

TKV/cvp ABERDEEN PROVING GROUND, MD., FEBRUARY 18, 1936.

REPORT ON INVESTIGATION OF THE CAUSES UNDERLYING ERRATIC POWDER PRESSURES OBTAINED FROM CRUSHER GAUGES

(IN CONNECTION WITH PROJECT RB 116) (0.0. 413.6/12432 - APG 413.6/487)

OBJECT OF TEST

To obtain comparative data regarding the behavior of crusher gauges, assembled under different conditions and with different tolerances, from controlled firings in the 3" A.A. Gun Liner M3, No. 138, chromium plated.

DISCUSSION

OCM Item 12462 directed certain tests to be performed on 3" A.A. Gun Liner M3, #138, which was chromium plated in the bore at the Naval Gun Factory, Washington Navy Yard. This test provided for proof firing to be followed by 50 rounds in 5-round series, with taking of periodic bore measurements and bore impressions. The results of this test, insofar as effect on the liner is concerned, are reported in Firing Record 3807, (0.P. 4987; 0.0. 472.93/4449; A.P.G. 472.91/362), and in First Partial Report on test of 3" A.A. Gun Liner M3, No. 138, chromium plated, and Fifth Report on 0.P. No. 4987, Ordnance Program 4987, OCM Item 12462, dated February 12, 1936.

The Proving Ground has experienced erratic results in powder pressure readings obtained from crusher gauges for some time. Prior to the adoption of the new standard firing record forms, which provide for recording individual pressures obtained as well as mean pressures, these erratic results were not so apparent. The old firing record forms reported the mean pressures only, and wide variance in individual readings were often

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FIRMA SECOND FILL

absorbed in the mean result. In cases where standard firings were made under these conditions of pressure taking or where established charge-pressure curves for a lot of powder were used to obtain data for firings, and the firings made from the curves gave contrary results, the effects of erratic individual pressures were forcefully brought to view.

The cannon crusher gauges in use today are of the Noble type, an outgrowth of the Rodman knife gauge. Those used at the Aberdeen Proving Ground have been in service for many years, many having been formerly used at Sandy Hook Proving Ground. The specifications for these gauges provide for pistons to be made of hardened tool steel, ground to size and the gauge bodies to be made of forged No. 3 steel. This latter steel corresponds to W.D. 1055, a medium carbon steel. In the absence of specified physical requirements and heat treatment of the bodies and pistons, it can be seen that there should be great variance in their ability to withstand scoring, distortion and permanent deformation. The clearance between the piston and the body is 0.0002" with tolerances of +.004" in cylinder diameter, and -.0004" in piston diameter.

The regulations at the Proving Ground provide for the selection of cannon pressure gauges for standardization firings having clearances of .0002" between piston and cylinder with tolerances of +.0002" on the cylinder diameter and -.0002" on the piston diameter. For other than standardization firings the clearance is .0002" between piston and cylinder, with tolerances of +.0004" on cylinder diameter and -.0004" on piston diameter.

Mr. R. H. Kent in a paper entitled "Report on Some Sources of Error in Piezo-electric and Crusher Gauge Measurements (In Connection with Project RB 117)", dated Aberdeen Proving Ground, Dec. 2, 1935, concludes that the pinching effect observed in the case of the piezo-electric gauges should also affect the measurements made with the copper crusher gauges. This pinching effect is caused by the pressure of the powder gases applied to the exterior cylindrical surface of the gauge body, distorting the inner cylinder wall and binding the piston, so as to prohibit free movement.

From all of the foregoing it was concluded that the firings to be conducted in the 3" A.A. Gun Liner M3, No. 138, presented an excellent opportunity to schedule some tests of crusher gauges in which their behavior under certain variables of assembly and selection could be observed.

In 0.0. 471.91/2052; A.P.G. 472.91/362-2, the Ordnance Office authorized tests to be conducted in this gun along the following lines: (a) Select 16 medium caliber crusher gauges which are in good condition, assemble pistons to 8 of these gauges to give total clearance in each case of .0005" between cylinder wall and piston. Assemble pistons to the other 8 crusher gauges to give a total clearance of .0010" between cylinder wall and piston.

(b) Assemble all gauges with the cylinder wall and piston wiped dry, no lubricant to be used about the gauges except on closing cap threads and body washer.

