 | 258.45 | 5.6740 |
| 105.35 | 284.61 | 273.27 | 11.3399 |
| 107.10 | 279.20 | 270.03 | 9.1983 |
| 108.88 | 273.76 | 256.21 | 7.5529 |
| 110.67 | 268.11 | 251.63 | 6.2329 |
| 112.48 | 262.37 | 256.98 | 5.3879 |
| 114.32 | 257.00 | 251.49 | 5.5126 |
| 116.18 | 225.20 | 232.52 | -7.3204 |
| 118.07 | 224.07 | 230.14 | -6.0624 |
| 120.00 | 225.71 | 231.15 | -5.4386 |
| 121.97 | 230.29 | 235.75 | -5.4686 |
| 123.97 | 237.58 | 244.18 | -6.6043 |
| 126.03 | 286.93 | 275.28 | 11.6572 |
| 128.14 | 295.04 | 295.42 | 10.6201 |
| 130.32 | 303.93 | 292.98 | 10.9529 |
| 132.57 | 309.33 | 297.72 | 11.6110 |
| 134.90 | 311.40 | 299.34 | 12.0555 |
| 137.33 | 299.38 | 292.73 | 6.6504 |
| 139.82 | 298.13 | 291.27 | 6.8624 |
| 142.57 | 294.95 | 288.78 | 6.1655 |
| 145.44 | 288.78 | 284.34 | 6.4412 |
| 148.33 | 282.63 | 279.44 | 3.1929 |
| 151.93 | 273.97 | 273.22 | 0.3472 |
| 155.75 | 282.78 | 275.14 | 7.6392 |
| 160.25 | 262.49 | 253.18 | 9.3185 |
| 166.07 | 138.17 | 171.93 | -33.7523 |
| 180.00 | 137.11 | 160.76 | -23.6516 |

ABS. CORRECTION = 1.04E 01 DEG. K

TABLE VI-41. APCOR4 OUTPUT



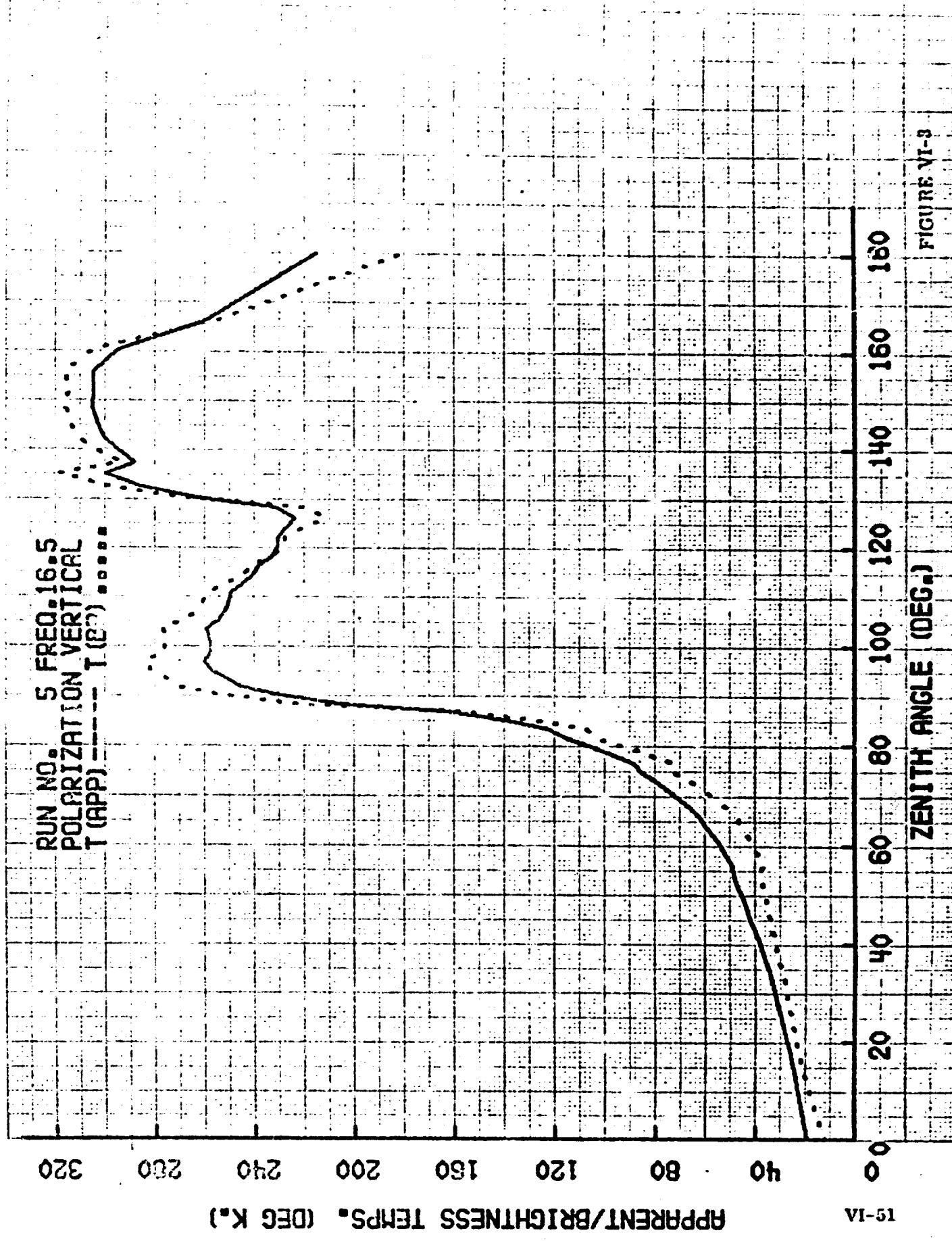


FIGURE VI-3

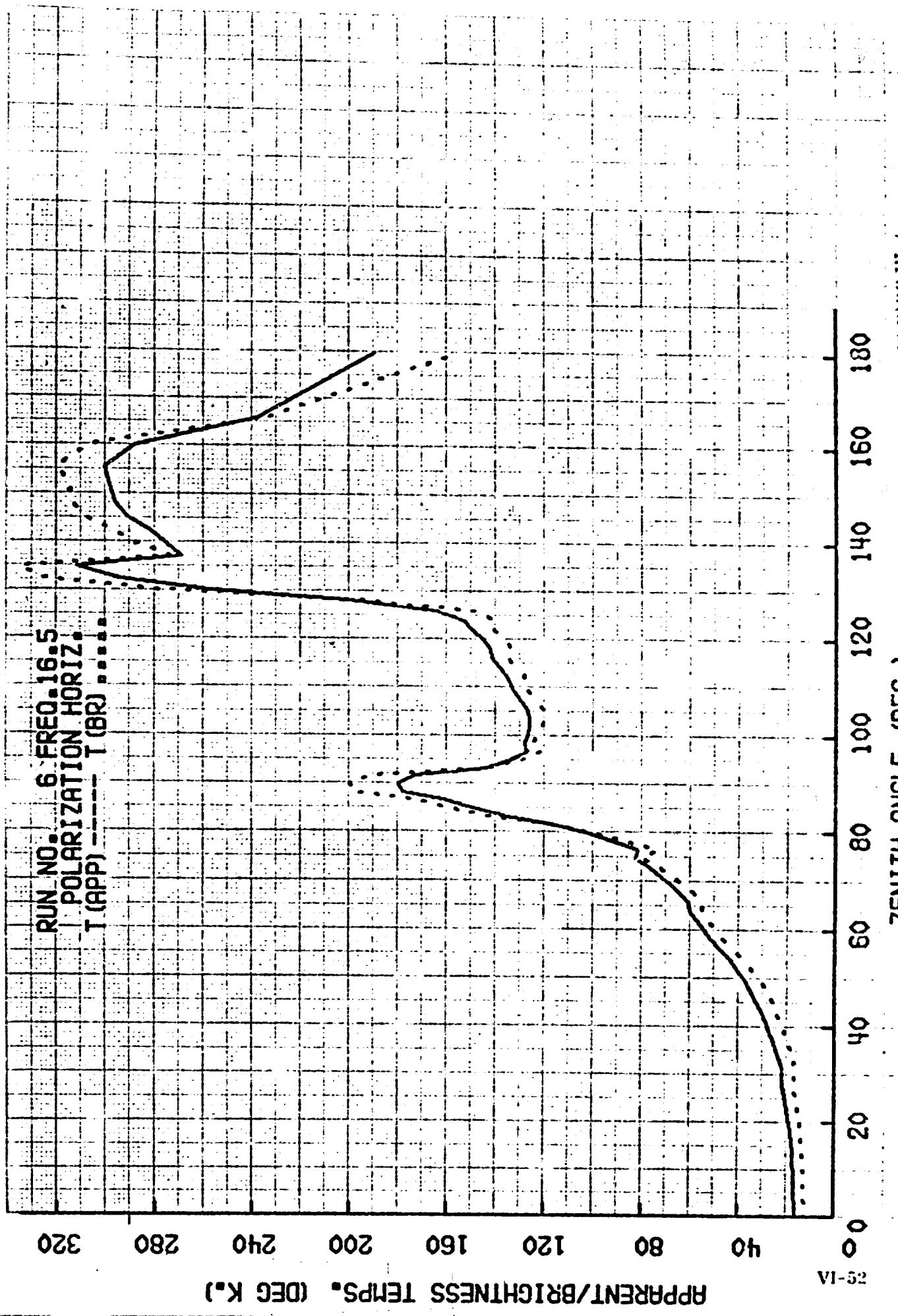


FIGURE VI-4

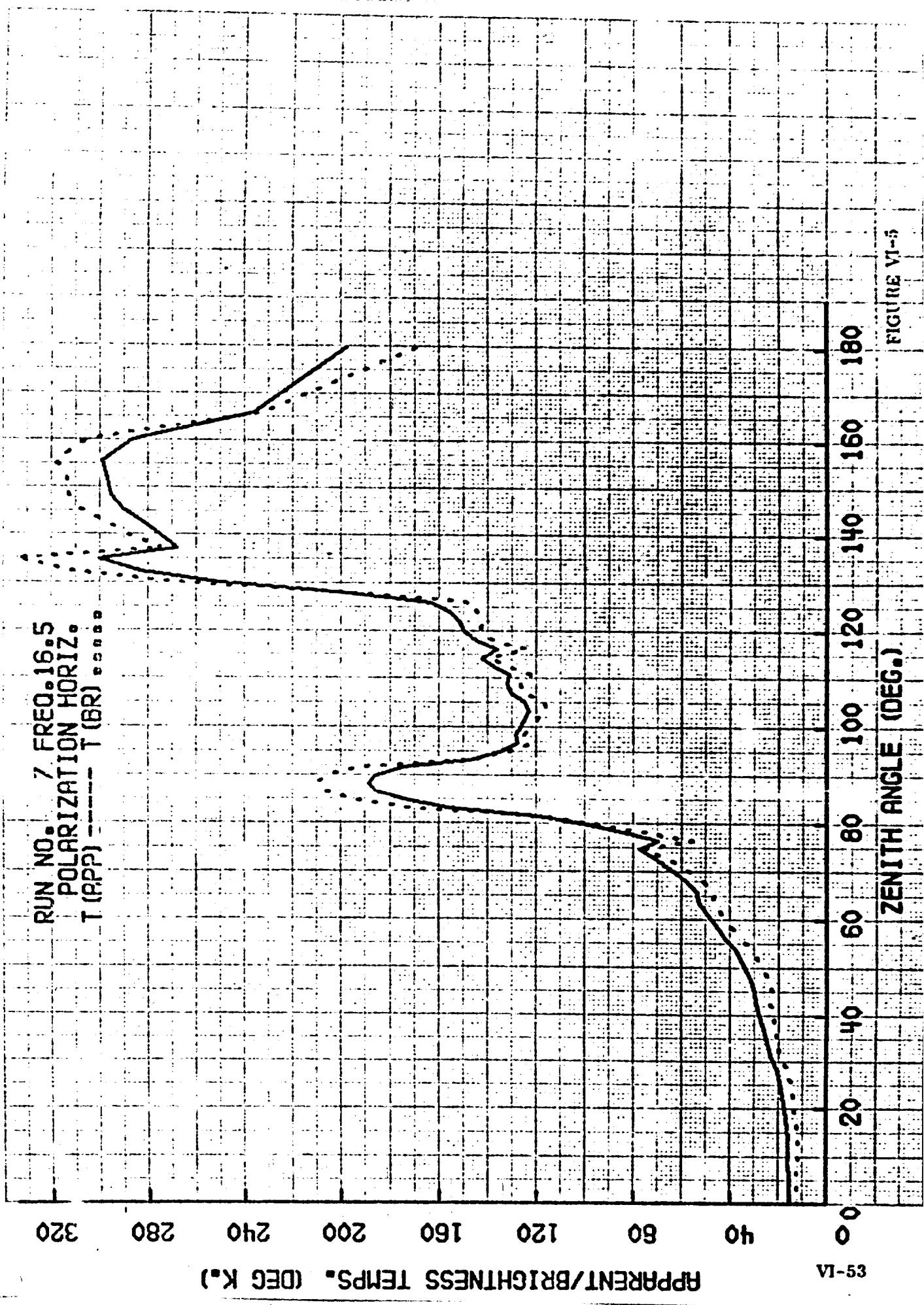
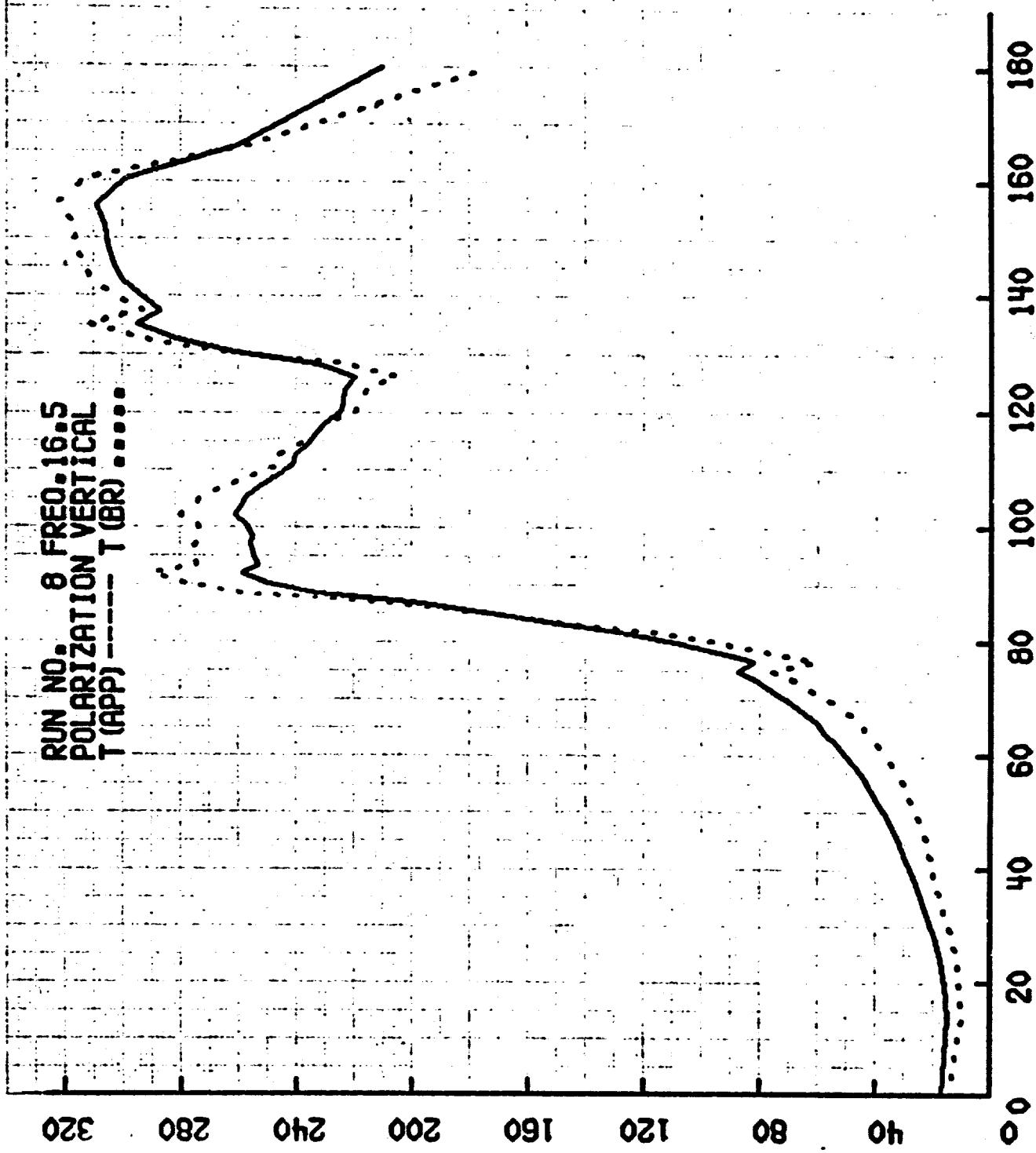


FIGURE VI-6

ZENITH ANGLE (DEG.)



APPARENT/BRIGHTNESS TEMPS. (DEG K.)

FIGURE V-1

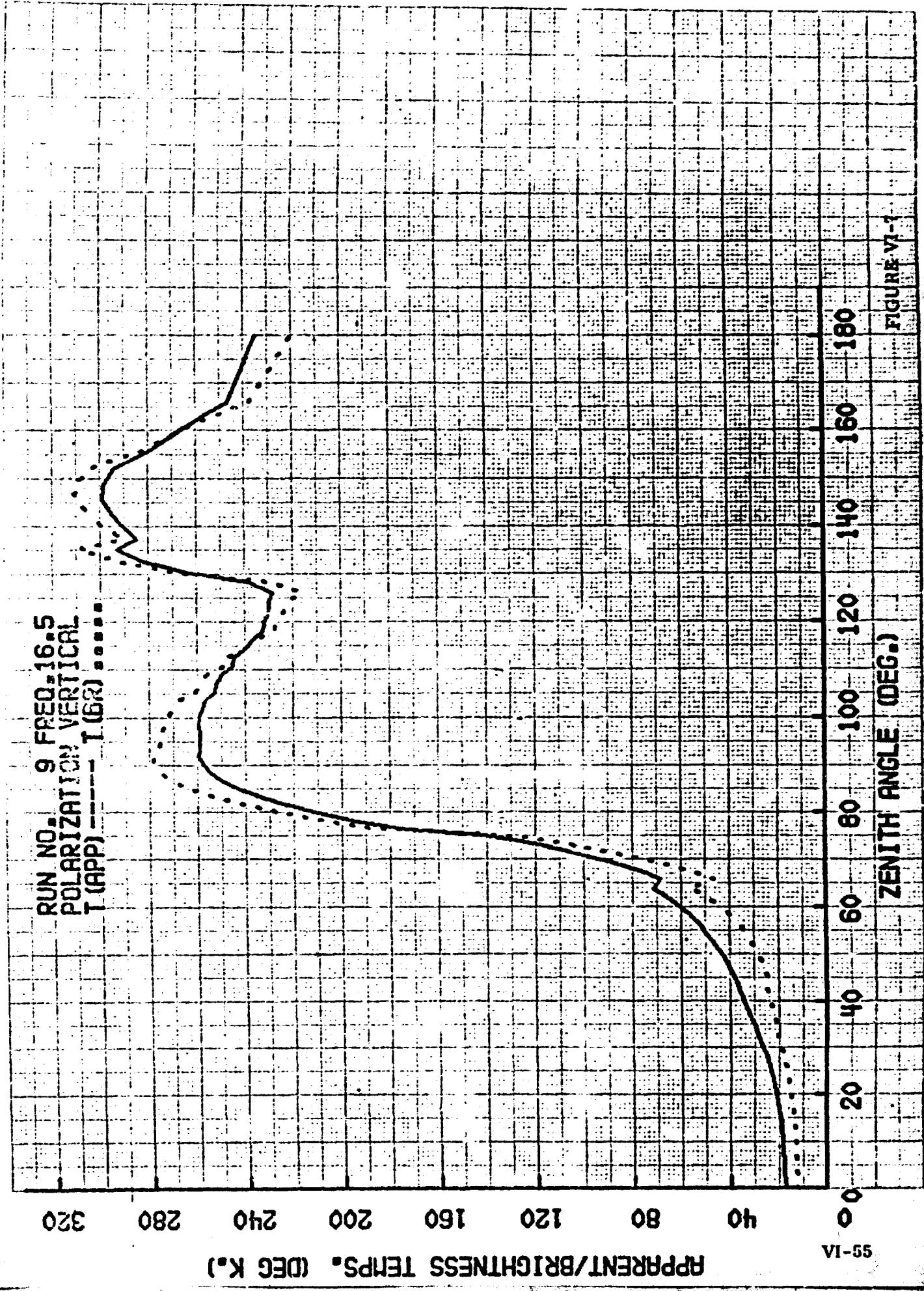
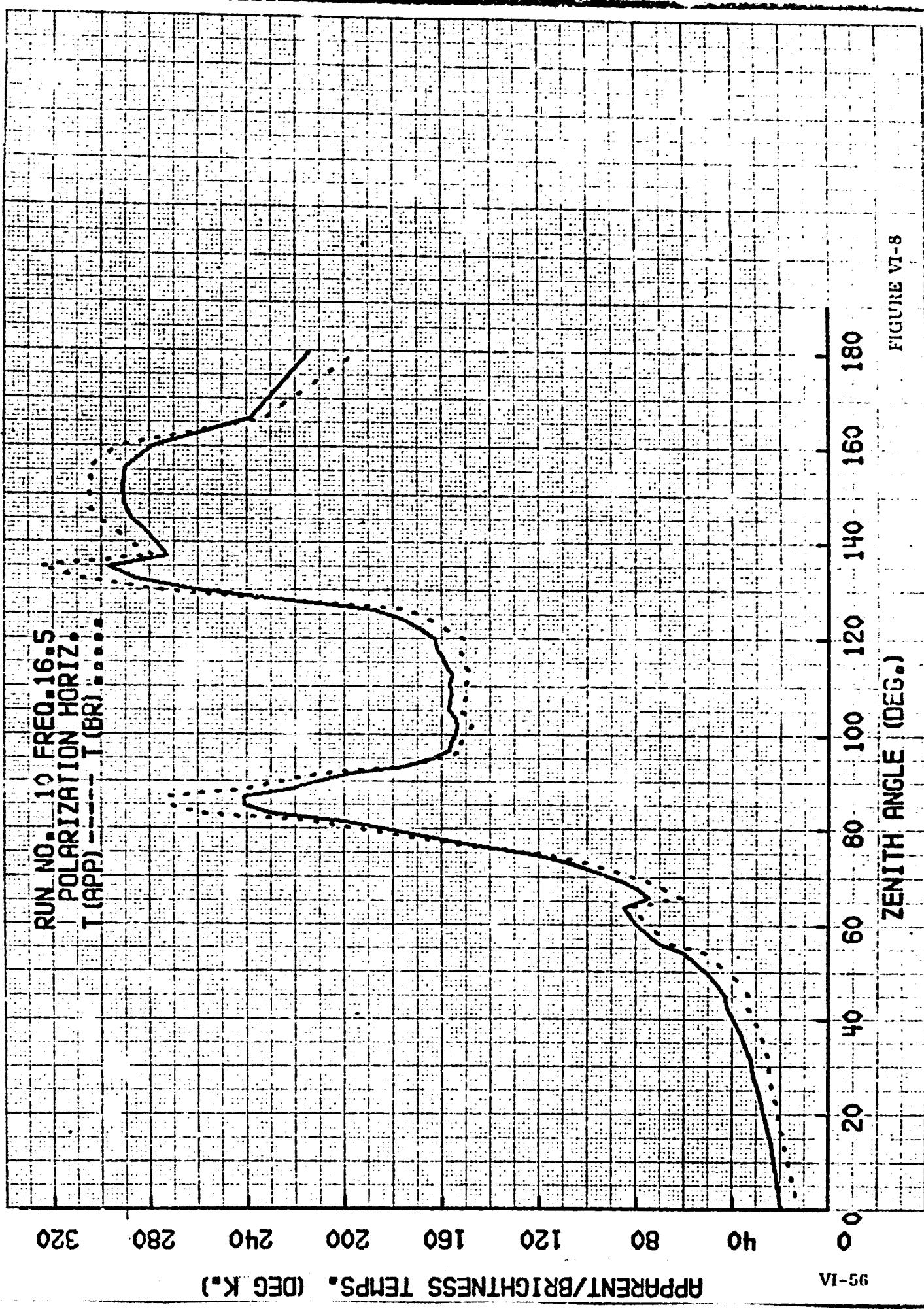
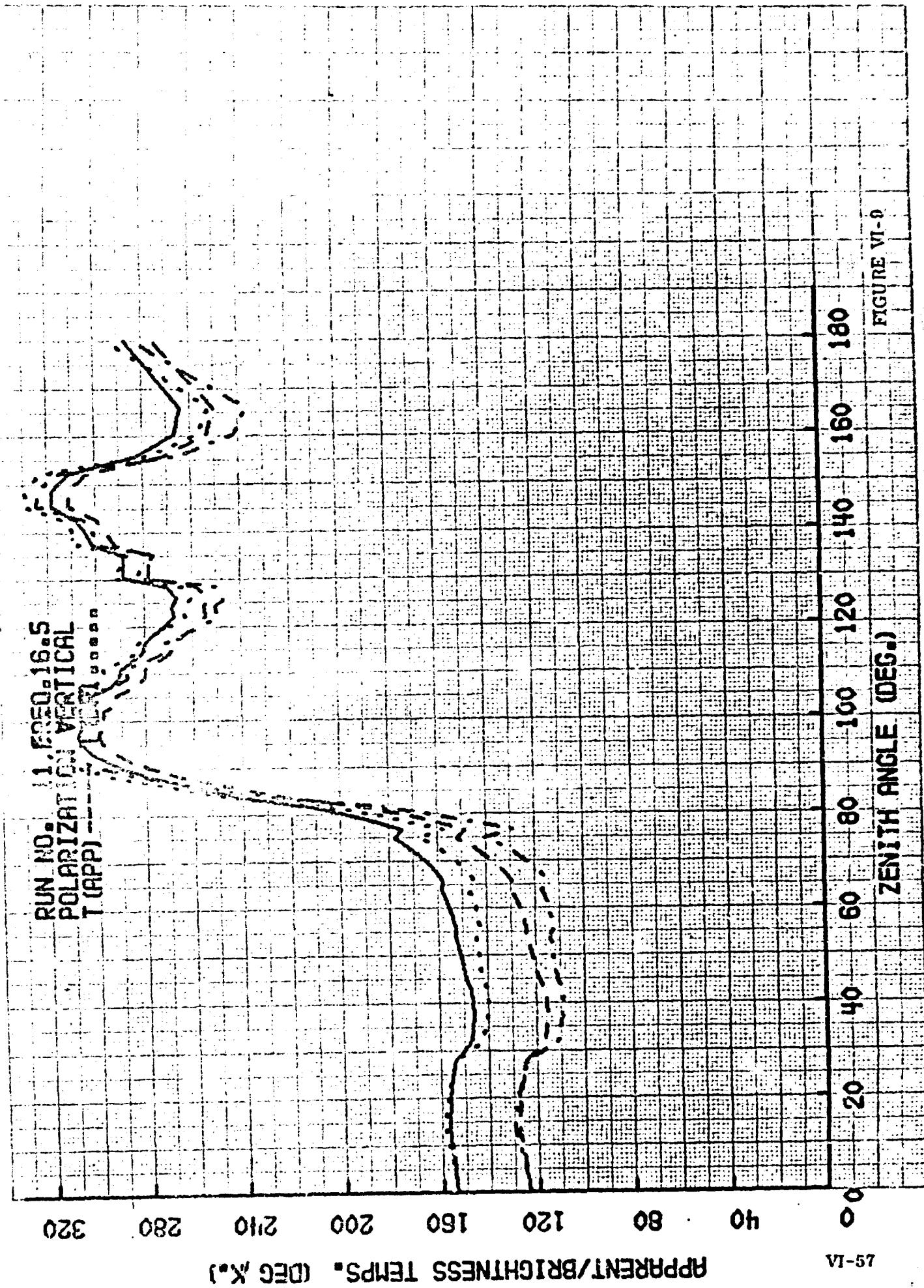


FIGURE VI-8



RUN NO. 11. FREQ = 16.5
POLARIZAT. = VERTICAL
T(RPP) =



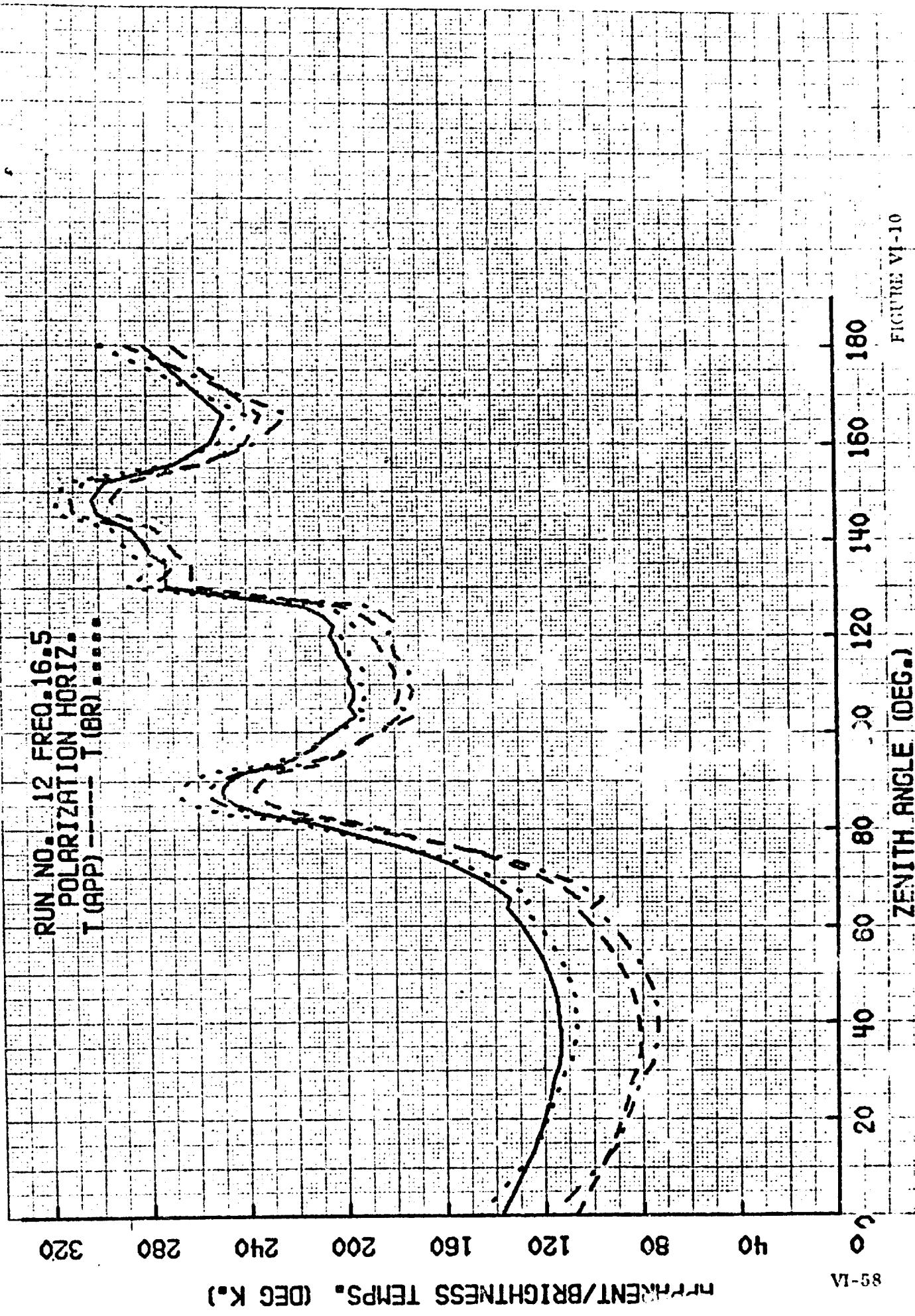


FIGURE VI-11
ZENITH ANGLE (DEG.)

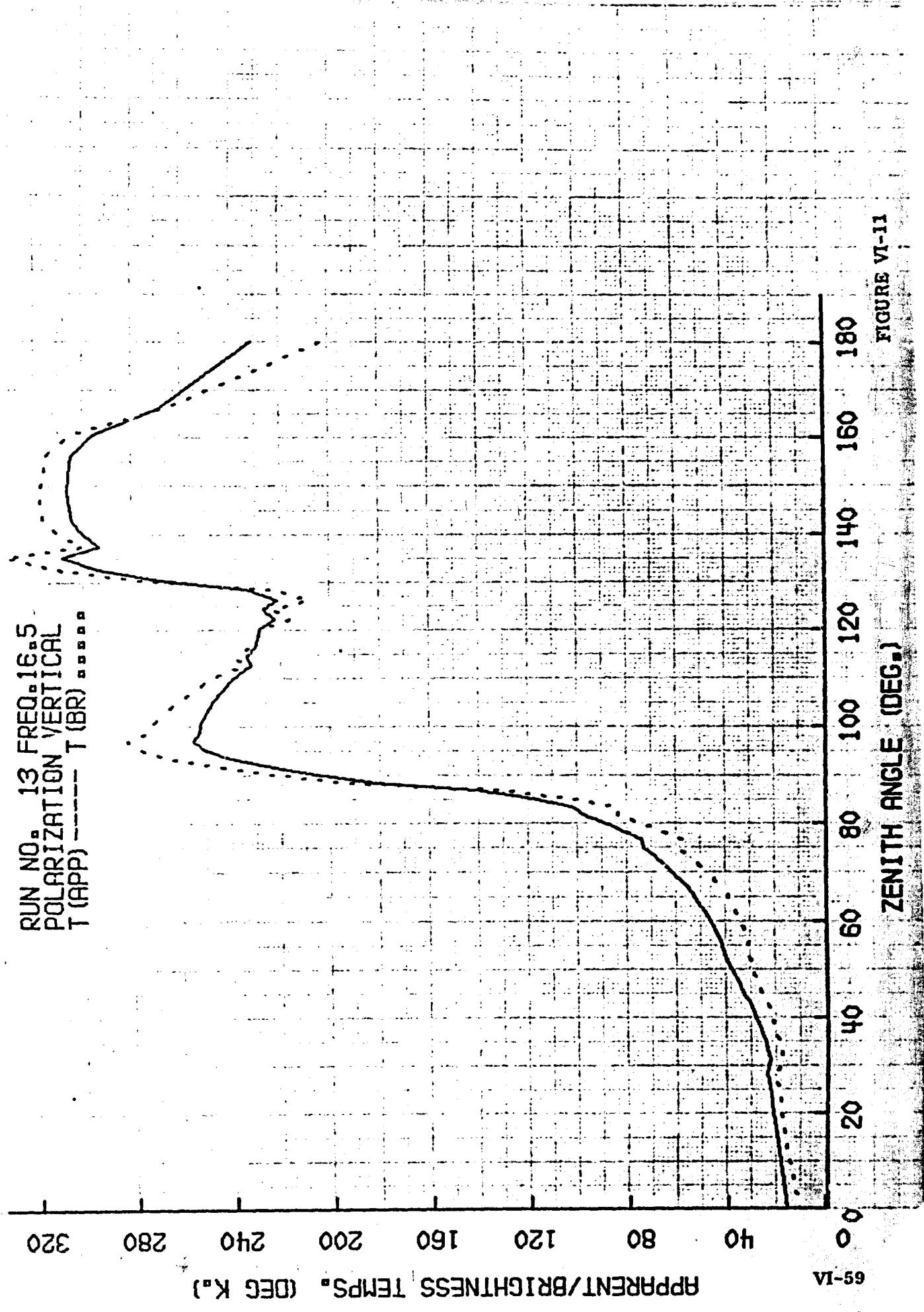


FIGURE VI-12

APPARENT/BRIGHTNESS TEMPS. (DEG K.)

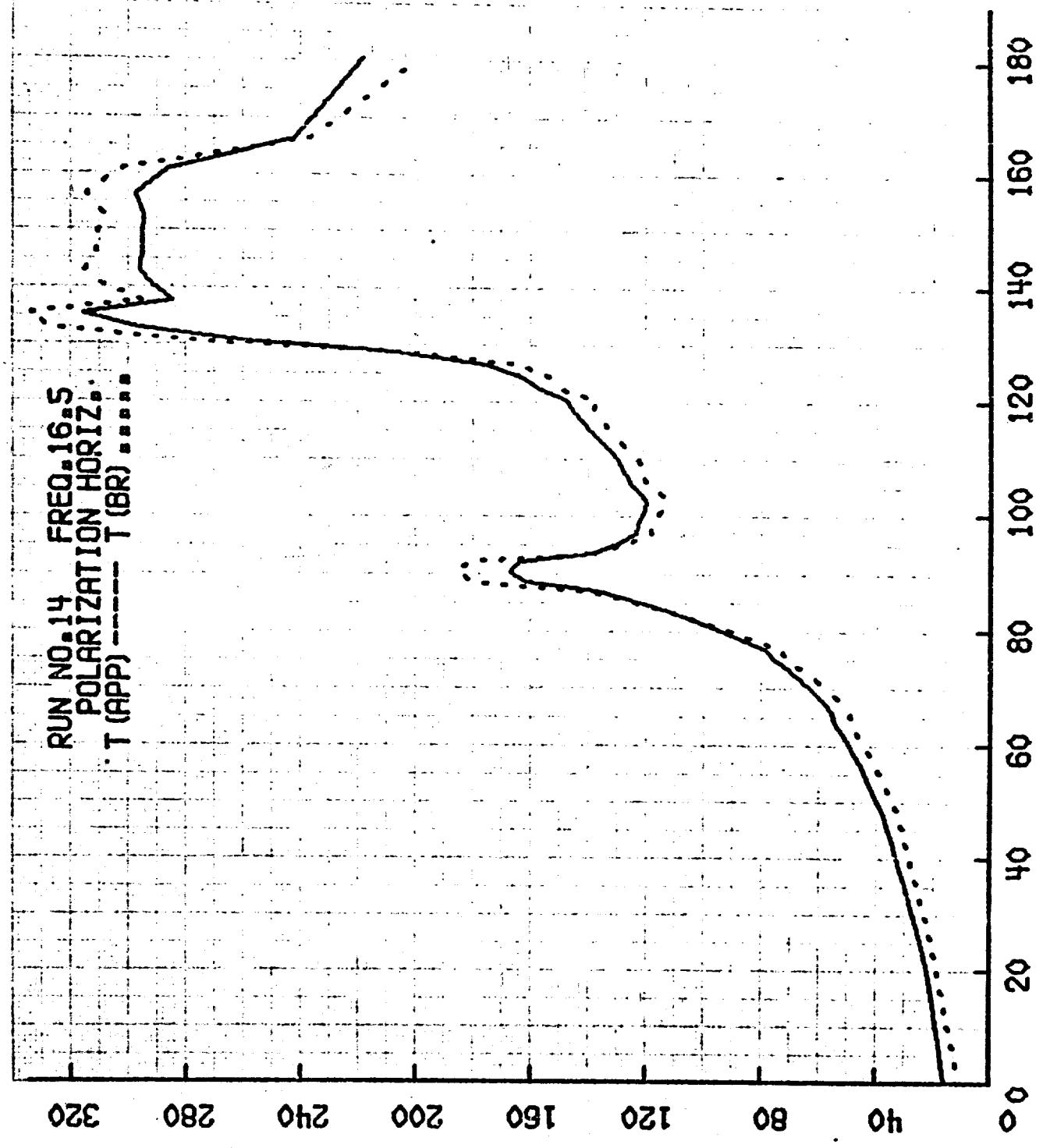


FIGURE VI-13

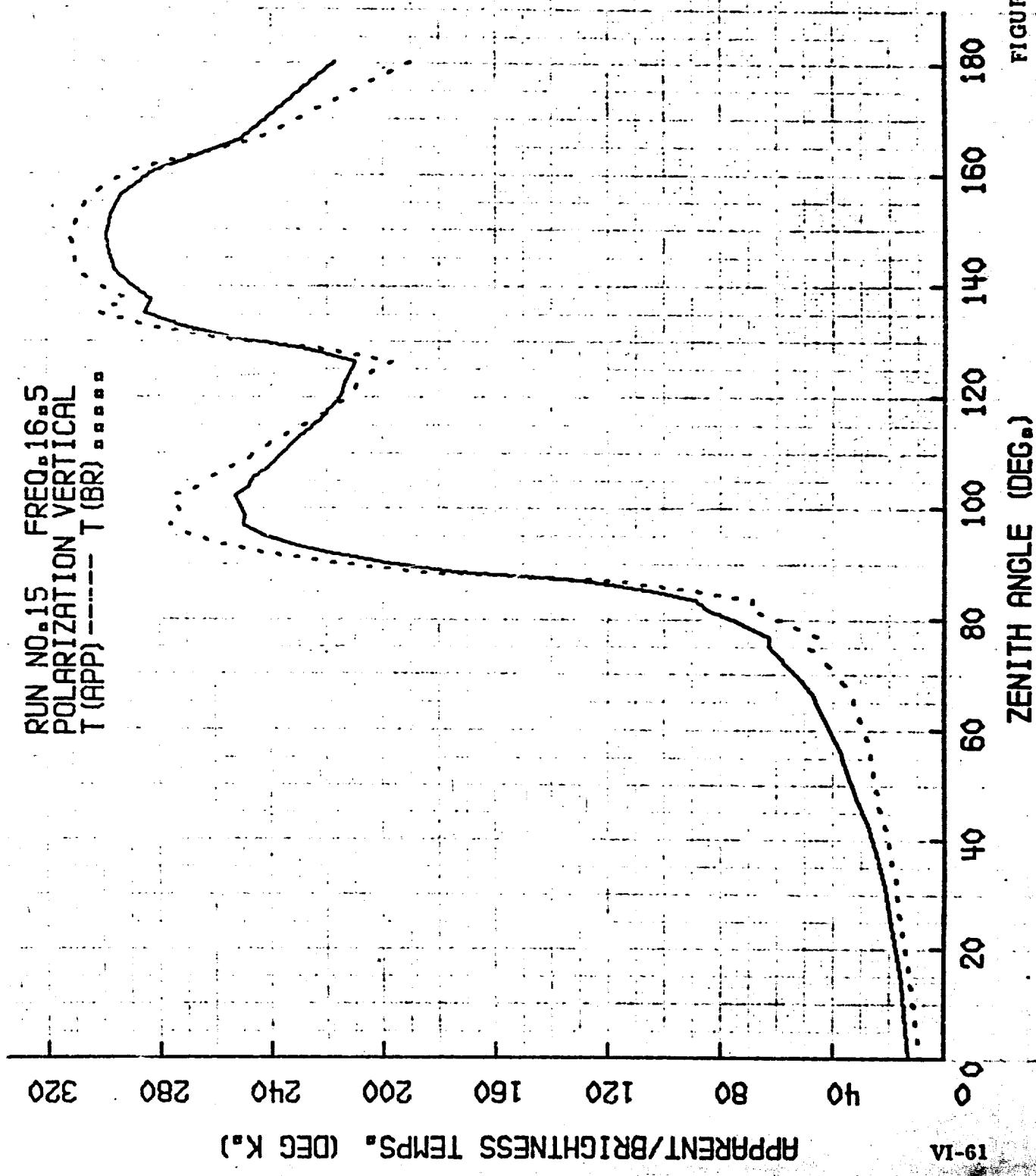


FIGURE VI-14

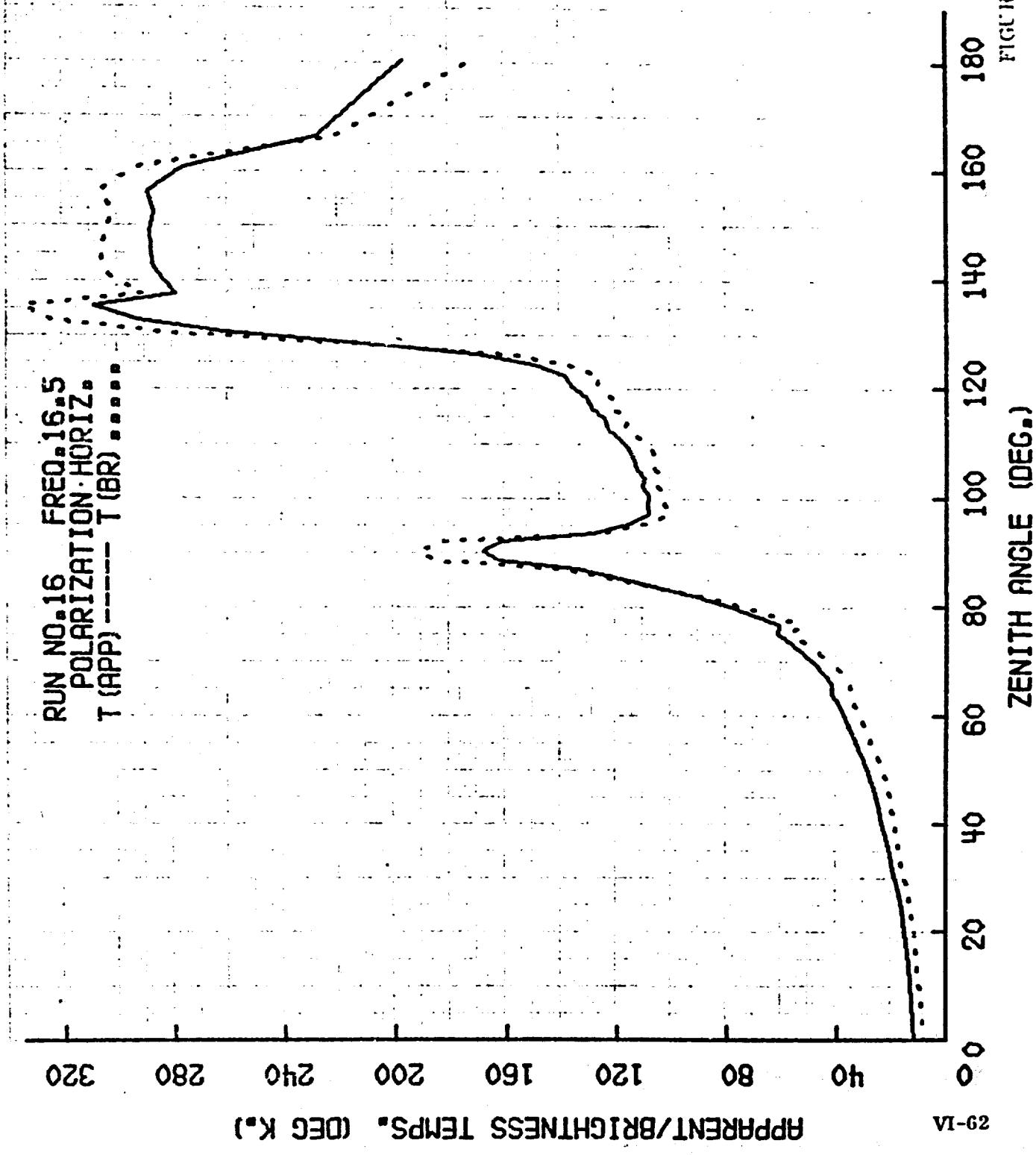


FIGURE VI-15

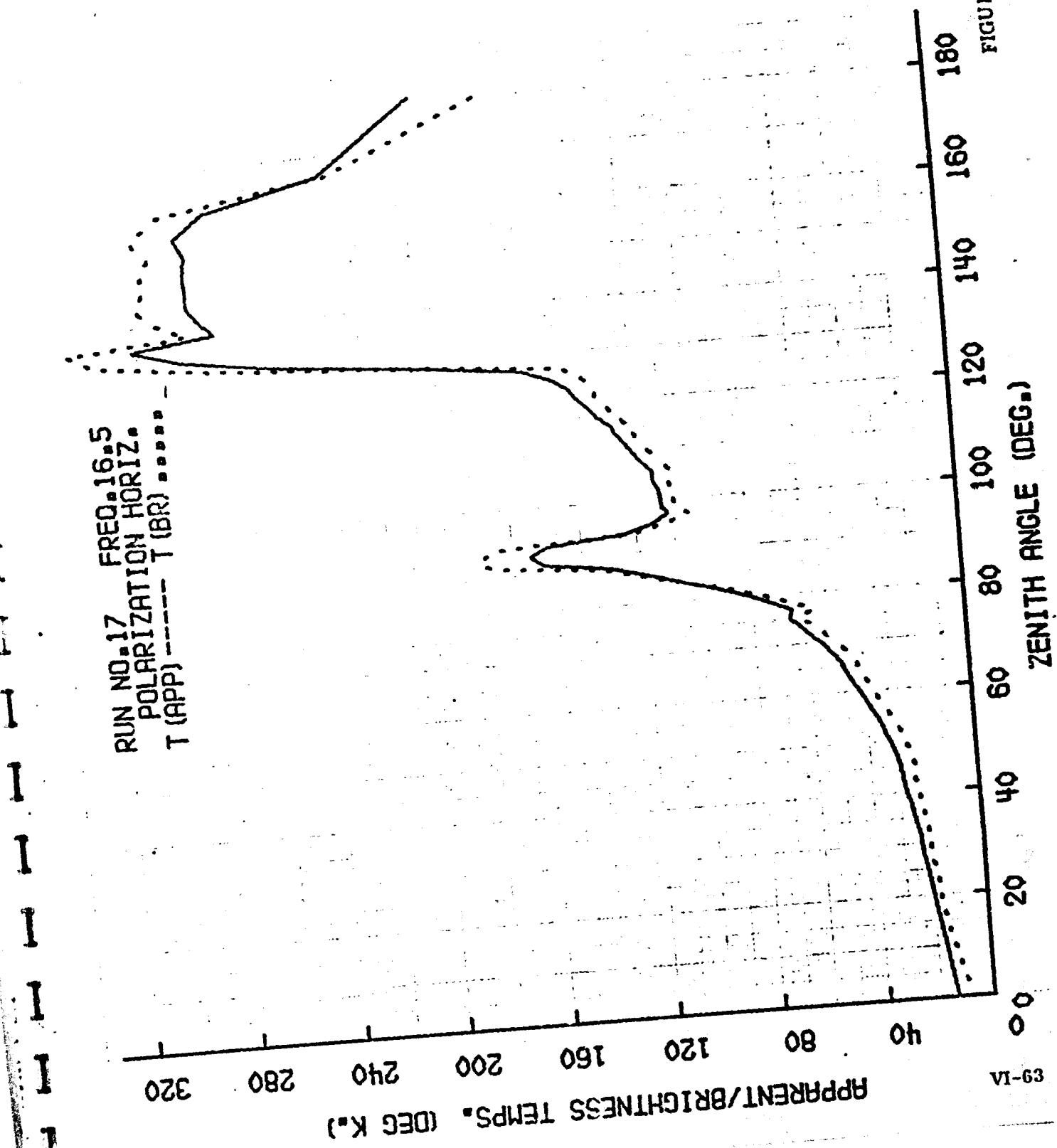


FIGURE VI-16

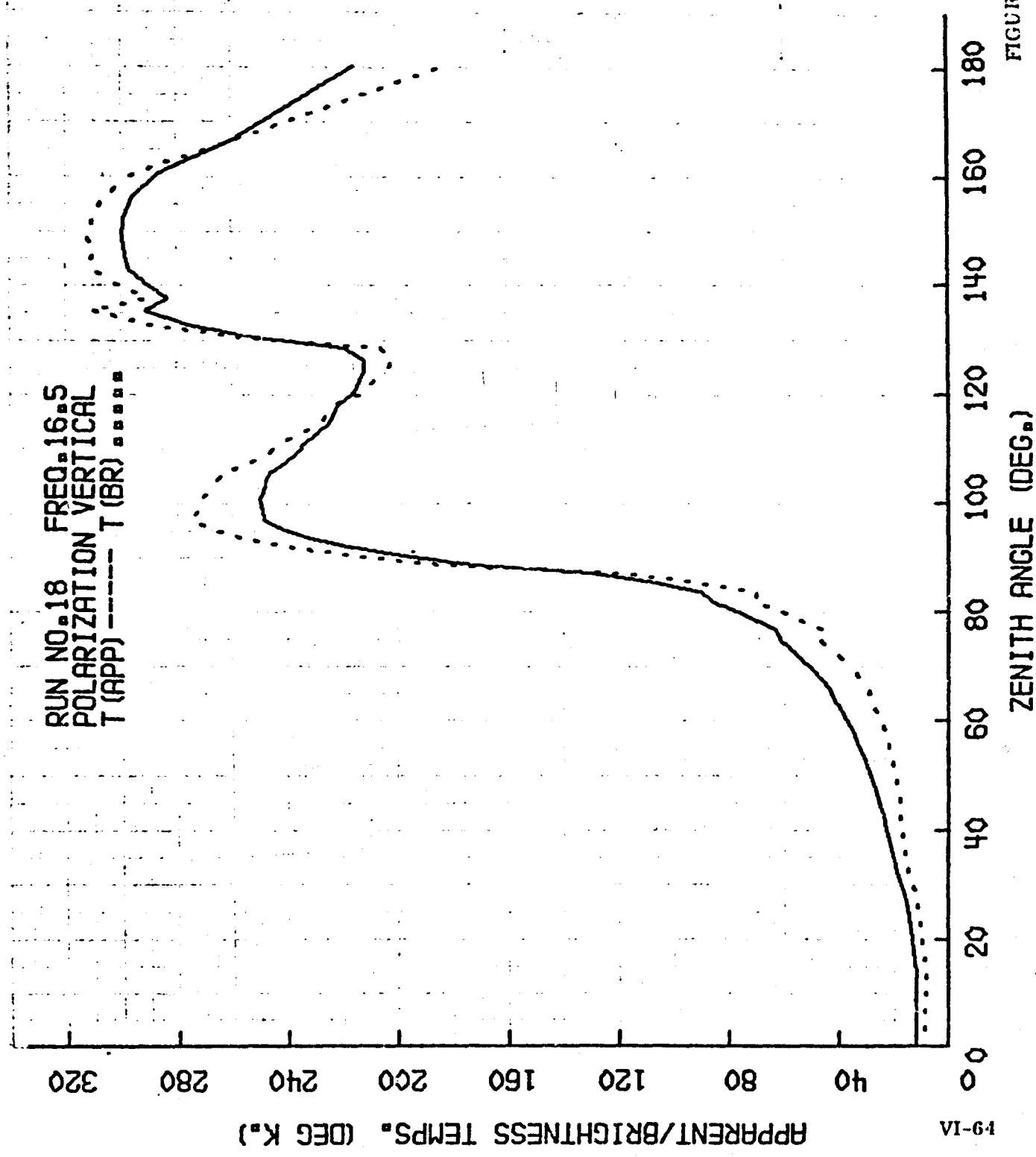


FIGURE VI-17

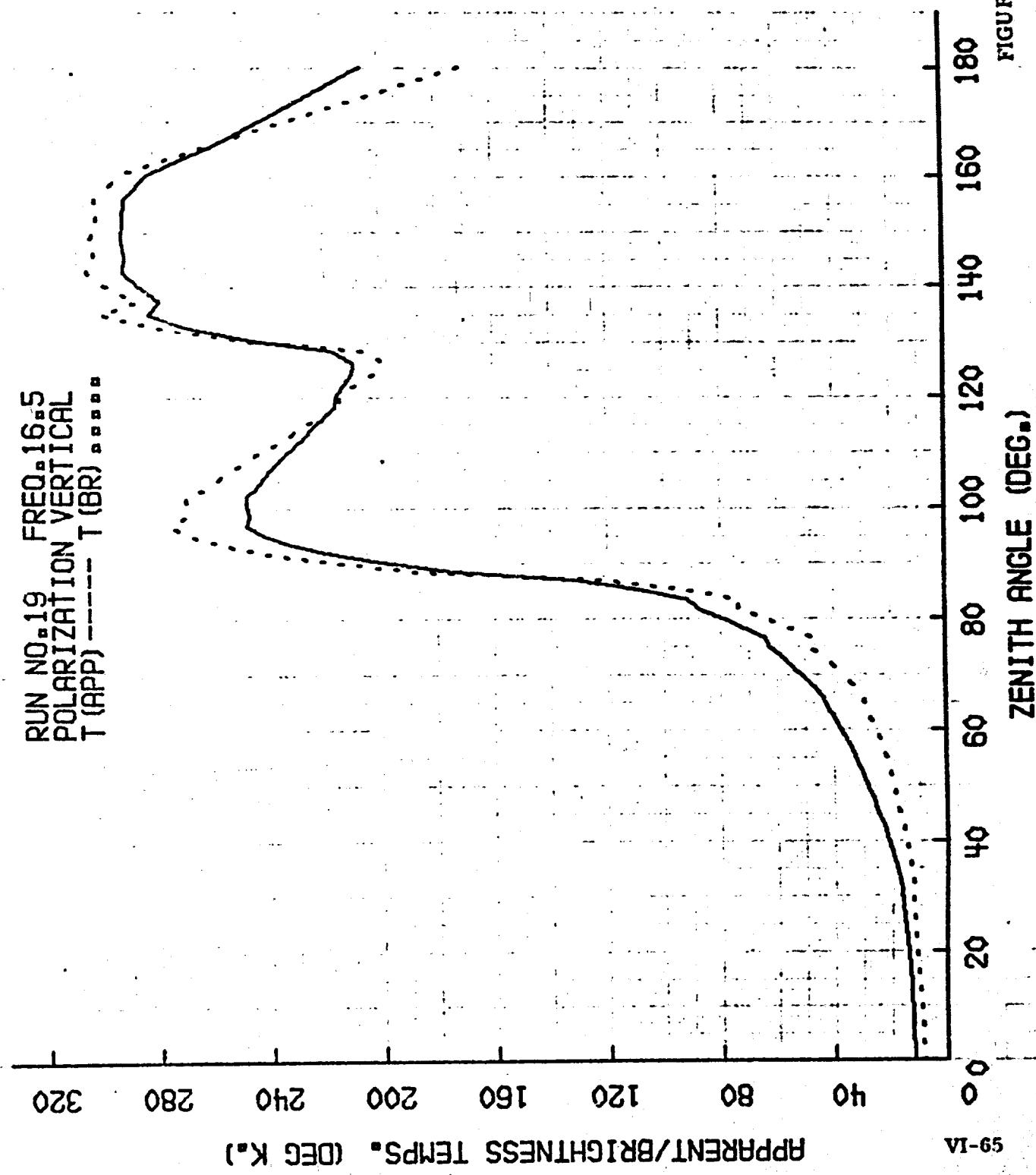


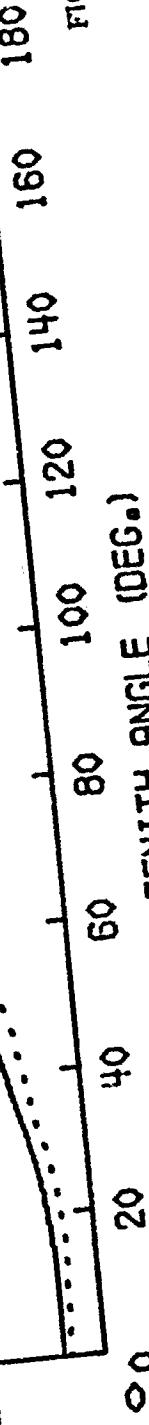
FIGURE VI-18

ZENITH ANGLE (DEG.)

99-1A

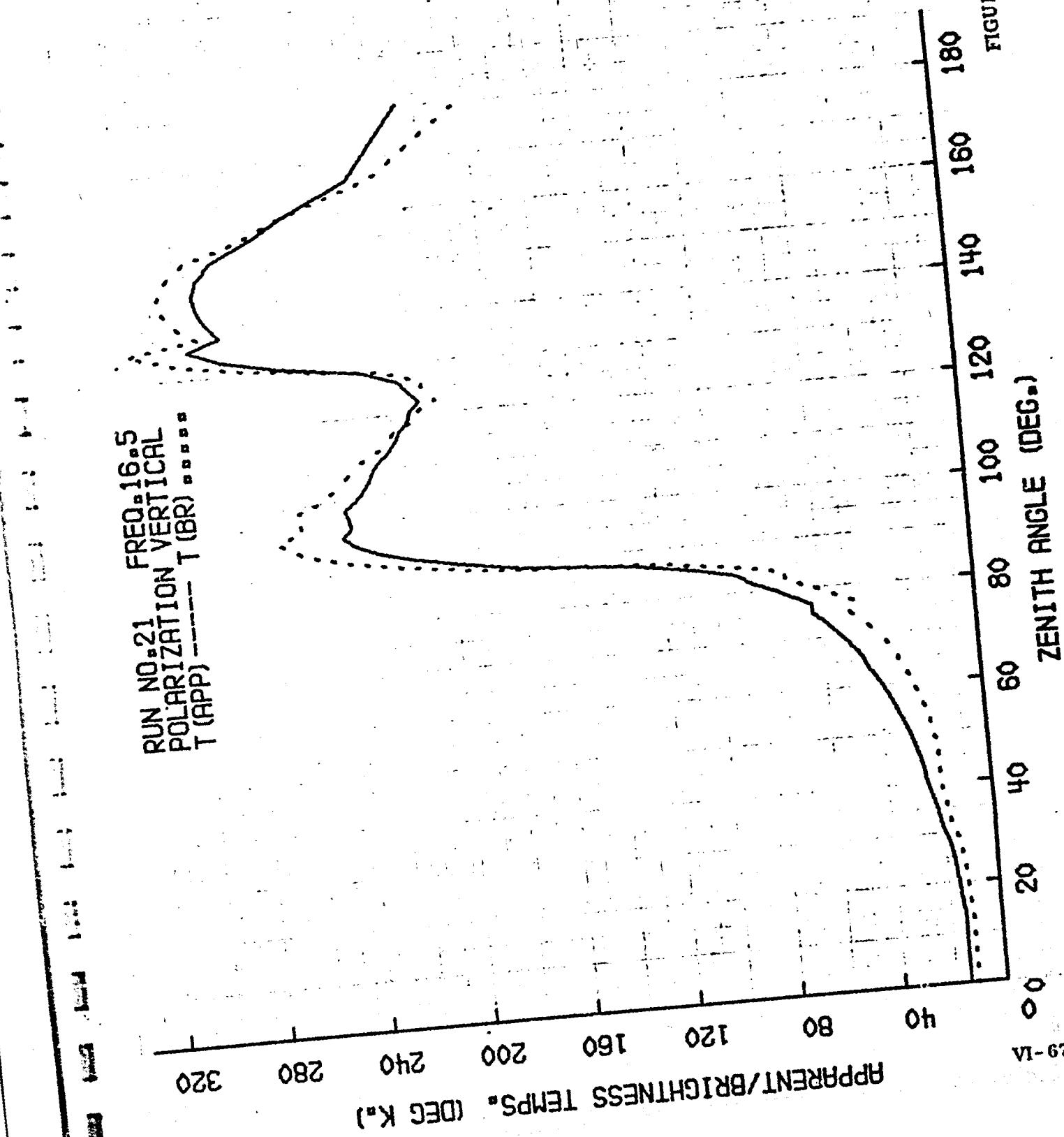
RUN NO. 20 FREQ. 16.5
POLARIZATION HORIZ.
T (APP) ----- T (BR) ····

APPARENT/BRIGHTNESS TEMPS. (DEG. K.)



79-1A

FIGURE VI-19



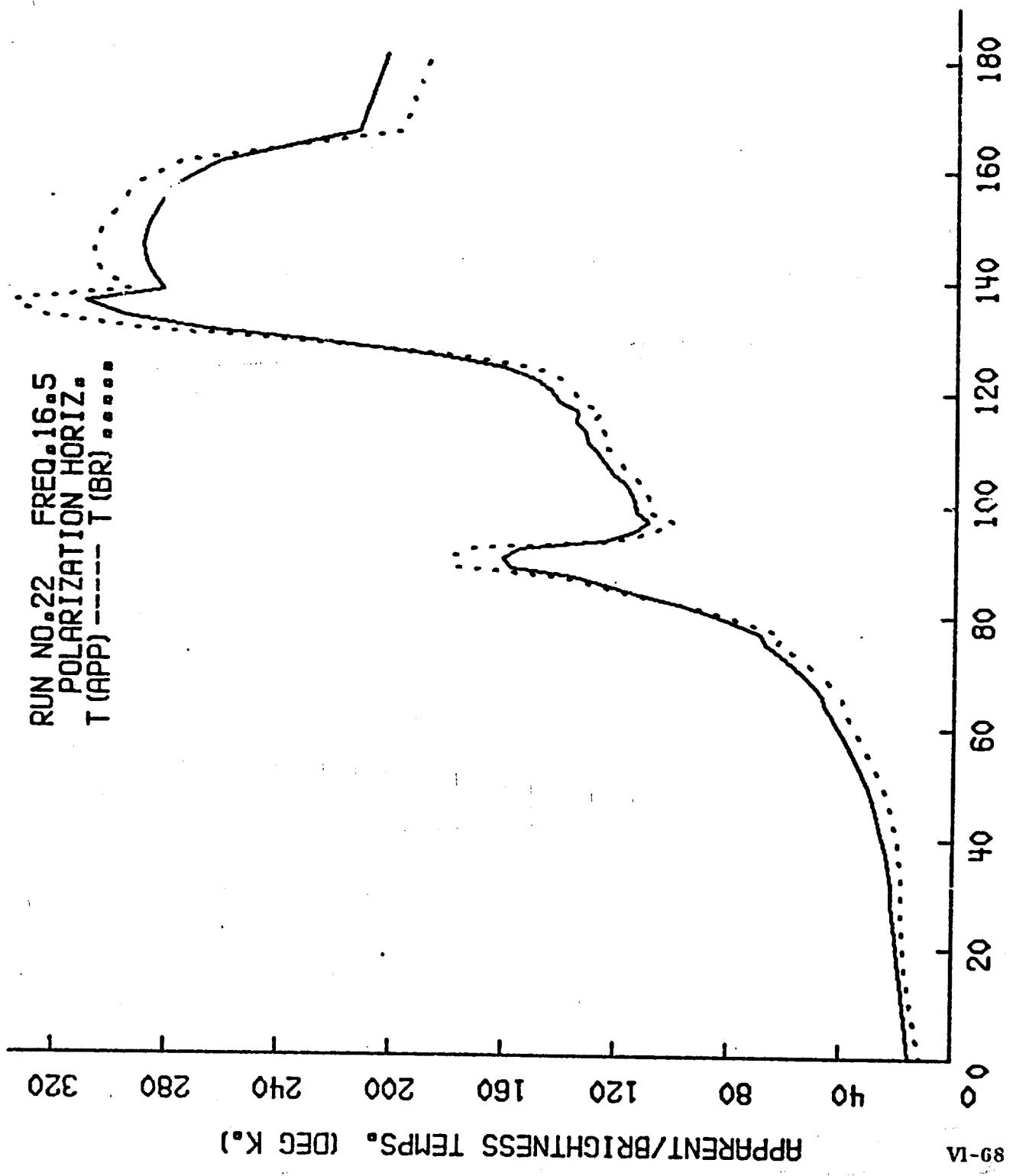


FIGURE VI-20

FIGURE VI-21

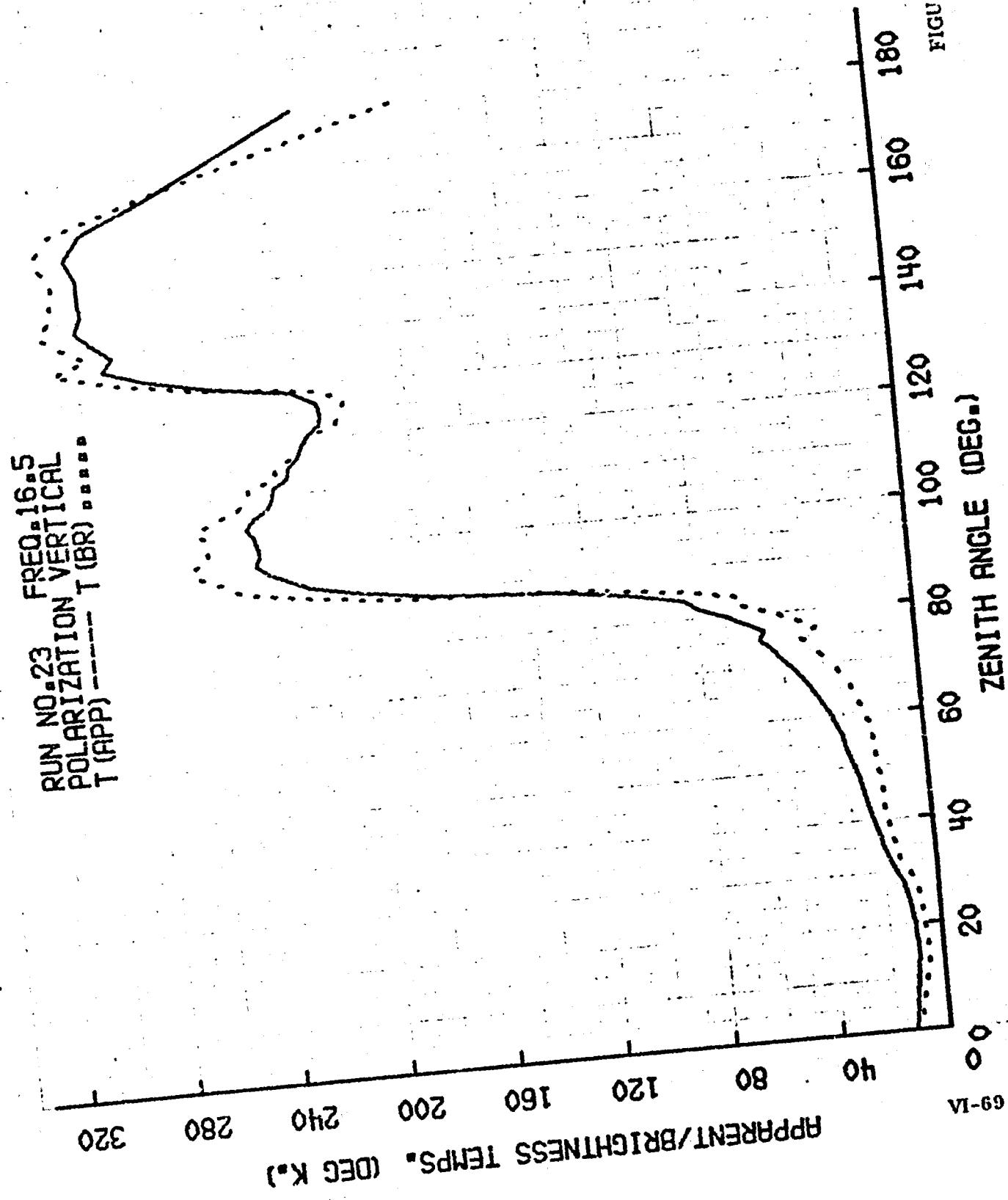


FIGURE VI-22

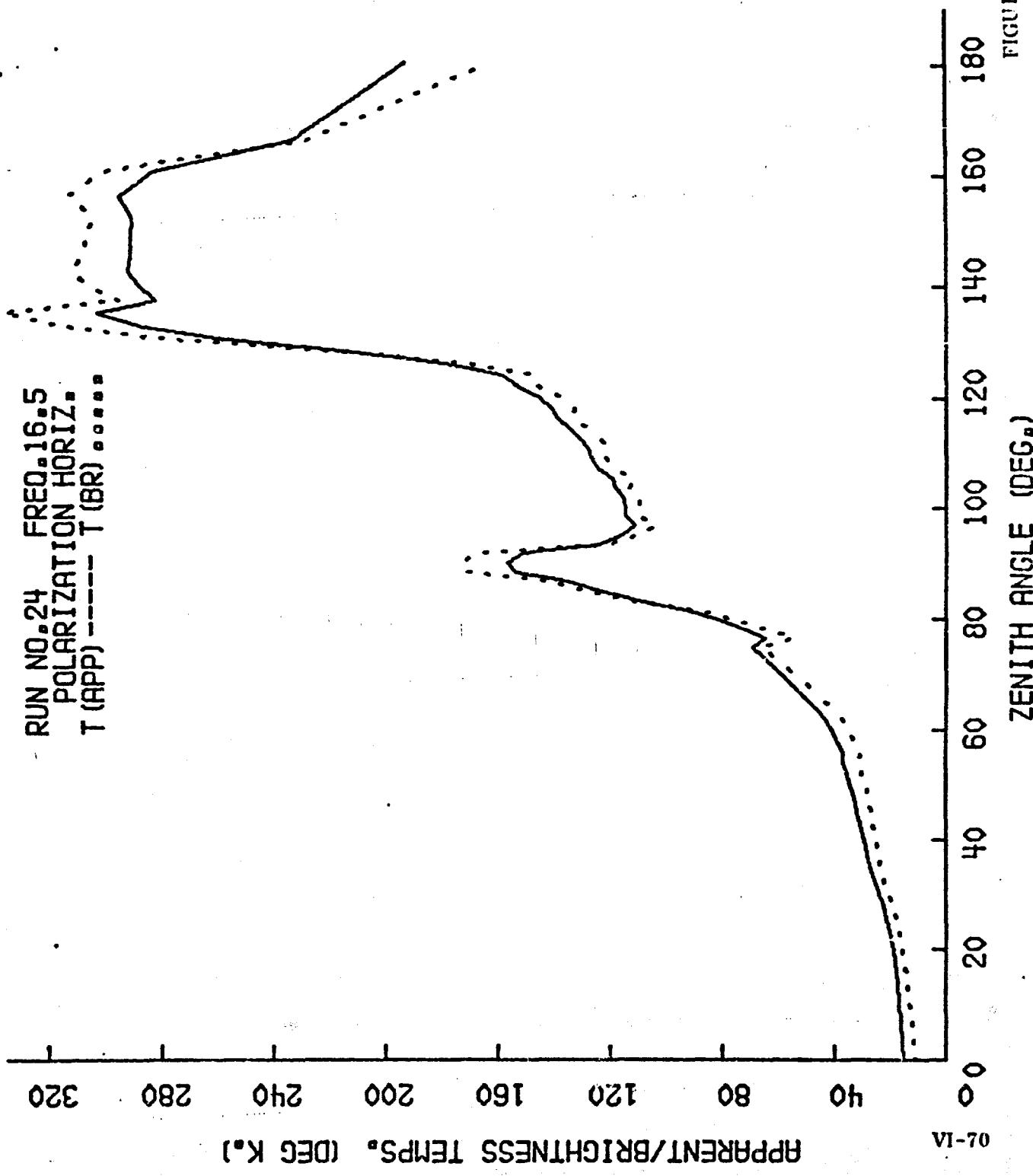
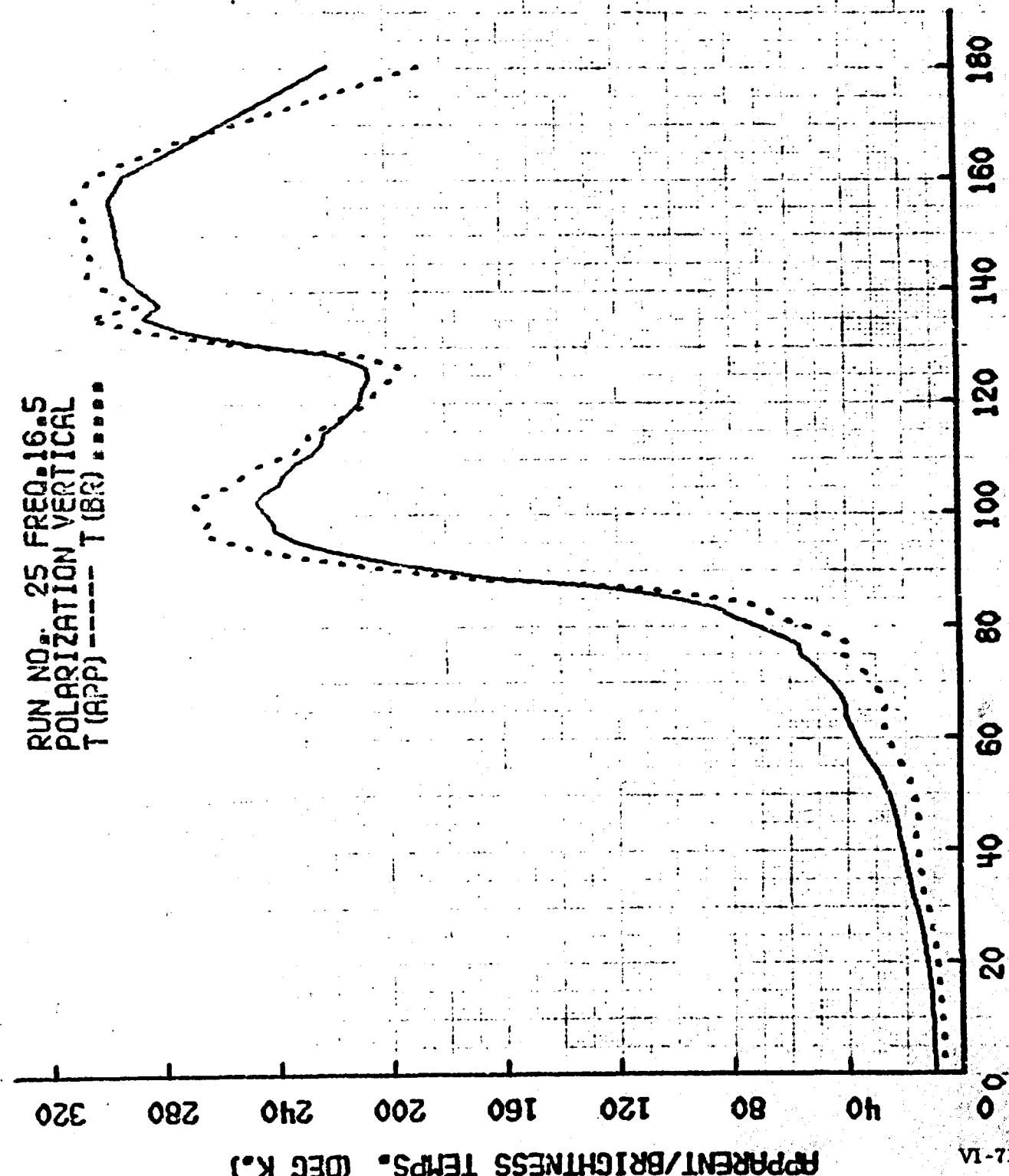


FIGURE VI-23

ZENITH ANGLE (DEG.)



RUN NO. 26 FREQ. 16.5
POLARIZATION HCPDZ.
 T_{APP} --- $T_{(GR)}$ ···

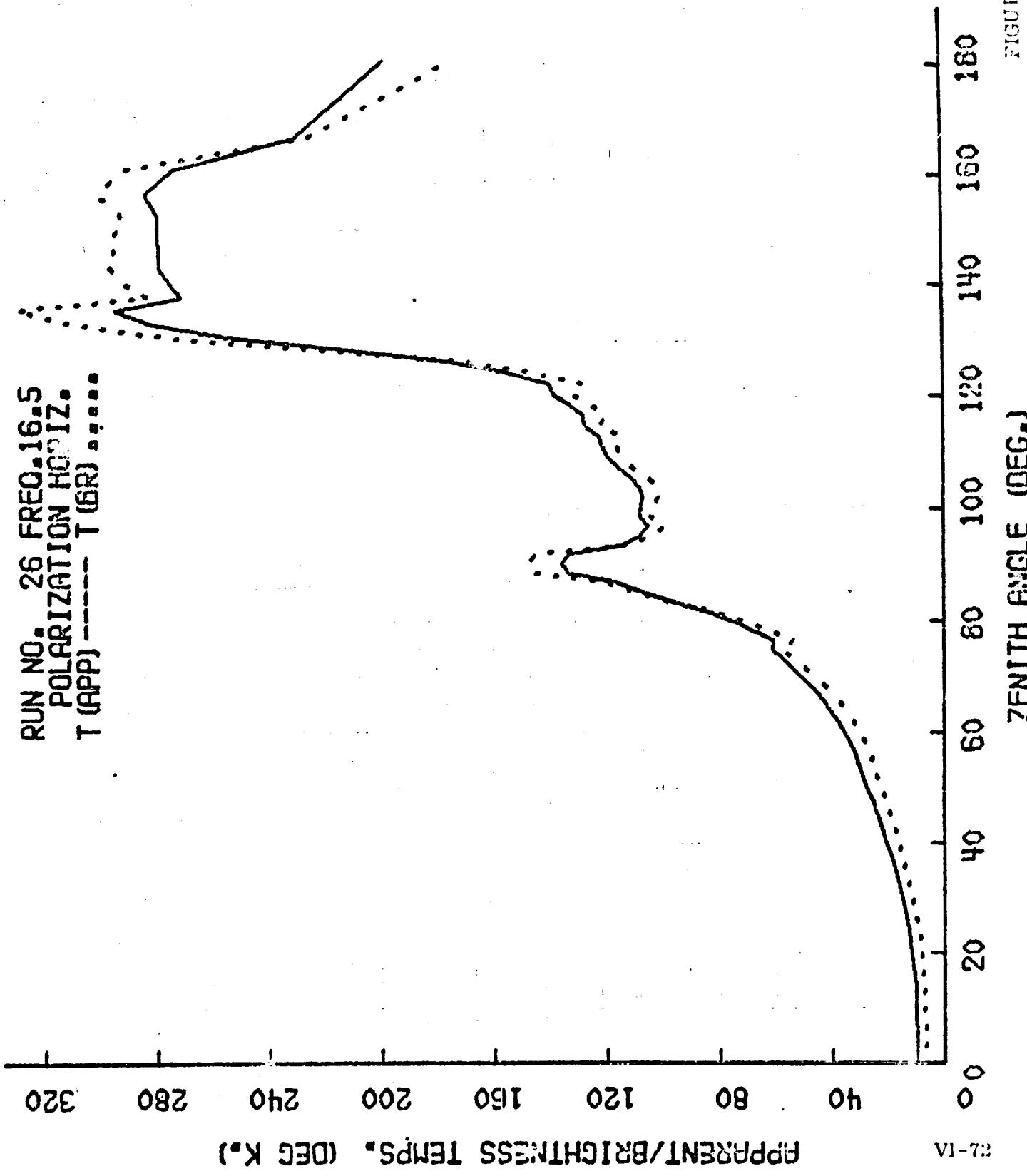


FIGURE VI-24

FIGURE VI-25

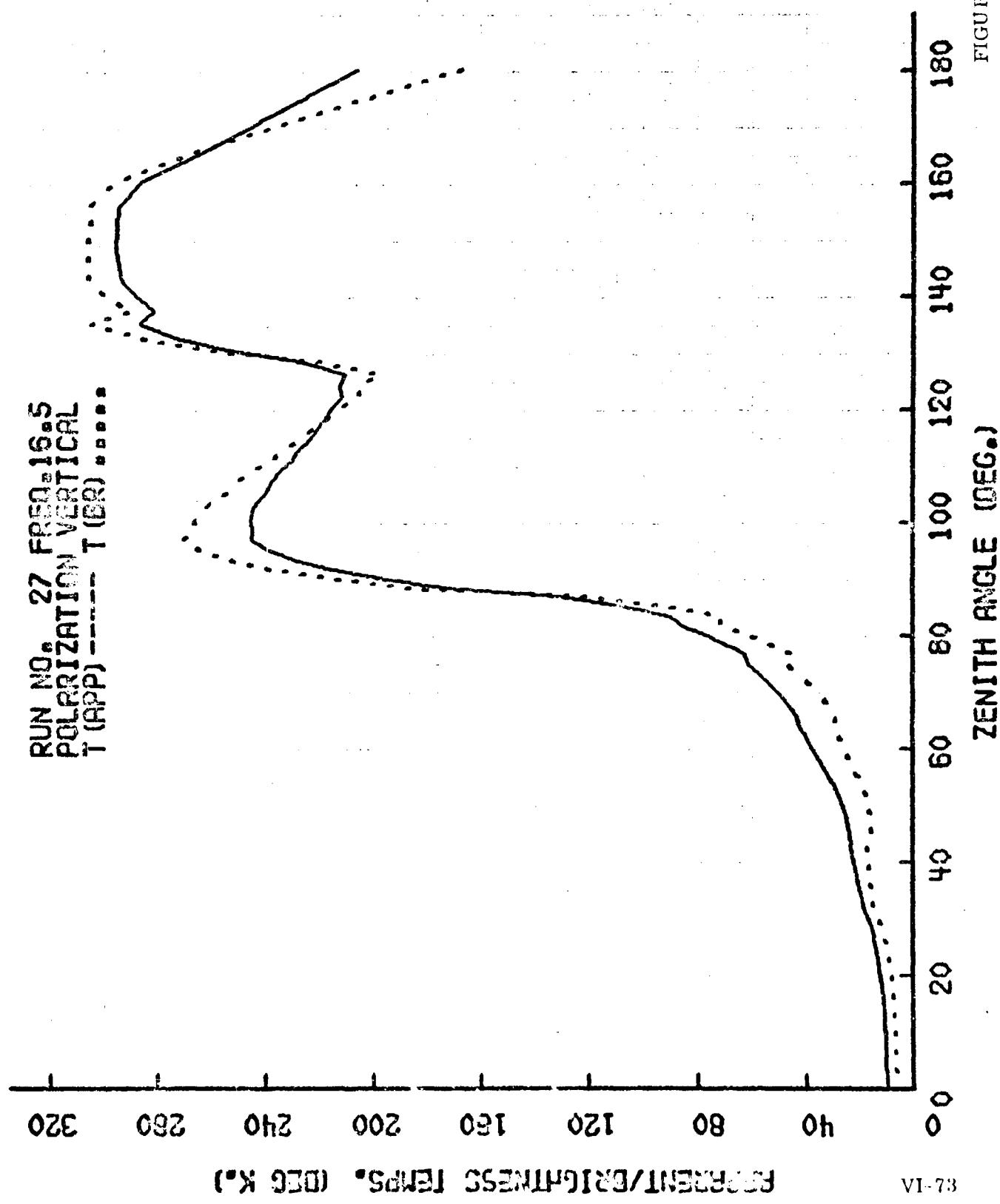
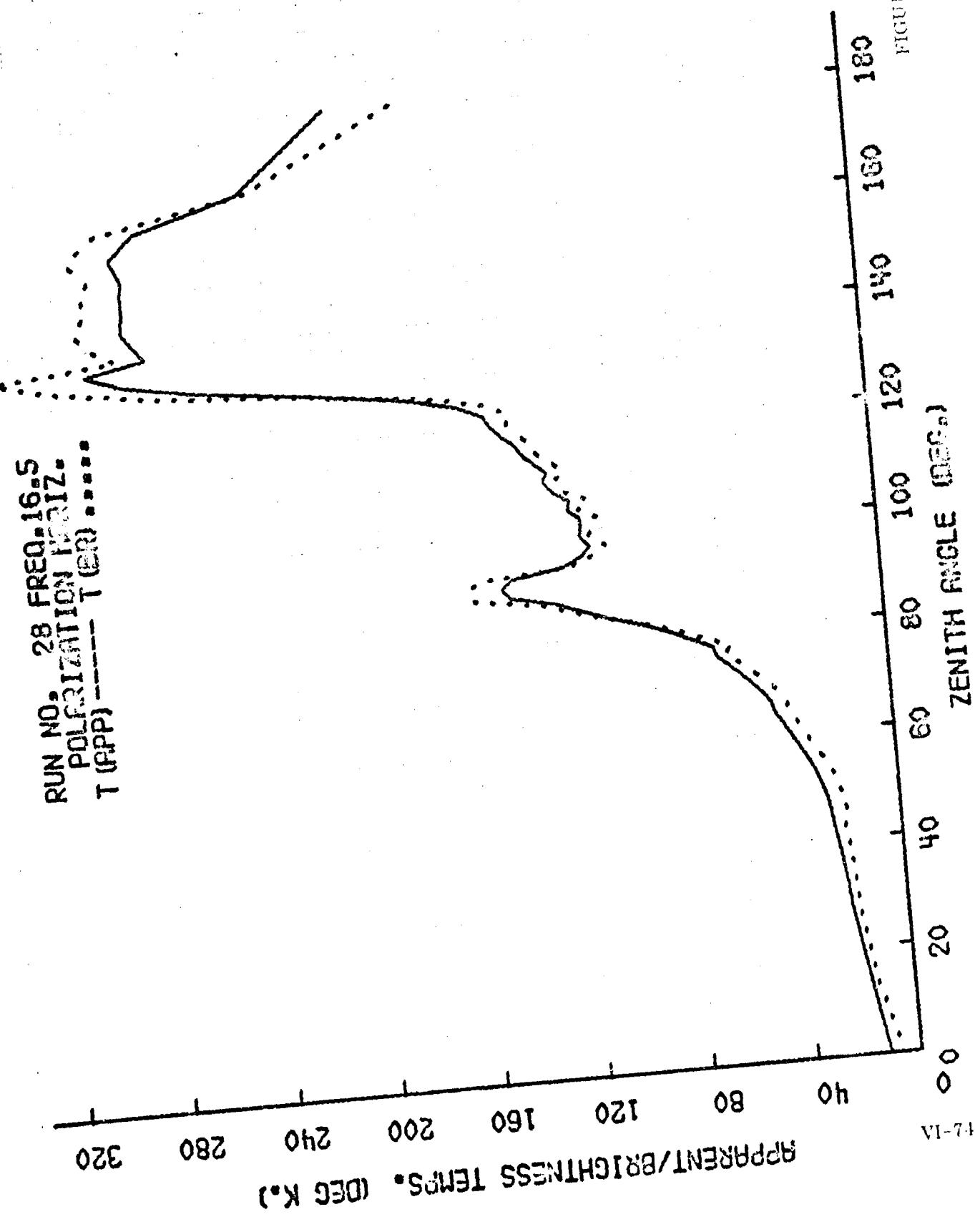


FIGURE VI-26



RUN NO. 29 FREQ. 16.5
POLARIZATION HORIZ.
T (APP) --- T (ER)

APPARENT BRIGHTEST TEMPS. (DEG K.)

40 80 120 160 200 240 280 320

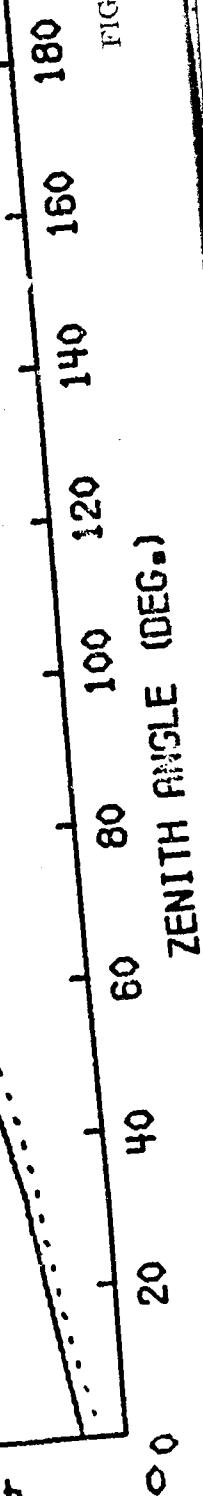


FIGURE VI-27

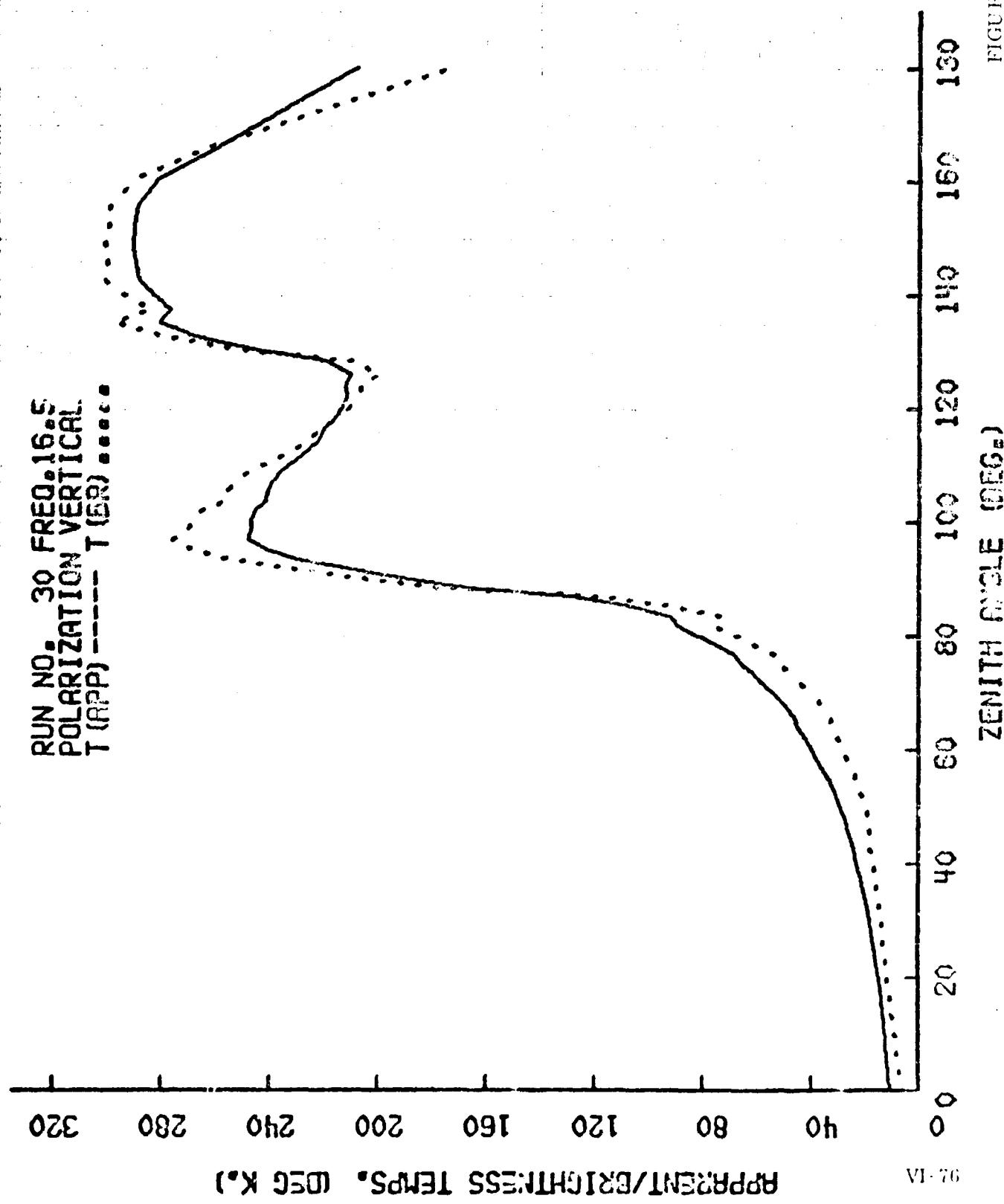
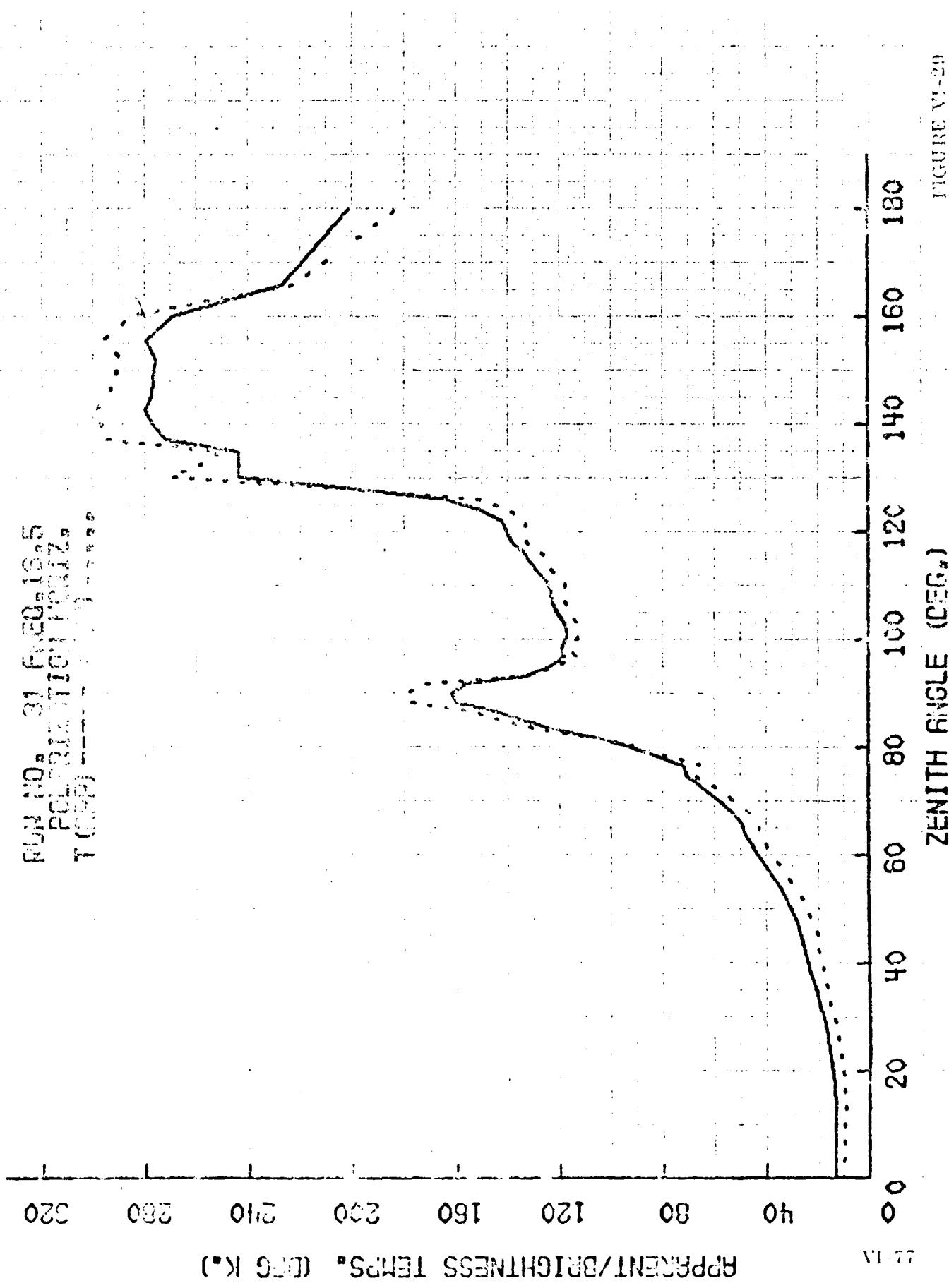


FIGURE VI-28

RUN NO. 31 FREQ 1825
PC 312 TIC 1125
T (deg K) 200 220 240 260



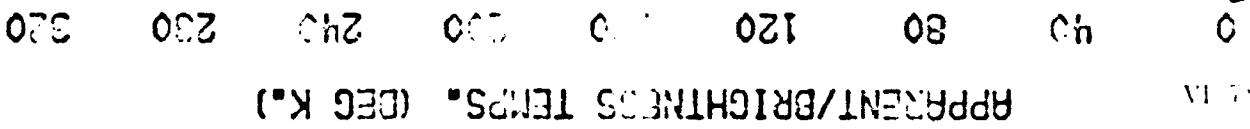
77-11

FIGURE VI-29

FIGURE VI-3d

IDENTICAL CYCLE (0.0°C)

RUN NO. 22 FREQ. 1655
POLARIZAT. VERTICAL
 $T_{GAPP} = T_{(88)}$ sec.



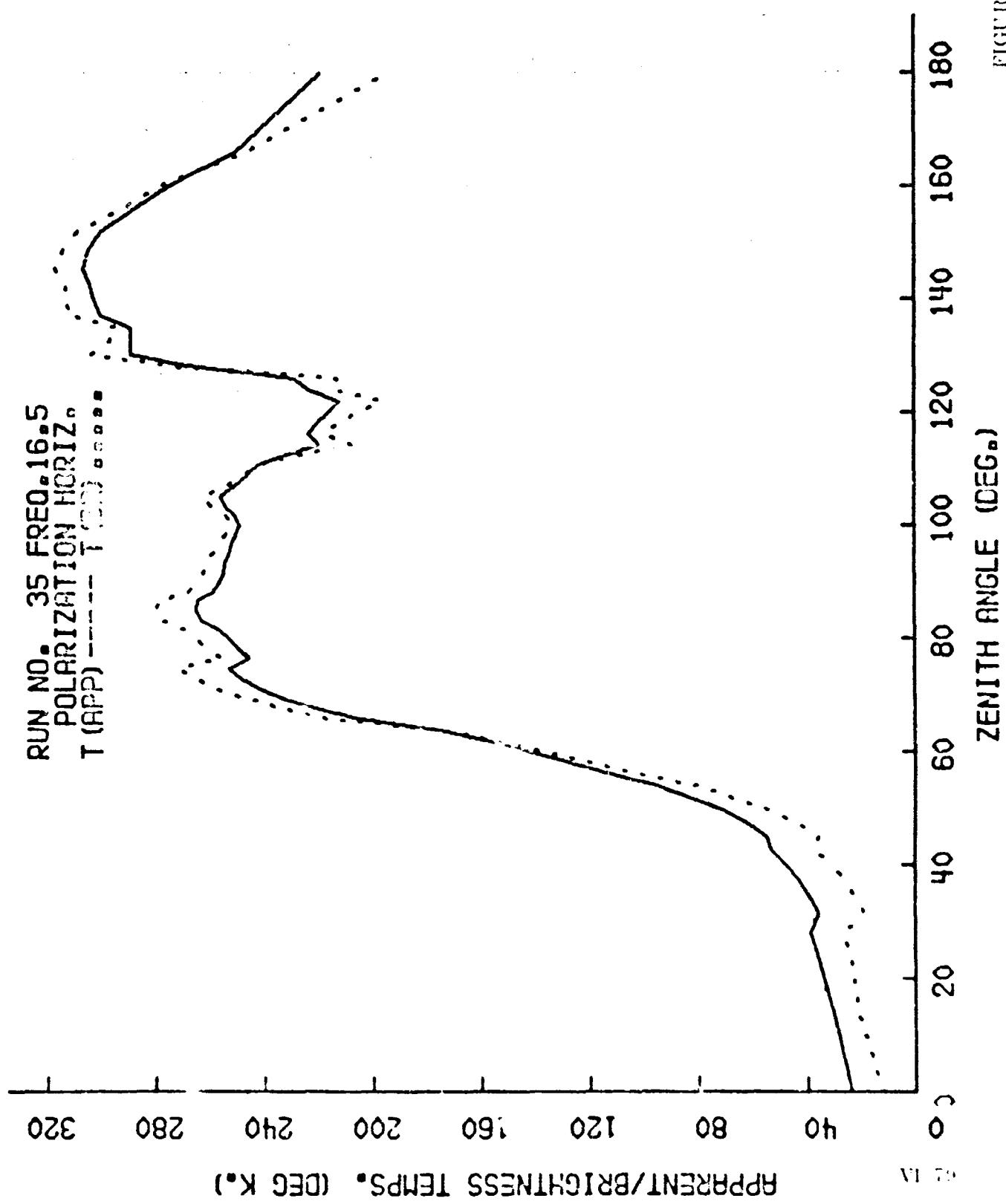
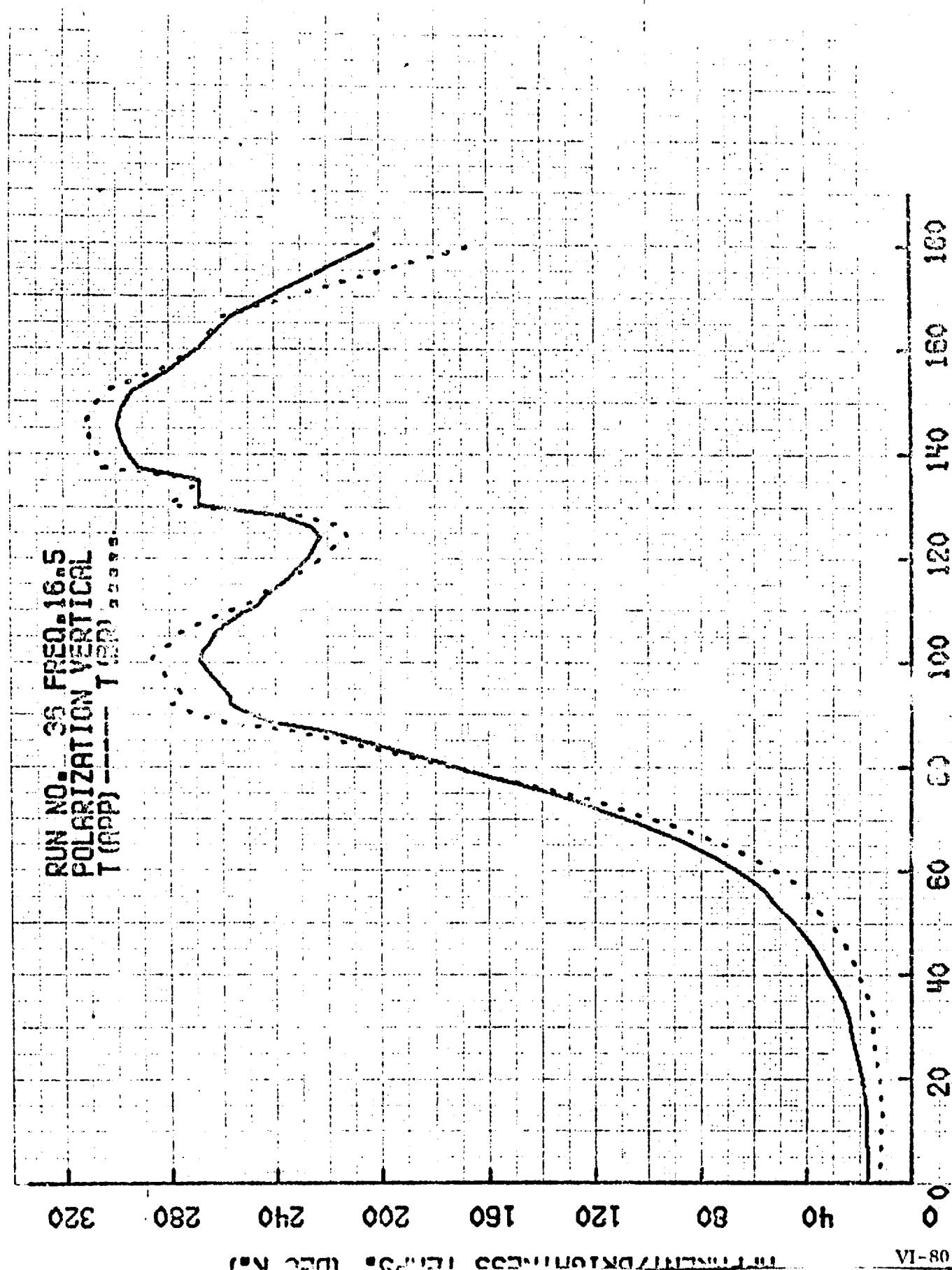


FIGURE VI-31

FIGURE VI-32

ZENITH ANGLE (DEG.)



