

AD 654386

CF-2899

11 November 1960

COPY NO.

34

HYDRODYNAMIC FORCES AND MOMENTS
ACTING ON A SLENDER BODY OF REVOLUTION
MOVING UNDER A REGULAR TRAIN OF WAVES

by

R. M. Sorenson

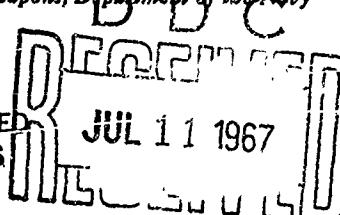
The CF series of papers is intended to be a flexible means for the reporting of preliminary investigations, or subject matter of limited interest. The information presented herein may be tentative, and subject to modification. This paper may not be reproduced except with the express permission of the issuing agency.

Initial distribution of this document is confined to persons and organizations within Section T immediately concerned with the subject matter. Upon special request, copies of this report may be made available to other organizations having a stated need for the information presented.

THE JOHNS HOPKINS UNIVERSITY
APPLIED PHYSICS LABORATORY
8621 GEORGIA AVENUE SILVER SPRING, MARYLAND

Operating under Contract NOrd 7386 with the Bureau of Naval Weapons, Department of the Navy

THIS DOCUMENT HAS BEEN APPROVED
FOR PUBLIC RELEASE AND SALE: ITS
DISTRIBUTION IS UNLIMITED



ARCHIVE COPY

251

THE KANSAS CITY UNIVERSITY
APPLIED PHYSICS LABORATORY
Under Contract with the
U.S. AIR FORCE

HYDRODYNAMIC FORCES AND MOMENTS ACTING ON A SLENDER BODY

OF REVOLUTION MOVING UNDER A REGULAR TRAIN OF WAVES

by

R. M. Sorensen

TABLE OF CONTENTS

| | |
|--|----|
| INTRODUCTION | 1 |
| COORDINATE SYSTEMS | 2 |
| THE FLUID AND ITS BOUNDARY CONDITIONS. | 2 |
| SINGULARITIES. | 5 |
| HYDRODYNAMIC FORCE | 5 |
| HYDRODYNAMIC MOMENT. | 14 |
| REFERENCES | 19 |
| SELECTED BIBLIOGRAPHY. | 20 |

Introduction

The author, not being a Hydrodynamicist, was much impressed by the difficulty experienced in finding procedures for computing or approximating hydrodynamic forces, on bodies, generated by waves. In particular, knowledge was desired concerning the hydrodynamic forces and moments acting on a body of revolution moving under waves. Very few papers were found which attempted these ends. Some of these are given in the selected bibliography. Most of the methods were valid for, or developed for, only very restricted cases such as balls or motion parallel to a mean surface, etc.

Attention finally centered on a paper by Cummins [1]. However, the exposition was found to be lacking, for our purposes, in the following respects:

- 1) restriction to Potential Flow
- 2) restriction to slender bodies of revolution
- 3) restriction to motion parallel to the mean free surface
- 4) restriction to constant velocity along an axis of the body.

We shall consider these points individually.

The restriction to potential flow is most easily treated. If anyone has done something similar for non-potential flows, we have not learned, as yet, of his work.

No mention need be made here concerning the limitation to treatment of slender bodies of revolution, except to remark that with the mapping techniques, e.g. Miles [2], available, this restriction is not as great as it first appears.

The restriction to motion parallel to the mean surface is, we think, removed by this paper. Even so, the orientation of the body must remain constant. This is not too hard to live with since this is just what would be required for numerical integration. That is, if we are integrating numerically with respect to time, say, then over a small time interval we would hold such things as orientation and velocity constant.

The restriction to constant velocity along an axis of the body is not needed. We shall still take the velocity as constant, but will not restrict it to being along an axis.

The present report, then, can not claim to be anything more than a slight extension of Cummin's results to a situation which may be useful in computer applications.

- 2 -

The organization and notation of this report is essentially that of Cummins. This should make comparison easy.

It is recommended that this report only be read if the reader has available a copy of [1].

Coordinate Systems

It will be necessary to consider two systems of coordinates.

The first system, considered as stationary will be called the earth system. It will be right-handed and orthogonal with its origin at the mean free surface of the fluid. The positive direction of the z-axis is to be upward (out of the fluid) and is assumed parallel to the local gravity vector. The fixed axis will be denoted by x, y, z.

The second set of coordinates is also to be right-handed and orthogonal. This will be called the body system and will be aligned in the body, fixed with respect to the body. The axis will be denoted by x, y, z.

The Fluid and Its Boundary Conditions

We consider a free surface disturbed by a regular train of waves. As a further assumption we consider a linear, irrotational wave theory for deep water. Such a theory might, for example, be specified by

$$\nabla^2 \phi = 0$$

$$\frac{P}{\rho} = g(z + \eta) + \phi_t + \text{constant}$$

$$\left. \phi_z \right|_{z=0} = \eta_t$$

$$\phi_z = 0 \text{ on the bottom}$$

$$\eta = -\frac{1}{g} \phi_t \text{ at } z = 0 \text{ in which } \eta \text{ is the surface elevation.}$$

The linear irrotational wave theory for deep water is satisfied by the velocity potential (earth system)

$$\phi_w = \frac{hc}{2} e^{\frac{2\pi z}{\lambda}} \cos \psi$$

$$\psi = \frac{2\pi}{\lambda} (x \cos \beta + y \sin \beta - ct + \alpha) \text{ in which}$$

- 3 -

λ = wavelength

h = waveheight (crest to trough)

c = celerity

α = phase angle

β = direction of propagation as measured from the x -axis.

