1968

ARL 68-0180 OCTOBER 1968



Acrospace Research Laboratories

ON CUMULATIVE DAMAGE AND RELIABILITY OF COMPONENTS

V. K. MURTHY B. P. LIENTZ SYSTEMS DEVELOPMENT CORPORATION SANTA MONICA, CALIFORNIA

Contract No. F33615-67-C-1865 Project No. 7071



This document has been approved for public release and sale; its distribution is unlimited.

OFFICE OF AEROSPACE RESEARCH

United States Air Force



NOTICES

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government producements' operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

Agencies of the Department of Defense, qualified contractors and other government agencies may obtain copies from the

> Defense Documentation Center Cameron Station Alexandria, Virginia 22314

This document has been released to the



Copies of ABL Technical Documentary Reports should not be returned to Aerospace Research Laboratories unless return is required by security considerations contractual obligations or notices on a specified document.

500 - November 1968 - CO455 - 58-1321

从图1 68-0180

ON CUMULATIVE DAMAGE AND RELIABILITY OF COMPONENTS

V. K. MURTI B. P. LIENTZ

SYSTEMS DEVELOPMENT CORPORATION SANTA MONICA, CALIFORNIA

OCTOBER 1968

Contract No. F33615-57-C-1865 Project No. 7071

This document has been approved for public release and sale; its distribution is unlimited.

AEROSPACE RESEARCH LABORATORIES OFFICE OF AEROSPACE RESEARCH UNITED STATES A 7 FORCE WRIGHT-PATTERSON AIR FORCE BASE, OHIO

POREMORD

This report was prepared for the Applied Mathematics Research Laboratory, Aerospace Research Laboratories, Wright-Patterson Air Force Base, by Dr. V. K. Murthy and Dr. B. P. Lientz, System Development Corporation, under Contract F33-615-67-C-1865. In this report the authors develop the concepts of cumulative damage for general reliability and renewal wodels.

ABSTRACT

Let T, X(t), and C denote the time to failure, the accumulated damage by time t, and the "critical" damage. Let F be the distribution function of T. Let "E" stand for the event of the component undergoing damage and $\{t_n\}$ denote the sequence of intervals of time between successive occurrences of "E". Let $T_n = \sum_{i=1}^n t_i$ and Y_i denote the amount of damage experienced at time T_n . Assume $\{t_n, V_i\}$ is a sequence of independent, identically distributed variables with distribution function H(t, y), so that $\{t_n\}$ and $\{Y_n\}$ are renewal processes. The i requality $F(t) \leq H(t, \infty)$ is obtained with equality if and only if $C \neq 0$. For "E" a Poisson process, sufficient conditions are given for F to be IHR and DMR. The classes of distribution functions are considered with the topology of complete convergence. Empirical estimates for F from observing occurrences of "E" are given.

TABLE OF CONTENTS

SECTION

NAME.

PAGE

1.0	SUMMARY	1
2.0	INTRODUCTION	2
3.0	RENEWAL PROCESS DAMAGE HODEL	4
4.0	EMPIRICAL ESTIMATION OF F	9
5.0	CONDITIONS FOR DMR AND IHR	13
0.0	ASYMPTOTIC PROPERTIES OF CUMULATIVE DAMAGE X(t)	20
7.0	EXTENSIONS TO MULTICOMPONENT STRUCTURES	25
	818LIOGRAPHY	27

1.0 SUMMARY

Let T, X(t), and C denote the time of failure, the accumulated damage by time t, and the "critical" damage the component can withstand, respectively. Let "E" stand for the event of the component undergoing damage and $\{t_n\}$ denote the sequence of intervals of time between successive occurrences of "E". Let $T_n = \sum_{i=1}^n t_i$ and let y denote the amount of damage experienced at time T_n . Assume $\{t_n, y_n\}$ is a sequence of independent, identically distributed random variables with distribution function f(t, y), so that $\{t_n\}$ and $\{y_n\}$ are renewal processes with $X(t) = \sum_{n=1}^{N_t} y_n$, where N_t is the number of events by time t with respect to $\{t_n\}$. If G(t, x) is the distribution function of X(t), then F, the distribution function of T, can be expressed in terms of G and H. The inequality $F(t) < H(t, \infty)$ is obtained, with equality holding if and only if C ≡ 0. For "E" a Poisson process, sufficient conditions are given for F to be IHR and DMR. The classes of distribution functions are considered with the topology of complete convergence. Empirical estimates for F from observed occurrences of "E" are given. The asymptotic properties of F are examined. Generalizations are made to several types of multicomponent structures.

