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ECONOMIC IMPLICATIONS OF A UNITED STATES SUPERSONIC TRANSPORT AIRCRAFT UPON AIRPORTS AND ENROUTE SUPPORT SERVICES

Volume II

Airports and Terminals

PRC R-890

31 December 1966

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LOS ANGELES, CALIFORNIA

Prepared for

Economics Staff Office of Supersonic Transport Development Federal Aviation Agency

PLANNING RESEARCH CORPORATION

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ECONOMIC IMPLICATIONS OF A UNITED STATES SUPERSONIC TRANSPORT AIRCRAFT UPON AIRPORTS AND ENROUTE SUPPORT SERVICES

VOLUME II AIRPORTS AND TERMINALS

PRC R-890

31 December 1966

Contract FA-55-66-15

By

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PLANNING RESEARCH CORPORATION LOS ANGELES, CALIF. WASHINGTON, D.C.

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CAPSULE REVIEW OF THE ECONOMIC ANALYSIS OF SST IMPACT UPON AIRPORTS AND ENROUTE SUPPORT SERVICES

The unique public costs to be incurred in airports and enroute support services as a result of the introduction of an SST are minimal; i.e., - zero to \$19 million.

Airports and Terminals	
(25 existing, potential SST)	zero to \$19 million
Enroute Support Services	zero
(Airways, Navigation, Communica- tions, Meteorology and Radiation)	

The public costs which would be incurred at existing, potential SST airports as a direct result of the introduction of succeeding aircraft types into scheduled airline service through 1975 were estimated to be \$33 million for the correction of pavement deficiencies at 25 major hubs from the present time through the introduction of the SST in 1974-5. The costs to government, Federal and local, for pavement improvement programs at the potential SST airports to adequately support the larger commercial airliners through the DC-8-63 would approximate \$14 million. Airport modifications imposed by the SST would cost an additional \$19 million. These potential improvements at airports represent public investment only and do not include airline and concessioner-financed facilities or airport modifications which are built with locally derived funding. Airport costs attributable to the SST are for modification programs only. New airport construction costs were not assessed against particular aircraft types because the designs of new hub airports programmed and under construction are based upon the total integrated requirements of civil aeronautics projected to 1990. Most hubs which serve traffic generating centers are today obsolescent—their designs having been based upon pre-jet, pre large-capacity aircraft criteria, thinking, and concepts. Limited with regard to size, location, and



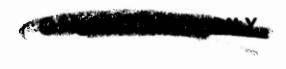
PRC R-890 iv

topography, the busier existing hubs are constrained within an economics viability envelope which in turn depends upon community support for its integrity. It is difficult, in fact unrealistic, to foresee extensive modification and expansion of existing hubs beyond 1975. Only the construction of wholly new commercial airport complexes to supplement or replace the existing overtaxed, inextensible airports can provide for continuing, orderly growth of air commerce into the supersonic and V/STOL era.

While the SST will require a \$19 million investment to strengthen pavements at airports it will initially serve, the total airport situation within the United States during the next four years will require a minimum investment of \$2 billion. The air traffic (both passenger and cargo) preference increase of the mid-1960's should continue unabated into the 1970's. Airports—without the SST as a consideration—are today a problem of national scope.

Examination of the adequacy of enroute support services disclosed that there are no identifiable costs which can be considered unique to the SST, or in fact, unique to any aircraft type. The trend in airways, navigation, and communications systems design is to provide independent, accurate, and reliable avionics systems within the aircraft and to lessen the dependency upon externally oriented systems. The expansion and improvement of air commerce support activities to keep pace with traffic growth are evolutionary technological advances which increase civil aeronautics capabilities. Meteorological and radiation systems thought to be required for safe and efficient flight of the Concorde and SST are already planned and programmed to be in operation prior to commercial flights by the SST. Any unique requirements which might evolve out of future studies in these areas (for example, the need for clear air turbulence detection systems) would probably result in airborne systems to satisfy these requirements rather than in additional external enroute support services. Such airborne systems would become integral parts of the aircraft and thus become an airline expense. It may therefore be stated that the SST will not require unique expenditures for enroute support services.



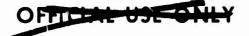


PRC R-890 v

Environmental enroute support systems requirements are essentially the same for both the Concorde and the SST. Utilizing a cost allocation technique whereby the first aircraft type to need a service is assigned the entire investment (as well as) operation and maintenance costs during the periods of exclusive benefit, the Concorde would be allocated these costs since it is scheduled for commercial airline service approximately three years prior to the SST.

Exhibit i presents the expenses identifiable only with the field of aviation and which would be financed by Federal, state, or local funds. This chart allocates these costs by aircraft type according to forecast entry into commercial service.

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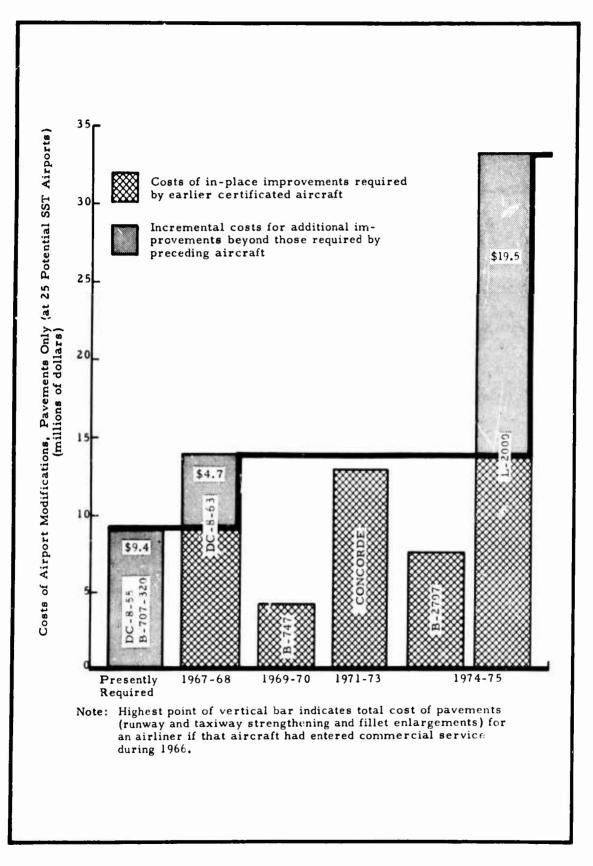


EXHIBIT i - INCREMENT AL PAVEMENT IMPROVEMENT (PUBLIC) COSTS AT 25 POTENTIAL SST AIRPORTS

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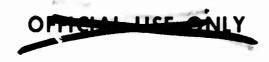
ABSTRACT

The economic impact of advanced high-capacity airliners upon the ground environment--airports and terminals--is examined in this volume. The modifications required to achieve compatibility with each of the four airliners:

- stretched subsonic (DC-8-63)
- high-capacity subsonic (B-747)
- Concorde
- United States SST

which will enter commercial service up to 1975 are defined for selected airports, and the costs of the aircraft-sponsored improvements are estimated.





1.

PRC R-890 ix

TABLE OF CONTENTS

		-	Page			
CAPS	SULE I	REVIEW	iii			
ABST	RACT	· · · · · · · · · · · · · · · · · · ·	vii			
I.	INTR	ODUCTION	1			
II.	OBJE	CTIVES	3			
III.	EFFORT PLAN					
	Α.	Methodology	5			
	в.	Implications	5			
	C.	The Airport Questionnaire	6			
IV.	COST	ALLOCATION TECHNIQUE	9			
	А.	Cost Allocation	9			
	в.	Cost Recovery	10			
v.		ONALE FOR SELECTION OF POTENTIAL	13			
VI.		LYSIS OF PAVEMENT ADEQUACY AT SELECTED OR'TS FOR LARGE COMMERCIAL AIRCRAFT	17			
	Α.	Methodology for Determining Overlays Required	17			
		 Bituminous or Flexible Overlays on Flexible Pavement	17			
		2. Bituminous or Flexible Overlays on Rigid Pavement	17			
		3. Portland Cement Concrete Overlays on Rigid Pavement	17			
	в.	Pavement Adequacy Determination	19			
	C.	Pavement Strengthening Costs at the Selected Airports	39			
VII.		FICATIONS TO POTENTIAL SST AIRPORTS ESTIMATES OF NON-AIRLINE COSTS	89			





PRC R-890 x

TABLE OF CONTENTS (Continued)