The fluid velocities are then given as

$$u = -\phi_x = \frac{\pi hc}{\lambda} \cos \beta e^{\frac{2\pi z}{\lambda}} \sin \psi$$

$$v = -\phi_y = \frac{\pi hc}{\lambda} \sin \beta e^{\frac{2\pi z}{\lambda}} \sin \psi$$

$$w = -\phi_z = \frac{\pi hc}{\lambda} e^{\frac{2\pi z}{\lambda}} \cos \psi$$

For a body moving toward the surface at a constant velocity \underline{V} we obtain the following relation between coordinates

$$\begin{pmatrix} x' \\ y' \\ z' \end{pmatrix} = \Theta_{EB} \begin{pmatrix} x \\ y \\ z \end{pmatrix} - \underline{V}t \quad \text{in which}$$

Θ_{EB} is the matrix of direction cosines relating the systems. Furthermore

$$\begin{pmatrix} u' \\ v' \\ w' \end{pmatrix} = \Theta_{EB} \begin{pmatrix} u \\ v \\ w \end{pmatrix} - \underline{V}$$

In the following we shall treat Θ_{EB} as a constant; and for convenience we set,

$$\Theta_{EB}^{-1} = \Theta_{BE} = (a_{ij})$$

$$\underline{V} = \begin{pmatrix} u_m \\ v_m \\ w_m \end{pmatrix}$$

- 4 -

$$\underline{P} = \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}$$

$$\gamma = \frac{hc}{2}$$

$$\delta = \frac{2\pi}{\lambda}$$

The potential function, with respect to the moving system, is then

$$\phi'_w = \phi_w + (O_{BE}^P) \cdot \underline{v} \quad \text{which may be written}$$

$$\phi'_w = \gamma e^{\delta [a_{31}x' + a_{32}y' + a_{33}z' + w_m t]} \cos \delta \left\{ [a_{11}x' + a_{12}y' + a_{13}z' + u_m t] \cos \beta + [a_{21}x' + a_{22}y' + a_{23}z' + v_m t] \sin \beta - ct + \alpha \right\} + (O_{BE}^P) \cdot \underline{v}$$

Hence we find that

$$(1) \quad u' = - (\phi'_w)_{x'} = - (\phi_w)_{x'} - [(O_{BE}^P) \cdot \underline{v}]_{x'} \\ = a_{11}(u - u_m) + a_{21}(v - v_m) + a_{31}(w - w_m)$$

$$(2) \quad v' = - (\phi'_w)_{y'} = - (\phi_w)_{y'} - [(O_{BE}^P) \cdot \underline{v}]_{y'} \\ = a_{12}(u - u_m) + a_{22}(v - v_m) + a_{32}(w - w_m)$$

$$(3) \quad w' = - (\phi'_w)_{z'} = - (\phi_w)_{z'} - [(O_{BE}^P) \cdot \underline{v}]_{z'} \\ = a_{13}(u - u_m) + a_{23}(v - v_m) + a_{33}(w - w_m)$$

- 5 -

Singularities

We shall represent the body in the same manner as in [1]. That is, we set

$$(4) \quad \mu = \mu_x i + \mu_y j + \mu_z k \text{ with}$$

$$\mu_x = -\frac{1}{4} a^2 u'$$

$$\mu_y = -\frac{1}{2} a^2 v'$$

$$\mu_z = -\frac{1}{2} a^2 w' .$$

Hydrodynamic Force

The Force is to be computed via:

$$(5) \quad dF = dF_L + dF_t \quad \text{in which}$$

$$dF_L = -l_1 \rho (\mu_x \frac{\partial}{\partial x} + \mu_y \frac{\partial}{\partial y} + \mu_z \frac{\partial}{\partial z}) q_w dx'$$

$$dF_t = -l_1 \rho \left(\frac{\partial u_x}{\partial t} i + \frac{\partial u_y}{\partial t} j + \frac{\partial u_z}{\partial t} k \right) dx'$$

The notation used is that of Cummins [1], see especially page 5 Eqn [19] - [21].

We have then the relation

$$u = \gamma \delta \cos \beta e^{\delta z} \sin \psi$$

$$v = \gamma \delta \sin \beta e^{\delta z} \sin \psi$$

$$w = -\gamma \delta e^{\delta z} \cos \psi$$

$$z = a_{31}x' + a_{32}y' + a_{33}z' + w_m t$$

$$\frac{\partial z}{\partial t} = w_m$$

$$\psi = \delta \left\{ [a_{11}x' + a_{12}y' + a_{13}z' + u_m t] \cos \beta + [a_{21}x' + a_{22}y' + a_{23}z' + v_m t] \sin \beta - ct + a \right\}$$

$$\frac{\partial \psi}{\partial t} = \delta (u_m \cos \beta + v_m \sin \beta - c)$$

$$u_t = w_m \delta u + \delta \cos \beta (u_m \cos \beta + v_m \sin \beta - c) (-w)$$

$$v_t = w_m \delta v + \delta \sin \beta (u_m \cos \beta + v_m \sin \beta - c) (-w)$$

$$w_t = w_m \delta w + \delta u_m u + \delta v_m v - \delta \frac{c}{\cos \beta} u$$

$$\begin{aligned} \frac{\partial}{\partial t} \mu_x &= -\frac{1}{4} a^2 \frac{\partial}{\partial t} (u') = -\frac{a^2}{4} \frac{d}{dt} \left[a_{11}(u-u_m) + a_{21}(v-v_m) + a_{31}(w-w_m) \right] \\ &= -\frac{a^2}{4} (a_{11}u_t + a_{21}v_t + a_{31}w_t) \end{aligned}$$

$$\begin{aligned} \frac{\partial}{\partial t} \mu_y &= -\frac{a^2}{2} \frac{\partial}{\partial t} (v') = -\frac{a^2}{2} \frac{d}{dt} \left[a_{12}(u-u_m) + a_{22}(v-v_m) + a_{32}(w-w_m) \right] \\ &= -\frac{a^2}{2} (a_{12}u_t + a_{22}v_t + a_{32}w_t) \end{aligned}$$

$$\begin{aligned} \frac{\partial}{\partial t} \mu_z &= -\frac{a^2}{2} \frac{\partial}{\partial t} (w') = -\frac{a^2}{2} \frac{d}{dt} \left[a_{13}(u-u_m) + a_{23}(v-v_m) + a_{33}(w-w_m) \right] \\ &= -\frac{a^2}{2} (a_{13}u_t + a_{23}v_t + a_{33}w_t) . \end{aligned}$$