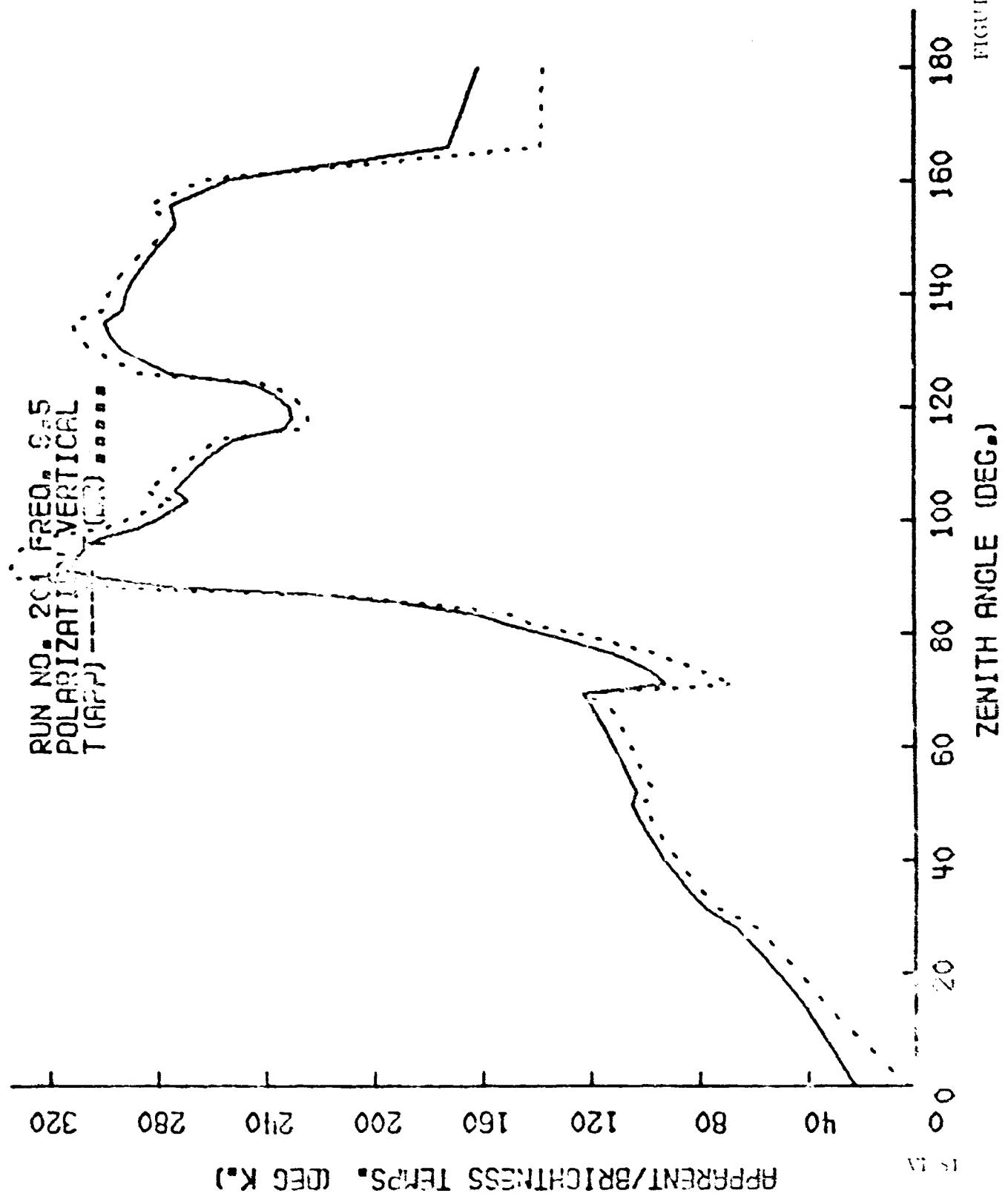


FIGURE VI-33

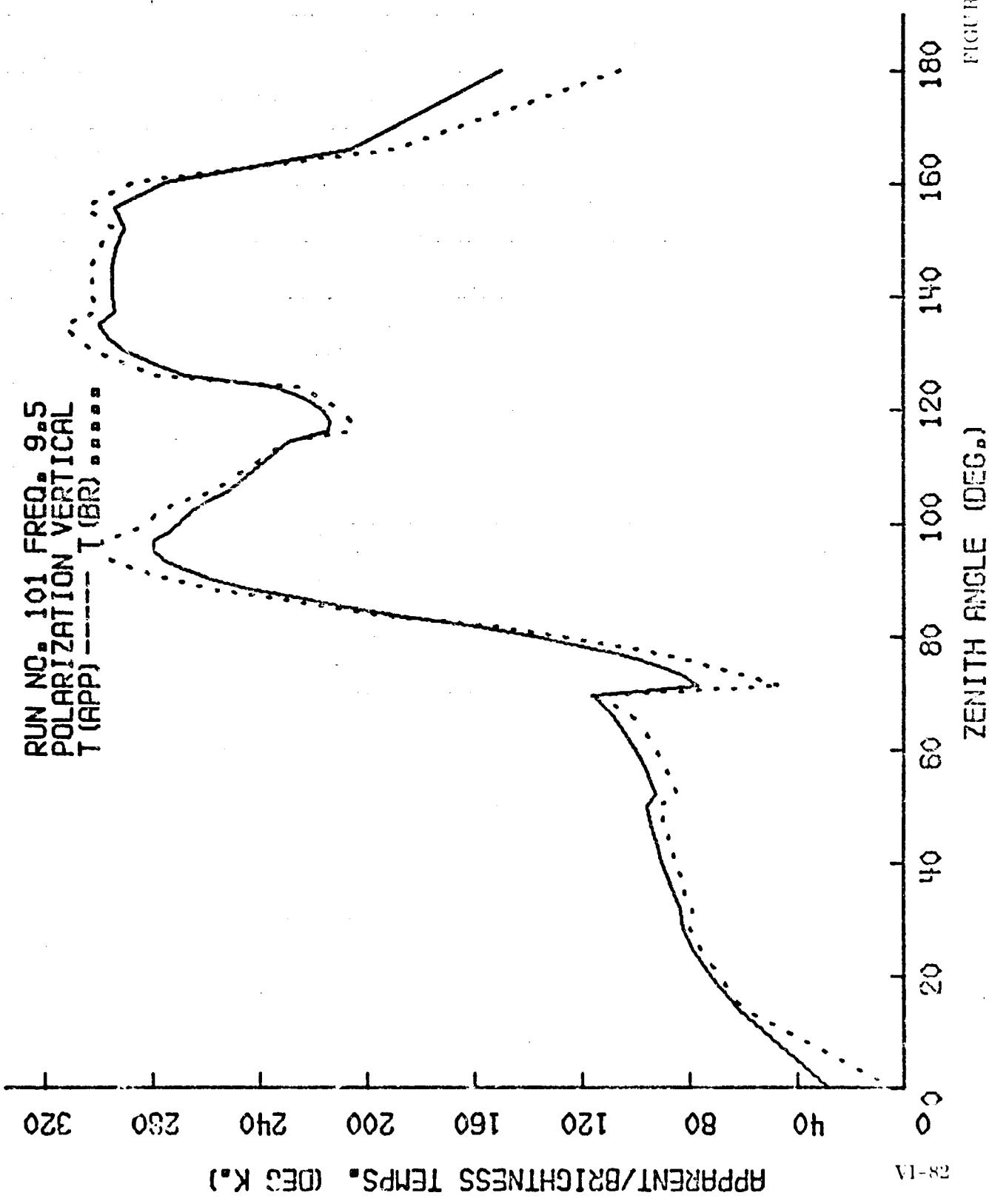


FIGURE VI-34

FIGURE VI-35

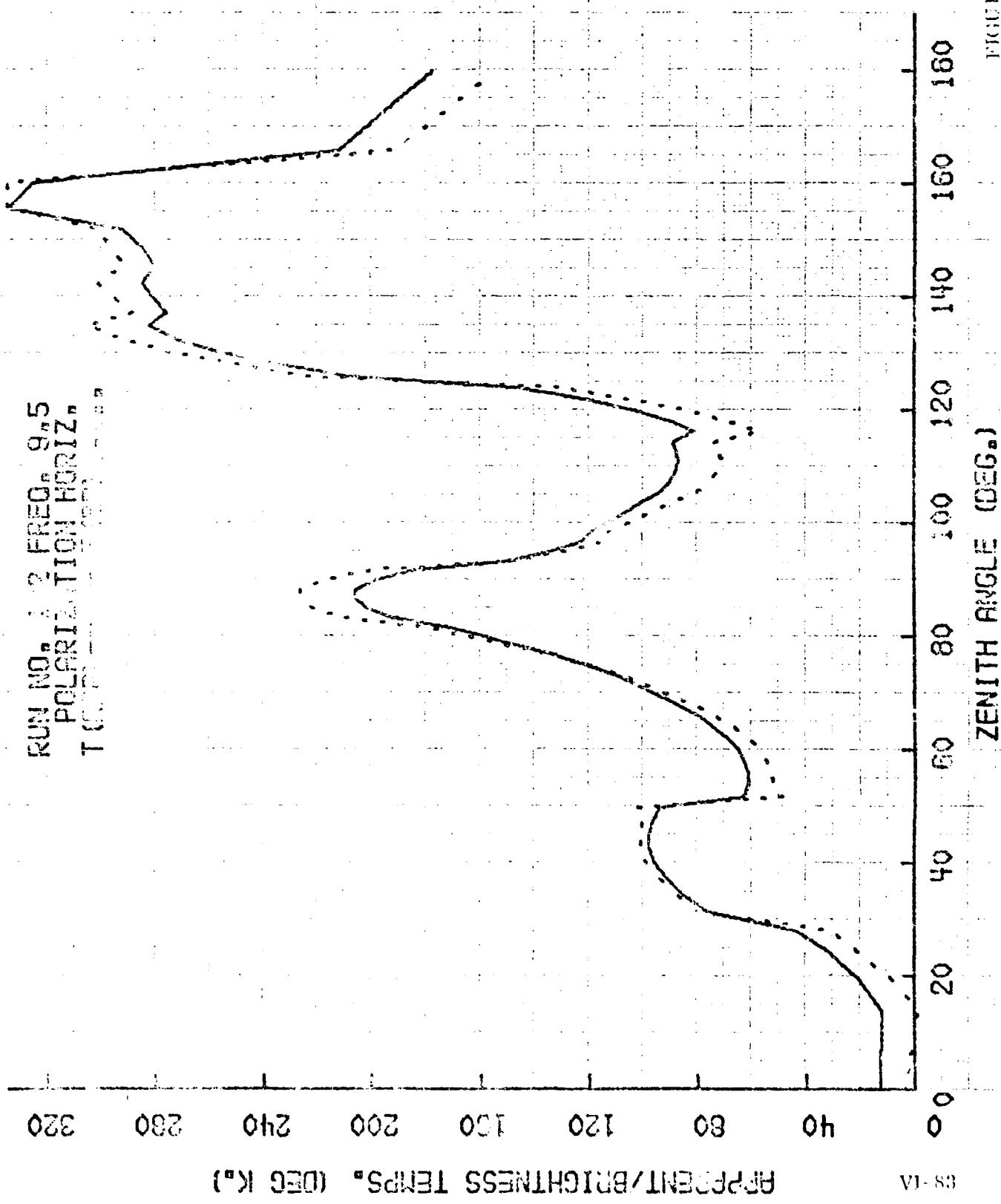
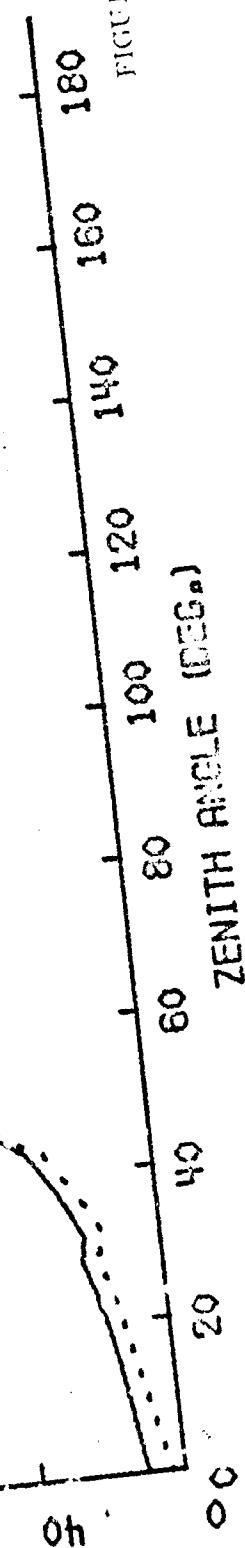
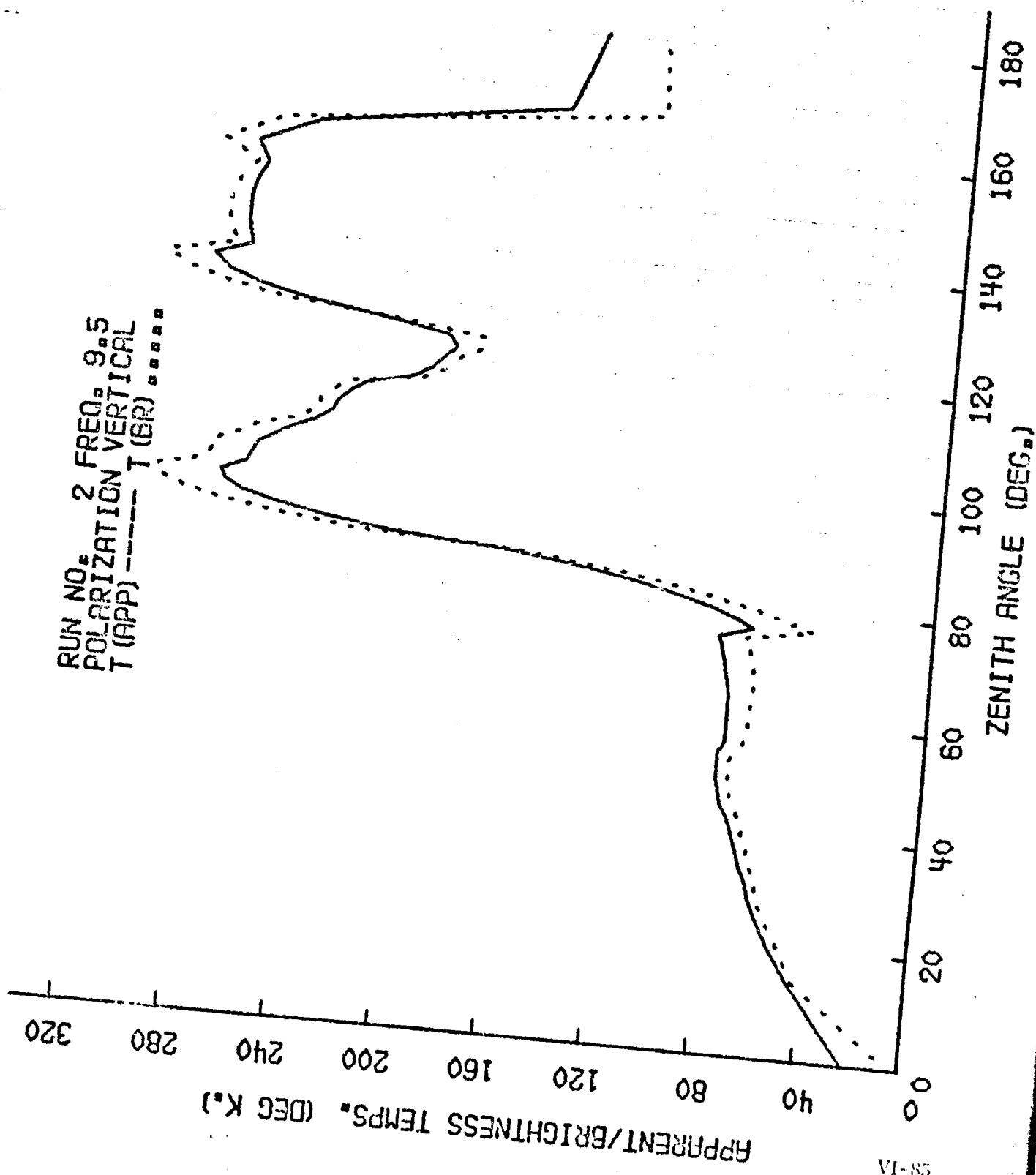


FIGURE VI-36



RUN NO. 1 FREQ. 9.5
POLARIZATION HORIZ.
T (APP)

VI-36



VI-85

FIGURE VI-37

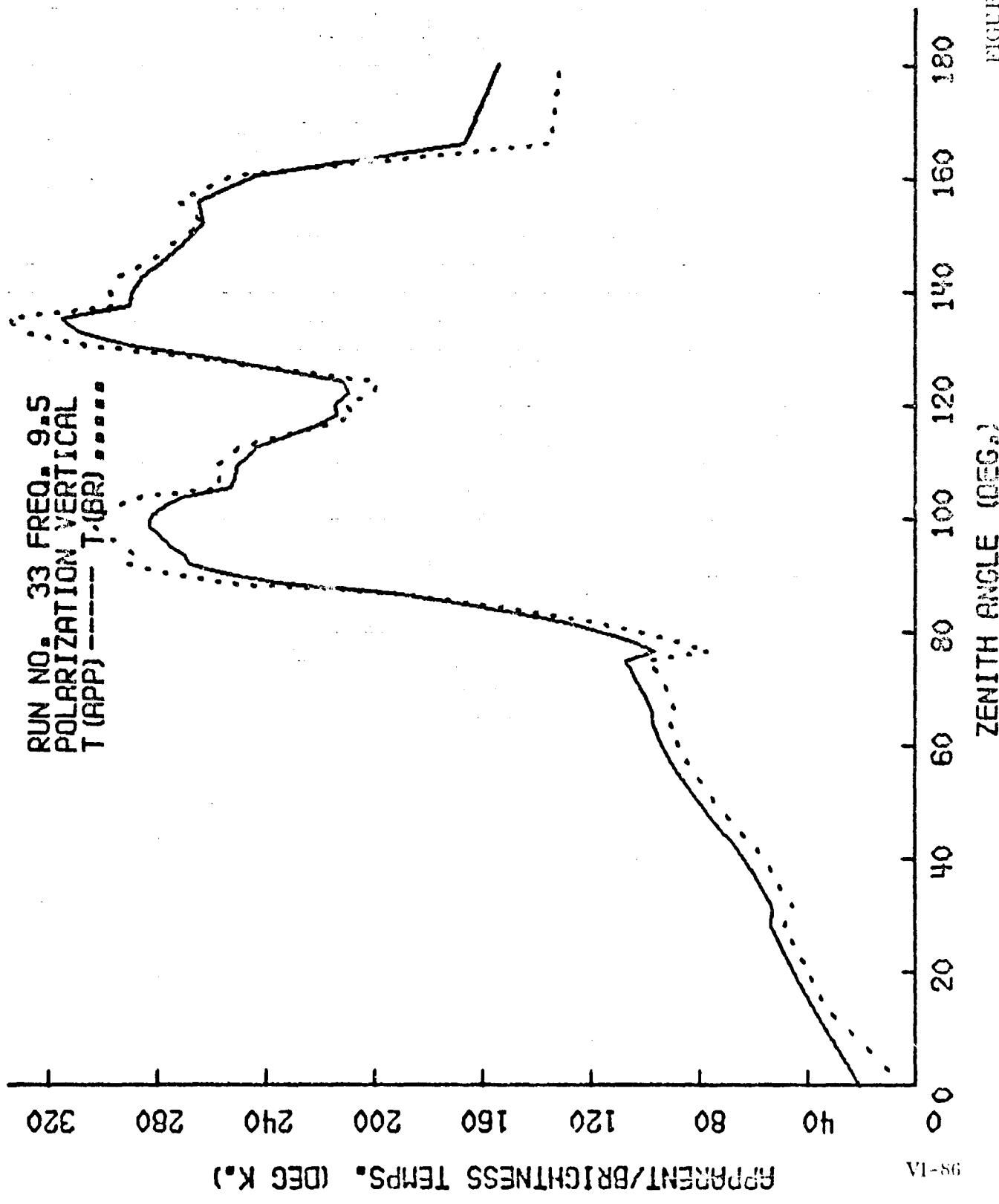
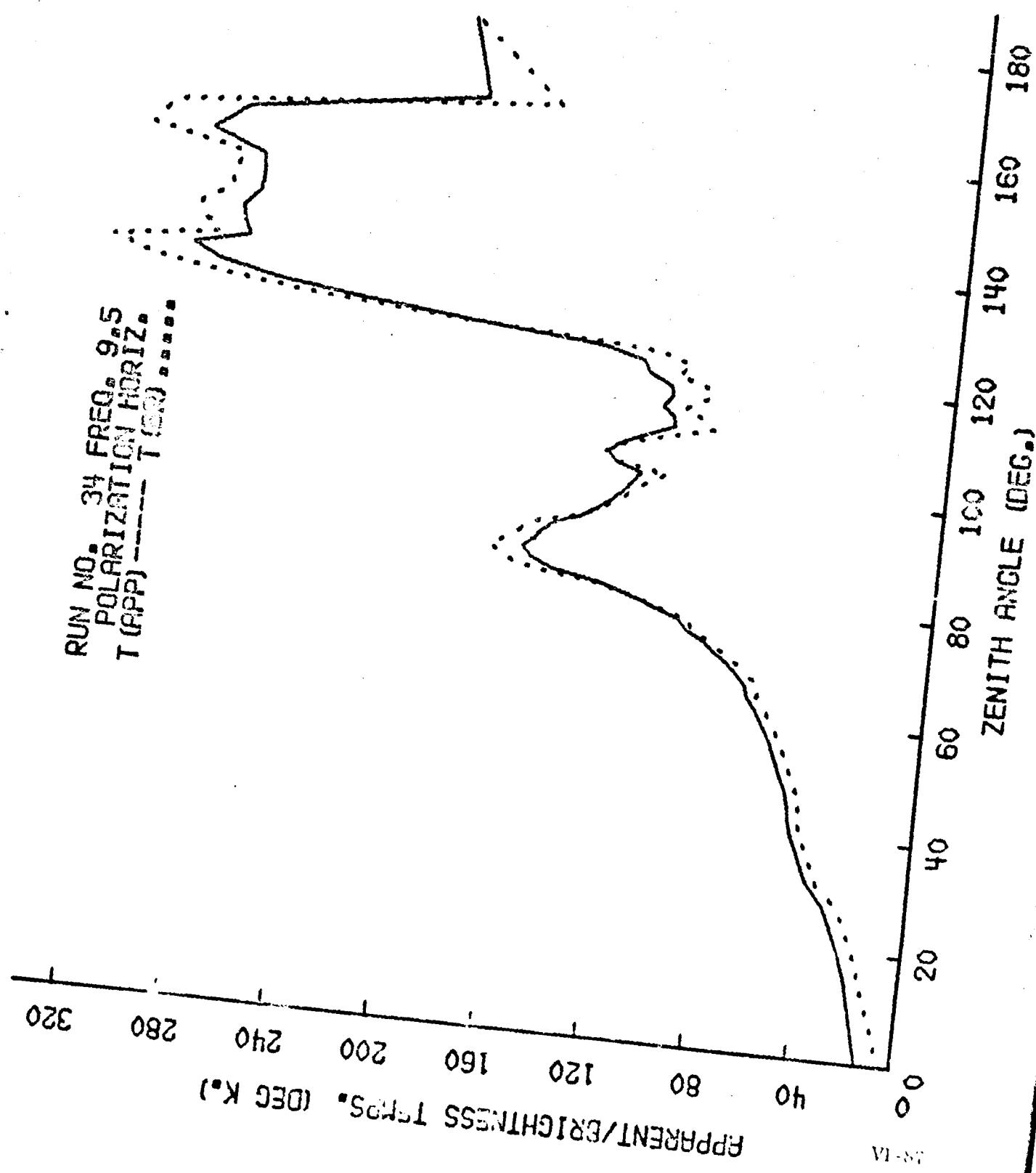


FIGURE VI-38

FIGURE VI-39



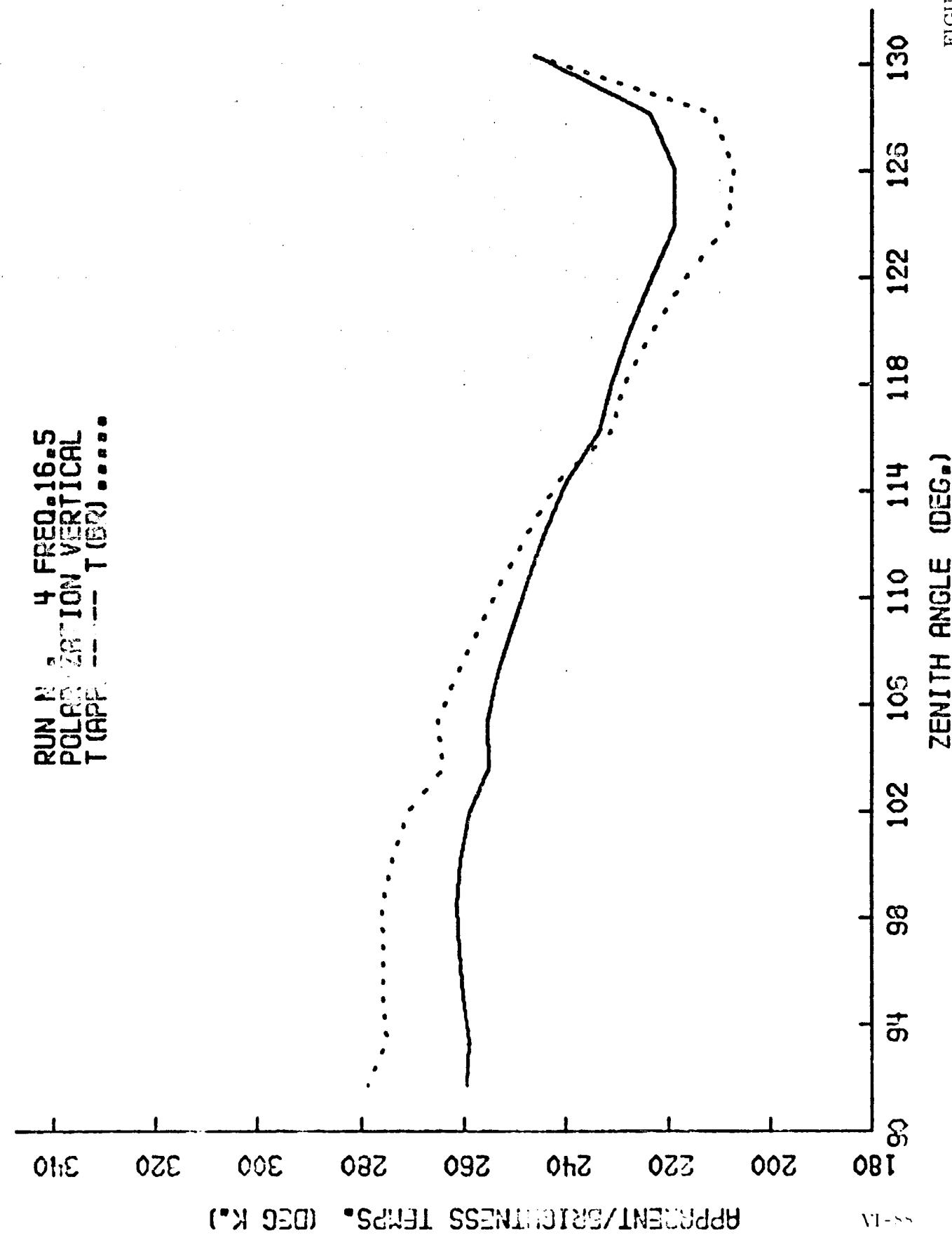


FIGURE VI-10

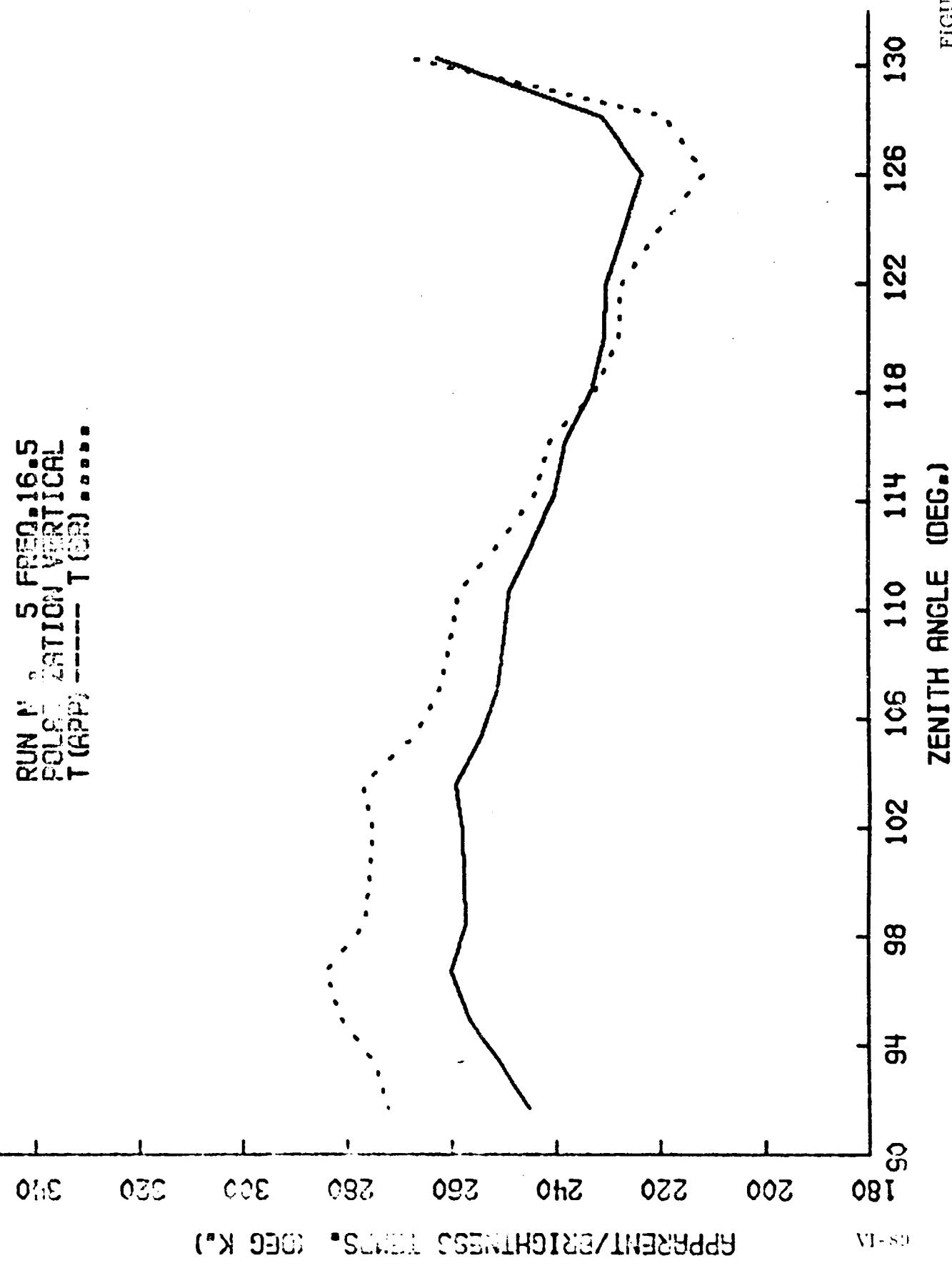


FIGURE VI-41

RUN NO. 6 FREQ. 16.5
POLARIZATION HORIZ.
T (APP) - - - T (BR) ····

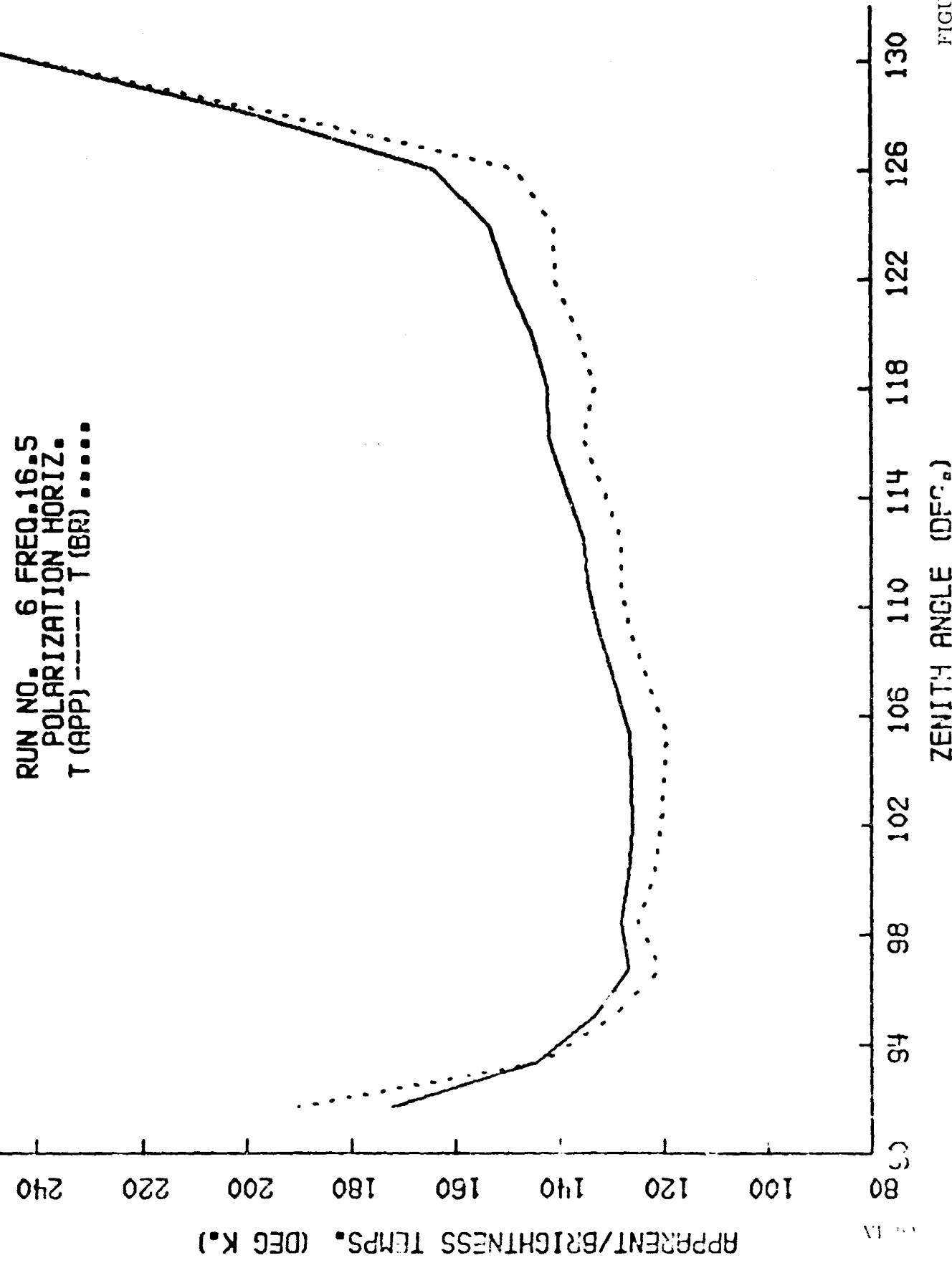
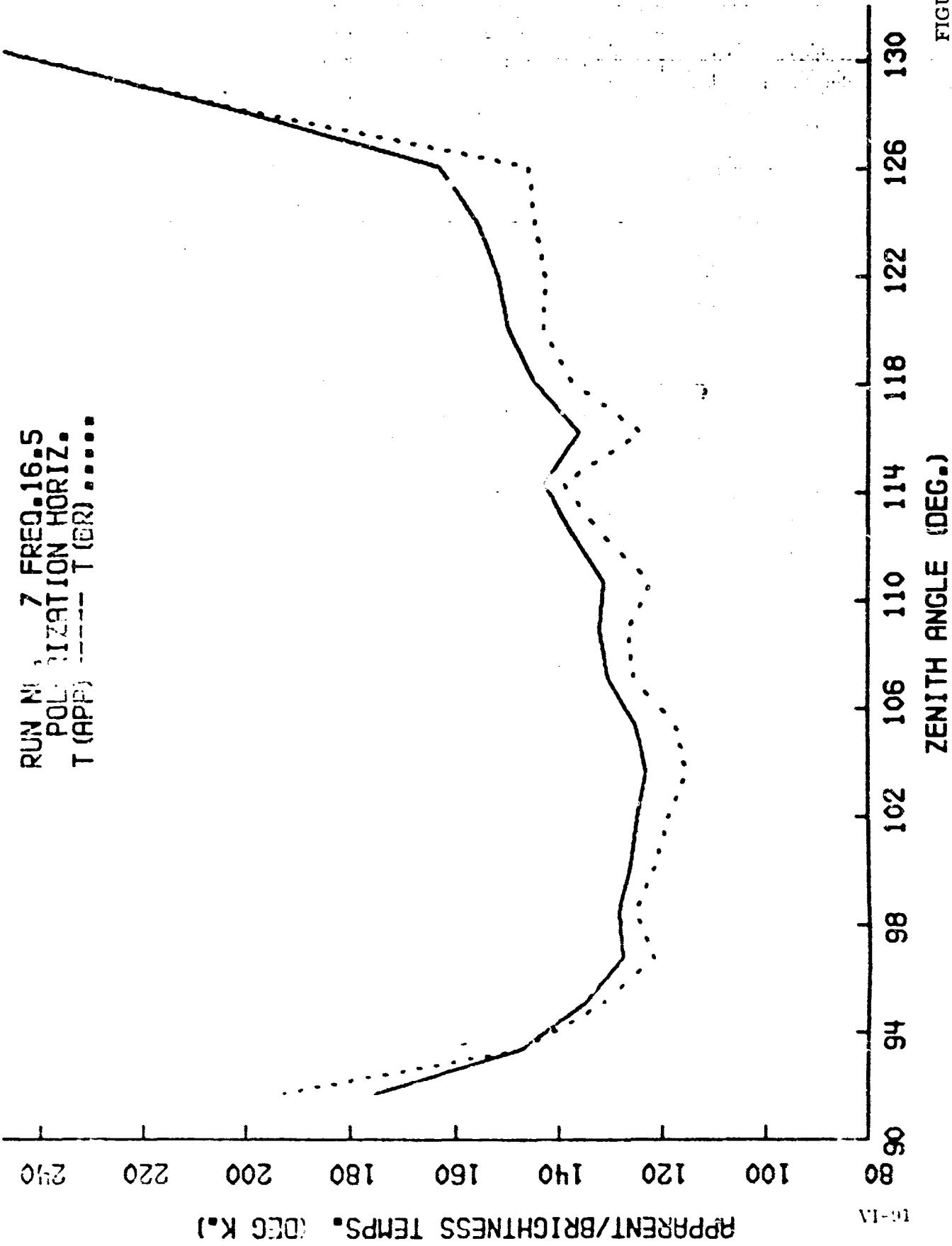


FIGURE VI-42



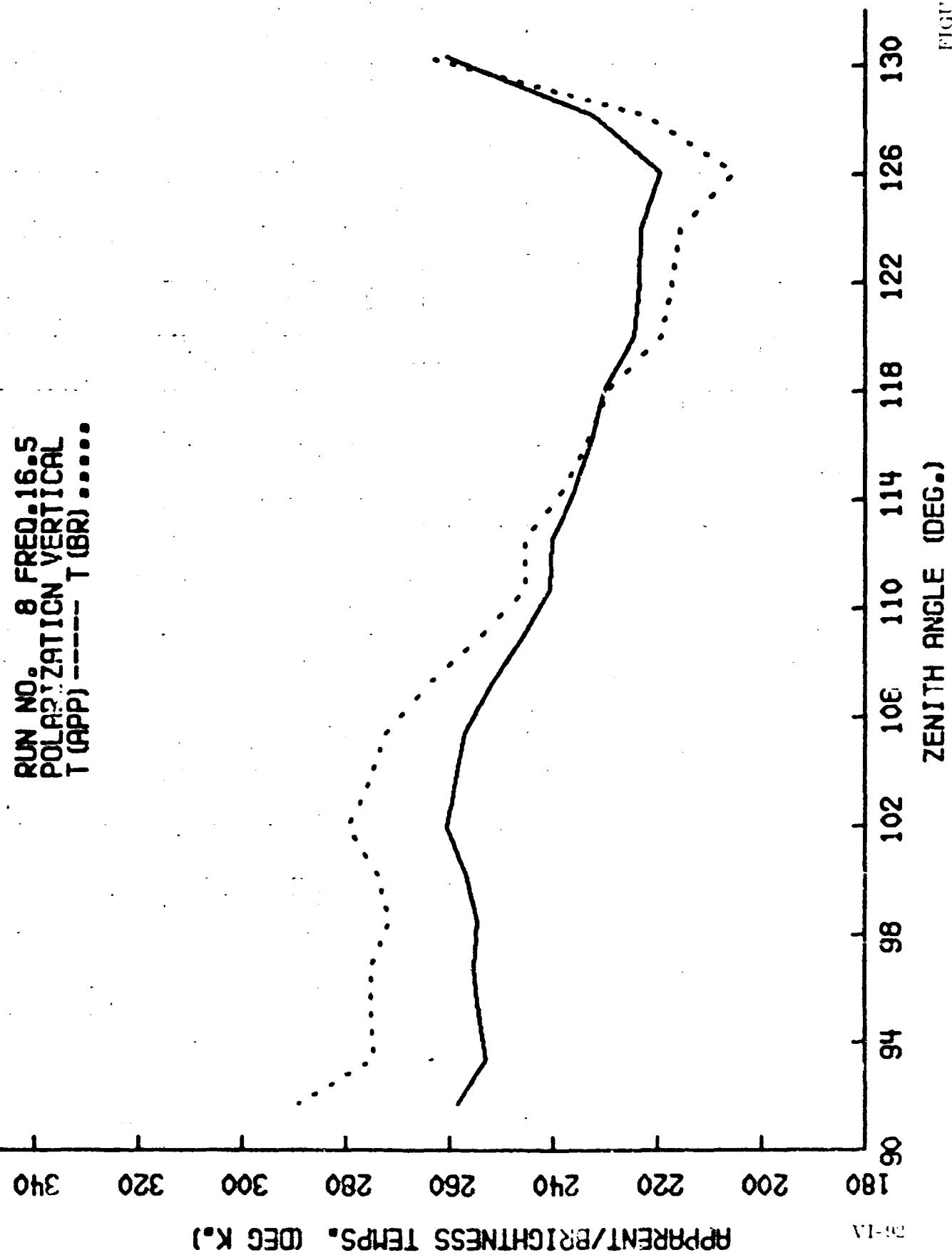


FIGURE VI-45

RUN NO. 9 FREQ. 16.5
POLARIZATION VERTICAL
T_(APP) ----- T_(BR)

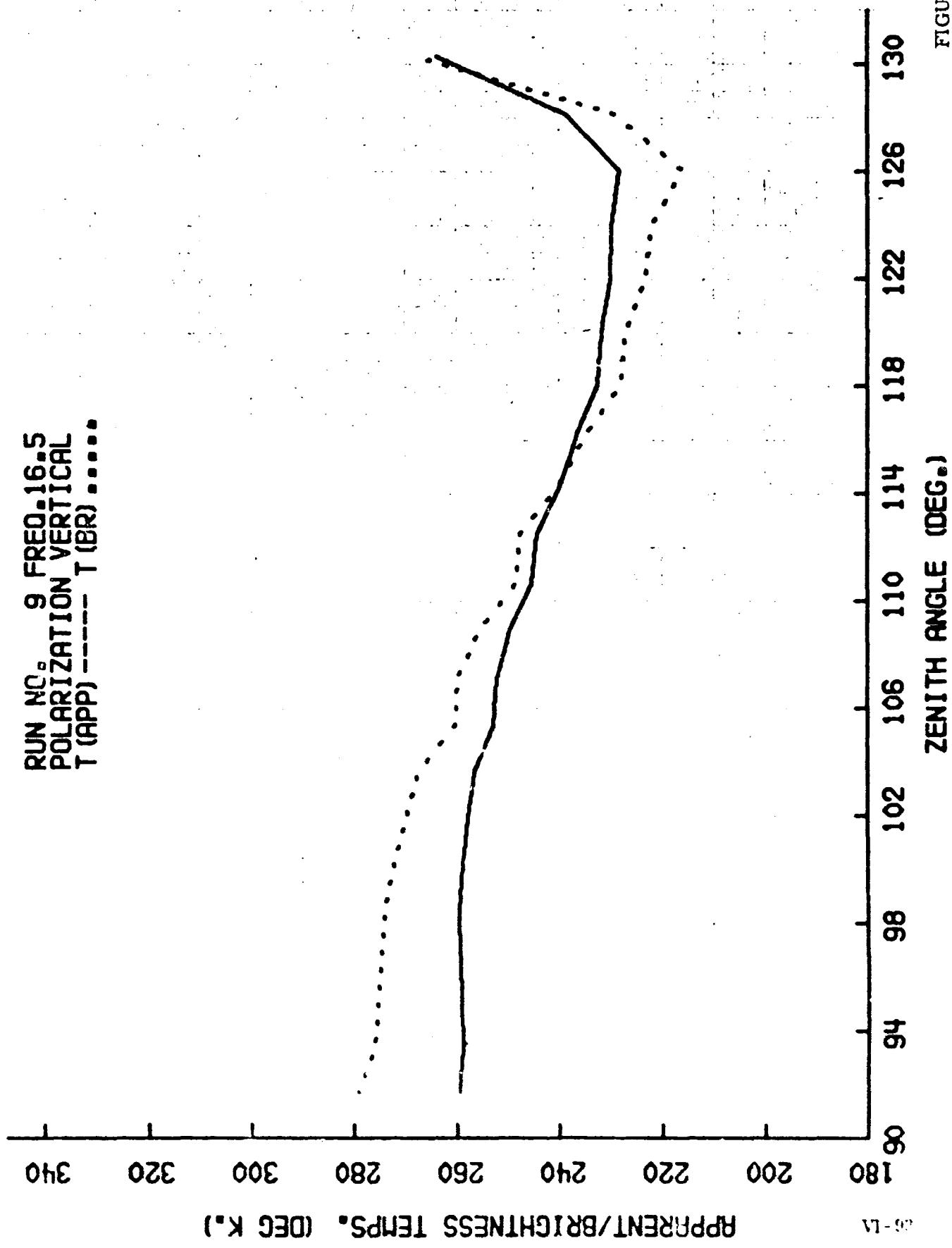


FIGURE VI-46

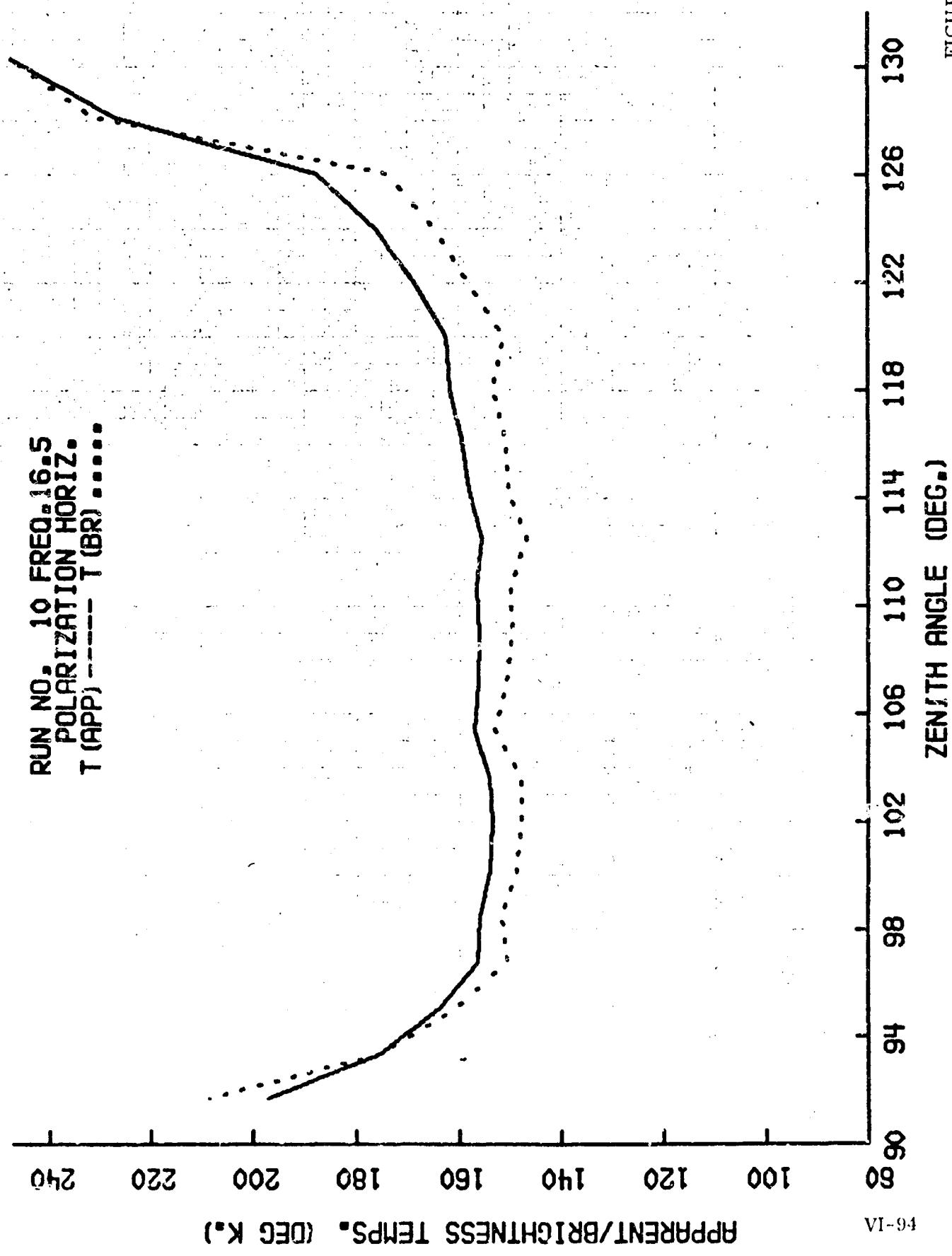


FIGURE VI-47

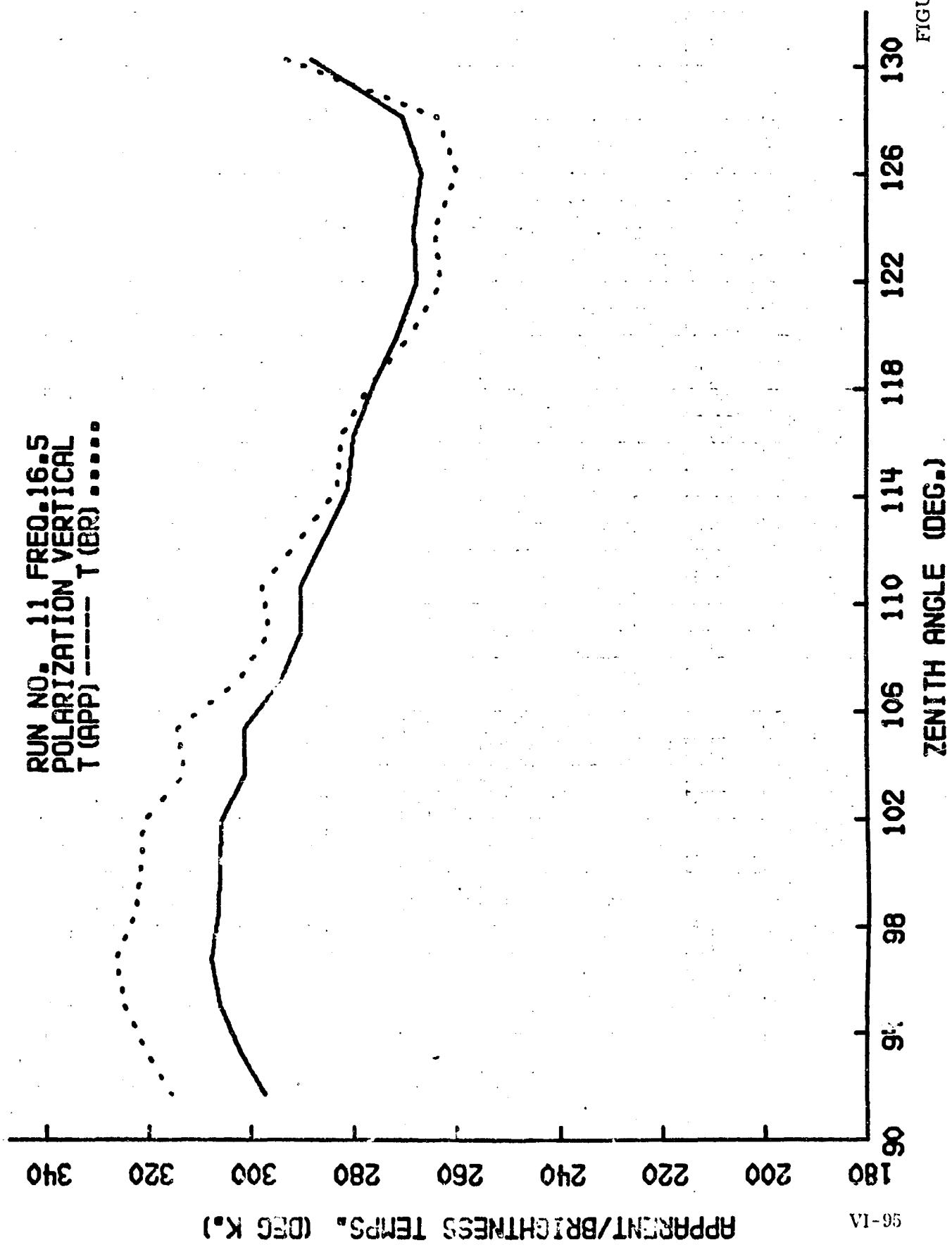
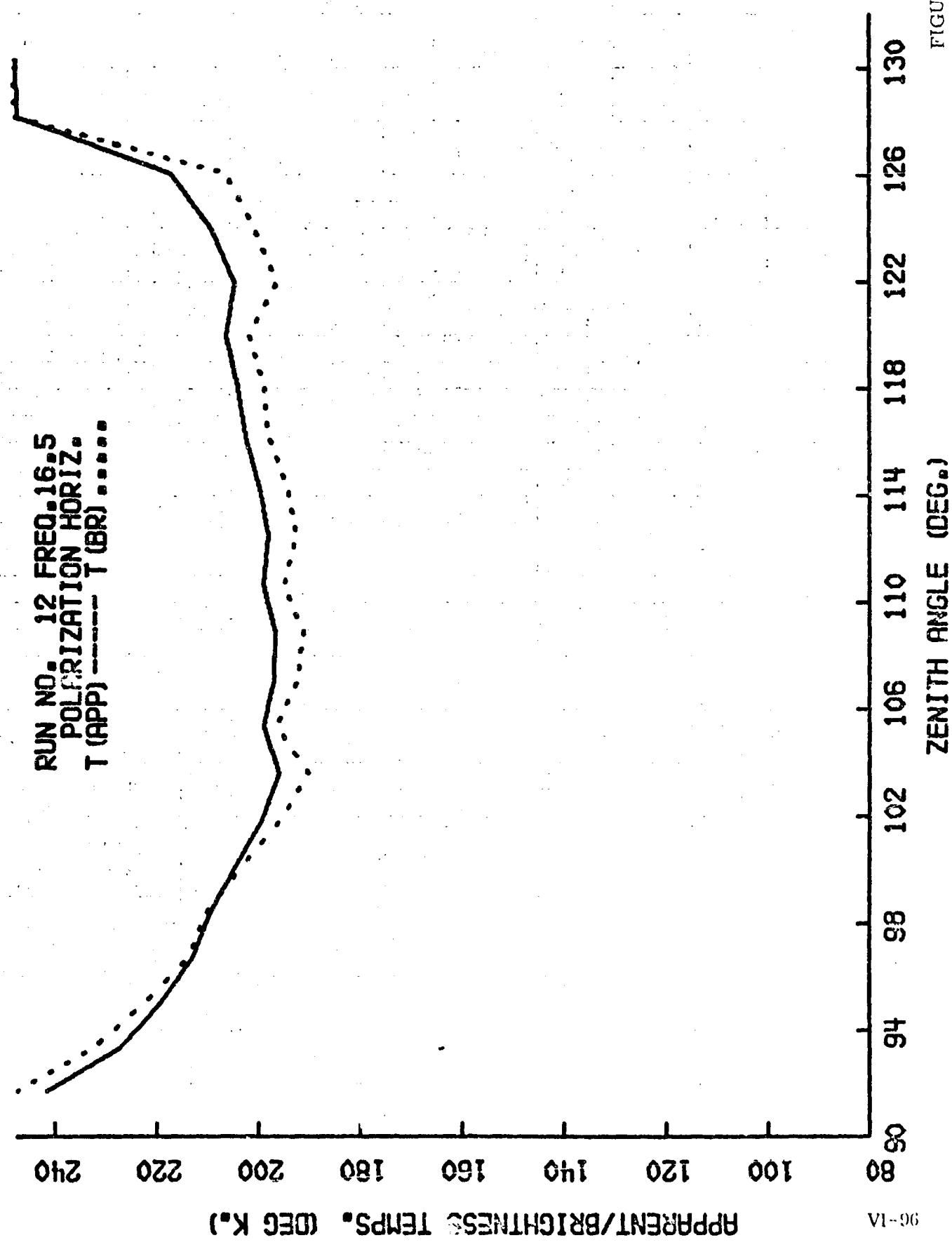
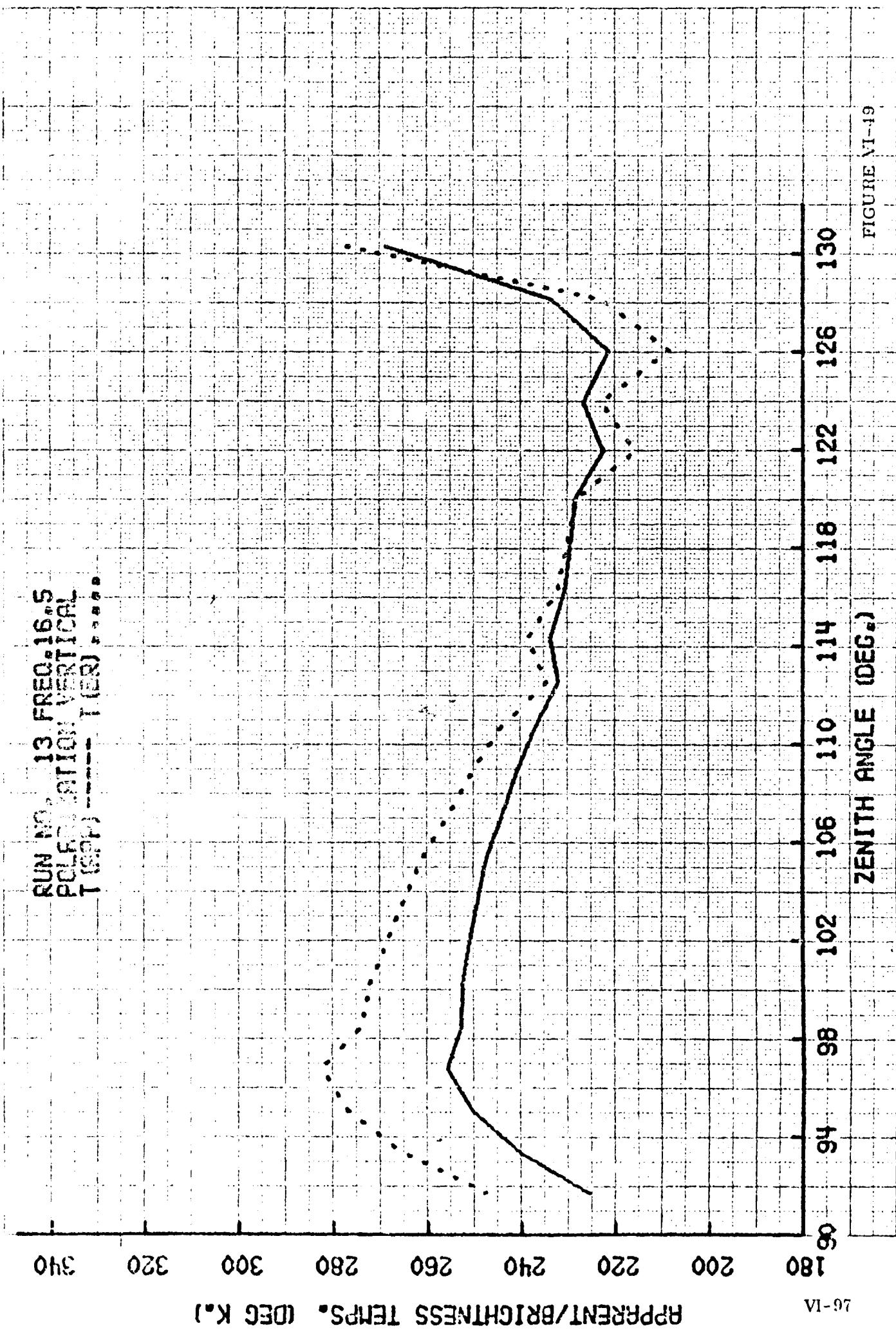


FIGURE VI-48





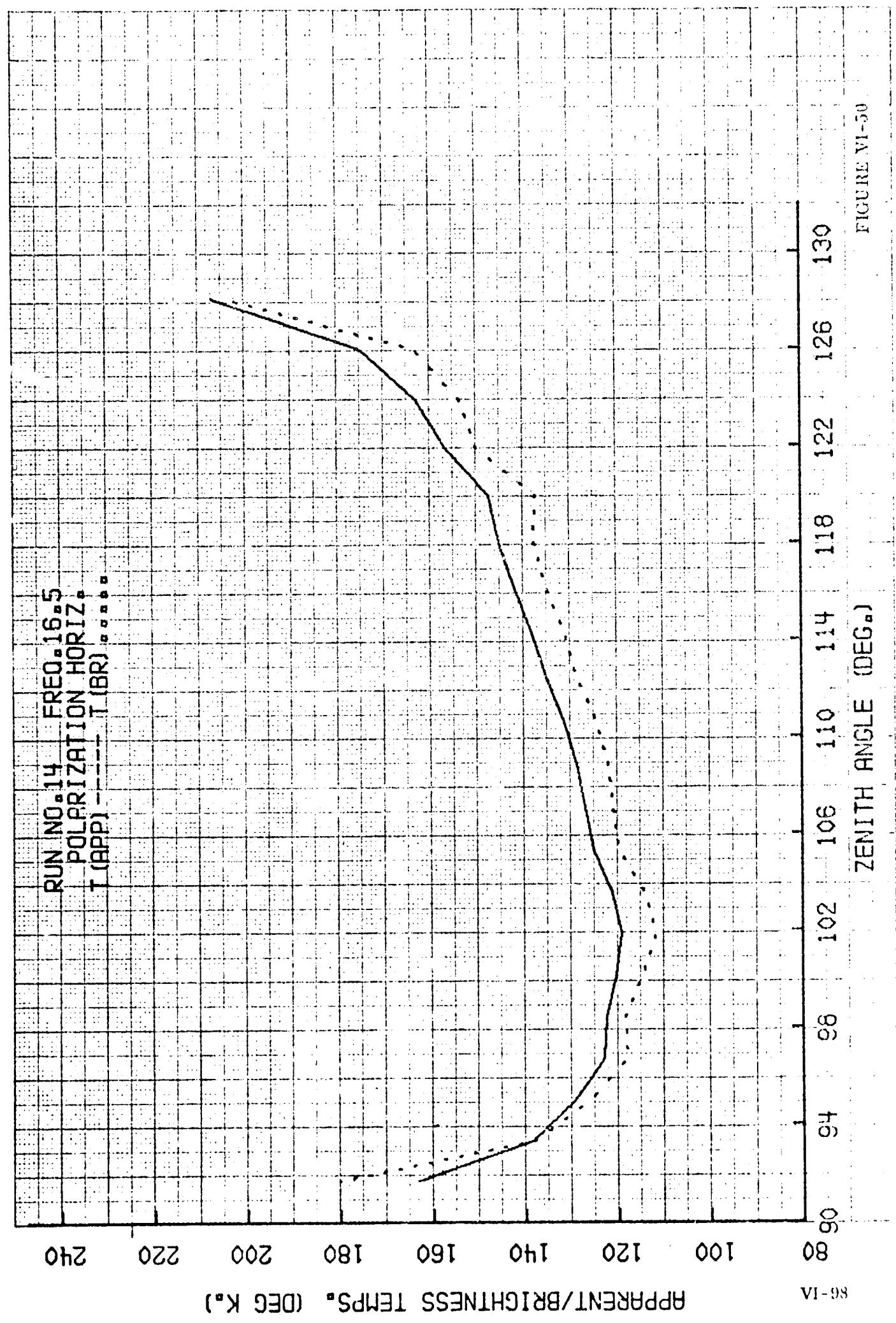
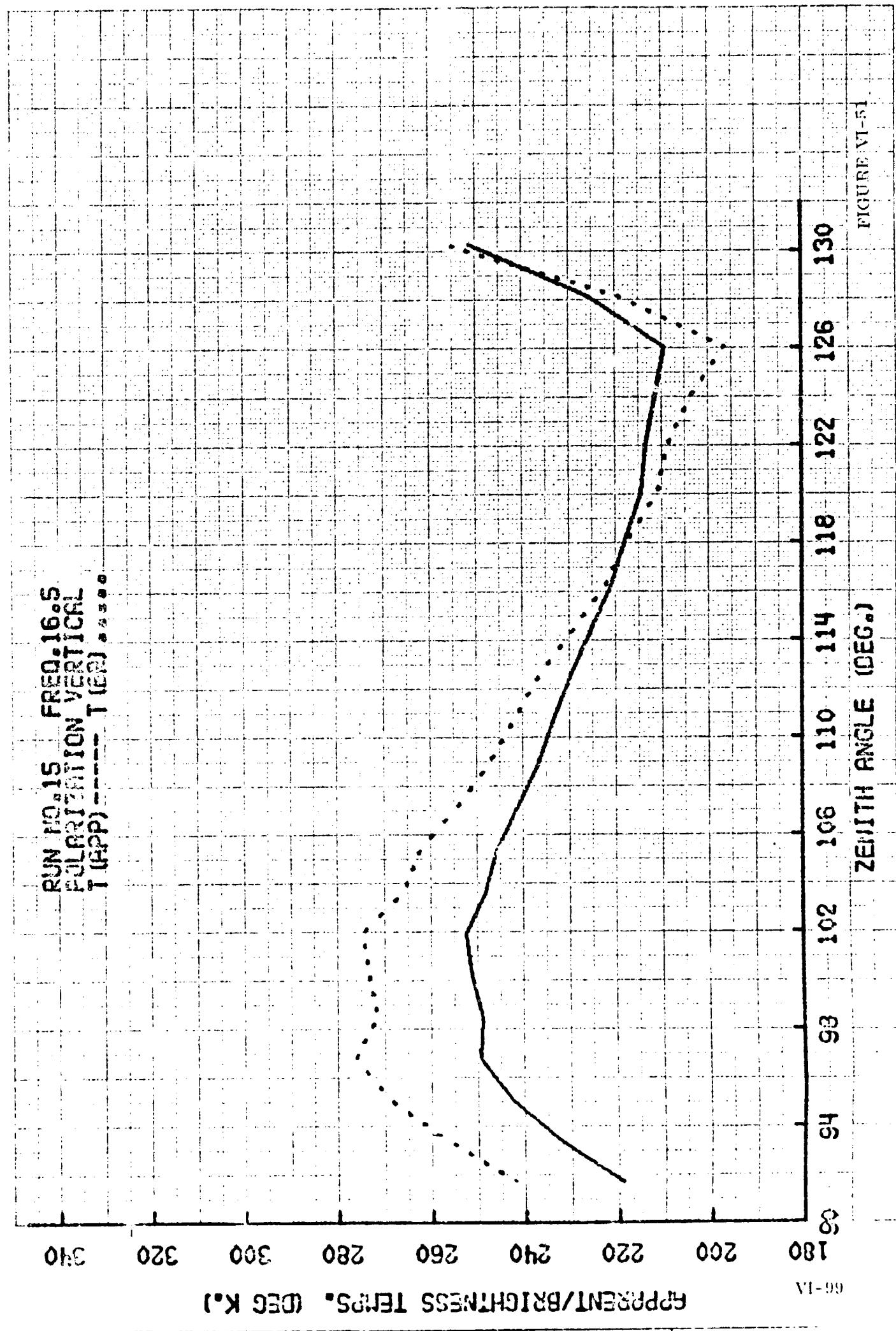


FIGURE VI-59



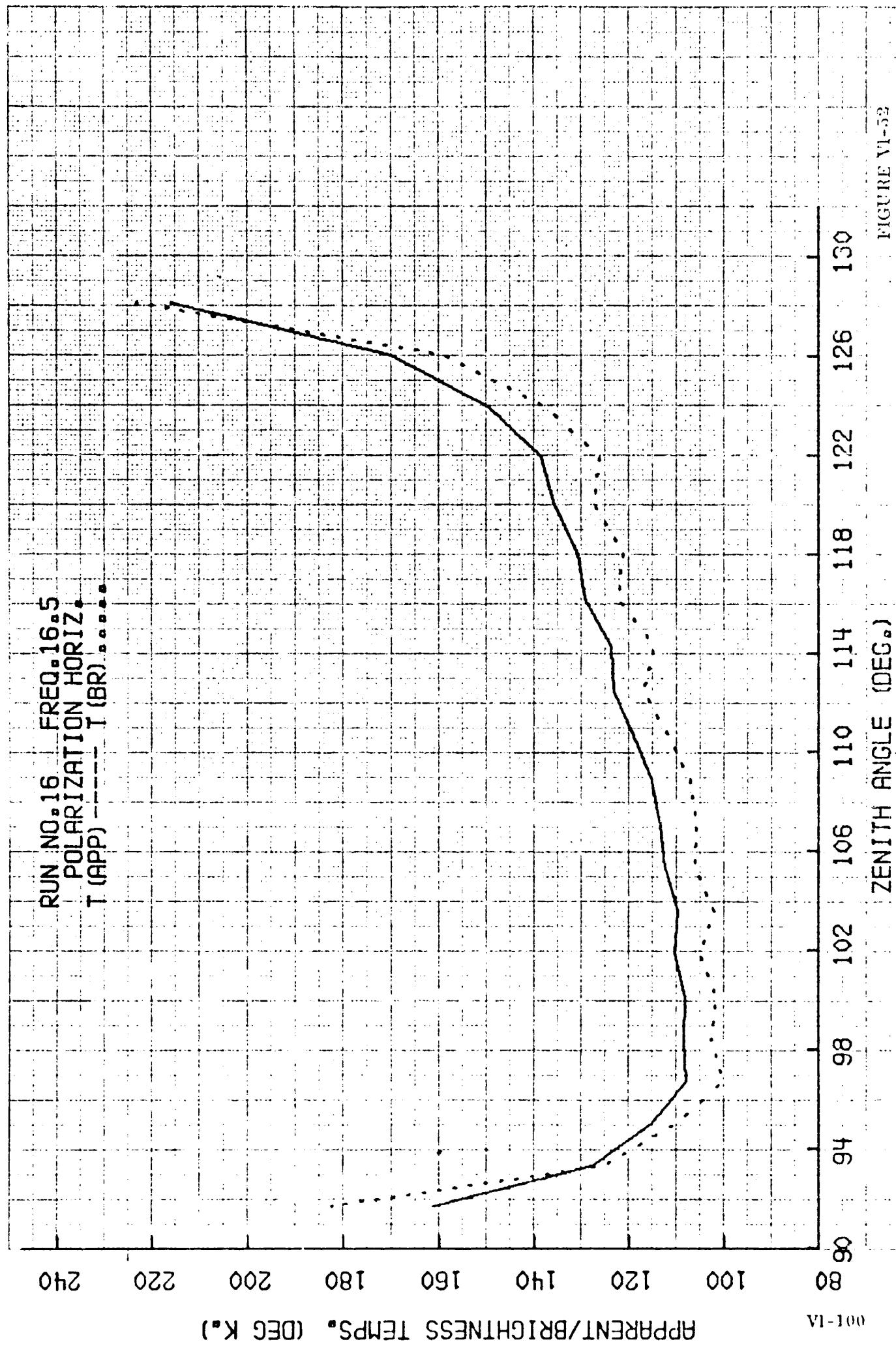


FIGURE VI-52

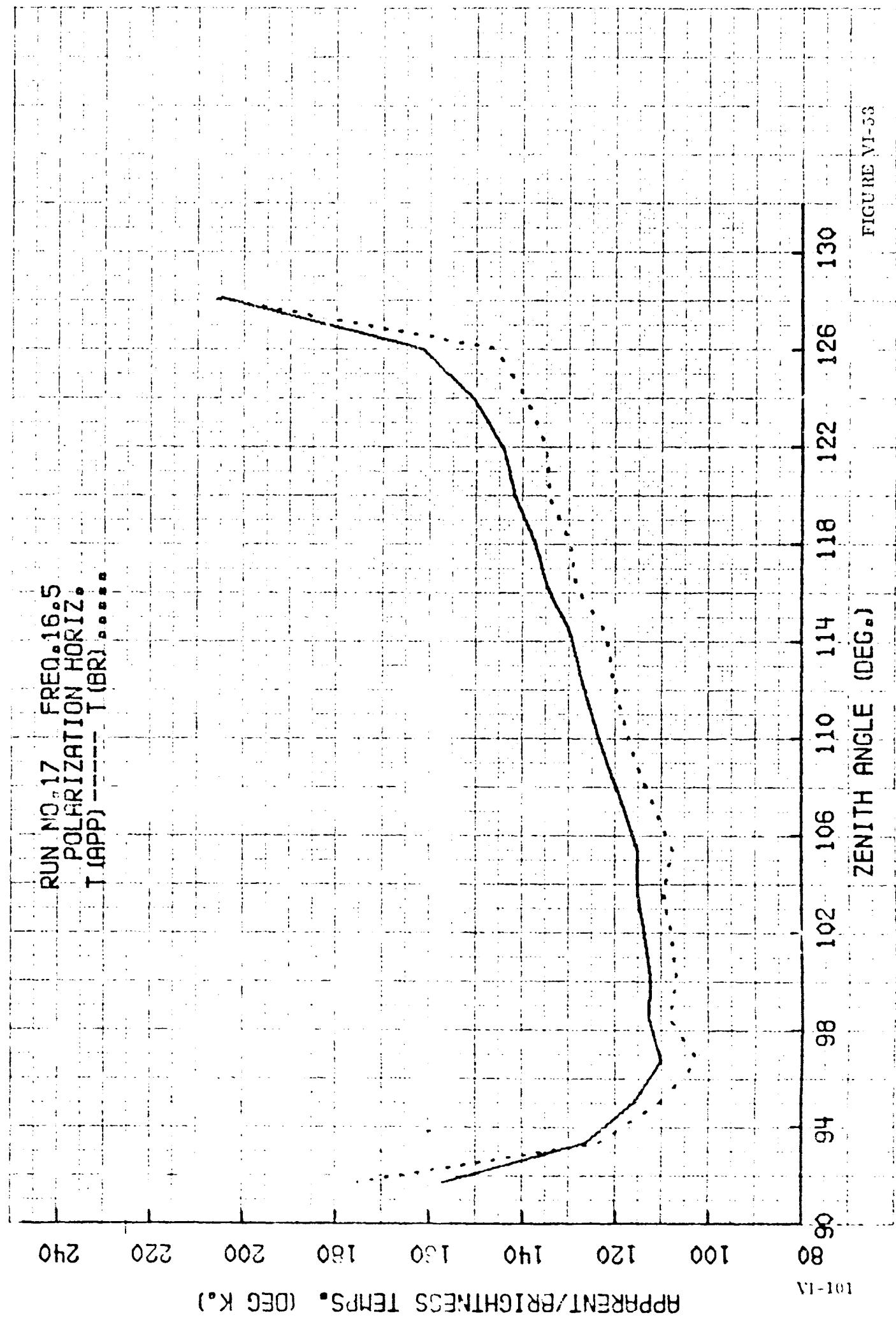
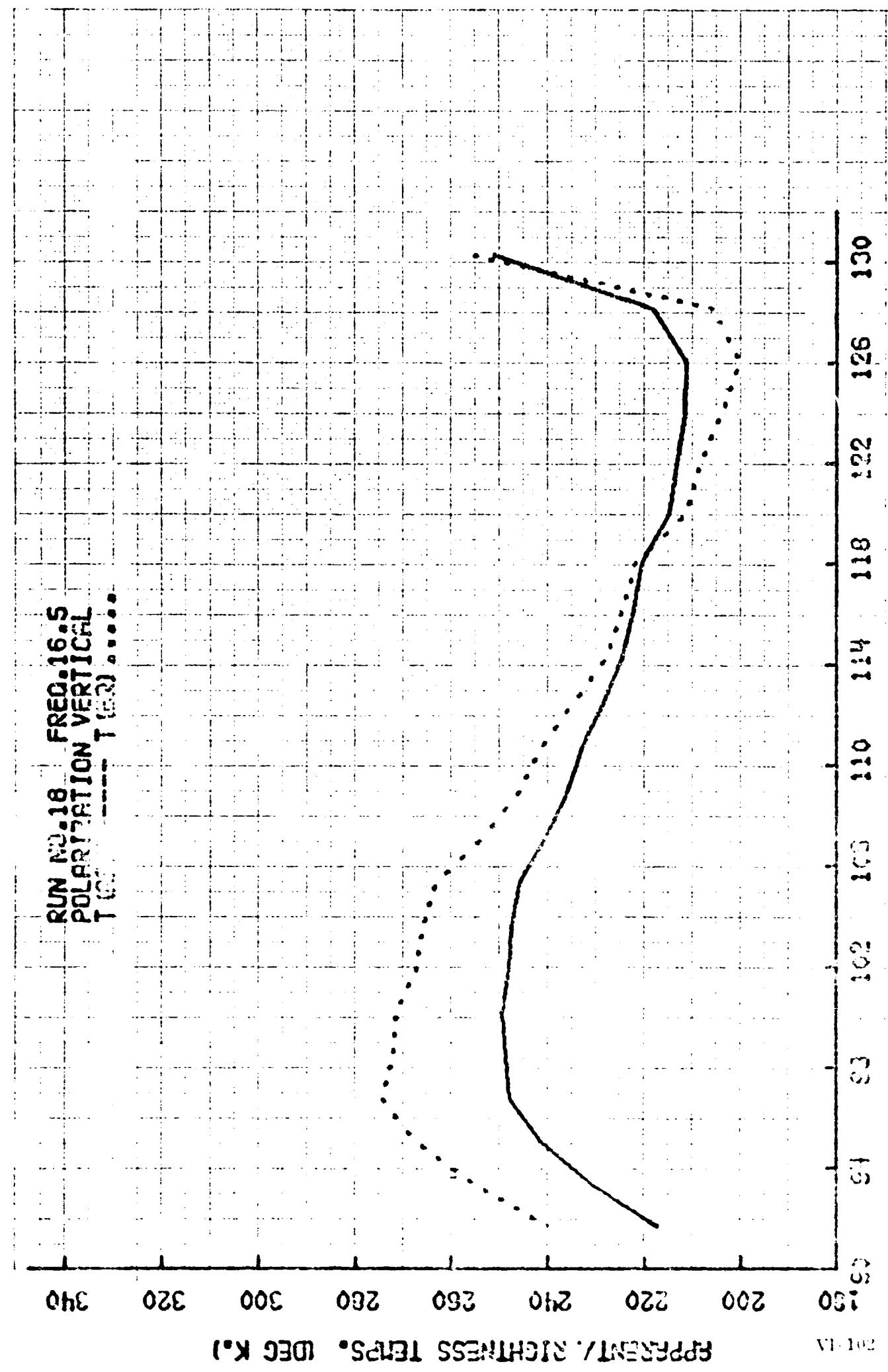


FIGURE VI-53

ZEROTH POLARIZATION (C₆₀)

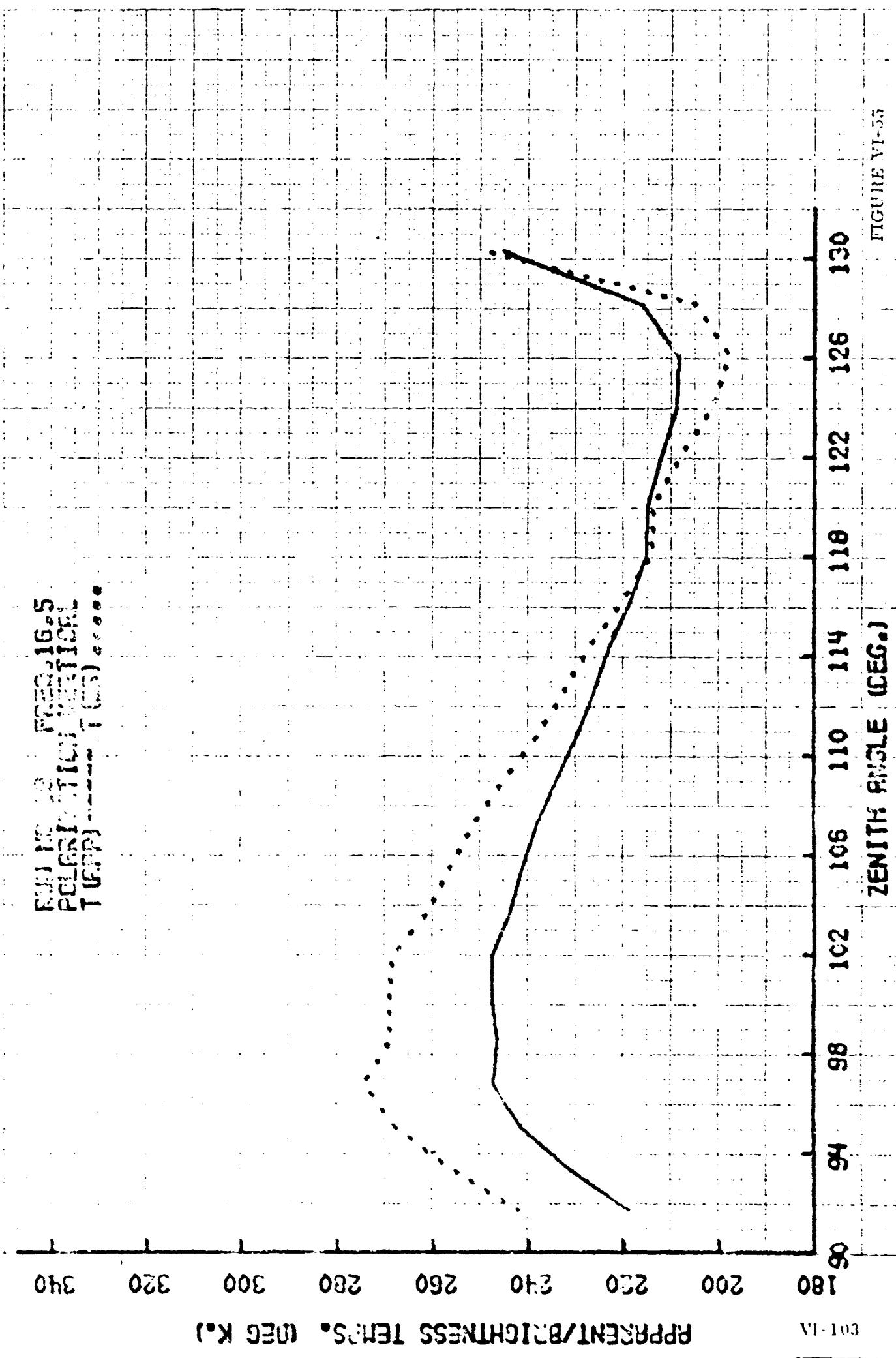


FIGURE VI-5

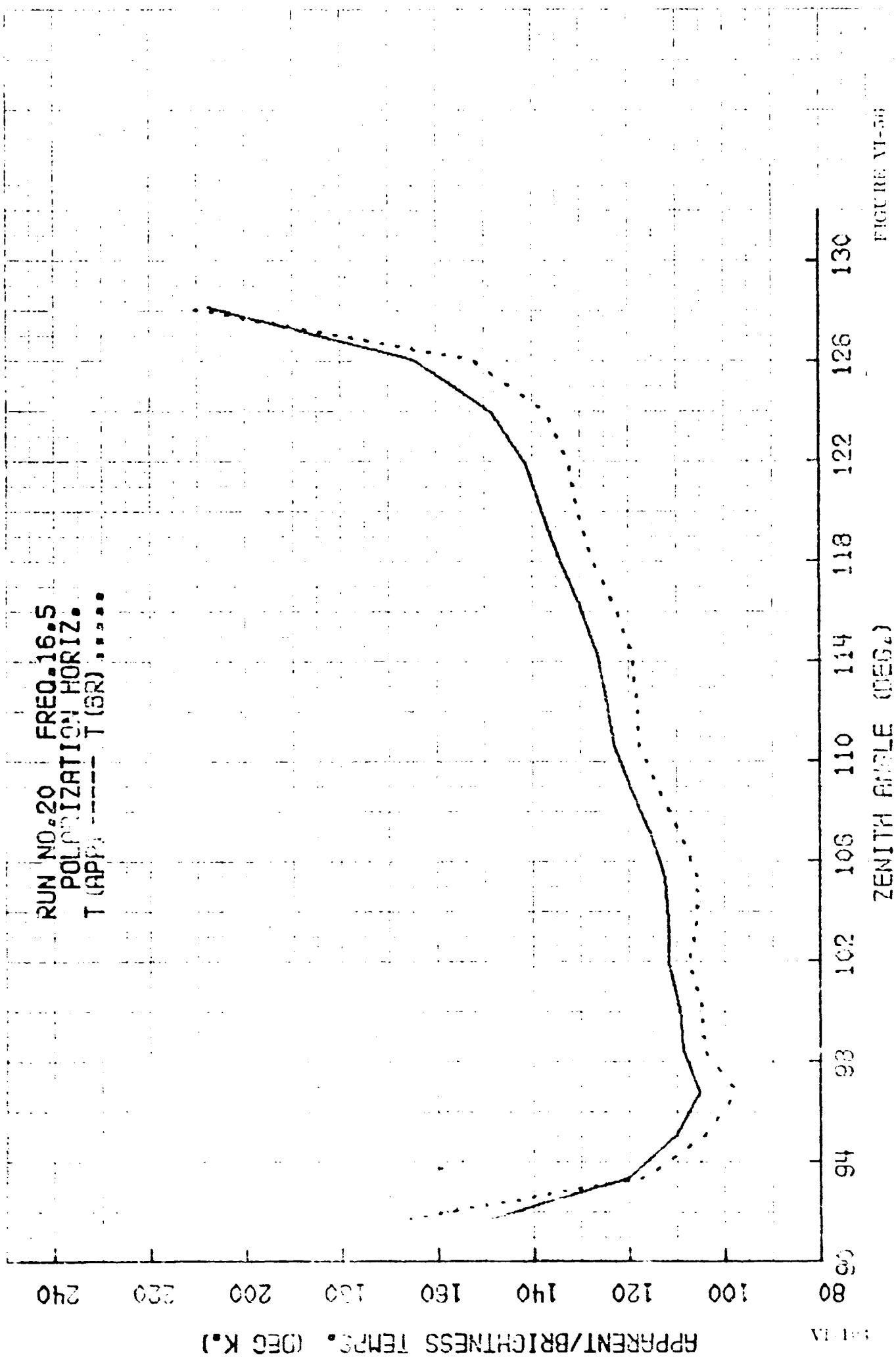


FIGURE VI-56

FIGURE VI-57

RUN NO. 21 FREQ. 16.5
FOR VERTICAL
 $T_{(app)} - T_{(true)}$

APPARENT/TRUE TEMPS. (DEG K.)

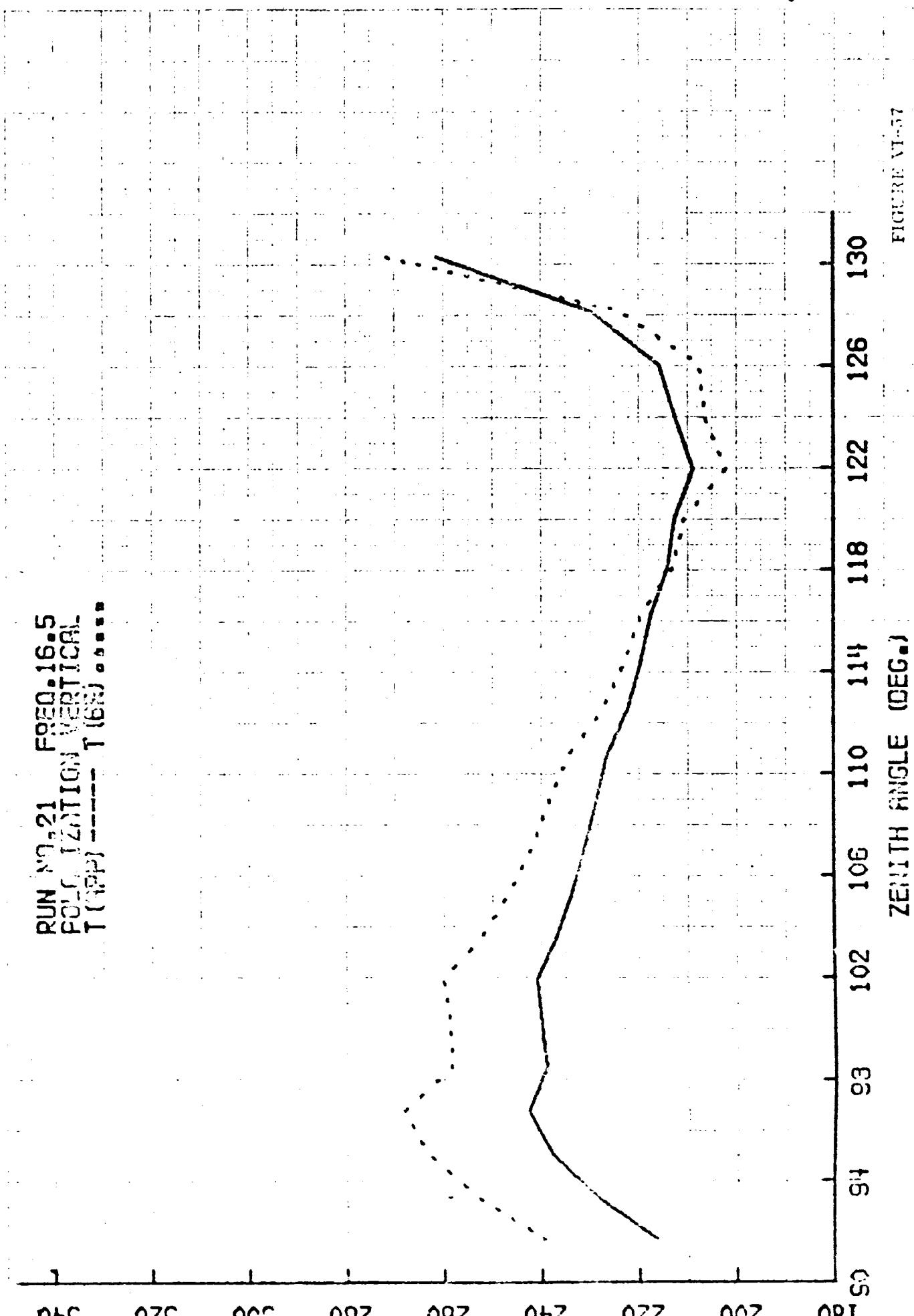
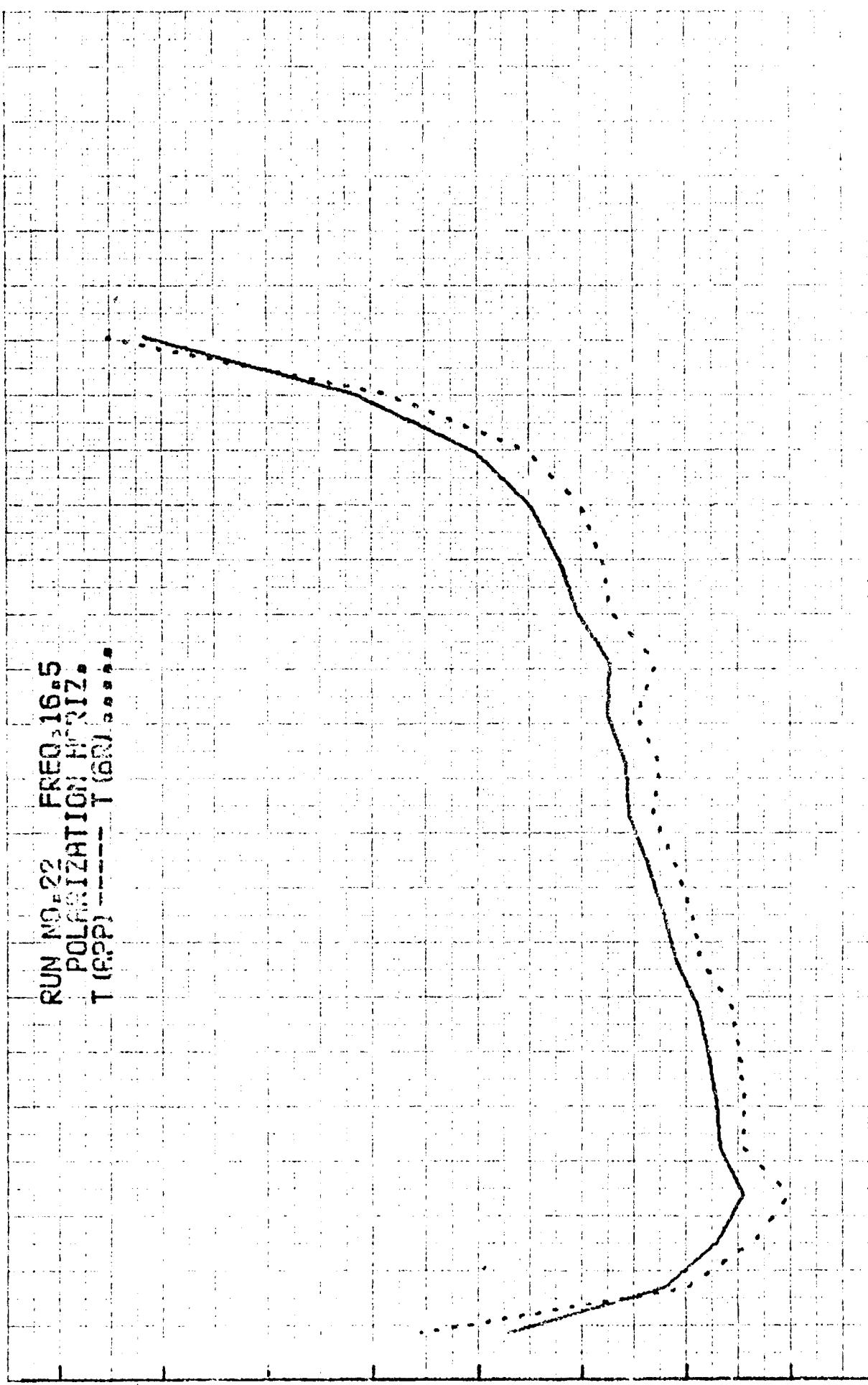


FIGURE VI-58

ZENITH ANGLE (DEG.)

APPARENT/BRIGHTNESS TEMPS. (DEG K.)

90-1A



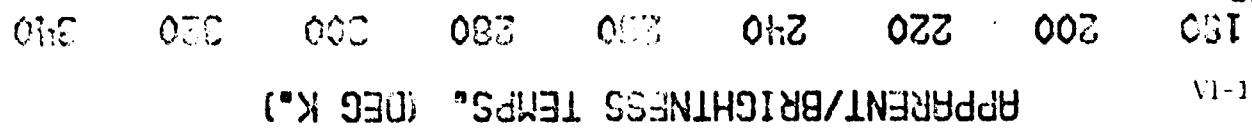
RUN NO. 22 FREQ. 16.5
POLARIZATION H₁₂.

APPARENT/BRIGHTNESS TEMPS. (DEG K.)

FIGURE VI-59

ZENITH ANGLE (DEG.)

RUN NO. 22
FREQ. 16.5
POSITION - T (E) 1000



VI-107

FIGURE A-6b

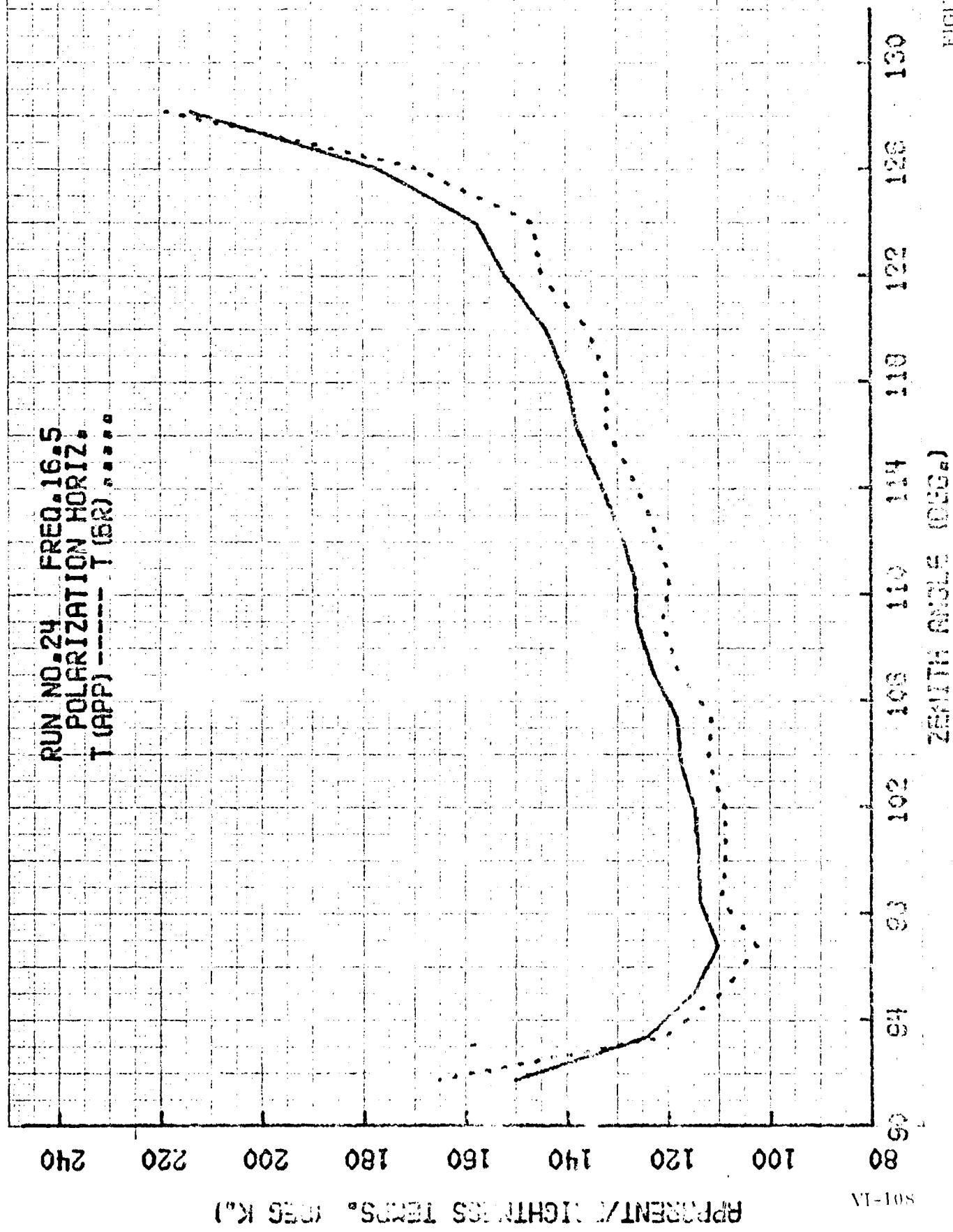


FIGURE VI-61

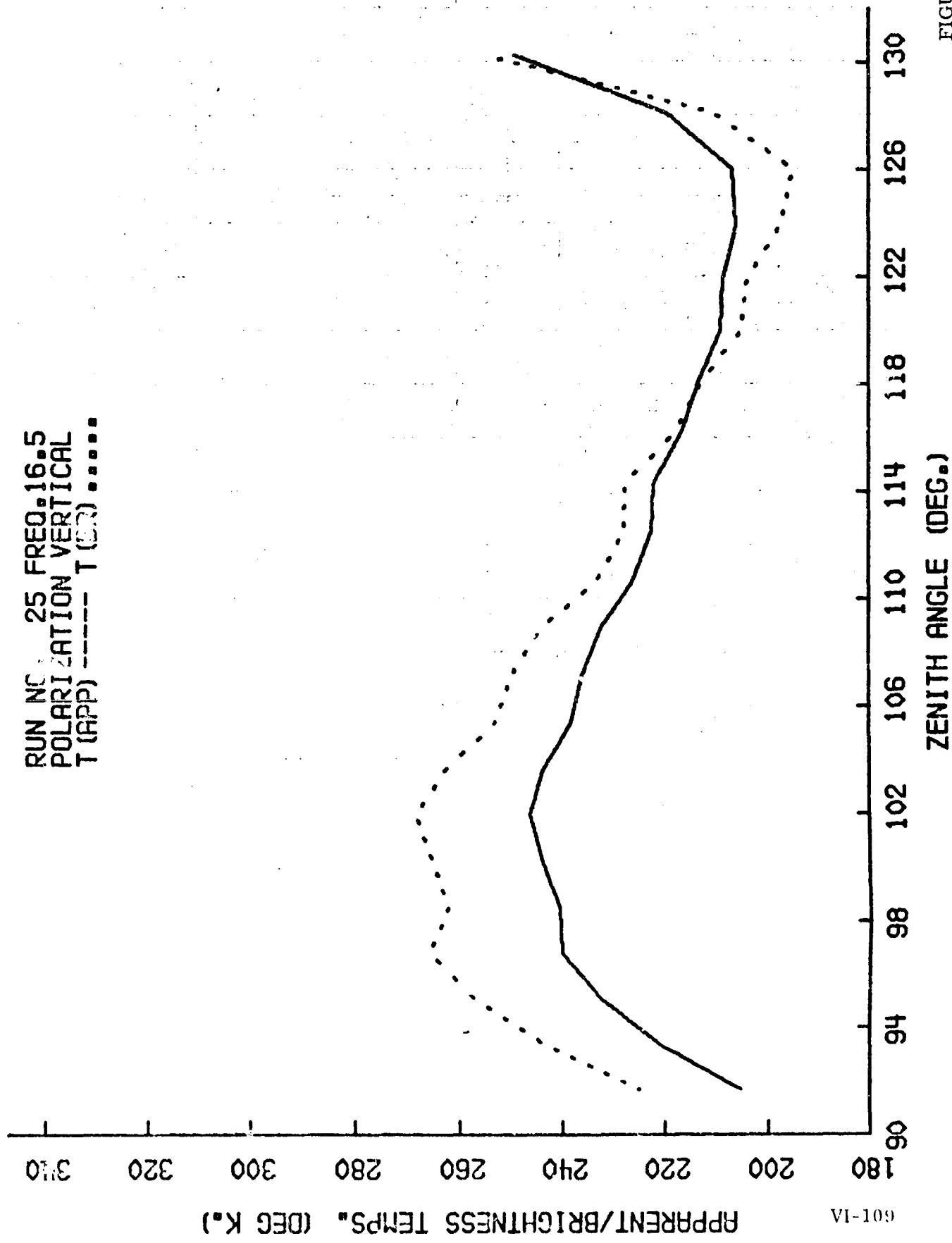
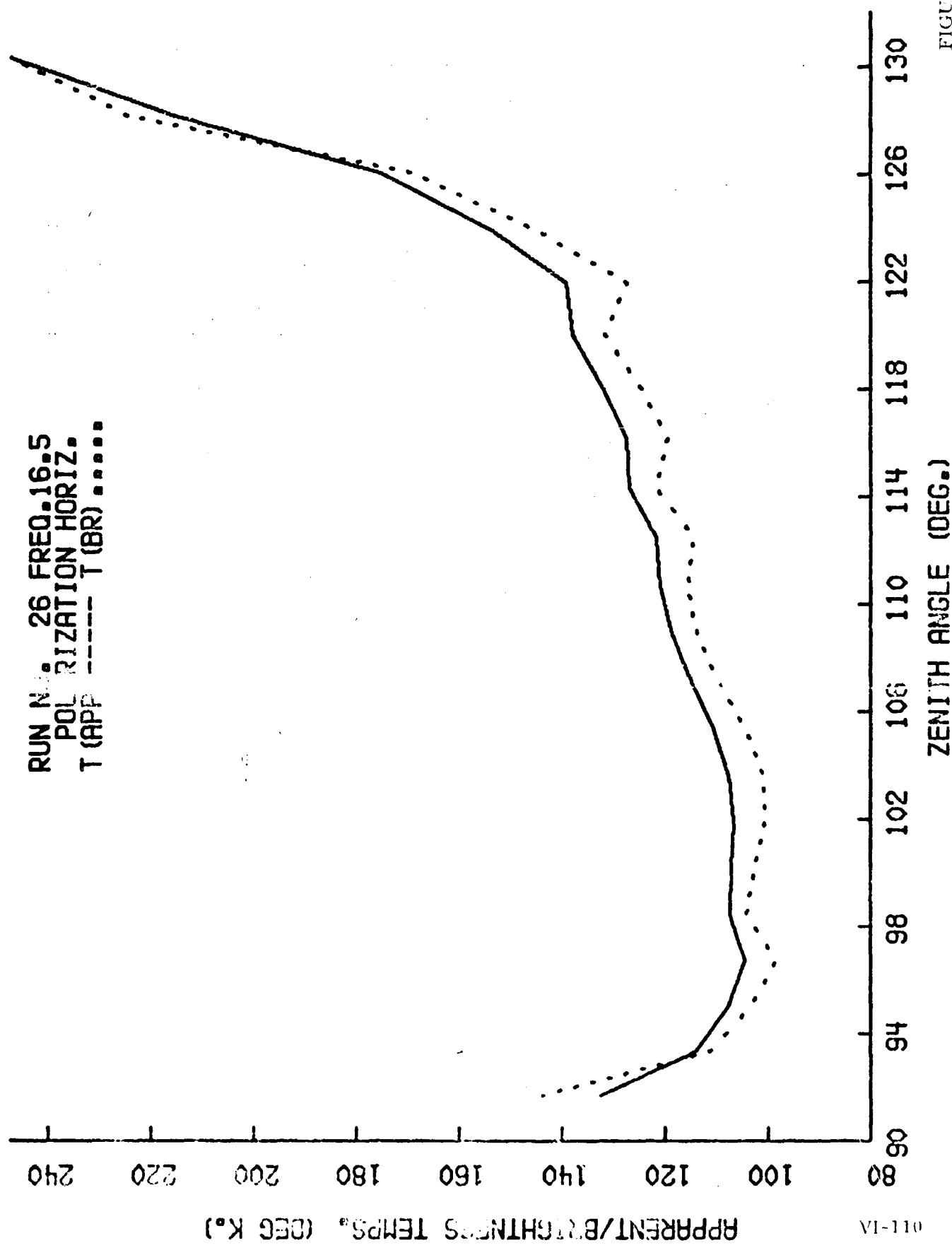


FIGURE VI-62



VI-110

RUN NO. 27 FREQ. 16.5
POLARIZATION VERTICAL
 $T_{(APP)}$ ----- $T_{(BR)}$

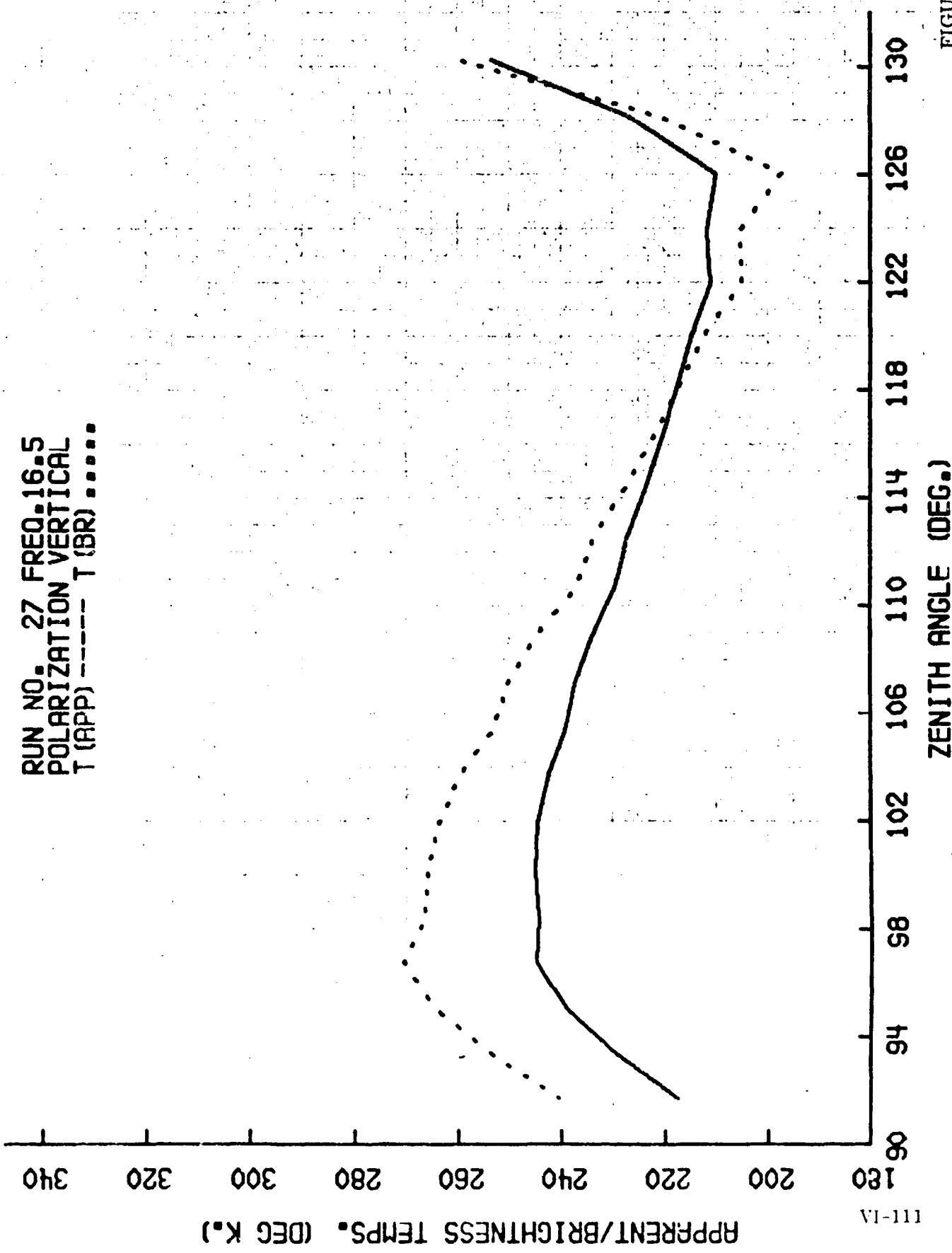
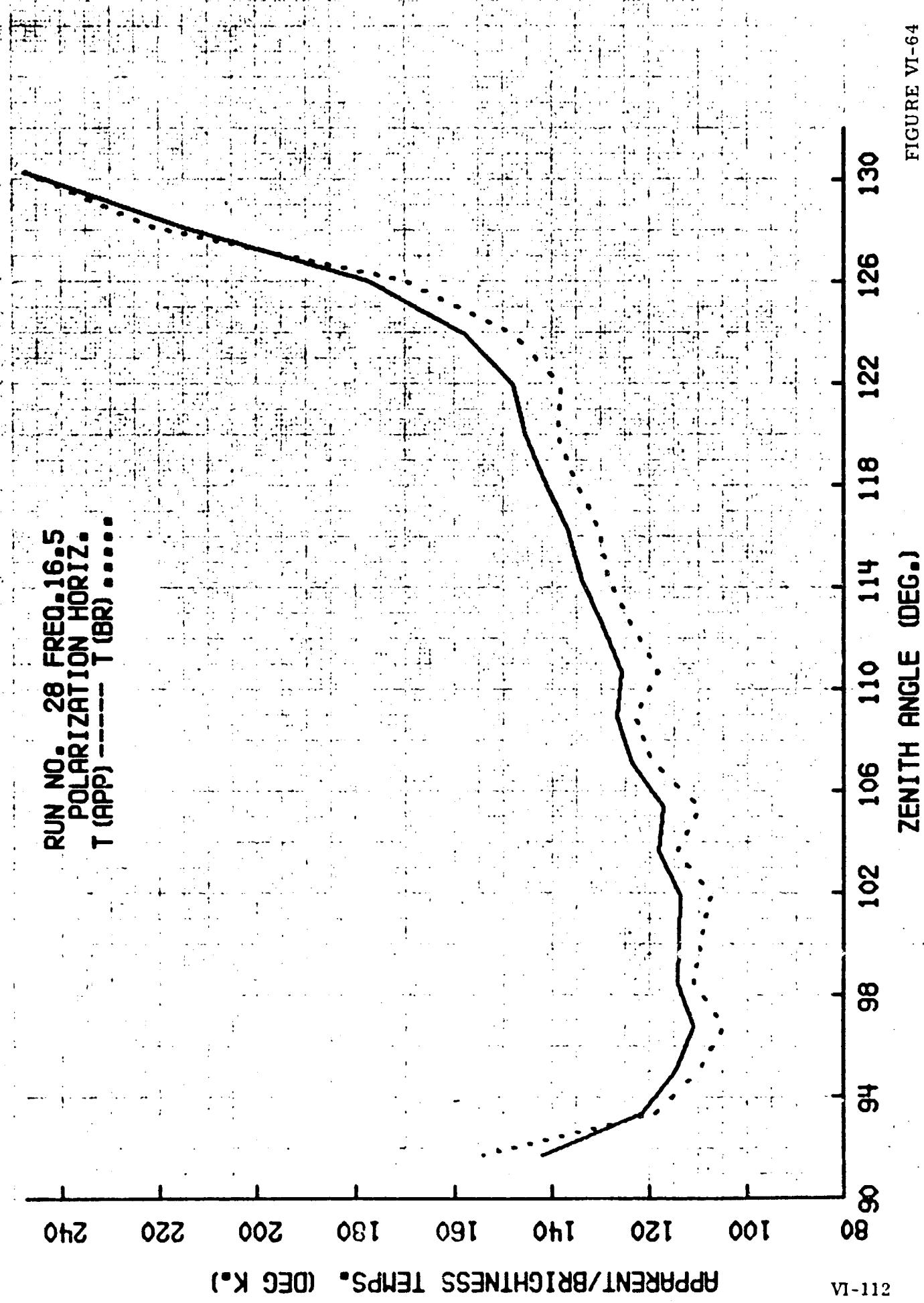