(c) All gauges to be assembled, disassembled, measured, etc., by the Gauge Section, using the same procedure at all times.

(d) Copper cylinders to be of the same lot and anneal with zero initial compression.

(e) Four gauges of each lot of 8 described in (a) above, to be assembled with standard copper obturator cups, the remaining gauges to have the copper cup replaced with a wax seal consisting of 2 parts cup grease, 2 parts beeswax and 1 part resin.

(f) The 16 gauges will be divided into four sets of four gauges each, each set to consist of:

1 gauge - .0005" clearance; copper cup 1 gauge - .0005" clearance; wax obturator 1 gauge - .0010" clearance; copper cup 1 gauge - .0010" clearance; wax obturator

These gauges are all numbered and sets will remain intact throughout the whole test.

(g) Forty rounds to be fired at five different

pressures:

8 at 20,000 lbs. per sq. in. 11 11 8 at 27,000 " 22 8 at 31,500 " 11 11 11 8 at 36,000 " - 11 11 ** 8 at 41,200 " 11 11 11

(h) Each round to have a set of four gauges, assembled as described in (f) above, inserted in the case.

(i) In half of the rounds at each pressure, the set of gauges is to be fixed in the bottom of the case. In the other half of the rounds, the gauges are to be placed in the case in accordance with current procedure at the Proving Ground.

Procedure

A lot of powder was selected from that available at the Proving Ground for use in this test. The powder selected was DuPont 1492 - 1918 - for 6" Gun M1900-03-05. It is a pyro powder, multiperforated grain having a web thickness of 0.0360". This powder is suitable for use in the 3" A.A. Gun M3.

Standard 3" cast iron proof slugs, weighing 15 lbs. each, were used in all firings. Cartridge cases, 3" A.A. Mk. II Al, drawing 71-5-3, unmodified, were used with M21 Primers, Lot 1355-15, in all rounds.

Firings were conducted in groups of five rounds each, the first round of each group being a warming round, the remaining four having gauges assembled as prescribed. This was necessary due to the limited number of gauges used, 16 in all or sufficient for 4 rounds, and the requirements of the original directive (OCM Item 12462) which called for five-round groups between stargauging, etc. Two groups were fired at each pressure, each group being fired on a different day usually since the gauges had to be disassembled and reassembled by the Gauge Section between groups and the necessary stargauging of the liner performed. Boulenge muzzle velocities were taken on all rounds.

The description of assembly of each group of five rounds follows:

Round	Fixed or <u>Loose in Case</u>	Gauge <u>No.</u>	Piston <u>Clearance</u>	Obturator Seal
Warming		No gau	ges –	
1	Fixed	5942 4525 4734 4190	.0010 .0010 .0005 .0005	Wax Copper Wax Copper
2	Fixed	4970 2422 4748 28 3 4	.0010 .0010 .0005 .0005	Wax Copper Wax Copper
3	Loose	5908 3640 4744 4329	.0010 .0010 .0005 .0005	Wax Copper Wax Copper
4	Loose	4774 1728 4875 325 9	.0010 .0010 .0005 .0005	Wax Copper Wax Copper

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The problem of fixing the four gauges in rounds 1 and 2 of each series presented difficulties. Various metal holders were devised and tried out in an effort to hold the four gauges upright in the case and against the case wall in order that there would be no interference with the action of the primer. The MII Al case is rather long, and the mouth opening is only 3" in diameter. With the facilities available at the Proving Ground there appeared to be no simple and inexpensive method of accomplishing this. The Research Division at the Proving Ground suggested that the four gauges be held together with strong rubber bands, each gauge in contact with the primer body and resting on the bottom of the inside of the case. It was believed that no interference with the primer action would occur. A simple fixture was devised for assembling the gauges in position in this manner, and this method was used for fixing the gauges in rounds 1 and 2 of each series.

The data obtained in the firings are shown on the attached sheets, Exhibits "A" to "F". The data shown on Exhibit "F" was obtained by firing 2 additional groups using a powder charge to give pressures lower than those used for the initial test shown on Exhibit "A". This was done to obtain additional data in the lower pressure range and to see if the high pressures shown on Exhibit "E" had permanently affected the gauges.