2.9 INTRODUCTION

In what follows, the word "device" is used to denote the given piece of equipment or hardware under consideration. At time t = 0, say, the device is put to use. As time passes by, the device steadily wears out until it fails or no longer performs the functions it should. Let T denote the time to failure. Let X(t) denote the accumulated wear out or damage the device has suffered by time t. X(t) is a random function of the argument t while T is a random variable. Let C denote the "critical" damage the device can stand. C is considered to be a constant without loss of generality. The inequality

(2.1)
$$X(t) > C$$

is now the event that by time t the accumulated damage the device has suffered is greater than the critical damage; in other words the device has failed by time t. Thus, (2.1) is the same event as $T \leq t$.

Let

(2.2)
$$P[X(t) \le x] = G(t, x)$$

and

(2.3)
$$P[T \le r] = F(t)$$
.

Then

(2.4) F(t) = 1 - G(t, C)

Equation (2.4) expresses the fundamental relationship between the accumulated damage X(t) and the time to failure T. Figure I illustrates these concepts.

• .



Figure I

3.0 RENEWAL PROCESS DAMAGE MODEL

Let 'E" stand for the event of the device undergoing damage. Let $\{t_i\}$ i = 1, 2, ..., denote the sequence of intervals of time between successive occurrences of "E". Let

(3.1)
$$T_n = t_1 + t_2 + \ldots + t_n, n = 1, 2, \ldots,$$

be the actual time instants corresponding to the occurrence of "E". In other words, T1, T2, T3, ..., are the successive instants of time when the device suffers damage. Let y_n denote the amount of damage the device experiences at time T_n , n = 1, 2, ... We will now assume that $\{t_n, y_n\}$ n = 1, 2, ..., is a sequence of independently, identically distributed random variables with the same distribution function H(t,y). Clearly now $\{t_n\}$, n = 1, 2, ..., and $\{y_n\}$, n = 1, 2, ..., are both ordinary renewal processes. Under this set-up the cumulative damage X(t) suffered by the device by time t is given by

(3.2)
$$X(t) = \sum_{n=1}^{N} y_n$$

(3.3)

where N_{t} is the number of events up to the specified time t with respect to the renewal process $\{t_n\}$. For the cumulative damage process X(t) given by (3.2) the corresponding distribution is given by

$$G(t,x) = P[X(t) \le x] = P\begin{bmatrix} N_t \\ \sum_{n=1}^{N} y_n \le x \\ n=1 \end{bmatrix} = 1 - H(t,\infty)$$

+
$$\int_{-\infty}^{\infty} \int_{0}^{t} G(t - t_1, x - x_1) dH_{t_1,x_1}(t_1,x_1)$$

ŏ

because $1 - H(t, \infty)$ denotes the probability that there is no event in the specified interval; that X(t) = 0 < x; in the remaining mutually exclusive cases, there is some first event in the interval and the last term on the right-hand side of (3.3) gives this probability.

If we use the fundamental relationship (2.4), the underlying law of failures associated with the cumulative damage process (3.2) is given by

(3.4)
$$F(t) = H(t, \infty) - \int_{-\infty}^{\infty} \int_{0}^{t} G(t - t_1, C - x_1) dH t_1, x_1(t_1, x_1).$$

Poisson Process for the Events "E"

We will now specialize (3.3) and (3.4) for the case of a Poisson process for the events "E" and discover some basic properties of the exponential law of failures. In this case

$$G(t, x) = P\left[\begin{array}{c} N_t \\ \sum_{n=1}^{N} y_n \leq x \end{array}\right]$$

(3.5)
$$= \sum_{n=0}^{\infty} P[N_t = n] P[y_1 + y_2 + \dots + y_n < x | N_t = n]$$

Since $H(\infty, x)$ denote the distribution of a y_i , we let $H^{(n)}(\infty, x)$ denote the n-fold convolution of $H(\infty, x)$ with itself. Also, since N_i is the number of

events in the interval (0, t) according to a Poisson process, say, with parameter λ

(3.6)
$$P[N_t = n] = \frac{e^{-\lambda t} (\lambda t)^n}{n!},$$

Hence

١

、

(3.7)
$$G(t,x) = \sum_{n=0}^{\infty} \frac{e^{-\lambda t} (\lambda t)^n}{n!} \quad \forall^{(n)} (\infty, x)$$

where

(3.8)
$$H^{(0)}(\infty, x) = \begin{cases} 0 \text{ for } x < 0 \\ 1 \text{ for } x \ge 0, \\ H^{(1)}(\infty, x) = H(\infty, x), \end{cases}$$

and for n > 1

$$H^{(n)}(\infty, x) = \int_{-\infty}^{\infty} H^{(n-1)}(\infty, x-z) dH(\infty, z)$$

Combining (3.7) and (3.8) we can write

(3.9)
$$G(t, x) = e^{-\lambda t} + \sum_{n=1}^{\infty} \frac{e^{-\lambda t} (\lambda t)^n}{n!} H^{(n)} (\infty, x)$$

From (2.4) and (3.9) we discover that in this case

(3.10)
$$F(t) = (1 - e^{-\lambda t}) - \sum_{n=1}^{\infty} \frac{e^{-\lambda t} (\lambda t)^n}{n!} il^{(n)} (\infty, C)$$

Equation (3.10) is a special case of equation (3.4) when the events "E" form a Poisson process. We will not interpret the fundamental implications of equations (3.4) and (3.10).

