

AD 678567

**Gulf General Atomic**  
Incorporated

P. O. Box 603, San Diego, California 92112

*Reports Distribution  
File Copy*



GAMD-8497

Category A

AN EULERIAN METHOD FOR CALCULATING STRENGTH  
DEPENDENT DEFORMATION

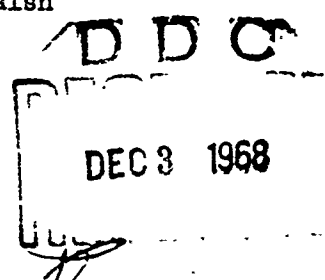
          
PART THREE

Work done by:

J. K. Dienes  
M. W. Evans  
L. J. Hageman  
W. E. Johnson  
J. M. Walsh

Report written by:

J. K. Dienes  
M. W. Evans  
L. J. Hageman  
W. E. Johnson  
J. M. Walsh



This document, which was prepared primarily for internal use at Gulf General Atomic, may contain preliminary or incomplete data. It is informal and is subject to revision or correction; it does not, therefore, represent a final report.

**This document has been approved for public release and sale; its distribution is unlimited.**

Advanced Research Projects Agency  
ARPA Order No. 71-62  
Ballistic Research Laboratories  
Contract No. DA-04-495-AMC-1481(X)  
GGA Project 6003

February 2, 1968

Reproduced by the  
CLEARINGHOUSE  
for Federal Scientific & Technical  
Information Springfield Va 22151

AN EULERIAN METHOD FOR CALCULATING STRENGTH  
DEPENDENT DEFORMATION

by

J. K. Dienes, M. W. Evans, L. J. Hageman,  
W. E. Johnson, and J. M. Walsh

PART THREE

THE FORTRAN IV PROGRAM AND INSTRUCTIONS FOR ITS USE

by

J. K. Dienes, M. W. Evans, L. J. Hageman,  
W. E. Johnson, and J. M. Walsh

## TABLE OF CONTENTS

1.	INTRODUCTION . . . . .	1
2.	DESCRIPTION OF THE PROGRAM . . . . .	3
	2.1 RPM . . . . .	3
	2.2 INPUT . . . . .	3
	2.3 CARDS . . . . .	7
	2.4 SETUP . . . . .	7
	2.5 CDT . . . . .	7
	2.6 ES . . . . .	8
	2.7 EDIT . . . . .	8
	2.8 MAP . . . . .	10
	2.9 PH1 . . . . .	10
	2.10 PH3 . . . . .	10
	2.11 PH2 . . . . .	10
	2.12 REZONE . . . . .	10
	2.13 ERROR . . . . .	11
	2.14 TAPE DUMPS . . . . .	11
3.	SET-UP OF PROBLEMS . . . . .	12
	3.1 Definition of RPM Input Variables . . . . .	13
	3.1.1 Identification . . . . .	13
	3.1.2 Dimensions . . . . .	14
	3.1.3 Projectile . . . . .	15
	3.1.4 Target . . . . .	15
	3.1.5 Sphere . . . . .	16
	3.1.6 Filler . . . . .	16
	3.1.7 Physical Constants . . . . .	16
	3.1.8 Calculational Constants . . . . .	17
	3.1.9 Output . . . . .	21
	3.1.10 Stopping . . . . .	22
	3.2 Format and order of OIL-RPM Input Cards . . . . .	22
	3.3 OIL-RPM Input for "Special Setups" . . . . .	23
4.	SAMPLE PROBLEM . . . . .	27
	4.1 OIL-RPM Output . . . . .	32
	4.2 UNIVAC 1108 Control Cards . . . . .	41

TABLE OF CONTENTS (Continued)

5.	RESTART OF PROBLEMS . . . . .	42
6.	LISTING OF THE FORTRAN IV PROGRAM . . . . .	45
7.	DICTIONARY . . . . .	138
	APPENDIX A . . . . .	169
	APPENDIX B . . . . .	171



## 1. INTRODUCTION

In PART ONE of the OIL-RPM report the equations of motion were derived from first principles and discussed from a fundamental point of view. PART TWO then described the difference equations, the equation of state, the constitutive equations and the differencing scheme for velocity gradients used in formulating the FORTRAN IV program. Here, in PART THREE, the computer program is listed in detail and the general information necessary to set up and run problems is provided. A dictionary of terms used in the program is also included, as well as a number of tables and charts describing the program in outline form. Forms for setting up a sample problem are also given. This information provides the user with a capability to run his own problems and, in addition, the intent is to describe the code in enough detail that any changes the user may require can be readily made.

The program is the result of contributions by quite a number of people whose names are cited in the references. Briefly, the techniques described here originated from the PIC particle-in-cell method developed at Los Alamos by Evans and Harlow<sup>(1)</sup> and programmed in machine language. The code was rewritten in FORTRAN and modified for application in the ORION program by Johnson<sup>(2)</sup> and the General Atomic version was called SHELL. At the suggestion of B. E. Freeman a continuous version was developed by Walsh and Johnson<sup>(3)</sup> for the solution of hypervelocity impact problems and called OIL. It made use of the equation of state programmed by Tillotson<sup>(4)</sup>. To develop OIL, the particles were replaced by a continuously varying mass in each cell. The capability to run multi-material problems could not be conveniently retained (the particles in PIC could be of different materials). However, the cost of running problems was significantly reduced and the flow profiles were substantially smoother, making it practical to run impact and explosion problems out to a time when the shock pressure was down to a few kilobars. The lowest pressure that could be resolved with PIC was several hundred kilobars.

In order to compute crater size from an impact directly, the shear strength of the cratered material had to be accounted for. The necessary changes to OIL were made in an experimental way by Johnson, Walsh, and Dienes in 1965. This modified version of OIL was called OIL-RPM.<sup>(5)</sup>

Subsequently, when it had been shown that crater size could be calculated with satisfactory accuracy, the program was streamlined by the authors so it could be used in production runs, and additional editing features were incorporated. The current version has been used in calculating over 50 different problems and the results have generally compared well with experiments, analytical solutions and other hydrodynamic codes.

## 2. DESCRIPTION OF THE PROGRAM

The equations of motion are integrated in Phases 1, 2 and 3 which account for the effect of pressure, transport, and shear stresses respectively. In addition to these subroutines, ten others have been introduced for the various peripheral tasks. These include INPUT, SETUP, CARDS, CDT (computes time step), EDIT, MAP (provides displays), ES (equation of state), REZONE and ERROR. "RPM" is used to denote both the routine controlling the main flow and the entire program; the choice is generally made clear by the context. A summary of the subroutines is given in Table 1 in the order in which they appear in the listing provided in Section 6. Included in the table are the names of the subroutines calling and called by each of the others. A few general comments are made in the paragraphs below on each of the subroutines.

### 2.1. RPM

The overall flow of the program is controlled by RPM, as shown in the flow chart of Fig. 1. RPM controls whether additional information is printed at intermediate phases of the calculation cycle for diagnostic purposes and debugging. The variable "INTER" controls these intermediate prints. When INTER = 0, no intermediate prints are made. When INTER  $\neq$  0 EDIT is called and on print cycles EDIT prints are made after PH1 and PH3 as well as after CDT. Details of the Phase 2 calculation are obtained in addition to the EDIT prints by putting INTER = 7, which causes printing of the energy and mass transported as each cell is processed. For debugging of Phase 3 difficulties one puts INTER = 99 and thereby obtains detailed prints of stresses, strain rates and a few other parameters. These options should be used with extreme caution since an intermediate print uses considerable paper.

### 2.2. INPUT

Instructions for running problems are interpreted by INPUT, which can either start or restart a calculation. It calls SETUP and CARDS, as necessary, to prescribe the initial conditions and to read the input deck. A flow chart showing the relation of INPUT, CARDS, and SETUP is provided in Fig. 2.

TABLE 1  
ORDER OF SUBROUTINES

Name	Called From	Calls
RPM	--	INPUT, CDT, EDIT PH1, PH2, PH3
INPUT	RPM	SETUP, CARDS
CARDS	INPUT, SETUP	--
SETUP	INPUT	CARDS, ERROR
CDT	RPM, EDIT	ES, ERROR
ES	CDT	--
EDIT	RPM, ERROR	MAP, REZONE, ERROR, CDT
MAP	EDIT	--
PH1	RPM	--
PH3	RPM	--
PH2	RPM	ERROR
REZONE	EDIT	--
ERROR	SETUP, CDT EDIT, PH2	EDIT

FLOW OF THE CONTROL SUBROUTINE "RPM"

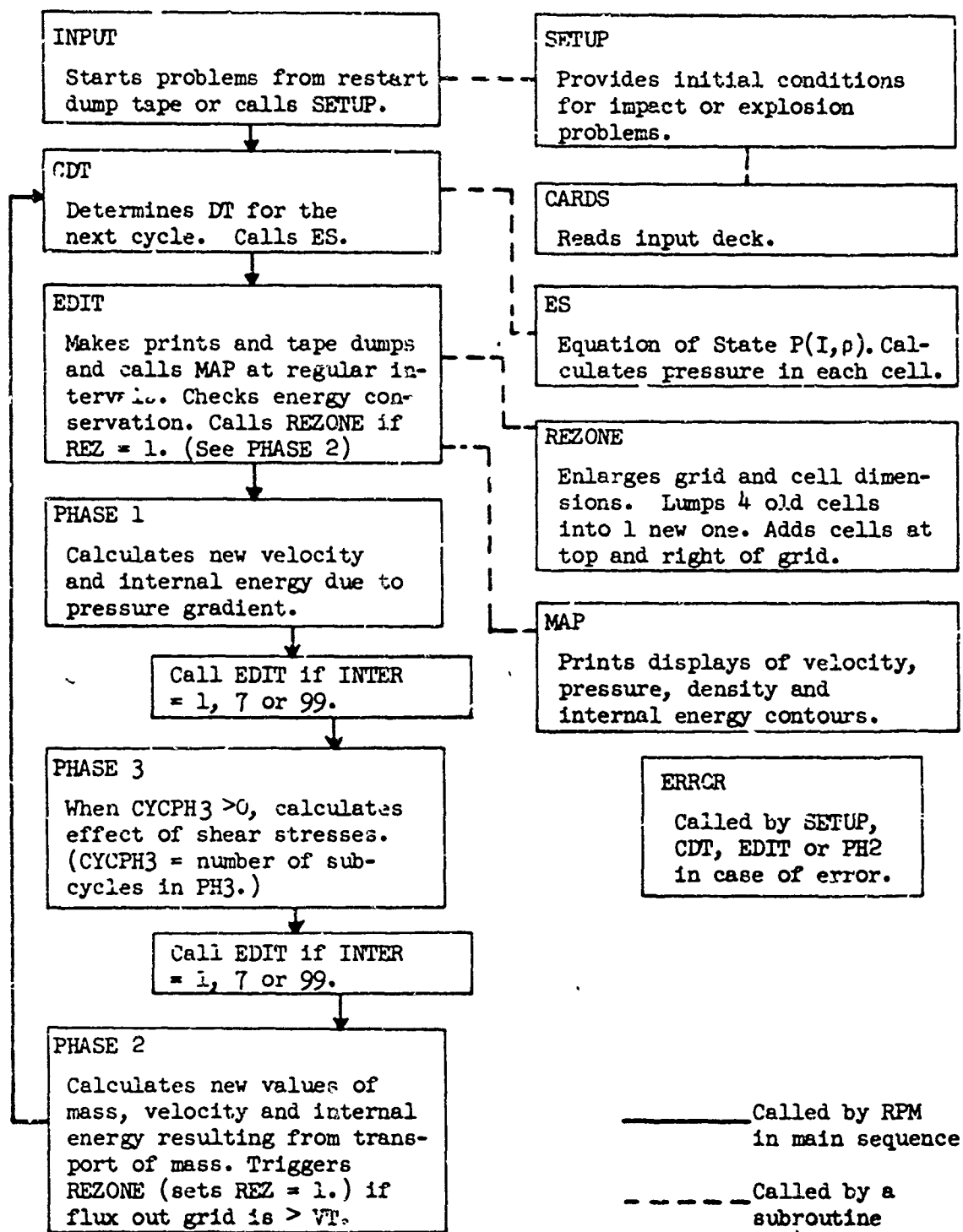


Fig. 1--Flow chart of main sequence

## FLOW DIAGRAM OF INPUT, CARDS AND SETUP

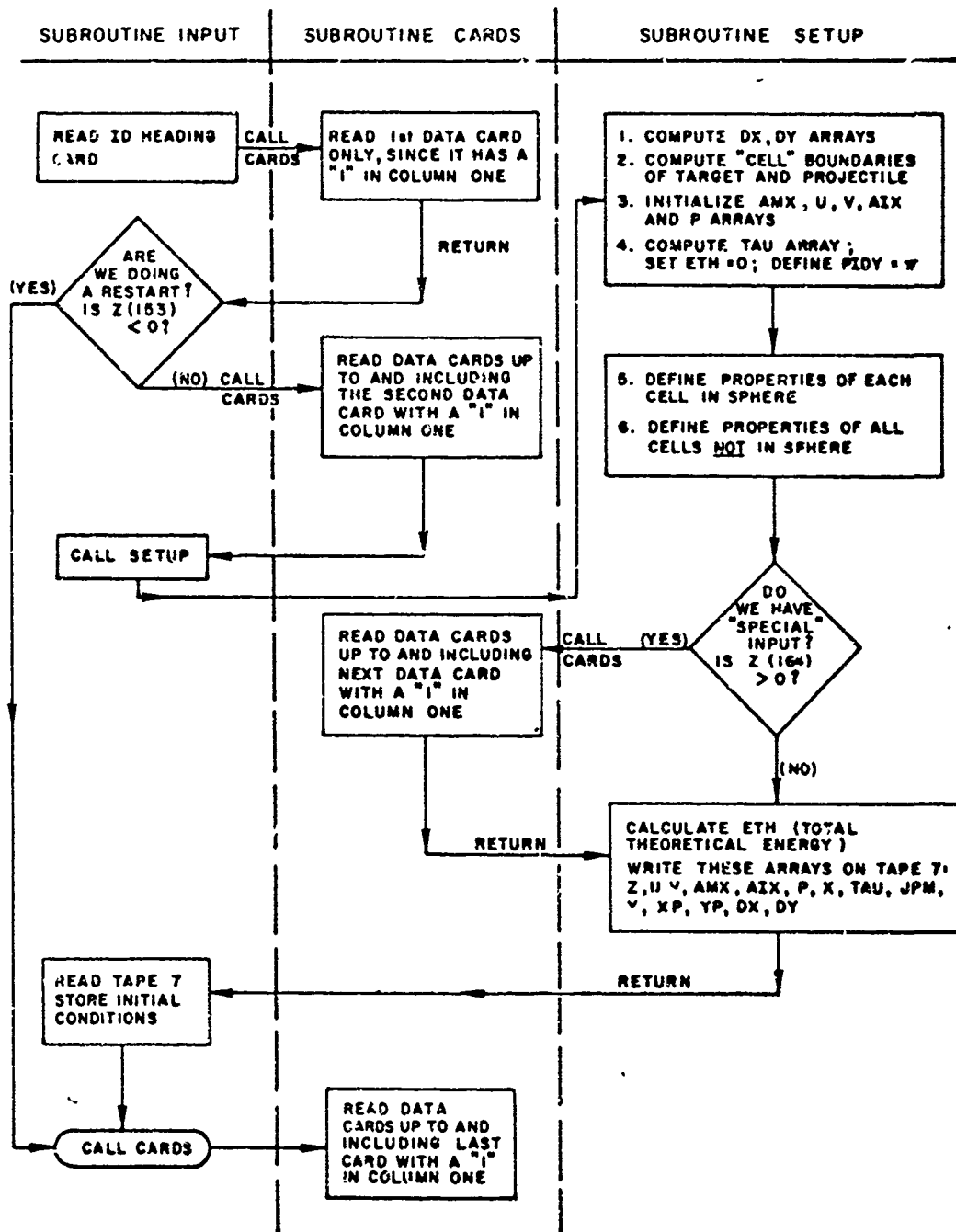


Fig. 2

### 2.3. CARDS

The reading of the input deck is called by this simple subroutine. Details are given in Fig. 2.

### 2.4. SETUP

The initial conditions for running problems are generated by SETUP. The most commonly used options are those in which a sphere or a cylinder (called the projectile) hits a target of finite thickness. The target of infinite thickness is an important special case. Another option is a geometry in which a sphere hits a thin plate (called the projectile) which has a filler behind it (typically void or of underdense "foamy" material) and then hits a second thin plate behind the filler. Further details are given in Section 3 describing how to set up various problems.

In an earlier report<sup>(3)</sup> describing the OIL code a description and FORTRAN listing of a special generator code, CLAM, was given. This program provides a very general method for specifying initial conditions and for setting up OIL-RPM problems. A few changes in CLAM are required to make the write statements for the CLAM dump tape compatible with the READ statements in OIL-RPM.

### 2.5. CDT

The principal function of this subroutine is to compute a time step which ensures stability of the finite difference equations. This is done by finding the minimum of  $D/w$  for all the cells. Here  $D$  denotes the minimum of the radial and axial cell dimensions, and  $w$  denotes the maximum of the radial velocity, axial velocity and sound speed. For vaporized material sound speed is computed by  $\sqrt{\gamma p/\rho}$  and for solid materials by the approximate relation  $C = C_0 + \bar{B} \sqrt{p}$  where  $p$  is the pressure in the cell. The coefficient  $\bar{B}$  is obtained by determining a typical slope for the isentropes in Ref. 4 and using the relation

$$C = V \sqrt{-\partial p / \partial V}$$

to evaluate  $\bar{B}$  at a particular point. The pressure array is updated in CDT by calling the equation of state subroutine ES.

The array JPM(I) which determines the location of the pressure maximum and hence the cells on which deviator stresses act is also computed in CDT.

Unrealistic behavior in free surface cells containing a small amount of mass would occur, in the absence of a special treatment, when a neighboring cell has a high pressure. This causes large accelerations of the mass in the cell containing a free surface, and eventually velocities which are physically unrealistic. This difficulty is alleviated by reducing the pressure computed by the equation of state by a factor which is the ratio of the smallest mass in an adjacent cell to the mass in the cell itself. This factor reduces the pressure at the interface to a value which accounts for the position of the free surface.

#### 2.6. ES

The equation of state subroutine is called by CDT to evaluate the pressure as a function of density and internal energy. The general method was originally described in Ref. 4, but a number of modifications have been made since that report was written. A general discussion is given in Section 4 of PART TWO. Values of the parameters for a number of materials are listed in Table 2. Parameters for some materials not given in Ref. 4 are supplied in Refs 6 and 7.

#### 2.7. EDIT

The pressure, velocities, density, specific internal energy, and mass for each cell are displayed by EDIT in a "long" print. It also prints out the total internal energy, kinetic energy, axial and radial momentum and mass above and below a dividing line which is the top of the cell whose J index is JPROJ. The changes in energy due to evaporation and losses out the boundaries are also accounted for in the EDIT prints. The crater depth is calculated by "packing down" material in each column to its normal density. This describes in a rough way the extent of the crater even while it still contains low density material.

"Short" EDIT prints display the integrated quantities, and the cell variables for the one column of cells that is adjacent to the axis. These



TABLE 2

EQUATION OF STATE CONSTANTS FOR SEVERAL MATERIALS.

	a	b	A dynes/cm <sup>2</sup>	B dynes/cm <sup>2</sup>	E <sub>0</sub> ergs/g	n	β	E <sub>s</sub>	ρ g/cm <sup>3</sup>	E'ε
W	.5	1.04	3.08 x 10 <sup>12</sup>	2.5 x 10 <sup>12</sup>	.225 x 10 <sup>12</sup>	10	10	1.11 x 10 <sup>10</sup>	19.17	5.6 x 10 <sup>10</sup>
Cu	.5	1.5	1.39	1.1	.325	5	5	1.38	8.9	6.9
Fe	.5	1.5	1.28	1.05	.095	5	5	2.44	7.9	10.2
Al	.5	1.63	.75	.65	.05	5	5	3.0	2.7	15.0
Be	.55	.62	1.7	.55	.175	5	5	10.0	1.8	45.0
Tl	.5	.60	1.03	.5	.07	5	5	3.5	5.5	12.5
Ni	.5	1.33	1.51	1.5	.09	5	5	2.95	8.9	9.4
Mo	.5	1.02	2.11	1.55	.045	5	5	2.2	10.2	9.0
Th	.4	.86	.53	.5	.025	9	.88	2.0	11.7	
Granite*	.5	1.3	.18	.18	.16	5	5	3.5	2.7	.13 x 10 <sup>-2</sup>
Andesite*	.5	1.3	.18	.18	.15	5	5	3.5	2.7	.15
Wet Tuff	.5	1.3	.10	.06	.11	5	5	3.2	2.0	.16
Dry Tuff	.5	1.3	.045	.03	.06	5	5	3.2	1.7	.18
Oil Shale	.5	1.0	.28	.11	.11	5	5	3.2	2.3	.15
Dolomite	.5	.5	.85	.30	.10	5	5	2.5	2.8	.14
Limestone	.5	.6	.4	.67	.10	5	5	2.5	2.7	.14
Ball's	.5	.6	.25	.30	.05	5	5	2.0	2.2	.15
CH <sub>2</sub>	.6	2.0	.075	.024	.07	10	5	2.4	.9	16.0
Pb	.4	2.4	.466	.0026	.02	10	2	.26	11.3	.97

\*These fits include additional parameters

short prints require only a few pages of printing, and hence are normally called for at more frequent intervals than the "long" prints.

Tracer points are positioned at the center of every other cell in SETUP, and the positions of these points are updated in PH2. The current position of each tracer point is printed in both the long and the short prints, providing the basis for a Lagrangian description of the flow. The positions are written on the restart dump tape and can be used by plot routines to make a plot of material deformation.

#### 2.8. MAP

This subroutine is called by EDIT and displays the properties of each cell in the active grid using an alphabetic scale. One obtains contour maps of the density, pressure, radial and axial velocities, and internal energy in the active grid.

#### 2.9. PH1

The effect of the pressure gradient in updating the velocities and the internal energy is computed here. The calculation method is described in detail in Section 3.2 of PART TWO.

#### 2.10. PH3

The deviator stresses acting on each cell edge and the hoop stress are determined in PH3 and the resulting velocity and energy increments are computed. Details are given in Section 5 of PART TWO. If CYCPH3 is -1, Phase 3 is bypassed and the effect of strength is not accounted for in the calculation. In this case the code is "hydrodynamic" in the classical sense.

#### 2.11. PH2

Mass transport and the associated flux of momentum and energy are accounted for in PH2. The tracer points are also moved with velocities obtained by a simple weighting scheme.

#### 2.12. REZONE

The masses of four cells are lumped into one in this subroutine. The JPM, DX, DY, X, Y, and TAU arrays are adjusted accordingly. Momentum and total energy are conserved, thereby converting some kinetic energy into

internal in a process loosely called "thermalizing." Every other tracer point is deleted in rezone, and new tracer points are placed in the added cells, retaining constant the total number of tracer points.

### 2.13. ERROR

This subroutine, which is called in the case of certain error conditions tested on by the code, prints a message identifying the error conditions, calls EDIT for a long print and tape dump, and then calls EXIT.

### 2.14. TAPE DUMPS

Each OIL-RPM tape dump consists of eight or nine records depending on whether tracer points are used. (See list below.) The first record contains three words: 555.0, the value of CYCLE at the time of the dump, and the value of N3 (N3 = 1 when tracer points are used; otherwise, N3 = 0). The last record also contains three words: 666.0, 666.0, 666.0. However, before each dump after cycle 0, TAPE 7 is backspaced one record and this last record is written over. Therefore, this last record remains only on the last dump of a run and in that case is followed by an end of file mark.

On cycle 0, after all input cards but the last have been read and the properties of all cells have been defined, SETUP does a tape dump. Thereafter, all tape dumps are made by EDIT at set intervals defined by NDUMP7. However, when NODUMP  $\neq$  0, all tape dumps after cycle 0 are suppressed. This makes it possible to restart a problem from a dump tape without writing on the dump tape which is sometimes useful in special studies.

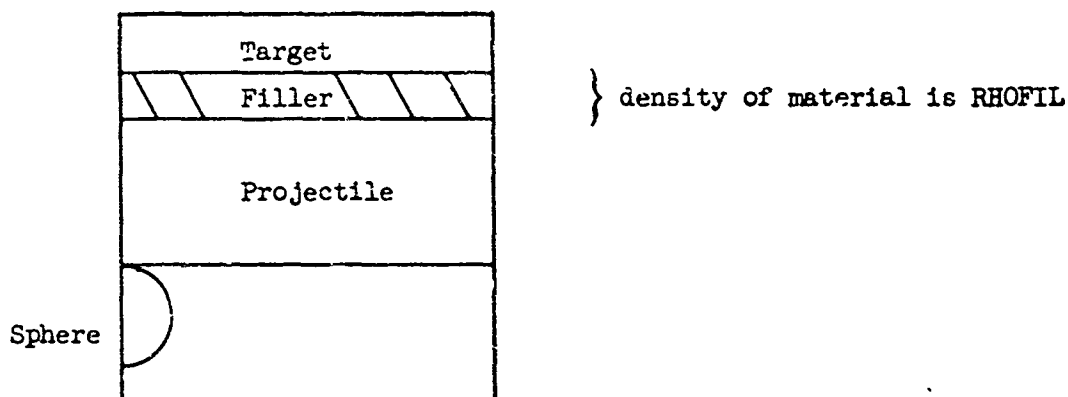
Record Number	Description
1	555.0, CYCLE, N3
2	Z(I), I = 1, NZT
3	U(I), V(I), AMX(I), AIX(I), P(I), I = 1, KMAF <sup>A</sup>
4	X(0), X(I), TAU(I), JPM(I), I = 1, IMAX)
5	Y(I), I = 0, JMAX
6	((XP(I,J), YP(I,J), I = 1, II), J = 1, JJ)
7	DX(I), I = 1, IMAX
8	DY(I), I = 1, JMAX
9	666.0, 666.0, 666.0

### 3. SET-UP OF PROBLEMS

Most calculations performed with the OIL-RPM code involve either a sphere or a cylinder hitting a target. Since the cylinder (which is called a "projectile" in the code) can be stationary, the set-up can also provide for a sphere hitting a two-layer target with or without filling material between the layers, as sketched in the diagram below.

The geometries described by the code are limited by the following requirements:

1. The Y-axis of the "sphere" must be on the Y-axis of the grid, i.e. the code cannot setup problems involving toroids.
2. The center of the sphere must coincide with a cell boundary. (Note: the center can be at the origin of the grid.)
3. The edge of the sphere should be contiguous with the projectile or target.
4. The projectile package is assumed to be below the target package.
5. The filler material can be placed only between the projectile package and the target package and extends out to the right boundary of the grid.
6. The right and top boundaries of the grid are transmissive, although the bottom boundary can be either reflective or transmissive.



The input cards for setting up an OIL-RPM problem define (1) the dimensions of the grid as well as the packages (sphere, projectile, and target); (2) the properties of the packages (density, velocity, and specific internal energy); (3) the physical constants used in the equation of state and yield-strength calculation; (4) the calculational constants used in defining various cutoffs and flags; (5) the frequency of printing and of writing on the restart tape; and (6) the time or cycle at which to stop execution.

Most of the input variables are equivalenced to an element in the Z-array, the first array in Blank Common. The variables, therefore, are identified on the input cards by their location in Blank Common (i.e., in the Z-array). The list that follows gives the variable name associated with each input number, its location in Blank Common, and a brief description of its function in the code.

Following this list will be a discussion of the format and order of the input cards, and the RPM Setup Sheets illustrating the input for a typical impact problem.

### 3.1. DEFINITION OF RPM INPUT VARIABLES

#### 3.1.1. Identification

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
PK(1)	151	The problem number can be any number with at most 2 places to the left and at most 4 to the right of the decimal point. (Range: 00.001 to 99.9999)
PROB	1	The problem number is repeated if this is a new problem just being set up. (It is <u>not</u> repeated for restarts from tape. See "RPM Input for Restart.")

### 3.1.2. Dimensions

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
IMAX	33	The number of columns in the calculational mesh. $IMAX \leq 50$ for the standard version. Unless $IMAX = 1$ for 1-D problem, IMAX must be <u>even</u> in order to rezone the grid.
JMAX	35	The number of rows in the calculational mesh. In the standard version $JMAX \leq 100$ , and $IMAX$ times $JMAX \leq 2500$ . JMAX must be <u>even</u> to rezone the grid.
I1	47	The right-most column to be calculated initially. It should be two columns beyond the last column with non-zero energy (kinetic or internal). ( $I1 \leq IMAX$ )
I2	48	The top row to be calculated initially. It should be two rows above the last column with non-zero energy. ( $I2 \leq JMAX$ ) I1 and I2 define the "active grid." I1 and I2 are automatically adjusted as the problem runs.
DXF	136	The value of all the DX's if DX is constant.
DYF	137	The value of all the DY's if DY is constant.
X(I)	269	The number of cms. from the axis to the right side of column I. The x-array is included in the input deck only if the radial dimension of the cells varies.
Y(J)	166	The number of cms. from the bottom of the grid to the top of row J. The Y-array is included in the input deck only if the axial dimension of the cells varies.

### 3.1.3. Projectile

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
PRYBOT	67	The number of cms. from the bottom of the grid to the bottom of the projectile.
PRYTOP	68	The number of cms. from the bottom of the grid to the top of the projectile.
PRXRT	69	The number of cms. from the axis to the right of the projectile.
VINI	112	Initial axial velocity of the projectile.
PROJU	73	Initial radial velocity of the projectile.
PROJI	16	Initial specific internal energy of the projectile.
RHINI	111	Initial density of the projectile.

### 3.1.4. Target

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
TAYBOT	86	The number of cms. between the bottom of the grid and the bottom of the target.
TAYTOP	89	The number of cms. between the bottom of the grid and the top of the target.
TAXRT	107	The number of cms. between the axis and the right of the target.
TARGV	52	Initial axial velocity of the target.
TARGI	72	Initial specific internal energy of the target.
RHINIT	15	Initial density of the target.

### 3.1.5. Sphere

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
RADIUS	162	The radius (in cms.) of the sphere.
YCENTR	163	The number of cms. from the bottom of the grid to the center of the sphere. (Note: The center of the sphere must be on a cell boundary and on the axis of the grid.)
VINSPH	102	Initial axial velocity of the sphere.
SIESPH	101	Initial specific internal energy of the sphere.
RHOSPH	100	Initial density of the sphere.
RHOOUT	103	Initial density of material in the outside part of a cell cut by the sphere boundary.

### 3.1.6. Filler

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
RHOFIL	51	Initial density of material between projectile and target.

### 3.1.7. Physical Constants

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
AMDM	21	The lowest compression of material considered "solid." If $\rho/\rho_0 \leq \text{AMDM}$ , and material is cold (specific internal energy $< ES'$ ) stresses and pressure are zero.
CZERO( $Y_0$ )	42	Parameters used in yield-strength equation: $Y = (Y_0 + Y_1\mu + Y_2\mu^2) \cdot (1 - E/E_0)$ where $\mu = \rho/\rho_0 - 1$ , and $E =$ specific internal energy. However, (1) If $Y < 0$ , stresses are set to 0. (2) If $E > E_0$ , then $Y = 0$ .
STK1( $Y_1$ )	11	
STK2( $Y_2$ )	28	
STEZ( $E_0$ )	29	



<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
BBAR	149	A constant used to approximate sound speed for the calculation of DT. $C = C_0 + \bar{B} \cdot \sqrt{P(K)}$ , where $C_0 = \sqrt{A/\rho_0}$ .
RHOZ	115	The normal density of the material. This value is used in the equation of state, the calculations of PMIN and $C_0$ , the strength calculations, and the "slaving" process.
ESA(a)	116	Gruneisen ratio at high energy, $\sim .5$ .
ESEZ( $E_0$ )	117	A constant in Gruneisen ratio.
ESB(b)	118	A constant in Gruneisen ratio.
ESCAPA(A)	119	Bulk modulus.
ESESP(ES')	120	Heat to vaporize material; must be larger than ESES.
ESESQ(ESQ)	121	Used to test whether material is "cold;" usually identical to ESESP.
ESES(ES)	122	Heat to bring material to vapor temperature; must be smaller than ESESP.
ESALPH( $\alpha$ )	123	Usually 5.
ESBETA( $\beta$ )	124	Usually 5.
ESCAPB(B)	125	Usually of the same order as A.

Equation of State constants, See Ref. 4 or Section 4, PART TWO

### 3.1.8. Calculational Constants

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
RHOMIN	138	The smallest density a cell can have and still influence the calculation of DT. (Usually $RHOMIN = RHOZ * 10^{-3}$ .)

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
DMIN	24	The allowable relative error in the energy sum. The error is the difference of the current total energy of all the cells and the total energy computed on cycle zero but adjusted for energy "evaporated" and lost across boundaries. The relative error is the difference divided by the total energy. If it exceeds DMIN, ERROR is called and the calculation is terminated.
DTMIN	144	The minimum value of DT (after STAB = FINAL) for the calculation to continue. DTMIN may be zero.
EVAP	75	This variable controls the "evaporation" of mass. If $\rho < EVAP * RHINI$ , the cell mass is evaporated. The mass, energy and momentum of evaporated cells are accumulated in PH2 and printed in EDIT. (Usually $EVAP = 10^{-4}$ .)
ROEPS	110	The "round-off epsilon" used in setting to zero certain calculated differences which could be due simply to machine round-off. (Usually $ROEPS = 10^{-5}$ or $10^{-6}$ .)
STAB	139	The stability fraction used in determining DT. The input value of STAB is its initial value. If $FINAL > 0.$ , STAB is doubled on each cycle until it equals FINAL. However, if $FINAL = 0.$ , the initial value of STAB is used throughout the run. STAB is usually $\leq 10^{-3}$ , but when all the energy is initially internal, setting $STAB \sim 10^{-8}$ is recommended.

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
FINAL	113	FINAL is used in determining DT. If FINAL is > 0., then it is the largest value the stability fraction (STAB) will have. If FINAL = 0., the stability fraction will have the same value for each cycle. (FINAL is usually ~ .4.)
JSTR	25	JSTR (J strength) gives the value of I2 (active grid, J direction) at which stress calculations (PH3) are turned on and tensions are allowed.
N6	56	N6 specifies the J index of the cell behind which tensions (negative pressures) are to be allowed. If N6 = 0., tensions are allowed everywhere.
CYCPH3	70	CYCPH3 = -1. if no stress calculation is wanted. Otherwise, it is the number of sub-cycles of PH3 per time step. (Usually about 4.)
NUMREZ	12	The maximum number of times the grid will be rezoned.
NMPMAX	85	The maximum number of tracer points to be used.
Y2	81	Y2 = -2. if tracer points are to be calculated. Y2 = 0. if no tracer points are to be calculated.
REZFCT	71	REZFCT = 1. if rezones are allowed. REZFCT = 0. if rezones are not allowed.
SS4	130	SS4 = 1. if a rezone is to be forced on the second cycle of a run. (Often used to test the setup of problems to be rezoned.)

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
SN	65	<p>SN = 0., if negative specific internal energy is to be set to zero.</p> <p>SN = 1., if negative specific internal energy is to be left along.</p>
CVIS	27	<p>CVIS = 0., if the bottom boundary of the grid is to be reflective.</p> <p>CVIS = -1., if the bottom boundary of the grid is to be transmittive.</p>
INTER	87	<p>INTER = 0., gives no intermediate prints.</p> <p>INTER = 1., gives EDIT prints after PH1 and PH3, as well as CDT.</p> <p>INTER = 7., gives, in addition to the extra EDIT prints, details of PH2 calculations.</p> <p>INTER = 99., gives, in addition to the extra EDIT prints, details of PH3 stress and strain rates.</p> <p>CAUTION: INTER = 7., or = 99., gives <u>many</u> pages of output.</p>
IVARDX	83	<p>IVARDX = 0., if DX is constant and the X array is to be calculated from the value of DXF.</p> <p>IVARDX = 1., if DX varies and the X array is included in the input deck.</p>
IVARDY	54	<p>IVARDY = 0., if DY is to be constant and the Y array is to be calculated from the value of DYF.</p> <p>IVARDY = 1., if DY varies and the Y array is included in the input deck.</p>

### 3.1.9. Output

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
JPROJ	147	JPROJ is usually assigned the value of J at the top of the projectile. In EDIT, JPROJ is used as the zero in calculating the crater depth and is the division for the printout of total energy, mass and momentum.
PRDELT	45	The number of seconds between EDIT prints when printing on time. Otherwise 0.
IPCYCL	49	The number of <u>cycles</u> between EDIT prints when printing on cycles. Otherwise 0.
PRLIM	44	PRLIM is the time <u>or</u> cycle at which the EDIT print interval is to be increased. PRLIM is multiplied by PRFACT each time the print interval is adjusted.
PRFACT	46	The factor by which the print interval is increased. PRDELT (or IPCYCL) and PRLIM are multiplied by PRFACT when $T = PRLIM$ .
NUMSCA	43	NUMSCA is the number of times the code will increase the interval time (or number of cycles) between EDIT prints.
NFRELP	5	NFRELP indicates the frequency of "long" EDIT prints. (A "long" print gives the velocities, pressure, mass, energy, density, and compression of all cells in the active grid; the "short" print gives this information only for the cells in the first column of the active grid.) A "long" print will occur every NFRELP short prints.

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
NDUMP7	6	NDUMP7 indicates the frequency of "tape dumps," where most of Blank Common is written on an output tape. A tape dump will occur every NDUMP7 EDIT prints. These "tape dumps" are used for restarting problems and for making automatic plots of tracer points.
NODUMP	96	NODUMP = 1. allows the user to pick up a run at some intermediate point on the restart tape without writing over the subsequent dumps on that tape.

### 3.1.10. Stopping

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
ICSTOP	7	The cycle for execution to stop when stopping on cycles.
TSTOP	50	The value of T for execution to stop when stopping on time rather than cycles. NOTE: This card, because of its "1" in column one, must always be included in the initial input deck. If stopping on cycles set to zero.
Z(150)	150	Dummy end card. Used in the RPM input deck for <u>setting up</u> problems. (Do not include this card in an input deck when <u>restarting</u> a problem.)

### 3.2. FORMAT AND ORDER OF OIL-RPM INPUT CARDS

Except for the ID header card, all RPM input cards have the same format and are normally punched on 7-word data cards.

The RPM setup sheets provide the information to be punched in Col. 1, Cols. 2-6, and Col. 7 for each input variable. The values of the variables are punched in the seven 9-space fields in Cols. 8-70. These values must

be punched with a decimal point even when they define integer variables. If the E-format is used, the exponent must be right-adjusted in the field. Only those variables which occur in consecutive order in Blank Common can be punched on the same card.

Col. 1	Cols. 2-6	Col. 7	Cols. 8-16	Cols. 17-25 etc.
Punch "1" on first and last two cards of deck. (See Setup Sheet.) Punch "2" on all cards defining integer variables. Otherwise no punch.	N Location in Blank Common of variable defined in Cols. 8-16.	Number of variables being defined on this card.	Z(N) Value of variable equivalenced to Z(N).	Z(N+1) Value of variable equivalenced to Z(N+1).

For a normal setup deck, the only data cards which must be in a specific order are those listed on the Setup Sheet with a "1" in column one, and they must be the first and the last two cards in the deck.

### 3.3. OIL-RPM INPUT FOR "SPECIAL SETUPS"

The properties (density, velocity, internal energy) of each cell are defined by the subroutine SETUP according to the input parameters associated with the sphere, cylinder, filler and target (e.g., SIESPH, VINI, RHOFIL, TARGV). The RPM "special setup" allows the user to assign a special mass (not density), velocity or internal energy to specific cells in the grid.

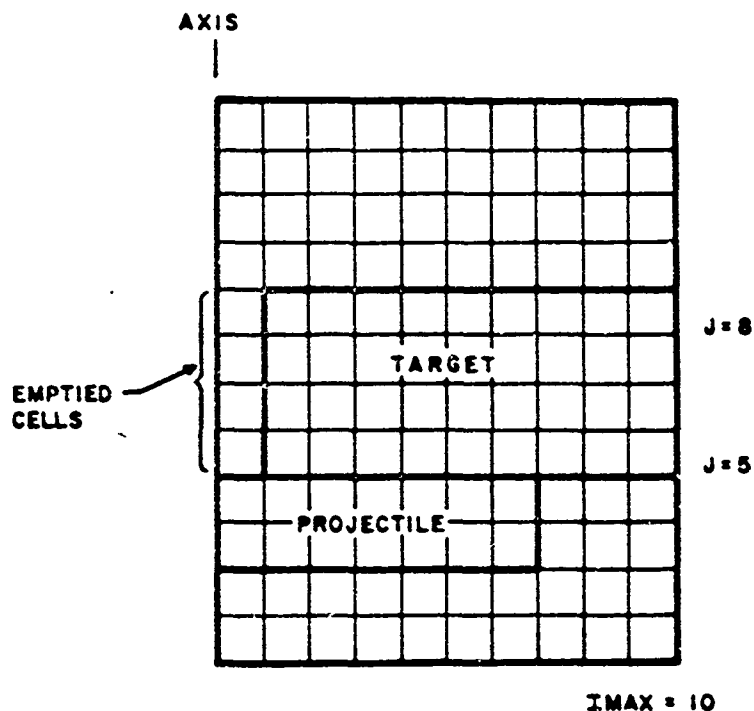
To assign special properties to a specific cell the user must do the following:

1. Find the I and J of the cell, then compute its K-index.  
( $K = (J - 1) * I_{MAX} + I + 1$ ).
2. Find the location in Blank Common of AMX(K), U(K), V(K), and AIX(K), whichever is being specifically defined. (See Table 3, page 26, "Location of Arrays in Blank Common.")
3. Using the format of the other RPM input cards, punch a card with the location and value for each property being assigned.

Precede these input cards by a flag card which has a "1" in column one and which sets  $Z(164) = PK(14) = 1$ . (See Figure 2, page "Flow Diagrams of INPUT, CARDS and SETUP.") Place the special input cards in the

RPM input deck just before the card that defines ICSTOP(Z(7)). The flag card (PK(14) = 1.) must be the second card with a "1" in the column one in the input deck.

EXAMPLE: Suppose one column of cells in the target next to the axis is to be empty. The target is to range from J = 5 to J = 8, and IMAS = 10. (NOTE: This problem requires special input because RPM places all packages next to the axis of the grid.)



1. Compute the K-index of the empty cells.

I = 1,	J = 5,	K = 4*10 + 1 + 1 = 42
I = 1,	J = 6	K = 52
I = 1,	J = 7	K = 62
I = 1,	J = 8	K = 72

2. Find the location in Blank Common of members of the AMX array which store the masses of these cells. Table 3 indicates that 482 is the location of AMX (1) in Blank Common.



<u>Variable Name</u>	<u>Location in Blank Common</u>
AMX(42)	523
AMX(52)	533
AMX(62)	543
AMX(72)	553

3. The input deck would be organized as follows:

Description of card	Col. 1	Col. 2-6	Col. 7	Col. 8-16
ID CARD				IMPACT
PK(1)	1	151	1	3.2
Z(1)=PROB	blank		1	3.2
.	.	.	.	.
.	.	.	.	.
.	.	.	.	.
NODUMP	2	96	1	0.
PK(14)	1	164	1	1.
AMX(42)	blank	523	1	0.
AMX(52)	blank	533	1	0.
AMX(62)	blank	543	1	0.
AMX(72)	blank	553	1	0.
ICSTOP	2	7	1	0.
TSTOP	1	50	1	1. - 06
Dummy End	1	150	1	0.

TABLE 3  
LOCATION OF ARRAYS IN BLANK COMMON\*

Name of Array	Location of First Member of Array
Z	1
PK	151
YY Note: $YY(1) = Y(0)$	166
XX Note: $XX(1) = X(0)$	270
DDX Note: $DDX(1) = DX(0)$	324
DDY Note: $DDY(1) = DY(0)$	378
AMX	482
AIX	2984
U	5486
V	7988
P	10490
TAU	12992
JPM	13044
UL	13096
PL	13300
XP	13504
YP	14830
CMXP	16156
CMYP	16161

\* These location numbers should not be used if the dimension of any array in Blank Common is changed.

#### 4. SAMPLE PROBLEM

The impact of an aluminum sphere on a target of like material was described in an earlier report,<sup>(8)</sup> and the setup of the problem will be described in this section as an example. The sphere diameter was .4763 cms (3/16 in.), and its velocity was 7.35 km/sec. The zoning was chosen so that the sphere radius contained exactly 6 cells, the free surface of the target was 16 zones above the bottom of the grid, and the cells were square. It was found that after 16 microseconds the velocities were down to a value where the subsequent material motion would be negligible. The grid was rezoned twice during the computation. About two hours of computer time and about 450 cycles were required to complete the problem.

Details of the setup are given by the OIL-RPM Setup Sheets which list the appropriate values for the input parameters and describe the format of the data cards. Also, the main section of the printed output are illustrated and briefly discussed in addition to the control cards for the UNIVAX 1108.

7-WORD DATA  
OIL-RPM SETUP SHEET

7	8	1	17	2	26	3	35	4	44	56	62	7	71	73
LOC							STANDARD	CIRITER						

PK(1) = Problem number in the form 92.3456.

PROB = Problem number (exactly the same as previous card).

IMAX = Number of columns. An even number  $\leq 50$ . unless IMAX = 1. } IMAX \* JMAX  $\leq 2500$   
 JMAX = Number of rows. An even number  $\leq 100$ . } unless variable di-  
 mensions are changed.

I1 = Number of columns in "active" grid + 2. (If IMAX = 1., I1 = 1.)

I2 = Number of rows in "active" grid + 2.

DXF = DX if it is constant. If DX varies DXF = 0.

DYF = DY if it is constant. If DY varies DYF = 0.

Insert X-array only if DX varies. (See Page 31) Insert Y-array only if DY varies. (See page 31)

1	67	1	1	1	1	1	1	1	1	1	1	1	1	1
1	68	1	0	1	1	1	1	1	1	1	1	1	1	1
1	69	1	0	1	1	1	1	1	1	1	1	1	1	1
1	70	1	0	1	1	1	1	1	1	1	1	1	1	1
1	71	1	0	1	1	1	1	1	1	1	1	1	1	1
1	72	1	0	1	1	1	1	1	1	1	1	1	1	1
1	73	1	0	1	1	1	1	1	1	1	1	1	1	1
1	74	1	0	1	1	1	1	1	1	1	1	1	1	1
1	75	1	0	1	1	1	1	1	1	1	1	1	1	1
1	76	1	0	1	1	1	1	1	1	1	1	1	1	1
1	77	1	0	1	1	1	1	1	1	1	1	1	1	1
1	78	1	0	1	1	1	1	1	1	1	1	1	1	1
1	79	1	0	1	1	1	1	1	1	1	1	1	1	1
1	80	1	0	1	1	1	1	1	1	1	1	1	1	1
1	81	1	0	1	1	1	1	1	1	1	1	1	1	1
1	82	1	0	1	1	1	1	1	1	1	1	1	1	1
1	83	1	0	1	1	1	1	1	1	1	1	1	1	1
1	84	1	0	1	1	1	1	1	1	1	1	1	1	1
1	85	1	0	1	1	1	1	1	1	1	1	1	1	1
1	86	1	0	1	1	1	1	1	1	1	1	1	1	1
1	87	1	0	1	1	1	1	1	1	1	1	1	1	1
1	88	1	0	1	1	1	1	1	1	1	1	1	1	1
1	89	1	0	1	1	1	1	1	1	1	1	1	1	1
1	90	1	0	1	1	1	1	1	1	1	1	1	1	1
1	91	1	0	1	1	1	1	1	1	1	1	1	1	1
1	92	1	0	1	1	1	1	1	1	1	1	1	1	1
1	93	1	0	1	1	1	1	1	1	1	1	1	1	1
1	94	1	0	1	1	1	1	1	1	1	1	1	1	1
1	95	1	0	1	1	1	1	1	1	1	1	1	1	1
1	96	1	0	1	1	1	1	1	1	1	1	1	1	1
1	97	1	0	1	1	1	1	1	1	1	1	1	1	1
1	98	1	0	1	1	1	1	1	1	1	1	1	1	1
1	99	1	0	1	1	1	1	1	1	1	1	1	1	1
1	100	1	0	1	1	1	1	1	1	1	1	1	1	1

PRYBOT = Y-value (cm) of bottom of projectile. PRYBOT = -1., if no projectile.  
 PRYTOP = Y-value (cm) of top of projectile.  
 PRXRT = X-value (cm) of right of projectile.  
 VINI = Initial axial velocity of projectile.  
 PROJU = Initial radial velocity of projectile.  
 PROJI = Initial specific internal energy of projectile.  
 RHINI = Initial density of projectile.  
 TAYBOT = Y-value (cm) of bottom of target. TAYBOT = -1., if no target.  
 TAYTOP = Y-value (cm) of top of target.  
 TAXRT = X-value (cm) of right of target.  
 TARGV = Initial axial velocity of target.  
 TARGI = Initial specific internal energy of target.  
 RHINIT = Initial density of target.

7-WORD DATA  
OIL-RPM SETUP SHEET

2 LOC	78	1	17	2	26	3	35	4	44	56	62	7	71	73
	1.462	1.23382												
	1.163	1.327												
	1.102	1.735												
	1.101	1.0												
	1.100	1.217												
	1.103	1.0												
	1.151	1.0												
	1.121	1.97												
	1.142	1.239												
	1.141	1.24												
	1.128	1.44												
	1.129	1.719												
	1.149	1.5												
	1.115	1.217												
	1.116	5.5												
	1.121	53.0												
	1.138	1.0												
	1.124	1.10												
	1.144	1.10												
	1.175	1.10												
	1.110	1.10												
	1.139	1.10												
	1.143	1.4												

RADIUS = radius (cm) of sphere. (RADIUS need not fall on cell boundary.)	$Y = [Y_0 + \mu (Y_1 + Y_2^\mu)](1 - E/E_C)$
YCENTR = Y-center (cm) of sphere. (YCENTR must coincide with a cell boundary.)	$\mu = \rho/\rho_C - 1$
VINSPH = Initial velocity of sphere.	Used in strength calculation
SIESPH = Initial specific internal energy of sphere.	
RHOSPH = Initial density of sphere.	Constant in "local sound speed" calculation. ( $C = C_0 + \text{BBAR} * \sqrt{P(K)}$ )
RHOOUT = Initial density of material adjacent to sphere.	
RHOFIL = Initial density of filling material between projectile and target.	Equation of State Constants. Normally ES=ESQ.
AMDM = Allowable expansion of material considered "solid." (Usually between .9 & .99.)	
CZERO (Y <sub>0</sub> )	a, E <sub>0</sub> , b, A, ES'
STK1 (Y <sub>1</sub> )	ESQ, ES, α, β, B
STK2 (Y <sub>2</sub> )	
STEZ (E <sub>0</sub> )	
BRAR = Constant in "local sound speed" calculation.	
RHOZ = Normal density (ρ <sub>0</sub> ) for the equation of state.	
5.10	7.52
3.10	5.19
RHOMIN = Minimum density for influencing DF. Usually 10 <sup>-3</sup> * RHOZ.	
DMIN = Allowable relative error for total energy sum. Usually 10 <sup>-3</sup> .	
DTMIN = Minimum value of DF for program to continue execution. DTMIN may be 0.	
EVAP = Minimum allowable compression. If ρ/ρ <sub>0</sub> < EVAP, mass of cell is "evaporated."	
RCEPS = Round-off epsilon. Usually 10 <sup>-5</sup> or 10 <sup>-6</sup> .	
STAB = Initial value of "stability fraction." Usually < 10 <sup>-3</sup> .	
FINAL = Final value of "stability fraction." Usually = .4.	

7-WOKU DATA  
OIL-RPM SETUP SHEET

2	LOC	78	1	17	2	26	3	35	4	44	55	62	7	71	73
2		125	1	128											
2		126	1	129											
2		127	1	130											
2		128	1	131											
2		129	1	132											
2		130	1	133											
2		131	1	134											
2		132	1	135											
2		133	1	136											
2		134	1	137											
2		135	1	138											
2		136	1	139											
2		137	1	140											
2		138	1	141											
2		139	1	142											
2		140	1	143											
2		141	1	144											
2		142	1	145											
2		143	1	146											
2		144	1	147											
2		145	1	148											
2		146	1	149											
2		147	1	150											
2		148	1	151											
2		149	1	152											
2		150	1	153											
2		151	1	154											
2		152	1	155											

JSPR = Value of I2 which triggers calculation of strength and negative pressures.