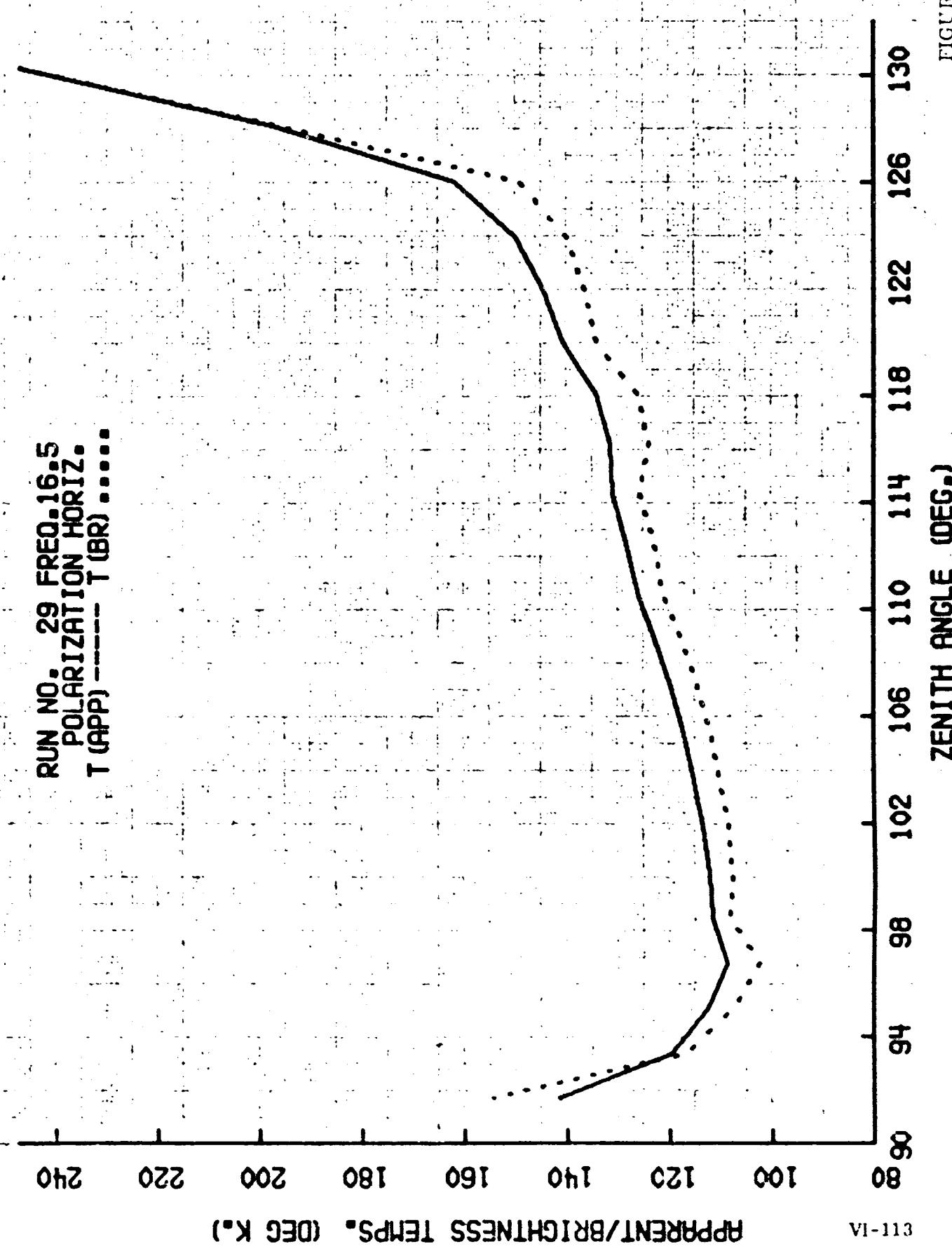
FIGURE VI-63



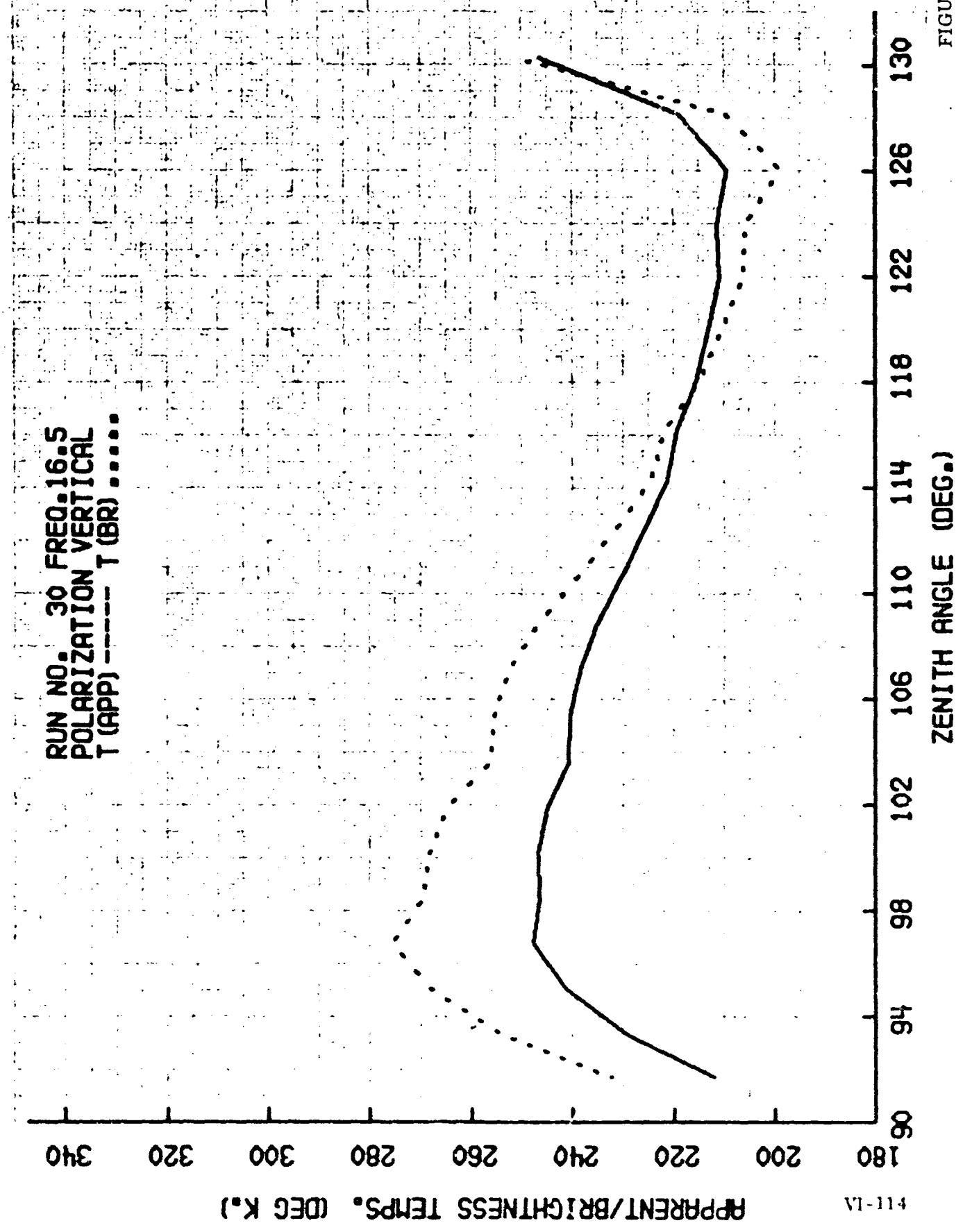
VI-112

FIGURE VI-64

FIGURE VI-65



RUN NO. 30 FREQ. 16.5
POLARIZATION VERTICAL
 $T_{(APP)}$ —— $T_{(BR)}$ ·····



VI-114

FIGURE VI-66

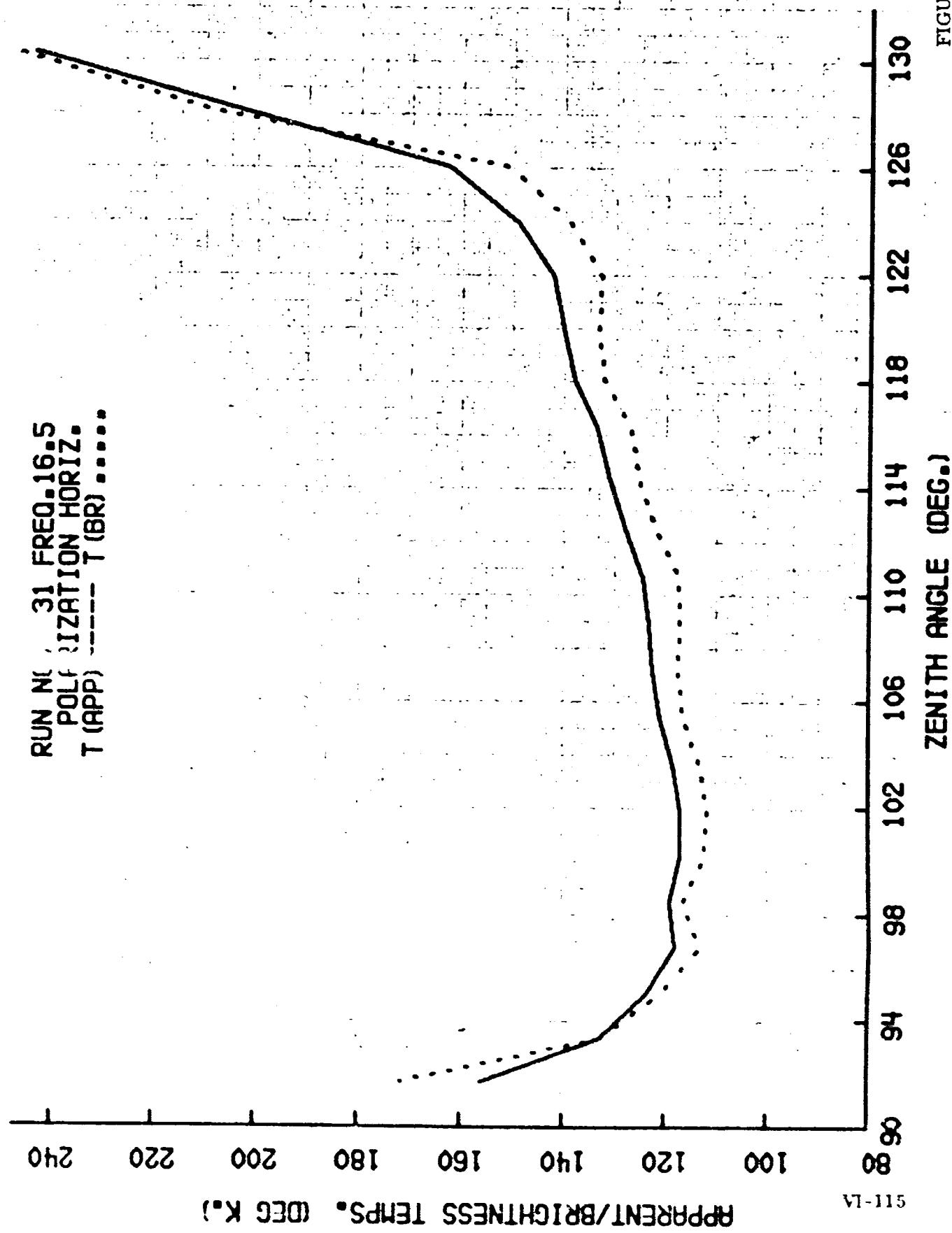


FIGURE VI-67

FIGURE VI-68

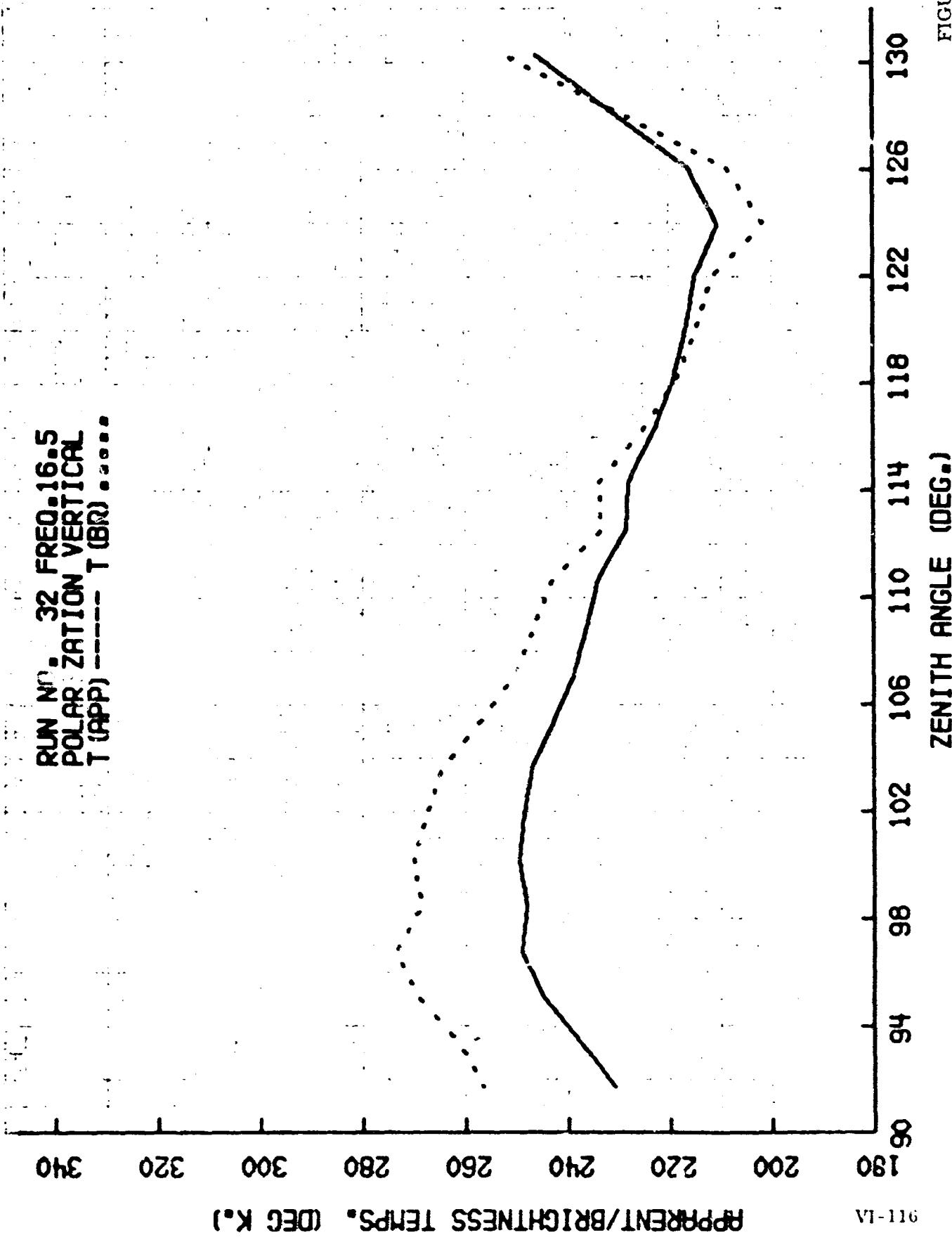


FIGURE VI-69

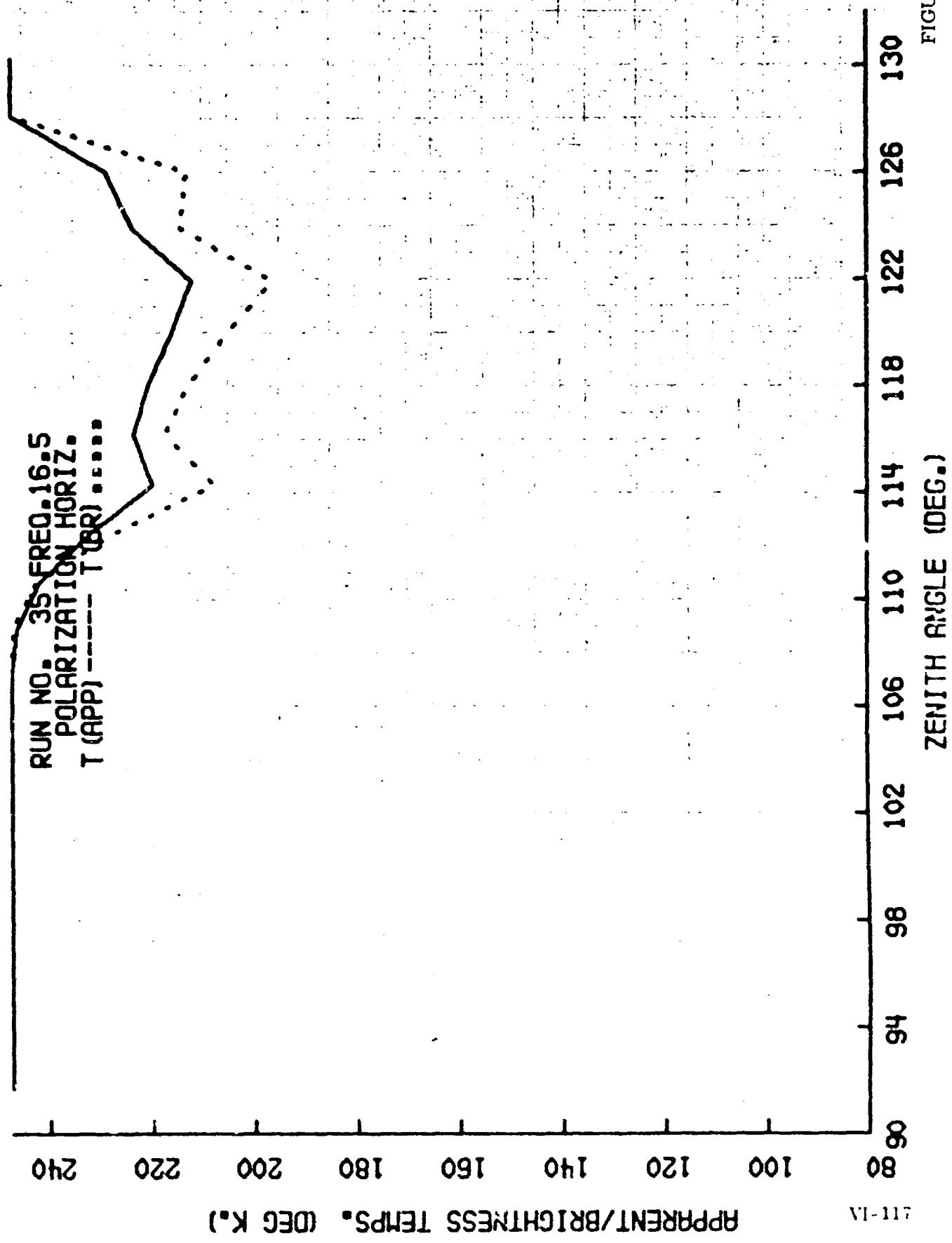


FIGURE VI-70

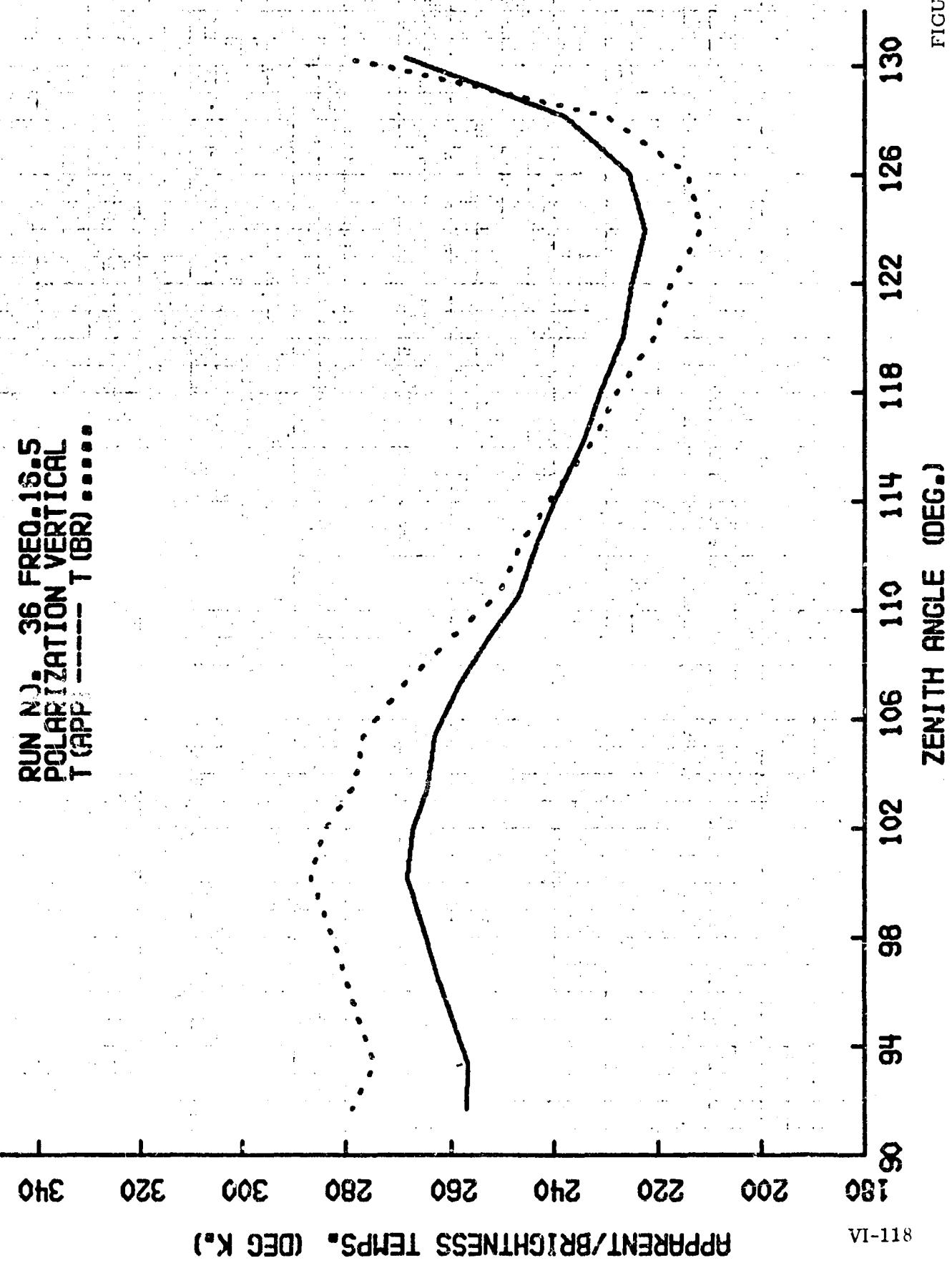


FIGURE VI-71

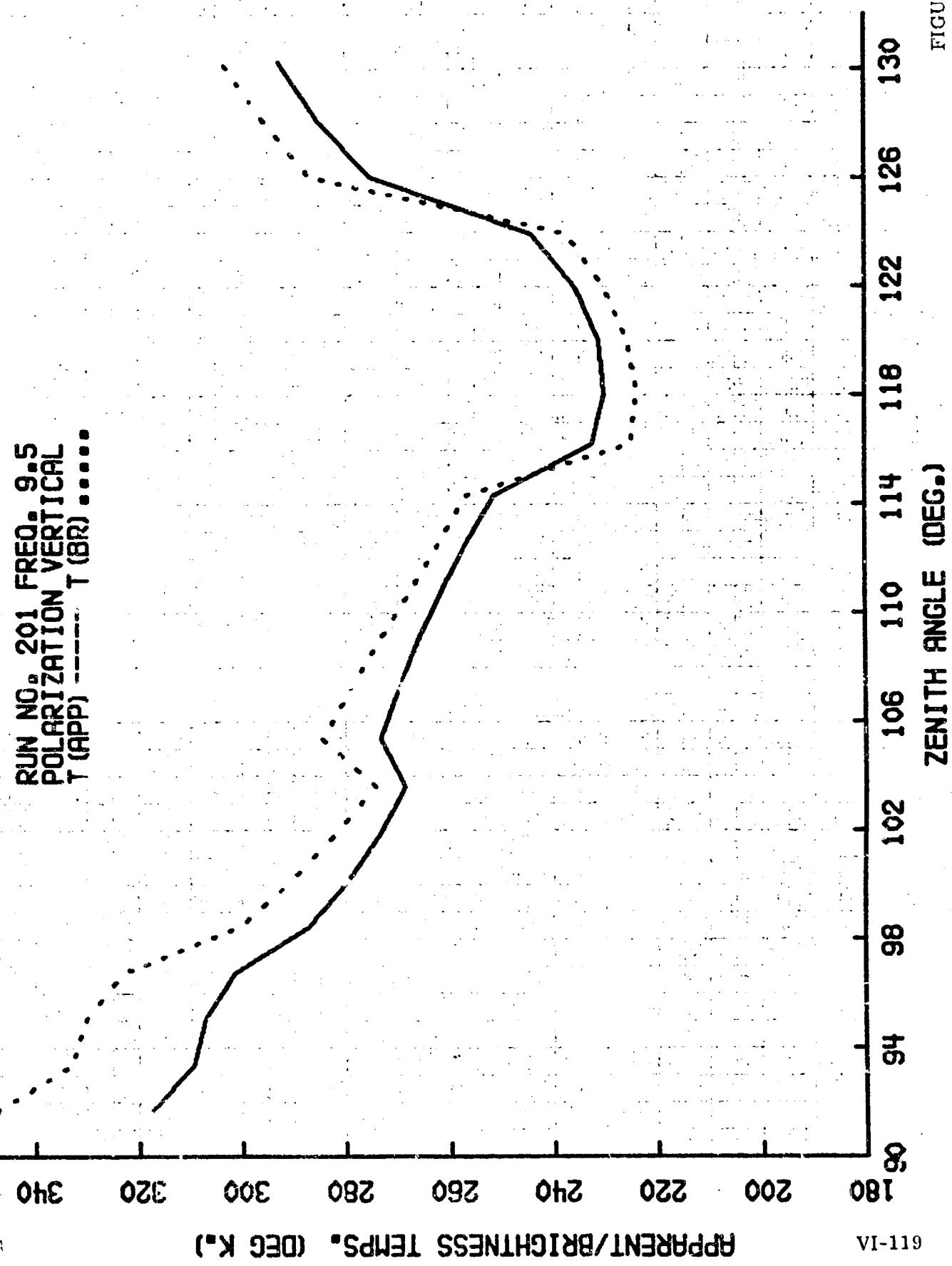
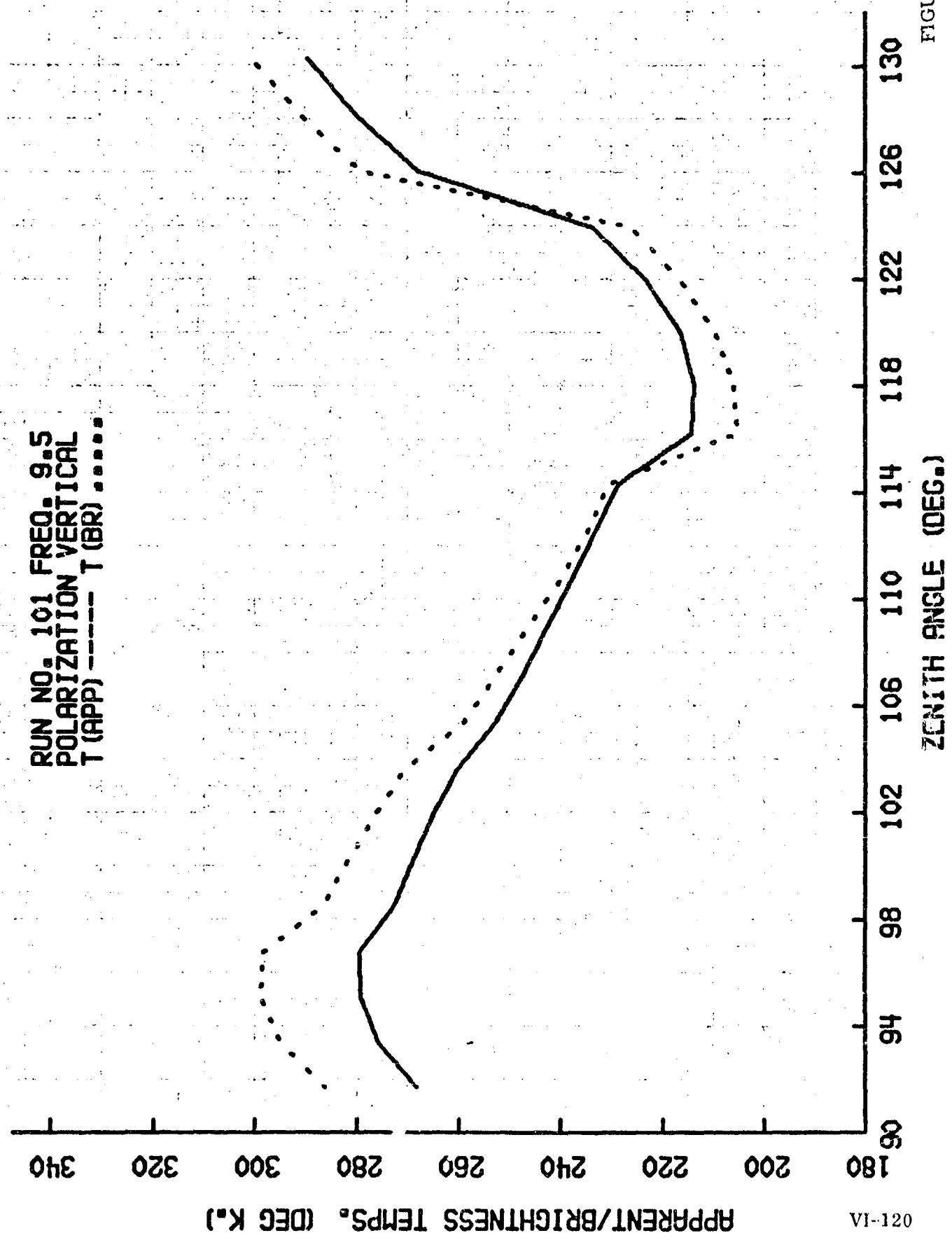


FIGURE VI-72



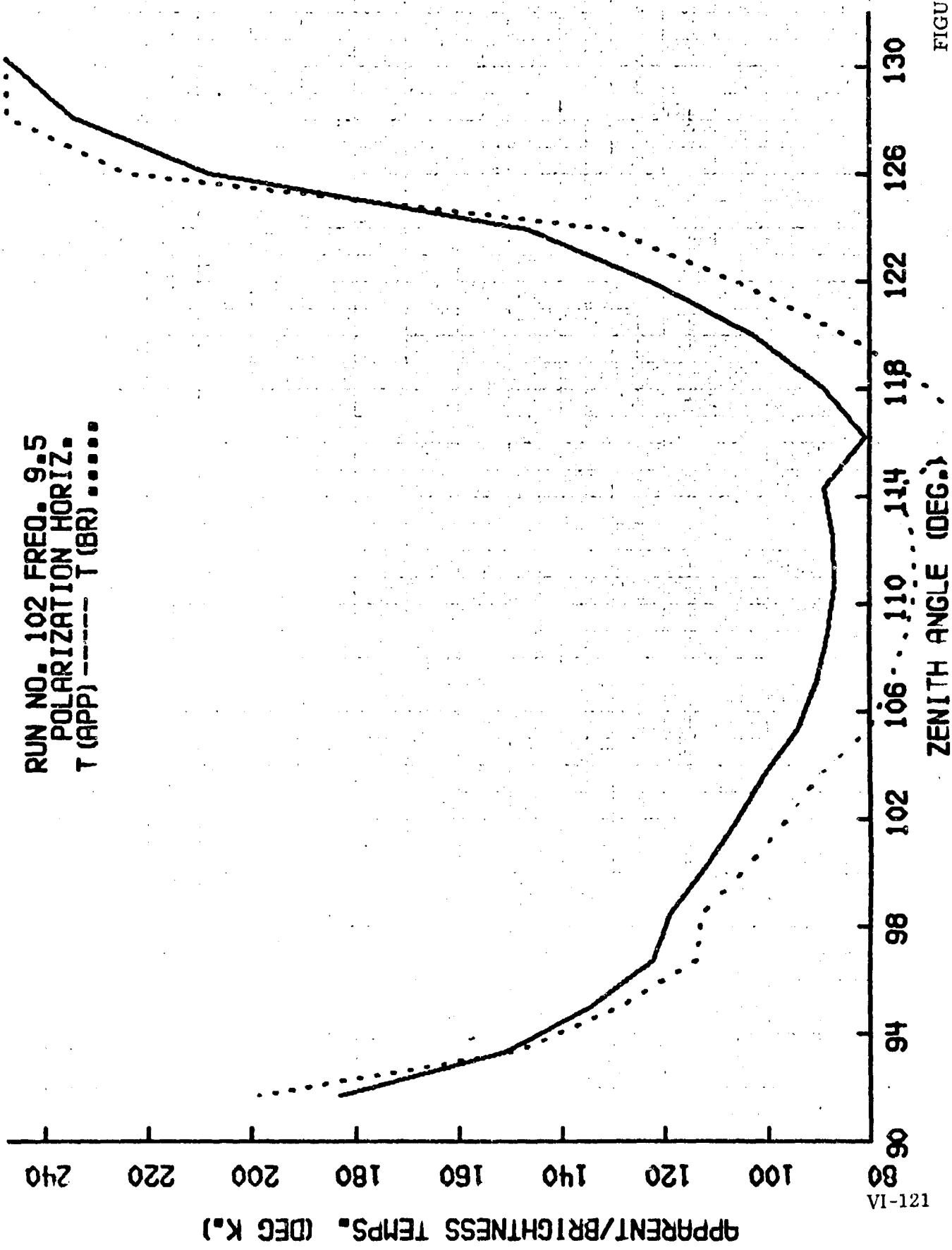


FIGURE VI-73

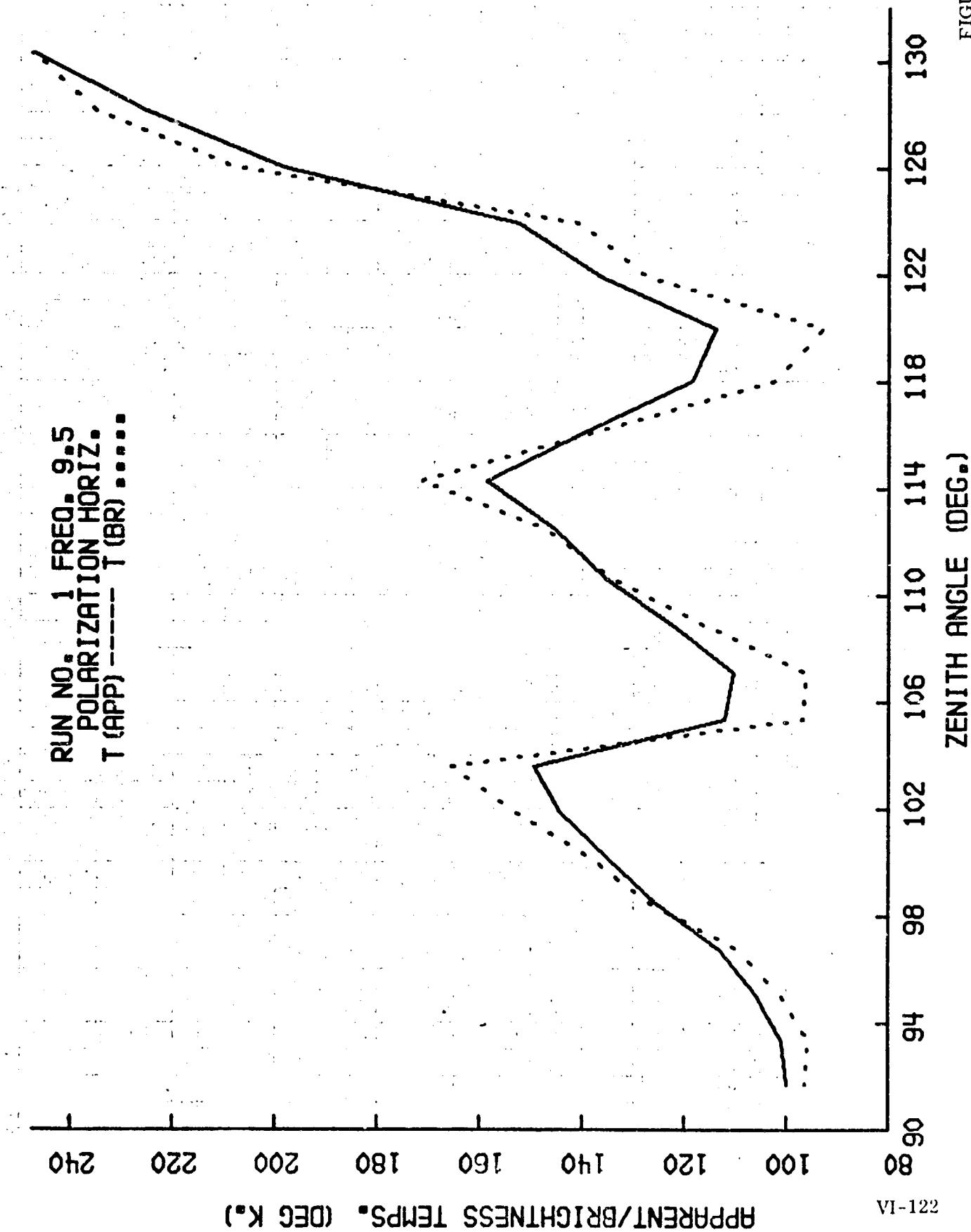


FIGURE VI-74

FIGURE VI-75

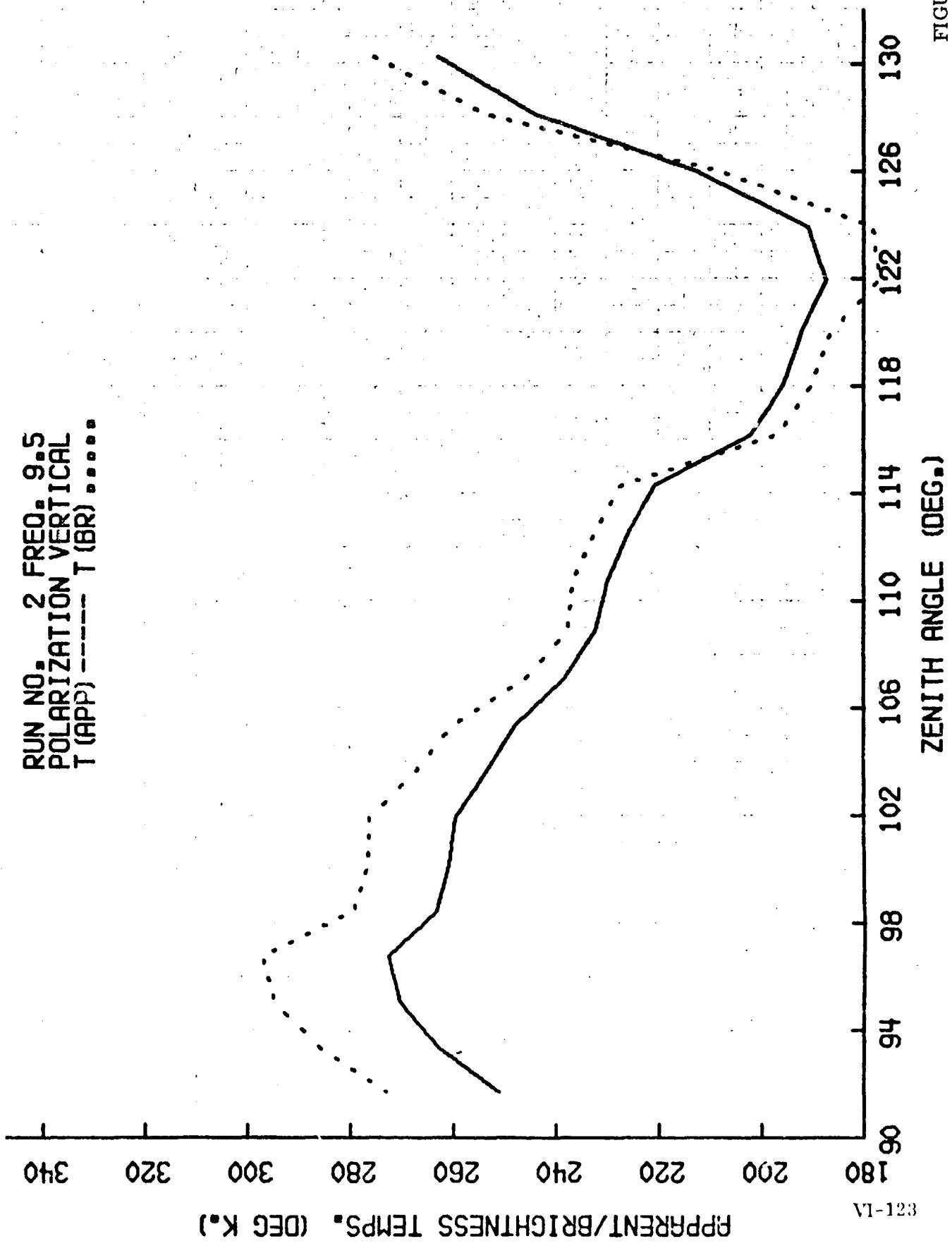
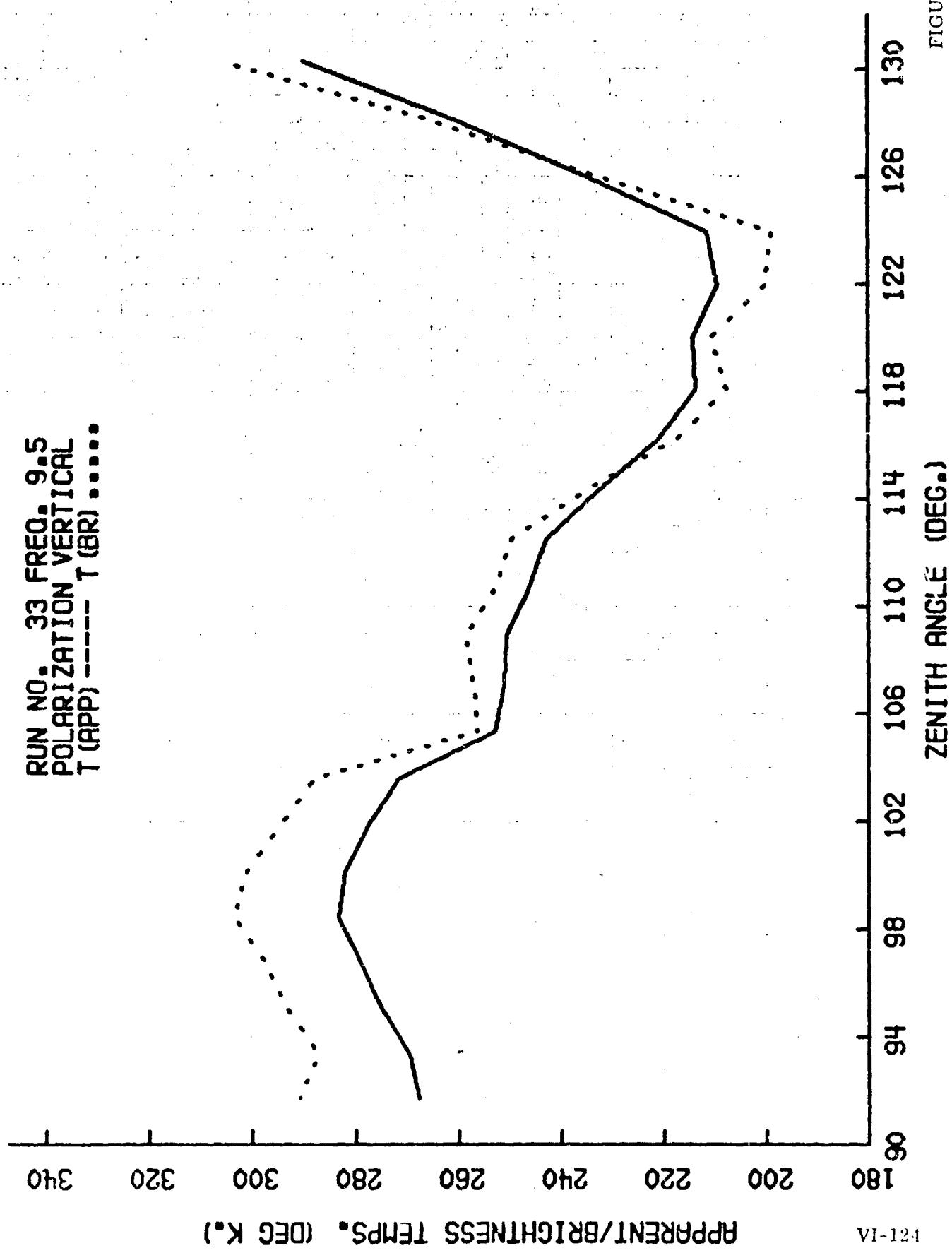
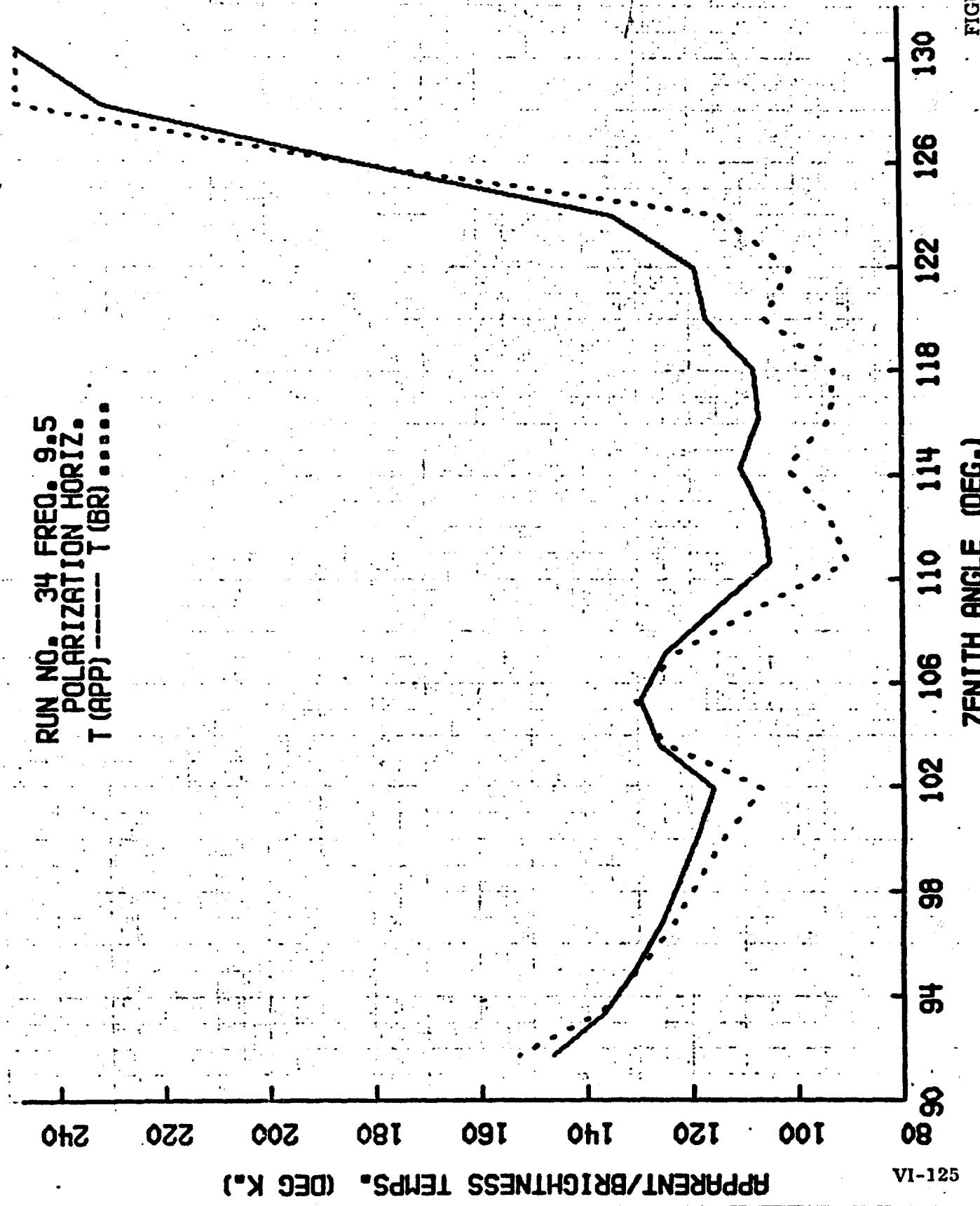


FIGURE VI-76



RUN NO. 34 FREQ. 9.5
POLARIZATION HORIZ.
 $T_{(APP)}$ —— $T_{(BR)}$ ·····



VI-125

FIGURE VI-77

BLANK

TABLE VI-42. ROCK3 OUTPUT

| RUN NO. | 2 | 07/25/69 | 9.5 GHz | V POLARIZATION | | |
|--------------------|-------------------------------|---------------------------|------------|----------------|------------------------|-----------------------------|
| ZENITH ANGLE (DEG) | BRIGHTNESS TEMPERATURE (NEST) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART | PERMITTIVITY IMAGINARY PART |
| 91.68 | 273.04 | 304.61 | 0.614875 | 5 | 58.77 | 32.19 |
| 93.37 | 276.03 | 305.64 | 0.6064126 | 6 | 58.68 | 32.11 |
| 95.06 | 294.82 | 300.94 | 0.959535 | 5 | 58.63 | 32.82 |
| 96.76 | 296.92 | 299.32 | 0.903520 | 5 | 58.68 | 33.23 |
| 98.46 | 279.20 | 285.20 | 0.967392 | 4 | 52.32 | 30.54 |
| 100.16 | 276.50 | 287.89 | 0.944712 | 4 | 54.19 | 37.53 |
| 101.86 | 276.14 | 295.67 | 0.915234 | 5 | 57.76 | 34.36 |
| 103.61 | 277.27 | 295.65 | 0.601140 | 5 | 58.18 | 36.07 |
| 105.19 | 247.00 | 294.16 | 0.643747 | 5 | 57.42 | 34.94 |
| 107.00 | 245.70 | 285.66 | 0.600391 | 5 | 53.33 | 38.02 |
| 108.86 | 217.62 | 285.99 | 0.779409 | 4 | 52.06 | 38.26 |
| 110.67 | 226.79 | 296.42 | 0.744056 | 5 | 57.51 | 36.88 |
| 112.49 | 231.44 | 297.60 | 0.715056 | 5 | 58.40 | 33.75 |
| 114.32 | 227.16 | 299.21 | 0.687613 | 5 | 58.67 | 33.76 |
| 116.18 | 197.79 | 232.63 | 0.790563 | 23 | 12.77 | 21.64 |
| 118.07 | 190.25 | 199.06 | 0.940381 | 32 | 7.66 | 5.93 |
| 120.00 | 146.39 | 192.49 | 0.959116 | 29 | 7.04 | 2.89 |
| 121.97 | 176.91 | 181.36 | 0.665210 | 16 | 6.49 | -1.95 |
| 123.97 | 178.24 | 183.67 | 0.957458 | 22 | 6.59 | -0.49 |
| 125.03 | 261.66 | 314.38 | 0.759513 | 5 | 36.16 | 32.77 |
| 126.14 | 293.71 | 378.87 | 0.589346 | 5 | 10.11 | 32.39 |
| 130.32 | 275.36 | 413.17 | 0.593341 | 6 | 6.06 | 27.41 |

| | | 16.5 GHz V POLARIZATION | | | | | | |
|---------|---|-------------------------|---------------------------------|----------------------------|------------|------------|--------------------------|--------------|
| BUN NO. | 4 | ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG. K) | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | REAL PART IMAGINARY PART | PERMITTIVITY |
| | | 91.48 | 278.64 | 269.48 | 0.933721 | 4 | 37.65 | 38.03 |
| | | 93.37 | 274.91 | 268.78 | 0.781854 | 3 | 31.25 | 37.34 |
| | | 95.00 | 275.72 | 260.53 | 0.870631 | 2 | 29.16 | 36.77 |
| | | 96.76 | 275.15 | 280.30 | 0.937222 | 1 | 28.96 | 36.57 |
| | | 98.46 | 275.90 | 280.30 | 0.944673 | 1 | 28.96 | 36.57 |
| | | 100.16 | 274.03 | 260.30 | 0.933646 | 1 | 28.56 | 36.57 |
| | | 101.86 | 270.99 | 270.40 | 0.919755 | 1 | 27.98 | 36.37 |
| | | 103.61 | 244.11 | 275.57 | 0.870721 | 1 | 24.59 | 36.89 |
| | | 105.35 | 244.96 | 281.82 | 0.861661 | 3 | 30.31 | 37.11 |
| | | 107.10 | 241.50 | 284.78 | 0.833497 | 4 | 23.21 | 37.72 |
| | | 108.88 | 217.02 | 287.80 | 0.777093 | 5 | 36.11 | 38.01 |
| | | 110.67 | 252.54 | 291.69 | 0.741426 | 6 | 39.96 | 37.91 |
| | | 112.48 | 247.21 | 296.37 | 0.731991 | 6 | 41.41 | 37.63 |
| | | 114.32 | 241.84 | 291.52 | 0.705684 | 7 | 43.02 | 37.24 |
| | | 116.18 | 211.25 | 287.25 | 0.684435 | 8 | 35.60 | 37.98 |
| | | 118.07 | 226.35 | 294.79 | 0.656512 | 9 | 41.92 | 37.53 |
| | | 120.00 | 223.09 | 296.09 | 0.633115 | 10 | 42.76 | 37.31 |
| | | 121.97 | 216.69 | 295.37 | 0.612160 | 11 | 42.10 | 37.48 |
| | | 123.97 | 238.59 | 289.40 | 0.596714 | 12 | 37.59 | 38.03 |
| | | 126.03 | 207.17 | 291.37 | 0.575732 | 13 | 39.30 | 37.94 |
| | | 128.14 | 211.19 | 309.32 | 0.555941 | 14 | 45.45 | 35.36 |
| | | 130.32 | 249.96 | 351.61 | 0.609887 | 15 | 13.38 | 27.72 |

TABLE VI-43. ROCK3 OUTPUT

RUN NO. 3 08/01/69 16.5 GHz V POLARIZATION

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMPERATURE (KELVIN) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART IMAGINARY PART | PERMITTIVITY IMAGINARY PART |
|--------------------|---------------------------------|---------------------------|------------|------------|--------------------------|-----------------------------|
| 91.48 | 22.23 | 306.55 | 0.970431 | 3 | 43.87 | 35.57 |
| 93.37 | 214.81 | 294.50 | 0.926282 | 4 | 64.13 | 35.85 |
| 95.26 | 211.53 | 293.46 | 0.924722 | 4 | 40.96 | 37.72 |
| 96.15 | 210.13 | 291.41 | 0.958795 | 4 | 39.14 | 37.95 |
| 98.46 | 279.65 | 284.13 | 0.953879 | 3 | 32.58 | 37.62 |
| 100.16 | 275.81 | 286.27 | 0.942826 | 4 | 36.56 | 37.31 |
| 101.48 | 275.07 | 291.21 | 0.919533 | 5 | 39.16 | 37.95 |
| 103.51 | 276.97 | 301.59 | 0.849670 | 6 | 45.27 | 35.29 |
| 105.13 | 242.34 | 292.20 | 0.856559 | 6 | 66.44 | 36.72 |
| 107.0 | 242.27 | 303.31 | 0.924267 | 6 | 45.66 | 36.01 |
| 108.48 | 240.35 | 311.11 | 0.775233 | 6 | 43.02 | 35.32 |
| 110.67 | 219.66 | 318.77 | 0.770194 | 6 | 40.86 | 35.61 |
| 112.48 | 210.87 | 319.76 | 0.742294 | 6 | 40.10 | 35.66 |
| 114.32 | 244.04 | 320.75 | 0.716633 | 5 | 39.28 | 35.72 |
| 116.18 | 241.26 | 325.64 | 0.746822 | 5 | 34.83 | 35.78 |
| 118.07 | 232.35 | 324.66 | 0.671522 | 5 | 35.79 | 35.81 |
| 120.00 | 229.12 | 327.45 | 0.692901 | 5 | 33.06 | 35.69 |
| 121.97 | 227.23 | 332.53 | 0.640439 | 4 | 27.96 | 34.92 |
| 123.97 | 220.47 | 332.23 | 0.619612 | 4 | 28.23 | 35.00 |
| 125.03 | 211.60 | 328.63 | 0.594294 | 4 | 31.89 | 35.58 |
| 125.14 | 219.19 | 340.69 | 0.600381 | 4 | 20.43 | 32.37 |
| 130.32 | 267.96 | 361.12 | 0.671999 | 6 | 18.91 | |

TABLE VI-45. ROCK3 OUTPUT

| RUN NO. | 8 | 08/01/69 | 16.9 GHz | V POLARIZATION | ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART | PERMITTIVITY IMAGINARY PART |
|---------|---|----------|----------|----------------|---------------------|--------------------------------|---------------------------|------------|------------|-----------|-----------------------------|
| | | | | | 91.46 | 269.33 | 311.33 | 0.875211 | 6 | 44.95 | 35.32 |
| | | | | | 93.37 | 274.58 | 287.56 | 0.806557 | 4 | 37.81 | 36.02 |
| | | | | | 95.05 | 275.15 | 284.50 | 0.973255 | 3 | 35.03 | 37.49 |
| | | | | | 94.75 | 275.70 | 202.32 | 0.942493 | 3 | 30.80 | 37.23 |
| | | | | | 96.46 | 271.67 | 280.00 | 0.948673 | 1 | 28.56 | 35.77 |
| | | | | | 100.45 | 274.01 | 284.56 | 0.941985 | 4 | 33.00 | 31.69 |
| | | | | | 101.08 | 279.86 | 236.52 | 0.920427 | 9 | 43.02 | 37.24 |
| | | | | | 103.61 | 275.59 | 301.57 | 0.889374 | 6 | 45.26 | 35.10 |
| | | | | | 105.15 | 272.54 | 204.53 | 0.857471 | 6 | 45.82 | 35.82 |
| | | | | | 107.0 | 264.45 | 301.55 | 0.824862 | 6 | 45.78 | 35.32 |
| | | | | | 109.88 | 254.18 | 104.05 | 0.792449 | 6 | 45.17 | 35.89 |
| | | | | | 110.67 | 245.39 | 301.08 | 0.76105 | 6 | 45.77 | 35.09 |
| | | | | | 112.8 | 245.12 | 311.40 | 0.73779 | 6 | 43.62 | 35.37 |
| | | | | | 114.32 | 238.35 | 316.14 | 0.712031 | 6 | 42.63 | 35.45 |
| | | | | | 115.13 | 243.16 | 317.93 | 0.687945 | 5 | 41.65 | 35.26 |
| | | | | | 119.07 | 279.30 | 322.98 | 0.688050 | 5 | 37.71 | 35.79 |
| | | | | | 120.00 | 219.27 | 312.73 | 0.642820 | 5 | 40.11 | 35.66 |
| | | | | | 121.97 | 217.16 | 322.19 | 0.624224 | 5 | 35.28 | 35.10 |
| | | | | | 123.97 | 215.73 | 327.85 | 0.615372 | 5 | 30.63 | 35.42 |
| | | | | | 124.03 | 205.25 | 326.42 | 0.590327 | 5 | 34.09 | 35.75 |
| | | | | | 124.03 | 222.66 | 365.58 | 0.611976 | 5 | 36.84 | 30.33 |
| | | | | | 124.32 | 265.02 | 381.48 | 0.572549 | 5 | 6.94 | 18.89 |

TABLE VI-46. ROCK3 OUTPUT

| RUN NO. | DATE | 14.5 GHz | V POLARIZATION | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART | PERMITTIVITY IMAGINARY PART |
|---------|---------|----------|----------------|------------------------------|------------|------------|---------------------------|--------------------------------|
| 91.68 | 9/1/69 | 2.70.14 | 2.71.56 | 3.924.76 | 2 | 30.06 | 37.04 | |
| 93.37 | 2.75.95 | 2.79.57 | 0.764.44 | 27.30 | 36.11 | | | |
| 95.06 | 2.75.29 | 2.77.58 | 0.8799.6 | 26.49 | 35.69 | | | |
| 96.76 | 2.74.38 | 2.75.88 | 0.9297.5 | 3 | 35.41 | | | |
| 98.46 | 2.73.93 | 2.76.45 | 0.9443.3 | 3 | 35.39 | | | |
| 100.16 | 2.72.14 | 2.75.84 | 0.9775.6 | 4 | 34.96 | | | |
| 102.84 | 2.69.66 | 2.75.72 | 0.9204.7 | 24.41 | 34.71 | | | |
| 103.61 | 2.67.57 | 2.77.76 | 0.8749.0 | 3 | 35.77 | | | |
| 104.35 | 2.60.43 | 2.80.50 | 0.8844.51 | 28.36 | 35.57 | | | |
| 107.10 | 2.59.61 | 2.90.87 | 0.8758.0 | 5 | 37.97 | | | |
| 108.85 | 2.55.61 | 2.92.11 | 0.7919.61 | 6 | 36.75 | | | |
| 110.67 | 2.48.18 | 3.02.95 | 0.7610.64 | 6 | 36.06 | | | |
| 112.48 | 2.47.61 | 3.14.61 | 0.7381.56 | 43.51 | 35.56 | | | |
| 114.32 | 2.39.89 | 3.17.20 | 0.7129.50 | 61.95 | 35.51 | | | |
| 115.18 | 2.34.75 | 3.15.84 | 0.6950.53 | 42.61 | 35.44 | | | |
| 116.07 | 2.27.94 | 3.17.22 | 0.6630.59 | 61.94 | 35.51 | | | |
| 120.00 | 2.27.07 | 3.25.16 | 0.6495.53 | 25.32 | 35.60 | | | |
| 121.97 | 2.23.32 | 3.27.10 | 0.6142.53 | 21.41 | 35.52 | | | |
| 123.97 | 2.21.90 | 3.34.16 | 0.6232.59 | 26.35 | 34.55 | | | |
| 126.53 | 2.16.08 | 3.34.73 | 0.6036.76 | 25.79 | 34.40 | | | |
| 127.14 | 2.29.36 | 3.49.56 | 0.6217.55 | 14.44 | 28.60 | | | |
| 130.32 | 2.67.69 | 3.82.75 | 0.6744.25 | 6.64 | 18.64 | | | |

RUN NO. 11 08/05/69 - 16.5 GHz V POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (NEC, K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART IMAGINARY PART |
|---------------------|---------------------------------|---------------------------|------------|------------|--------------------------|
| 91.60 | 315.43 | 320.91 | 0.500396 | 8 | 25.16 36.22 |
| 91.37 | 324.79 | 333.45 | 0.76107 | 9 | 27.05 34.73 |
| 91.06 | 326.42 | 332.42 | 0.76119 | 9 | 26.06 36.96 |
| 91.76 | 322.41 | 331.00 | 0.94017 | 8 | 29.49 35.24 |
| 91.45 | 321.59 | 325.84 | 0.95854 | 8 | 33.68 35.73 |
| 101.16 | 320.97 | 328.33 | 0.946011 | 7 | 32.19 35.61 |
| 101.86 | 312.88 | 327.04 | 0.923194 | 7 | 28.02 34.95 |
| 103.61 | 314.36 | 326.50 | 0.894492 | 7 | 30.66 35.43 |
| 105.35 | 302.94 | 328.03 | 0.877891 | 6 | 25.72 36.43 |
| 107.10 | 296.41 | 326.83 | 0.839244 | 6 | 31.69 35.56 |
| 108.88 | 297.54 | 325.94 | 0.807615 | 6 | 31.68 35.55 |
| 110.67 | 289.84 | 334.15 | 0.790623 | 6 | 24.64 34.95 |
| 112.48 | 293.03 | 332.38 | 0.763040 | 6 | 26.36 34.55 |
| 114.32 | 292.54 | 335.93 | 0.772061 | 5 | 20.11 34.97 |
| 116.18 | 276.93 | 335.36 | 0.712560 | 5 | 24.69 36.05 |
| 118.07 | 269.07 | 332.12 | 0.619051 | 5 | 25.20 34.22 |
| 120.00 | 262.90 | 330.18 | 0.627679 | 5 | 28.37 35.03 |
| 121.97 | 264.19 | 335.84 | 0.628027 | 5 | 30.32 35.38 |
| 123.97 | 259.79 | 334.50 | 0.62871 | 5 | 24.74 34.08 |
| 125.03 | 263.68 | 311.53 | 0.602319 | 5 | 25.92 34.43 |
| 126.14 | 293.24 | 271.57 | 0.652465 | 5 | 19.78 32.04 |
| 130.32 | | | | | 7.69 20.89 |

TABLE VI-47. ROCK3 OUTPUT

RUN NO. 13 08/06/69 16.5 GHz V POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG. K) | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | REAL PART PERMITTIVITY | IMAGINARY PART |
|---------------------|---------------------------------|----------------------------|------------|------------|------------------------|----------------|
| 91.58 | 247.73 | 290.77 | 0.557594 | 3 | 36.79 | 37.98 |
| 91.37 | 265.64 | 294.21 | 0.618532 | 3 | 41.51 | 37.61 |
| 95.03 | 277.04 | 291.16 | 0.920150 | 3 | 39.12 | 37.95 |
| 95.76 | 282.45 | 290.48 | 0.958054 | 4 | 38.72 | 37.94 |
| 98.46 | 274.04 | 282.97 | 0.952461 | 3 | 31.43 | 37.38 |
| 101.16 | 272.14 | 283.57 | 0.941681 | 3 | 32.02 | 37.51 |
| 101.86 | 268.59 | 285.56 | 0.619244 | 4 | 34.07 | 37.04 |
| 103.61 | 264.91 | 282.76 | 0.819581 | 5 | 37.71 | 38.02 |
| 105.35 | 261.08 | 284.28 | 0.856824 | 6 | 41.42 | 37.63 |
| 107.10 | 255.46 | 297.50 | 0.823837 | 6 | 43.63 | 37.04 |
| 108.85 | 250.21 | 301.84 | 0.792054 | 6 | 45.34 | 36.25 |
| 111.67 | 244.21 | 305.38 | 0.762159 | 6 | 45.96 | 35.75 |
| 112.48 | 244.61 | 303.36 | 0.732774 | 6 | 45.70 | 35.97 |
| 114.32 | 238.50 | 317.83 | 0.713531 | 6 | 41.51 | 35.55 |
| 114.18 | 232.32 | 318.16 | 0.644876 | 5 | 40.45 | 35.61 |
| 116.07 | 220.20 | 324.52 | 0.671464 | 5 | 35.83 | 35.81 |
| 120.00 | 228.16 | 329.54 | 0.655386 | 5 | 30.87 | 35.45 |
| 121.97 | 215.74 | 324.39 | 0.627109 | 5 | 36.04 | 35.81 |
| 123.97 | 222.97 | 336.67 | 0.628393 | 4 | 23.76 | 33.62 |
| 124.03 | 218.59 | 329.39 | 0.593903 | 4 | 32.13 | 35.60 |
| 124.14 | 222.93 | 345.06 | 0.611420 | 5 | 16.99 | 30.43 |
| 130.32 | 277.20 | 390.94 | 0.684948 | 5 | 9.93 | 17.52 |

TABLE VI-48. ROCK3 OUTPUT

RUN NO. 13 08/07/69 16.9 GHZ V POLARIZATION

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMPERATURE (DEG.K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART | PERMITTIVITY IMAGINARY PART |
|--------------------|--------------------------------|---------------------------|------------|------------|-----------|-----------------------------|
| 91.58 | 242.20 | 287.59 | 0.547956 | 2 | 36.01 | 36.01 |
| 91.37 | 216.55 | 289.44 | 0.505912 | 3 | 37.62 | 38.03 |
| 95.06 | 260.97 | 286.91 | 0.509010 | 3 | 36.98 | 37.94 |
| 56.76 | 276.15 | 286.26 | 0.535010 | 3 | 34.65 | 37.91 |
| 98.46 | 271.71 | 281.34 | 0.555018 | 2 | 29.86 | 36.98 |
| 101.16 | 273.28 | 285.74 | 0.592564 | 6 | 26.15 | 37.85 |
| 101.48 | 274.68 | 293.35 | 0.519824 | 5 | 40.88 | 37.73 |
| 103.61 | 265.51 | 292.68 | 0.589242 | 5 | 40.20 | 37.63 |
| 105.35 | 242.20 | 297.28 | 0.845576 | 6 | 43.46 | 37.10 |
| 107.10 | 254.37 | 298.39 | 0.523793 | 6 | 44.03 | 36.49 |
| 109.48 | 267.18 | 300.49 | 0.791948 | 6 | 44.61 | 36.50 |
| 110.67 | 242.06 | 304.90 | 0.752124 | 6 | 45.85 | 35.77 |
| 112.48 | 216.50 | 308.56 | 0.744431 | 6 | 45.56 | 35.41 |
| 114.32 | 229.44 | 303.26 | 0.707736 | 6 | 45.34 | 35.35 |
| 115.18 | 272.24 | 310.14 | 0.612017 | 6 | 45.31 | 31.34 |
| 116.07 | 217.46 | 313.35 | 0.63981A | 6 | 44.14 | 35.34 |
| 120.00 | 210.97 | 316.00 | 0.637493 | 6 | 43.63 | 35.36 |
| 121.97 | 209.05 | 318.38 | 0.630582 | 5 | 40.68 | 35.62 |
| 123.97 | 203.94 | 320.47 | 0.602020 | 5 | 39.51 | 35.70 |
| 125.93 | 196.44 | 318.23 | 0.580552 | 5 | 41.24 | 35.57 |
| 126.03 | 219.39 | 344.57 | 0.609750 | 3 | 17.46 | 30.73 |
| 126.32 | 256.67 | 375.15 | 0.662129 | 4 | 7.17 | 20.06 |

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TABLE VI-49. ROCK3 OUTPUT

RUN NO. 19 08/07/59 16.9 MHZ V POLARIZATION

| ZENITH ANGLE (deg) | BRIGHTNESS TEMPERATURE (deg.K) | WATER TEMPERATURE (deg.K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART IMAGINARY PART |
|--------------------------|--------------------------------------|---------------------------------|------------|------------|--|
| 91.48 | 240.11 | 246.27 | 0.541000 | 2 | 34.61 37.91 |
| 91.37 | 255.16 | 287.42 | 0.800177 | 2 | 36.14 36.01 |
| 95.05 | 267.54 | 285.50 | 0.924177 | 3 | 34.00 37.83 |
| 96.76 | 274.54 | 285.13 | 0.946319 | 3 | 33.55 37.77 |
| 98.45 | 272.09 | 282.92 | 0.951297 | 3 | 30.51 37.16 |
| 100.16 | 271.39 | 283.53 | 0.961472 | 3 | 31.99 37.50 |
| 101.85 | 247.33 | 265.40 | 0.719244 | 4 | 33.02 37.81 |
| 103.51 | 245.67 | 292.78 | 0.869301 | 3 | 39.48 37.87 |
| 105.35 | 242.91 | 294.28 | 0.869507 | 6 | 43.99 35.91 |
| 107.10 | 213.49 | 257.73 | 0.73927 | 6 | 43.70 37.02 |
| 108.86 | 246.06 | 299.63 | 0.71930 | 6 | 44.59 36.66 |
| 110.67 | 241.61 | 305.18 | 0.762181 | 6 | 45.87 35.74 |
| 112.48 | 234.55 | 337.19 | 0.733430 | 6 | 45.43 35.52 |
| 114.32 | 227.80 | 307.17 | 0.757316 | 6 | 45.55 35.38 |
| 116.15 | 224.47 | 314.01 | 0.684590 | 6 | 43.82 35.36 |
| 119.07 | 221.72 | 316.49 | 0.664719 | 5 | 40.75 35.61 |
| 120.00 | 211.34 | 315.32 | 0.638573 | 5 | 43.12 35.61 |
| 121.97 | 268.59 | 322.19 | 0.621893 | 5 | 39.74 35.69 |
| 122.37 | 203.97 | 323.41 | 0.504337 | 5 | 37.86 35.76 |
| 124.03 | 270.37 | 325.73 | 0.599800 | 5 | 35.49 35.60 |
| 124.14 | 275.65 | 335.32 | 0.598587 | 4 | 25.23 34.23 |
| 130.32 | 256.26 | 376.21 | 0.663999 | 4 | 7.05 19.84 |

TABLE VI-50. ROCK3 OUTPUT

RUN NO. 19 08/07/69 16.9 GHz V POLARIZATION

ZENITH
ANGLE
(DEG.)

BRIGHTNESS
TEMPERATURE
(DEG. K)

| | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART IMAGINARY PART |
|--------|----------------------------------|------------|------------|---|
| 91.68 | 242.27 | 287.20 | 0.545586 | 35.35 37.97 |
| 91.47 | 256.49 | 294.36 | 0.84125 | 37.10 38.03 |
| 91.35 | 268.13 | 285.78 | 0.906703 | 34.18 37.86 |
| 91.26 | 274.40 | 284.92 | 0.947302 | 33.34 37.74 |
| 91.19 | 269.19 | 280.70 | 0.948673 | 36.56 36.57 |
| 100.16 | 283.79 | 281.81 | 0.946065 | 30.30 37.10 |
| 101.58 | 280.61 | 285.26 | 0.919241 | 36.66 37.91 |
| 101.5 | 281.21 | 284.83 | 0.820508 | 25.19 37.96 |
| 104.3 | 246.85 | 297.21 | 0.857992 | 38.30 38.01 |
| 107.10 | 251.71 | 295.26 | 0.824192 | 42.23 37.45 |
| 106.83 | 245.67 | 294.59 | 0.791963 | 45.13 35.85 |
| 111.47 | 219.45 | 301.01 | 0.761441 | 45.09 35.40 |
| 112.94 | 212.65 | 306.70 | 0.732991 | 45.04 35.40 |
| 114.32 | 227.52 | 301.81 | 0.707193 | 45.62 35.40 |
| 114.19 | 220.14 | 308.92 | 0.681311 | 45.61 35.40 |
| 114.07 | 214.24 | 310.84 | 0.656137 | 45.11 35.33 |
| 127.60 | 214.52 | 318.63 | 0.641670 | 40.94 35.60 |
| 121.37 | 208.53 | 320.21 | 0.621914 | 39.72 35.69 |
| 123.97 | 271.83 | 320.15 | 0.601663 | 35.77 35.69 |
| 127.03 | 198.10 | 322.71 | 0.585674 | 37.59 35.79 |
| 128.14 | 205.20 | 335.06 | 0.588153 | 25.48 34.31 |
| 130.32 | 249.66 | 371.26 | 0.634865 | 7.70 20.97 |

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TABLE VI-51. ROCK3 OUTPUT

TABLE VI-52. ROCK3 OUTPUT

| RUN NO. | ZENITH ANGLF | BRIGHTNESS TEMPERATURE (deg.K) | WATER TEMPERATURE (deg.K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART | PERMITTIVITY IMAGINARY PART |
|---------|--------------|--------------------------------|---------------------------|------------|------------|------------------------|-----------------------------|
| 21 | 08/78/69 | 16.5 GHz | V POLARIZATION | | | | |
| 130.32 | 112.67 | 214.67 | 294.92 | 0.93771 | 2 | 33.25 | 37.73 |
| | 117.48 | 227.37 | 295.28 | 0.93957 | 2 | 34.30 | 37.67 |
| | 114.32 | 222.91 | 301.53 | 0.94019 | 2 | 30.74 | 37.22 |
| | 114.08 | 219.57 | 307.02 | 0.94095 | 2 | 29.07 | 36.74 |
| | 114.07 | 212.97 | 308.16 | 0.94591 | 4 | 21.13 | 32.10 |
| | 121.00 | 210.39 | 313.93 | 0.93743 | 6 | 22.14 | 33.47 |
| | 121.97 | 211.89 | 311.77 | 0.94298 | 6 | 27.59 | 36.22 |
| | 121.97 | 210.32 | 324.72 | 0.95643 | 5 | 25.67 | 35.39 |
| | 124.03 | 227.54 | 337.82 | 0.95802 | 4 | 25.63 | 35.39 |
| | 128.14 | 223.79 | 347.95 | 0.91789 | 4 | 26.56 | 34.57 |
| | 271.86 | 386.46 | 0.68209 | 6 | 35.72 | 37.06 | |

RUN NO. 23 06/08/69 16.5 GHz V POLARIZATION

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMPERATURE (DEG. K) | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | PERMEABILITY REAL PART | IMAGINARY PART |
|-----------------------|---------------------------------------|----------------------------------|------------|------------|---------------------------|----------------|
| 91.68 | 246.09 | 290.55 | 0.566972 | 3 | 38.60 | 37.99 |
| 92.17 | 242.38 | 281.39 | 0.746295 | 2 | 36.39 | 37.88 |
| 93.06 | 260.84 | 281.33 | 0.693048 | 2 | 29.86 | 35.90 |
| 94.76 | 264.99 | 279.22 | 0.954544 | 2 | 27.81 | 35.31 |
| 95.46 | 257.97 | 271.28 | 0.96572 | 4 | 21.24 | 32.08 |
| 100.16 | 258.10 | 272.89 | 0.95944 | 4 | 22.27 | 33.56 |
| 101.88 | 218.01 | 277.49 | 0.90069 | 3 | 26.21 | 35.66 |
| 103.61 | 242.04 | 269.41 | 0.868820 | 5 | 37.33 | 38.03 |
| 105.35 | 215.14 | 289.97 | 0.856484 | 5 | 38.10 | 39.02 |
| 107.10 | 245.76 | 287.59 | 0.877924 | 5 | 36.01 | 39.01 |
| 108.88 | 241.67 | 294.34 | 0.772094 | 6 | 41.61 | 37.59 |
| 110.67 | 240.50 | 305.16 | 0.722161 | 5 | 45.67 | 35.74 |
| 112.46 | 230.87 | 303.38 | 0.72592 | 6 | 45.67 | 35.99 |
| 114.32 | 230.55 | 313.27 | 0.799017 | 6 | 44.16 | 35.14 |
| 115.18 | 223.62 | 314.37 | 0.644867 | 6 | 43.64 | 35.37 |
| 116.07 | 220.61 | 316.39 | 0.644817 | 5 | 40.68 | 35.42 |
| 120.00 | 216.04 | 322.05 | 0.644493 | 5 | 38.17 | 35.77 |
| 121.97 | 206.50 | 319.16 | 0.60755 | 5 | 40.35 | 35.63 |
| 123.97 | 206.31 | 324.46 | 0.607019 | 5 | 35.99 | 35.01 |
| 126.03 | 202.44 | 327.00 | 0.591714 | 4 | 33.51 | 35.72 |
| 128.16 | 212.55 | 340.48 | 0.598898 | 3 | 20.63 | 32.65 |
| 130.32 | 238.25 | 378.58 | 0.6668161 | 6.79 | 19.39 | |

RUN NO. 25 09/12/69 14.3 GHZ V POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (R.G.K) | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | REAL PART IMAGINARY PART |
|---------------------------|--------------------------------------|----------------------------------|------------|------------|-----------------------------|
| 91.48 | 226.9 | 277.52 | 0.997629 | 2 | 25.13 |
| 91.37 | 223.34 | 287.79 | 0.771321 | 2 | 29.32 |
| 91.09 | 216.92 | 279.75 | 0.945195 | 2 | 27.65 |
| 91.76 | 245.39 | 279.25 | 0.935610 | 2 | 35.33 |
| 91.46 | 261.97 | 275.92 | 0.941726 | 3 | 27.98 |
| 101.16 | 245.08 | 273.29 | 0.933324 | 2 | 24.33 |
| 101.08 | 240.36 | 285.70 | 0.919267 | 4 | 35.26 |
| 101.61 | 262.61 | 289.92 | 0.99714 | 3 | 37.66 |
| 101.32 | 242.76 | 284.15 | 0.990051 | 3 | 34.73 |
| 107.10 | 247.84 | 294.33 | 0.974432 | 6 | 37.91 |
| 107.99 | 243.63 | 297.06 | 0.727037 | 6 | 41.59 |
| 110.67 | 231.11 | 295.16 | 0.742320 | 7 | 42.16 |
| 112.48 | 227.74 | 299.12 | 0.734441 | 4 | 44.94 |
| 114.32 | 227.51 | 303.99 | 0.707793 | 5 | 45.23 |
| 116.18 | 217.82 | 305.77 | 0.687062 | 6 | 45.46 |
| 116.07 | 212.73 | 308.75 | 0.656977 | 6 | 45.63 |
| 120.00 | 205.08 | 307.79 | 0.633664 | 6 | 45.77 |
| 121.97 | 203.88 | 314.16 | 0.616140 | 5 | 43.74 |
| 123.97 | 197.37 | 314.24 | 0.595000 | 5 | 43.70 |
| 125.03 | 174.95 | 320.10 | 0.582355 | 5 | 39.81 |
| 126.14 | 210.62 | 340.01 | 0.594830 | 4 | 21.02 |
| 130.32 | 254.80 | 375.90 | 0.663274 | 4 | 29.93 |

TABLE VI-54. ROCK3 OUTPUT

RUN NO. 27 08/12/69 16.3 GHZ V POLARIZATION

| ZENITH ANGLE (DEG) | BRIGHTNESS TEMPERATURE (DEG.K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART | PERMITTIVITY [IMAGINARY PART] |
|--------------------|--------------------------------|---------------------------|------------|------------|-----------|-------------------------------|
| 91.48 | 260.90 | 245.75 | 0.941190 | 2 | 34.16 | 37.65 |
| 93.97 | 243.34 | 245.54 | 0.795563 | 2 | 34.73 | 37.81 |
| 95.06 | 254.59 | 263.58 | 0.898627 | 2 | 31.55 | 37.91 |
| 96.76 | 270.60 | 281.25 | 0.341681 | 2 | 30.44 | 37.16 |
| 99.45 | 265.77 | 277.79 | 0.945577 | 3 | 25.47 | 35.78 |
| 100.16 | 265.77 | 280.00 | 0.939664 | 1 | 28.26 | 35.57 |
| 101.48 | 261.61 | 281.04 | 0.919369 | 2 | 29.56 | 35.49 |
| 101.61 | 259.72 | 284.98 | 0.871225 | 4 | 33.41 | 37.59 |
| 105.35 | 233.27 | 285.38 | 0.867059 | 5 | 36.38 | 37.88 |
| 107.10 | 210.26 | 293.51 | 0.424577 | 5 | 41.07 | 37.70 |
| 109.06 | 264.74 | 237.92 | 0.792031 | 6 | 63.80 | 36.78 |
| 117.67 | 236.96 | 239.15 | 0.751552 | 6 | 44.34 | 36.75 |
| 118.49 | 213.87 | 305.32 | 0.731553 | 6 | 49.84 | 35.59 |
| 118.42 | 227.64 | 308.97 | 0.707216 | 6 | 49.57 | 35.39 |
| 118.18 | 222.33 | 311.35 | 0.158254 | 6 | 45.04 | 35.02 |
| 118.07 | 217.22 | 314.02 | 0.660154 | 6 | 43.61 | 35.36 |
| 120.00 | 212.61 | 316.44 | 0.639553 | 9 | 42.44 | 35.47 |
| 121.97 | 215.33 | 315.69 | 0.617612 | 5 | 42.90 | 35.43 |
| 123.97 | 215.24 | 323.51 | 0.605894 | 5 | 36.77 | 35.81 |
| 125.03 | 197.30 | 322.61 | 0.585551 | 5 | 37.68 | 35.79 |
| 126.14 | 220.45 | 346.57 | 0.616620 | 4 | 16.14 | 29.86 |
| 130.32 | 259.90 | 380.08 | 0.670391 | 3 | 6.66 | 19.09 |

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TABLE VI-55. ROCK3 OUTPUT

RUN NO. 30 08/12/69 16.5 GHz V POLARIZATION

| ZENITH ANGLE (deg.) | BRIGHTNESS TEMPERATURE (deg. K) | WATER TEMPERATURE (deg. K) | EMISSIVITY | ITERATIONS | REAL PART IMAGINARY PART |
|---------------------|---------------------------------|----------------------------|------------|------------|--------------------------|
| 91.68 | 212.20 | 282.19 | 0.527362 | 2 | 30.67 37.20 |
| 93.37 | 254.57 | 284.55 | 0.850111 | 2 | 35.97 36.50 |
| 95.06 | 210.24 | 285.78 | 0.907272 | 3 | 34.38 37.68 |
| 96.75 | 275.42 | 285.59 | 0.949250 | 3 | 34.00 37.63 |
| 98.46 | 249.65 | 280.70 | 0.948673 | 1 | 28.56 36.97 |
| 100.16 | 248.26 | 280.57 | 0.939979 | 2 | 29.10 36.79 |
| 101.86 | 244.68 | 284.92 | 0.919450 | 3 | 30.41 37.13 |
| 103.51 | 246.18 | 286.00 | 0.893711 | 1 | 28.56 36.57 |
| 105.35 | 215.60 | 286.04 | 0.859014 | 5 | 36.34 38.02 |
| 107.10 | 212.42 | 295.34 | 0.824173 | 6 | 42.29 37.44 |
| 108.88 | 246.49 | 296.99 | 0.791945 | 6 | 66.31 36.78 |
| 110.67 | 218.71 | 300.19 | 0.761477 | 6 | 64.81 35.55 |
| 112.48 | 231.20 | 301.66 | 0.732462 | 6 | 65.23 35.32 |
| 114.32 | 224.53 | 301.50 | 0.703249 | 6 | 49.69 35.98 |
| 116.18 | 221.70 | 307.17 | 0.681649 | 6 | 49.55 35.38 |
| 118.07 | 214.74 | 307.91 | 0.655790 | 6 | 49.38 35.35 |
| 120.00 | 210.43 | 313.94 | 0.637141 | 6 | 44.05 35.34 |
| 121.97 | 206.26 | 316.13 | 0.617600 | 5 | 62.64 35.45 |
| 123.97 | 206.03 | 322.91 | 0.605763 | 5 | 36.86 35.10 |
| 125.03 | 198.91 | 322.82 | 0.585818 | 5 | 37.49 35.19 |
| 126.14 | 209.83 | 329.33 | 0.595969 | 5 | 22.47 33.26 |
| 128.32 | 251.26 | 372.14 | 0.656568 | 7.97 | 20.75 |

TABLE VI-56. ROCK3 OUTPUT

RUN NO. 32 08/13/69 16.9 GHZ V POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG. K) | MATTER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | REAL PART | IMAGINARY PART |
|---------------------|---------------------------------|-----------------------------|------------|------------|-----------|----------------|
| 91.68 | 26.59 | 292.70 | 0.542733 | 3 | 40.38 | 37.01 |
| 91.37 | 25.22 | 203.58 | 0.603198 | 3 | 36.84 | 36.03 |
| 95.06 | 29.32 | 284.99 | 0.904135 | 3 | 33.32 | 37.76 |
| 98.76 | 23.62 | 283.47 | 0.944755 | 3 | 31.93 | 37.49 |
| 98.46 | 26.24 | 277.12 | 0.947437 | 2 | 27.72 | 36.27 |
| 100.16 | 29.95 | 281.17 | 0.9460781 | 2 | 29.58 | 35.93 |
| 101.45 | 24.75 | 284.48 | 0.19274 | 4 | 32.92 | 37.68 |
| 103.41 | 24.42 | 287.24 | 0.849870 | 5 | 37.44 | 38.03 |
| 105.35 | 26.89 | 289.25 | 0.816922 | 5 | 36.53 | 38.03 |
| 107.10 | 20.23 | 297.78 | 0.725697 | 6 | 36.60 | 37.98 |
| 108.88 | 26.42 | 297.16 | 0.72137 | 6 | 43.39 | 37.12 |
| 110.67 | 263.02 | 304.06 | 0.761692 | 5 | 45.77 | 35.89 |
| 112.46 | 23.25 | 302.29 | 0.712521 | 6 | 45.45 | 35.17 |
| 114.32 | 223.56 | 313.06 | 0.709671 | 6 | 44.27 | 35.33 |
| 115.18 | 225.23 | 311.41 | 0.582775 | 6 | 44.93 | 35.32 |
| 116.07 | 211.92 | 312.75 | 0.659451 | 6 | 44.40 | 35.33 |
| 120.00 | 214.69 | 315.57 | 0.636856 | 5 | 42.92 | 35.43 |
| 121.97 | 211.67 | 320.23 | 0.621937 | 5 | 39.71 | 35.69 |
| 123.97 | 211.60 | 315.07 | 0.597547 | 5 | 42.67 | 35.43 |
| 125.03 | 218.78 | 323.74 | 0.496163 | 4 | 30.76 | 35.46 |
| 128.14 | 229.98 | 350.91 | 0.625108 | 4 | 13.73 | 20.02 |
| 130.32 | 252.16 | 371.48 | 0.655289 | 4 | 7.66 | 20.92 |

TABLE VI-57. ROCK3 OUTPUT

RUN NO. 33 08/14/69 9.5 GHz V-POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG. K) | WATER TEMPERATURE (DEG. K) | EMISSIVITY | ITERATIONS | REAL PART PERMITTIVITY | IMAGINARY PART |
|---------------------------|---------------------------------------|----------------------------------|------------|------------|---------------------------|----------------|
| 91.68 | 220.68 | 215.26 | 0.605827 | 6 | 55.42 | 33.1* |
| 93.47 | 216.96 | 300.45 | 0.44621 | 5 | 58.80 | 32.7 |
| 95.06 | 293.30 | 297.35 | 0.95991 | 5 | 58.67 | 33.64 |
| 96.76 | 277.57 | 292.26 | 0.98341 | 5 | 58.67 | 33.25 |
| 98.46 | 303.54 | 307.43 | 0.975697 | 6 | 58.36 | 32.02 |
| 100.16 | 371.08 | 310.53 | 0.951201 | 6 | 57.59 | 32.16 |
| 101.88 | 294.22 | 311.56 | 0.319554 | 6 | 57.25 | 32.28 |
| 103.61 | 216.81 | 314.35 | 0.485351 | 6 | 56.17 | 32.77 |
| 104.35 | 216.32 | 284.58 | 0.862293 | 6 | 51.63 | 38.16 |
| 107.10 | 257.07 | 294.39 | 0.808921 | 5 | 57.40 | 35.01 |
| 109.88 | 254.45 | 304.01 | 0.774760 | 5 | 58.41 | 32.27 |
| 110.67 | 242.74 | 305.53 | 0.747057 | 5 | 58.05 | 32.10 |
| 112.48 | 240.46 | 310.59 | 0.720097 | 6 | 57.57 | 32.17 |
| 114.32 | 217.18 | 300.25 | 0.607454 | 5 | 58.74 | 32.99 |
| 114.18 | 217.41 | 280.70 | 0.664010 | 1 | 47.74 | 40.14 |
| 114.07 | 207.69 | 273.19 | 0.647281 | 5 | 40.73 | 40.80 |
| 120.00 | 216.64 | 286.58 | 0.613299 | 4 | 53.35 | 38.01 |
| 121.97 | 200.32 | 278.98 | 0.596694 | 2 | 46.69 | 40.35 |
| 123.97 | 190.91 | 263.19 | 0.573324 | 3 | 50.59 | 39.27 |
| 125.03 | 223.24 | 344.79 | 0.574627 | 5 | 30.39 | 40.71 |
| 125.14 | 245.92 | 391.02 | 0.599046 | 5 | 7.86 | 29.87 |
| 130.32 | 375.46 | 459.29 | 0.599839 | 5 | 5.13 | 26.21 |

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| RUN NO. | 08/14/69 | 16.5 GHz | V POLARIZATION |
|---------------------------|---------------------------------------|----------------------------------|----------------|
| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (KELVIN) | WATER TEMPERATURE (DEG. K) | EMISSIVITY |
| 91.68 | 278.85 | 293.13 | 0.561794 |
| 91.37 | 271.60 | 284.57 | 0.789465 |
| 91.06 | 271.64 | 281.59 | 0.800216 |
| 90.76 | 240.57 | 284.09 | 0.94232 |
| 90.45 | 281.45 | 287.71 | 0.97147 |
| 101.16 | 246.85 | 292.57 | 0.965034 |
| 101.08 | 274.30 | 294.26 | 0.919974 |
| 101.41 | 278.35 | 293.83 | 0.89163 |
| 105.15 | 276.73 | 300.56 | 0.845645 |
| 107.10 | 270.09 | 301.69 | 0.724075 |
| 108.84 | 260.42 | 307.21 | 0.731937 |
| 112.67 | 250.46 | 298.31 | 0.71535 |
| 112.48 | 246.26 | 304.31 | 0.732895 |
| 116.32 | 240.17 | 307.13 | 0.716679 |
| 116.18 | 232.44 | 309.26 | 0.661431 |
| 116.07 | 227.64 | 313.19 | 0.660242 |
| 127.00 | 220.76 | 314.26 | 0.638264 |
| 121.97 | 217.51 | 320.78 | 0.622549 |
| 123.37 | 211.77 | 323.77 | 0.603184 |
| 124.03 | 214.14 | 331.12 | 0.596583 |
| 128.19 | 229.94 | 349.09 | 0.620596 |
| 130.32 | 280.06 | 392.95 | 0.6687126 |

ITERATIONS REAL PART IMAGINARY PART

| | | |
|---|-------|-------|
| 4 | 40.71 | 37.76 |
| 3 | 33.11 | 37.71 |
| 3 | 32.05 | 37.51 |
| 3 | 32.53 | 37.61 |
| 4 | 35.36 | 37.97 |
| 5 | 40.35 | 37.81 |
| 5 | 41.55 | 37.61 |
| 5 | 41.24 | 37.67 |
| 6 | 44.94 | 36.48 |
| 6 | 45.35 | 35.24 |
| 6 | 44.81 | 35.55 |
| 6 | 43.99 | 36.91 |
| 6 | 45.40 | 35.86 |
| 6 | 45.77 | 35.47 |
| 6 | 45.57 | 35.39 |
| 6 | 43.04 | 35.35 |
| 5 | 43.32 | 35.39 |
| 5 | 39.25 | 35.72 |
| 5 | 37.27 | 35.10 |
| 4 | 29.37 | 32.22 |
| 4 | 24.70 | 28.00 |
| 5 | 5.84 | 17.29 |

TABLE VI-59. ROCK3 OUTPUT

RUN NO. 101 07/21/69 9.5 GHz V POLARIZATION

| ZENITH ANGLE (UFG) | BRIGHTNESS TEMPERATURE (DEG.K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | REAL PART PERMITTIVITY | IMAGINARY PART |
|--------------------|--------------------------------|---------------------------|------------|------------|------------------------|----------------|
| 91.68 | 215.15 | 302.19 | 0.619327 | 5 | 50.67 | 32.96 |
| 93.37 | 214.90 | 303.41 | 0.864592 | 6 | 56.85 | 32.35 |
| 95.06 | 218.75 | 301.72 | 0.959637 | 6 | 50.86 | 32.65 |
| 96.76 | 218.28 | 299.50 | 0.933574 | 6 | 50.72 | 33.16 |
| 98.46 | 216.76 | 290.36 | 0.970412 | 5 | 55.69 | 36.92 |
| 100.15 | 211.72 | 290.05 | 0.945550 | 5 | 55.51 | 36.69 |
| 101.84 | 276.27 | 291.58 | 0.913876 | 5 | 56.12 | 36.01 |
| 101.61 | 270.46 | 294.46 | 0.879353 | 5 | 57.53 | 34.86 |
| 105.35 | 259.09 | 299.50 | 0.843391 | 5 | 56.79 | 35.60 |
| 107.10 | 252.74 | 296.90 | 0.809556 | 5 | 58.25 | 33.98 |
| 108.88 | 246.41 | 302.44 | 0.778151 | 5 | 55.87 | 32.51 |
| 110.67 | 240.26 | 280.87 | 0.746208 | 2 | 48.30 | 37.93 |
| 112.46 | 214.77 | 284.72 | 0.714917 | 4 | 51.86 | 38.75 |
| 114.32 | 220.30 | 287.73 | 0.686304 | 4 | 54.21 | 37.52 |
| 115.18 | 215.49 | 241.79 | 0.757031 | 14 | 15.77 | 26.53 |
| 118.07 | 206.10 | 262.60 | 0.667311 | 8 | 30.01 | 38.31 |
| 120.00 | 219.77 | 281.16 | 0.616051 | 2 | 48.77 | 39.86 |
| 121.97 | 216.59 | 301.75 | 0.593374 | 5 | 58.66 | 32.65 |
| 123.97 | 226.19 | 324.09 | 0.582477 | 6 | 50.33 | 35.90 |
| 126.03 | 279.20 | 396.61 | 0.619950 | 6 | 7.1 | 29.04 |
| 128.16 | 290.63 | 426.01 | 0.611721 | 6 | 5.79 | 27.01 |
| 130.32 | 300.78 | 440.26 | 0.597901 | 7 | 5.33 | 26.39 |

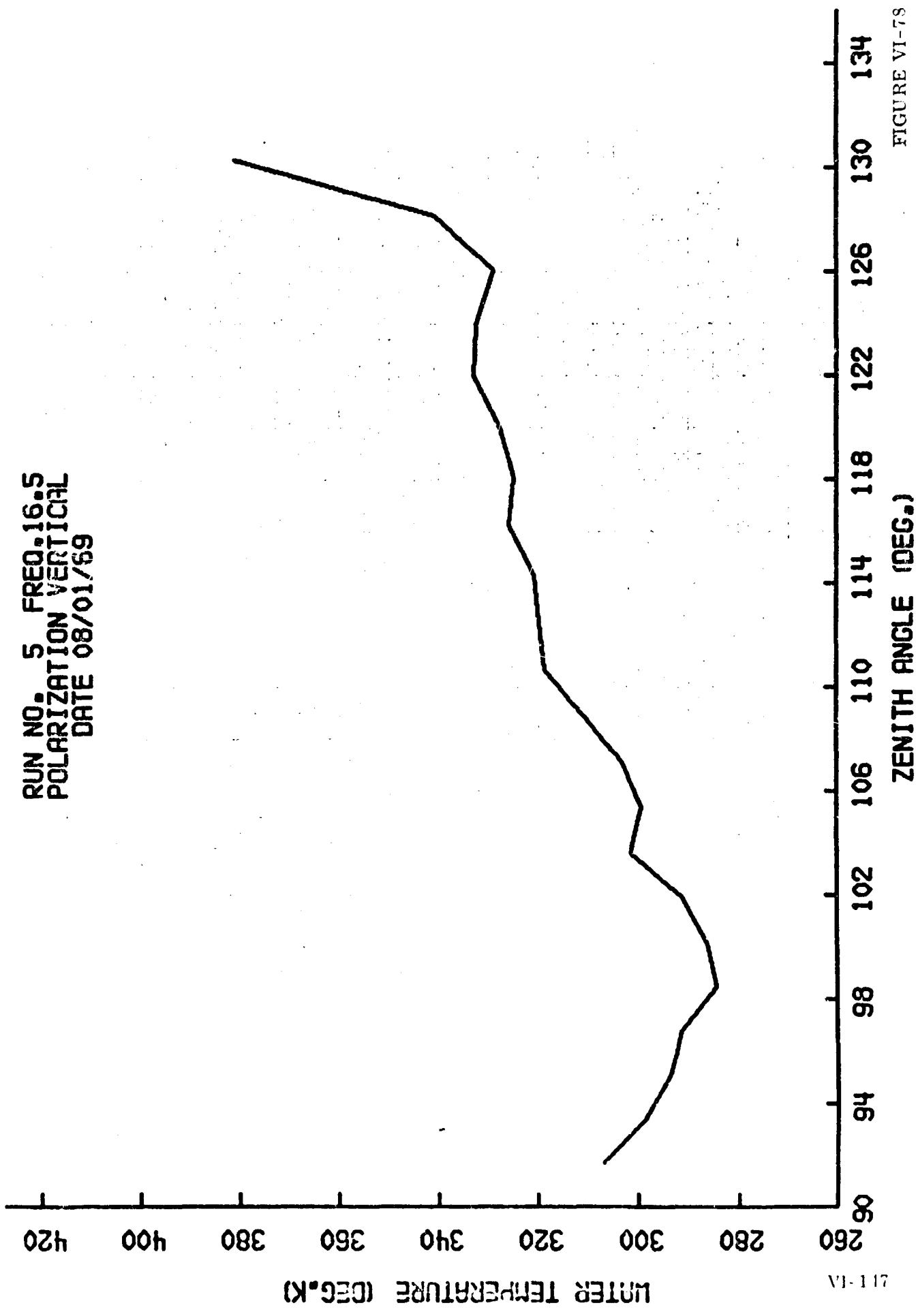
1

RUN NO. 201 07/17/69 9.5 GHz V POLARIZATION

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | WATER TEMPERATURE (DEG.K) | EMISSIVITY | ITERATIONS | PERMITTIVITY REAL PART IMAGINARY PART |
|---------------------------|--------------------------------------|---------------------------------|------------|------------|--|
| 91.68 | 392.19 | 425.87 | 0.393691 | 9 | 5.61 6.73 25.76 |
| 91.37 | 333.05 | 402.06 | 0.637110 | 14 | 2.38 6.73 28.38 |
| 95.06 | 330.32 | 351.52 | 0.673940 | 14 | 24.15 6.73 39.87 |
| 95.76 | 323.03 | 327.37 | 0.971237 | 6 | 67.57 58.57 37.17 |
| 91.46 | 370.50 | 303.91 | 0.975324 | 6 | 58.42 58.42 32.22 |
| 107.15 | 270.47 | 298.50 | 0.948692 | 5 | 58.56 58.56 33.47 |
| 101.88 | 281.81 | 295.04 | 0.915559 | 5 | 58.23 58.23 34.00 |
| 103.51 | 274.13 | 297.27 | 0.Rin354 | 5 | 58.13 58.13 33.96 |
| 105.35 | 274.61 | 310.29 | 0.851037 | 6 | 54.17 54.17 33.82 |
| 107.10 | 279.20 | 323.13 | 0.R17811 | 6 | 51.05 51.05 35.53 |
| 108.48 | 273.75 | 328.46 | 0.7R6342 | 6 | 46.36 46.36 37.72 |
| 110.67 | 248.11 | 315.34 | 0.751613 | 6 | 55.72 55.72 33.00 |
| 112.48 | 252.37 | 317.79 | 0.722947 | 6 | 54.36 54.36 33.73 |
| 114.32 | 257.00 | 319.98 | 0.695967 | 6 | 53.18 53.18 34.38 |
| 115.18 | 225.20 | 283.26 | 0.661879 | 3 | 50.65 50.65 39.24 |
| 114.07 | 224.07 | 290.41 | 0.635547 | 5 | 55.72 55.72 36.50 |
| 127.00 | 225.71 | 300.34 | 0.614379 | 5 | 58.79 58.79 32.96 |
| 121.37 | 230.29 | 314.18 | 0.598561 | 5 | 56.24 56.24 32.73 |
| 123.97 | 237.54 | 333.14 | 0.516645 | 6 | 42.30 42.30 39.16 |
| 126.03 | 286.93 | 400.52 | 0.622079 | 6 | 6.85 6.85 28.55 |
| 128.14 | 296.04 | 421.26 | 0.611996 | 6 | 5.75 5.75 26.95 |
| 130.32 | 303.93 | 439.36 | 0.597844 | 7 | 5.34 5.34 26.40 |

TABLE VI-61. ROCK3 OUTPUT

RUN NO. 5 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/01/69



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FIGURE VI-78

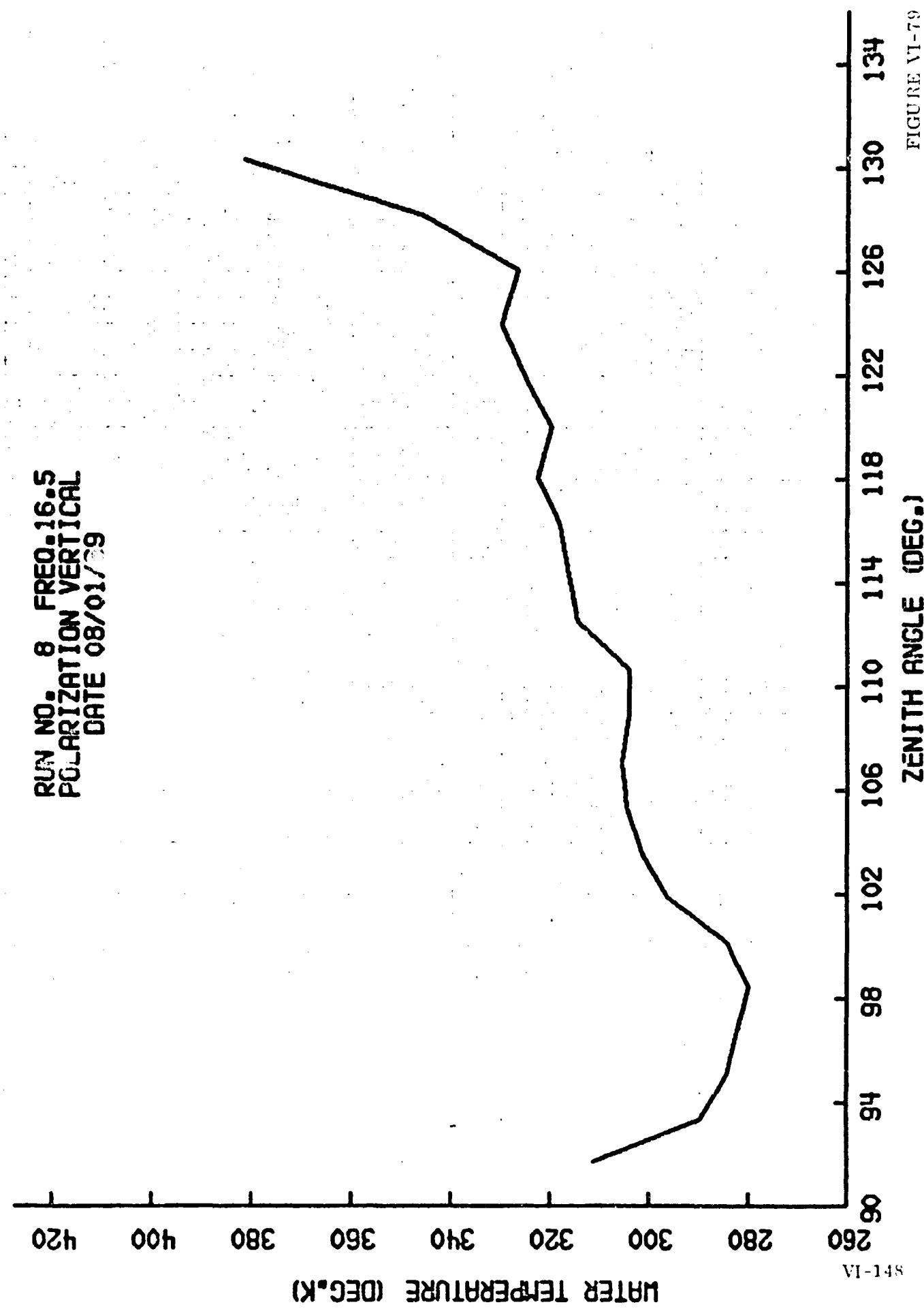


FIGURE VI-79

FIGURE VI-80

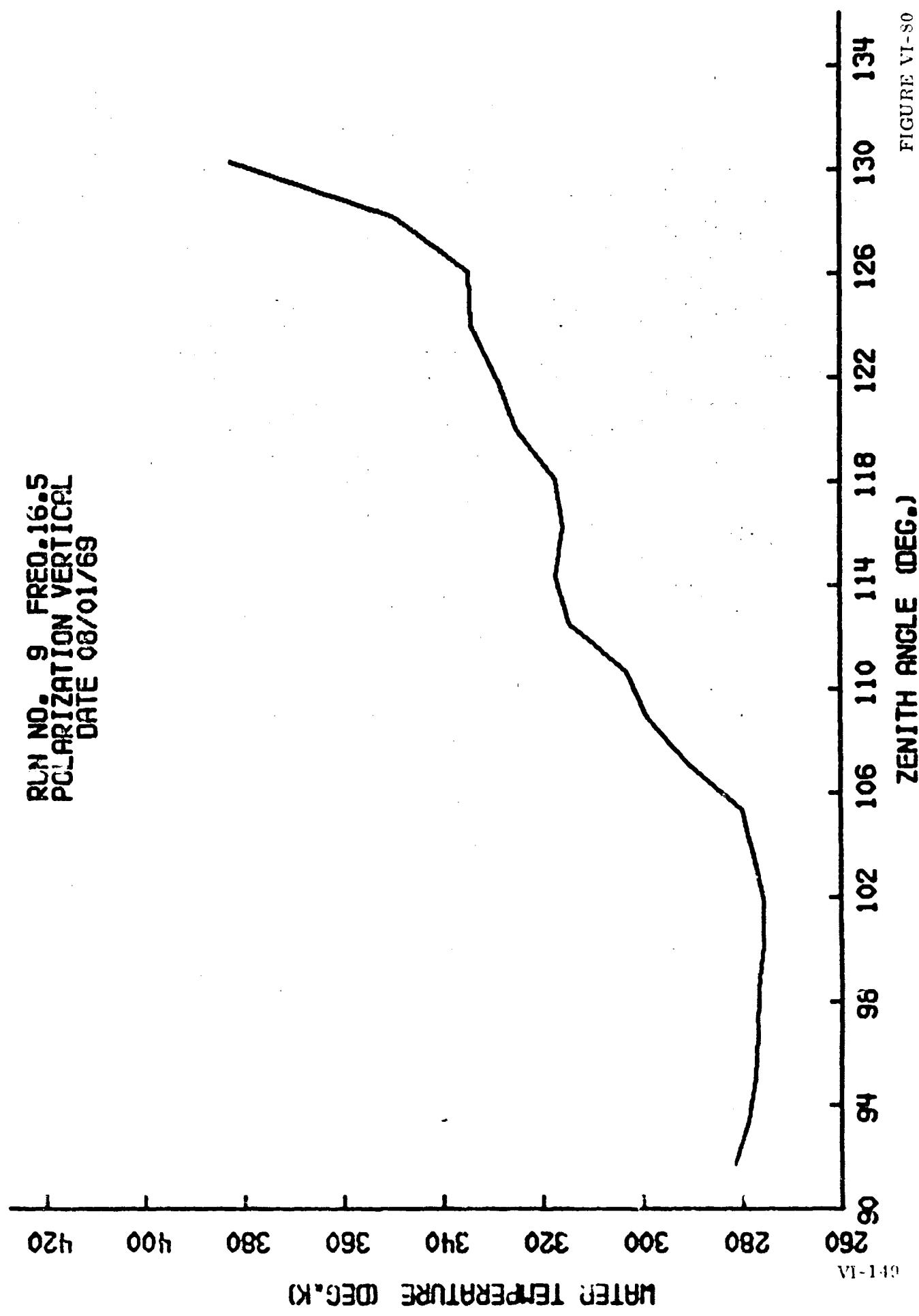
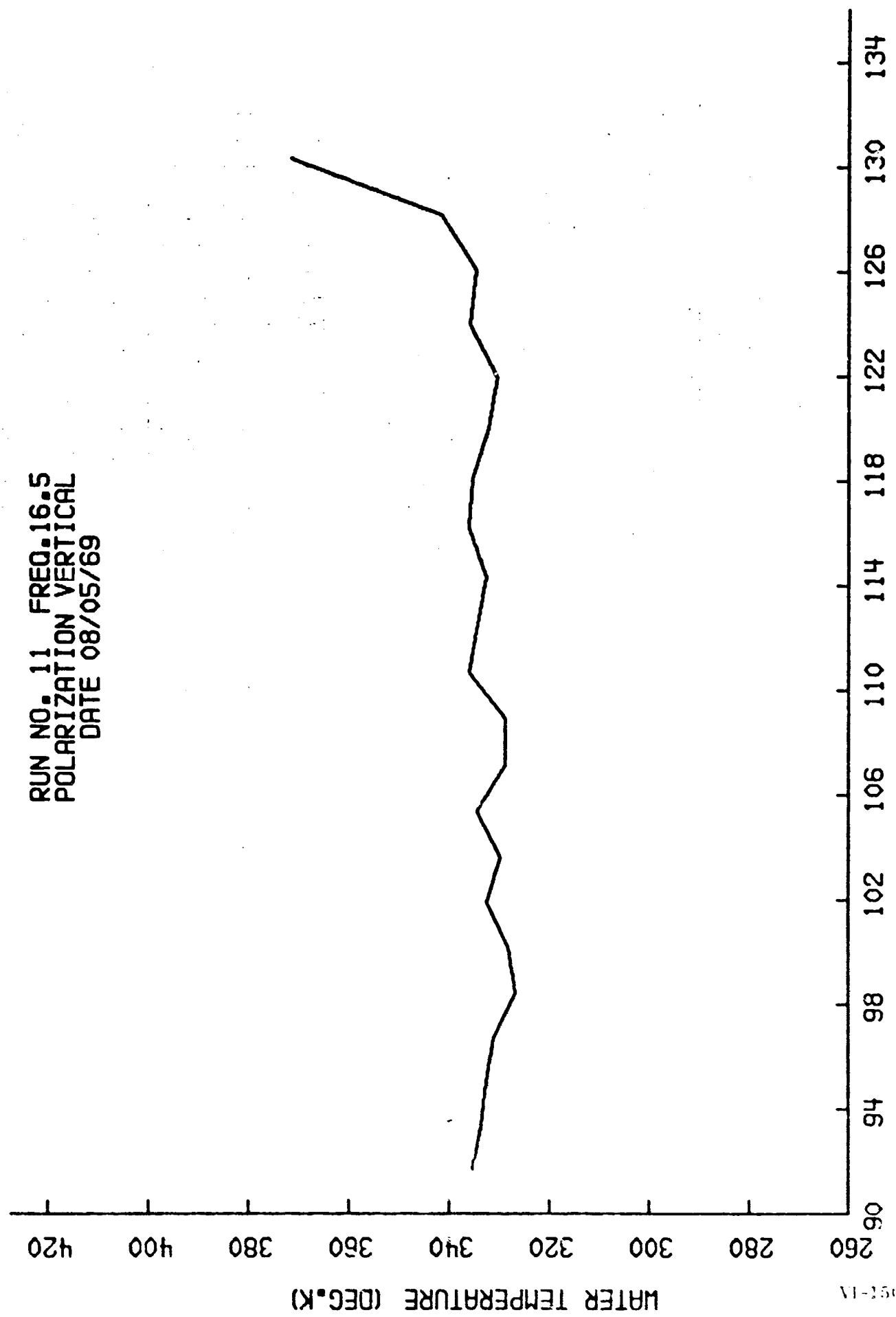


FIGURE VI-81

ZENITH ANGLE (DEG.)