Pressures obtained were not corrected in any way for erosion, etc.

Analysis of Data

Exhibit "A"

It will be noted that the results obtained in the firings of the first series, Rounds 14, 15, 16 and 17, showed very little difference between gauges with different characteristics. When these firings were repeated three days later (Rounds 19, 20, 21 and 22) under as near identical conditions as possible, it is noted that the gauges having pistons with .0005" clearance and wax obturators in Rounds 19, 20 and 22, showed considerable dispersion from the other gauges assembled with them in the rounds.

The dispersions from the mean values for all combinations of variables as shown in columns 13 to 16, inclusive, indicate that the gauges having large piston clearance (.0010") and assembled with copper cup obturators show very much less dispersion in pressure than any other combination tested.

Attention is invited to gauge No. 4744 assembled in the 3rd round of each series. This gauge has a piston with

- 5 -

.0005" clearance and was always assembled with a wax obturator. Its behavior, however, is unlike that of other gauges with similar characteristics, and the results obtained from it are more like those obtained with the .0010" clearance gauges. This gauge was carefully checked and rechecked several times to find out the cause for this paradoxical behavior. No explanation is offered.

Exhibit "B"

The results shown for these series continue to follow the trend indicated in Exhibit "A". The mean dispersions are of greater magnitude due to the greater effect of the low reading gauges. The dispersion in columns 11 and 12 indicate that fixing the gauges in the round is not an advantage, but contributes to greater deviations.

Gauge No. 4744 continues to behave at variance with similar gauges. Gauges having large piston clearance and copper obturator cups have the least dispersion.

Exhibit "C"

The results of previous firings are unchanged by these series. Through a misunderstanding one gauge in each series, Rounds 35 and 42 were assembled with copper cups instead of wax. This change was considered in arriving at the mean values.

Exhibits "D" and "E"

The results of these firings are consistent with previous results.

Exhibit "F"

These series were fired to see what effect, if any, the repeated firings had on the gauges.

It was expected that the results would be consistent with those shown on Exhibit "A". Such was not the case, and it appears that some of the gauges have been permanently deformed, or otherwise changed so that they no longer behave normally.

CONCLUSIONS

From the data obtained in these tests it appears that gauges with tight pistons will give consistently lower pressures and greater dispersions than will be given by gauges having pistons with greater clearance.

That these tests do not give sufficient data on which to base the limits of clearance between pistons and cylinders in gauges. That definite conclusions cannot be drawn from this data regarding the effects of fixation of gauges, or use of wax compounds in lieu of copper obturator cups; due to the confusing effects of the variables introduced into the tests.

RECOMMENDATIONS

That further tests be made to determine the maximum piston clearance which can be allowed.

That no further tests be made at this time having reference to fixation of gauges in the round.

That further investigation of lubrication of the gauge parts be conducted.

That the search for a substitute for copper obturating cups be continued.