We find, from these, that

$$(6) \quad \frac{\partial}{\partial t} \mu_x = -\frac{\delta a^2}{4} \left\{ \left(a_{11}v_m + a_{31}u_m - \frac{c a_{31}}{\cos \beta} \right) u + (a_{21}w_m + a_{31}v_m) v \right. \\ \left. + \left[a_{31}w_m - (a_{11}\cos \beta + a_{21}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] w \right\}$$

$$(7) \quad \frac{\partial}{\partial t} \mu_y = - \frac{\delta a^2}{2} \left\{ \left(a_{12}w_m + a_{32}u_m - \frac{ca_{32}}{\cos \beta} \right) u + (a_{22}w_m + a_{32}v_m) v + \left[a_{32}w_m - (a_{12}\cos \beta + a_{22}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] w \right\}$$

$$(8) \quad \frac{\partial}{\partial t} \mu_z = - \frac{\delta a^2}{2} \left\{ \left(a_{13}w_m + a_{33}u_m - \frac{ca_{33}}{\cos \beta} \right) u + (a_{23}w_m + a_{33}v_m) v + \left[a_{33}w_m - (a_{13}\cos \beta + a_{23}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] w \right\} .$$

If, furthermore, we consider the relations

$$z_x' = a_{31} ; z_y' = a_{32} ; z_z' = a_{33}$$

$$\psi_x' = \delta (a_{11}\cos \beta + a_{21}\sin \beta)$$

$$\psi_y' = \delta (a_{12}\cos \beta + a_{22}\sin \beta)$$

$$\psi_z' = \delta (a_{13}\cos \beta + a_{23}\sin \beta)$$

$$\frac{\partial}{\partial t} e^{\delta z} \cos \psi = z_? \delta e^{\delta z} \cos \psi - \psi_? e^{\delta z} \sin \psi$$

$$\frac{\partial}{\partial t} e^{\delta z} \sin \psi = z_? \delta e^{\delta z} \sin \psi + \psi_? e^{\delta z} \cos \psi$$

$$\frac{\partial}{\partial t} u = z_? \delta u - \psi_? \cos \beta w$$

$$\frac{\partial}{\partial t} v = z_? \delta v - \psi_? \sin \beta w$$

$$\frac{\partial}{\partial t} w = z_? \delta w + \psi_? \gamma \delta e^{\delta z} \sin \psi ,$$

we find

$$(9) \quad u_x' = \delta \left\{ 2a_{11}a_{31}u + 2a_{31}a_{21}v + \left[a_{31}^2 - (a_{11} \cos \beta + a_{21} \sin \beta)^2 \right] w \right\}$$

$$(10) \quad u_y' = \delta \left\{ (a_{11}a_{32} + a_{31}a_{12})u + (a_{21}a_{32} + a_{31}a_{22})v + \left[a_{31}a_{22} - (a_{11} \cos \beta + a_{21} \sin \beta)(a_{12} \cos \beta + a_{22} \sin \beta) \right] w \right\}$$

$$(11) \quad u_z' = \delta \left\{ (a_{11}a_{33} + a_{31}a_{13})u + (a_{21}a_{33} + a_{31}a_{23})v + \left[a_{31}a_{33} - (a_{11} \cos \beta + a_{21} \sin \beta)(a_{13} \cos \beta + a_{23} \sin \beta) \right] w \right\}$$

$$(12) \quad v_x' = \delta \left\{ (a_{12}a_{31} + a_{32}a_{11})u + (a_{22}a_{31} + a_{32}a_{21})v + \left[a_{32}a_{31} - (a_{12} \cos \beta + a_{22} \sin \beta)(a_{11} \cos \beta + a_{21} \sin \beta) \right] w \right\}$$

$$(13) \quad v_y' = \delta \left\{ 2a_{12}a_{32}u + 2a_{22}a_{32}v + \left[a_{32}^2 - (a_{12} \cos \beta + a_{22} \sin \beta)^2 \right] w \right\}$$

$$(14) \quad v_z' = \delta \left\{ (a_{12}a_{33} + a_{32}a_{13})u + (a_{22}a_{33} + a_{32}a_{23})v + \left[a_{32}a_{33} - (a_{12} \cos \beta + a_{22} \sin \beta)(a_{13} \cos \beta + a_{23} \sin \beta) \right] w \right\}$$

$$(15) \quad w_x' = \delta \left\{ (a_{13}a_{31} + a_{33}a_{11})u + (a_{23}a_{31} + a_{33}a_{21})v + \left[a_{33}a_{31} - (a_{13} \cos \beta + a_{23} \sin \beta)(a_{11} \cos \beta + a_{21} \sin \beta) \right] w \right\}$$

$$(16) \quad w_y' = \delta \left\{ (a_{13}a_{32} + a_{33}a_{12})u + (a_{23}a_{32} + a_{33}a_{22})v + \left[a_{33}a_{32} - (a_{13} \cos \beta + a_{23} \sin \beta)(a_{12} \cos \beta + a_{22} \sin \beta) \right] w \right\}$$

$$(17) \quad w_z' = \delta \left\{ 2a_{13}a_{33}u + 2a_{23}a_{33}v + \left[a_{33}^2 - (a_{13} \cos \beta + a_{23} \sin \beta)^2 \right] w \right\}$$