N6 = Value of J below which negative pressures are not allowed.

CYCPH3 = Number of times of subcycle PH3. CYCPH3 = -1., for no PH3.

NUMREZ = Maximum number of rezones allowed.

NMPMAX = Maximum number of tracer points desired. NMPMAX ≤ 1250.

Y2 = -2., if tracer points are wanted. Y2 = 0. for no tracer points.

REZFACT = 1. for allowing rezones. REZFACT = 0. for no rezones.

SS4 = 1. for forcing rezone on second cycle of run. Usually SS4 = 0.

SN = 1. leave negative S.I.E. alone. SN = 0. sets negative S.I.E. to 0.

CVIS = -1. for transmittive bottom boundary. CVIS = 0. for reflective bottom boundary.

INTER = Intermediate print flag.

IVARDX = 1. if DX varies and the X-array is read in. IVARDX = 0. if DX is constant.

IVARDY = 1. if DY varies and the Y-array is read in. IVARDY = 0. if DY is constant.

JPROJ = Usually the J-value of top row of projectile. Used in EDIT print, crater depth calculation.

PRDELT = Time between EDIT prints. PRDELT = 0. if printing on cycles.

IPCYCL = Cycles between EDIT prints. IPCYCL = 0. if printing on time.

PRLIM = Time or cycle at which to increase interval between prints.

PRFACT = Factor by which to increase print interval.

NUMSCA = Maximum number of times print interval can be increased.

NFRELP = Ratio of "short" prints to "long" prints.

NDUMP7 = Ratio of prints to tape dumps.

NODUMP = 0. allows tape dumps. NODUMP = 1. suppresses tape dumps after cycle 0.

ICSTOP = Cycle to stop execution. ICSTOP = 0. if stopping on time.

TSTOP = Time (value of T) to stop execution. TSTOP = 0. if stopping on cycles.

Dummy end card.

7-WORD DATA  
OIL-RPM SETUP SHEET--X AND Y ARRAYS\*

2 LOC	78	1	17	2	26	3	35	4	44	5	6	62	7	71	73
1	1710														
2	1717														
3	1847														
4	1917														
5	1918														
6	1905														
7	1912														
8	1922														
9	1927														
10	1937														
11	1807														
12	1877														
13	1947														
14	2017														
15	2087														
16	2157														
17	2227														
18	2297														
19	2367														
20	2437														
21	2507														
22	2577														
23	2643														

X(0),..., X(50)  
Input these values only if DX varies.

Y(0),..., Y(100)  
Input these values only if DY varies.

\*These location numbers (Cols. 2-6) must be changed if the dimension of Z, FK, or YI is changed.

#### 4.1. OIL-RPM Output

The pages of OIL-RPM output which follow were produced by the sample problem, "Standard Crater," described above. The printed headings make most of the listing self-explanatory. Sections needing further description are numbered in the listing and discussed below.

1. The first few pages of the output for a setup run\* display the input deck and describe the initial conditions of the problem. (Each time the CARDS routine is called "INPUT CARDS" is printed.)
2. When a sphere is placed, SETUP assures that the value of YCENTR is on a c .1 boundary and prints the input and adjusted values of YCENTR.
3. On every cycle subroutine CDT prints the value of T, the time, and DT, the time step. The integers following "CDT" in the printout are the I and J of the cell controlling the time step. MAXCUV represents the maximum sound speed or velocity in the active grid. Likewise, MAXUV represents the maximum velocity. UMIN and PMIN are velocity and pressure cutoffs, respectively, used in MAP and PH2.
4. The first page printed by EDIT gives the total energies, mass and momenta of the cells above the JPROJ row and of the cells below and in the JPROJ row. (JPROJ is an input parameter, usually the J of the top row of the projectile package.)
5. On each cycle EDIT calculates the relative error in the total energy sum. On print cycles EDIT prints the maximum error calculated and the number of the cycle in which the maximum error occurred.
6. The total work done due to stresses calculated in PH3 is printed under "PLASTIC-WORK."
7. Also printed is a running total of the mass, energy, and axial and radial momentum lost when material crosses a transmissive boundary or is "evaporated" in PH2.

---

\*For a restart run only the input deck is printed.



8. The "J OF PRESSURE MAXIMUM" describes the shock front by giving the location of the peak pressure in each column.
9. The tracer point coordinates are printed in centimeter units. The I and J of the cell in which a tracer point originated is also printed. This enables the user to follow the movement of a given tracer point. However, if the mass of a cell is "evaporated" the coordinates of the tracer points in that cell are set to zero and thereafter are not printed out.
10. The range of values assigned to the symbols on the contour maps are adjusted as the calculation proceeds. Therefore, a given symbol in the compression map, for instance, does not represent the same compression from one print to the next. A negative pressure, velocity, or internal energy is denoted by a symbol representing its absolute value and preceded by a minus sign.
11. The crater depth is measured from JPROJ. After a crater is formed, the negative values for the crater depth will describe the crater's "lip". The volume of the crater is printed along with the volume of a hemisphere of radius equal to the crater's depth in column one.
12. The J-index, radial velocity, axial velocity, pressure, mass, density, specific internal energy, compression, and distance (in cms.) from the bottom of the grid are printed for non-empty cells. The "long" EDIT print lists these properties for every column of the active grid, whereas the "short" EDIT print describes the non-empty cells in column one only.
13. Several error conditions are tested for during execution, and when one is detected, subroutine ERROR is called. ERROR in turn identifies the error test, prints the entire Z-array, and calls EDIT to do a long print and tape dump before stopping.

STANDARD CRATER

INPUT CARDS

(1)

1 151 1 1.373500+01

INPUT CARDS

-0	1	1	1.373500+01
-0	33	1	4.200000+01
-0	35	1	3.391973+01
-0	47	1	3.000000+00
-0	48	1	1.600000+01
-0	130	1	3.370000-02
-0	137	1	3.370000-02
-0	67	1	-1.000000+00
-0	68	1	0.000000
-0	69	1	0.000000
-0	112	1	0.000000
-0	75	1	0.000000
-0	10	1	0.000000
-0	111	1	2.700000+00
-0	36	1	3.352000-01
-0	64	1	1.000000+10
-0	107	1	1.000000+10
-0	22	1	0.000000
-0	72	1	0.000000
-0	15	1	2.700000+00
-0	162	1	2.362000-01
-0	103	1	3.370000-01
-0	102	1	7.350000+05
-0	104	1	0.000000
-0	100	1	2.700000+00
-0	103	1	0.000000
-0	51	1	0.000000
-0	21	1	9.700000-01
-0	42	1	2.390000+09
-0	11	1	2.400000+10
-0	28	1	4.100000+10
-0	29	1	7.000000+09
-0	143	1	2.000000-01
-0	115	1	2.700000+00
-0	116	5	5.000000-01
-0	124	5	3.000000+10
-0	133	1	1.000000-03
-0	24	1	1.000000-03
-0	144	1	1.000000-09
-0	75	1	1.000000-04
-0	110	1	1.000000-06
-0	139	1	1.000000-03

5.000000+10 1.630000+00 7.520000+11 1.300000+11  
 3.000000+10 5.000000+00 5.000000+00 6.500000+11

```

-U 113 1 4.000000-01
  2 25 1 2.000000+01
  2 50 1 1.000000+01
-U 70 1 4.000000+00
  2 14 1 2.000000+00
  2 28 1 5.070000+02
-U 61 1 -2.000000+00
-U 71 1 1.000000+00
-U 130 1 0.000000
-U 65 1 1.000000+00
-U 27 1 -1.000000+00
  2 27 1 0.000000
  2 27 1 0.000000
  2 54 1 0.000000
  2 147 1 1.000000+01
-U 45 1 1.000000-06
  2 45 1 0.000000
-U 44 1 1.000000-06
-U 40 1 2.000000+00
  2 43 1 1.000000+01
  2 2 1 2.000000+00
  2 0 1 1.000000+00
  2 90 1 0.000000
  2 7 1 0.000000
  1 50 1 1.000000-06

```

② INPUT YCENTR = 3.970000-U1 ADJUSTED YCENTR = 3.970000-01

INITIAL CONDITIONS

```

SPHERE PACKAGE 1 PACKAGE 2 FILLER
DENSITY 6.7000+00 2.7000+00 2.7000+00 0.0000
S.I.C. 0.0000 0.0000 0.0000
V 7.3500+05 0.0000 0.0000
U 0.0000 0.0000
MAJUS 2.3020-U1 TOP 0.0000 1.0000+10
YCENTER 3.9700-U1 CENTER-1.0000+00 0.3520-U1
Right 0.0000 1.0000+10

```

INPUT CARDS

```

1 150 1 0.000000

```

IFCYCLE= 0 ICUSTOP= 0 JSTRE 20 N6= 10 IMAX= 42 JMAX= 54 I1= 8 I2= 18 JPROJ= 16 NIMPMAX= 567 INTFR= 0 NUMSCA=10  
 NRELEP= 5 NDUMP7= 1 NODUMPE U IVAROX= 0 IVAROY= 0

3

CJT 17 12 F= 5.733052-07 UT= 1.7105428-08 MAXCUV= 9.2836024+05 MAXUV= 9.2836024+05 UMIN= 9.2836023-01 PMIN= 1.3228399+06  
CJT 17 11 F= 5.9040084-07 UT= 1.7104032-08 MAXCUV= 9.2430734+05 MAXUV= 9.2430734+05 UMIN= 9.2430732-01 PMIN= 1.170649+06  
CJT 17 11 F= 6.0750927-07 UT= 1.7900208-08 MAXCUV= 8.041763+05 MAXUV= 8.417681-01 UMIN= 8.417681-01 PMIN= 1.259821+06  
CJT 10 12 F= 6.2554947-07 UT= 1.7412566-08 MAXCUV= 9.1198503+05 MAXUV= 9.1198503+05 UMIN= 9.1198502-01 PMIN= 1.2995066+06  
CJT 10 12 F= 6.4296203-07 UT= 1.6202935-09 MAXCUV= 8.7238675+05 MAXUV= 8.7238675+05 UMIN= 8.7238675-01 PMIN= 1.2430821+06  
CJT 10 11 F= 6.0116+96-07 UT= 1.0313324-08 MAXCUV= 8.0712820+05 MAXUV= 8.6712820+05 UMIN= 8.6712819-01 PMIN= 1.2355892+06  
CJT 10 11 F= 6.7947629-07 UT= 1.9107477-08 MAXCUV= 8.3108422+05 MAXUV= 8.3108422+05 UMIN= 8.3108422-01 PMIN= 1.1842350+06  
CJT 10 26 F= 6.9050570-07 UT= 1.9526040-08 MAXCUV= 8.1324770+05 MAXUV= 7.9660646+05 UMIN= 8.1324768-01 PMIN= 1.1588137+06  
CJT 9 27 F= 7.101141-07 UT= 1.9712737-08 MAXCUV= 8.0557049+05 MAXUV= 7.6116204+05 UMIN= 8.0557048-01 PMIN= 1.1478743+06  
CJT 10 27 F= 7.3782514-07 UT= 1.9644013-08 MAXCUV= 8.0630364+05 MAXUV= 7.2520110+05 UMIN= 8.0630363-01 PMIN= 1.1449189+06  
CJT 9 28 F= 7.5751495-07 UT= 1.9847501-08 MAXCUV= 8.0009749+05 MAXUV= 7.1909469+05 UMIN= 8.0009748-01 PMIN= 1.1400757+06  
CJT 11 27 F= 7.736752-07 UT= 1.9906493-08 MAXCUV= 7.9772964+05 MAXUV= 6.8658096+05 UMIN= 7.9772963-01 PMIN= 1.1367017+06  
CJT 10 28 F= 7.9727402-07 UT= 1.9937062-09 MAXCUV= 7.9648253+05 MAXUV= 6.7095737+05 UMIN= 7.9648252-01 PMIN= 1.1349247+06  
CJT 11 28 F= 8.1721167-07 UT= 2.0000527-08 MAXCUV= 7.9050396+05 MAXUV= 6.5999599+05 UMIN= 7.9050095-01 PMIN= 1.12644013+06  
CJT 10 29 F= 8.3730020-07 UT= 2.0092037-08 MAXCUV= 7.9036246+05 MAXUV= 6.6331750+05 UMIN= 7.9036284-01 PMIN= 1.1262046+06  
CJT 12 28 F= 8.3739223-07 UT= 2.0253253-08 MAXCUV= 7.8407156+05 MAXUV= 6.5883274+05 UMIN= 7.8407155-01 PMIN= 1.1172400+06  
CJT 11 29 F= 8.7704347-07 UT= 2.0244903-08 MAXCUV= 7.8439185+05 MAXUV= 6.5202171+05 UMIN= 7.8439184-01 PMIN= 1.1176964+06  
CJT 10 30 F= 8.9789040-07 UT= 2.0351241-08 MAXCUV= 7.8029636+05 MAXUV= 6.4354466+05 UMIN= 7.8029636-01 PMIN= 1.1118606+06  
CJT 12 29 F= 9.1624169-07 UT= 2.0382380-08 MAXCUV= 7.791045+05 MAXUV= 6.3772411+05 UMIN= 7.7910423-01 PMIN= 1.1101619+06  
CJT 10 31 F= 9.3862407-07 UT= 2.0512100-08 MAXCUV= 7.7417693+05 MAXUV= 6.3620342+05 UMIN= 7.7417693-01 PMIN= 1.1031409+06  
CJT 12 30 F= 9.5913017-07 UT= 2.0516787-08 MAXCUV= 7.7400029+05 MAXUV= 6.3356149+05 UMIN= 7.7400029-01 PMIN= 1.1028993+06  
CJT 11 31 F= 9.7905295-07 UT= 2.0635466-08 MAXCUV= 7.6954887+05 MAXUV= 6.2956331+05 UMIN= 7.6954986-01 PMIN= 1.0965463+06  
CJT 13 30 F= 9.9999999-07 UT= 2.0698330-08 MAXCUV= 7.6721163+05 MAXUV= 6.2401286+05 UMIN= 7.6721162-01 PMIN= 1.0932159+06

ω





DEPTH OF CRATER MEASURED FROM APPROX  
J OF CRATER CENTER

I	J	M(I,J)	V	P	APA	RHO	AIR	COMP	Z
1	1	20.4	1.9850-02	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.626-n-n-n
2	2	20.6	5.9550-02	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.746-n-n-n
3	3	20.4	9.4250-02	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.746-n-n-n
4	4	20.1	1.1892-01	9.442923+05	5.307507-04	2.700000+00	1.012454+01	1.000000+00	1.746-n-n-n
5	5	20.2	1.7865-01	4.051168+07	5.307226-04	2.700194+00	2.204175+02	1.000000+00	1.667400+00
6	6	20.2	2.1825-01	1.742542+03	5.308603-04	2.700222+00	4.323703+03	1.000000+00	1.627700+00
7	7	20.1	2.5885-01	7.217934+09	5.314527-04	2.705866+00	1.033507+06	1.000000+00	1.544100+00
8	8	19.6	2.9775-01	2.094352+09	5.327891-04	2.710394+00	1.033507+06	1.014294+00	1.504600+00
9	9	19.5	3.3745-01	1.094989+10	5.332212-04	2.739377+00	2.090493+07	1.046244+00	1.466000+00
10	10	19.4	3.7715-01	3.771526+10	5.346175-04	2.820859+00	2.820859+00	1.113510+00	1.429000+00
11	11	19.4	4.1685-01	1.041870+11	5.360967-04	3.006876+00	1.665623+09	1.113510+00	1.429000+00
12	12	13.7	4.5655-01	1.915185+11	6.294958-04	3.202370+00	4.869445+00	1.186061+00	1.389500+00
13	13	14.1	4.9625-01	2.098914+11	6.362822-04	3.231334+00	5.282827+09	1.186061+00	1.389500+00
14	14	14.8	5.3595-01	1.645387+11	6.195575-04	3.150794+00	3.202842+09	1.166961+00	1.310100+00
15	15	15.3	5.7565-01	1.222793+11	6.072731-04	3.066935+00	1.254604+09	1.135900+00	1.270000+00
16	16	15.6	6.1535-01	1.106218+11	6.003596-04	3.052616+00	1.254604+09	1.135900+00	1.270000+00
17	17	15.9	6.5505-01	1.153054+11	6.003596-04	3.070369+00	-5.420134+08	1.135900+00	1.270000+00
18	18	16.0	6.9475-01	1.149554+11	6.018959-04	3.061961+00	-1.400760+09	1.135900+00	1.270000+00
19	19	16.0	7.3445-01	1.126793+11	6.058797-04	3.031358+00	-2.051599+09	1.135900+00	1.270000+00
20	20	16.0	7.7415-01	3.269714+10	5.987195-04	3.005082+00	-6.423063+08	1.112903+07	1.071000+00
21	21	16.0	8.1385-01	5.356553+10	5.430447-04	2.966267+00	2.091332+09	1.096617+00	1.032200+00
22	22	16.0	8.5355-01	7.942581+10	5.653011-04	2.875794+00	4.004941+05	1.055111+00	9.924099-n-1
23	23	16.0	8.9325-01	6.214014+10	5.403380-04	2.795581+00	6.403131+09	1.035053+00	9.527095-n-1
24	24	16.0	9.3295-01	1.803364+10	5.194259-04	2.642422+00	6.615177+09	9.746750-n-1	9.130099-n-1
25	25	16.0	9.7265-01	0.000000	4.980866-04	2.315326+00	5.984096+09	6.574550-n-1	8.733099-n-1
26	26	16.0	10.1235-01	0.000000	4.767300-04	2.093356+00	4.255820+09	7.750246-n-1	8.336399-n-1
27	27	16.0	10.5205-01	0.000000	4.553700-04	1.841802-02	4.091461+09	5.710376-n-1	7.939999-n-1
28	28	16.0	10.9175-01	0.000000	4.340148-06	1.591802-02	4.091461+09	5.710376-n-1	7.939999-n-1

CRATER VOLUME BASED ON (27,3) \* PI \* D(11)+3  
1.1032-n-2

CRATER VOLUME  
6.2737-02

I = 1 N(I,J) = .000 CM(I,J) = .3970000-01

I	J	M(I,J)	V	P	APA	RHO	AIR	COMP	Z
46	46	0.000000	-0.000000	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.626-n-n-n
47	47	0.000000	-0.000000	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.746-n-n-n
48	48	0.000000	7.357571-n-1	0.000000	5.307440-04	2.700000+00	-0.000000	1.000000+00	1.746-n-n-n
49	49	0.000000	4.320798-n-10	9.442923+05	5.307507-04	2.700000+00	1.012454+01	1.000000+00	1.746-n-n-n
50	50	0.000000	4.196922-n-11	4.051168+07	5.307226-04	2.700194+00	2.204175+02	1.000000+00	1.667400+00
51	51	0.000000	5.426982-n-11	1.742542+03	5.308603-04	2.700222+00	4.323703+03	1.000000+00	1.627700+00
52	52	0.000000	7.029706-n-12	7.217934+09	5.314527-04	2.705866+00	1.033507+06	1.000000+00	1.544100+00
53	53	0.000000	1.044659-n-13	2.094352+09	5.327891-04	2.710394+00	1.033507+06	1.014294+00	1.504600+00
54	54	0.000000	3.709333-n-13	1.094989+10	5.332212-04	2.739377+00	2.090493+07	1.046244+00	1.466000+00
55	55	0.000000	4.414344-n-14	3.771526+10	5.346175-04	2.820859+00	2.820859+00	1.113510+00	1.429000+00
56	56	0.000000	6.000444-n-14	1.041870+11	5.360967-04	3.006876+00	1.665623+09	1.113510+00	1.429000+00
57	57	0.000000	1.028163-n-15	1.915185+11	6.294958-04	3.202370+00	4.869445+00	1.186061+00	1.389500+00
58	58	0.000000	1.321037-n-15	2.098914+11	6.362822-04	3.231334+00	5.282827+09	1.186061+00	1.389500+00
59	59	0.000000	1.443688-n-15	1.645387+11	6.195575-04	3.150794+00	3.202842+09	1.166961+00	1.310100+00
60	60	0.000000	1.744583-n-15	1.222793+11	6.072731-04	3.066935+00	1.254604+09	1.135900+00	1.270000+00
61	61	0.000000	1.211031-n-15	1.106218+11	6.003596-04	3.052616+00	1.254604+09	1.135900+00	1.270000+00
62	62	0.000000	1.378011-n-15	1.153054+11	6.003596-04	3.070369+00	-5.420134+08	1.135900+00	1.270000+00
63	63	0.000000	1.359992-n-15	1.149554+11	6.018959-04	3.061961+00	-1.400760+09	1.135900+00	1.270000+00
64	64	0.000000	1.862008-n-15	1.126793+11	6.058797-04	3.031358+00	-2.051599+09	1.135900+00	1.270000+00
65	65	0.000000	1.892303-n-15	3.269714+10	5.987195-04	3.005082+00	-6.423063+08	1.112903+07	1.071000+00
66	66	0.000000	4.230744-n-15	5.356553+10	5.430447-04	2.966267+00	2.091332+09	1.096617+00	1.032200+00
67	67	0.000000	2.694380-n-15	7.942581+10	5.653011-04	2.875794+00	4.004941+05	1.055111+00	9.924099-n-1
68	68	0.000000	3.175320-n-15	6.214014+10	5.403380-04	2.795581+00	6.403131+09	1.035053+00	9.527095-n-1
69	69	0.000000	3.694300-n-15	1.803364+10	5.194259-04	2.642422+00	6.615177+09	9.746750-n-1	9.130099-n-1
70	70	0.000000	4.280370-n-15	0.000000	4.980866-04	2.315326+00	5.984096+09	6.574550-n-1	8.733099-n-1
71	71	0.000000	4.862327-n-15	0.000000	4.767300-04	2.093356+00	4.255820+09	7.750246-n-1	8.336399-n-1
72	72	0.000000	5.444322-n-15	0.000000	4.553700-04	1.841802-02	4.091461+09	5.710376-n-1	7.939999-n-1

\*\*\* ERROR EXIT - SEE STATEMENT NUMBER 65 IN CDT

(13)

I= 8 J= 10 K=705

Z=ZLUCK

I	REAL FORMAT Z(I)	INTEGER FORMAT Z(I)
1	.137350+02	17831957620
2	-.100000+01	-17381195770
3	.000000	0
4	.000000	0
5	.500000-38	5
6	.500000-38	1
7	.000000	0
8	.314159+01	17553718998
9	.000000	0
10	.000000	0
11	.240000+11	21971239664
12	.500000-38	2
13	.000000	0
14	.000000	0
15	.270000+01	17530901606
16	.000000	0
17	.000000	0
18	.166740+01	17425984211
19	.500000-38	1
20	.500000-38	2
21	.970000-00	17310060380
22	.000000	0
23	.000000	0
24	.100000-02	16040629108
25	.500000-38	28
26	.000000	0
27	-.100000+01	-17381195770
28	.410000+11	22091785517
29	.700000+10	21718429208
30	-.500000-38	-1
31	.000000	0
32	.000000	0
33	.500000-38	42
34	.500000-38	43
35	.600000-38	54
36	.600000-38	55
37	.540000-38	2269
38	.540000-38	2270
39	.000000	0
40	.000000	0
41	.000000	0
42	.239000+10	21549523980
43	.500000-38	10
44	.100000-05	14700101090



4.2. UNIVAC 1108 CONTROL CARDS

∇ ASG P = 1184	Program Tape
∇ ASG 7 = 2213	Restart Tape*
∇ XQT CUR	
IN	
TRI P	
TOC	
∇ P HDG	STANDARD CRATER
∇ XQT RPM:	

	STANDARD CRATER			
1	151	1	13.735	} Input deck
.	.	.	.	
.	.	.	.	
.	65	1	1.0	
.	.	.	.	
1	50	1	1.0	-06

\* Can assign a drum area for tape dumps instead of a tape by using:

∇D ASG 7 = 100000

## 5. RESTART OF PROBLEMS

Periodically during a calculation RPM writes on tape the problem parameters and the current state of the material in each cell. By reading this tape the user can "restart" and continue a calculation from an intermediate point. Because the initial conditions are saved on tape, SETUP is not called and the following three cards are the only ones which must be in the restart input deck:

Description of Card	Col. 1	Col. 2-6	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT		
PK(1),PK(2), PK(3)	1	151	3	3.2	88.	-1.
TSTOP	1	50	1	1. - 06		

PK(1) = The same problem number used when the problem was initially setup. (NOTE: This can be any number between 00.0000 and 99.9999.)

PK(2) = The restart cycle number. The problem can be restarted on any cycle which is marked as a tape dump cycle in the printed output.

PK(3) = The restart flag. If it is -1. EDIT makes a long print of the restart cycle. However the user may wish to avoid making a long print on the restart cycle. He can do this by setting PK(3) = -2.

TSTOP = The new time at which execution will stop.

Other variables besides TSTOP may be redefined when restarting a problem. The copy of the "Setup Sheet for OIL-RPM Restarts" on page 44 lists those variables most likely to be redefined at an intermediate point in the calculation.

The cards in a restart input deck can be in any order as long as the first card is the ID card, the second card defines PK(1), PK(2) and PK(3) and has a "1" in column one, and the last card has a "1" in column one.

Examples:

1.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 1		
PK(1),PK(2) PK(3)	1	151	3	26.1	32.	-1.
INTER	2	87	1	0.		
RHOMIN		138	1	1. -03		
ICSTOP	2	7	1	135.		
TSTOP	1	50	1	0.		

2.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 2		
PK(1),PK(2) PK(3)	1	151	3	35.013	2019.	-2.
TSTOP	1	50	1	1.0 -05		

3.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 3		
PK(1),PK(2) PK(3)	1	151	3	8.2	128.	-2.
ICSTOP	2	7	1	200.		
TSTOP	1	50	1	0.		

\*All numbers must be right-adjusted within chr field.

7-WORD DATA  
 SETUP SHEET FOR OIL-RPM "RESTART"

2 LOC	7 8	1	17	2	26	3	35	4	44	5	6	7	7173
	N												
1	1115	1											

(a) Problem number. (b) Pickup cycle #. (c) Restart flag (-1. or -2.)

- CYCPH3 = Number of times to subcycle PH3.
- AMDM = Allowable expansion of material considered "solid": ~.95 to .99.
- RHOMIN = Minimum  $\rho$  for influencing DT.
- FINAL = Final value of "stability fraction."
- DMIN = Allowable relative error for total energy sum:  $\sim 10^{-4}$ .
- DTMIN = Minimum for DT.
- VT = Minimum  $\Delta\rho$  from one cell across a grid boundary to trigger rezone.
- SN = 0., when negative S.I.E. is to be set to 0. If SN = 1., negative S.I.E. left alone.
- EVAP =  $\rho/\rho_0$  of cells to be "evaporated."
- ROEPS = Round-off epsilon.
- JPROJ = Used in EDIT print and crater depth calculation.
- NFRELP = Ratio of "short" print frequency to "long" print frequency.
- NDUMPF7 = Ratio of print frequency to tape dump frequency.
- ICSTOP = Cycle to stop. Set to 0. if stopping on time.
- TSTOP = Time (value of T) to stop. Set to 0. if stopping on cycles. (This must be the last card of a restart deck.)

## 6. LISTING OF THE FORTRAN IV PROGRAM

This section consists simply of a listing of the FORTRAN IV program.

C	RPM	10
C	.....	20
C		30
C		40
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	50
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,	60
2	Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),	70
3	GAMC(102),	80
4	PK(15), Z(150) ,	90
5	XP(26,51),YP(26,51),	100
6	PL(204) ,UL(204) ,PR(204) ,	110
7	RSN(52), RST(52),	120
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	130
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	140
5	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)	150
C	*** DIMENSIONED ARRAYS	160
C	*** Z-BLOCK IS SAVED ON TAPE.	170
	COMMON Z	180
	COMMON PK	190
	COMMON YY, XX	200
	COMMON DDX, DDY	210
	COMMON AMX, AIX, U, V, P	220
	COMMON TAU, JPM	230
	COMMON UL, PL	240
	COMMON XP, YP, CMXP, CMYP	250
C	*** NON-DIMENSIONED VARIABLES	260
	COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR, ,	270
1	AMVT, DEL, DELER, DELET, DELM, DTODX, DXYMIN, EAMMP, EAMPY, ,	280
2	E, ERDUMP, I, I3, IWS, J, K, KA, KB, ,	290
3	LL, MD, ME, MZT, NERR, NK, NPRINT, ,	300
4	NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID, ,	310
5	SUM, TESTRH, TWOPI, URR, WS, WSA, WSB, WSC, WFLAGF, ,	320
6	WFLAGL, FLAGP	330
	COMMON LAST	335
C		340
C	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	350
C	X(0), Y(0), DX(0), DY(0)	360
C		370
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	380
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	390
C		400
C	*** SPECIAL EQUIVALENCES FOR PH2 ONLY	410
C		420
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	430
1	(PL,GAMC,PR), (PL(103),SIGC)	440
		450
C	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	460
C		470
	EQUIVALENCE (UL,RSN),	480
1	(PL,RST), (P,UK),	490
2	(P(157),VK), (P(313),SNB),	500
3	(P(365),STB), (P(417),RHO)	510
		520
C	*** SPECIAL EQUIVALENCES FOR EDIT	530
C		540
	EQUIVALENCE (PR(1), IJ), (PR(6), JK)	550
C		560
C	*** Z-STORAGE EQUIVALENCES	570

C

EQUIVALENCE				(Z( 1),PROB )	(Z( 2),CYCLE )	580
1(Z( 3),DT )	(Z( 4),NUMSP )	(Z( 5),NFRELP)	(Z( 6),NDUMP7)			590
2(Z( 7),ICSTOP)	(Z( 8),PIDY )	(Z( 9),TOPMU )	(Z( 10),RTMU )			600
3(Z( 11),STK1 )	(Z( 12),NUMREZ)	(Z( 13),ETH )	(Z( 14),UN14 )			610
4(Z( 15),RHINIT)	(Z( 16),PROJI )	(Z( 17),UN17 )	(Z( 18),XMAX )			620
5(Z( 19),NZ )	(Z( 20),NREZ )	(Z( 21),AMDM )	(Z( 22),UVMAX )			630
6(Z( 23),UN23 )	(Z( 24),DMIN )	(Z( 25),JSTR )	(Z( 26),DTNA )			640
7(Z( 27),CVIS )	(Z( 28),STK2 )	(Z( 29),STEZ )	(Z( 30),NC )			650
8(Z( 31),UN31 )	(Z( 32),NRC )	(Z( 33),IMAX )	(Z( 34),IMAXA )			660
9(Z( 35),JMAX )	(Z( 36),JMAXA )	(Z( 37),KMAX )	(Z( 38),KMAXA )			670

EQUIVALENCE						680
1(Z( 39),BOTH )	(Z( 40),BOTMV )	(Z( 41),NUMSPT)	(Z( 42),CZERO )			690
2(Z( 43),NUMSCA)	(Z( 44),PRLIM )	(Z( 45),PRDELTA)	(Z( 46),PRFACT)			700

EQUIVALENCE						710
1(Z( 47),I1 )	(Z( 48),I2 )	(Z( 49),IPCYCL)	(Z( 50),TSTOP )			720
2(Z( 51),RHOFIL)	(Z( 52),TARGV )	(Z( 53),N3 )	(Z( 54),IVARDY)			730
3(Z( 55),VT )	(Z( 56),N6 )	(Z( 57),RTM )	(Z( 58),RTMV )			740
4(Z( 59),UN59 )	(Z( 60),N10 )	(Z( 61),N11 )	(Z( 62),GAMMA )			750
5(Z( 63),TOPM )	(Z( 64),BOTMU )	(Z( 65),SN )	(Z( 66),TOPMV )			760
6(Z( 67),PRYBOT)	(Z( 68),PRYTOP)	(Z( 69),PRXRT )	(Z( 70),CYCPH3)			770
7(Z( 71),REZFACT)	(Z( 72),TARGI )	(Z( 73),PROJU )	(Z( 74),BBOUND)			780
8(Z( 75),EVAP )	(Z( 76),ECK )	(Z( 77),NECYCL)	(Z( 78),II )			790
9(Z( 79),JJ )	(Z( 80),NMP )	(Z( 81),Y2 )	(Z( 82),EZPH1 )			800

EQUIVALENCE						810
1(Z( 83),IVARDX)	(Z( 84),T )	(Z( 85),NMPMAX)	(Z( 86),PMIN )			820
2(Z( 87),INTER )	(Z( 88),TAYBOT)	(Z( 89),TAYTOP)	(Z( 90),IEMAP )			830
3(Z( 91),MC )	(Z( 92),MR )	(Z( 93),MZ )	(Z( 94),MB )			840

EQUIVALENCE						850
1(Z( 95),REZ )	(Z( 96),NODUMP)	(Z( 97),UN97 )	(Z( 98),UN98 )			860
2(Z( 99),UN99 )	(Z(100),EVAPM )	(Z(101),EVAPEN)	(Z(102),EVAPMU)			870
3(Z(103),EVAPMV)	(Z(104),EZPH2 )	(Z(105),SNL )	(Z(106),STL )			880
4(Z(107),TAXRT )	(Z(108),IDNMAP)	(Z(109),IPRMAP)	(Z(110),ROEPS )			890
5(Z(111),RHINI )	(Z(112),VINI )	(Z(113),FINAL )	(Z(114),IVMAP )			900
6(Z(115),RH0Z )	(Z(116),ESA )	(Z(117),ESEZ )	(Z(118),ESB )			910
7(Z(119),ESCAPA)	(Z(120),ESESP )	(Z(121),ESESQ )	(Z(122),ESES )			920
8(Z(123),ESALPH)	(Z(124),ESBETA)	(Z(125),ESCAPB)	(Z(126),IUMAP )			930
9(Z(127),SS1 )	(Z(128),SS2 )	(Z(129),UMIN )	(Z(130),SS4 )			940

EQUIVALENCE						950
1(Z(131),PRTIME)	(Z(132),EOR )	(Z(133),EOT )	(Z(134),EOB )			960
2(Z(135),EMOR )	(Z(136),DXF )	(Z(137),DYF )	(Z(138),RHOMIN)			970
3(Z(139),STAB)	(Z(140),XIENRG)	(Z(141),XKENRG)	(Z(142),XTENRG)			980
4(Z(143),STT )	(Z(144),DTMIN )	(Z(145),TRNSFC)	(Z(146),EMOT )			990
5(Z(147),JPROJ )	(Z(148),CNAUT )	(Z(149),BBAR )	(Z(150),EMOB )			1000

..... 1020

..... 1030

..... 1040

END OF COMMON 1050

..... 1060

..... 1070

..... 1080

\*\*\* INIALIZE BLANK COMMON 1081

LAST = 1 1082

IQ = 0 1083

IQ = IQ+1 1084

Z(IQ) = 0. 1085

IF(LAST.NE.0) GO TO 5 1086

C  
C  
C  
C  
C  
C  
C

5

10	CALL INPUT	1090
20	CALL CDT	1110
	CALL EDIT	1130
C	*** ASK WFLAGL WHETHER THIS IS THE LAST CYCLE.	1140
C	WFLAGL IS SET IN EDIT.	1145
	IF (WFLAGL.GT.0.) GO TO 40	1150
	CALL PH1	1160
C	*** NPRINT=1 ON EDIT PRINT CYCLES.	1162
C	INTER.NE.0 WHEN INTERMEDIATE EDIT PRINTS ARE WANTED.	1164
	IF (INTER.NE.0.AND.NPRINT.EQ.1) CALL EDIT	1170
C	*** CYCPH3=-1. WHEN PHASE 3 IS NOT USED. OTHERWISE,	1172
C	CYCPH3=NUMBER OF TIMES PHASE 3 CALCULATIONS ARE	1174
C	SUBCYCLED.	1176
	IF (CYCPH3.EQ.(-1.)) GO TO 30	1180
	CALL PH3	1190
	IF (INTER.NE.0.AND.NPRINT.EQ.1) CALL EDIT	1200
30	CALL PH2	1210
	GO TO 20	1220
40	CALL EXIT	1230
	END	1240-



```

SUBROUTINE INPUT
.....
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , INP 40
2 Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102), INP 50
3 GAMC(102), INP 60
4 PK(15), Z(150) , INP 70
5 XP(26,51),YP(26,51), INP 80
6 PL(204) ,UL(204) ,PR(204) , INP 90
7 RSN(52), RST(52), INP 100
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , INP 110
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , INP 120
5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3) INP 130
*** DIMENSIONED ARRAYS INP 140
*** Z-BLOCK IS SAVED ON TAPE. INP 150
COMMON Z INP 160
COMMON PK INP 170
COMMON YY, XX INP 180
COMMON DDX, DDY INP 190
COMMON AMX, AIX, U, V, P INP 200
COMMON TAU, JPM INP 210
COMMON UL, PL INP 220
COMMON XP, YP, CMXP, CMYP INP 230
*** NON-DIMENSIONED VARIABLES INP 240
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR , INP 250
1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY , INP 260
2E ,ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB , INP 270
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT, INP 280
4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID , INP 290
5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF, INP 300
6WFLAGL,WFLAGP INP 310
*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE INP 320
X(0), Y(0), DX(0), DY(0) INP 330
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) INP 340
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) INP 350
*** SPECIAL EQUIVALENCES FOR PH2 ONLY INP 360
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), INP 370
1 (PL,GAMC,PR), (PL(103),SIGC) INP 380
*** SPECIAL EQUIVALENCES FOR PH3 ONLY INP 390
EQUIVALENCE (UL,RSN), INP 400
1 (PL,RST), (P,UK), INP 410
2 (P(157),VK), (P(313),SNB), INP 420
3 (P(365),STB), (P(417),RH0) INP 430
*** SPECIAL EQUIVALENCES FOR EDIT INP 440
EQUIVALENCE (PR(1), IJ), (PR(6), JK) INP 450
*** Z-STORAGE EQUIVALENCES INP 460
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ), INP 470

```

```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), INP 590
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), INP 600
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), INP 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), INP 620
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), INP 630
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), INP 640
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), INP 650
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), INP 660
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) INP 670
EQUIVALENCE INP 680
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), INP 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDEL), (Z( 46),PRFACT) INP 700
EQUIVALENCE INP 710
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), INP 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), INP 730
3(Z( 55),VT ),(Z( 56),N6 ),(Z( 57),RTM ),(Z( 58),RTMV ), INP 740
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), INP 750
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), INP 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), INP 770
7(Z( 71),REZFCT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBOUND), INP 780
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), INP 790
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) INP 800
EQUIVALENCE INP 810
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), INP 820
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), INP 830
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) INP 840
EQUIVALENCE INP 850
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), INP 860
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), INP 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), INP 880
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), INP 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), INP 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), INP 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), INP 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), INP 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) INP 940
EQUIVALENCE INP 950
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), INP 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), INP 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), INP 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), INP 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) INP1000
C INP1010
C ..... INP1020
C ..... INP1030
C END OF COMMON INP1040
C ..... INP1050
C ..... INP1060
C ..... INP1070
C *** MZT MUST EQUAL NUMBER OF WORDS IN Z-ARRAY. INP1080
C MZT=150 INP1090
C *** SET WFLAGF=1. TO SAY THIS IS FIRST CYCLE OF THIS RUN. INP1095
C WFLAGF=1. INP1100
C ..... INP1110
C *** READ AND PRINT ID HEADING CARD (FIRST CARD IN
C INPUT DECK) INP1115
C READ (5,370) IWS INP1120
C WRITE (6,370) IWS INP1130

```

C	*** CARDS ROUTINE WILL READ AND PRINT FIRST DATA CARD.	INP1140
C	CALL CARDS	INP1150
C	*** PK(3).LT.0. MEANS THIS PROBLEM IS BEING RESTARTED FROM	INP1152
C	TAPE 7 AND SETUP IS NOT NEEDED.	INP1155
C	IF (PK(3).LT.0.) GO TO 70	INP1160
C	*** SINCE THE SETUP ROUTINE WRITES ON TAPE 7, MAKE	INP1170
C	SURE THIS IS A SETUP AND NOT A RESTART RUN TO AVOID	INP1180
C	WRITING OVER A GOOD DUMP TAPE.	INP1190
C	CALL CARDS	INP1190
C	*** Z(1)=PROB IS DEFINED BY THE SECOND CARD OF A SETUP	INP1200
C	DECK,BUT IS NOT DEFINED IN A RESTART DECK.	INP1205
C	THEREFORE IF Z(1)=0., THIS IS A RESTART RUN, AND IF	INP1210
C	Z(1).NE.0.,THIS IS A SETUP RUN.	INP1215
5	IF(PROB.EQ.0.)GO TO 230	INP1220
	CALL SETUP	INP1230
	GO TO 70	INP1240
10	CONTINUE	INP1250
	CALL CARDS	INP1260
C	*** INITIALIZE P-STORAGE.	INP1265
20	DO 30 K=1,KMAXA	INP1270
30	P(K)=0.0	INP1280
C	*** SET T AND NC SO THEY WILL EQUAL ZERO ON FIRST EDIT	INP1282
C	PRINT AFTER BEING INCREMENTED BY CDT.	INP1284
	T=T-DTNA	INP1290
	NC=NC-1	INP1300
C	*** CHECK FATAL INPUT ERRORS.	INP1305
32	IF(RHOZ.LE.0.) GO TO 260	INP1310
34	IF(ESCAPA.LT.0.) GO TO 270	INP1320
36	IF(IMAX.EQ.0.OR.JMAX.EQ.0) GO TO 280	INP1340
C	*** DEFINE CONSTANTS USED THROUGHOUT CALCULATION.	INP1345
	CNAUT=SQRT(ESCAPA/RHOZ)	INP1350
	WS=ESESP-ESES	INP1360
	IF (WS.LE.0.) WS=1.	INP1370
	SS1=1./WS	INP1380
	TESTRH = .2*RHOZ	INP1390
	CYCLE=NC	INP1400
	NRZ=NREZ-NUMREZ	INP1420
	SOLID=AMDM*RHOZ	INP1430
	GAMMA=ESA+1.	INP1440
	TWOPI=2.*PIDY	INP1450
	PMIN=10.**6	INP1460
	TRANSFC=.4	INP1470
	VT=10.**(-5)	INP1475
	SS2=1.	INP1480
C	*** SET NUMBER OF SYMBOLS TO BE USED IN PRINTED CONTOUR	INP1482
C	MAPS.	INP1484
	IDNMAP=28.	INP1490
	IIPMAP=26.	INP1500
	IIVMAP=26.	INP1510
	IUMAP=26.	INP1520
	IEMAP=26.	INP1530
C	*** PRINT VALUES OF MOST INPUT PARAMETERS.	INP1555
	WRITE (6,310) NUMREZ,JSTR,N6,IMAX,JMAX,I1,I2,JPROJ,NMPMAX,INTER,NU	INP1560
	INMSCA,IPCYCL,ICSTOP,NFRELP,NDUMP7,NODUMP,IVARDX,IVARDY	INP1570
	WRITE(6,320) DXF,DYF,RHOMIN,TESTRH,RHOZ,RHINI,RHINIT,AMDM,SOLID, V	INP1580
	INP1590	INP1590
	2TK1,STK2,STEZ,ESA,ESB,ESCAPA,ESCAPB,ESALPH,ESBETA,ESEZ,ESES,ESESP,INP1600	INP1600

	3ESESQ,REZFC,SS4,Y2,TRNSFC,DTMIN,PRDEL,PRFACT,PRLIM,TSTOP	INP1610
C	*** PRINT DX,DY ARRAYS WHEN THE CELL DIMENSIONS ARE	INP1620
C	VARIABLE.	INP1625
	IF (IVARDX.EQ.0) GO TO 40	INP1630
	WRITE (6,330)	INP1640
	WRITE (6,350) (I,DX(I),I=1,IMAX)	INP1650
40	IF (IVARDY.EQ.0) GO TO 50	INP1660
	WRITE (6,340)	INP1670
	WRITE (6,350) (J,DY(J),J=1,JMAX)	INP1680
50	CONTINUE	INP1690
C	*** WHEN T.GT.0., PROBLEM IS BEING RESTARTED.	INP1695
	IF (T.GT.0.) GO TO 60	INP1700
C	*** DEFINE TIME OF FIRST EDIT PRINT AFTER CYCLE 0.	INP1705
	PRTIME=PRDEL	INP1710
	GO TO 300	INP1720
C	*** PRDEL = 0. WHEN PRINTING ON CYCLES RATHER TIME.	INP1725
60	IF (PRDEL.EQ.0.) GO TO 300	INP1730
C	*** DEFINE TIME OF FIRST EDIT PRINT AFTER RESTART CYCLE.	INP1735
	IWS=T/PRDEL+1.	INP1740
	PRTIME=FLOAT(IWS)*PRDEL	INP1750
	GO TO 300	INP1760
C	*** READ DUMP TAPE 7.	INP1770
70	CONTINUE	INP1800
	IWS=0	INP1810
80	REWIND 7	INP1820
90	READ (7) PR(1),PR(2),N3	INP1830
C	*** NR = NUMBER OF RECORDS WRITTEN BY EACH TAPE DUMP.	INP1832
C	WHEN N3=1,TRACER POINTS ARE BEING USED AND MAKE UP	INP1834
C	ANOTHER RECORD IN EACH TAPE DUMP.	INP1836
	NR=N3+7	INP1840
C	*** FIRST WORD OF FIRST RECORD OF EACH DUMP SHOULD BE	INP1842
C	555.0. TEST THIS THREE TIMES BEFORE EXITING.	INP1844
	IF (PR(1)-555.0) 100,110,100	INP1850
100	IWS=IWS+1	INP1860
	IF (MOD(IWS,3)) 220,220,80	INP1870
110	IF (PR(2)) 100,120,120	INP1880
C	*** WHEN SETTING UP A PROBLEM PR(2) = PK(2) = 0. WHEN	INP1882
C	RESTARTING A PROBLEM, TAPE 7 IS READ UNTIL	INP1884
C	PR(2).GE.PK(2), THE RESTART CYCLE NUMBER.	INP1886
120	IF (PK(2)-PR(2)) 150,150,130	INP1890
130	DO 140 L=2,NR	INP1900
140	READ (7)	INP1910
	GO TO 90	INP1920
150	READ (7) (Z(I),I=1,MZT)	INP1930
C	*** MAKE SURE PROBLEM NUMBER ON TAPE (PROB) MATCHES	INP1932
C	PROBLEM NUMBER ON INPUT CARDS (PK(1)).	INP1934
	IF (ABS(PROB-PK(1))-0.01) 160,160,210	INP1940
160	READ (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAX)	INP1950
	READ (7) X(0),(X(I),TAU(I),JPM(I),I=1,IMAX)	INP1960
	READ (7) (Y(I),I=0,JMAX)	INP1970
C	*** Y2=-1. WHEN TRACER POINTS ARE USED.	INP1980
	IF (Y2.GT.(-1.)) GO TO 170	INP1990
	READ (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ)	INP2000
170	READ (7) (DX(I),I=1,IMAX)	INP2010
	READ (7) (DY(J),J=1,JMAX)	INP2020
	READ (7) PR(1),PR(2),PR(3)	INP2030
C	*** THE FIRST WORD OF THE LAST RECORD OF EACH DUMP SHOULD	INP2032

	3ESESQ,REZFCT,SS4,Y2,TRNSFC,DTMIN,PRDELTA,PRFACT,PRLIM,TSTOP	INP1610
C	*** PRINT DX,DY ARRAYS WHEN THE CELL DIMENSIONS ARE	INP1620
C	VARIABLE.	INP1625
	IF (IVARDX.EQ.0) GO TO 40	INP1630
	WRITE (6,330)	INP1640
	WRITE (6,350) (I,DX(I),I=1,IMAX)	INP1650
40	IF (IVARDY.EQ.0) GO TO 50	INP1660
	WRITE (6,340)	INP1670
	WRITE (6,350) (J,DY(J),J=1,JMAX)	INP1680
50	CONTINUE	INP1690
C	*** WHEN T.GT.0., PROBLEM IS BEING RESTARTED.	INP1695
	IF (T.GT.0.) GO TO 60	INP1700
C	*** DEFINE TIME OF FIRST EDIT PRINT AFTER CYCLE 0.	INP1705
	PRTIME=PRDELTA	INP1710
	GO TO 300	INP1720
C	*** PRDELTA = 0. WHEN PRINTING ON CYCLES RATHER TIME.	INP1725
60	IF (PRDELTA.EQ.0.) GO TO 300	INP1730
C	*** DEFINE TIME OF FIRST EDIT PRINT AFTER RESTART CYCLE.	INP1735
	IWS=T/PRDELTA+1.	INP1740
	PRTIME=FLOAT(IWS)*PRDELTA	INP1750
	GO TO 300	INP1760
C	*** READ DUMP TAPE 7.	INP1770
70	CONTINUE	INP1800
	IWS=0	INP1810
80	REWIND 7	INP1820
90	READ (7) PR(1),PR(2),N3	INP1830
C	*** NR = NUMBER OF RECORDS WRITTEN BY EACH TAPE DUMP.	INP1832
C	WHEN N3=1,TRACER POINTS ARE BEING USED AND MAKE UP	INP1834
C	ANOTHER RECORD IN EACH TAPE DUMP.	INP1836
	NR=N3+7	INP1840
C	*** FIRST WORD OF FIRST RECORD OF EACH DUMP SHOULD BE	INP1842
C	555.0. TEST THIS THREE TIMES BEFORE EXITING.	INP1844
	IF (PR(1)-555.0) 100,110,100	INP1850
100	IWS=IWS+1	INP1860
	IF (MOD(IWS,3)) 220,220,80	INP1870
110	IF (PR(2)) 100,120,120	INP1880
C	*** WHEN SETTING UP A PROBLEM PR(2) = PK(2) = 0. WHEN	INP1882
C	RESTARTING A PROBLEM, TAPE 7 IS READ UNTIL	INP1884
C	PR(2).GE.PK(2), THE RESTART CYCLE NUMBER.	INP1886
120	IF (PK(2)-PR(2)) 150,150,130	INP1890
130	DO 140 L=2,NR	INP1900
140	READ (7)	INP1910
	GO TO 90	INP1920
150	READ (7) (Z(I),I=1,MZT)	INP1930
C	*** MAKE SURE PROBLEM NUMBER ON TAPE (PROB) MATCHES	INP1932
C	PROBLEM NUMBER ON INPUT CARDS (PK(1)).	INP1934
	IF (ABS(PROB-PK(1))-.01) 160,160,210	INP1940
160	READ (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAXA)	INP1950
	READ (7) (X(I),TAU(I),JPM(I),I=1,IMAX)	INP1960
	READ (7) (Y(I),I=0,JMAX)	INP1970
C	*** Y2=-1. WHEN TRACER POINTS ARE USED.	INP1980
	IF (Y2.GT.(-1.)) GO TO 170	INP1990
	READ (7) (XP(I,J),YP(I,J),I=1,II),J=1,II)	INP2000
170	READ (7) (DX(I),I=1,IMAX)	INP2010
	READ (7) (DY(J),J=1,JMAX)	INP2020
	READ (7) PR(1),PR(2),PR(3)	INP2030
C	*** THE FIRST WORD OF THE LAST RECORD OF EACH DUMP SHOULD	INP2032

```

C          BE 555.0 OR 666.0.
175 IF(PR(1)-555.0) 240,10,180
180 IF(PR(2)-666.0) 250,10,250
200 CALL CARDS
    CALL SETUP
    GO TO 20
C          *** PROBLEM NUMBER ON TAPE 7 NOT THE SAME AS PROBLEM
C          NUMBER ON INPUT CARDS.
210 NK=150
    GO TO 290
C          *** CANNOT FIND FIRST WORD OF FIRST RECORD.
220 NK=100
    GO TO 290
C          *** NOT A RESTART AND YET Z(1) = 0.
230 NK=5
    GO TO 290
C          *** FIRST WORD OF LAST RECORD IS INCORRECT.
240 NK=175
    GO TO 290
C          *** FIRST WORD OF LAST RECORD IS INCORRECT.
250 NK=180
    GO TO 290
C          *** RHOZ.LE.0.
260 NK=32
    GO TO 290
C          *** ESCAPA.LT.0.
270 NK=34
    GO TO 290
C          *** IMAX OR JMAX IS ZERO
280 NK=36
290 NR=1
C          *** PRINT FIRST THREE WORDS OF DUMP (PR(1),PR(2),N3)
C          AND Z(151),Z(152),Z(153).
    WRITE(6,360) PR(1), Z(151), PR(2), Z(152), N3, Z(153)
    CALL ERROR
300 RETURN
C
310 FORMAT (//12X,9H NUMREZ=,I2,7H JSTR=,I3,5H N6=I3,7H IMAX=,I3,7H
1H JMAX=,I3,5H I1=,I3,5H I2=,I3,8H JPROJ=,I3,9H NMPMAX=,I5,8H
2 INTER=,I2,9H NUMSCA=,I2,7H IPCYCL=,I3,9H ICSTOP=,I4,9H NFRELP
3=,I3,9H NDUMP7=,I3,9H NODUMP=,I2,9H IVARDX=,I2,9H IVARDY=,I2//
4)
320 FORMAT (1X,120H          DXF          DYF          RHOMIN          TESTRH
1          RHOZ          RHINI          RHI: 1          AMDM          SOLID
2 VT/1X,1P10E12.4//1X,120H          PS          SN
3          BBAR          CNAUT          FINAL          STAB          DMIN          CVI
4S          SS2/1X,1P10E12.4//1X,120H          CYCPH3          CZERO
5 STK1          STK2          STEZ          ESA          ESB          ESCAPA
6          ESCAPB          ESALPH/1X,1P10E12.4//1X,96H          ESBETA          ES
7EZ          ESES          EESP          ESESQ          REZFCT          SS4
8          Y2/1X,1P8E12.4//1X,72H          TRNSFC          DTMIN          PRDEL
9          PRFACT          PRLIM          TSTOP/1X,1P6E12.4)
330 FORMAT (//7(3H I,6X,2HDR,7X))
340 FORMAT (//7(3H J,6X,2HDZ,7X))
350 FORMAT (7(I4,2X,1PE9.3,3X))
360 FORMAT (1H1,5X,72H*** CHECK FIRST RECORD OF THE DUMP AND FIRST DAT
1A CARD OF THE INPUT DECK // 4X,7HON TAPE,41X,8HON CARDS / 4X,