RUN NO. 13 FREQ. 16.5
POLARIZATION VERTICAL
DATE 03/06/69

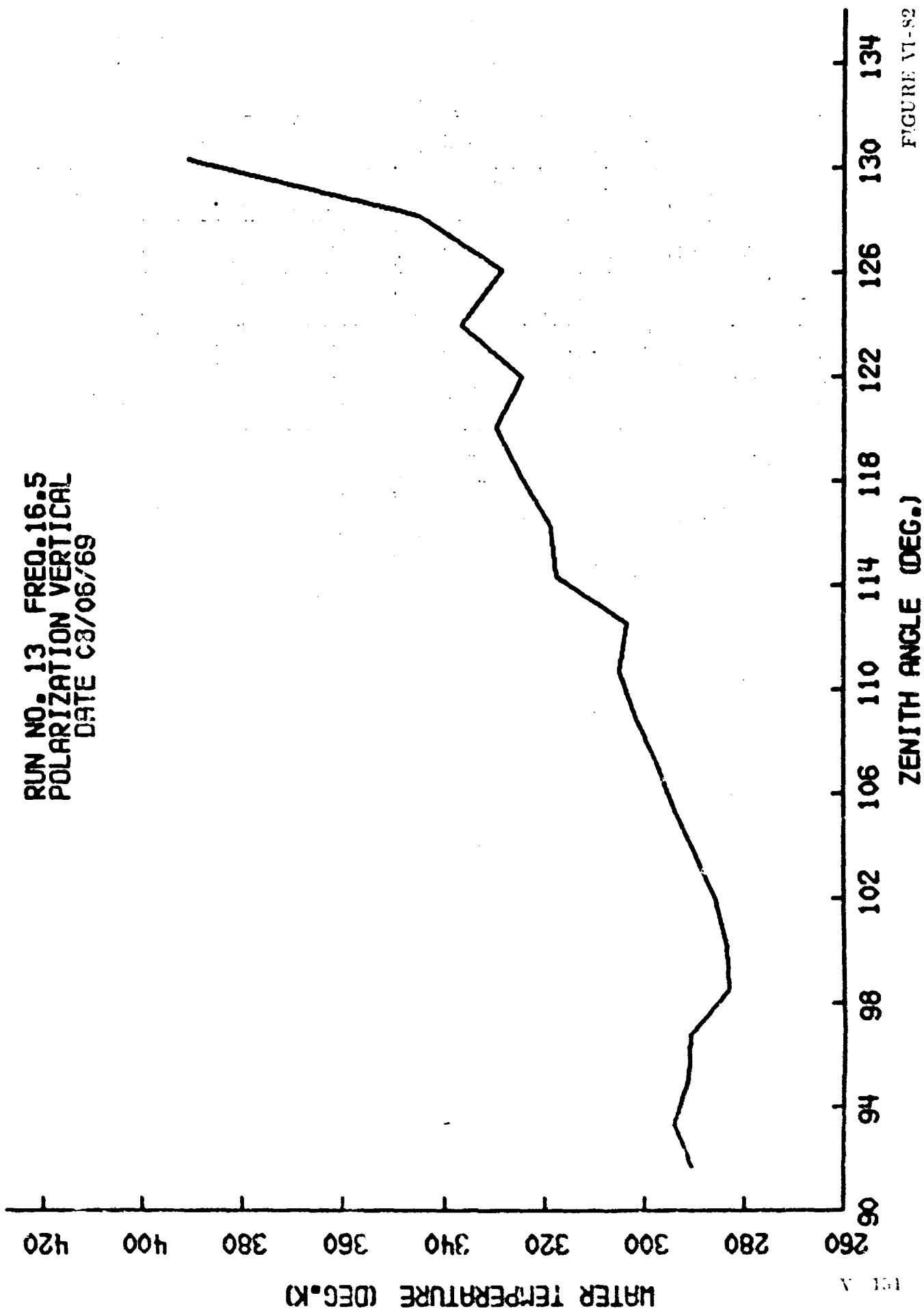
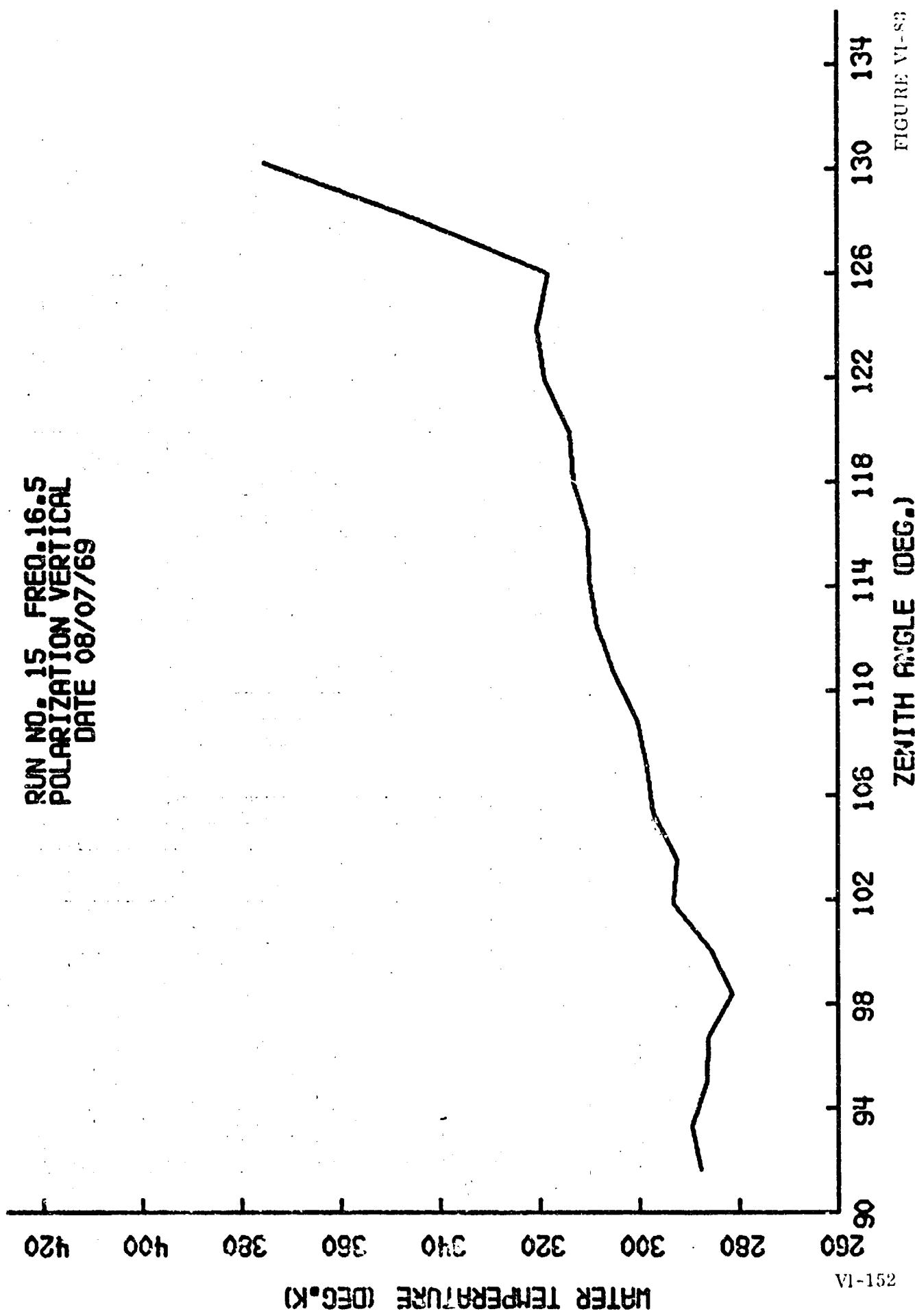


FIGURE VI-S2

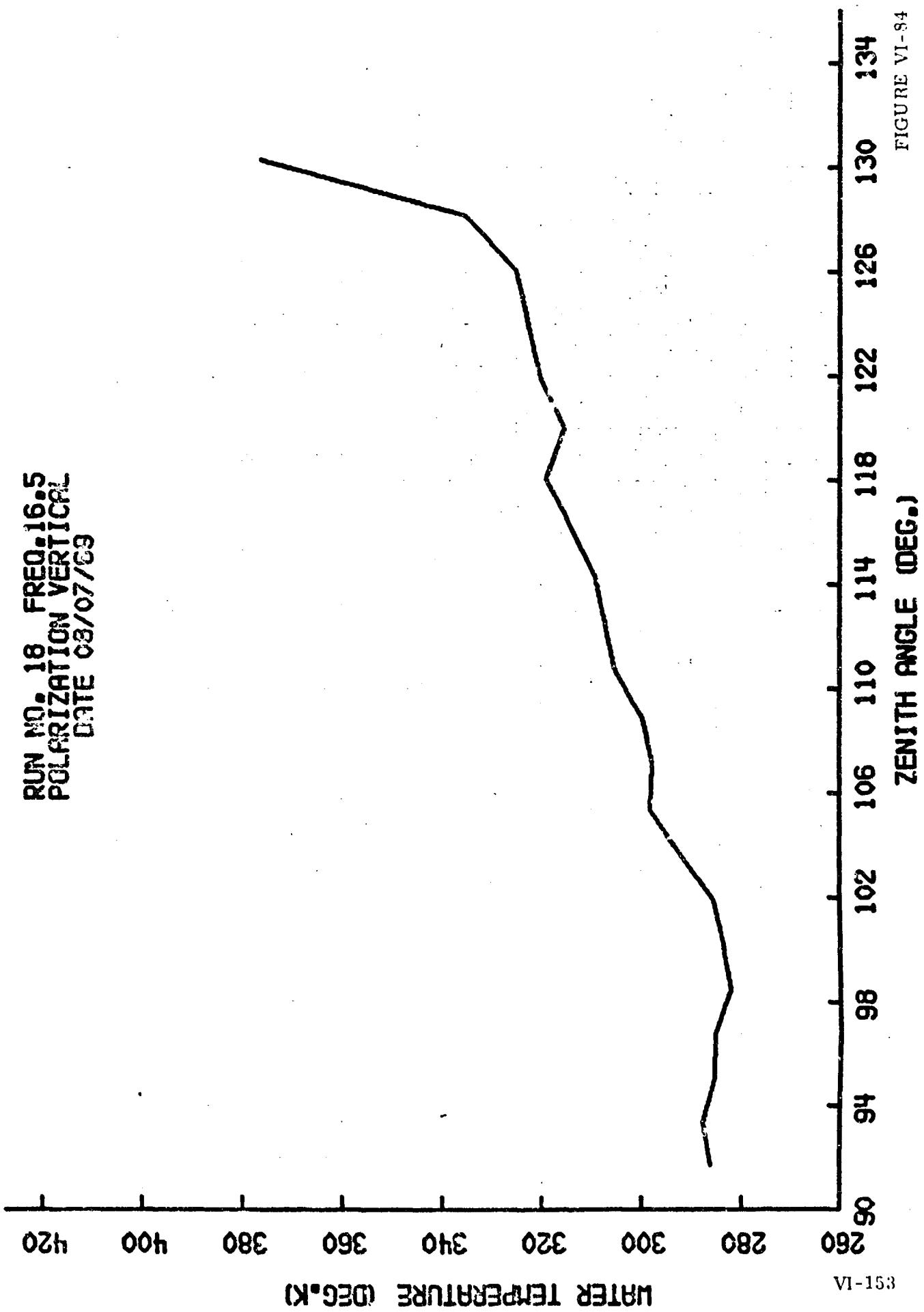
RUN NO. 15 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/07/69



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FIGURE VI-S3

FIGURE VI-84



RUN NO. 19 FREQ. 16.5
POLARIZATION VERTICAL
DATE 03/07/69

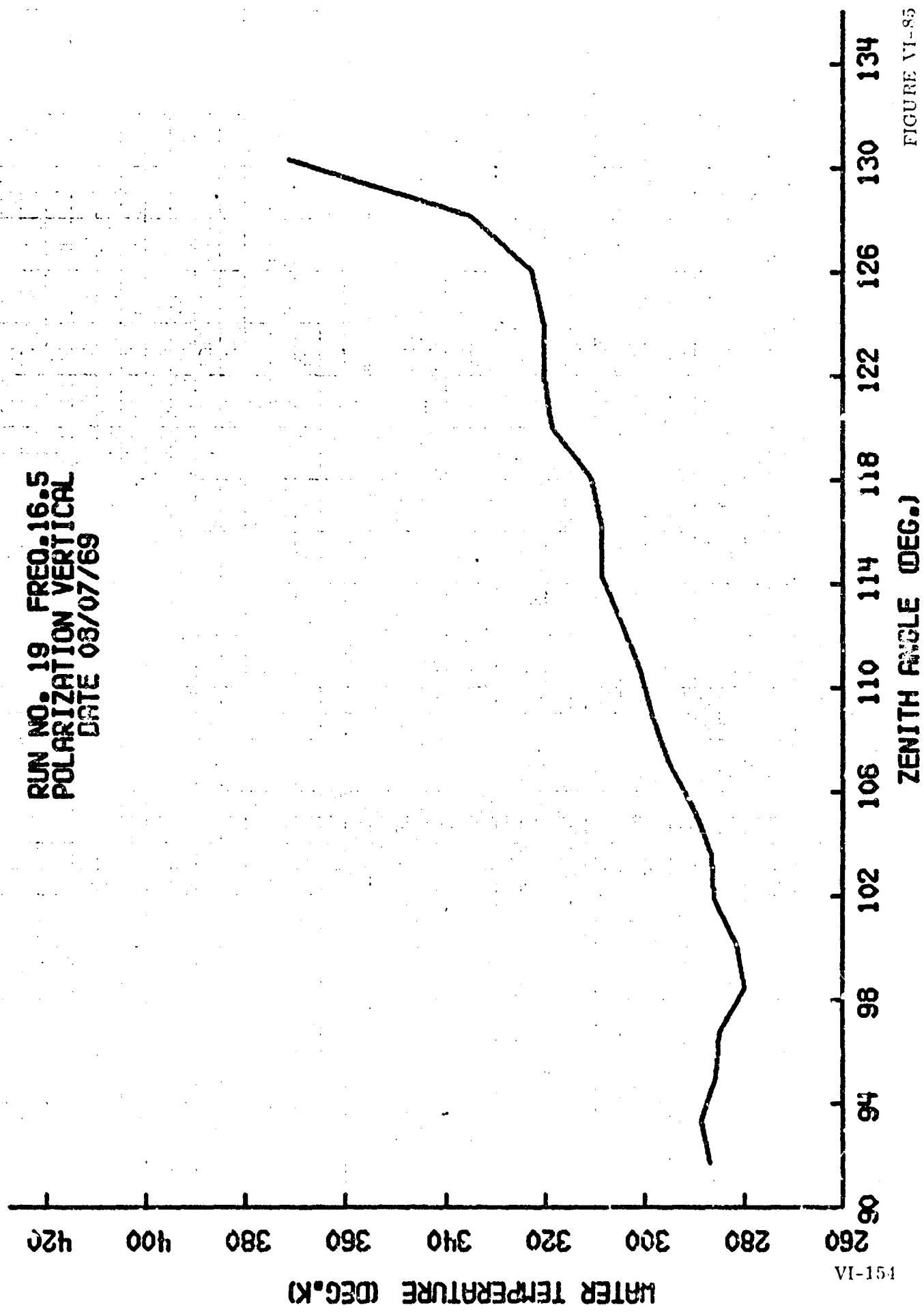


FIGURE VI-85

VI-154

RUN NO. 21 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/08/69

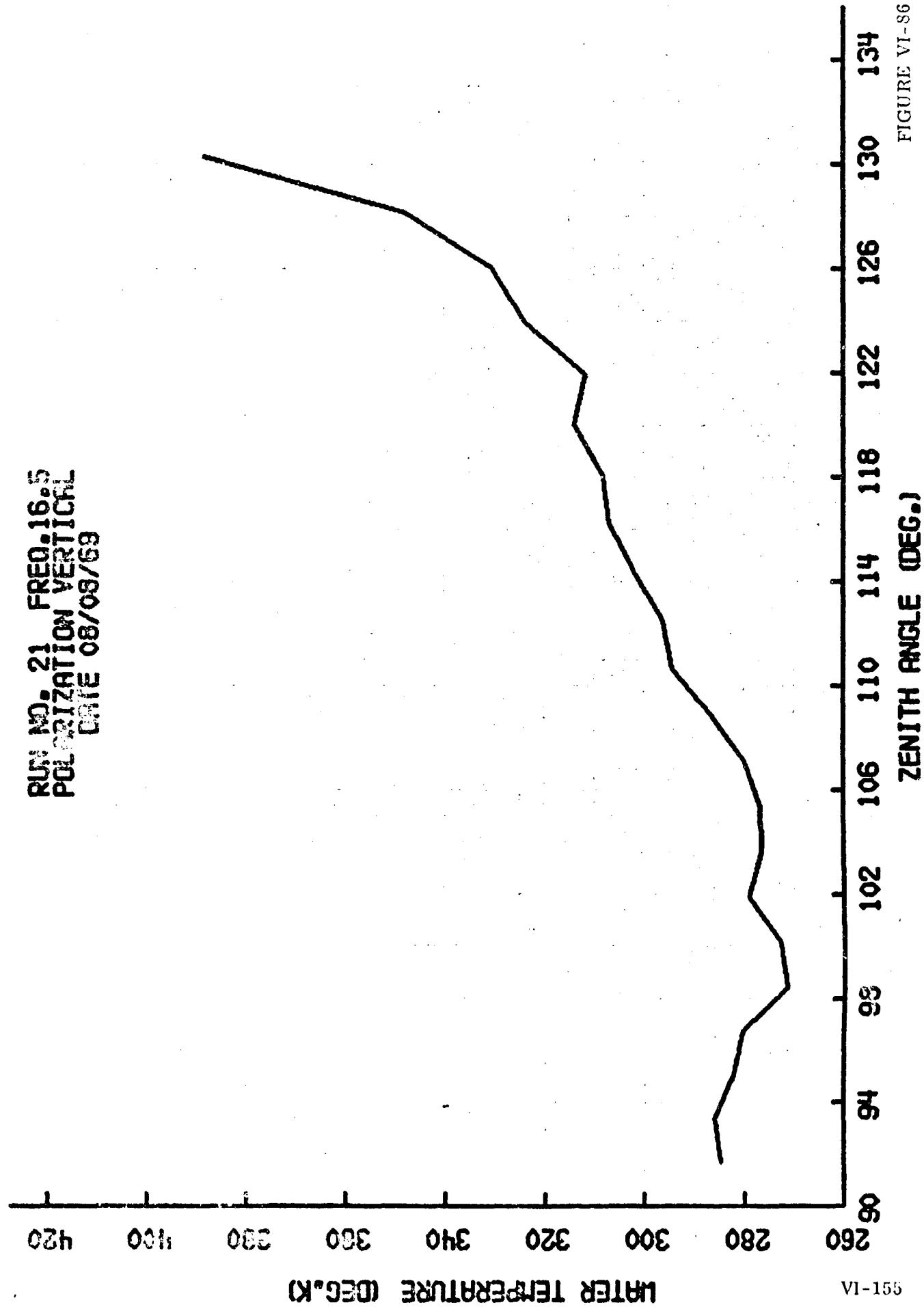


FIGURE VI-86

RUN NO. 23 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/08/69

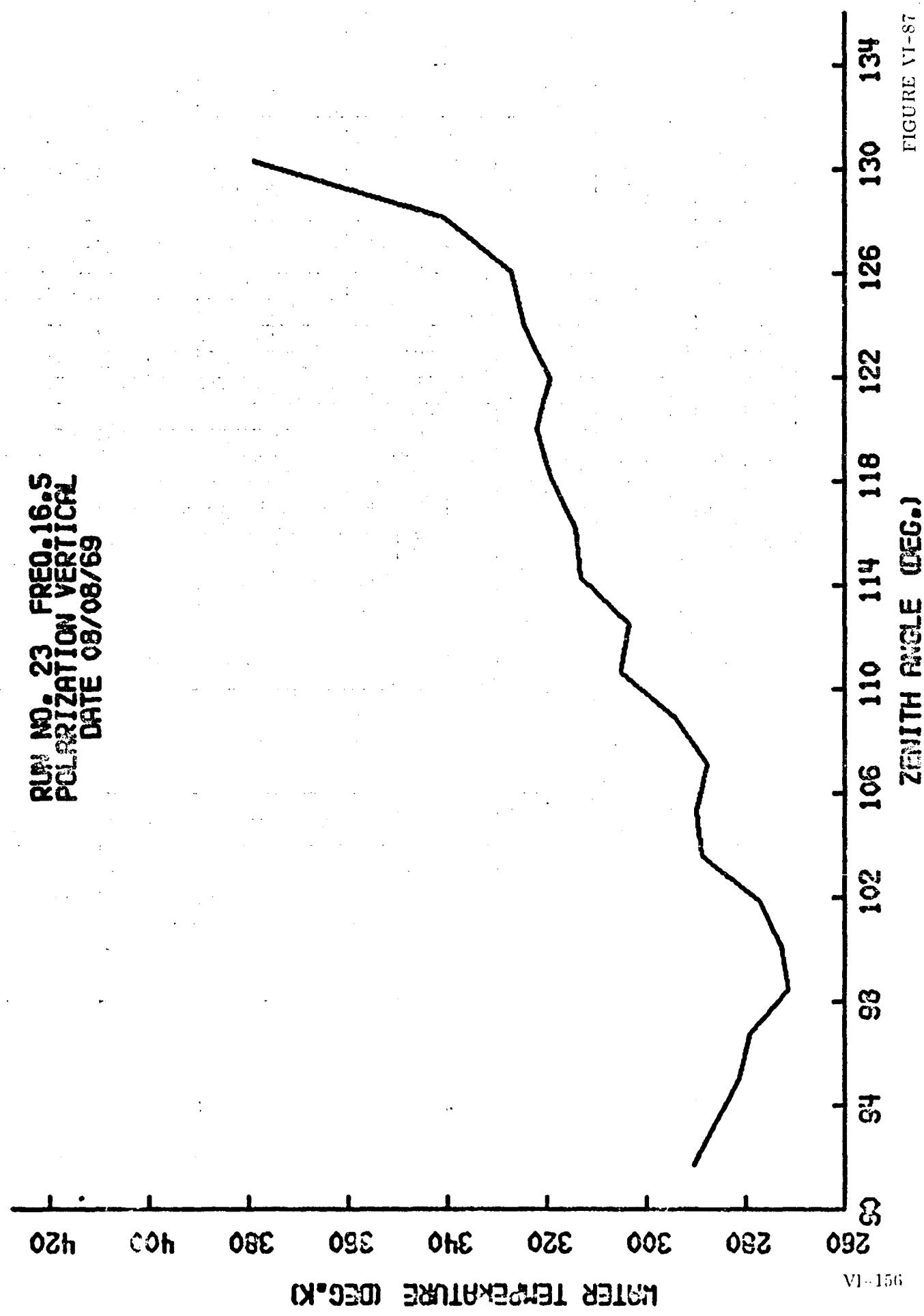
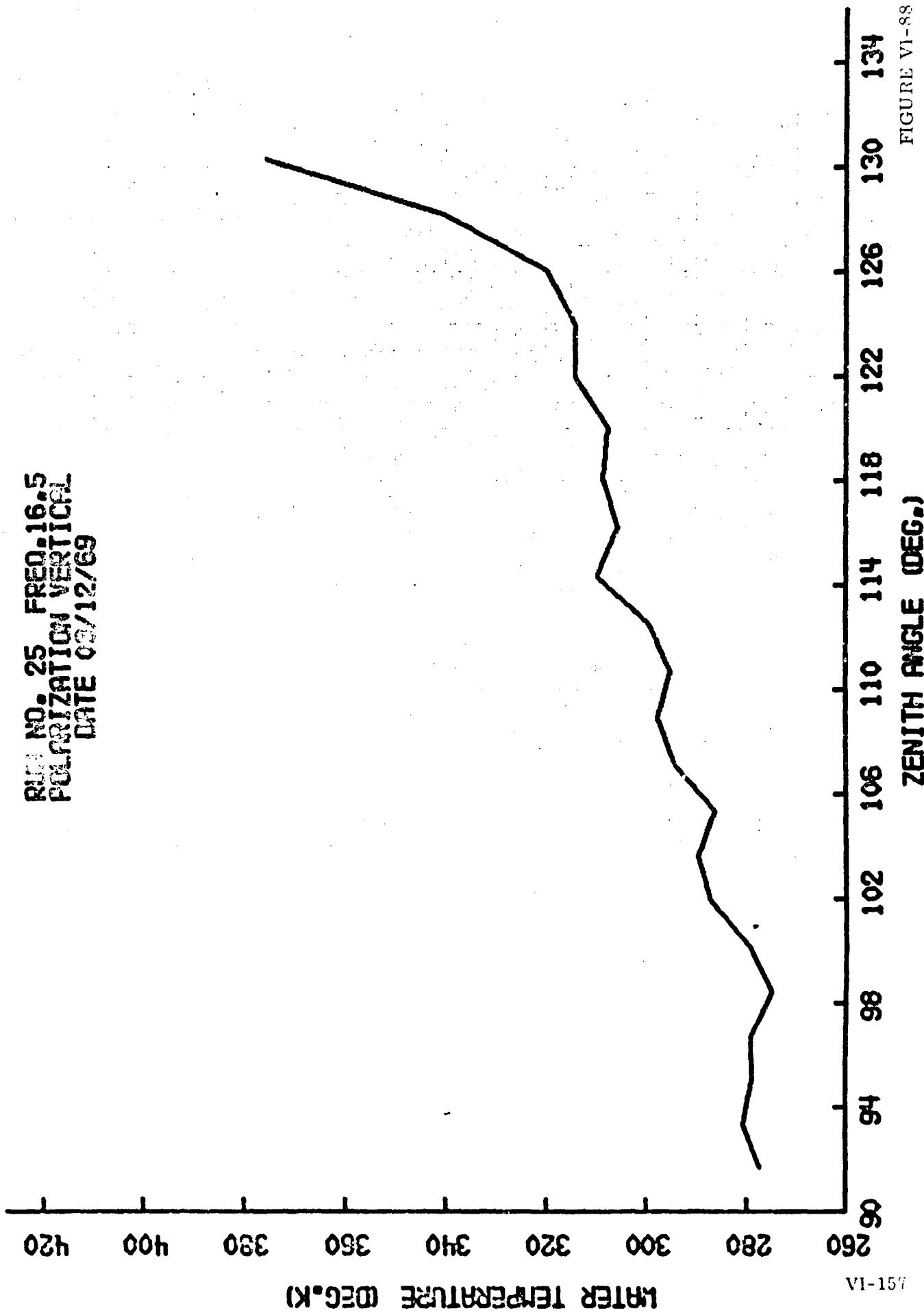
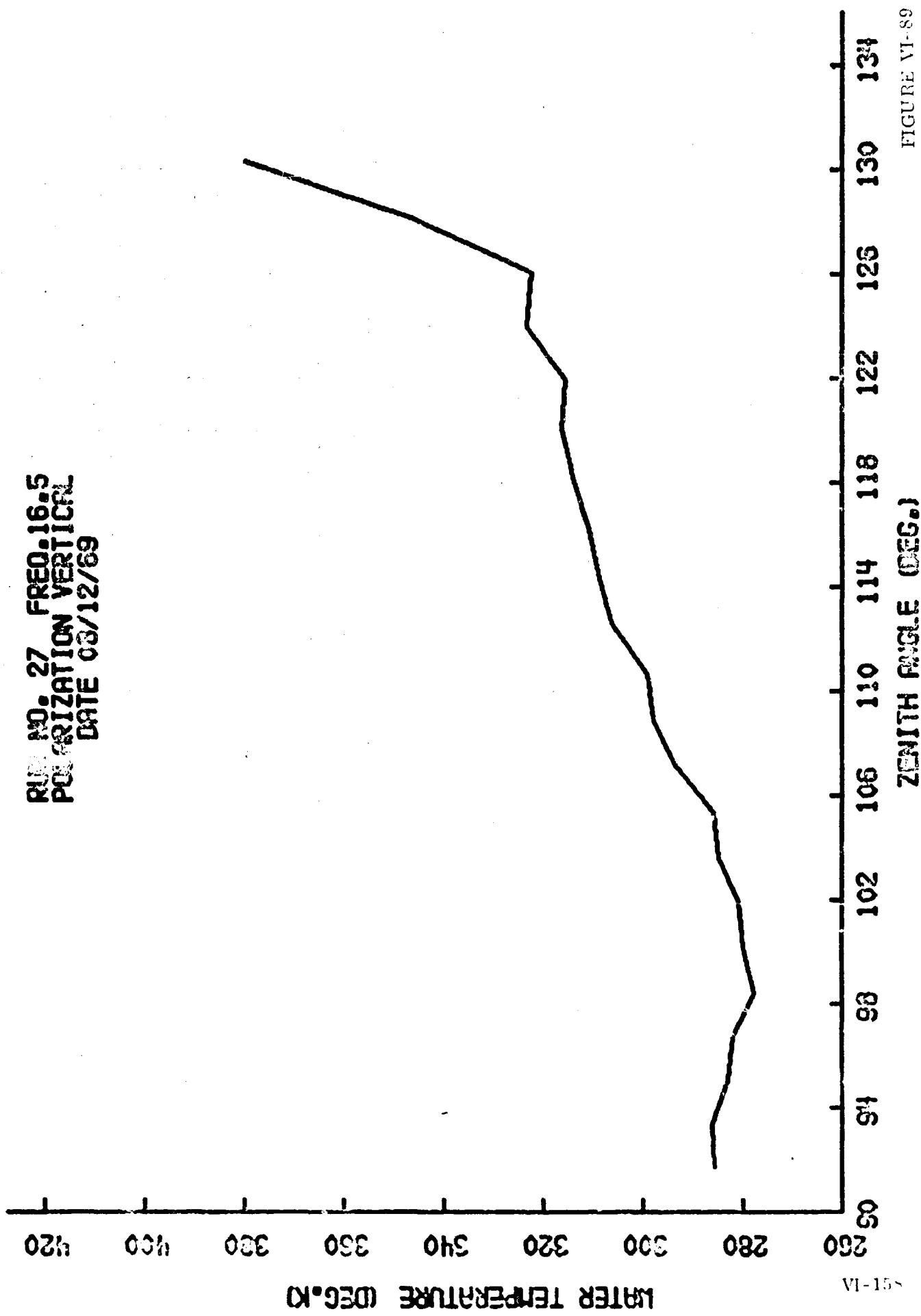


FIGURE VI-88



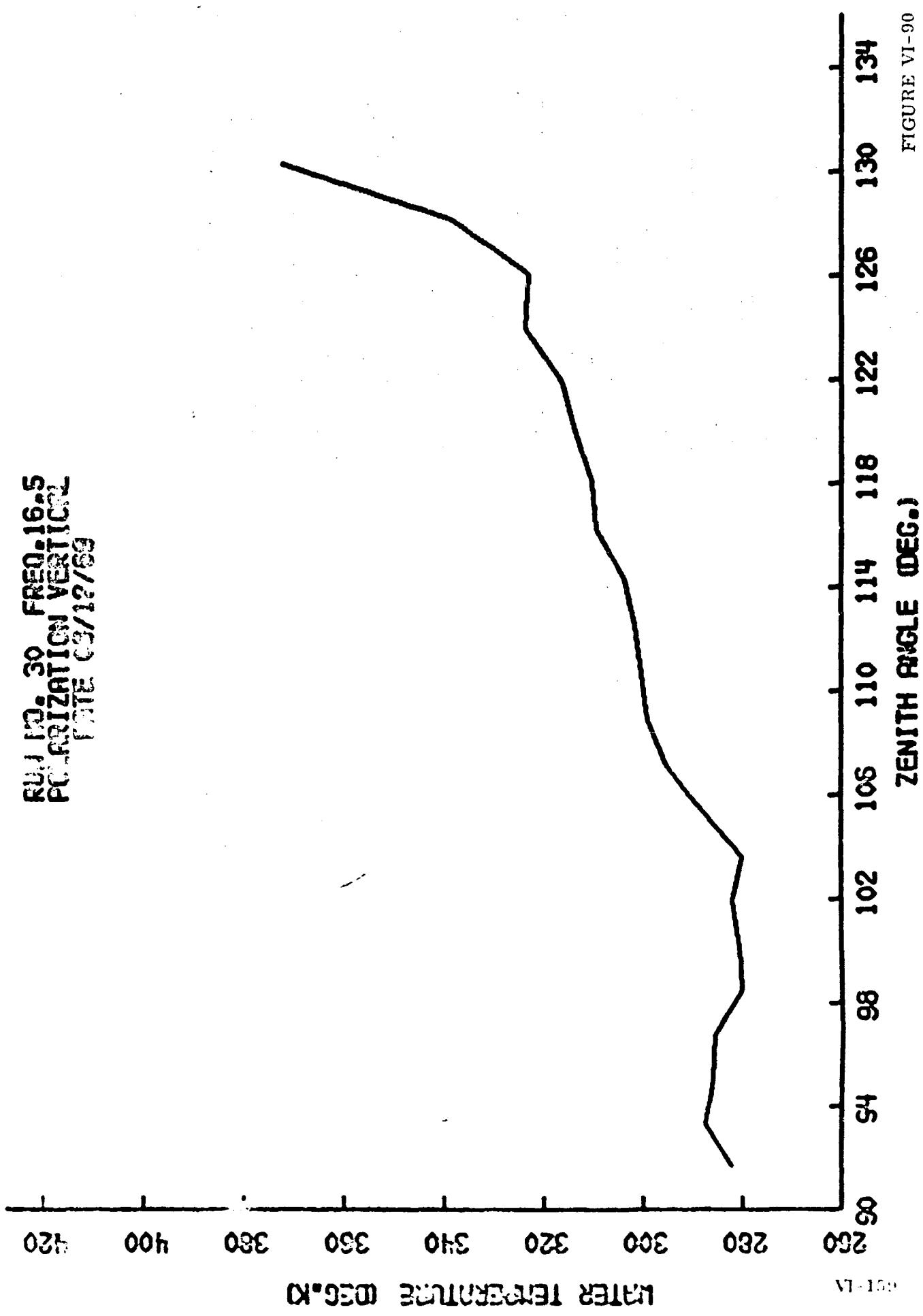
RUN NO. 27 FREQ. 16.5
PCU ORGANIZATION VERTICALLY
DATE 03/12/69



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FIGURE VI-89

FIGURE VI-90



RUN NO. 32 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/13/69

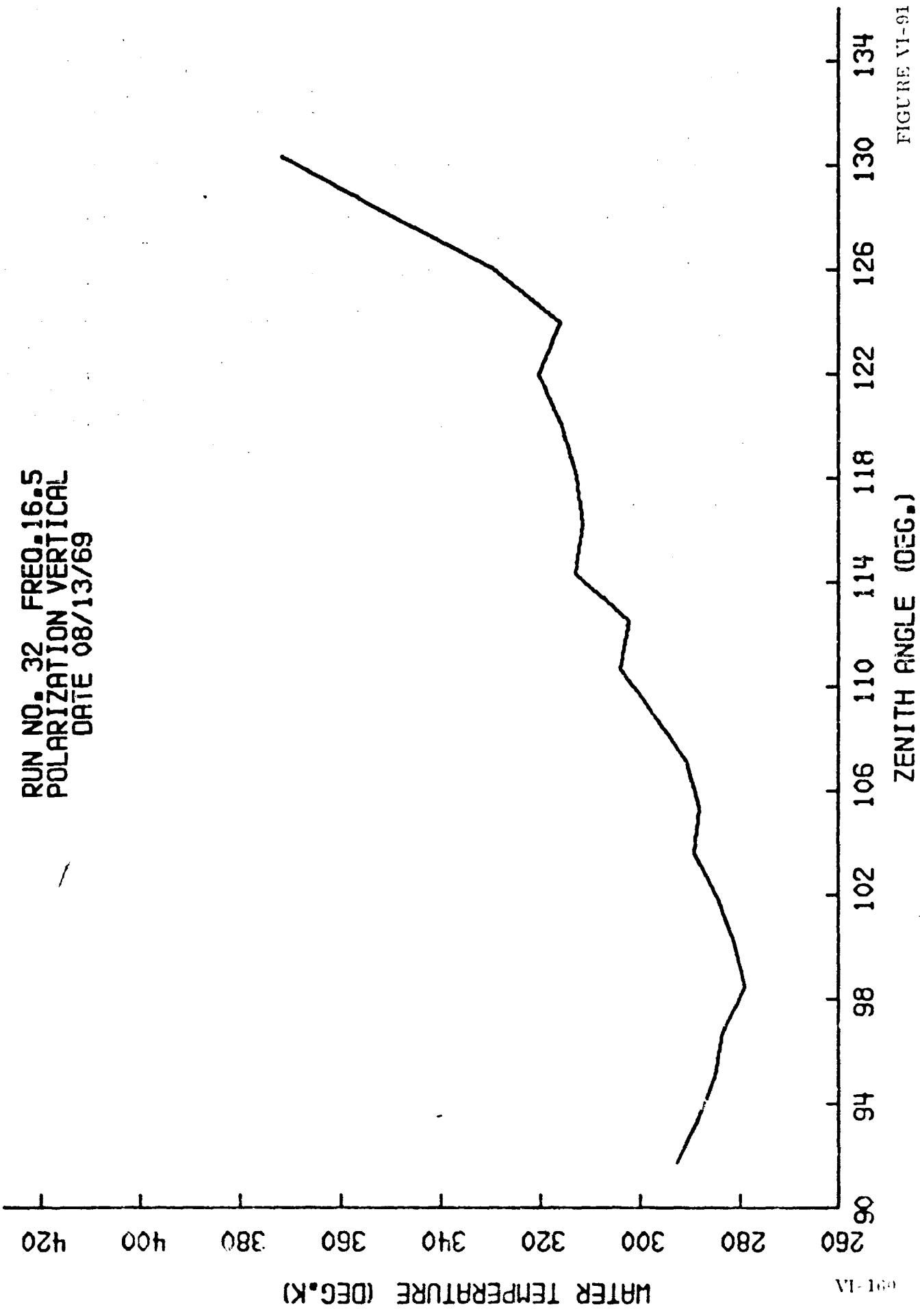
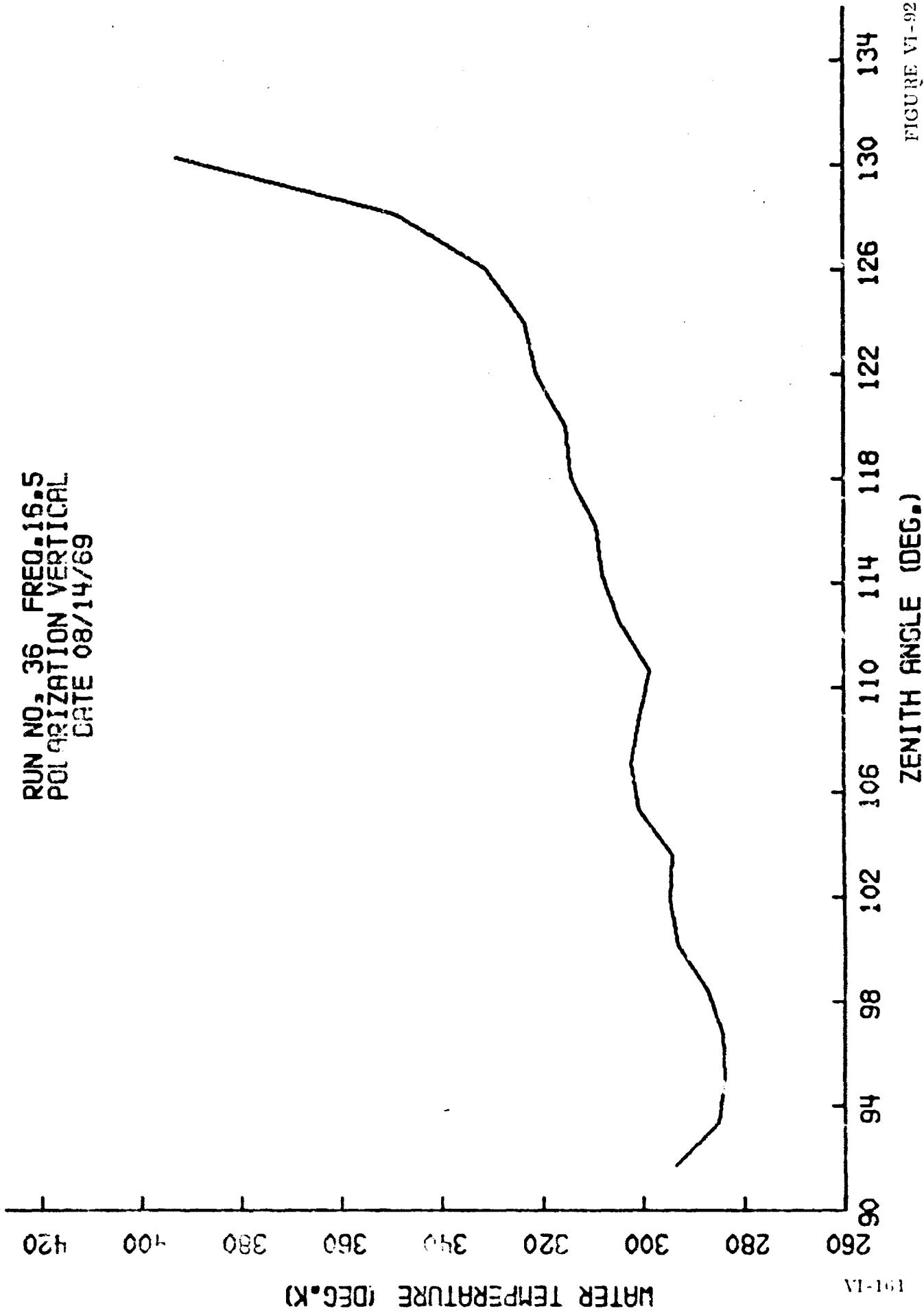


FIGURE VI-91

RUN NO. 36 FREQ. 16.5
POLARIZATION VERTICAL
DATE 08/14/69



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FIGURE VI-92

RUN NO. 201 FREQ. 9.5
POLARIZATION VERTICAL
DATE 07/17/69

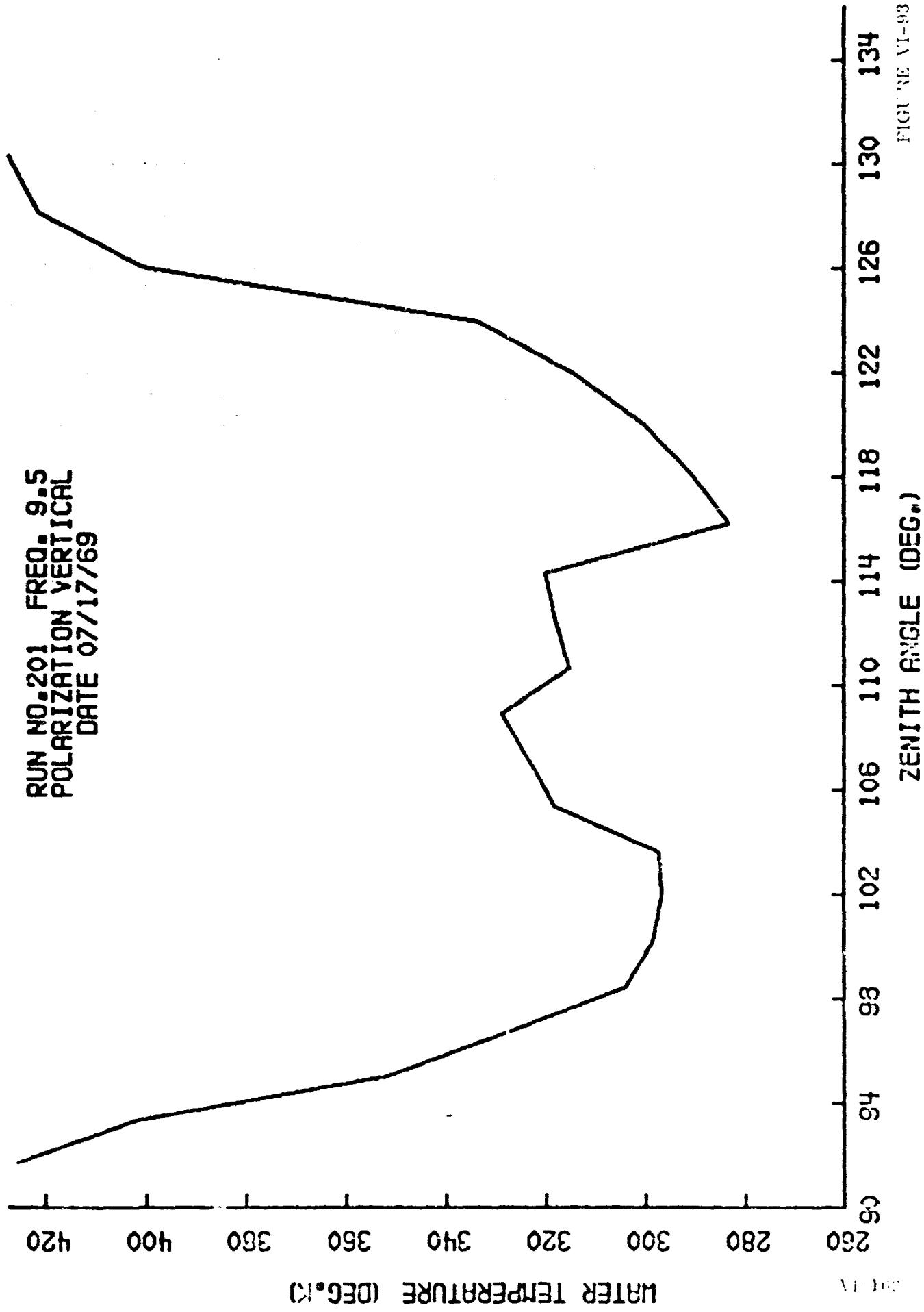


FIGURE VI-93

RL NO. 101 FREQ. 9.5
FIG. ORBITATION VERTICRL
DATE 07/21/69

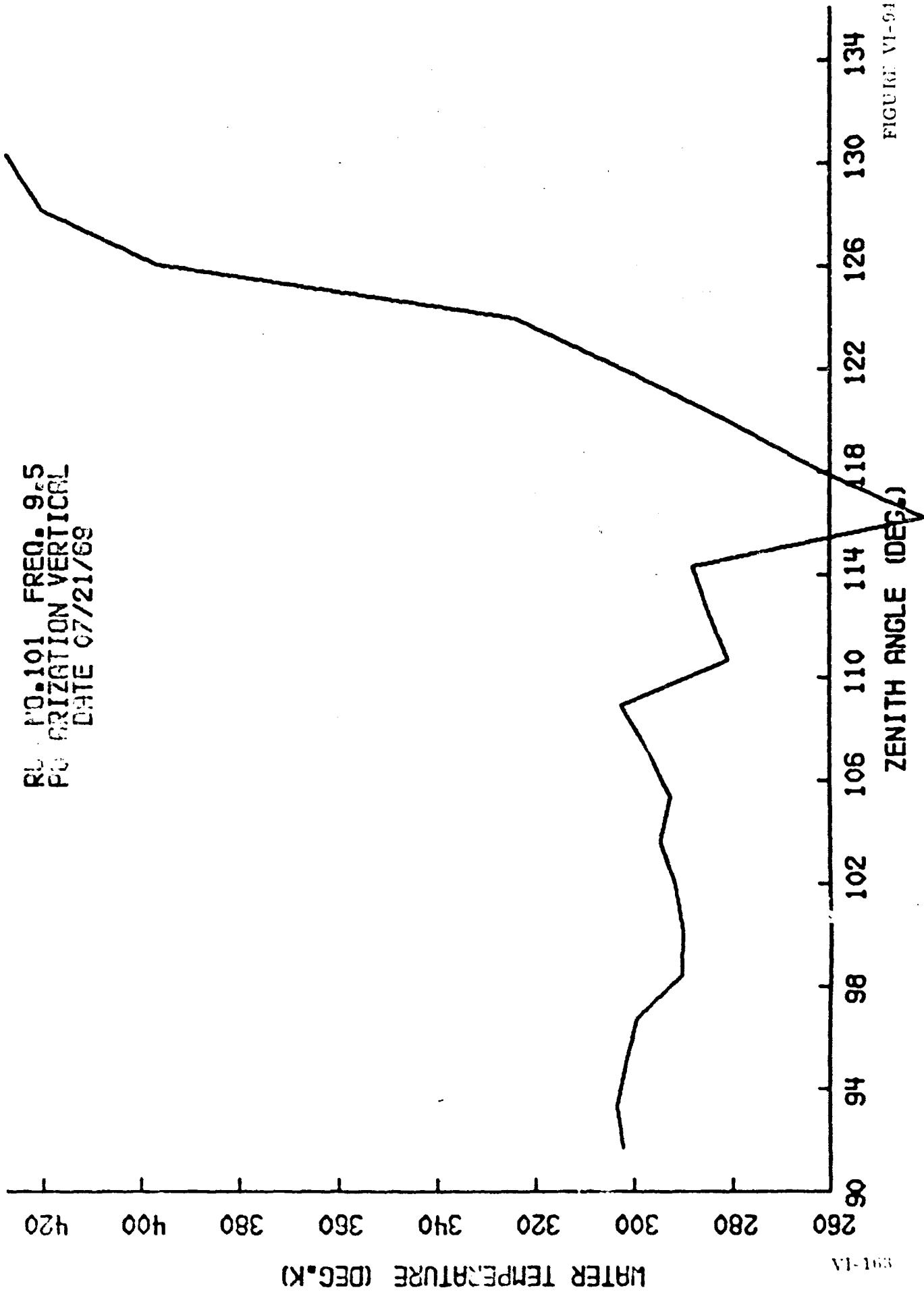
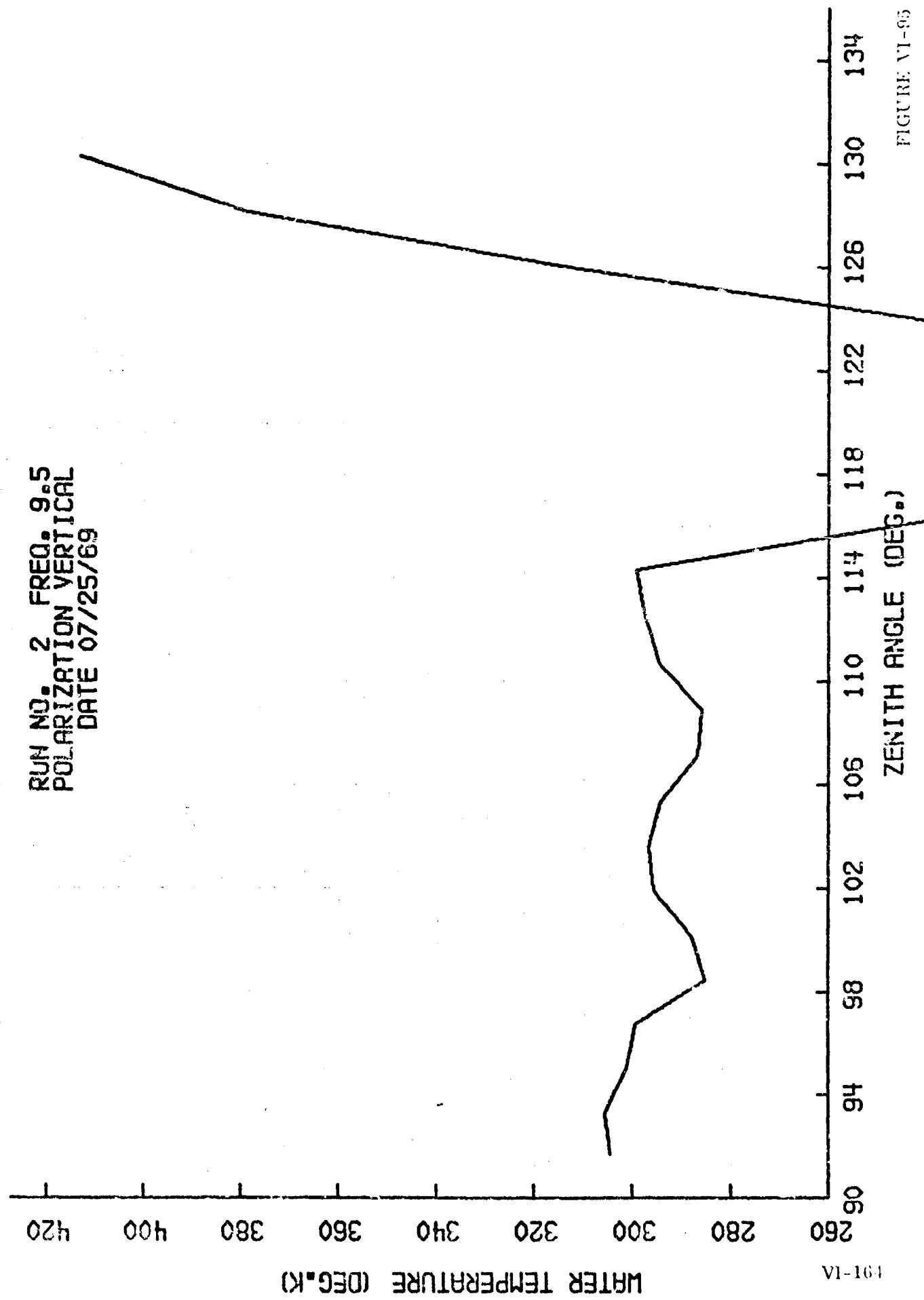
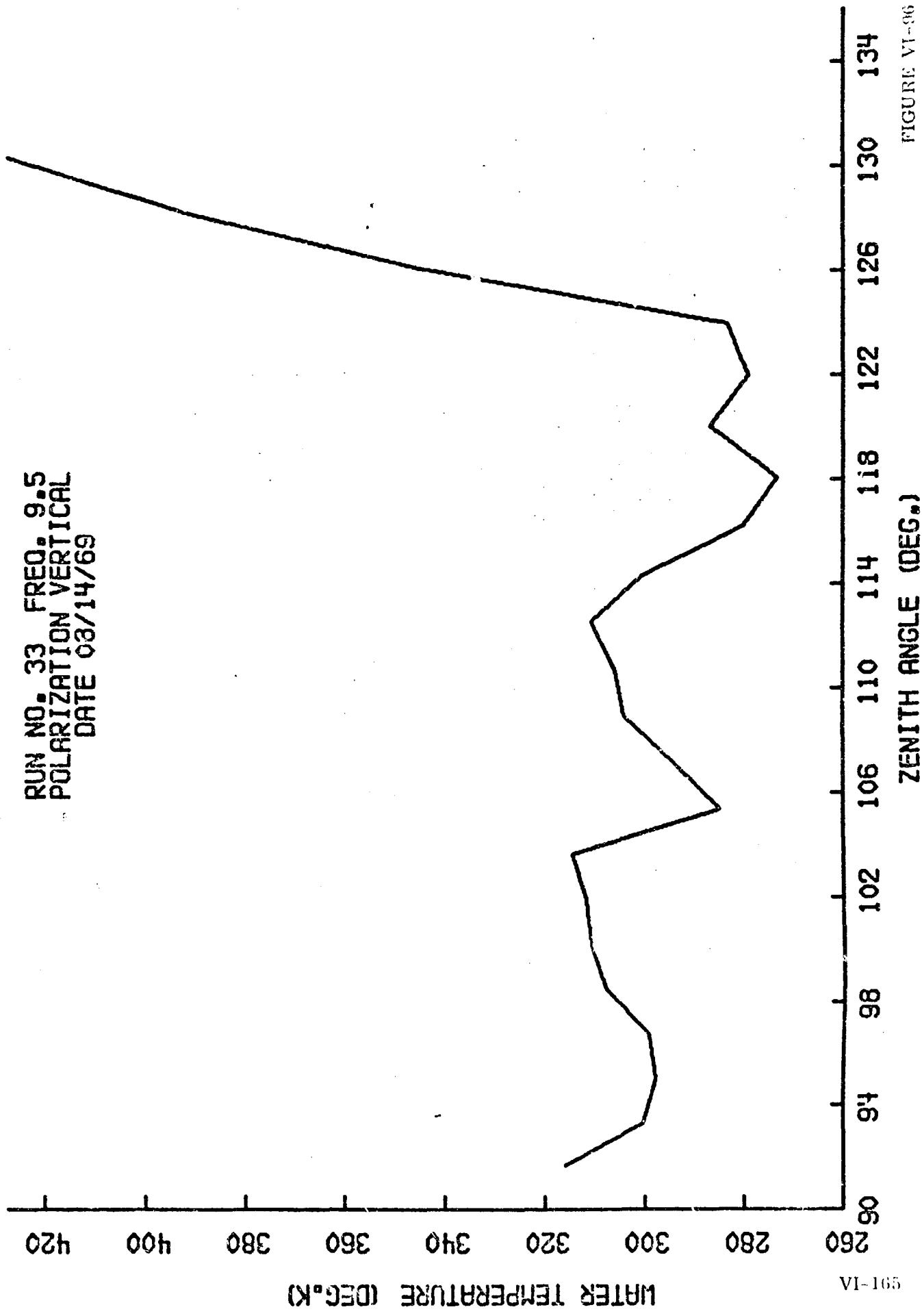


FIGURE VI-95



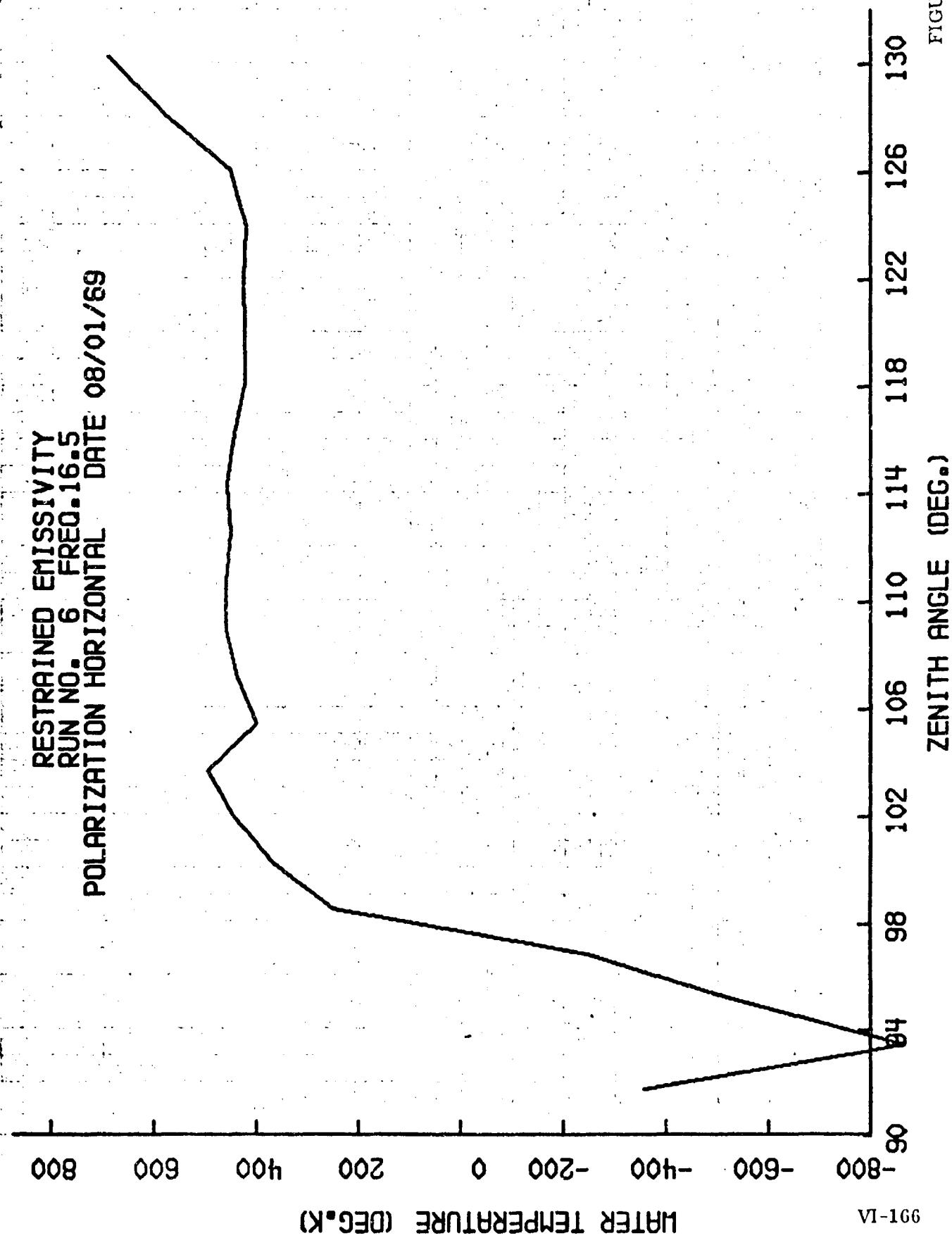
RUN NO. 33 FREQ. 9.5
POLARIZATION VERTICAL
DATE 03/14/69



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FIGURE VI-166

RESTRAINED EMISSIVITY
RUN NO. 6 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/01/69



VI-166

FIGURE VI-97

RESTRAINED EMISSIVITY
RUN NO. 7 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/01/69

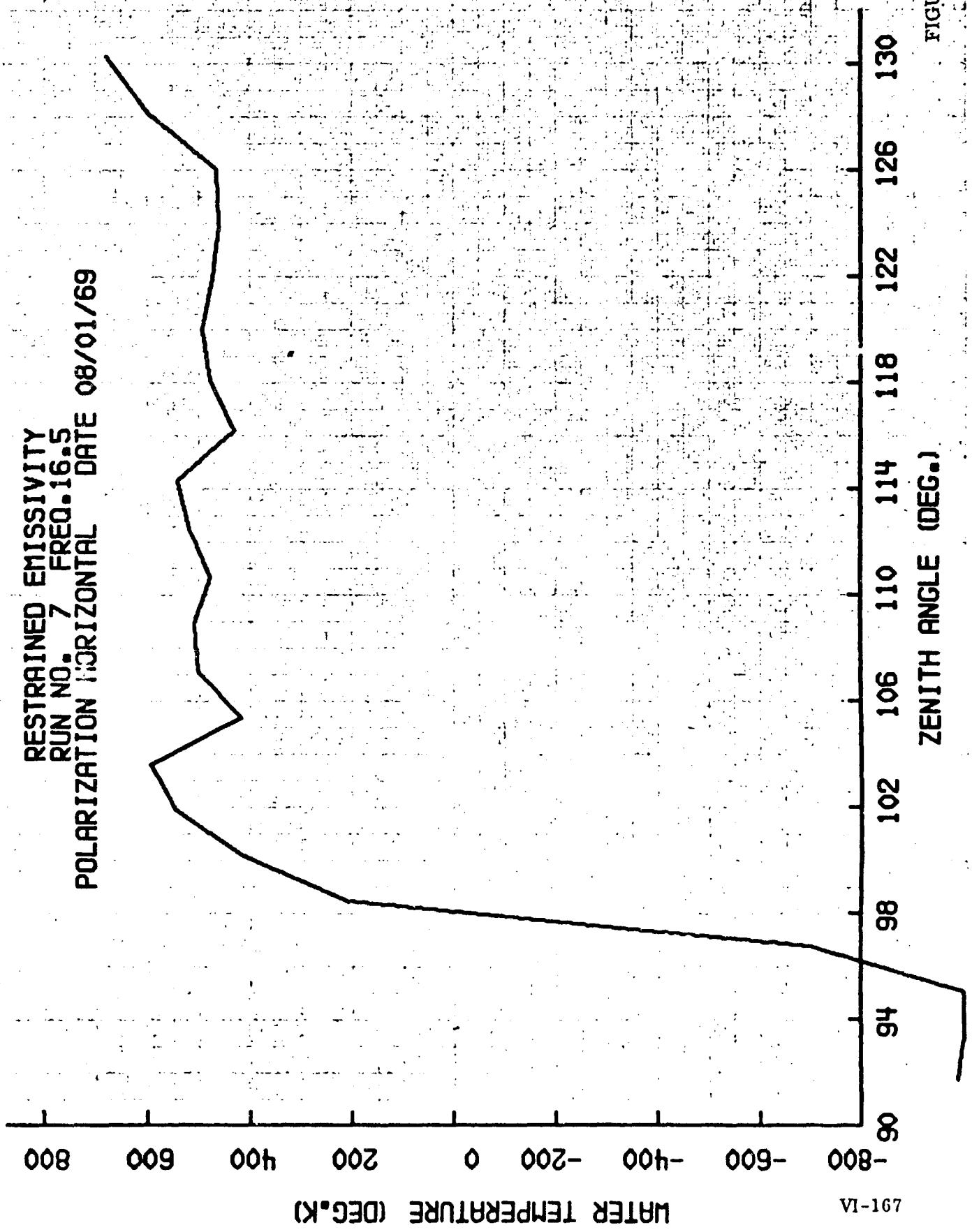


FIGURE VI-98

FIGURE VI-99

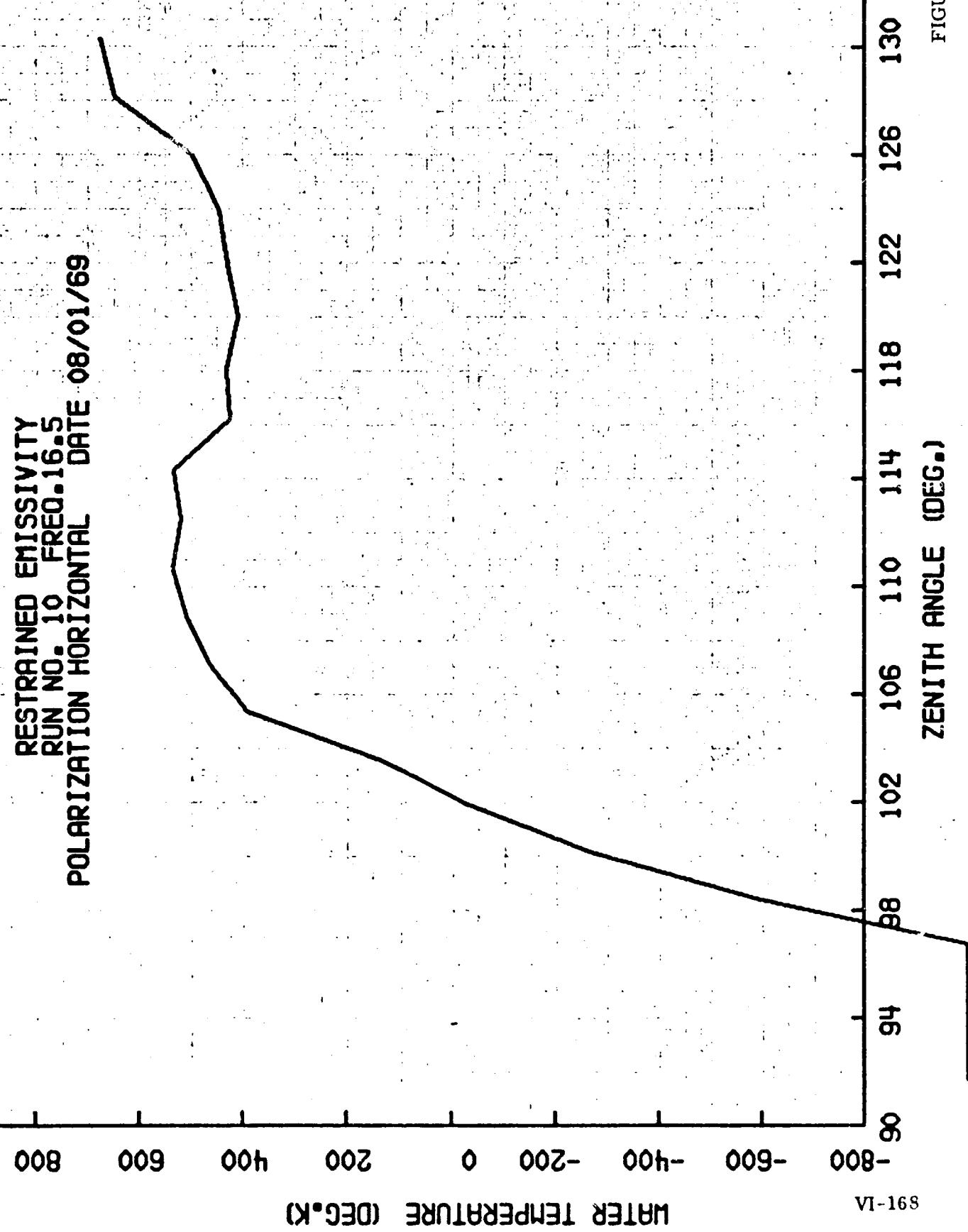


FIGURE VI-100

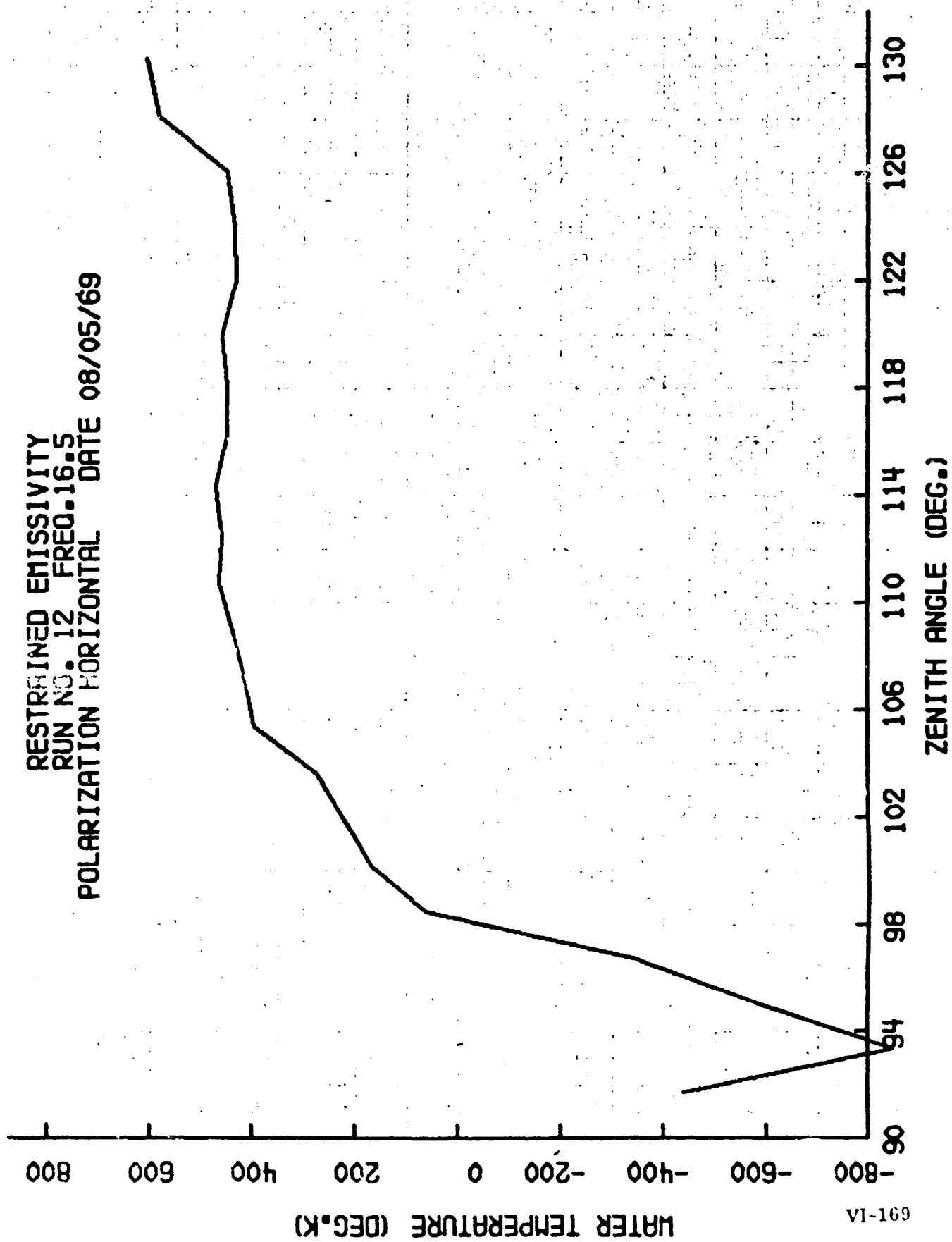


FIGURE VI-101

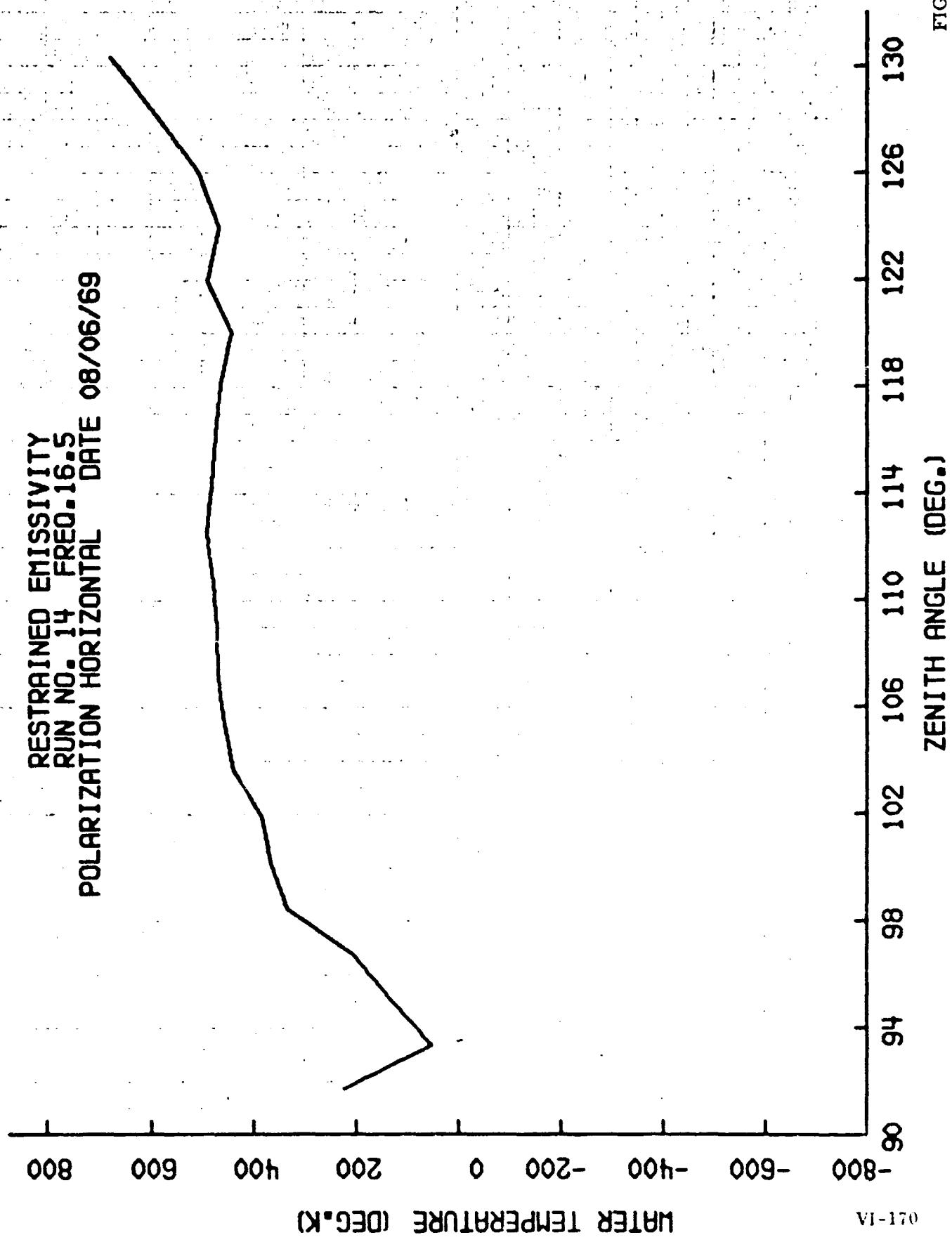
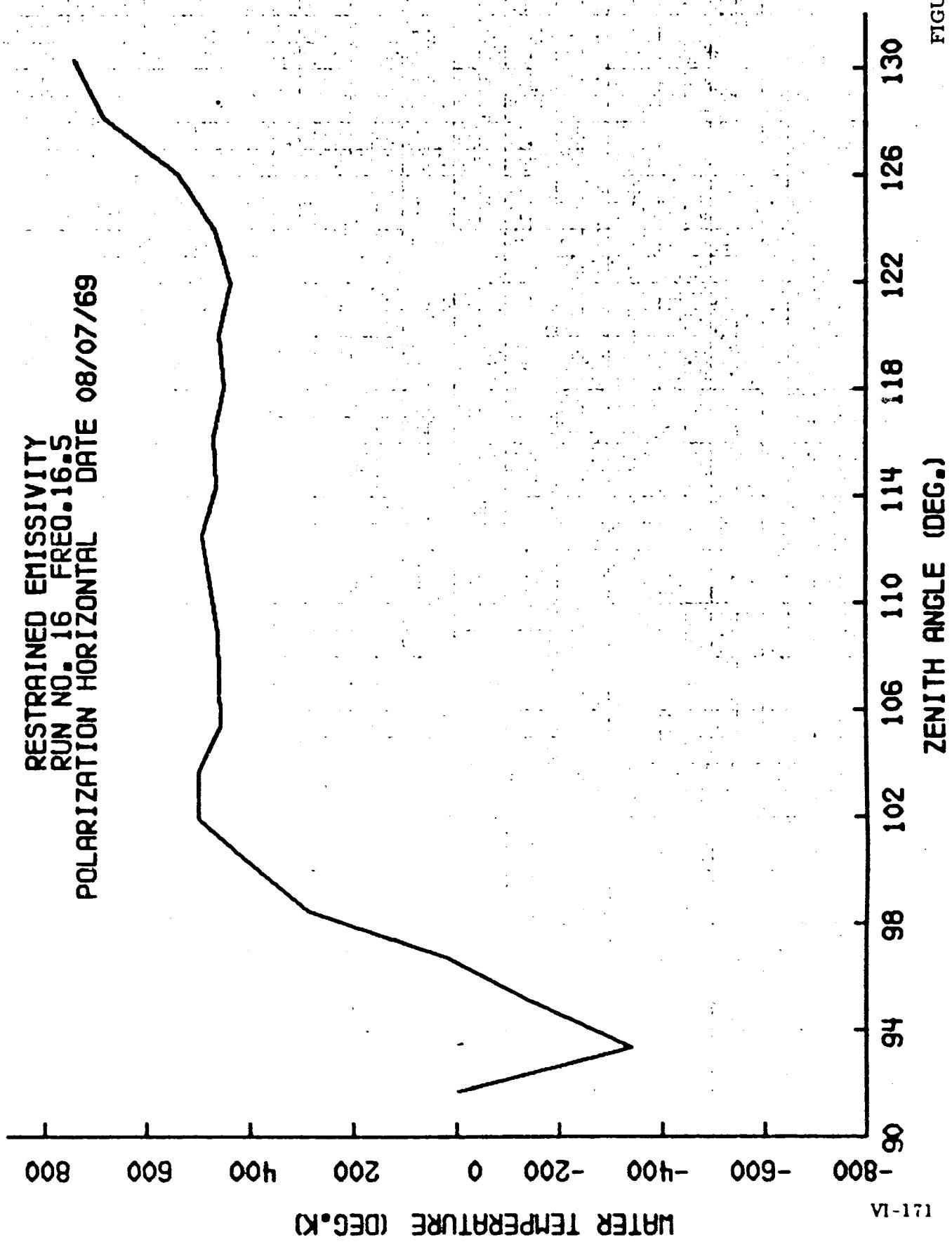


FIGURE VI-102



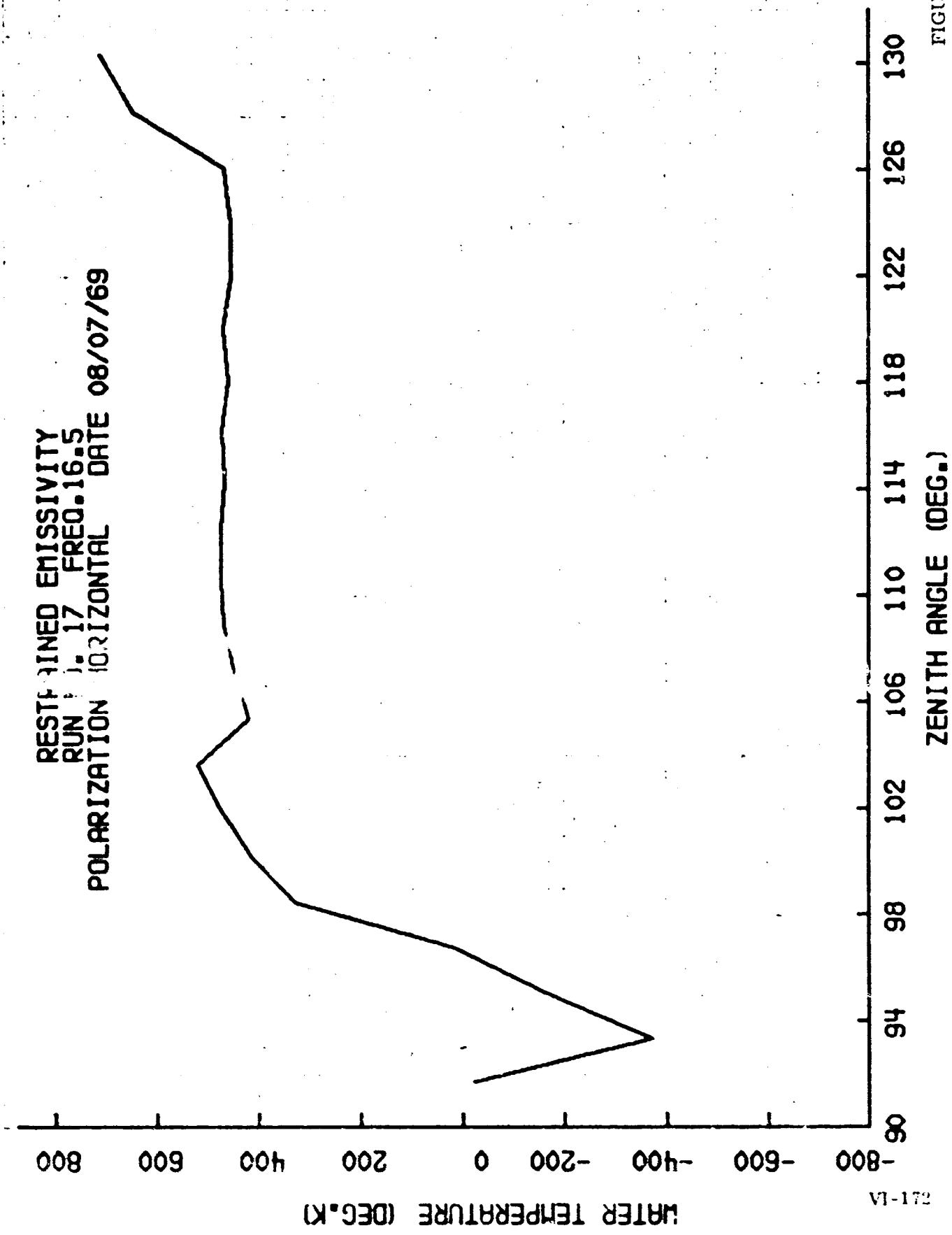


FIGURE VI-103

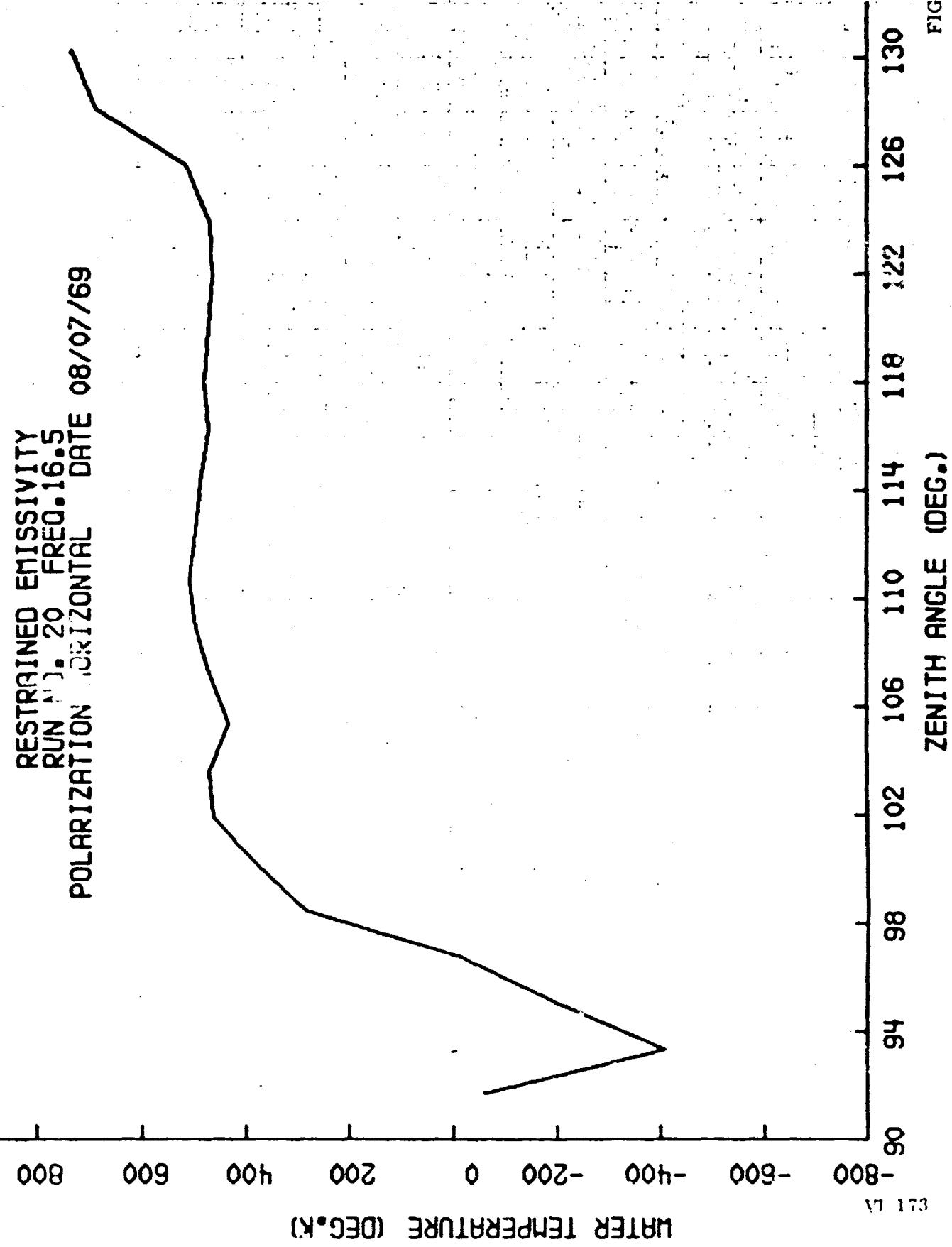


FIGURE VI-104

FIGURE VI-105

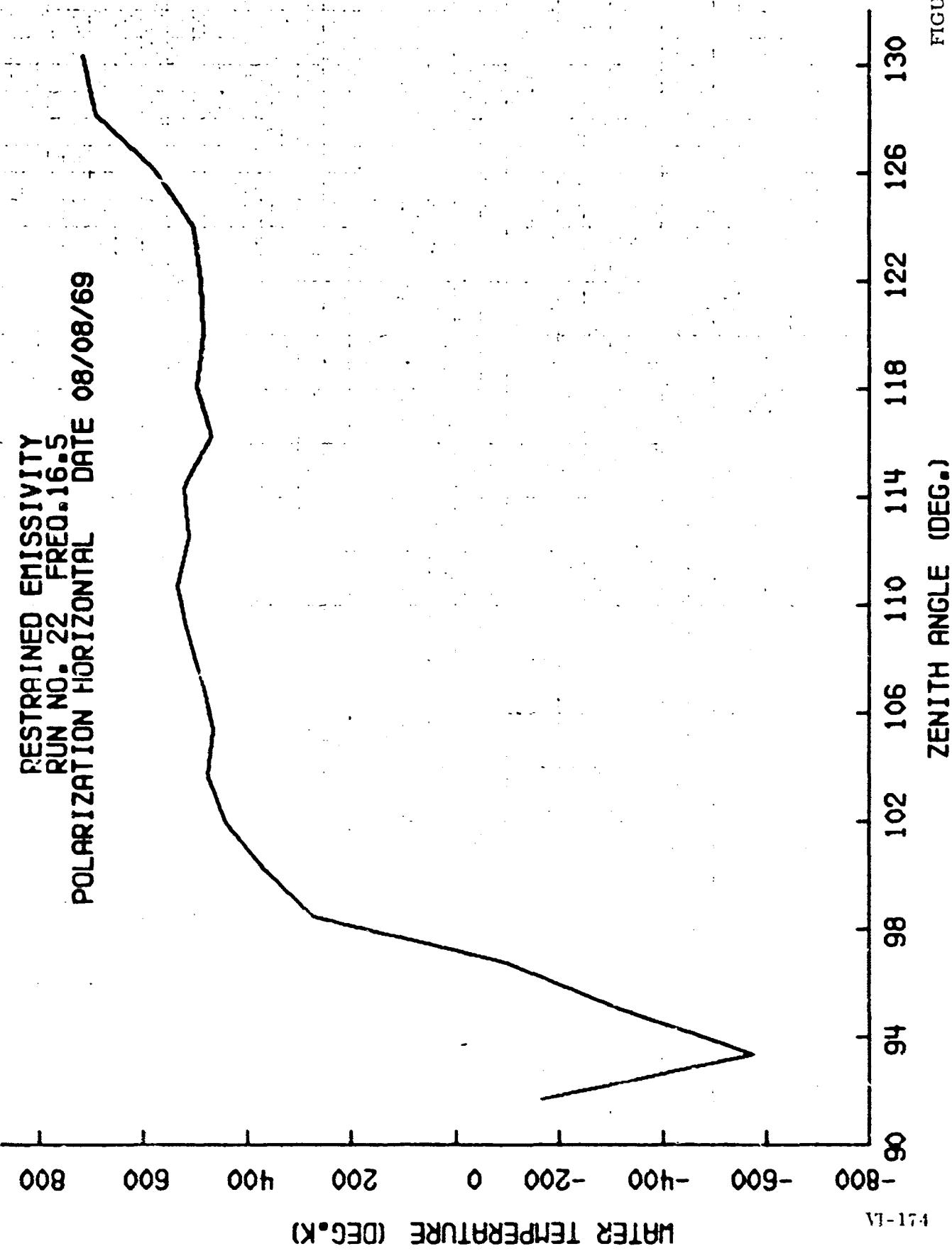


FIGURE VI-106

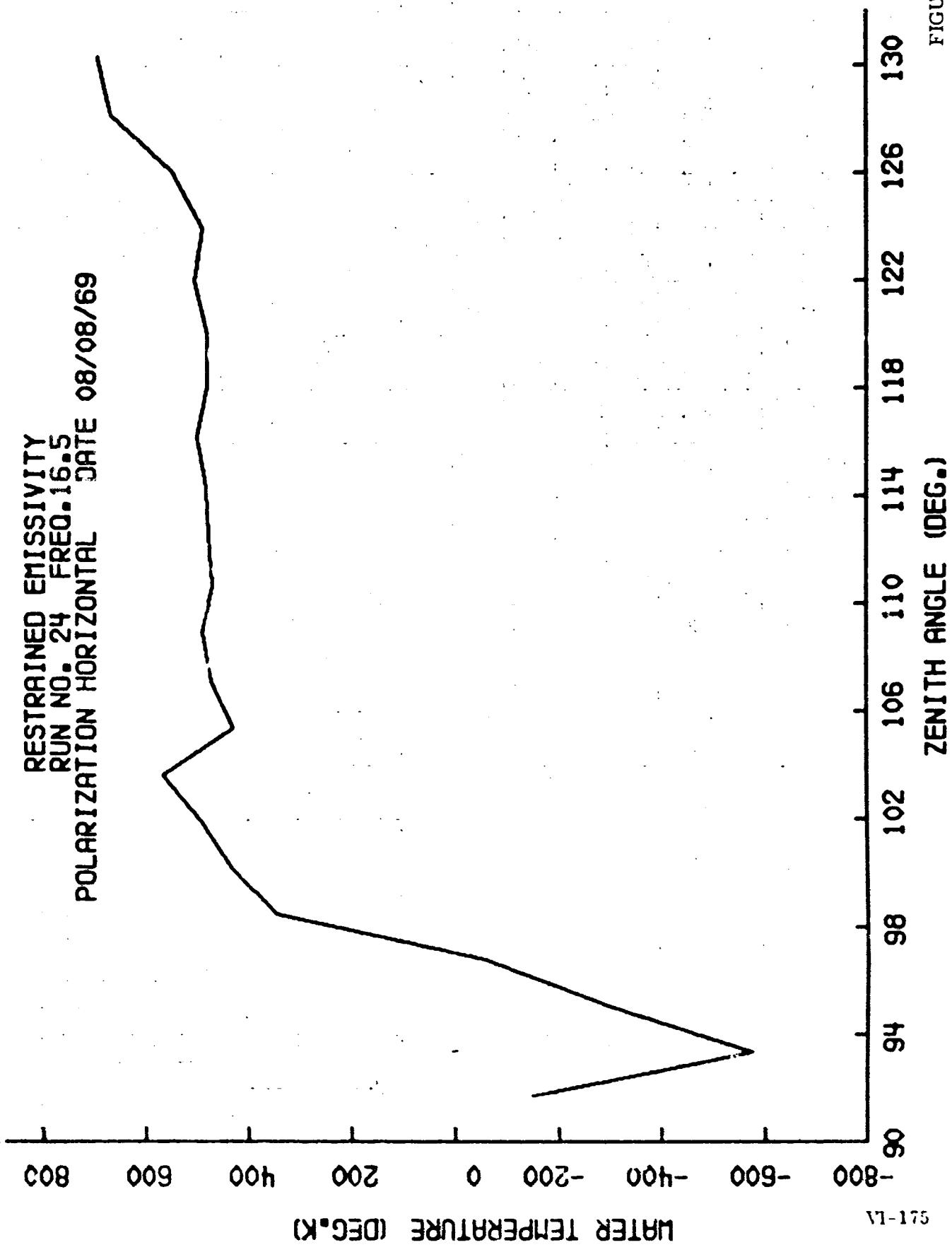


FIGURE VI-107

RESTRAINED EMISSIVITY
RUN NO. 26 FREQ. 16.5
POLARIZATION: HORIZONTAL DATE 08/12/69

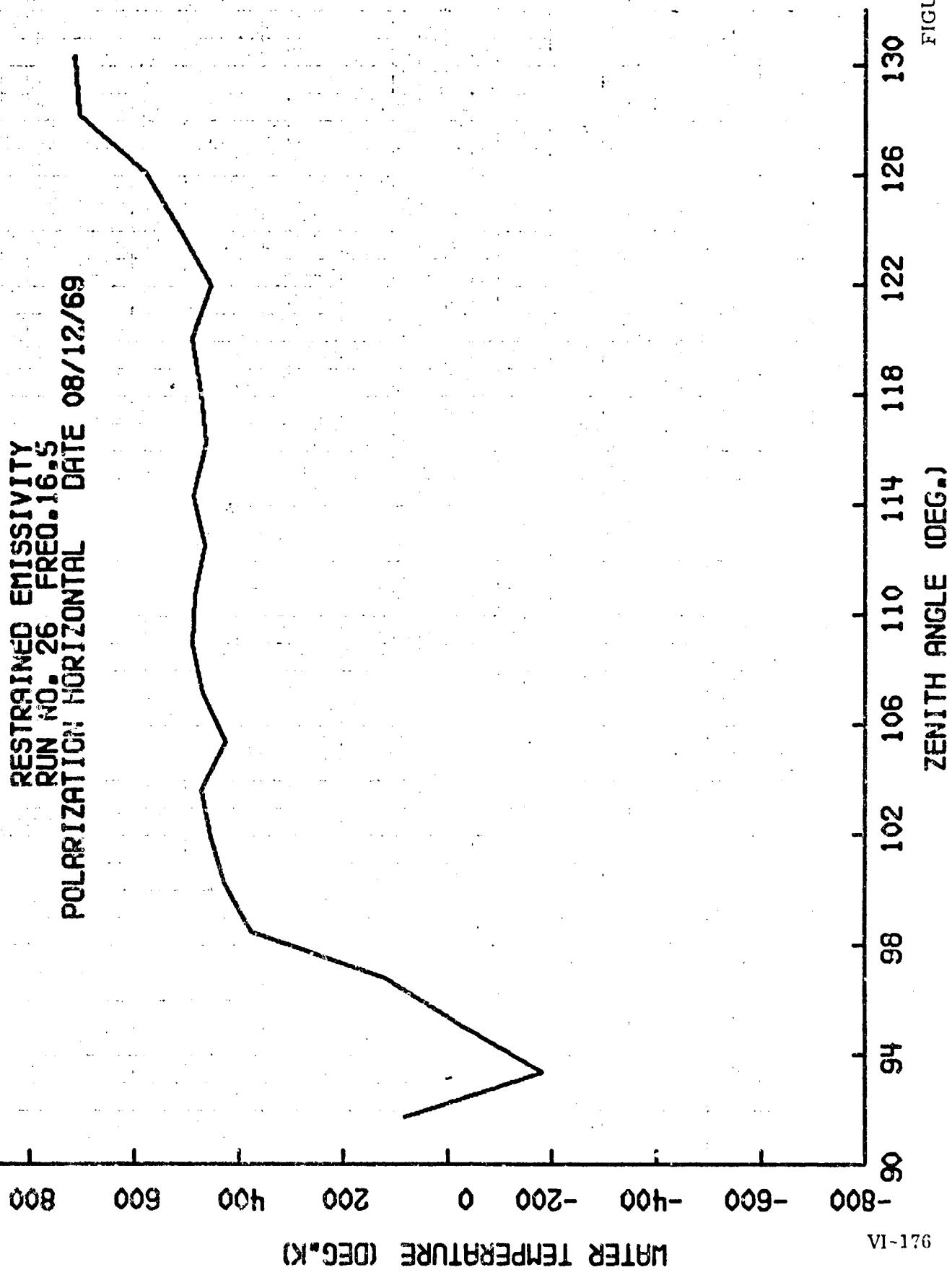
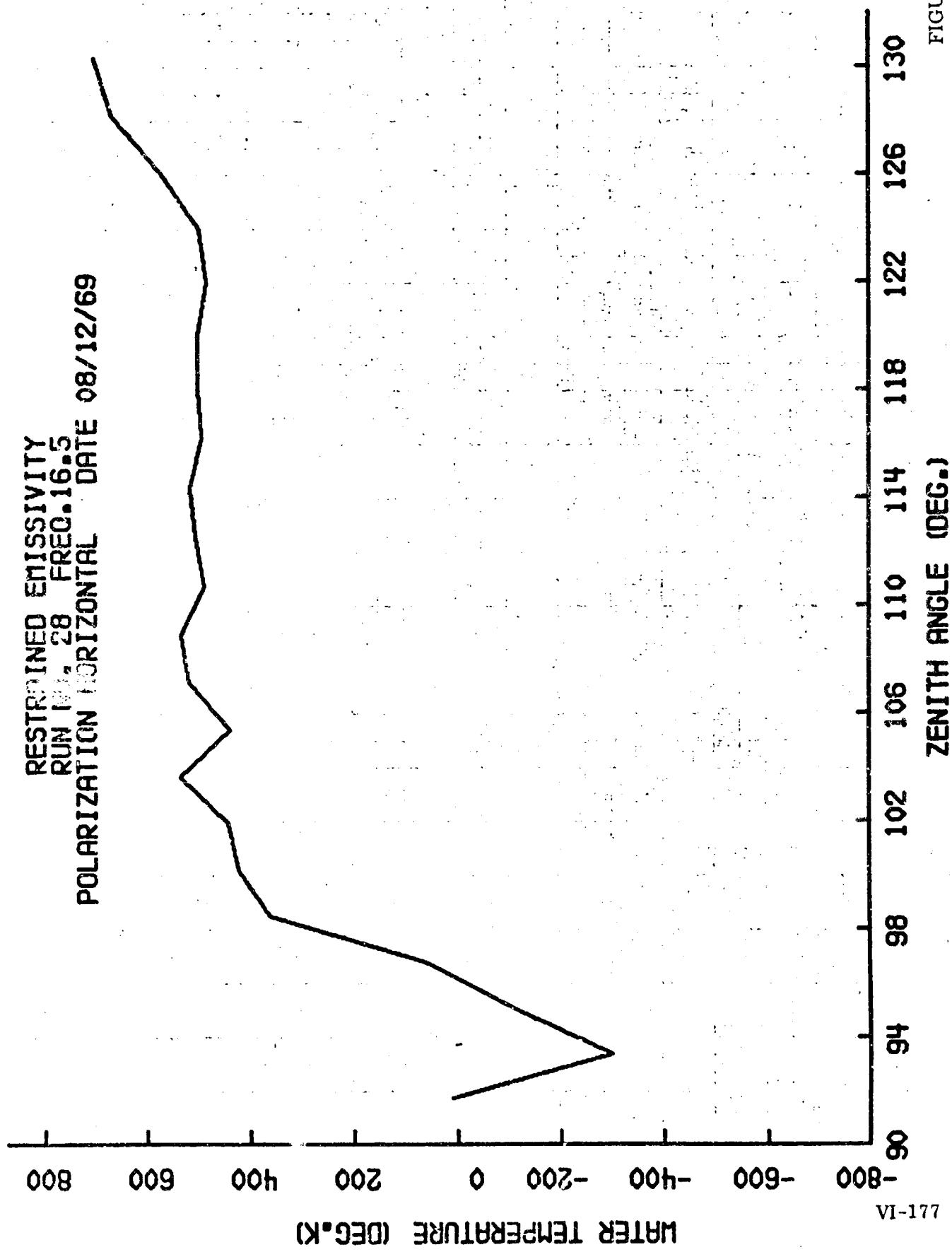


FIGURE VI-108



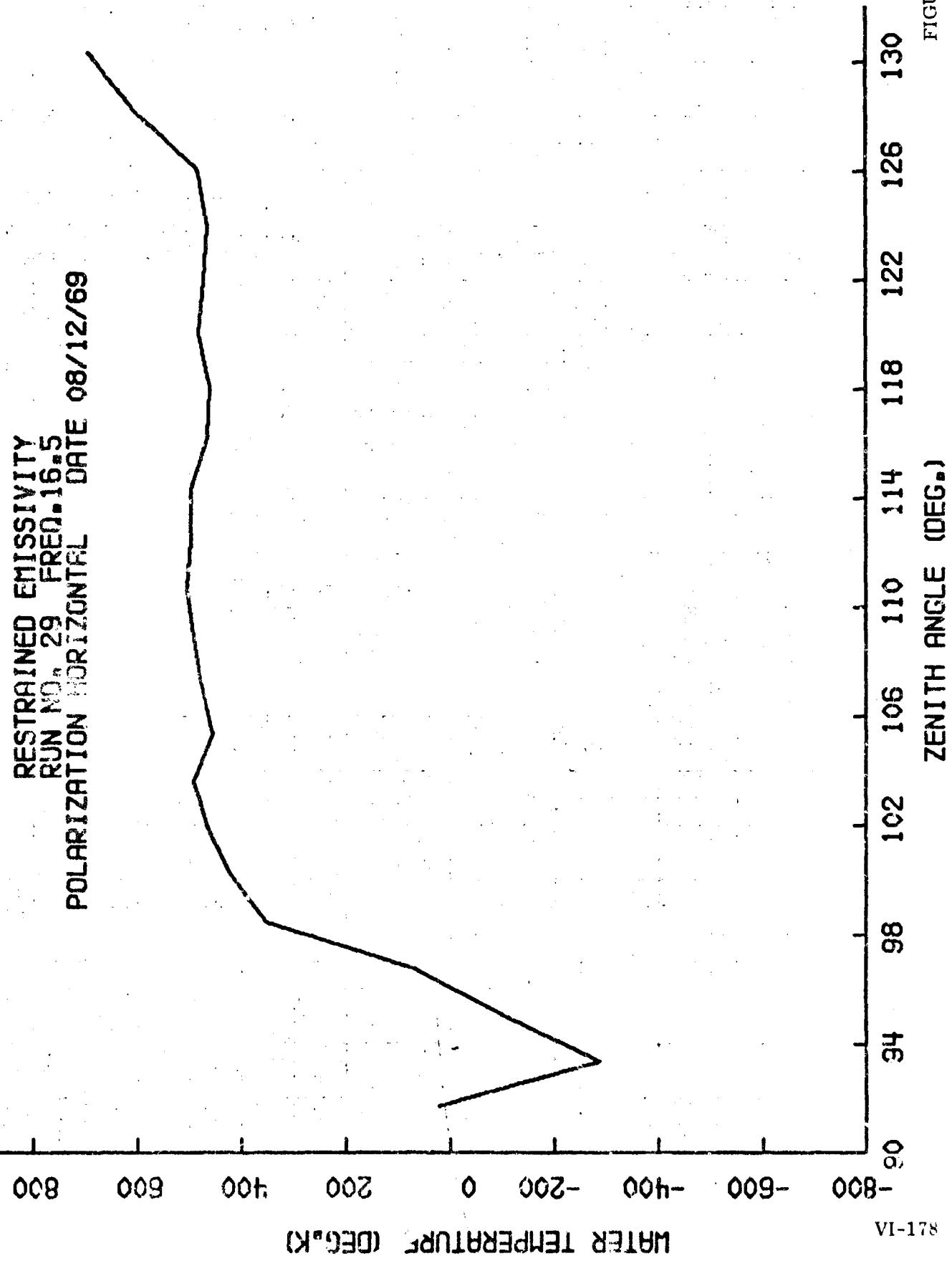
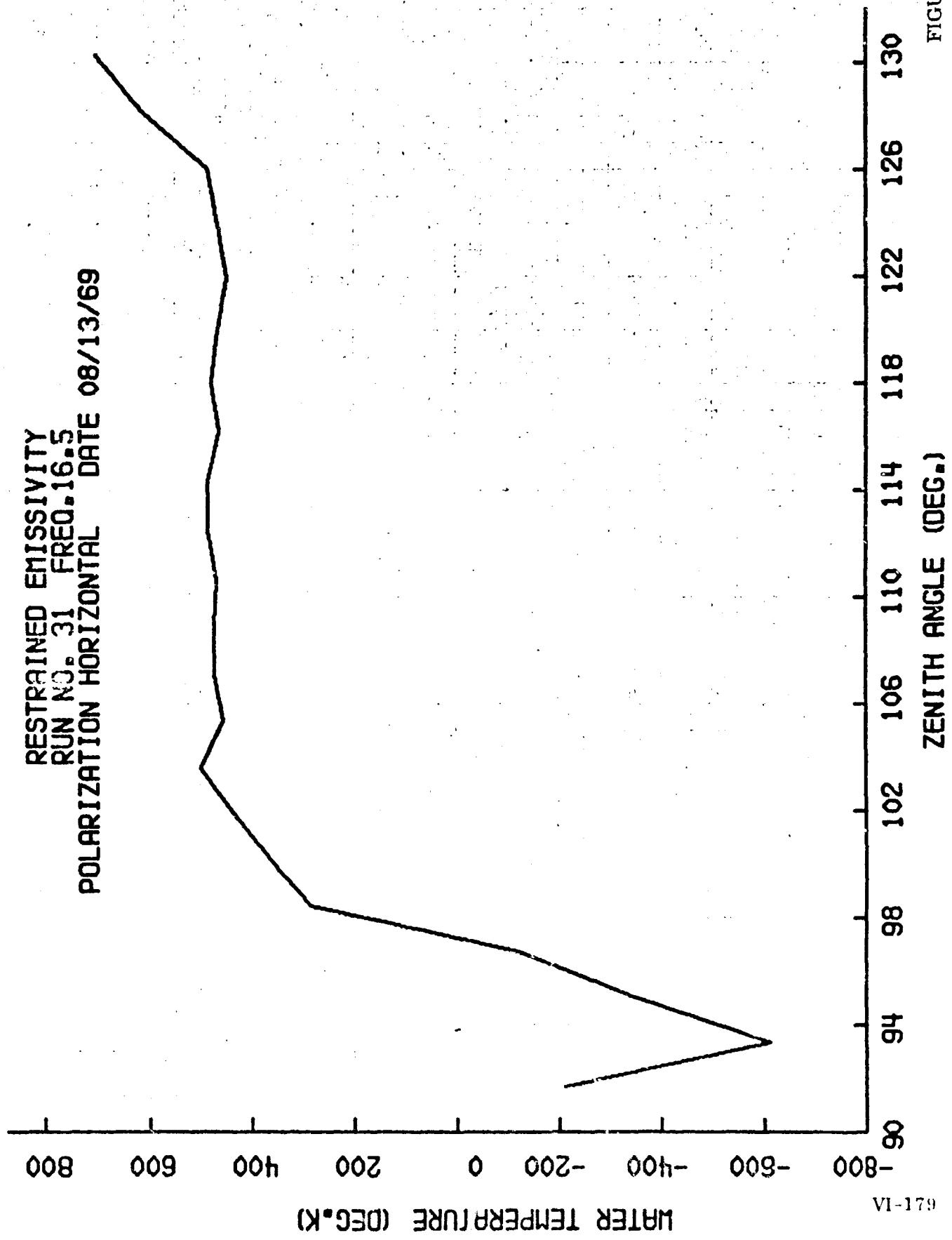
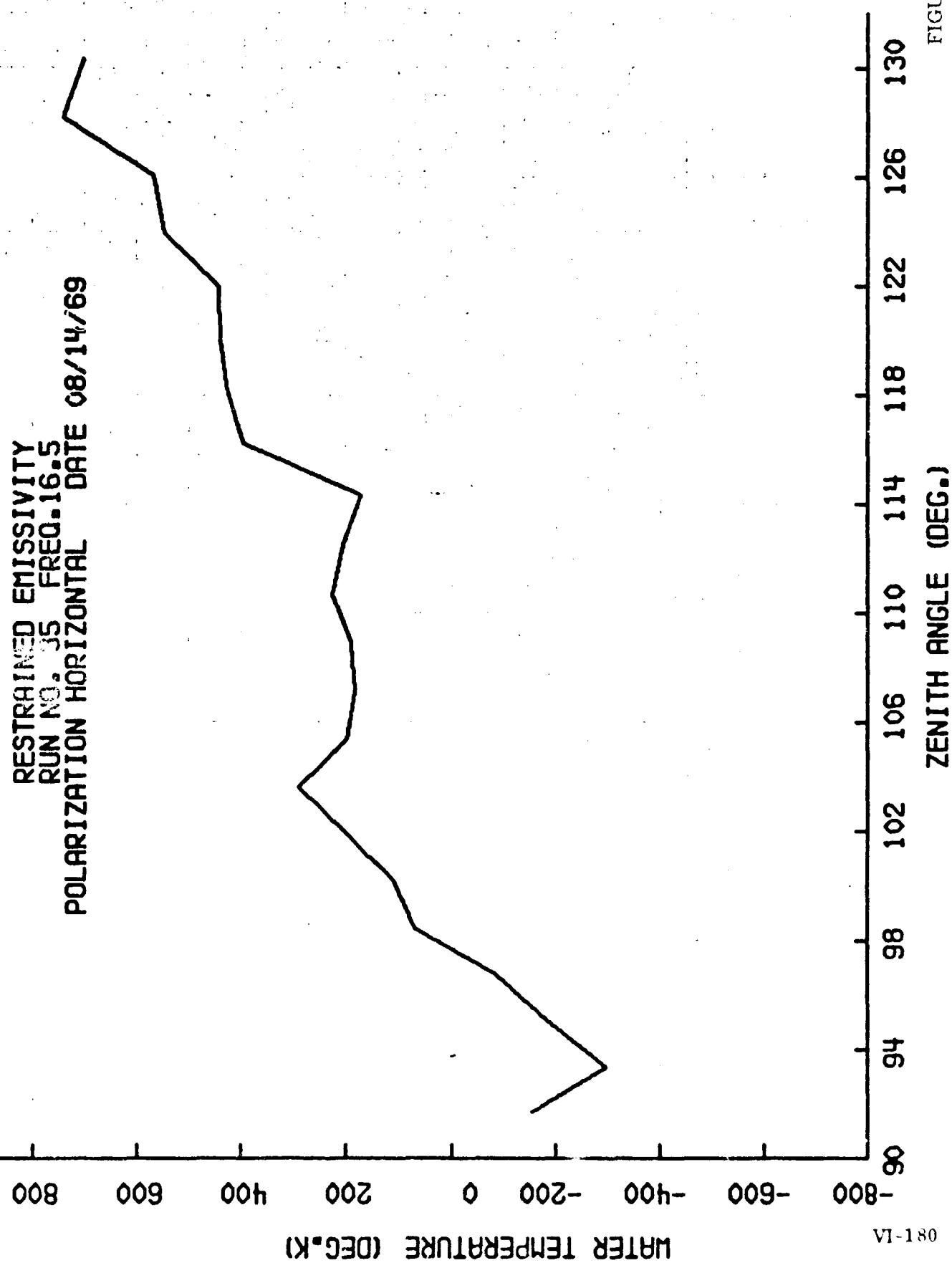


FIGURE VI-109

FIGURE VI-110





VI-180

FIGURE VI-111

RUNS 6 AND 5 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/01/69 VERT--- HORIZ---

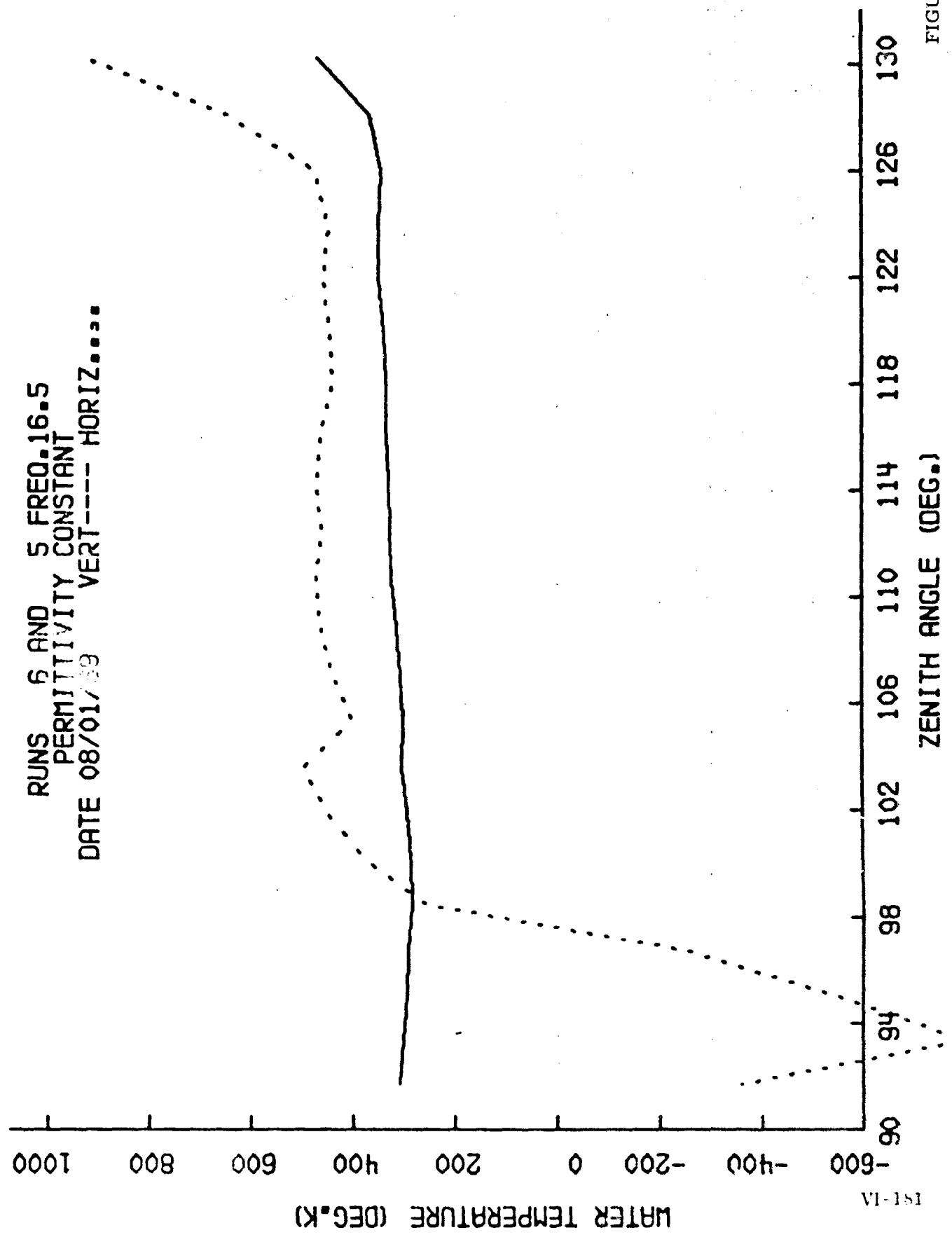
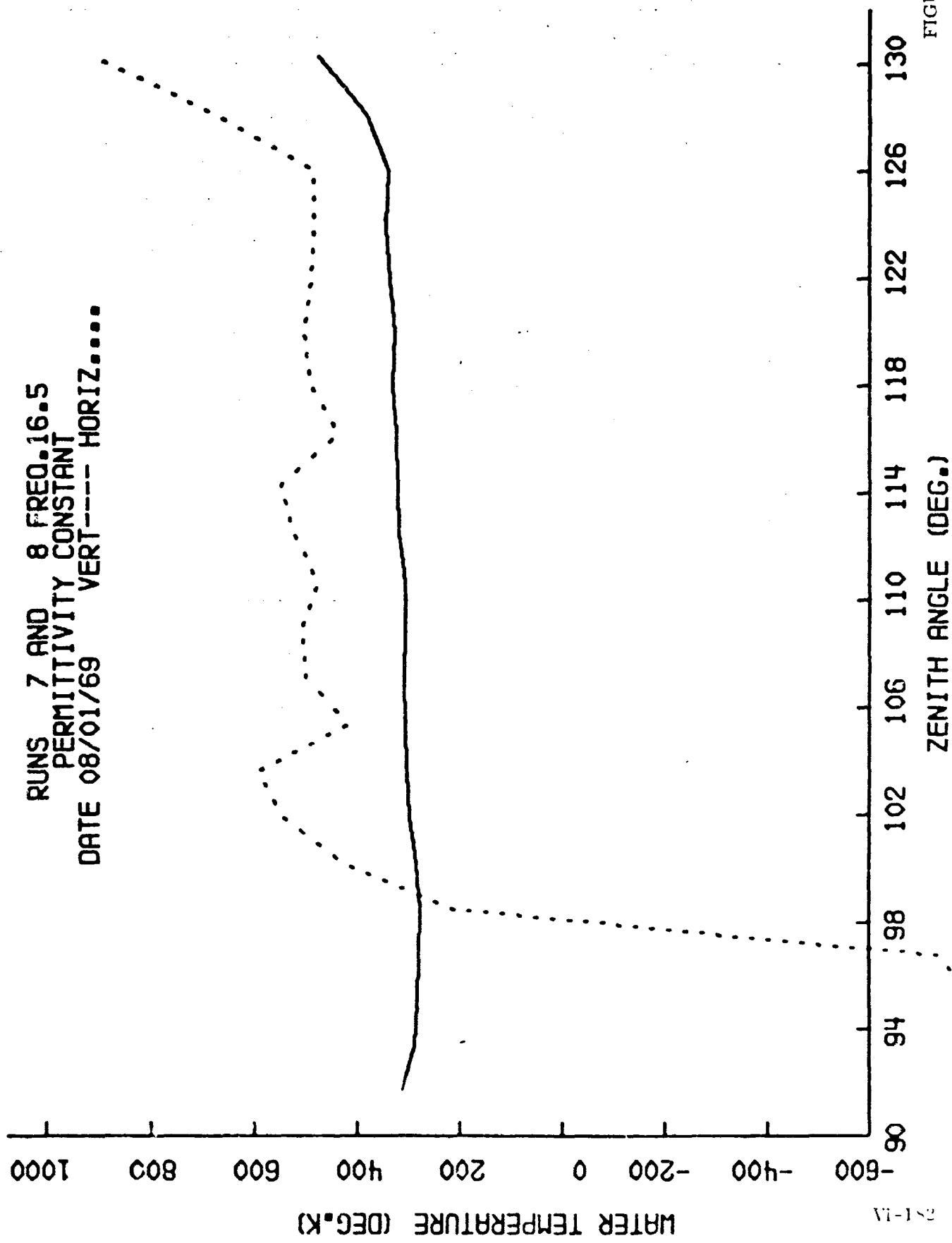


FIGURE VI-112

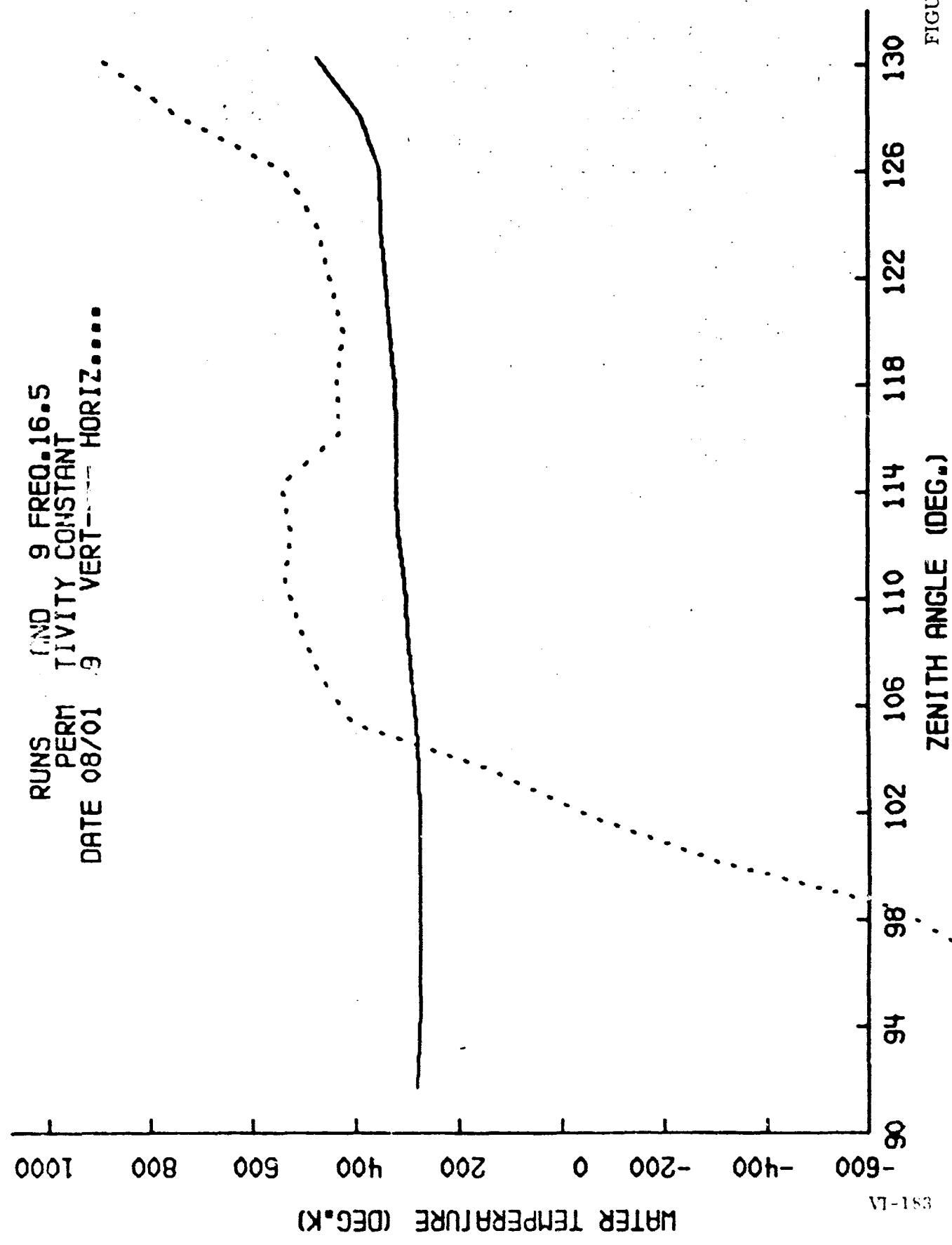
RUNS 7 AND 8 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/01/69 VERT--- HORIZ....



