USNRDL-TR-67-99 II July 1967

1 6 1 23.1

REGRESSION PARAMETERS FOR PAIRS OF EQUALLY UNCERTAIN VARIABLES

s by

677

0

J

PD

E.C. Freiling

G. R. Crocker

U.S. NAVAL RADIOLOGICAL DEFENSE LABORATORY

SAN FRANCISCO · CALIFORNIA · 94135

This document has been covered for public religions deviation is unlineard. PHYSICAL CHEMISTRY BRANCH E. C. Freiling, Head

NUCLEAR TECHNOLOGY DIVISION R. Cole, Head

ADMINISTRATIVE INFORMATION

The work reported is part of a project sponsored by the Division of Biology and Medicine of the Atomic Energy Commission under Contract AT (49.7)-1963.

DDC AVAILABILITY NOTICE

This document has been approved for public release and sale; its distribution is unlimited.

Abbassion for	/
CFSTI	WRITE STATION /
000	BUFF SECTION
UNARKOUNCED	- 1-
JUSTIFICATION	

BY GRATE BUTCH/AYAILADILITY O Dist. | Avail. 2000 C.L.L.

Eugene P. Cooper Eugene P. Cooper

Technical Director

Qe.

D.C. Campbell, CAPT USN Commanding Officer and Director

ABSTRACT

The correlation of radiochemical data from samples of fractionated nuclear debris involves the treatment of two variables whose uncertainties are comparable. We considered three new criteria for the establishment of regression parameters for such correlations (least square perpendicular distances between points and the line, bisection of the angle formed by the certain-x and certain-y regression lines, and adoption of the geometric mean of the certain-x and certain-y regression slopes). We concluded that the geometric-mean slope b was most satisfactory. It is related to the usual certain-x regression slope $b_{x,x}$ and the coefficient of correlation r by the simple expression

 $\hat{\mathbf{b}} = \mathbf{b}_{\mathbf{x},\mathbf{x}}/|\mathbf{r}|$

SUMMARY

Problem

The correlation of radiochemical data from fractionated debris does not meet the usual requirements for the application of least-squares analysis; namely, that one variable be known with much greater certainty than the other. Occasionally the mechanical application of the usual least-squares treatment produces results which appear to be specious.

Findings

Alternative treatments were developed and investigated. These are based upon criteria which are more appropriate to the situation at hand and also give results which are more reasonable: least square perpendicular distances between points and the line, bisection of the angle formed by the certain-x and certain-y regression lines, and adoption of the geometric mean of the certain-x and certain-y regression slopes. Of these, the geometric-mean slope was found to be the most satisfactory.

INTRODUCTION

In applying standard least-squares methods to the statistical analysis of relations between two variables one assumes the independent variable to be much better known than the dependent variable and then proceeds to determine a regression line by minimizing the squared deviations of the latter variable. There arise situations where this assumption is not at all fulfilled. A good example is the correlation of radiochemical data from fractionated nuclear debris, where dependent and independent variables are of nearly equal uncertainty. Here the regression slopes can be heavily influenced by uncertain data lying near the population extremities. Situations frequently arise where the calculated line differs significantly from what the eye would select, leaving the viewer with an uncomfortable feeling about the reliability of the correlation parameters. An example will be presented in a later section.

Several obvious solutions occur to this state of affairs. One is to minimize the squares of the perpendicular distances from the regression line instead of those of the vertical distances. Another is to use the geometric mean of the slopes of the lines for y on x and for x on y. Still another is to bisect the angle formed by these lines.

The purpose of this report is to develop, test, and evaluate these methods with a view to applying the results to the correlation of radiochemical data from fractionated nuclear debris.

1

日本語語のないので、「「「

A A SHARE AND

NCTATION

The notation below refers to quantities taken from standard statistical development. Additional notation will be introduced in the text.

- y_i = dependent variable
- x_i = independent variable
- n = number of data points

Figures 1 and 2 illustrate the notation and some relations between the quantities listed. A more complete set of relations is given in Table 1. Since these relations are either standard (see, for example, Ref. 1) or immediately derivable (from Figs. 1 and 2), their derivations are not belabored.

DERIVATION OF EQUATIONS

In this section equations will be derived in their most concise form. An investigator desiring to apply the equations to work completed or in progress will find these forms inconvenient. Therefore a later section will summarize the equations in practical form, i.e., in terms of the parameters most likely to be available. Specifically, these are $a_{x,y}$, $b_{x,x}$, r, and $\langle x_i \rangle$.