We may write

$$dF_{\ell} = -4\pi\rho \left[\mu_x (\underline{q}_w)_x' + \mu_y (\underline{q}_w)_y' + \mu_z (\underline{q}_w)_z' \right] dx', \text{ so that}$$

$$\begin{aligned} dF_{\ell,x} &= -4\pi\rho \left[\mu_x \mu_x' + \mu_y \mu_y' + \mu_z \mu_z' \right] dx' \\ &= -4\pi\rho \left\{ -\frac{\delta a^2}{4} \left[a_{11}(u-u_m) + a_{21}(v-v_m) + a_{31}(w-w_m) \right] \left[2a_{11}a_{31}u + 2a_{31}a_{21}v \right. \right. \\ &\quad \left. \left. + \left(a_{31}^2 - [a_{11}\cos\beta + a_{21}\sin\beta]^2 \right) w \right] - \frac{\delta a^2}{2} \left[a_{12}(u-u_m) + a_{22}(v-v_m) \right. \right. \\ &\quad \left. \left. + a_{32}(w-w_m) \right] \left[(a_{11}a_{32} + a_{31}a_{12})u + (a_{21}a_{32} + a_{31}a_{22})v + \left(a_{31}a_{32} - [a_{11}\cos\beta \right. \right. \\ &\quad \left. \left. + a_{21}\sin\beta] [a_{12}\cos\beta + a_{22}\sin\beta] \right) w \right] - \frac{\delta a^2}{2} \left[a_{13}(u-u_m) + a_{23}(v-v_m) \right. \right. \\ &\quad \left. \left. + a_{33}(w-w_m) \right] \left[(a_{11}a_{33} + a_{31}a_{13})u + (a_{21}a_{33} + a_{31}a_{23})v + \left(a_{31}a_{33} - [a_{11}\cos\beta \right. \right. \\ &\quad \left. \left. + a_{21}\sin\beta] [a_{13}\cos\beta + a_{23}\sin\beta] \right) w \right] \right\} dx' \end{aligned}$$

considering terms of first order only (neglect terms containing products of the variables). This may be reduced to

$$\begin{aligned} dF_{\ell,x} &= -4\pi\rho \left\{ \frac{\delta a^2}{4} (a_{11}u_m + a_{21}v_m + a_{31}w_m) \left[2a_{11}a_{31}u + 2a_{31}a_{21}v + \left(a_{31}^2 - [a_{11}\cos\beta \right. \right. \right. \\ &\quad \left. \left. + a_{21}\sin\beta] ^2 \right) w \left. \right] + \frac{\delta a^2}{2} (a_{12}u_m + a_{22}v_m + a_{32}w_m) \left[(a_{11}a_{32} + a_{31}a_{12})u + (a_{21}a_{32} \right. \\ &\quad \left. + a_{31}a_{22})v + \left(a_{31}a_{32} - [a_{11}\cos\beta + a_{21}\sin\beta] [a_{12}\cos\beta + a_{22}\sin\beta] \right) w \right] \\ &\quad + \frac{\delta a^2}{2} (a_{13}u_m + a_{23}v_m + a_{33}w_m) \left[(a_{11}a_{33} + a_{31}a_{13})u + (a_{21}a_{33} + a_{31}a_{23})v \right. \\ &\quad \left. + \left(a_{31}a_{33} - [a_{11}\cos\beta + a_{21}\sin\beta] [a_{13}\cos\beta + a_{23}\sin\beta] \right) w \right] \right\} dx' \end{aligned}$$

$$\begin{aligned}
 dF_{\ell,x} = & -4\pi\rho \left(\frac{\delta a^2}{4} \right) \left\{ 2 \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) a_{11}a_{31} + (a_{12}u_m + a_{22}v_m + a_{32}w_m) (a_{11}a_{32} \right. \right. \\
 & + a_{31}a_{12}) + (a_{13}u_m + a_{23}v_m + a_{33}w_m) (a_{11}a_{33} + a_{21}a_{13}) \Big] u + 2 \left[(a_{11}u_m + a_{21}v_m \right. \\
 & + a_{31}w_m) (a_{31}a_{21}) + (a_{12}u_m + a_{22}v_m + a_{32}w_m) (a_{21}a_{32} + a_{31}a_{22}) + (a_{13}u_m + a_{23}v_m \\
 & + a_{33}w_m) (a_{21}a_{33} + a_{31}a_{23}) \Big] v + \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left(a_{31}^2 - [a_{11}\cos \beta \right. \right. \\
 & \left. \left. + a_{21}\sin \beta \right]^2 \right) + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) \left(a_{31}a_{32} - [a_{11}\cos \beta + a_{21}\sin \beta] \right) \left[a_{12}\cos \beta \right. \\
 & \left. + a_{22}\sin \beta \right] + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) \left(a_{31}a_{33} - [a_{11}\cos \beta + a_{21}\sin \beta] \right) \left[a_{13}\cos \beta \right. \\
 & \left. + a_{23}\sin \beta \right] \Big] w \Big\} dx' \\
 dF_{t,x} = & -4\pi\rho \left(-\frac{\delta a^2}{4} \right) \left\{ \left(a_{11}w_m + a_{31}u_m - \frac{ca_{31}}{\cos \beta} \right) u + (a_{21}w_m + a_{31}v_m) v \right. \\
 & \left. + \left[a_{31}w_m - (a_{11}\cos \beta + a_{21}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] w \right\} dx' \\
 (18) \quad dF_x = & \pi\rho\delta a^2 \left\{ \left(a_{11}w_m + a_{31}u_m - \frac{ca_{31}}{\cos \beta} - 2 \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) a_{11}a_{31} + (a_{12}u_m \right. \right. \right. \\
 & + a_{22}v_m + a_{32}w_m) (a_{11}a_{32} + a_{31}a_{12}) + (a_{13}u_m + a_{23}v_m + a_{33}w_m) (a_{11}a_{33} + a_{21}a_{13}) \Big] u \\
 & + \left(a_{21}w_m + a_{31}v_m - 2 \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) (a_{31}a_{21}) + (a_{12}u_m + a_{22}v_m \right. \right. \\
 & + a_{32}w_m) (a_{21}a_{32} + a_{31}a_{22}) + (a_{13}u_m + a_{23}v_m + a_{33}w_m) (a_{21}a_{33} + a_{31}a_{23}) \Big] v \\
 & - \left((a_{11}\cos \beta + a_{21}\sin \beta)(w_m \cos \beta + v_m \sin \beta - c) - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left(a_{31}^2 \right. \right. \right. \\
 & \left. \left. - [a_{11}\cos \beta + a_{21}\sin \beta]^2 \right) + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) \left(a_{31}a_{32} - [a_{11}\cos \beta \right. \right. \\
 & \left. \left. + a_{21}\sin \beta \right] \left[a_{12}\cos \beta + a_{22}\sin \beta \right] \right) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) \left(a_{31}a_{33} \right. \\
 & \left. - [a_{11}\cos \beta + a_{21}\sin \beta] \left[a_{13}\cos \beta + a_{23}\sin \beta \right] \right) \Big] w \right\} dx'
 \end{aligned}$$