```

24HWS =,F6.1,4X,7H(555.0),24X, 8HZ(151) =,F8.4,3X,16H(PROBLEM NUMBE  
3R) / 8H CYCLE =,F6.1,4X,18H(CYCLE BEING READ),13X, 8HZ(152) =F5.1,  
46X,15H(RESTART CYCLE) / 4X,4HN3 =,I4,6X,19H(TRACER POINT FLAG) ,  
512X, 8HZ(153) =,F5.1,6X,14H(RESTART FLAG)

.370

FORMAT (I1,71H

1

END

INP2520  
INP2530  
INP2540-

	SUBROUTINE CARDS	CRD 10
	DIMENSION TABLE(1),CARD(7),LABLE(1)	CRD 20
	DIMENSION INPERR(1)	CRD 30
	COMMON TABLE	CRD 40
	EQUIVALENCE(TABLE(1),LABLE(1))	CRD 50
	INPERR=0	CRD 60
	WRITE (6,80)	CRD 70
10	READ (5,90) IEND,LOC,NUMWPC,(CARD(I),I=1,NUMWPC)	CRD 80
	WRITE (6,100) IEND,LOC,NUMWPC,(CARD(I),I=1,NUMWPC)	CRD 90
	IF (NUMWPC.LT.1) GO TO 50	CRD 100
	IF (LOC.LT.1) GO TO 70	CRD 110
	DO 30 I=1,NUMWPC	CRD 120
	J=LOC+I-1	CRD 130
	IF (IEND.NE.2) GO TO 20	CRD 140
	LABLE(J)=JFIX(CARD(I))	CRD 150
	GO TO 30	CRD 160
20	TABLE(J)=CARD(I)	CRD 170
30	CONTINUE	CRD 180
40	IF (IEND.NE.1) GO TO 10	CRD 190
	IF (INPERR.EQ.0) RETURN	CRD 200
	STOP	CRD 210
50	IF (LOC.NE.0) GO TO 70	CRD 220
	DO 60 I=1,7	CRD 230
	IF (CARD(I).NE.0.) GO TO 70	CRD 240
60	CONTINUE	CRD 250
	WRITE (6,120)	CRD 260
	GO TO 40	CRD 270
70	WRITE (6,110)	CRD 280
	INPERR=1	CRD 290
	GO TO 40	CRD 300
C	FORMATS	CRD 310
C		CRD 320
80	FORMAT (/18H INPUT CARDS///)	CRD 330
90	FORMAT (I1,I5,I1,0P7E9.4)	CRD 340
100	FORMAT (1H I4,I7,I3,1P7E14.6)	CRD 350
110	FORMAT (//42H *** ERROR ON PRECEDING DATA CARD *****/)	CRD 360
120	FORMAT (//18H BLANK CARD *****/)	CRD 370
	END	CRD 380-



```

SUBROUTINE SETUP
..... SET 10
..... SET 20
..... SET 30
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) , SET 40
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , SET 50
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102), SIGC(102), SET 60
3 GAMC(102), SET 70
4 PK(15), Z(150) , SET 80
5 XP(26,51),YP(26,51), SET 90
6 PL(204) ,UL(204) ,PR(204) , SET 100
7 RSN(52), RST(52), SET 110
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , SET 120
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , SET 130
5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3) SET 140
C *** DIMENSIONED ARRAYS SET 150
C *** Z-BLOCK IS SAVED ON TAPE. SET 160
COMMON Z SET 170
COMMON PK SET 180
COMMON YY, XX SET 190
COMMON DDX, DDY SET 200
COMMON AMX, AIX, U, V, P SET 210
COMMON TAU, JPM SET 220
COMMON UL , PL SET 230
COMMON XP , YP, CMXP, CMYP SET 240
C *** NON-DIMENSIONED VARIABLES SET 250
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR , SET 260
1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY , SET 270
2E ,ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB , SET 280
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT, SET 290
4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID , SET 300
5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF, SET 310
6WFLAGL,WFLAGP SET 320
C *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE SET 340
C X(0), Y(0), DX(0), DY(0) SET 350
C SET 360
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) SET 370
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) SET 380
C *** SPECIAL EQUIVALENCES FOR PH2 ONLY SET 390
C SET 410
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), SET 420
1 (PL,GAMC,PR), (PL(103),SIGC) SET 430
C *** SPECIAL EQUIVALENCES FOR PH3 ONLY. SET 450
C SET 460
EQUIVALENCE (UL,RSN), SET 470
1 (PL,RST), (P,UK), SET 480
2 (P(157),VK), (P(313),SNB), SET 490
3 (P(365),STB), (P(417),RHO) SET 500
C *** SPECIAL EQUIVALENCES FOR EDIT. SET 520
C SET 530
EQUIVALENCE (PR(1), IJ), (PR(6), JK) SET 540
C *** Z-STORAGE EQUIVALENCES SET 560
C SET 570
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ), SET 580

```

1	(Z( 3),DT )	(Z( 4),NUMSP )	(Z( 5),NFRELP)	(Z( 6),NDUMP7)	SET 590
2	(Z( 7),ICSTOP)	(Z( 8),PIDY )	(Z( 9),TOPMU )	(Z( 10),RTMU )	SET 600
3	(Z( 11),STK1 )	(Z( 12),NUMREZ)	(Z( 13),ETH )	(Z( 14),UN14 )	SET 610
4	(Z( 15),RHINIT)	(Z( 16),PROJI )	(Z( 17),UN17 )	(Z( 18),XMAX )	SET 620
5	(Z( 19),NZ )	(Z( 20),NREZ )	(Z( 21),AMDM )	(Z( 22),UVMAX )	SET 630
6	(Z( 23),UN23 )	(Z( 24),DMIN )	(Z( 25),JSTR )	(Z( 26),DTNA )	SET 640
7	(Z( 27),CVIS )	(Z( 28),STK2 )	(Z( 29),STEZ )	(Z( 30),NC )	SET 650
8	(Z( 31),JN31 )	(Z( 32),NRC )	(Z( 33),IMAX )	(Z( 34),IMAXA )	SET 660
9	(Z( 35),JMAX )	(Z( 36),JMAXA )	(Z( 37),KMAX )	(Z( 38),KMAXA )	SET 670
	EQUIVALENCE				SET 680
1	(Z( 39),BOTM )	(Z( 40),BOTMV )	(Z( 41),NUMSPT)	(Z( 42),CZERO )	SET 690
2	(Z( 43),NUMSCA)	(Z( 44),PRLIM )	(Z( 45),PRDELTA)	(Z( 46),PRFACT)	SET 700
	EQUIVALENCE				SET 710
1	(Z( 47),I1 )	(Z( 48),I2 )	(Z( 49),IPCYCL)	(Z( 50),TSTOP )	SET 720
2	(Z( 51),RHOFIL)	(Z( 52),TARGV )	(Z( 53),N3 )	(Z( 54),IVARDY)	SET 730
3	(Z( 55),VT )	(Z( 56),N6 )	(Z( 57),RTM )	(Z( 58),RTMV )	SET 740
4	(Z( 59),UN59 )	(Z( 60),N10 )	(Z( 61),N11 )	(Z( 62),GAMMA )	SET 750
5	(Z( 63),TOPM )	(Z( 64),BOTMU )	(Z( 65),SN )	(Z( 66),TOPMV )	SET 760
6	(Z( 67),PRYBOT)	(Z( 68),PRYTOP)	(Z( 69),PRXRT )	(Z( 70),CYCPH3)	SET 770
7	(Z( 71),REZFACT)	(Z( 72),TARGI )	(Z( 73),PROJU )	(Z( 74),BBOUND)	SET 780
8	(Z( 75),EVAP )	(Z( 76),ECK )	(Z( 77),NECYCL)	(Z( 78),II )	SET 790
9	(Z( 79),JJ )	(Z( 80),NMP )	(Z( 81),Y2 )	(Z( 82),EZPH1 )	SET 800
	EQUIVALENCE				SET 810
1	(Z( 83),IVARDX)	(Z( 84),T )	(Z( 85),NMPMAX)	(Z( 86),PMIN )	SET 820
2	(Z( 87),INTER )	(Z( 88),TAYBOT)	(Z( 89),TAYTOP)	(Z( 90),IEMAP )	SET 830
3	(Z( 91),MC )	(Z( 92),MR )	(Z( 93),MZ )	(Z( 94),MB )	SET 840
	EQUIVALENCE				SET 850
1	(Z( 95),REZ )	(Z( 96),NODUMP)	(Z( 97),UN97 )	(Z( 98),UN98 )	SET 860
2	(Z( 99),UN99 )	(Z(100),EVAPM )	(Z(101),EVAPEN)	(Z(102),EVAPMU)	SET 870
3	(Z(103),EVAPMV)	(Z(104),EZPH2 )	(Z(105),SNL )	(Z(106),STL )	SET 880
4	(Z(107),TAXRT )	(Z(108),IDNMAP)	(Z(109),IPRMAP)	(Z(110),ROEPS )	SET 890
5	(Z(111),RHINI )	(Z(112),VINI )	(Z(113),FINAL )	(Z(114),IVM/P )	SET 900
6	(Z(115),RHOZ )	(Z(116),ESA )	(Z(117),ESEZ )	(Z(118),ESB )	SET 910
7	(Z(119),ESCAPA)	(Z(120),EESPP )	(Z(121),EESQ )	(Z(122),ESES )	SET 920
8	(Z(123),ESALPH)	(Z(124),ESBETA)	(Z(125),ESCAPB)	(Z(126),IUMAP )	SET 930
9	(Z(127),SS1 )	(Z(128),SS2 )	(Z(129),UMIN )	(Z(130),SS4 )	SET 940
	EQUIVALENCE				SET 950
1	(Z(131),PRTIME)	(Z(132),EOR )	(Z(133),EOT )	(Z(134),EOB )	SET 960
2	(Z(135),EMOR )	(Z(136),DXF )	(Z(137),DYF )	(Z(138),RHOMIN)	SET 970
3	(Z(139),STAB)	(Z(140),XIENRG)	(Z(141),XKENRG)	(Z(142),XTENRG)	SET 980
4	(Z(143),STT )	(Z(144),DTMIN )	(Z(145),TRNSFC)	(Z(146),EMOT )	SET 990
5	(Z(147),JPROJ )	(Z(148),CNAUT )	(Z(149),BBAR )	(Z(150),EMOB )	SET1000
	EQUIVALENCE				SET1010
	*** SPECIAL EQUIVALENCES FOR SETUP ONLY				SET1020
	EQUIVALENCE (RADIUS,PK(12)), (YCENTR,PK(13)), (RHOSPH,Z(100)),				SET1030
1	(SIESPH,Z(101)), (VINSPH,Z(102)), (RHOOUT,Z(103))				SET1040
	EQUIVALENCE				SET1050
	COMMON/ SPHERE / ADDVL, AREAFC, ISPHMX, JCENTR, JSPHBT, JSPHTP,				SET1060
1	RSQRD, VOLSPH, XL2 , XR2 , YBOTTM, YC2 ,				SET1070
2	YDIFFB, YDIFFI, YDIFFO, YDIFFT, YLINTA, YLINTB,				SET1080
3	YLOWER, YRINTA, YRINTB, YTOP , YUPPER				SET1090
	EQUIVALENCE				SET1100
	.....				SET1110
	.....				SET1120
	.....				SET1130
	END OF COMMON				SET1140
	.....				SET1150

C	.....	SET1160
C		SET1170
C	IF (IVARDY.GT.0) GO TO 30	SET1180
C		SET1190
C	*** IF DY VARIABLE, Y(I) WILL BE READ IN RATHER THAN	SET1200
C	CALCULATED.	SET1210
C		SET1220
C	Y(1)=DYF .	SET1230
C	DO 10 J=2,JMAX	SET1240
C	Y(J)=Y(J-1)+DYF	SET1250
10	CONTINUE	SET1260
C		SET1270
C	*** IF DY VARIABLE, DY(I) WILL BE CALCULATED FROM THE Y(I)	SET1280
C	READ IN. IF DY CONSTANT, DY(I) WILL EQUAL DYF FOR	SET1290
C	ALL I.	SET1300
C		SET1310
C	DO 20 I=1,JMAX	SET1320
20	DY(I)=DYF	SET1330
C	GO TO 50	SET1340
C		SET1350
C	*** CALCULATE VARIABLE DY(I).	SET1360
C	DO 40 I=1,JMAX	SET1370
30	DY(I)=Y(I)-Y(I-1)	SET1380
40	CONTINUE	SET1390
50		SET1400
C		SET1410
C	*** IF DX VARIABLE, X(I) WILL BE READ IN RATHER THAN	SET1420
C	CALCULATED	SET1430
C		SET1440
C	IF (IVARDX.GT.0) GO TO 80	SET1450
C	X(1)=DXF	SET1460
C	DO 60 I=2,IMAX	SET1470
C	X(I)=X(I-1)+DXF	SET1480
60	CONTINUE	SET1490
C		SET1500
C	*** IF DX VARIABLE, DX(I) WILL BE CALCULATED FROM	SET1520
C	THE X(I) READ IN. IF DX CONSTANT, DX(I) WILL	SET1525
C	EQUAL DXF FOR ALL I.	SET1530
C		SET1540
C	DO 70 I=1,IMAX	SET1550
C	DX(I)=DXF	SET1560
70	CONTINUE	SET1570
C	GO TO 100	SET1580
C		SET1590
C	*** CALCULATE VARIABLE DX(I)	SET1600
C		SET1610
80	DO 90 I=1,IMAX	SET1620
90	DX(I)=X(I)-X(I-1)	SET1625
C	*** MAKE SURE DX AND DY ARRAYS HAVE BEEN DEFINED.	SET1630
C	IF (DX(1).GT.0..AND.DY(1).GT.0.) GO TO 100	SET1640
95	GO TO 770	SET1650
100	CONTINUE	SET1660
C		SET1662
C	*** PK(3) = -3. WHEN RESTARTING FROM A CLAM TAPE.	SET1664
C	PROPERTIES OF CELLS HAVE ALREADY BEEN DEFINED	SET1666
C	BUT TRACER POINTS HAVE NOT.	SET1670
C	IF (PK(3).EQ.(-3.)) GO TO 700	SET1672
C	*** PRYBOT=-1. MEANS THE PROJECTILE PACKAGE	

```

C          IS NOT BEING USED.                                SET1674
IF (PRYBOT.LT.0.) GO TO 200                                SET1680
C          *** DEFINE CELL BOUNDARIES (MB,MC,MR) OF PROJECTILE SET1690
C          PACKAGE.                                         SET1695
IF (IVARDY.GT.0) GO TO 110                                SET1700
C          *** CALCULATION FOR CONSTANT DY.                 SET1705
MB=INT(PRYBOT/DYF+.5)+1                                   SET1710
IF (MB.GT.JMAX) GO TO 200                                 SET1720
M=1                                                        SET1730
MC=INT(PRYTOP/DYF+.5)                                     SET1740
IF (MC.GT.JMAX) MC=JMAX                                   SET1750
GO TO 160                                                 SET1760
C          *** CALCULATION FOR VARIABLE DY.                 SET1765
110  DYSUM=0.                                              SET1770
      I=0                                                  SET1780
C          *** SEARCH FOR J-VALUE OF BOTTOM OF PROJECTILE (MB). SET1785
IF (PRYBOT.EQ.0.) GO TO 130                               SET1790
DO 120 I=1,JMAX                                           SET1800
DYSUM=DYSUM+DY(I)                                         SET1810
IF (PRYBOT.LT.DYSUM+.5*DY(I+1).AND.PRYBOT.GE.DYSUM-.5*DY(I)) GO TO SET1820
1 130                                                     SET1830
120  CONTINUE                                             SET1840
      GO TO 200                                           SET1850
130  MB=MIN0(I+1,JMAX)                                    SET1860
      M=1                                                  SET1870
C          *** SEARCH FOR J-VALUE OF TOP OF PROJECTILE (MC). SET1875
DO 140 I=MB,JMAX                                          SET1880
DYSUM=DYSUM+DY(I)                                         SET1890
IF (PRYTOP.GE.DYSUM-.5*DY(I).AND.PRYTOP.LT.DYSUM+.5*DY(I+1)) GO TO SET1900
1 150                                                     SET1910
140  CONTINUE                                             SET1920
      MC=JMAX                                             SET1930
      GO TO 160                                           SET1940
150  MC=I                                                 SET1950
C          *** CALCULATION OF I-VALUE OF RIGHT SIDE OF PROJECTILE (MR) SET1955
160  IF (IVARDX.GT.0) GO TO 170                            SET1960
C          *** CALCULATION FOR CONSTANT DX.                 SET1965
MR=INT(PRXRT/DXF+.5)                                     SET1970
IF (MR.GT.IMAX) MR=IMAX                                   SET1980
GO TO 210                                                 SET1990
C          *** CALCULATION FOR VARIABLE DX.                 SET1995
170  DXSUM=0.                                             SET2000
      DO 180 I=1,IMAX                                     SET2010
      DXSUM=DXSUM+DX(I)                                   SET2020
      IF (PRXRT.GE.DXSUM-.5*DX(I).AND.PRXRT.LT.DXSUM+.5*DX(I+1)) GO TO 1 SET2030
190  CONTINUE                                             SET2040
180  MR=IMAX                                             SET2050
      GO TO 210                                           SET2060
190  MR=I                                                 SET2070
      GO TO 210                                           SET2080
C          *** M=0 MEANS THE PROJECTILE PACKAGE IS NOT BEING USED. SET2090
200  M=0                                                  SET2100
C          *** TAYBOT=-1. MEANS THE TARGET PACKAGE IS NOT BEING USED. SET2110
210  IF (TAYBOT.LT.0.) GO TO 310                          SET2115
C          *** DEFINE CELL BOUNDARIES(MZ,N,ME) OF TARGET PACKAGE. SET2120
IF (IVARDY.GT.0) GO TO 220                                SET2130
                                                    SET2140

```

C	*** CALCULATION FOR CONSTANT DY.	SET2145
	MZ=INT(TAYBOT/DYF+.5)+1	SET2150
	IF (MZ.GT.JMAX) GO TO 310	SET2160
	MD=1	SET2170
	N=INT(TAYTOP/DYF+.5)	SET2180
	IF (N.GT.JMAX) N=JMAX	SET2190
	GO TO 270	SET2200
C	*** CALCULATION FOR VARIABLE DY.	SET2205
220	DYSUM=0.	SET2210
	I=0	SET2220
C	*** SEARCH FOR J-VALUE OF BOTTOM OF TARGET (MZ).	SET2225
	IF (TAYBOT.EQ.0.) GO TO 240	SET2230
	DO 230 I=1,JMAX	SET2240
	DYSUM=DYSUM+DY(I)	SET2250
	IF (TAYBOT.GE.DYSUM-.5*DY(I).AND.TAYBOT.LT.DYSUM+.5*DY(I+1)) GO TO	SET2260
1	240	SET2270
230	CONTINUE	SET2280
	GO TO 310	SET2290
240	MZ=MIN0(I+1,JMAX)	SET2300
	MD=1	SET2310
C	*** SEARCH FOR J-VALUE OF TOP OF TARGET (N).	SET2315
	DO 250 I=MZ,JMAX	SET2320
	DYSUM=DYSUM+DY(I)	SET2330
	IF (TAYTOP.GE.DYSUM-.5*DY(I).AND.TAYTOP.LT.DYSUM+.5*DY(I+1)) GO TO	SET2340
1	260	SET2350
250	CONTINUE	SET2360
	N=JMAX	SET2370
	GO TO 270	SET2380
260	N=I	SET2390
C	*** CALCULATION OF I-VALUE OF RIGHT SIDE OF TARGET (ME).	SET2395
270	IF (IVARDX.GT.0) GO TO 280	SET2400
C	*** CALCULATION FOR CONSTANT DX.	SET2405
	ME=INT(TAXRT/DXF+.5)	SET2410
	IF (ME.GT.IMAX) ME=IMAX	SET2420
	GO TO 320	SET2430
C	*** CALCULATION FOR VARIABLE DX.	SET2435
280	DXSUM=0.	SET2440
	DO 290 I=1,IMAX	SET2450
	DXSUM=DXSUM+DX(I)	SET2460
	IF (TAXRT.GE.DXSUM-.5*DX(I).AND.TAXRT.LT.DXSUM+.5*DX(I+1)) GO TO	SET2470
100	320	SET2480
290	CONTINUE	SET2490
	ME=IMAX	SET2500
	GO TO 320	SET2510
300	ME=I	SET2520
	GO TO 320	SET2530
C	*** MD = 0 MEANS THE TARGET PACKAGE IS NOT BEING USED.	SET2540
310	MD=0	SET2550
320	KMAX=IMAX+JMAX+1	SET2560
	KMAXA=KMAX+1	SET2570
	JMAXA=JMAX+1	SET2580
	IMAXA=IMAX+1	SET2590
C	*** INITIALIZE PROPERTY ARRAYS.	SET2595
	DO 330 K=1,KMAX	SET2600
	U(K)=0.0	SET2610
	V(K)=0.0	SET2620
	P(K)=0.0	SET2630

	AMX(K)=0.0	SET2640
	AIX(K)=0.0	SET2650
330	CONTINUE	SET2660
	PIDY=3.1415927	SET2670
	WS=X(1)**2	SET2680
C	*** CALCULATE CELL-FACE AREA, THE AREA GENERATED BY SEGMENT	SET2682
C	X(I),X(I+1) ROTATED ABOUT THE Z-AXIS.	SET2684
	TAU(1)=PIDY*WS	SET2690
	DO 340 I=2,IMAX	SET2700
	WSA=X(I)**2	SET2710
	TAU(I)=PIDY*(WSA-WS)	SET2720
	WS=WSA	SET2730
340	CONTINUE	SET2740
	ETH=0.0	SET2750
C	*** RADIUS.GT.0. MEANS SPHERE IS TO BE USED.	SET2760
C	SEE SPECIAL EQUIVALENCES FOR SETUP FOR LOCATION	SET2770
C	OF PARAMETERS DEFINING DIMENSIONS AND PROPERTIES OF	SET2780
C	SPHERE.	SET2790
	IF (RADIUS.LE.0.) GO TO 540	SET2850
C	*** COMPUTE ISPHMX, THE I-INDEX OF THE RIGHT-MOST COLUMN	SET2860
C	CONTAINING A PART OF THE SPHERE.	SET2870
	DO 350 I=1,IMAX	SET2900
	IF (X(I).GE.RADIUS-.000001*DX(I)) GO TO 360	SET2910
350	CONTINUE	SET2920
360	ISPHMX=I	SET2930
	TOTSPH=0.	SET2940
C	*** COMPUTE JCENTR=J-INDEX OF SPHERE-CENTER	SET2950
	DO 370 J=0,JMAX	SET2960
	IF ((Y(J)+.5*DY(J+1)).GT.YCENTR) GO TO 380	SET2970
370	CONTINUE	SET2980
C	*** YCENTR SHOULD FALL ON CELL BOUNDARY,	SET2990
C	PRINT OUT INPUT VALUE AND ADJUSTED VALUE.	SET3000
380	WRITE (6,790) YCENTR,Y(J)	SET3010
	YCENTR=Y(J)	SET3020
	JCENTR=J	SET3030
C	COMPUTE JRADA AND JRADB.	SET3035
C	*** JRADB = THE NUMBER OF CELLS CONTAINING A PART OF THE	SET3040
C	SPHERE FROM THE CENTER TO BOTTOM EDGE	SET3050
C	*** JRADA = THE NUMBER OF CELLS CONTAINING A PART OF THE	SET3060
C	SPHERE FROM THE CENTER TO TOP EDGE.	SET3070
	JRADB=0	SET3080
	JRADA=0	SET3090
	JB=JCENTR	SET3100
	JA=JCENTR+1	SET3110
	SUM1=0.	SET3120
	SUM2=0.	SET3130
	IF (JCENTR.EQ.0) GO TO 400	SET3140
390	SUM1=SUM1+DY(JB)	SET3150
	JB=JB-1	SET3160
	JRADB=JRADB+1	SET3170
	IF (SUM1.LT.(RADIUS-.000001*DY(JB))) GO TO 390	SET3180
400	SUM2=SUM2+DY(JA)	SET3190
	JA=JA+1	SET3200
	JRADA=JRADA+1	SET3210
	IF (SUM2.LT.(RADIUS-.000001*DY(JA))) GO TO 400	SET3220
C	*** COMPUTE(1)JSPHTP=J-INDEX OF UPPER-MOST ROW	SET3230
C	*** WHICH CONTAINS PART OF THE SPHERE	SET3240

C	***	(2)JSPHBT=J-INDEX OF LOWEST ROW	SET3250
C	***	WHICH CONTAINS PART OF THE SPHERE	SET3250
		JSPHBT=MAX0(1,JCENTR-JRADB+1)	SET3270
		JSPHTP=MIN0(JMAX,JCENTR+JRADA)	SET3280
C		YC2=YCENTR**2	SET3290
		RSQRD=RADIUS**2	SET3300
C	***	FOR EACH CELL IN RECTANGLE FROM X=0.	SET3310
C	***	TO X=(ISPHMX-1)*DXF AND FROM	SET3320
C	***	Y=(JSPHBT-1)*DYF TO Y=(JSPHTP)*DYF	SET3330
C	***	FIND VOLSPH=VOLUME OF SPHERE IN CELL K	SET3340
C	***	AND SET MASS AND SPEC. INT. ENERGY.	SET3350
		DO 530 I=1,ISPHMX	SET3360
		K=(JSPHBT-1)*IMAX+I+1	SET3370
C	***	X(I-1)=VALUE OF X AT LEFT OF COLUMN	SET3380
C	***	X(I)=VALUE OF X AT RIGHT OF COLUMN	SET3390
		XL2=(X(I-1))**2	SET3400
		XR2=(X(I))**2	SET3410
C	***	YLINTA=Y LEFT-INTERCEPT-ABOVE-CENTER	SET3420
C	***	YLINTB=Y LEFT-INTERCEPT-BELOW-CENTER	SET3430
		WS=SQRT(RSQRD-XL2)	SET3440
		YLINTA=YCENTR+WS	SET3450
		YLINTB=YCENTR-WS	SET3460
C	***	DOES CURVE INTERSECT X=X(I)	SET3470
		IF (RSQRD.LE.XR2) GO TO 410	SET3480
C	***	YES	SET3490
		WS=SQRT(RSQRD-XR2)	SET3500
		YRINTA=YCENTR+WS	SET3510
		YRINTB=YCENTR-WS	SET3520
		GO TO 420	SET3530
410		YRINTA=YCENTR	SET3540
		YRINTB=YCENTR	SET3550
420		CONTINUE	SET3560
		DO 520 J=JSPHBT,JSPHTP	SET3570
C	***	SKIP IF SPECIAL CELL	SET3610
		IF (AMX(K).NE.0.) GO TO 520	SET3620
		YTOP=Y(J)	SET3630
		YBOTTM=Y(J-1)	SET3640
		YDIFFT=(YTOP-YCENTR)**2	SET3650
		YDIFFB=(YBOTTM-YCENTR)**2	SET3660
		YDIFFO=AMAX1(YDIFFT,YDIFFB)	SET3670
		YDIFFI=AMIN1(YDIFFT,YDIFFB)	SET3680
C	***	IS ALL OF CELL WITHIN SPHERE BOUNDARY.	SET3690
		IF ((YDIFFO+XR2).GT.RSQRD) GO TO 430	SET3700
C	***	YES. DEFINE VOLUME OF CELL.	SET3710
		VOLSPH=TAU(I)*DY(J)	SET3720
		GO TO 470	SET3725
C	***	NO. IS ALL OF CELL OUTSIDE SPHERE BOUNDARY.	SET3730
430		IF ((YDIFFI+XL2).LT.RSQRD) GO TO 440	SET3735
C	***	YES.	SET3740
		VOLSPH=0.	SET3750
		GO TO 510	SET3752
C	***	NO. PART OF CELL IS WITHIN SPHERE. COMPUTE VOLUME	SET3754
C		OF PART OF CELL INSIDE THE SPHERE AND STORE	SET3756
C		IN VOLSPH.	SET3760
440		IF (J.GT.JCENTR) GO TO 450	SET3770
		YLOWER=AMAX1(YBOTTM,YLINTB)	

```

YUPPER=AMIN1(YTOP,YRINTB) SET3790
ADDVL=(YTOP-YUPPER)*TAU(I) SET3790
GO TO 460 SET3800
450 YLOWER=AMAX1(YBOTTM,YRINTA) SET3810
YUPPER=AMIN1(YTOP,YLINTA) SET3820
ADDVL=(YLOWER-YBOTTM)*TAU(I) SET3830
460 VOLSPH=ADDVL+PIDY*((RSQRD-YC2-XL2)*(YUPPER-YLOWER)-((YUPPER**3-YLOW
1ER**3)/3.+YCENTR*(YUPPER**2-YLOWER**2)) SET3840
470 WS=VOLSPH*RHOSPH SET3860
AMX(K)=WS SET3870
C *** CHECK WHETHER THE CELL IS FULL SET3880
WSA=TAU(I)*DY(J) SET3890
WSB=WSA-VOLSPH SET3900
IF (ABS(WSB/WSA).LT.ROEPS) GO TO 490 SET3910
C *** ADD RHOOUT MATERIAL TO CELL. SET3920
WSB=WSB*RHOOUT SET3930
AMX(K)=WS+WSB SET3940
C *** CHECK WHETHER MASS IS TOO SMALL TO KEEP SET3945
IF (AMX(K)/WSA.LT.EVAP*RHINI) GO TO 510 SET3950
C *** USE A WEIGHTED AVERAGE OF THE PROPERTIES OF THE SPHERE SET3960
AND THE PROJECTILE FOR CELLS PARTIALLY IN THE SPHERE. SET3965
AIX(K)=(WS*SIESPH+WSB*PROJI)/AMX(K) SET3970
V(K)=(WS*VINSPH+WSB*VINI)/AMX(K) SET3980
GO TO 500 SET3990
C *** ESSENTIALLY ALL OF CELL IS IN SPHERE SET4030
490 AIX(K)=SIESPH SET4040
V(K)=VINSPH SET4050
C *** SUM SPHERE VOLUME SET4060
500 TOTSPH=TOTSPH+VOLSPH SET4070
GO TO 520 SET4080
510 AMX(K)=0. SET4090
C *** END OF J-LOOP SET4100
520 K=K+IMAX SET4110
C *** END OF I-LOOP SET4120
530 CONTINUE SET4130
540 WRITE (6,800) RHOSPH,RHINI,RHINIT,RHOFIL,SIESPH,PROJI,TARGI,VINSPH SET4140
1,VINI,TARGV,PROJU,RADIUS,PRYTOP,TAYTOP,YCENTR,PRYBOT,TAYBOT,PRXRT, SET4150
2TAXRT SET4160
C *** RESET BORROWED Z-STORAGE TO ZERO. SET4162
EVAPM = 0. SET4164
EVAPEN = 0. SET4166
EVAPMU = 0. SET4168
EVAPMV = 0. SET4169
C *** M=0 MEANS THE PROJECTILE PACKAGE IS NOT BEING USED. SET4170
IF (M.EQ.0) GO TO 610 SET4220
DO 600 I=M,MR SET4230
K=(MB-1)*IMAX+I+1 SET4240
C *** ASSIGN PROPERTIES TO CELLS IN PROJECTILE. SET4250
DO 590 J=MB,MC SET4260
IF (AMX(K).NE.0.) GO TO 550 SET4270
AMX(K)=RHINI*DY(J)*TAU(I) SET4280
550 IF (V(K).NE.0.) GO TO 560 SET4290
V(K)=VINI SET4300
560 IF (U(K).NE.0.) GO TO 570 SET4310
U(K)=PROJU SET4320
570 IF (AIX(K).NE.0.) GO TO 580 SET4330
AIX(K)=PROJI SET4340

```



580	CONTINUE	SET4350
590	K=K+IMAX	SET4360
600	CONTINUE	SET4370
C	*** MD=0 MEANS THE TARGET PACKAGE IS NOT BEING USED.	SET4380
610	IF (MD.EQ.0) GO TO 650	SET4390
C	*** ASSIGN PROPERTIES TO CELLS IN TARGET.	SET4395
	DO 640 I=MD,ME	SET4400
	K=(MZ-1)*IMAX+I+1	SET4410
	DO 630 J=MZ,N	SET4420
	IF (V(K).NE.0.) GO TO 620	SET4430
	V(K)=TARGV	SET4440
	IF (AMX(K).NE.0.) GO TO 630	SET4450
	AMX(K)=RHINIT*DY(J)*TAU(I)	SET4460
620	AIX(K)=TARGI	SET4470
630	K=K+IMAX	SET4480
640	CONTINUE	SET4490
650	CONTINUE	SET4500
C		SET4510
	CYCLE=0.0	SET4520
	DT=0.0	SET4530
	NREZ=NUMREZ	SET4540
	NZ=1	SET4550
C	*** RHOFIL=0. WHEN THERE IS NO FILLER MATERIAL BETWEEN	SET4560
C	PROJECTILE AND TARGET.	SET4565
	IF (RHOFIL.EQ.0.) GO TO 680	SET4570
C	*** FILL BETWEEN PACKAGES WITH MATERIAL OF DENSITY=RHOFIL.	SET4580
	MC=MC+1	SET4590
	MZ=MZ-1	SET4600
	DO 670 I=1,IMAX	SET4610
	K=(MC-1)*IMAX+I+1	SET4620
	DO 660 J=MC,MZ	SET4630
	AMX(K)=RHOFIL*DY(J)*TAU(I)	SET4640
660	K=K+IMAX	SET4650
670	CONTINUE	SET4660
680	N3=0	SET4670
C	*** PK(14).GT.0. MEANS SOME CELLS WILL BE DEFINED	SET4672
C	AFTER PACKAGES ARE SET UP.	SET4674
	IF (PK(14).GT.0.) CALL CARDS	SET4680
C	*** CALCULATE INITIAL VALUE OF TOTAL ENERGY TO BE ADJUSTED	SET4682
C	WHEN MATERIAL IS EVAPORATED OR CROSSES A TRANSMITTIVE	SET4684
C	BOUNDARY AND TO BE USED IN EDIT TO CHECK ERROR IN	SET4686
C	ENERGY SUM.	SET4688
	DO 690 K=2,KMAX	SET4690
	ETH=ETH+AMX(K)*(.5*(U(K)**2+V(K)**2)+AIX(K))	SET4700
690	CONTINUE	SET4710
	XMAX=X(IMAX)	SET4720
	TXMAX=XMAX*2.0	SET4730
	YMAX=Y(JMAX)	SET4740
	TYMAX=YMAX*2.0	SET4750
700	IF (Y2.GT.(-1.)) GO TO 750	SET4760
C	*** PUT TRACER POINT IN CENTER OF EVERY OTHER NONEMPTY CELL	SET4770
C	IN EVERY OTHER ROW. THE TRACER POINT COORDINATES OF	SET4772
C	EMPTY CELLS ARE (0,0).	SET4774
	II=IMAX/2	SET4780
	JJ=JMAX/2	SET4790
	DO 720 J=1,JJ	SET4800
	DO 720 I=1,II	SET4810

	K=2*((J-1)*IMAX+I)	SET4820
	IF (AMX(K).EQ.0.) GO TO 710	SET4830
	XP(I,J)=FLOAT(2*I-1)-.5	SET4840
	YP(I,J)=FLOAT(2*J-1)-.5	SET4850
710	NMP=NMP+1	SET4860
C	*** NMPMAX IS THE MAXIMUM NUMBER OF TRACER POINTS TO	SET4862
C	BE USED AND IS DEFINED IN THE INPUT DECK.	SET4864
	IF (NMP.GE.NMPMAX) GO TO 730	SET4870
720	CONTINUE	SET4880
	GO TO 740	SET4890
730	JJ=J	SET4900
C	*** N3=1 MEANS TRACER POINTS ARE BEING USED, ADDING	SET4902
C	ONE MORE RECORD TO EACH TAPE DUMP.	SET4904
740	N3=1	SET4910
750	REWIND 7	SET4920
	WS=555.0	SET4930
C	WRITE OUTPUT FOR OIL ON TAPE.	SET4940
	WRITE (7) WS,CYCLE,N3	SET4950
	WRITE (7) (Z(I),I=1,MZT)	SET4960
	WRITE (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAX)	SET4970
	WRITE (7) X(0),(X(I),TAU(I),JPM(I),I=1,IMAX)	SET4980
	WRITE (7) (Y(I),I=0,JMAX)	SET4990
	IF (Y2.GT.(-1.)) GO TO 760	SET5000
	WRITE (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ)	SET5010
760	WRITE (7) (DX(I),I=1,IMAX)	SET5020
	WRITE (7) (DY(J),J=1,JMAX)	SET5030
	WS=666.0	SET5040
	WRITE (7) WS,WS,WS	SET5050
	GO TO 780	SET5060
C	*** DX AND/OR DY ARRAY NOT PROPERLY DEFINED.	SET5062
C	CHECK VALUE OF DXF AND DYF IF ZONES ARE CONSTANT.	SET5064
C	IF VARIABLE, CHECK LOCATION NUMBERS USED FOR	SET5065
C	READING IN X AND/OR Y ARRAY (SPECIALLY IF ANY	SET5066
C	VARIABLE DIMENSIONS WERE CHANGED.	SET5068
770	NK=95	SET5070
	NR=2	SET5080
	CALL ERROR	SET5090
780	RETURN	SET5100
C		SET5110
790	FORMAT (/5X,15HINPUT YCENTR = ,1PE12.6,6X,18HADJUSTED YCENTR = ,1P	SET5120
	1E12.6)	SET5130
800	FORMAT (////17X,18HINITIAL CONDITIONS//11X,6HSPHERE,13X,9HPACKAGE	SET5140
	11,21H PACKAGE 2 FILLER//8H DENSITY,1P1E12.4,6X,1P3E12.4/8H S.	SET5150
	2I.E.,1P1E12.4,6X,1P2E12.4/8H V,1P1E12.4,6X,1P2E12.4/8H	SET5160
	3 U,13X,1P1E12.4/8H RADIUS,1P1E12.4,5X,3HTOP,1P1E10.4,1P1E12.4/8H	SET5170
	4YCENTER,1P1E12.4,2X,6HBOTTOM,1P1E10.4,1P1E12.4/23X,5HRIGHT,1P1E10.	SET5180
	54,1P1E12.4)	SET5190
	END	SET5200-

	SUBROUTINE CDT	CDT 10
	.....	CDT 20
		CDT 30
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	CDT 40
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,	CDT 50
2	Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),	CDT 60
3	GAMC(102),	CDT 70
4	PK(15), Z(150) ,	CDT 80
5	XP(26,51),YP(26,51),	CDT 90
6	PL(204) ,UL(204) ,PR(204) ,	CDT 100
7	RSN(52), RST(52),	CDT 110
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	CDT 120
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	CDT 130
5	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3)	CDT 140
	*** DIMENSIONED ARRAYS	CDT 150
	*** Z-BLOCK IS SAVED ON TAPE.	CDT 160
	COMMON Z	CDT 170
	COMMON PK	CDT 180
	COMMON YY, XX	CDT 190
	COMMON DDX, DDY	CDT 200
	COMMON AMX, AIX, U, V, P	CDT 210
	COMMON TAU, JPM	CDT 220
	COMMON UL, PL	CDT 230
	COMMON XP, YP, CMXP, CMYP	CDT 240
	*** NON-DIMENSIONED VARIABLES	CDT 250
	COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR,	CDT 260
1	AMVT, DELEB, DELER, DELET, DELM, DTOCX, DXYMIN, EAMMP, EAMPY,	CDT 270
2	E, ERDUMP, I, I3, IWS, J, K, KA, KB,	CDT 280
3	LL, MD, ME, MZT, NERR, NK, NPRINT,	CDT 290
4	NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID,	CDT 300
5	SUM, TESTRH, TWOPI, URR, WS, WSA, WSB, WSC, WFLAGF,	CDT 310
6	WFLAGL, WFLAGP	CDT 320
		CDT 330
	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	CDT 340
	X(0), Y(0), DX(0), DY(0)	CDT 350
		CDT 360
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	CDT 370
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	CDT 380
		CDT 390
	*** SPECIAL EQUIVALENCES FOR PH2 ONLY.	CDT 400
		CDT 410
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	CDT 420
1	(PL,GAMC,PR), (PL(103),SIGC)	CDT 430
		CDT 440
	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	CDT 450
		CDT 460
	EQUIVALENCE (UL,RSN),	CDT 470
1	(PL,RST), (P,UK),	CDT 480
2	(P(157),VK), (P(313),SNB),	CDT 490
3	(P(365),STB), (P(417),RH0)	CDT 500
		CDT 510
	*** SPECIAL EQUIVALENCES FOR EDIT	CDT 520
		CDT 530
	EQUIVALENCE (PR(1), IJ), (PR(6), JK)	CDT 540
		CDT 550
	*** Z-STORAGE EQUIVALENCES	CDT 560
		CDT 570
	EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),	CDT 580

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), CDT 590  
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), CDT 600  
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), CDT 610  
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), CDT 620  
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), CDT 630  
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), CDT 640  
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), CDT 650  
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), CDT 660  
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) CDT 670  
EQUIVALENCE CDT 680  
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), CDT 690  
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDELTA),(Z( 46),PRFACT) CDT 700  
EQUIVALENCE CDT 710  
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), CDT 720  
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), CDT 730  
3(Z( 55),VT ),(Z( 56),N6 ),(Z( 57),RTM ),(Z( 58),RTMV ), CDT 740  
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), CDT 750  
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), CDT 760  
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), CDT 770  
7(Z( 71),REZFACT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBOUND), CDT 780  
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL), (Z( 78),II ), CDT 790  
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) CDT 800  
EQUIVALENCE CDT 810  
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), CDT 820  
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), CDT 830  
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) CDT 840  
EQUIVALENCE CDT 850  
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), CDT 860  
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), CDT 870  
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), CDT 880  
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), CDT 890  
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), CDT 900  
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), CDT 910  
7(Z(119),ESCAPA),(Z(120),EESPE ),(Z(121),ESESQ ),(Z(122),ESES ), CDT 920  
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), CDT 930  
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) CDT 940  
EQUIVALENCE CDT 950  
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EGB ), CDT 960  
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), CDT 970  
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), CDT 980  
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), CDT 990  
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) CDT1000  
CDT1010  
..... CDT1020  
..... CDT1030  
END OF COMMON CDT1040  
..... CDT1050  
..... CDT1060  
..... CDT1070  
\*\*\* SPECIAL EQUIV FOR ES AND CDT CDT1080  
EQUIVALENCE (RHOW,NULLE) CDT1090  
..... CDT1100  
\*\*\*CHECK COURANT CONDITION AND PARTICLE VELOCITY. CDT1110  
\*\*\*RECORD I AND J OF ZONE WHERE DT IS CONTROLLED. CDT1120  
\*\*\*FIRST CALCULATE PRESSURES FROM EQ. OF ST. CDT1130  
..... CDT1140  
..... CDT1220

10	TRIAL=0.	CDT1230
	SRATIO=10.**10	CDT1240
C	**WSC WILL BE MAXIMUM U OR V	CDT1250
	WSC=0.	CDT1260
	DO 60 I=1,I1	CDT1270
	K=I+1	CDT1280
	DO 60 J=1,I2	CDT1290
	RHOW=AMX(K)/(TAU(I)*DY(J))	CDT1330
	CALL ES	CDT1340
C	*** IF DENSITY OF CELL K IS LESS THAN RHOMIN, IT'S	CDT1342
C	VELOCITY OR SOUND SPEED IS NOT USED IN DETERMINING DT.	CDT1344
	IF (RHOW.LT.RHOMIN) GO TO 30	CDT1350
	IF (ABS(P(K)).LT.PMIN) P(K)=0.	CDT1360
	IF (CNAUT.GT.0.) GO TO 20	CDT1370
C		CDT1380
C	***CALCULATE SOUND SPEED FOR POLYTOPIC GAS WITH	CDT1390
C	***GAMMA EQUAL TO ESA+1.	CDT1400
	WS=SQRT(GAMMA*ABS(P(K))/RHOW)	CDT1410
	GO TO 40	CDT1420
C		CDT1430
C	***CHECK FOR NEGATIVE PRESSURE.	CDT1440
20.	IF (P(K).GT.0.) GO TO 30	CDT1450
C	*** NEGATIVE PRESSURES NOT ALLOWED ALONG GRID BOUNDARY	CDT1452
C	AND NOT ALLOWED ANYWHERE UNTIL ACTIVE GRID REACHES	CDT1454
C	JSTR(INPUT PARAMETER FOR TURNING ON STRENGTH	CDT1456
C	CALCULATIONS).	CDT1458
	IF ((IMAX.NE.1.AND.I.EQ.IMAX).OR.J.EQ.JMAX.OR.I2.LT.JSTR) P(K)=0.	CDT1460
C		CDT1470
C	***PRESSURE IS NEGATIVE OR ZERO	CDT1480
	WS=CNAUT	CDT1490
	GO TO 40	CDT1500
C		CDT1510
C	***PRESSURE IS POSITIVE.	CDT1520
30	WS=CNAUT+BBAR*SQRT(P(K))	CDT1530
	WSA=SQRT(GAMMA*P(K)/RHOW)	CDT1540
	WS=AMAX1(WS,WSA)	CDT1550
C	*** WS IS SOUND SPEED OF CELL K.	CDT1552
C	*** WSB IS MAXIMUM OF RADIAL AND AXIAL VELOCITY OF CELL K.	CDT1554
C	*** WSC STORES MAXIMUM VELOCITY OF CELLS USED TO DETERMINE	CDT1556
C	DT. PRINTED AS MAXUV.	CDT1558
40	WSB=AMAX1(ABS(U(K)),ABS(V(K)))	CDT1560
	WSC=AMAX1(WSC,WSB)	CDT1570
	WS=AMAX1(WS,WSB)	CDT1580
C	*** TRIAL STORES MAXIMUM OF VELOCITY AND SOUND SPEED USED	CDT1582
C	TO DETERMINE DT. PRINTED AS MAXCUV.	CDT1584
	IF (WS.LE.TRIAL) GO TO 50	CDT1590
	TRIAL=WS	CDT1600
50	IF (WS.LE.0.) GO TO 60	CDT1610
	DXYMIN=AMIN1(DX(I),DY(J))	CDT1620
	RATIO=DXYMIN/WS	CDT1630
	IF (RATIO.GT.SRATIO) GO TO 60	CDT1640
C	*** I AND J OF CELL CONTROLLING DT STORED IN N10 AND N11	CDT1642
C	FOR PRINTOUT.	CDT1644
	N10=I	CDT1650
	N11=J	CDT1660
C	*** SRATIO IS SMALLEST VALUE CALCULATED FOR RATIO.	CDT1665
	SRATIO=RATIO	CDT1670

```

C
C
C          ***END OF I, J LOOP
60      K=K+IMAX
C          *** IF TRIAL.LE.0. THERE IS PROBABLY AN ERROR IN THE INP JT
C          PARAMETERS FOR THE INITIAL VELOCITY, ENERGY OR DENSITY
C          OF THE PACKAGES.
65      IF (TRIAL.LE.0.) GO TO 170
C          *** IF FINAL.EQ.0.USE STAB FOR VALUE OF STABILITY FRACTION
C          IF FINAL.GT.0,USE A GEOMETRIC PROGRESSION WITH STAB
C          AS THE INITIAL VALUE AND FINAL AS THE FINAL VALUE.
C          IF (FINAL.EQ.0.) GO TO 70
C          STAB=2.*STAB
C          STAB=AMIN1(STAB,FINAL)
70      DT=STAB*SRATIO
C          IF (STAB.LT.FINAL) GO TO 80
C          *** AFTER STAB.GE.FINAL CHECK ON SIZE OF DT. DTMIN IS AN
C          INPUT PARAMETER AND CAN BE SET TO 0.
75      IF (DT.LE.DTMIN) GO TO 150
80      CONTINUE
C
C          *** IS CONTROL-CELL ISOLATED
C          K=(N11-1)*IMAX+N10+1
C          WS=0.
C          IF (N10.GT.1) WS=AMX(K-1)
C          IF (N10.LT.IMAX) WS=AMX(K+1)+WS
C          IF (N11.GT.1) WS=AMX(K-IMAX)+WS
C          IF (N11.LT.JMAX) WS=AMX(K+IMAX)+WS
C          IF (WS.GT.0.) GO TO 90
C          *** ISOLATED, SO DESTROY IT.
C          WS=(AIX(K)+(U(K)**2+V(K)**2)*.5)*AMX(K)
C          EVAPM=EVAPM+AMX(K)
C          EVAPEN=EVAPEN+WS
C          ETH=ETH-WS
C          EVAPMU=EVAPMU+AMX(K)*U(K)
C          EVAPMV=EVAPMV+AMX(K)*V(K)
C          WRITE (6,290) N10,N11,T,DT,TRIAL,WSC,UMIN,PMIN
C          AMX(K)=0.
C          AIX(K)=0.
C          P(K)=0.
C          U(K)=0.
C          V(K)=0.
C          *** RECALCULATE DT.
C          GO TO 10
C          *** INCREMENT TIME AND CYCLE.
90      T=T+DTNA
95      IF (T.LT.0.) GO TO 160
C          NC=NC+1
C          CYCLE=NC
C
C          *** RESET NPRINT. NPRINT=1 ON PRINT CYCLES.
C          NPRINT=0
C          *** DEFINE VELOCITY AND ENERGY CUTOFFS USED IN MAP AND PH2.
C          UMIN=TRIAL*ROEPS
C          SIEMIN=UMIN**2
C          PMIN=RHOZ*CNAUT*UMIN
C          IF (PMIN.LT.ROEPS) PMIN=UMIN*RHOZ*TRIAL
C          WRITE (6,290) N10,N11,T,DT,TRIAL,WSC,UMIN,PMIN