				Page	
	Α.		nary of Airport Pavement Strengthening	89	
	в.		nary of Other Pavement Costs at ted Airports	92	
	C.		usions Regarding Pavement and tural Modification Costs	97	
VIII.			PARTICIPATION BY THE FEDERAL ENT IN AIRPORT DEVELOPMENT	101	
	А.	The N	lational Airport Plan	101	
		1.	Background	101	
		2.	The National Airport Plan, FY 1966-70		
		3.	Federal Aviation AgencyCivil Aeronautics Board	112	
	B. Federal-Aid Airport Program				
		1.	Federal Airport Act	113	
		2.	Programmed Assistance in Airports Development	113	
			a. New or Replacement Airports	114	
			b. Area or Regional Airports	114	
			c. Airports to Relieve Congestion	115	
			d. Long-Range Planning	115	
		3.	Allocation of Federal Funds	115	
			a. Rationale	115	
			b. Priorities Schedules	116	
	c.	Proba	ble Federal Assistance beyond 1970	116	
IX.	CONC	LUSIC	ONS	119	
х.	RECO	OMMEI	NDATIONS	121	
	А.	Identi	fication of Potential Gateway Airports	121	



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PRC R-890 xi

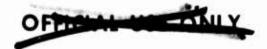
TABLE OF CONTENTS (Continued)

Page

1246.462

	в.	New Airport Construction Programming 121
	C.	Standardized Pavement Analysis Method 122
	D.	Airport Adequacy Survey 122
XI.	SOUR	CES





PRC R-890 xiii

LIST OF EXHIBITS

]

Contraction of

1

80

Page

1.	Potential SST Airports Seen against Population	
••	Density	16
2.	Design Chart for Concrete Overlays	20
3.	Pavement Strengthening Costs	90
4.	Pavement Strengthening Costs (by Aircraft) for Potential SST Airports as they Exist in 1966	91
5.	Fillet Requirements	94
6.	Fillet Modification Costs (by Airport)	96
7.	Incremental Pavement Improvement (Public) Costs at 25 Potential SST Airports	98
8.	Recommended Development of 28 Selected Airports in the 1966 National Airport Plan	102
9.	National Airport Plan Statistical Summary	105
10.	Summary of Estimated Required Airport Development Cost by Item by State, Fiscal Years 1966-1970	108



. - . 182

1



I. INTRODUCTION

In support of the Supersonic Transport Development Office of the Federal Aviation Agency, Planning Research Corporation performed a cost definition analysis of the economic implications to free world governmental authorities which would result from improvements and modifications to airways and ground support facilities because of the introduction of a supersonic transport (SST) into scheduled commercial service by U.S. and foreign airlines.

The government-provided support to the SST examined in the total study concerns two distinct areas:

- The Ground Environment; i.e., Airports and Terminals
- Enroute Support Services; i.e., Airways, Navigation, Communications, Meteorology, and Radiation.

Each of these areas was examined to determine the nature and associated costs of the facility modifications and improved support capabilities which may be required in the time period 1967-1975 by the existing subsonic jet family as well as by the improved passenger transport aircraft which may join or succeed them. This approach was necessary so that the costs of each facility and support improvement might be allocated among all commercial jet aircraft which may require or derive benefit from those improvements. In this way, it was possible to assign to the SST only its appropriate share of the estimated costs. Proportionate shares were allocated among current subsonics, stretched subsonic aircraft (DC-8-63), high-capacity subsonic aircraft (Boeing 747) and the supersonic Concorde.

This volume examines the government-provided support which the SST may require at airports.





II. OBJECTIVES

The purpose of this aspect of Planning Research Corporation's study was to identify major costs which may have to be incurred in qualifying potential gateway airports for scheduled SST commercial service.

Adequacy of selected airports for operation of an SST (either the Boeing Model 2707 or the Lockheed L-2000) was examined within the context of the environment predicted to exist at the introduction of an SST into scheduled commercial service--about 1974-1975. Competing aircraft types considered in this study were:

- current subsonics (B-707-320, DC-8-55)
- stretched subsonics (DC-8-63)
- high-capacity subsonics (B-747 and L-500)
- Concorde

It was not intended to ignore or to repeat the excellent, thorough airport compatibility studies which each competing SST airframe manufacturer recently completed, or that work performed by the able staffs of 15 cooperating airport authorities. Rather, the approach of PRC was to independently validate and update these efforts, to perform similar evaluations of 13 additional airports, and to expand the scope of these airport studies, identifying and time-orienting the discrete improvements necessitated by each of the five competing aircraft types.

In this manner, the costs associated with each improvement could then be attributed to a particular aircraft-type or allocated among competing aircraft, as appropriate.





III. EFFORT PLAN

A. Methodology

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The goal of the study was to determine the costs of improvements which domestic airports may be required to make to qualify for future commercial passenger aircraft. To achieve that objective, it was first necessary to select those centers of population which are now (1966) or have the potential to become gateway terminals by 1975, when the SST is expected to enter commercial service. With the aid of the experienced judgment within the aviation community and the Federal Aviation Agency 28 terminals were selected.

The plan then was to brief selected airport operators during the spring 1966 AOCI Conference in Washington, D. C., and to mail to each selected airport authority a copy of a uniform questionnaire which PRC had devised as the basis for data gathering at the airports. The intent was to take as little as possible of the consultants' and the airport operator's time during the visit. Each addressee was urged to review the questionnaire prior to the visit and either prepare his response or select and supply information which would permit a joint completion of the questionnaire. The airport operator was given the option to provide, during the visit or by mail thereafter, the materials from which the Planning Research Corporation professional staff members could construct his response. In addition, vice presidents for property and facilities of the major carriers and/or their staffs were interviewed. In this manner, the airport study benefitted from the comments and valued judgments of both the landlords and their tenants.

B. Implications

In 1965-1966 SST surveys of gateway airports conducted by the competing airframe designers during the SST Development Program, the Boeing Company measured airport compatibility at each of 15 facilities in relation to its SST design. The Lockheed California Company did the same for its competing entry. Each of these two distinct and separate studies





concluded that existing and planned facilities could, with minimal modifications, accept scheduled commercial operation of an SST. Boeing and Lockheed indicated that modifications in certain areas will be required. Cost estimates of each of these opportunities for improvement for the 15 airports were also developed.

Unlike the two above-mentioned studies, the Planning Research Corporation effort did not sample gateway airports to determine expected SST impact upon the ground environment. PRC instead selected those major United States hubs which are now gateway airports (including the 15 sites studied by Boeing and Lockheed for compatibility with their respective SST designs), in addition to others with the traffic-generating potential to become international air terminals by 1975, the scheduled first full year of SST commercial operation.

While Boeing and Lockheed in their Phase II studies considered the SST as the next generation of commercial jets to join airline fleets, the Planning Research Corporation study assessed SST-airport compatibility in the context of a more realistic environment. PRC examined the serial airport modifications sponsored by: continuing preference for air traffic over competing surface transportation modes; increased capacity, stretched DC-8 subsonic airliners; the commercial, high-capacity subsonic, Boeing 747; the foreign, free world Concorde; and the United States supersonic transport, the SST. As a consequence, the capital investment costs to qualify major hub airports for SST operation developed by PRC are less than those derived by applying data from the Boeing and Lockheed airport compatibility studies.

C. <u>The Airport Questionnaire</u>

The Airport Operator Questionnaire was prepared to achieve the following goals:

- Provide uniform information about the physical facilities at each of the selected, potential SST airports.
- Minimize the effort, time, and other resources required of each airport authority.





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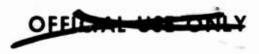
• Guide and control discussion during the visit to each airport by members of the FAA Economics Staff for SST Development and Planning Research Corporation consultants.

 Provide consistent, valid, and unambiguous information to serve as the basis for an economic analysis of the impact of advanced design commercial passenger aircraft upon airports and terminals.

The questionnaire provided for orderly representation of the existing facilities at each airport and indication of improvements required by the planned high-capacity aircraft, including the SST. Each entry was based upon engineering studies or experienced judgment. Where available, estimates of the costs of each improvement (i.e., investment) were also included. Those areas whose adequacy is assured were so identified.

The improvements or modifications required by each aircraft-type were defined against either the existing physical facilities or (if engineering changes were in progress) the physical plant as it will exist upon completion of the construction program now underway.