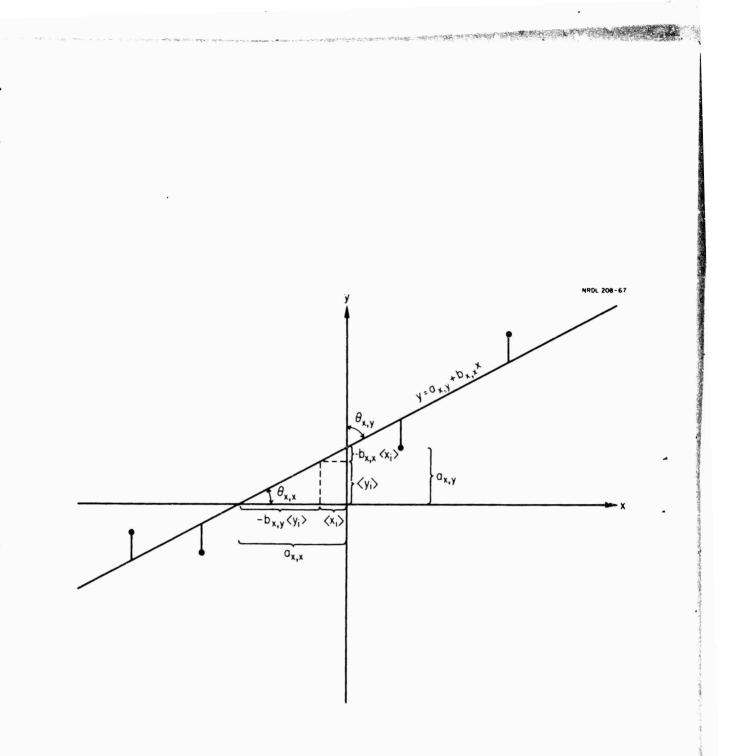


Fig. 1 Illustrated Quantities and Relations for a Regression Line Obtained by Minimizing Deviations in the y-direction.

a mean should be a start of the

•

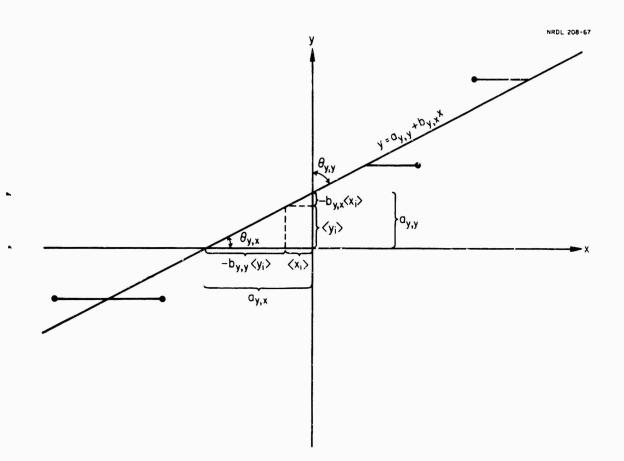


Fig. 2 Illustrated Quantities and Relations for a Regression Line Obtained by Minimizing Deviations in the x-direction.

TABLE 1

Summary	of	Basic	Relations	3
---------	----	-------	-----------	---

Quantity	8	Expressed in Terms of b	of S
^b x,x	- ⁸ x,y ⁸ x,x	$\frac{1}{b_{x,y}}$	<u>S(x,y)</u> S(x,x)
^b у,у	- ⁸ y,x ⁸ y,y	$\frac{1}{b_{y,x}}$	<u>S(x,y)</u> S(y,y)
r ²	a <mark>x,y ^ay,x</mark> ax,x ^a y,y	^b x,x ^b y,y	$\frac{[s(x,y)]^2}{s(x,x)s(y,y)}$
^e x,x	- a _{x,y} /b _{x,x}	$\langle x_i \rangle$ - $b_{x,y} \langle y_i \rangle$	$\langle x_{i} \rangle - \frac{S(x,x)}{S(x,y)} \langle y_{i} \rangle$
ау,у	- a _{y,x} /b _{y,y}	$\langle y_i \rangle$ - $b_{y,x} \langle x_i \rangle$	$\langle y_i \rangle - \frac{S(y,y)}{S(x,y)} \langle x_i \rangle$

_

.