```

```

DTNA=DT CDT2170
C *** TESTRH = .2*RHOZ CDT2171
C THE PRESSURE OF COLD,FREE SURFACE CELLS IS REDUCED BY ACDT2172
C FACTOR,F, WHICH ACCOUNTS FOR THE EFFECT OF FREE SURFACE CDT2173
C LOCATION ON THE PRESSURE GRADIENT, F IS THE DENSITY OF CDT2174
C THE LOWEST DENSITY ADJACENT CELL DIVIDED BY THE NORMAL CDT2175
C DENSITY,OR F IS TESTRH - WHICHEVER IS SMALLEST CDT2176
WT=TESTRH CDT2180
DO 140 I=1,I1 CDT2190
K=I+1 CDT2200
DO 140 J=1,I2 CDT2210
RHOW=AMX(K)/(DY(J)*TAU(I)) CDT2220
WTB=WT CDT2230
IF (AIX(K).GE.ESESQ) GO TO 140 CDT2240
IF (RHOW.LT.SOLID) GO TO 140 CDT2250
IF (I.EQ.IMAX) GO TO 100 CDT2260
WTA=AMX(K+1)/(DY(J)*TAU(I+1)) CDT2270
IF (WTA.LT.WT) WTB=WTA CDT2280
100 IF (I.EQ.1) GO TO 110 CDT2290
WTA=AMX(K-1)/(DY(J)*TAU(I-1)) CDT2300
IF (WTA.LT.WTB) WTB=WTA CDT2310
110 IF (J.EQ.JMAX) GO TO 120 CDT2320
KA=K+IMAX CDT2330
WTA=AMX(KA)/(DY(J+1)*TAU(I)) CDT2340
IF (WTA.LT.WTB) WTB=WTA CDT2350
120 IF (J.EQ.1) GO TO 130 CDT2360
KB=K-IMAX CDT2370
WTA=AMX(KB)/(DY(J-1)*TAU(I)) CDT2380
IF (WTA.LT.WTB) WTB=WTA CDT2390
130 IF (WTB.LT.WT) P(K)=P(K)*WTB/RHOZ CDT2400
140 K=K+IMAX CDT2410
GO TO 190 CDT2420
C CDT2430
C *** DT TOO SMALL CDT2440
150 NK=75 CDT2450
GO TO 180 CDT2460
C *** T IS NEGATIVE CDT2470
160 NK=95 CDT2480
GO TO 180 CDT2490
C *** DT WILL BE NEGATIVE OR ZERO. CDT2500
170 NK=65 CDT2510
GO TO 180 CDT2520
180 NR=3 CDT2530
CALL ERROR CDT2540
C CDT2550
C ***FIND THE MAXIMUM PRESSURE ON EACH COLUMN AND CDT2560
C ***STORE ITS CELL NUMBER AS JPM. THIS WILL BE USED CDT2570
C ***IN DETERMINING THE REGION IN WHICH PHASE 3 IS CDT2580
C ***USED. WSA WILL BE A RUNNING MAXIMUM OF THE CDT2590
C ***PRESSURE IN THE GRID. CDT2600
190 WSA=-1.E30 CDT2610
DO 260 I=1,I1 CDT2620
C *** WS WILL BE LOCAL MAXIMUM OF COLUMN I. CDT2621
WS=-1.E30 CDT2630
K=(I2-1)*IMAX+I+1 CDT2640
JP=I2 CDT2650
JINTL=1 CDT2660

```

C	*** START AT TOP OF COLUMN AND LOOK FOR PRESSURE PEAK.	CDT2665
200	DO 210 J=JINTL,I2	CDT2670
C	IF (P(K).LT.WS) GO TO 220	CDT2680
C	WS=P(K)	CDT2690
C	*** JP IS J-INDEX OF CELL WITH PEAK PRESSURE.	CDT2695
C	JP=JP-1	CDT2700
210	K=K-IMAX	CDT2710
C	*** IF YOU FALL THROUGH, THEN THERE WAS NO MAXIMUM IN THIS	CDT2720
C	COLUMN	CDT2730
C	GO TO 250	CDT2740
C	*** COME HERE IF PRESSURE HAS PASSED A LOCAL MAXIMUM	CDT2750
C	*** PTEMP IS PEAK PRESSURE OF COLUMN I.	CDT2760
220	PTEMP=P(K+IMAX)	CDT2770
C	IF (PTEMP.LT.WSA) GO TO 230	CDT2780
C	*** WSA WILL BE PEAK PRESSURE IN ACTIVE GRID (ABSOLUTE	CDT2790
C	MAXIMUM).	CDT2800
C	WSA=PTEMP	CDT2805
C	GO TO 240	CDT2810
C	*** PTEMP IS LOCAL MAXIMUM BUT IS LESS THAN ABSOLUTE	CDT2820
C	MAXIMUM	CDT2830
230	IF (PTEMP.GT.0.3*WSA) GO TO 240	CDT2840
C	*** THIS LOCAL MAXIMUM IS NOT BIG ENOUGH TO USE FOR JPM	CDT2850
C	JINTL=J+1	CDT2860
C	*** WE MAY HAVE REACHED BOTTOM OF COLUMN	CDT2870
C	IF (JINTL.GE.I2) GO TO 250	CDT2880
C	*** CONTINUE DOWN COLUMN SEARCHING FOR SUFFICIENTLY LARGE	CDT2890
C	LOCAL MAXIMUM.	CDT2900
C	JP=JP-1	CDT2910
C	*** IF POSITION OF PEAK PRESSURE IN COLUMN I DOES NOT	CDT2920
C	ADVANCE FROM ONE CYCLE TO THE NEXT, DO NOT CHANGE	CDT2930
C	VALUE OF JPM.	CDT2940
240	JP=JP+1	CDT2945
C	IF (JP.LE.JPM(I)) GO TO 260	CDT2950
C	JPM(I)=JP	CDT2952
C	***IF JPM IS ZERO THE SHOCK HAS NEVER REACHED THIS	CDT2954
C	***LOCATION. IF IT IS NONZERO THE SHOCK HAS PASSED	CDT2960
C	***AND WE MUST CONTINUE TO INCREASE I UNTIL THE	CDT2970
C	***RIGHT BOUNDARY OF THE SHOCK IS REACHED.	CDT2980
250	IF (JPM(I).LE.0) GO TO 270	CDT2982
C	*** END OF I LOOP.	CDT2984
260	CONTINUE	CDT2986
C	*** IF PEAK PRESSURE OF COLUMN I HAS GONE BELOW A THIRD	CDT2990
C	THE GRID MAXIMUM, AND IF JPM(I)=0. FROM THE PREVIOUS	CDT3000
C	CYCLE, WE HAVE REACHED THE RIGHT EDGE OF THE SHOCK.	CDT3010
270	CONTINUE	CDT3020
C	*** JPM(I) MUST BE MONOTONIC DECREASING	CDT3030
C	K=I1-1	CDT3040
		CDT3050
		CDT3060
		CDT3070
		CDT3075
		CDT3080
		CDT3090
		CDT3100
		CDT3110
		CDT3130
		CDT3140
		CDT3150



	DO 280 IWS=1,K	CDT3160
	I=I1-IWS	CDT3170
280	IF (JPM(I).LT.JPM(I+1)) JPM(I)=JPM(I+1)	CDT3180
	RETURN	CDT3190
C		CDT3200
290	FORMAT (/4H CDT,I3,I4,4H T=,1PE13.7,5H DT=,1PE13.7,9H MAXCUV=,1	CDT3210
	1PE13.7,8H MAXUV=,1PE13.7,7H UMIN=,1PE13.7,7H PMIN=,1PE13.7)	CDT3220
	END	CDT3230-

	SUBROUTINE ES	ES	10
C	.....	ES	20
C		ES	30
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	ES	40
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,	ES	50
2	Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),	ES	60
3	GAMC(102).	ES	70
4	PK(15), Z(150) ,	ES	80
5	XP(26,51),YP(26,51),	ES	90
6	PL(204) ,UL(204) ,PR(204) ,	ES	100
7	RSN(52), RST(52),	ES	110
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	ES	120
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	ES	130
\$	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)	ES	140
C	*** DIMENSIONED ARRAYS	ES	150
C	*** Z-BLOCK IS SAVED ON TAPE.	ES	160
	COMMON Z	ES	170
	COMMON PK	ES	180
	COMMON YY, XX	ES	190
	COMMON DDX, DDY	ES	200
	COMMON AMX, AIX, U, V, P	ES	210
	COMMON TAU, JPM	ES	220
	COMMON UL, PL	ES	230
	COMMON XP, YP, CMXP, CMYP	ES	240
C	*** NON-DIMENSIONED VARIABLES	ES	250
	COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR, ,	ES	260
1	AMVT, DELEB, DELER, DELET, DELM, DTODX, DXYMIN, EAMMP, EAMPY, ,	ES	270
2	E, ERDUMP, I, I3, IWS, J, K, KA, KB, ,	ES	280
3	LL, MD, ME, MZT, NERR, NK, NPRINT, ,	ES	290
4	NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID, ,	ES	300
5	SUM, TESTRH, TWOPI, URR, WS, WSA, WSB, WSC, WFLAGF, ,	ES	310
6	WFLAGL, WFLAGP	ES	320
C		ES	330
C	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	ES	340
C	X(0), Y(0), DX(0), DY(0)	ES	350
C		ES	360
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	ES	370
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	ES	380
C		ES	390
C	*** SPECIAL EQUIVALENCES FOR PH2 ONLY	ES	400
C		ES	410
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	ES	420
1	(PL,GAMC,PR), (PL(103),SIGC)	ES	430
C		ES	440
C	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	ES	450
C		ES	460
	EQUIVALENCE (UL,RSN),	ES	470
1	(PL,RST), (P,UK),	ES	480
2	(P(157),VK), (P(313),SNB),	ES	490
3	(P(365),STB), (P(417),RHO)	ES	500
C		ES	510
C	*** SPECIAL EQUIVALENCES FOR EDIT	ES	520
C		ES	530
	EQUIVALENCE (PR(1), IJ), (PR(6), JK)	ES	540
C		ES	550
C	*** Z-STORAGE EQUIVALENCES	ES	560
C		ES	570
	EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),	ES	580

```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), ES 590
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), ES 600
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), ES 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), ES 620
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), ES 630
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), ES 640
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), ES 650
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), ES 660
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) ES 670
EQUIVALENCE ES 680
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), ES 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDEL), (Z( 46),PRFACT) ES 700
EQUIVALENCE ES 710
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), ES 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), ES 730
3(Z( 55),VT ),(Z( 56),N6 ),(Z( 57),RTM ),(Z( 58),RTMV ), ES 740
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), ES 750
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), ES 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), ES 770
7(Z( 71),REZFACT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBOUND), ES 780
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), ES 790
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) ES 800
EQUIVALENCE ES 810
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), ES 820
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), ES 830
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) ES 840
EQUIVALENCE ES 850
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), ES 860
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), ES 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), ES 880
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), ES 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), ES 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), ES 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), ES 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), ES 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) ES 940
EQUIVALENCE ES 950
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), ES 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), ES 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), ES 980
4(Z(143),SIT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), ES 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) ES 1000
ES 1010
*** SPECIAL EQUIV FOR ES AND CDT ES 1012
EQUIVALENCE (RHOW,NULLE) ES 1014
..... ES 1020
..... ES 1030
END OF COMMON ES 1040
..... ES 1050
..... ES 1060
*** P(K) CALCULATED FROM RHOW AND AIX(K). ES 1065
RHOW IS CALCULATED IN CDT ES 1070
..... ES 1070
IF (ESCAPA.LE.0.) GO TO 30 ES 1110
ETA=RHOW/RHOZ ES 1120
VOW=1./ETA ES 1130
IF (AIX(K).LE.0.) GO TO 20 ES 1140

```

C  
C  
C  
C  
C  
C  
C  
C  
C

C	*** P1 AND P4 ARE THERMAL PRESSURE TERMS.	ES 1145
	P1=AIX(K)*RHOW*ESA	ES 1150
	P4=ESb/(AIX(K)/(ESEZ*ETA**2)+1.)*AIX(K)*RHOW	ES 1160
C	*** P5 IS MECHANICAL PRESSURE TERM	ES 1165
10	P5=ESCAPA*(ETA-1.)	ES 1170
	P2=-1.	ES 1180
C	*** IF MATERIAL IS UNDER-DENSE AND ITS ENERGY IS BETWEEN	ES 1182
C	ESES AND ESESP, A COMBINATION OF THE EXPANDED AND	ES 1184
C	CONDENSED EQUATIONS OF STATE IS USED.	ES 1186
	IF (ETA.GE.1.) GO TO 50	ES 1190
C	*** ESESP = ENERGY TO VAPORIZE MATERIAL. MUST EXCEED ESES.	ES 1195
	IF (A.X(K).GT.ESESP) GO TO 40	ES 1200
C	*** ESES = ENERGY TO BRING MATERIAL TO VAPOR TEMPERATURE.	ES 1205
	IF (AIX(K).GT.ESES) P2=1.	ES 1210
C	*** P2=1 MEANS BOTH THE EXPANDED AND COMPRESSED	ES 1212
C	FORMULATIONS WILL BE USED. OTHERWISE, P2=-1.	ES 1214
	GO TO 50	ES 1220
C	*** WHEN SPECIFIC INTERNAL ENERGY OF CELL IS NEGATIVE,	ES 1222
C	THERMAL PRESSURES ARE SET TO ZERO.	ES 1224
20	P1=0.	ES 1230
	P4=0.	ES 1240
C	*** WHEN SPECIFIC INTERNAL ENERGY IS NEGATIVE OR ZERO AND	ES 1242
C	DENSITY IS LESS THAN SOLID, SET PRESSURE TO ZERO.	ES 1244
	IF (ETA.LT.AMDM) GO TO 80	ES 1250
	GO TO 10	ES 1260
C	*** IDEAL GAS	ES 1265
30	P(K)=ESA*RHOW*AIX(K)	ES 1270
	GO TO 90	ES 1280
C	*** EXPANDED STATE	ES 1290
40	P8=(1.-VOW)	ES 1300
	P9=EXP(ESALPH*P8)	ES 1310
	P12=EXP(-ESBETA*P8**2)	ES 1320
	P(K)=P1+(P4+P5*P9)*P12	ES 1330
	IF (P2.LT.0.) GO TO 70	ES 1340
	P1=SS1*(AIX(K)-ESES)	ES 1350
	P(K)=P1*P(K)+(1.-P1)*P3	ES 1360
	GO TO 70	ES 1370
C	*** CONDENSED STATE	ES 1380
C	P6 IS MECHANICAL PRESSURE TERM.	ES 1385
50	P6=ESCAPB*((ETA-1.)**2)	ES 1390
	P(K)=P1+P4+P5+P6	ES 1400
	IF (P2.LT.0.) GO TO 60	ES 1410
C	*** USING COMBINATION OF CONDENSED AND EXPANDED EQUATIONS	ES 1412
C	OF STATE.	ES 1414
	IF (P(K).LT.0.) P(K)=0.	ES 1420
	P3=P(K)	ES 1430
	GO TO 40	ES 1440
C	*** USING CONDENSED EQUATION OF STATE	ES 1445
60	IF (P(K).GE.0.) GO TO 90	ES 1450
C	*** IF MATERIAL IS EXPANDED OR J-INDEX OF CELL IS LESS	ES 1452
C	THAN N6, SET NEGATIVE PRESSURE TO ZERO. (N6 IS INPUT	ES 1454
C	PARAMETER)	ES 1456
	IF (J.LE.N6.OR.ETA.LE.AMDM) GO TO 80	ES 1460
	GO TO 90	ES 1470
C	*** SET NEGATIVE PRESSURES TO ZERO WHEN USING COMBINED	ES 1472
C	OR EXPANDED EQUATIONS OF STATE.	ES 1474
70	IF (P(K).GE.0.) GO TO 90	ES 1480

80 P(K)=0.  
90 RETURN  
END

ES 1490  
ES 1500  
ES 1510-

	SUBROUTINE EDIT	10
C	.....	20
C		30
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	40
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,CRAD(52),	50
2	Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102),	60
3	GAMC(102),	70
4	PK(15), Z(150) ,	80
5	XP(26,51),YP(26,51),	90
6	PL(204) ,UL(204) ,PR(204) ,	100
7	RSN(52), RST(52),	110
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	120
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	130
5	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3)	140
C	*** DIMENSIONED ARRAYS	150
C	*** Z-BLOCK IS SAVED ON TAPE.	160
	COMMON Z	170
	COMMON PK	180
	COMMON YY, XX	190
	COMMON DDX, DDY	200
	COMMON AMX, AIX, U, V, P	210
	COMMON TAU, JPM	220
	COMMON UL, PL	230
	COMMON XP, YP, CMXP, CMYP	240
C	*** NON-DIMENSIONED VARIABLES	250
	COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR, ,	260
1	AMVT, DELEB, DELER, DELET, DELM, DTODX, DXYMIN, EAMMP, EAMPY, ,	270
2	E, ERDUMP, I, I3, IWS, J, K, KA, KB, ,	280
3	LL, MD, ME, MZT, NERR, NK, NPRINT, ,	290
4	NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID, ,	300
5	SUM, TESTRH, TWOPI, JRR, WS, WSA, WSB, WSC, WFLAGF, ,	310
	6WFLAGL, WFLAGP	320
C		330
C	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	340
C	X(0), Y(0), DX(0), DY(0)	350
C		360
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	370
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	380
C		390
C	*** SPECIAL EQUIVALENCES FOR PH2 ONLY	400
C		410
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	420
1	(PL,GAMC,PR), (PL(103),SIGC)	430
C		440
C	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	450
C		460
	EQUIVALENCE (UL,RSN),	470
1	(PL,RST), (P,UK),	480
2	(P(157),VK), (P(313),SNB),	490
3	(P(365),STB), (P(417),RH0)	500
C		510
C	*** SPECIAL EQUIVALENCES FOR EDIT	520
C		530
	EQUIVALENCE (PR(1), IJ), (PR(6), JK), (UL(103),CRAD)	540
C		550
C	*** Z-STORAGE EQUIVALENCES	560
C		570
	EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),	58.

1(Z( 3),DT )	(Z( 4),NUMSP )	(Z( 5),NFRELP)	(Z( 6),NDUMP7)	590		
2(Z( 7),ICSTOP)	(Z( 8),PIDY )	(Z( 9),TOPMU )	(Z( 10),RTMU )	600		
3(Z( 11),STK1 )	(Z( 12),NUMREZ)	(Z( 13),ETH )	(Z( 14),UN14 )	610		
4(Z( 15),RHINIT)	(Z( 16),PROJI )	(Z( 17),UN17 )	(Z( 18),XMAX )	620		
5(Z( 19),NZ )	(Z( 20),NREZ )	(Z( 21),AMDM )	(Z( 22),UVMAX )	630		
6(Z( 23),UN23 )	(Z( 24),DMIN )	(Z( 25),JSTR )	(Z( 26),DTNA )	640		
7(Z( 27),CVIS )	(Z( 28),STK2 )	(Z( 29),STEZ )	(Z( 30),NC )	650		
8(Z( 31),UN31 )	(Z( 32),NRC )	(Z( 33),IMAX )	(Z( 34),IMAXA )	660		
9(Z( 35),JMAX )	(Z( 36),JMAXA )	(Z( 37),KMAX )	(Z( 38),KMAXA )	670		
EQUIVALENCE				680		
1(Z( 39),BOTM )	(Z( 40),BOTMV )	(Z( 41),NUMSPT)	(Z( 42),CZERO )	690		
2(Z( 43),NUMSCA)	(Z( 44),PRLIM )	(Z( 45),PRDELTA)	(Z( 46),PRFACT)	700		
EQUIVALENCE				710		
1(Z( 47),I1 )	(Z( 48),I2 )	(Z( 49),IPCYCL)	(Z( 50),TSTOP )	720		
2(Z( 51),RHOFIL)	(Z( 52),TARGV )	(Z( 53),N3 )	(Z( 54),IVARDY)	730		
3(Z( 55),VT )	(Z( 56),N6 )	(Z( 57),RTM )	(Z( 58),RTMV )	740		
4(Z( 59),UN59 )	(Z( 60),N10 )	(Z( 61),N11 )	(Z( 62),GAMMA )	750		
5(Z( 63),TOPM )	(Z( 64),BOTMU )	(Z( 65),SN )	(Z( 66),TOPMV )	760		
6(Z( 67),PRYBOT)	(Z( 68),PRYTOP)	(Z( 69),PRXRT )	(Z( 70),CYCPH3)	770		
7(Z( 71),REZFCT)	(Z( 72),TARGI )	(Z( 73),PROJU )	(Z( 74),BBOUND)	780		
8(Z( 75),EVAP )	(Z( 76),ECK )	(Z( 77),NECYCL)	(Z( 78),II )	790		
9(Z( 79),JJ )	(Z( 80),NMP )	(Z( 81),Y2 )	(Z( 82),EZPH1 )	800		
EQUIVALENCE				810		
1(Z( 83),IVARDX)	(Z( 84),T )	(Z( 85),NMPMAX)	(Z( 86),PMIN )	820		
2(Z( 87),INTER )	(Z( 88),TAYBOT)	(Z( 89),TAYTOP)	(Z( 90),IEMAP )	830		
3(Z( 91),MC )	(Z( 92),MR )	(Z( 93),MZ )	(Z( 94),MB )	840		
EQUIVALENCE				850		
1(Z( 95),REZ )	(Z( 96),NODUMP)	(Z( 97),UN97 )	(Z( 98),UN98 )	860		
2(Z( 99),UN99 )	(Z(100),EVAPM )	(Z(101),EVAPEN)	(Z(102),EVAPMU)	870		
3(Z(103),EVAPMV)	(Z(104),EZPH2 )	(Z(105),SNL )	(Z(106),STL )	880		
4(Z(107),TAXRT )	(Z(108),IDNMAP)	(Z(109),IPRMAP)	(Z(110),ROEPS )	890		
5(Z(111),RHINI )	(Z(112),VINI )	(Z(113),FINAL )	(Z(114),IVMAP )	900		
6(Z(115),RHOZ )	(Z(116),ESA )	(Z(117),ESEZ )	(Z(118),ESB )	910		
7(Z(119),ESCAPA)	(Z(120),EESP )	(Z(121),ESESQ )	(Z(122),ESES )	920		
8(Z(123),ESALPH)	(Z(124),ESBETA)	(Z(125),ESCAPB)	(Z(126),IUMAP )	930		
9(Z(127),SS1 )	(Z(128),SS2 )	(Z(129),UMIN )	(Z(130),SS4 )	940		
EQUIVALENCE				950		
1(Z(131),PRTIME)	(Z(132),EOR )	(Z(133),EOT )	(Z(134),EOB )	960		
2(Z(135),EMOR )	(Z(136),DXF )	(Z(137),DYF )	(Z(138),RHOMIN)	970		
3(Z(139),STAB)	(Z(140),XIENRG)	(Z(141),XKENRG)	(Z(142),XTENRG)	980		
4(Z(143),STT )	(Z(144),DTMIN )	(Z(145),TRNSFC)	(Z(146),EMOT )	990		
5(Z(147),JPROJ )	(Z(148),CNAUT )	(Z(149),BBAR )	(Z(150),EMOB )	1000		
.....				1010		
.....				1020		
END OF COMMON				1030		
.....				1040		
.....				1050		
.....				1060		
.....				1070		
**: SPECIAL EQUIV. FOR EDIT				1080		
EQUIVALENCE (PR(1),TJETAR)				(PR(2),TKETAR)	(PR(3),TETAR )	1090
1	(PR(4),TARMAS)	(PR(5),TARMV )	(PR(6),TARMVP)	1100		
2	(PR(7),RAMOMA)	(PR(8),PRAMOA)	(PR(9),TIEPRO)	1110		
3	(PR(10),TKEPRO)	(PR(11),TEPRO)	(PR(12),PRMAS)	1120		
4	(PR(13),PRMV )	(PR(14),PRMVP)	(PR(15),RAMOMB)	1130		
5	(PR(16),PRAMOB)			1140		
DIMENSION PROPI(50)				1150		

C  
C  
C  
C  
C  
C  
C  
C

C		1160
C	*** ERDUMP=1. WHEN ERROR CALLS EDIT FOR A TAPE DUMP ONLY	1162
	IF (ERDUMP.GT.0.) GO TO 150	1170
C	*** ENERGY SUM (ESUM) AND RELATIVE ERROR IN SUM (RELERR)	1172
C	COMPUTED. ECK IS LARGEST ERROR COMPUTED AND ON PRINT	1174
C	CYCLES IS PRINTED AND COMPARED TO DMIN, MAXIMUM	1176
C	ALLOWABLE ERROR.	1178
	ESUM=0.	1180
	DO 10 K=2,KMAX	1190
10	ESUM=ESUM+AMX(K)*(.5*(U(K)**2+V(K)**2)+AIX(K))	1200
	RELERR=(ESUM-ETH)/ETH	1210
	IF (ABS(RELERR).LT,ABS(ECK)) GO TO 20	1220
	ECK=RELERR	1230
	NECYCL=NC	1240
20	CONTINUE	1250
C	*** NPRINT = 1 WHEN EDIT IS CALLED TO DO AN INTERMEDIATE	1252
C	PRINT. SKIP TESTS ON TIME TO STOP, PRINT, REZONE,ETC.	1254
C	WHICH ALREADY HAVE BEEN DONE FOR THIS CYCLE.	1256
	IF (NPRINT.EQ.1) GO TO 190	1260
C	*** I3=1 SIGNALS A SHORT PRINT	1270
	I3=1	1280
C	*** IF THIS IS FIRST CYCLE OF RUN, WFLAGF=1.	1290
	IF (WFLAGF.GT.0.) GO TO 120	1300
C	*** IS THIS THE TIME OR CYCLE TO STOP EXECUTION	1305
	IF (ICSTOP.LE.NC.AND.ICSTOP.GT.0) GO TO 30	1310
	IF (T*(1.+ROEPS).GE.TSTOP.AND.TSTOP.GT.0.) GO TO 30	1320
C	*** SHOULD THE GRID BE REZONED	1325
	IF ((REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT.0).OR.SS4.NE.0.) GO	1330
	1 TO 190	1340
C		1350
	GO TO 40	1360
C	*** SET WFLAGL=1. TO SAY THIS IS LAST CYCLE OF RUN	1370
30	WFLAGL=1.	1380
	I3=I1	1390
	NPRINT=1	1400
	NUMSPT=NDUMP7	1410
	NUMSP=0	1420
	GO TO 190	1430
40	ASSIGN 140 TO LOCA	1440
	ASSIGN 110 TO LOCB	1450
C	*** ARE WE PRINTING ON TIME OR CYCLE INTERVALS.	1455
	IF (PRDEL.NE.0.) GO TO 50	1460
45	IF (IPCYCL.NE.0) GO TO 100	1470
	GO TO 430	1480
C	*** PRINTING ON TIME. IS IT TIME TO PRINT	1485
50	IF (T*(1.+ROEPS).GE.PRTIME) GO TO 70	1490
C	*** NO. BUT WILL NEXT CYCLE BYPASS THE PRINT TIME	1495
	IF (PRTIME.GE.T+DT) GO TO 60	1500
	DT=PRTIME-T	1510
	DTNA=DT	1520
60	GO TO LOCA, (140,130)	1530
C	*** YES, IT IS TIME TO PRINT. NPRINT=1 FLAGS THIS AS A	1532
C	PRINT CYCLE.	1534
70	NPRINT=1	1540
C	*** AVOID TRUNCATION	1550
	T=PRTIME	1560
C	*** IS IT TIME TO RESCALE PRINT INTERVAL	1565



	IF (T*(1.+ROEPS).LT.PRLIM.OR.NUMSCA.LE.0) GO TO 80	1570
C	*** CHANGE PRINT INTERVAL AND THE TIME FOR THE NEXT	1580
C	RESCALING.	1585
	PRDEL=PRDEL*PRFACT	1590
	PRLIM=PRLIM*PRFACT	1600
	NUMSCA=NUMSCA-1	1610
C	*** DEFINE TIME FOR NEXT PRINT.	1615
80	PRTIME=T+PRDEL	1620
	IWS=(PRTIME+.5*PRDEL)/PRDEL	1630
	WS=IWS	1640
	PRTIME=WS*PRDEL	1650
C	*** WILL WE BYPASS TIME TO PRINT	1655
	IF (PRTIME.GE.T+DT) GO TO 90	1660
C	*** YES, ADJUST DT	1665
	DT=PRTIME-T	1670
	DTNA=DT	1680
90	GO TO LOCB, (110,130)	1690
C	*** PRINTING ON CYCLES. IS THIS A PRINT CYCLE	1695
100	IF (MOD(NC,IPCYCL).NE.0) GO TO LOCA, (140,130)	1700
C	*** YES. NPRINT = 1 FLAGS THIS AS A PRINT CYCLE.	1705
	NPRINT=1	1710
C	*** IS THIS THE CYCLE TO RESCALE PRINT INTERVAL	1715
	IF (NC.LT.PRLIM.OR.NUMSCA.LE.0) GO TO LOCB, (110,130)	1720
C		1730
C	*** YES. MULTIPLY NUMBER OF CYCLES BETWEEN PRINTS BY PRFACT	1740
C		1750
	IPCYCL=INT(PRFACT)*IPCYCL	1760
	PRLIM=PRFACT*PRLIM	1770
	NUMSCA=NUMSCA-1	1780
	GO TO LOCB, (110,130)	1790
C	*** TEST FOR SHORT OR LONG PRINT	1800
C	*** NUMSP COUNTS NUMBER OF SHORT PRINTS SINCE LAST LONG	1802
C	PRINT. NUMSPT COUNTS NUMBER OF CYCLES SINCE LAST	1804
C	TAPE DUMP.	1806
110	NUMSP=NUMSP+1	1810
	NUMSPT=NUMSPT+1	1820
	IF (NUMSP.NE.NFRELP) GO TO 190	1830
	NUMSP=0	1840
C	*** I3=I1 SIGNALS A LONG PRINT	1850
120	I3=I1	1860
C	*** PRINT OF RESTART CYCLE WILL BE SHORT IF PK(3).LT.-1.	1865
	IF (PK(3).LT.-1..AND.WFLAGF.GT.0.) I3=1	1870
	GO TO 190	1880
C	*** CHECK FOR ENERGY DISCREPANCY	1890
130	IF (ABS(ECK).GT.DMIN) GO TO 440	1900
C	*** IF LAST CYCLE, REWIND TAPE	1910
140	IF (WFLAGL.EQ.0.) GO TO 470	1920
	REWIND 7	1930
	GO TO 470	1940
150	NUMSPT=0	1950
	IF (NODUMP.NE.0) GO TO 170	1960
	BACKSPACE 7	1970
	WS=555.0	1980
	WRITE (7) WS,CYCLE,N3	1990
	WRITE (7) (Z(L),L=1,MZT)	2000
	WRITE (7) (U(K),V(K),AMX(K),AIX(K),P(K),K=1,KMAX)	2010
	WRITE (7) X(0),(X(K),TAU(K),JPM(K),K=1,IMAX)	2020

	WRITE (7) (Y(K),K=0,JMAX)	2030
C	*** ARE TRACER POINTS BEING GENERATED	2035
	IF (Y2.GT.(-1.)) GO TO 160	2040
C	*** YES. WRITE TRACER POINT COORDINATES (XP,YP) ON TAPE.	2045
	WRITE (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ)	2050
160	WRITE (7) (DX(I),I=1,IMAX)	2060
	WRITE (7) (DY(J),J=1,JMAX)	2070
	WS=666.0	2080
	WRITE (7) WS,WS,WS	2090
	WRITE (6,550) NC	2100
	IF (WFLAGL.EQ.0.) GO TO 170	2110
	END FILE 7	2120
170	CONTINUE	2130
	IF (ERDUMP.GT.0.) CALL EXIT	2140
	GO TO 260	2150
180	N=2	2160
	GO TO 220	2170
C	*** INITIALIZE PR ARRAY, TEMPORARY STORAGE FOR ENERGY, MASS	2172
C	AND MOMENTUM TOTALS PRINTED OUT.	2174
190	DO 200 I=1,16	2180
200	PR(I)=0.	2190
C		2200
C	RAMOMA=RADTAL MOMENTUM ABOVE JPROJ	2210
C	RAMOMA=RADTAL MOMENTUM BELOW JPROJ	2220
C	PRAMOA=POSITIVE RADIAL MOMENTUM ABOVE JPROJ	2230
C	PRAMOB=POSITIVE RADIAL MOMENTUM BELOW JPROJ	2240
C		2250
	IF (JPROJ.EQ.0) GO TO 180	2260
	N=IMAX*JPROJ+1	2270
	DO 210 K=2,N	2280
	WS=AMX(K)	2290
	PRMAS=PRMAS+WS	2300
	TIEPRO=TIEPRO+WS*AIX(K)	2310
	TKEPRO=TKEPRO+.5*WS*(U(K)**2+V(K)**2)	2320
	WSA=WS*V(K)	2330
	PRMV=PRMV+WSA	2340
	IF (WSA.GT.0.) PRMVP=PRMVP+WSA	2350
	RAMOMB=RAMOMB+AMX(K)*U(K)	2360
	IF (U(K).GT.0.) PRAMOB=PRAMOB+AMX(K)*U(K)	2370
210	CONTINUE	2380
	N=N+1	2390
220	DO 230 K=N,KMAX	2400
	WS=AMX(K)	2410
	TARMAS=TARMAS+WS	2420
	TIETAR=TIETAR+WS*AIX(K)	2430
	TKETAR=TKETAR+.5*WS*(U(K)**2+V(K)**2)	2440
	WSA=WS*V(K)	2450
	TARMV=TARMV+WSA	2460
	IF (WSA.GT.0.) TARMVP=TARMVP+WSA	2470
	RAMOMA=RAMOMA+AMX(K)*U(K)	2480
	IF (U(K).GT.0.) PRAMOA=PRAMOA+AMX(K)*U(K)	2490
230	CONTINUE	2500
	TETAR=TIETAR+TKETAR	2510
	TEPRO=TIEPRO+TKEPRO	2520
	DO 240 J=1,8	2530
	PR(J+16)=PR(J)+PR(J+8)	2540
240	CONTINUE	2550

	IF (IMAX.GT.1) GO TO 250	2560
C		2570
C	*** IF DOING A 1-D PROBLEM DIVIDE TOTALS BY NZ WHERE	2580
C	NZ=4**(NUMBER OF TIMES THE GRID HAS BEEN REZONED.)	2585
C		2590
	PROPI(1)=ETH/NZ	2600
	PROPI(2)=ECK/NZ	2610
	PROPI(4)=EZPH1/NZ	2620
	PROPI(5)=EZPH2/NZ	2630
	PROPI(6)=BBOUND/NZ	2640
	DO 250 J=1,24	2650
250	PROPI(J+6)=PR(J)/NZ	2660
	PROPI(31)=BOTM/NZ	2670
	PROPI(32)=RTM/NZ	2680
	PROPI(33)=TOPM/NZ	2690
	PROPI(34)=EVAPM/NZ	2700
	PROPI(35)=EMOB/NZ	2710
	PROPI(36)=EMOR/NZ	2720
	PROPI(37)=EMOT/NZ	2730
	PROPI(38)=EVAPEN/NZ	2740
	PROPI(39)=BOTMU/NZ	2750
	PROPI(40)=RTMU/NZ	2760
	PROPI(41)=TOPMU/NZ	2770
	PROPI(42)=EVAPMU/NZ	2780
	PROPI(43)=BOTMV/NZ	2790
	PROPI(44)=RTMV/NZ	2800
	PROPI(45)=TOPMV/NZ	2810
	PROPI(46)=EVAPMV/NZ	2820
	PROPI(47)=EOB/NZ	2830
	PROPI(48)=EOR/NZ	2840
	PROPI(49)=EOT/NZ	2850
	WRITE (6,530) PROB,T,NC,PROPI(1),PROPI(2),NECYCL,(PROPI(J),J=4:6)	2860
	WRITE (6,540) (PROPI(J),J=7,49)	2870
	GO TO 270	2880
260	WRITE (6,530) PROB,T,NC,ETH,ECK,NECYCL,EZPH1,EZPH2,BBOUND	2890
	WRITE (6,540) ((PR(J),J=1,24),BOTM,RTM,TOPM,EVAPM,EMOB,EMOR,EMOT,E	2900
	EVAPEN,BOTMU,RTMU,TOPMU,EVAPMU,BOTMV,RTMV,TOPMV,EVAPMV,EOB,EOR,EOT)	2910
270	WRITE (6,580) (JPM(I),I=1,I1)	2920
C	*** ENERGY TOTALS STORED FOR LATER USE IN TRACER POINT	2930
C	PLOTS.	2935
	XIENRG=PR(17)	2940
	XKENRG=PR(18)	2950
	XTENRG=PR(19)	2960
C	*** IS THIS A TAPE DUMP OR REZONE CYCLE	2965
	IF (NUMSPT.EQ.NDUMP7.OR.(REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT.	2970
	10)) GO TO 150	2980
C	*** ARE TRACER POINTS BEING GENERATED	2990
280	IF (Y2.GT.(-1.)) GO TO 305	3000
C	*** YES, PRINT TRACER POINT COORDINATES IN CM.	3002
	WRITE (6,590)	3005
	N=0	3010
	DO 300 J=1,JJ	3020
	DO 300 I=1,I1	3030
	IF (XP(I,J).LE.0..AND.YP(I,J).LE.0.) GO TO 300	3040
	IP=INT(XP(I,J))	3050
	JP=INT(YP(I,J))	3060
	KK=JP*IMAX+IP+2	3070

	IF (AMX(KK).GT.0.) GO TO 290	3080
	XP(I,J)=0.	3090
	YP(I,J)=0.	3100
	GO TO 300	3110
290	N=N+1	3120
	CMXP(N)=X(IP)+DX(IP+1)*(XP(I,J)-INT(XP(I,J)))	3130
	CMYP(N)=Y(JP)+DY(JP+1)*(YP(I,J)-INT(YP(I,J)))	3140
C		3150
C	*** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT	3160
C	ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN	3170
C	XP AND YP ARRAYS WHEN THEY ARE WEEDED OUT	3180
C	DURING REZONE.)	3190
C		3200
	IJ(N)=2** (NRZ+1) * (I-1) + 1	3210
	JK(N)=2** (NRZ+1) * (J-1) + 1	3220
	IF (N.LT.5) GO TO 300	3230
	WRITE (6,510) (IJ(M),JK(M),CMXP(M),CMYP(M),M=1,N)	3240
	N=0	3250
300	CONTINUE	3260
	IF (N.EQ.0) GO TO 305	3270
	WRITE (6,510) (IJ(M),JK(M),CMXP(M),CMYP(M),M=1,N)	3280
305	IF (IMAX.EQ.1) GO TO 370	3290
C	*** PRINT SYMBOLIC CONTOUR MAPS OF COMPRESSION, PRESSURE,	3292
C	VELOCITY, AND INTERNAL ENERGY UNLESS DOING A 1-D	3294
C	PROBLEM.	3296
	CALL MAP	3300
C	*** COMPUTE CRATER DEPTH AND VOLUME. AID SUMS DEPTH.	3310
	AID = 0.	3320
	WRITE(6,490)	3322
C	*** START AT AXIS	3325
	DO 330 I =1,I1	3330
	CRAD(I) = .5*DX(I)+X(I-1)	3340
	PL(I) = 0.	3350
	UL(I) = 0.	3360
	DO 320 J =1,I2	3370
	K=(J-1)*IMAX + I + 1	3380
C	*** WS IS COMPRESSION	3385
	WS = AMX(K)/(TAU(I)*DY(J)*RHOZ)	3390
	IF(WS.LT.(.99)) GO TO 310	3400
	GO TO 325	3410
310	AID = AID + 1.-WS	3420
C	*** NOT AT BOTTOM OF CRATER YET	3425
320	CONTINUE	3430
325	IAID = INT(AID)	3440
C	*** UL(I) IS CM. DEPTH OF CRATER IN COLUMN I	3442
C	*** PL(I) IS CELL DEPTH OF CRATER IN COLUMN I	3444
	UL(I) = Y(IAID) + DY(IAID+1)*(AID-FLOAT(IAID)) - Y(JPROJ)	3450
	IF(UL(I).GT.0..OR.UL(I).LT.0.) PL(I) = AID	3460
	AID = 0.	3470
330	CONTINUE	3480
C	*** PRINT CRATER DEPTHS	3485
	DO 340 I=1,I1	3490
	IF(UL(I).LT.0..OR.UL(I).GT.0.) GO TO 335	3500
	GO TO 340	3510
335	WRITE(6,495) I, PL(I), CRAD(I), UL(I)	
340	CONTINUE	3530
C	*** COMPUTE CRATER VOLUME AND VOLUME OF HEMISPHERE WITH	3532

C	RADIUS=UL(1). PRINT VOLUMES WHEN THEY ARE POSITIVE.	3534
	WSB=0.	3540
	DO 345 I=1,I1	3550
	IF(UL(I).LT.0.) GO TO 350	3560
C	*** WSB GIVES CRATER VOLUME	3565
	WSB = UL(I)*TAU(I)+WSB	3570
345	CONTINUE	3580
350	CONTINUE	3590
C	*** PRINT CRATER VOLUME ONLY WHEN GREATER THAN ZERO	3595
	IF(WSB.GT.0.) GO TO 355	3600
	GO TO 360	3610
C	*** WSC GIVES VOLUME OF HEMISPHERE	3615
355	WSC=2.0944*(UL(1))**3	3620
	WRITE(6,500) WSB, WSC	3630
360	CONTINUE	3640
C	*** SHORT PRINT MEAN I3=1 AND PROPERTIES ARE PRINTED ONLY	3645
C	FOR CELLS IN FIRST COLUMN. LONG PRINT MEANS I3=I1 AND	3650
C	PROPERTIES ARE PRINTED FOR ALL CELLS IN ACTIVE GRID.	3660
370	DO 420 I=1,I3	3670
	KSPACE=0	3680
	WFLAGP=1.	3690
	J=I2+1	3700
	K=I2*IMAX+I+1	3705
	DO 410 L=1,I2	3710
	J=J-1	3720
	K=K-IMAX	3730
375	IF (AMX(K)) 450,400,380	3740
380	IF (WFLAGP.EQ.0.) GO TO 390	3750
	WRITE (6,560) I,X(I),DX(I)	3760
	WFLAGP=0.	3770
390	WS=AMX(K)/(TAU(I)*DY(J))	3780
	WSA=WS/RHOZ	3790
	WSC=P(K)	3800
	WRITE (6,520) J,U(K),V(K),WSC,AMX(K),WS,AIX(K),WSA,Y(J)	3810
	KSPACE=0	3820
	GO TO 410	3830
400	KSPACE=KSPACE+1	3840
	IF (KSPACE.GT.1) GO TO 410	3850
	WRITE (6,570)	3860
410	CONTINUE	3870
420	CONTINUE	3880
	IF (NPRINT.EQ.1) GO TO 130	3890
	ASSIGN 130 TO LOCA	3900
	ASSIGN 130 TO LOCB	3910
	IF (PRDELTA.NE.0.) GO TO 50	3920
	GO TO 100	3930
C	*** PRINT DELTA NOT SPECIFIED IN INPUT	3960
430	NK=45	3970
	GO TO 460	3980
C	*** ENERGY CHECK	3990
440	NK=130	4000
	GO TO 460	4010
C	*** NEGATIVE MASS	4020
450	NK=375	4030
460	NR=5	4050
	CALL ERROR	4060
470	WFLAGP=0.	4070

```

WFLAGF=0. 4080
C      *** SHOULD GRID BE REZONED ON THIS CYCLE 4085
      IF ((REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT.0).OR.SS4.NE.0.) GO 4090
1 TO 480 4100
      RETURN 4110
480     CALL REZONE 4120
C      *** MUST CALL CDT TO RECALCULATE PRESSURES 4130
      TNOW=T 4140
      DTNOW=DT 4150
      REZ=0. 4160
      SS4=0. 4170
      CALL CDT 4180
      T=TNOW 4190
      DT=DTNOW 4200
      DTNA=DT 4210
      NUMREZ=NUMREZ-1 4220
C 4230
C      *** NREZ = NUMBER OF REZONES ALLOWED (INPUT VALUE OF NUMREZ) 4240
C      NUMREZ = NUMBER OF REZONES ALLOWED MINUS THE NUMBER 4250
C      OF REZONES PERFORMED SINCE T=0. 4260
C 4270
      NRZ=NREZ-NUMREZ 4280
C      *** NZ USED IN PRINTOUT OF TOTALS FOR 1-D PROBLEMS 4285
      NZ=4.**NRZ 4290
C 4300
      NUMSPT=NDUMP7 4310
      GO TO 120 4320
C 4330
C      FORMATS 4340
C 4350
490     FORMAT (1H0,17X,35HDEPTH OF CRATER MEASURED FROM JPROJ//12X,1H1,5X 4360
1,18HJ OF CRATER BOTTOM,12X,1HR,11X,17HDEPTH IN CM. D(I)//) 4370
495     FORMAT (I13,9X,0PF6.1,13X,1PE10.4,9X,1PE10.4) 4380
500     FORMAT (/6X,13HCRATER VOLUME,11X,43HCRATER VOLUME BASED ON (2/3) 4390
1* PI * D(1)**3/7X,1PE10.4,26X,1PE10.4) 4400
510     FORMAT (5(I4,I4,1P2E9.2)) 4410
520     FORMAT (I4,1X,1P2E14.6,3E15.6,E14.6,E15.6,E14.6) 4420
530     FORMAT(8H1PROBLEM,6X,4HTIME,8X,5HCYCLE,3X,13HTOT.EN.THEOR.3X, 4430
1 19HMAX.REL.ERROR-CYCLE,3X,18HIE SET TO ZERO-PH1,3X, 4435
2 18HIE SET TO ZERO-PH2,3X,12HPLASTIC-WORK/1F8.4,2X,1PE13.7, 4440
3 3X,I4,4X,1PE13.7,3X,1PE13.7,1X,I4,6X,1PE13.7,8X,1PE13.7,6X, 4450
4 1PE13.7/) 4460
540     FORMAT (18X,2HIE,14X,2HKE,7X,13HTOT.EN. (SUM),7X,4HMASS,12X,2HMV,8 4470
1X,12HMV(POSITIVE),8X,2HMU,8X,12HMU(POSITIVE)/11H J.GT.JPROJ,1P8E15 4480
2.7/11H J.LE.JPROJ,1P8E15.7/14X,12H-----,3X,12H-----, 4490
33X,12H-----,3X,12H-----,3X,12H-----,3X,12H--- 4500
4-----,3X,12H-----,3X,12H-----,3X/7H TOTALS,4X,1P 4510
58E15.7//9H BOUNDARY,9X,6HBOTTOM,9X,5HRIGHT,10X,3HTOP,8X,12HSEVAPO 4520
6RATEDS//9H MASS OUT,2X,1P4E15.7/11H ENERGY OUT,1P4E15.7/7H MJ OUT, 4530
74X,1P4E15.7/7H MV OUT,4X,1P4E15.7//11H WORK DONE ,1P3E15.7//) 4540
550     FORMAT (1H0//21H TAPE 7 DUMP ON CYCLEI5//) 4550
560     FORMAT (1H ///4H I =I3,6X,6HR(I) =F12.3,6X,7HDR(I) =E14.7//3H J8X 4560
1,1HU13X,1HV13X,3H P 12X,3HAMX12X,3HRHO11X,3HAIX12X,4HCOMP11X,2H Z/ 4570
2) 4580
570     FORMAT (1H0) 4590
580     FORMAT (/22H J OF PRESSURE-MAXIMUM/(25I5)) 4600
590     FORMAT(/103H TRACER POINTS - INITIAL LOCATION IN CELL COORDINATES 4610

```

1 (I,J) - CURRENT LOCATION IN CM. COORDINATES (X,Y) // 5(4H I,3X,  
21HJ,5X,1HX,8X,1HY,3X))  
END

4612  
4614  
4620-

```

SUBROUTINE MAP
.....
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) ,
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102),
3 GAMC(102),
4 PK(15), Z(150) ,
5 XP(26,51),YP(26,51),
6 PL(204) ,UL(204) ,PR(204) ,
7 RSN(52), RST(52),
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,
5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3)

*** DIMENSIONED ARRAYS
*** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
COMMON PK
COMMON YY, XX
COMMON DDX, DDY
COMMON AMX, AIX, U, V, P
COMMON TAU, JPM
COMMON UL, PL
COMMON AP, YP, CMXP, CMYP

*** NON-DIMENSIONED VARIABLES
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR ,
1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY ,
2E ,ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB ,
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT,
4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID ,
5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF,
6WFLAGL,WFLAGP

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
X(0), Y(0), DX(0), DY(0)

EQUIVALENCE (X(2), X(1)), (YY(2), Y(1))
EQUIVALENCE (DDX(2), DX(1)), (DDY,2), DY(1))

*** SPECIAL EQUIVALENCES FOR PH2 ONLY

EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
1 (PL,GAMC,PR), (PL(103),SIGC)

*** SPECIAL EQUIVALENCES FOR PH3 ONLY

EQUIVALENCE (UL,RSN),
1 (PL,RST), (P,UK),
2 (P(157),VK), (P(313),SNB),
3 (P(365),STB), (P(417),RH0)

*** SPECIAL EQUIVALENCES FOR EDIT

EQUIVALENCE (PR(1), IJ), (PR(6), JK)

*** Z-STORAGE EQUIVALENCES

EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),

```



```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), MAP 590
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), MAP 600
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), MAP 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), MAP 620
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), MAP 630
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), MAP 640
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), MAP 650
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), MAP 660
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) MAP 670
EQUIVALENCE MAP 680
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), MAP 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDELTA),(Z( 46),PRFACT) MAP 700
EQUIVALENCE MAP 710
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IFCYCL),(Z( 50),TSTOP ), MAP 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IARDY), MAP 730
3(Z( 55),VT ),(Z( 56),NG ),(Z( 57),RTM ),(Z( 58),RTMV ), MAP 740
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), MAP 750
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), MAP 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT),(Z( 70),CYCPH3), MAP 770
7(Z( 71),REZFACT),(Z( 72),TARG ),(Z( 73),PROJU ),(Z( 74),BBOUND), MAP 780
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), MAP 790
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) MAP 800
EQUIVALENCE MAP 810
1(Z( 83),VARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), MAP 820
2(Z( 87),ENTER),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), MAP 830
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) MAP 840
EQUIVALENCE MAP 850
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), MAP 860
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAFEN),(Z(102),EVAPMU), MAP 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), MAP 880
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), MAP 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), MAP 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), MAP 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), MAP 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), MAP 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) MAP 940
EQUIVALENCE MAP 950
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), MAP 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), MAP 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), MAP 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMGT ), MAP 990
5(Z(147),JPROJ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) MAP1000
MAP1010
..... MAP1020
MAP1030
END OF COMMON MAP1040
MAP1050
..... MAP1060
MAP1070
DIMENSION VALUE(40) MAP1080
DIMENSION ALE(41) MAP1090
DATA ALE/2H ,2H .,2H -,2H A,2H B,2H C,2H D,2H E,2H F, MAP1100
1 2H G,2H H,2H I,2H J,2H K,2H L,2H M,2H N,2H O, MAP1110
2 2H P,2H Q,2H R,2H S,2H T,2H U,2H V,2H W,2H X, MAP1120
3 2H Y,2H Z,2H +,2H *,2H 1,2H 2,2H 3,2H 4,2H 5, MAP1130
4 2H 6,2H 7,2H 8,2H 9,2H 0/ MAP1140
DIMENSION XUM(41) MAP1150

```

C  
C  
C  
C  
C  
C

```

DATA XUM/2H :2H-.,2H-.,2H-A,2H-B,2H-C,2H-D,2H-E,2H-F,
1      2H-G,2H-H,2H-I,2H-J,2H-K,2H-L,2H-M,2H-N,2H-O,
2      2H-P,2H-Q,2H-R,2H-S,2H-T,2H-U,2H-V,2H-W,2H-X,
3      2H-Y,2H-Z,2H-+,2H-*,2H-1,2H-2,2H-3,2H-4,2H-5,
4      2H-6,2H-7,2H-8,2H-9,2H 0/

```

```

MAP1160
MAP1170
MAP1180
MAP1190
MAP1200
MAP1210
MAP1220
MAP1230
MAP1240
MAP1250
MAP1260
MAP1270
MAP1280
MAP1290
MAP1300
MAP1310
MAP1320
MAP1330
MAP1340
MAP1350
MAP1360
MAP1370
MAP1380
MAP1390
MAP1400
MAP1410
MAP1420
MAP1430
MAP1440
MAP1480
MAP1485
MAP1510
MAP1520
MAP1530
MAP1540
MAP1550
MAP1560
MAP1570
MAP1580
MAP1590
MAP1600
MAP1610
MAP1620
MAP1630
MAP1640
MAP1650
MAP1660
MAP1670
MAP1680
MAP1690
MAP1700
MAP1710
MAP1720
MAP1730
MAP1740
MAP1750

```

```

C
C      *** SEARCH FOR MINIMUM AND MAXIMUM COMPRESSIONS
C      TO SCALE COMPRESSION MAP
C

```

```

      IDL=I1
      JDL=I2
      IF (NC.NE.0) GO TO 10
      IDL=MIN0(IMAX,55)
      JDL=JMAX
10     WSMAX=0.
      WSMIN=10.
C

```

```

      DO 20 J=1,JDL
      K=(J-1)*IMAX+1
      DO 20 I=1,IDL
      K=K+1
      WSA=AMX(K)/(TAU(I)*DY(J)*RHOZ)
      IF (WSA.EQ.0.) GO TO 20
      WSMAX=AMAX1(WSMAX,WSA)
      WSMIN=AMIN1(WSMIN,WSA)
20     CONTINUE
      IF (WSMIN.LT.WSMAX) GO TO 30
      WSMIN=0.
C

```

```

C      *** DEFINE LINEAR SCALE FACTOR AND PRINT KEY TO
C      COMPRESSION MAP.
C

```

```

30     DSCALE=(WSMAX-WSMIN)/FLOAT(IDNMAP)
      IF ((AINT(DSCALE*100.)).LT.(DSCALE*100.)) GO TO 50
      DSCALE=AINT(DSCALE*100.)/100.
      GO TO 60

```

```

50     DSCALE=AINT(DSCALE*100.+1.)/100.