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IV. COST ALLOCATION TECHNIQUE

Because the SST will not join airline fleets until 1974-1975, it was necessary to also investigate and identify the impact to airports and airways of those aircraft types which will precede an SST into commercial airline service. The total study effort was directed toward allocating--for each ground facility and enroute support service improvement which may be required by an SST and/or by other advanced high-capacity aircraft--the U.S. supersonic transport's appropriate share of the estimated public costs, attributing proportionate shares among the:

- current subsonic family
- stretched subsonics (DC-8-63)
- high-capacity subsonics (B-747)
- Concorde

A. Cost Allocation

The cost allocation methodology employed is applicable only to commercial aviation, i.e., to the common carriers, and deliberately excepts general aviation and national defense activities. Where national defense programs were identified, which also benefit any of the abovementioned aircraft, costs associated therewith were separately accounted for. An example of such a defense program is research into radiation effects upon aircrews of very high-altitude aircraft, such as the U-2, RB-57F, and XB-70. Costs identified in this study are those for research and development and for procurement and construction.

The technique for cost allocation is straightforward. Modifications which would be required because of increased air passenger traffic, normal programmed maintenance, and obsolescence and exhaustion of existing facilities and systems (if only those aircraft now in commercial service were to be considered) were made the cost baseline. Incremental improvements and modifications beyond this cost datum were identified with one of the four advanced aircraft types which are expected to join airline fleets by 1975.



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PRC R-890 10 v

Allocation was a function of time. Costs were allocated by order of precedence among the five potential modifications sponsors (DC-8-55, Boeing 707-320; DC-8-63; Boeing 747; Concorde, SST). This approach is historically self-sustaining. Current Department of Defense practice for cost analyses of weapons systems assumes all prior investments as "sunk costs;" i.e., costs which were incurred at a point in time which antedates the current program. It follows, then, that if aircraft Y requires facilities or service modifications in 1970 which are beyond the normal planning baseline, but less than those required by aircraft X in 1968, X would be assigned the total costs of the incremental modifications beyond the cost datum. These would be considered "sunk costs" for aircraft Y and Y would enjoy the benefit of the improvements without sharing the investment costs. It is not intended to infer, however, that in reality the actual recovery of costs would be so straightforward. Improvements at airports are usually financed by a revenue bond issue. The bonds then are retired with airport revenues; e.g., concessionershared earnings, property utilization and rental income, and landing fees imposed upon all using aircraft. Landing fees are based upon aircraft takeoff or landing weight and frequency of operation.

B. Cost Recovery

Cost allocation is a management tool for guiding the decision maker in choosing among available alternatives:

- whether to construct "system" A, B, C, or D
- whether a mix or combination of "systems" would be preferable
- whether to construct any of the proposed "systems."

Intended and developed solely as one of many predecision guides for weighing opportunities for action, cost allocation attempts to predict and approximate the investment (the resources commitment) which each of the feasible options would require. Cost allocation is <u>not</u> a plan for recovering the resources commitment once the (selected) system becomes fully operational. That process is called "cost recovery." Cost allocation occurs before the fact--prior to the decision. It is a management tool. Cost recovery





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occurs after the fact--after a new system becomes operational. It is the product of a management decision. In the real world, cost recovery defines precisely and according to sound accounting principles the contract between landlord and tenant in economic terms.

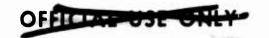
Within the aviation community, the rationale and procedures which are actually observed for determining "how to pay" for an improvement are quite different from those followed in predecision cost allocation.

Once the Equirement for a particular airport improvement program has been successfully demonstrated and the probable capital investment estimated, it is necessary to develop a detailed plan for recovering all costs, including financing charges. Public approval of a revenue bond issue is essential, together with support of the financial community and the ability and willingness of concessioners, air carriers, general aviation, and other benefitting users to support the required financing program within the structure of appropriate user charges. An airport cannot commit itself or its operating authority to a capital investment program without first having devised a sound cost-recovery plan. Almost without exception, cost-recovery capabilities exercise a controlling influence upon the size and scheduling of an improvement program on the airport.

The SST will bear its fair share within the cost-recovery plan for capital improvements at the airports it will serve, even if such modifications are completed prior to the SST entry into airline service. An improvement to the landing area would be paid for jointly by all benefitting aircraft. The SST, together with other using commercial and general aviation aircraft, will pay landing fees based on aircraft weight and flight frequency.

Further, if the SST requires that planned improvements at an airport be accomplished earlier than scheduled, the costs thereof would be allocated as described previously, but actually recovered as user-charges from all aircraft using that airport. Improvements to the terminal complex are not formally paid for within the landing fee structure. Instead, tenants (airlines and concessioners) within the terminal area defray the costs through readjustment of lease and rental agreements and pass on these costs to the customers and air travelers in fares and services and commodities prices.

USE



V. RATIONALE FOR SELECTION OF POTENTIAL SST AIRPORTS

Planning Research Corporation recognized two approaches which could be taken to determine the economic impact of an SST upon airports. The first would be to sample gateway airports and to suggest, from the study results, an average cost to qualify an international air terminal for the commercial SST service. Essentially, this was the method used by the FAA in sponsoring the Phase II airport compatibility studies by the two airframe design competitors.

PRC chose to discard this philosophy because the Boeing and Lockheed airport surveys had as their primary purposes the measurement of the "degree of fit" between each SST design and specified gateway airports. Further, 1975 (the first full year of SST commercial operation) is only 9 years into the future. This permits valid selection of potential SST airports because of the short time frame. It should be noted that the PRC effort is primarily directed toward assessing modification costs associated with a United States SST, not toward providing a basis for source selection. Having discarded the sampling concept as inadequate to the study goals, PRC established the following criteria for selection of potential SST airports up to the year 1975:

- Inclusion of all 15 gateway airports studied by Boeing and Lockheed.
- Inclusion of those major airports, medium or large hubs, which serve principal centers of population and which by 1975 should be able to originate or attract international air
 t ffic, passenger business, and tourist travel, as well as a cargo.
- Consideration of those airports recommended by the Airport Operators Council International.
- Consideration of those airports suggested by the FAA.



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Exercising these criteria, PRC selected the following 28 airports for evaluation within this study effort. Of the 28 airports, 3 were new airports presently under construction: Dallas-Fort Worth Regional Airport, Houston Intercontinental Airport, and Mid-Continent International Airport (Kansas City, Missouri). Construction of an entirely new terminal complex at Tampa International Airport was scheduled to begin before the end of calendar 1966.

Fifteen of the airports were previously examined in detail by each of the competing SST airframe manufacturers during Phase II of the FAA supersonic transport development program. These airports are identified by an asterisk in the following listing.

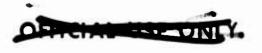
> Anchorage International Airport* Atlanta Airport Cleveland Hopkins International Airport Dallas-Fort Worth Regional Airport Detroit Metropolitan Wayne County Airport* Dulles International Airport (Washington, D.C.)* Friendship International Airport (Baltimore, Md.)* Greater Pittsburgh Airport Honolulu International Airport* Houston Intercontinental Airport John F. Kennedy International Airport (New York City)* Lambert-St. Louis Municipal Airport Logan International Airport (Boston, Mass.)* Los Angeles International Airport* Metropolitan Oakland International Airport Miami International Airport* Mid-Continent International Airport (Kansas City, Mo.) Minneapolis-St. Paul International Airport New Orleans International Airport O'Hare International Airport (Chicago, Ill.)* Philadelphia International Airport* Portland International Airport* Puerto Rico International Airport

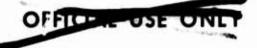


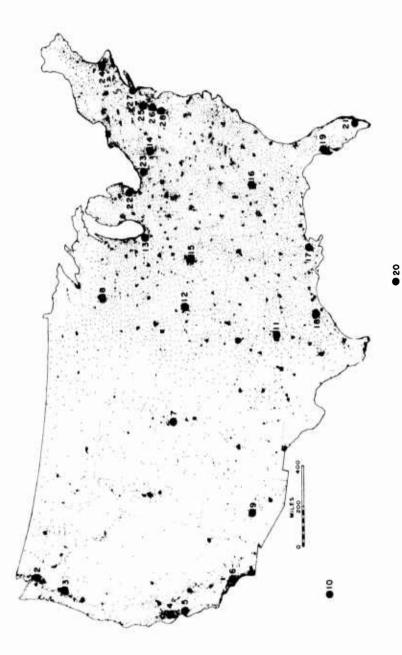


San Francisco International Airport* Seattle-Tacoma International Airport* Sky Harbor Municipal Airport (Phoenix, Arix.) Stapleton International Airport (Denver, Colo.) Tampa International Airport

The selected airports are depicted in relation to population density in Exhibit 1.