Marcal to se section consideration of

1000 B

Geometric Mean Slope

The geometric mean slope b is given simply by

$$b^{2} = b_{x,x} b_{y,x}$$

= s(y,y)/s(x,x)

To complete the definition of this line, it is reasonable to impose the condition that it pass through the point $P_0(x_0, y_0)$ formed by the intersection of the two regression lines

 $y = a_{x,y} + b_{x,x} x$

 $y = a_{y,y} + b_{y,x} x.$

and

and

The coordinates of this point are

$$x_{0} = \frac{a_{y,y} - a_{x,y}}{b_{x,x} - b_{y,x}}$$
$$y_{0} = \frac{b_{x,x} + a_{y,y} - b_{y,x}}{b_{x,x} - b_{y,x}}$$

Hence, the intercept with the y-axis of the line with slope $\stackrel{\frown}{\rm b}$ and passing through $\rm P_{o}$ is

$$a_{y} = y_{0} - b_{x_{0}}^{A}$$

$$= \frac{a_{y,y} (b_{x,x} - b) - a_{x,y} (b_{y,x} - b)}{b_{x,x} - b_{y,x}}$$

and that with the x-axis is

$$\hat{\mathbf{a}}_{\mathbf{x}} = \mathbf{x}_{0} - \frac{1}{h} \mathbf{y}_{0}$$
$$= - \hat{\mathbf{a}}_{\mathbf{y}} / h$$

The Bisector of the Angle $\theta_{x,x} - \theta_{y,x}$

The line bisecting the angle between $\Theta_{x,x}$ and $\Theta_{y,x}$ will form the angle

$$\widetilde{\Theta} = \frac{1}{2} \left(\Theta_{\mathbf{x},\mathbf{x}} + \Theta_{\mathbf{y},\mathbf{x}} \right)$$

with the x-axis. Hence we can write

$$\tan 2\Theta = \tan \left(\Theta_{x,x} + \Theta_{y,x}\right)$$

and by familiar trigonometric relations obtain an expression for the slope \widetilde{b} of the bisector:

$$\frac{2\widetilde{b}}{1-\widetilde{b}^2} = \frac{\overset{b}{x,x} + \overset{b}{y,x}}{1-\overset{b}{x,x} \overset{b}{y,x}}$$

from which

$$\tilde{b} = \frac{b_{x,x} \ b_{y,x} \ -1}{b_{x,x} \ +b_{y,x}} + \sqrt{\left(\frac{b_{x,x} \ b_{y,x} \ -1}{b_{x,x} \ +b_{y,x}}\right)^{2} + 1}$$

where the plus sign is chosen to make \tilde{b} approach $b_{x,x}$ and $b_{y,x}$ when these latter two quantities approach each other.

As in the case of the geometric mean slope, the line will be made to pass through P_o . Proceeding as in that case:

$$\widetilde{a}_y = y_0 - \widetilde{b}x_0$$

and

$$\widetilde{a}_{x} = x_{o} - \frac{1}{\widetilde{b}} y_{o} = - \widetilde{a}_{y}/\widetilde{b}$$

For the former intercept

$$\widetilde{a}_{y} = \underline{a}_{y,y}(b_{x,x}^{2}+1) - \underline{a}_{x,y}(b_{y,x}^{2}+1) - (a_{y,y}-a_{x,y})\sqrt{(b_{x,x}^{2}+1)(b_{y,x}^{2}+1)} \\ b_{x,x}^{2} - b_{y,x}^{2}$$

7

in a construction of the second second of the second of th

Least Squared Perpendicular Deviations

The square of the distance d_i of point $P_i(x_i, y_i)$ from a line $y = a_y + b_x$ is known from analytic geometry to be

$$a_i^2 = (y_i - a_y - bx_i)^2 / (b^2 + 1).$$

Summing over i, differentiating partially with respect to a_y , and setting the result equal to zero give

$$\langle y_{i} \rangle - a_{y} - b \langle x_{i} \rangle = 0.$$

Carrying out a similar treatment with respect to $\overset{o}{b}$ gives

b
$$(\langle y_i^2 \rangle - \langle x_i^2 \rangle - 2a_y^{\nu} \langle y_i \rangle + a_y^{\nu}) - (b^2 - 1)(\langle x_i y_i \rangle - a_y^{\nu} \langle x_i \rangle) = 0$$

Substitution for a_y and solution for b gives

$$b = \frac{S(y,y) - S(x,x)}{2S(x,y)} + \sqrt{\frac{S(y,y) - S(x,x)}{2S(x,y)}}^{2} + 1$$

or

$$b = \frac{1}{2} (b_{y,x} - b_{x,y}) + \sqrt{\frac{1}{4} (b_{y,x} - b_{x,y})^2 + 1}$$

where the plus sign is chosen to make b approach b y, x and b x, y when these latter two quantities approach each other.