T. K. Vincent, Captain, Ord. Dept., Proof Officer.

K. F. Adamson, Lt. Col., Ord. Dept., Chief Proof Officer, Gun Testing Division.

RECAPITULATION - PRESSURE DATA- SPECIAL GAUGES IN S"A.A. GUN, M.S. WITH CHROMIUM PLATED FINER #138

SELECTED PRESSURE GAUGES (MED CAL); 4 PER ROUND, ALL ASSEMBLING, MEASURING ETC BY GAUGE SECTION

1	3	2	3	4	2	6	7	8	9	10	11	12	13	14	15	16	17	/ 8
SERIA NUMBE OF ROUN	R PRE	SSURE	MEDIUM CALIBER GAUGE NO.	PRESSURE #/SQ.IN. (.075'Mic Spindle)	MEAN OF GAUGES WITH & DOOS" PISTON CL.	GAUGES WITH	MEAN OF GAUGES with Copper obt. Cups	MEAN OF GAUGES with WILL obturator	MEAN OF GAUGES ASSEMBLED TO ROUND	INDIV MEAN DISPERSION PRESSURE	FILED	MAX. DISPERSION GAUGES LOOSE IN ROUND	IN DIV DISPERSION 0.0005" PISTON CLEARANCE	INDIN DISPERSION O DOIO PISTON CLEARANCE	INDIV DISPERSION COPPER OBT. CUPS	DISPERSION WAX OBT	FIRING	REMARKS
14	20,00 (3*-2 X144	2027]	5942 4525 4734 4190	19,550 19,000 18,950 19,300	\$ 19.125	19,275	19.150	19.250	19.200	+ 350	600	X	• 175	111 -111	•11- •1+	- 20 0	16.1131	Very consistent
15	PYR	05 (5500	4970 2422 4748 2834	18,900 19,100 19.050 19.050	} 18,850	19,000	8.8.7.5	18.915	18.925	- 25 +175 +125 -275	450	X	* 3.00	+100	14+	+15	D JAK.	Very consident
46			5908 3640 4744 4329	- 19.550 - 19.650 - 19.200 - 19.100	} 19:150	19.600	19,075	} 19.37S	19,375	+ 175 +275 -175 -275	X	550	+ 10	02+ 02+	+ 3.75	+175	-Fikel	Ving consident
17			4774 1728 4875 3259	19240 19500 19.150 20.150	} 19.650) H.370	118.91	19,195	19,510	- 270 - 10 - 340 + 640	X	1000	- 500	+120	- 315 -	++5		TIGHT PISTON - WAY - ROW greasure GREATEST DISP - TIGHT ASTON, COPPER CI
19	20,6	000	5942 4525 4734 4190	18,975 19,100 15,150	\$ 17.275	} 14.0+0	025.91	17.065	18,150	+ \$25 + 450 - 3,000 + 1,250	4:250	X	- k./35 +3./15	+++++++++++++++++++++++++++++++++++++++	-180	-1910	1	TIGHT PISTON, WAX. Low pressure
20			4970 2422 4748 2834	- 19.000 - 19.000 - 13.500 - 13.50 - 13.50		} 19,000	18,675	1-250	17.460	+1540 +1540 -3960 + 890	5,500	X	· 2.715 • 2.715		1225	-1150	13,1436	TIGHT PISTON WAX - Low press
21			5908 3640 4744 4329	19.400 19.200 17.450 19.250	3 18.350	} 19.300] 19.230	18,425	18.825	+ 575 + 375 - 1375 + 425	X	1920	-4+0	+ 100	+ 30	- 115	PAN	TIGHT PISTON, WAX-low press
22			4774 1728 4875 3259	19.025 19.150 12.800 19.750) 16,275	} 19,090	19,450] (S.415	17.680	+1345 +1470 -4880 +2070	X	6950	-3,415	+4	+ 300	+3.07 -3.07	+FiRED	TIGHT PISTON, WAX-Low prese
MEAN	1 ES 200	000		18,640	18.075	(4,210	19,230	(8000	181000	-	3,700	2.610	2460	197	445	2340		
						1												EXHIBIT "A" -

RECAPITULATION

TION - PRESSURE DATA - SPECIAL GADGES IN 5" HAUDA, MS CHROMIUM PLATED LINER #138

SELECTED PRESSURE UASUES (MED.CAN), + per round, 1411 assembling measuring etc by GADUE SECTION