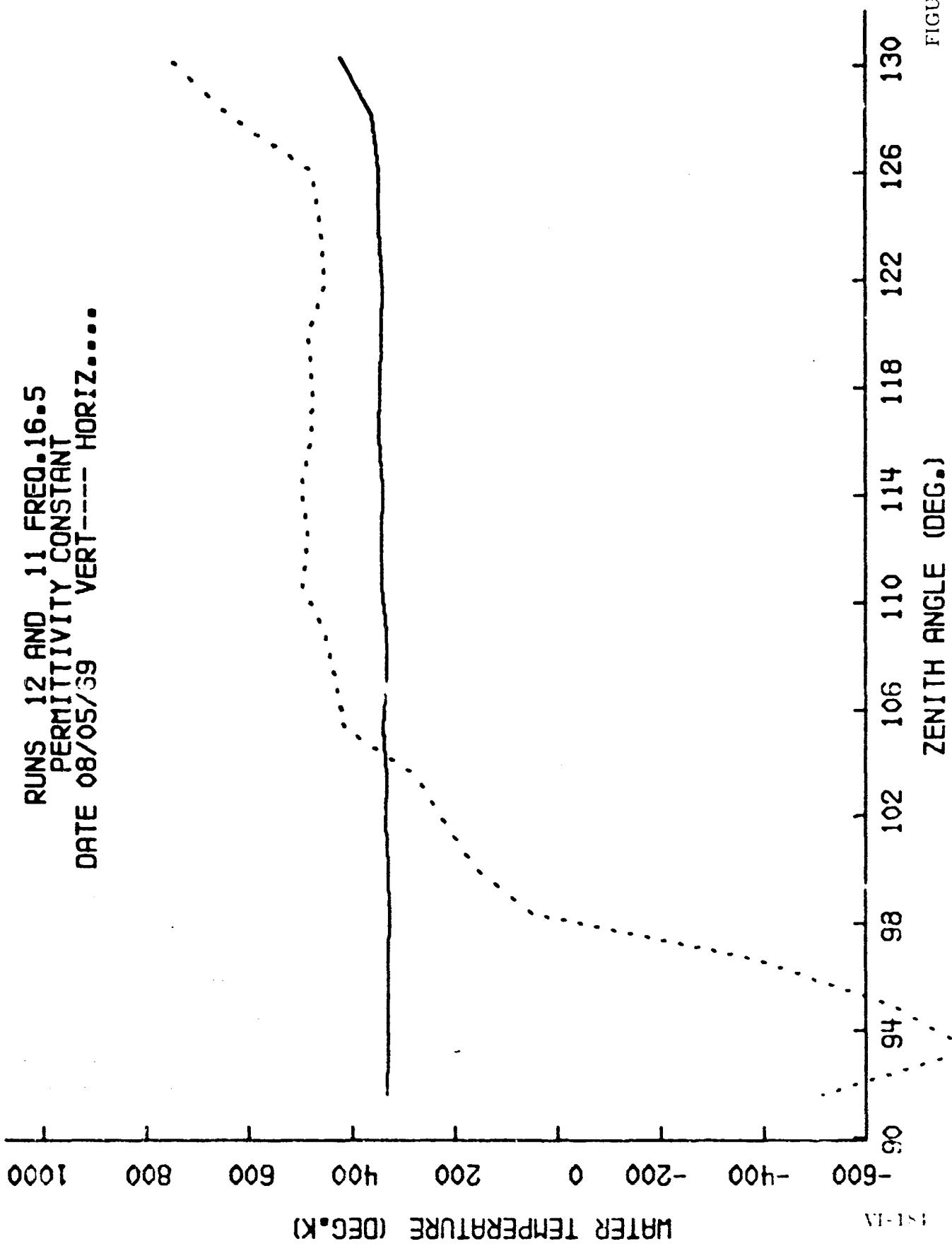
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FIGURE VI-113

FIGURE VI-114



RUNS 12 AND 11 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/05/59 VERT---HORIZ.....



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FIGURE VI-115

RUNS 4 HND 13 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/06/69 VERT---HORIZ....

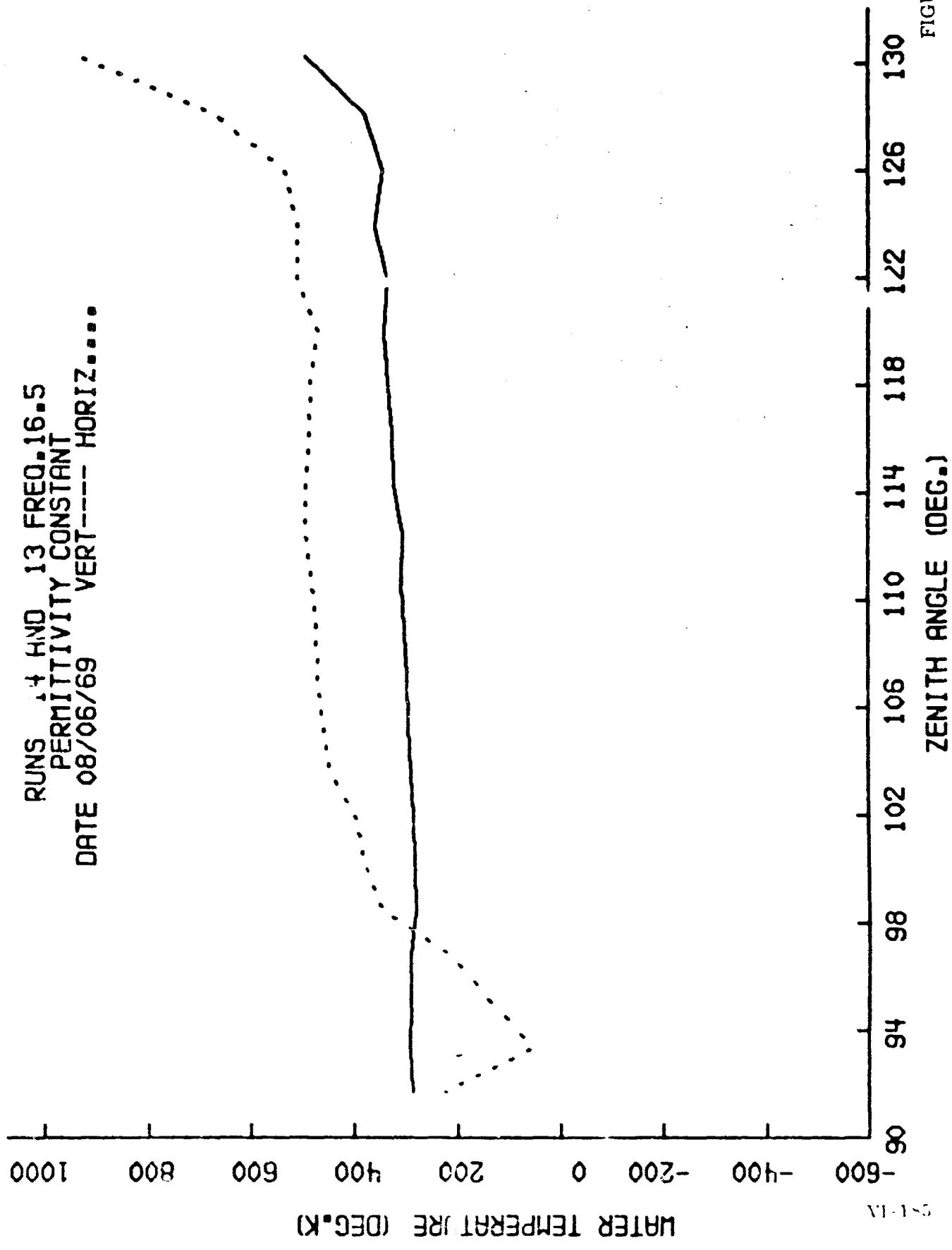
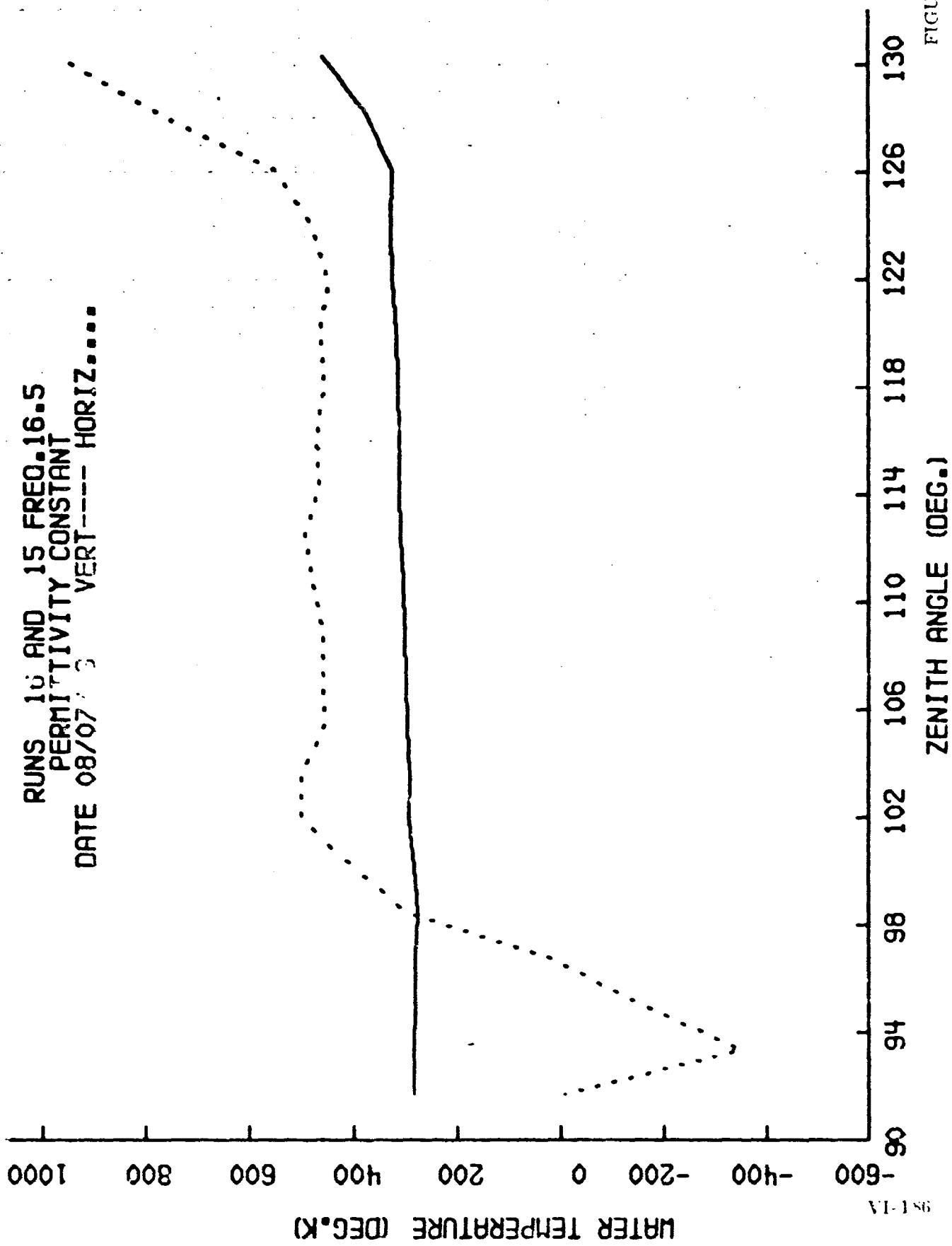


FIGURE VI-116

RUNS 16 AND 15 FREQ.16.5
PERMITTIVITY CONSTANT
DATE 08/07/73 VERT--- HORIZ....



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FIGURE VI-117

RUNS 17 AND 18 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/07/69 VERT--- HORIZ....

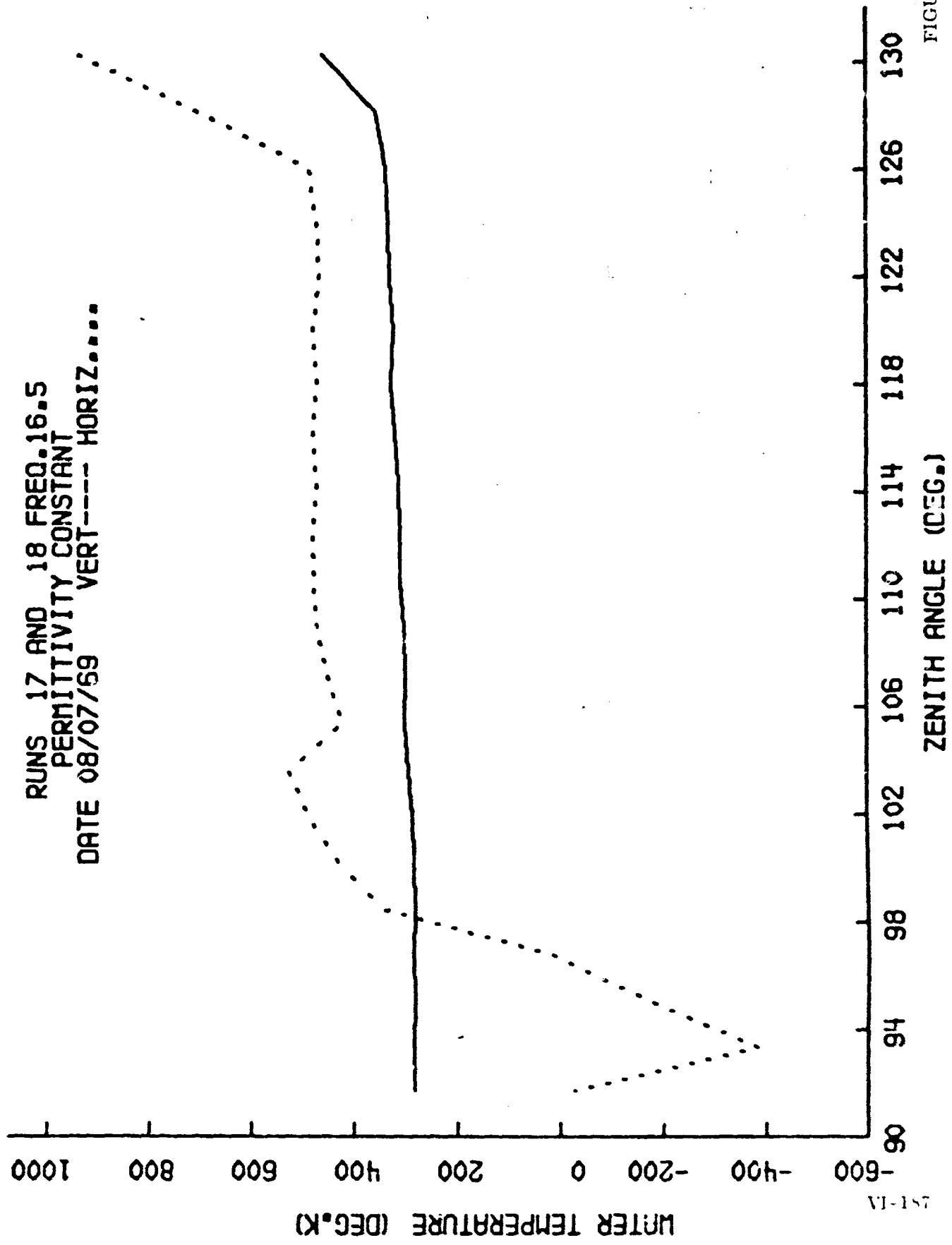


FIGURE VI-118

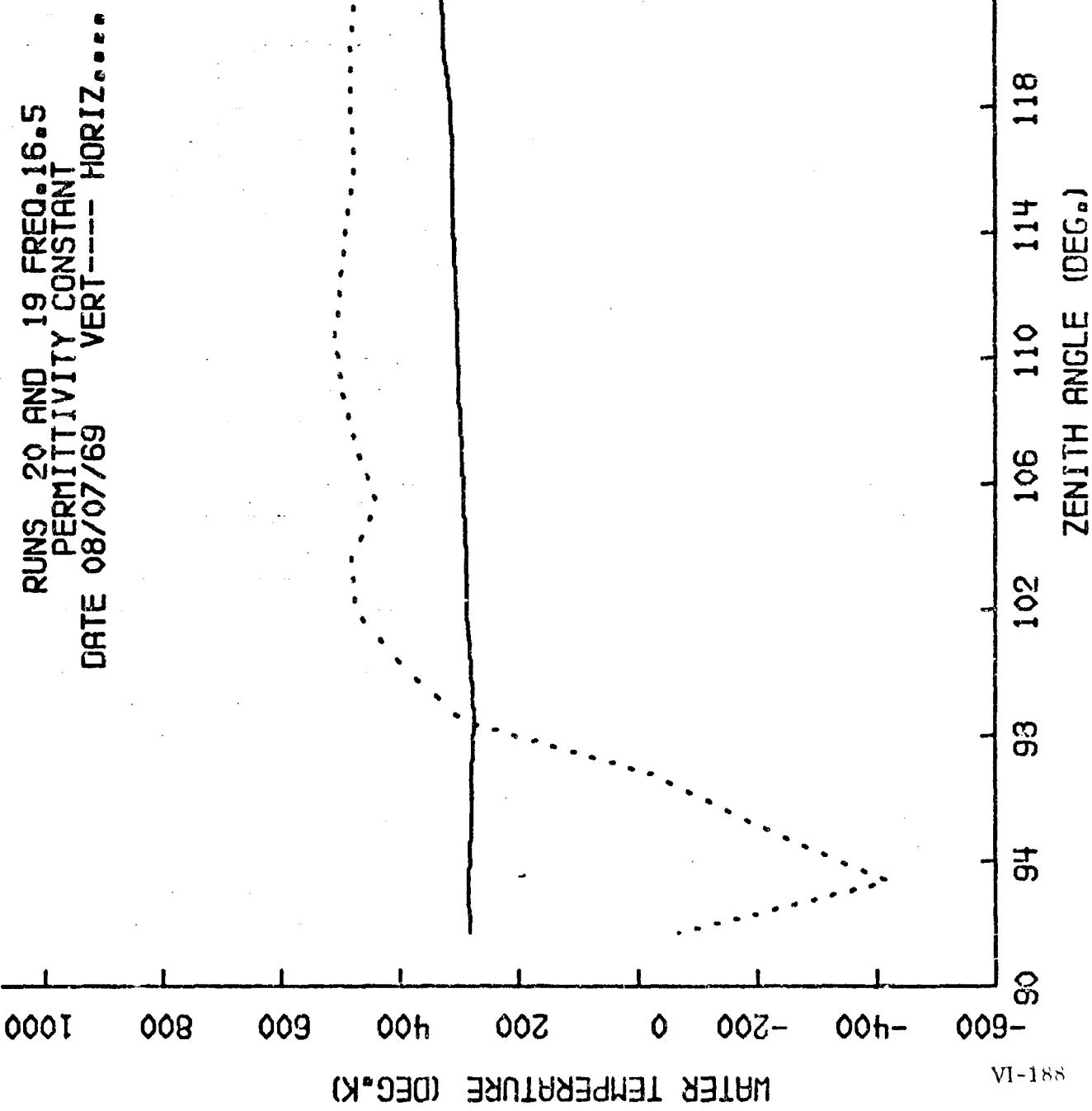


FIGURE VI-119

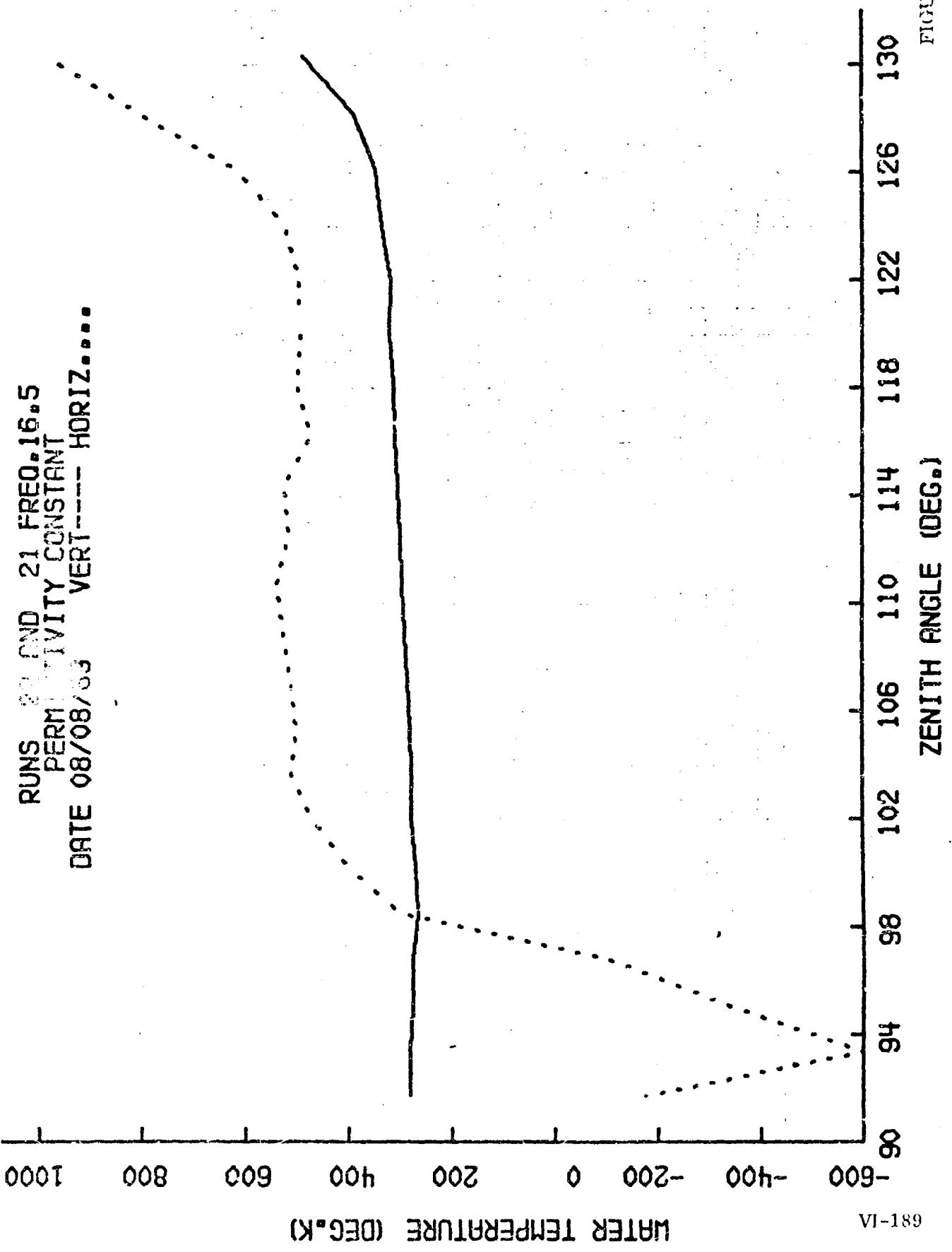
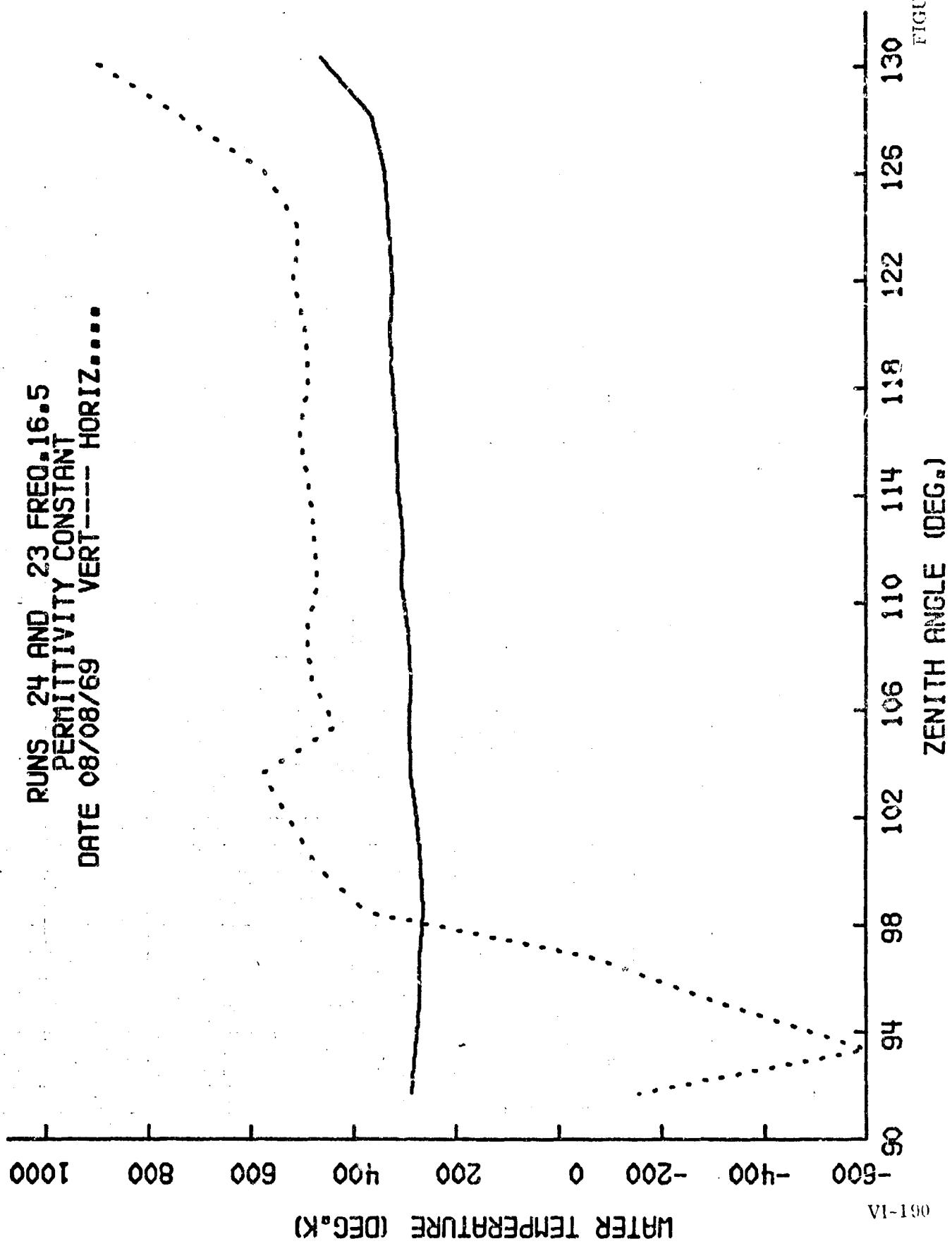
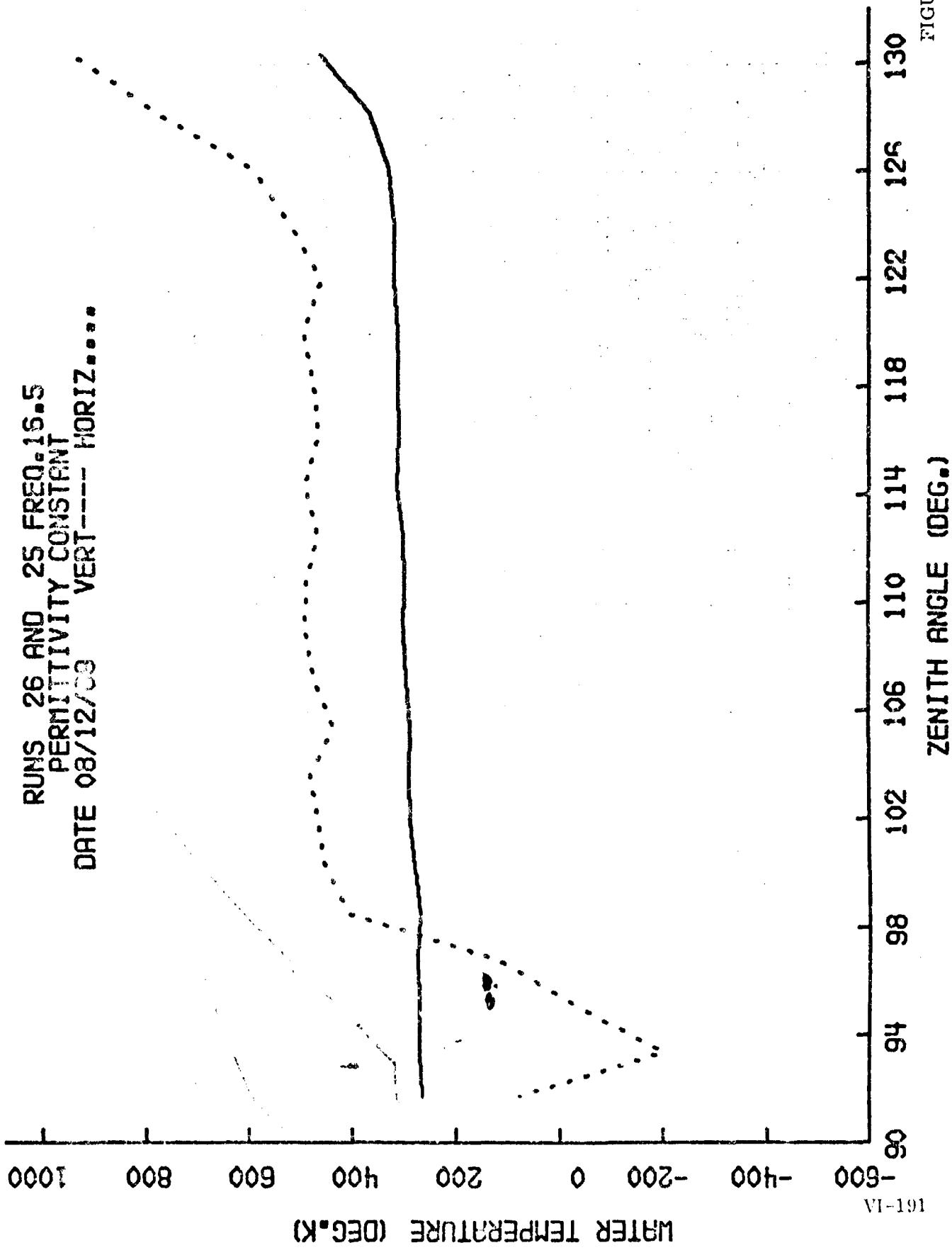


FIGURE VI-120

FIGURE VI-121



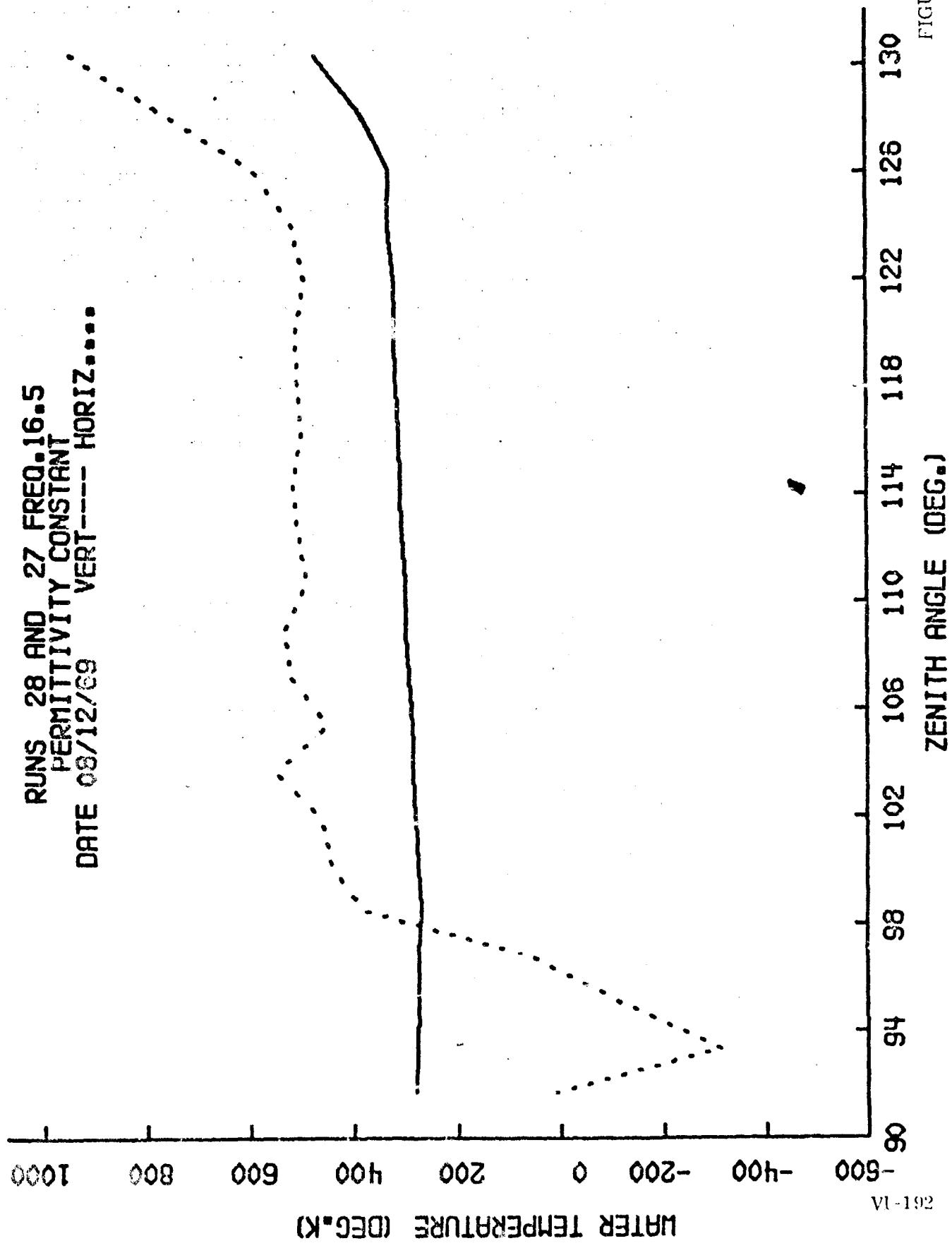
RUNS 26 AND 25 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/12/59 VERT---- HORIZ----



VI-191

FIGURE VI-122

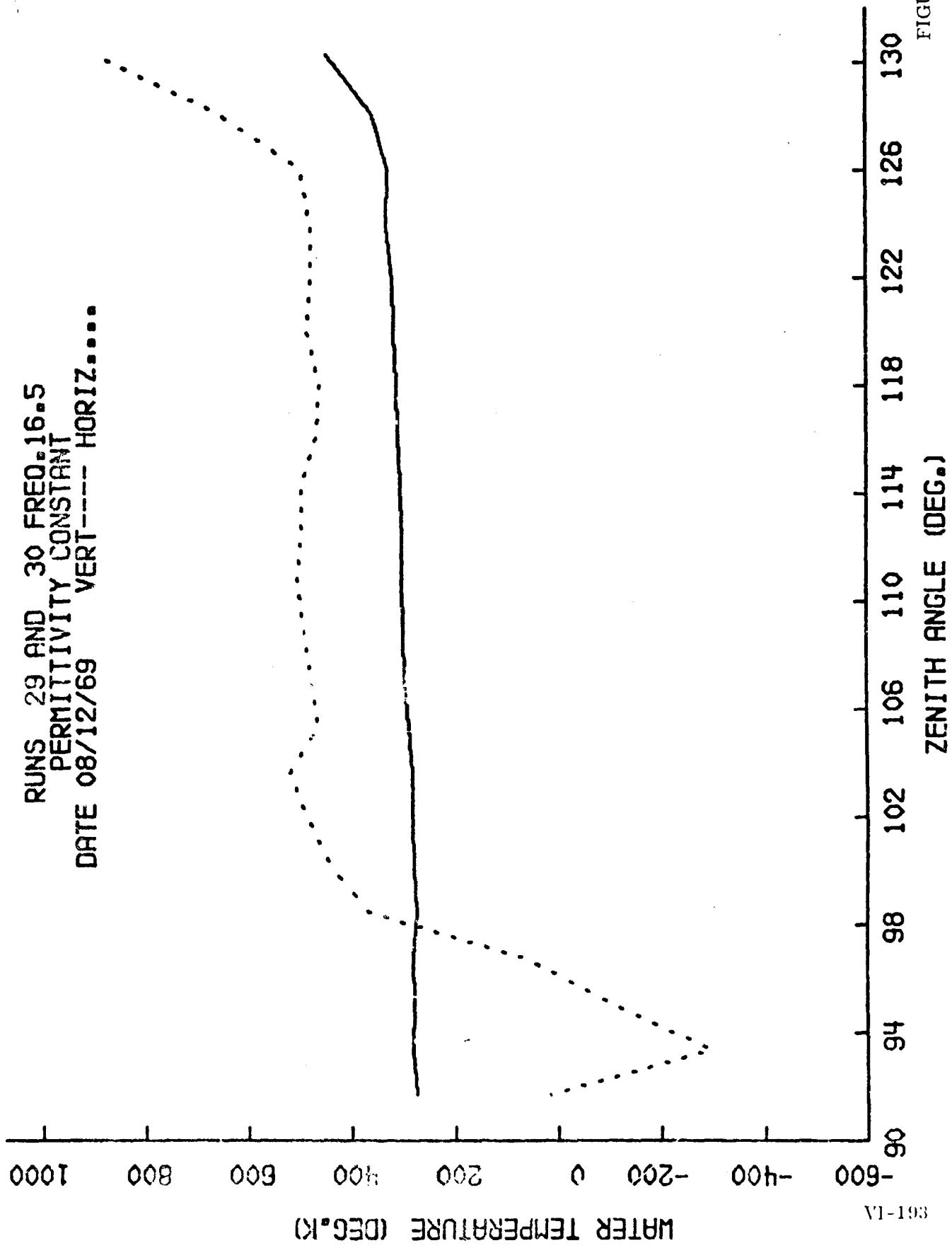
RUNS 28 AND 27 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 03/12/69 VERT--- HORIZ....



VI-192

FIGURE VI-123

RUNS 29 AND 30 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/12/69 VERT---- HORIZ----



VI-193

FIGURE VI-124

RUNS 31 AND 32 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/15/73 VERT---- HORIZ....

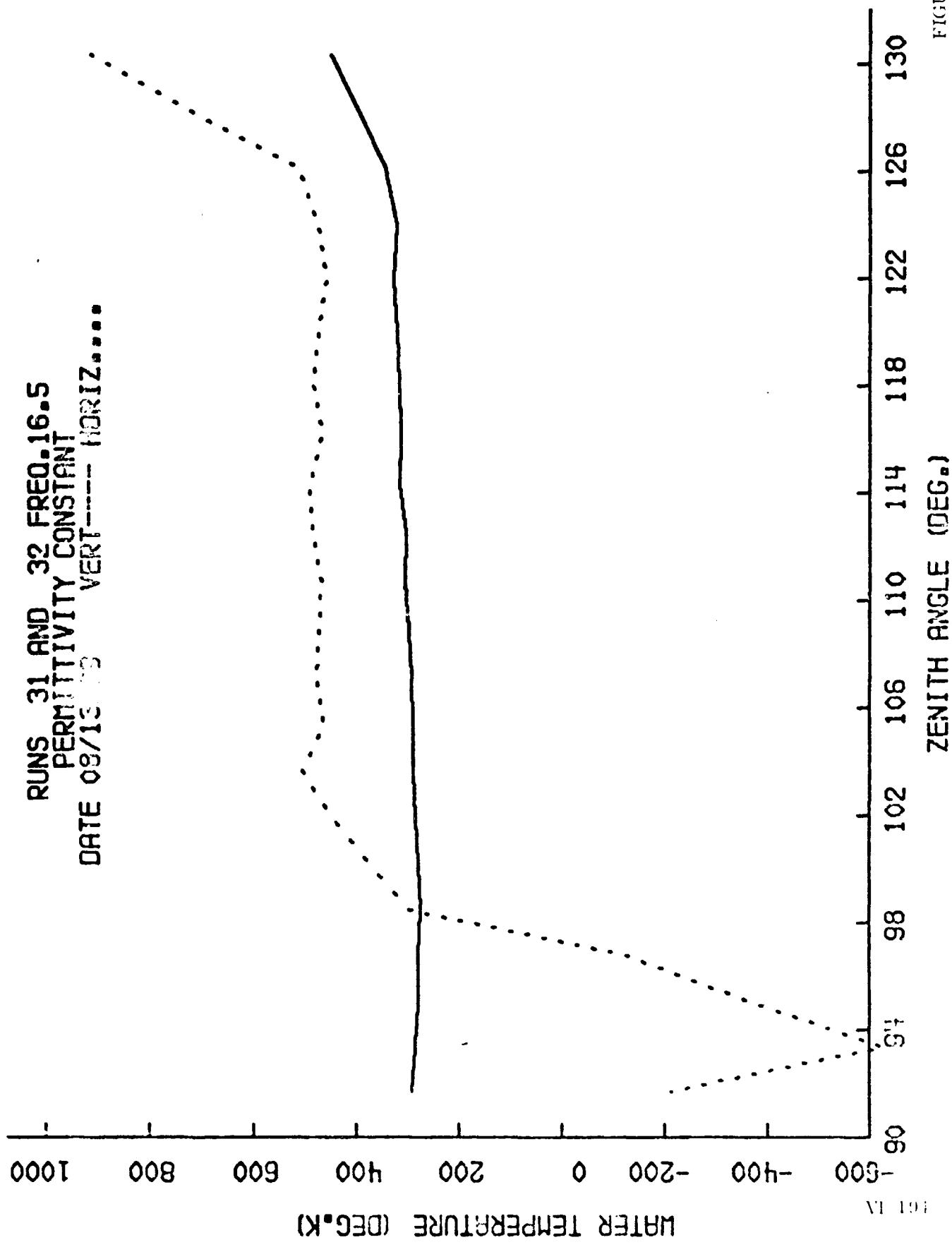
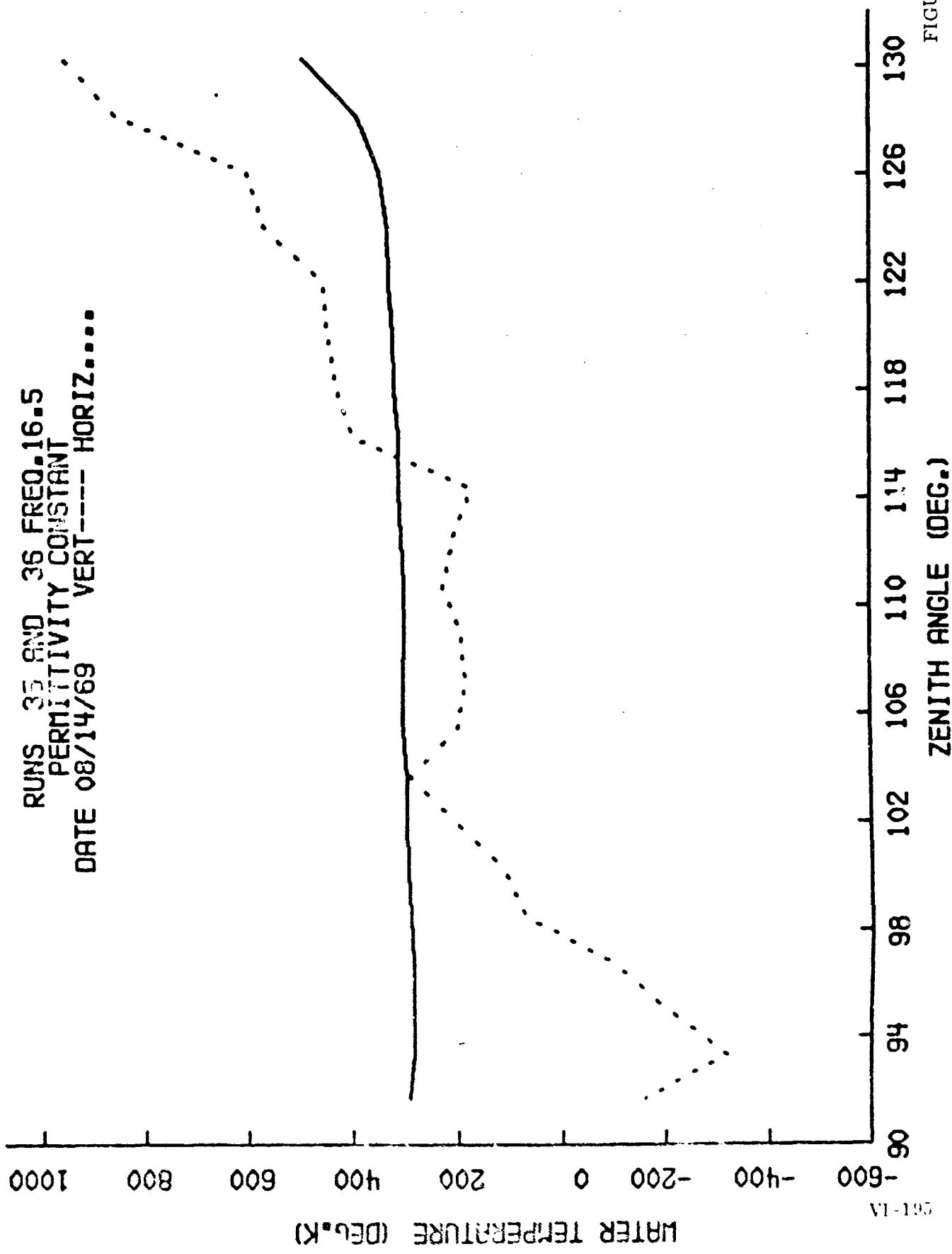


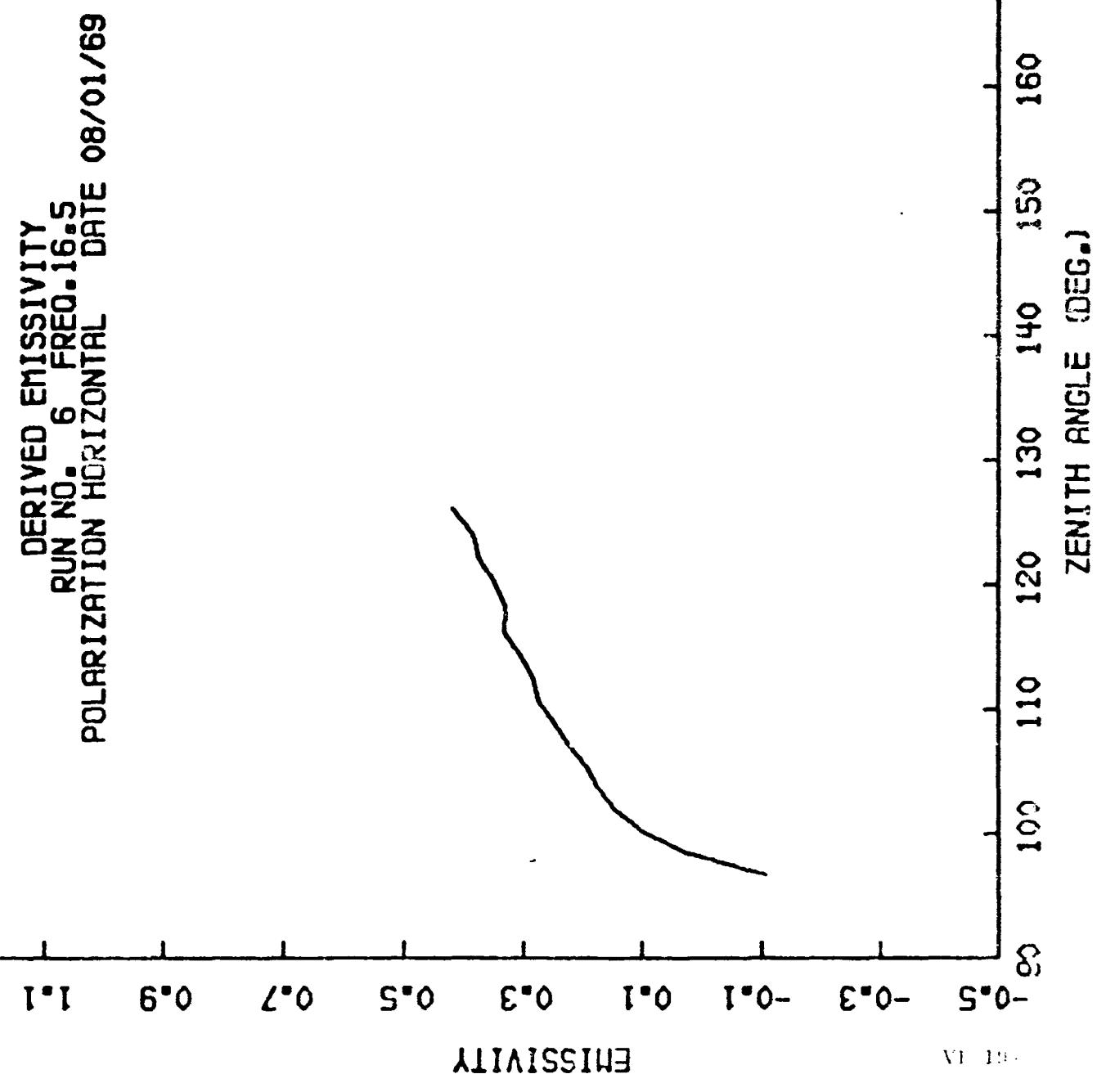
FIGURE VI-125

RUNS 35 AND 36 FREQ. 16.5
PERMITTIVITY CONSTANT
DATE 08/14/69 VERT--- HORIZ....



VI-195

FIGURE VI-126



VI-19

FIGURE VI-197

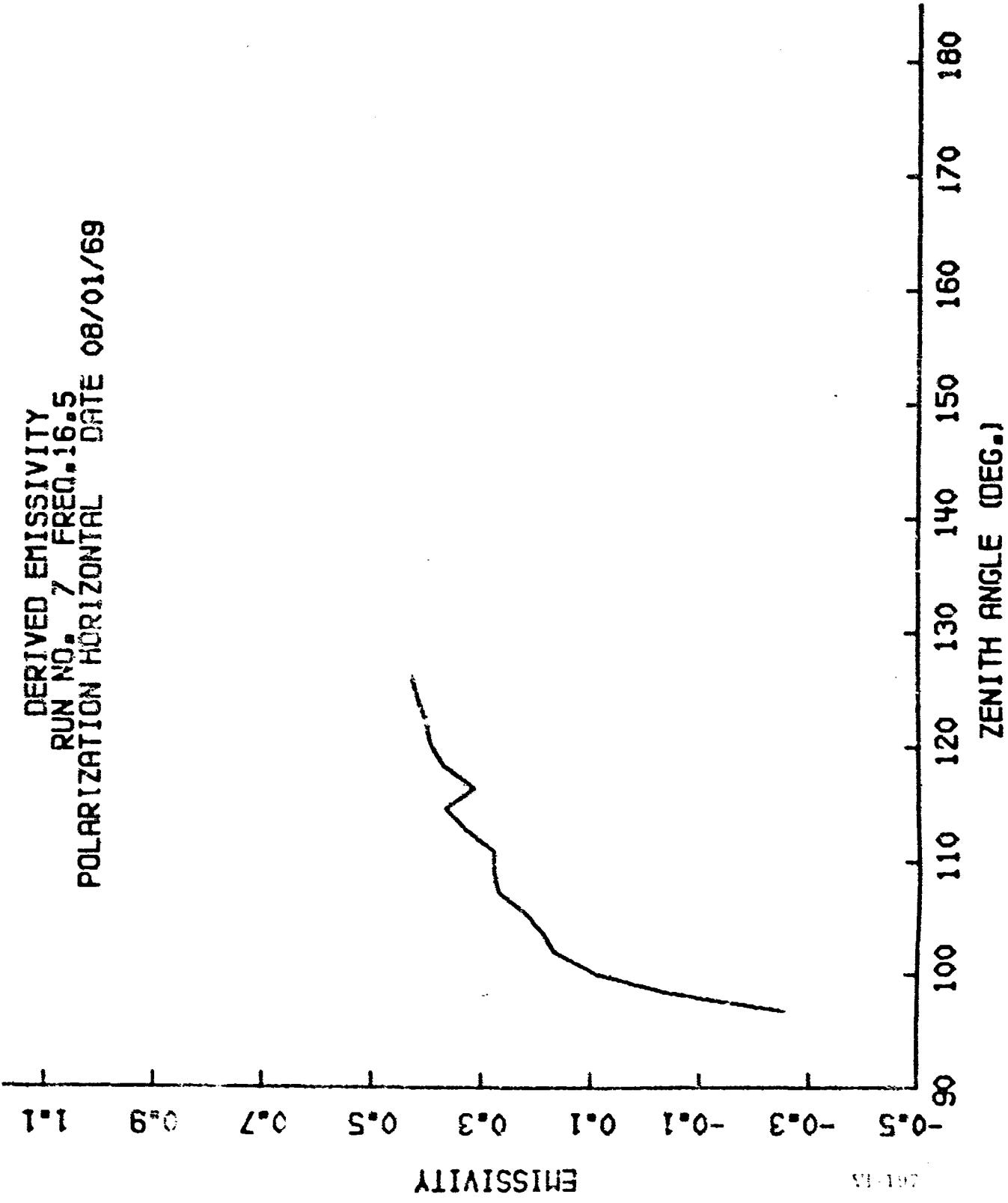


FIGURE VI-128

DERIVED EMISSIVITY
RUN NO. 10 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/01/69

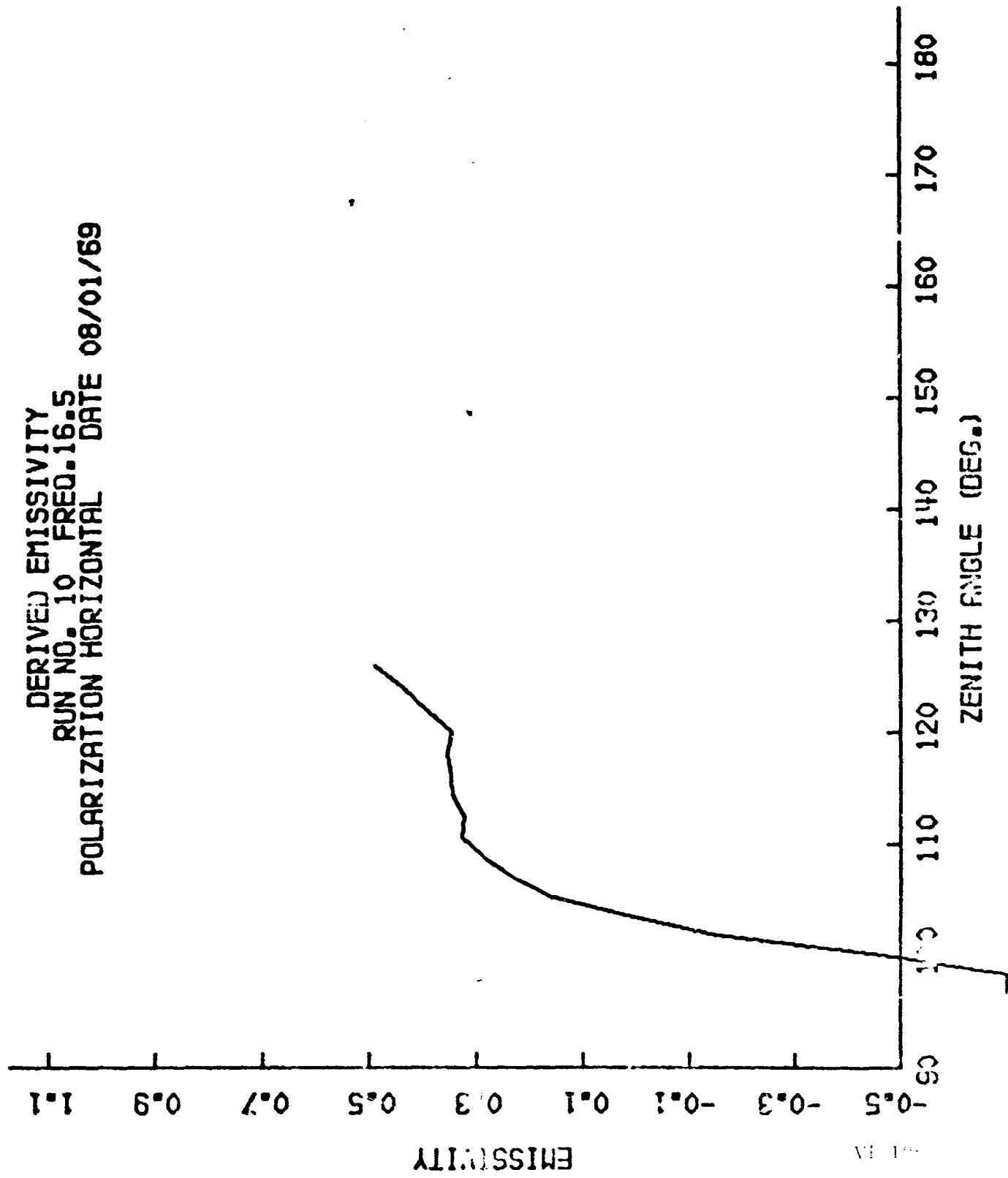
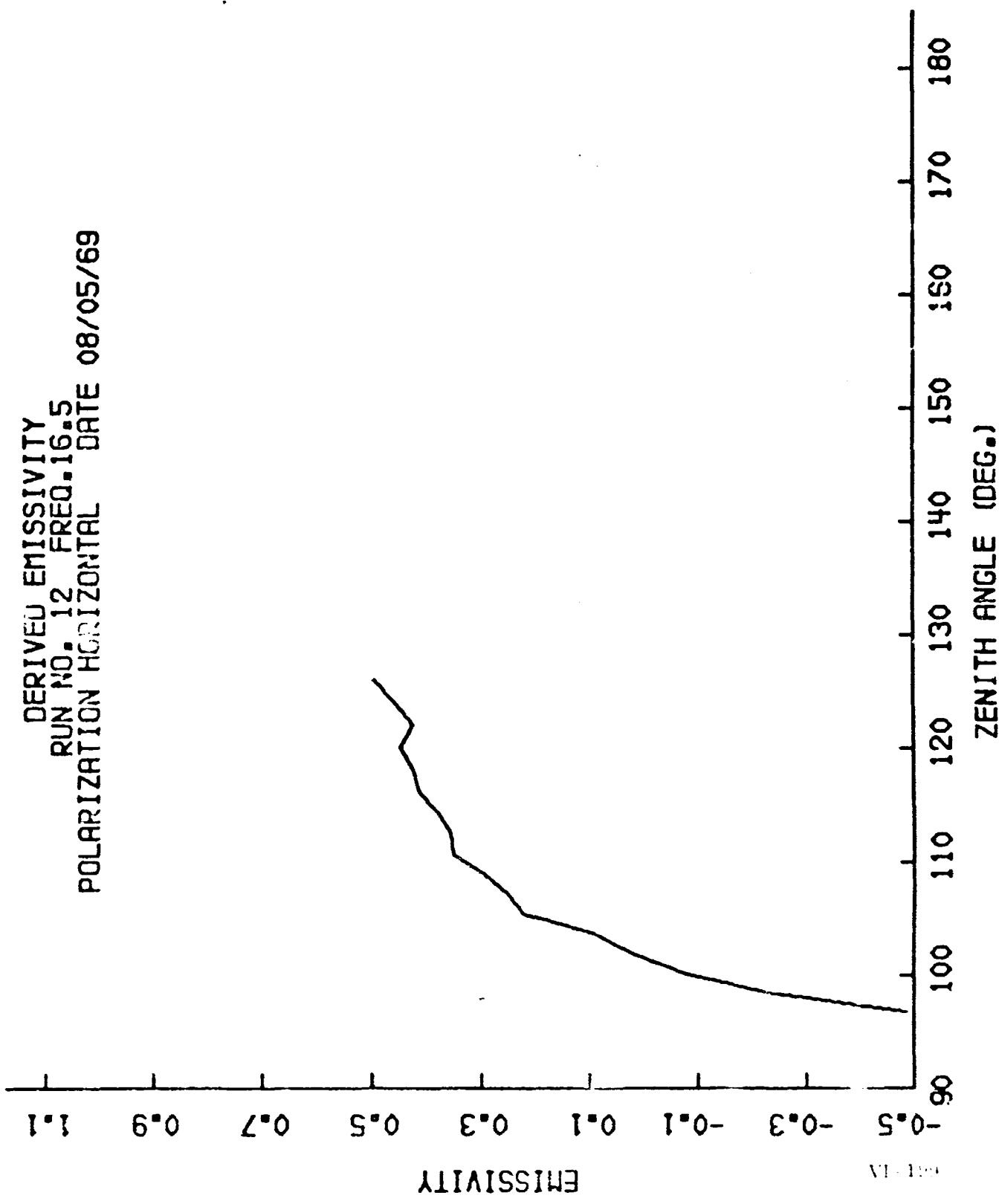


FIGURE VI-129

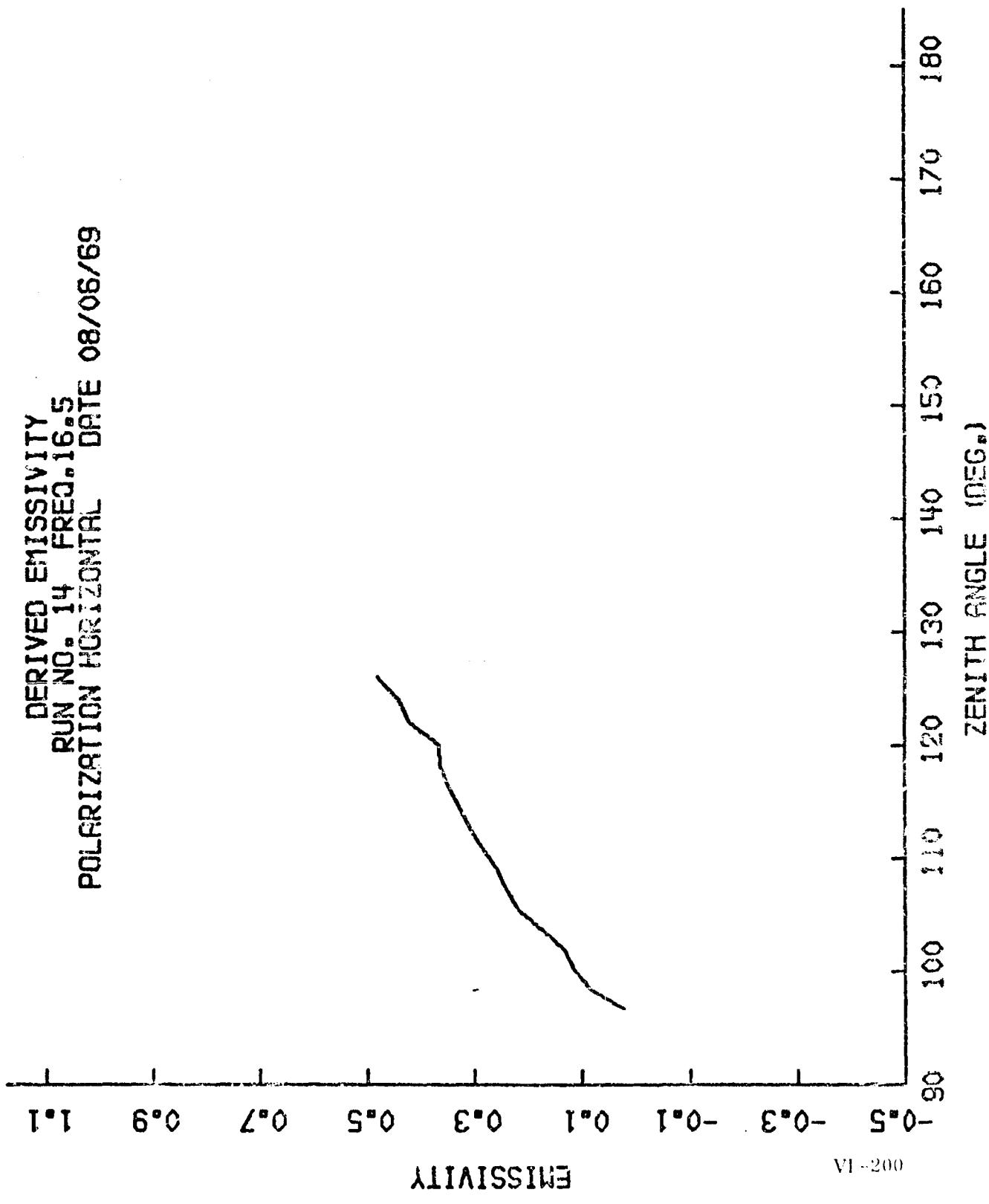
DERIVED EMISSIVITY
RUN NO. 12 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/05/69



VI-130

FIGURE VI-130

DERIVED EMISSIVITY
RUN NO. 14 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/06/69



VI-200

FIGURE VI-131

DERIVED EMISSIVITY
POLARIZATION 100° ZENITH 16° S
DATE 09/07/69

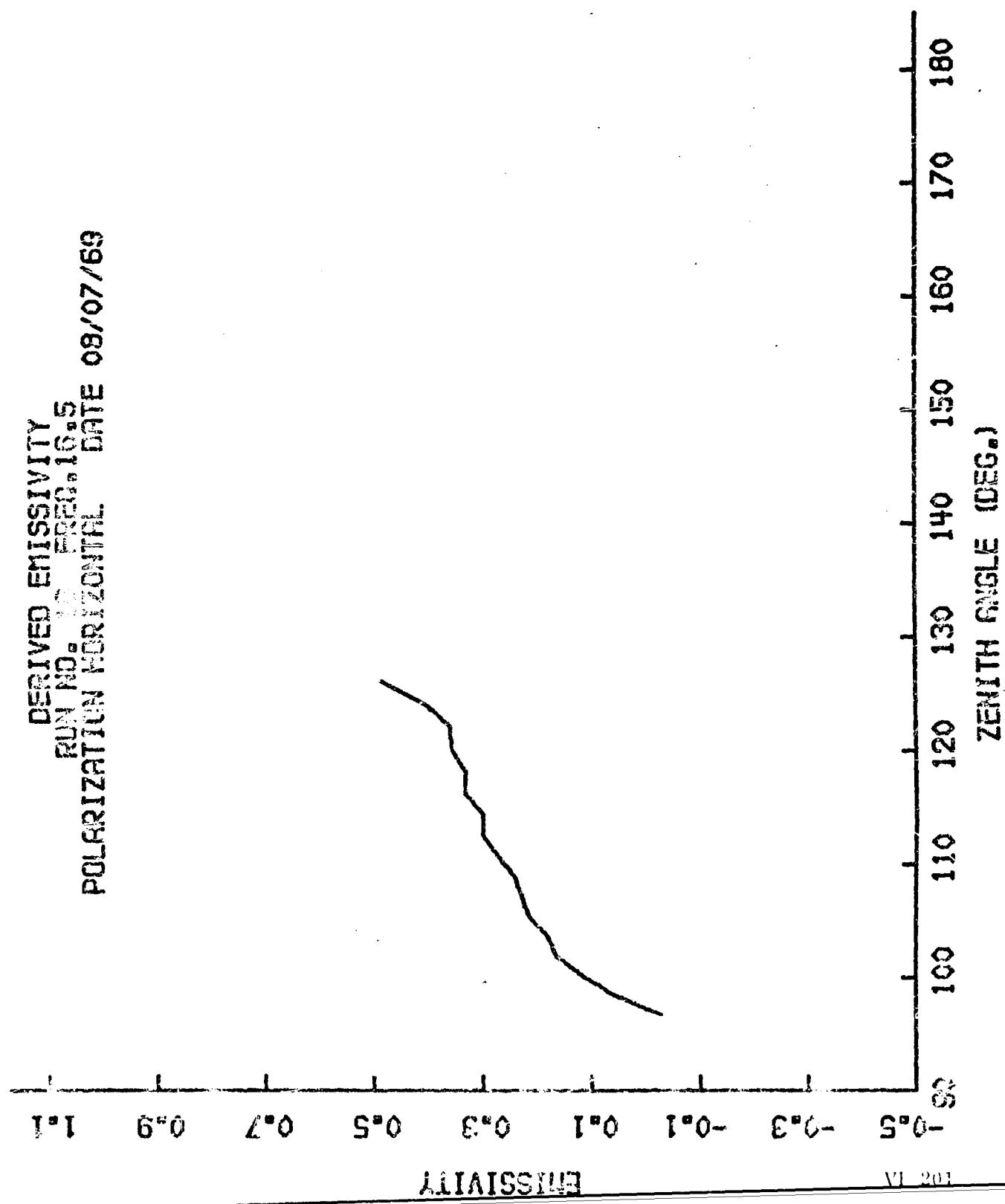
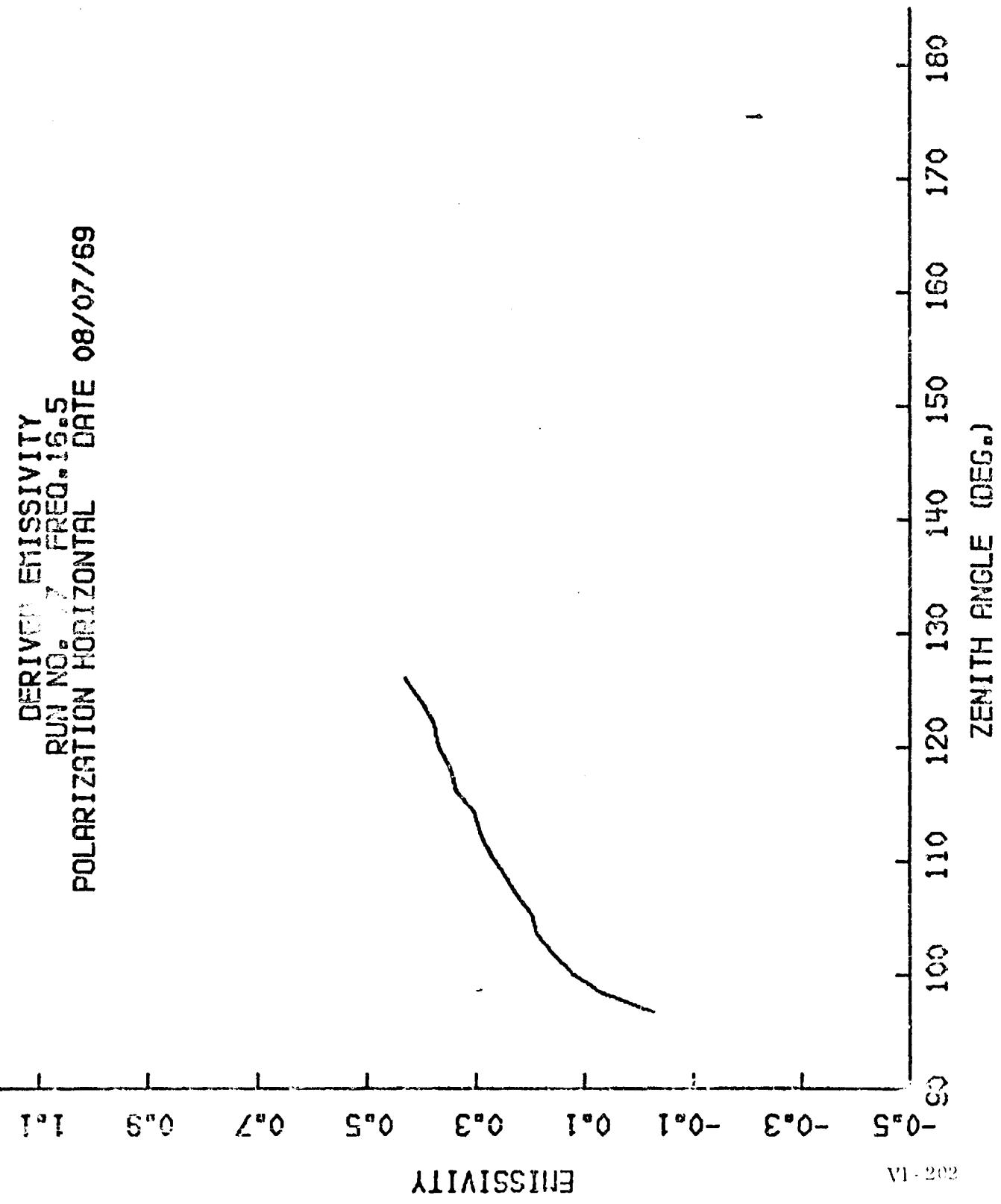


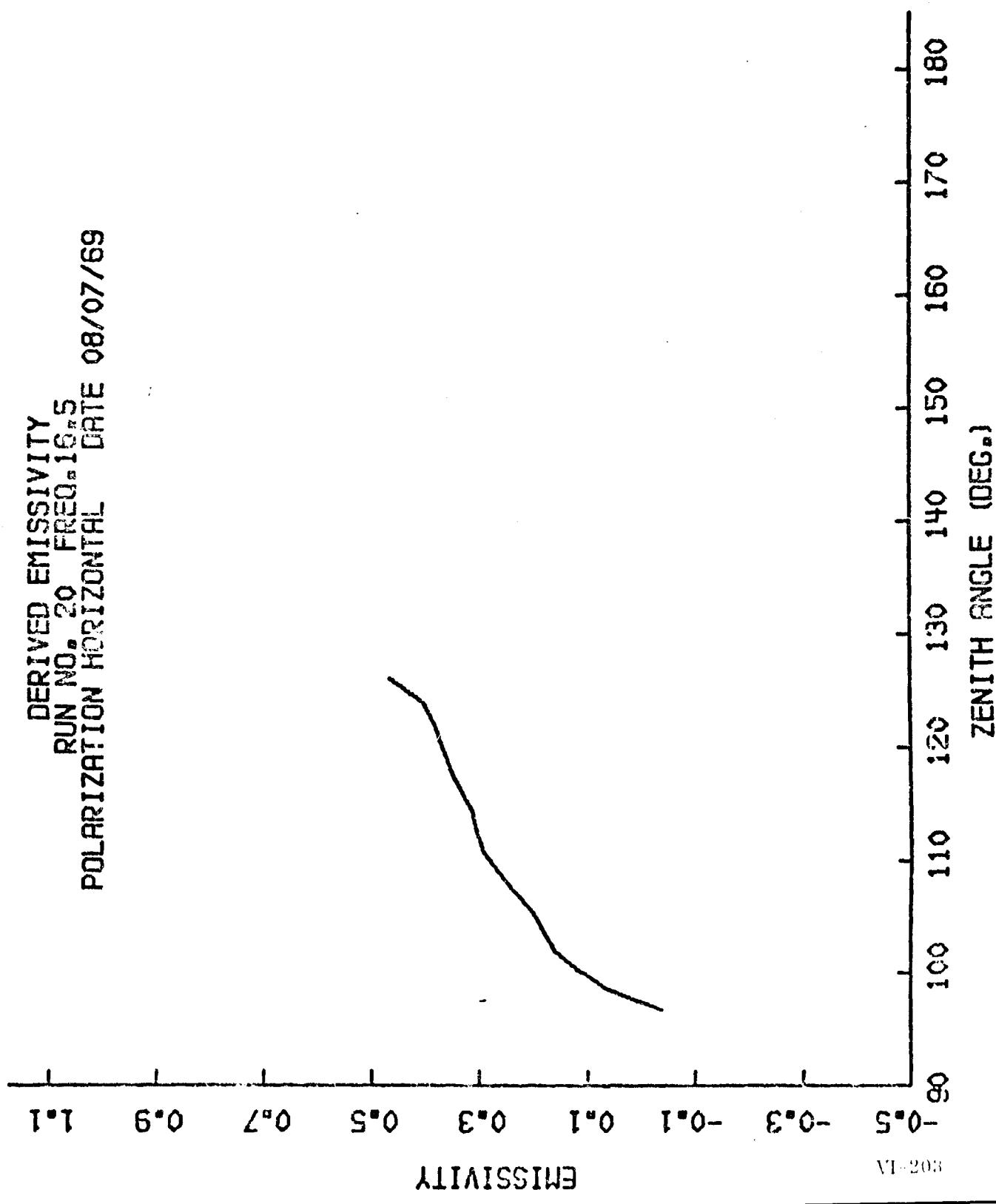
FIGURE VI-132

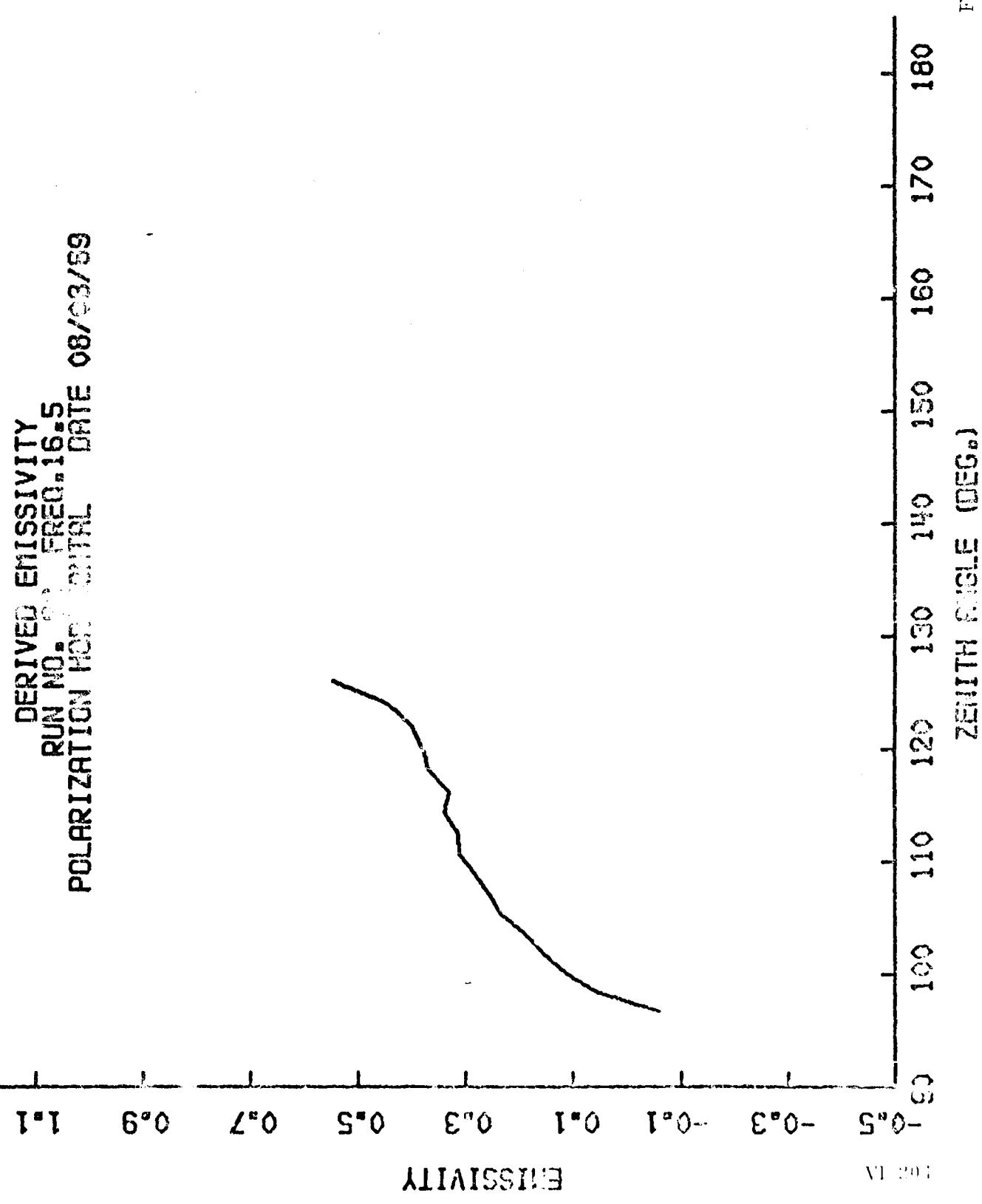


V1-202

FIGURE VI-139

DERIVED EMISSIVITY
RUN NO. 20 FREQ. 16⁵
POLARIZATION HORIZONTAL DATE 08/07/69





VI-294

FIGURE VI-135

DERIVED EMISSIVITY
RUN NO. 201 FREQ. 16.5
POLARIZATION HCP DATE 08/09/69

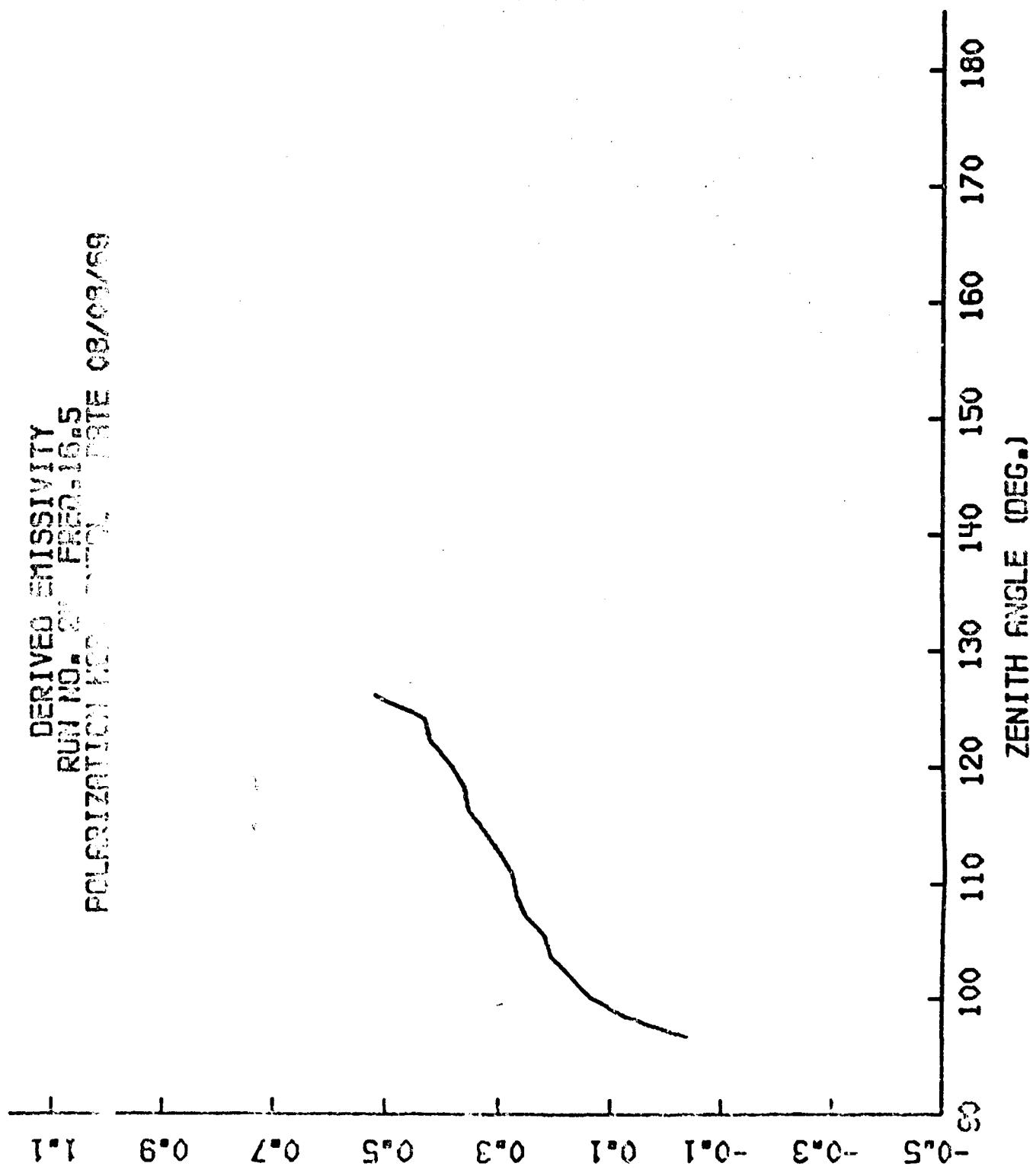
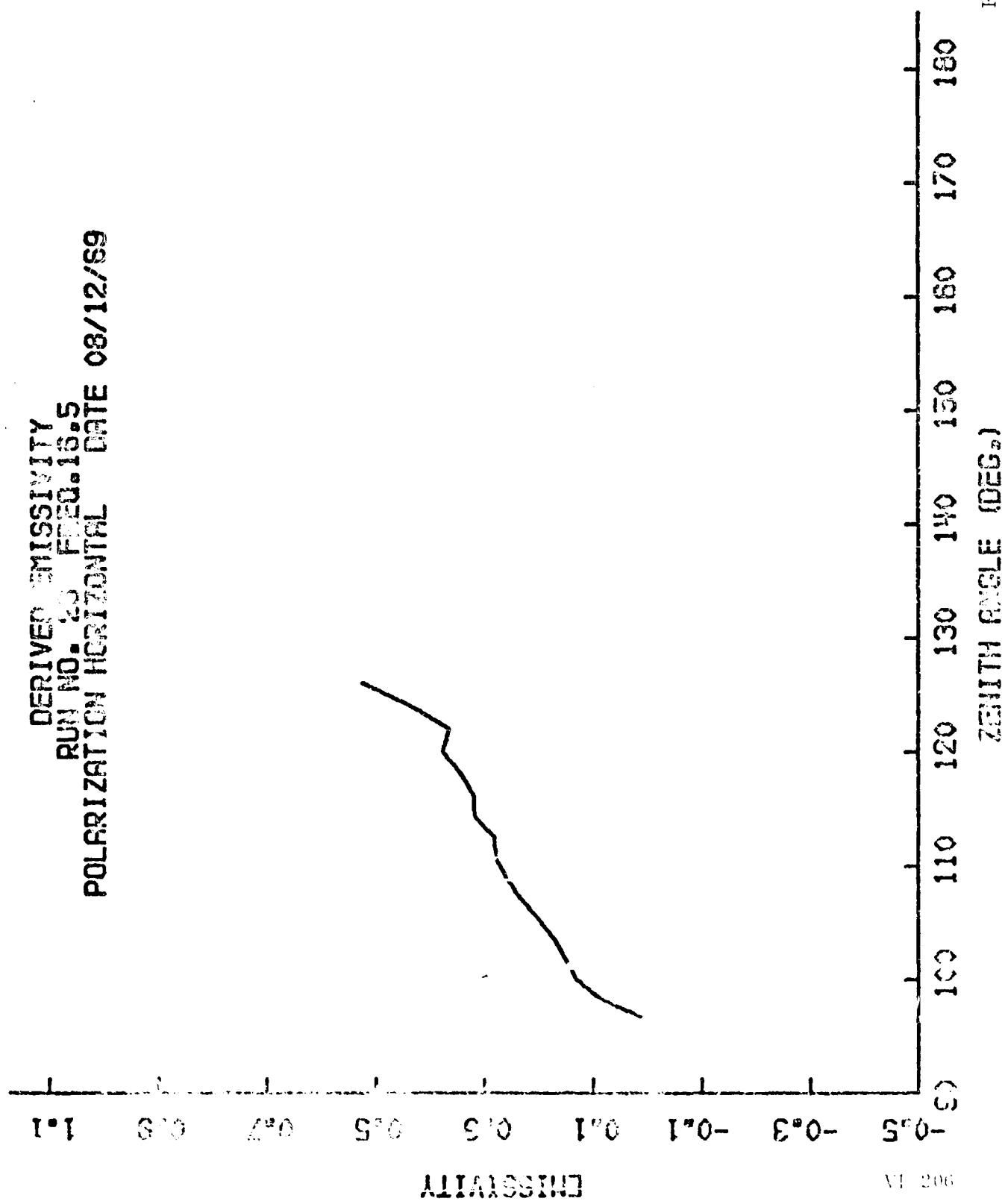


FIGURE VI-136

DERIVED EMISSIVITY
RUN NO. 23 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 03/12/69



DERIVED EMISSIVITY
EQUI NO. 1655
ZENITH ANGLE = 16.5°
POLARIZATION HORIZONTAL DATE 08/12/69

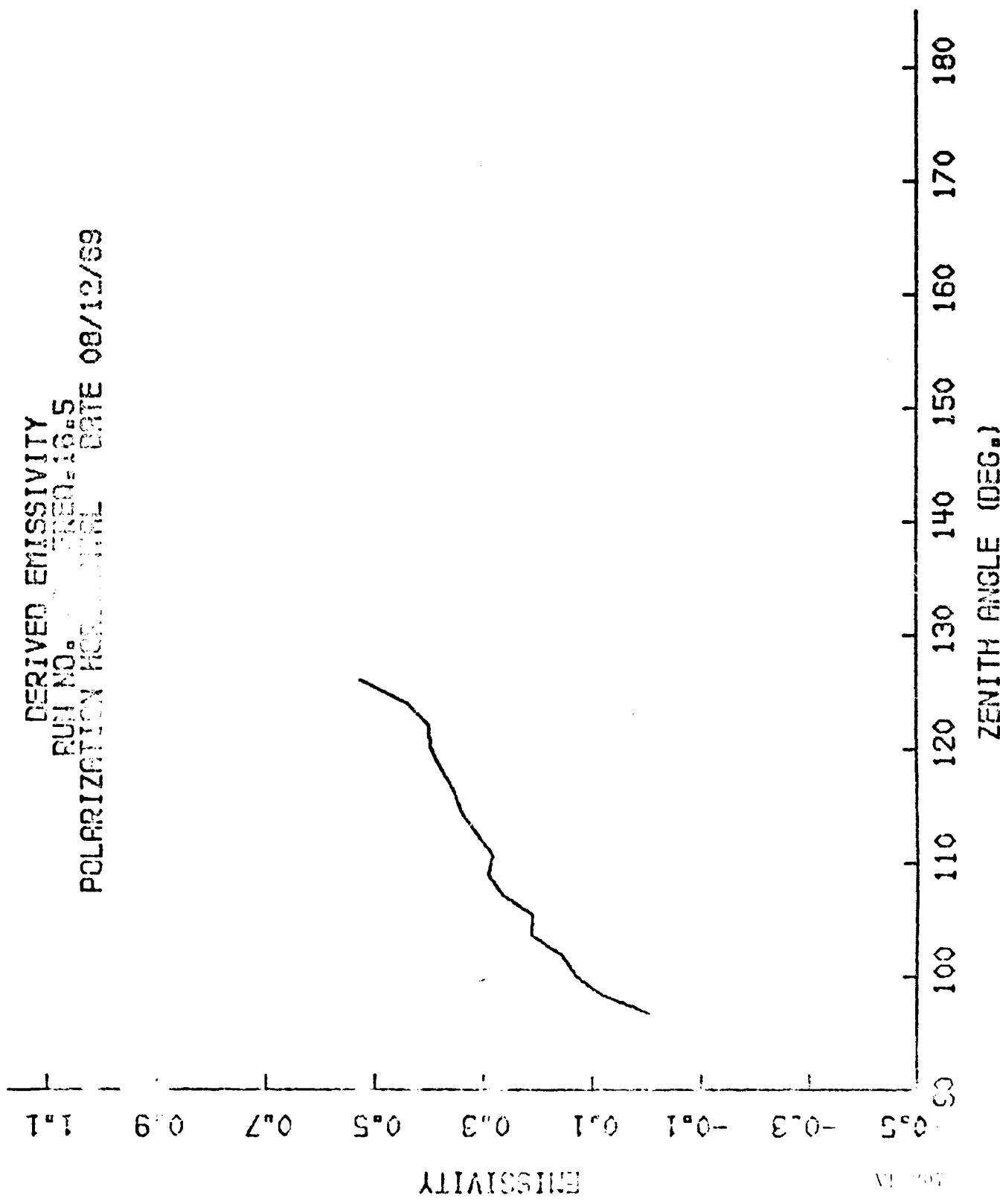


FIGURE VI-138

DERIVED EMISSIVITY
RUN NO. 29 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/12/69

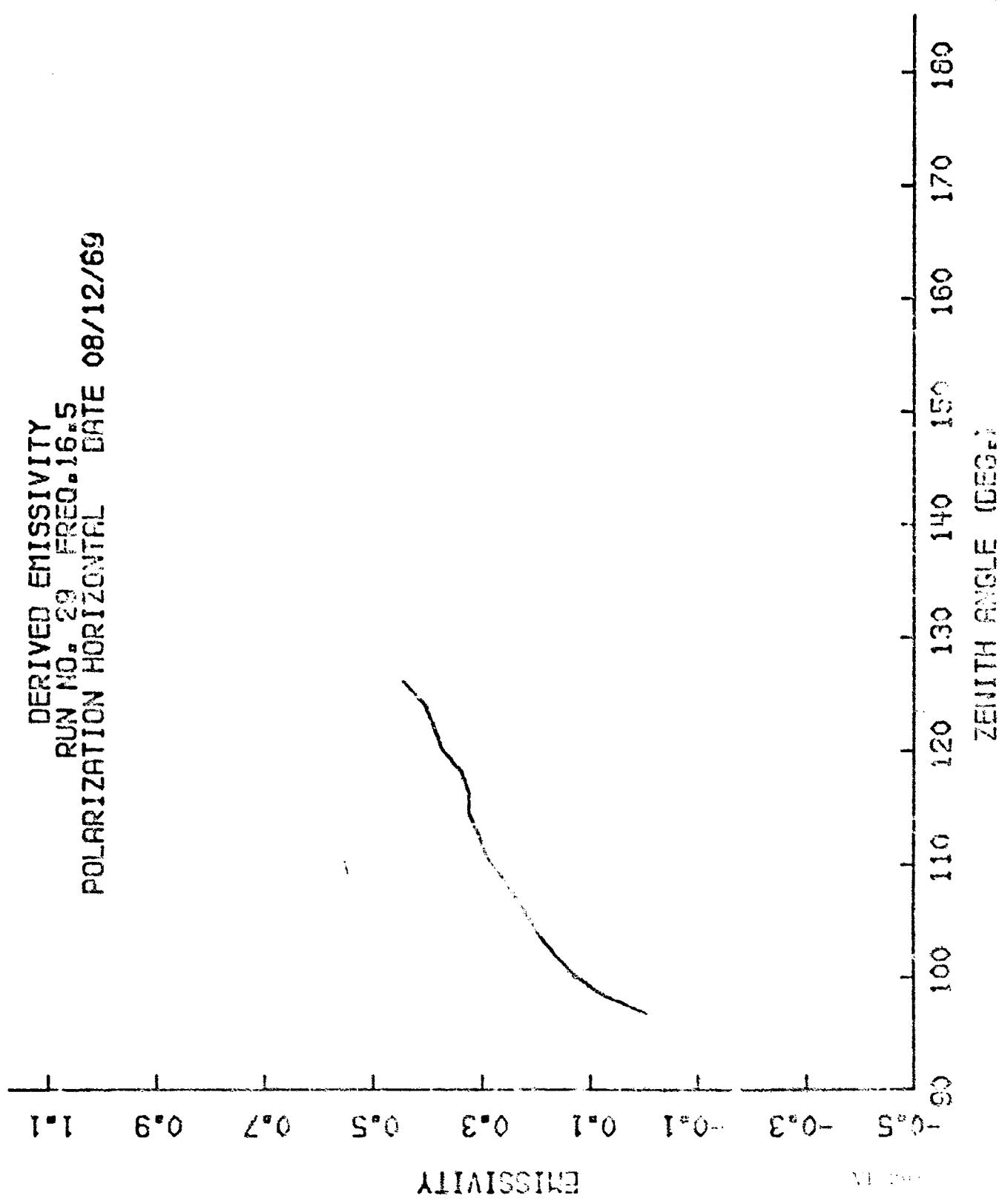


FIGURE VI-139

DERIVED
EMISSION
RUN NO. 16.5
POLARIZATION HC
DATE 08/13/69

-0.5 -0.3 -0.1 0.1 0.3 0.5 0.7 0.9 0.0

EMISSION

ZENITH ANGLE (DEG.)