Let D stand for the event that by time t the device has experienced damage. Now

$$P(D) = (c_1 \leq t) = H(t, \infty).$$

Let A stand for the event that the device failed by time t and \overline{A} its complement. Clearly

D = (DA) U(DÃ)

• AU (DĀ), since AcD.

Hence,

. . .

(3.12)
$$P(D) = P(A) + P(D\tilde{A})$$

but

(3.13)
$$P(A) = F(t)$$

and

(3.14)
$$P(D\bar{A}) = \int_{-\infty}^{\infty} \int_{0}^{t} G(t - t_1, C - x_1) dH_{t_1, x_1}(t_1, x_1)$$

Thus equation (3.4) is clearly identical with equation (3.12).

We discover from (3.4) in the general case that

$$(3.15) F(t) \leq H(t, \infty),$$

the equality sign holding if and only if

$$(3.16)$$
 C = 0.

The condition (3.16) that the critical damage C is zero is equivalent to saying that the cumulative damage process X(t) is a constant independent of t, i.e., the device does not deteriorate due to damage or wear out. In this case the event "E" of the device undergoi. damage between t and t + dt is synony-mous with the event of the device failing between t and t + dt.

There has been a popular misconception that the exponential law of failures is characterized by the situation that the cumulative damage is independent of time. Equations (3.10), (3.15), and (3.16) now establish that when the cumulative damage process is constant in time, the underlying law of failures is identical with the distribution of the intervals between consecutive occurrences of "E" and is exponential only when the events "E" are Poisson.

4.0 EMPIRICAL ESTIMATION OF F

Let $H_k(.,.)$ denote the two dimensional empirical distribution function for H(.,.). That is, $H_k(t,x) = 1/n$ (number of observations (T_i, X_i) with $T_i < t$ and $X_i < x$).

This will then produce an ${\bf F}_{\bf k}$ where

$$F_{k}(t) = H_{k}(t, \infty) - \int_{-\infty}^{+\infty} \int_{0}^{\infty} G_{k}(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1}).$$

4.1 Theorem

Let G be a continuous function with respect to the usual product topology on E^2 . Then $F_k(t) + F(t)$ completely, or, in the sense of Feller, property.

Proof. One has

$$(4.1.1) |F_{k}(t) - F(t)| \leq |H_{k}(t, \infty) - H(t, \infty)| + \int_{-\infty}^{+\infty} \int_{0}^{t} G_{k}(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1}) + \int_{-\infty}^{+\infty} \int_{0}^{t} G(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1})|.$$

The first term in (4.1.1) tends to 0 since H_{k} is the empirical distribution function for H. For the second term one has

$$(4.1.2) \left| \int_{-\infty}^{+\infty} \int_{0}^{t} G_{k}(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1}) - \int_{-\infty}^{+\infty} \int_{0}^{t} G(t - t_{1}, C - x_{1}) dH(t_{1}, x_{1}) \right|$$

$$\leq \left| \int_{-\infty}^{+\infty} \int_{0}^{t} G(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1}) - \int_{-\infty}^{+\infty} \int_{0}^{t} G(t - t_{1}, C - x_{1}) dH(t_{1}, x_{1}) \right|$$

$$+ \left| \int_{-\infty}^{+\infty} \int_{0}^{t} G_{k}(t - t_{1}, C - x_{1}) - G(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1}) \right|$$

The first summand in (4.1.2) tends to 0 as $k \neq \infty$ by the two dimensional version of the Helly-Bray theorem. The second term in (4.1.2) is bounded by

(4.1.3)
$$\int_{-\infty}^{+\infty} \int_{0}^{t} \left| G_{k}(t - t_{1}, C - x_{1}) - G(t - t_{1}, C - x_{1}) \right| dH_{k}(t_{1}, x_{1}).$$

To show this tends to 0 and k tends to ∞ we first consider

$$\psi_{k}(a, t) = \int_{-a}^{a} \int_{0}^{t} g_{k}(t - t_{1}, C - x_{1}) dH_{k}(t_{1}, x_{1})$$

where

$$g_k(t - t_1, C - x_1) = |G_k(t - t_1, C - x_1) - G(t - t_1, C - x_1)|.$$

Expressing the finite multiple integral as the limit of Riemann-Stieljies sums and interchanging limits one obtains

$$\psi_k$$
 (a, t) + 0 as k + ∞ .