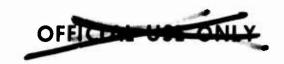


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19 TAMPA International	20 PUERTO RICO International	21 MIAMI International	22 DETROIT Metropolitan	23 CLEVELAND HOPKINS International	24 LOGAN International
13 CHICAGO O'HARE International	14 GREATER PITTSBURGH	15 LAMBERT-ST, LOUIS Municipal	16 ATLANTA	17 NEW ORLEANS International	18 HC "STON Intercontinental
7 STAPLETON International (Denver)	8 MINNEAPOLIS- ST. PAUL International	9 SKY HARBOR Municipal (Phoenix)	10 HONOLULU International	11 DALLAS- FT. WORTH Regional	12 MID-CONTINENT International (Kansas City)
I ANCHORAGE International	2 SEATTLE-TACOMA International	<pre>3 PORTLAND International</pre>	4 Metropolitan OAKLAND International	5 SAN FRANCISCO International	6 LOS ANGELES International

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EXHIBIT 1 - POTENTIAL SST AIRPORTS SEEN AGAINST POPULATION DENSITY



VI. ANALYSIS OF PAVEMENT ADEQUACY AT SELECTED AIRPORTS FOR LARGE COMMERCIAL AIRCRAFT

A. Methodology for Determining Overlays Required

There are several types of overlays that can be used to strengthen inadequate pavements. Those that will be considered here are (1) bituminous or flexible overlays on flexible pavement; (2) bituminous or flexible overlays on rigid pavement; and (3) Portland Cement concrete overlays on rigid pavements.

1. Bituminous or Flexible Overlays on Flexible Pavement

The FAA and the Corps of Engineers agree, in a situation where inadequate flexible pavement is found, that

$$t = h - h_e$$

where

t = thickness of needed flexible overlay

h = required thickness to support anticipated load

h = thickness of existing flexible pavement

An adjustment is allowed by FAA if the existing surface course is in good condition. It is then counted as 1-1/2 inches of base per inch of existing bituminous surface. Minimum bituminous overlay is 3 inches. If a base course is used in the overlay, it should have a minimum thickness of 4 inches.

2. Bituminous or Flexible Overlays on Rigid Pavement

FAA recommends a design procedure utilizing the formula

$$t = 2.5 (Fh - h_{e})$$

where F = a factor representing the strength of the subgrade varying from 0.8 for firm subgrades to 1.0 for the softer soils.



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PRC R-890 18

An adjustment for an all-bituminous overlay is allowed in which each inch of flexible overlay (including base course) is equal to 1.5 inches of all-bituminous overlay.

Extensive trials of this procedure during the present study have not produced congruous results, however. As an example, the L-500 at Seattle-Tacoma International Airport requires 10 inches of concrete. Critical portions of runway 16-34 are 12 inches thick, but other portions have 8 inches of concrete with a 5-inch bituminous overlay. With the use of the above procedure and the reasonable assumption that a k value of 300 can be considered a firm subgrade,

> $t = 2.5 (0.8 \times 10 - 8)$ t = 0

This infers that no overlay is needed, which surely is not the case, because 10 inches of concrete are required (derived from the Westergaard analysis) and only 8 are provided.

On another section of the same runway, only 6 inches of concrete under an 8-inch bituminous overlay have been provided. Thus,

> $t = 2.5 (0.8 \times 10 - 6)$ t = 5

The adjustment for all bituminous overlays may be used in this situation.

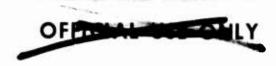
$$t = 5/1.5$$

 $t = 3.3$

Adding the result to the 6-inch concrete, the total concrete and bituminous pavement combination requirement is 9.3 inches, less than the equivalent single-slab concrete requirement.

Because of such unreasonable results, which occur with alarming frequency and without apparent cause, the overlay thicknesses computed by this formula have been adjusted where necessary to bring about a





degree of conformity to reason. Although arbitrary by nature, this procedure seems to be warranted under the circumstances. Determination of a more correct mathematical solution to this design problem may be possible, but is outside the present effort.

3. Portland Cement Concrete Overlays on Rigid Pavement

The Portland Cement Association has developed a procedure for determining the thickness of rigid overlays on existing rigid slabs. It uses the formula:

$$h_{c} = \sqrt{h^{1.87} - Ch_{e}^{2}}$$

where

h

= required rigid overlay

h = equivalent single slab thickness requirement

h_a = existing rigid pavement thickness

C = a factor for condition of existing pavement, from
 0.35 for badly cracked or crushed concrete to 1.0
 for good condition.

Exhibit 2 which follows is a graphical representation of the formula in the relevant range, and may be used to determine overlay thicknesses for this case.

B. Pavement Adequacy Determination

The eight aircraft being considered are compared as to their effect on airport pavements on the 25 existing potential SST airports in the tables which follow this section. The requirements for upgrading of pavements are discussed for each airport in turn. These requirements are expressed for each of five groups of aircraft: current jets, stretched jets, high-capacity subsonic jets, Concorde, and the SST. Pavement overlay thicknesses are computed for the aircraft of each group having the greatest requirement.

In the tables, the induced stress in psi on the present rigid pavement is shown under each aircraft. The required pavement thickness is also shown to the nearest half inch just below the stress.

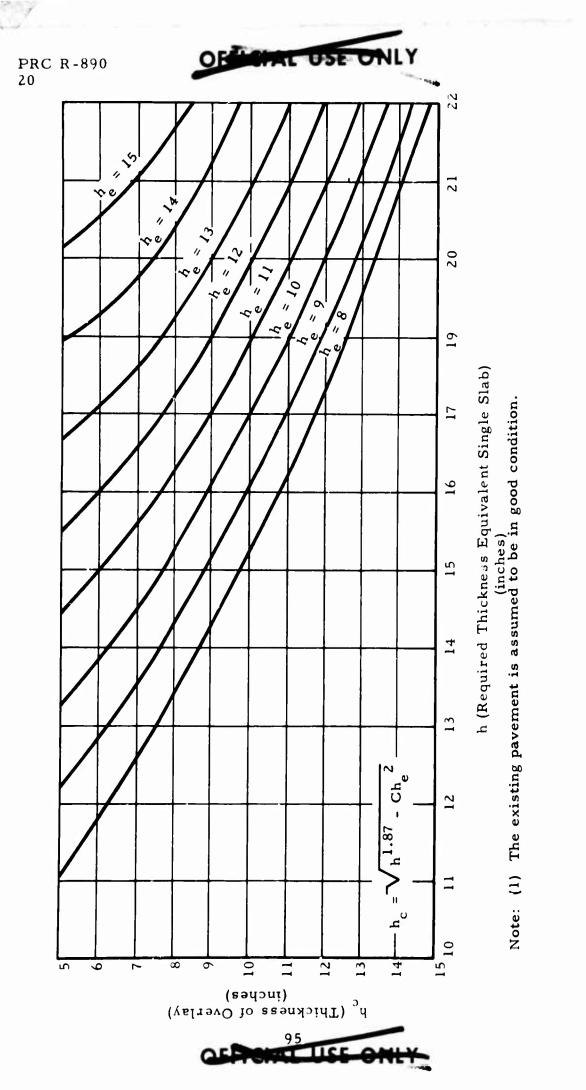


EXHIBIT 2 - DESIGN CHART FOR CONCRETE OVERLAYS⁽¹⁾



When an overlay presently exists on rigid pavement, the requirement is shown as the existing rigid pavement plus the bituminous overlay required for each airplane.

1. Anchorage International Airport

All pavements at Anchorage are of flexible construction. The FAA subgrade classification is F6. No CBR rating is available.

Minimum thickness of applicable flexible pavement is 35 inches. This thickness appears slightly inadequate for the L-2000. However, the ground rule of 95 percent weight on main gear is conservative for this airplane, and no additional pavement is believed to be required.

All other flexible areas are 37 inches thick and are considered adequate.

2. Friendship International Airport, Baltimore

All pavements at Baltimore are of flexible construction except small areas near the terminal. The FAA subgrade classification is Fl, and the CBR rating has been stated as 25.

Both the pavement constructed in 1950 (20-inch depth) and the later pavement (25 inches) are sufficient for the aircraft loads being considered.