The intercept with the y-axis is obtained by eliminating $\langle\, y_{\,j}\,\rangle$ from the equation

$$a_{y}^{\prime} = \langle y_{i} \rangle - b \langle x_{i} \rangle$$

and the equation

 $a_{x,y} = \langle y_i \rangle - b_{x,x} \langle x_i \rangle$

to get

$$a_{y} = a_{x,y} + (b_{x,x} - b) \langle x_{i} \rangle$$

Analogously to the previous cases,

$$\mathbf{a}_{\mathbf{x}}^{\boldsymbol{v}} = \langle \mathbf{x}_{\mathbf{i}} \rangle - \frac{1}{\underline{v}} \langle \mathbf{y}_{\mathbf{i}} \rangle$$

Summary

The equations in this section have been derived in manners chosen for directness and have not always appeared in the most desirable form. To remedy this, Table 2 summarizes the results of this section in a way which illustrates the similarity among the chosen methods and the circumstances under which the parameters will converge. It is convenient at this point to introduce the quantity B, defined by either of the equations

or

$$b^2 - 2Bb - 1 = 0$$

 $b = B + \sqrt{B^2 + 1}$

although we will not have use for it until we discuss the application of the equations.

For conversion of the equations to practical form, it is helpful to first convert the ingredients to practical form, and this is done in Table 3 by manipulation of relationships in Table 1. Application of Table 3 to previously developed equations gives Table 4.

APPLICATION

Consideration of some of the properties of the quantities we have discussed will provide helpful orientation.

Quantity		Treatment	
	Geometric Mean Slope	Least-Square Perpendicular Deviations	Slope of Bisecting Line
a _y	y _o - bx _o	$\langle y_i \rangle - b \langle x_i \rangle$	y _o - bx _o
a _x	$\mathbf{x}_{o} = \frac{1}{b} \mathbf{y}_{o}$	$\langle x_{i} \rangle - \frac{1}{\sigma} \langle y_{i} \rangle$	$x_{o} - \frac{1}{b} y_{o}$
B ^a	$\frac{b_{y,x} - b_{x,y}}{2\sqrt{b_{y,x} - b_{x,y}}}$	b <mark>y,x - b</mark> x,y 2	$\frac{b_{y,x} - b_{x,y}}{1 + b_{y,x} b_{x,y}}$

Summary of Equations in Symmetrical Form

TABLE 2

a. Defined by either of the equations $b^2 - 2Bb - 1 = 0$ or $b = B + \sqrt{B^2 + 1}$.

THOME 2	TA	EL	E	3
---------	----	----	---	---

Summary of Equations for Conversion to Practical Form

Quantity	Equation	
^a x,x	-a _{x,y} /b _{x,x}	
a y,x	(1-r ²) $\langle x_i \rangle - r^2 \frac{a_{x,y}}{b_{x,x}}$	(a)
^а у,у	$a_{x,y} - \frac{1-r^2}{r^2} b_{x,x} \langle x_i \rangle$	(a)
b _{x,y}	$\frac{1}{b_{x,x}}$	
b y,x	$\frac{b_{x,x}}{r^2}$	
b y,y	$\frac{r^2}{b_{x,x}}$	
$\langle y_1 \rangle$	$a_{x,y} + b_{x,x} \langle x_1 \rangle$	

(a) Ezekiel² calls r^2 the coefficient of determination and 1- r^2 the coefficient of non-determination. He des gnates the latter by k^2 . He calls k the coefficient of alienation.

11

antinanti-republicantan antikan antikan

TABLE 4

	Summary of Equations in Practical Form	ctical Form	
Treatment	$\frac{a_{y}-a_{x,y}}{\langle x_{1}\rangle}$	e E	م
Geometric Mean (∧)	$\frac{r-1}{r}b_{x,x}$	$\frac{b_{x,x}}{2 r } = \frac{2}{r}$	بر <mark>x¹x</mark> م
Least-Square Perpendicular Devlations (U)	$2r^{2}b_{x,x}^{2}-b_{x,x}^{2}+r^{2} - \sqrt{(b_{x,x}^{2}-r^{2})^{2}+4r^{4}b_{x,x}}^{2}$	2 b, 2 - r ² x.x 2r ² b, x, x	ı
Bisector (~)	$\frac{r^{2}(b_{\mathbf{x},\mathbf{x}}^{2}+1) - \sqrt{(b_{\mathbf{x},\mathbf{x}}^{2}+1)(b_{\mathbf{x},\mathbf{x}}^{2}+r^{4})}}{(r^{2}+1) b_{\mathbf{x},\mathbf{x}}}$	$\frac{b_{x,x}}{b_{x,x}} - \frac{2}{r^2}$ $(r^2 + 1) \ b_{x,x}$	ı
a. Defined by	a. Defined by either of the equations $b^2 - 2Bb - 1 = 0$ or $b = B + \sqrt{B^2 + 1}$.) or $b = B + \sqrt{B^2 + 1}$	