Hence,

$$\begin{array}{ccc} \text{Lim} & \text{Lim} & \psi_k (a, t) = 0 \\ a \to \infty & k \to \infty \end{array}$$

and since $g_{\mathbf{k}}$ is unded and $E_{\mathbf{k}}(.,.)$ is a distribution function, we obtain

In the particular case for the Poisson process one defines $G_k(t, x)$ by

(4.1.4)
$$G_{k}(t,x) = \sum_{n=0}^{\infty} e^{-\lambda t} \frac{(\lambda t)^{n}}{n!} H_{k}(n) \quad (\infty, x)$$

where $H_k(.,.)$ is the two dimensional empirical distribution function.

4.2 Theorem

With G_k as in (4.1.4) and G as in (3.3), $G_k(.,.)$ converges completely to G(.,.).

Proof. One first observes the following inequality

$$(4.2.1) \quad |G_{k}(t, x) - G(t, x)| \leq \sum_{n=0}^{\infty} e^{-\lambda t} \frac{(\lambda t)^{n}}{n!} | H_{k}^{(n)}(\omega, x) - H^{(n)}(\omega, x)|$$

For the right-hand side we employ Lemma 2, p. 252 of [1] which states that for π_k^{i} and $\pi_k^{$

$$\left|\left|\Re_{\mathbf{k}}^{(n)}(\mathbf{u}) - \Re^{(n)}(\mathbf{u})\right|\right| \leq n \left|\left|H_{\mathbf{k}}^{(\mathbf{u})}(\mathbf{u}) - \Re^{(n)}(\mathbf{u})\right|\right|$$

holds. If we let $k + \infty$ it follows that $H_k^{(n)} + H^{(n)}$ by theorem 1, p. 249 of [1]. Now by letting $k + \infty$ in (4.2.1), since the limit can be brought inside the summation sign, it can be seen that the right hand side tends to 0.

5.0 CONDITIONS FOR DMR AND IHR

In this section we assume $\{t_i\}$ forms a Poisson process and derive sufficient conditions for F, defined in (3.10), to be DMR (decreasing mean residual life) and IHR (increasing hazard rate). The section is concluded with an example whose derived F is IHR.

Set $p_n = H^{(n)}$ (\approx , C). Then one has the following theorem.

5.1 Theorem

A sufficient condition for F to be DMR is for the following inequalities to be satisfied for all N > M for some **positive integer** M.

(5.1.1)
$$\sum_{j=0}^{k} {\binom{k}{j}} p_{j} \left(\sum_{i=k-j+2}^{N} p_{i} \right) \leq \sum_{j=k-N+1}^{k} {\binom{k}{j}} p_{j+1} \left(\sum_{i=k-j+1}^{N} p_{i} \right)$$

for $0 \le k \le N-1$.

(5.1.2)
$$\sum_{j=k-N+2}^{N} {\binom{k}{j}} p_{j} \left(\sum_{i=k-j+2}^{N} p_{i} \right)^{\leq} \sum_{j=k-N+1}^{N-1} {\binom{k}{j}} p_{j+1} \left(\sum_{i=k-j+1}^{N} p_{i} \right)^{\leq}$$

for $N \leq k \leq 2N-2$.

Froof. The quantity we wish to consider is

(5.1.3)
$$\psi(t) = \frac{t}{1-F(t)} \frac{1}{1-F(t)}$$

tor t > 0.

To show this is non-increasing in t, we evaluate $\psi(t)$ by substituting the expression for F in (3.10) and obtain

(5.1.4)
$$\psi(t) = \frac{\sum_{n=0}^{\infty} \frac{p_n}{\lambda} e^{-\lambda t} \sum_{j=0}^{n} \frac{(\lambda t)^j}{j!}}{e^{-\lambda t} \sum_{n=0}^{\infty} \frac{(\lambda t)^n}{n!} p_n}$$

Without loss of generality we can assume $\lambda=1$. Differentiating ψ with respect to t one has $\psi^{+}(t) < 0$ if and only if

(5.1.5)
$$\left(\sum_{n=0}^{\infty} \frac{p_n t^n}{n!}\right) \left(\sum_{n=2}^{\infty} p_n \left(\sum_{j=0}^{n-2} \frac{t^j}{j!}\right) + \left(\sum_{n=1}^{\infty} p_n \left(\sum_{j=0}^{n-2} \frac{t^j}{j!}\right)\right) \left(\sum_{n=0}^{\infty} \frac{t^n}{n!}\right) \right) \left(\sum_{n=0}^{\infty} \frac{t^n}{n!}\right)$$