```

```

60     CONTINUE

```

```

      DO 70 I=1,IDNMAP
70     VALUE(I)=WSMIN+FLOAT(I)*DSCALE
      WRITE (6,860)
      ILIM1=1
      ILIM2=20

```

```

80     IF (IDNMAP.LT.ILIM2) ILIM2=IDNMAP
      WRITE (6,870) (ALE(I+1),I=ILIM1,ILIM2)
      WRITE (6,960) (VALUE(I),I=ILIM1,ILIM2)

```

```

      IF (IDNMAP.EQ.ILIM2) GO TO 90
      ILIM1=ILIM2+1
      ILIM2=ILIM2+20
      GO TO 80

```

```

90     CONTINUE

```

```

      WRITE (6,980)
C

```

```

      J=JDL
100    K=(J-1)*IMAX+1
C
      DO 150 I=1,IDL

```

	K=K+1	MAP1760
	IF (AMX(K).GT.0.) GO TO 110	MAP1770
	GO TO 130	MAP1780
110	WSA=AMX(K)/(TAU(I)*DY(J) :10Z)	MAP1790
	IF (WSA.GT.WSMIN) GO TO .20	MAP1800
C	*** PRINT A DOT TO REPRESENT SMALLEST COMPRESSION.	MAP1805
	MA=2	MAP1810
	GO TO 140	MAP1820
120	TMA=(WSA-WSMIN)/DSCALE+1.	MAP1830
	MA=TMA	MAP1840
	IF (WSA.GT.FLOAT(MA-1)*DSCALE+WSMIN) MA=MA+1	MAP1850
	GO TO 140	MAP1860
C	*** PRINT A BLANK FOR EMPTY CELLS.	MAP1865
130	MA=1	MAP1870
140	PR(I)=ALE(MA)	MAP1880
150	CONTINUE	MAP1890
C	*** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5.	MAP1895
	IF (MOD(J,5).NE.0) GO TO 160	MAP1900
	WRITE (6,880) J,(PR(I),I=1,IDL)	MAP1910
	GO TO 170	MAP1920
160	WRITE (6,890) (PR(I),I=1,IDL)	MAP1930
170	J=J-1	MAP1940
	IF (J.GT.0) GO TO 100	MAP1950
C	*** PRINT AND LABEL X-AXIS OF MAP.	MAP1960
	PR(1)=ALE(30)	MAP1970
	WRITE (6,880) J,(PR(1),I=1,IDL)	MAP1980
	WRITE (6,900) (I,I=0,IDL,5'	MAP1990
C		MAP2000
C	*** SEARCH FOR MINIMUM AND MAXIMUM PRESSURES	MAP2010
C	TO SCALE PRESSURE MAP	MAP2020
C		MAP2030
	WSMAX=0.	MAP2040
C		MAP2050
	DO 180 J=1,JDL	MAP2060
	DO 180 I=1,IDL	MAP2070
	K=(J-1)*IMAX+I+1	MAP2080
	WSA=ABS(P(K))	MAP2090
	IF (WSA.EQ.0.) GO TO 180	MAP2100
	WSMAX=AMAX1(WSMAX,WSA)	MAP2110
180	CONTINUE	MAP2120
	WSMIN=10.*PMIN	MAP2130
	WRITE (6,910)	MAP2140
C	*** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO PRESSURES.	MAP2145
	IF (WSMAX.NE.0.) GO TO 190	MAP2150
	J=JDL	MAP2160
	GO TO 260	MAP2170
C		MAP2180
C	*** DEFINE LOGARITHMIC SCALE FACTOR AND PRINT KEY TO	MAP2220
C	PRESSURE MAP.	MAP2230
190	MAXEXP=INT(ALOG10(WSMAX))	MAP2240
	MINEXP=INT(ALOG10(WSMIN))	MAP2250
	PSCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IPRMAP)	MAP2260
	IF ((AINT(PSCLE*1000.)).LT.(PSCLE*1000.)) GO TO 210	MAP2270
	PSCLE=AINT(PSCLE*1000.)/1000.	MAP2280
	GO TO 220	MAP2290
210	PSCLE=AINT(PSCLE*1000.+1.)/1000.	MAP2300
220	CONTINUE	MAP2310

230	DO 230 I=1,IPRMAP	MAP2320
	VALUE(I)=10.**(MINEXP+FLOAT(I)*PSCLE)	MAP2330
	ILIM1=1	MAP2340
	ILIM2=10	MAP2350
240	IF (IPRMAP.LT,ILIM2) ILIM2=IPRMAP	MAP2360
	WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2)	MAP2370
	WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)	MAP2380
	IF (IPRMAP.EQ,ILIM2) GO TO 250	MAP2390
	ILIM1=ILIM2+1	MAP2400
	ILIM2=ILIM2+10	MAP2410
	GO TO 240	MAP2420
250	CONTINUE	MAP2430
	WRITE (6,980)	MAP2440
C		MAP2450
	J=JDL	MAP2460
260	K=(J-1)*IMAX+1	MAP2470
C		MAP2480
	DO 320 I=1,IDL	MAP2490
	K=K+1	MAP2500
	IF (AMX(K).GT.0.) GO TO 270	MAP2510
C	*** PRINT A BLANK FOR EMPTY CELLS.	MAP2515
	MA=1	MAP2520
	GO TO 310	MAP2530
270	IF (P(K).NE.0.) GO TO 280	MAP2540
C	*** PRINT A ZERO FOR NONEMPTY CELLS WITH ZERO PRESSURE.	MAP2545
	MA=41	MAP2550
	GO TO 310	MAP2560
280	FLOTMA=(ALOG10(ABS(P(K)))-FLOAT(MINEXP))/PSCLE+3.	MAP2570
	INTMA=INT(FLOTMA)	MAP2580
	IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 290	MAP2590
	MA=INTMA	MAP2600
	GO TO 300	MAP2610
290	MA=INTMA+1	MAP2620
C	*** DO NOT USE DOT AND DASH IN PRESSURE MAP.	MAP2625
300	IF (MA.LE.3) MA=4	MAP2630
310	CONTINUE	MAP2640
	PR(I)=ALE(MA)	MAP2650
C	*** USE XUM ARRAY OF SYMBOLS FOR NEGATIVE PRESSURES.	MAP2655
320	IF (P(K).LT.0.) PR(I)=XUM(MA)	MAP2660
C		MAP2670
	IF (MOD(J,5).NE.0) GO TO 330	MAP2680
	WRITE (6,880) J,(PR(I),I=1,IDL)	MAP2690
	GO TO 340	MAP2700
330	WRITE (6,890) (PR(I),I=1,IDL)	MAP2710
340	J=J-1	MAP2720
	IF (J.GT.0) GO TO 260	MAP2730
C	*** PRINT AND LABEL X-AXIS OF MAP.	MAP2740
	PR(1)=ALE(30)	MAP2750
	WRITE (6,880) J,(PR(1),I=1,IDL)	MAP2760
	WRITE (6,900) (I,I=0,IDL,5)	MAP2770
C		MAP2780
C	*** SEARCH FOR MINIMUM AND MAXIMUM RADIAL	MAP2790
C	VELOCITIES TO DEFINE SCALE FACTOR OF	MAP2800
C	RADIAL VELOCITY MAP	MAP2810
C		MAP2820
	WSMAX=0.	MAP2830
C		MAP2840

	DO 350 J=1,JDL	MAP2850
	DO 350 I=1,IDL	MAP2860
	K=(J-1)*IMAX+I+1	MAP2870
	WSA=ABS(U(K))	MAP2880
	IF (WSA.EQ.0.) GO TO 350	MAP2890
	WSMAX=AMAX1(WSMAX,WSA)	MAP2900
350	CONTINUE	MAP2910
	WSMIN=10.*UMIN	MAP2920
	WRITE (6,930)	MAP2930
C	*** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.	MAP2935
	IF (WSMAX.NE.0.) GO TO 360	MAP2940
	J=JDL	MAP2950
	GO TO 430	MAP2960
C		MAP2970
C		MAP3020
C	*** USCLE IS LOGARITHMIC SCALE FACTOR OF RADIAL VELOCITY	MAP3030
C	MAP.	MAP3040
360	MAXEXP=INT(ALOG10(WSMAX))	MAP3050
	MINEXP=INT(ALOG10(WSMIN))	MAP3060
	USCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IUMAP)	MAP3070
	IF ((AINT(USCLE*1000.)).LT.(USCLE*1000.)) GO TO 380	MAP3080
	USCLE=AINT(USCLE*1000.)/1000.	MAP3090
	GO TO 390	MAP3100
380	USCLE=AINT(USCLE*1000.+1.)/1000.	MAP3110
390	CONTINUE	MAP3120
C	*** PRINT KEY TO MAP.	MAP3125
	DO 400 I=1,IUMAP	MAP3130
400	VALUE(I)=10.**(MINEXP+FLOAT(I)*USCLE)	MAP3140
	ILIM1=1	MAP3150
	ILIM2=10	MAP3160
410	IF (IUMAP.LT.ILIM2) ILIM2=IUMAP	MAP3170
	WRITE (6,920) (ALE(I,3),I=ILIM1,ILIM2)	MAP3180
	WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)	MAP3190
	IF (IUMAP.EQ.ILIM2) GO TO 420	MAP3200
	ILIM1=ILIM2+1	MAP3210
	ILIM2=ILIM2+10	MAP3220
	GO TO 410	MAP3230
420	CONTINUE	MAP3240
	WRITE (6,980)	MAP3250
C		MAP3260
	J=JDL	MAP3270
430	K=(J-1)*IMAX+1	MAP3280
C		MAP3290
	DO 490 I=1,IDL	MAP3300
	K=K+1	MAP3310
	IF (AMX(K).GT.0.) GO TO 440	MAP3320
C	*** EMPTY CELL.	MAP3325
	MA=1	MAP3330
	GO TO 480	MAP3340
440	IF (U(K).NE.0.) GO TO 450	MAP3350
C	*** ZERO RADIAL VELOCITY.	MAP3355
	MA=41	MAP3360
	GO TO 480	MAP3370
450	FLOTMA=(ALOG10(ABS(U(K)))-FLOAT(MINEXP))/USCLE+3.	MAP3380
	INTMA=INT(FLOTMA)	MAP3390
	IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 460	MAP3400
	MA=INTMA	MAP3410

400	GO TO 470	MAP3420
	MA=INTMA+1	MAP3430
C	*** DO NOT USE DOT OR DASH IN RADIAL VELOCITY MAP.	MAP3435
470	IF (MA.LE.3) MA=4	MAP3440
480	CONTINUE	MAP3450
	PR(I)=ALE(MA)	MAP3460
C	*** USE XUM ARRAY FOR NEGATIVE RADIAL VELOCITIES.	MAP3465
490	IF (U(K).LT.0.) PR(I)=XUM(MA)	MAP3470
C	*** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE	MAP3480
C	OF 5.	MAP3485
	IF (MOD(J,5).NE.0) GO TO 500	MAP3490
	WRITE (6,880) J,(PR(I),I=1,IDL)	MAP3500
	GO TO 510	MAP3510
500	WRITE (6,890) (PR(I),I=1,IDL)	MAP3520
510	J=J-1	MAP3530
	IF (J.GT.0) GO TO 430	MAP3540
C	*** PRINT AND LABEL X-AXIS OF MAP.	MAP3550
	PR(1)=ALE(30)	MAP3560
	WRITE (6,880) J,(PR(1),I=1,IDL)	MAP3570
	WRITE (6,900) (I,I=0,IDL,5)	MAP3580
C		MAP3590
C	*** SEARCH FOR MINIMUM AND MAXIMUM AXIAL	MAP3600
C	VELOCITIES TO DEFINE SCALE FACTOR OF	MAP3610
C	AXIAL VELOCITY MAP	MAP3620
C		MAP3630
	WSMAX=0.	MAP3640
C		MAP3650
	DO 520 J=1,JDL	MAP3660
	DO 520 I=1,IDL	MAP3670
	K=(J-1)*IMAX+I+1	MAP3680
	WSA=ABS(V(K))	MAP3690
	IF (WSA.EQ.0.) GO TO 520	MAP3700
	WSMAX=AMAX1(WSMAX,WSA)	MAP3710
520	CONTINUE	MAP3720
	WSMIN=10.*UMIN	MAP3730
	WRITE (6,940)	MAP3740
C	*** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.	MAP3745
	IF (WSMAX.NE.0.) GO TO 530	MAP3750
	J=JDL	MAP3760
	GO TO 600	MAP3770
C		MAP3780
C		MAP3820
C	*** VSCLE IS LOGARITHMIC SCALE FACTOR FOR AXIAL VELOCITY	MAP3830
C	MAP.	MAP3840
530	MAXEXP=INT(ALOG10(WSMAX))	MAP3850
	MINEXP=INT(ALOG10(WSMIN))	MAP3860
	VSCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IVMAP)	MAP3870
	IF ((AINT(VSCLE*1000.)).LT.(VSCLE*1000.)) GO TO 550	MAP3880
	VSCLE=AINT(VSCLE*1000.)/1000.	MAP3890
	GO TO 560	MAP3900
550	VSCLE=AINT(VSCLE*1000.+1.)/1000.	MAP3910
560	CONTINUE	MAP3920
C	*** PRINT KEY TO AXIAL VELOCITY MAP.	MAP3925
	DO 570 I=1,IVMAP	MAP3930
570	VALUE(I)=10.**(MINEXP+FLOAT(I)*VSCLE)	MAP3940
	ILIM1=1	MAP3950
	ILIM2=10	MAP3960

580	IF (IVMAP.LT.ILIM2) ILIM2=IVMAP	MAP3970
	WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2)	MAP3980
	WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)	MAP3990
	IF (IVMAP.EQ.ILIM2) GO TO 590	MAP4000
	ILIM1=ILIM2+1	MAP4010
	ILIM2=ILIM2+10	MAP4020
	GO TO 580	MAP4030
590	CONTINUE	MAP4040
	WRITE (6,980)	MAP4050
C		MAP4060
	J=JDL	MAP4070
600	K=(J-1)*IMAX+1	MAP4080
C		MAP4090
	DO 660 I=1,IDL	MAP4100
	K=K+1	MAP4110
	IF (AMX(K).GT.0.) GO TO 610	MAP4120
C	*** EMPTY CELL.	MAP4125
	MA=1	MAP4130
	GO TO 650	MAP4140
610	IF (V(K).NE.0.) GO TO 620	MAP4150
C	*** ZERO AXIAL VELOCITY.	MAP4155
	MA=41	MAP4160
	GO TO 650	MAP4170
620	FLOTMA=(ALOG10(ABS(V(K)))-FLOAT(MINEXP))/VSCLE+3.	MAP4180
	INTMA=INT(FLOTMA)	MAP4190
	IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 630	MAP4200
	MA=INTMA	MAP4210
	GO TO 640	MAP4220
630	MA=INTMA+1	MAP4230
C	*** DO NOT USE DOT OR DASH IN AXIAL VELOCITY MAP.	MAP4235
640	IF (MA.LE.3) MA=4	MAP4240
650	CONTINUE	MAP4250
	PR(I)=ALE(MA)	MAP4260
C	*** USE XUM ARRAY FOR NEGATIVE AXIAL VELOCITIES.	MAP4265
660	IF (V(K).LT.0.) PR(I)=XUM(MA)	MAP4270
C	*** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5.	MAP4280
	IF (MOD(J,5).NE.0) GO TO 670	MAP4290
	WRITE (6,880) J,(PR(I),I=1,IDL)	MAP4300
	GO TO 680	MAP4310
670	WRITE (6,890) (PR(I),I=1,IDL)	MAP4320
680	J=J-1	MAP4330
	IF (J.GT.0) GO TO 600	MAP4340
C	*** PRINT AND LABEL X-AXIS OF MAP.	MAP4350
	PR(1)=ALE(30)	MAP4360
	WRITE (6,880) J,(PR(1),I=1,IDL)	MAP4370
	WRITE (6,900) (I,I=0,IDL,5)	MAP4380
C		MAP4390
C		MAP4400
C	*** SEARCH FOR MINIMUM AND MAXIMUM SPECIFIC INTERNAL	MAP4410
C	ENERGIES TO DEFINE SCALE FACTOR OF ENERGY MAP	MAP4420
	WSMAX=0.	MAP4430
C		MAP4440
	DO 690 J=1,JDL	MAP4450
	DO 690 I=1,IDL	MAP4460
	K=(J-1)*IMAX+I+1	MAP4470
	WSA=ABS(AIX(K))	MAP4480
	IF (WSA.EQ.0.) GO TO 690	MAP4490

WSMAX=AMAX1(WSMAX,WSA)	MAP4500
690 CONTINUE	MAP4510
WSMIN=10.*SIEMIN	MAP4520
WRITE (6,950)	MAP4530
C *** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.	MAP4535
IF (WSMAX.NE.0.) GO TO 700	MAP4540
J=JDL	MAP4550
GO TO 770	MAP4560
C	MAP4570
C	MAP4610
C *** ESCLE IS LOGARITHMIC SCALE FACTOR FOR INTERNAL ENERGY	MAP4620
C MAP.	MAP4630
700 MAXEXP=INT(ALOG10(WSMAX))	MAP4640
MINEXP=INT(ALOG10(WSMIN))	MAP4650
ESCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IEMAP)	MAP4660
IF ((AINT(ESCLE*1000.)).LT.(ESCLE*1000.)) GO TO 720	MAP4670
ESCLE=AINT(ESCLE*1000.)/1000.	MAP4680
GO TO 730	MAP4690
720 ESCLE=AINT(ESCLE*1000.+1.)/1000.	MAP4700
C *** PRINT KEY TO INTERNAL ENERGY MAP.	MAP4705
730 CONTINUE	MAP4710
DO 740 I=1,IEMAP	MAP4720
740 VALUE(I)=10.**(MINEXP+FLOAT(I)*ESCLE)	MAP4730
ILIM1=1	MAP4740
ILIM2=10	MAP4750
750 IF (IEMAP.LT.ILIM2) ILIM2=IEMAP	MAP4760
WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2)	MAP4770
WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)	MAP4780
IF (IEMAP.EQ.ILIM2) GO TO 760	MAP4790
ILIM1=ILIM2+1	MAP4800
ILIM2=ILIM2+10	MAP4810
GO TO 750	MAP4820
760 CONTINUE	MAP4830
WRITE (6,980)	MAP4840
C	MAP4850
J=JDL	MAP4860
770 K=(J-1)*IMAX+1	MAP4870
C	MAP4880
DO 830 I=1,IDL	MAP4890
K=K+1	MAP4900
IF (AMX(K).GT.0.) GO TO 780	MAP4910
C *** EMPTY CELL.	MAP4915
MA=1	MAP4920
GO TO 820	MAP4930
780 IF (AIX(K).NE.0.) GO TO 790	MAP4940
C *** ZERO INTERNAL ENERGY.	MAP4945
MA=41	MAP4950
GO TO 820	MAP4960
790 FLOTMA=(ALOG10(ABS(AIX(K)))-FLOAT(MINEXP))/ESCLE+3.	MAP4970
INTMA=INT(FLOTMA)	MAP4980
IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 800	MAP4990
MA=INTMA	MAP5000
GO TO 810	MAP5010
800 MA=INTMA+1	MAP5020
C *** DO NOT USE DOT AND DASH IN INTERNAL ENERGY MAP.	MAP5025
810 IF (MA.LE.3) MA=4	MAP5030
820 CONTINUE	MAP5040



	PR(I)=ALE(MA)	MAP5050
830	IF (AIX(K).LT.0.) PR(I)=XUM(MA)	MAP5060
C	*** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5.	MAP5070
	IF (MOD(J,5).NE.0) GO TO 840	MAP5080
	WRITE (6,880) J,(PR(I),I=1,IDL)	MAP5090
	GO TO 850	MAP5100
840	WRITE (6,890) (PR(I),I=1,IDL)	MAP5110
850	J=J-1	MAP5120
	IF (J.GT.0) GO TO 770	MAP5130
C	*** PRINT AND LABEL X-AXIS OF MAP.	MAP5140
	PR(1)=ALE(30)	MAP5150
	WRITE (6,880) J,(PR(1),I=1,IDL)	MAP5160
	WRITE (6,900) (I,I=0,IDL,5)	MAP5170
C		MAP5180
C		MAP5190
	RETURN	MAP5200
C		MAP5210
C	*** FORMATS	MAP5215
860	FORMAT (1H1,4X,15HCOMPRESSION //)	MAP5220
870	FORMAT (16H SYMBOL ,20(3X,A2))	MAP5230
880	FORMAT (I10,2H I,54A2)	MAP5240
890	FORMAT (10X,2H I,54A2)	MAP5250
900	FORMAT (I12,10I10/////)	MAP5260
910	FORMAT (1H1,4X,15HPRESSURE //)	MAP5270
920	FORMAT (16H SYMBOL ,10(3X,A2,5X))	MAP5280
930	FORMAT (1H1,4X,15HRADIAL VELOCITY//)	MAP5290
940	FORMAT (1H1,4X,15HAXIAL VELOCITY //)	MAP5300
950	FORMAT (1H1,4X,15HINTERNAL ENERGY//)	MAP5310
960	FORMAT (16H MAXIMUM VALUE ,20(F5.2))	MAP5320
970	FORMAT (16H MAXIMUM VALUE ,1P10E10.2)	MAP5330
980	FORMAT (//)	MAP5340
	END	MAP5350-

```

SUBROUTINE PH1
.....
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , PH1 50
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102), PH1 60
3 GAMC(102), PH1 70
4 PK(15), Z(150) , PH1 80
5 XP(26,51),YP(26,51), PH1 90
6 PL(204) ,UL(204) ,PR(204) , PH1 100
7 RSN(52), RST(52), PH1 110
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , PH1 120
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , PH1 130
5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3) PH1 140
*** DIMENSIONED ARRAYS PH1 150
*** Z-BLOCK IS SAVED ON TAPE. PH1 160
COMMON Z PH1 170
COMMON PK PH1 180
COMMON YY, XX PH1 190
COMMON DDX, DDY PH1 200
COMMON AMX, AIX, U, V, P PH1 210
COMMON TAU, JPM PH1 220
COMMON UL, PL PH1 230
COMMON XP, YP, CMXP, CMYP PH1 240
*** NON-DIMENSIONED VARIABLES PH1 250
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR , PH1 260
1AMVT ,DELEB ,GELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY , PH1 270
2E ,ERDUMP,I ,13 ,IWS ,J ,K ,KA ,KB , PH1 280
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT, PH1 290
4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID , PH1 300
5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF, PH1 310
6WFLAGL,WFLAGP PH1 320
*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE PH1 340
X(0), Y(0), DX(0), DY(0) PH1 350
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) PH1 370
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) PH1 380
*** SPECIAL EQUIVALENCES FOR PH2 ONLY PH1 400
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), PH1 420
1 (PL,GAMC,PR), (PL(103),SIGC) PH1 430
*** SPECIAL EQUIVALENCES FOR PH3 ONLY PH1 450
EQUIVALENCE (UL,RSN), PH1 470
1 (PL,RST), (P,UK), PH1 480
2 (P(157),VK), (P(313),SNB), PH1 490
3 (P(365),STB), (P(417),RHO) PH1 500
*** SPECIAL EQUIVALENCES FOR EDIT PH1 520
EQUIVALENCE (PR(1), IJ), (PR(6), JK) PH1 540
*** Z-STORAGE EQUIVALENCES PH1 560
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ), PH1 580

```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), PH1 590  
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), PH1 600  
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), PH1 610  
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), PH1 620  
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMD ),(Z( 22),UVMAX ), PH1 630  
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), PH1 640  
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), PH1 650  
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), PH1 660  
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) PH1 670  
EQUIVALENCE PH1 680  
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), PH1 690  
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDEL), (Z( 46),PRFACT) PH1 700  
EQUIVALENCE PH1 710  
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), PH1 720  
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), PH1 730  
3(Z( 55),VT ),(Z( 56),N6 ),(Z( 57),RTM ),(Z( 58),RTMV ), PH1 740  
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), PH1 750  
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), PH1 760  
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), PH1 770  
7(Z( 71),REZFACT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBOUND), PH1 780  
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), PH1 790  
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) PH1 800  
EQUIVALENCE PH1 810  
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), PH1 820  
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), PH1 830  
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) PH1 840  
EQUIVALENCE PH1 850  
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), PH1 860  
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), PH1 870  
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), PH1 880  
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), PH1 890  
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), PH1 900  
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), PH1 910  
7(Z(119),ESCAPA),(Z(120),EESP ),(Z(121),ESESQ ),(Z(122),ESES ), PH1 920  
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), PH1 930  
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) PH1 940  
EQUIVALENCE PH1 950  
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), PH1 960  
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), PH1 970  
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH1 980  
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), PH1 990  
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) PH11000  
PH11010  
.....PH11020  
PH11030  
END OF COMMON PH11040  
PH11050  
.....PH11060  
\*\*\* PH1 COMPUTES THE EFFECT OF THE PRESSURE GRADIENTS ON PH11062  
UPDATING THE VELOCITIES AND INTERNAL ENERGIES. PH11064  
PH11070  
\*\*\* NRT AND NRC ARE USED TO ADVANCE THE ACTIVE GRID. PH11075  
NRT=0 PH11080  
NRC=0 PH11090  
\*\*\* VEL=1. FLAGS FIRST PASS. ON SECOND PASS, VEL = 0. PH11095  
VEL=1.0 PH11100

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

C	*** RC = DISTANCE FROM AXIS TO CENTER OF CELL K.	PH11102
C	RR = DISTANCE FROM AXIS TO CENTER OF CELL K+1.	PH11104
10	RC=DX(1)/2.0	PH11110
	RR=RC+(DX(1)+DX(2))/2.0	PH11120
	K=2	PH11130
C	*** FOR ALL CELLS IN COLUMN NEXT TO AXIS, SET PRESSURE	PH11132
C	AT LEFT SIDE OF CELL = PRESSURE IN CELL, AND SET	PH11134
C	RADIAL VELOCITY AT LEFT SIDE OF CELL = 0.	PH11136
	DO 20 J=1,JMAX	PH11140
	PL(J)=P(K)	PH11150
	UL(J)=0.0	PH11160
20	K=K+IMAX	PH11170
	DO 140 I=1,I1	PH11180
	K=I+1	PH11190
C	*** DEFINE PRESSURE AND AXIAL VELOCITY AT BOTTOM	PH11192
C	BOUNDARY OF GRID.	PH11194
	VBLO=V(K)	PH11200
	PBLO=P(K)	PH11210
C	*** IF BOTTOM BOUNDARY OF GRID IS REFLECTIVE, SET	PH11212
C	AXIAL VELOCITY AT THAT BOUNDARY = 0.	PH11214
	IF (CVIS.GT.(-.5)) VBLO=0.	PH11220
	TAUDTS=TAU(I)*DT	PH11230
	DO 130 J=1,I2	PH11240
	N=K+IMAX	PH11250
	PIDTS=1.0/(PIDY*DT*DY(J))	PH11260
	IF (AMX(K).LE.0.) GO TO 30	PH11270
	IF (I.LT.IMAX) GO TO 50	PH11280
C	*** FOR ALL CELLS IN LAST COLUMN OF GRID, SET PRESSURE	PH11282
C	AT RIGHT OF CELL = PRESSURE IN CELL. COMPUTE	PH11284
C	ENERGY LOST ACROSS RIGHT BOUNDARY AND SUBTRACT IT	PH11286
C	FROM ETH, THEORETICAL ENERGY TOTAL.	PH11288
	PRR=P(K)	PH11290
	E=PRR*U(K)/PIDTS*X(I)	PH11300
	ETH=ETH-E	PH11310
	EOR=EOR-E	PH11320
	GO TO 40	PH11330
C	*** CELL K IS EMPTY	PH11335
30	PL(J)=0.	PH11340
	UL(J)=U(K+1)*RR	PH11350
	PBLO=0.	PH11360
	VBLO=V(N)	PH11370
	GO TO 130	PH11380
40	URR=RC*U(K)	PH11390
	GO TO 70	PH11400
C	*** IF CELL ON RIGHT IS EMPTY SET SPECIAL P AND U	PH11410
50	IF (AMX(K+1).GT.0.) GO TO 60	PH11420
	PRR=0.	PH11430
	URR=U(K)*RC	PH11440
	GO TO 70	PH11450
60	PRR=(P(K)+P(K+1))/2.	PH11460
	URR=(U(K)*RC+U(K+1)*RR)/2.	PH11470
70	IF (J.LT.JMAX) GO TO 80	PH11480
C	*** FOR ALL CELLS IN TOP ROW OF GRID, SET PRESSURE AND	PH11482
C	AXIAL VELOCITY AT TOP OF CELL = PRESSURE AND AXIAL	PH11484
C	VELOCITY IN CELL. COMPUTE ENERGY LOST ACROSS TOP	PH11486
C	BOUNDARY.	PH11486
	PABOVE=P(K)	PH11490

	E=PABOVE*V(K)/2.*TAUDTS	PH11500
	ETH=ETH-E	PH11510
	EOT=EOT-E	PH11520
	VABOVE=V(K)	PH11530
	GO TO 110	PH11540
C	*** IF CELL ABOVE IS EMPTY SET SPECIAL P AND V	PH11550
80	IF (AMX(N).GT.0.) GO TO 90	PH11560
	PABOVE=0.	PH11570
	VABOVE=V(K)	PH11580
	GO TO 100	PH11590
90	PABOVE=(P(K)+P(N))/2.	PH11600
	VABOVE=(V(K)+V(N))/2.	PH11610
100	IF (J.GT.1) GO TO 110	PH11620
C	*** IF BOTTOM BOUNDARY OF GRID IS REFLECTIVE, ADD TO ETH	PH11622
C	THE ENERGY GENERATED BY PRESSURE AT THAT BOUNDARY.	PH11624
	IF (CVIS.GT.-.5) GO TO 110	PH11630
	E=PBLO*V(K)/2.*TAUDTS	PH11640
	ETH=ETH+E	PH11650
	EOB=EOB+E	PH11660
110	IF (VEL.EQ.0.) GO TO 120	PH11670
C	*** COMPUTE UPDATED VELOCITIES ON FIRST PASS (VEL = 1.)	PH11675
	V(K)=V(K)+(PBLO-PABOVE)*TAUDTS/(AMX(K))	PH11680
	U(K)=U(K)+(PL(J)-PRR)/(AMX(K))*RC/PIDTS*2.0	PH11690
120	CONTINUE	PH11700
C	*** AIX(X) CHANGED ON BASIS OF GRADIENTS COMPUTED IN FIRST	PH11702
C	PASS. ON SECOND PASS AIX(K) CHANGED AGAIN ON BASIS	PH11704
C	OF GRADIENTS CALCULATED FROM THE UPDATED VELOCITIES.	PH11706
	WS=(VBLO-VABOVE)*TAUDTS/2.	PH11710
	WS=(UL(J)-URR)/PIDTS+WS	PH11720
	WSA=AIX(K)+WS*P(K)/AMX(K)	PH11730
	AIX(K)=WSA	PH11740
	VBLO=VABOVE	PH11750
	PL(J)=PRR	PH11760
	UL(J)=URR	PH11770
	PBLO=VABOVE	PH11780
C	*** RC, N, RR REDEFINED FOR NEXT CELL IN ROW J.	PH11785
130	K=N	PH11790
	RC=RR	PH11800
140	RR=(X(I+1)+X(I+2))/2.0	PH11810
	IF (VEL.EQ.0.) GO TO 150	PH11820
	VEL=0.0	PH11830
	GO TO 10	PH11840
150	DO 190 I=1,I1	PH11850
	K=I+1	PH11860
	DO 180 J=1,I2	PH11870
C	*** SN = 0 (INPUT PARAMETER) SETS NEGATIVE INTERNAL	PH11872
C	ENERGIES TO ZERO.	PH11874
	IF (AIX(K).GE.0..OR.SN.GT.0.) GO TO 170	PH11880
	E=AIX(K)*AMX(K)	PH11890
	ETH=ETH-E	PH11900
	EZPH1=EZPH1-E	PH11910
	IF (INTER.EQ.0) GO TO 160	PH11920
C	*** PRINT PROPERTIES OF CELLS WHOSE NEGATIVE ENERGY IS	PH11922
C	SET TO ZERO WHEN DOING INTERMEDIATE PRINTS (INTER.GT.0).	PH11924
	WRITE (6,240) I,J,AMX(K),AIX(K),U(K),V(K)	PH11930
160	AIX(K)=0.0	PH11940
170	IF (I.NE.I1) GO TO 180	PH11950

```

C          *** ENLARGE ACTIVE GRID IN I-DIRECTION IF A CELL IN THE I1 PH11952
C          COLUMN HAS NONZERO VELOCITY OR ENERGY. PH11954
IF (U(K).NE.0..OR.V(K).NE.0..OR.AIX(K).NE.0.) NRC=1 PH11960
180 K=K+IMAX PH11970
LL=K-2*IMAX PH11980
C          *** ENLARGE ACTIVE GRID IN J-DIRECTION IF A CELL IN THE I2 PH11982
C          ROW HAS NONZERO VELOCITY OR ENERGY. PH11984
IF (U(LL).NE.0..OR.V(LL).NE.0..OR.AIX(LL).NE.0.) NRT=1 PH11990
190 CONTINUE PH12000
I1=I1+NRC PH12010
I2=I2+NRT PH12020
C          *** DONT ALLOW ACTIVE GRID TO EXCEED IMAX BY JMAX GRID. PH12025
IF (I1-IMAX) 210,210,200 PH12030
200 I1=IMAX PH12040
210 IF (I2-JMAX) 230,230,220 PH12050
220 I2=JMAX PH12060
230 RETURN PH12070
C PH12080
240 FORMAT (4H PH1,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE15.8, PH12090
14H V=,1PE15.8,18H SIE SET TO ZERO) PH12100
END PH12110-

```

	SUBROUTINE PH3	PH3 10
C	.....	PH3 20
C		PH3 30
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	PH3 40
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,	PH3 50
2	Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),	PH3 60
3	GAMC(102),	PH3 70
4	PK(15), Z(150) ,	PH3 80
5	XP(26,51),YP(26,51),	PH3 90
6	PL(204) ,UL(204) ,PR(204) ,	PH3 100
7	RSN(52), RST(52),	PH3 110
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	PH3 120
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	PH3 130
5	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)	PH3 140
C	*** DIMENSIONED ARRAYS	PH3 150
C	*** Z-BLOCK IS SAVED ON TAPE.	PH3 160
	COMMON Z	PH3 170
	COMMON PK	PH3 180
	COMMON YY, XX	PH3 190
	COMMON DDX, DDY	PH3 200
	COMMON AMX, AIX, U, V, P	PH3 210
	COMMON TAU, JPM	PH3 220
	COMMON UL, PL	PH3 230
	COMMON XP, YP, CMXP, CMYP	PH3 240
C	*** NON-DIMENSIONED VARIABLES	PH3 250
	COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR ,	PH3 260
1	AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY ,	PH3 270
2	ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB ,	PH3 280
3	MD ,ME ,MZT ,NERR ,NK ,NPRINT,	PH3 290
4	NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID ,	PH3 300
5	SSUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF,	PH3 310
	6WFLAGL,WFLAGP	PH3 320
C		PH3 330
C	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	PH3 340
C	X(0), Y(0), DX(0), DY(0)	PH3 350
C		PH3 360
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	PH3 370
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	PH3 380
C		PH3 390
C	*** SPECIAL EQUIVALENCES FOR PH2 ONLY	PH3 400
C		PH3 410
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	PH3 420
1	(PL,GAMC,PR), (PL(103),SIGC)	PH3 430
C		PH3 440
C	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	PH3 450
C		PH3 460
	EQUIVALENCE (UL,RSN),	PH3 470
1	(PL,RST), (P,UK),	PH3 480
2	(P(157),VK), (P(313),SNB),	PH3 490
3	(P(365),STB), (P(417),RHO)	PH3 500
C		PH3 510
C	*** SPECIAL EQUIVALENCES FOR EDIT	PH3 520
C		PH3 530
	EQUIVALENCE (PR(1), IJ), (PR(6), JK)	PH3 540
C		PH3 550
C	*** Z-STORAGE EQUIVALENCES	PH3 560
C		PH3 570
	EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),	PH3 580

```

1(Z( 5),JT      ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), PH3 590
2(Z( 7),ICSTOP),(Z( 8),PIDY  ),(Z( 9),TOPMU ),(Z( 10),RTMU  ), PH3 600
3(Z( 11),STK1  ),(Z( 12),NUMREZ),(Z( 13),ETH   ),(Z( 14),UN14  ), PH3 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17  ),(Z( 18),XMAX  ), PH3 620
5(Z( 19),WZ    ),(Z( 20),NREZ  ),(Z( 21),AMDM  ),(Z( 22),UVMAX  ), PH3 630
6(Z( 23),UN23  ),(Z( 24),UMIN  ),(Z( 25),JSTR  ),(Z( 26),DTNA  ), PH3 640
7(Z( 27),CVIS  ),(Z( 28),STK2  ),(Z( 29),STEZ  ),(Z( 30),NC    ), PH3 650
8(Z( 31),UN31  ),(Z( 32),NRC   ),(Z( 33),IMAX  ),(Z( 34),IMAXA ), PH3 660
9(Z( 35),JMAX  ),(Z( 36),JMAXA ),(Z( 37),KMAX  ),(Z( 38),KMAXA ) PH3 670
EQUIVALENCE PH3 680
1(Z( 39),BOTM  ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), PH3 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDELTA),(Z( 46),PRFACT) PH3 700
EQUIVALENCE PH3 710
1(Z( 47),I1    ),(Z( 48),I2    ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), PH3 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3    ),(Z( 54),IVARDY), PH3 730
3(Z( 55),VT     ),(Z( 56),N6    ),(Z( 57),RTM   ),(Z( 58),RTMV  ), PH3 740
4(Z( 59),UN59  ),(Z( 60),N10   ),(Z( 61),N11   ),(Z( 62),GAMMA ), PH3 750
5(Z( 63),TOPM  ),(Z( 64),BOTMU ),(Z( 65),SN    ),(Z( 66),TOPMV ), PH3 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), PH3 770
7(Z( 71),REZFACT),(Z( 72),TARGI ),(Z( 73),FROJU ),(Z( 74),BBOUND), PH3 780
8(Z( 75),EVAP  ),(Z( 76),ECK   ),(Z( 77),NECYCL),(Z( 78),II    ), PH3 790
9(Z( 79),JJ    ),(Z( 80),NMP   ),(Z( 81),Y2    ),(Z( 82),EZPH1 ) PH3 800
EQUIVALENCE PH3 810
1(Z( 83),IVARUX),(Z( 84),T     ),(Z( 85),NMPMAX),(Z( 86),PMIN  ), PH3 820
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), PH3 830
3(Z( 91),MC     ),(Z( 92),MR    ),(Z( 93),MZ    ),(Z( 94),MB    ) PH3 840
EQUIVALENCE PH3 850
1(Z( 95),REZ   ),(Z( 96),NODUMP),(Z( 97),UN97  ),(Z( 98),UN98  ), PH3 860
2(Z( 99),UN99  ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), PH3 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL   ),(Z(106),STL   ), PH3 880
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), PH3 890
5(Z(111),RHINI ),(Z(112),VINI  ),(Z(113),FINAL ),(Z(114),IVMAP ), PH3 900
6(Z(115),RHOZ  ),(Z(116),ESA   ),(Z(117),ESEZ  ),(Z(118),ESB   ), PH3 910
7(Z(119),ESCAPA),(Z(120),EGESP ),(Z(121),ESESQ ),(Z(122),ESES  ), PH3 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), PH3 930
9(Z(127),SS1   ),(Z(128),SS2   ),(Z(129),UMIN  ),(Z(130),SS4   ) PH3 940
EQUIVALENCE PH3 950
1(Z(131),PRTIME),(Z(132),EOR   ),(Z(133),EOT   ),(Z(134),EOB   ), PH3 960
2(Z(135),EMOR  ),(Z(136),DXF   ),(Z(137),DYF   ),(Z(138),RHOMIN), PH3 970
3(Z(139),STAB ),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH3 980
4(Z(143),STT   ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT  ), PH3 990
5(Z(147),JPROJ),(Z(148),CNAUT ),(Z(149),BBAR  ),(Z(150),EMOB  ) PH31000
C PH31010
C ..... PH31020
C ..... PH31030
C END OF COMMON PH31040
C ..... PH31050
C ..... PH31060
C DX(0)=-DX(1) PH31070
C DY(0)=-DY(1) PH31080
C PH31090
C *** TURN ON R-P TREATMENT WHEN ACTIVE-GRID REACHES JSTR PH31100
C IF (I2.LT.JSTR) GO TO 400 PH31110
C *** TURN OFF JSTR PH31120
C JSTR=0 PH31130
C PW=0. PH31140
C ..... PH31150
C *** USE P-STORAGE FOR U,V,SIE BEING CALC.

```



	DO 10 K=2,KMAX	PH31160
10	P(K)=0.	PH31170
C	*** CALCULATE SUBCYCLE DT	PH31180
	ICP3 = INT(CYCPH3)	PH31190
C	*** CALCULATE FACTOR FOR VARIABLE DT	PH31200
	N=ICP3*(ICP3+1)	PH31210
	DTFACT=2./FLOAT(N)	PH31220
C	*** LOOP THRU SUBCYCLES	PH31230
	DO 380 NN=1,ICP3	PH31240
C	*** DECREASING DT	PH31250
	WS=ICP3-NN+1	PH31260
	DTSTR=WS*DTFACT*DT	PH31270
C		PH31280
C	*** INITIALIZE UK,VK FOR ROW1,2 AND BORDER BELOW	PH31290
C	*** NOTE THAT THESE ARE STORED WITH AN EXTRA CELL TO	PH31300
C	RIGHT AND LEFT OF MESH. SO K = 2 IS AXIS CELL.	PH31310
C		PH31320
	VFACT=-1.	PH31330
C	*** IF REFLECTIVE,PUT NEG. V IN BORDER CELLS	PH31340
	IF (CVIS.LT.0.) VFACT=1.	PH31350
C	*** BUT IF TRANS., USE V	PH31360
	NKB=1	PH31370
	NK=2	PH31380
	NKA=3	PH31390
C	*** SET LIMITS USED IN PH3	PH31400
	M=I1+1	PH31410
	LL=I1-1	PH31420
	DO 20 K=2,M	PH31430
	L=K+IMAX	PH31440
	I=K-1	PH31450
C	*** SET VALUES ADJOINING BOTTOM ROW	PH31460
	RHO(K,NK)=AMX(K)/(TAU(I)*DY(1))	PH31470
	RHO(K,NKB)=RHO(K,NK)	PH31480
	RHO(K,NKA)=AMX(L)/(TAU(I)*DY(2))	PH31490
	UK(K,NK)=U(K)	PH31500
	UK(K,NKB)=U(K)	PH31510
	UK(K,NKA)=U(L)	PH31520
	VK(K,NK)=V(K)	PH31530
	VK(K,NKB)=V(K)*VFACT	PH31540
20	VK(K,NKA)=V(L)	PH31550
C	*** BORDER CELL TO LEFT	PH31560
	DO 30 N=1,3	PH31570
	RHO(1,N)=RHO(2,N)	PH31580
	UK(1,N)=UK(2,N)	PH31590
30	VK(1,N)=VK(2,N)	PH31600
C	*** SNB AND STB HAVE BEEN SET TO 0. BY SETTING ALL	PH31610
C	P STORAGE TO 0.	PH31620
C	*** SET NORMAL STRESSES ON BOTTOM IF REFLECTIVE	PH31630
	IF (CVIS.LT.0.) GO TO 100	PH31640
	IF (IMAX.GT.1) GO TO 40	PH31650
C	***IMAX=1	PH31660
	WSA=1.-AIX(2)/STEZ	PH31670
	IF (WSA.LT.0) WSA=0.	PH31680
	WSB=AMX(2)/(TAU(1)*DY(1)*RHOZ)-1.	PH31690
	STRENG=(CZERO+WSB*(STK1+WSB*STK2))*WSA	PH31700
	IF (STRENG.LT.0.) STRENG=0.	PH31710
	SNB(2)=STRENG*SQRT(2)*ABS(V(2))/V(2)	PH31720

	GO TO 100	PH31730
C		PH31740
C	***PUT IWS = RIGHT BOUNDARY OF JPM ARRAY	PH31750
40	IWS=1	PH31760
	DO 50 I=1,IMAX	PH31770
	IF (JPM(I).EQ.0) GO TO 60	PH31780
	IWS=IWS+1	PH31790
50	CONTINUE	PH31800
C		PH31810
60	DO 90 K=2,IWS	PH31820
	WSA=.5*DX(K)+DX(K-1)+.5*DX(K-2)	PH31830
	DUODX=(U(K+1)-U(K-1))/WSA	PH31840
	DVODX=(V(K+1)-V(K-1))/WSA	PH31850
	DVODY=2*V(K)/DY(1)	PH31860
	UOX=2*U(K)/(X(K-1)+X(K-2))	PH31870
	WSA=DUODX+DVODY+UOX	PH31880
	TH03=WSA/3.	PH31890
	WS=DUODX**2+DVODY**2+UOX**2+.5*(DVODX**2)-TH03*WSA	PH31900
	IF (WS.LE.0.) GO TO 70	PH31910
	WSA=1.-AIX(K)/STEZ	PH31920
	IF (WSA.LT.0.) WSA=0.	PH31930
	WSB=AMX(K)/(TAU(K-1)*DY(1)*RHOZ)-1.	PH31940
	STRENG=(CZERO+WSA*(STK1+WSB*STK2))*WSA	PH31950
	IF (STRENG.LT.0.) STRENG=0.	PH31960
	B=STRENG*SQRT(2./WS)	PH31970
	GO TO 80	PH31980
70	B=0.	PH31990
80	SNB(K)=B*(DVODY-TH03)	PH32000
90	CONTINUE	PH32010
100	L=I2-1	PH32020
C	*** DO ROWS	PH32030
	DO 370 J=1,L	PH32040
	K=(J-1)*IMAX+2	PH32050
C	*** STRESS AT AXIS =0.	PH32060
	SNL=0.	PH32070
	STL=0.	PH32080
C	*** LOOP ON CELLS ACROSS ROW	PH32090
	DO 330 I=1,LL	PH32100
	IK=I+1	PH32110
C	*** IF NOT SOLID, SKIP STRESS CALCULATION	PH32120
	IF (RHO(IK,NK).LT.SOLID) GO TO 170	PH32130
C	*** IF ABOVE JPM(I)+1 WE ARE DONE WITH THIS ROW UNLESS ALSO	PH32140
C	BELOW JPM(I-1)	PH32150
	JFLAG=0	PH32160
	IF (J.LE.JPM(I)+1) GO TO 110	PH32170
	IF (I.EQ.1) GO TO 340	PH32180
	IF (J.GT.JPM(I-1)) GO TO 340	PH32190
	JFLAG=1	PH32200
C	*** CALCULATE STRENGTH	PH32210
110	WSA=1.-AIX(K)/STEZ	PH32220
	IF (WSA.LT.0.) GO TO 170	PH32230
	WSB=RHO(IK,NK)/RHOZ-1.	PH32240
	STRENG=(CZERO+WSA*(STK1+WSB*STK2))*WSA	PH32250
	IF (STRENG.LT.0.) GO TO 170	PH32260
C		PH32270
C	.....	PH32280
C	*** HOOP STRESS***	PH32290

```

C .....PH32300
HOOP=0. PH32310
IF (J.EQ.JPM(I)+1.OR.JFLAG.EQ.1) GO TO 170 PH32320
C *** SKIP HOOP AND RT CALC IF 1-D PH32330
IF (IMAX.EQ.1) GO TO 140 PH32340
C *** DIFFERENCES ARE CENTERED AT CELL-CENTER PH32350
UOX=UK(IK,NK)/(X(I)+X(I-1))*2. PH32360
WS=1./(.5*DX(I+1)+DX(I)+.5*DX(I-1)) PH32370
DUODX=(UK(IK+1,NK)-UK(IK-1,NK))*WS PH32380
DVODX=(VK(IK+1,NK)-VK(IK-1,NK))*WS PH32390
WS=1./(.5*DY(J+1)+DY(J)+.5*DY(J-1)) PH32400
DUODY=(UK(IK,NKA)-UK(IK,NKB))*WS PH32410
DVODY=(VK(IK,NKA)-VK(IK,NKB))*WS PH32420
ASSIGN 120 TO LOCA PH32430
GO TO 240 PH32440
C *** CALCULATED TH03,B PH32450
120 HOOP=B*(UOX-TH03) PH32460
C .....PH32470
C .....*** END OF HOOP CALC. PH32480
C .....PH32490
C *** IF THE CELL ON RIGHT IS NOT SOLID, STRESSES ARE ZERO PH32500
IF (RHO(IK+1,NK).LT.SOLID.OR.IK.EQ.LL) GO TO 140 PH32510
C *** DIFFERENCES ARE CENTERED AT RIGHT EDGE OF CELL PH32520
WS=2./(DX(I)+DX(I+1)) PH32530
DUODX=(UK(IK+1,NK)-UK(IK,NK))*WS PH32540
DVODX=(VK(IK+1,NK)-VK(IK,NK))*WS PH32550
WS=1./(DY(J+1)+2.*DY(J)+DY(J-1)) PH32560
DUODY=(UK(IK,NKA)+UK(IK+1,NKA)-UK(IK,NKB)-UK(IK+1,NKB))*WS PH32570
DVODY=(VK(IK,NKA)+VK(IK+1,NKA)-VK(IK,NKB)-VK(IK+1,NKB))*WS PH32580
UOX=(UK(IK+1,NK)+UK(IK,NK))/X(I)*.5 PH32590
C PH32600
ASSIGN 130 TO LOCA. PH32610
C *** CALC. TH03 AND B PH32620
GO TO 240 PH32630
130 SNR=B*(DUODX-TH03) PH32640
STR=B*(DUODY+DVODX)*.5 PH32650
GO TO 150 PH32660
140 SNR=0. PH32670
STR=0. PH32680
C *** IF THE CELL ABOVE IS NOT SOLID, STRESSES ABOVE ARE PH32690
150 IF (RHO(IK,NKA).LT.SOLID.OR.J.EQ.L) GO TO 180 PH32700
C PH32710
C *** DIFFERENCES ARE CENTERED AT TOP EDGE OF CELL PH32720
WS=2./(DY(J+1)+DY(J)) PH32730
DUODY=(UK(IK,NKA)-UK(IK,NK))*WS PH32740
DVODY=(VK(IK,NKA)-VK(IK,NK))*WS PH32750
WS=1./(DX(I+1)+2.*DX(I)+DX(I-1)) PH32760
DUODX=(UK(IK+1,NK)+UK(IK+1,NKA)-UK(IK-1,NK)-UK(IK-1,NKA))*WS PH32770
DVODX=(VK(IK+1,NK)+VK(IK+1,NKA)-VK(IK-1,NK)-VK(IK-1,NKA))*WS PH32780
UOX=(UK(IK,NKA)+UK(IK,NK))/(X(I)+X(I-1)) PH32790
ASSIGN 160 TO LOCA PH32800
GO TO 240 PH32810
160 SNT=B*(DVODY-TH03) PH32820
STT=B*(DUODY+DVODX)*.5 PH32830
GO TO 190 PH32840
170 SNR=0. PH32850
STR=0. PH32860