We first note that while S(u,v) may be either positive or negative, S(u,u) must always be positive. Reference to Table 1 shows that S(x,y), $b_{x,x}$, $b_{y,y}$, $b_{x,y}$, $b_{y,x}$ and r will therefore all have the same sign. It is also obvious from Table 1 that the value of r will lie between those of $b_{x,x}$ and $b_{y,y}$, while the value of 1/r will lie between those of $b_{x,y}$ and $b_{y,y}$.

Table 2 shows that the sign of the quantity B is the same in all three treatments and governed by $b_{y,x} - b_{x,y}$. From its definition, each value of B is seen to change sign as the value of b^2 goes through 1. However, most correlations of fractionation data give values in the range of $0 \le b \le 1$, so that B will lie primarily in the range $B \le 0$.

Reference to Table 4 shows that, for $r^2 = 1$ (perfect correlation), all B's are equal. Since for positive correlation $\partial B/\partial r$ at $r^2 = 1$ is the same for both the geometric-mean and angle-bisection treatments, these will have similar values for good positive correlations.

In general

$$\widetilde{B}: \widetilde{B}: \widetilde{B} = |\mathbf{r}| : 1 : 2\mathbf{r}^2/(\mathbf{r}^2 + 1)$$

so that $|\widetilde{B}| \ge |\widetilde{B}| \ge |\widetilde{B}|$. Now, the relation between b and B is complicated, but for the range of interest it can be visualized geometrically as shown by Fig. 3. From this figure it is apparent that as -B increases, b decreases, and therefore:

 $\widetilde{b} \ge \widetilde{b} \ge \widetilde{b}$ (0 \le \widetilde{b} , \widetilde{b} , $\widetilde{b} \le 1$)

Figure 4 shows the application of these methods to the correlation of Te¹³² data from Shot Sedan.³ Two outliers are evident among the data. These were included in all the calculations except one, and that one is indicated on the graph. The slopes for certain-x $(b_{x,x})$ and certain-y $(b_{y,x})$ are seen to be extreme. The slope for angle bisection ($\tilde{b} = 0.654$)

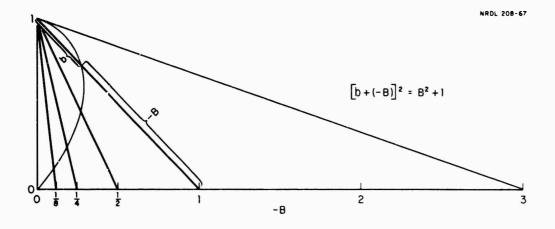


Fig. 3 Geometrical Relation Between b and -B. The members of the family of right triangles all have unit height and a base equal to -B. If a distance -B is laid off along a hypotenuse, the length of the remainder of the hypotenuse corresponds to b. The locus of these points is shown by the curved line.

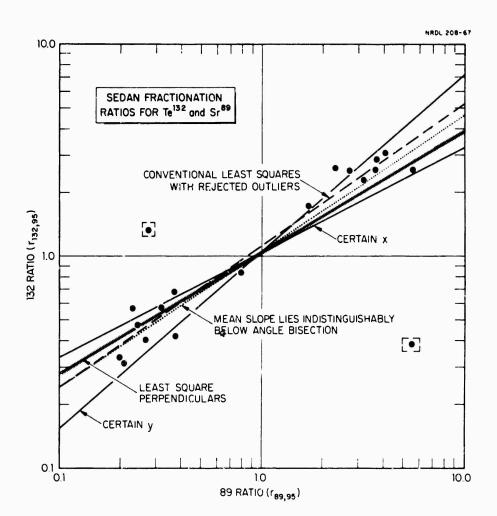


Fig. 4 Comparison of Regression Parameters. Outliers are in dashed squares.