Now restrict the summations to finite summations for N > 2. One has

(5.1.6)
$$\left(\sum_{n=0}^{N} -\frac{p_{n}t^{n}}{n!}\right) \left(\sum_{n=2}^{N} -p_{n} -\sum_{j=0}^{n-2} -\frac{t^{j}}{j!}\right) s \left(\sum_{n=1}^{N} -p_{n} -\sum_{j=0}^{n-1} -\frac{t^{j}}{j!}\right)$$

$$= \sum_{n=0}^{N-1} -p_{n+1} - \frac{t^{n}}{n!} - \frac{t^{n$$

considering the coefficients of the polynomials one has for the left-hand side of (5.1.5)

(5.1.7)
$$\sum_{k=0}^{N-1} \sum_{j=0}^{k} \frac{p_{j}}{j!} \left(\sum_{i=k-j+2}^{N} \frac{p_{i}}{(k-j)!} \right) t^{k}$$
$$+ \sum_{k=N}^{2N-2} \sum_{j=k-N+2}^{N} \frac{p_{j}}{j!} \left(\sum_{i=k-j+2}^{N} \frac{p_{j}}{(k-j)!} \right) t^{k}.$$

For the right-hand side one has

(5.1.8)
$$\sum_{k=0}^{N-1} \sum_{j=0}^{k} \frac{p_{j+1}}{j!} \left(\sum_{j=k-j+1}^{N} \frac{p_{j}}{(k-j)!} \right) t^{k} + \sum_{k=N}^{2N-2} \sum_{j=k-N+1}^{N} \frac{p_{j+1}}{j!} \left(\sum_{j=k-j+1}^{N} \frac{p_{j}}{(k-j)!} \right) t^{k}.$$

Substituting the expressions in (5.1.7) and (5.1.8) into (5.1.6) and comparing coefficients one obtains (5.1.1) and (5.1.2).

5.2 Theorem

A sufficient condition for F to be IHR is for the following to hold for $N \ge M$ for some $M \ge 1$

(5.2.1)
$$\sum_{j=0}^{k} {\binom{k}{j}} p_{j+1} p_{k-j+1} \ge \sum_{j=0}^{k} {\binom{k}{j}} p_{j} p_{k-j+2}$$

for $0 \le k \le N-1$.

and

(5.2.2)
$$\sum_{j=k-N+1}^{N-1} {\binom{k}{j}} p_{j+1} p_{k-j+1} \ge \sum_{j=k-N+2}^{N} {\binom{k}{j}} p_{j} p_{k-j+2}$$

for N < k < 2N-2.

Proof. We wish to show

$$\frac{F(t+x) - F(t)}{1 - F(t)}$$
 is nondecreasing in t for $x > 0$.

Substituting for F one has

(5.2.3)
$$\psi_{\chi}(t) = 1 - \frac{e^{-\lambda x} \sum_{n=0}^{\infty} \frac{(\lambda(t+x))^n}{n!} p_n}{\sum_{n=0}^{\infty} \frac{(\lambda t)^n}{n!} p_n}$$

As in (5.1), we first can set $\lambda=1$ and then simplify by finding e^{X} $(1-\psi_{X}(t))$ which is

(5.2.4)
$$\phi_{x}(t) = e^{x}(1-\psi_{x}(t)) = \frac{\sum_{n=0}^{\infty} \frac{(t+x)^{n}}{n!} p_{n}}{\sum_{n=0}^{\infty} \frac{t^{n}}{n!} p_{n}}$$

We wish to derive conditions on $\{p_n\}$ so that the expression in (5.2.4) will be nonintreasing. Differentiating $\phi_x(t)$ with respect to t one has $\phi_x^{-1}(t) \ge 0$ if and only if

$$\sum_{n=0}^{\infty} \frac{t^n}{n!} p_n \left(\sum_{n=0}^{\infty} \frac{(t+x)^n}{n!} p_{n+1} \right) \leq \sum_{n=0}^{\infty} \frac{(t+x)^n}{n!} p_n \left(\sum_{n=0}^{\infty} \frac{t^n}{n!} p_{n+1} \right)$$

or, equivalently

(5.2.5)
$$\frac{\sum_{n=0}^{\infty} \frac{t^n}{n!} p_n}{\sum_{n=0}^{\infty} \frac{t^n}{n!} p_{n+1}} \leq \frac{\sum_{n=0}^{\infty} \frac{(t+x)^n}{n!} p_n}{\sum_{n=0}^{\infty} \frac{(t+x)^n}{n!} p_{n+1}}.$$