Proceeding similarly we find

$$(19) \quad dF_y = \pi \rho \delta a^2 \left\{ \left(2 \left[a_{12}w_m + a_{32}u_m - \frac{ca_{32}}{\cos \beta} \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{12}a_{31} + a_{32}a_{11}) \right. \right. \right. \\ \left. \left. \left. + (a_{12}u_m + a_{22}v_m + a_{32}w_m) (4a_{12}a_{32} + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m)(a_{12}a_{33} + a_{32}a_{13})) \right] \right) u \right. \\ \left. + \left(2 \left[a_{22}w_m + a_{32}v_m \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{22}a_{31} + a_{32}a_{21}) + (a_{12}u_m + a_{22}v_m \right. \right. \right. \\ \left. \left. \left. + a_{32}w_m)(4a_{22}a_{32}) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m)(a_{22}a_{33} + a_{32}a_{23}) \right] \right) v + \left(2 \left[a_{32}w_m \right. \right. \right. \\ \left. \left. \left. - (a_{12}\cos \beta + a_{22}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{32}a_{31} \right. \right. \\ \left. \left. - [a_{12}\cos \beta + a_{22}\sin \beta][a_{11}\cos \beta + a_{21}\sin \beta] \right) + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) \left(a_{32}^2 \right. \right. \\ \left. \left. - [a_{12}\cos \beta + a_{22}\sin \beta]^2 \right) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) \left(a_{32}a_{33} - [a_{12}\cos \beta \right. \right. \\ \left. \left. + a_{22}\sin \beta][a_{13}\cos \beta + a_{23}\sin \beta] \right) \right] \right) w \right\} dx'$$

$$(20) \quad dF_z = \pi \rho \delta a^2 \left\{ \left(2 \left[a_{13}w_m + a_{33}u_m - \frac{ca_{33}}{\cos \beta} \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{13}a_{31} + a_{33}a_{11}) \right. \right. \right. \\ \left. \left. \left. + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m)(a_{13}a_{32} + a_{33}a_{12}) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m)(2a_{13}a_{33}) \right] \right) u \right. \\ \left. + \left(2 \left[a_{23}w_m + a_{33}v_m \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{23}a_{31} + a_{33}a_{21}) + 2(a_{12}u_m + a_{22}v_m \right. \right. \right. \\ \left. \left. \left. + a_{32}w_m)(a_{23}a_{32} + a_{33}a_{22}) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m)(2a_{23}a_{33}) \right] \right) v + \left(2 \left[a_{33}w_m \right. \right. \right. \\ \left. \left. \left. - (a_{13}\cos \beta + a_{23}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{33}a_{31} \right. \right. \\ \left. \left. - [a_{13}\cos \beta + a_{23}\sin \beta][a_{11}\cos \beta + a_{21}\sin \beta] \right) + (a_{12}u_m + a_{22}v_m + a_{32}w_m) \left(a_{33}a_{32} \right. \right. \\ \left. \left. - [a_{13}\cos \beta + a_{23}\sin \beta][a_{12}\cos \beta + a_{22}\sin \beta] \right) + (a_{13}u_m + a_{23}v_m + a_{33}w_m) \left(a_{33}^2 \right. \right. \\ \left. \left. - [a_{13}\cos \beta + a_{23}\sin \beta]^2 \right) \right] \right) w \right\} dx'$$

- 12 -

Let L_1 be the x-coordinate of the rear of the body, and let L_2 be that of the front. Then

$$F_x = \int_{L_1}^{L_2} dF_x dx'; F_y = \int_{L_1}^{L_2} dF_y dx'; F_z = \int_{L_1}^{L_2} dF_z dx'.$$

Now, in each of dF_x , dF_y , dF_z , the only terms which vary with x' are a , u , v , w . If we set $\pi a^2 = A$ then each of dF_x , dF_y , dF_z is of the form,

$$\rho \delta A (c_1 u + c_2 v + c_3 w) dx', \text{ in which } c_1, c_2, c_3 \text{ are constant.}$$

Hence, each of F_x , F_y , F_z is of the form

$$\rho \delta \left(c_1 \int_{L_1}^{L_2} A u dx' + c_2 \int_{L_1}^{L_2} A v dx' + c_3 \int_{L_1}^{L_2} A w dx' \right).$$

This may be written as

$$\frac{\hbar c \rho \delta}{\lambda} \left[(c_1 \cos \beta + c_2 \sin \beta) \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' - c_3 \int_{L_1}^{L_2} A e^{\delta z} \cos \psi dx' \right].$$