3. Logan International Airport (Boston, Massachusetts)

An FAA subgrade classification of F6 at Logan International results in a requirement of 38 inches of flexible pavement for the L-2000. Other aircraft being considered have requirements of less than 38 inches. Since all runway areas (both critical and noncritical) are flexible pavement of 42-inch thickness, no additional pavement is required. Aprons near the terminal are constructed on an extremely deep gravel fill, which together with the 39-inch flexible pavement, provides adequate strength.

4. O'Hare International Airport (Chicago, Illinois)

Flexible pavements at O'Hare, with a subgrade rating of F4, are sufficiently thick for the aircraft considered in the study.

Rigid pavements, however, are designed for a maximum allowable stress of 330 psi. Allowable stress in noncritical areas has been increased to 440 psi to account for a lower safety factor. The subgrade is





reported by airport authorities to be k = 190 and k = 250. Using the thickness requirements resulting from the Westergaard analysis previously described, neither the 15-inch critical nor the 11-inch noncritical pavement on runway 32L-14R is sufficient for unlimited stress. Major taxiways and the terminal area are also of insufficient thickness.

Since bituminous leveling courses have been placed in certain areas of runways and taxiways, it is assumed that upgrading of these areas would be done with bituminous material. Required overlays are:

	On 15-inch concrete	On 11-inch concrete
Current jets	2	2
Stretched subsonics	2	3
High-capacity subsonics	0	0
Concorde	2	2
SST	7	6

5. Detroit Metropolitan Wayne County Airport

Rigid pavements at Detroit were designed for a maximum allowable stress of 350 psi. The allowable stress is increased in noncritical areas by 1/3, since it is assumed that for a critical area safety factor of 2, the noncritical area safety factor would be 1.5. The maximum allowable stress in critical areas of 350 psi, however, was not arrived at by arbitrary application of a safety factor, but was furnished by airport officials. All of the aircraft being considered create overstress conditions on all critical pavements, with the exception of the L-500.

With the use of bituminous overlays the following inches of overlay are required:





Critica	Noncritical Areas	
13-inch	12-inch	<u>ll-inch</u>
3	5	2
4	6	2 - 1 / 2
2	3-1/2	0
4	6	2 - 1 / 2
8	9	5
	<u>13-inch</u> 3 4 2 4	3 5 4 6 2 3-1/2 4 6

The overlay required is for the maximum induced stress, which is caused by the DC-8-55 in the current jet group, and the B-747 in the high-capacity group. The DC-8-63 is, of course, alone in the stretched jet category. Of the SST's being considered, the Lockheed model produces the greatest stress and the Boeing design the least.

6. <u>Honolulu International Airport</u>

Both rigid and flexible pavements are in use at Honolulu. Civil transports use runway 8-26, the west end of which extends onto Hickam Air Force Base property.

Subgrade classifications for both the Corps of Engineers and FAA calculations are available, but vary considerably because of the native soil conditions, ranging from coral rock to swamp mud. For thickness calculations, a minimum of F9 and CBR 4 have been used. CBR 15 was found applicable in the areas of more stable subgrade.

The FAA methodology indicates all flexible pavement is adequate. Only marginal deficiencies are found using the Corps of Engineers method except for the L-2000 where 7 inches of asphalt overlay is required for the critical area of runway 8-26 and taxiway A.

The L-2000 overstresses the Portland Cement concrete at the Hickam Field end of runway 8-26. However, it is the only aircraft which creates an overstress, and it is not sufficient to justify an overlay in this case because the concrete strength is not accurately known.

The 12-inch concrete terminal apron, however, is overstressed by five of the eight aircraft considered.



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The bituminous overlays required are as follows:

Current jets	2-1/2	inches
Stretched subsonics	3	inches
High-capacity subsonics	0	inches
Concorde	3	inches
SST	6	inches

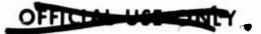
7. Los Angeles International Airport

Both rigid and flexible pavements are in use at Los Angeles. The subgrade west of Sepulveda Boulevard has ratings of Fa, CBR 10, and k = 250 to 300. East of Sepulveda the ratings are F5, CBR 5, and k = 300. Allowable stress for rigid pavements has been set at 400 psi and raised to 533 psi in noncritical areas.

Portland Cement concrete thicknesses of 15, 12, and 10 inches are used. The modulus of subgrade reaction is 300 for all except the 10-inch pavement, where it is rated at 250. Stresses in the 10-inch pavement are in excess of that allowed for three of the aircraft in the study. However, the other parallel runway which is stronger could be used.

Twelve-inch critical pavements are overstressed by 8 percent by the current jets. Since performance to date has been satisfactory, no change is deemed necessary. Stretched jets and the Concorde induce a 12-14 percent overstress. High-capacity jets induce less than allowable stresses but the L-2000 overstresses this area by 28 percent. If bituminous overlays are used, the DC-8-63 will require a 2-1/2-inch overlay, and the L-2000 will require 4.5 inches. No overlay is required for the other aircraft.

Flexible pavements were analyzed by both FAA and Corps of Engineer's methods, and a surprising variance in results was obtained. Necessary thicknesses are believed closer to the Corps of Engineers results than to the FAA figures at this airport, however, because areas designed by the latter method have proved a source of pavement problems. There is a possibility that the subgrade tests of the two methods were not taken under controlled conditions.





As seen in the attached flexible airport paving chart for Los Angeles, critical portions of runway 7L-25R do not meet requirements but, as stated above, a parallel runway could be used. Therefore, no overlay is recommended for this runway.

Certain noncritical areas of runways 7R-25L are also deficient. Current jets and the Concorde would require 6 inches of additional bituminous pavement, stretched jets 7 inches, high-capacity jets 8 inches, Concorde 6 inches, and SST 14 inches.

Taxiway 2J requires overlays of 9, 12, 18, 9, and 25 inches for the current, stretched, high-capacity, Concorde and SST, respectively.

Taxiway 53J and portions of K require additional pavement. Amounts are 9 inches for current jets and Concorde, 10 inches for DC-8-63, 11 inches for high-capacity jets, and 18 inches for SST.

Runway 25L-7R in its flexible section, critical portion, requires 4.5 inches of additional pavement for L-2000 operations. Terminal aprons of flexible construction also need a 4.5-inch overlay for the L-2000.

8. John F. Kennedy International Airport, New York City

Pavements at JFK are, for the most part, constructed of Portland Cement concrete. Runway pavements are designed for a maximum allowable stress level of 430 psi, and other rigid pavements for a level of 365 psi. Subgrade reaction modulus is k = 300.

The table below indicates the induced stresses, as a percentage of allowable stress, for the aircraft being considered. Annotations are t = thickness, k = modulus of subgrade reaction, and $S_2 = allowable$ stress.

								•		
		c	L-	В-				DC-		DC -
t	<u>k</u>	<u>a</u>	2000	2707	Concorde	<u>B-747</u>	<u>L-500</u>	8-63	<u>B-707</u>	8-55
12	300	430	119	94	105	88	77	106	98	100
13	300	365	129	100	112	95	82	112	104	106





PRC P-890 26

Except for the L-2000, these aircraft create runway stresses within acceptable margins. The L-2000 stress levels indicate that an overlay of 3 inches of bituminous material is necessary at critical areas of the 12-inch concrete to support unlimited load repetitions.

The DC-8-63 and the Concorde runway stresses, while in excess of that allowed, do not justify an overlay. In this analysis, it was assumed that 95 percent of the weight was on the main gear but there are indications that this may be conservative.

The 13-inch rigid pavement, because of lower allowable stress, will require bituminous overlays of 0, 2.5, 0, 2, and 4.5 inches for the current jets, stretched jets, high-capacity jets, Concorde, and SST, respectively.

Flexible pavements at JFK require 2, 2, 2, and 8 inches of additional pavement to serve the stretched and high-capacity jets, Concorde, and SST, respectively.

Only runway 13R-31L was considered for costing overlays.

9. Miami International Airport

Both flexible and rigid pavements are in use at Miami. The CBR value given is 60, and an FAA subgrade classification of Fa has been obtained. Using these values, it has been determined that all flexible pavements are adequate.

Most terminal aprons and short sections of the runways are made of Portland Cement concrete. The subgrade value is k = 400, and allowable stress varies from 350 on the 10-inch to 400 on the 8-inch concrete. For noncritical sections, this stress has been adjusted upward to account for a safety factor of 1.3. A portion of the terminal area, where concrete is of 8-inch depth, has received a 3-inch asphaltic overlay. Other 8-inch concrete in the terminal area is scheduled for a 3-inch minimum overlay in the near future.