Since we are considering this expression for any x > 0, (5.2.5) will hold if and only if

$$\mu(t) = \frac{\sum_{n=0}^{\infty} \frac{t^n}{n!} p_n}{\sum_{n=0}^{\infty} \frac{t^n}{n!} p_{n+1}}$$

is nondecreasing in t. Differentiating $\mu(t)$ one has $\mu'(t) \ge 0$ if and only if

$$\left(\sum_{n=0}^{\infty} \frac{t^{n}}{n!} p_{n+1}\right)^{2} \geq \left(\sum_{n=0}^{\infty} \frac{t^{n}}{n!} p_{n}\right) \left(\sum_{n=0}^{\infty} \frac{t^{n}}{n!} p_{n+2}\right).$$

Restricting to finite summations. say N, one has

(5.2.6)
$$\left(\sum_{n=0}^{N-1} \frac{t^n}{n!} p_{n+1}\right)^2 \leq \left(\sum_{n=0}^{N} \frac{t^n}{n!} p_n\right) \left(\sum_{n=0}^{N-2} \frac{t^n}{n!} p_{n+2}\right)$$

The polynomial on the left-hand side of (5.2,6) is

(5.2.7)
$$\sum_{k=0}^{N-1} \sum_{j=0}^{k} \frac{1}{j!(k-j)!} p_{j+1} p_{k-j+1} t^{k} +$$

$$\sum_{k=N}^{2N-2} \sum_{j=k-N+1}^{N-1} \frac{1}{j!(k-j)!} p_{j+1} p_{k-j+1} t^{k}$$

and the polynomial on the right side of (5.2.6) is

$$(5.2.8) \qquad \sum_{k=0}^{N-1} \left[\sum_{j=0}^{k} \frac{1}{j!(k-j)!} p_{j} p_{k-j+2} \right] t^{k} + \sum_{k=N}^{2N-2} \left[\sum_{j=k-N+2}^{N} \frac{1}{j!(k-j)!} p_{j} p_{k-j+2} \right] t^{k}.$$

Comparing respective coefficients in (5.2.7) and (5.2.8) one obtains the statement of the theorem.

5.3 Example

An example of a distribution function F satisfying (5.1.1), (5.1.2), (5.2.1), and (5.2.2). Assume (y_j) are independent, ident. ally distributed random variables with common distribution function exponential with, say, parameter 1. Then p_n is given by

(5.3.1)
$$p_{n}(x) = p\left[\sum_{j=1}^{n} y_{j} \leq x\right] = 1 - e^{-x} \left[\sum_{j=0}^{n-1} \frac{x^{j}}{j!}\right]$$

That the expressions in the statements of the theorems 5.1 and 5.2 are satisfied can be seen by direct substitution.

6.0 ASYMPTOTIC PROPERTIES OF CUMULATIVE DAMAGE X(t)

(6.1)
$$G(t, x) = P[X(t) \le x] = P\left[\sum_{n=1}^{N} \frac{Y_n}{n} \le x\right]$$

= 1 - H't,
$$\infty$$
) + $\int_{-\infty}^{\infty} \int_{0}^{t} G(t - t_{1}, x - x_{1}) d_{t_{1}, x_{1}} H(t_{1}, x_{1})$

For the renewal process $\{t_n, y_i\}$, n = 1, 2, ..., with common distribution H(t, y), let

$$\mu_{\mathbf{r}} = E\left(\mathbf{t}_{n}^{\mathbf{r}}\right)$$

$$\nu_{\mathbf{r}} = E\left(\mathbf{y}_{n}^{\mathbf{r}}\right)$$

$$\mu_{\mathbf{ij}} = E\left(\mathbf{t}_{n}^{\mathbf{i}}\mathbf{y}_{n}^{\mathbf{j}}\right)$$

Define the transform

Sugar-

(6.2)
$$H^{\star}(\mathbf{s},\theta) = \int_{0}^{\infty} \int_{-\infty}^{\infty} e^{-\mathbf{s}t+\mathbf{i}\theta \mathbf{y}} d_{\mathbf{t},\mathbf{y}} H(\mathbf{t},\mathbf{y})$$

Applying the transform (6.2) to both sides of equation (6.1) we obtain

(6.3)
$$G^{*}(s, \theta) = 1 - H^{*}(s, 0) + G^{*}(s, \theta) H^{*}(s, \theta)$$

Hence

(6.4)
$$G^{*}(s, \theta) = \frac{1 - H^{*}(s, \theta)}{1 - H^{*}(s, \theta)}$$

Noting that the left hand side of equation (6.4) is the characteristic function of the distribution function $G^{*}(s, y)$ and that for the real part of s greater than zero, the right hand side is differentiable with respect to θ , we obtain that the first absolute moment of $G^{*}(s, y)$ is finite and