L.	2	3	4	2	6	7	- 3	7	10		1	13	/.	5	1 10	· >]	e
NUMBER OF ROUND	PRESSURE #/sq.in.	CALIBER GAUGE NO.	+ (SQ IN (-075 MER SPINDLE)	MEAN OF GAUGES WITH 0.0005" PISTON CL	GAULES	GAUGES	GAUGES	ALL GAUDED HSSETABLED TO KOUND	DISPEDIAN PRESSURE	GAUGES FIXED IN ROUND	DISPERSION GAJGES LOOSE IN ROUND	0 0005"	DISPERSION WITH D. ODIO PISTON TEARANE	DISPERSION	UNDIA DISPERSION	FIRINA	KEMARK:
24	27,000	4525	-26.400	1	\$ 25,790	125815	1= -50	23780	+2.620 + 1,395 -6,680 +2670	4,350		-4675	4 610 - 610	-640	+4-20		
	PYRO POUDER	4970 2422 4748 2834	-25.050 126.550 12.700 24.350	} 21.775 } 18.525	} 25,800	25420	18 175	1000	+ 2.885 + 4.385 - 9.465	13820		-5 825	- 750	+1100	+6175	4691	
26		5908 3640 4744	- 26.000 - 24,150 - 20.700 - 22.300	} 21.500	\$ 25,075	23225	23 350	23.240	+2.710 + 860 - 7.540		2,300	- 800	+ 925 925	+925	+2650	LAN. LA	
21		4774 1728 4875	* 25.750 • 26.850 • 12.450 • 21.100	16.775		23975		21.540	+4.210 +5.310 -9.040 - 440		14 400	- 4 325	022- 022+ 026+ 026- 021- 021+	+ 2 875	+6.650		
29	27000	59+2 4525 4734	-26,000 -25,300 -18,450 -26400	1 27.425	25,650	25850	\$22.225	24,040	+1,260 +1,260 -5.590 +2,560	7,950		- 3975 + 2975	- 320 - 26 -	- 550 - 550	- 3775 -		
30		4970 2422 4748	-25,700 -26.000 -17.600 -24,950	\$ 21.275	25,850		2.650	23.86	+2,1+0 +2,4+0 -5,4+0 +1 340			- 2 675 +3675	-150 +150	+ 525	- 4.030	936	
31	-	5908 3640 4744	126.500 27.850 26.600 27.200	3 26,900	27.175	2	26 500	27,040	ALL MATLES		1.320		+ 675	+ 325	- 50 + 50	4N. 16,1	
32		4774 1728 4875	~25.150 ~25.700 ~18 400 ~26.100	22.250	25,425	25900	רר.וב	23 840	+1,310 +1,840 -2,940 +3,144				- 275 + 275	- 200	276, C+	7	
MEAN VALUES	27.000		23,660	21.430	25.880	25,400	21.900	23.660		9,890			252	890	3920		
																	EXHIBIT

RECAPITULATION PRESSURE DATA SPECIAL VASUES IN STRACTIONS THROTOPIN PLATED FILLER "13"

DELECTED ARESORE CAUSES (MER TAL) A prevented ALL ADDING MERSING OF by ANESSE PART

	. 03	*	125	*	5	Τ	-7	8	4		I + ,	1	1 12		15	1 15	1	
1 20	SERVAL HUMBER OP ROUMB	ехраны Рассыка Пран	MEDION CALIEER DAULE NO	PRESSURE ASOIN OTS" MICK SPINDLE)	MEAN OP GAUGES WITH 0.0005" PISTON CL.	GAUGES WITH	GAUGES WITH COPPER.	GAUGES WITH WAX	ALL DAULP	DUPERSION	DIDPERSION	HIAK LIDPEKSIM GAUGES LOOSE IN ROUND	DISPERSION DISPERSION DISPERSION DISTON PISTON CLEARANCE	IN DIV DISPERSION WITH O DOID" PISTON CLEARANCE	COPPER	INDIA DISPERSION NAK DETUKATHI	FIRINU DATÉ	REMARKS
Non A	34	31.500 (451-4)	54+2 4525 4754 4190	29,500 30,900 17,800 -30,900	} 24.350	30.200	30,400			+2,225 +3,625 -9,415 +2,625	13,100		-1.550	- 700 + 700	0	+5,850 -5,850	4	
	35	PHRO	4970 2422 4748 2834	-28,275 -30,550 -13,400 -30,450	21.925	} 29,410	24,800	328.275	25.670	• •			- 8,525 + 8,525	-1,140 +1,140	+ \$750	* 0	17. 1436 P.M.	This gauge assembled with copper cu
- 13	36		5408 3640 4744 4329	* 30,225 * 31,600 * 26,500 * 31,000	28,750	30,910	31. 300	} 28.300	29.830	+ ,395 +1,770 -3 33, +1,170		5,100	-2.250	- 1690 + 640	+ 300	+1,860	JAN.	
	37		1728 4875	· 27,900 · 31.000 · 13,900 · 13,900	13600	} 29450	22 50	}20.00	121.525	+ 6,375 + 4,475 - 7,625 8 225		(7.29%)	+ 365	-1550	+ 8,850	+7000		
	34	31,600	5942 4525 4734 4190	026,06.	24.415	30,700	31,000	\$ 24.115	27.590	+2,760 +3,460 -9,540 +2,360			-6.475	926 + 926 -	+ 50	-6,175 -6,175	-	
	40		4970 2422 4748	-28.200	23.025	29.050	} } 29.625	\$ 22.450	24040	+2.160			-6.375	- 850 + 850	+ 175	+ 5,350 - 5,750	21.1936 M	
	41		3640	· 30,100 · 28,050 · 26,550 · 26,550 · 28,200	27.315	29.015	28125) 28.325	28,220	+ 1,880 - 170 - 1,670 - 20		3.220	- 825 + 825	+ 1.025 - 1.025	- 75	+1,775	JAN. 2 A	
	42		1728	29.900 30.200 v15,500 26.850		30.050	* 24,180	\$29,900	25610	+ 4,290 + 4,590 - 10,110 + 1,240		14,100	- 4,675	021- 021+	1 LO20 - 8,610 - 1,670	* 0	1	This gauge assembled with coppasions
	MEAN	0		26.470	23.085	29.860	28.850		26.400		14125	0.265	4490	203	* 1590	4.735		
							NOT CONS		AVERRGES I	WNES	20 VE							EXHIBIT "C"