Even with the present and projected overlays, the 8-inch concrete aprons are deficient. Need for an additional bituminous overlay of 4 irches for current jets, 4.5 inches for the Concorde and stretched jets, 2 inches for the high-capacity jets, and 7 inches for the SST is estimated.



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There are several small areas of 6-inch concrete, but it must be assumed that they do not and will not receive the loads of the large jets. If passage over these areas by large jet transports is foreseen, their thickness should be at least doubled by concrete overlays.

Eight-inch concrete at portions of the runways is also inadequate. Flexible overlays required are 7, 7, 5, 7, and 9 inches for current jets, stretched jets, high-capacity jets, Concorde, and SST, respectively.

Apron areas which are constructed with 10-inch concrete require overlays of bituminous material of 4, 5, 2, 5, and 6 inches for current stretched, high-capacity, Concorde and SST jets, respectively. Bituminous overlays have been used in these estimates because of the choice of this material by airport officials in the past.

For costing purposes, only runway 9L-27R was considered. This runway is of flexible construction.

10. Philadelphia International Airport

All runways and a portion of taxiways at Philadelphia are of flexible construction. Both FAA and Corps of Engineers evaluation procedures show them to be adequate for all aircraft under study.

Rigid pavements, including terminal apron and certain taxiways, are of 12-inch thickness, and airport engineers claim the subgrade to be k = 250. They also recommend using the relatively low allowable stress of 295 psi, due to experience with the pavement in the past. The analysis shows this concrete to be of insufficient thickness for all of the aircraft considered. The required thicknesses of bituminous strengthening course for the various airplates are these:

L-2000--12 in. B-2707--6.5 in. Concorde--8 in. B-747--5 in. L-500--2.5 in. DC-8-63--8 in. B-707--6.5 in. DC-8-55--7.5 in.

11. Portland International Airport

As presented in the accompanying chart for Portland, a slight discrepancy exists between requirements indicated by the FAA procedure and thicknesses suggested by the Corps of Engineers method. Airport authorities maintain that the values of F4 and CBR 15 should be used for





runway 10R-28L and adjacent taxiways, and that a CBR of 10.6 is to be used for runway 10L-28R and its major taxiway. F2 and CBR 15 are used at the apron area. The L-2000 is the only aircraft shown by the analysis to be incompatible with existing pavements. Considering the claim by Lockheed engineers that their SST design has a center of gravity which puts a weight on the main gear of 3.35 percent less than the 95 percent used in the Corps of Engineers equations, it is suggested that the overlay required by the analysis be reduced by 1 inch. This decrease is considered in calculating costs attributable to this aircraft. Required overlays, including this reduction, are as follows:

Runway 10R-28L

Critical 3 in. Noncritical 3 in. Runway 10L-28R Critical 2 in. Noncritical 0 in. Taxiways (portion) 2 in. Taxiways (portion) 6 in.

12. San Francisco International Airport

Both rigid and flexible construction techniques have been used for pavement at San Francisco International Airport. All rigid pavement is 13 inches thick with a subgrade rating of k = 400. Design stress allowable is 325 psi. The Westergaard analysis employed indicates induced stress conditions as a percent of allowable stress as follows:

L-2000--132 in. B-2707--105 in. Concorde--117 in. B-747--98 in. L-500--85 in. DC-8-63--118 in. B-707--108 in. DC-8-55--111 in.

On the basis of these stresses and the allowable working stress, the recommended amounts of bituminous overlay are as follows:





Current jets	2 inches
Stretched subsonics	3 inches
High-capacity subsonics	0 inches
Concorde	3 inches
SST	5.5 inches

Flexible pavements, with subgrade ratings of F2 and CBR 15, are adequate in noncritical areas except for the L-2000, which requires a 4-inch overlay. On the weakest portions of taxiways and aprons, the L-2000 requires 7 inches of bituminous overlay. The deficiencies created by other aircraft are marginal.

13. Seattle-Tacoma International Airport

All applicable pavements at Seattle-Tacoma are of rigid construction. Some areas, however, have received substantial flexible overlays. The subgrade rating is k = 300 and design stress, including the factor of safety, is 400 psi.

Critical areas of 12-inch thickness are adequate for current jets, although slightly overstressed. Induced stresses from the high-capacity class (L-500, B-747) are well within the requirements. Bituminous overlays of 2 inches, however, are needed for unlimited operations of the DC-8-63 and Concorde and 5 inches for the L-2000.

The 10-inch concrete apron and taxiway 3 require correspondingly greater asphalt overlays, as follows:

Current jets	4 inches
Stretched subsonics	5 inches
High-capacity subsonics	2.5 inches
Concorde	5 inches
SST	8 inches maximum

The existing overlays on the 6- and 8-inch concrete runways are sufficient in all cases.



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Existing Pavement	<u>L-2000</u>	<u>B-2707</u>	Concorde	<u>B-747</u>	L-500	DC - 8-63		DC - 8-55
8 + 5	7	2	3	$1^{(1)}$	0	3	2	2
6 + 8	7	2	4	1 ⁽¹⁾	0	4	3	3

Note: (1) Taken as 0 in cost calculations because of improbability and impracticality of 1-inch overlay.

14. Dulles International Airport, Washington, D.C.

All pavements at Dulles International Airport are rigid and are designed to withstand loads even greater than those considered in this study. The aircraft examined induce stresses from 25 percent to 50 percent under the allowable maximum. Therefore, no additional paving expenditures are required.

15. Cleveland Hopkins International Airport

The majority of pavements at Cleveland are rigid; some have received bituminous overlays. The subgrade is rated Rb, which may be compared (in the case of good drainage and severe frost) to a modulus of subgrade reaction of k = 300. The pavement was originally designed to support dual-wheel loads of 161,000 pounds. Using a flexural strength of 700 psi and a safety factor of 1.8, it is estimated that allowable stress is near 390 psi. Some areas of reinforced concrete are believed to have higher allowable stresses.

Runway 23L and the 8-inch apron have received 3 to 4 inches of bituminous overlay.

The apron is deficient for all loads considered except the L-500. An additional 3 inches of bituminous surface is needed to accommodate current jets without pavement distress. The DC-8-63 requires the addition of 4 inches and the L-2000 an extra 6 inches. The Concorde requires 4 inches more, and the B-2707, 2 inches more.

Taxiways require a bituminous surface addition of 3 inches to accommodate the L-2000. Taxiways are satisfactory for all other aircraft considered.

Runway 23L in critical areas is apparently adequate for all aircraft despite the slight analytical deficiency for the Lockheed version of the SST. Noncritical areas are satisfactory as now constructed.

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Runway 27R and other areas are not likely to be used repeatedly by large jet aircraft.

16. Greater Pittsburgh Airport

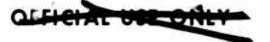
Both rigid and flexible construction are used in Pittsburgh. The subgrade is rated by FAA at E-7 with good drainage and severe frost, resulting in F4 or Rb classifications. This is believed approximately equivalent to k = 300 in this particular case. The design allowable stress was intended to support an equivalent single-wheel load of 60,000 pounds. From this it is estimated at 400 psi in critical areas and 545 psi in noncritical portions, assuming safety factors of 1.7 and 1.25, respectively.

The terminal apron is 10-inch concrete on an 8-inch base. Taxiways and holding aprons are 12-inch rigid pavement, as are the majority of turnoffs. Runway 28R, which is 10,500 feet long, has 500-foot critical sections of 12-inch concrete at each end. The balance is 10-inch concrete. Runway 28L has 500-foot critical sections at each end; one is 17-inch flexible pavement, the other, 12-inch rigid. Other sections are 12-inch rigid, 500-feet; 10-inch rigid, 2,500 and 1,500 feet; and 17-inch flexible, 2,500 feet.

Critical flexible pavement is deficient by 7 inches for current jets and 8 inches for the DC-8-60 series. No further increment is necessary for the L-500, but the B-747 requires 3 inches. The Concorde and Lockheed 2000 airplanes require 8 inches. The Boeing SST requires 5.5 inches. Noncritical sections must have a 3-inch overlay for L-2000, DC-8-63, and Concorde.

Rigid pavement is slightly overstressed by current jets, primarily in noncritical areas. Stretched jets also overstress noncritical areas, and create a 14 percent overstress in critical areas as well. Stresses induced by high-capacity jets are acceptable. The SST's induce maximum overstresses of 28 percent in critical areas.