(6.5)
$$i \int_{-\infty}^{\infty} y d_y G'(s, y) = \frac{(1 - H^*(s, 0))H^{*'}(s, 0)}{(1 - U^*(s, 0))^2} |_{0} = 0$$

= $\frac{i R^*(s)}{1 - H^*(s, 0)}$

where the symbol prime denotes differentiation with respect to θ and

(6.6)
$$R^{\star}(\mathbf{s}) = \frac{1}{\mathbf{i}} H^{\star'}(\mathbf{s}, \theta) \Big|_{\theta = 0}$$

If v_1 , v_2 and v_{11} are finite, we obtain from Murthy [2] that

(6.7)
$$\int_{-\infty}^{\infty} y \, d_y G^{\dagger}(s, y) = \frac{R^{\dagger}(s)}{1 - H^{\dagger}(s, 0)}$$
$$= \frac{v_1}{\mu_1 s} + \frac{v_1 \mu_2}{2\mu_1^2} - \frac{\mu_{11}}{\mu_1} + 0(1), \text{ as } s + 0$$

Since the left-hand side of equation (6.7) is the Laplace-Stieltjes transform (L-S.T) of E(X(t)), we obtain that

(6.8)
$$E(X(t)) = t \frac{v_1}{v_1} + \frac{v_1v_2}{2v_1^2} - \frac{v_{11}}{v_1} + O(1), \text{ as } t \to \infty.$$

Similarly

(6.9)
$$-\int_{-\infty}^{\infty} y^{2} d_{y}G^{*}(\mathbf{s}, \mathbf{y}) = \frac{H^{*}(\mathbf{s}, \theta)}{1 - H^{*}(\mathbf{s}, 0)} + \frac{2}{2} \frac{H^{*}(\mathbf{s}, \theta)}{\left[1 - H^{*}(\mathbf{s}, 0)\right]^{2}}^{2}$$

$$-\frac{q^{(s)}}{1-H(s,0)} + 2 \frac{[iR^{(s)}]^2}{[1-H(s,0)]^2}$$

where

$$Q^{\star}(\mathbf{s}) = -H^{\star}(\mathbf{s}, \theta)$$
 is the L-S.T
 $\theta = 0$

$$Q(t) = \int_{-\infty}^{\infty} y^2 d_y H(t, y).$$

Hence

of

(6.10)
$$\int_{-\infty}^{\infty} v^2 d_y G^*(s, y) = \frac{0(s)}{1 - H^*(s, 0)} + \frac{2[R^*(s)]^2}{[1 - H^*(s, 0)]^2}$$

If ν_2 , ν_3 , μ_{21} and μ_{12} are finite, we obtain after a straightforward calculation that

(6.11)
$$E\left(X^{2}(t)\right) = \frac{\sqrt{2}}{2}t^{2} + t\left(\frac{2u_{2}^{-}v_{1}^{2}}{u_{1}^{-3}} - \frac{4v_{1}u_{11}}{u_{1}^{-2}} + \frac{v_{2}}{u_{1}}\right)$$

+ $\frac{3v_{1}^{-}2u_{2}^{-2}}{2u_{1}^{-4}} - \frac{2v_{1}^{-2}u_{3}}{3u_{1}^{-3}} + \frac{2u_{1}^{-2}}{u_{1}^{-2}} + \frac{2v_{1}u_{21}}{u_{1}^{-2}}$
- $\frac{4v_{1}u_{11}u_{22}}{u_{1}^{-3}} + \frac{u_{2}^{-}v_{2}}{2u_{1}^{-2}} - \frac{u_{12}}{u_{1}^{-2}} + 0(1), \text{ as } t + \infty.$

Combining (6.8) and (6.11) we finally discover that

ţ

(6.12)
$$\operatorname{Var} (X(t)) = t \left(\frac{v_2}{\mu_1} + \frac{v_1^2 u_2}{\mu_1^3} - \frac{2v_1 \mu_{11}}{\mu_1^2} \right) \\ + \frac{5v_1^2 u_2^2}{4\mu_1^4} - \frac{2v_1^2 u_3}{3\mu_1^3} - \frac{3v_1 \mu_{11} \mu_2}{\mu_1^3} + \frac{\mu_{11}^2}{\mu_1^2} \\ + \frac{2v_1 \mu_{21}}{\mu_1^2} + \frac{\mu_2 v_2}{2\mu_1^2} - \frac{\mu_{12}}{\mu_3} + 0(1), \text{ as } t \neq \infty.$$

7.0 EXTENSIONS TO MULTICOMPONENT STRUCTURES

In the previous section the damage y_n was considered a scalar. In the case of a general structure consisting of m components, at each occurrence of E, say, at time $T_n = t_1 + t_2 \dots + t_n$, the damage the structure suffers can be denoted by an m dimensional random vector.