RECAPITULATION - PRESSURE DATA SPECIAL GAUGES IN 3" A.A. SUMINA STANDA PLATED LINER #130

SELECTED PRESSURE GAUGES (MED. (AL); of per round, All assembling measuring etc by base ser un

1																	1 9
SERIAL	EXPECTED	MEDIUM	PRESSURE	MEN	HN OF	GAUGE	5 WITH	MEAN OF	NDW	MAX	MAN	- INVI	VIDUAL DIS	PERSION	WITH .	DATE	
OF ROUND	PRESSURE	GAUNE No.	# SEIN (075" MICK SPINDLE)	2000.0	D.ODIO" PISTON CL.	COPPER	WAX	GAUDES	DISPERSION PRESSURE	USPERSION GAJGES FIXED	GAUGES LOOSE	PISTON CL	O 0010" Piston ci	COPPER	WAX	OF FIRING	REMARKS
49	36,000 (4#-9120) 1492	5942 4525 4734 4190	· 34,000 · 33,950 · 20.800 · 38,975	29.890	33,475	36,460	27,400	31,930	+2070 +2020 -11,130 +7.045	13,175		-9185 +9.185	- 500 - 500 - 1375 - 1375 - 1375 - 1375 - 1375 - 1715 - 1715 - 1715 - 3450 - 3450 - 800 - 1330 - 1330 - 1330 - 3450 - 1330 - 1330 - 1300 - 1000 - 10	-2 515 +2515	+6600 -6.600		
02	Portei	4970 2422 4748 2834	-34.300 -37.050 -20.525 -35.600	28060	35,675	36.325	27,410	31 870	+7,430 +5,180 -11,245 +3,730	16.525		-7 540	- 1375 +1375	+ 725	+ 6.890 - 6,940	1936-	
51		\$908 3640 4744 4329	* 34.675 * 38, 100 * 33.600 * 38.775	36.190	36390	38.450	34/20	36.300	-1,625 +1.800 -2.700 +2.475		5,175	-2,585 +2,585	- 1715 +1715	-325 + 325	- 222 +	U A A	
52	· · .	4774 1728 4875 3259	-29.450 -37.350 -14.950 -36,975	26,960	33 400	37,160	22.200	29.700	- 250 +7,650 -14,750 +7,275		22 400	-10 015	- 3 450 + 3 950	+ (90	+ 7.250		
54	36.000	5442 4525 4734 4190	139.550 +41,150 122.600 142,700	32.650	} 40,350	1 41 925	21015	00196	+3050 +4650 -13,900 + 6,200	20.100		- 10.020	-800	- 775 +775	+8475 -8475		di se
22		4970 2422 4748 2834	-38,100 -37,100 -22.600 -37.400	30,00 •	38.600	38250	30350	34300	+3.800 +4.800 -11,700 +3,100	16.500		- 7.400 + 7.400	- 200	028 L	+7750 -7750	36	
56		5908 3640 4744 4329	140.800 -38,125 -38.600 -39.100	38.850	39.470	32610	39.700	39150	+1,650 -1,025 - 550 - 50		2675	- 250	+1,330 -1330	- 485 + 485	-1,100	JAN 28.15	
57		4774 1728 4875 3259	×30.900 ×38.800 ×21.00+ ×29.200	25,100	34:850	34000	\$25,950	29 975	+ 925 +8,825 - 8975 - 775		17,800	- 4100	- 3950 + 3950	+4400	- 4950 - 4950		
	36000		33700	30,960	36.600	37645	29.800	33,715		17.825	12,000	6.400	1700	1285	5450		
			1													H	EXHIBIT