100 110 120 130 140 150 160 170 180

100 110 120 130 140 150 160 170 180

FIGURE VI-140

DERIVED EMISSIVITY
RUN NO. 35 FREQ. 16.5
POLARIZATION HORIZONTAL DATE 08/14/69

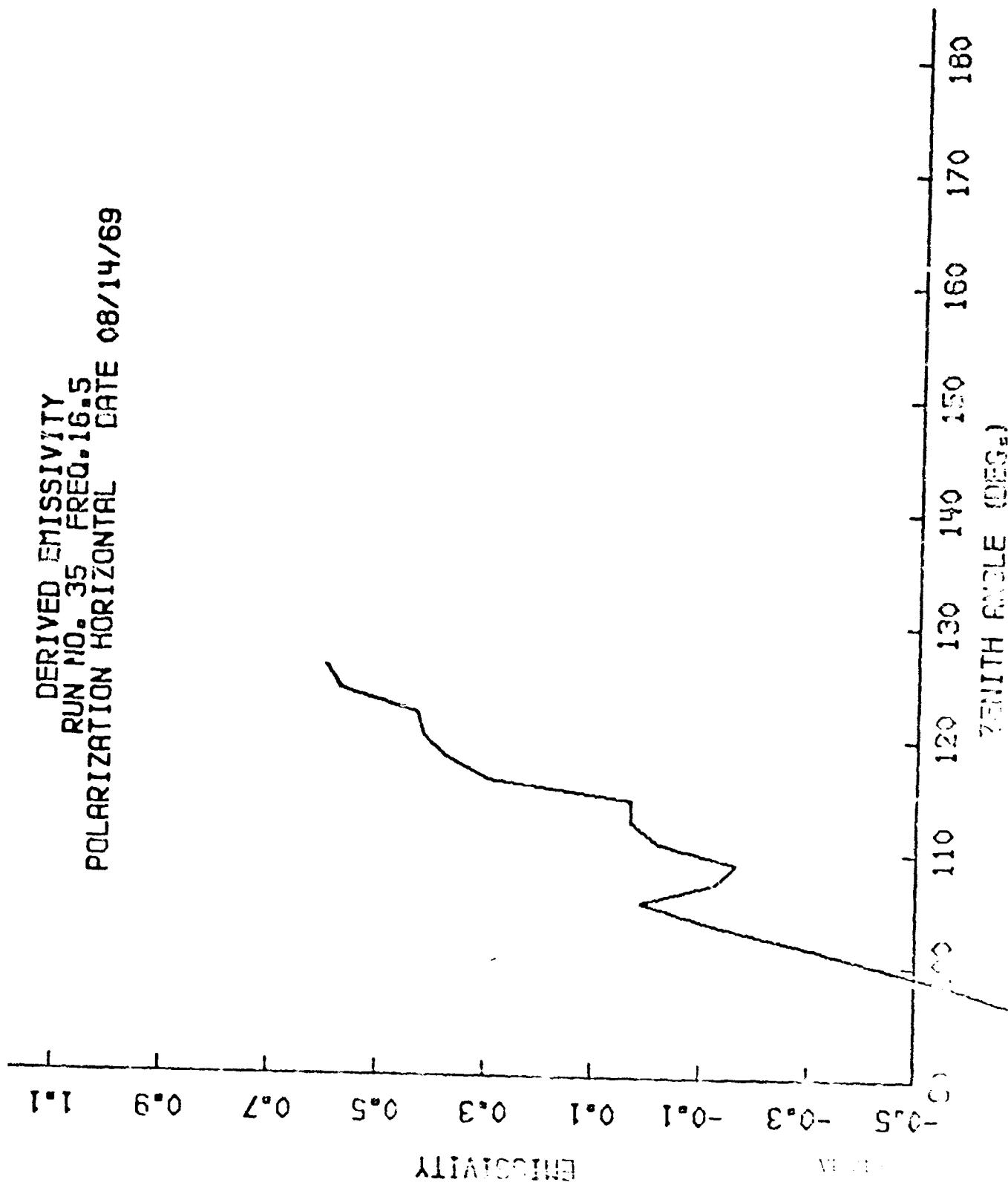


FIGURE VI-11

DERIVED EMISSIVITY
RUN NO. 4 FREQ. 16.5
POLARIMETRIC VERTICAL DATE 07/29/69

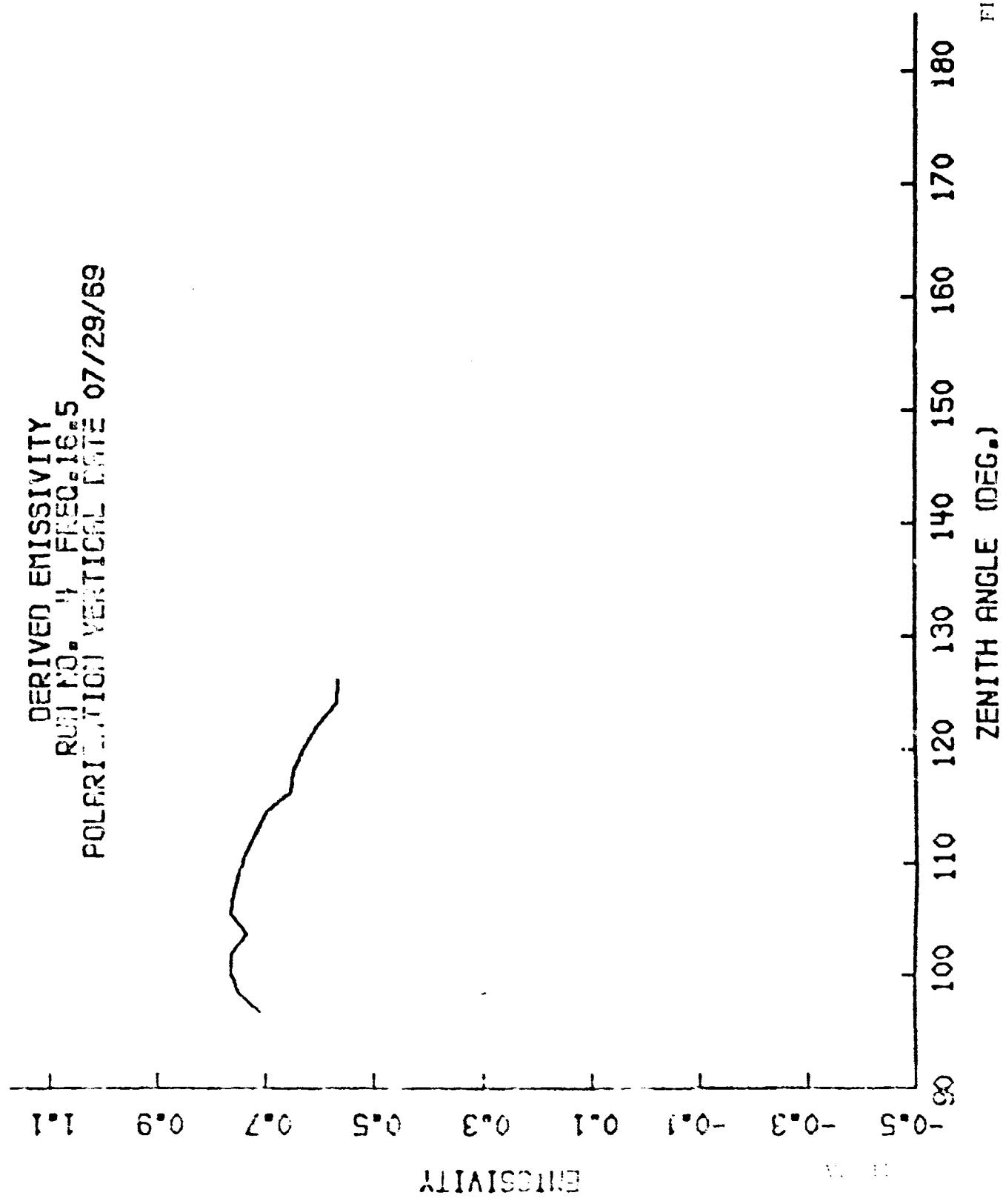


FIGURE VI-142

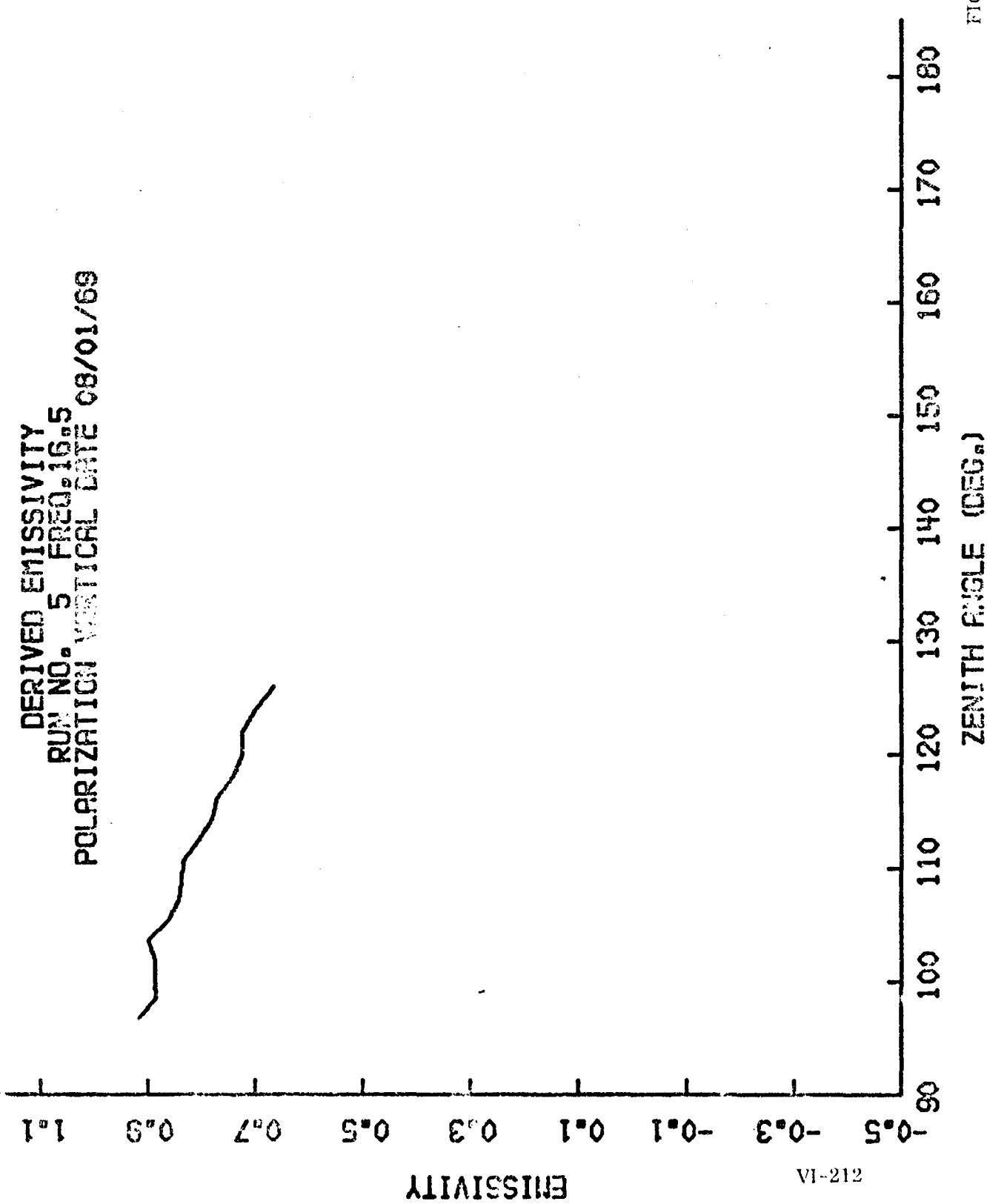


FIGURE VI-143

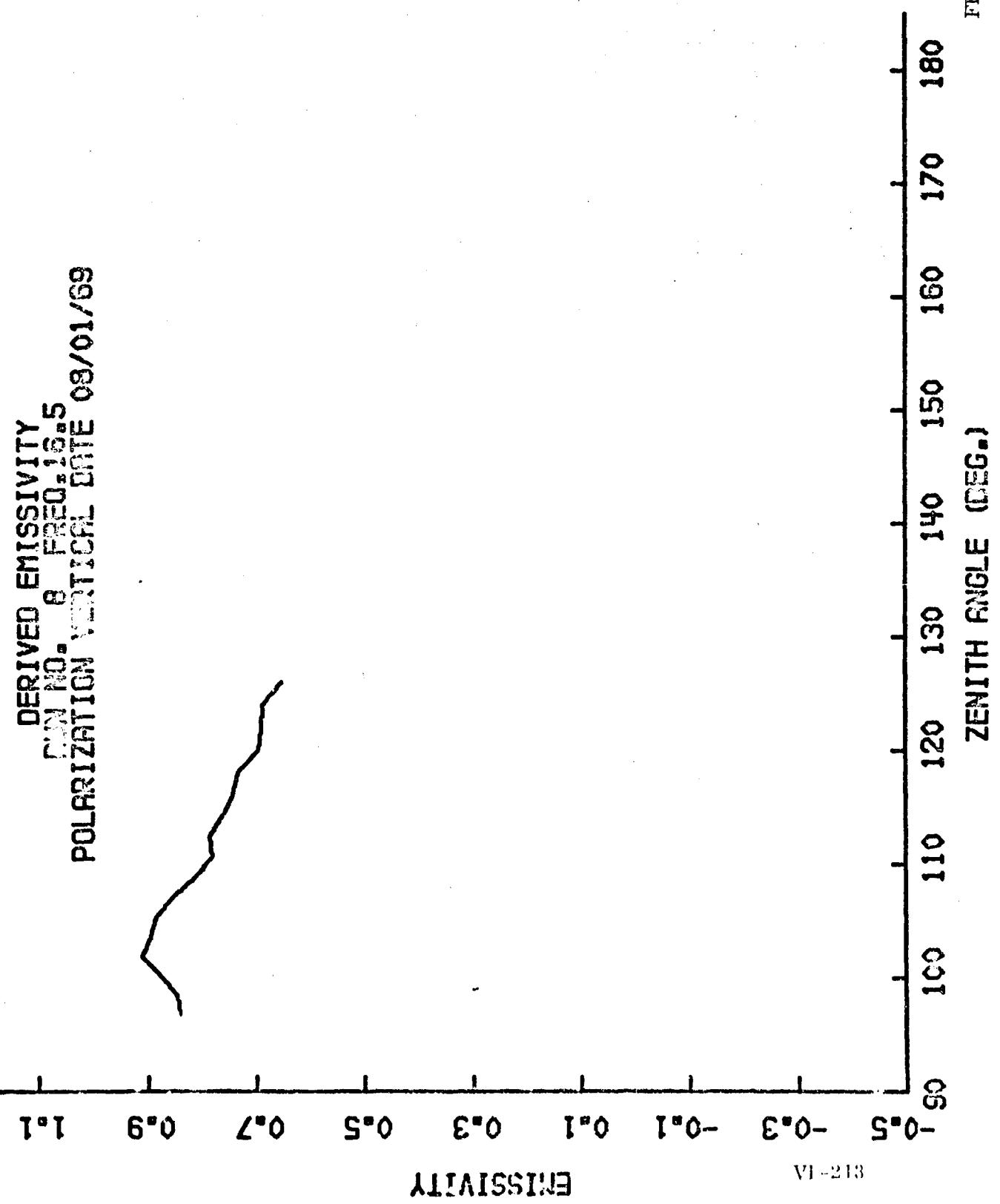
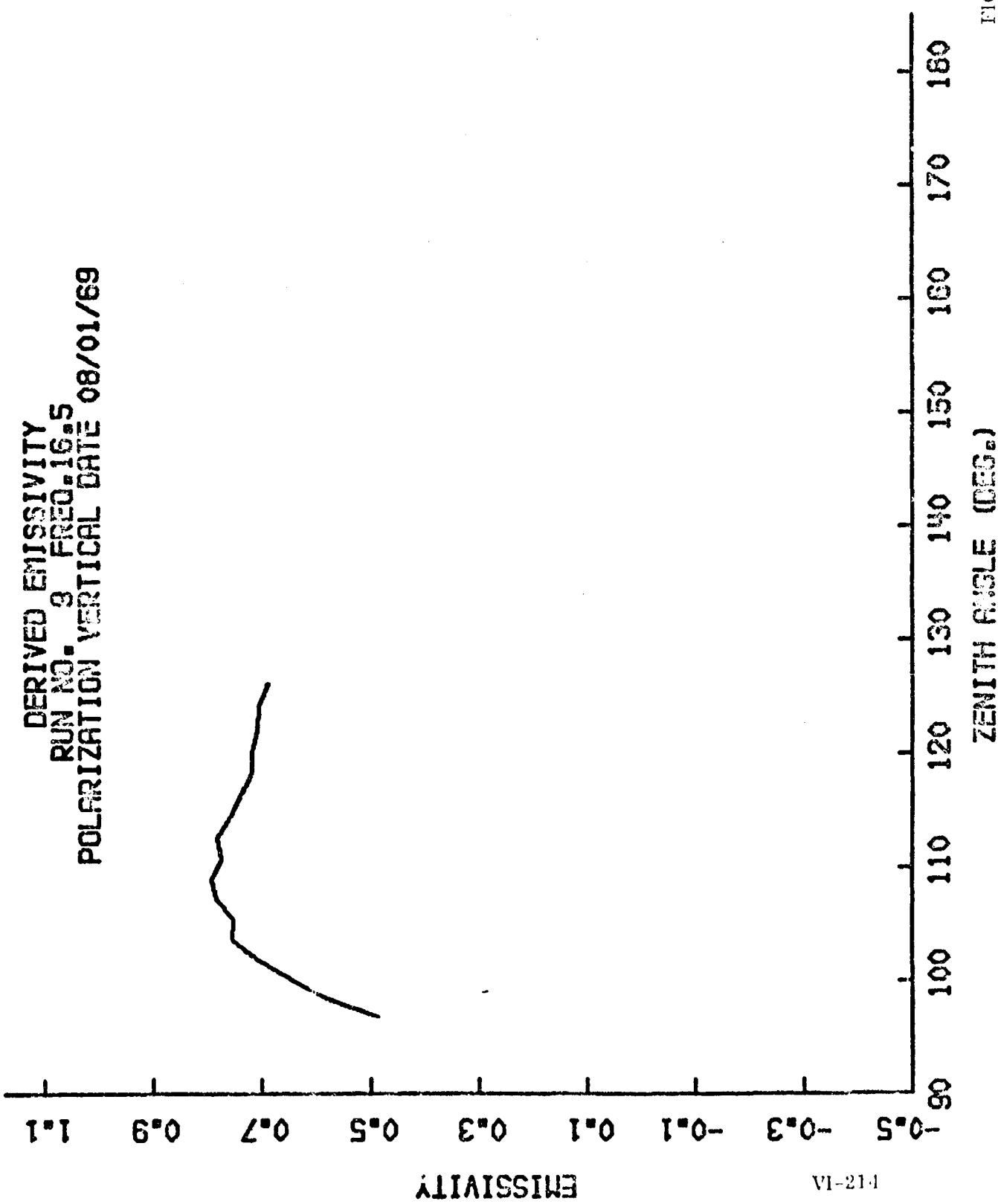
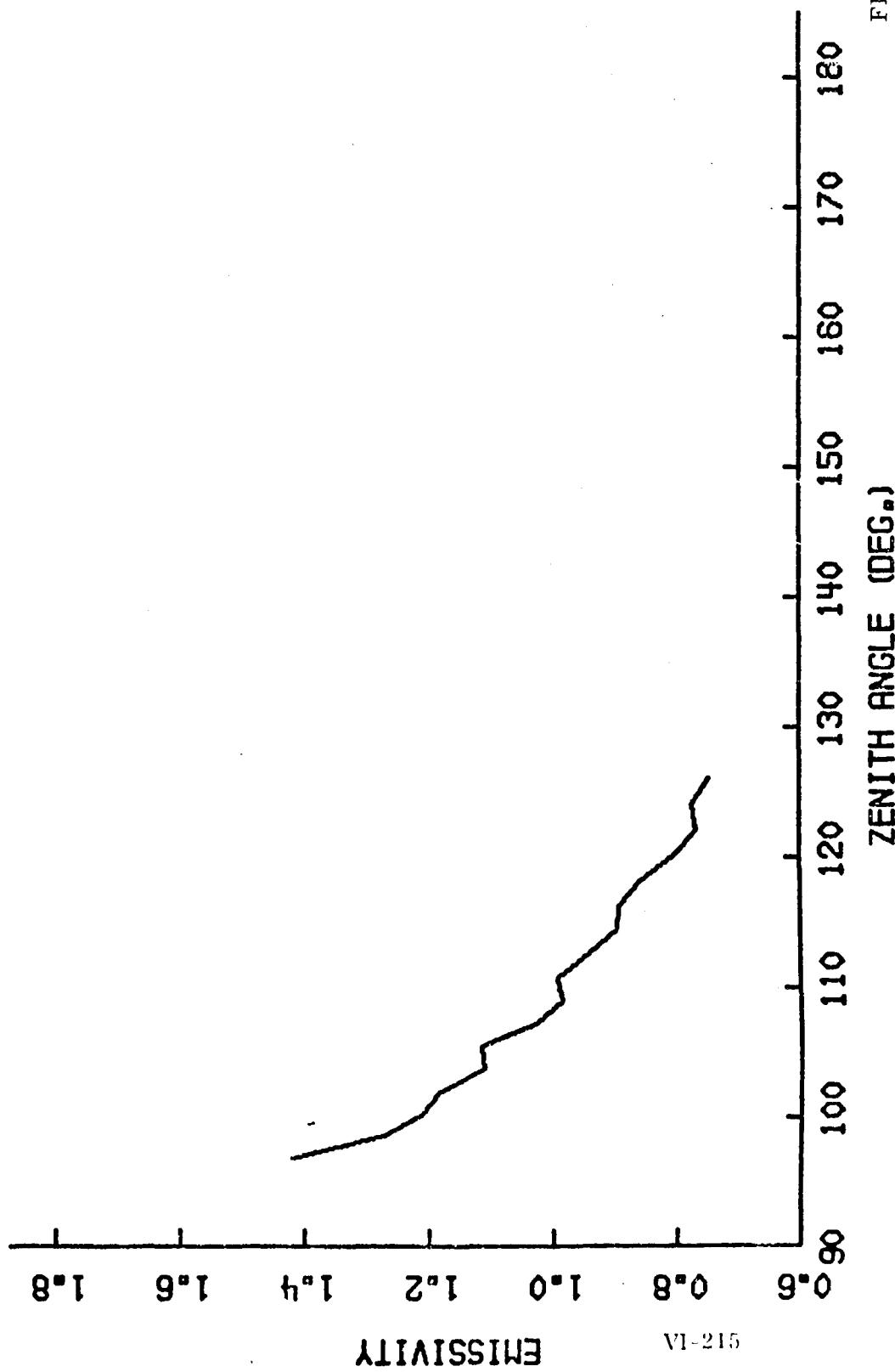


FIGURE VI-14;

FIGURE VI-145



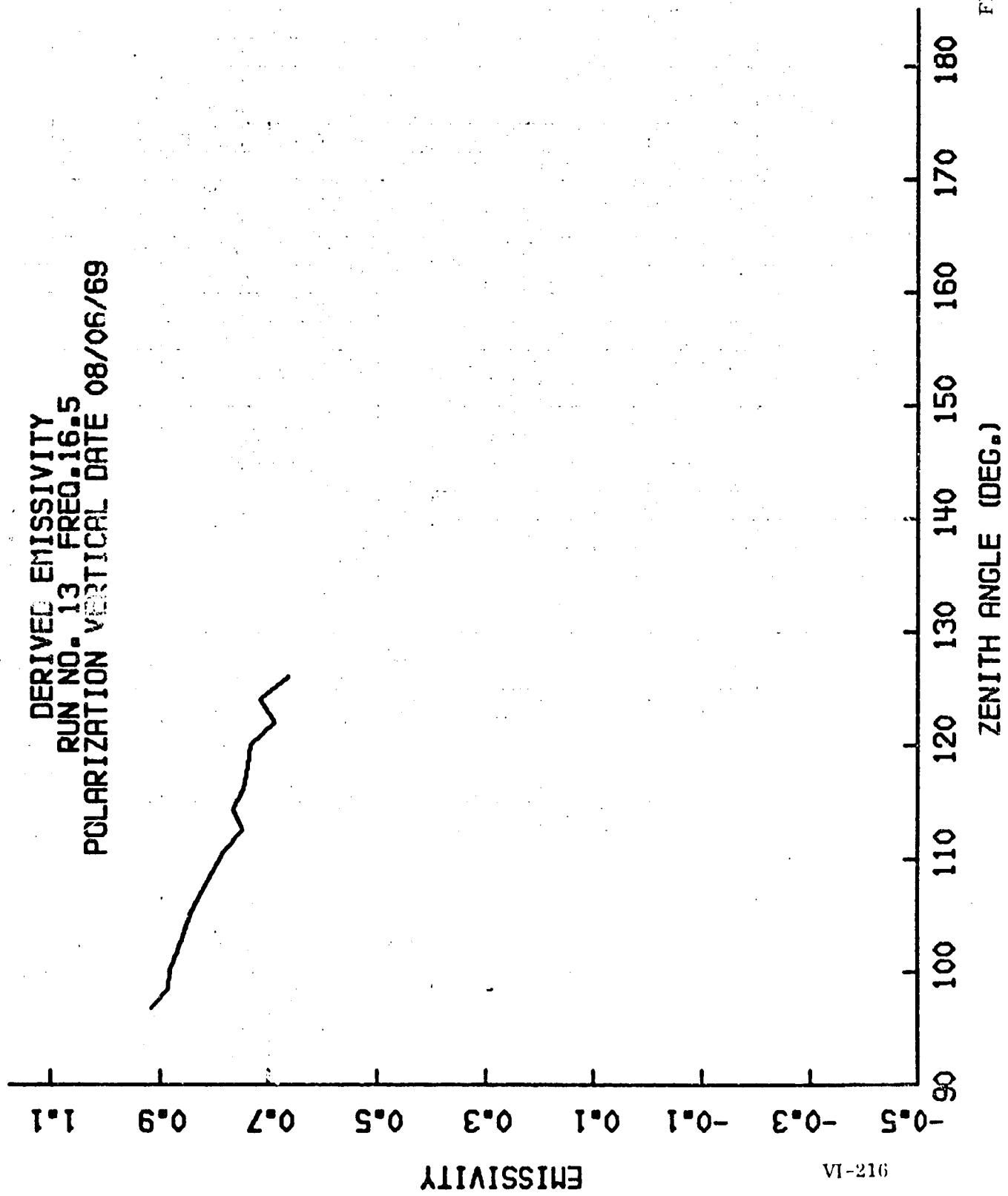
DERIVED EMISSIVITY
RUN NO. 11 FREQ. 16²5
POLARIZATION VERTICAL DATE 08/05/69



VI-215

FIGURE VI-146

DERIVED EMISSIVITY
RUN NO. 13 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/06/69



VI-216

FIGURE VI-147

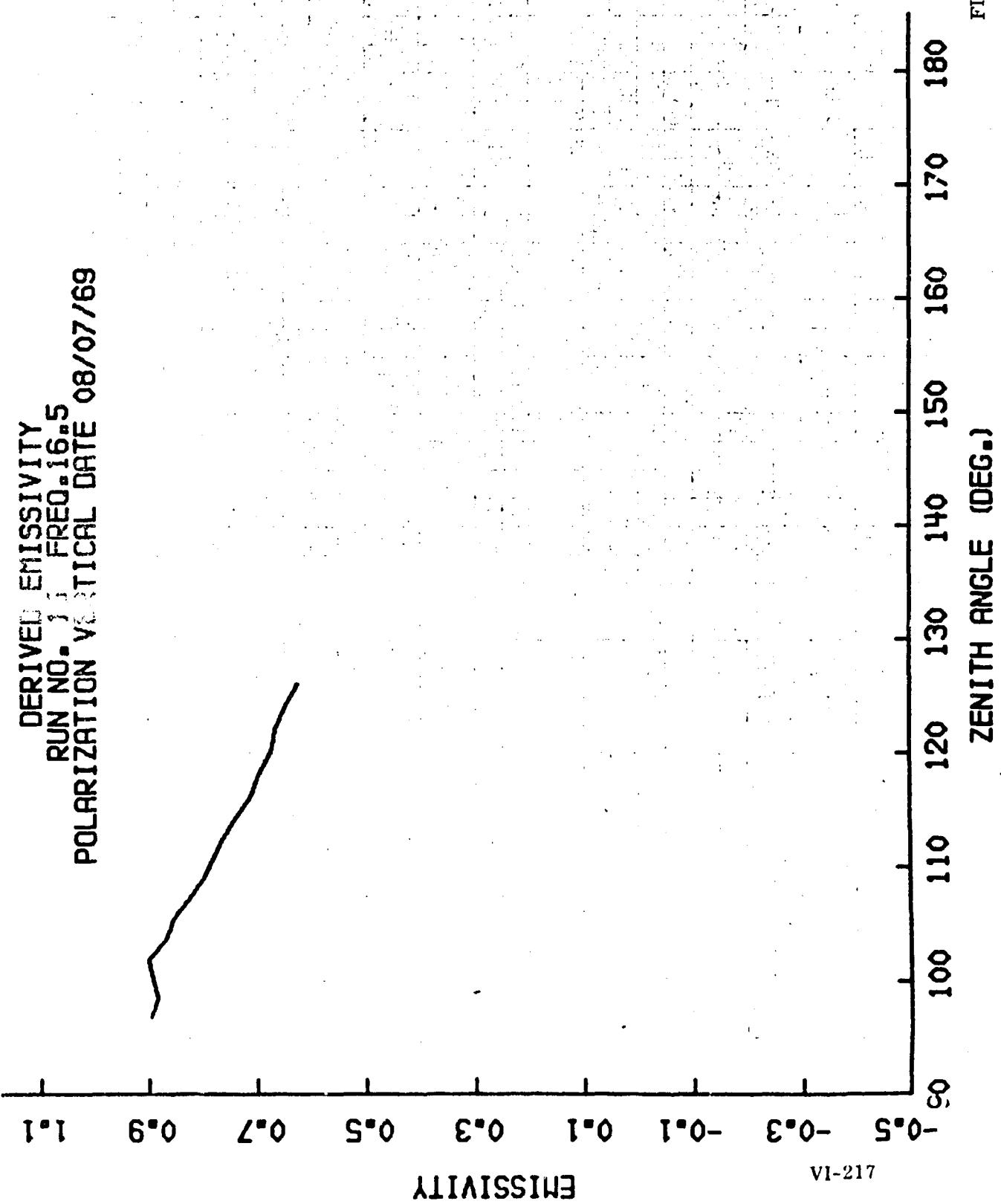
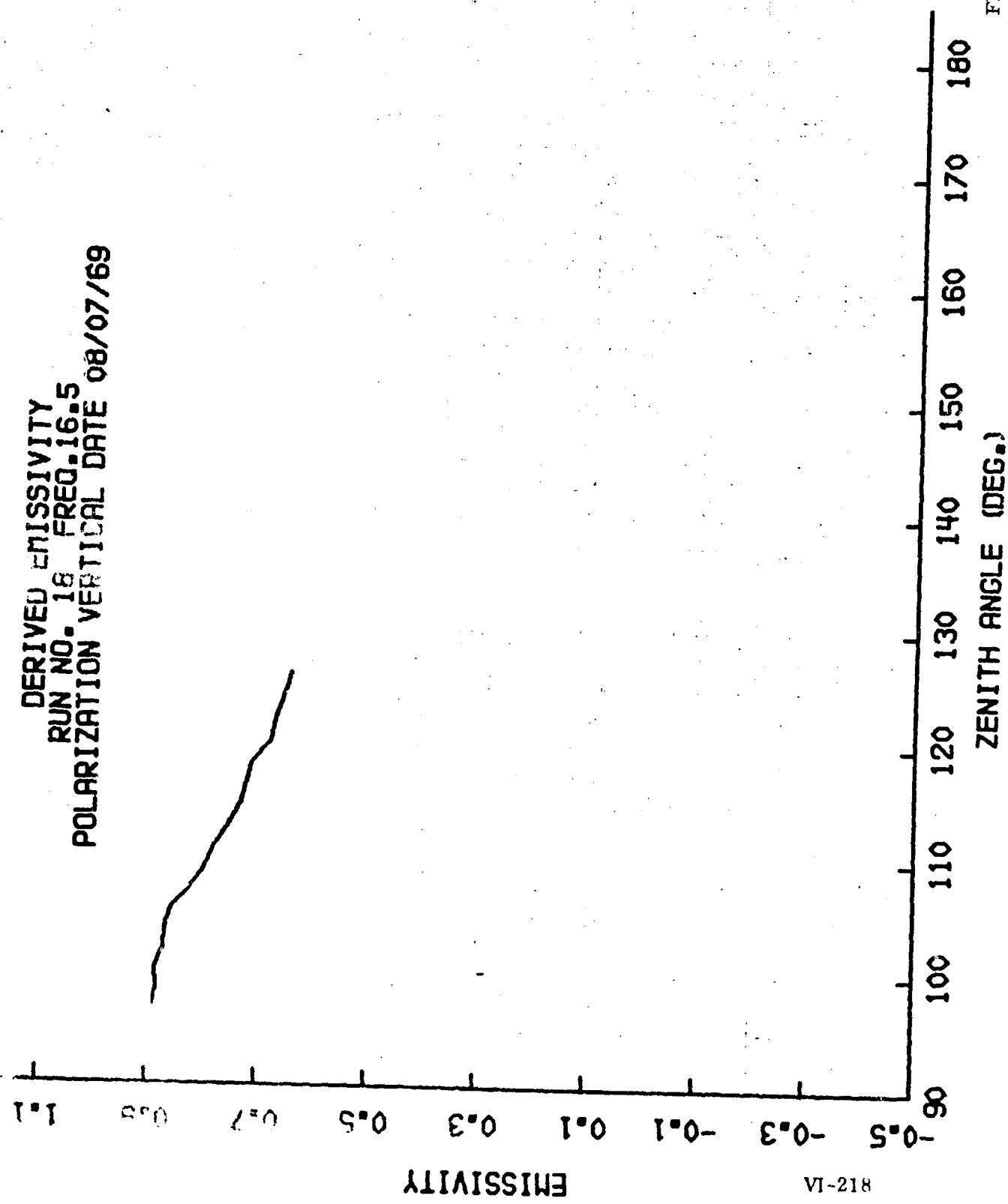


FIGURE VI-148

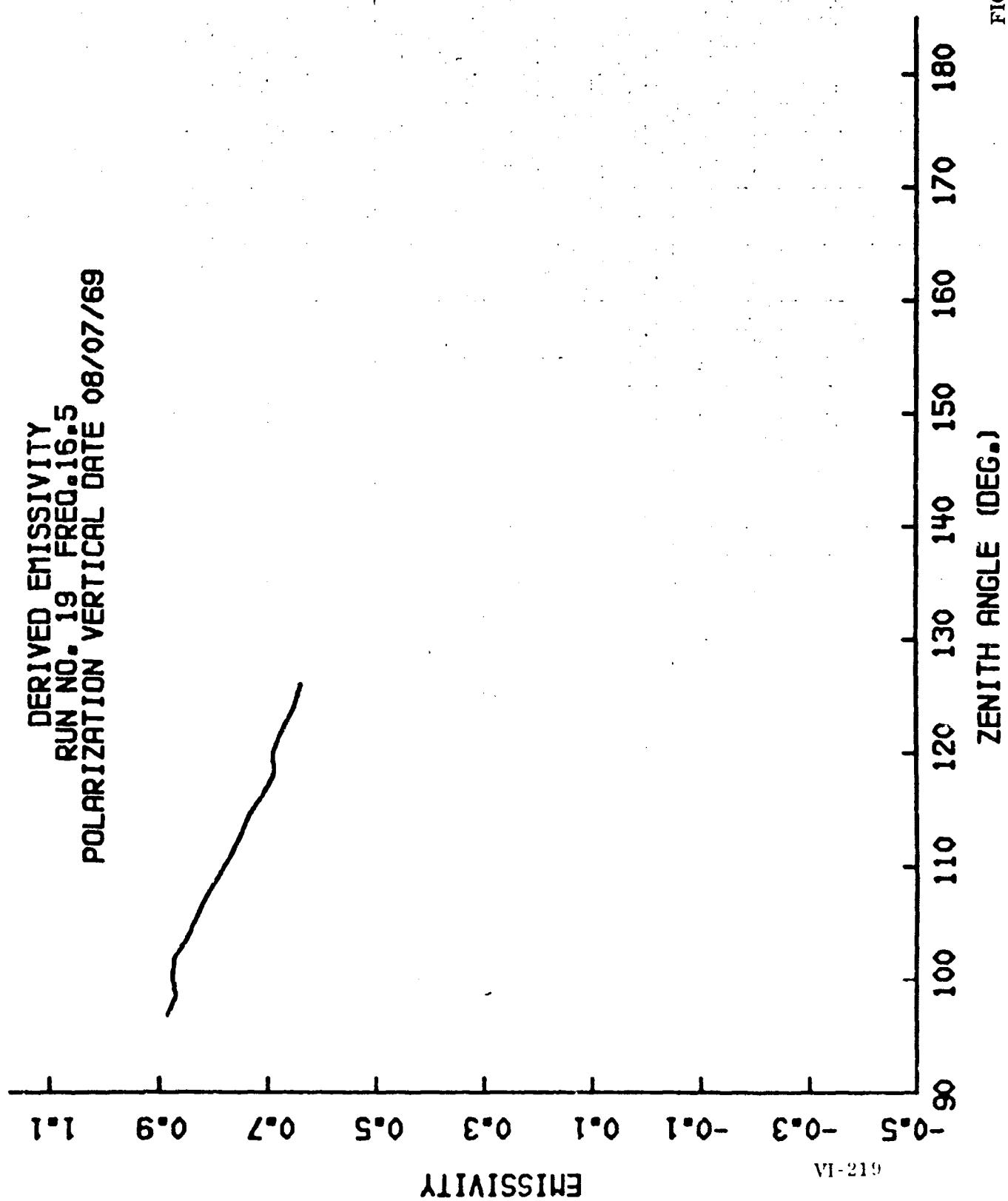
DERIVED EMISSIVITY
RUN NO. 18 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/07/69

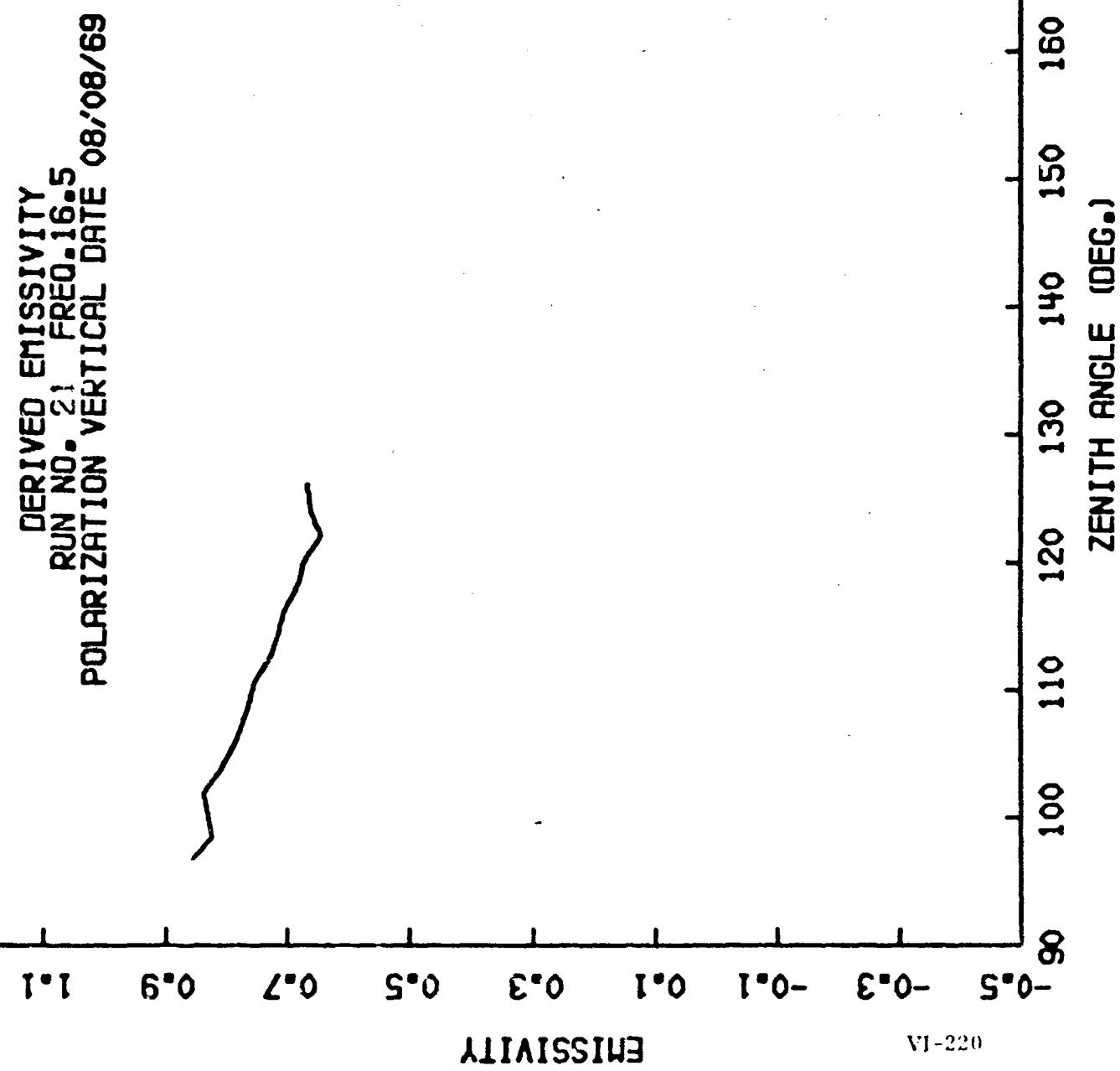


VI-218

FIGURE VI-149

FIGURE VI-150





VI-220

FIGURE VI-151

DERIVED EMISSIVITY
RUN NO. 25 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/12/69

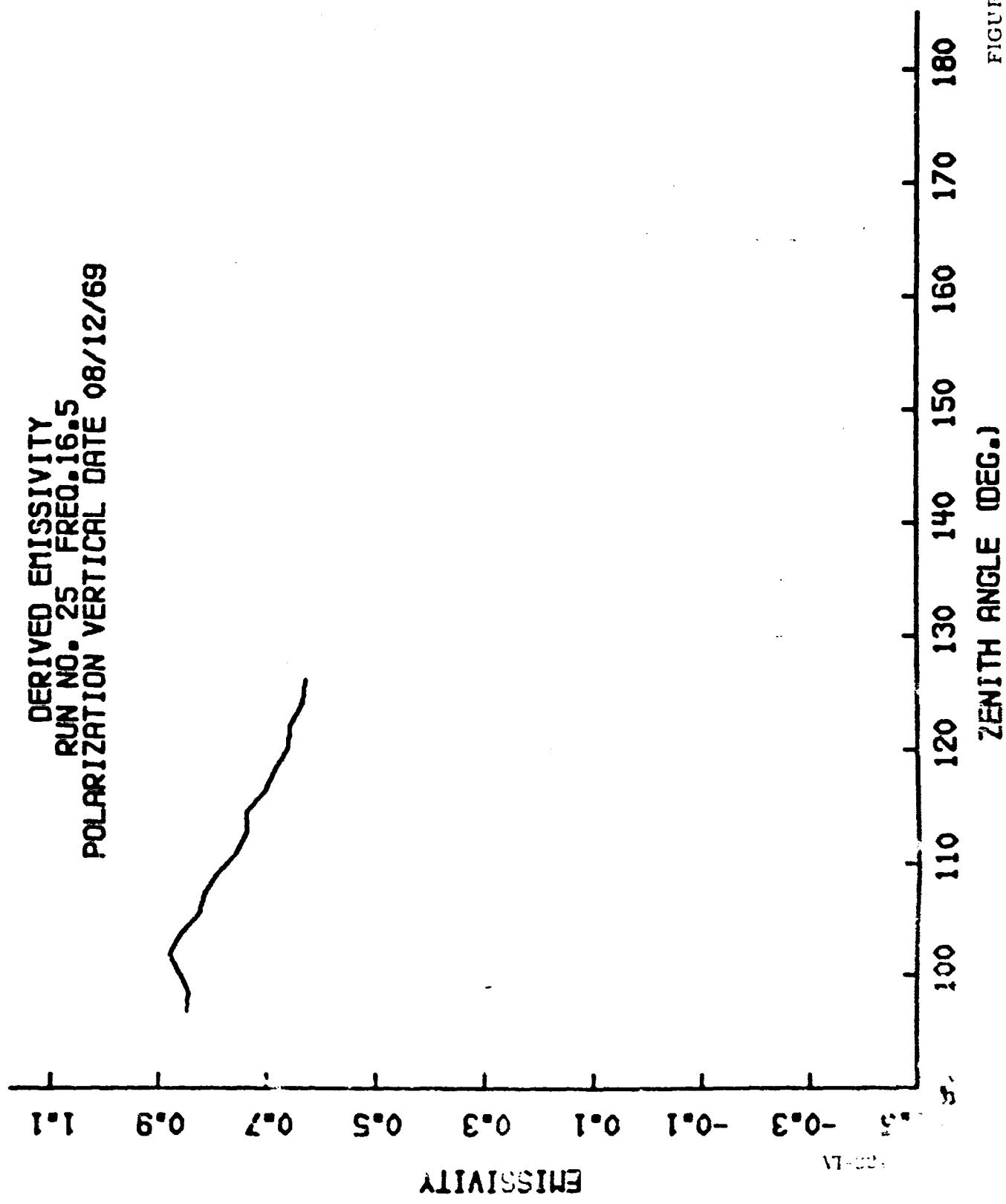
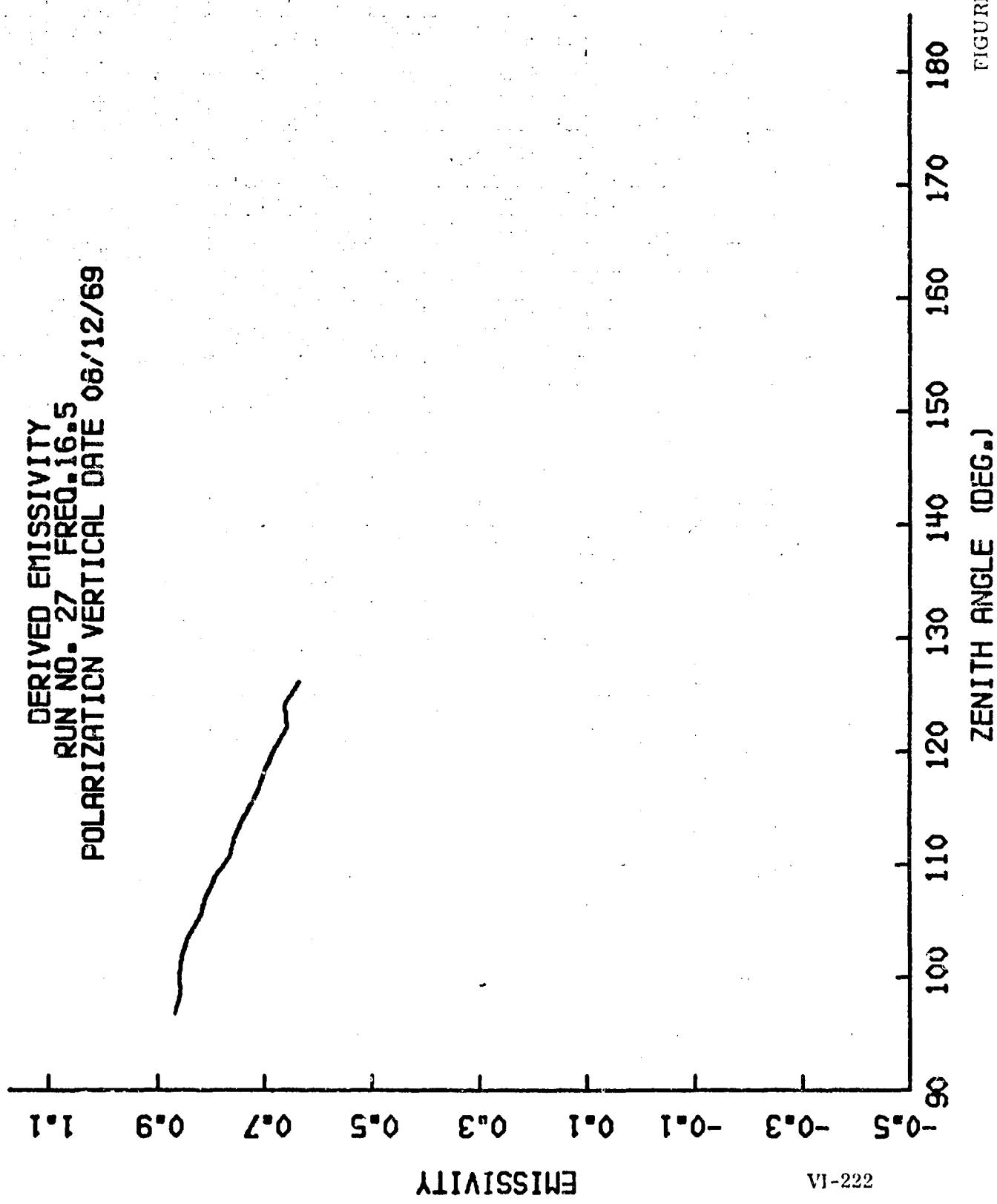


FIGURE VI-152

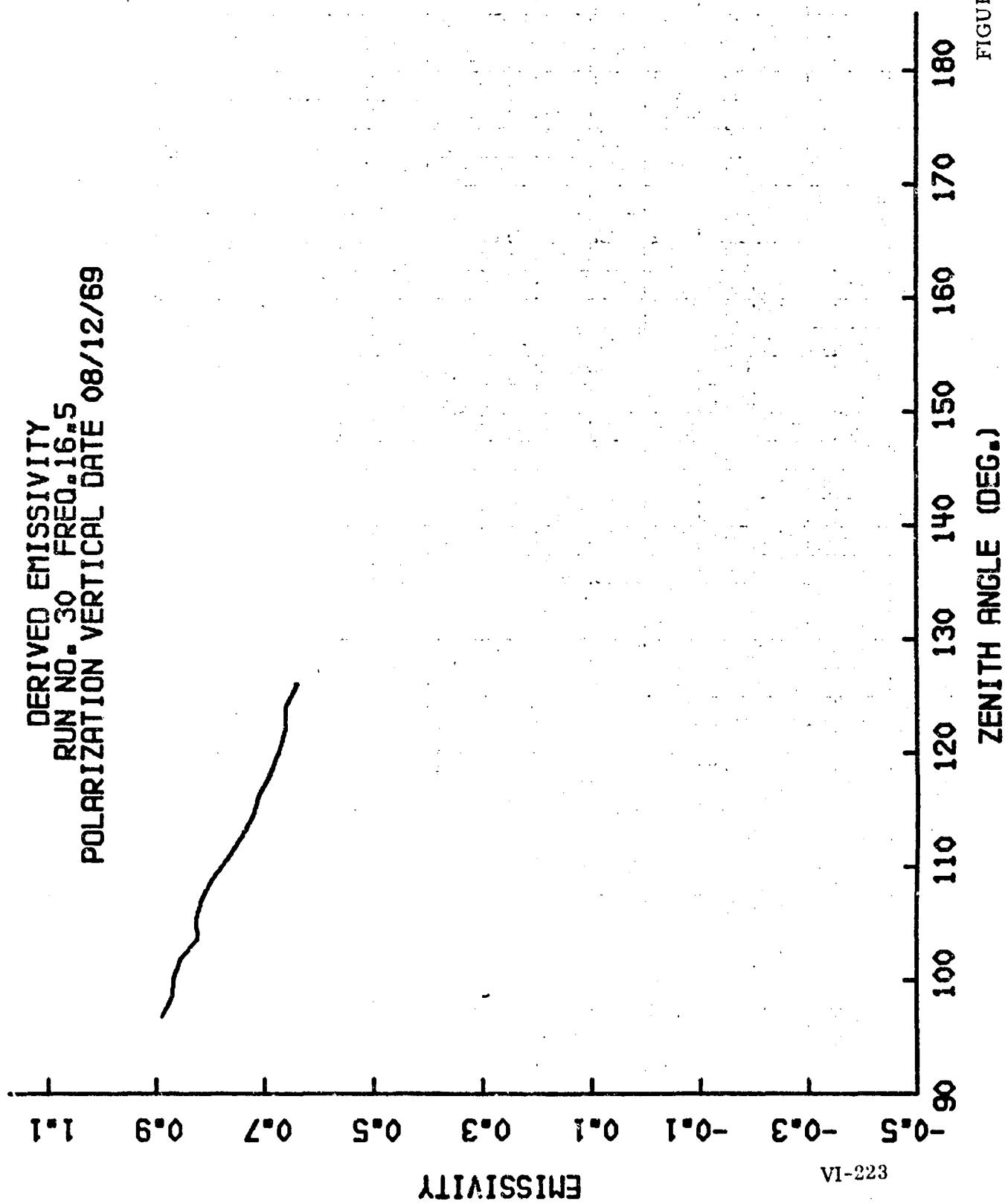
DERIVED EMISSIVITY
RUN NO. 27 FREQ. 16.5
POLARIZATION VERTICAL DATE 06/12/69



VI-222

FIGURE VI-153

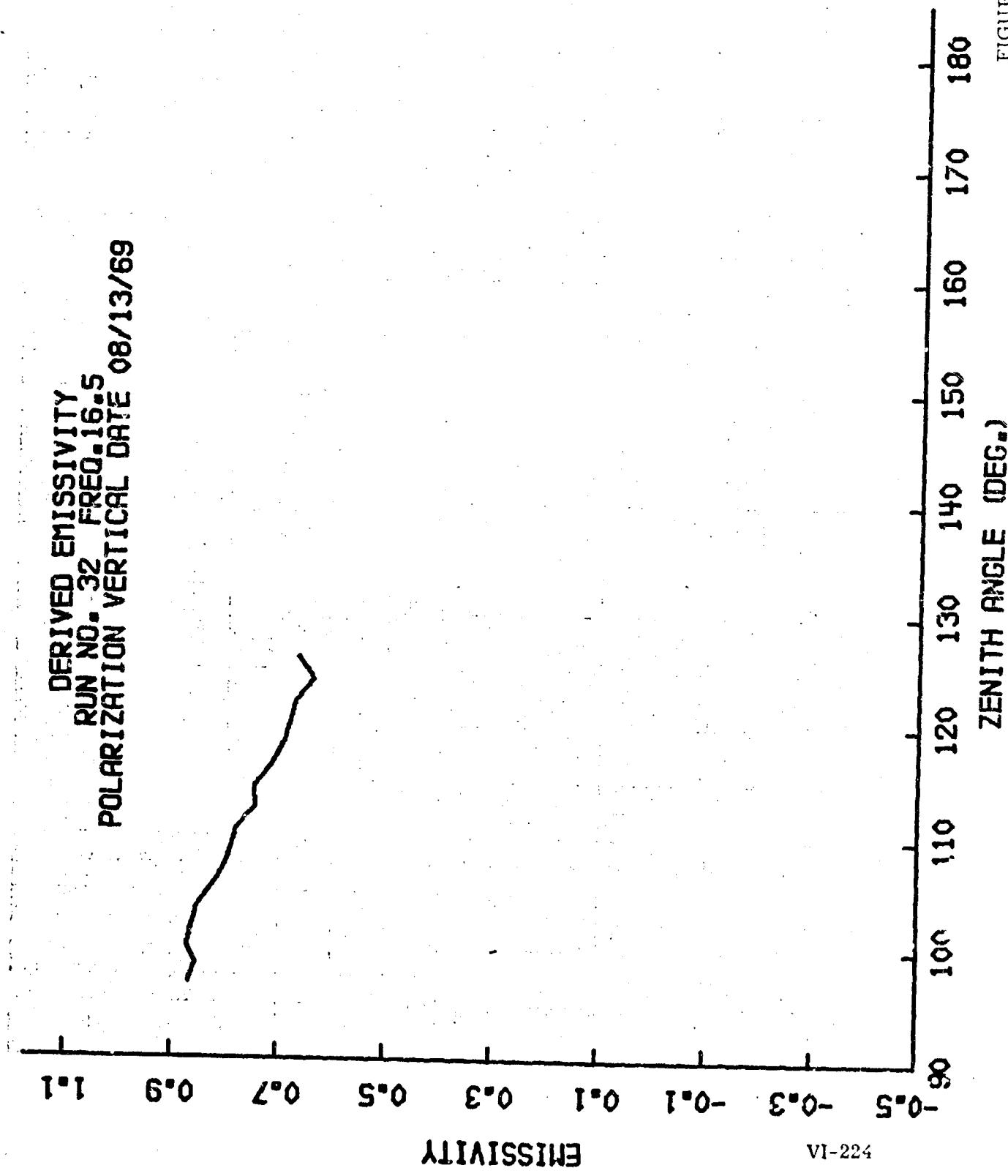
DERIVED EMISSIVITY
RUN NO. 30 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/12/69



VI-223

FIGURE VI-154

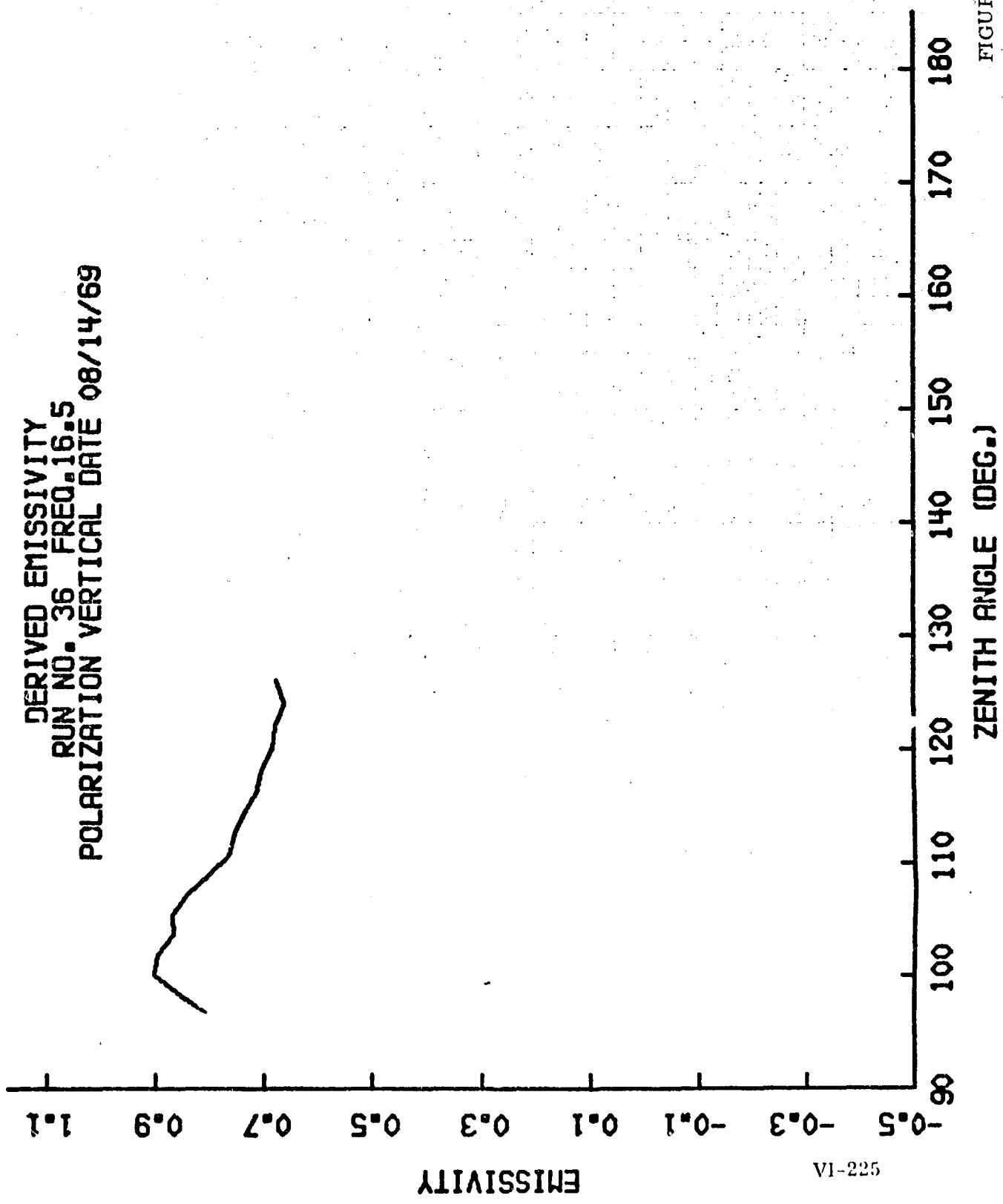
DERIVED EMISSIVITY
RUN NO. 32 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/13/69



VI-224

FIGURE VI-155

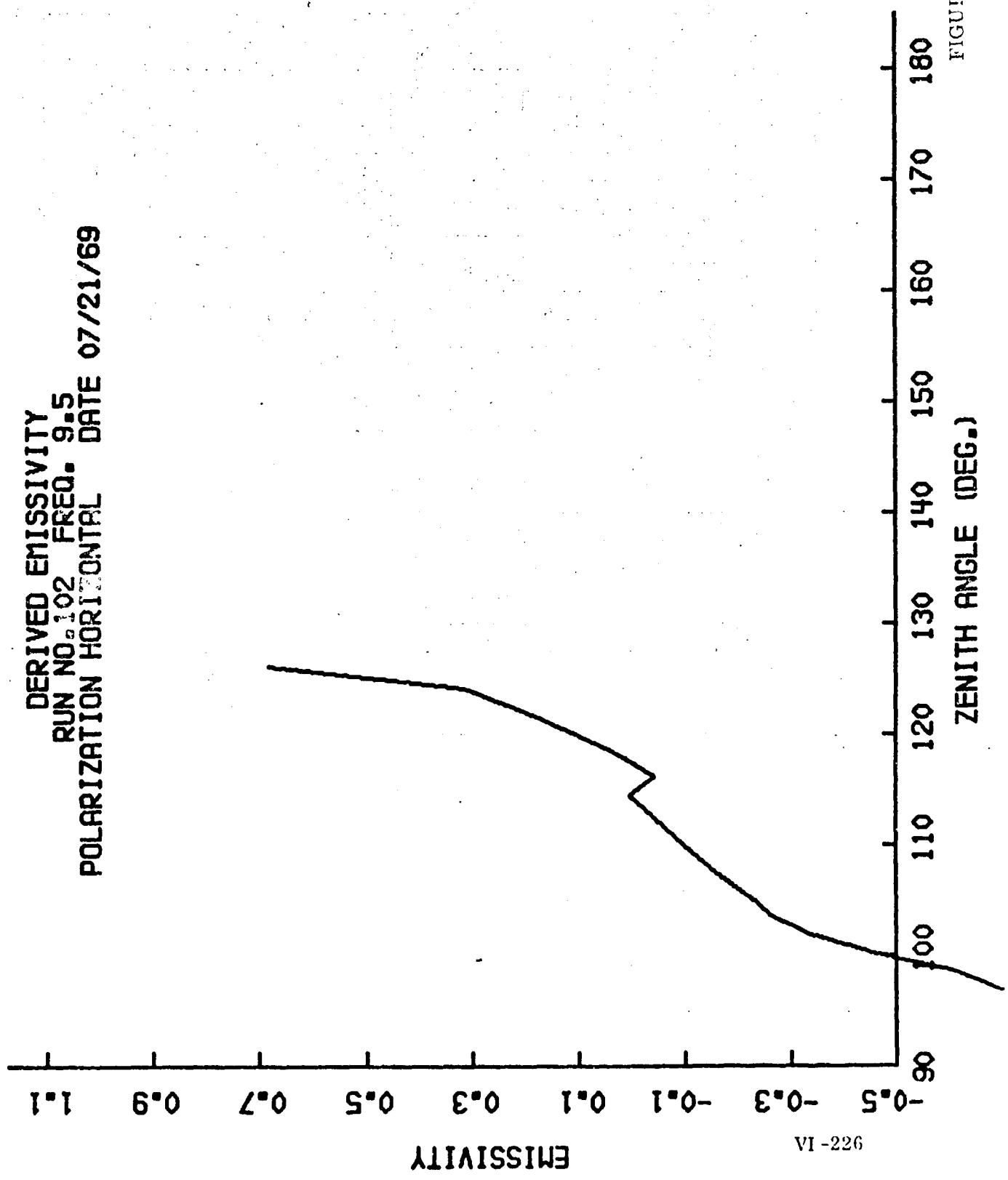
DERIVED EMISSIVITY
RUN NO. 36 FREQ. 16.5
POLARIZATION VERTICAL DATE 08/14/69



VI-225

FIGURE VI-156

DERIVED EMISSIVITY
RUN NO. 102 FREQ. 9.5
POLARIZATION HORIZONTAL DATE 07/21/69



VI-226

FIGURE VI-157

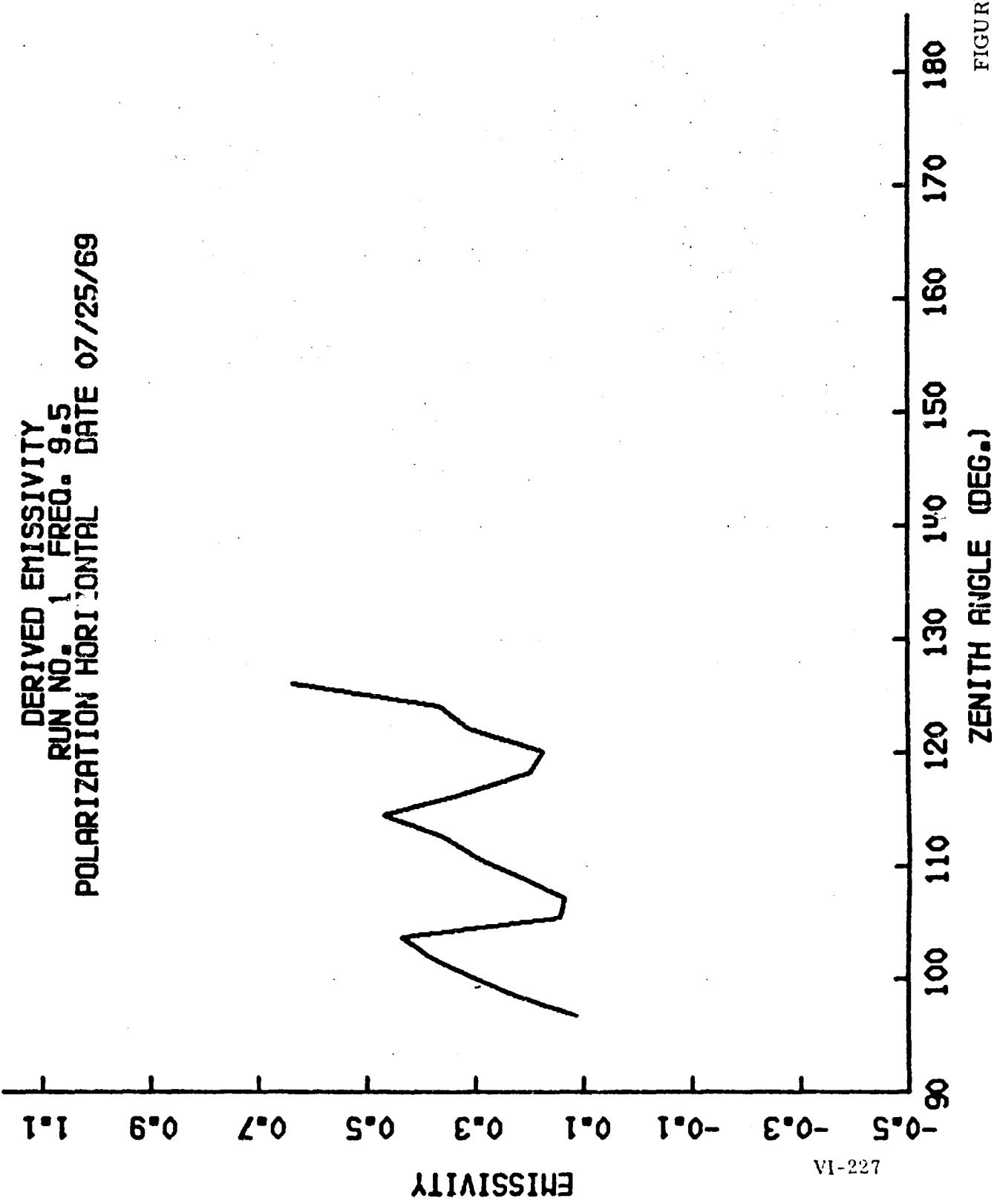
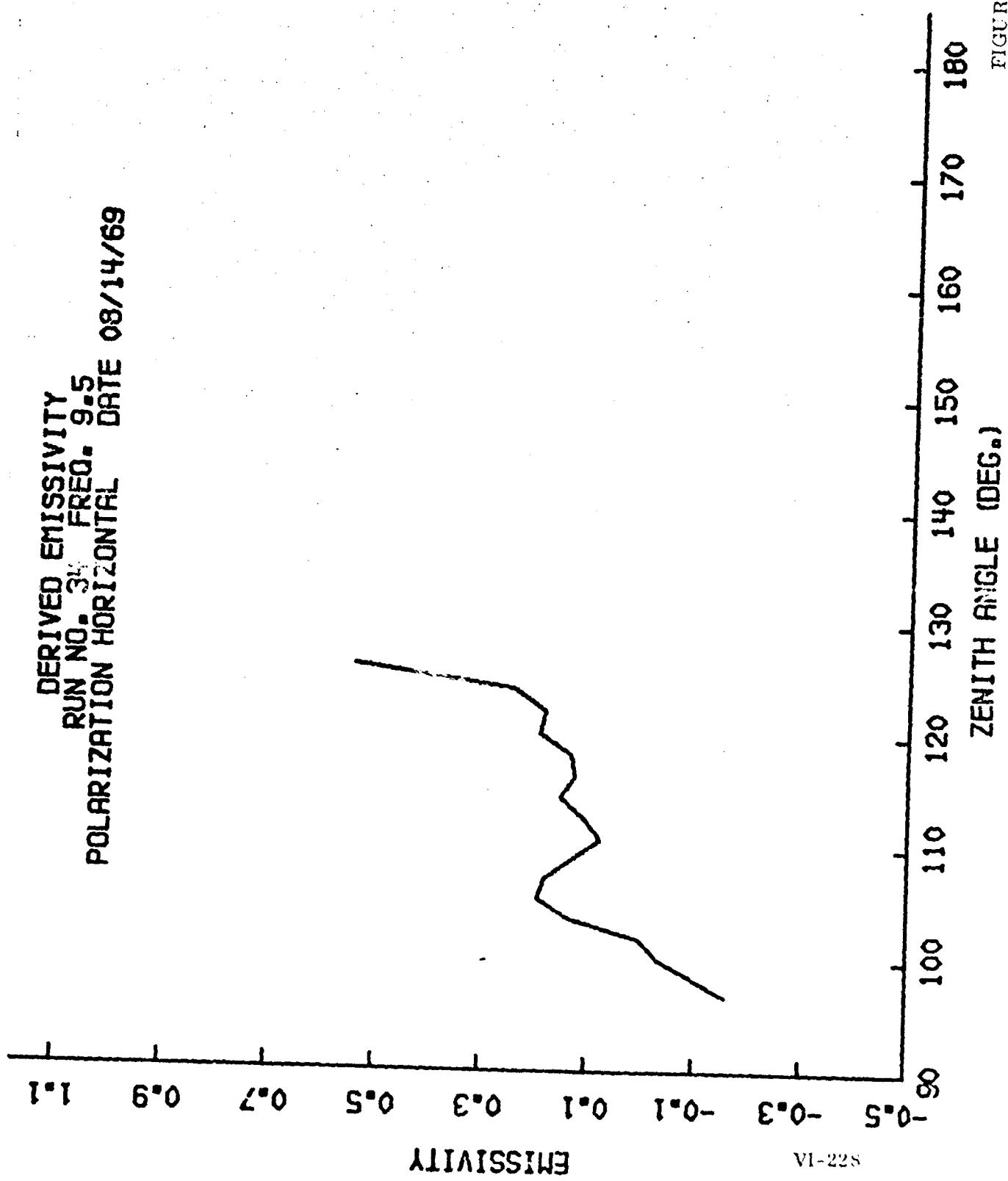


FIGURE VI-158

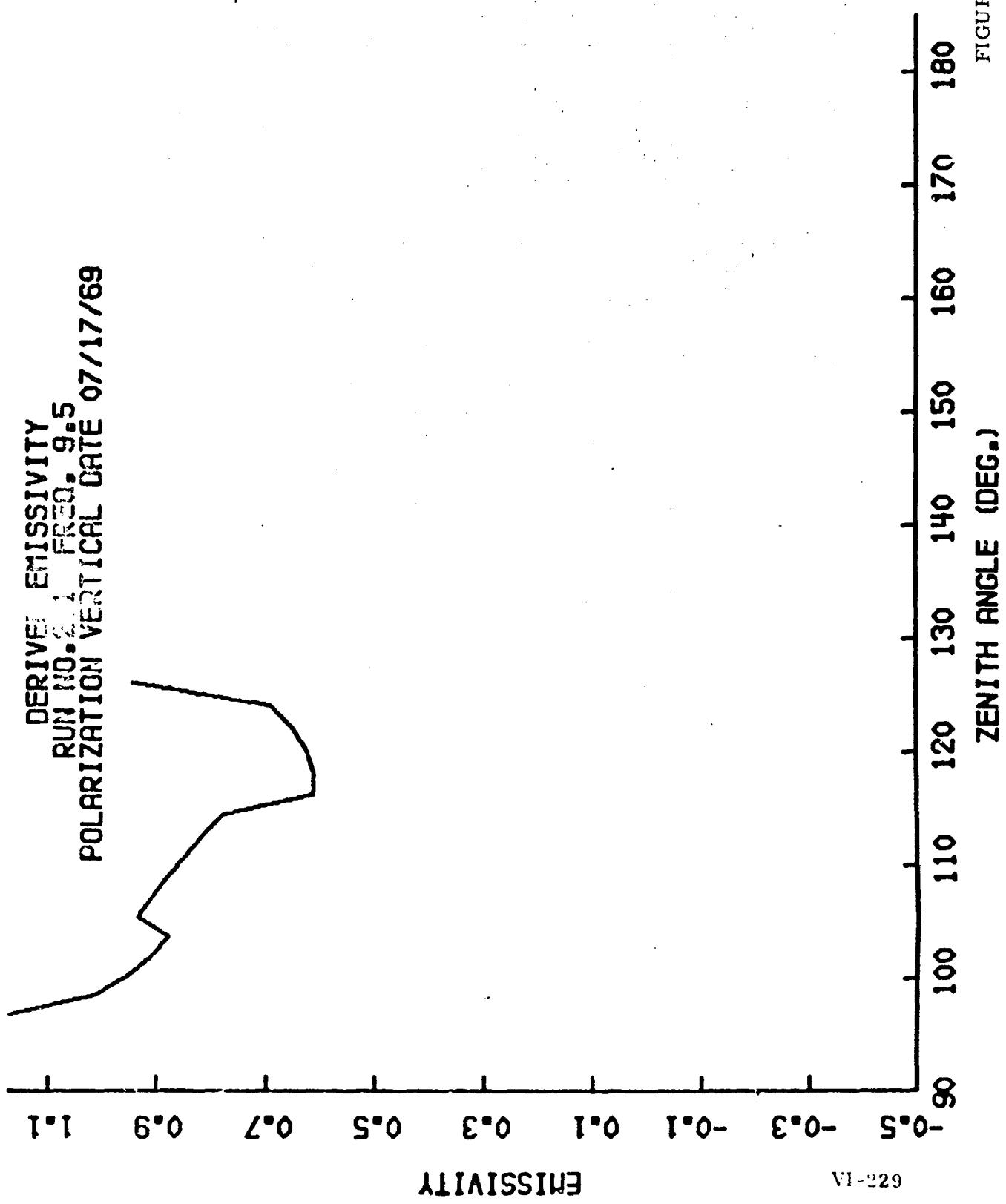
DERIVED EMISSIVITY
RUN NO. 34 FREQ. 9.5
POLARIZATION HORIZONTAL DATE 08/14/69



VI-228

FIGURE VI-159

DERIVED EMISSIVITY
RUN NO. 21 FREQ. 9.5
POLARIZATION VERTICAL DATE 07/17/69



VI-229

FIGURE VI-160

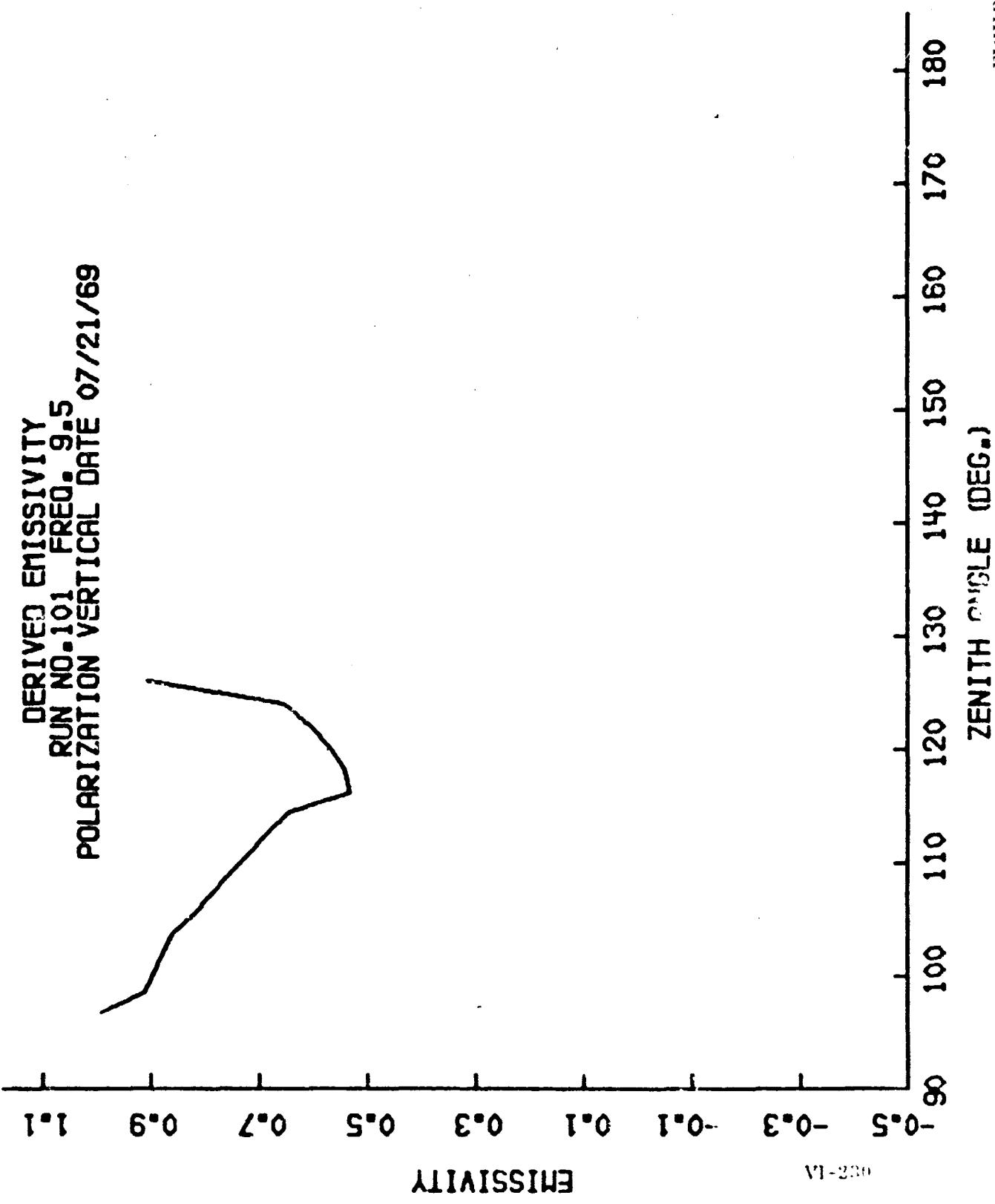


FIGURE VI-161

DERIVED EMISSIVITY
RUN NO. 2 FREQ. 9.5
POLARIZATION VERTICAL DATE 07/25/69

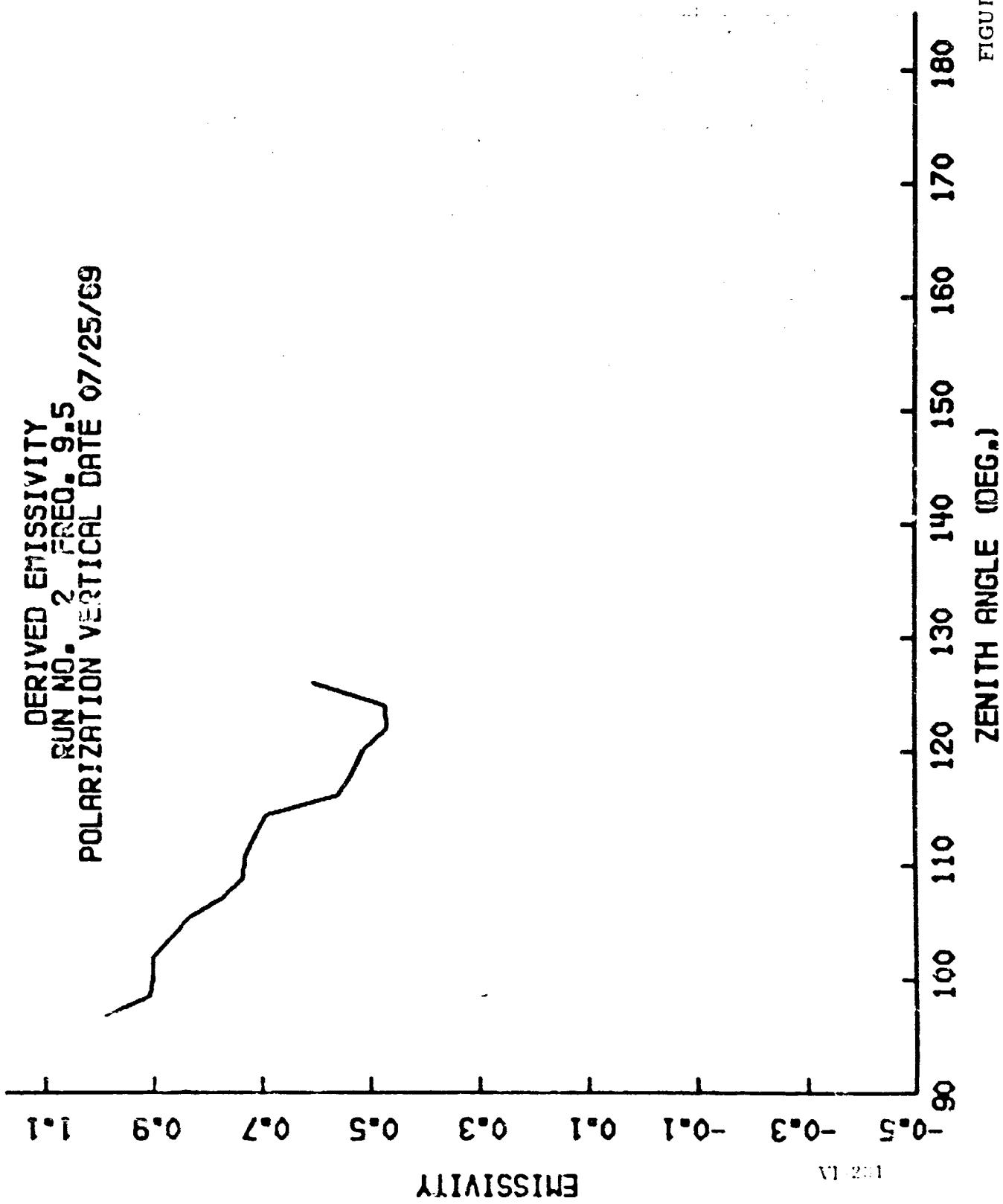


FIGURE VI-162

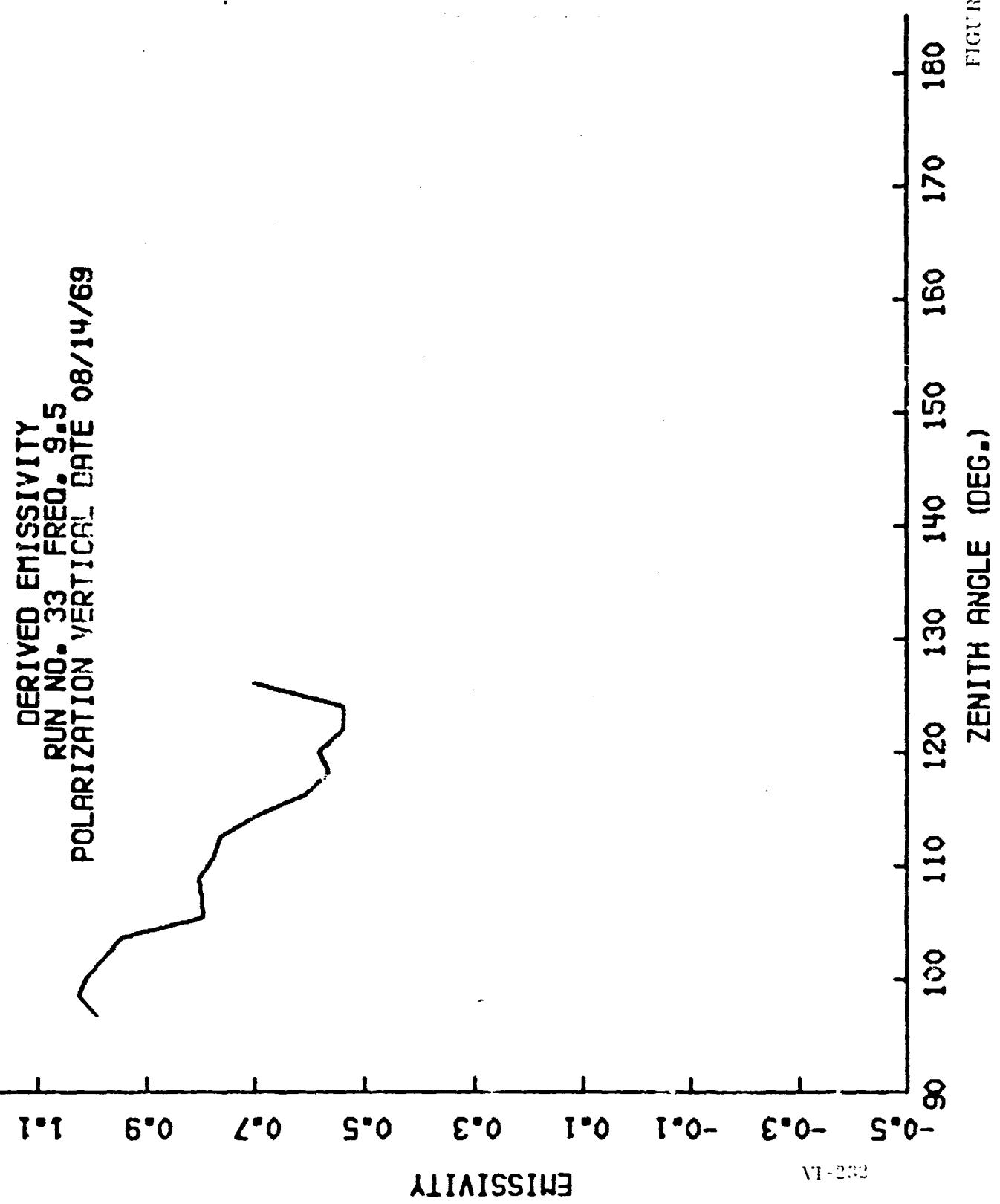


FIGURE VI-163

DERIVED EMISSIVITY

RUN NO. 4 FREQ 16.5GHZ
 DATE 07/29/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 275.75 | 0.70955 |
| 98.46 | 275.90 | 0.75554 |
| 100.16 | 274.05 | 0.76224 |
| 101.88 | 270.99 | 0.76275 |
| 103.61 | 264.11 | 0.73326 |
| 105.35 | 264.95 | 0.76199 |
| 107.10 | 261.50 | 0.75772 |
| 108.88 | 257.02 | 0.74568 |
| 110.67 | 252.58 | 0.73432 |
| 112.48 | 247.21 | 0.71575 |
| 114.32 | 241.84 | 0.69719 |
| 116.18 | 231.25 | 0.65162 |
| 118.07 | 228.55 | 0.64563 |
| 120.00 | 223.09 | 0.52720 |
| 121.97 | 216.69 | 0.60134 |
| 123.97 | 208.59 | 0.56736 |
| 126.03 | 207.17 | 0.56576 |

TABLE VI-62

DERIVED EMISSIVITY

RUN NO. 5 FREQ 16.5GHZ
 DATE 08/01/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 284.15 | 0.91796 |
| 98.46 | 276.65 | 0.88617 |
| 100.16 | 275.80 | 0.88324 |
| 101.88 | 275.00 | 0.88813 |
| 103.61 | 276.97 | 0.90083 |
| 105.35 | 267.36 | 0.86151 |
| 107.10 | 262.27 | 0.84281 |
| 108.88 | 260.35 | 0.83764 |
| 110.67 | 258.66 | 0.83404 |
| 112.48 | 250.87 | 0.80525 |
| 114.32 | 244.04 | 0.78070 |
| 116.18 | 241.26 | 0.77230 |
| 118.07 | 232.55 | 0.74049 |
| 120.00 | 228.12 | 0.72537 |
| 121.97 | 227.53 | 0.72467 |
| 123.97 | 220.47 | 0.69881 |
| 126.03 | 211.60 | 0.66592 |

TABLE VI-63

DERIVED EMISSIVITY

RUN NO. 6 FREQ 16.5GHZ
 DATE 08/01/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 120.79 | 0.10575 |
| 98.46 | 124.88 | 0.02544 |
| 100.16 | 122.10 | 0.09705 |
| 101.88 | 120.59 | 0.14445 |
| 103.61 | 120.07 | 0.17512 |
| 105.35 | 119.53 | 0.19606 |
| 107.10 | 122.74 | 0.22524 |
| 108.88 | 126.04 | 0.25080 |
| 110.67 | 127.90 | 0.27510 |
| 112.48 | 127.91 | 0.28564 |
| 114.32 | 131.39 | 0.30867 |
| 116.18 | 135.74 | 0.33174 |
| 118.07 | 132.99 | 0.32919 |
| 120.00 | 135.88 | 0.34594 |
| 121.97 | 140.54 | 0.37467 |
| 123.97 | 140.65 | 0.38394 |
| 126.03 | 147.99 | 0.42063 |

TABLE VI-64

DERIVED EMISSIVITY

RUN NO. 7 FREQ 16.5GHZ
DATE 08/01/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 121.45 | 0.25510 |
| 98.46 | 124.93 | 0.03349 |
| 100.16 | 121.20 | 0.09421 |
| 101.88 | 118.79 | 0.16529 |
| 103.61 | 115.13 | 0.18728 |
| 105.35 | 117.25 | 0.21986 |
| 107.10 | 125.45 | 0.26568 |
| 108.88 | 126.38 | 0.27421 |
| 110.67 | 122.02 | 0.27390 |
| 112.48 | 131.88 | 0.32477 |
| 114.32 | 139.07 | 0.36166 |
| 116.18 | 124.04 | 0.30880 |
| 118.07 | 137.28 | 0.36579 |
| 120.00 | 142.79 | 0.39324 |
| 121.97 | 142.56 | 0.40008 |
| 123.97 | 144.45 | 0.41451 |
| 126.03 | 145.85 | 0.42550 |

Table VI-65

DERIVED EMISSIVITY

RUN NO. 8 FREQ 16.5GHZ
 DATE 08/01/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 275.20 | 0.83918 |
| 98.46 | 271.67 | 0.84379 |
| 100.16 | 274.01 | 0.87444 |
| 101.88 | 279.86 | 0.91064 |
| 103.61 | 275.59 | 0.89565 |
| 105.35 | 272.54 | 0.88555 |
| 107.10 | 264.45 | 0.85324 |
| 108.88 | 254.18 | 0.81136 |
| 110.67 | 245.39 | 0.78010 |
| 112.48 | 245.42 | 0.78441 |
| 114.32 | 238.35 | 0.75995 |
| 116.18 | 233.16 | 0.74309 |
| 118.07 | 229.50 | 0.73205 |
| 120.00 | 219.27 | 0.69576 |
| 121.97 | 217.16 | 0.69087 |
| 123.97 | 215.73 | 0.68827 |
| 126.03 | 205.25 | 0.65184 |

TABLE VI-66

DERIVED EMISSIVITY

RUN NO. 9 FREQ 16.5GHZ
 DATE 08/01/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 274.38 | 0.48740 |
| 98.46 | 273.93 | 0.58864 |
| 100.16 | 272.14 | 0.64747 |
| 101.86 | 269.66 | 0.71089 |
| 103.61 | 267.60 | 0.75548 |
| 105.35 | 260.33 | 0.75224 |
| 107.10 | 259.48 | 0.78564 |
| 108.88 | 255.61 | 0.79299 |
| 110.67 | 248.18 | 0.77484 |
| 112.48 | 247.61 | 0.78194 |
| 114.32 | 239.89 | 0.75684 |
| 116.18 | 234.75 | 0.74121 |
| 118.07 | 227.94 | 0.71774 |
| 120.00 | 227.07 | 0.71582 |
| 121.97 | 223.32 | 0.70726 |
| 123.97 | 221.90 | 0.70506 |
| 126.03 | 215.08 | 0.68765 |

TABLE VI-67

DERIVED EMISSIVITY

RUN NO. 10 FREQ 16.5GHZ
DATE 08/01/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 150.82 | ~1.57794 |
| 98.46 | 151.76 | ~0.88717 |
| 100.16 | 148.66 | ~0.46446 |
| 101.88 | 147.66 | ~0.15337 |
| 103.61 | 147.85 | 0.01597 |
| 105.35 | 152.97 | 0.16238 |
| 107.10 | 150.74 | 0.23186 |
| 108.88 | 149.43 | 0.28548 |
| 110.67 | 149.84 | 0.32378 |
| 112.48 | 146.66 | 0.32061 |
| 114.32 | 150.30 | 0.34175 |
| 116.18 | 150.98 | 0.34540 |
| 118.07 | 153.13 | 0.35318 |
| 120.00 | 151.18 | 0.34204 |
| 121.97 | 158.05 | 0.38976 |
| 123.97 | 164.52 | 0.43382 |
| 126.03 | 173.74 | 0.48725 |

TABLE VI-68

DERIVED EMISSIVITY

RUN NO. 11 FREQ 16.5GHZ
 DATE 08/05/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 326.42 | 1.41899 |
| 98.46 | 322.41 | 1.26931 |
| 100.16 | 321.59 | 1.21044 |
| 101.88 | 320.97 | 1.18070 |
| 103.61 | 312.88 | 1.10530 |
| 105.35 | 314.36 | 1.11235 |
| 107.10 | 302.54 | 1.02522 |
| 108.88 | 295.41 | 0.98185 |
| 110.67 | 297.64 | 0.99074 |
| 112.48 | 289.88 | 0.93907 |
| 114.32 | 283.03 | 0.89468 |
| 116.18 | 282.54 | 0.89235 |
| 118.07 | 276.93 | 0.85543 |
| 120.00 | 269.07 | 0.80571 |
| 121.97 | 262.90 | 0.76661 |
| 123.97 | 264.19 | 0.77542 |
| 126.03 | 259.79 | 0.74746 |

TABLE VI-69

DERIVED EMISSIVITY

RUN NO. 12 FREQ 16.5GHZ
DATE 08/05/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 213.60 | -0.48556 |
| 98.46 | 210.12 | -0.22619 |
| 100.16 | 203.07 | -0.07896 |
| 101.88 | 195.29 | 0.01990 |
| 103.61 | 190.08 | 0.08725 |
| 105.35 | 196.21 | 0.21927 |
| 107.10 | 191.96 | 0.24997 |
| 108.88 | 191.01 | 0.29157 |
| 110.67 | 194.76 | 0.35044 |
| 112.48 | 192.15 | 0.35460 |
| 114.32 | 193.96 | 0.38045 |
| 116.18 | 197.78 | 0.41342 |
| 118.07 | 198.57 | 0.42553 |
| 120.00 | 201.43 | 0.44733 |
| 121.97 | 195.93 | 0.42580 |
| 123.97 | 200.14 | 0.45721 |
| 126.03 | 205.90 | 0.49536 |

TABLE VI-70

DERIVED EMISSIVITY

RUN NO. 13 FREQ 16.5GHZ
 DATE 08/06/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 282.45 | 0.91872 |
| 98.46 | 274.04 | 0.88499 |
| 100.16 | 272.18 | 0.88149 |
| 101.88 | 268.59 | 0.86853 |
| 103.61 | 264.91 | 0.85519 |
| 105.35 | 261.08 | 0.84313 |
| 107.10 | 255.46 | 0.82262 |
| 108.88 | 250.21 | 0.80363 |
| 110.67 | 244.21 | 0.78290 |
| 112.48 | 234.61 | 0.74811 |
| 114.32 | 238.50 | 0.76591 |
| 116.18 | 232.30 | 0.74437 |
| 118.07 | 230.20 | 0.73846 |
| 120.00 | 228.16 | 0.73255 |
| 121.97 | 215.76 | 0.68731 |
| 123.97 | 222.97 | 0.71565 |
| 126.03 | 208.59 | 0.66315 |

TABLE VI-71

FORTRAN IV PROGRAM EMISS (LINK-EDITED AS EMISS) STARTED --- 11/26/69

DERIVED EMISSIVITY

RUN NO. 14 FREQ 16.5GHZ
DATE 08/06/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 117.93 | 0.02055 |
| 98.46 | 118.47 | 0.08218 |
| 100.16 | 114.81 | 0.11110 |
| 101.88 | 111.87 | 0.13105 |
| 103.61 | 114.27 | 0.16954 |
| 105.35 | 119.68 | 0.21500 |
| 107.10 | 120.93 | 0.23718 |
| 108.88 | 121.98 | 0.25489 |
| 110.67 | 124.47 | 0.27909 |
| 112.48 | 128.68 | 0.30582 |
| 114.32 | 131.35 | 0.32436 |
| 116.18 | 135.17 | 0.34605 |
| 118.07 | 137.83 | 0.36206 |
| 120.00 | 137.56 | 0.36552 |
| 121.97 | 150.06 | 0.41984 |
| 123.97 | 153.74 | 0.43888 |
| 126.03 | 163.48 | 0.49062 |

TABLE VI-72

DERIVED EMISSIVITY

RUN NO. 15 FREQ 16.5GHZ
DATE 08/07/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 274.15 | 0.89516 |
| 99.46 | 271.71 | 0.88216 |
| 100.16 | 273.28 | 0.89314 |
| 101.88 | 274.68 | 0.90059 |
| 103.61 | 265.91 | 0.86742 |
| 105.35 | 262.20 | 0.85472 |
| 107.10 | 254.30 | 0.82541 |
| 108.88 | 247.18 | 0.79305 |
| 110.67 | 242.06 | 0.78188 |
| 112.48 | 236.50 | 0.76277 |
| 114.32 | 229.44 | 0.73804 |
| 116.18 | 222.24 | 0.71282 |
| 118.07 | 217.46 | 0.69558 |
| 120.00 | 210.97 | 0.67392 |
| 121.97 | 209.05 | 0.66819 |
| 123.97 | 203.94 | 0.65555 |
| 125.03 | 195.44 | 0.62416 |

TABLE VI-73

DERIVED EMISSIVITY

RUN NO. 16 FREQ 16.5GHZ
DATE 09/07/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 100.35 | -0.02786 |
| 98.46 | 102.65 | 0.05908 |
| 100.16 | 101.80 | 0.11379 |
| 101.88 | 105.18 | 0.16528 |
| 103.61 | 102.29 | 0.17895 |
| 105.35 | 105.18 | 0.21379 |
| 107.10 | 106.02 | 0.22536 |
| 108.88 | 107.23 | 0.24010 |
| 110.67 | 111.71 | 0.27237 |
| 112.48 | 115.89 | 0.29836 |
| 114.32 | 114.83 | 0.29573 |
| 116.18 | 122.17 | 0.32960 |
| 118.07 | 121.34 | 0.33048 |
| 120.00 | 127.21 | 0.35586 |
| 121.97 | 126.18 | 0.35563 |
| 123.97 | 137.40 | 0.40244 |
| 126.03 | 158.99 | 0.48555 |

TABLE VI-74

DERIVED EMISSIVITY

RUN NO. 17 FREQ 16.5GHZ
DATE 08/07/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 102.51 | -0.02568 |
| 98.46 | 108.15 | 0.07259 |
| 100.16 | 107.10 | 0.12318 |
| 101.88 | 108.00 | 0.16116 |
| 103.61 | 109.63 | 0.19123 |
| 105.35 | 107.82 | 0.19399 |
| 107.10 | 111.61 | 0.22707 |
| 108.88 | 115.59 | 0.25071 |
| 110.67 | 118.28 | 0.27394 |
| 112.48 | 120.79 | 0.29281 |
| 114.32 | 122.10 | 0.30539 |
| 116.18 | 128.39 | 0.33533 |
| 118.07 | 129.91 | 0.34772 |
| 120.00 | 134.51 | 0.37025 |
| 121.97 | 134.95 | 0.37766 |
| 123.97 | 139.24 | 0.39914 |
| 125.03 | 146.09 | 0.42954 |

TABLE VI-75

DERIVED EMISSIVITY

RUN NO. 18 FREQ 16.5GHZ
DATE 08/07/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 274.54 | 0.88711 |
| 98.46 | 272.99 | 0.88304 |
| 100.16 | 271.39 | 0.88450 |
| 101.88 | 267.33 | 0.87002 |
| 103.61 | 265.67 | 0.86531 |
| 105.35 | 262.91 | 0.85778 |
| 107.10 | 253.49 | 0.82310 |
| 108.88 | 246.06 | 0.79539 |
| 110.67 | 241.61 | 0.78231 |
| 112.48 | 234.55 | 0.75804 |
| 114.32 | 227.80 | 0.73499 |
| 116.18 | 224.47 | 0.72461 |
| 118.07 | 221.72 | 0.71519 |
| 120.00 | 211.34 | 0.67970 |
| 121.97 | 208.59 | 0.67144 |
| 123.97 | 203.99 | 0.65534 |
| 126.03 | 200.37 | 0.64472 |

TABLE VI-76

DERIVED EMISSIVITY

RUN NO. 19 FREQ 16.5GHZ
 DATE 08/07/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 274.40 | 0.88489 |
| 98.46 | 269.19 | 0.86882 |
| 100.16 | 269.29 | 0.87437 |
| 101.88 | 268.41 | 0.87330 |
| 103.61 | 261.21 | 0.84726 |
| 105.35 | 256.85 | 0.83292 |
| 107.10 | 251.71 | 0.81539 |
| 108.88 | 245.40 | 0.79327 |
| 110.67 | 238.45 | 0.76987 |
| 112.48 | 232.65 | 0.75059 |
| 114.32 | 227.52 | 0.73377 |
| 116.18 | 220.24 | 0.70888 |
| 118.07 | 214.24 | 0.68872 |
| 120.00 | 214.12 | 0.68996 |
| 121.97 | 208.53 | 0.67141 |
| 123.97 | 201.83 | 0.64883 |
| 126.03 | 198.10 | 0.63599 |

TABLE VI-77

DERIVED EMISSIVITY

RUN NO. 20 FREQ 16.5GHZ
DATE 08/07/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 97.40 | 0.03758 |
| 98.46 | 104.41 | 0.06077 |
| 100.16 | 104.73 | 0.11292 |
| 101.88 | 107.49 | 0.16063 |
| 103.61 | 105.80 | 0.18010 |
| 105.35 | 105.63 | 0.20043 |
| 107.10 | 109.29 | 0.23163 |
| 108.88 | 113.86 | 0.26219 |
| 110.67 | 117.72 | 0.29060 |
| 112.48 | 118.29 | 0.30137 |
| 114.32 | 119.24 | 0.31199 |
| 116.18 | 122.85 | 0.33141 |
| 118.07 | 127.40 | 0.35333 |
| 120.00 | 130.40 | 0.36867 |
| 121.97 | 132.38 | 0.38195 |
| 123.97 | 137.04 | 0.40456 |
| 125.03 | 152.46 | 0.46576 |

TABLE VI-78

DERIVED EMISSIVITY

RUN NO. 21 FREQ 16.5GHZ

DATE 08/08/69

POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPRATURE (DEG.K) | EMISSIVITY |
|---------------------------|-------------------------------------|------------|
| 96.76 | 268.06 | 0.85545 |
| 98.46 | 258.31 | 0.82142 |
| 100.16 | 258.51 | 0.82941 |
| 101.88 | 259.94 | 0.83868 |
| 103.61 | 252.08 | 0.81049 |
| 105.35 | 246.36 | 0.79097 |
| 107.10 | 241.78 | 0.77562 |
| 108.88 | 238.16 | 0.76364 |
| 110.67 | 234.46 | 0.75271 |
| 112.48 | 227.37 | 0.72842 |
| 114.32 | 222.91 | 0.71408 |
| 116.18 | 219.57 | 0.70378 |
| 118.07 | 212.97 | 0.68129 |
| 120.00 | 210.38 | 0.67350 |
| 121.97 | 201.89 | 0.64438 |
| 123.97 | 205.32 | 0.66240 |
| 126.03 | 207.54 | 0.66838 |

TABLE VI-79

DERIVED EMISSIVITY

RUN NO. 22 FREQ 16.5GHZ
 DATE 08/08/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 100.17 | 0.06114 |
| 98.46 | 109.12 | 0.05720 |
| 100.16 | 108.89 | 0.11362 |
| 101.88 | 109.71 | 0.15522 |
| 103.61 | 111.31 | 0.19064 |
| 105.35 | 117.16 | 0.23594 |
| 107.10 | 119.01 | 0.25860 |
| 108.88 | 122.21 | 0.28263 |
| 110.67 | 126.34 | 0.31243 |
| 112.48 | 124.95 | 0.31580 |
| 114.32 | 129.48 | 0.34070 |
| 116.18 | 125.40 | 0.33083 |
| 118.07 | 134.15 | 0.36937 |
| 120.00 | 135.00 | 0.38058 |
| 121.97 | 139.23 | 0.40075 |
| 123.97 | 150.19 | 0.44389 |
| 126.03 | 177.12 | 0.54797 |

TABLE VI-80

DERIVED EMISSIVITY

RUN NO. 23 FREQ 16.5GHZ
DATE 08/08/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 264.99 | 0.84677 |
| 98.46 | 257.97 | 0.82572 |
| 100.16 | 258.10 | 0.83425 |
| 101.88 | 258.01 | 0.83565 |
| 103.61 | 262.06 | 0.85568 |
| 105.35 | 255.88 | 0.83382 |
| 107.10 | 245.78 | 0.79574 |
| 108.88 | 241.47 | 0.78159 |
| 110.67 | 240.90 | 0.78213 |
| 112.48 | 230.87 | 0.74706 |
| 114.32 | 230.55 | 0.74809 |
| 116.18 | 223.62 | 0.72466 |
| 118.07 | 220.61 | 0.71549 |
| 120.00 | 216.08 | 0.70361 |
| 121.97 | 205.50 | 0.56730 |
| 123.97 | 204.93 | 0.56232 |
| 126.03 | 202.48 | 0.55469 |

TABLE VI-SI

DERIVED EMISSIVITY

RUN NO. 24 FREQ 16.5GHZ
 DATE 08/08/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 102.77 | 0.03708 |
| 98.46 | 109.71 | 0.07577 |
| 100.16 | 108.95 | 0.13450 |
| 101.88 | 109.04 | 0.17048 |
| 103.61 | 112.34 | 0.20479 |
| 105.35 | 111.66 | 0.21488 |
| 107.10 | 118.14 | 0.24949 |
| 108.88 | 121.17 | 0.26573 |
| 110.67 | 119.00 | 0.27276 |
| 112.48 | 123.09 | 0.29767 |
| 114.32 | 127.08 | 0.32373 |
| 116.18 | 132.21 | 0.35273 |
| 118.07 | 132.01 | 0.35992 |
| 120.00 | 135.99 | 0.38178 |
| 121.97 | 144.96 | 0.41963 |
| 123.97 | 145.57 | 0.42882 |
| 125.03 | 169.67 | 0.51749 |

TABLE VI-82

DERIVED EMISSIVITY

RUN NO. 25 FREQ 16.5GHZ
 DATE 08/12/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|------------------------|--------------------------------------|------------|
| 96.76 | 265.39 | 0.84768 |
| 98.46 | 261.97 | 0.84210 |
| 100.16 | 265.08 | 0.86123 |
| 101.88 | 268.36 | 0.87737 |
| 103.61 | 262.61 | 0.85759 |
| 105.35 | 252.76 | 0.82199 |
| 107.10 | 249.84 | 0.81303 |
| 108.88 | 243.63 | 0.79112 |
| 110.67 | 233.11 | 0.75429 |
| 112.48 | 227.74 | 0.73589 |
| 114.32 | 227.51 | 0.73524 |
| 116.18 | 217.82 | 0.70147 |
| 118.07 | 212.73 | 0.68357 |
| 120.00 | 205.08 | 0.65631 |
| 121.97 | 203.83 | 0.65415 |
| 123.97 | 197.37 | 0.63314 |
| 126.03 | 194.95 | 0.62688 |

TABLE VI-83

DERIVED EMISSIVITY

RUN NO. 26 FREQ 15.5GHZ
DATE 08/12/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 98.61 | 0.01343 |
| 98.46 | 104.19 | 0.09358 |
| 100.16 | 102.71 | 0.13160 |
| 101.88 | 100.83 | 0.15293 |
| 103.61 | 100.58 | 0.17332 |
| 105.35 | 104.46 | 0.20306 |
| 107.10 | 109.81 | 0.23570 |
| 108.88 | 114.07 | 0.26055 |
| 110.67 | 115.75 | 0.27891 |
| 112.48 | 114.42 | 0.28360 |
| 114.32 | 121.71 | 0.32029 |
| 116.18 | 119.51 | 0.31939 |
| 118.07 | 124.66 | 0.34537 |
| 120.00 | 131.74 | 0.37744 |
| 121.97 | 127.54 | 0.36521 |
| 123.97 | 145.45 | 0.43586 |
| 125.03 | 169.33 | 0.52523 |