A. 1 . .

is slightly greater than that for the mean slope (b = 0.645), but the lines are indistinguishable on the graph. The slopes of these lines are somewhat larger than that for the least square perpendiculars.

RECOMMENDATION

The choice of a method from the alternatives presented must be made in light of the realizations that: (1) The choice is not critical; (2) Cases with low values of r are of little practical significance; (3) Cases of $r \approx 1$, $b \approx 1$ and $b \approx 0$ do not usually present a problem. The considerations we have presented argue in favor of the geometric-mean regression line (\hat{b}) for the following reasons: (1) Its parameters are very simple to calculate from quantities usually obtained by the conventional practice of regarding x as certainly known; (2) Since it gives results which are nearly equal to those obtained from the angle-bisection treatment, it has all the advantages of that method; and (3) It gives results for the slope which are intermediate to those obtained by rejecting outliers. and those obtained by least square perpendiculars.

Although little experience has been obtained to date on the application of this method, no circumstances which would dictate another choice are foreseeable at this time.

The similarity between the lines obtained by rejection of "utliers and the geometric-mean line indicates that the geometric mean should receive further attention as a means of handling the general problem of outliers.

REFERENCES

- 1. C. A. Bennett and N. L. Franklin, <u>Statistical Analysis in Chemistry</u> and the Chemical Industry, Wiley, <u>New York (1954)</u>.
- 2. M. Ezekiel and K. A. Fox, <u>Methods of Correlation and Regression</u> Analysis, Wiley, New York (1959).
- 3. W. B. Lane, "Some Radiochemical and Physical Measurements of Debris From an Underground Nuclear Detonation," Project Sedan, Atomic Energy Commission Report PNE 229F, U. S. Naval Radiological Defense Laboratory, June 1963.

a to the state of the state of

Security Classification					
DOCUMENT	CONTROL DATA -	P & D			
(Security classification of title, body of abstract and in			overall report is classified)		
ORIGINATING ACTIVITY (Corporate author)			ECURITY CLASSIFICATION		
U. S. Naval Radiological Defense I	aboratory	UNCLAS	SIFIED		
San Francisco, California 94135	·	25. GROUP			
REGRESSION PARAMETERS FOR PAIRS OF	EQUALLY UNCER	TAIN VARIAB	LES		
DESCRIPTIVE NOTES (Type of report and inclusive dates)					
AUTHOR(S) (First name, iniddle initial, last name)					
Edward C. Freiling Glenn R. Crocker					
REPORT DATE	78. TOTAL NO	OF PAGES	76. NO. OF REFS		
16 October 1967		29	3		
CONTRACT OR GRANT NO.	98. ORIGINATO		BER(\$)		
AEC Contract AT(49-7)-1963					
29 3					
	9b. OTHER RE this report)	PORT NO(S) (Any o	ther numbers that may be assigned		
	or public relea	se and sale;	; its distribution		
SUPPLEMENTARY NOTES		G MILITARY ACT			
		c Energy Con			
	i Washi	ngton, D. C.	20545		
	a doni				
The correlation of radiochemi debris involves the treatment of t able. We considered three new cri meters for such correlations (leas and the line, bisection of the ang gression lines, and adoption of th regression slopes). We concluded factory. It is related to the usu efficient of correlation r by the	cal data from wo variables w teria for the st square perpe gle formed by t the geometric me that the geome al certain-x r	samples of the hose uncertant establishmer ndicular dis he certain- an of the ce tric-mean si egression si	Fractionated nuclear inties are compar- it of regression para stances between point and certain-y re- ertain-x and certain- ope b was most satis		
The correlation of radiochemi debris involves the treatment of t able. We considered three new cri meters for such correlations (leas and the line, bisection of the ang gression lines, and adoption of th regression slopes). We concluded factory. It is related to the usu efficient of correlation r by the	cal data from wo variables w teria for the st square perpe gle formed by t be geometric me that the geome that the geome al certain-x r simple express	samples of the hose uncertant establishmer ndicular dis he certain- an of the ce tric-mean si egression si	Fractionated nuclear inties are compar- it of regression para stances between point and certain-y re- ertain-x and certain- ope b was most satis		

Andrea an andrea

¢.	KEY WORDS	LINK		LIN	ĸ	LIN	ĸc
		ROLE	WT	ROLE	WT	ROLE	w
Regression	n						
Fractiona							
Statistic							
Niclear de	ebris						
Least squ	ares						
-							
						1	
						1	
				Í			
				İ			
D . NOV 14	72 (BACK)						
				TIMO	LASSIF	TTT	