We may then write

$$(21) \quad F_x = \frac{\delta \rho \hbar c}{\lambda} \left\{ \left[\left(a_{11} w_m \cos \beta + a_{31} u_m \cos \beta - c a_{31} - 2 \cos \beta [(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{11} a_{31}) \right. \right. \right. \\ \left. \left. \left. + (a_{12} u_m + a_{22} v_m + a_{32} w_m)(a_{11} a_{32} + a_{31} a_{12}) + (a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{11} a_{33} + a_{21} a_{13}) \right] \right) \right. \\ \left. + \left(a_{21} w_m + a_{31} v_m - 2 [(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{31} a_{21}) + (a_{12} u_m + a_{22} v_m + a_{32} w_m)(a_{21} a_{32}) \right. \right. \\ \left. \left. + a_{31} a_{22}) + (a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{21} a_{33} + a_{31} a_{23})] \right) \sin \beta \right] \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' \\ - \left(\left[a_{11} \cos \beta + a_{21} \sin \beta \right] \left[w_m \cos \beta + v_m \sin \beta - c \right] - \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m) (a_{31}^2 \right. \right. \\ \left. \left. - [a_{11} \cos \beta + a_{21} \sin \beta]^2 \right) + 2(a_{12} u_m + a_{22} v_m + a_{32} w_m) (a_{31} a_{32} - [a_{11} \cos \beta \right. \right. \\ \left. \left. + a_{21} \sin \beta] [a_{12} \cos \beta + a_{22} \sin \beta] \right] + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m) (a_{31} a_{33} - [a_{11} \cos \beta \right. \right. \\ \left. \left. + a_{21} \sin \beta] [a_{13} \cos \beta + a_{23} \sin \beta] \right] \right) \int_{L_1}^{L_2} A e^{\delta z} \cos \psi dx' \right\}$$

$$(22) \quad F_y = \frac{\epsilon_0 \pi h c}{\lambda} \left\{ \left[\left(2 \left[a_{12} w_m \cos \beta + a_{32} u_m \cos \beta - c a_{32} \right] - \cos \beta \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{12} a_{31} + a_{32} a_{11}) + (a_{12} u_m + a_{22} v_m + a_{32} w_m) (4 a_{12} a_{32} + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{12} a_{33} + a_{32} a_{13})) \right] \right. \right. \right.$$

$$+ \left(2 \left[a_{22} w_m + a_{32} v_m \right] - \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{22} a_{31} + a_{32} a_{21}) + (a_{12} u_m + a_{22} v_m + a_{32} w_m)(4 a_{22} a_{32}) + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{22} a_{33} + a_{32} a_{23}) \right] \right) \sin \beta \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' \\ - \left. \left. \left. \left(2 \left[a_{32} w_m - (a_{12} \cos \beta + a_{22} \sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] - \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{32} a_{31} - [a_{12} \cos \beta + a_{22} \sin \beta][a_{11} \cos \beta + a_{21} \sin \beta]) + 2(a_{12} u_m + a_{22} v_m + a_{32} w_m) (a_{32}^2 - [a_{12} \cos \beta + a_{22} \sin \beta]^2) + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{32} a_{33} - [a_{11} \cos \beta + a_{22} \sin \beta][a_{13} \cos \beta + a_{23} \sin \beta]) \right] \right) \int_{L_1}^{L_2} A e^{\delta z} \cos \psi dx' \right\}$$

$$(23) \quad F_z = \frac{\epsilon_0 \pi h c}{\lambda} \left\{ \left[\left(2 \left[a_{13} w_m \cos \beta + a_{33} u_m \cos \beta - c a_{33} \right] - \cos \beta \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{13} a_{31} + a_{33} a_{11}) + 2(a_{12} u_m + a_{22} v_m + a_{32} w_m)(a_{13} a_{32} + a_{33} a_{12}) + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m)(2 a_{13} a_{33}) \right] \right. \right. \right.$$

$$+ \left(2 \left[a_{23} w_m + a_{33} v_m \right] - \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{23} a_{31} + a_{33} a_{21}) + 2(a_{12} u_m + a_{22} v_m + a_{32} w_m)(a_{23} a_{32} + a_{33} a_{22}) + 2(a_{13} u_m + a_{23} v_m + a_{33} w_m)(2 a_{23} a_{33}) \right] \right) \sin \beta \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' \\ - \left. \left. \left. \left(2 \left[a_{33} w_m - (a_{13} \cos \beta + a_{23} \sin \beta)(u_m \cos \beta + v_m \sin \beta - c) \right] - \left[(a_{11} u_m + a_{21} v_m + a_{31} w_m)(a_{33} a_{31} - [a_{13} \cos \beta + a_{23} \sin \beta][a_{11} \cos \beta + a_{21} \sin \beta]) + (a_{12} u_m + a_{22} v_m + a_{32} w_m)(a_{33} a_{32} - [a_{13} \cos \beta + a_{23} \sin \beta][a_{12} \cos \beta + a_{22} \sin \beta]) + (a_{13} u_m + a_{23} v_m + a_{33} w_m)(a_{33}^2 - [a_{13} \cos \beta + a_{23} \sin \beta]^2) \right] \right) \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' \right\} . \right.$$

Of course, we must remember when evaluating the integrals that z , ψ , A are functions of x' .