Strengthening courses are necessary for each of the concrete areas at the Pittsburgh airport, according to the analysis conducted. It is assumed that bituminous courses are acceptable, and the needed thicknesses of overlay by aircraft requirements are as follows:





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PRC R-890 32

	Runways	28L, 28R	Taxiways and	Terminal
	Critical	Noncritical	Hold Aprons	Apron
L-2000	3	2.5	3	6.5
B-2707	0	0	0	3
Concorde	2	0	2	5
B-747	0	0	0	2.5
L-500	0	0	0	0
DC-8-63	2	0	2	5
B-707	0	0	0	4
DC-8-55	0	0	0	4

For costing purposes, runway 28R-10L was the only runway considered.

17. Minneapolis-St. Paul International Airport

All pavements at Minneapolis are rigid. Flexural strengths of 700 psi have been designed into the concrete. Safety factors of 1.9 for critical areas and 1.6 for noncritical areas were designated by airport engineers, resulting in allowable stresses of 368 and 438 psi. The subgrade is rated at k = 300.

According to the Westergaard analysis, additional pavement is needed for all aircraft considered except the L-500. Required bituminous overlays are:

	9-inch <u>Noncritical</u>	ll-inch <u>Critical</u>	l2-inch <u>Noncritical</u>	l2-inch Critical
Current jets	5	5	0	3
Stretched subsonics	6	6	0	4
High-capacity subsoni	св 3	2.5	0	0
Concorde	6	6	0	4
SST	8	8	3	6





18. Metropolitan Oakland International Airport

Both rigid and flexible pavements are found at Oakland International. The rigid pavement has an allowable stress of 400 psi, and a k factor of 185. Flexible pavement is 13 inches thick and a subgrade rating of Fa has been set by airport engineers.

Flexible pavements are adequate for all aircraft evaluated by the FAA method. No CBR data is available.

Induced stresses in the 13-inch rigid pavement (without overlay) are satisfactory for the high-capacity jets, but are more than allowable for all others. For the stretched jets, a 2.5-inch bituminous overlay is recommended. The Concorde requires the same 2.5-inch overlay, while the SST requires 7 inches. Current jets need 2 inches.

In the terminal area, a 3-inch bituminous overlay already exists which is satisfactory for all aircraft considered except the L-2000, which needs an additional 4 inches of bituminous overlay.

19. Sky Harbor Municipal Airport (Phoenix, Arizona)

The main runway at Phoenix, 8R-26L, is the only runway considered for large future aircraft operations. It is 10,300 feet long by 150 feet wide, and is primarily paved with 19-inch flexible pavement. The west 1,000 feet and the east 1,700 feet consist of rigid pavement which is equivalent to 12 inches in thickness. The subgrade rating of the flexible pavement has an FAA value of Fl and a CBR of 17. The subgrade under the rigid pavement is assumed to have a k value of 300.

All the taxiways are flexible pavement 75 feet in width. They are 19 inches thick and have a subgrade rating of Fl.

Pavement in the apron area is half rigid, half flexible. The rigid pavement is equivalent to 12 inches of concrete and has an assumed k subgrade of k = 300. All rigid pavement is assumed to have a safety factor of 1.8 in determining the allowable flexural stress of 350 psi. In actual beam tests, the concrete fractured under a stress of 635 psi. The flexible pavement in the apron area has a subgrade rating of E-4 to E-7, which is approximately equivalent to an F1 rating under conditions of good





drainage and no frost. Its thickness varies: the subbase is 3 to 6 inches thick, the base is 9 inches, and the surface is 2 to 3 inches. For the purpose of this analysis, an average value of 17 inches has been assumed.

Required strengthening of these pavements by bituminous overlays is as follows:

	8R-26L Critical <u>Concrete</u>	Concrete Apron	8R-26L Noncritical	Flexible Taxiways	Flexible Apron
I-2000	7.5	7.5	4	6	8
B-2707	2.5	2.5	0	0	3
Concorde	4	4	0	3	5
B-747	2 ·	2	0	0	2
L-500	0	0	0	2	4
DC-8-63	4	4	0	3	5
B-707	3	3	0	2	4
DC-8-55	3	3	0	2	4

20. Lambert-St. Louis Municipal Airport

All pavement at the St. Louis airport is of rigid construction. Subgrade is Rb, or k = 200. Single-wheel load ratings of 100,000 pounds were used in design, and the allowable stress is estimated to be near 400 psi. This results from a flexural strength of 700 psi and a safety factor of 1.7.

Only one of the three main runways, 12R-30L, was considered in this study for use by future aircraft. The stresses induced and the required thicknesses, as shown on the accompanying chart, indicate that the aircraft considered are able to use this airport repeatedly without danger of concrete distress, with the exception of the L-2000.

The L-2000 will require a bituminous overlay of 5 inches in the critical areas.





21. Tampa International Airport

Both rigid and flexible pavements are in use at Tampa. Subgrades have been assigned a rating of E-3, which is equivalent to F2 and Ra. Thicknesses at the longest runway are 12-inch and 10-inch concrete in critical and noncritical sections, respectively. The major taxiways and a portion of the apron are flexible pavement 14-16 inches thick. The balance of this apron is rigid pavement 13 inches thick.

Since airport authorities report that the subgrade is designated Ra for rigid pavement analysis, and was designed to support dual-tandem gross loads of 350,000 pounds, the k factor used is 300. Results of actual plate bearing tests were not available. The allowable stress, based on a relatively low level of coverages and a safety factor of 1.7, is 400 psi.

Bituminous overlays of 2 inches on the critical concrete runway would be needed for the DC-8-55, DC-8-63, and Concorde, and 5 inches for the L-2000. The L-2000 would also need a 2.5-inch s rengthening of runway centers. Concrete apron areas are believed adequate despite one nominal deficiency.

Where asphaltic concrete occurs in critical areas such as the taxiways and certain aprons, some strengthening is required. Needed thicknesses are 0, 2, 0, 2.5, and 2.5 inches for the current, stretched, highcapacity, Concorde, and SST groups, respectively.

22. New Orleans International Airport

It is anticipated that the large jet aircraft of the type considered in this study will use runway 28-10 at New Orleans. It is an east-west runway 9,227 feet long and 150 feet wide. As originally constructed in 1944, it consisted of a subbase of 2 feet of batch material from the nearby river bed above the very soft subgrade. Portland Cement concrete was placed on this subbase in lanes of approximately 20 feet in width. For each lane along the full length of the runway the outer edges were 9 inches thick and the center 7 inches thick. Later subsidence caused considerable unevenness, both in the transverse and in the longitudinal grades, and an overlay of bituminous material for leveling purposes became necessary in 1956. Minimum thickness in





areas of least settlement was 4 inches, ranging to a maximum of 18 inches. In 1965, further leveling was found necessary because of continued uneven settlement. Low areas were first leveled with a granular base course, the maximum thickness of which was 8 inches. This was followed by a new concrete runway of 12-inch thickness on critical ends and a 10-inch center portion.

The original subgrade was regarded as having an FAA classification of Re. It may be considered to be Ra under the new concrete, however, because the previous paving acts as a subbase and upgrades the classification. This, in turn, can be equated to a k factor of at least 300 for Westergaard analyses of the new pavement. On the basis of a design strength permitting operation of 350,000-pound aircraft on dualtandem gear, allowable stress would normally be 400 psi. Because of the very deep and unusually strong subbase provided by previous pavements, however, 450 psi has been used in critical areas and 600 psi in the runway center. This corresponds with safety factors of 1.8 and 1.3, respectively.

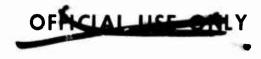
Taxiways have, in general, evolved through the same phases of settlement and leveling courses that have been described for runways. A new set of concrete taxiways of 12-inch thickness is now being constructed over the previous leveling courses.

Aprons are of two thicknesses; the older apron areas are the original 9-inch concrete on an 11-inch sand shell subbase, and the later pavements (used by heavy airline traffic) are of 12-inch concrete on 15 inches of subbase. According to FAA officials, settlement at the aprons has not been as extensive nor as uneven as on runways and taxiways.

Since the subbases under apron areas are less thick than those under the new concrete elsewhere, the subgrade factor of Re (or possibly Rd) is still applicable. A k factor of 200 and an allowable stress of 300 psi have therefore been used.