```

```

180  SNT=0.
      STT=0.
      IF (AMX(K).GT.U.) GO TO 190
      .O TO 230
190  .F (INTER.NE.99) GO TO 200
      WRITE (6,410) I,J,IK,NKB,NK,NKA,HOOP,SNL,STL,SNR,STR,STRENG,SNB(
1) ,STB(
IK) ,SNT,STT
C      *** ALL STRESSES ON CELL K HAVE BEEN CALCULATED. NOW T
C      *** NEW VALUES OF U,V, AND S.I.E. CAN BE DETERMINED.
200  SNLX=SNL*X(I-1)
      WS=TWOPI*DTSTR/AMX(K)
      IF (IMAX.EQ.1) GO TO 210
      DELU=WS*(DY(J)*(SNR*X(I)-SNLX)+TAU(I)/TWOPI*(STT-STB(
IK) )-HOOP*DX(
1I) *DY(J))
210  STLX=STL*X(I-1)
      DELV=WS*((SNT-SNB(
IK) ) *TAU(I)/TWOPI+DY(J)*(STR*X(I)-STLX))
C
C      *** NOW CALC. CHANGE OF ENERGY
C      *** UKT AND VKT ARE TEMPORARY STORAGE
      UKT=UK(
IK,
NK)
      VKT=VK(
IK,
NK)
      WS=TAU(1)*.5*((UKT+UK(
IK,
NKA) ) *STT+(VKT+VK(
IK,
NKA) ) *SNT)-((UKT+UK(
1(
IK,
NKB) ) *STB(
IK) )+(VKT+VK(
IK,
NKB) ) *SNB(
IK) ))
      WSA=PIDY*DY(J)*(X(I)*((UK(
IK+1,
NK) )+UKT)*SNR+(VK(
IK+1,
NK) )+VKT)*STR)
1-(X(I-1)*((UK(
IK-1,
NK) )+UKT)*SNL+(VK(
IK-1,
NK) )+VKT)*STL))
      WSB=(WSA+WS)/AMX(K)*DTSTR
      WSC=DELU*(UKT+DELU/2.)+DELV*(VKT+DELV/2.)
      DELI=WSB-WSC
      IF (INTER.NE.99) GO TO 220
      WRITE (6,420) I,J,IK,DELU,DELV,DELI
220  U(K)=U(K)+DELU
      V(K)=V(K)+DELV
      AIX(K)=AIX(K)+DELI
      BBOUND=BBOUND+DELI*AMX(K)
C      *** CELL K IS DONE. MOVE TOP TO BOTTOM AND RIGHT TO LEFT
230  SNB(
IK) =SNT
      STB(
IK) =STT
      SNL=SNR
      STL=STR
      GO TO 280
C  -----
C      *** CALCULATE TH03 AND B
C
240  WSA=DUODX+DVODY+UOX
      TH03=WSA/3.
      WS=DUODX**2+DVODY**2+UOX**2+.5*(DUODY+DVODX)**2-TH03*WSA
      IF (WS.LE.0.) GO TO 250
      B=STRENG*SQRT(2./WS)
      GO TO 260
250  B=0.
260  IF (INTER.NE.99) GO TO 270
      WRITE (6,430) DUODX,DVODY,UOX,TH03,DUODY,DVODX,WS,B,LOCA
C
270  GO TO LOCA, (130,160,120)
C
C  -----

```

C	END OF TH03 AND B CALCULATION	PH33430
C	-----	PH33440
C		PH33450
280	IF (INTER.NE.99) GO TO 330	PH33460
	E=0.	PH33470
	DO 290 LJD=2,KMAX	PH33480
	E=E+AMX(LJD)*(.5*(U(LJD)**2+V(LJD)**2)+AIX(LJD))	PH33490
290	CONTINUE	PH33500
	WRITE (6,440) I,J,E	PH33510
	DO 300 LJD=2,IK	PH33520
	UBAR=.5*(UK(LJD,NK)+UK(LJD,NKA))	PH33530
	VBAR=.5*(VK(LJD,NK)+VK(LJD,NKA))	PH33540
300	E=E-TAU(LJD-1)*(UBAR*STB(LJD)+VBAR*SNB(LJD))*DTSTR	PH33550
	IKK=IK+1	PH33560
	DO 310 LJD=IKK,I1	PH33570
	IF (J.GT.JPM(LJD-2)) GO TO 320	PH33580
	UBAR=.5*(UK(LJD,NK)+UK(LJD,NKB))	PH33590
	VBAR=.5*(VK(LJD,NK)+VK(LJD,NKB))	PH33600
310	E=E-TAU(LJD-1)*(UBAR*STB(LJD)+VBAR*SNB(LJD))*DTSTR	PH33610
320	UBAR=.5*(UK(IK+1,NK)+UK(IK,NK))	PH33620
	VBAR=.5*(VK(IK+1,NK)+VK(IK,NK))	PH33630
	E=E-TWOPI*DY(J)*X(I)*(UBAR*SNL+VBAR*STL)*DTSTR	PH33640
	WRITE (6,440) I,J,E	PH33650
	PW=PW+DELI*AMX(K)	PH33660
	WRITE (6,450) PW	PH33670
330	K=K+1	PH33680
C	*** END OF LOOP ON I	PH33690
C	*** MOVE NK-POINTERS AND STORE A NEW ROW OF VELOCITIES	PH33700
340	IF (J.EQ.L) GO TO 370	PH33710
	NKA=NKA+1	PH33720
	NK=NK+1	PH33730
	NKB=NKB+1	PH33740
	IF (NKA.GT.3) NKA=1	PH33750
	IF (NK.GT.3) NK=1	PH33760
	IF (NKB.GT.3) NKB=1	PH33770
	K=(J+1)*IMAX+2	PH33780
	DO 350 I=1,I1	PH33790
	IK=I+1	PH33800
	UK(IK,NKA)=U(K)	PH33810
	VK(IK,NKA)=V(K)	PH33820
	RHO(IK,NKA)=AMX(K)/(TAU(I)*DY(J+1))	PH33830
350	K=K+1	PH33840
C	*** END LOOP	PH33850
	IF (IMAX.NE.1) GO TO 360	PH33860
	UK(3,NKA)=UK(2,NKA)	PH33870
	VK(3,NKA)=VK(2,NKA)	PH33880
	RHO(3,NKA)=RHO(2,NKA)	PH33890
C		PH33900
360	UK(1,NKA)=UK(2,NKA)	PH33910
	VK(1,NKA)=VK(2,NKA)	PH33920
	RHO(1,NKA)=RHO(2,NKA)	PH33930
C	*** END OF J-LOOP	PH33940
370	CONTINUE	PH33950
C	*** END OF RIGID-PLASTIC CALCULATION FOR ONE DTSTR	PH33960
380	CONTINUE	PH33970
	DO 390 K=2,KMAX	PH33980
390	P(K)=0.	PH33990

```

400 RETURN PH34000
C PH34010
410 FORMAT (/6I5,/7H HOOP=,1PE12.6,7H SNL =,1PE12.6,7H STL =,1PE12.6,7H STR =,1PE12.6,7H STRENG=,1PE12.6,7H SNB =,1PE12.6,7H STB =,1PE12.6,7H SNT =,1PE12.6,7H STT =,1PE12.6/) PH34020
420 FORMAT (/3I5,/7H DELU=,1PE12.6,7H DELV=,1PE12.6,7H DELI=,1PE12.6,7H B =,1PE12.6,I7) PH34030
430 FORMAT (7H DUODX=,1PE12.6,7H DVODY=,1PE12.6,7H UOX =,1PE12.6,7H TPX =,1PE12.6,7H DUODY=,1PE12.6,7H DVODX=,1PE12.6,7H WS =,1PE12.6,7H B =,1PE12.6,I7) PH34040
440 FORMAT (4X,2HI=I2,4X,2HJ=I2,4X,2HE=IPE13.7) PH34050
450 FORMAT (4X,3HPW=1PE12.6) PH34060
END PH34070
PH34080
PH34090
PH34100
PH34110
PH34120-

```

```

SUBROUTINE PH2
.....
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , PH2 10
2 Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102), PH2 20
3 GAMC(102), PH2 30
4 PK(15), Z(150) , PH2 40
5 XP(26,51),YP(26,51); PH2 50
6 PL(204) ,UL(204) ,PR(204) , PH2 60
7 RSN(52), RST(52); PH2 70
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , PH2 80
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , PH2 90
5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3) PH2 100
C *** DIMENSIONED ARRAYS PH2 110
C *** Z-BLOCK IS SAVED ON TAPE. PH2 120
COMMON Z PH2 130
COMMON PK PH2 140
COMMON YY, XX PH2 150
COMMON DDX, DDY PH2 160
COMMON AMX, AIX, U, V, P PH2 170
COMMON TAU, JPM PH2 180
COMMON UL, PL PH2 190
COMMON XP, YP, CMXP, CMYP PH2 200
C *** NON-DIMENSIONED VARIABLES PH2 210
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR , PH2 220
1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY , PH2 230
2E ,ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB , PH2 240
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT, PH2 250
4NR ,NRZ ,NULL ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID , PH2 260
5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF, PH2 270
6WFLAGL,WFLAGP PH2 280
C PH2 290
C PH2 300
C PH2 310
C PH2 320
C PH2 330
C PH2 340
C PH2 350
C PH2 360
C PH2 370
C PH2 380
C PH2 390
C PH2 400
C PH2 410
C PH2 420
C PH2 430
C PH2 440
C PH2 450
C PH2 460
C PH2 470
C PH2 480
C PH2 490
C PH2 500
C PH2 510
C PH2 520
C PH2 530
C PH2 540
C PH2 550
C PH2 560
C PH2 570
C PH2 580
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))
*** SPECIAL EQUIVALENCES FOR PH2 ONLY
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
1 (PL,GAMC,PR), (PL(103),SIGC)
*** SPECIAL EQUIVALENCES FOR PH3 ONLY
EQUIVALENCE (UL,RSN),
1 (PL,RST), (P,UK),
2 (P(157),VK), (P(313),SNB),
3 (P(365),STB), (P(417),RH0)
*** SPECIAL EQUIVALENCES FOR EDIT
EQUIVALENCE (PR(1), IJ), (PR(6), JK)
*** Z-STORAGE EQUIVALENCES
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),

```

```

1(Z( 3),DT      ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), PH2 590
2(Z( 7),ICSTOP),(Z( 8),PIDY  ),(Z( 9),TOPMU ),(Z(10),RTMU  ), PH2 600
3(Z(11),STK1  ),(Z(12),NUMREZ),(Z(13),ETH   ),(Z(14),UN14  ), PH2 610
4(Z(15),RHINIT),(Z(16),PROJI  ),(Z(17),UN17  ),(Z(18),XMAX  ), PH2 620
5(Z(19),NZ    ),(Z(20),NREZ  ),(Z(21),AMDM  ),(Z(22),UVMAX  ), PH2 630
6(Z(23),UN23  ),(Z(24),DMIN  ),(Z(25),JSTR  ),(Z(26),DTNA  ), PH2 640
7(Z(27),CVIS  ),(Z(28),STK2  ),(Z(29),STEZ  ),(Z(30),NC    ), PH2 650
8(Z(31),UN31  ),(Z(32),NRC   ),(Z(33),IMAX  ),(Z(34),IMAXA ), PH2 660
9(Z(35),JMAX  ),(Z(36),JMAXA ),(Z(37),KMAX  ),(Z(38),KMAXA ) PH2 670
EQUIVALENCE PH2 680
1(Z(39),BOTM  ),(Z(40),BOTMV ),(Z(41),NUMSPT),(Z(42),CZERO ), PH2 690
2(Z(43),NUMSCA),(Z(44),PRLIM ),(Z(45),PRDELT),(Z(46),PRFACT) PH2 700
EQUIVALENCE PH2 710
1(Z(47),I1    ),(Z(48),I2    ),(Z(49),IPCYCL),(Z(50),TSTOP ), PH2 720
2(Z(51),RHOF1L),(Z(52),TARGV ),(Z(53),N3     ),(Z(54),IVARDY), PH2 730
3(Z(55),VT     ),(Z(56),N6    ),(Z(57),RTM    ),(Z(58),RTMV  ), PH2 740
4(Z(59),UN59  ),(Z(60),N10   ),(Z(61),N11   ),(Z(62),GAMMA ), PH2 750
5(Z(63),TOPM  ),(Z(64),BOTMU ),(Z(65),SN     ),(Z(66),TOPMV ), PH2 760
6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT ),(Z(70),CYCPH3), PH2 770
7(Z(71),REZFCT),(Z(72),TARGI ),(Z(73),PROJU  ),(Z(74),BBOUND), PH2 780
8(Z(75),EVAP  ),(Z(76),ECK   ),(Z(77),NECYCL),(Z(78),II    ), PH2 790
9(Z(79),JJ    ),(Z(80),NMP   ),(Z(81),Y2     ),(Z(82),EZPH1 ) PH2 800
EQUIVALENCE PH2 810
1(Z(83),IVARDX),(Z(84),T     ),(Z(85),NMPMAX),(Z(86),PMIN  ), PH2 820
2(Z(87),INTER ),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),ICMAP ), PH2 830
3(Z(91),MC     ),(Z(92),MR    ),(Z(93),MZ     ),(Z(94),MB     ) PH2 840
EQUIVALENCE PH2 850
1(Z(95),REZ   ),(Z(96),NODUMP),(Z(97),UN97  ),(Z(98),UN98  ), PH2 860
2(Z(99),UN99  ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), PH2 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL  ),(Z(106),STL  ), PH2 880
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), PH2 890
5(Z(111),RHINI ),(Z(112),VINI  ),(Z(113),FINAL ),(Z(114),IVMAP ), PH2 900
6(Z(115),RHOZ  ),(Z(116),ESA   ),(Z(117),ESEZ  ),(Z(118),ESB  ), PH2 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), PH2 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), PH2 930
9(Z(127),SS1  ),(Z(128),SS2  ),(Z(129),UMIN  ),(Z(130),SS4  ) PH2 940
EQUIVALENCE PH2 950
1(Z(131),PRTIME),(Z(132),EOR   ),(Z(133),EOT   ),(Z(134),EOB   ), PH2 960
2(Z(135),EMOR  ),(Z(136),DXF   ),(Z(137),DYF   ),(Z(138),RHOMIN), PH2 970
3(Z(139),STAB ),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH2 980
4(Z(143),STT  ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT  ), PH2 990
5(Z(147),JPROJ),(Z(148),CNAUT ),(Z(149),BBAR  ),(Z(150),EMOB  ) PH21000
C PH21010
C *** SPECIAL EQUIVALENCE FOR PH2 PH21012
EQUIVALENCE (WSOUT,UOTK) PH21014
C .....PH21020
C .....PH21030
C END OF COMMON PH21040
C .....PH21050
C .....PH21060
C .....PH21070
C SUME=0. PH21090
C *** ARE TRACER POINTS BEING GENERATED PH21095
IF (Y2.GT.(-1.)) GO TO 260 PH21100
C *** YES. CALCULATE NEW POSITIONS OF POINTS IN ACTIVE GRID. PH21105
DO 250 J=1,JJ PH21110

```



	DO 250 I=1,II	PH21120
	IF (XP(1,J).LE.0.) GO TO 250	PH21130
	IX=XP(1,J)	PH21140
	IY=YP(1,J)	PH21150
	IF (IX.GT.I1) GO TO 250	PH21160
	IF (IY.GT.I2) GO TO 250	PH21170
	K=IY*IMAX+IX+2	PH21180
C	*** SKIP CALCULATION IF POINT IS IN EMPTY CELL	PH21190
C	(AHEAD OF THE MASS IT REPRESENTS).	PH21195
	IF (AMX(K).EQ.0.) GO TO 250	PH21200
C	*** FRX AND FRY GIVE LOCATION OF TRACER POINT IN	PH21202
C	CELL(IX+1,IY+1).	PH21204
	FRX=XP(1,J)-AINT(XP(1,J))	PH21210
	FRY=YP(1,J)-AINT(YP(1,J))	PH21220
C		PH21230
C	*** IWS=1 FLAGS TRACER POINTS IN CELLS ON RIGHT OR	PH21230
C	LEFT BOUNDARY OF GRID.	PH21232
C	IWS=2 FLAGS TRACER POINTS IN CELLS ON TOP OR	PH21234
C	BOTTOM BOUNDARY OF GRID.	PH21236
C	IWS=0 FLAGS TRACER POINTS IN CELLS WHICH ARE NOT	PH21240
C	ON A GRID BOUNDARY.	PH21245
	IWS=0	PH21250
C	*** SEE IF TRACER POINT IS IN A BOUNDARY CELL.	PH21255
	IF (IX.LT.1) GO TO 130	PH21260
	IF (IX.GT.IMAX-2) GO TO 110	PH21270
	IF (IY.LT.1) GO TO 160	PH21280
	IF (IY.GT.JMAX-2) GO TO 140	PH21290
C	*** NOT IN BOUNDARY CELL. IS POINT ON LEFT SIDE OF CELL	PH21295
10	IF (FRX.LT..5) GO TO 40	PH21300
C	*** POINT IS ON RIGHT SIDE OF CELL. IS CELL ON RIGHT EMPTY	PH21305
20	IF (AMX(K+1).EQ.0.) GO TO 30	PH21310
C	*** RADIAL COMPONENT BASED ON AVERAGE OF RADIAL VELOCITIES	PH21312
	OF CELL K AND CELL ON RIGHT OR LEFT.	PH21314
	UEFF=(FRX-.5)*U(K+1)+(1.5-FRX)*U(K)	PH21320
	GO TO 50	PH21330
C	*** CELL ON RIGHT OR LEFT EMPTY-USE RADIAL COMPONENT	PH21342
C	OF CELL K.	PH21344
30	UEFF=U(K)	PH21340
	GO TO 50	PH21350
C	*** POINT IS ON LEFT SIDE OF CELL. IS CELL ON LEFT EMPTY	PH21355
40	IF (AMX(K-1).EQ.0.) GO TO 30	PH21360
C	*** RADIAL COMPONENT BASED ON AVERAGE OF TWO CELLS.	PH21365
	UEFF=(.5-FRX)*U(K-1)+(.5+FRX)*U(K)	PH21370
C	*** WHEN IWS = 2 AXIAL COMPONENT OF CELL HAS ALREADY BEEN	PH21372
C	CALCULATED.	PH21374
50	IF (IWS.GT.1) GO TO 100	PH21380
C	*** IS POINT IN BOTTOM HALF OF CELL	PH21385
60	IF (FRY.LT..5) GO TO 90	PH21390
C	*** POINT IS IN TOP HALF. IS CELL ABOVE EMPTY	PH21395
70	KA=K+IMAX	PH21400
	IF (AMX(KA).EQ.0.) GO TO 80	PH21410
C	*** AXIAL COMPONENT BASED ON AVERAGE OF AXIAL VELOCITIES	PH21412
C	OF CELL K AND CELL ABOVE OR BELOW.	PH21414
	VEFF=(FRY-.5)*V(KA)+(1.5-FRY)*V(K)	PH21420
	GO TO 100	PH21430
C	*** CELL ABOVE OR BELOW IS EMPTY. USE AXIAL COMPONENT OF	PH21432
C	CELL K.	PH21434

00	VEFF=V(K)	PH21440
	GO TO 100	PH21450
00	KA=K-IMAX	PH21460
	IF (AMX(KA).EQ.0.) GO TO 80	PH21470
	VEFF=(.5-FRY)*V(KA)+(.5+FRY)*V(K)	PH21480
C	*** IX+1 IS I-INDEX AND IY+1 IS J-INDEX OF CELL TRACER	PH21482
C	POINT IS IN. COMPUTE NEW LOCATION OF TRACER POINT.	PH21484
100	DTODX=DT/DX(IX+1)	PH21490
	XP(I,J)=XP(I,J)+UEFF*DTODX	PH21500
	DTODY=DT/DY(IY+1)	PH21510
	YP(I,J)=YP(I,J)+VEFF*DTODY	PH21520
C	***IWS.LT.1 MEANS TRACER POINT WAS NOT IN BOUNDARY CELL	PH21522
C	BEFORE BEING MOVED, AND ITS NEW POSITION NEED NOT	PH21524
C	BE CHECKED - GO TO END OF LOOP.	PH21526
	IF (IWS.LT.1) GO TO 250	PH21530
	GO TO 200	PH21540
C	*** POINT IN CELL ON RIGHT BOUNDARY.	PH21542
110	IF (FRX.LT..5) GO TO 40	PH21550
	IWS=1	PH21560
	UEFF=U(K)	PH21570
C	*** IS POINT IN CELL ON BOTTOM BOUNDARY	PH21575
120	IF (IY.LT.1) GO TO 170	PH21580
C	*** IS POINT IN CELL ON TOP BOUNDARY	PH21585
	IF (IY.GT.JMAX-2) GO TO 190	PH21590
	GO TO 60	PH21600
C	*** POINT IN CELL ON AXIS.	PH21605
130	IF (FRX.GT..5) GO TO 20	PH21610
	IWS=1	PH21620
	UEFF=2.*FRX*U(K)	PH21630
	GO TO 120	PH21640
C	*** POINT IN CELL ON TOP BOUNDARY.	PH21645
140	IF (FRY.LT..5) GO TO 10	PH21650
	IWS=2	PH21660
150	VEFF=V(K)	PH21670
	GO TO 10	PH21680
C	*** POINT IN CELL ON BOTTOM BOUNDARY. RADIAL COMPONENT	PH21682
C	HAS NOT BEEN COMPUTED.	PH21684
160	IF (FRY.GT..5) GO TO 10	PH21690
	IWS=2	PH21700
	IF (CVIS.LT.0.) GO TO 150	PH21710
	VEFF=2.*FRY*V(K)	PH21720
	GO TO 10	PH21730
C	*** POINT IN CELL ON BOTTOM BOUNDARY. AXIAL COMPONENT	PH21732
C	HAS BEEN COMPUTED.	PH21734
170	IF (FRY.GT..5) GO TO 70	PH21740
C	*** COMPUTE AXIAL COMPONENT ON BASIS OF BOTTOM BOUNDARY	PH21742
C	CONDITION.	PH21744
	IF (CVIS.LT.0.) GO TO 180	PH21750
C	*** REFLECTIVE.	PH21755
	VEFF=2.*FRY*V(K)	PH21760
	GO TO 100	PH21770
C	*** TRANSMITTIVE.	PH21775
180	VEFF=V(K)	PH21780
	GO TO 100	PH21790
C	*** POINT IN CELL ON TOP BOUNDARY.	PH21795
190	IF (FRY.LT..5) GO TO 90	PH21800
	GO TO 180	PH21810

```

C      *** SPECIAL TESTS FOR TRACER POINTS WHICH WERE IN PH21812
C      BOUNDARY CELLS BEFORE BEING MOVED. PH21814
C      *** IF POINT MOVED BELOW GRID, TEST ON BOTTOM BOUNDARY PH21816
C      CONDITION, IF REFLECTIVE MOVE POINT BACK INTO GRID, PH21818
C      IF TRANSMITTIVE SET X-COORDINATE TO -1. PH21819
200  IF (YP(I,J).LT.0.) GO TO 220 PH21820
C      *** IF POINT CROSSED TOP BOUNDARY SET ITS X-COORDINATE PH21822
C      TO -1. PH21824
C      IF (INT(YP(I,J)).LT.JMAX) GO TO 230 PH21830
210  XP(I,J)=-1. PH21840
C      GO TO 250 PH21850
220  IF (CVIS.LT.0.) GO TO 210 PH21860
C      *** REFLECTIVE. PH21865
C      YP(I,J)=-YP(I,J) PH21870
C      *** ADJUST X-COORDINATE IF ITS CALCULATED POSITION IS PH21872
C      NEGATIVE. PH21874
230  IF (XP(I,J).LT.0.) GO TO 240 PH21880
C      *** IF POINT CROSSED RIGHT BOUNDARY SET ITS X-COORDINATE PH21882
C      TO -1. PH21884
C      IF (INT(XP(I,J)).LT.IMAX) GO TO 250 PH21890
C      GO TO 210 PH21900
240  XP(I,J)=-XP(I,J) PH21910
C      *** END OF LOOP FOR TRACER POINT MOVEMENT. PH21915
250  CONTINUE PH21920
C
C      *** SET TO ZERO ACTIVE GRID AND REZONE FLAGS. PH21925
260  NRT=0 PH21930
C      NRC=0 PH21940
C      REZ=0.0 PH21950
C      PIDTS=1.0/(PIDY*DT) PH21960
C      TWOPDT=2./PIDTS PH21970
C      K=2 PH21980
C      *** CALCULATE FLUXES ON LEFT SIDE OF CELLS IN AXIS COLUMN. PH21985
C      DO 310 J=1,JMAX PH21990
C      IF (AMX(K).LE.0.) GO TO 270 PH22000
C      IF (U(K).LT.0.) GO TO 280 PH22010
270  FLEFT(J)=0. PH22020
C      GO TO 300 PH22030
280  GAMC(J)=AMX(K)*U(K)*DT/DX(1) PH22040
C      IF ((GAMC(J)+AMX(K)).GE.0.) GO TO 290 PH22050
C      GAMC(J)=-AMX(K) PH22060
290  FLEFT(J)=2.*GAMC(J)*U(K)/SS2 PH22070
300  GAMC(J)=0. PH22080
C      YAMC(J)=0. PH22090
C      SIGC(J)=J. PH22100
310  K=K+IMAX PH22110
C      *** DO LOOP IN I-DIRECTION - MOVE UP COLUMNS - SPECIAL PH22112
C      TREATMENT FOR FLUXES AT BOTTOM BOUNDARY OCCURS BEFORE PH22114
C      J-LOOP BEGINS. PH22116
C      GO 1150 I=1, I1 PH22120
C      J=1 PH22130
C      K=I+1 PH22140
315  IF (AMX(K)) 1220, 330, 320 PH22150
320  IF (-V(K).GT.UMIN) GO TO 340 PH22160
330  AMMV=0.0 PH22170
C      GO TO 390 PH22180
340  AMMY=AMX(K)*V(K)*DT/DY(J) PH22190

```

	IF (AMMY+AMX(K)) 350,360,360	PH22200
350	AMMY=-AMX(K)	PH22210
360	IF (CVIS) 370,380,380	PH22220
C	*** BOTTOM BOUNDARY IS TRANSMITTIVE, MATERIAL IS MOVING	PH22230
C	OUT, REMOVE ITS ENERGY FROM ETH.	PH22240
370	AMMU=AMMY*U(K)	PH22250
	AMMV=AMMY*V(K)	PH22260
	DELEB=AIX(K)+(U(K)**2+V(K)**2)/2.0	PH22270
	DELEB=AMMY*DELEB	PH22280
	EMOB=EMOB-DELEB	PH22290
	ETH=ETH+DELEB	PH22300
	BOTM=BOTM-AMMY	PH22310
	BOTMV=BOTMV-AMMV	PH22320
	BOTMU=BOTMU-AMMU	PH22330
	GO TO 400	PH22340
C	*** BOTTOM BOUNDARY IS REFLECTIVE, NET MOMENTUM CHANGE	PH22350
C	IN Z DIRECTION IS 2*MV/SS2.	PH22360
380	IF (V(K).GE.0.) GO TO 330	PH22370
	AMMV=2.*AMMY*V(K)/SS2	PH22380
390	AMMY=0.0	PH22390
	AMMU=0.	PH22400
	DELEB=0.0	PH22410
C	*** BEGIN DO LOOP IN J(Z) DIRECTION.	PH22420
400	DO 1140 J=1,I2	PH22430
	MSLAVE=0	PH22440
	NSLAVE=0	PH22450
	IF (J.EQ.JMAX) GO TO 420	PH22460
C	NOT AT TOP OF MESH	PH22470
C	L IS INDEX OF CELL ABOVE K	PH22480
	L=K+IMAX	PH22490
C	IS CELL K EMPTY	PH22500
	IF (AMX(K).GT.0.) GO TO 540	PH22510
C	IF CELL ABOVE IS ALSO EMPTY THEN FLUX=0 OR	PH22520
C	IF FLUX WOULD BE OUT OF EMPTY CELL, THEN FLUX=0.	PH22530
	IF (AMX(L).EQ.0..OR.V(L).GE.0.) GO TO 430	PH22540
C	CELL ABOVE NOT EMPTY. MASS MOVING IN DIRECTION OF	PH22550
C	CELL K WHICH IS EMPTY.	PH22560
C	IS CELL ABOVE COLD AND SOLID	PH22570
	IF (AIX(L).GT.ESESQ.OR.AMX(L)/(TAU(I)*DY(J+1)).GE.RHOZ) GO TO 410	PH22580
C	COLD, BUT NOT UP TO NORMAL DENSITY	PH22590
C	IS NEXT CELL ABOVE C OLD	PH22600
	IF ((J+1).EQ.JMAX) GO TO 410	PH22610
	LA=L+IMAX	PH22620
	IF (AIX(LA).LT.ESESQ.AND.AMX(LA)/(TAU(I)*DY(J+1)).GT.SOLID) GO TO	PH22630
	1430	PH22640
C	CELL ABOVE IS HOT. DO NOT HOLD BACK.	PH22650
410	M=L	PH22660
	V ABOVE=V(L)	PH22670
	WLF=DY(J+1)	PH22680
	GO TO 460	PH22690
C	TOP OF MESH. IS MASS MOVING OUT.	PH22700
420	IF (V(K).GT.0.) GO TO 440	PH22710
C	SET FLUX TERMS TO ZERO.	PH22720
430	AMPY=0.	PH22730
	GO TO 590	PH22740
C	MASS MOVING OUT OF TOP BOUNDARY	PH22750
440	V ABOVE=V(K)	PH22760

	WDYF=DY(J)	PH22770
450	M=K	PH22780
C	CALCULATE MASS FLUX AT TOP OF CELL	PH22790
460	IF (ABS(VABOVE).LE.UMIN) GO TO 430	PH22800
	UVMAX=TRNSFC*DY(J)/DT	PH22810
	IF (ABS(VABOVE).LT.UVMAX) GO TO 480	PH22820
	IF (VABOVE.GT.0.) GO TO 470	PH22830
	VABOVE=-UVMAX	PH22840
	GO TO 480	PH22850
470	VABOVE=UVMAX	PH22860
480	AMPY=AMX(M)*VABOVE*DT/WDYF	PH22870
	IF (MSLAVE.NE.0) GO TO 500	PH22880
490	EAMPY=.5*(U(M)**2+V(M)**2)+AIX(M)	PH22890
	UAMPY=U(M)	PH22900
	VAMPY=V(M)	PH22910
	GO TO 590	PH22920
500	IF (VABOVE.GT.0.) GO TO 510	PH22930
	M=L	PH22940
	GO TO 490	PH22950
510	M=K	PH22960
	GO TO 490	PH22970
520	WSA=.5*(V(K)+V(L))	PH22980
	WSB=1.0+(V(L)-V(K))*DT/((DY(J+1)+DY(J))/2.0)	PH22990
	WDYF=(DY(J)+DY(J+1))/2.	PH23000
	VABOVE=WSA/WSB	PH23010
	IF (MSLAVE.NE.0) GO TO 460	PH23020
	IF (VABOVE) 530,430,450	PH23030
530	M=L	PH23040
	GO TO 460	PH23050
C	CELL K IS NOT EMPTY. HOW ABOUT CELL ABOVE K.	PH23060
540	IF (AMX(L).GT.0.) GO TO 550	PH23070
C	CELL ABOVE IS EMPTY. IS FLUX INTO IT.	PH23080
	IF (V(K).LE.0.) GO TO 430	PH23090
C	FLUX TOWARD EMPTY CELL	PH23100
	IF (J.EQ.1) GO TO 440	PH23110
C	SHOULD MASS BE HELD UP UNTIL CELL IS FULL	PH23120
	LB=K-IMAX	PH23130
	IF (AIX(LB).GT.ESESQ.OR.AIX(K).GT.ESESQ.OR.AMX(LB)/(TAU(I)*DY(J-1)	PH23140
	1).LT.SOLID.OR.AMX(K)/(TAU(I)*DY(J)).GT.SOLID) GO TO 440	PH23150
	GO TO 430	PH23160
550	IF (V(K).GT.0..AND.V(L).LT.0.) GO TO 560	PH23170
	IF ((J+1).EQ.JMAX) GO TO 580	PH23180
	LA=L+IMAX	PH23190
	IF (AMX(LA).GT.0..OR.V(K).GE.0..OR.V(L).GE.0.) GO TO 570	PH23200
C	K AND L NOT EMPTY BUT CELL ABOVE L IS EMPTY	PH23210
C	TEST FOR SLAVING L TO K	PH23220
	IF (AMX(L)/(TAU(I)*DY(J+1)).GE.RHOZ.OR.AIX(K).GT.ESESQ.OR.AIX(L).GPH23230	PH23240
	1T.ESESQ) GO TO 520	PH23250
C	YES: SLAVE L TO K	PH23260
	MSLAVE=L	PH23270
	M=K	PH23280
	GO TO 520	PH23290
C	*** \$REFLECTIVE\$ TREATMENT	PH23300
560	VMK=V(K)*AMX(K)	PH23310
	VML=V(L)*AMX(L)	PH23320
	WSA=VMK+VML	PH23330
	AMPY=WSA*DT/((DY(J)+DY(J+1))/2.0)	PH23330

	VAMPY=(VMK*V(K)+VML*V(L))/WSA	PH23340
	UAMPY=(VMK*U(K)+VML*U(L))/WSA	PH23350
	SAVEK=AIX(K)+.5*(U(K)**2+V(K)**2)	PH23360
	EAMPY=(VMK*SAVEK+VML*(AIX(L)+.5*(U(L)**2+V(L)**2)))/WSA	PH23370
	GO TO 590	PH23380
570	IF (J.EQ.1) GO TO 520	PH23390
580	LB=K-IMAX	PH23400
	IF (AMX(LB).NE.0..OR.V(L).LE.0..OR.V(K).LE.0.) GO TO 520	PH23410
C	SHOULD K BE SLAVED TO L	PH23420
	IF (AMX(K)/(TAU(I)*DY(J)).GE.RHOZ.OR.AIX(L).GE.ESESQ.OR.AIX(K).GT.	PH23430
	1ESESQ) GO TO 520	PH23440
C	YES. SLAVE K TO L.	PH23450
	MSLAVE=K	PH23460
	MEL	PH23470
	GO TO 520	PH23480
C	*** CHECK FOR ONE-D	PH23490
590	IF (ABS(AMPY).LT.ROEPS*AMX(K).AND.ABS(AMPY).LT.ROEPS*AMX(K+IMAX))	PH23500
	1AMPY=0.	PH23510
	IF (IMAX.EQ.1) GO TO 620	PH23520
	IF (I.EQ.IMAX) GO TO 610	PH23530
C	NOT AT RIGHT BOUNDARY	PH23540
C	IS CELL K.EMPTY	PH23550
	IF (AMX(K).GT.0.) GO TO 730	PH23560
C	SET FLUX=0 IF CELL ON RIGHT IS EMPTY	PH23570
C	OR IF VELOCITY IS AWAY FROM EMPTY CELL K	PH23580
	IF (AMX(K+1).EQ.0..OR.U(K+1).GE.0.) GO TO 620	PH23590
C	CELL TO RIGHT IS NOT EMPTY. SHALL WE LET MASS MOVE	PH23600
C	INTO CELL K WHICH IS EMPTY.	PH23610
	IF (AIX(K+1).GT.ESESQ.OR.AMX(K+1)/(TAU(I+1)*DY(J)).GT.RHOZ) GO TO	PH23620
	1600	PH23630
C	COLD AND NOT UP TO NORMAL DENSITY	PH23640
C	IS NEXT CELL TO RIGHT COLD	PH23650
	IF ((I+1).EQ.IMAX) GO TO 600	PH23660
	IF (AIX(K+2).LT.ESESQ.AND.AMX(K+2)/(TAU(I+2)*DY(J)).GT.SOLID) GO T	PH23670
	10 620	PH23680
C	***CELL ON RIGHT IS HOT. DO NOT HOLD BACK	PH23690
600	M=K+1	PH23700
	URR=U(M)	PH23710
	N=I+1	PH23720
	GO TO 650	PH23730
C	RIGHT EDGE OF MESH	PH23740
610	IF (U(K).GT.0.) GO TO 630	PH23750
C	NO MASS COMES IN FROM OUTSIDE	PH23760
C	SET FLUX TERMS TO ZERO	PH23770
620	AMMP=0.	PH23780
	GO TO 790	PH23790
C	MASS MOVING OUT OF RIGHT EDGE	PH23800
630	URR=U(K)	PH23810
640	N=I	PH23820
	M=K	PH23830
C	CALCULATE MASS FLUX AT RIGHT OF CELL	PH23840
650	IF (ABS(URR).LE.UMIN) GO TO 620	PH23850
	UVMAX=TRNSFC*DX(I)/DT	PH23860
	IF (ABS(URR).LT.UVMAX) GO TO 670	PH23870
	IF (UKR.GT.0.) GO TO 660	PH23880
	URR=-UVMAX	PH23890

	GO TO 670	PH23900
660	URR=UVMAX	PH23910
670	AMMP=AMX(M)/TAU(N)*TWOPDT*X(I)*URR	PH23920
C	SET SPECIFIC ENERGY + MOMENTUM	PH23930
	IF (NSLAVE.NE.0) GO TO 690	PH23940
680	EAMMP=.5*(U(M)**2+V(M)**2)+AIX(M)	PH23950
	UAMMP=U(M)	PH23960
	VAMMP=V(M)	PH23970
	GO TO 790	PH23980
690	IF (URR.GT.0.) GO TO 700	PH23990
	M=K+1	PH24000
	GO TO 680	PH24010
700	M=K	PH24020
	GO TO 680	PH24030
710	WSA=.5*(U(K)+U(K+1))	PH24040
	WSB=1.+(U(K+1)-U(K))*DT/((DX(I+1)+DX(I))/2.0)	PH24050
	URR=#SA/WSB	PH24060
	IF (NSLAVE.NE.0) GO TO 650	PH24070
	IF (URR) 720,620,640	PH24080
720	M=K+1	PH24090
	N=I+1	PH24100
	GO TO 650	PH24110
C	CELL K IS NOT EMPTY	PH24120
730	IF (AMX(K+1).GT.0.) GO TO 750	PH24130
C	CELL ON RIGHT OF K IS EMPTY	PH24140
	IF (U(K).LE.0.) GO TO 620	PH24150
C	SHOULD MASS GO INTO EMPTY CELL	PH24160
	IF (I.EQ.1) GO TO 740	PH24170
	IF (AIX(K-1).GT.ESESQ.OR.AIX(K).GT.ESESQ.OR.AMX(K-1)/(TAU(I-1)*DY(J)).LT.SOLID.OR.AMX(K)/(TAU(I)*DY(J)).GT.SOLID) GO TO 630	PH24180
	GO TO 620	PH24190
740	IF (AIX(K).GE.ESESQ.OR.AMX(K)/(TAU(I)*DY(J)).GE.RHOZ) GO TO 630	PH24210
	GO TO 620	PH24220
750	IF (U(K).GT.0..AND.U(K+1).LT.0.) GO TO 760	PH24230
	IF ((I+1).EQ.IMAX) (J TO 780	PH24240
	IF (AMX(K+2).GT.0..OR.U(K).GE.0..OR.U(K+1).GE.0.) GO TO 770	PH24250
C	K AND K+1 NOT EMPTY BUT CELL K+2	PH24250
C	IS EMPTY. TEST FOR SLAVING K+1 TO K	PH24270
	IF (AIX(K).GE.ESESQ.OR.AIX(K+1).GE.ESESQ.OR.AMX(K+1)/(TAU(I)*DY(J)).GE.RHOZ) GO TO 710	PH24280
	YES, SLAVE K+1 TO K	PH24290
C	NSLAVE=K+1	PH24300
	N=I	PH24310
	M=K	PH24320
	GO TO 710	PH24330
C	*** \$REFLECTIVE\$ TREATMENT	PH24340
760	UMK=U(K)*AMX(K)	PH24350
	UMKP=U(K+1)*AMX(K+1)	PH24360
	WSA=TWOPDT*X(I)	PH24370
	UOTK=UMK/TAU(I)	PH24380
	UOTKP=UMKP/TAU(I+1)	PH24390
	SB=UOTK+UOTKP	PH24400
	AMMP=WSB*WSA	PH24410
	UAMMP=(UOTK*U(K)+UOTKP*U(K+1))/WSB	PH24420
	VAMMP=(UOTK*V(K)+UOTKP*V(K+1))/WSB	PH24430
	SAVEK=AIX(K)+.5*(U(K)**2+V(K)**2)	PH24440
	EAMMP=(UOTK*SAVEK+UOTKP*(AIX(K+1)+.5*(U(K+1)**2+V(K+1)**2)))/WSB	PH24450
		PH24460

	GO TO 790	PH24470
770	IF (I.EQ.1) GO TO 710	PH24480
780	IF (AMX(K-1).NE.0..OR.U(K+1).LE.0..OR.U(K).LE.0.) GO TO 710	PH24490
C	SHOULD K BE SLAVED TO K+1	PH24500
	IF (AIX(K).GE.ESESQ.OR.AIX(K+1).GE.ESESQ.OR.AMX(K)/(TAU(I)*DY(J)).	PH24510
	1GE.RHOZ) GO TO 710	PH24520
C	YES, SLAVE K TO K+1	PH24530
	NSLAVE=K	PH24540
	N=I+1	PH24550
	M=K+1	PH24560
	GO TO 710	PH24570
C	WILL K BECOME MORE THAN EMPTY	PH24580
790	IF (ABS(AMMP).LT.AMX(K)*ROEPS.AND.ABS(AMMP).LT.ROEPS*AMX(K+1)) AMMP	PH24590
	1P=0.	PH24600
	WSOUT=0.	PH24610
	WSA=0.	PH24620
	WSB=0.	PH24630
	IF (AMMP.GT.0.) GO TO 830	PH24640
	WSA=-AMMP	PH24650
800	IF (AMPY.GT.0.) GO TO 840	PH24660
	WSA=WSA-AMPY	PH24670
810	IF (GAMC(J).LT.0.) GO TO 850	PH24680
	WSA=WSA+GAMC(J)	PH24690
820	IF (AMMY.LT.0.) GO TO 860	PH24700
	WSA=WSA+AMMY	PH24710
	GO TO 870	PH24720
830	WSB=AMMP	PH24730
	GO TO 800	PH24740
840	WSB=WSB+AMPY	PH24750
	GO TO 810	PH24760
850	WSOUT=-GAMC(J)	PH24770
	GO TO 820	PH24780
860	WSOUT=WSOUT-AMMY	PH24790
870	DELM=WSA-WSB-WSOUT	PH24800
	IF (AMX(K)+DELM.GE.0.) GO TO 970	PH24810
C	*** INTERMEDIATE PRINT FOR CELLS OVER-EMPTYING.	PH24815
	IF (INTER.EQ.0) GO TO 880	PH24820
	WRITE (6,1290) I,J,AMX(K),DELM,AMMY,GAMC(J),AMPY,AMMP	PH24830
880	IF (WSOUT.GT.AMX(K)) GO TO 920	PH24840
C	*** OTHERWISE,MAKE WSB PLUS WSOUT EXACTLY	PH24850
C	*** EQUAL TO AMX(K)	PH24860
	WS=AMX(K)-WSOUT	PH24870
	IF (AMMP.GT.0.) GO TO 900	PH24880
	AMPY=WS	PH24890
890	DELM=WSA-WSOUT-AMMP-AMPY	PH24900
C	*** INTERMEDIATE PRINT FOR OVER-EMPTIED CELL AFTER	PH24902
C	*** RIGHT AND/OR TOP FLUXES ADJUSTED.	PH24904
	IF(INTER.EQ.0) GO TO 970	PH24906
	WRITE(6,1350) AMX(K),DELM,AMMY,GAMC(J),AMPY,AMMP	PH24908
	GO TO 970	PH24910
900	IF (AMPY.GT.0.) GO TO 910	PH24920
	AMMP=WS	PH24930
	GO TO 890	PH24940
910	AMMP=WS/(AMMP+AMPY)*AMMP	PH24950
	AMPY=WS-AMMP	PH24960
	GO TO 890	PH24970
C	*** CELL OVER-EMPTIED DOWN OR LEFT. PUT IT BACK.	PH24980



920	IF (AMMP.LT.0.) GO TO 930	PH24990
	AMMP=0.	PH25000
	AMUR=0.	PH25010
	AMVR=0.	PH25020
	DELER=0.	PH25030
930	IF (AMPY.LT.0.) GO TO 940	PH25040
	AMPY=0.	PH25050
	AMUT=0.	PH25060
	AMVT=0.	PH25070
	DELET=0.	PH25080
940	MASS=AMX(K)	PH25090
	UMOM=MASS*U(K)	PH25100
	VMOM=MASS*V(K)	PH25110
	ENGY=MASS*(.5*U(K)**2+.5*V(K)**2+AIX(K))	PH25120
	MASS=MASS-AMMP	PH25130
	UMOM=UMOM-AMMP*U(K+1)	PH25140
	VMOM=VMOM-AMMP*V(K+1)	PH25150
	ENGY=ENGY-AMMP*(.5*U(K+1)**2+.5*V(K+1)**2+AIX(K+1))	PH25160
	MASS=MASS-AMPY	PH25170
	UMOM=UMOM-AMPY*U(L)	PH25180
	VMOM=VMOM-AMPY*V(L)	PH25190
	ENGY=ENGY-AMPY*(.5*U(L)**2+.5*V(L)**2+AIX(L))	PH25200
	MASS=MASS+AMMY	PH25210
	UMOM=UMOM+AMMU	PH25220
	VMOM=VMOM+AMMV	PH25230
	ENGY=ENGY+DELEB	PH25240
	MASS=MASS+GAMC(J)	PH25250
	UMOM=UMOM+FLEFT(J)	PH25260
	VMOM=VMOM+YAMC(J)	PH25270
	ENGY=ENGY+SIGC(J)	PH25280
	WSA=-AMIN1(0.,GAMC(J))/WSOUT	PH25290
	WSB=-AMIN1(0.,AMMY)/WSOUT	PH25300
	LB=K-IMAX	PH25310
	IF (LB.LT.0) WSA=1.	PH25320
	IF (LB.LT.0) GO TO 950	PH25330
	IF (AMMY.EQ.0..OR.WSB.EQ.0.) GO TO 950	PH25340
	WSC=AMX(LB)+WSB*MASS	PH25350
	WSD=AIX(LB)+.5*(U(LB)**2+V(LB)**2)	PH25360
	U(LB)=(AMX(LB)*U(LB)+WSB*UMOM)/WSC	PH25370
	V(LB)=(AMX(LB)*V(LB)+WSB*VMOM)/WSC	PH25380
	AIX(LB)=(AMX(LB)*WSD+WSB*ENGY)/WSC-.5*(U(LB)**2+V(LB)**2)	PH25390
	AMX(LB)=WSC	PH25400
950	IF (GAMC(J).EQ.0..OR.WSA.EQ.0.) GO TO 960	PH25410
	WSC=AMX(K-1)+WSA*MASS	PH25420
	WSD=AIX(K-1)+.5*(U(K-1)**2+V(K-1)**2)	PH25430
	U(K-1)=(AMX(K-1)*U(K-1)+WSA*UMOM)/WSC	PH25440
	V(K-1)=(AMX(K-1)*V(K-1)+WSA*VMOM)/WSC	PH25450
	AIX(K-1)=(AMX(K-1)*WSD+WSA*ENGY)/WSC-.5*(U(K-1)**2+V(K-1)**2)	PH25460
	AMX(K-1)=WSC	PH25470
C	*** INTERMEDIATE PRINT FOR OVER-EMPTIED CELLS AFTER	PH25472
C	MASS PUT BACK.	PH25474
960	IF (INTER.EQ.0) GO TO 1100	PH25480
	WRITE(6,1360) AMX(K), DELM, AMMY, GAMC(J), AMPY, AMMP	PH25490
	GO TO 1100	PH25500
970	IF (AMPY.EQ.0.) GO TO 960	PH25510
C	CALCULATE ENERGY AND MOMENTUM FLUX AT TOP	PH25520
	AMUT=AMPY*UAMPY	PH25530

	AMVT=AMPY*VAMPY	PH25540
	DELET=AMPY*EAMPY	PH25550
C	IS THIS AT TOP BOUNDARY	PH25560
	IF (J.NE.JMAX) GO TO 990	PH25570
C	YES, TOP. ADJUST ENERGY.	PH25580
	ETH=ETH-DELET	PH25590
	EMOT=EMOT+DELET	PH25600
	TOPM=TOPM+AMPY	PH25610
	TOPMV=TOPMV+AMVT	PH25620
	TOPMU=TOPMU+AMUT	PH25630
C	IS AMPY LARGE ENOUGH TO TRIGGER REZONE	PH25640
	IF (AMPY/((TAU(I)*DY(J)).GE.VT) REZ=1.	PH25650
	GO TO 990	PH25660
C	AMPY=0. SET MOMENTUM AND ENERGY FLUX=0.	PH25670
980	AMUT=0.	PH25680
	AMVT=0.	PH25690
	DELET=0.	PH25700
990	IF (AMPP.EQ.0.) GO TO 1000	PH25710
C	CALCULATE ENERGY + MOMENTUM FLUX AT RIGHT	PH25720
	AMUR=AMPP*UAMPP	PH25730
	AMVR=AMPP*VAMPP	PH25740
	DELER=AMPP*EAMPP	PH25750
C	IS THIS AT RIGHT BOUNDARY	PH25760
	IF (I.NE.IMAX) GO TO 1010	PH25770
C	YES, RIGHT. ADJUST ENERGY.	PH25780
	ETH=ETH-DELER	PH25790
	EMOR=EMOR+DELER	PH25800
	RTM=RTM+AMPP	PH25810
	RTMV=RTMV+AMVR	PH25820
	RTMU=RTMU+AMUR	PH25830
C	IS AMPP LARGE ENOUGH TO TRIGGER REZONE	PH25840
	IF (AMPP/((TAU(I)*DY(J)).GE.VT) REZ=1.	PH25850
	GO TO 1010	PH25860
C	AMPP=0. SET MOMENTUM AND ENERGY FLUX=0.	PH25870
1000	AMUR=0.	PH25880
	AMVR=0.	PH25890
	DELER=0.	PH25900
C	REPARTITION ENERGY + MOMENTUM	PH25910
1010	IF (DELM.EQ.0.) GO TO 1080	PH25920
1020	WSA=.5*(U(K)**2+V(K)**2)	PH25930
	SIGMU=-AMUT-AMUR+AMMU+FLEFT(J)	PH25940
	SIGMV=-AMVT-AMVR+AMMV+YAMC(J)	PH25950
	WS=DELM+AMX(K)	PH25960
	IF (WS.LE.0.) GO TO 1070	PH25970
	UNEW=(SIGMU+AMX(K)*U(K))/WS	PH25980
	DELU=UNEW-U(K)	PH25990
	IF (ABS(DELU).LT.UMIN) GO TO 1030	PH26000
	U(K)=UNEW	PH26010
1030	VNEW=(SIGMV+AMX(K)*V(K))/WS	PH26020
	DELV=VNEW-V(K)	PH26030
	IF (ABS(DELV).LT.UMIN) GO TO 1040	PH26040
	V(K)=VNEW	PH26050
1040	WSB=-DELET-DELER+DELEB+SIGC(J)	PH26060
	SIENEW=((AIX(K)+WSA)*AMX(K)+WSB)/WS-.5*(U(K)**2+V(K)**2)	PH26070
	DELI=SIENEW-AIX(K)	PH26080
	IF (ABS(DELI).GT.SIEMIN) GO TO 1050	PH26090
C	*** SUME SUMS ENERGY FLUXES TOO SMALL TO USE. SUME IS	PH26092