TABLE VI-84

DERIVED EMISSIVITY

RUN NO. 27 FREQ 16.5GHZ
DATE 08/12/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 270.60 | 0.86814 |
| 98.46 | 266.19 | 0.85590 |
| 100.16 | 265.77 | 0.86089 |
| 101.88 | 263.51 | 0.85482 |
| 103.61 | 259.72 | 0.84259 |
| 105.35 | 253.27 | 0.81999 |
| 107.10 | 250.26 | 0.81068 |
| 108.88 | 244.74 | 0.79132 |
| 110.67 | 236.96 | 0.76466 |
| 112.48 | 233.87 | 0.75526 |
| 114.32 | 227.68 | 0.73405 |
| 116.18 | 222.33 | 0.71500 |
| 118.07 | 217.22 | 0.69976 |
| 120.00 | 212.61 | 0.68339 |
| 121.97 | 205.03 | 0.65922 |
| 123.97 | 205.24 | 0.66141 |
| 126.03 | 197.30 | 0.63512 |

TABLE VI-85

DERIVED EMISSIVITY

RUN NO. 28 FREQ 16.5GHZ
 DATE 08/12/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 104.80 | -0.00467 |
| 98.46 | 111.07 | 0.08685 |
| 100.16 | 109.56 | 0.12989 |
| 101.88 | 107.38 | 0.15506 |
| 103.51 | 114.50 | 0.21007 |
| 105.35 | 109.80 | 0.20854 |
| 107.10 | 119.62 | 0.26301 |
| 108.88 | 123.09 | 0.28713 |
| 110.67 | 118.34 | 0.28073 |
| 112.48 | 123.63 | 0.31071 |
| 114.32 | 128.50 | 0.33718 |
| 116.18 | 130.26 | 0.35027 |
| 118.07 | 135.11 | 0.37423 |
| 120.00 | 139.11 | 0.39416 |
| 121.97 | 138.27 | 0.39691 |
| 123.97 | 148.12 | 0.43904 |
| 126.03 | 170.23 | 0.52525 |

TABLE VI-86

DERIVED EMISSIVITY

RUN NO. 29 FREQ 16.5GHZ
 DATE 08/12/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 102.49 | 0.00460 |
| 98.46 | 108.21 | 0.08240 |
| 100.16 | 107.86 | 0.12911 |
| 101.88 | 108.39 | 0.16379 |
| 103.61 | 110.24 | 0.19417 |
| 105.35 | 111.98 | 0.21838 |
| 107.10 | 114.40 | 0.24091 |
| 108.88 | 117.85 | 0.26415 |
| 110.67 | 121.57 | 0.29150 |
| 112.48 | 123.00 | 0.30579 |
| 114.32 | 125.76 | 0.32580 |
| 116.18 | 124.03 | 0.32514 |
| 118.07 | 125.98 | 0.33969 |
| 120.00 | 134.25 | 0.37624 |
| 121.97 | 136.50 | 0.38900 |
| 123.97 | 140.03 | 0.40593 |
| 126.03 | 149.53 | 0.44446 |

TABLE VI-87

DERIVED EMISSIVITY

RUN NO. 30 FREQ 16.5GHZ
 DATE 08/12/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS (DEG.K) | TEMPERATURE | EMISSIVITY |
|------------------------|-----------------------|-------------|------------|
| 96.76 | 275.42 | | 0.88960 |
| 98.46 | 269.45 | | 0.86878 |
| 100.16 | 268.26 | | 0.86795 |
| 101.88 | 264.58 | | 0.85519 |
| 103.61 | 255.18 | | 0.82367 |
| 105.35 | 255.60 | | 0.82483 |
| 107.10 | 252.42 | | 0.81516 |
| 108.88 | 246.49 | | 0.79452 |
| 110.67 | 238.71 | | 0.76762 |
| 112.48 | 231.20 | | 0.74154 |
| 114.32 | 224.53 | | 0.71878 |
| 116.18 | 221.70 | | 0.71043 |
| 118.07 | 214.74 | | 0.68553 |
| 120.00 | 210.45 | | 0.67253 |
| 121.97 | 206.26 | | 0.65952 |
| 123.97 | 206.03 | | 0.66094 |
| 126.03 | 198.91 | | 0.63713 |

TABLE VI- 88

DERIVED EMISSIVITY

RUN NO. 31 FREQ 16.5GHZ
 DATE 08/13/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 113.03 | ~0.05800 |
| 98.46 | 116.50 | 0.04798 |
| 100.16 | 112.28 | 0.09935 |
| 101.88 | 111.67 | 0.14568 |
| 103.61 | 113.35 | 0.18445 |
| 105.35 | 116.54 | 0.22104 |
| 107.10 | 117.50 | 0.24150 |
| 108.88 | 117.31 | 0.25235 |
| 110.67 | 117.58 | 0.26895 |
| 112.48 | 121.94 | 0.29555 |
| 114.32 | 125.21 | 0.31757 |
| 116.18 | 126.67 | 0.33003 |
| 118.07 | 132.35 | 0.35770 |
| 120.00 | 133.13 | 0.36570 |
| 121.97 | 132.82 | 0.37159 |
| 123.97 | 139.12 | 0.40180 |
| 126.03 | 150.99 | 0.45178 |

TABLE VI-89

DERIVED EMISSIVITY

RUN NO. 32 FREQ 15.5GHZ
 DATE 08/13/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 273.42 | 0.86839 |
| 98.46 | 268.58 | 0.85451 |
| 100.16 | 269.96 | 0.86883 |
| 101.88 | 267.50 | 0.86228 |
| 103.61 | 264.42 | 0.85340 |
| 105.35 | 256.89 | 0.82562 |
| 107.10 | 250.23 | 0.80156 |
| 108.88 | 245.42 | 0.78882 |
| 110.67 | 243.09 | 0.77942 |
| 112.48 | 233.26 | 0.74386 |
| 114.32 | 233.66 | 0.74809 |
| 116.18 | 225.23 | 0.71807 |
| 118.07 | 218.82 | 0.69579 |
| 120.00 | 214.69 | 0.68215 |
| 121.97 | 211.67 | 0.67312 |
| 123.97 | 201.60 | 0.63777 |
| 126.03 | 203.78 | 0.56552 |

TABLE VI-90

DERIVED EMISSIVITY

RUN NO. 35 FREQ 16.5GHZ
DATE 08/14/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 256.91 | -0.67486 |
| 98.46 | 254.17 | -0.55700 |
| 100.16 | 251.27 | -0.41585 |
| 101.88 | 254.28 | -0.27725 |
| 103.61 | 259.28 | -0.11524 |
| 105.35 | 262.39 | 0.01350 |
| 107.10 | 253.90 | -0.12781 |
| 108.88 | 247.04 | -0.16460 |
| 110.67 | 242.37 | -0.01631 |
| 112.48 | 227.24 | 0.03174 |
| 114.32 | 207.68 | 0.03248 |
| 116.18 | 217.28 | 0.29541 |
| 118.07 | 212.76 | 0.37853 |
| 120.00 | 205.07 | 0.41867 |
| 121.97 | 196.32 | 0.42968 |
| 123.97 | 214.24 | 0.57146 |
| 126.03 | 212.91 | 0.59828 |

TABLE VI-91

DERIVED EMISSIVITY

RUN NO. 36 FREQ 16.5GHZ
DATE 08/14/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 280.57 | 0.80861 |
| 98.46 | 283.45 | 0.85997 |
| 100.16 | 286.85 | 0.90310 |
| 101.88 | 284.30 | 0.89481 |
| 103.61 | 278.35 | 0.86571 |
| 105.35 | 276.73 | 0.86591 |
| 107.10 | 270.09 | 0.83965 |
| 108.88 | 260.42 | 0.79968 |
| 110.67 | 250.46 | 0.76167 |
| 112.48 | 245.24 | 0.75325 |
| 114.32 | 240.10 | 0.73506 |
| 116.18 | 232.44 | 0.71273 |
| 118.07 | 227.64 | 0.70197 |
| 120.00 | 220.76 | 0.68239 |
| 121.97 | 217.51 | 0.67565 |
| 123.97 | 211.77 | 0.66047 |
| 126.03 | 214.18 | 0.67522 |

TABLE VI-92

DERIVED EMISSIVITY

RUN NO.201 FREQ 9.5GHZ
DATE 07/17/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 323.03 | 1.17371 |
| 98.46 | 300.50 | 1.00943 |
| 100.16 | 290.47 | 0.95129 |
| 101.88 | 281.81 | 0.90928 |
| 103.61 | 274.13 | 0.87580 |
| 105.35 | 284.61 | 0.93202 |
| 107.10 | 279.20 | 0.90522 |
| 108.88 | 273.76 | 0.87704 |
| 110.67 | 268.11 | 0.84585 |
| 112.48 | 262.37 | 0.81128 |
| 114.32 | 257.00 | 0.77432 |
| 116.18 | 225.20 | 0.61084 |
| 118.07 | 224.07 | 0.50993 |
| 120.00 | 225.71 | 0.52243 |
| 121.97 | 230.29 | 0.54962 |
| 123.97 | 237.58 | 0.69720 |
| 126.03 | 285.73 | 0.93938 |

TABLE VI-93

DERIVED EMISSIVITY

RUN NO.101 FREQ 9.5GHZ
DATE 07/21/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 298.28 | 0.99374 |
| 98.46 | 286.76 | 0.91323 |
| 100.16 | 281.72 | 0.89591 |
| 101.88 | 276.27 | 0.87975 |
| 103.61 | 270.46 | 0.86226 |
| 105.35 | 259.09 | 0.82148 |
| 107.10 | 252.74 | 0.79100 |
| 108.88 | 245.41 | 0.75848 |
| 110.67 | 240.26 | 0.72333 |
| 112.48 | 234.77 | 0.68541 |
| 114.32 | 230.39 | 0.64804 |
| 116.18 | 205.49 | 0.53220 |
| 118.07 | 206.10 | 0.54297 |
| 120.00 | 209.77 | 0.56553 |
| 121.97 | 216.59 | 0.60404 |
| 123.97 | 226.19 | 0.65380 |
| 126.03 | 279.20 | 0.90598 |

TABLE VI-94

DERIVED EMISSIVITY

RUN NO.102 FREQ 9.5GHZ
DATE 07/21/69
POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 114.00 | -0.85982 |
| 98.46 | 113.05 | -0.61240 |
| 100.16 | 104.18 | -0.46346 |
| 101.88 | 96.43 | -0.33855 |
| 103.61 | 89.94 | -0.26214 |
| 105.35 | 80.31 | -0.22251 |
| 107.10 | 75.89 | -0.17096 |
| 108.88 | 72.74 | -0.12525 |
| 110.67 | 71.08 | -0.08285 |
| 112.48 | 71.49 | -0.04010 |
| 114.32 | 74.52 | 0.00594 |
| 116.18 | 57.02 | -0.04199 |
| 118.07 | 68.40 | 0.02855 |
| 120.00 | 84.64 | 0.11148 |
| 121.97 | 105.52 | 0.20722 |
| 123.97 | 130.19 | 0.31496 |
| 126.03 | 223.92 | 0.68368 |

TABLE VI-95

DERIVED EMISSIVITY

RUN NO. 1 FREQ 9.5GHZ

DATE 07/25/69

POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------------|--------------------------------------|------------|
| 96.76 | 109.75 | 0.11312 |
| 98.46 | 125.65 | 0.22498 |
| 100.16 | 138.16 | 0.30572 |
| 101.88 | 153.16 | 0.38222 |
| 103.61 | 165.41 | 0.43544 |
| 105.35 | 96.89 | 0.14309 |
| 107.10 | 96.31 | 0.13429 |
| 108.88 | 115.24 | 0.21148 |
| 110.67 | 134.32 | 0.29420 |
| 112.48 | 147.23 | 0.35749 |
| 114.32 | 171.37 | 0.46740 |
| 116.18 | 136.27 | 0.32874 |
| 118.07 | 102.14 | 0.19835 |
| 120.00 | 93.07 | 0.17166 |
| 121.97 | 127.51 | 0.31089 |
| 123.97 | 140.61 | 0.36409 |
| 126.03 | 207.99 | 0.63512 |

TABLE VI-96

DERIVED EMISSIVITY

RUN NO. 2 FREQ 9.5GHZ
DATE 07/25/69
POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 296.92 | 0.98918 |
| 98.46 | 279.20 | 0.90588 |
| 100.15 | 276.50 | 0.90183 |
| 101.88 | 275.14 | 0.90273 |
| 103.61 | 267.29 | 0.86570 |
| 105.35 | 260.00 | 0.83503 |
| 107.10 | 245.70 | 0.77359 |
| 108.88 | 237.62 | 0.73448 |
| 110.67 | 236.79 | 0.73200 |
| 112.48 | 232.44 | 0.71379 |
| 114.32 | 227.18 | 0.59129 |
| 116.18 | 196.79 | 0.56048 |
| 118.07 | 190.25 | 0.53186 |
| 120.00 | 185.39 | 0.51442 |
| 121.97 | 175.91 | 0.47061 |
| 123.97 | 178.24 | 0.47344 |
| 126.03 | 208.46 | 0.50404 |

TABLE VI-97

DERIVED EMISSIVITY

RUN NO. 33 FREQ 9.5GHZ
 DATE 08/14/69
 POLARIZATION V

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 297.57 | 0.99982 |
| 98.46 | 303.54 | 1.02568 |
| 100.16 | 301.08 | 1.01066 |
| 101.88 | 294.22 | 0.97543 |
| 103.61 | 287.81 | 0.94597 |
| 105.35 | 256.32 | 0.79514 |
| 107.10 | 257.00 | 0.79741 |
| 108.88 | 258.45 | 0.80170 |
| 110.67 | 252.74 | 0.77512 |
| 112.48 | 249.46 | 0.76145 |
| 114.32 | 235.18 | 0.69389 |
| 116.18 | 217.41 | 0.61017 |
| 118.07 | 207.69 | 0.56565 |
| 120.00 | 210.54 | 0.58188 |
| 121.97 | 200.32 | 0.53783 |
| 123.97 | 198.71 | 0.53560 |
| 126.03 | 233.24 | 0.69944 |

TABLE VI-98

DERIVED EMISSIVITY

RUN NO. 34 FREQ 9.5GHZ
 DATE 08/14/69
 POLARIZATION H

| ZENITH ANGLE (DEG.) | BRIGHTNESS TEMPERATURE (DEG.K) | EMISSIVITY |
|---------------------|--------------------------------|------------|
| 96.76 | 123.59 | 0.16041 |
| 98.46 | 118.82 | 0.09384 |
| 100.16 | 113.44 | 0.03333 |
| 101.88 | 106.61 | 0.00163 |
| 103.61 | 124.84 | 0.13582 |
| 105.35 | 130.57 | 0.19405 |
| 107.10 | 122.87 | 0.18137 |
| 108.88 | 107.23 | 0.12895 |
| 110.67 | 90.56 | 0.07566 |
| 112.48 | 94.28 | 0.10877 |
| 114.32 | 101.84 | 0.15394 |
| 116.18 | 93.43 | 0.12845 |
| 118.07 | 92.91 | 0.13500 |
| 120.00 | 105.83 | 0.19509 |
| 121.97 | 101.00 | 0.18466 |
| 123.97 | 114.05 | 0.24522 |
| 126.03 | 185.63 | 0.54157 |

TABLE VI-99

FIGURE VI-164

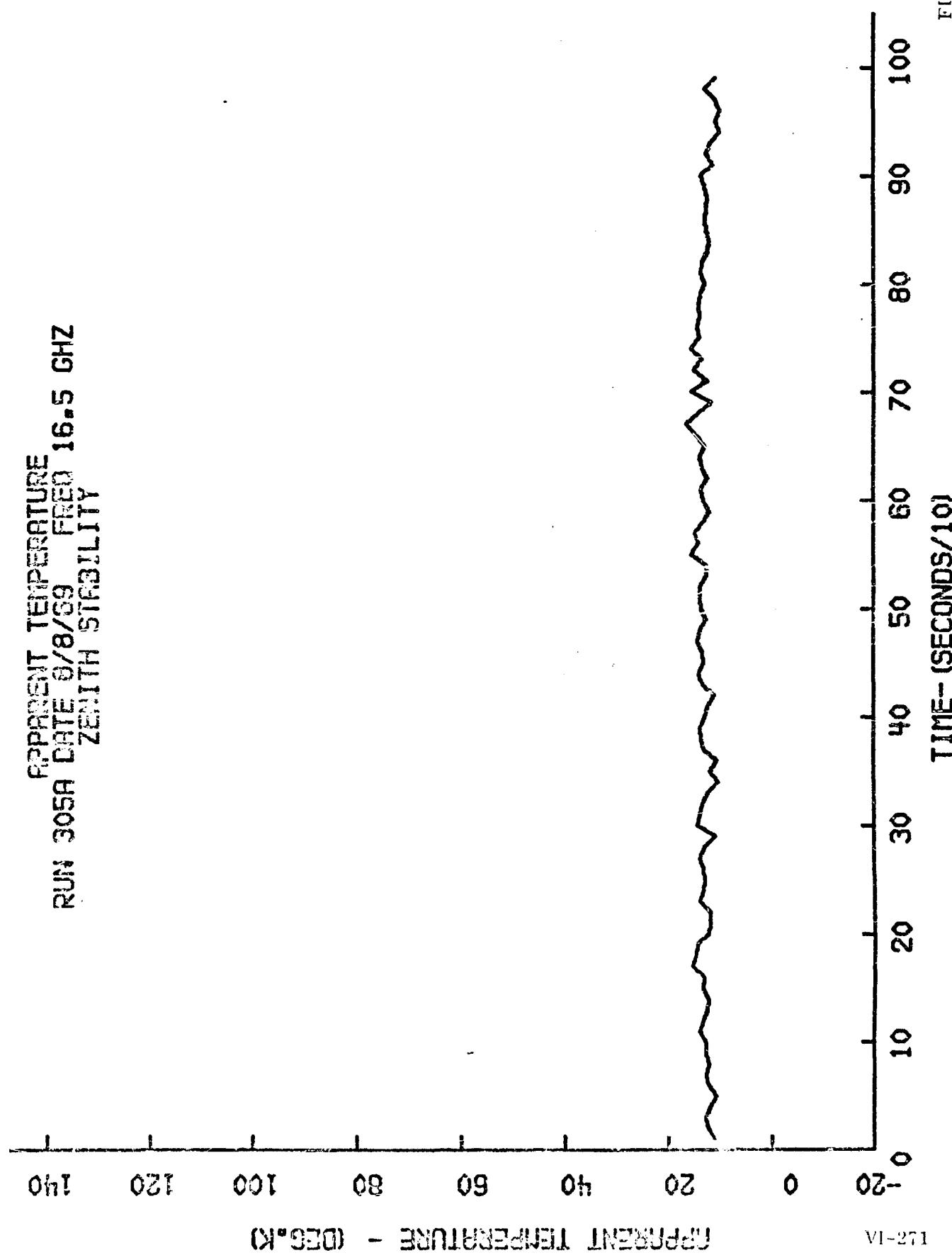
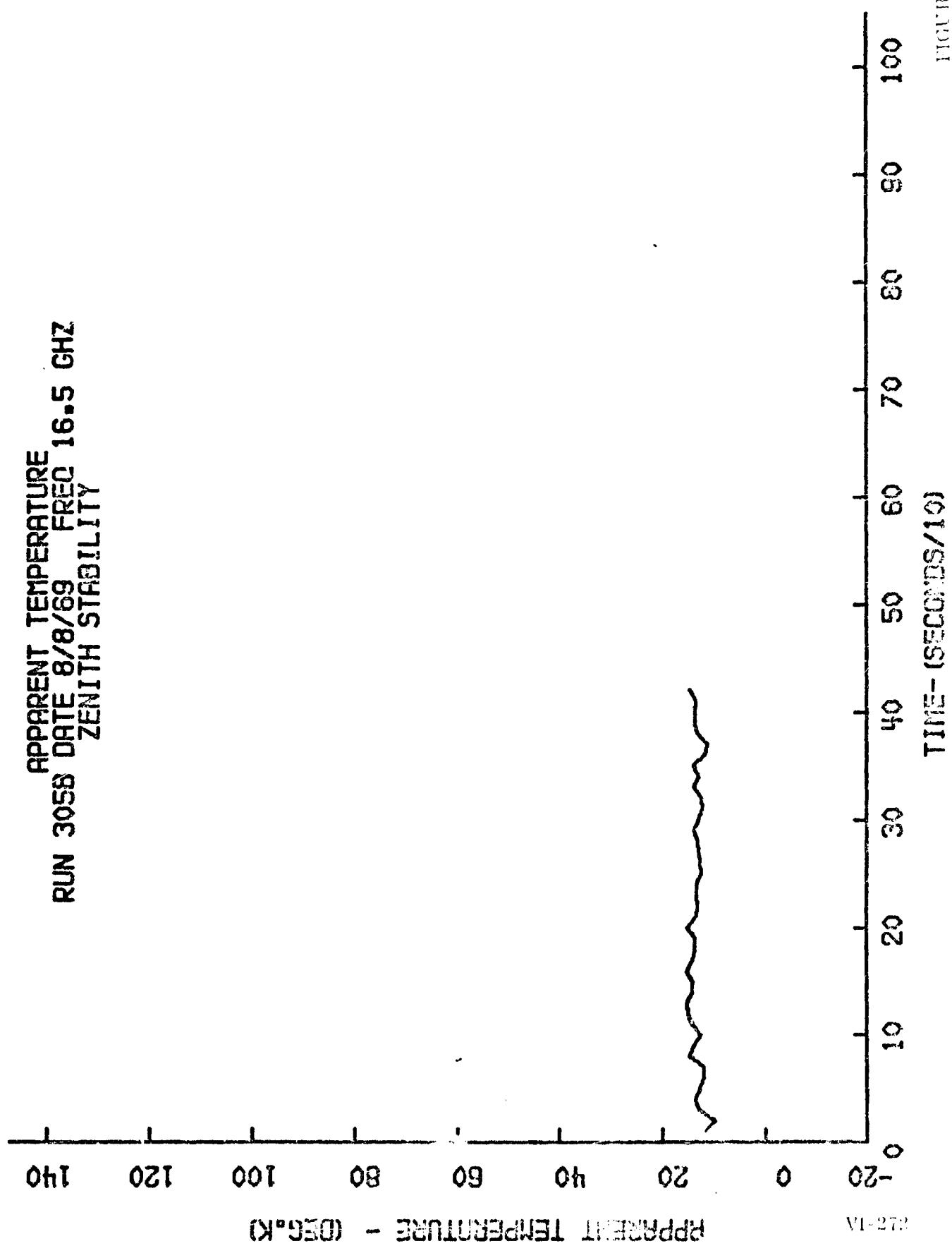


FIGURE VI-165



RUN 312A DATE 8/12/69 FREQ 16.5 GHZ
APPARENT TEMPERATURE - ZENITH STABILITY

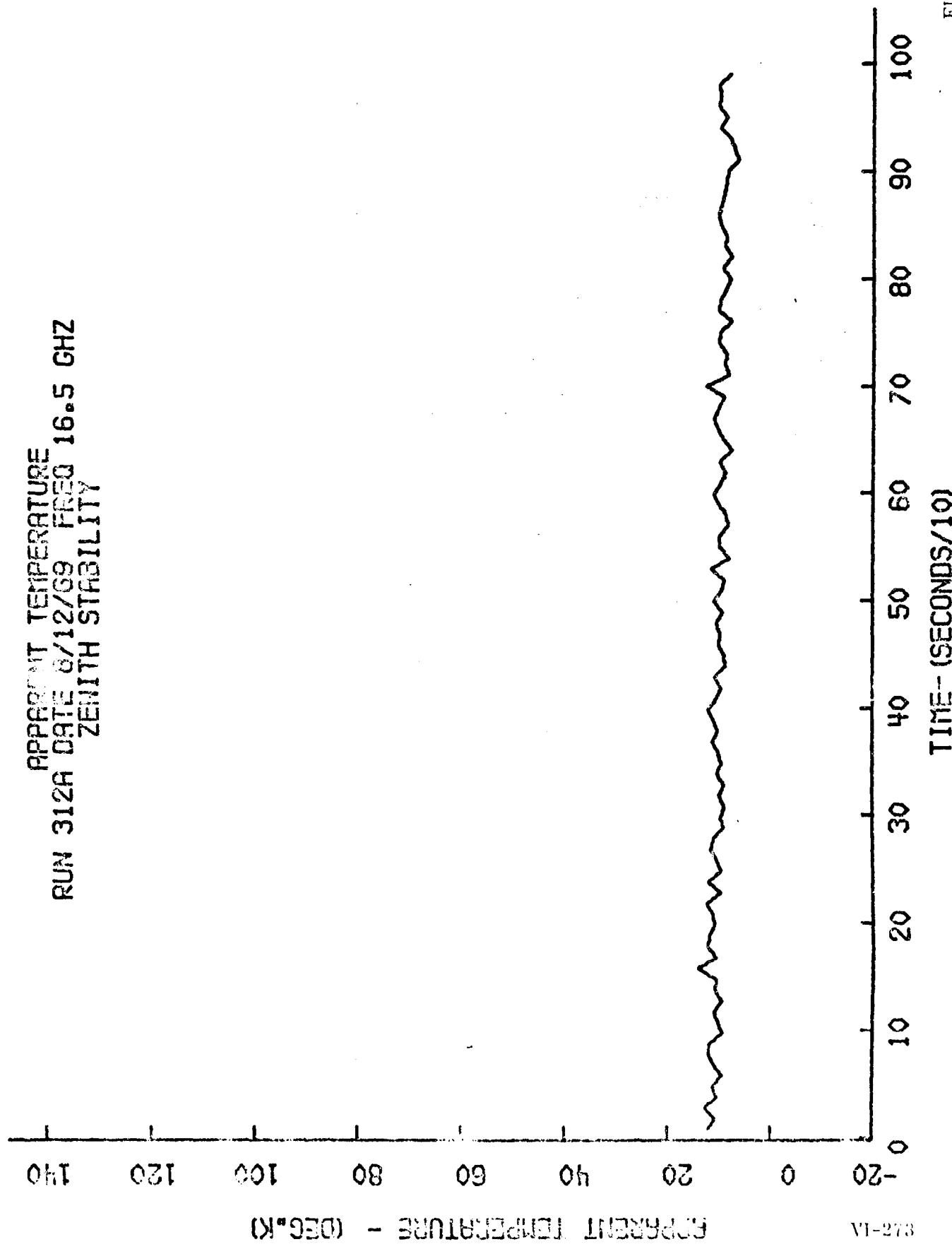


FIGURE VI-166

RUN 3128 DATE 8/12/63 FREQ 16.5 GHZ
APPARENT TEMPERATURE
ZENITH STABILITY

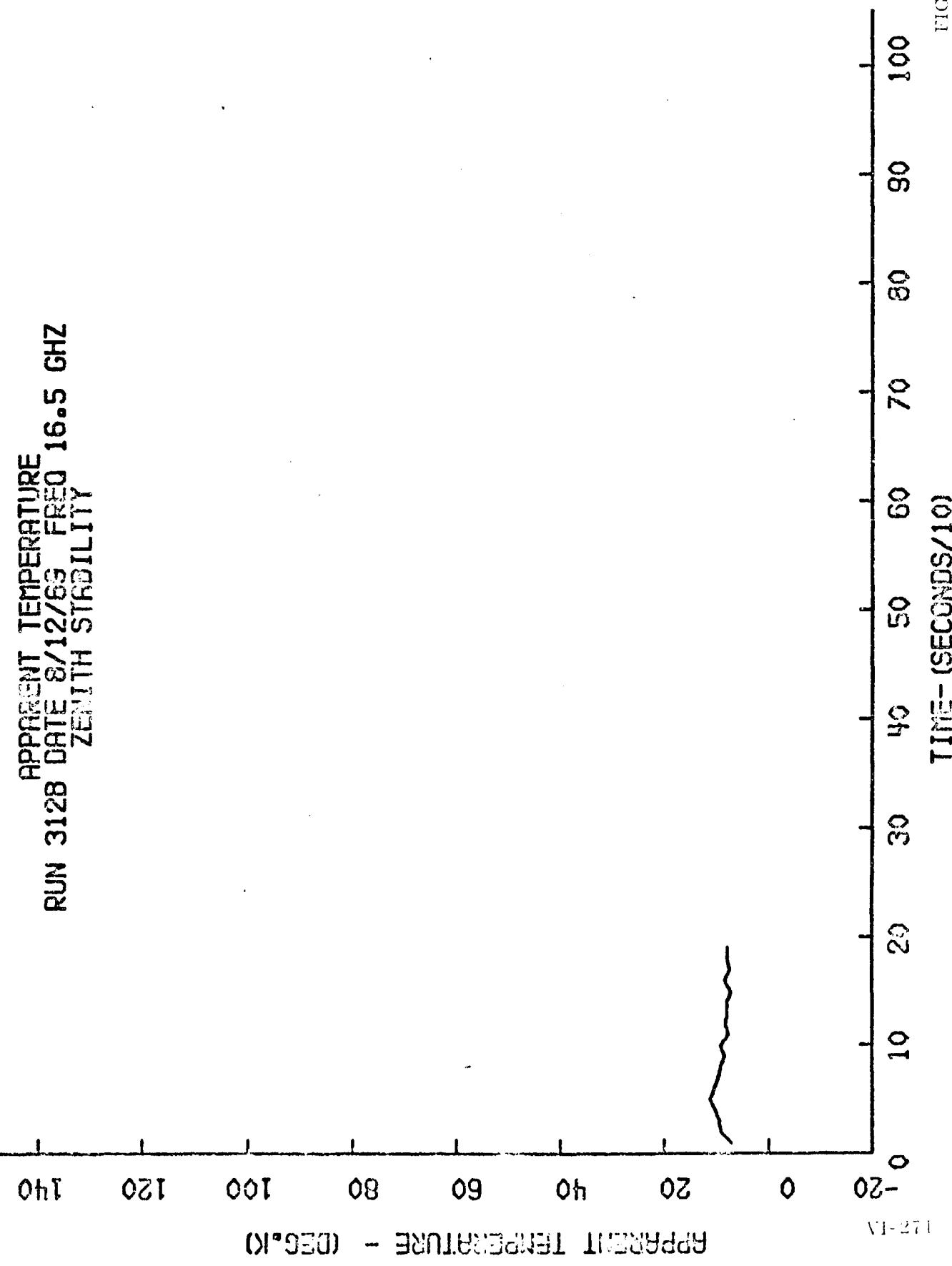


FIGURE VI-167

RUN 301A DATE 8/1/69 FREQ 16.5 GHZ
POL VERT ZENITH ANGLE 115

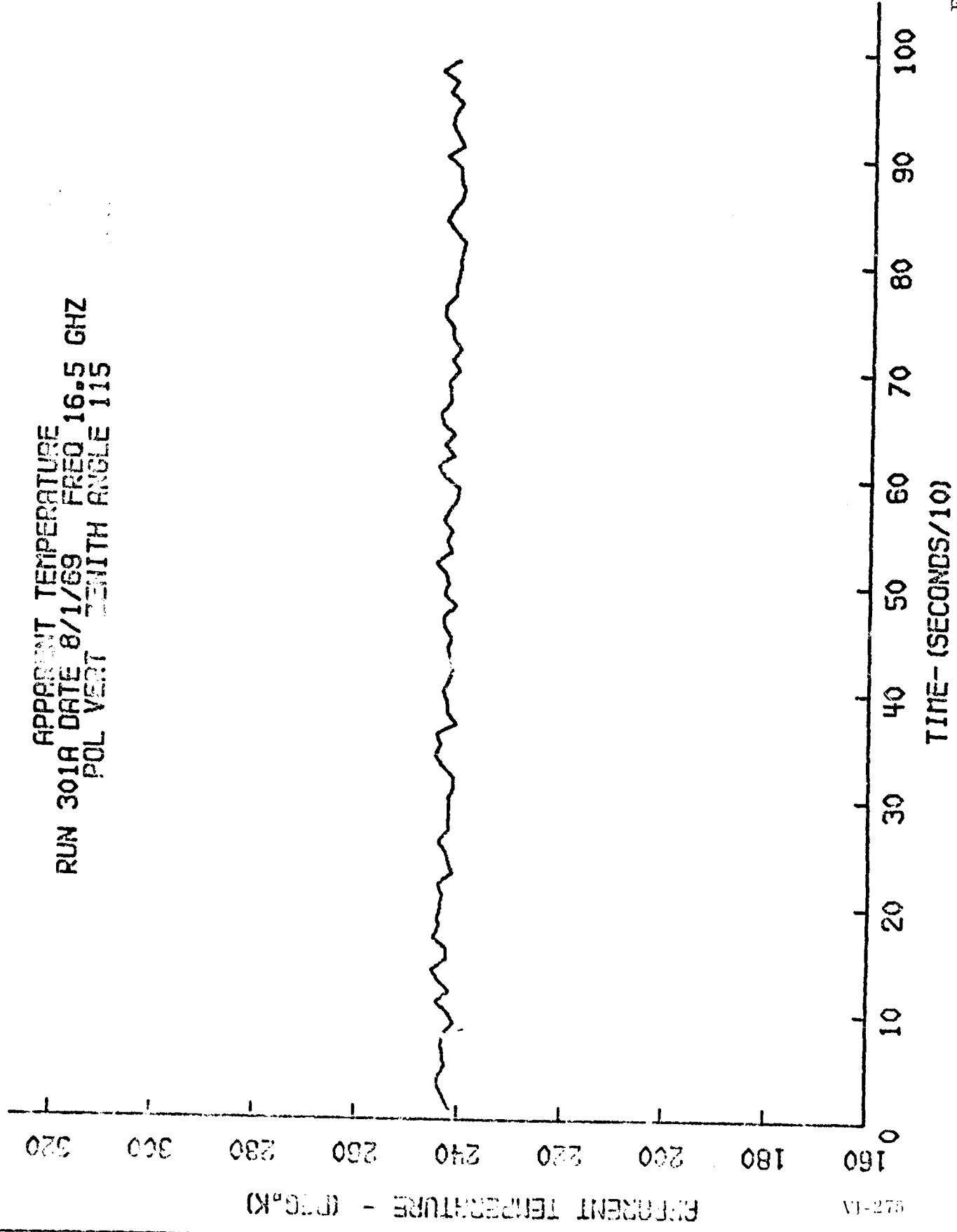
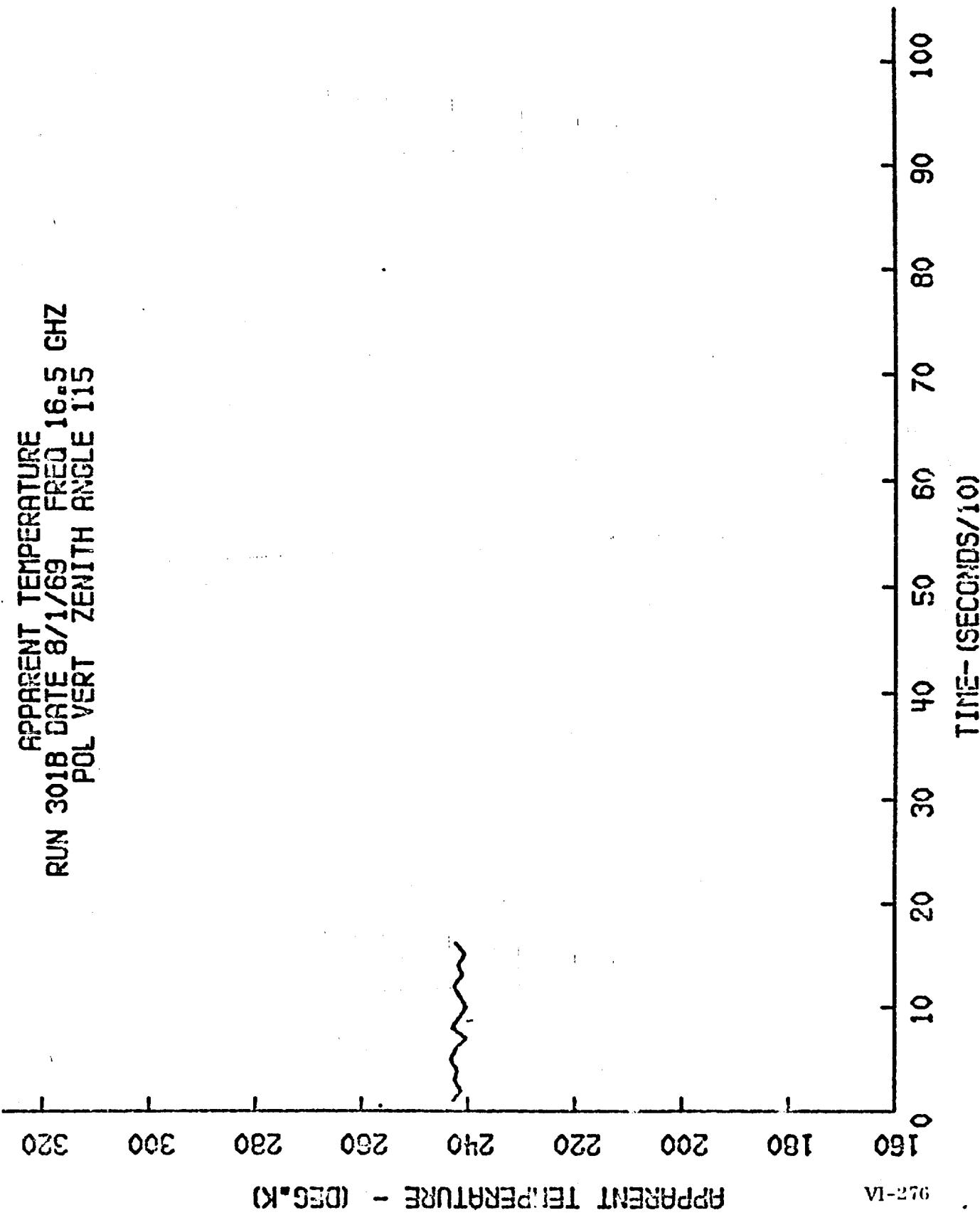
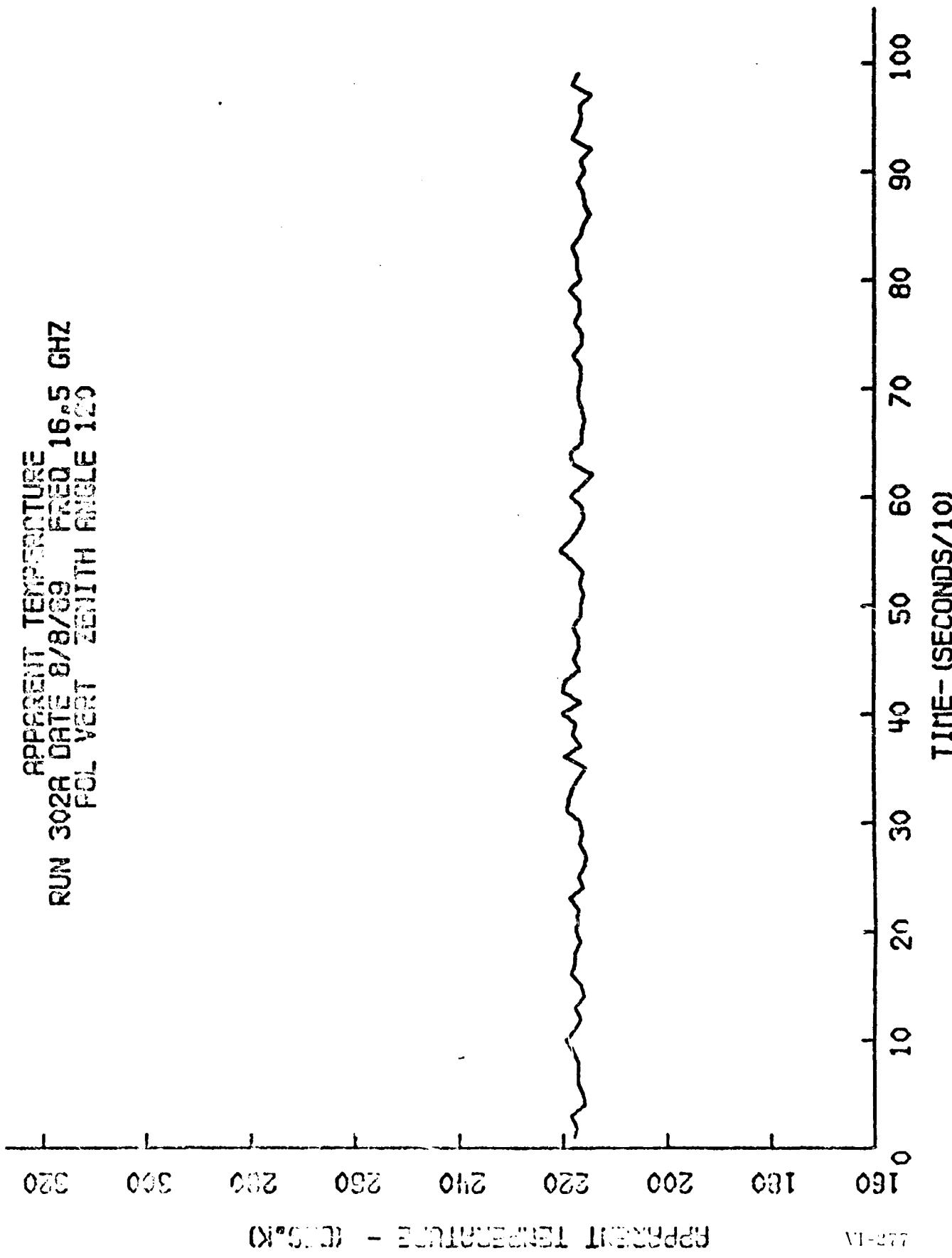


FIGURE VI-168

RUN 301B DATE 8/1/69 FREQ 16.5 GHZ
APPARENT TEMPERATURE
POL VERT ZENITH ANGLE 115



RUN 302A DATE 8/89 FREQ 16.5 GHZ
FOL VERT ZENITH FIGLE 120



VI-277

FIGURE VI-170

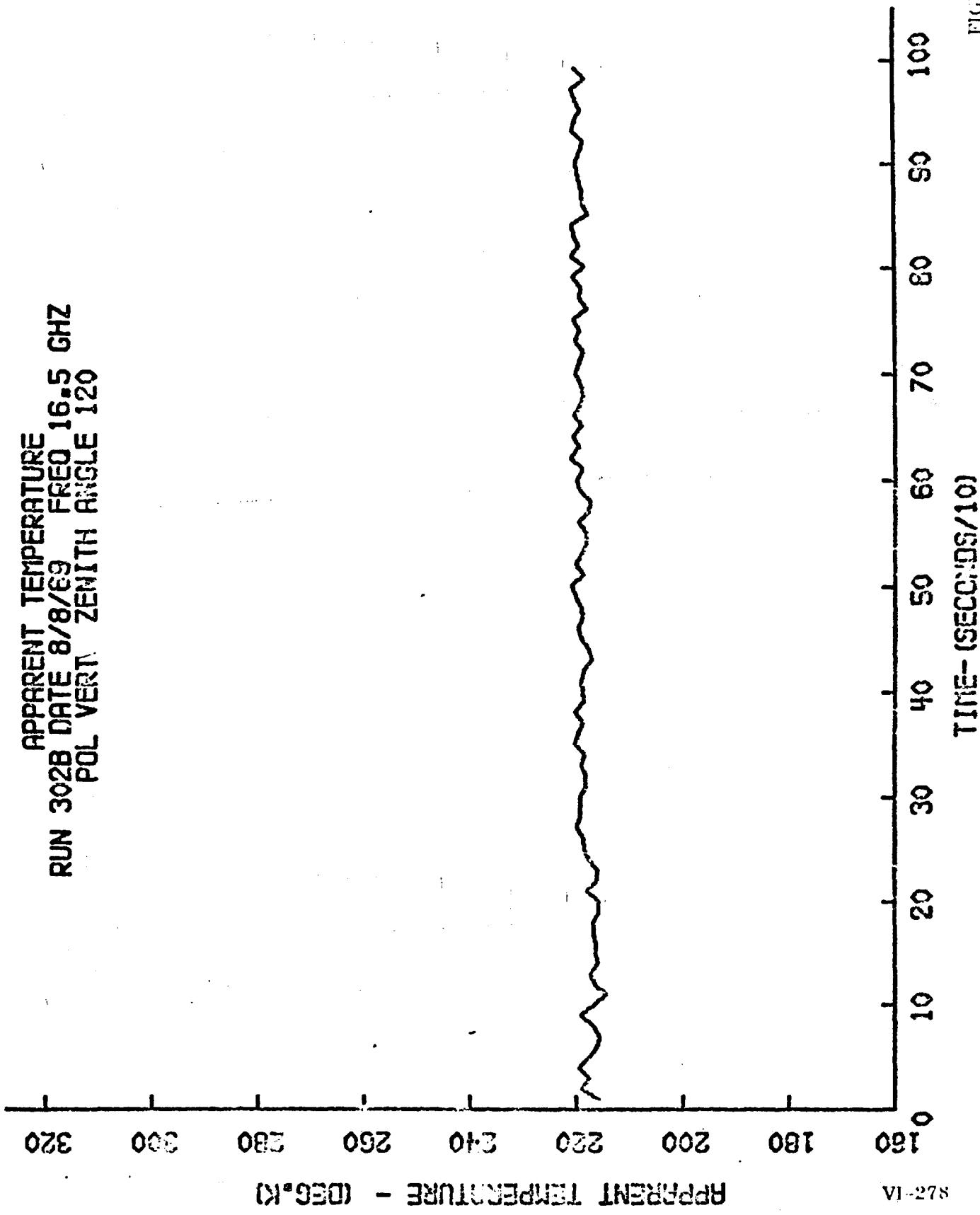
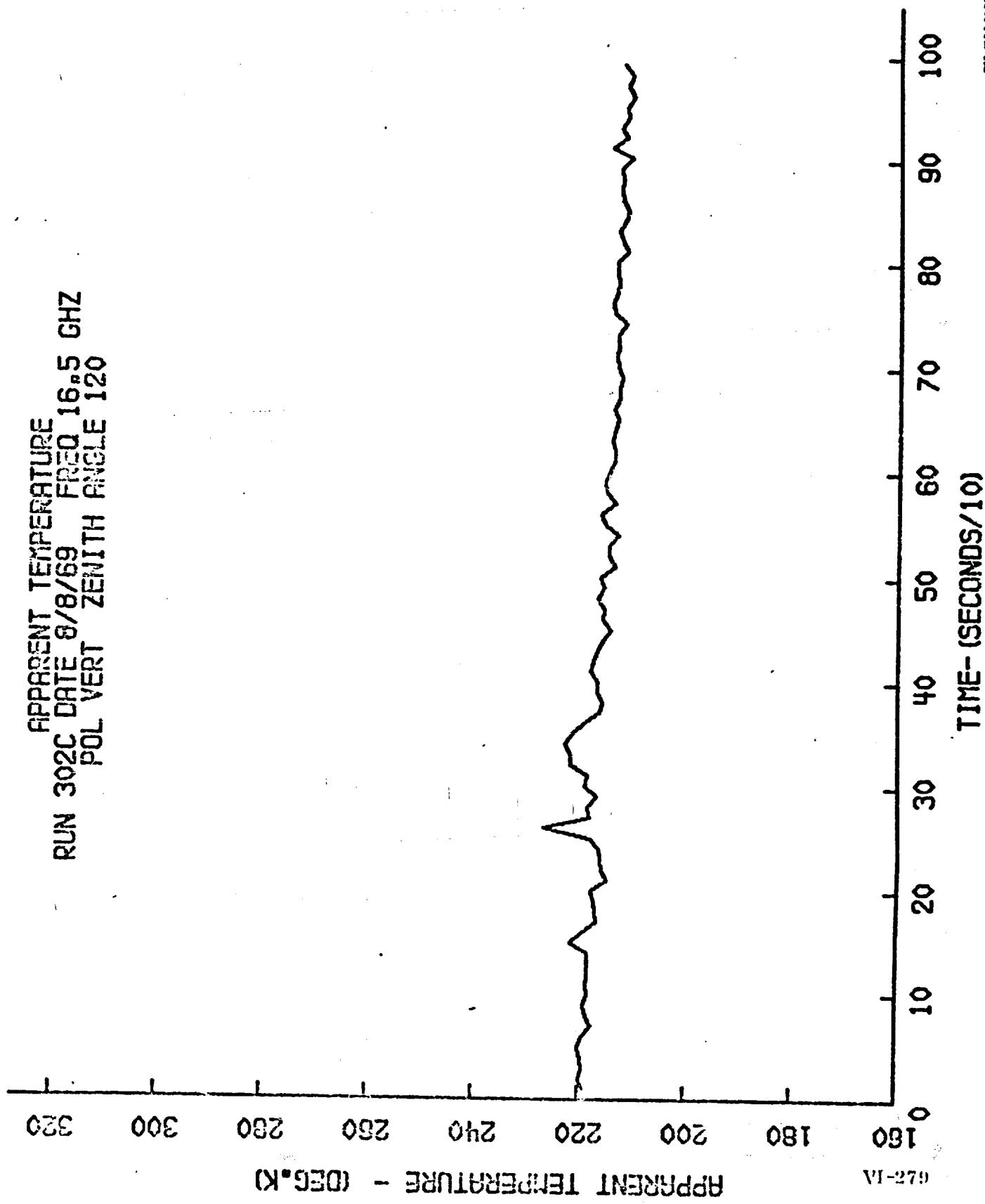
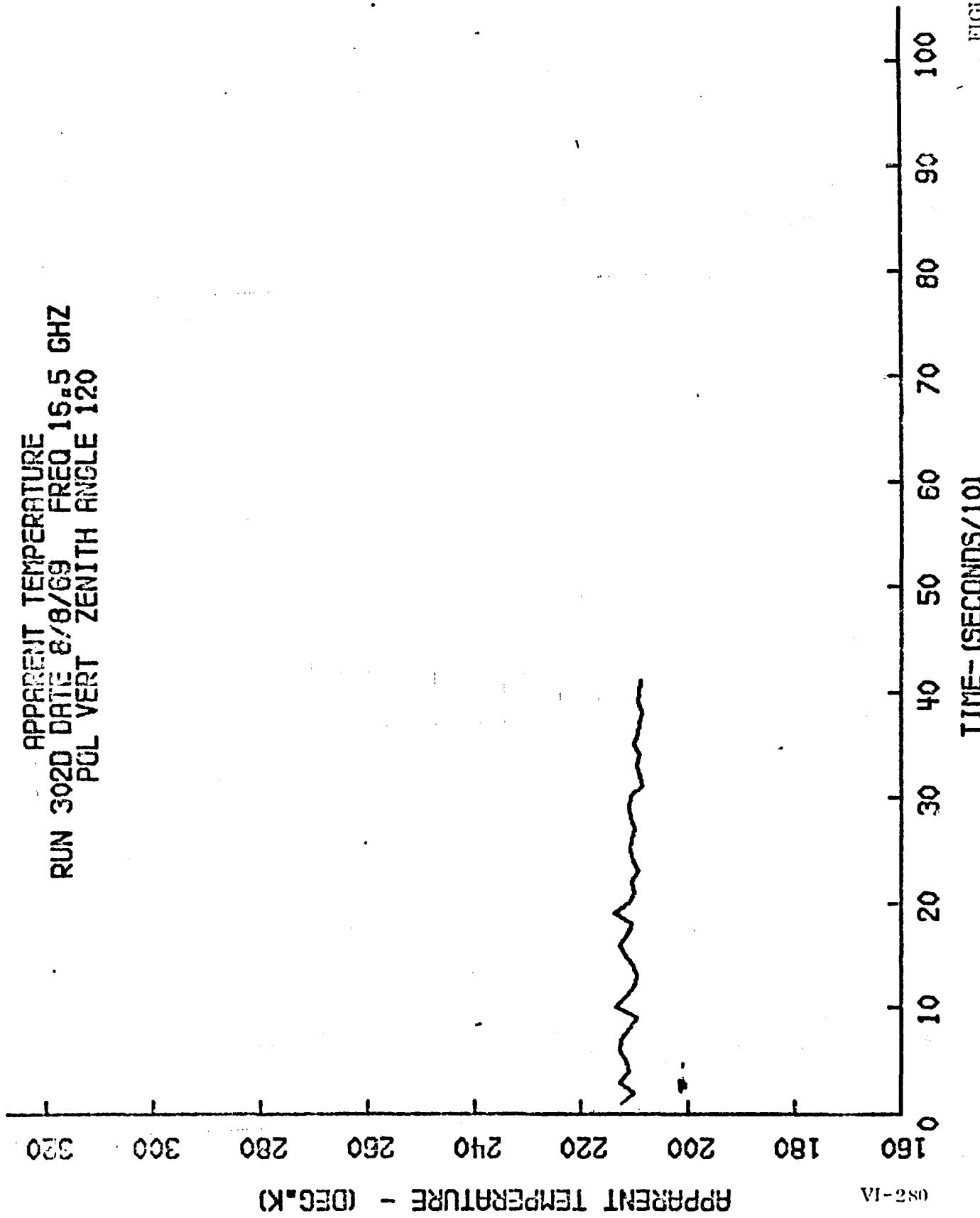


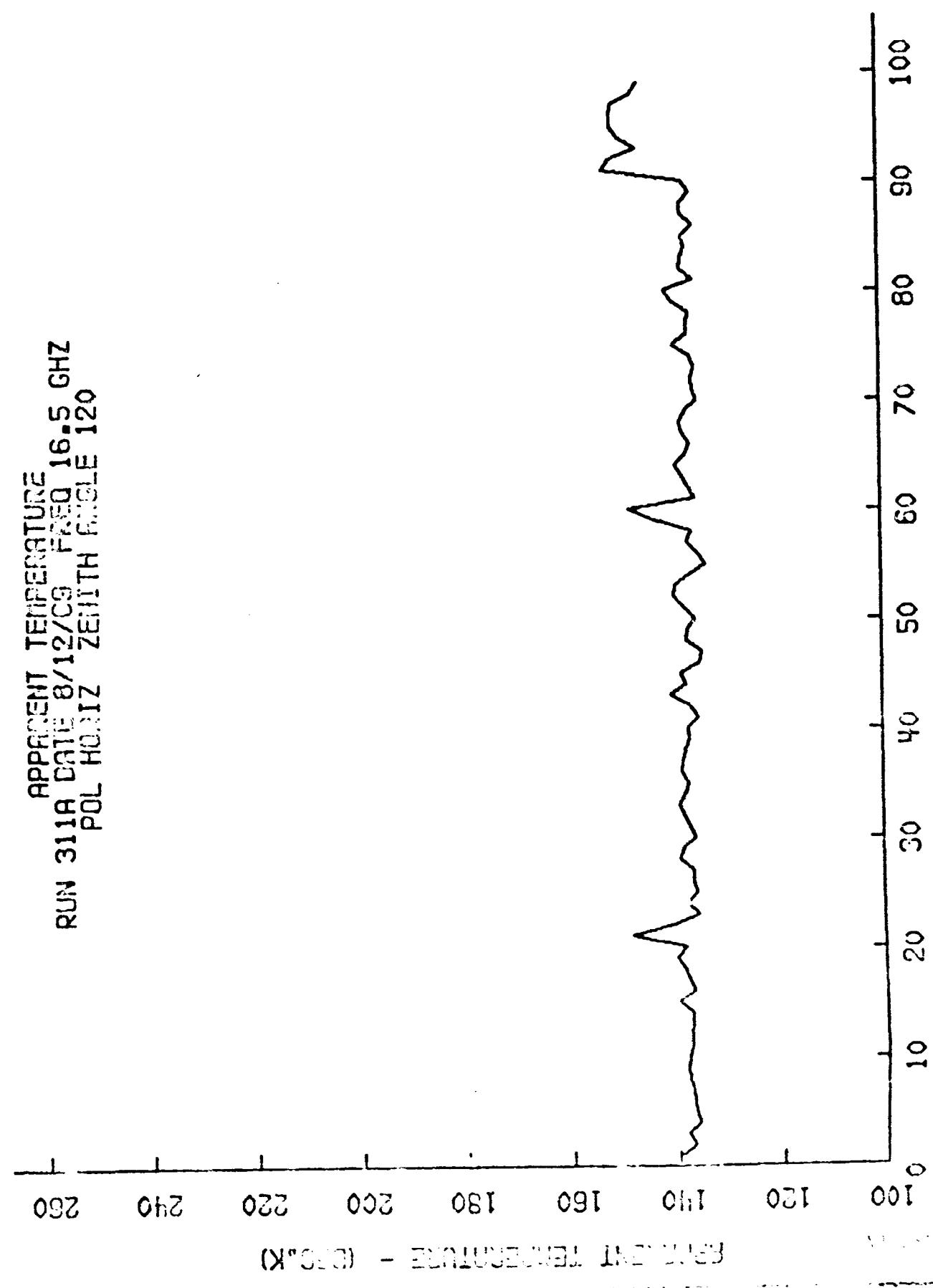
FIGURE VI-172



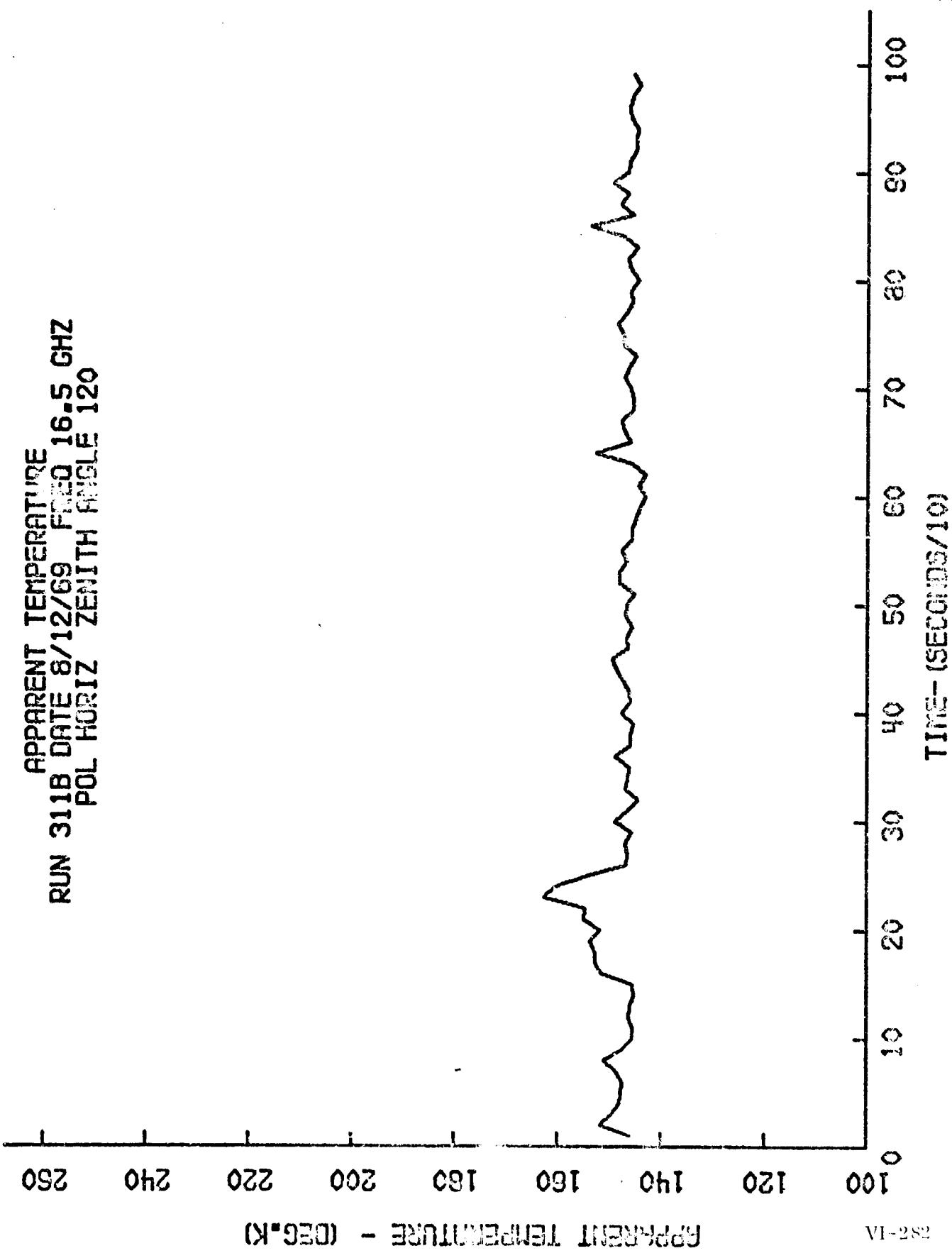
APPARENT TEMPERATURE
RUN 3020 DATE 8/6/69 FREQ 16.5 GHZ
PUL VERT ZENITH ANGLE 120

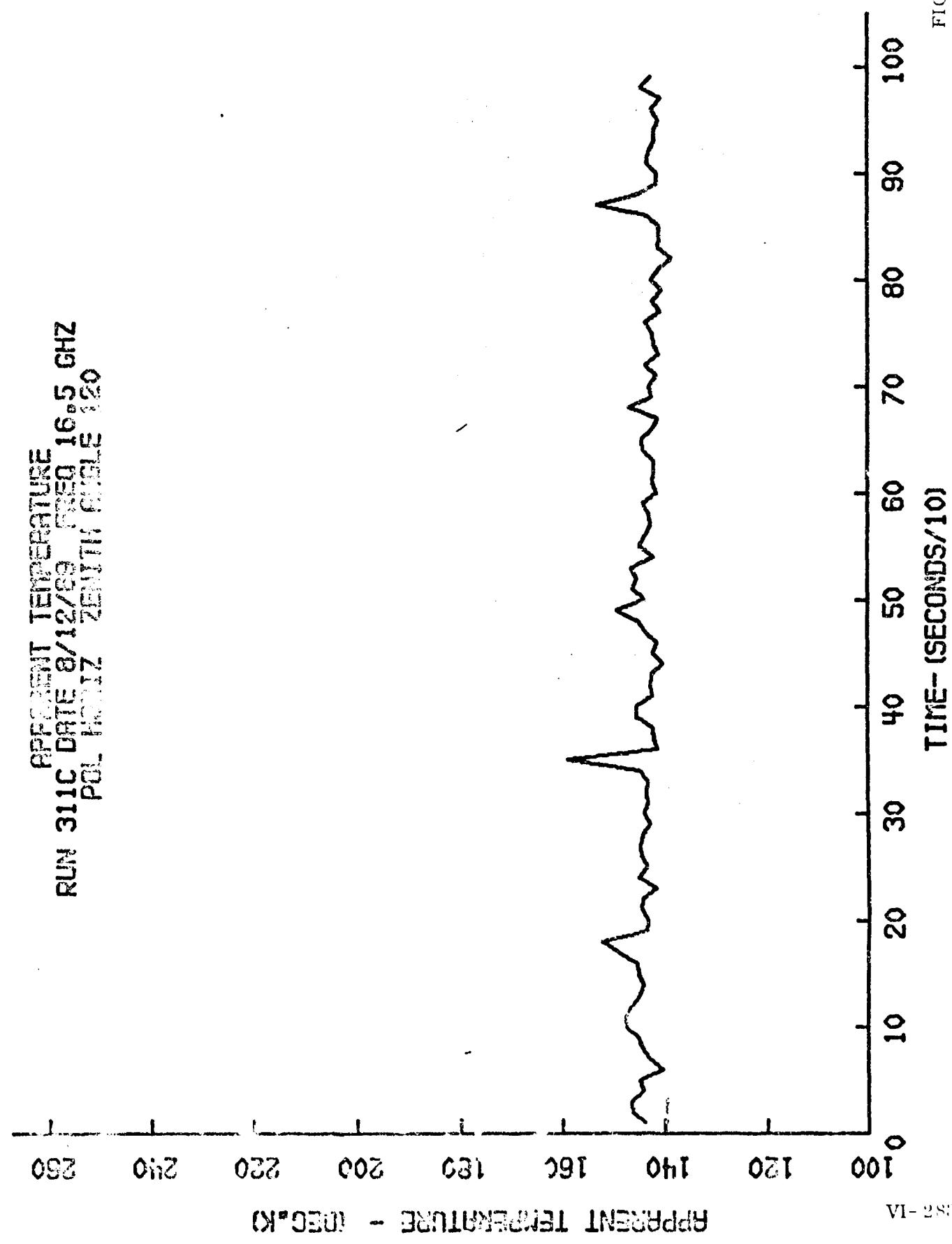


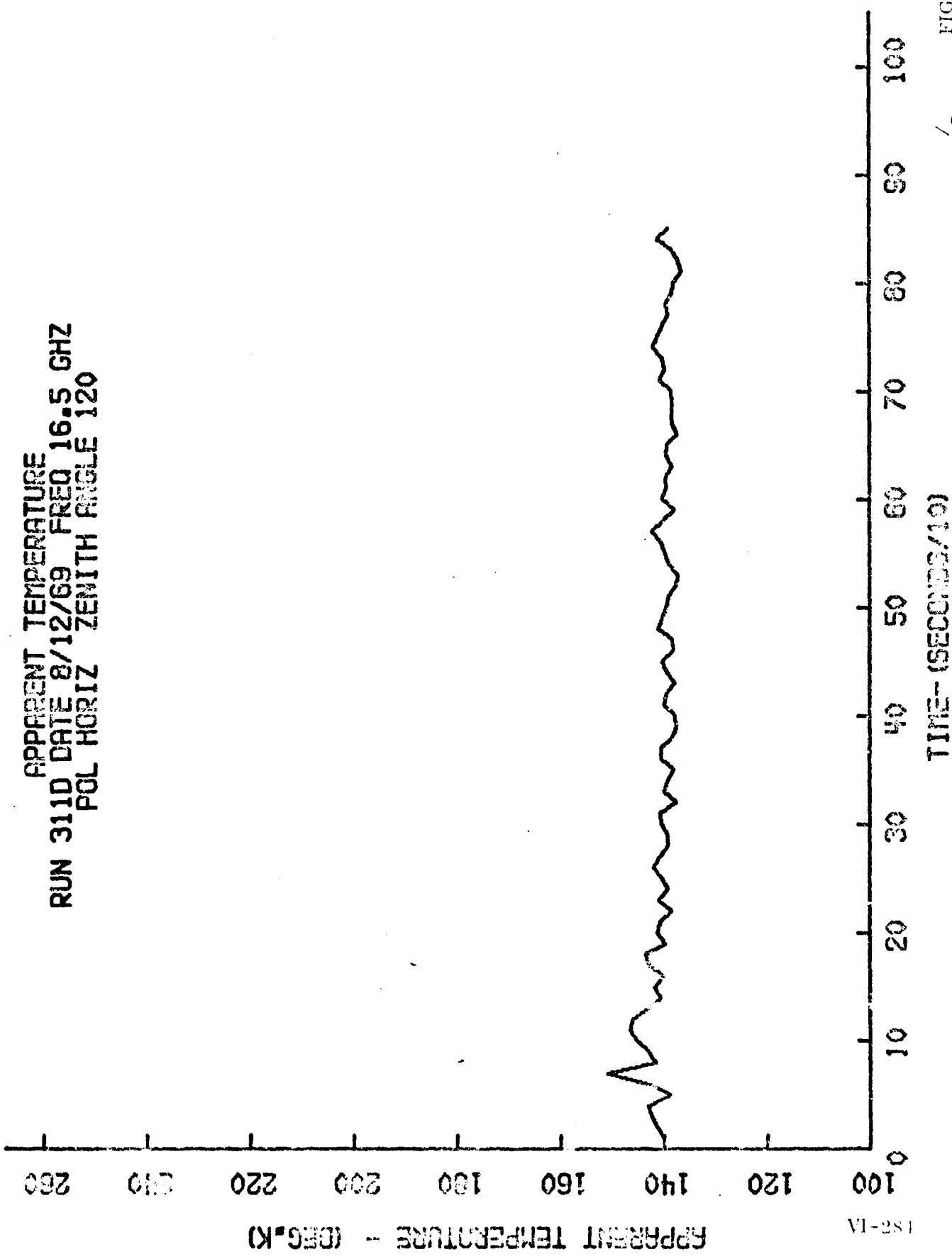
TIME (SECONDS/10)



RUN 311B DATE 8/12/69 FREQ 16.5 GHZ
POL HORIZ ZENITH ANGLE 120



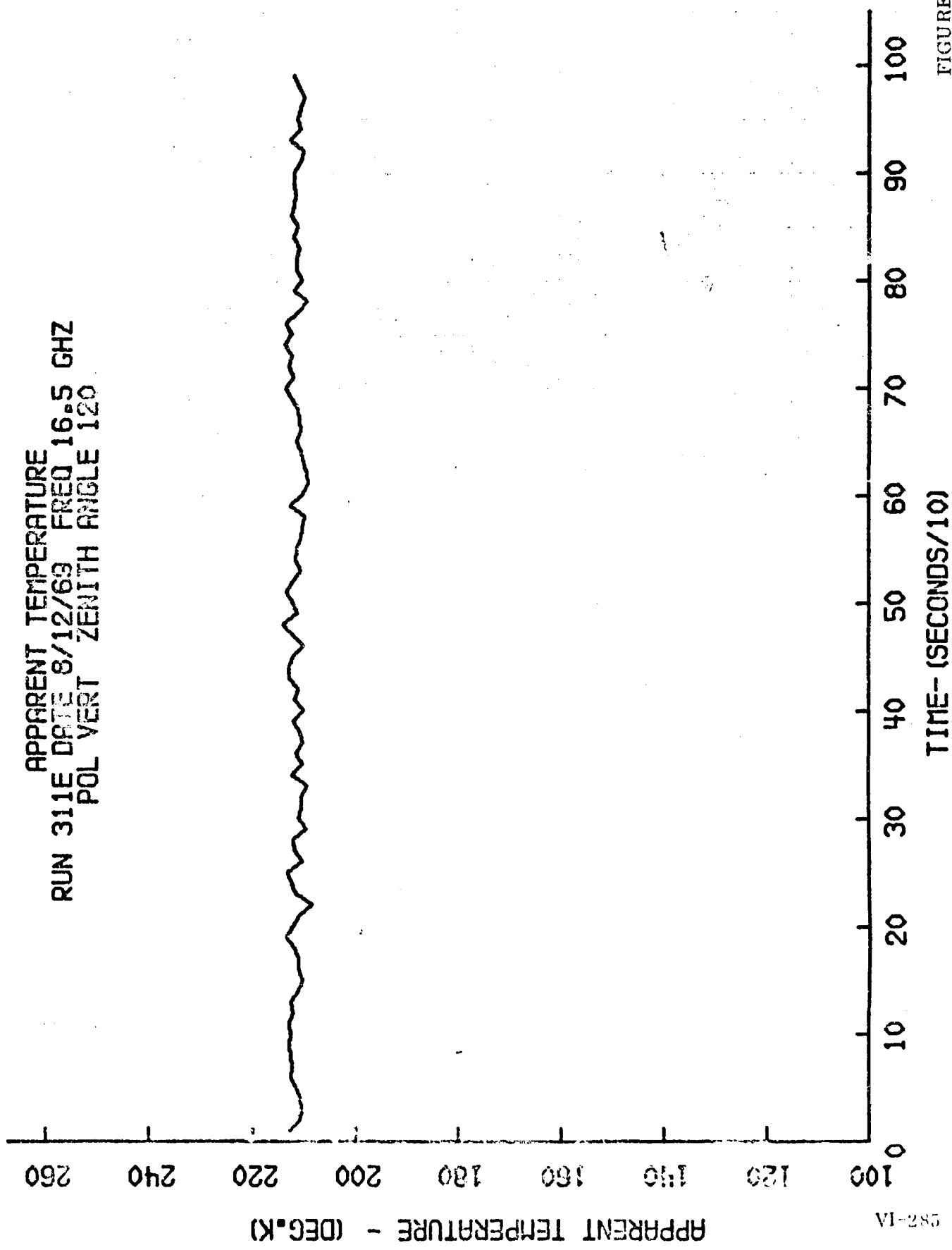




148-1A

FIGURE VI-177

APPARENT TEMPERATURE
RUN 311E DATE 8/12/63 FREQ 16.5 GHZ
POL VERT ZENITH ANGLE 120



VI-285

FIGURE VI-17S

APPARENT TEMPERATURE
RUN 311F DATE 8/12/69 FREQ 16.5 GHZ
POL VERT ZENITH ANGLE 120

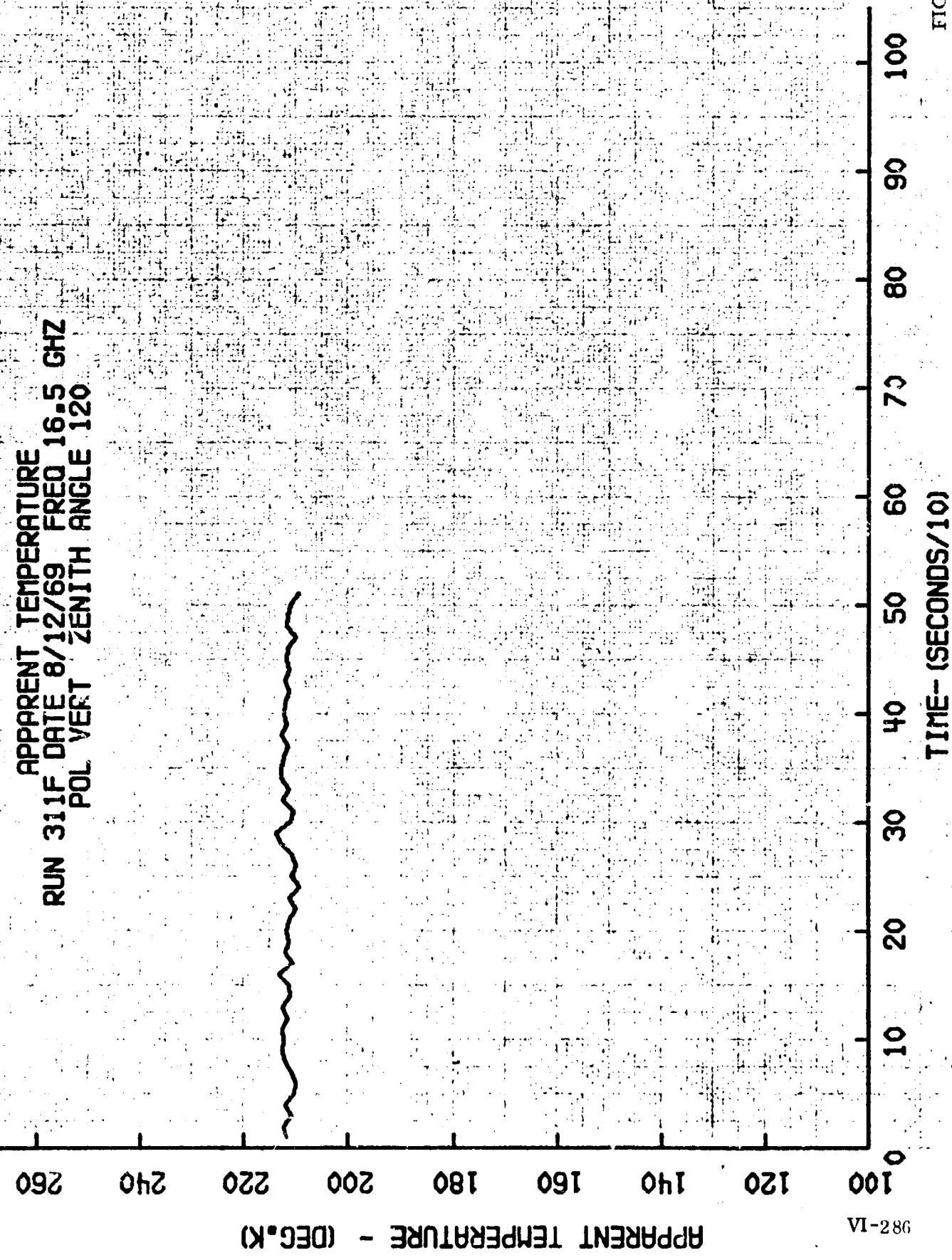
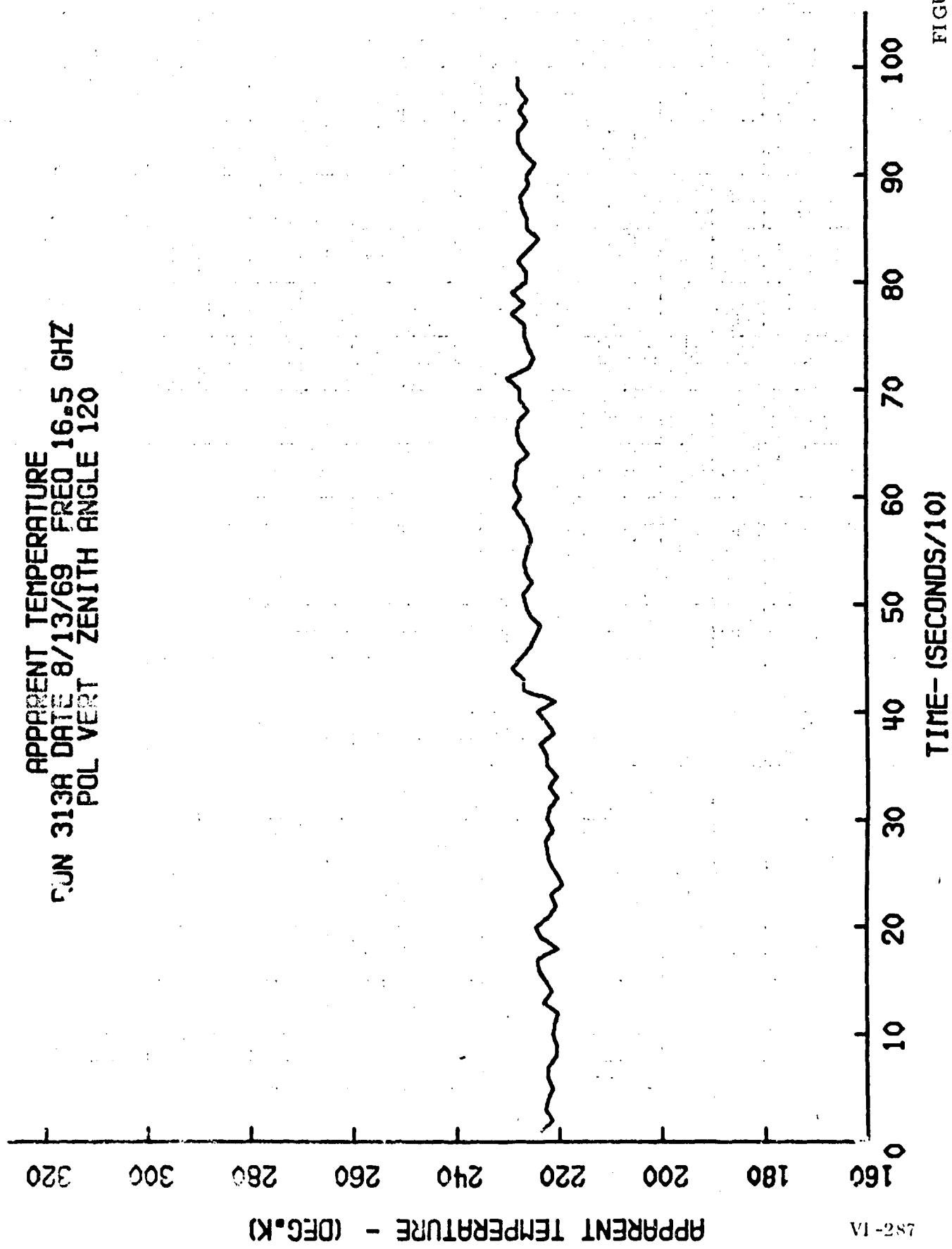


FIGURE VI-179

RUN 313A DATE 8/13/69 FREQ 16.5 GHZ
POL VERT ZENITH ANGLE 120



APPARENT TEMPERATURE
RUN 313B DATE 8/13/69 FREQ 16.5 GHZ
POL VERT ZENITH ANGLE 120

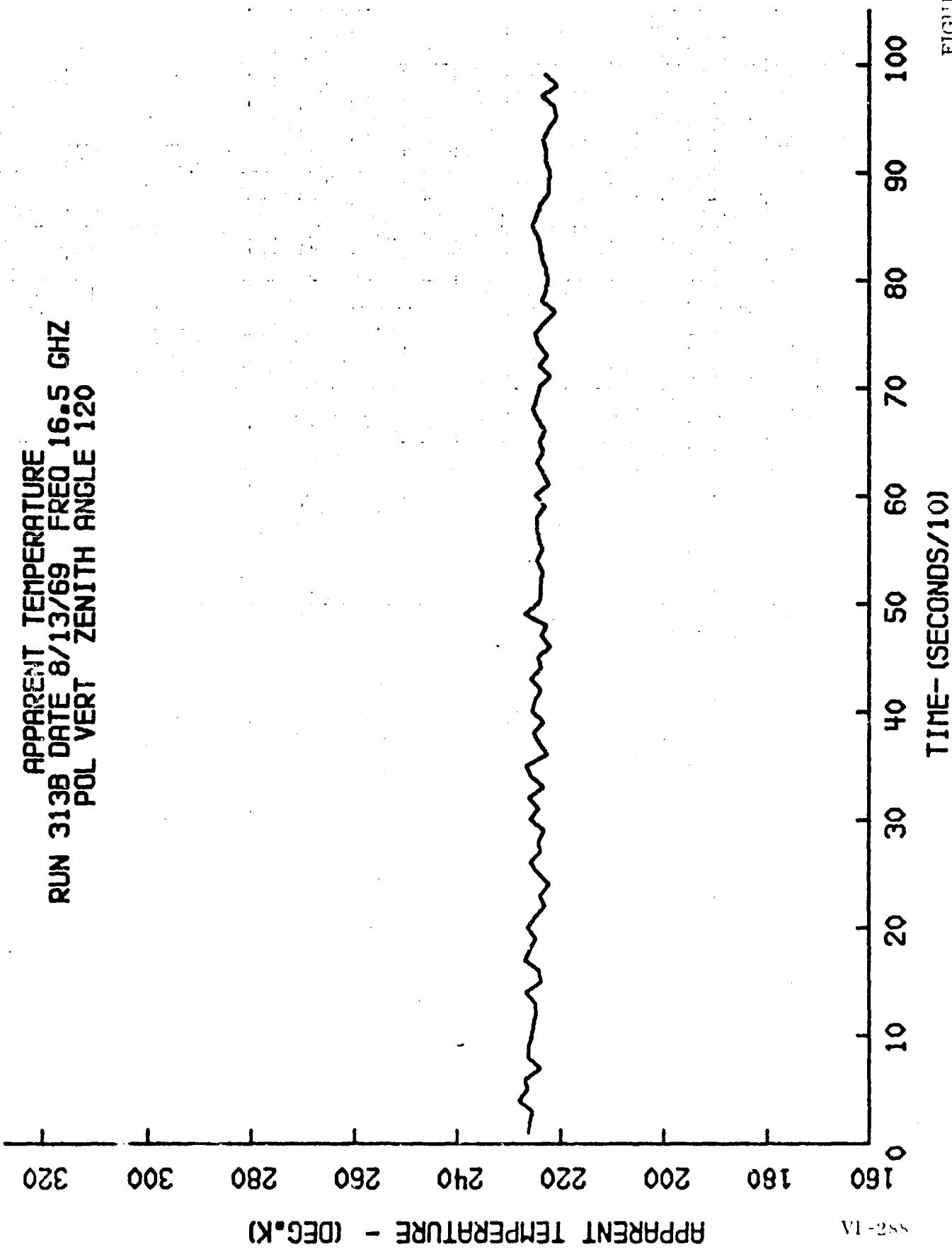


FIGURE VI-1A

FIGURE VI-1A

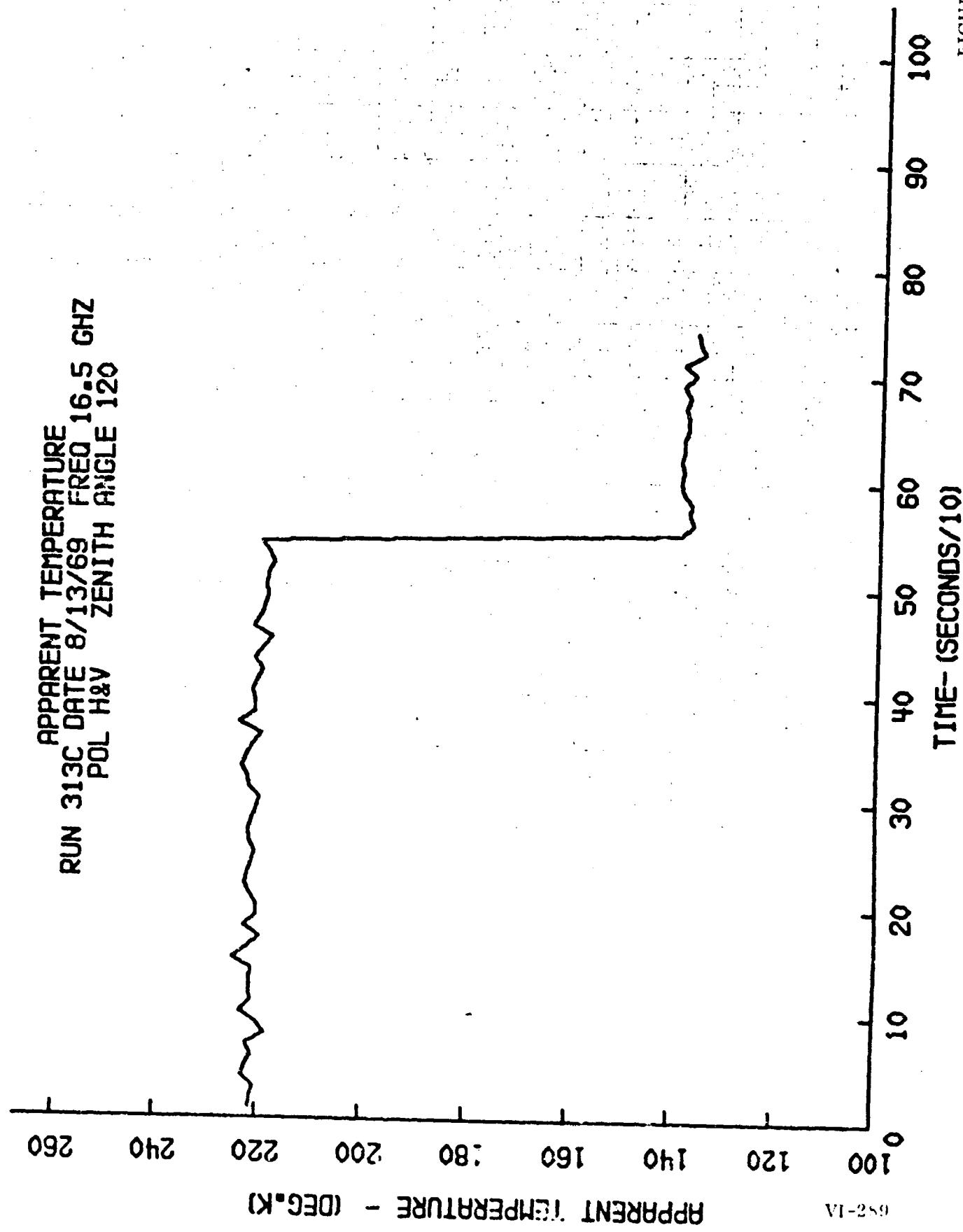
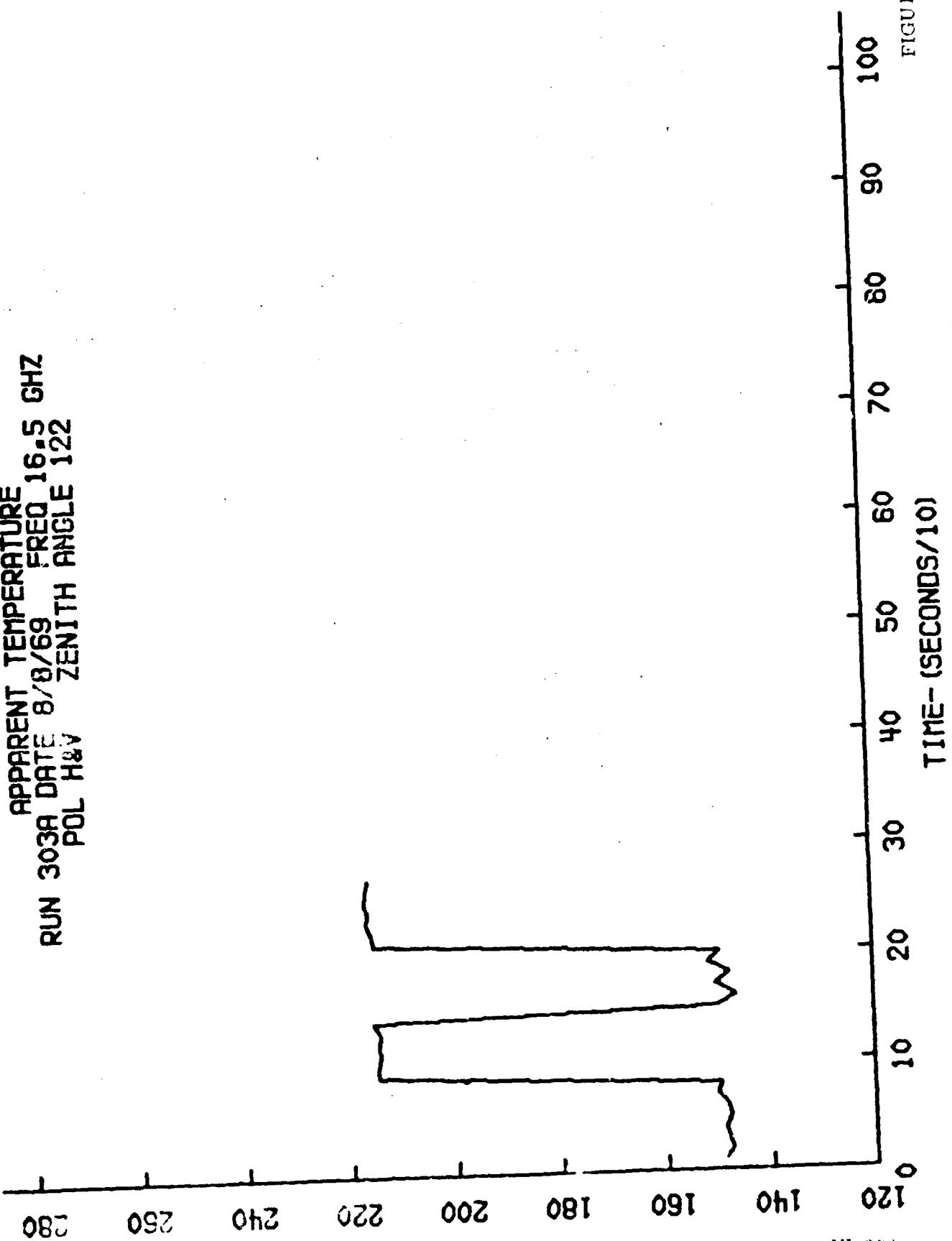


FIGURE VI-182

APPARENT TEMPERATURE
RUN 303A DATE 8/8/69 FREQ 16.5 GHZ
POL H&V ZENITH ANGLE 122

APPARENT TEMPERATURE - (DEG.K)



VI-290

FIGURE VI-183

RUN 304A DATE 3/8/69 FREQ 16.5 GHZ
PGL H.C. WITH ANGLE 115

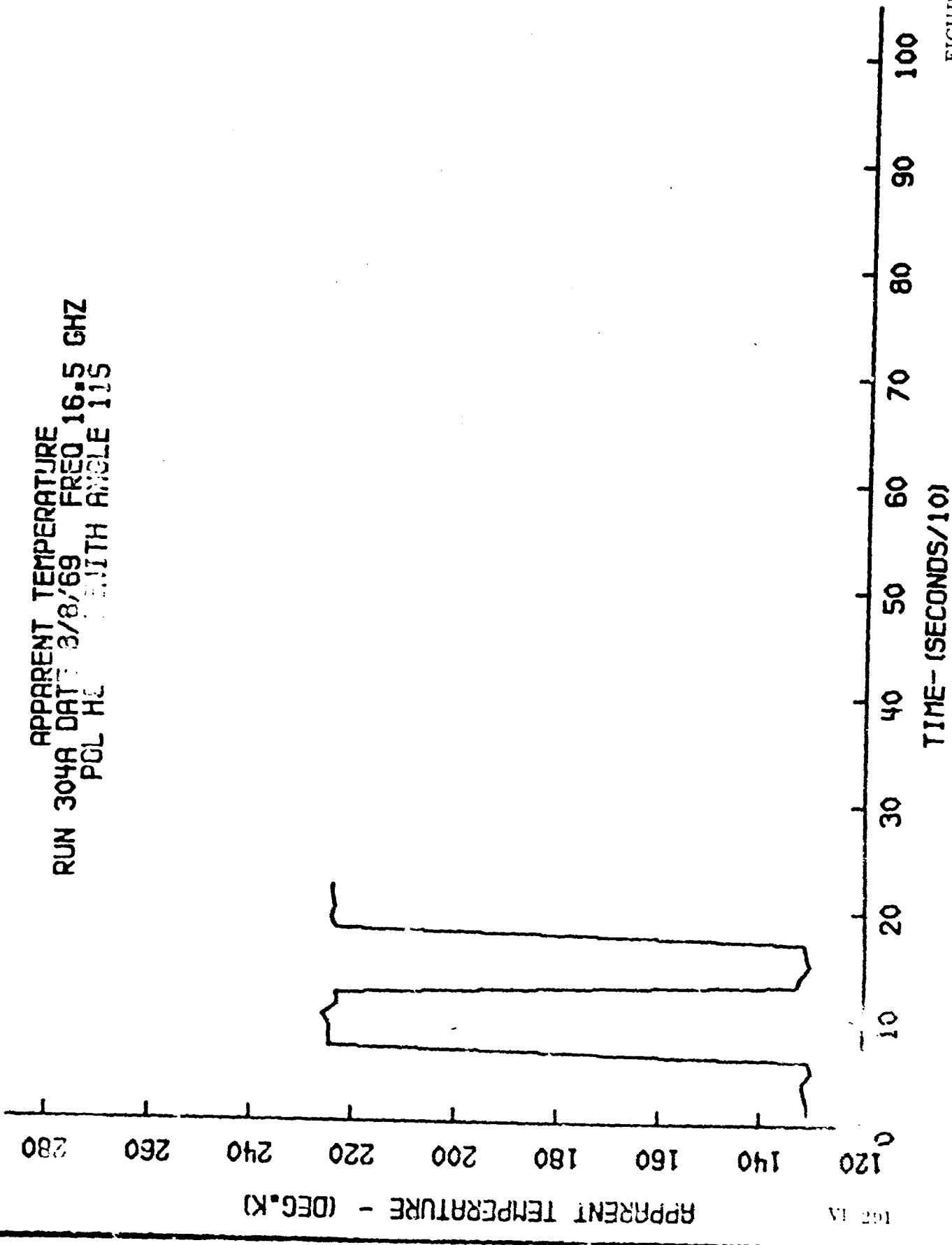


FIGURE VI-1-4

FIGURE VI-185

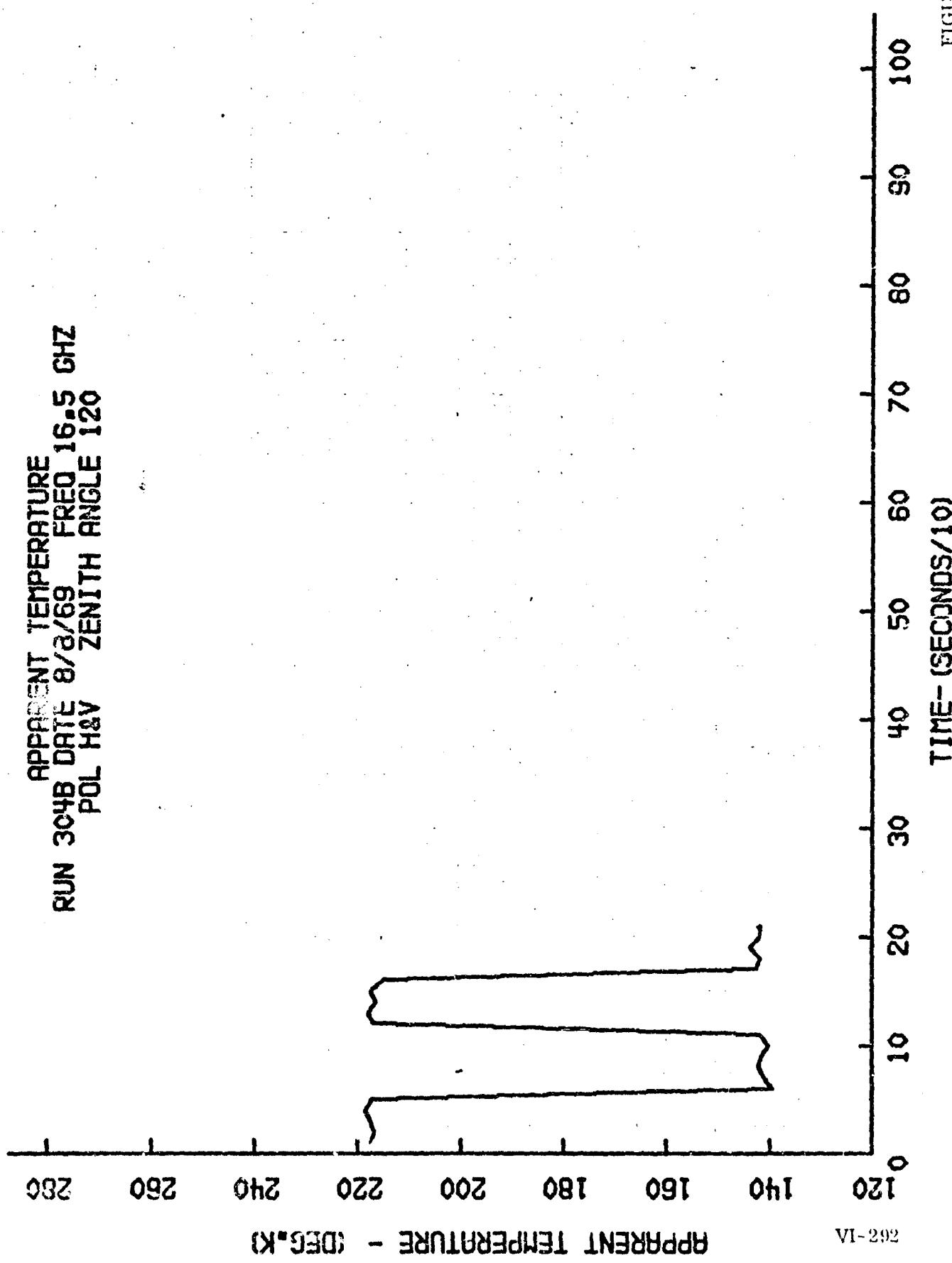
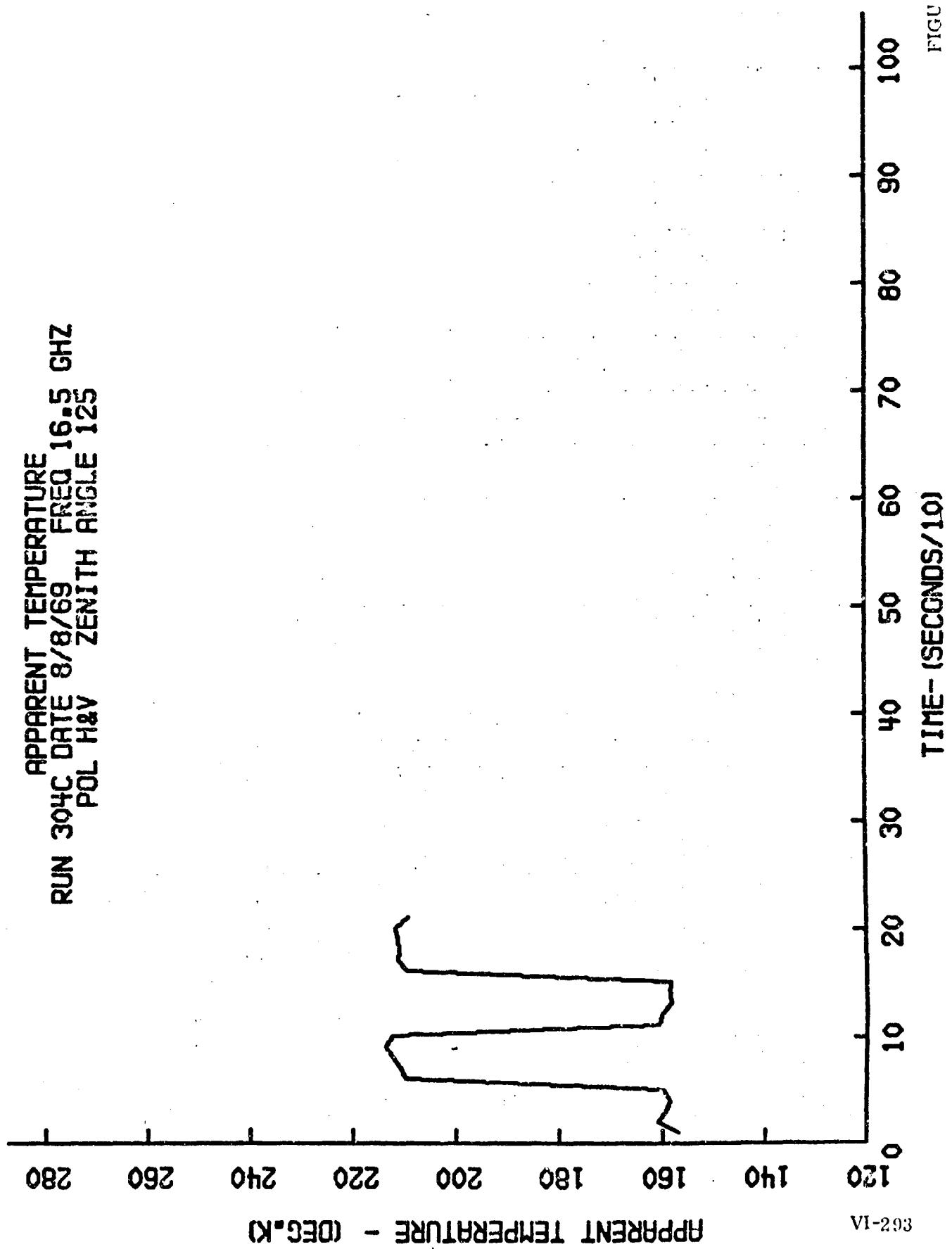
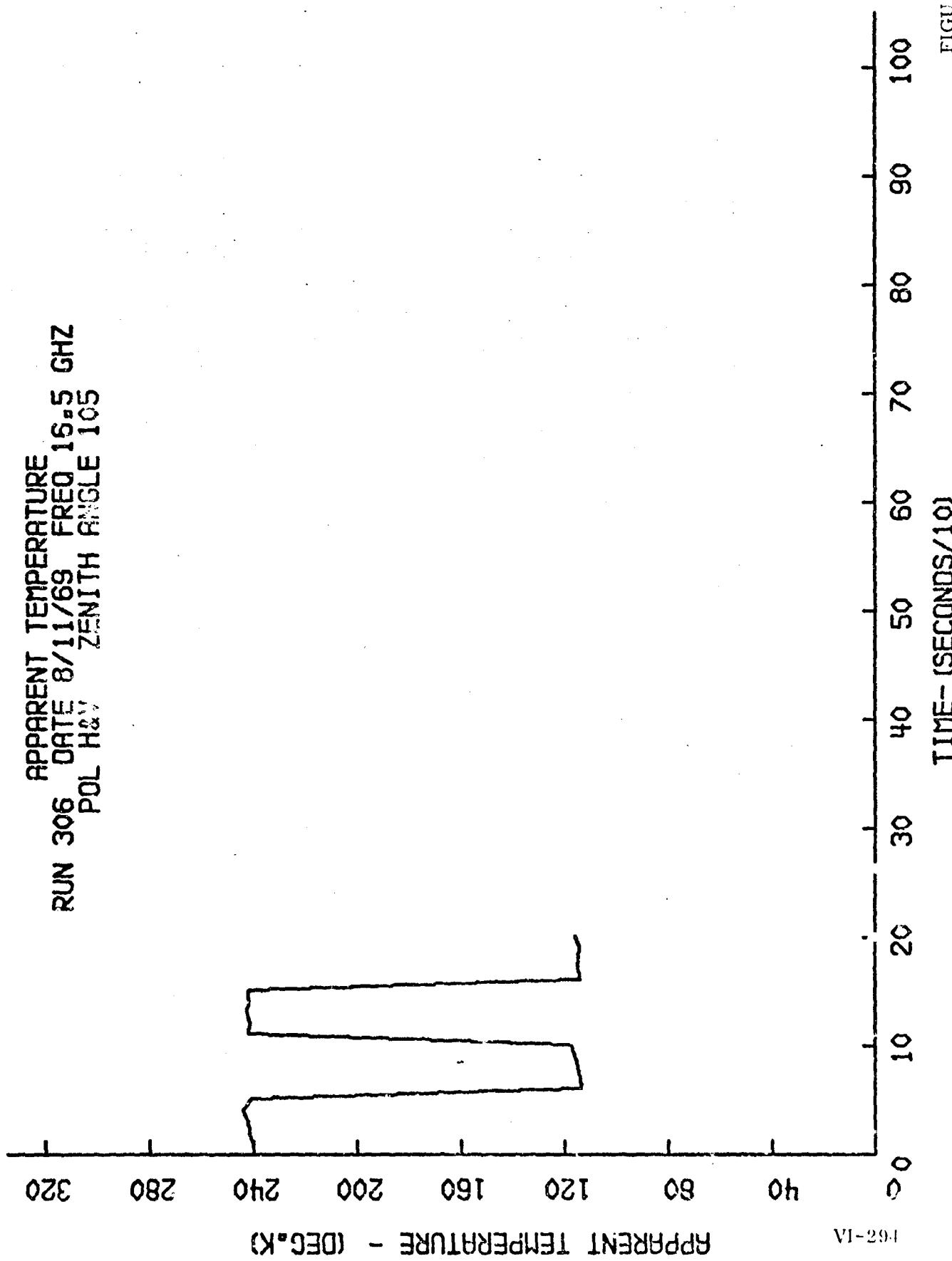


FIGURE VI-186



VA-293

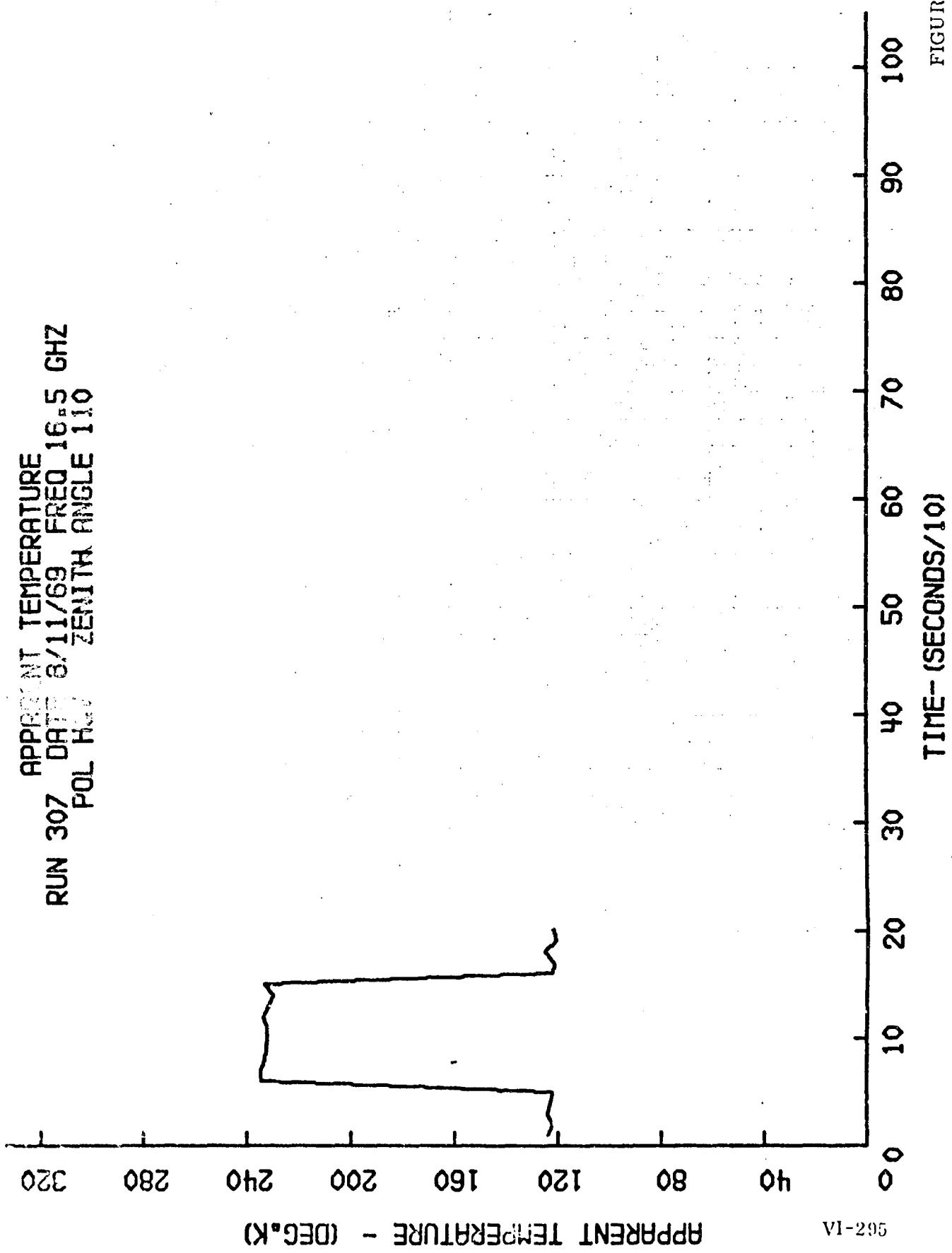
RUN 306 DATE 8/11/69 FREQ 16.5 GHZ
POL H & V ZENITH ANGLE 105