Hydrodynamic Moment

The analysis as done by Cummins, from Eq. [40] on page 7 to Eq. [59] on page 10 of Ref. [1] is carried over with but little change. For convenience we shall write some of the pertinent formulae.

$$(24) \quad M = M_\ell + M_t$$

$$(25) \quad M_\ell = \sum_i (r \times F_\ell) + l \pi \rho \sum_i (q_w \times A)_i$$

$$(26) \quad M_t = \rho \frac{d}{dt} \int_S \Phi(r \times n) d\sigma$$

To evaluate the surface integral we proceed as in Cummins. Corresponding to his Eq. [48] we have

$$(27) \quad dM_t = \rho a x' \left[\frac{d}{dt} \int_0^{2\pi} (\phi'_w + \phi_s)(j \sin \theta - k \cos \theta) d\theta \right] dx'$$

Writing

$$\phi'_w(x', a \cos \theta, a \sin \theta) = \phi'_w(x', 0, 0) - a(v' \cos \theta + w' \sin \theta)$$

and

$$\phi_s = -a(v' \cos \theta + w' \sin \theta), \text{ as in Cummins,}$$

we obtain

$$(28) \quad dM_t = -2\pi \rho a^2 x' \left[\frac{\partial}{\partial t} (w') j - \frac{\partial}{\partial t} (v') k \right] dx' .$$

We may write

$$(29) \quad dM_\ell = r x dF_\ell + l \pi \rho (q_w \times \mu) dx' .$$

This is

$$(30) \quad dM_{\ell} = (-x'dF_{\ell,z} + \pi\rho a^2 u' w' dx') j + (x'dF_{\ell,y} - \pi\rho a^2 u' v' dx') k, \text{ since}$$

$q_w x u = \frac{1}{4} a^2 u' (w' j - v' k)$ and the terms $z' dF_{\ell,x}$, $-y' dF_{\ell,x}$ do not appear because the legally moment is, in this case, evaluated along the x' -axis.

Then

$$(31) \quad dM = \left(-x'dF_{\ell,z} + \pi\rho a^2 u' w' dx - 2\pi\rho a^2 x' \frac{\partial}{\partial t} (w') dx' \right) j + \left(x'dF_{\ell,y} - \pi\rho a^2 u' v' dx' + 2\pi\rho a^2 x' \frac{\partial}{\partial t} (v') dx' \right) k$$

We shall write this as

$$(32) \quad dM = dM_y j + dM_z k .$$

Then we find that

$$dM_y = \pi\rho a^2 \left\{ u' w' - x' (u' w'_x + 2v' w'_y + 2w' w'_z + 2a_{13} u_t + 2a_{23} v_t + 2a_{33} w_t) \right\} dx'$$

$$dM_z = \pi\rho a^2 \left\{ x' (u' v'_x + 2v' v'_y + 2w' v'_z + 2a_{12} u_t + 2a_{22} v_t + 2a_{32} w_t) - u' v' \right\} dx'$$

If as a first approximation we take

$$u' w' = - (a_{11} u_m + a_{21} v_m + a_{31} w_m) w' - (a_{13} u_m + a_{23} v_m + a_{33} w_m) u'$$

$$u' v' = - (a_{11} u_m + a_{21} v_m + a_{31} w_m) v' - (a_{12} u_m + a_{22} v_m + a_{32} w_m) u'$$

$$u' w'_x = - (a_{11} u_m + a_{21} v_m + a_{31} w_m) w'_x,$$

$$v' w'_y = - (a_{12} u_m + a_{22} v_m + a_{32} w_m) w'_y, \text{ etc.,}$$

we find that

$$(33) \quad dM_y = \pi \rho a^2 \left\{ x' \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) w'_x + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) w'_y \right. \right. \\ \left. \left. + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) w'_z - 2a_{13}u_t - 2a_{23}v_t - 2a_{33}w_t \right] \right. \\ \left. - (a_{13}u_m + a_{23}v_m + a_{33}w_m) u' - (a_{11}u_m + a_{21}v_m + a_{31}w_m) w \right\} dx'$$

$$(34) \quad dM_z = \pi \rho a^2 \left\{ (a_{11}u_m + a_{21}v_m + a_{31}w_m) v' + (a_{12}u_m + a_{22}v_m + a_{32}w_m) u' \right. \\ \left. - x' \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) v'_x + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) v'_y \right. \right. \\ \left. \left. + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) v'_z - 2a_{12}u_t + 2a_{22}v_t + 2a_{32}w_t \right] \right\} dx' .$$

A straightforward, but messy, substitution for the primed variables will show that each of dM_y , dM_z is of the form

$$\pi \rho a^2 \left[(c_1 + c_2 x') u + (c_3 + c_4 x') v + (c_5 + c_6 x') w \right] dx'$$

in which $c_1, c_2, c_3, c_4, c_5, c_6$ are constants. On putting $\pi a^2 = A$ and integrating, we find that dM_y and dM_z have the form

$$\rho \delta_r \left[(c_1 \cos \beta + c_3 \sin \beta) \int_{L_1}^{L_2} A e^{\delta z} \sin \psi dx' + (c_2 \cos \beta \right. \\ \left. + c_4 \sin \beta) \int_{L_1}^{L_2} A x' e^{\delta z} \sin \psi dx' - \int_{L_1}^{L_2} (c_5 \right. \\ \left. + c_6 x') A e^{\delta z} \cos \psi dx' \right] .$$