C	SUBTRACTED FROM ETH AT THE END OF THIS ROUTINE.	PH26094
	SUME=SUME+DELI*WS	PH26100
	GO TO 1060	PH26110
1050	AIX(K)=SIENEW	PH26120
1060	AMX(K)=WS	PH26130
	GO TO 1090	PH26140
1070	AMX(K)=0.	PH26150
	AIX(K)=0.	PH26160
	U(K)=0.	PH26170
	V(K)=0.	PH26180
	GO TO 1100	PH26190
C	DELM=0. BUT IS THERE INDIVIDUAL FLOW	PH26200
1080	IF (AMMP.NE.0.) GO TO 1020	PH26210
	IF (AMPY.NE.0.) GO TO 1020	PH26220
	IF (AMMY.NE.0.) GO TO 1020	PH26230
	IF (GAMC(J).NE.0.) GO TO 1020	PH26240
1090	IF (I.NE.I1) GO TO 1100	PH26250
	IF (U(K).NE.0..OR.V(K).NE.0..OR.AIX(K).NE.0.) NRC=1	PH26260
C	*** SPECIAL INTERMEDIATE PRINT FOR CHECKING ENERGY	PH26262
C	CONSERVATION - PRINTS ONLY IF INTER = 7 IN INPUT DECK.	PH26264
1100	IF (INTER.NE.7) GO TO 1130	PH26270
	ENERGY=DELER+DELET-SIGC(J)	PH26280
	DO 1110 NN=1,JMAX	PH26290
	ENERGY=ENERGY+SIGC(NN)	PH26300
1110	CONTINUE	PH26310
	DO 1120 LJD=2,KMAX	PH26320
	ENERGY=ENERGY+AMX(LJD)*(AIX(LJD)+.5*(U(LJD)**2+V(LJD)**2))	PH26330
1120	CONTINUE	PH26340
	WRITE (6,1300) I,J,ENERGY	PH26350
	WRITE (6,1310) AMPY,AMMP,AMMY,GAMC(J)	PH26360
	WRITE (6,1320) DELET,DELER,DELEB,SIGC(J)	PH26370
1130	CONTINUE	PH26380
	GAMC(J)=AMMP	PH26390
	FLEFT(J)=AMUR	PH26400
	YAMC(J)=AMVR	PH26410
	SIGC(J)=DELER	PH26420
	AMMY=AMPY	PH26430
	AMMU=AMUT	PH26440
	AMMV=AMVT	PH26450
	DELEB=DELET	PH26460
C		
C	*** END OF J-LOOP.	PH26465
C		
1140	K=K+IMAX	PH26470
	LL=K-IMAX	PH26480
	IF (U(LL).NE.0..OR.V(LL).NE.0..OR.AIX(LL).NE.0.) NRT=1	PH26490
C		
C	*** END OF I-LOOP.	PH26495
C		
1150	CONTINUE	PH26500
C	*** ADVANCE ACTIVE GRID.	PH26505
	I1=I1+NRC	PH26510
	I2=I2+NRT	PH26520
	IF (IMAX-I1) 1160,1170,1180	PH26530
1160	I1=IMAX	PH26540
1170	CONTINUE	PH26550
1180	IF (JMAX-I2) 1190,1200,1210	PH26560

1190	I2=JMAX	PH26570
1200	CONTINUE	PH26580
1210	GO TO 1230	PH26590
C	*** NEGATIVE MASS	PH26600
1220	NK=315	PH26610
	NR=9	PH26620
	CALL ERROR	PH26630
1230	SUM=0.0	PH26640
C	*** EVAPORATE LOW-DENSE CELLS ON BASIS OF EVAP, INPUT	PH26642
C	PARAMETER.	PH26644
	DO 1260 I=1,I1	PH26650
	K=I+1	PH26660
	DO 1270 J=1,I2	PH26670
	IF (AMX(K).EQ.0.) GO TO 1270	PH26680
	IF (AMX(K)/(TAU(1)*DY(J)).GT.EVAP*RHINI) GO TO 1250	PH26690
	WS=(U(K)**2+V(K)**2)/2.0	PH26700
	EVAPM=EVAPM+AMX(K)	PH26710
	WS=AMX(K)*(AIX(K)+WS)	PH26720
	EVAPEN=EVAPEN+WS	PH26730
	ETH=ETH-WS	PH26740
	EVAPMU=EVAPMU+AMX(K)*U(K)	PH26750
	EVAPMV=EVAPMV+AMX(K)*V(K)	PH26760
C	*** INTERMEDIATE PRINT FOR CELLS EVAPORATED.	PH26765
	IF (INTER.EQ.0) GO TO 1240	PH26770
	WRITE(6,1340) I,J,AMX(K),AIX(K),U(K),V(K)	PH26780
1240	AMX(K)=0.0	PH26790
	AIX(K)=0.0	PH26800
	P(K)=0.0	PH26810
	U(K)=0.0	PH26820
	V(K)=0.0	PH26830
	GO TO 1270	PH26840
C	*** SET NEGATIVE INTERNAL ENERGIES TO ZERO WHEN SN=0.	PH26842
C	(INPUT PARAMETER).	PH26844
1250	IF (AIX(K).GE.0..0.(.SN.GT.0.) GO TO 1270	PH26850
C	*** SUM SUMS NEGATIVE INTERNAL ENERGY SET TO ZERO.	PH26855
	SUM=SUM+AIX(K)*AMX(K)	PH26860
C	*** INTERMEDIATE PRINT FOR CELLS WHOSE NEGATIVE	PH26862
C	INTERNAL ENERGY IS SET TO ZERO.	PH26864
	IF (INTER.EQ.0) GO TO 1260	PH26870
	WRITE (6,1330) I,J,AMX(K),AIX(K),U(K),V(K)	PH26880
1260	AIX(K)=0.	PH26890
1270	K=K+IMAX	PH26900
1280	CONTINUE	PH26910
C	*** ETH = THEORETICAL ENERGY SUM, USED IN EDIT FOR	PH26912
C	ENERGY CHECK.	PH26914
C	*** EZPH2 = ENER. SET TO ZERO IN PH2 SINCE TIME=0.	PH26916
C	*** SUM = NEGATIVE INTERNAL ENERGY SET TO ZERO ON THIS	PH26917
C	CYCLE.	PH26918
C	*** SUME = SUM OF THE ENERGY FLUXES IGNORED ON THIS CYCLE.	PH26919
	ETH=ETH-SUM-SUME	PH26920
	EZPH2=EZPH2-SUME-SUM	PH26930
	RETURN	PH26940
C		PH26950
1290	FORMAT (5H NEG, I3, I4, 4H M=, 1PE14.7, 6H DELM=, 1PE14.7, 6H BOT=, 1PE14.7, 6H	PH26960
	114.7, 7H LEFT=, 1PE14.7, 6H TOP=, 1PE14.7, 5H RT=, 1PE14.7)	PH26970
1300	FORMAT (5H I= I3, 6X, 5H J= I3, 6X, 9H ENERGY=1PE15.8)	PH26980
1310	FORMAT (7H AMPY=1PE15.8, 6X, 6H AMMP=1PE15.8, 6X, 6H AMMY=1PE15.8, 9H	PH26990

```

1GAMC(J)=1PE15.8)
1320  FORMAT (7H DELET=1PE15.8,6X,6HDELER=1PE15.8,6X,6HDELEB=1PE15.8,9H PH27000
      1SIGC(J)=1PE15.8) PH27010
1330  FORMAT (4H PH2,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE15.8,PH27030
      14H V=,1PE15.8,18H SIE SET TO ZERO) PH27040
1340  FORMAT (4H PH2,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE15.8,PH27042
      14H V=,1PE15.8,19H CELL EVAPORATED) PH27044
1350  FORMAT (12H ADJUST FLUX,4H M=,1PE14.7,6H DELM=,1PE14.7,6H BOT=, PH27045
      11PE14.7,7H LEFT=,1PE14.7,6H TOP=,1PE14.7,5H RT=,1PE14.7) PH27046
1360  FORMAT (12H ADJUST MASS,4H M=,1PE14.7,6H DELM=,1PE14.7,6H BOT=, PH27047
      11PE14.7,7H LEFT=,1PE14.7,6H TOP=,1PE14.7,5H RT=,1PE14.7) PH27048
      END PH27050-

```

	SUBROUTINE REZONE	REZ	10
C	.....	REZ	20
C		REZ	30
	DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,	REZ	40
1	X(52) ,XX(54) ,TAU(52) ,JPM(52) ,	REZ	50
2	Y(102) ,YY(104) ,FLEFT(102),YAMC(102), SIGC(102),	REZ	60
3	GAMC(102),	REZ	70
4	PK(15), Z(150) ,	REZ	80
5	XP(26,51),YP(26,51),	REZ	90
6	PL(204) ,UL(204) ,PR(204) ,	REZ	100
7	RSN(52), RST(52),	REZ	110
8	CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,	REZ	120
9	DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,	REZ	130
\$	SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)	REZ	140
C	*** DIMENSIONED ARRAYS	REZ	150
C	*** Z-BLOCK IS SAVED ON TAPE.	REZ	160
	COMMON Z	REZ	170
	COMMON PK	REZ	180
	COMMON YY, XX	REZ	190
	COMMON DDX, DDY	REZ	200
	COMMON AMX, AIX, U, V, P	REZ	210
	COMMON TAU, JPM	REZ	220
	COMMON UL , PL	REZ	230
	COMMON XP , YP, CMXP, CMYP	REZ	240
C	*** NON-DIMENSIONED VARIABLES	REZ	250
	COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR ,	REZ	260
	1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN,EAMMP ,EAMPY ,	REZ	270
	2E ,ERDUMP,I ,I3 ,IWS ,J ,K ,KA ,KB ,	REZ	280
	3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT,	REZ	290
	4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN,SNR ,SNT ,STR ,SOLID ,	REZ	300
	5SUM ,TESTRH,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF,	REZ	310
	6WFLAGL,WFLAGP	REZ	320
C		REZ	330
C	*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE	REZ	340
C	X(0), Y(0), DX(0), DY(0)	REZ	350
C		REZ	360
	EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))	REZ	370
	EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))	REZ	380
C		REZ	390
C	*** SPECIAL EQUIVALENCES FOR PH2 ONLY	REZ	400
C		REZ	410
	EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),	REZ	420
1	(PL,GAMC,PR), (PL(103),SIGC)	REZ	430
C		REZ	440
C	*** SPECIAL EQUIVALENCES FOR PH3 ONLY	REZ	450
C		REZ	460
	EQUIVALENCE (UL,RSN),	REZ	470
1	(PL,RST), (P,UK),	REZ	480
2	(P(157),VK), (P(313),SNB),	REZ	490
3	(P(365),CTB), (P(417),RHO)	REZ	500
C		REZ	510
C	*** SPECIAL EQUIVALENCES FOR EDIT	REZ	520
C		REZ	530
	EQUIVALENCE (PR(1), IJ), (PR(6), JK)	REZ	540
C		REZ	550
C	*** Z-STORAGE EQUIVALENCES	REZ	560
C		REZ	570
	EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),	REZ	580

```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), REZ 590
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), REZ 600
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), REZ 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), REZ 620
5(Z( 19),NZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), REZ 630
6(Z( 23),UN23 ),(Z( 24),DMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), REZ 640
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), REZ 650
8(Z( 31),UN31 ),(Z( 32),NRC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), REZ 660
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) REZ 670
EQUIVALENCE REZ 680
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), REZ 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDELTA),(Z( 46),PRFACT) REZ 700
EQUIVALENCE REZ 710
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTOP ), REZ 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), REZ 730
3(Z( 55),VT ),(Z( 56),N6 ),(Z( 57),RTM ),(Z( 58),RTMV ), REZ 740
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), REZ 750
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), REZ 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), REZ 770
7(Z( 71),REZFCT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBOUND), REZ 780
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), REZ 790
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) REZ 800
EQUIVALENCE REZ 810
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), REZ 820
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), REZ 830
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) REZ 840
EQUIVALENCE REZ 850
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), REZ 860
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), REZ 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), REZ 880
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),RCEPS ), REZ 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), REZ 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), REZ 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), REZ 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP ), REZ 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) REZ 940
EQUIVALENCE REZ 950
1(Z(131),FRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), REZ 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), REZ 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), REZ 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), REZ 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) REZ1000
C REZ1010
C ..... REZ1020
C REZ1030
C END OF COMMON REZ1040
C ..... REZ1050
C ..... REZ1060
C REZ1070
C *** INITIALIZE P-STORAGE. CDT CALLED AGAIN AND PRESSURES REZ1072
C RECALCULATED AFTER GRID REZONED AND BEFORE PH1,PH3 REZ1074
C AND PH2 ARE CALLED. REZ1076
C
DO 10 K=2,KMAX REZ1080
P(K)=0. REZ1090
10 CONTINUE REZ1100
NJMAX=JMAX/2 REZ1110

```

	IF (IMAX.EQ.1) GO TO 20	REZ1120
	NIMAX=IMAX/2	REZ1130
	GO TO 70	REZ1140
C	*** 1-D	REZ1145
20	IMAX=2	REZ1150
	NIMAX=1	REZ1160
	K=2	REZ1170
	L=2*JMAX+2	REZ1180
C	*** STORE PROPERTIES TEMPORARILY IN UNUSED PART OF ARRAYS.	REZ1185
	DO 30 J=1,JMAX	REZ1190
	AMX(L)=AMX(K)	REZ1200
	U(L)=U(K)	REZ1210
	V(L)=V(K)	REZ1220
	AIX(L)=AIX(K)	REZ1230
	K=K+1	REZ1240
	L=L+1	REZ1250
30	CONTINUE	REZ1260
	K=2	REZ1270
	L=2*JMAX+2	REZ1280
C	*** ADD ANOTHER COLUMN OF CELLS. EACH CELL IN NEW COLUMN	REZ1282
C	WILL HAVE SAME VELOCITIES AND SIE AND 3 TIMES THE	REZ1284
C	MASS OF AXIS CELL.	REZ1286
	DO 50 J=1,JMAX	REZ1290
	DO 40 I=1,2	REZ1300
	AMX(K)=AMX(L)	REZ1310
	U(K)=U(L)	REZ1320
	V(K)=V(L)	REZ1330
	AIX(K)=AIX(L)	REZ1340
	K=K+1	REZ1350
	AMX(L)=3.*AMX(L)	REZ1360
40	CONTINUE	REZ1370
50	L=L+1	REZ1380
	L=2*JMAX+1	REZ1390
C	*** ADJUST ETH BY ADDING ENERGY OF CELLS IN NEW COLUMN.	REZ1395
	DO 60 K=3,L,2	REZ1400
	ETH=ETH+AMX(K)*(AIX(K)+(V(K)**2)/2.)	REZ1410
60	CONTINUE	REZ1420
70	DO 120 J=1,NJMAX	REZ1430
	K=(J-1)*NIMAX+2	REZ1440
	L=(J-1)*2*IMAX+2	REZ1450
	DO 110 I=1,NIMAX	REZ1460
	M=L+IMAX	REZ1470
C	*** SUM MASS OF FOUR CELLS TO BE MADE INTO ONE CELL.	REZ1475
	WSA=AMX(L)+AMX(M)+AMX(L+1)+AMX(M+1)	REZ1480
	IF (WSA.EQ.0.) GO TO 80	REZ1490
C	*** SUM KINETIC ENERGY OF FOUR CELLS.	REZ1495
	WSB=AMX(L)*(U(L)**2+V(L)**2)+AMX(M)*(U(M)**2+V(M)**2)+AMX(L+1)*(U(	REZ1500
	L+1)**2+V(L+1)**2)+AMX(M+1)*(U(M+1)**2+V(M+1)**2)	REZ1510
C	*** COMPUTE VELOCITIES OF NEW CELL FROM VELOCITIES OF	REZ1512
C	THE FOUR CELLS.	REZ1514
	U(K)=(U(L)*AMX(L)+U(M)*AMX(M)+U(L+1)*AMX(L+1)+U(M+1)*AMX(M+1))/WSA	REZ1520
	V(K)=(V(L)*AMX(L)+V(M)*AMX(M)+V(L+1)*AMX(L+1)+V(M+1)*AMX(M+1))/WSA	REZ1530
C	*** COMPUTE INTERNAL ENERGY OF NEW CELL.	REZ1535
	AIX(K)=AIX(L)*AMX(L)+AIX(M)*AMX(M)+AIX(L+1)*AMX(L+1)+AMX(M+1)*AIX(	REZ1540
	M+1)	REZ1550
	AMX(K)=WSA	REZ1560
	WS=U(K)**2+V(K)**2	REZ1570



<pre> C      E=AIX(K)+WSB/2.0       *** COMPUTE SIZE OF NEW CELL.       AIX(K)=E/AMX(K)-.5*WS       IF (K-2) 100,100,90 C      *** NEW CELL EMPTY. 80     AMX(K)=0.       AIX(K)=0.       U(K)=0.       V(K)=0. C      *** INITIALIZE STORAGE OF CELL QUANTITIES OF OLD GRID. 90     AMX(L)=0.0       U(L)=0.0       V(L)=0.0       AIX(L)=0.0       AMX(M)=0.0       U(M)=0.0       V(M)=0.0       AIX(M)=0.0       AMX(L+1)=0.0       U(L+1)=0.0       V(L+1)=0.0       AIX(L+1)=0.0       AMX(M+1)=0.0       U(M+1)=0.0       V(M+1)=0.0       AIX(M+1)=0.0 100    K=K+1       L=L+2 C      *** END OF I-LOOP 110    CONTINUE C      *** END OF J-LOOP 120    CONTINUE C      *** OLD PART OF ENLARGED GRID HAS NOW BEEN REZONED.       PROPERTIES OF NEW PART OF GRID WILL BE ASSIGNED       BELOW. C C      *** CALCULATE NEW DY'S UP TO EDGE OF OLD GRID BY       COMBINING THE OLD DY'S . CALCULATE NEW Y'S FROM       THE NEW DY'S.       DO 130 J=1,NJMAX       DY(J)=DY(2*J-1)+DY(2*J)       Y(J)=Y(J-1)+DY(J) 130    CONTINUE C      *** ASSIGN THE VALUE OF THE LAST DY CALCULATED ABOVE       TO ALL CELLS ABOVE THE OLD GRID.       NJMAX1=NJMAX+1       DO 140 J=NJMAX1,JMAX       DY(J)=DY(NJMAX)       Y(J)=Y(J-1)+DY(J) 140    CONTINUE C      *** IMAX IS SET TO 2 IF DOING A 1-D PROBLEM       IF (IMAX.EQ.2) DX(2)=DX(1)       DX(1)=DX(1)+DX(2)       X(1)=DX(1)       WS=X(1)**2       TAU(1)=PIDY*WS C      *** ARE YOU DOING A 1-D PROBLEM </pre>	<pre> REZ1580 REZ1585 REZ1590 REZ1600 REZ1605 REZ1610 REZ1620 REZ1630 REZ1640 REZ1650 REZ1660 REZ1670 REZ1680 REZ1690 REZ1700 REZ1710 REZ1720 REZ1730 REZ1740 REZ1750 REZ1760 REZ1770 REZ1780 REZ1790 REZ1800 REZ1810 REZ1820 REZ1830 REZ1835 REZ1840 REZ1845 REZ1850 REZ1852 REZ1854 REZ1856 REZ1860 REZ1862 REZ1864 REZ1870 REZ1880 REZ1890 REZ1900 REZ1902 REZ1904 REZ1910 REZ1920 REZ1930 REZ1940 REZ1950 REZ1955 REZ1960 REZ1970 REZ1980 REZ1990 REZ2000 REZ2005 </pre>
--	--

	IF (IMAX.EQ.2) GO TO 300	REZ2010
C	*** CALCULATE NEW DX'S OUT TO EDGE OF OLD GRID BY	REZ2012
C	COMBINING OLD DX'S. CALCULATE NEW X'S AND CELL-FACE	REZ2014
C	AREAS FROM THE NEW DX'S.	REZ2016
	DO 150 I=2,NIMAX	REZ2020
	DX(I)=DX(2*I-1)+DX(2*I)	REZ2030
	X(I)=X(I-1)+DX(I)	REZ2040
	*SA=X(I)**2	REZ2050
	TAU(I)=PIDY*(WSA-WS)	REZ2060
	WS=WSA	REZ2070
150	CONTINUE	REZ2080
C	*** ASSIGN THE VALUE OF THE LAST DX CALCULATED ABOVE	REZ2082
C	TO ALL CELLS TO THE RIGHT OF THE OLD GRID.	REZ2084
	NIMAX1=NIMAX+1	REZ2090
	DO 160 I=NIMAX1,IMAX	REZ2100
	DX(I)=DX(NIMAX)	REZ2110
	X(I)=X(I-1)+DX(I)	REZ2120
	WSA=X(I)**2	REZ2130
	TAU(I)=PIDY*(WSA-WS)	REZ2140
	WS=WSA	REZ2150
160	CONTINUE	REZ2160
C		REZ2170
C	*** INITIALIZE CELL BOUNDARIES	REZ2180
C		REZ2190
	JPB=0	REZ2200
	JPA=0	REZ2210
	JTB=0	REZ2220
	JTA=0	REZ2230
	IPRT=0	REZ2240
	ITRT=0	REZ2250
C		REZ2260
	IF (PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX).AND.TAYTOP.LE.Y(NJMAX	REZ2270
	1).AND.TAXRT.LE.X(NIMAX)) GO TO 300	REZ2280
C		REZ2290
C	*** COMPUTE JPB, JPA - BOTTOM AND TOP CELL BOUNDARIES OF	REZ2300
C	PROJECTILE	REZ2310
C		REZ2320
	IF (PRYBOT.LT.0..OR.(PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX))) GO TO	REZ2330
	1 TO 230	REZ2340
	J=0	REZ2350
	IF (PRYBOT.EQ.0.) GO TO 180	REZ2360
	DYSUM=0.	REZ2370
	DO 170 J=1,JMAX	REZ2380
	DYSUM=DYSUM+DY(J)	REZ2390
	IF (PRYBOT.GE.DYSUM-.5*DY(J).AND.PRYBOT.LT.DYSUM+.5*DY(J+1)) GO TO	REZ2400
	1 180	REZ2410
170	CONTINUE	REZ2420
	GO TO 230	REZ2430
180	JPB=MIN0(J+1,JMAX)	REZ2440
	DO 190 J=JPB,JMAX	REZ2450
	DYSUM=DYSUM+DY(J)	REZ2460
	IF (PRYTOP.GE.DYSUM-.5*DY(J).AND.PRYTOP.LT.DYSUM+.5*DY(J+1)) GO TO	REZ2470
	1 200	REZ2480
190	CONTINUE	REZ2490
200	JPA=J	REZ2500
C		REZ2510
C	*** COMPUTE IPRT - RIGHT CELL BOUNDARY OF PROJECTILE	REZ2520

C	DXSUM=0.	REZ2530
	DO 210 I=1,IMAX	REZ2540
	DXSUM=DXSUM+DX(I)	REZ2550
	IF (PRXRT.GE.DXSUM-.5*DX(I).AND.PRXRT.LT.DXSUM+.5*DX(I+1)) GO TO 2	REZ2560
	120	REZ2570
210	CONTINUE	REZ2580
220	IPRT=I	REZ2590
C		REZ2600
C	*** COMPUTE JTB, JTA - BOTTOM AND TOP CELL BOUNDARIES OF	REZ2610
C	TARGET	REZ2620
C		REZ2630
C		REZ2640
230	IF (TAYBOT.LT.0..OR.(TAYTOP.LE.Y(NJMAX).AND.TAXRT.LE.X(NIMAX))) GO TO 2	REZ2650
	1 TO 300	REZ2660
	J=0	REZ2670
	IF (TAYBOT.EQ.0.) GO TO 250	REZ2680
	DYSUM=0.	REZ2690
	DO 240 J=1,JMAX	REZ2700
	DYSUM=DYSUM+DY(J)	REZ2710
	IF (TAYBOT.GE.DYSUM-.5*DY(J).AND.TAYBOT.LT.DYSUM+.5*DY(J+1)) GO TO 2	REZ2720
	1 250	REZ2730
240	CONTINUE	REZ2740
	GO TO 300	REZ2750
250	JTB=MIN0(J+1,JMAX)	REZ2760
	DO 260 J=JTB,JMAX	REZ2770
	DYSUM=DYSUM+DY(J)	REZ2780
	IF (TAYTOP.GE.DYSUM-.5*DY(J).AND.TAYTOP.LT.DYSUM+.5*DY(J+1)) GO TO 2	REZ2790
	1 270	REZ2800
260	CONTINUE	REZ2810
270	JTA=J	REZ2820
C		REZ2830
C	*** COMPUTE ITRT - RIGHT CELL BOUNDARY OF TARGET	REZ2840
C		REZ2850
	DXSUM=0.	REZ2860
	DO 280 I=1,IMAX	REZ2870
	DXSUM=DXSUM+DX(I)	REZ2880
	IF (TAXRT.GE.DXSUM-.5*DX(I).AND.TAXRT.LT.DXSUM+.5*DX(I+1)) GO TO 2	REZ2890
	190	REZ2900
280	CONTINUE	REZ2910
290	ITRT=I	REZ2920
300	CONTINUE	REZ2930
C	*** REDEFINE IMAX AND JMAX FOR ORDERING THE K ARRAYS	REZ2932
C	BELOW.	REZ2934
	IMAX=NIMAX	REZ2940
	JFILB=JPA+1	REZ2950
	JFILA=JTB-1	REZ2960
	JMAX=NJMAX	REZ2970
	I1=I1/2	REZ2980
	I2=I2/2	REZ2990
C	*** IS THIS A 1-D PROBLEM	REZ2995
	IF (IMAX.GT.1) GO TO 320	REZ3000
C	*** YES.ADD TARGET MATERIAL	REZ3005
	JMP1=JMAX+1	REZ3010
	JMAX=2*JMAX	REZ3020
	DO 310 J=JMP1,JMAX	REZ3030
	K=J+1	REZ3040
	AMX(K)=RHINIT*TAU(1)*DY(J)	REZ3050

	IF (TARGI.GT.0.) I2=J	REZ3060
	AIX(K)=TARGI	REZ3070
	ETH=ETH+AMX(K)*AIX(K)	REZ3080
310	CONTINUE	REZ3090
	JPROJ=JPROJ/2	REZ3100
	I1=1	REZ3110
	GO TO 520	REZ3120
C	*** PREPARE TO SHUFFLE K ARRAYS SUCH AS TO PRESERVE	REZ3130
C	K=(J-1)*IMAX+I+1, THEN ADD MATERIAL TO NEW PART	REZ3140
C	OF GRID.	REZ3145
320	DO 360 N=1,JMAX	REZ3150
	J=JMAX+1-N	REZ3160
	K=(J-1)*IMAX+I+IMAX	REZ3170
	L=(J-1)*(IMAX+IMAX)+I+IMAX	REZ3180
	DO 350 I=1,IMAX	REZ3190
	AMX(L)=AMX(K)	REZ3200
	AIX(L)=AIX(K)	REZ3210
	U(L)=U(K)	REZ3220
	V(L)=V(K)	REZ3230
	IF (J-1) 340,340,330	REZ3240
330	AMX(K)=0.0	REZ3250
	AIX(K)=0.0	REZ3260
	V(K)=0.0	REZ3270
	U(K)=0.0	REZ3280
340	K=K-1	REZ3290
	L=L-1	REZ3300
350	CONTINUE	REZ3310
360	CONTINUE	REZ3320
C	*** REDEFINE IMAX,JMAX SO THEY WILL REPRESENT NUMBER	REZ3322
C	OF COLUMNS AND ROWS IN NEW GRID (SAME AS IN OLD GRID).	REZ3324
	IMAX=NIMAX*2	REZ3330
	JMAX=NJMAX*2	REZ3340
	IL=NIMAX+1	REZ3350
	JL=NJMAX+1	REZ3360
	IF (PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX).AND.TAYTOP.LE.Y(NJMAX	REZ3370
	1).AND.TAXRT.LE.X(NIMAX)) GO TO 510	REZ3380
C	*** ADD APPROPRIATE MATERIAL	REZ3390
C	IN CELLS ABOVE (BUT NOT TO THE RIGHT OF) OLD GRID.	REZ3395
	DO 430 I=1,NIMAX	REZ3400
	K=(JL-1)*IMAX+I+1	REZ3410
	DO 420 J=JL,JMAX	REZ3420
	IF (PRYBOT.LT.0.) GO TO 370	REZ3430
	IF (J.GE.JPB.AND.J.LE.JPA.AND.I.LE.IPRT) GO TO 390	REZ3440
C	*** NOT PROJECTILE-MATERIAL	REZ3450
370	IF (RHOFIL.EQ.0.) GO TO 380	REZ3460
	IF (J.GE.JFILB.AND.J.LE.JFILA) GO TO 400	REZ3470
C	*** NOT FILLER-MATERIAL	REZ3480
380	IF (TAYBOT.LT.0.) GO TO 420	REZ3490
	IF (J.GE.JTB.AND.J.LE.JTA.AND.I.LE.ITRT) GO TO 410	REZ3500
C	*** NOT TARGET. THUS,VACUUM.	REZ3510
	GO TO 420	REZ3520
C	*** ADD PROJ. MATERIAL	REZ3530
390	AMX(K)=RHINI*TAU(I)*DY(J)	REZ3540
	IF (PROJU.EQ.0..AND.VINI.EQ.0..AND.PROJI.EQ.0.) GO TO 420	REZ3550
	IF (I.GT.I1) I1=I	REZ3560
	IF (J.GT.I2) I2=J	REZ3570
	U(K)=PROJU	REZ3580

	V(K)=VINI	REZ3590
	AIX(K)=PROJI	REZ3600
	GO TO 420	REZ3610
C	*** ADD FILLER	REZ3620
400	AMX(K)=RHOFIL*TAU(I)*DY(J)	REZ3630
	GO TO 420	REZ3640
C	*** ADD TARGET MATERIAL	REZ3650
410	AMX(K)=RHINIT*TAU(I)*DY(J)	REZ3660
	IF (TARGV.EQ.0..AND.TARGI.EQ.0.) GO TO 420	REZ3670
	IF (I.GT.I1) I1=I	REZ3680
	IF (J.GT.I2) I2=J	REZ3690
	V(K)=TARGV	REZ3700
	AIX(K)=TARGI	REZ3710
420	K=K+IMAX	REZ3720
430	CONTINUE	REZ3730
C	*** ADD APPROPRIATE MATERIAL TO CELLS ON THE RIGHT	REZ3732
C	OF THE OLD GRID.	REZ3734
	DO 500 I=IL,IMAX	REZ3740
	K=I+1	REZ3750
	DO 490 J=1,JMAX	REZ3760
	IF (PRYBOT.LT.0.) GO TO 440	REZ3770
	IF (J.GE.JPB.AND.J.LE.JPA.AND.I.LE.IPRT) GO TO 460	REZ3780
C	*** NOT PROJECTILE MATERIAL.	REZ3785
440	IF (RHOFIL.EQ.0.) GO TO 450	REZ3790
	IF (J.GE.JFILB.AND.J.LE.JFILA) GO TO 470	REZ3800
C	*** NOT FILLER MATERIAL.	REZ3805
450	IF (TAYBOT.LT.0.) GO TO 490	REZ3810
	IF (J.GE.JTB.AND.J.LE.JTA.AND.I.LE.ITRT) GO TO 480	REZ3820
C	*** NOT TARGET MATERIAL. THUS,VACUUM.	REZ3825
	GO TO 490	REZ3830
C	*** ADD PROJECTILE MATERIAL.	REZ3835
460	AMX(K)=RHINI*TAU(I)*DY(J)	REZ3840
	IF (PROJU.EQ.0..AND.VINI.EQ.0..AND.PROJI.EQ.0.) GO TO 490	REZ3850
	IF (I.GT.I1) I1=I	REZ3860
	IF (J.GT.I2) I2=J	REZ3870
	U(K)=PROJU	REZ3880
	V(K)=VINI	REZ3890
	AIX(K)=PROJI	REZ3900
	GO TO 490	REZ3910
C	*** ADD FILLER.	REZ3915
470	AMX(K)=RHOFIL*TAU(I)*DY(J)	REZ3920
	GO TO 490	REZ3930
C	*** ADD TARGET MATERIAL.	REZ3935
480	AMX(K)=RHINIT*TAU(I)*DY(J)	REZ3940
	IF (TARGV.EQ.0..AND.TARGI.EQ.0.) GO TO 490	REZ3950
	IF (I.GT.I1) I1=I	REZ3960
	IF (J.GT.I2) I2=J	REZ3970
	V(K)=TARGV	REZ3980
	AIX(K)=TARGI	REZ3990
490	K=K+IMAX	REZ4000
500	CONTINUE	REZ4010
C	*** REDEFINE JPROJ,USUALLY J-INDEX OF TOP CELL IN	REZ4012
C	PROJECTILE (INPUT PARAMETER).	REZ4014
510	JPROJ=JPROJ/2	REZ4020
C	*** REDEFINE ACTIVE GRID MARKERS.	REZ4030
C		REZ4040
	I1=I1+2	REZ4050

520	I2=I2+2	REZ4060
	IF (I1.GT.IMAX) I1=IMAX	REZ4070
	IF (I2.GT.JMAX) I2=JMAX	REZ4080
C	*** CALL TO REZONE AND COT COUNTED AS A CALCULATIONAL	REZ4082
C	CYCLE, SO NC AND T ARE INCREMENTED BEFORE PROCEEDING	REZ4084
C	ON TO PH1,PH3 AND PH2.	REZ4086
	WS=T+DTNA	REZ4090
	NK=NC+1	REZ4100
C		REZ4110
	WRITE (5,620) WS,NK,UX(1)	REZ4120
C	*** REDEFINE CONSTANTS AND CELL LIMITS FOR CALCULATING	REZ4122
C	TENSIONS AND STRESSES.	REZ4124
	KMAX=IMAX*JMAX+1	REZ4130
	IMAXA=IMAX+1	REZ4140
	JMAXA=JMAX+1	REZ4150
	KMAXA=KMAX+1	REZ4160
	N6=N6/2	REZ4170
	JSTR=JSTR/2	REZ4180
	IF (NUMREZ.GT.NREZ) NREZ=NUMREZ	REZ4190
	NPLACE=NREZ-NUMREZ+2	REZ4200
C	*** CALCULATE NEW ETI	REZ4210
	ETH=0.	REZ4230
	DO 530 K=2,KMAX	REZ4240
	ETH=ETH+AMX(K)*(AIX(K)+.5*(U(K)**2+V(K)**2))	REZ4250
530	CONTINUE	REZ4260
C	***DIVIDE JPM(1) BY 2 TO GET NEW PEAK PRESSURE CELLS.	REZ4270
	DO 550 I=1,IMAX	REZ4280
	L=2*I	REZ4290
	IF (L.GT.IMAX) GO TO 540	REZ4300
	JPM(I)=JPM(L)/2	REZ4310
	GO TO 550	REZ4320
540	JPM(I)=0	REZ4330
550	CONTINUE	REZ4340
	IF (Y2.GT.(-1.)) GO TO 610	REZ4350
C		REZ4360
C	*** SCALE EXISTING TRACER POINTS	REZ4370
C		REZ4380
	DO 560 J=1,JJ	REZ4390
	DO 560 I=1,II	REZ4400
	XP(I,J)=XP(I,J)/2.	REZ4410
	YP(I,J)=YP(I,J)/2.	REZ4420
560	CONTINUE	REZ4430
C		REZ4440
C	*** REMOVE TRACER POINTS FROM EVERY OTHER CELL AND EVERY	REZ4450
C	OTHER ROW	REZ4460
C		REZ4470
	NMP=0	REZ4480
	M=0	REZ4490
	DO 570 J=1,JJ,2	REZ4500
	M=M+1	REZ4510
	L=0	REZ4520
	DO 570 I=1,II,2	REZ4530
	L=L+1	REZ4540
	XP(L,M)=XP(I,J)	REZ4550
	YP(L,M)=YP(I,J)	REZ4560
570	NMP=NMP+1	REZ4570
	JTPB=1	REZ4580

```
JTPT=INT(FLOAT(JJ)/2+.6)
ITPL=INT(FLOAT(II)/2+.6)+1
```

```
C
C
C
C
```

```
*** INITIALIZE REMAINING TRACER POINT STORAGE AND
*** PLACE NEW TRACER POINTS FIRST IN NEW CELLS ABOVE OLD
GRID THEN IN NEW CELLS TO THE RIGHT OF OLD GRID.
```

```
580
```

```
DO 600 J=JTPB,JTPT
DO 600 I=ITPL,II
XP(I,J)=0.
YP(I,J)=0.
K=2*((J-1)*IMAX+1)
IF (AMX(K).EQ.0.) GO TO 590
ICELL=2*I-1
JCELL=2*J-1
```

```
C
C
C
```

```
*** PLACE NEW TRACER POINTS IN CELLS SO THEY LINE UP
WITH EXISTING TRACER POINTS BY USING NPLACE WHICH
IS A FUNCTION OF THE NUMBER OF REZONES PERFORMED.
```

```
XP(I,J)=FLOAT(ICELL-1)+1./2.**NPLACE
YP(I,J)=FLOAT(JCELL-1)+1./2.**NPLACE
```

```
590
```

```
NMP=NMP+1
```

```
600
```

```
CONTINUE
```

```
IF (J.GE.JJ) GO TO 610
```

```
C
```

```
*** GO BACK THROUGH LOOPS ADDING POINTS ON RIGHT SIDE OF
OLD GRID.
```

```
C
```

```
JTPB=JTPT+1
```

```
JTPT=JJ
```

```
ITPL=1
```

```
GO TO 580
```

```
610
```

```
RETURN
```

```
C
```

```
620
```

```
FORMAT (1H ////22H PROBLEM REZONED AT T=,1PE12.6,6X,5HCYCLEI4,6X,6REZ4840
1HDX(1)=,E12.6////)
END
```

```
REZ4590
REZ4600
REZ4610
REZ4620
REZ4630
REZ4635
REZ4640
REZ4650
REZ4660
REZ4670
REZ4680
REZ4690
REZ4700
REZ4710
REZ4720
REZ4722
REZ4724
REZ4726
REZ4730
REZ4740
REZ4750
REZ4760
REZ4770
REZ4772
REZ4774
REZ4780
REZ4790
REZ4800
REZ4810
REZ4820
REZ4830
REZ4840
REZ4850
REZ4860-
```

```

SUBROUTINE ERROR
.....
C
C
DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
1 X(52),XX(54),TAU(52),JPM(52),
2 Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),
3 GAMC(102),
4 PK(15),Z(150),
5 XP(26,51),YP(26,51),
6 PL(204),UL(204),PR(204),
7 RSN(52),RST(52),
8 CMXP(5),CMYP(5),IJ(5),JK(5),
9 DX(52),DDX(54),DY(102),DDY(104),
$ SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)
C
C
*** DIMENSIONED ARRAYS
*** Z-BLOCK IS SAVED ON TAPE.
COMMON Z
COMMON PK
COMMON YY, XX
COMMON DDX, DDY
COMMON AMX, AIX, U, V, P
COMMON TAU, JPM
COMMON UL, PL
COMMON XP, YP, CMXP, CMYP
C
C
*** NON-DIMENSIONED VARIABLES
COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR,
1AMVT, DELEB, DELER, DELET, DELM, DTODX, DXYMIN, EAMMP, EAMPY,
2E, ERDUMP, I, I3, IWS, J, K, KA, KB,
3LL, MD, ME, MZT, NERR, NK, NPRINT,
4NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID,
5SUM, TESTRI, TWOPI, URR, WS, WSA, WSB, WSC, WFLAGF,
6WFLAGL, WFLAGP
C
C
*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
X(0), Y(0), DX(0), DY(0)
C
C
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))
C
C
*** SPECIAL EQUIVALENCES FOR PH2 ONLY
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
(PL,GAMC,PR), (PL(103),SIGC)
C
C
*** SPECIAL EQUIVALENCES FOR PH3 ONLY
EQUIVALENCE (UL,RSN),
1 (PL,RST), (P,UK),
2 (P(157),VK), (P(313),SNB),
3 (P(365),STB), (P(417),RHO)
C
C
*** SPECIAL EQUIVALENCES FOR EDIT
EQUIVALENCE (PR(1), IJ), (PR(6), JK)
C
C
*** Z-STORAGE EQUIVALENCES
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ),

```



```

1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7); ERR 599
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z( 10),RTMU ), ERR 600
3(Z( 11),STK1 ),(Z( 12),NUMREZ),(Z( 13),ETH ),(Z( 14),UN14 ), ERR 610
4(Z( 15),RHINIT),(Z( 16),PROJI ),(Z( 17),UN17 ),(Z( 18),XMAX ), ERR 620
5(Z( 19),HZ ),(Z( 20),NREZ ),(Z( 21),AMDM ),(Z( 22),UVMAX ), ERR 630
6(Z( 23),UN23 ),(Z( 24),PMIN ),(Z( 25),JSTR ),(Z( 26),DTNA ), ERR 640
7(Z( 27),CVIS ),(Z( 28),STK2 ),(Z( 29),STEZ ),(Z( 30),NC ), ERR 650
8(Z( 31),UN31 ),(Z( 32),ARC ),(Z( 33),IMAX ),(Z( 34),IMAXA ), ERR 660
9(Z( 35),JMAX ),(Z( 36),JMAXA ),(Z( 37),KMAX ),(Z( 38),KMAXA ) ERR 670
EQUIVALENCE ERR 680
1(Z( 39),BOTM ),(Z( 40),BOTMV ),(Z( 41),NUMSPT),(Z( 42),CZERO ), ERR 690
2(Z( 43),NUMSCA),(Z( 44),PRLIM ),(Z( 45),PRDELTA),(Z( 46),PRFACT) ERR 700
EQUIVALENCE ERR 710
1(Z( 47),I1 ),(Z( 48),I2 ),(Z( 49),IPCYCL),(Z( 50),TSTCP ), ERR 720
2(Z( 51),RHOFIL),(Z( 52),TARGV ),(Z( 53),N3 ),(Z( 54),IVARDY), ERR 730
3(Z( 55),VT ),(Z( 56),NG ),(Z( 57),RTM ),(Z( 58),RTMV ), ERR 740
4(Z( 59),UN59 ),(Z( 60),N10 ),(Z( 61),N11 ),(Z( 62),GAMMA ), ERR 750
5(Z( 63),TOPM ),(Z( 64),BOTMU ),(Z( 65),SN ),(Z( 66),TOPMV ), ERR 760
6(Z( 67),PRYBOT),(Z( 68),PRYTOP),(Z( 69),PRXRT ),(Z( 70),CYCPH3), ERR 770
7(Z( 71),REZFACT),(Z( 72),TARGI ),(Z( 73),PROJU ),(Z( 74),BBCUND), ERR 780
8(Z( 75),EVAP ),(Z( 76),ECK ),(Z( 77),NECYCL),(Z( 78),II ), ERR 790
9(Z( 79),JJ ),(Z( 80),NMP ),(Z( 81),Y2 ),(Z( 82),EZPH1 ) ERR 800
EQUIVALENCE ERR 810
1(Z( 83),IVARDX),(Z( 84),T ),(Z( 85),NMPMAX),(Z( 86),PMIN ), ERR 820
2(Z( 87),INTER ),(Z( 88),TAYBOT),(Z( 89),TAYTOP),(Z( 90),IEMAP ), ERR 830
3(Z( 91),MC ),(Z( 92),MR ),(Z( 93),MZ ),(Z( 94),MB ) ERR 840
EQUIVALENCE ERR 850
1(Z( 95),REZ ),(Z( 96),NODUMP),(Z( 97),UN97 ),(Z( 98),UN98 ), ERR 860
2(Z( 99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU), ERR 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), ERR 880
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), ERR 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), ERR 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), ERR 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),ESESQ ),(Z(122),ESES ), ERR 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAP3),(Z(126),IUMAP ), ERR 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) ERR 940
EQUIVALENCE ERR 950
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), ERR 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), ERR 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), ERR 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), ERR 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) ERR1000
ERR1010
C .....ERR1020
C .....ERR1030
C END OF COMMON ERR1040
C .....ERR1050
C .....ERR1060
C .....ERR1070
IF (NERR.EQ.1) GO TO 120 ERR1080
GO TO (10,20,30,40,50,60,70,80,90,100), NR ERR1090
10 WRITE (6,130) NK ERR1100
GO TO 110 ERR1110
20 WRITE (6,140) NK ERR1120
GO TO 110 ERR1130
30 WRITE (6,150) NK ERR1140
GO TO 110 ERR1150

```

40	WRITE (6,160) NK	ERR1150
	GO TO 110	ERR1170
50	WRITE (6,170) NK	ERR1180
	GO TO 110	ERR1190
60	WRITE (6,180) NK	ERR1200
	GO TO 110	ERR1210
70	WRITE (6,190) NK	ERR1220
	GO TO 110	ERR1230
80	WRITE (6,200) NK	ERR1240
	GO TO 110	ERR1250
90	WRITE (6,210) NK	ERR1260
	GO TO 110	ERR1270
100	WRITE (6,220) NK	ERR1280
110	WRITE (6,230) I,J,K,(M,Z(M),Z(M),M=1,150)	ERR1290
C	*** IF NR=1, ERROR IS IN INPUT DECK	ERR1292
	IF(NR.EQ.1) GO TO 120	ERR1294
C	*** IF NR=5 AND NK=130, EDIT PRINT HAS JUST BEEN DONE. BY	ERR1296
C	SETTING ERDUMP=1, EDIT WILL DO A TAPE DUMP BUT NOT	ERR1298
C	ANOTHER PRINT.	ERR1300
	IF (NR.EQ.5.AND..K.EQ.130) ERDUMP=1.	ERR1310
	NERR = 1	ERR1315
	I3=I1	ERR1320
	NPRINT=1	ERR1330
	NFLAGL=1.	ERR1340
	NUMSPT=NDUMP7	ERR1350
	CALL EDIT	ERR1360
120	CALL EXIT	ERR1370
C		ERR1380
C		ERR1390
130	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1400
	1 INPUT )	ERR1410
140	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1420
	1 SETUP )	ERR1430
150	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1440
	1 CDT )	ERR1450
160	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1460
	1 ES )	ERR1470
170	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1480
	1 EDIT )	ERR1490
180	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1500
	1 MAP )	ERR1510
190	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1520
	1 PH1 )	ERR1530
200	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1540
	1 PH3 )	ERR1550
210	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1560
	1 PH2 )	ERR1570
220	FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,15,10H IN	ERR1580
	1 REZONE)	ERR1590
230	FORMAT (//5X,6H I=,I3,6H J=I3,6H K=I3//16X,7HZ-BLOCK//6X,ERR1600	
	115H REAL FORMAT ,5X,15H INTEGER FORMAT/2X,1H,8X,4HZ(I),17X,4HZ(	ERR1610
	2I)//(I4,2X,E15.6,5X,I15))	ERR1620
	END	ERR1630-

## 7. DICTIONARY

This section includes a description of the use and location of each of the variables in the program. The following terminology is used in the dictionary:

"Local"		Means name is local to subroutine (not in Blank Common).
"Local <sup>(C)</sup> "		Means name is in Blank Common (or equivalenced to a variable in Blank Common), but its value is never passed to another subroutine.
"Global"		Means name is in Blank Common (or equivalenced to a variable in Blank Common) and its value is passed from one routine to another.
= Z(N)		Means variable is equivalenced to a member of the Z-array, the first array in Blank Common. These variables are usually used in setting up and restarting.
ADDVL	Local	Used in SETUP. Used in finding volume of cells containing sphere-boundary.
AID	Local <sup>(C)</sup>	Used in EDIT in calculation of crater depth.
AIX	Global	Specific interal energy in a cell. (IMAX by JMAX array.)
ALE	Constants	Used in MAP. This array has alphabetic characters for pressure, density, velocity, and energy maps. (Defined in DATA statement.)
AMDM	= Z(21)	INPUT parameter. A cell with compression > AMDM is considered solid. Usual value: 0.95 to 0.99. Used in ES in testing whether to allow negative pressures (tensions). Used in INPUT to calculate SOLID = AMDM * RHOZ, which is used in CPT and PH3.
AMMP	Local	Used in PH2. Mass moving across right boundary of a cell. (See Appendix B)

AMMU	Local	Used in PH2. Radial momentum transported across the bottom boundary of a cell. (See Appendix B)
AMMV	Local <sup>(C)</sup>	Used in PH2. Axial momentum transported across the bottom boundary of a cell. (See Appendix B)
AMMY	Local <sup>(C)</sup>	Used in PH2. Amount of mass moving across bottom of a cell. (See Appendix B)
AMPY	Local <sup>(C)</sup>	Used in PH2. Amount of mass moving across top of a cell. (See Appendix B)
AMUR	Local <sup>(C)</sup>	Used in PH2. Radial momentum transported across right boundary of a cell. (See Appendix B)
AMUT	Local <sup>(C)</sup>	Used in PH2. Radial momentum transported across top boundary of cell. (See Appendix B)
AMVR	Local <sup>(C)</sup>	Used in PH2. Axial momentum transported across right boundary of a cell. (See Appendix B)
AMVT	Local <sup>(C)</sup>	Used in PH2. Axial momentum transported across top boundary of a cell. (See Appendix B)
AMX	Global	Mass in a cell. (IMAX by JMAX array.)
AREAFC	Local <sup>(C)</sup>	Used in SETUP. Area of a cell-face. Used in setting up a sphere. Equivalenced to DELEB.
B	Local	Used and calculated in PH3
BEAR	= Z(149)	Used in CDT. An INPUT parameter used in local sound-speed calculation whose value depends on the kind of material. (Local sound-speed is approximated as $C_0 + (BEAR) \cdot \sqrt{P(K)}$ .)
BBOUND	= Z(74)	Calculated in PH3. Printed in EDIT under "Plastic-Work." Total work done by the plastic stresses.
BOIM	= Z(39)	Calculated in PH2. Printed in EDIT. Total mass lost out bottom of grid.
BOIMU	= Z(64)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out bottom of grid.

BOTMV	= Z(40)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out bottom of grid.
CMXP	Local <sup>(C)</sup> }	Used and calculated in EDIT for printing the centimeter coordinates of the tracer points.
CMYP	Local <sup>(C)</sup> }	
CNAUT	= Z(148)	Used in CDT, INPUT. Approximate sound-speed of material; calculated in INPUT as
		$C_0 = \sqrt{\frac{ESCAPA}{RHOZ}} = \sqrt{A/\rho} .$
CRAD	Local <sup>(C)</sup>	Used in EDIT for printing radii of crater depths. Equivalenced to UL array.
CVIS	= Z(27)	INPUT parameter. Used to describe the bottom boundary-condition. Used in PH1, PH2, PH3. Bottom boundary is transmittive when CVIS = -1., reflective when CVIS = 0.
CYCLE	= Z(2)	Used in INPUT, SETUP, CDT, EDIT. Cycle number (an integer value in floating point form).
CYCPH3	= Z(70)	Used in MAIN and PH3. INPUT parameter: Number of times to subcycle PH3. If value is -1., PH3 is omitted.
CZERO	= Z(42)	INPUT parameter. Value of $Y_0$ for yield strength calculation. Used in PH3. (See STRENG)
DDX	Global	An array equivalenced to the DX array such that $DDX(1) = DX(0)$ .
DDY	Global	An array equivalenced to the DY array such that $DDY(1) = DY(0)$ .
DELEB	Local <sup>(C)</sup>	Used in PH2. Total energy associated with mass transported across bottom boundary of a cell. (See Appendix B)
DELER	(Local <sup>(C)</sup>	Used in PH2. Total energy associated with mass transported across right boundary of a cell. (See Appendix B)
DELET	Local <sup>(C)</sup>	Used in PH2. Total energy associated with mass transported across top boundary of a cell. (See Appendix B)

DELI	Local	Used in PH2, PH3. Change of specific internal energy of a cell.
DEIM	Local <sup>(c)</sup>	Used in PH2 for total mass moving into or out of a cell.
DELU	Local	Used in PH2, PH3. Change of radial velocity of a cell.
DELV	Local	Used in PH2, PH3. Change of axial velocity of a cell.
DMIN	= Z(24)	INPUT parameter. Allowable relative error in energy sum. If error is > DMIN then calculation is terminated. Used in EDIT. If everything is working right you should be able to use $10^{-3}$ for DMIN.
DSCALE	Local	Used in MAP as linear scale factor for compression map.
DT	= Z(3)	Time step. Calculated in CDT. Used in SETUP, EDIT, PH1, PH2 and PH3.
DTFACT	Local	Used in PH3 in calculating a variable time step when subcycling the PH3 calculations.
DTMIN	= Z(144)	INPUT parameter. Used in CDT. After STAB = FINAL, if $DT < DTMIN$ execution is stopped.
DTNA	= Z(26)	DT from previous time cycle. Used in INPUT, CDT, EDIT, REZONE and PH1.
DTNOW	Local	Used in EDIT. Used for saving DT when calling CDT to recalculate pressures after a REZONE.
DTODX	Local <sup>(c)</sup>	Used in PH2 for $D^2/DX$ .
DTODY	Local	Used in PH2 for $DT/DY$ .
DTSTR	Local	Used in PH3. DT for recycling through PH3.
DUODX	Local	Used in PH3. $DU/DX$ .
DUODY	Local	Used in PH3. $DU/DY$ .
DVODX	Local	Used in PH3. $DV/DX$ .