RECAPITULATION - PRESSURE DATA SPECIAL GAUGES IN 3"A A GUN, M 3 - CHROMIUM PLATED LINER #138

SELECTED PRESSURE GAUGE - (MED.CAL); 4 per round, All assembling. measuring etc by GAUGE Sections

	1	2	3	4	2	6	7	8	4	10		12	13			1 16		18
1	SERIAL	EXPECTED	MEDIUM	PRESSURE	- MEAI	N OF GAU	bes wr	- H	MEANOP	INDIA	MAx	MAX	- 114 514	UNAL UN	ERSINI -	0.7H -	DATE	
	NUMBER	PRESSURE	CALIBER	# SQ.IN.		D.n.u."	CODER		ALL	INEAN DIS PERIN	CISPERSION	LISPERSION		0 0015	COUVER	WAX	OF	REMARK
	DF	# SQ.IN	GAUSE	(.075 MICR	PISTON CL	PISTON CL.	OBTION	OTURANA	IN	POPEL IPP	FILED	LONE	PLATOCICL	PISTON CL	OIST. CUPS	087	30.1936	
-		41,200	Caus	SPINDLE)		7	0.01.(0(3	1	KOOND	+ 530	reald		-	-2300		+5430	• • •	
	27	41,200	4525	142 200		40,400	8	32670	1	+11 890	13,903			+2 300	-250			
		(4=13-2)	4734	1225	lacut	,	142950	Y	731,810	- 10 515			- 7,990	12.0-		-5.430		
		X1492	4190	43200	3 22 213		ř		٦	+ 5,340			+ - 090		+ 250			
	60	POWDER	4970	42600	Fr	142775		3)	+4,185	16850			-175		+ 8,100	20	
	_		2422	142950		1	Summe	34,500	>38,415	+4,535				+175	+ 475		٩	
1			4748	-26100	\$ 34.050		142.413	Y	1	-12,315			- 7,950			- 8,100	02	
1			2834	-42000	5	,	3		2	+3,585			+ 1.950		-475		. m2	
0	61	C	5908	41050		41.025	,	1)	- 100		1,250		+ 25		+ 700	2 H	
1			3640	41000	2	J .	Julia	140,000	141.150	- 120			- 775	- 25	-420	200	4	
2			4744	40650	41.125		2	3	(- 300			+715		+450	~ 100	Í	
2	62		4329	33050	-)	2	2	5	-3790		02871		-5.150	1 4 6 0	+2.175		
51	62		4114	-42250		138,200	2	130,275	1. 200	+1 010		13,030		- 2 . 50	+ 950		1	
			4175	127500	1-1-1	2	142400	Y	236340	- 8.440			-6,925			-2.775		
5.			32.59	141450	34.4 13		y		5	+ 5,110			+6925		- 950		. 1	
1	64	41.200	5942	139,200		111200)	5	+ 3.850	21700		1	-2.100		+ 8,750	•	
1			4525	143.400		} 41.30 -	h	\$30,450	135450	+7.950				+2.100	+2.950			
6			4734	21.700	129600		\$ 40,450	\$	1	-13.750			- 7,900			- 8,750		
1			4190	37.500] =		٢)	+ 2.050			+7.900		- 2.950			
12	65		4970	142.350		\$ 41,600.	2	1)	+ 8,075	19.300			+750	1.000	+9.650	36	
3	1		2422	40.850	2	. د	235.850	132.100	> 34.275	+ 6.575			- 2 000	- 150	+2000	. 9150	9	
*			4748	23.050	26,950		V - I - I	5	1	-11,225			- 3,400		5000	- 9.630	0-	
<u>s</u> .	66		2834	- 30.030))	1.	<	- 750		4175	. + 0.100	0201-	- 31000	+1.435	nZ.	
			3700	44750		143,600	2	241515	1.000	+2050		-1,1 (3		+650	+1375		. u	
2			47441	40.075	1		42,875	Y	141.200	-2125			- 710			-1.435	Ť	
9	S		4329	- 41.500	40100		Y	٠	5	- 100			+ 710		-1.375		5.	
0	67		4774	32.500		22220r		3)	+ 210		11900		- 825		+ 3.600		
1	,		1728	021.4E		5 22.223	h	\$28.900	137 290	+1,860				+ 822	-1,525			
2			4875	25.300	31250		35,675	3	(- 6,990			- 5,950			-3600		
3			3259	37.200		_	1		2	+ 4.910			+ 5,950		+1 525		. Y .	
3 #					211.90	10000	10 510	24.55	27 -10		10 0	9300	5310	+ 750 - 250 - 020 + 650 + 825 + 825 + 825	16.22	4993		
5				51,240	24.180	40.220	40,510	34.000	21240		10.400.	0,000		1498	1011		·	
																		EXHIBIT