The assumption in this case is that the sequence $\{t_n, y_n\}$, n = 1, 2, ... is a renewal process with a common (m+1) dimensional distribution given by

(7.2)
$$P\{t_n < t, y_n < y\} = H(t, y_1, y_2, ..., y_m).$$

The corresponding m dimensional damage process is then

(7.3)
$$\begin{pmatrix} x_{1}(t) \\ x_{2}(t) \\ \vdots \\ \vdots \\ x_{m}(t) \end{pmatrix} = \begin{pmatrix} N_{t} \\ \Sigma \\ n=1 \\ N_{t} \\ y_{2n} \\ n=1 \\ \vdots \\ N_{t} \\ \Sigma \\ n=1 \\ y_{mm} \end{pmatrix}$$

Now the m dimensional joint distribution of life lengths of the m components is given by

(7.4)
$$F(t_1, t_2, ..., t_m) = P[X_1(t_1) > C_1, ..., X_m(t_m) > C_m],,$$

where C_i , i = 1, 2, ..., m is the critical threshold for the ith component of the structure.

Using procedures similar to the single component situation, we can obtain explicitly $F(t_1, t_2, ..., t_m)$ in terms of $H(t, y_1, y_2, ..., y_m)$ and its convolutions evaluated at the critical threshold. Also, the mean vector and the variance-covariance matrix of the m dimensional cumulative damage process $X(t_m)$ can be easily evaluated.

BIBLIOGRAPHY

- [1] Feller, William. An Introduction to Probability Theory and its Applications, Vol. II New York: John Wiley and Sons, 1966.
- [2] Murthy, V.K. On the General Renewal Process, Ph.D. Thesis, University of North Carolina, Chapel Hill, N.C., 1960

DOCUMENT	CONTROL DATA - R	& D				
(Security classification of title, bady of abstract and is			areasti report in Laozoffody			
ORIGINATING ACTIVITY (Caspande aufor)		3. REPORT BECURITY CLASSIFICATION				
System Development Corporation		Unclassified				
Santa Monica, California 90406	DA. SROUP					
BEPORT TITLE						
On Cumulative Damage and Reliabilit	v of Components					
DE TRIPTIVE NOTEL (Type of report and technolog entre) Scientific. Interim.						
Scientific, Interim.						
V. K. Marthy and B. P. Lientz						
•						
REPORT DATE	TE TOTAL HO O	PPACES	TA. NO. OF REFT			
October 1968	32		2			
F33-615-67-C-1865	NO. ORIGINATOR	S REPORT NUR	#85\${9}			
A PROJECT NO	SP-3	199				
7071		C4 - 51 55				
• Dob Element 61102F	B. OTHER REPO this report)	RT NO(S) (Aug	cher madere fuel may be coolgood			
4 DoD Subelement 681304	ARL	ARL 68-0180				
O. DISTRIBUTION STA EMENT	1		a a a a a a a a a a a a a a a a a a a			
1. This document has been approved	for rublic relea	co hao co	10.			
its distribution is unlimited	TOT PROTIC TETES	30 alal 3a.	10.			
1. SUPPLEMENTARY NO TTS	12 SPONSO 31KG	MILITARY ACT	{ ¥ } T Y			
	Aerospace	Research i	Laboratories (ARM)			
Tech Other	Office of	Office of erospace Research, USAF				
3 8037840 7	Wright-Par	terson AF	B, Ohio 45433			
Lat T, X(t), and C denote the time to	failure, the acc	umulated of	dawage by time t. and			
the "critical" damage. Let F be the	-		•			
-						
the event of the component undergoing			*1			
intervals of time between successive of	occurrences of "E	Let T	$= \frac{1}{1} t_i$ and Y_i			
denote the amount of damage experience	ed at time T ₂ . A	ssume (t	Y is a sequence			
of independent, indentically distribut		···•				
so that (t_n) and $\{Y_n\}$ are renewal proc						
5 A.						
with equality if and only if C=0. For						
are given for F, to be IHR and DMR. 1						
considered with the topology of comple	ete convergence.	Empirical	l estimates for F			
from observing occurrences of "E" are	given.					

.

Unclassified Security Classifics. ... Inclase if ini Sourity Classification

KEY WORDS		LINK 2		× 3	LINK C	
	ROLE	* *		4 T	ROLE	**
locumulated damage						
lomplete convergence topology			•	ł		
Increasing hazard rate						
Decreasing mean residual life	Ì					
Proper convergence						
		•				
		, į				
		1			Ì	
		-				
						Ì
	9 					ł
						}
			1 1			
	1					
				1		
]]
		ł				
	1					
		l				{
				[l
		1	1		1	

Security Classification

.