DVODY	Local	Used in PH3. DV/DY.
DX	Global	The radial dimension of cells. Equivalenced to DDX such that $DDX(1) = DX(0)$ .
DXF	= Z(136)	An INPUT parameter used to calculate the DX array if the radial dimension of the cells is uniform.
DXSUM	Local	Used in SETUP and REZONE to find cell dimensions of packages when DX is not constant.
DXYMIN	Local <sup>(C)</sup>	Used in CDT. Minimum (DX, DY) of a cell. Used in calculation of SRATIO and DT.
DY	Global	The axial-dimension of cells. Equivalenced to DDY so that $DDY(1) = DY(0)$ .
DYF	= Z(137)	INPUT parameter. DY of all cells, if DY is constant.
DYSUM	Local	Used in SETUP and REZONE to find cell dimensions of packages when DY is not constant.
E	Local <sup>(C)</sup>	Used in REZONE, PH1, and PH3. Temporary storage for energy calculations.
EAMMP	Local <sup>(C)</sup>	Used in PH2. Specific internal energy of mass moving across right edge of cell.
EAMPY	Local <sup>(C)</sup>	Used in PH2. Specific internal energy of mass moving across top of cell.
ECK	= Z(76)	Used in EDIT. Relative error in energy sum. If $ ECK  > DMIN$ , execution is stopped.
EMOB	= Z(150)	Calculated in PH2. Printed in EDIT. Energy change out of bottom of mesh.
EMOR	= Z(135)	Calculated in PH2. Printed in EDIT. Energy change out right side of mesh.
EMOT	= Z(146)	Calculated in PH2. Printed in EDIT. Energy change out of top of mesh.
ENERGY	Local	Used in PH2 to sum energy of cells.
ENGY	Local	Used in PH2 as temporary storage for energy of a cell.

EOB	= Z(134)	Calculated in PH1. Printed in EDIT. Energy change due to work done at bottom boundary.
EOR	= Z(132)	Calculated in PH1. Printed in EDIT. Energy change due to work done at right boundary.
EOT	= Z(133)	Calculated in PH1. Printed in EDIT. Energy change due to work done at top boundary.
ERDUMP	Local <sup>(c)</sup>	Used in EDIT and ERROR. Flags EDIT to stop execution because ERROR has been called.
ESA	= Z(116)	INPUT parameter. Value of "a" in equation of state. Used in ES. (= $\gamma - 1$ when using perfect gas equation of state.)
ESALPH	= Z(123)	INPUT parameter. Value of " $\alpha$ " in equation of state. Used in ES.
ESB	= Z(118)	INPUT parameter. Value of "b" in equation of state. Used in ES.
ESBETA	= Z(124)	INPUT parameter. Value of " $\beta$ " in equation of state. Used in ES.
ESCAPA	= Z(119)	INPUT parameter. Value of "A" in equation of state. Used in ES.
ESCAPB	= Z(125)	INPUT parameter. Value of "B" in equation of state. Used in ES.
ESCLE	Local	Used in MAP as a logarithmic scale factor for energy map.
ESES	= Z(122)	INPUT parameter. Value of ES in equation of state. Used in ES.
ESESP	= Z(120)	INPUT parameter. Value of ES' in equation of state. Used in ES.
ESESQ	= Z(121)	INPUT parameter. ESESQ is usually equal to ESESP. It is used to test whether a cell should be considered hot or cold in free-surface treatment. Used in CDT and PH2.



ESEZ	= Z(117)	INPUT parameter. Value of "E <sub>0</sub> " in equation of state. Used in ES.
ESUM	Local	Used in EDIT to sum energy and calculate relative error of energy sum.
ETA	Local	Used and calculated in ES. = $\rho/\rho_0$ .
ETH	= Z(13)	Theoretical value of total energy in the mesh. Used in SETUP, EDIT, REZONE, PH1, PH2, PH3. Calculated in SETUP initially; in PH2 thereafter. It is redefined in REZONE.
EVAP	= Z(75)	INPUT parameter. Used in PH2. Any cell with density less than EVAP times initial density of "projectile" is "evaporated" and its energy subtracted from theoretical energy of system. ( $10^{-3}$ to $10^{-8}$ are appropriate values.)
EVAPEN	= Z(101)	Calculated in PH2 and CDT. Printed in EDIT. Sum of energy lost through "evaporation" described under EVAP. Adjusted in CDT when "evaporating" energy of isolated cells. Initialized in SETUP. Equivalenced to SIESPH in SETUP.
EVAPM	= Z(100)	Calculated in PH2. Printed in EDIT. Sum of mass lost through "evaporation" described under EVAP. Used in PH2 and CDT when "evaporating" mass of isolated cells. Initialized in SETUP. Equivalenced to RHOSPH in SETUP.
EVAPMU	= Z(102)	Calculated in PH2. Printed in EDIT. Sum of radial momenta lost through "evaporation." Used in PH2 and CDT when "evaporating" momentum of isolated cells. Initialized in SETUP. Equivalenced to VINSPPH in SETUP.
EVAPMV	= Z(103)	Calculated in PH2. Sum of axial momenta lost through "evaporation". Printed in EDIT. Used in PH2 and CDT when "evaporating" momentum of isolated cells. Initialized in SETUP. Equivalenced to RHOOUT in SETUP.

EZPH1	= Z(82)	Energy gained through setting negative internal energies to zero in PH1. Printed in EDIT.
EZPH2	= Z(104)	Calculated in PH2. Sum of specific internal energy fluxes less than SIEMIN and negative internal energies set to zero. Printed in EDIT.
FINAL	= Z(113)	INPUT parameter. Maximum value of stability fraction (STAB). If FINAL = 0; the stability fraction will be constant. Used in CDF.
FLEFT	Local <sup>(C)</sup>	Used in PH2. Radial momentum of mass moving across left side of cell. Equivalenced to UL array. (See Appendix B)
FLOTMA	Local	Used in MAP.
FRX	Local	Used in PH2 for moving tracer-points.
FRY	Local	Used in PH2 for moving tracer-points.
GAMC	Local <sup>(C)</sup>	Used in PH2. Mass moving across left side of cell. Equivalenced to PL and PR arrays. (See Appendix B)
GAMMA	= Z(62)	Calculated value of GAMMA = ESA + 1. Calculated in INPUT. Used in CDT.
HOOP	Local	Used in PH3. Hoop stress.
I	Local <sup>(C)</sup>	Used in most subroutines as index in radial direction.
IAID	Local	Used in EDIT in crater depth calculation.
ICELL	Local	Used in REZONE when placing tracer points in new cells.
ICP3	Local	Used in PH3: = INT(CYCPH3).
ICSTOP	= Z(7)	INPUT parameter. Used in EDIT. Execution stops on ICSTOP cycle when stopping on cycles rather than time.
IDL	Local	Used in MAP. Number of columns in maps. On cycle 0, IDL = IMAX; otherwise IDL = 11.

IDNMAP	= Z(103)	} Defined in INPUT. Used in MAP to specify the number of symbols to be used in the density, energy, pressure, u-velocity, and v-velocity maps, respectively.
IEMAP	= Z(90)	
IPRMAP	= Z(109)	
IUMAP	= Z(116)	
IVMAP	= Z(114)	
II	= Z(78)	Used in REZONE, EDIT, and SETUP. The number of tracer points in each row.
IJ	Local <sup>(C)</sup>	Used in EDIT. Used to identify which column a tracer point originated in. Equivalenced to PR(1) in EDIT.
IK	Local	Used in PH3 as index, = I + 1.
IKK	Local	Used in PH3, = IK + 1.
ILIM1	Local	Used in MAP as index for printing values of symbols.
ILIM2	Local	See ILIM1.
IMAX	= Z(33)	INPUT parameter. Number of columns in mesh. IMAX must be an even number if grid is to be rezoned with the exception that IMAX = 1 for a 1-D problem. Used in SETUP, CDT, REZONE, EDIT, PH1, PH2, and PH3.
IMAXA	= Z(34)	IMAX + 1. Used in SETUP and REZONE.
INTER	= Z(87)	INPUT parameter. If INTER $\neq$ 0, EDIT will print after CDT, PH1 and PH3. If INTER = 99, in addition to extra EDIT prints, stresses are printed in PH3. (LOTS of printing.) If INTER = 7, energy totals are printed in PH2 in addition to the extra EDIT prints. Used in MAIN, EDIT, PH1 and Ph2 and PH3.
INTMA	Local	Used in MAP. <del>z</del>
IP	Local	Used in EDIT. The column a tracer point is in.
IPCYCL	= Z(49)	INPUT parameter. Used in EDIT. The number of cycles between EDIT prints when printing on cycles rather than time.
IPRT	Local	Used in REZONE. Number of columns in projectile after rezoning.

ISPHMX	Local	Used in SETUP. I-index of right-most column which contains sphere material.
ITPL	Local	Used in REZONE for adding tracer-points in added cells.
ITRT	Local <sup>(C)</sup>	Used in REZONE. Number of columns in target after rezoning.
IVARDX	= Z(83)	Used in SETUP. Flag for variable radial dimension of cells.
IVARDY	= Z(54)	Used in SETUP. Flag for variable axial dimension of cells.
IWS	Local <sup>(C)</sup>	Used as local index in INPUT, SETUP, CDT, EDIT, PH2 and PH3.
IX	Local	Used as index in PH2 for tracer-point movement.
IY	Local	Used as index in PH2 for tracer-point movement.
I1	= Z(47)	INPUT parameter. I1 is used to limit calculation in radial direction to "active mesh." Beyond I1 nothing is yet disturbed from initial conditions. I1 is specified initially as (2 + the column-number of the last column in which there is a non-zero velocity or internal energy). However, I1 is never larger than IMAX. I1 is increased automatically as inactive cells become active. If IMAX = 1, then I1 = 1. Used in CDT, EDIT, REZONE, PH1, PH2 and PH3.
I2	= Z(48)	INPUT parameter. Like I1 but for axial-disturbance-limit. I2 is specified initially as (2 + the number of the upper-most row in which there is a non-zero velocity or internal energy). I2 is increased automatically as inactive cells become active. However, I2 is never larger than JMAX. Used in SETUP, CDT, EDIT, REZONE, PH1, PH2, PH3.
I3	Local <sup>(C)</sup>	Used in EDIT as a flag for "short" or "long" prints.
J	Local <sup>(C)</sup>	Used as row-index in most subroutines.

JA	Local	Used in SETUP to calculate J-index of top of sphere.
JB	Local	Used in SETUP to calculate J-index of bottom of sphere.
JCELL	Local	Used in REZONE when placing tracer points in added cells.
JCENTR	Local	Used in SETUP. J-index of row just below center of sphere.
JDL	Local	Used in MAP. Number of rows in maps. On cycle 0, JDL = JMAX; otherwise, JDL = I2.
JFILA	Local	Used in REZONE. The J-index of the row immediately below the target.
JFILB	Local	Used in REZONE. The J-index of the row immediately above the projectile.
JFLAG	Local	Used in PH3. Used in connection with JFM for deciding where to stop calculating stresses.
JINTL	Local	Used in CDT in defining JPM array.
JJ	= Z(79)	Used in REZONE, EDIT and SETUP. Number of tracer points in each column.
JK	Local <sup>(c)</sup>	Used in EDIT. Used to identify which row a tracer point originated in. Equivalenced to PR(6).
JMAX	= Z(35)	INPUT parameter. Number of rows in mesh. JMAX must be an even number if grid is to be rezoned. Used in SETUP, CDT, EDIT, REZONE, PH1, PH2, PH3.
JMAXA	= Z(36)	JMAX + 1. Used in SETUP and REZONE.
JMPL	Local	Used in REZONE. Limit on do-loop, = JMAX/2 + 1.
JP	Local	Used as an index in CDT. Used in EDIT. The row a tracer point is in.
JPA	Local	Used in REZONE. The J-index of the top row of projectile.
JPB	Local	Used in REZONE. The J-index of the bottom row of projectile.

JFM	Global	Calculated in CDT; used in PH3. Initialized, adjusted and saved on tape in SETUP, INPUT, EDIT and REZONE. JFM(I) is J-index of cell with local maximum pressure in column I.
JPROJ	= Z(147)	INPUT parameter. Usually the J-index of top cell in projectile. Used in SETUP and EDIT. Adjusted in REZONE. The zero point in the crater depth calculation. A division for printout of total energies, mass and momenta.
JRADA	Local	Used in SETUP. The J-index of the top cell on the axis containing a part of the sphere.
JRADB	Local	Used in SETUP. The J-index of the bottom cell on the axis containing a part of the sphere.
JSPHBT	Local	Used in SETUP as index in placing sphere.
JSPHTP	Local	Used in SETUP as index in placing sphere.
JSTR	= Z(25)	INPUT parameter. When active-grid gets to JSTR in J direction, stress calculations begin and negative pressures are permitted. JSTR needs to be large enough so that a shock can become well established before stress calculations begin and negative pressures are allowed. Otherwise, meaningless perturbations are calculated in material which is still at rest. Used in PH3, CDT and REZONE.
JJA	Local	Used in REZONE as index.
JJB	Local	Used in REZONE as index.
JJPB	Local	Used in REZONE. Index for "weeding out" and adding tracer points.
JJPT	Local	Used in REZONE. See JJPB.
K	Local <sup>(c)</sup>	Used as cell-index in all subroutines.
KA	Local <sup>(c)</sup>	Used as index in CDT and PH2.
KB	Local <sup>(c)</sup>	Used as index in CDT.

KK	Local	Used as index in EDIT to remove tracer points from empty cells.
KMAX	= Z(37)	Calculated in SETUP (IMAX*JMAX+1). Used in PH3, SETUP, EDIT, REZONE. Largest value of K (cell-index).
KMAXA	= Z(38)	Calculated in SETUP (KMAX+1). Used in INPUT, SETUP, EDIT and REZONE.
KSPACE	Local	Used in EDIT for spacing printed output.
L	Local	Used as index in EDIT, INPUT, PH2, PH3, REZONE.
LA	Local	Used as index in PH2.
LB	Local	Used as index in PH2.
LJD	Local	Used as index in PH2 and PH3.
LL	Local <sup>(c)</sup>	Used as index in PH1, PH2 and PH3.
LOCA	Local	Used in EDIT and PH3 in assigned GO TO statements.
LOCB	Local	Used in EDIT in assigned GO TO statements.
M	Local	Used as index in SETUP, EDIT, PH2, REZONE, PH3, ERROR.
MA	Local	Used in MAP to specify symbol to be printed for each cell.
MASS	Local	Used in PH2 for temporary storage of the mass of a cell.
MAXEXP	Local	Used in MAP to define logarithmic scale factor for each map.
MB	= Z(94)	Used and calculated in SETUP. The J-index of the bottom row of projectile.
MC	= Z(91)	Used and calculated in SETUP. The J-index of the top row of projectile.
MD	Local <sup>(c)</sup>	Used in SETUP. Flag indicating whether or not there is a target.

ME	Local <sup>(C)</sup>	Used and calculated in SETUP. The number of columns in the target. (If target extends beyond mesh, ME = IMAX.)
MINEXP	Local	Used in MAP to define logarithmic scale factor for each map.
MR	= Z(92)	Used and calculated in SETUP. The number of columns in the projectile.
MSLAVE	Local	Used in PH2 as storage for slaved-cell index when transporting mass across top edge of cell.
MZ	= Z(93)	Used and calculated in SETUP. The J-index of the bottom row of the target.
MZT	Global	Defined in INPUT (MZT = 150). Used in SETUP and EDIT. The number of Z-block words.
N	Local	Used as an index in PH3, PH1, PH2, REZONE and EDIT. In SETUP, N is the J-index of the top row of the target.
N3	= Z(53)	Defined in SETUP. Used in SETUP, EDIT, INPUT in reading and writing tapes. = 0 if there are no tracer points; = 1 if tracer points are used.
N6	= Z(56)	INPUT parameter. Used in ES. Negative pressures are allowed in cells above J = N6 after active-J reaches JSTR value. The value of N6 is reset in REZONE. N6 = 0 allows negative pressures everywhere. On the other hand, to make sure that negative pressures are always set to zero give N6 a very large value (many times as large as JMAX) since in REZONE N6 is cut in half in order to keep it at the same distance (in cm.) from the bottom of the grid.
N10	Global	Used in CDT to identify I-index of cell which controls DT.
N11	Global	Used in CDT to identify J-index of cell which controls DT.



NC	= Z(30)	Cycle number. Set initially to -1 in INPUT. Incremented thereafter in CDT.
NDUMP7	= Z(6)	INPUT parameter. Used in EDIT to control frequency of tape dumps. A tape dump will occur every (NDUMP7) EDIT prints.
NECYCL	= Z(77)	Defined and printed in EDIT. The cycle number associated with the largest relative error in the energy sum.
NERR	Global	Used in ERROR as exit flag. Prevents ERROR from being called more than once during a single run.
NFRELP	= Z(5)	INPUT parameter. Used in EDIT to control frequency of "long" prints. A "long" print will occur every (NFRELP) "short" prints.
NIMAX	Local	Used in REZONE as storage for $IMAX/2$ when $IMAX > 1$ . $NIMAX = 1$ when $IMAX = 1$ .
NIMAX1	Local	Used in REZONE as storage for $NIMAX + 1$ .
NJMAX	Local	Used in REZONE as storage for $JMAX/2$ .
NJMAX1	Local	Used in REZONE as storage for $NJMAX + 1$ .
NK	Global	Used in PH2, PH3, EDIT, INPUT, CDT, REZONE and ERROR. Tells which statement of a subroutine caused ERROR to be called.
NKA	Local	Used in PH3 as index.
NKB	Local	Used in PH3 as index.
NMP	= Z(80)	Number of tracer points in use. Used in INPUT, SETUP, REZONE, EDIT and PH2. Initially calculated in SETUP; recalculated in REZONE.
NMPMAX	= Z(85)	INPUT parameter. Maximum number of tracer points to be generated. If fewer points are needed, NMP will have the number actually generated. NMPMAX must not be larger than the number allowed in dimensions of XP and YP. Used in SETUP and REZONE.

NN	Local	Used as index in PH3 and PH2.
NODUMP	= Z(96)	INPUT parameter. Used in EDIT. When NODUMP = 1, no tape dumps are made except on cycle 0. Allows user to restart a problem without writing on the restart tape.
NPLACE	Local	Used in REZONE for lining up added tracer points with original ones.
NPRINT	Global	Used in MAIN, CDT and EDIT. Prevents DT and PRTIME from being altered on intermediate prints. Also, NPRINT = 1 flags EDIT to print and check energy discrepancy.
NR	Global	Used in PH2, EDIT, SETUP and CDT to identify which subroutine called ERROR. Used in ERROR for printing error message.
NRC	= Z(32)	Used in PH1 and PH2 in advancing active grid.
NREZ	= Z(20)	Defined in SETUP. Equals maximum number of rezones allowed. Used in REZONE to line up new tracer points with those already in grid. Used in EDIT to determine the original I and J of each tracer point.
NRT	Local	Used in PH1 and PH2 in advancing active grid.
NRZ	Global	Initialized in SETUP. Equals number of rezones so far performed. Used in EDIT for printout of 1-D problems and for determining the original I and J of each tracer point.
NSLAVE	Local	Used in PH2 as storage for slaved-cell index when transporting mass across right edge of cell.
NULLE	Global	Equivalenced to RHOW in CDT and ES.
NUMREZ	= Z(12)	INPUT parameter. Initially equals number of rezones allowed in one run. Diminished by one after each rezone. Used in EDIT and REZONE.

NUMSCA	= Z(43)	INPUT parameter. Number of times the print interval is to be rescaled. Used in EDIT. See PRDELTA for further details.
NUMSP	= Z(4)	Used in EDIT to count the number of "short" prints since the last "long" print.
NUMSPF	= Z(41)	Used in EDIT to count the number of prints (short and long) since the last tape dump.
NZ	= Z(19)	Defined and used in EDIT for 1-D problems. NZ = 4**NRZ. After rezoning the grid NZ is used to scale the values printed by EDIT for the total mass, energy and momentum.
P	Global	Cell-pressure. IMAX by JMAX array. Calculated in ES. Used by PH1. The P-storage space is used for UK, VK, and RHO storage in PH3. The P-array is initialized at the beginning of PH3.
P1	Local	} Used in ES as storage for various terms in the pressure equations.
P2	Local	
P3	Local	
P4	Local	
P5	Local	
P6	Local	
P8	Local	
P9	Local	
P12	Local	
PABOVE	Local	Used in PH1 as storage for pressure at top of cell.
PBLO	Local	Used in PH1 as storage for pressure at bottom of cell.
PIDTS	Local <sup>(c)</sup>	Defined and used in PH1 as $1./(\pi*DT*DY)$ . Defined and used in PH2 as $1./(\pi*DT)$ .
PIDY	= Z(8)	Defined in INPUT: = $\pi$ . Used in REZONE, SETUP, PH1, PH2, and PH3.
PK	Global	Used in SETUP and INPUT for defining input parameters. (See Appendix A.) PK(3) used in EDIT to signal a "long" or "short" print on first cycle of a restart run.

PL            Local<sup>(c)</sup>        Used in PH1 for saving pressures on left side of cell. Used in EDIT for crater depth printout. Equivalenced in standard OIL-RFM as follows:  
                                  PL = RST (for PH3)  
                                  PL = PR = GAMC (for PH2)  
                                  PL(103) = SIGC (for PH2)

FMIN        = Z(86)        Used as a pressure cut-off. Calculated and printed in CDT as  $(C_0) \cdot (\rho_0) \cdot (U_{min})$ . Initially defined in INPUT as  $10^6$ .

PR            Local<sup>(c)</sup>        Used in INPUT and EDIT for temporary storage.

PRAMOA      Local            Printed and calculated in EDIT. The positive radial momentum above JPROJ. Equivalenced to PR(8) in EDIT only.

PRAMOB      Local            Printed and calculated in EDIT. The positive radial momentum below JPROJ. Equivalenced to PR(16) in EDIT only.

PRDELTA    = Z(45)        INPUT parameter. Gives the initial time interval between EDIT prints. There are five parameters which control printing frequency: PRDELTA, IPCYCL, PRLIM, PRACT, and NUMSCA. If the user is printing on time (PRDELTA  $\neq$  0. and IPCYCL = 0.), DT will be adjusted so that a print will occur exactly every PRDELTA seconds. If the user is printing on cycles (PRDELTA = 0., IPCYCL  $\neq$  0.), a print will occur every IPCYCL cycles. PRLIM, PRACT and NUMSCA are used to increase the print interval. PRLIM is the time (or cycle) at which PRDELTA (or IPCYCL) and PRLIM are multiplied by PRACT. The new value of PRLIM establishes the next time (or cycle) when the print interval will be rescaled. This process continues at most NUMSCA times.

EXAMPLE: You wish to print every  $1 \times 10^{-8}$  sec. until you reach  $1 \times 10^{-7}$  sec., then every  $1 \times 10^{-7}$  sec. until  $1 \times 10^{-6}$  sec. and every  $1 \times 10^{-6}$  sec. thereafter:

                 PRDELTA =  $1. \times 10^{-8}$                     PRACT = 10.  
                  PRLIM =  $1. \times 10^{-7}$                     NUMSCA = 2.

PRFACT	= Z(46)	INPUT parameter. Used in EDIT as a factor for rescaling PRDELT, IPCYCL, and PRLIM when PRLIM-time or cycle is reached. (See PRDELT.) Should be > 1.
PRLIM	= Z(44)	INPUT parameter: time or cycle at which to rescale PRDELT (or IPCYCL) and PRLIM by PRFACT. (See PRDELT.)
PRMAS	Local <sup>(C)</sup>	Used and calculated in EDIT. Total mass below JPROJ. Equivalenced to PR(12) in EDIT only.
PRMV	Local <sup>(C)</sup>	Used and calculated in EDIT. Total axial momentum below JPROJ. Equivalenced to PR(12) in EDIT only.
PRMVP	Local <sup>(C)</sup>	Used and calculated in EDIT. Total positive axial momentum below JPROJ. Equivalenced to PR(14) in EDIT only.
PROB	= Z(1)	INPUT parameter. Identifying problem number. Used in EDIT and INPUT.
FROJI	= Z(16)	INPUT parameter. Initial specific internal energy of projectile. Used in SETUP and REZONE.
PROJU	= Z(73)	INPUT parameter. Initial radial velocity of projectile. (Usually = 0) Used in SETUP and REZONE.
PROPI	Local	Calculated and used in EDIT. For 1-D problems the totals for energy, mass, momentum per unit area are printed. (i.e., they are divided by 4** (Number of rezones)) and stored in PROPI for printing.
PRR	Local	Used in PH1 as temporary storage of pressure and pressure averages.
PRTIME	= Z(131)	Initially set to PRDELT in INPUT. Thereafter calculated in EDIT. When T = PRTIME, it is time to print.
PRXRT	= Z(69)	INPUT parameter. The outer radius of projectile (in cms.). PRXRT must be at a cell-boundary. Used in SETUP and REZONE.
PRYBOT	= Z(67)	INPUT parameter. Y-value of bottom of projectile (in cms.). PRYBOT should be at a cell-boundary. If no "projectile" is to be generated, PRYBOT should be set to -1. Used in SETUP and REZONE.

PSCLE	Local	Used in MAP as a logarithmic scale factor for the pressure maps.
PTEMP	Local	Used in CDT when calculating JPM array (the maximum pressure location in each column).
PW	Local	Used in PH3 to calculate plastic work when INTER = 99.
RADIUS	= PK(12) = Z(162)	INPUT parameter. Radius of sphere (in cms.). The radius need not be a multiple of DX. Used in SETUP. Equivalenced to PK(12) in SETUP.
RAMOYA	Local	Printed and calculated in EDIT. Total radial momentum above JPROJ. Equivalenced to PR(7) in EDIT only.
RATIO	Local	Used in CDT in calculation of DT. Ratio of $(DX, DY)_{min}$ to $(U, V, \text{local sound speed})_{max}$ .
RC	Local	Used and calculated in PH1 as distance from axis to center of a cell.
RELERR	Local	Used in EDIT for storing and printing maximum relative error in the energy sum.
REZ	= Z(95)	Flag defined in PH2 and used in EDIT. Signals when the REZONE subroutine should be called. (The rezone flag is turned on when material begins to flow out through transmissive boundaries. In REZONE each set of four cells in the mesh is made into one cell. The new mass is the sum of masses in the four original cells. Momentum and total energy are conserved but in so doing some kinetic energy is changed to internal. (The result is that rezoning has a stabilizing influence.) When all permitted rezones have been done, material is allowed to flow out through transmissive boundaries and the mass and energy are lost from the system.
REZFCT	= Z(71)	INPUT flag for rezoning. If = 1., the grid is rezoned (NUMREZ) times. If = 0., no rezoning is done. Tested in PH2 and EDIT.

RHINI	= Z(111)	INPUT parameter. Initial density of projectile. Used in SETUP and REZONE. In PH2 it is used to determine whether material should be evaporated. (See EVAP)
RHINIT	= Z(15)	INPUT parameter. Initial density of target. Used in SETUP and REZONE.
RHO	Local <sup>(c)</sup>	Used in PH3 for temporary storage of cell density.
RHOFIL	= Z(51)	INPUT parameter. Initial density of filler material between the projectile and target. Used in SETUP and REZONE.
RHC*	= Z(138)	INPUT parameter. Cells with $\rho < \text{RHOMIN}$ are by-passed in calculation of DT.
RHOOUT	= Z(103)	INPUT parameter. Used in SETUP. In cells containing sphere boundary RHOOUT is the density of material outside sphere. Equivalenced to Z(103) and EVAPMV in SETUP.
RHOSPH	= Z(100)	INPUT parameter. Used in SETUP as the initial density of sphere. Equivalenced to Z(100) and EVAFM in SETUP.
RHOW	Global	Density of cell. Calculated in CDT, used in ES. Equivalenced to NULLE in CDT and ES.
RHOZ	= Z(115)	INPUT parameter. Normal density. Used in INPUT, CDT, ES, EDIT, PH2 and PH3.
ROEPS	= Z(110)	INPUT parameter. Round-off epsilon used in calculating cutoffs. Used in CDT to calculate UMIN. $\text{UMIN} = (\text{ROEPS})( \text{maximum } u \text{ or } v )$ Used in SETUP, EDIT and PH2.
RR	Local	Used and calculated in PH1. Distance (cms.) from axis to center of cell on the right.
RTM	= Z(57)	Calculated in PH2. Printed in EDIT. Total mass lost out right side of grid.

RTMU	= Z(10)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out right side of grid.
RTMV	= Z(58)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out right side of grid.
SAVEK	Local	Used and calculated in PH2. Factor used in calculation of energy fluxes across right and top boundaries of cells on reflective boundaries.
SIMIN	Global	Used in MAP, PH2. Calculated in CDT. SIE cut-off value = $(UMIN)^2$ .
SIENEW	Local	Used and calculated in PH2. New value of specific internal energy.
SIESPH	= Z(101)	INPUT parameter. Initial value of specific internal energy of sphere. Equivalenced to Z(101) and EVAPEN in SETUP.
SIGC	Local <sup>(c)</sup>	Used in PH2 for energy carried by mass moving across left side of cell. Equivalenced to PL(103). (See Appendix B.)
SIGMU	Local	Used in PH2 for radial momentum moving across cell-boundaries.
SIGMV	Local	Used in PH2 for axial momentum moving across cell-boundaries.
SN	= Z(65)	INPUT flag: When = 0. negative internal energy is to be set to 0. When = 1. negative internal energy is to be left alone. Used in PH1 and PH2.
SNB	Local <sup>(c)</sup>	Used in PH3 for normal stress at bottom of a cell. Equivalenced to P(313).
SNL	= Z(105)	Used in PH3 for normal stress at left of a cell.
SNLX	Local	Used in PH3. = SNL * X(I-1).
SNR	Local <sup>(c)</sup>	Used in PH3 for normal stress at right of a cell. (=S <sub>11</sub> at right.)
SNT	Local <sup>(c)</sup>	Used in PH3 for normal stress at top of a cell. (= S <sub>22</sub> at top.)



SOLID	Global	Calculated in INPUT as (RHOZ * AMDM). Used in PH2, PH3 and CDT.
SRATIO	Local	Used in CDT to calculate DT. The smallest ratio of minimum cell dimension to maximum velocity.
SS1	= Z(127)	Calculated in INPUT. Used in ES: = 1./ (ESESP-ESES).
SS2	= Z(128)	INPUT parameter controlling reflective (and axis) boundary treatment. Usually = 1. Used in PH2.
SS4	= Z(130)	INPUT parameter. If SS4 ≠ 0., REZONE is called on second cycle of run. Used in EDIT.
STAB	= Z(139)	INPUT parameter. Used in CDT. Initial value of "stability fraction" for the calculation of DT. If FINAL = 0., STAB is constant. Otherwise its value progresses from STAB to FINAL in a geometric progression.
STB	Local <sup>(C)</sup>	Used in PHj for shear stress at bottom of cell. Equivalenced to P(365).
STEZ	= Z(29)	INPUT parameter: E <sub>0</sub> . Used in yield-strength calculation in PH3. See STRENG.
STK1	= Z(11)	INPUT parameter: Y <sub>1</sub> . Used in yield-strength calculation in PH3. See STRENG.
STK2	= Z(28)	INPUT parameter: Y <sub>2</sub> . Used in yield-strength calculation in PH3. See STRENG.
STL	= Z(106)	Used in PH3 for shear stress at left of cell.
STLX	Local	Used in PH3. = STL * X(I-1).
STR	Local <sup>(C)</sup>	Used in PH3 for shear stress at right of cell.
STRENG	Local	Calculated and used in PH3: yield strength of material. (Y <sub>0</sub> , Y <sub>1</sub> , Y <sub>2</sub> supplied by user.)

$$\text{STRENG} = (Y_0 + Y_1 \mu + Y_2 \mu^2) \cdot (1 - \frac{E}{E_0})$$

If STRENG < 0., stresses are set to 0.

If  $E > E_0$ , STRENG = 0.

$Y_0$  is ZZERO,

$Y_1$  is STK1,

$Y_2$  is STK2,

$\rho_0$  is RHOZ,

E is AIX of cell,

$E_0$  is STEZ,

$\rho$  is density of cell,

$\mu = \rho/\rho_0 - 1.$

STT	= Z(143)	Used in PH3 for shear stress at top of cell.
SUM	Local <sup>(C)</sup>	Used in PH2. Sums negative internal energy when negative internal energy is set to zero.
SUME	Local	Used in PH2. Sums energy changes.
SUM1	Local	Used in SETUP to define JRADA.
SUM2	Local	Used in SETUP to define JRADB.
T	= Z(84)	Time in seconds. Initially defined in INPUT. Incremented in CDT. Adjusted in EDIT for printing. Printed by CDT, EDIT, REZONE.
TARGI	= Z(72)	INPUT parameter. Initial value of specific internal energy of target. Used in SETUP and REZONE.
TARGV	= Z(52)	INPUT parameter. Initial value of axial-velocity of target. Used in SETUP and REZONE.
TARMAS	Local <sup>(C)</sup>	Used in EDIT. Total mass above JPROJ. Equivalenced to PR(4) in EDIT only.
TARMV	Local <sup>(C)</sup>	Used in EDIT. Total axial momentum above JPROJ. Equivalenced to PR(5) in EDIT only.
TARMVP	Local <sup>(C)</sup>	Used in EDIT. Total positive axial momentum above JPROJ. Equivalenced to PR(6) in EDIT only.
TAU	Global	Calculated in SETUP and REZONE. Area of cell face: $= \pi(X(I)^2 - X(I-1)^2)$ . Used in most subroutines.

TAUDTS	Local	Used and calculated in PH1: = TAU*DT.
TAXRT	= Z(107)	INPUT parameter. Outer radius of target (in cms.). TAXRT should be at a cell-boundary. Used in SETUP and REZONE.
TAYBOT	= Z(88)	INPUT parameter. Axial location of bottom of target (in cms). TAYBOT should be at a cell-boundary. If no "target," TAYBOT = -1. Used in SETUP and REZONE.
TAYTOP	= Z(89)	INPUT parameter. Axial location of top of target (in cms). TAYTOP should be at a cell-boundary. Used in SETUP and REZONE.
TEPRO	Local <sup>(c)</sup>	Used in EDIT. Total energy below JPROJ. Equivalenced to PR(11) in EDIT only.
TESTRH	Global	Calculated in INPUT: = (.2)*RHOZ. Used in CDT in defining pressure scale factor.
TETAR	Local <sup>(c)</sup>	Used in EDIT. Total energy above JPROJ. Equivalenced to PR(3) in EDIT only.
THO3	Local	Used and calculated in PH3: = $\frac{1}{3} \left( \frac{\partial u}{\partial r} + \frac{\partial r}{\partial z} + \frac{u}{r} \right)$ .
TIEPRO	Local <sup>(c)</sup>	Used in EDIT. Total internal energy below JPROJ. Equivalenced to PR(9) in EDIT only.
TIETAR	Local <sup>(c)</sup>	Used in EDIT. Total internal energy above JPROJ. Equivalenced to PR(1) in EDIT only.
TKEPRO	Local <sup>(c)</sup>	Used in EDIT. Total kinetic energy below JPROJ. Equivalenced to PR(10) in EDIT only.
TKETAR	Local <sup>(c)</sup>	Used in EDIT. Total kinetic energy above JPROJ. Equivalenced to PR(2) in EDIT only.
TMA	Local	Used in MAP to associate a given density with the printed symbol.
TNOW	Local	Used in EDIT: = time now; saved when EDIT calls CDT after calling REZONE.
TOFM	= Z(63)	Calculated in PH2. Printed in EDIT. Total mass lost out top of grid.

TOPMU	= Z(9)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out top of grid.
TOPMV	= Z(66)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out top of grid.
TOTSPH	Local	Used in SETUP. Total volume of sphere.
TRIAL	Local	Used in CDF. Maximum sound-speed or velocity used to define DT.
TRNSFC	= Z(145)	Defined in INPUT: = .4. Used in PH2 to define maximum transport velocity. (See UVMAX.)
TSTOP	= Z(50)	INPUT parameter. Value of T at which execution stops when stopping on time rather than cycles.
TWOPDT	Local	Calculated and used in PH2: = $2*\pi*DT$ .
TWOPI	Global	Calculated in INPUT. Used in PH3: = $2\pi$ .
U	Global	Radial velocity of cell. (IMAX by JMAX array.)
UAMP	Local	Used in PH2 for U of mass moving across right cell-edge.
UAMPY	Local	Used in PH2 for U of mass moving across top cell-edge.
UBAR	Local	Used in PH3 in calculating energy sum.
USEF	Local	Used in PH2 to move tracer-points.
UK	Local <sup>(C)</sup>	Used in PH3. Temporary storage for part of U array.
UKT	Local	Used in PH3. Temporary storage for U(K).
UL	Local <sup>(C)</sup>	Used in PH1 for U on left. Used in EDIT for crater depth printout. Equivalenced as follows in standard OIL-RPM: UL(103) = CRAD (for EDIT) UL = RSN (for PH3) UL = FLEFT (for PH2) UL(103) = YAMC (for PH2)
UMIN	= Z(129)	Calculated in CDF. Used as velocity cutoff in PH2, PH3, and MAP: = (ROEPS)*(maximum sound-speed or velocity).

UMK	Local	Calculated and used in PH2. Temporary storage for $U(K)*AMX(K)$ .
UMKP	Local	Calculated and used in PH2. Temporary storage for $U(K+1)*AMX(K+1)$ .
UMOM	Local	Calculated and used in PH2: = $MASS*U(K)$ .
UNxxx	= Z(xxx)	Unused Z-storage.
UNEW	Local	Calculated and used in PH2. New value of U.
UOTK	Local	Calculated and used in PH2: = $UMK/TAU(I)$ .
UOTKP	Local	Calculated and used in PH2: = $UMKP/TAU(I+1)$ .
UOX	Local	Used in PH3: = $U/X$ .
URR	Local <sup>(C)</sup>	Used in PH <sub>1</sub> and PH2. Temporary storage for velocity and velocity averages.
USCLE	Local	Used in MAP as logarithmic scale factor of radial velocity map.
UVMAX	= Z(22)	Used and calculated in PH2. Maximum transport velocity. In radial direction $UVMAX = TRNSFC*DX(I)/DT$ . In axial direction $UVMAX = TRNSFC*DY(J)/DT$ .
V	Global	Axial velocity of cell. (IMAX by JMAX array.)
VABOVE	Local	Used in PH1 and PH2 as storage for velocity at top of cell.
VALUE	Local	Used in MAP in printing maximum value of each map symbol.
VAMMP	Local	Used in PH2 for axial velocity of mass moving across right cell-edge.
VAMPY	Local	Used in PH2 for axial velocity of mass moving across top cell-edge.
VBAR	Local	Used in PH3 in calculating energy sum.
VBLO	Local	Used in PH1 as storage for velocity at bottom of cell.
VEFF	Local	Used in PH2 to move tracer points.

VEL	Local	Used in PH1 as subcycle flag.
VFACT	Local	Used in PH3 in setting boundary conditions.
VINI	= Z(112)	INPUT parameter. Initial axial velocity of projectile. Used in SETUP and REZONE.
VINSPH	= Z(102)	INPUT parameter. Initial axial velocity of sphere. Used in SETUP. Equivalenced to Z(102) and EVAPMU in SETUP.
VK	Local <sup>(c)</sup>	Used in PH3. Temporary storage for part of V array.
VKT	Local	Used in PH3. Temporary storage for V(K).
VMK	Local	Calculated and used in PH2: = V(K)*AMX(K).
VML	Local	Calculated and used in PH2: = V(K+IMAX)*AMX(K+IMAX).
VNEW	Local	Calculated and used in PH2. New value of V.
VOLSPH	Local	Calculated and used in SETUP. Volume of toroid generated by a cell. Used in setting up sphere.
VOX	Local	Calculated and used in ES. = (normal density)/(density of cell).
VSCLE	Local	Used in MAP as logarithmic scale factor for axial velocity map.
VT	= Z(55)	INPUT parameter. Used in PH2 as minimum mass flux (across top or right side of one boundary cell in one cycle) needed to trigger a rezone. Usually $VT \sim \rho_0 \times 10^{-4}$ .
WDYF	Local	Used in PH2 as temporary storage for DY(J) or DY(J+1).
WFLAGF	Global	Used in INPUT and EDIT. Flags first cycle. Set = 1. in INPUT. Set = 0. in EDIT.
WFLAGL	Global	Used in MAIN and EDIT. Flags last cycle. Set = 1. in EDIT.
WFLAGP	Local <sup>(c)</sup>	Used in EDIT. Flags beginning of printout of properties for each cell in a given column.

WS	Local <sup>(C)</sup>	Used in most subroutines for local working storage.
WSA	Local <sup>(C)</sup>	Used in most subroutines for local working storage.
WSB	Local <sup>(C)</sup>	Used in most subroutines for local working storage.
WSC	Local <sup>(C)</sup>	Used in most subroutines for local working storage.
WSD	Local	Used in PH2 local working storage.
WSMAX	Local	Used in MAP to define scale factors.
WSMIN	Local	Used in MAP to define scale factors.
WSOUT	Local	Used in PH2 for adjusting over-emptied cells.
WT	Local	Used in CDT for local working storage.
WTA	Local	See WT.
WTB	Local	See WT.
X	Global	Distance (cms) from axis to outside of cell. Equivalenced to XX array such that $X(0) = XX(1)$ .
XIENRG	= Z(140)	Total internal energy. Calculated in EDIT and used for printing labels on tracer point plots.
XKENRG	= Z(141)	Total kinetic energy. Calculated in EDIT and used for printing labels on tracer point plots.
XL2	Local	Calculated and used in SETUP for placing sphere: $= (X(1-1))^2$ .
XMAX	= Z(18)	Calculated in SETUP: $= X(IMAX)$ .
XP	Global	Tracer-point x-coordinates. Used in INPUT, SETUP, EDIT, PH2 and REZONE.
XR2	Local	Calculated and used in SETUP for placing sphere: $= (X(1))^2$ .
XTENRG	= Z(142)	Total energy. Calculated in EDIT and used for printing labels on tracer point plots.
XUM	Constants	Used in MAP. Has negative alphabetic characters for maps. Defined in DATA statement.

XX	Global	Equivalenced to X array so as to make X(0) available.
Y	Global	Distance (cms) from bottom of grid to top of cell. Equivalenced to YY array such that Y(0) = YY(1).
Y2	= Z(81)	INPUT tracer point flag: when = -2, tracer points are calculated; when = 0, tracer points not calculated.
YAMC	Local <sup>(c)</sup>	Calculated and used in PH2. Axial momentum of mass moving across 1 ft side of cell. Equivalenced to UL(103). (See Appendix B)
YBOTM	Local	Calculated and used in SETUP in placing sphere: = Y(J-1).
YC2	Local	Calculated and used in SETUP in placing sphere: = (YCENTR) <sup>2</sup> .
YCENTR	= PK(13) = Z(163)	INPUT parameter. Distance (cms) of center of sphere from bottom of grid. YCENTR must be at a cell-boundary. Used in SETUP. Equivalenced to PK(13) in SETUP only.
YDIFFB	Local	Calculated and used in SETUP in placing sphere.
YDIFFI	Local	Calculated and used in SETUP in placing sphere.
YDIFFO	Local	Calculated and used in SETUP in placing sphere.
YDIFFT	Local	Calculated and used in SETUP in placing sphere.
YLINTA	Local	Calculated and used in SETUP in placing sphere.
YLINTB	Local	Calculated and used in SETUP in placing sphere.
YLOWER	Local	Calculated and used in SETUP in placing sphere.
YMAX	Local	Calculated in SETUP: = Y(JMAX).
YP	Global	Tracer-point y-coordinates. Used in INPUT, SETUP, EDIT, PH2 and REZONE.
YRINTA	Local	Calculated and used in SETUP in placing sphere.
YRINTB	Local	Calculated and used in SETUP in placing sphere.
YTOP	Local	Calculated and used in SETUP in placing sphere.



YUPPER	Local	Calculated and used in SETUP in placing sphere.
YY	Global	Equivalenced to Y array so as to make Y(0) available.
Z	Special Global	Storage for most of the input parameters. The Z-array (150 words) is written on tape for restarts. Used in INPUT, MAIN, and SETUP. (See Appendix A)

APPENDIX A  
Z-STORAGE LISTED NUMERICALLY

See Dictionary for meaning and use.

*1. PROB	30. NC	59. UN59
2. CYCLE	31. UN31	60. N10
3. DT	32. NRC	61. N11
4. NUMSP	2*33. IMAX	62. GAMMA
2*5. NFRELP	34. IMAXA	63. TOFM
2*6. NDUMP7	2*35. JMAX	64. ROTMU
2*7. ICSTOP	36. JMAXA	*65. SN
8. PIDY	37. KMAX	66. TOPMV
9. TOPMU	38. KMAXA	*67. PRYBOT
10. RTMU	39. BOTM	*68. PRYTOP
*11. STKL	40. BOTMV	*69. PRXRT
2*12. NUMREZ	41. NUMSPT	*70. CYCPH3
13. ETH	*42. CZERO	*71. REZFCT
14. UN14	2*43. NUMSCA	*72. TARGI
*15. RHINIT	*44. PRLIM	*73. PROJU
*16. PROJI	*45. REDELT	74. BBOUND
17. UN17	*46. PRFACT	*75. EVAP
18. XMAX	2*47. I1	76. ECK
19. NZ	2*48. I2	77. NECYCL
20. NREZ	2*49. IPCYCL	78. II
*21. AMDM	1*R 50. TSTOP	79. UJ
22. UVMAX	*51. RHOFIL	80. NMP
23. UN23	*52. TARGV	*81. Y2
*24. DMIN	53. N3	82. EZPH1
2*25. JSTR	2*54. IVARDY	2*83. IVARDX
26. DTNA	55. VT	84. T
*27. CVIS	2*56. N6	2*85. NMPMAX
*28. STK2	57. RTM	86. FMIN
*29. STEZ	58. PTMV	2*87. INTER

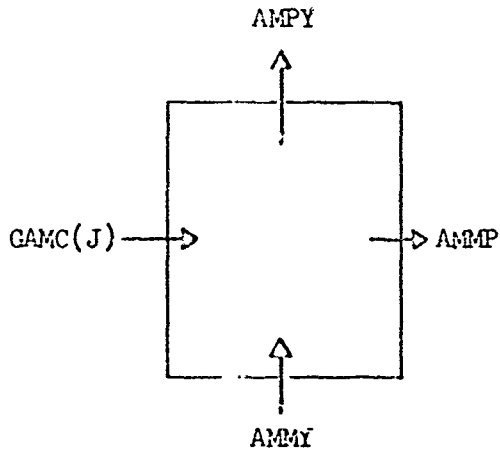
\* User-supplied input-values.  
2\* Must have a "2" in column 1.

1\* Must have a "1" in column 1.  
R Must be included in a restart input  
input deck.

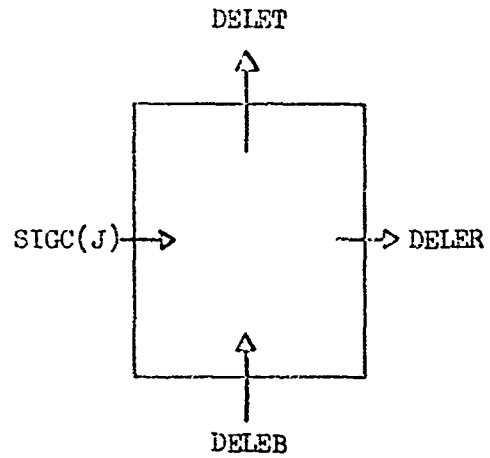
*88. TAYBOT	*122. ESES	*R153. PK(3): When = -1., program will restart from tape and do a "long" EDIT print of the pickup cycle.
*89. TAYTOP	*123. ESALPH	When = -2., program will restart from tape and do a "short" EDIT print of the pickup cycle.
90. IEMAP	*124. ESBETA	
91. MC	*125. ESCAPB	
92. MR	126. IUMAP	
93. MZ	127. SS1	
94. MB	128. SS2	
95. REZ	129. UMIN	*162. Radius of sphere (RADIUS).
2*96. NODUMP	*130. SS4	*163. Y-center of sphere (YCENTR).
97. UN97	131. PRTIME	1*164. When Z(164) > 0. CARDS will be called by SETUP to read "special" input. (See "OIL- RPM Input for Special Setup" on page 23.)
98. UN98	132. EOR	
99. UN99	133. EOT	
*100. EVAFM(RHOSPH)	134. EOB	
*101. EVAPEN(SIESPH)	135. EMOR	
*102. EVAPMU(VINSPH)	*136. DXF	
*103. EVAPMV(RHOOUT)	*137. DYF	
104. EZPH2	*138. RHOMIN	
105. SNL	*139. STAB	
106. STL	140. XIENRG	
*107. TAJRT	141. XKENRG	
108. IDNMAP	142. XTENRG	
109. IPRMAP	143. SPT	
*110. ROEPS	*144. DTMIN	
*111. RHINI	145. TRNSFC	
*112. VINI	146. EMOT	
*113. FINAL	2*147. JPROJ	
114. IVMAP	148. CNAUT	
*115. RHOZ	*149. BBAR	
*116. ESA	1*150. EMOB = 0 (Last card of input unless restarting from tape.)	
*117. ESEZ	PK array follows the Z array in Blank Common; so PK(1) from the beginning of Blank Common is equivalent to Z(151).	
*118. ESB		
*119. ESCAPA	1*151. FK(1) should be the same as PROB.	
*120. ESESP	*152. Cycle to restart on.	
*121. ESESQ		

APPENDIX B  
 VARIABLES USED FOR FLUXES ACROSS CELL BOUNDARIES

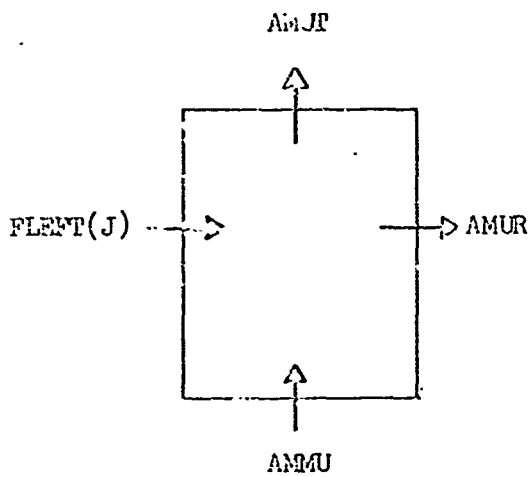
Mass



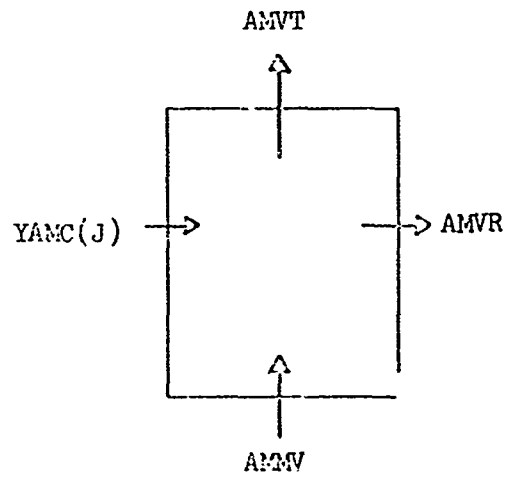
Energy



Radial Momentum



Axial Momentum



#### REFERENCES

1. Evans, M.W. and F.H. Harlow, "The Particle-in-Cell Method for Hydrodynamics Calculations," Los Alamos Scientific Laboratory Report LA-2139, November 1957.
2. Johnson, W.E., "Computer Development to Improve SHELL Code," General Atomic Report GA-4673, Contract AF29(601)-6028, October 1963.
3. Johnson, W.E., "OIL, A Continuous Two-Dimensional Eulerian Hydrodynamic Code," General Atomic Report GAMD-5580, October 1964.
4. Tillotson, J.H., "Metallic Equations of State for Hypervelocity Impact," General Atomic Report GA-3216, July 1962.
5. Dienes, J.K., W.E. Johnson and J.M. Walsh, "Annual Status Report on the Theory of Hypervelocity Impact," General Atomic Report GA-6509, June 1965.
6. Allen, R.T., "Equation of State of Rocks and Minerals," General Atomic Report GAMD-7834, March 1967.
7. Walsh, J.M., J.H. Tillotson and W.E. Johnson, "Theory of Hypervelocity Impact, Quarterly Progress Report," General Atomic Report GACD-4518, July 1963.
8. Dienes, J.K. and M.W. Evans, "Cratering Calculations with a Hydrodynamic Strength Code," General Atomic Report GAMD-7369, September 1966.