EXHIBITE

RECAPITULATION - PRESSURE DATA - PECIAL GAUGES IN 3"A A GUN MUS CAROMIDM PLATED LINER "132

DELECTED PRESTURE GAUGES (MEDIAL TVER ROUND ALL ASSEMBLING, MEALIRINGER BY DAVER SECTION

1	2	3	×	. 3	6	7	3	٣	10	"	1 =	13	/ *	15	15	12	· s
SERIAL	- EXPECTED	MEDIUM	PRESSURE	MEAN	OF GAL	DRES WITH										· JATE	51-+0+01+
	PRESSURE	CHUGE	15014 (075" MICR		.0010	COPPER	NAX	VALES	DISPERSING	17 A JUE -	LAX. LET	0.0005	0.0015	COPPER	WAX	FIRING	REMARKS
	+	NO.	SPINDLe)	PISTON CL	PISTONICL.	OBT CUPS	OBTURATOR	ROUND	PRESSU	FILED	7 D CJ. 1	PISTONICL	HSTONCL.	UBT CUPS	0BT +1000	A	
69	16,500 (2"-1403) X1492	4525 4734 4190	-16.450	}15675	\$ 17.000	16.875	15.900	16.340	002 + 007 + 0441 - 011 +			-775 +715	+100	+225	-1000		
70	PYRO	4748	- 17.950 - 17.850 - 13.700 - 13.450	13.575	\$ 17 900	\$ 15,825	15,825	15,740	+2,210 +2,110 -2,040 -2290			+125	02 + 02 ~	+2.025	-21122	1.1936 A.M	
וך		5408	- 17.575 - 17.500 - 16.875 - 16.875 - 19.600	15.740	} 17,540	17.225	17.2.25	16.640	+ 935 + 860 + 235		2975	+ 1,140 -1,140	+ 35 - 35 -	+215	+350 -350	UAN. 3	
72		4774 1728 4875	+ 16.150 - 16.200 - 11.200 - 14.925	213070	} 16,175	13,615	13.675	14620	042.1+ 05.1+ 05.1+ 205.4			-1.855 +1.855		1,250	+2.475		
75	16,500	4525 4734	17.300 17.150 14.800 14.800	} 15.375	} 17,225	\$ 16.050	16.050	16300	+ 1000 + 850 - 1.500 - 350	2350		-515 +575		+1.100	•1.220	4	
76		4970 2422 4748	18,700 18,475 14.850 10,950	\$ 12,900	} 18,590	\$14.715	16.775	15745	+2.955 +2,730 - ,895 - 4,995	7,750		+1,950 -1.950	+110	+3,765	-1,925	1436 -	
27		5908 3640 4744	* 18.000 • 17.350 • 17.150 • 17.150 • 15.250	\$ 16.200	\$ 17.675	\$ 16.300	17.575	16440	+1.060 + 410 + 210 - 1.690			+ 950 - 950	- 325	+1.050	- 425	AN SI.	
78		1728 4875	* 17.025 * 16.700 * 12.850 * 16,325	14.590	\$ 16.870	\$ 16.515	14.940	15.725	+ 1,300 + 975 -2,875 + 600		4,175	-1,740 +1,740		+ 185	-2090		
			16,050	14,640	17.370	16000	16 000	16.000		4200	3725	1140	111	1235	2690		
																	EXHIBIT "F"

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