The results of the integration are

$$(35) \quad M_y = \frac{\pi \rho h c}{\lambda} \left\{ - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{13}\cos \beta + a_{23}\sin \beta) + (a_{13}u_m + a_{23}v_m + a_{33}w_m)(a_{11}\cos \beta + a_{21}\sin \beta) \right] \int_{L_1}^{L_2} A e^{\frac{2\pi z}{\lambda}} \sin \psi dx + \frac{2\pi}{\lambda} \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left([a_{13}a_{31} + a_{33}a_{11}] \cos \beta + [a_{23}a_{31} + a_{33}a_{21}] \sin \beta \right) + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) \left([a_{13}a_{32} + a_{33}a_{12}] \cos \beta + [a_{23}a_{32} + a_{33}a_{22}] \sin \beta \right) + 4(a_{13}u_m + a_{23}v_m + a_{33}w_m)(a_{13}\cos \beta + a_{23}\sin \beta) - 2w_m(a_{13}\cos \beta + a_{23}\sin \beta) - 2(a_{33}u_m \cos \beta - a_{23}v_m \sin \beta) \right] \int_{L_1}^{L_2} Ax' e^{\frac{2\pi z}{\lambda}} \sin \psi dx' + \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)a_{33} + (a_{13}u_m + a_{23}v_m + a_{33}w_m)a_{31} \right] \int_{L_1}^{L_2} A e^{\frac{2\pi z}{\lambda}} \cos \psi dx' + \frac{2\pi}{\lambda} \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left(a_{33}a_{31} - [a_{13}\cos \beta + a_{23}\sin \beta][a_{11}\cos \beta + a_{21}\sin \beta] \right) + 2(a_{12}u_m + a_{22}v_m + a_{32}w_m) \left(a_{33}a_{32} - [a_{13}\cos \beta + a_{23}\sin \beta][a_{12}\cos \beta + a_{22}\sin \beta] \right) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) \left(a_{33}^2 - [a_{13}\cos \beta + a_{23}\sin \beta]^2 \right) + 2a_{13}\cos \beta(u_m \cos \beta + v_m \sin \beta - c) - 2a_{33}w_m + 2a_{23}\sin \beta(u_m \cos \beta + v_m \sin \beta - c) \right] \int_{L_1}^{L_2} Ax' e^{\frac{2\pi z}{\lambda}} \cos \psi dx' \right\}$$

- 18 -

$$(36) \quad M_z = \frac{\pi \rho h c}{\lambda} \left\{ \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m)(a_{12}\cos \beta + a_{22}\sin \beta) + (a_{21}u_m + a_{22}v_m + a_{32}w_m)(a_{11}\cos \beta + a_{21}\sin \beta) \right] \int_{L_1}^{L_2} A e^{\frac{2\pi z}{\lambda}} \sin \psi dx' - \frac{2\pi}{\lambda} \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left([a_{12}a_{31} + a_{32}a_{11}] \cos \beta + [a_{22}a_{31} + a_{32}a_{21}] \sin \beta \right) \right. \right. \\ + 4(a_{12}u_m + a_{22}v_m + a_{32}w_m) (a_{12}a_{32}\cos \beta + a_{22}a_{32}\sin \beta) + 2(a_{13}u_m + a_{23}v_m + a_{33}w_m) \left([a_{12}a_{33} + a_{32}a_{13}] \cos \beta + [a_{22}a_{33} + a_{32}a_{23}] \sin \beta \right) - 2w_m (a_{12}\cos \beta + a_{22}\sin \beta) - 2a_{32}(u_m \cos \beta - c) - 2v_m a_{32}\sin \beta \left. \right] \int_{L_1}^{L_2} Ax' e^{\frac{2\pi z}{\lambda}} \sin \psi dx' \\ - \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) a_{32} + (a_{21}u_m + a_{22}v_m + a_{32}w_m) a_{31} \right] \int_{L_1}^{L_2} A e^{\frac{2\pi z}{\lambda}} \cos \psi dx' \\ + \frac{2\pi}{\lambda} \left[(a_{11}u_m + a_{21}v_m + a_{31}w_m) \left(a_{32}a_{31} - [a_{12}\cos \beta + a_{22}\sin \beta] [a_{11}\cos \beta + a_{21}\sin \beta] \right) + 2(a_{21}u_m + a_{22}v_m + a_{32}w_m) \left(a_{32}^2 - [a_{12}\cos \beta + a_{22}\sin \beta]^2 \right) \right. \\ + 2(a_{31}u_m + a_{32}v_m + a_{33}w_m) \left(a_{32}a_{33} - [a_{12}\cos \beta + a_{22}\sin \beta] [a_{13}\cos \beta + a_{23}\sin \beta] \right) \\ + 2(a_{12}\cos \beta + a_{22}\sin \beta)(u_m \cos \beta + v_m \sin \beta - c) - 2a_{32}w_m \left. \int_{L_1}^{L_2} Ax' e^{\frac{2\pi z}{\lambda}} \cos \psi dx' \right] \}$$

References:

1. Cummins, W. E., Hydrodynamic Forces and Moments Acting on a Slender Body of Revolution Moving Under a Regular Train of Waves. David Taylor Model Basin Report 910 (1954)
2. Miles, J. W., Potential Theory of Unsteady Supersonic Flow. Chapter 12, pp 158-177. Cambridge, 1959

SELECTED BIBLIOGRAPHY

1. Cummins, William E., Hydrodynamic Forces and Moments Acting on a Slender Body of Revolution Moving under a Regular Train of Waves. David Taylor Model Basin Report 910 (Dec. 1954)
2. Cummins, William E., The Forces and Moments Acting on a Body Moving in an Arbitrary Potential Stream. David Taylor Model Basin Report 780 (June 1953)
3. Breslin, J. P. and Kaplan, P., Theoretical Analysis of Hydrodynamic Effects on Missiles Approaching the Free Surface, including the Influence of Waves. Stevens Institute of Technology, Sept. 1957
4. Kaplan, Paul, "Applications of Slender Body Theory to the Forces Acting on Submerged Bodies or Surface Ships in Regular Waves." Journal of Ship Research No. 3 of 1 (1957)
5. Kaplan, Paul "Virtual Mass and Slender-Body Theory for Bodies in Waves," Proceedings of the Sixth Annual Conference on Fluid Mechanics, University of Texas, Sept. 1959
6. Korvin-Kroukovsky, B. V., "Forces Acting on a Submerged Body Moving under Waves," Proceedings of the Fourth Midwestern Conference on Fluid Mechanics, Purdue University, 1955.
7. Goodman, T. R., Launching of Airborn Missiles Underwater, Parts I-IV. Allied Research Associates, Inc., Boston, Massachusetts.
8. Miles, J. W., Potential Theory of Unsteady Supersonic Flow, chapter 12, pp 158-177. Cambridge, 1959
9. Allen, J. H., Estimation of the Forces and Moments Acting on Inclined Bodies of Revolution of High Fineness Ratio. NACA Research Memorandum Number A 9126.