4-29-1A

FIGURE VI-187

RUN 307 DATE 6/11/69 FREQ 16.5 GHZ
APPARENT TEMP POL H ZENITH ANGLE 110

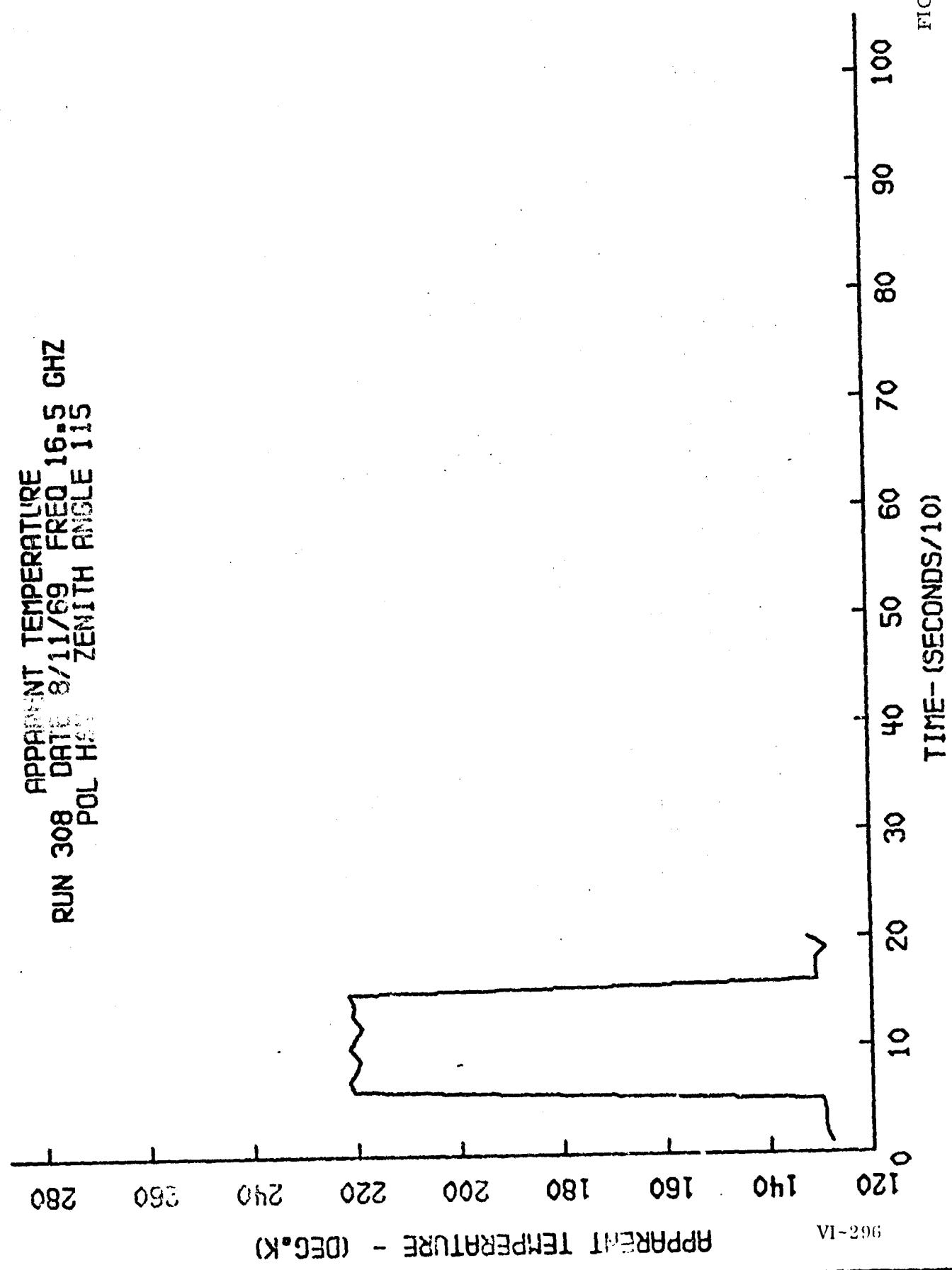


APPARENT TEMPERATURE - (DEG.K)

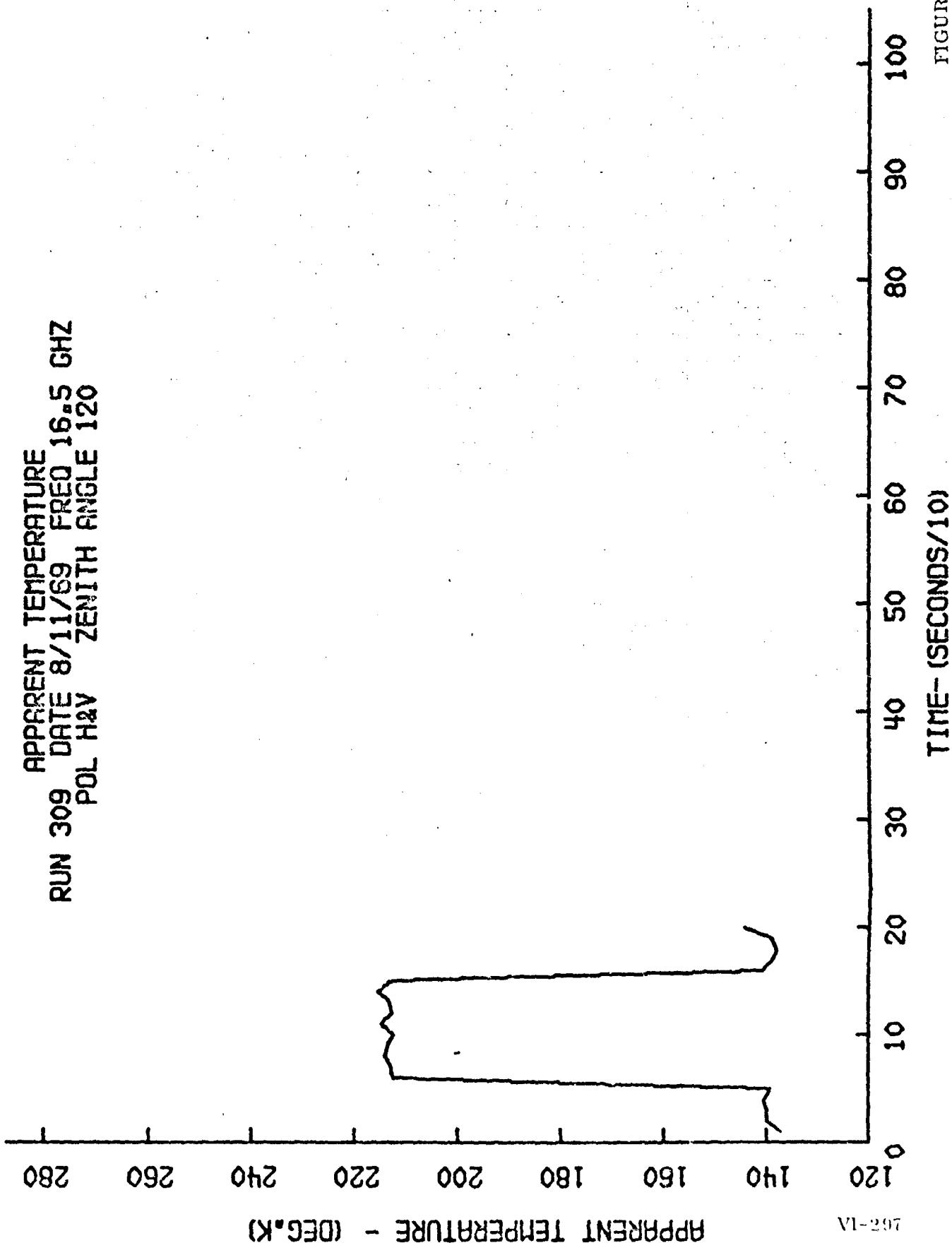
VI-295

FIGURE VI-188

FIGURE VI-189



RUN 309 DATE 8/11/69 FREQ 16.5 GHZ
APPARENT TEMPERATURE
POL H&V ZENITH ANGLE 120°

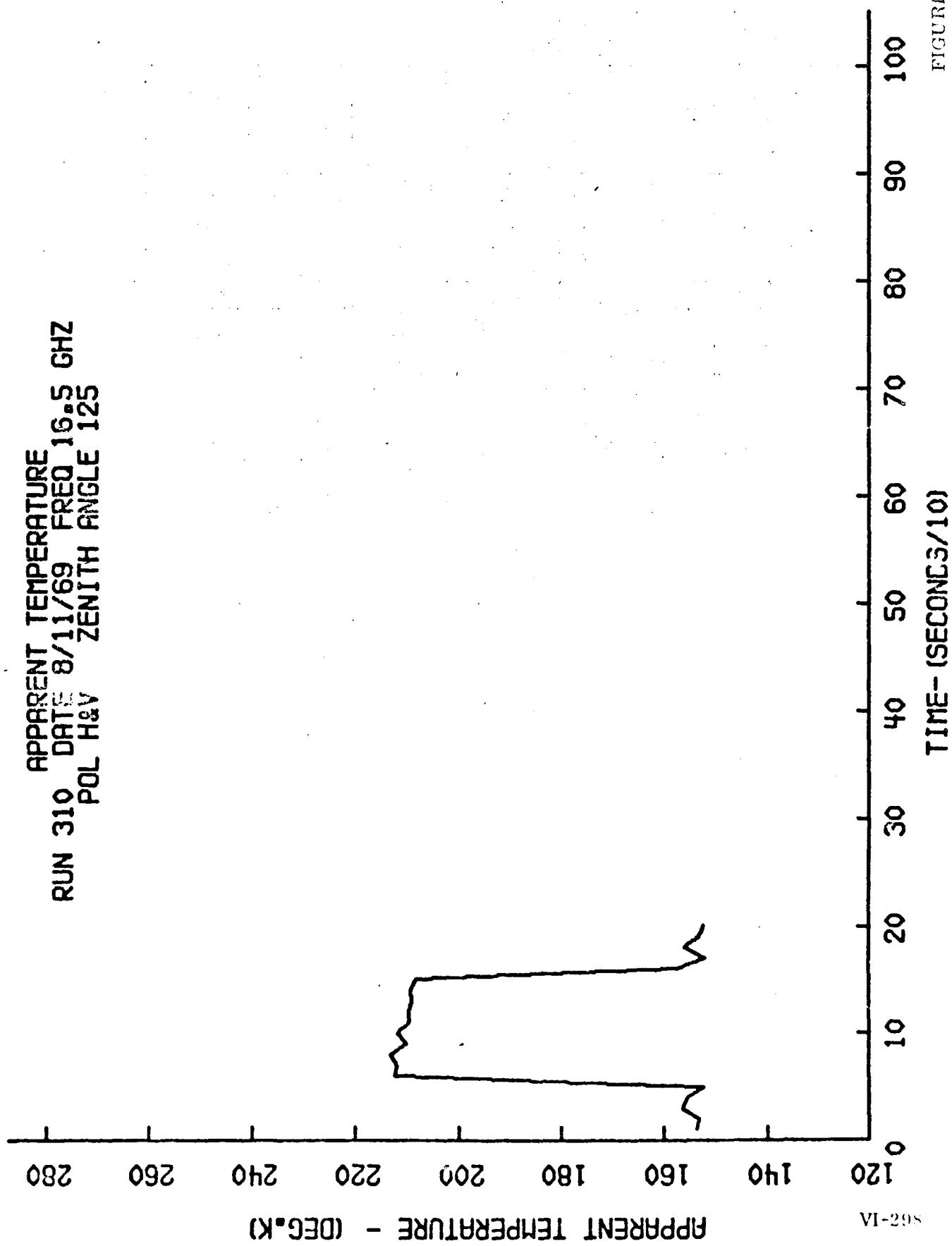


APPARENT TEMPERATURE - (DEG.K)

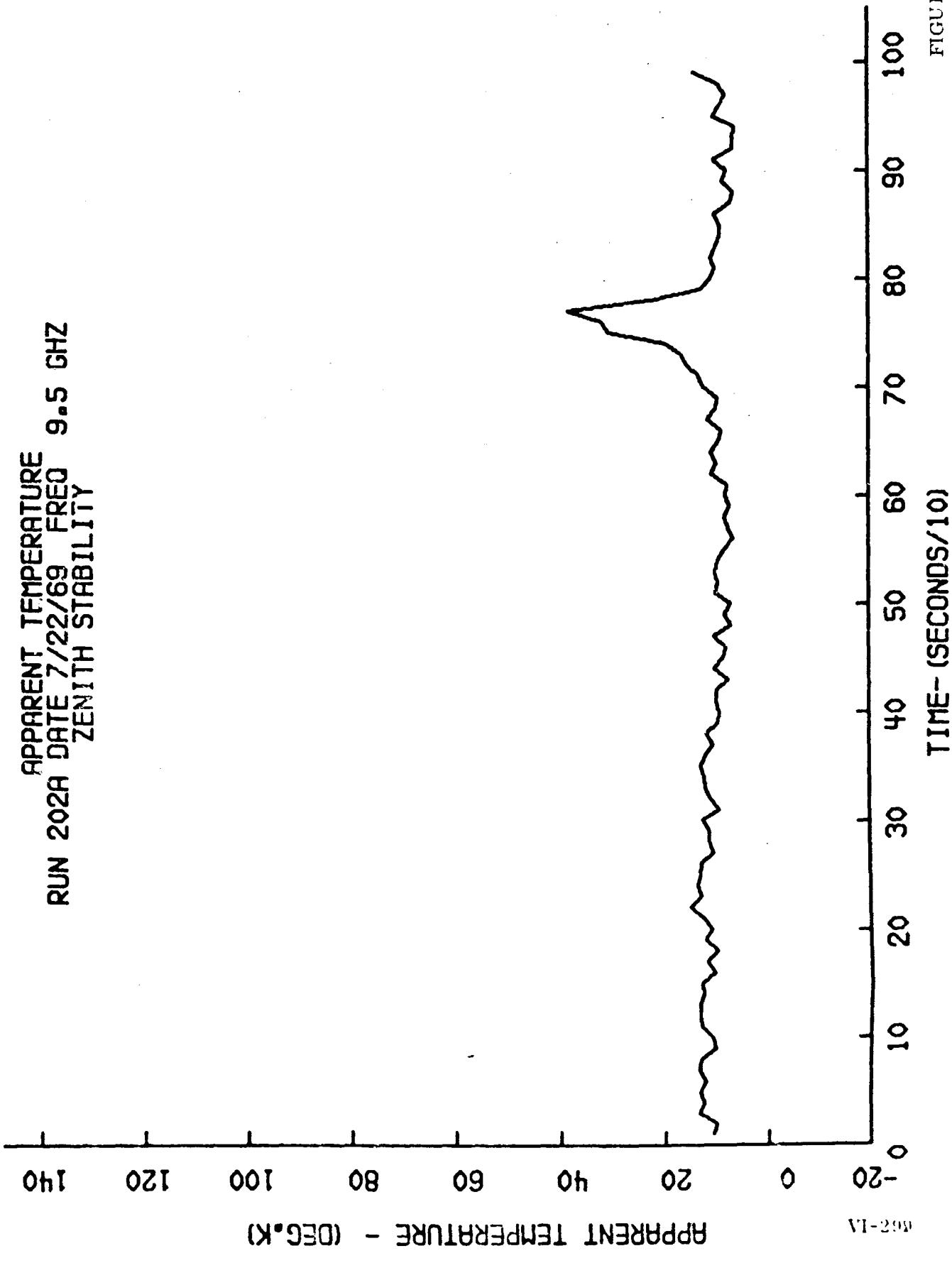
VI-297

FIGURE VI-190

RUN 310 DATE 8/11/69 FREQ 16.5 GHZ
POL H & V ZENITH ANGLE 125



APPARENT TEMPERATURE
RUN 202A DATE 7/22/69 FREQ 9.5 GHZ
ZENITH STABILITY



RUN 202B APPARENT TEMPERATURE
DATE 7/22/69 FREQ 9.5 GHZ
ZENITH STABILITY

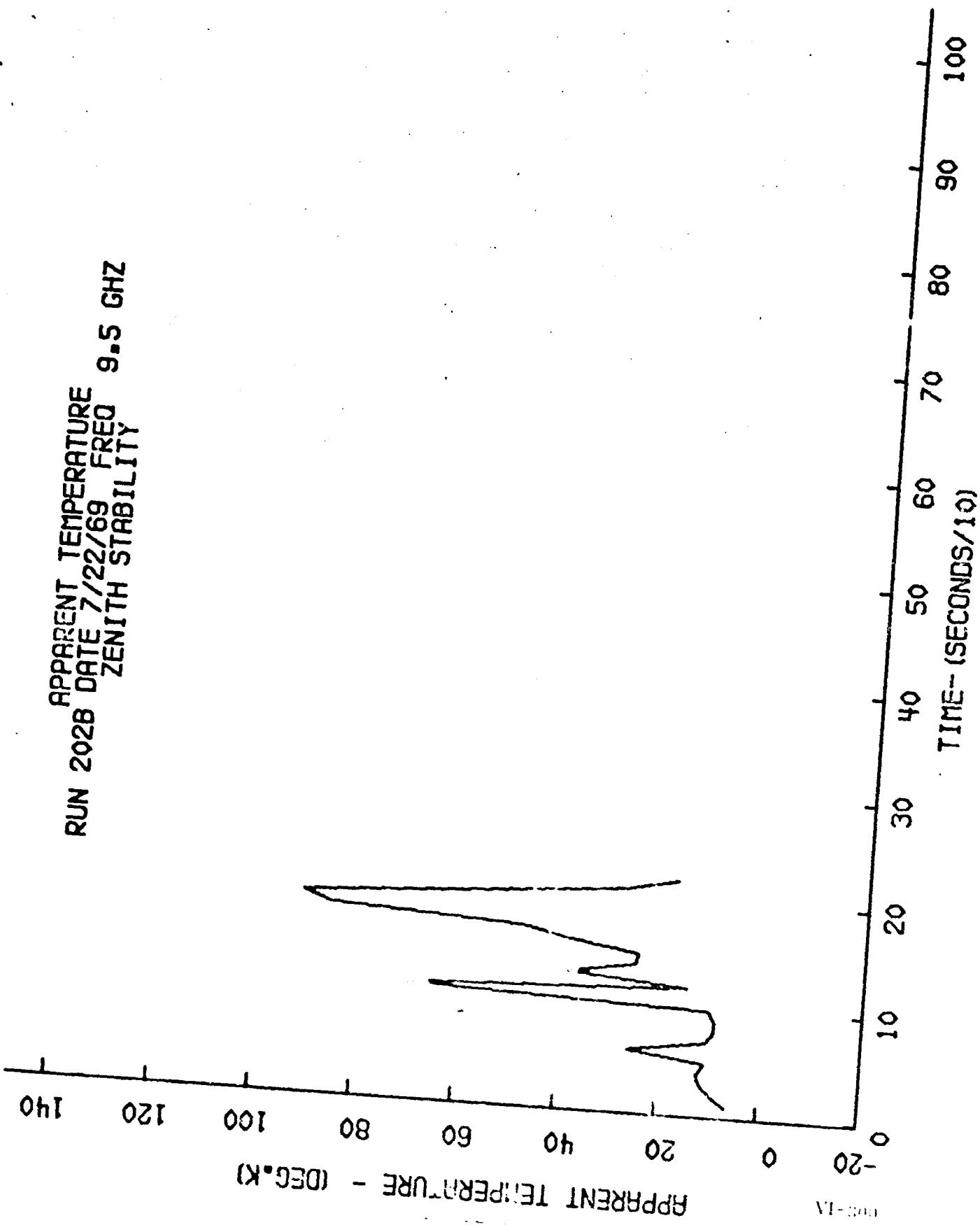


FIGURE VI-1A

FIGURE VI-193

SECTION VII

ANALYSIS OF RESULTS

The derived sea water temperatures from the 16.5 GHz vertical runs were analyzed to determine a relationship to the thermometric temperature. These vertical run temperatures are plotted in Figures VI-78 through VI-96. The nominal average thermometric temperature during the period of these measurements was about 299°K. The 299°K crossing on the curves occurs at zenith angles varying from a low of 102.9° to a high of 113.5° with an average zenith angle of 108.9°.

If the temperatures at a zenith angle of 108.9° are tabulated from all of the curves, the average of the tabulation is 299.0°K with a standard deviation of 5.19°. The deviation is caused primarily by two runs, Run 5 which was the first 16.5 GHz run made and Run 21. If these two runs were eliminated from the tabulation the average temperature would be 299.03°K with a standard deviation of 2.5°. The values observed are considered within the stability and overall accuracy limitations of the equipment that was used.

The actual value of the invariant angle may be different than the angle indicated by this relatively small amount of data. The important point is that correlation with the thermometric temperature does exist within the accuracy of the test set-up. In order to provide a check on similar data an examination was made of some measurements taken in 1966. These were sponsored by JPL (Ref 5) and were taken from a west coast location. The data from two runs, where the thermometric temperature was 288° and 292°K, was extracted and processed through the iterative computer program ROCK 3. The derived water temperature was 288° at a zenith angle of 110.7° for the first run and was 292° at a zenith angle of 121.9° for the second run.

The temperature derived from the horizontal runs, the derived emissivity from the horizontal runs and the slope of the curves of temperature as derived from the vertical runs have been examined for correlation with sea state. To aid in this examination a table has been made which lists the runs in general order of the roughness of the sea. This data is shown in Table VII-1. No distinct correlation with sea state has been found. The large variations in apparent sea water temperature for the horizontally polarized runs near the horizon are caused by the presence

of clouds on or near the horizon. The curves with the largest dips coincide with the days when there were a large amount of dark rain bearing clouds on the horizon. The distortion of the derived water temperature curves is due primarily to the lack of fine profile data on these clouds just above the horizon.

The horizontal derived emissivity curves (Figures VI-127 thru VI-141) are significantly different than the theoretical emissivity curve (Figure III 1). These curves should have the greatest sensitivity to changes in sea state. No direct correlation with sea state has been noted with these curves. Sea state correlation may have been better if equipment with higher sensitivity had been used or if the geometry of the site had permitted a wider range of viewing angles. The relatively constant deviation from specular emissivity of these curves is unexplained.

TABLE VII-1
RUNS IN ORDER OF DECREASING SEA STATE

| <u>Run</u> | <u>Date</u> | <u>Time</u> | <u>Comment</u> |
|------------|-------------|-------------|---|
| 9 | 8/1 | 1610 | Sea white caps, good 3 ft swell, 1-2 ft chop |
| 10 | 8/1 | 1637 | Sea white caps, good 3 ft swell, 1-2 ft chop |
| 11 | 8/5 | 1555 | 3 ft swell, slight wind ripple |
| 12 | 8/5 | 1628 | 2-3 ft swell, 1-2 inch wind ripple |
| 206 | 8/5 | 1649 | 2-3 ft swell, 1-2 inch wind ripple |
| 27 | 8/12 | 1621 | 2-3.5 ft swell NW, wind NE 10-15, 4-8 inch chop |
| 311 | 8/12 | 1432 | Approx. 3 ft swell |
| 26 | 8/12 | 1313 | 2-3 ft swell from NW, 8-12 inch wind ripple |
| 25 | 8/12 | 1225 | 2-3 ft swell from NW, 6-12 inch wind ripple |
| 28 | 8/12 | 1655 | 2-3 ft swell, 4-8 inch chop |
| 302 | 8/8 | 0955 | 1.5-2 ft swell, rough 12-18 inch chop |
| 303 | 8/8 | 1332 | 1.5 ft swell, 12-18 inch chop, quite rough, very few white caps |
| 23 | 8/8 | 1455 | Same as run 303 |
| 24 | 8/8 | 1531 | Same as run 303 |
| 304 | 8/8 | 1605 | Same as run 24 |
| 305 | 8/8 | 1638 | Choppy sea 2 ft |
| 14 | 8/6 | 1550 | 2-3 ft waves |
| 13 | 8/6 | 1309 | 1-2 ft swell, 8-12 inch wind chop |
| 29 | 8/12 | 1845 | 1.5-2 ft swell, 6-8 inch chop |
| 21 | 8/8 | 1132 | 1-1.5 ft sea [sea probably rougher than indicated] |
| 22 | 8/8 | 1240 | 1-1.5 ft sea [since all 8/8 rougher] |
| 313 | 8/13 | 0930 | 1-2 ft swell |
| 31 | 8/13 | 1038 | 1-2 ft swell, 15-20 ft period, 4 - 8 inch chop, wind N 5-10 |
| 32 | 8/13 | 1115 | 1-2 ft swell |
| 301 | 8/1 | 1532 | 1-1.5 ft swell and chop |
| 30 | 8/12 | 1915 | 1-1.5 ft swell, 6-8 inch chop |

TABLE VII-1 (Cont.)

| <u>Run</u> | <u>Date</u> | <u>Time</u> | <u>Comment</u> |
|------------|-------------|-------------|--|
| 312 | 8/12 | 1945 | 1-1.5 ft swell, 6-8 inch chop |
| 307 | 8/11 | 1400 | 2 ft swell, period 15-20 ft, gentle but distinct chop, some white caps |
| 306 | 8/11 | 1222 | Swell from NW, slight chop, wind NW 5-10 |
| 308 | 8/11 | 1617 | Similar to Run 306 |
| 309 | 8/11 | 1657 | Water much calmer than Run 306 |
| 17 | 8/7 | 1655 | 1 ft swell, 6-8 inch wind chop, wind S 5-10 |
| 18 | 8/7 | 1729 | 1 ft swell, 6-8 inch wind chop, wind S 5-10 |
| 19 | 8/7 | 1915 | 1 ft swell, 6-8 inch wind chop, wind S 5-10, 10 ft period |
| 20 | 8/7 | 1949 | Wind SE 10-15 |
| 15 | 8/7 | 1216 | Approx. 1 ft swell, long period 20 ft, 3-4 inch wind chop, WNW 1-2 mph |
| 16 | 8/7 | 1255 | Same as 15 |
| 201 | 7/17 | 1750 | Se approx. 1 ft (interpretation from pictures) |
| 5 | 8/1 | 1132 | Less than 1 ft swell, slight chop |
| 6 | 8/1 | 1206 | Less than 1 ft swell, slight chop |
| 310 | 8/11 | 1755 | Wind died down, water quite calm |
| 101 | 7/21 | 1445 | Vent bldg log, sea calm, wind NE 10-15 |
| 102 | 7/21 | 1510 | Vent bldg log, sea calm, wind NE 10-15 |
| 1 | 7/25 | 1248 | Sea calm, slight swell |
| 2 | 7/25 | 1345 | Same as 1 |
| 33 | 8/14 | 1010 | Sea calm, perceptible swell, very small wind ripple |
| 34 | 8/14 | 1047 | Sea calm, slight wind ripple 6 inch slow swell |
| 35 | 8/14 | 1325 | Sea calm |
| 36 | 8/14 | 1415 | Sea calm, slight swell with wind ripple |
| 7 | 8/1 | 1347 | Slight swell 3-6 inches, no chop, glassy surface |
| 8 | 8/1 | 1417 | Slight swell 3-6 inches, no chop, glassy surface |
| 202 | 7/22 | 1400 | No sea information |
| 203 | 7/22 | 1815 | No sea information |
| 204 | 7/22 | 1831 | No sea information |
| 4 | 7/24 | 2030 | No sea information |

SECTION VIII

CONCLUSIONS

There has been strong evidence presented of the correlation between vertically polarized radiometric temperatures and the thermometric temperature of sea water. The particular measurements made on this experiment at a frequency of 16.5 GHz suggest a sea state invariant angle of about 110° zenith where the r.m.s. deviation from the mean radiometric temperature was within 5°K of the thermometric temperature of the sea water. The stability, sensitivity and calibration accuracy of the radiometer together with the stability of the environment are considered to be of this magnitude. State-of-the-art radiometric equipment with improved stability and sensitivity should improve this resolution by a factor of five or ten.

No correlation with sea surface roughness (sea state) was obtained with either the vertical or horizontally polarized measurements. This may be caused by insufficient equipment sensitivity or by the viewing angle restrictions imposed by the site.

The horizontally polarized data does not appear to have a direct correlation with sea surface thermometric temperature. This negative result bears importance in those systems which contemplate using horizontally polarized radiometric measurements for determining temperature. Other frequencies or viewing angles may provide a degree of correlation, but based on the inference here this should be validated by other tests before implementation.

The applicability of radiometric measurements by an aircraft or satellite, particularly in the area of surface temperature measurement is feasible. The viewing angle implied by this experiment would not be optimum for a spacecraft but other frequencies may provide other optimum viewing angles.

SECTION IX

RECOMMENDATIONS

Based on the data and its analysis the following recommendations are made for possible future work:

- 1.) A theoretical investigation should be made, using a relatively sophisticated model of the sea surface, to determine the interrelationship of frequency, viewing angle, sea state and polarization. This should result in a theoretical description of the dependency of a sea state invariant angle on frequency.
- 2.) Field tests at frequencies other than 16.5 GHz should be conducted to verify the theory developed in the above.
- 3.) Representative field test data should be obtained over a full range of viewing angles. This will require a site where angles close to nadir can be observed.
- 4.) The effects of pollutants, froth and water contaminants should be theoretically analyzed and subsequently introduced in field experiments under controlled conditions.
- 5.) The equipment sensitivity for radiometric measurements of the sea surface should be the best the state-of-the-art offers. Sensitivities of 0.3^0K for a 0.1 second integration time should be attainable up to frequencies of 30 to 35 GHz, and 0.5^0K should be attainable up to 60 GHz. Integration times as small as practical should be used for the critical data measurements. Longer integration times for smoothing may be introduced by computer processing during the data reduction.
- 6.) The final recommendation is general in nature, but most important for any field tests. Adequate auxillary instrumentation must be a prime requisite for any program. This is necessary to enable complete and proper interpretation of prime radiometric data. The water thermometric temperature measuring system must be well designed. It must be sturdy to withstand rough seas yet light enough to float on the surface of the water. The temperature sensors must be waterproof. The system used in this experiment was good, but water leakage was a problem in some of the thermistor probes.

REFERENCES

- 1.) A. Stogryn, IEEE Transactions on Antenna and Propagation, Vol. AP-15 No. 2, March 1967, pp. 278.
- 2.) C. Braun and Donald Mercer, The Measurement of Sea Surface Temperature With an Infrared Radiometer, Internal Report NESC, ESSA.
- 3.) J. B. Hasted, "The Dielectric Properties of Water", Progress in Dielectrics, vol. 3, pp. 101-149 (1961).
- 4.) A. von Hippel, "The Dielectric Relaxation Spectra of Water, Ice and Aqueous Solutions and Their Interpretation", Technical Reports 1 and 2, Contract N00014-67A-0204-0003, Lab. for Insulation Res, MIT (April 1967).
- 5.) Technical Report for Microwave Radiometer Field Measurement Program, Raytheon Report FR-66-293, Contract 951-265, (August 31, 1966).

APPENDIX A

THEORETICAL EMISSIVITY OF SPECULAR SEA WATER

Applying Kirchoff's law, the emissivity of a specular surface can be derived from the reflectivity

$$\epsilon = 1 - \rho \quad (1)$$

The reflectivity for horizontally polarized waves is given by the Fresnel formula:

$$\rho_h = \left[\frac{\cos\phi - e^{1/2} \cos\theta}{\cos\phi + e^{1/2} \cos\theta} \right]^2 \quad (2)$$

and likewise for a vertically polarized wave:

$$\rho_v = \left[\frac{e \cos\phi - e^{1/2} \cos\theta}{e \cos\phi + e^{1/2} \cos\theta} \right]^2 \quad (3)$$

where ϕ = incidence angle

θ = angle of transmitted beam with respect to normal

$e = e' - je''$ = complex dielectric permittivity

Using Snell's law:

$$e^{1/2} \sin\theta = \sin\phi \quad (4)$$

Introducing the polar form for the complex number

$$e \cos^2\theta = e - \sin^2\phi = r e^{-j\gamma} \quad (5)$$

The polar quantities can be calculated explicitly as follows:

$$r = [(e' - \sin^2\phi)^2 + (e'')^2]^{1/2} \quad (6)$$

$$\gamma = \tan^{-1} \left[\frac{e''}{e' - \sin^2\phi} \right] \quad (7)$$

Using the definition in (5) the absolute values in equation (2) and (3) can be evaluated. Substituting these results into equation (1) yields after some manipulation:

$$\epsilon_h = \frac{4\cos\phi r^{1/2} \cos(\gamma/2)}{[\cos\phi + r^{1/2} \cos(\gamma/2)]^2 + r \sin^2(\gamma/2)} \quad (8)$$

$$\epsilon_v = \frac{4\cos\phi r^{1/2} [\cos(\gamma/2) e' + \sin(\gamma/2) e'']}{[e' \cos\phi + r^{1/2} \cos(\gamma/2)]^2 + [e'' \cos\phi + r^{1/2} \sin(\gamma/2)]^2} \quad (9)$$

Some simplification of (8) and (9) can be accomplished by the introduction of two parameters:

$$a = r^{1/2} \cos(\gamma/2) \quad (10)$$

$$b = r^{1/2} \sin(\gamma/2) \quad (11)$$

Then (8) and (9) become:

$$\epsilon_h = \frac{4a\cos\phi}{(\cos\phi + a)^2 + b^2} \quad (12)$$

$$\epsilon_v = \frac{4\cos\phi (ae' + be'')}{(e' \cos\phi + a)^2 + (e'' \cos\phi + b)^2} \quad (13)$$

From equation (5), at normal incidence

$$e = r^{-j\gamma}$$

Thus γ is defined as the dielectric loss angle and "a" is the refractive index and "b" is often called the "absorption" coefficient.

APPENDIX B

DIELECTRIC PERMITTIVITY OF SEA WATER

Hasted (Ref 3) and Von Hippel (Ref 4) have reviewed the dielectric properties of pure water. According to the latter, it is accurate to consider only the dipole relaxation through the microwave region, thus only bipolar absorption will be considered. A single relaxation time is considered sufficient to explain the water absorption spectrum. This time is sufficiently short to place the relaxation dispersion region of liquid water in the microwave region. The Debye formula then gives the frequency dependency of the dielectric permittivity:

$$\epsilon' = \epsilon_{\infty} + \frac{\epsilon_0 - \epsilon_{\infty}}{1 + (\nu \lambda_s)^2} \quad (1)$$

$$\epsilon'' = \frac{(\epsilon_0 - \epsilon_{\infty}) \nu \lambda_s}{1 + (\nu \lambda_s)^2} + \frac{\sigma}{c \nu \epsilon_0} \quad (2)$$

where

ϵ' = real component of dielectric permittivity

ϵ'' = imaginary component of dielectric permittivity

ν = wave number (cm^{-1})

λ_s = relaxation wavelength (cm)

ϵ_0 = static permittivity

ϵ_{∞} = high frequency limit of permittivity

σ = conductivity (mhos/meter)

c = velocity of light (cm/seconds)

$\epsilon_0 = \text{permittivity of vacuum} = \frac{10}{36\pi}^{-9}$

since

$$\nu \approx \frac{\omega}{c}$$

$$c = \frac{\lambda}{\tau}$$

where

$$\omega = 2\pi f$$

τ = relaxation time (seconds)

we can simplify equation (1) and (2) as follows:

$$e' = e_{\infty} + \frac{e_0 - e_{\infty}}{1 + (\omega\tau)^2}$$

$$e'' = \frac{\omega\tau(e_0 - e_{\infty})}{1 + (\omega\tau)^2} + \frac{\sigma}{\omega e_0}$$

e_0 , τ , and σ can be approximated as the product of two second order polynomials of the form:

$$x = (b_2S^2 + b_1S + b_0)(c_2T^2 + c_1T + c_0)$$

or

$$x = a_0 + a_1T + a_2S + a_3T^2 + a_4S^2 + a_5TS + a_6T^2S + a_7TS^2 + a_8T^2S^2 \quad (3)$$

where

S = Salinity (Parts per 1000)

T = Temperature

a, b and c are constants

x = e_0 , τ or σ

Table 1 tabulates the coefficients for the variables of the expanded equation based on (3) above.

TABLE B-1

| Variable | Constant | Parameters | |
|----------|----------|-------------------------------|-------------------------------|
| | | τ | e_c |
| T | a_0 | $0.19289557 \times 10^{-10}$ | $0.88194946 \times 10^{-02}$ |
| | a_1 | $-0.68020489 \times 10^{-12}$ | $-0.40348652 \times 10^{-00}$ |
| S | a_2 | $-0.1136996 \times 10^{-12}$ | $-0.43917148 \times 10^{-00}$ |
| | a_3 | $0.95864633 \times 10^{-14}$ | $0.65923705 \times 10^{-03}$ |
| T^2 | a_4 | $0.11417367 \times 10^{-14}$ | $0.16737911 \times 10^{-02}$ |
| S^2 | a_5 | $0.58628615 \times 10^{-02}$ | $0.43269204 \times 10^{-02}$ |
| | a_6 | $-0.87595500 \times 10^{-16}$ | $-0.92285569 \times 10^{-05}$ |
| TS | a_7 | $-0.54576833 \times 10^{-16}$ | $-0.42856433 \times 10^{-04}$ |
| T^2S | a_8 | $0.82521420 \times 10^{-18}$ | $0.44409604 \times 10^{-07}$ |
| T^2S^2 | | | $0.39287711 \times 10^{-06}$ |

APPENDIX C

SEA WATER TEMPERATURE DERIVIATION METHODS

There have been several methods proposed for radiometric sensing of the sea water temperature and conversion of this radiometric temperature to actual temperature. Several of these methods will be outlined in the following sections.

A. Ratio Method

The brightness temperature has been defined in Section III in terms of a basic radiometric formula. This formula is repeated here for reference.

$$T_{bh} = \epsilon_\phi T_w + (1 - \epsilon_\phi) T_{s\theta} \quad (1)$$

where

T_s = sky temperature

ϵ = emissivity

ϕ = observation angle

θ = $180^\circ - \phi$

The horizontally and vertically polarized brightness temperatures as defined by equation (C-1) can be expressed as a ratio:

$$\frac{T_{bh}}{T_{bv}} = \frac{\epsilon_{h\phi} T_w + (1 - \epsilon_{h\phi}) T_{s\theta}}{\epsilon_{v\phi} T_w + (1 - \epsilon_{v\phi}) T_{s\theta}} \quad (2)$$

$$\frac{T_{bh}}{T_{bv}} = \frac{\epsilon_{h\phi} \left(\frac{T_w}{T_{s\theta}} - 1 \right) + 1}{\epsilon_{v\phi} \left(\frac{T_w}{T_{s\theta}} - 1 \right) + 1} \quad (3)$$

This expression involves four unknowns, namely $\epsilon_{h\phi}$, $\epsilon_{v\phi}$, T_w and $T_{s\theta}$, and can be simplified to two unknowns by introducing a factor k in the equation as follows:

$$\frac{T_{bh}}{T_{vh}} = \frac{\epsilon_{h\phi} k + 1}{\epsilon_{v\phi} k + 1} \quad (4)$$

in which,

$$k = \left[\frac{T_w}{T_{s\theta}} - 1 \right]$$

In Appendix A, the formulas for ϵ_v and ϵ_h are developed, these are expressed as:

$$\epsilon_h = \frac{4a\cos\phi}{(\cos\phi + a)^2 + b^2} \quad (5)$$

$$\epsilon_v = \frac{4(ac' + be'')\cos\phi}{(e'\cos\phi + a)^2 + (e''\cos\phi + b)^2} \quad (6)$$

Both parameters "a" and "b" are functions of permittivity and incidence angle. In practice both "a" and "b" will vary from their theoretical values for a specular surface. The value of "b" has less of a variation from theoretical, therefore we set values of e' , e'' and b based on an assumed initial value of sea water temperature. Substituting (5) and (6) in equation (4) we can now solve for "a". Using this derived value of "a" which carries information on the actual temperature of the water, we calculate ϵ_v . The true sea water temperature can now be derived from the relation:

$$T_w = \frac{T_{bv} - (1 - \epsilon_v\phi)T_{s\phi}}{\epsilon_v\phi}$$

The vertical component of emissivity, ϵ_v , varies with frequency, angle ϕ and temperature T . The frequency is known and the angle is known for a calm sea and can be approximated for a rough sea. We are attempting to derive the temperature T . In using the ratio T_{bh}/T_{bv} to obtain the parameter "a", and hence ϵ_v , we are in some way trying to correlate T and ϵ_v . The assumption is that different T values will lead to specific ratio values, hence to "a" and finally to a unique ϵ_v . In order for this sequence to be meaningful we must first have some sensitivity in the ratio T_{bh}/T_{bv} to changes in T . We can examine this point by considering the right-hand side of equation (4).

we have

$$R = \frac{T_{bh}}{T_{bv}} = \frac{k\epsilon_v + 1}{k\epsilon_v + 1}$$

where

$$k = \left[\frac{T_w}{T_{s\theta}} - 1 \right]$$

In this method, the temperature dependence of the ratio T_{bh}/T_{bv} is in ϵ_v and ϵ_h , which in turn reflect a temperature dependence through e' and e'' . Parameter k is usually set to a value representing an initial assumption for T and $T_{s\phi}$. This

Procedure is based on the correct assumption that a poor choice in k has small consequence on derived emissivity. Specifically, for k ranging from 15.0 to 40.0, the resulting calculated ϵ changes by about 0.01.

A computer program has been employed to calculate the theoretical values of ϵ_v , ϵ_h and the ratio T_{bh}/T_{bv} (in which $k = 40$ corresponding to a temperature T of 280.0 degrees Kelvin and a $T_{s\phi}$ of 7.0 degrees Kelvin) for angles ϕ varying from zero to 70 degrees, and for sets of e' and e'' representing ocean salinity of 30 parts/thousand, and a temperature range of zero to 30°C. Assuming that these theoretical values are representative of the actual emissivities and the ratio T_{bh}/T_{bv} , it is possible to make a number of interesting observations:

1. ϵ_v and ϵ_h vary very slightly with temperature. At $\phi = 60$ degrees, we have the values listed below:

TABLE C-1

| T | ϵ_v | ϵ_h | R |
|-----|--------------|--------------|-------|
| 0°C | .6233 | .2159 | .3716 |
| 10 | .6151 | .2115 | .3695 |
| 20 | .6132 | .2101 | .3639 |
| 30 | .6159 | .2117 | .3693 |

From the above, we can see that, over a 10°C interval (i.e. 10° - 20°) ϵ_v changes by .0019, or about .0002/°C. Also, ϵ_v and ϵ_h seem to exhibit a minimum near T = 20°C and therefore T is a double-valued function of ϵ . In effect, in trying to obtain a value for ϵ_v , useable in equation (1), we are trying to guess in a very narrow range - this guess has a built-in ambiguity in that there are two temperatures for each value of ϵ_v , i.e., we must somehow know on which side of the minimum our temperature is located. This can be difficult since the minimum is at a commonly encountered temperature.

2. We have noted the difficulty involved in obtaining a value of ϵ_v corresponding to a specific T. We will now examine the method used for obtaining ϵ_v . Table C-1 also lists corresponding values of the ratio T_{bh}/T_{bv} - these are theoretical values and represent the manner in which we would expect that ratio to vary, if we vary the temperature of the sea surface. Three observations can be made at this point:

- i) The variation with temperature is slight, i.e., over a 10°C range we have a change in the ratio of .0006, or about .00006/°C. This number is literally swamped by the temperature sensitivity of the radiometer used in the measurements.

- ii) T is a double-valued function of R . Again, the minimum is near 20°C and we, therefore, have a difficult time knowing which T corresponds to a given R .
- iii) T_{bh} has a higher theoretical dependency on sea state. Thus, any variation in T_{bh} , due to sea state, will affect the ratio T_{bh}/T_{bv} and will in turn influence the final water temperature calculation.

The above numbers and ensuing discussion are based on data for 9.5 GHz (even though data for ϵ' and ϵ'' is actually for 9.3 GHz, which is sufficiently close for our purposes) and an incidence angle, ϕ , of 60 degrees. The nature of the data is similar at other values of ϕ . For reference purposes, similar tables are presented below for $\phi = 40$ and 20 degrees.

Table C-2 $\phi = 40^{\circ}$

| T | V | H | R |
|-----|-------|-------|-------|
| 0°C | .4699 | .3110 | .6790 |
| 10 | .4620 | .3051 | .6777 |
| 20 | .4600 | .3035 | .6778 |

Table C-3 $\phi = 20^{\circ}$

| T | V | H | R |
|-----|-------|-------|-------|
| 0°C | .4038 | .3667 | .9134 |
| 10 | .3966 | .3600 | .9131 |
| 20 | .3947 | .3582 | .9130 |
| 30 | .3968 | .3601 | .9131 |

4. Conclusions

The analysis presented in the preceding sections argues against the meaningfulness of using the method originally proposed for obtaining ϵ . The problem revolves primarily about the fact that ϵ_v and ϵ_h vary very slightly over the temperature of interest for sea water, with the resulting effect that the ratio T_{bh}/T_{bv} contains very little retrievable information with regard to temperature. What it does contain is, in part, indicated by a plot of the ratio versus ϕ . The plot shown in Figure C-1 is based on a theoretical expression for the ratio, at a fixed value of k . We find in Figure C-1 that, for ϕ between 25 and 75 degrees, the relationship between R and ϕ follows an approximate straight line, with a slope of 62.5 degrees per unit change in

the ratio T_{bh}/T_{bv} . A 6.25 change in ϕ will cause a 0.1 change in the ratio. We note that a 0.1 change in the ratio is actually quite large; it represents, roughly, a 25°K change in the final derived value of T , when everything else is held constant. Thus, the angular dependence completely overshadows the slight temperature dependence.

A rough sea results in brightness temperature samples over a cone of angles around the antenna beam nadir angle at which it is viewed, and hence, is expected to affect the ratio T_{bh}/T_{bv} quite markedly.

It appears that this method amounts to nothing less than the derivation of an ϵ which reflects such information as the angle of observation (which is known in any case) and errors in measured T_b which we would like to avoid.

B. Low ϕ Analysis

At low values of incidence angles the values of ϵ_h and ϵ_v vary less as a function of angle than at high incidence angles. This is readily apparent if one refers to Figure III-1. Using the equations developed in Appendix A, we can express ϵ_v and ϵ_h as a function of temperature T_w , hence we have T_{bh} and T_{bv} as functions of T_w .

From equation (1) we have:

$$T_{bv} = \epsilon_v T_w + (1 - \epsilon_v) T_s \quad (7)$$

rearranging terms

$$T_{bv} = \epsilon_v (T_w - T_s) + T_s \quad (8)$$

substituting the expression, from Appendix A, for ϵ_v

$$T_{bv} = \frac{4\cos\phi (ae' + be'')}{(e' \cos\phi + a)^2 + (e'' \cos\phi + b)^2} (T_w - T_s) + T_s \quad (9)$$

and similarly $T_{bh} = \frac{4a\cos\phi}{(\cos\phi + a^2) + b^2} (T_w - T_s) + T_s \quad (10)$

Assuming that the right hand side of equations (9) and (10) are exact expressions of the measured brightness temperature T_b , we can then reduce our problem to that of determining what value of T_w will give the data value T_b .

Two difficulties in this approach are:

1. The theoretical expression for T_{bv} (or T_{bh}) does not in fact correspond to data T_{bv} in a sufficiently sensitive fashion.

2. T_{bv} (or T_{bh}) is not sufficiently sensitive to T_w .

The essential point in this method is the manner in which we obtain a value for ϵ_v . The value of ϵ_v should be determined over a range of incidence angles where the effects of sea state are minimized. As the sea surface roughens, the effective angle over which the radiometer is viewing the water surface is a weighted sampling of a cone whose axis lies on the nominally defined incidence angle. Therefore, for a sea surface which is not flat, we should really apply equation (9) or (10) not at one angle ϕ , but should average over a cone of angles appropriately weighted to consider wave height and period, and the duration of the measurement. If however, ϵ_v and T_s varied only slightly over the cone, as they do for low incidence angles, equations (9) and (10) would be accurate to within that slight variation. The range of incidence angles that might be considered in this method would range from 0° to 40° or 50° corresponding to zenith angles from 130° or 140° to 180° .

The underlying restriction on this method with regard to this particular field experiment is the observation angles required for implementation. Site restrictions confined the water observation to zenith angles from 90° to about 130° .

C. Invariant Angle Analysis

If one assumes that there is a range of zenith angles over which the radiometric temperature is invariant with sea state, then the specular equation for brightness temperature would be most nearly correct at these angles. The brightness temperature has previously been expressed as a function of temperature in equation (9). That equation is repeated here for reference.

$$T_{bv} = \frac{4\cos\phi (ae' + be'')}{(e' \cos\phi + a)^2 + (e'' \cos\phi + b)^2} (T_w - T_s) + T_s \quad (9)$$

There will be a unique value of sea water temperature that satisfies the measured values of T_{bv} and T_s . This unique value will be equal to the thermometric temperature of the water at an invariant angle. At angles other than invariant the derived value of water temperature will depart from the thermometric value. It would further be deduced that the deviation from the thermometric temperature (i.e. the slope of the derived water temperature) would be dependent upon sea state. The derivation of water temperature from equation (9) is accomplished by iteration using a computer. An initial value of T_w is assumed and a , b , e' and e'' are computed for this temperature using the equations developed in Appendix A and B. Equation (9) is then used to calculate the value of T_{bv} . This calculated value is then compared to the measured value of T_{bv} . If the two are not in agreement to within $\pm 1^\circ$, the value of T_w is adjusted to a new value based on the following formula:

$$T_{w\text{new}} = \frac{T_{w\text{old}} + T_{bv} - (1 - \epsilon)T_s}{2}$$

This iteration is repeated until agreement in the calculated and measured values of T_{bv} is reached. This was the method used in reducing the vertically polarized measurements in this program.

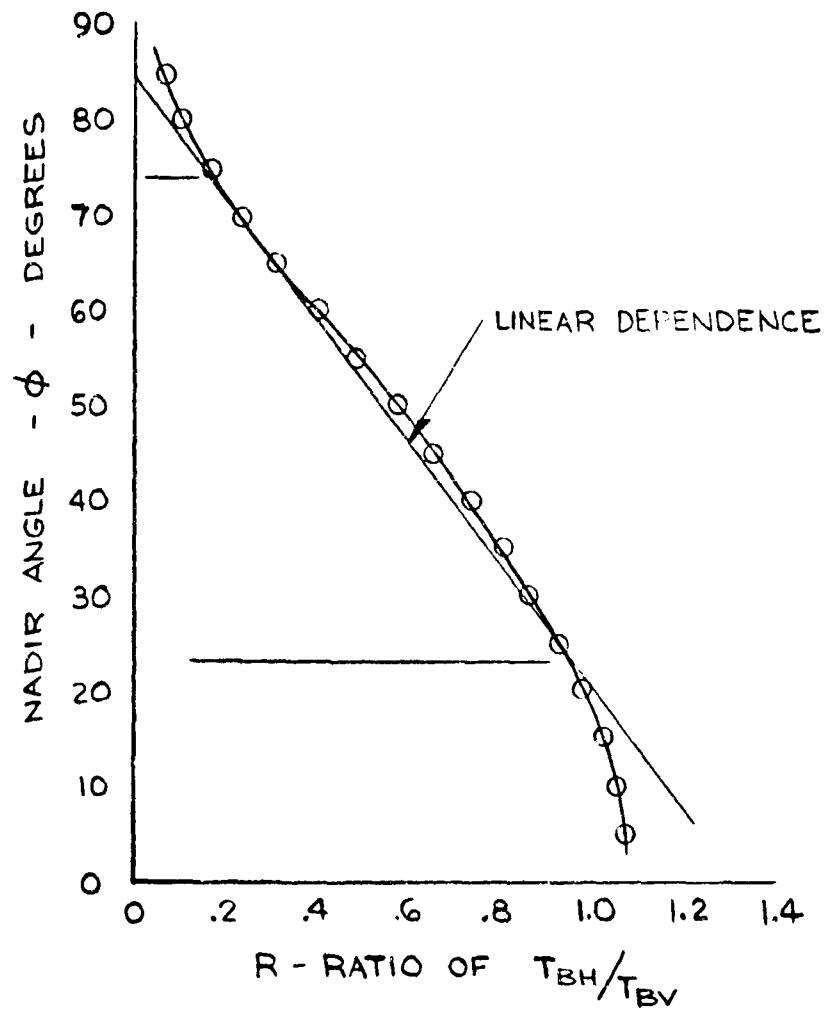


Figure C-1. BRIGHTNESS TEMPERATURE RATIO VERSUS NADIR ANGLE

APPENDIX D

ANTENNA PATTERN CORRECTION

A. Geometry

The gain patterns of microwave and millimeter-wave antennas is simply the manifestation of diffraction of electromagnetic waves by a finite aperture. Most of the power received by the antenna is contained in the main lobe of the diffraction pattern. The remaining power is received via the side and back lobes.

If one were investigating astronomical radio sources of very small angular extent, it would be important to remove the effect of the main lobe "pattern". However, for extended sources, such as the atmosphere or sea surface, the brightness temperature variation within the main lobe half-width is not sufficient to necessitate the removal of the main lobe effects. The following discussion will concentrate on the correction for side and back lobe effects.

The geometry of the situation is indicated in Figure (D-1). Environmental temperatures are given in the $(\hat{x}, \hat{y}, \hat{z})$ coordinate system where the unit vector \hat{z} is oriented in the zenith direction. The antenna axis is inclined at angle θ_0 to the zenith and defines the unit vector \hat{z}' . If the \hat{x}' direction is chosen to coincide with the \hat{x} direction, the set $(\hat{x}', \hat{y}', \hat{z}')$ defines Cartesian coordinates in the antenna-centered frame.

Polar angles in either frame are defined with respect to the z axes, while azimuthal angles are defined with respect to the x axes. Figure D-2 shows the angular coordinates of a pencil beam in both environment and antenna-centered frames.

B. Analytical Approach

The apparent (measured) temperature seen by an antenna oriented at a zenith angle θ_0 is given by

$$T_a(\theta_0) = \frac{\int T_b(\theta, \phi) g(\theta', \phi') d\Omega'}{\int g(\theta', \phi') d\Omega'} \quad (D-1)$$

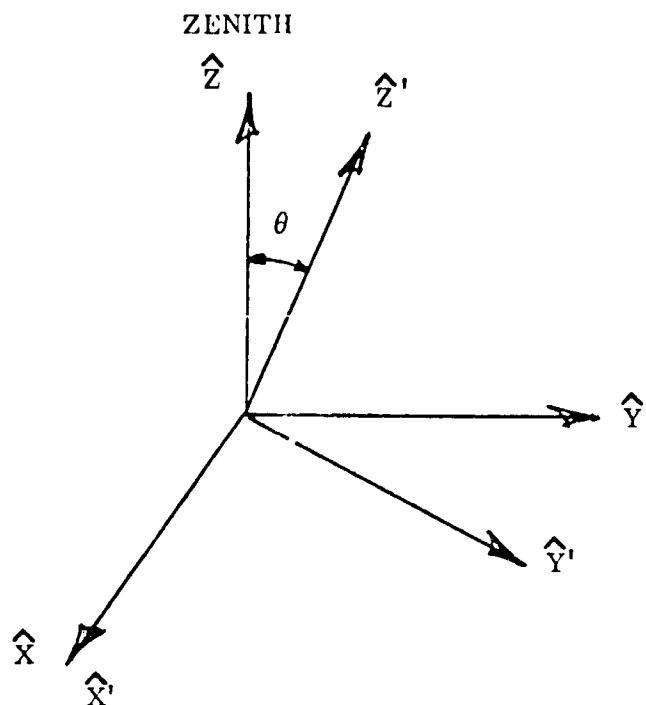


FIGURE D-1. ANTENNA PATTERN AND ENVIRONMENT COORDINATES

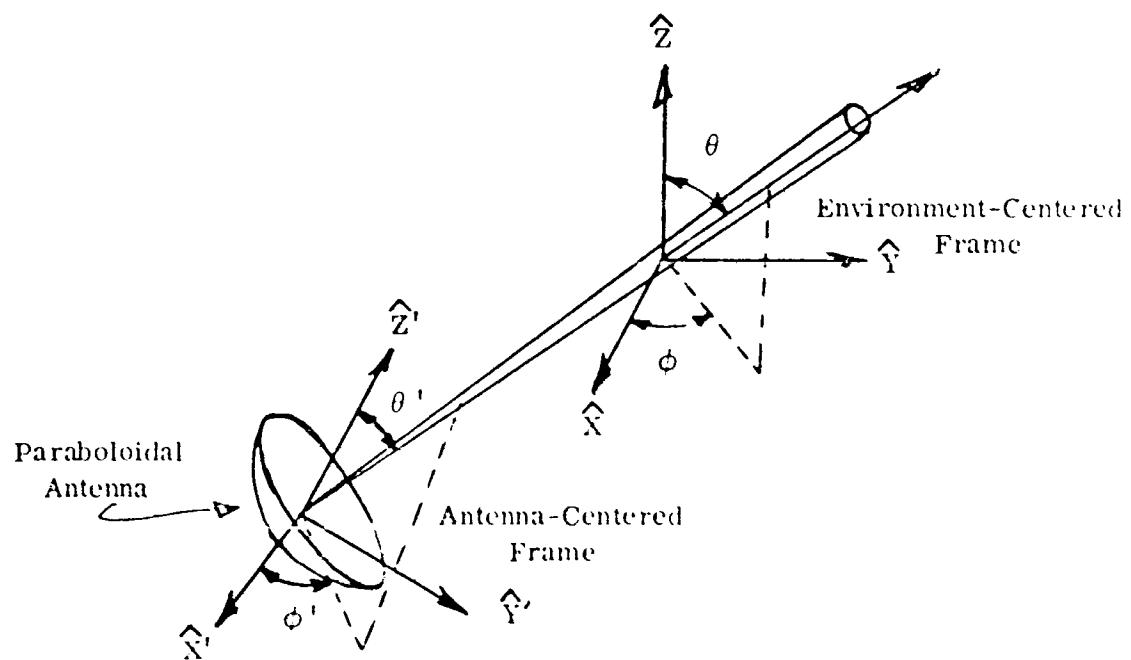


FIGURE D-2. ANGULAR COORDINATES OF ANTENNA PENCIL BEAM IN ANTENNA AND ENVIRONMENT CENTERED FRAMES

where

$T_b(\theta, \phi)$ = brightness temperature of environment at zenith angle θ and azimuthal angle ϕ

θ' = polar angle of environmental point in antenna-centered coordinates

ϕ' = azimuthal angle in antenna-centered coordinates

g = antenna gain function in antenna-centered system

$d\Omega'$ = element of solid angle in antenna system

If one assumes the environment to be azimuthally symmetric (certainly true for clear skies), then T_b depends on θ only and equation (D-1) can be written

$$T_a(\theta_0) = \int_0^{\pi} k(\theta_0, \theta) T_b(\theta) d\theta \quad (D-2)$$

where

$$k(\theta_0, \theta) = \frac{\sin \theta}{\int_0^{\pi} \int_0^{2\pi} g(\theta', \phi') \sin \theta' d\phi' d\theta'} \int_0^{2\pi} g(\theta', \phi') \sin \theta' d\phi' \quad (D-3)$$

Equation (D-2) is a Fredholm integral equation of the first kind with kernel k . It can be solved numerically in the following way.

First, one introduces a quadrature rule to change the integral in equation (D-2) into a sum:

$$T_a(\theta_0) = \sum_j k_j(\theta_0) T_b(\theta_j) \quad (D-4)$$

The set of finite angles (θ_i) may be chosen to be equidistant if desired. If the antenna temperature T_a is also measured at these angles, then a set of linear matrix equations results:

$$T_a(\theta_i) = \sum_j G_{ij} T_b(\theta_j) \quad (D-5)$$

where G_{ij} is a $m \times m$ matrix derived from k .

Since T_a and T_b are very close in magnitude, it is convenient to calculate their difference. Equation (D-5) can be written

$$T_a(\theta_i) = T_b(\theta_i) + \sum_j (G_{ij} - \delta_{ij}) T_b(\theta_j)$$

where, δ_{ij} is the unit matrix; or in symbolic matrix notation,

$$T_b = T_a - (G - I)T_b \quad (D-6)$$

Equation (D-6) has a formal solution which may be expressed as an infinite series:

$$T_b = T_a - (G - I)T_a + (G - I)(G - I)T_a - \dots \quad (D-7)$$

In equation (D-6) and (D-7), I represents the unit matrix.

Truncation of the series in Equation (D-7) is equivalent to solving the following iterative set

$$\begin{aligned} T_b^{(n)} &= T_a - (G - I)T_b^{(n-1)} \\ T_b^{(0)} &= T_a \end{aligned} \quad (D-8)$$

Usually only one or two iterations are necessary in order to achieve a satisfactory solution to equation (D-5) if T_a is given by empirical data.

An obvious method to calculate G_{ij} involves using a quadrature rule based on equidistant intervals in θ . This approach leads to the form

$$k_i(\theta_0) = w_i k(\theta_0, \theta_i)$$

where, w_i is an appropriate weight. Because of the highly peaked nature of k , the important sum condition

$$\sum_i k_i(\theta_0) = 1$$

does not hold sufficiently well to insure the accuracy needed for solution of equation (D-6). A better method of calculation involves writing equation (D-2) as

$$T_a(\theta_0) = \int_0^\pi T_b(\theta) dP(\theta, \theta_0) \quad (D-9)$$

where

$$P(\theta, \theta_0) = \int_0^{\theta} k(\theta_0, \bar{\theta}) d\bar{\theta} \quad (D-10)$$

Then the trapezoidal rule may be applied to equation (D-9), yielding

$$T_a(\theta_0) = \sum_{i=1}^I T_b(\theta_i) 1/2 [P(\theta_{i+1}, \theta_i) - P(\theta_{i-1}, \theta_i)] \quad (D-11)$$

or

$$G_{ij} = 1/2 [P(\theta_{j+1}, \theta_i) - P(\theta_{j-1}, \theta_i)] \quad (D-11)$$

Next it is necessary to indicate the method of computing P . Using equation (D-3) and (D-10) we write,

$$P(\bar{\theta}, \theta_0) = \int H(\bar{\theta} - \theta') g(\theta', \phi') d\Omega' / \int g(\theta', \phi') d\Omega' \quad (D-13)$$

where, $H(\bar{\theta})$ is the Heaviside unit step function. The solid angle integration in the numerator of equation (D-13) has been written in the antenna-centered system instead of the zenith-centered system. One may interpret equation (D-13) as saying that $P(\bar{\theta}, \theta_0)$ is the fraction of the received power entering the cone with half-angle θ centered on the zenith.

Now if $\theta_0 = 0$, then $\theta = \theta'$, and equation (D-13) becomes

$$P(\bar{\theta}, 0) = \frac{\int_0^{\pi} \int_0^{2\pi} g(\theta', \phi') d\phi' \sin\theta' d\theta'}{\int_0^{\pi} \int_0^{2\pi} g(\theta', \phi') d\phi' \sin\theta' d\theta'} \quad (D-14)$$

A great simplification is achieved by specializing to the case where the antenna is azimuthally symmetrical i.e., there is no gain dependence on ϕ' . In this case, equation (D-14) becomes

$$P(\bar{\theta}, 0) = \frac{\int_0^{\pi} g(\theta') \sin\theta' d\theta'}{\int_0^{\pi} g(\theta') \sin\theta' d\theta'} \quad (D-15)$$

and equation (D-13) can be written

$$P(\bar{\theta}, \theta_0) = \int_0^{\pi} \frac{\Delta \phi(\theta_0, \bar{\theta}, \theta')}{2\pi} dP(\theta', 0) \quad (D-16)$$

where,

$$\begin{aligned} \Delta \phi(\theta_0, \bar{\theta}, \theta') &= \int_0^{2\pi} H(\bar{\theta} - \theta') d\phi' \\ &= \Phi_1(\theta_0, \bar{\theta}, \theta') - \Phi_2(\theta_0, \bar{\theta}, \theta') \end{aligned} \quad (D-17)$$

Now the angles $\phi_i^*(\theta_0, \theta, \theta')$ represent the azimuthal angles corresponding to the intersections of two cones: the first cone is defined in the antenna-centered frame by constant polar angle ℓ' ; the second cone is defined in the environment-centered frame by constant polar angle θ . In order to determine the analytic relations for ϕ_i^* , the geometrical configuration of Figure D-2 can be used to express the transformation of coordinates between antenna and environment-centered frames:

$$\sin\theta' \cos\phi' = \sin\theta \cos\phi \quad (D-18)$$

$$\sin\theta' \sin\phi' = \cos\theta_0 \sin\theta \sin\phi - \sin\theta_0 \cos\theta \quad (D-19)$$

$$\cos\theta' = \sin\theta_0 \sin\theta \sin\phi + \cos\theta_0 \cos\theta \quad (D-20)$$

The angles ϕ' defined by fixed values of θ_0, θ , and θ' can be found from equation (D-18) if values of ϕ are already determined; these latter must be obtained by solving equation (D-20). The set of equations (D-18), (D-19), and (D-20) are invariant under the transformation

$$\phi \rightarrow \pi - \phi, \phi \rightarrow \pi - \phi' \quad (D-21)$$

hence, the two solutions in equation (D-17) are related. By rewriting equation (D-20) as,

$$\sin\phi = \frac{\cos\theta' - \cos\theta_0 \cos\theta}{\sin\theta_0 \sin\theta} \quad (D-22)$$

one can see that it has two solutions: ϕ_2 and $\phi_1 = \pi - \phi_2$. The final result is obtained by inserting either value in equation (D-18) in the form, for example,

$$\phi_2^*(\theta_0, \theta, \theta') = \cos^{-1} \left(\frac{\sin\theta \cos\phi_2}{\sin\theta'} \right) \quad (D-23)$$

The other branch of the solution is given by

$$\phi_1^*(\theta_0, \theta, \theta') = \pi - \phi_2^*(\theta_0, \theta, \theta') \quad (D-24)$$

C. Calculations

Two computer programs have been coded to perform the antenna pattern removal.

The first program has the task of calculating the matrix elements G_{ij} from the equation (D-12). The matrix

$$M \approx G - I$$

is the output on punched cards or magnetic tape for use with the second program.
In the course of calculation the condition

$$\sum_j M_{ij} = 0 \quad (D-26)$$

is tested.

The second program, APCOR4, has the task of solving for brightness temperatures by the iterative method presented in equation (D-8). It accepts the matrix elements, M , and performs a given number of iterations on the apparent temperature data which are obtained at the specified angular mesh (θ_i) by polynomial interpolation. The mesh chosen for the present data consisted of 69 angles defined by

$$\cos\theta_n = \frac{n - 35}{34}$$

This set appeared to give adequate resolution near the horizon, while keeping the computer time to a reasonable level. For the 9.5 GHz data, an averaged gain pattern was used for both polarizations. In the 16.5 GHz band separate antenna patterns were employed for both polarizations, and the computer performed the azimuthal averaging.

From preliminary calculations it was concluded that satisfactory antenna pattern correction may be obtained with one iteration. Therefore, all the processed data show a single application of equation (D-8).

APPENDIX E

DETERMINATION OF RADIOMETER ABSOLUTE CALIBRATION AND SENSITIVITY, AND CONVERSION OF OUTPUT RADIOMETRIC VOLTAGES TO APPARENT TEMPERATURES

This appendix describes the mathematical expressions used to calculate the absolute temperature calibrations and sensitivities of the radiometers used in this experiment. The expressions developed for this purpose are based on the nomenclature shown in Figure E-1. An expression is also provided for conversion of radiometer output voltages, E_a , to apparent temperatures, T_a , at the input to the antenna feed.

The losses of all microwave components and waveguides have been accurately measured, with the exception of the antenna feed losses. These were estimated on the basis of equivalent waveguide length present in each antenna feed. The losses for the above components are listed in Table E-1. As indicated in Figure E-1, all the radiometers incorporate a basic 2-point input calibration scheme consisting of two waveguide terminations at accurately known temperatures and a mechanical waveguide switch. This allows the use of a 2-point calibration or the use of a 3-point calibration using the zenith sky temperature as the third calibration point.

The measured input-output response of each radiometer is linear over the dynamic signal range (0-400 degrees Kelvin). Therefore, within this range, the scale factor used in radiometer calibration and data conversion is a linear function. Referring to the response curve in Figure E-2, the scale factor (k) for a two point calibration is given by,

$$k = \frac{T_{c1} - T_{c2}}{E_{c1} - E_{c2}}, \text{ degrees Kelvin per volt} \quad (1)$$

Similarly, for an output voltage E_a ,

$$k = \frac{T_{c2} - T_a}{E_{c2} - E_a}, \text{ degrees Kelvin per volt} \quad (2)$$

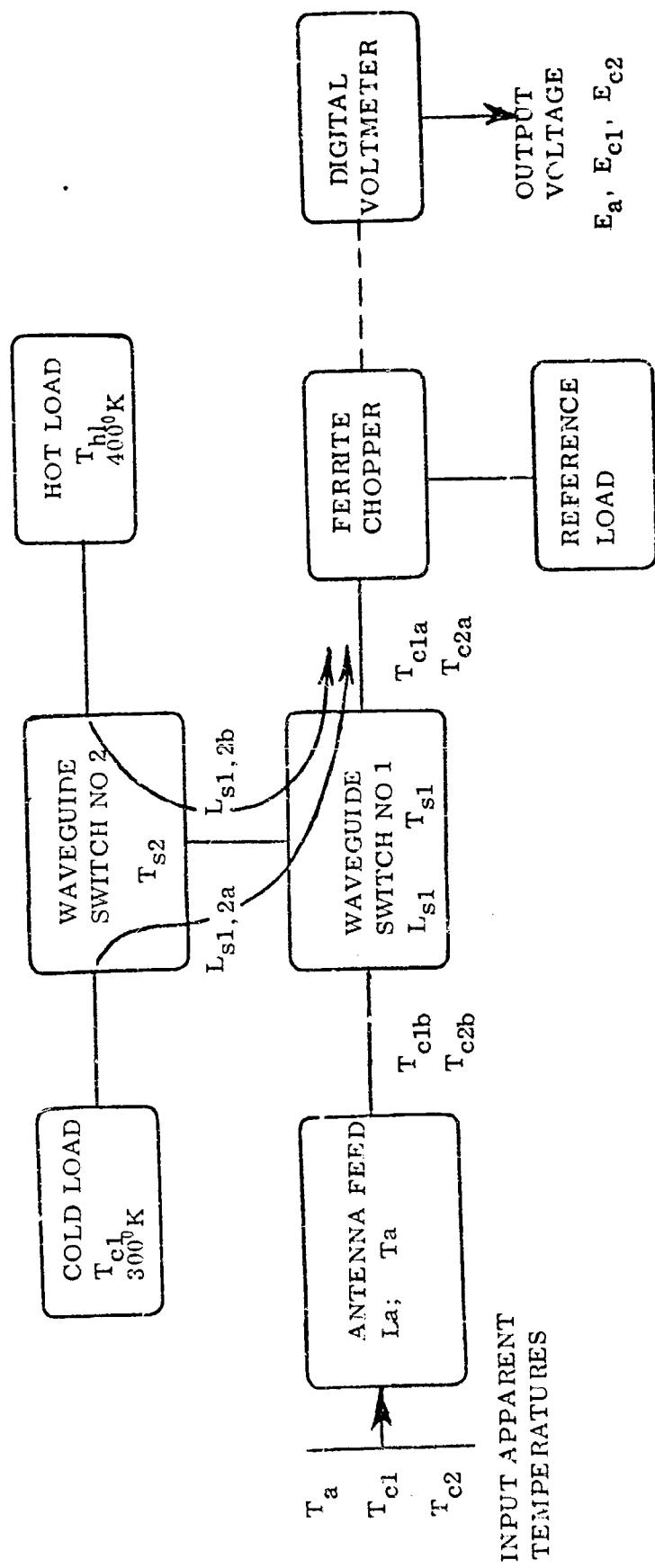


FIGURE E-1. RADIOMETER CALIBRATION CIRCUITRY

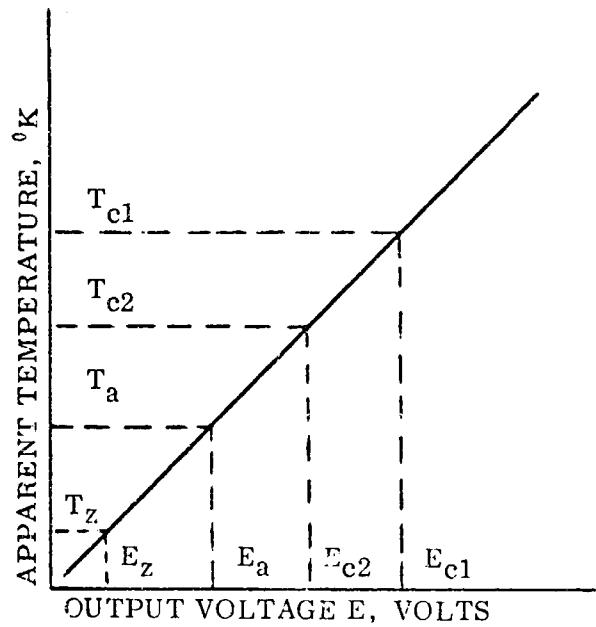


FIGURE E-2. INPUT-OUTPUT RESPONSE
SHOWING CALIBRATION POINTS

TABLE E-1
RADIOMETER INPUT COMPONENT LOSSES

| Item | 9.5 GHz | | 16.5 GHz | | 94 GHz | |
|---|-----------|--------|-----------|--------|-----------|--------|
| | Loss (db) | Factor | Loss (db) | Factor | Loss (db) | Factor |
| 1. Antenna feed* (L_a in Figure E-1). | 0.250 | 1.059 | 0.350 | 1.084 | 1.000 | 1.259 |
| 2. Antenna flange to input of ferrite chopper (L_{s1}) in Figure E-1). | 0.087 | 1.020 | 0.280 | 1.066 | 0.460 | 1.112 |
| 3. Cold Load to input of ferrite chopper ($L_{s1,2a}$) in Figure E-1. | 0.287 | 1.068 | 0.300 | 1.071 | 2.920 | 1.959 |
| 4. Hot Load to input of ferrite chopper ($L_{s1,2b}$ in figure E-1). | 0.316 | 1.075 | 0.330 | 1.079 | 2.220 | 1.667 |

* These values have been estimated from losses in equivalent lengths of waveguide.

where,

T_{c1} is the apparent temperature of the maximum (Hot Load) calibration signal, referred to the antenna feed input, degrees K.

T_{c2} is the apparent temperature of the minimum (Cold Load) calibration signal, referred to the antenna feed input, degrees K.

T_a is the apparent temperature of the material under observation, at the antenna feed, degrees K.

E_{c1} is the radiometer output when the input signal is T_{c1} , volts.

E_{c2} is the radiometer output when the input signal is T_{c2} , volts.

E_a is the radiometer output when the input signal is T_a , volts.

The scale factor k for a three point calibration is determined from a least squares approximation for a best fit straight line, and is given by:

$$k = \frac{\frac{T_z + T_{c1} + T_{c2}}{3} - \frac{T_z E_z + T_{c1} E_{c1} + T_{c2} E_{c2}}{E_z + E_{c1} + E_{c2}}}{\frac{E_z + E_{c1} + E_{c2}}{3} - \frac{(E_z)^2 + (E_{c1})^2 + (E_{c2})^2}{E_z + E_{c1} + E_{c2}}} \quad (3)$$

where,

T_z is the zenith sky temperature

E_z is the radiometer output when the input signal is T_z , volts
and the other parameters are as previously defined.

The radiometer temperature sensitivity can be readily calculated from knowledge of T_{c1} and T_{c2} , as well as the mean values of E_{c1} and E_{c2} . The minimum detectable temperature sensitivity of a radiometer is defined as the root-mean-square output signal fluctuation in the absence of an input signal. This definition implies that the radiometer input is terminated in its characteristic impedance for the requisite output reading. Therefore, in the radiometers under discussion, the input should be terminated with the Cold Calibration Load when the output reading is taken. This results in an effective null input signal condition, which represents maximum sensitivity in a Dicke-type radiometer.

Based on the above definition, the rms temperature sensitivity of a given radiometer is expressed by,

$$T = \left(\frac{E_{out} p/p}{6} \right) \times k, \text{ degrees Kelvin rms} \quad (4)$$

The factor "6" is used to convert peak-to-peak noise voltages to rms voltages, in accordance with standard practice. Equation (4) may be expressed in terms of known quantities. Thus,

$$\Delta T = \left(\frac{E_{c2} p/p}{6} \right) \left(\frac{(T_{c1} - T_{c2})}{(E_{c1} - E_{c2})} \right) \text{ mean , degrees K rms} \quad (5)$$

In practice, approximately ten (10) printouts are taken for E_{c1} and E_{c2} during the sensitivity check. The peak-to-peak fluctuation of E_{c2} is then noted for use in the first term of the above equation. Following this, the mean values of E_{c1} and E_{c2} are determined. With values of T_{c1} and T_{c2} established the rms temperature sensitivity can be calculated.

A microwave signal with an apparent temperature T_a , is affected by transmission through a lossy medium, such as a waveguide component, in accordance with equation (6).

$$T_{out} = T_a \left(\frac{1}{L} \right) + T_o \left(1 - \frac{1}{L} \right) \text{ degrees K} \quad (6)$$

or

$$T_{out} = T_o + (T_a - T_o) \frac{1}{L} \text{ , degrees K} \quad (7)$$

As indicated in Table E-1, the losses of WGS2 and WGS1, from the Cold Load and Hot Load to the input of the ferrite switch, were measured in combination. This combined loss will be indicated in the equations to follow by the symbols $L_{s1,2a}$ for the Cold Load path and $L_{s1,2b}$ for the Hot Load path, respectively. Since the loss in WGS2 is considerably higher than in WGS1, in the X-band channels, the temperature of WGS2 will be associated with $L_{s1,2a}$ and $L_{s1,2b}$.

Referring to Figure E-1, at point 1,

$$T_{c1a} = T_{s2} + (T_{hl} - T_{s2}) \frac{1}{L_{s1,2b}} \text{ , degrees K} \quad (8)$$

and

$$T_{c2a} = T_{s2} + (T_{cl} - T_{s2}) \frac{1}{L_{s1,2a}} \text{ , degrees K} \quad (9)$$

To obtain T_{c1} and T_{c2} , an inverted form of equation (6) must be used, with T_{c1a} and T_{c2a} representing T_{out} . Solving for T_a in equation (6),

$$T_a = \frac{T_{out} - T_o (1 - \frac{1}{L})}{\frac{1}{L}}$$

$$\text{or } T_a = L(T_{out} - T_o) + T_o, \text{ degrees K} \quad (10)$$

At point 2, we obtain from equations (8) and (10),

$$T_{c1b} = L_{s1} [T_{s2} + (T_{hl} - T_{s2}) \frac{1}{L_{s1,2b}} - T_{s1}] + T_{s1}, \text{ degrees K} \quad (11)$$

At point 3, we obtain from equations (10) and (11),

$$T_{c1} = L_a \left\{ L_{s1} [T_{s2} + (T_{hl} - T_{s2}) \frac{1}{L_{s1,2b}} - T_{s1}] + T_{s1} - T_a \right\} + T_a$$

$$\text{or } T_{c1} = L_a [L_{s1} (T_{s2} - T_{s1}) + \frac{L_{s1}}{L_{s1,2b}} (T_{hl} - T_{s2}) + T_{s1} - T_a] + T_a, \quad (12)$$

degrees K

Similarly, at point 2 we obtain from equations (9) and (10),

$$T_{c2b} = L_{s1} [T_{s2} + (T_{cl} - T_{s2}) \frac{1}{L_{s1,2a}} - T_{s1}] + T_{s1}, \text{ degrees K} \quad (13)$$

At point 3, we obtain from equations (13) and (10),

$$T_{c2} = L_a \left\{ L_{s1} [T_{s2} + (T_{cl} - T_{s2}) \frac{1}{L_{s1,2a}} - T_{s1}] + T_{s1} - T_a \right\} + T_a$$

$$\text{or } T_{c2} = L_a [L_{s1} (T_{s2} - T_{s1}) + \frac{L_{s1}}{L_{s1,2a}} (T_{cl} - T_{s2}) + T_{s1} - T_a] + T_a, \quad (14)$$

degrees K

Equations (12) and (14) are required for calculation of radiometer calibration temperatures, T_{c1} and T_{c2} , referred to the antenna feed input. These quantities are used in equation (5) to determine radiometer temperature sensitivity.

The conversion of radiometer output voltages, E_a , to apparent temperatures, T_a , at the antenna feed horn is accomplished by means of an inverted form of equation (2).

Thus,

$$T_a = T_{c2} - k(E_{c2} - E_a), \text{ degrees K} \quad (15)$$

Note that E_{c2} rather than E_{c1} is used in this expression. The reason, of course, is that the value of E_{c2} , representing the Cold Load, is closer to the value of E_a . This optimizes the accuracy of the conversion. The value of k is determined by means of equation (1). Finally, as in the case of the radiometer sensitivity calculation, approximately ten (10) printouts are taken for E_{c1} , E_{c2} , E_z and E_a . The mean values of these quantities are then determined prior to insertion in equation (15) for calculation of apparent temperature T_a .

APPENDIX F

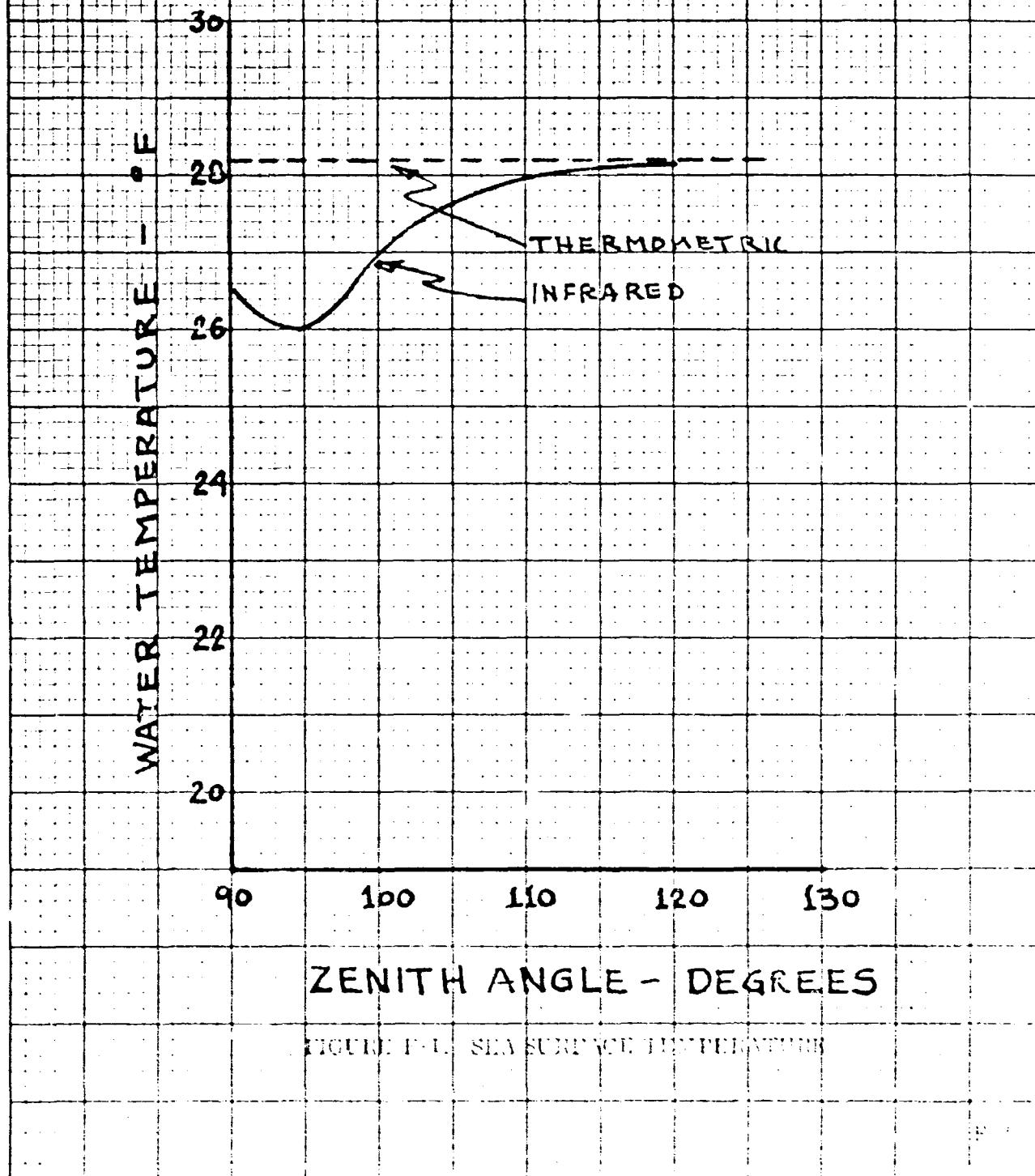
INFRARED RADIOMETER SUPPLEMENTARY MEASUREMENTS

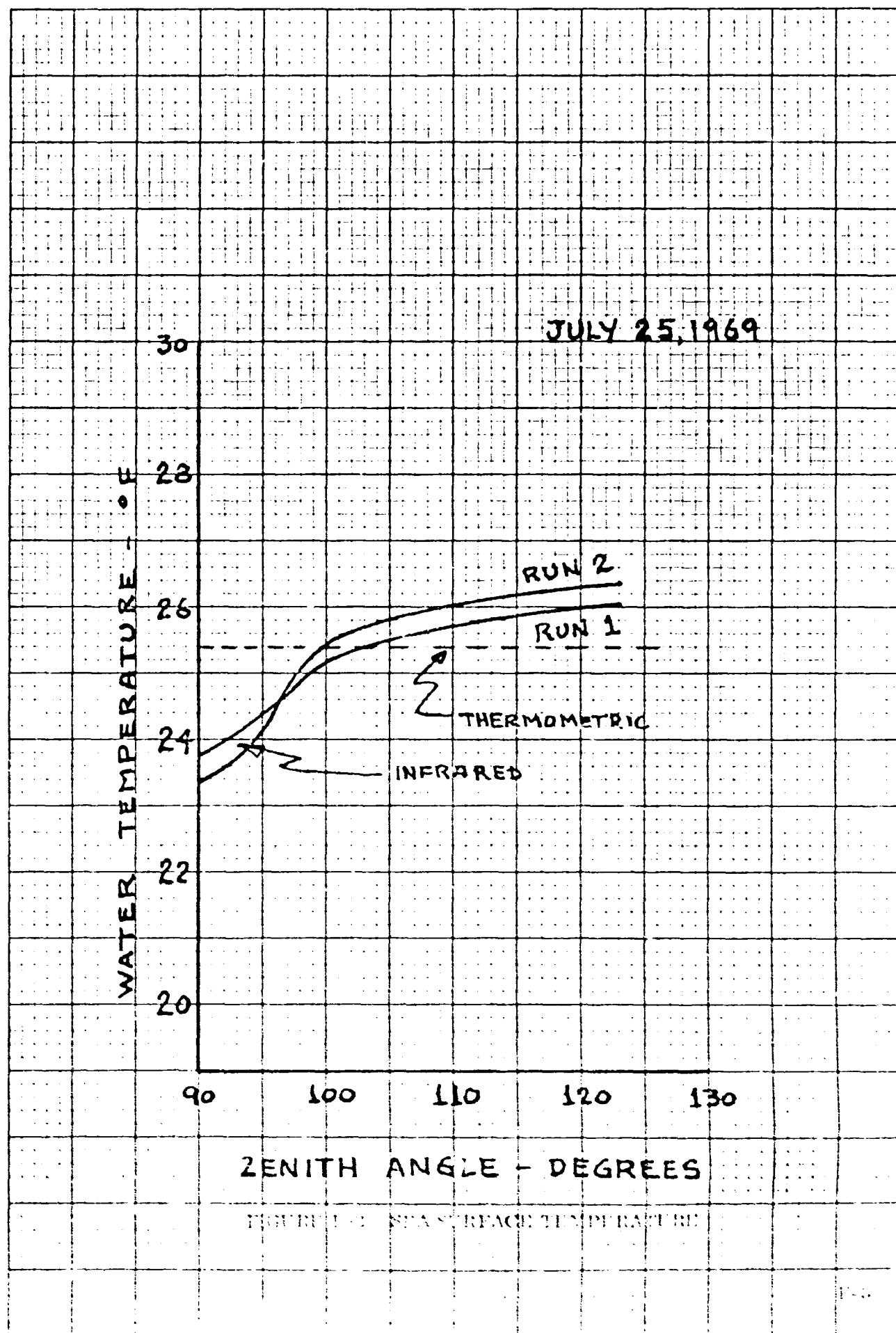
An Infrared Radiometer was supplied and operated by personnel from NESC. This was a Barnes PRT-5 radiometer which had a spectral response from 8 to 16 micrometers.

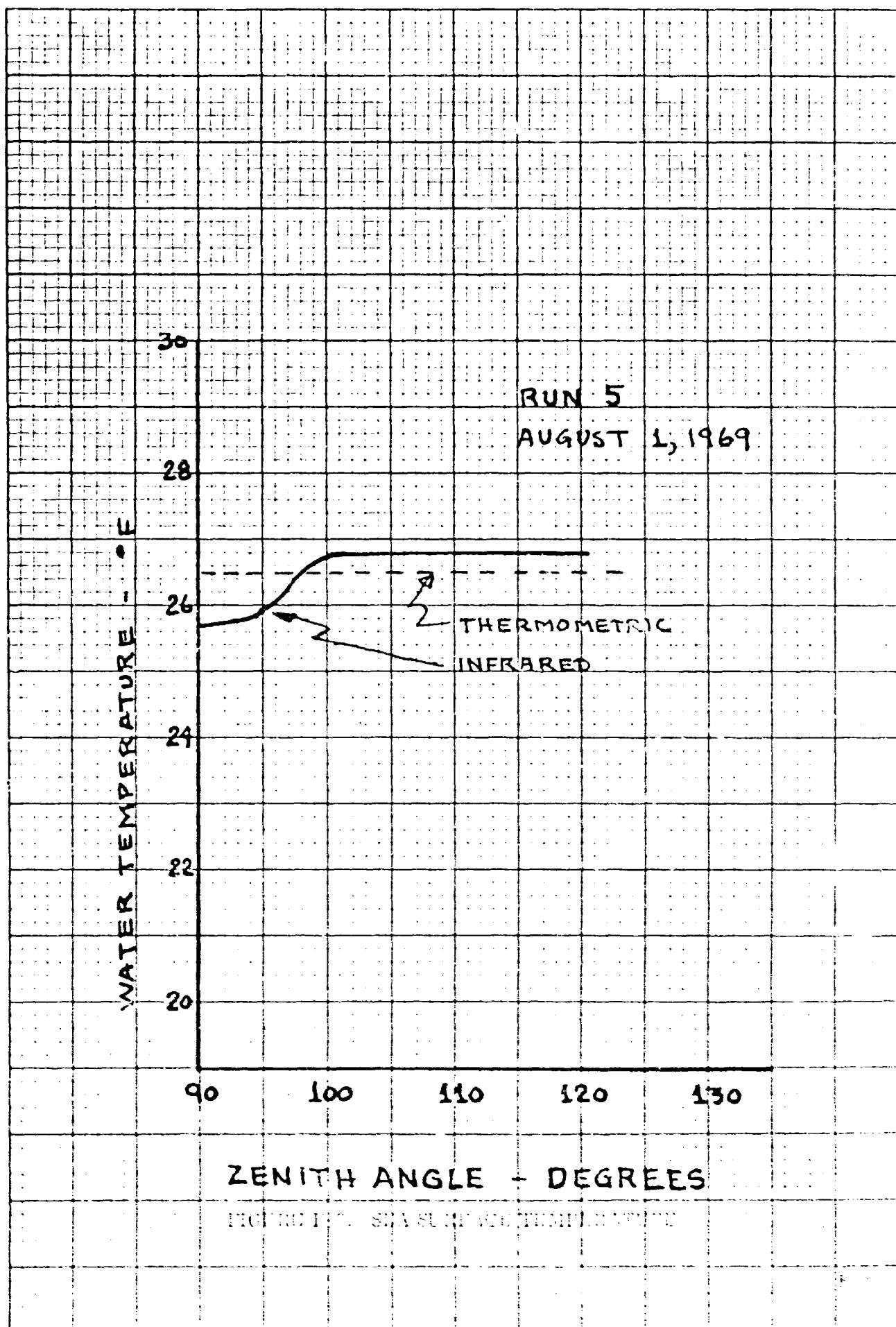
The sea surface temperatures as measured by the PRT-5 were corrected for specular reflectance of the sky background and the resulting temperatures are plotted in Figures F-1 through F-8.

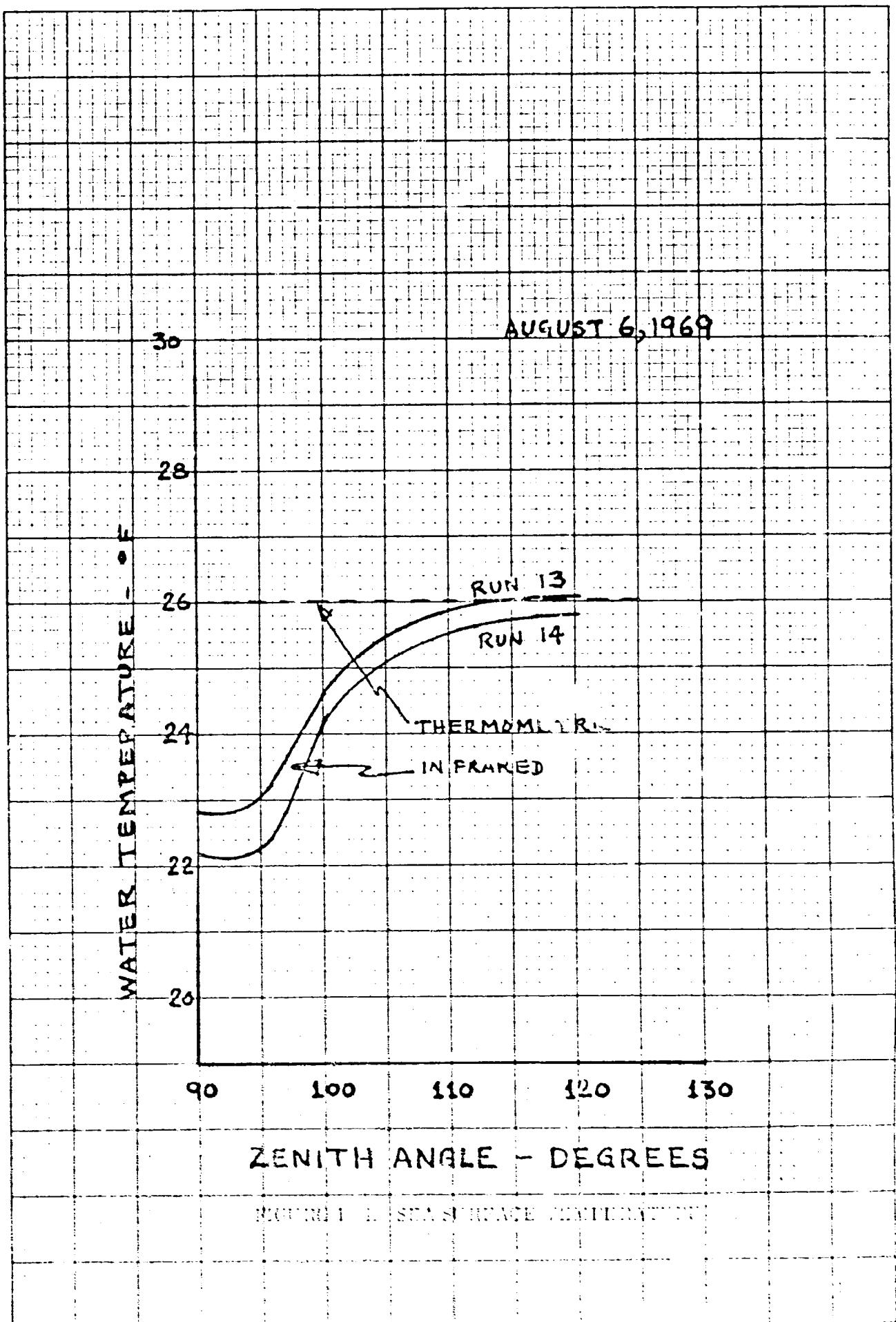
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TO V 4-63
7 X 10 INCHES
KEUFFEL & ESSER CO.

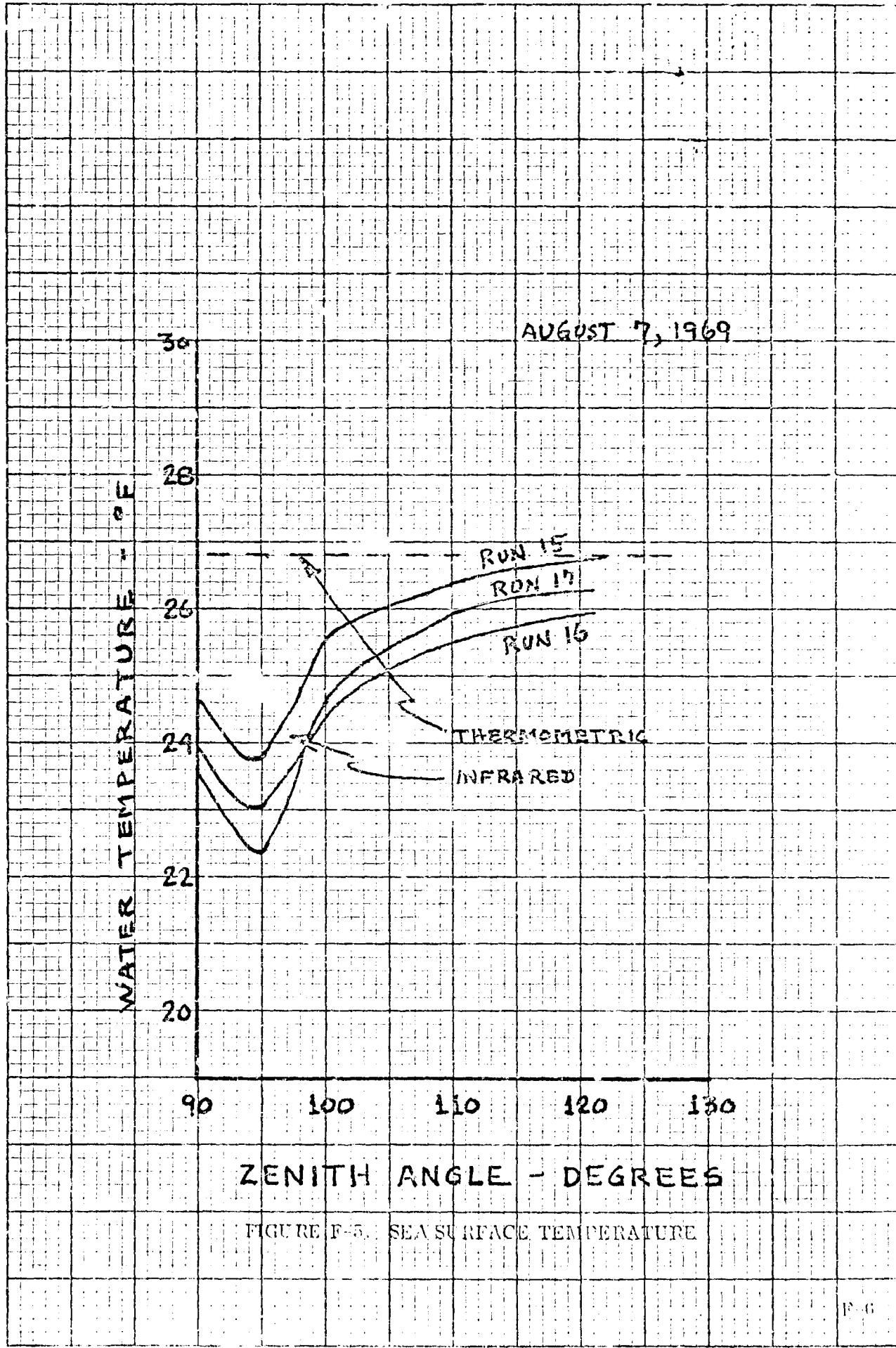
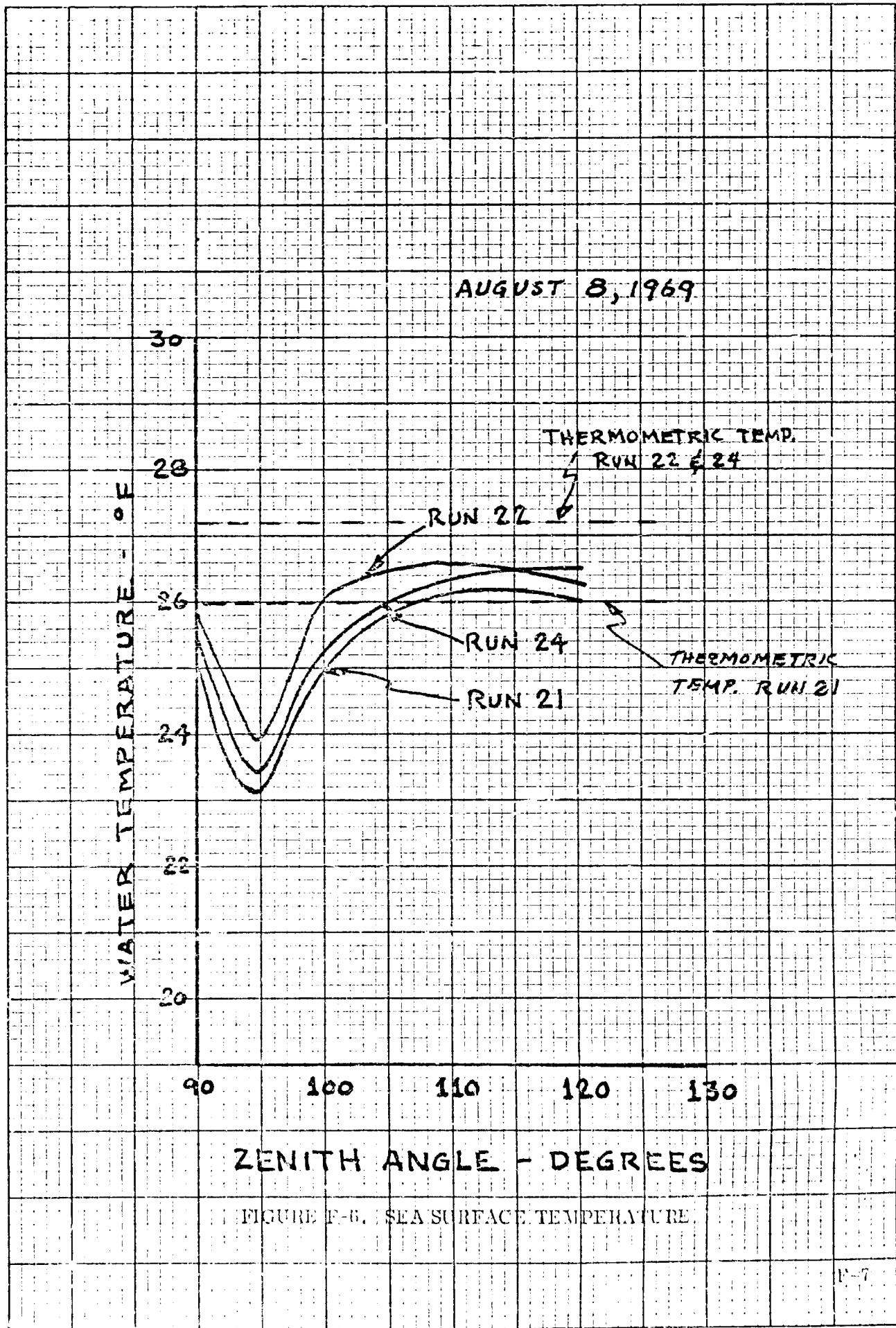
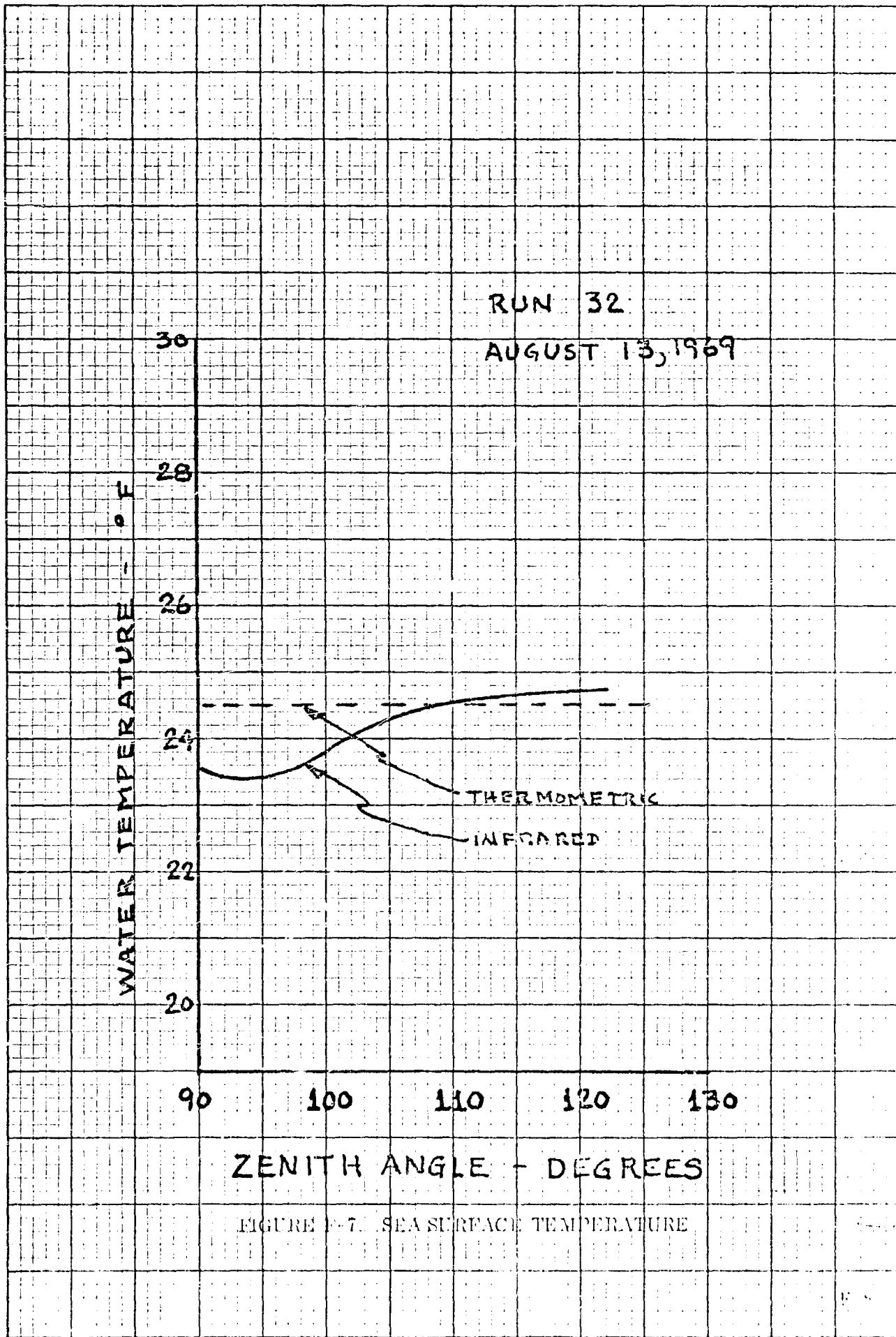


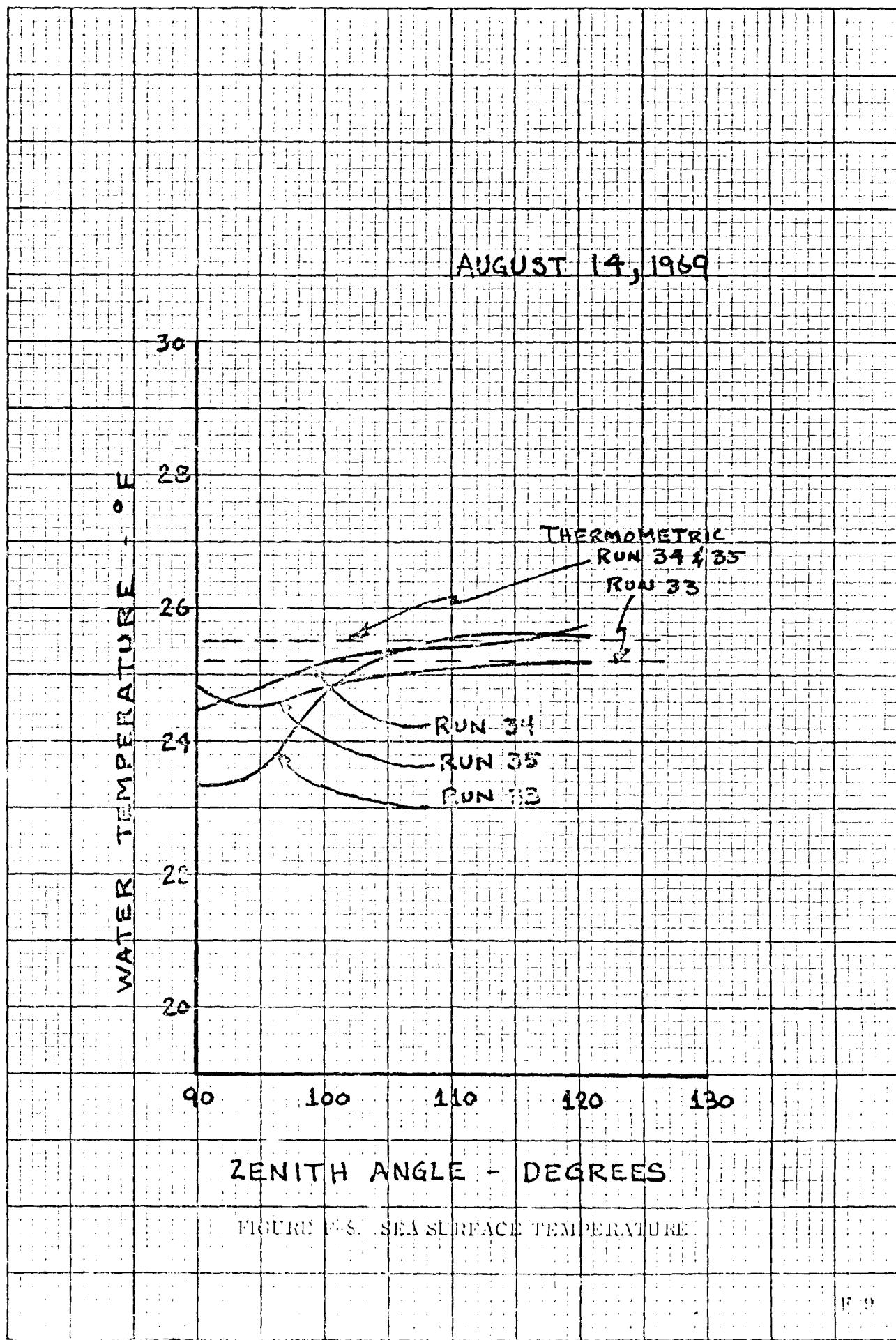
FIGURE F-6
SEA SURFACE TEMPERATURE
RECUTTER & MURKIN CO.



10 1/2 7 x 10 INCHES
453 MM. 250 MM.
KLEINER & ESSER CO.



162 - TO 1 4 162
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| 13. ABSTRACT <p>RCA Astro-Electronics conducted a field experiment to verify a theoretical approach toward remote sensing of sea surface temperature using passive microwave radiation. There is a correspondence between the radiometric temperature of the sea and its thermometric temperature. This correspondence is influenced by the horizontal and vertical emissivity, the incidence angle at which the radiometric measurement is being made, contaminants on the water surface, and by the sea surface roughness. The experiment addressed itself to two basic questions: 1) Can one measure the vertically and/or horizontally polarized microwave radiometric emissions from the sea water and obtain an accurate measure of the thermometric temperature? 2) Can one also make a determination of sea state from such measurements? The radiometric measurements were made from North Island of the Chesapeake Bay Bridge and Tunnel District. The Chesapeake Bay Bridge-Tunnel links the city of Norfolk and Cape Charles, Virginia, across 17.6 miles of water. North Island is at the northern end of the Thimble Shoal Channel Tunnel. The bulk of the microwave measurements were made at a frequency of 16.5 GHz. The following conclusions are drawn from an analysis of the data: 1) There is a correlation between the thermometric temperature and the vertically polarized microwave radiometric temperature, 2) There was no observed correlation of the thermometric temperature with the horizontally polarized microwave radiometric temperature, 3) While theoretical considerations strongly indicate that the horizontally polarized microwave radiometric temperatures should have a strong dependence on sea state, no definitive trends were found in the measured data.</p> | | |

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