The new runway pavements and taxiways are considered sufficiently strong for all aircraft in the study despite a nominal deficiency shown by the analysis for one airplane. However, the apron areas, including the





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original area and the later enlargements, are shown to need considerable strengthening. In actuality, concrete would probably be used for this strengthening, but the bituminous overlay method will provide satisfactory results for costing purposes. Thicknesses are as follows:

	9-inch Apron	12-inch Apron
L-2000	18	13
B-2707	12.5	7
Concorde	14	9
B-747	11	6
L-500	9	4
DC - 8 - 63	14	9
B-707	12.5	7
DC-8-55	12.5	7

23. Puerto Rico International Airport (San Juan)

All pavements at San Juan, Puerto Rico are rigid. The subgrade classification is E-1, which can be translated to a value of k = 300for Westergaard computations. Allowable stress is approximately 400 psi, with a safety factor of 1.8. In noncritical areas with a safety factor of 1.3, allowable stress is 550 psi.

The major runway, 7-25, is 10,000 feet long and 200 feet wide. The ends of this runway are of 13-inch Portland Cement concrete, and the center is 12 inches thick. Aprons and taxiways are 13 inches thick.

Pavements were designed to support a 350,000-pound aircraft with a standard dual-tandem main gear.

A 3-inch overlay of bituminous surfacing is needed for operations of the L-2000 on critical pavements. All other aircraft are within the requirements shown by the Westergaard analysis.

24. Stapleton International Airport (Denver, Colorado)

The flexible pavement at Denver's Stapleton Airport includes the east-west runway and adjacent high-speed turnoffs. It rests on a subgrade of F3 rating, and a soil classified as E6.



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This runway measures 10,000 feet by 150 feet. The critical pavement consists of 15 inches of subbase, 10 inches of base, a 3-inch original surface course, and a later bituminous overlay of 3 inches, totaling 31 inches. Noncritical areas are identical except that the subbase is only 10 inches thick. This runway is adequate for the aircraft being considered.

The high-speed turnoffs have 4 inches of asphalt surface on 16 inches of base and subbase. Slight deficiencies here are believed to exist, but the nature of the turnoffs is noncritical since the loads thereon will be landing aircraft with gross weights much lower than the maximum.

The major taxiway parallel to the east-west runway is of 5-inch Portland Cement concrete which rests on an 8-inch subbase and an Rb subgrade.

This subgrade can be equated to k = 250. Allowable stress is estimated at 350 psi with a safety factor of 1.8. Stresses created by all aircraft are unacceptable. Overlays of 16, 17.5, 14, 17, and 21 inches are required for current, stretched, and high-capacity jets, and Concorde and SST, respectively.

The new north-south runway is 11,500 feet by 150 feet and is 12 inches thick on critical ends and 10 inches in the center. It is supported by 3 feet of sand subbase which raises the soil classification to E2, Ra, or k = 300. The design gross load is 350,000 pounds on dual-tandem gear, or an allowable stress of 400 psi. Adjacent taxiways are 12 inch concrete on 2 feet of sand. The critical ends of this runway and its taxiway need strengthening for the DC-8-63, Concorde, and L-2000 in the amounts of 2, 2.5, and 5 inches, respectively. Noncritical portions require 3 inches of the bituminous overlay for the L-2000.

The concrete apron measures approximately 3,000 feet by 2,000 feet. Construction is 12 inches of concrete on 8 inches of subbase. Subgrade is rated by FAA at Rb, taken as k = 200 for the Westergaard equations. On the basis of an allowable stress of 400 psi, current jets require 2.5 inches of overlay, stretched jets, 4 inches, Concorde, 3 inches, B-2707, 2 inches, and L-2000, 7 inches.

Only runway 17L-35R was considered for costing purposes.

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25. Atlanta Airport

The airport at Atlanta, Georgia has pavements which are constructed of Portland Cement concrete in some areas and of flexible and bituminous materials in other areas. The subgrade rating given b the FAA is E-7. With the assumption of no heavy frost and poor drainage, this would be equivalent to an F5. The main runway, 9L-27R, is of rigid pavement 9 inches in the noncritical area and 11 inches in the critical areas. The major instrument runway is 9L-27R, which is 10,000 feet long by 150 feet wide. Two other runways are available but it is assumed that they will not receive the larger jet traffic because of the short length. No design allowable stress is given, but the safety factor is said to be 1.7.

It is usually safe to assume a flexural strength of near 700 psi for concrete. In the case of Atlanta, however, those consulted indicate this to be rather high. Six hundred psi has been used, resulting in an allowable stress of 350 psi. For the purpose of analyzing rigid pavement, the F5 rating is equated to k = 250, according to FAA regional engineers.

On this basis, all of the aircraft studied overstress the 9-inch concrete pavement considerably. Asphaltic overlays of 8, 9, 7, 9, and 11 inches are necessary for the current, stretched, high-capacity, Concorde, and supersonic aircraft, respectively.

The 11-inch critical ends of the runway will require 6, 6-1/2, 4, 6-1/2, and 10 inches of asphaltic overlay for the current, stretched, high-capacity, Concorde, and SST, respectively.

The 14-inch critical ends will require 0, 2, 0, 2, and 6 inches respectively for the foregoing aircraft.

No overlays are required on the flexible pavement.

C. Pavement Strengthening Costs at the Selected Airports

The analysis of airport pavement requirements for the eight aircraft included in the study has resulted, in many cases, in a demonstration of a need for additional pavement. In actual practice, paving action for strengthening purposes may or may not follow theoretical analysis, and when it does, it may take the form of concrete overlays, bituminous



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overlays, concrete inlays, or other alternatives. Recommended action in the present study has taken the form of a bituminous overlay in all cases, for the following reasons:

1. Installation of bituminous material in the range of thicknesses being treated here is generally less expensive than concrete.

2. Even in cases where it is felt that concrete overlays would be required by airport officials, bituminous requirements were estimated because the minimum concrete overlay of 5 inches in some cases, would have excluded costs appropriately attributable to one aircraft whose requirement fell below that minimum and thus penalized (in a comparative sense) another whose requirement was just above the minimum. Better cost distribution was felt available by using bituminous overlays, the minimum of which is 2 inches.

3. It is felt that through use of a consistent ground rule regarding choice of overlay material, the comparative analysis presented here is more meaningful than it would have been if arbitrary decisions had been made at each airport area. This in no way is intended to reflect on the relative merits of either concrete or asphalt.

In the determination of the costs of the pavement improvements, an effort has been made to use present installed costs of bituminous overlays at each airport, wherever such information was available. It was found that a constant cost per square yard or per ton was not applicable, due to wide variations from one area to another. Natural resources of the locale and proximity of the airport to major processing plants obviously influenced the unit price.

However, no attempt was made to reduce costs as a function of the thickness of a single overlay, as it was felt that the value of this procedure would not be proportional to the additional effort.

The areas to be overlaid have been calculated by use of exact dimensions wherever possible. It was necessary, however, to estimate these dimensions in some cases, especially where only a portion of a runway, taxiway, or apron was in need of strengthening.





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In this connection, it is recognized that overlays of various thicknesses would be problematical on a surface with an existing level grade. Costs associated with feathering edges or removing present pavement for replacement were not considered, however. The allocation of such costs to a specific aircraft would be difficult and even if accomplished would add little to the comparative analysis.

It was further assumed in cost calculations that critical runway areas consisted of 1,000 feet at each end of runways, unless available data indicated otherwise.

Two pavement design factors, runway gradient and roughness, were found by the competing SST designers to be satisfactory where current FAA standards are observed.

The following tables illustrate the overlay costs by aircraft. Special attention is given to each area in need of strengthening at each of the airports. The pavement area costed is described. The overlay thicknesses in inches and the cost are then enumerated by aircraft type. Dollars are expressed in thousands. Only the areas necessary for the operation of the large jets being studied were considered to be in need of overlay, and other areas were not included in cost figures. This usually included only the main runway, adjacent holding areas and taxiways, and applicable apron areas.

The costs for overlaying existing flexible pavement were based on thicknesses required by the Corp of Engineers method wherever possible, and on the FAA method in cases where no CBR data were obtainable. However, footnotes indicate the requirement via the FAA method wherever the Corps of Engineers method was used.

Consensus within the aviation community exists expressing dissatisfaction with the FAA pavement analysis method. Virtually without exception the observation was repeated to PRC researchers that the CBR method is preferred--is more realistic than that sponsored by the FAA. Where pavements were laid in accordance with the FAA method, more instances of more severe distress have occurred than when the CBR approach was employed.





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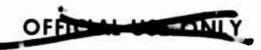
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Note: (1) Adjusted upward 50 percent for bituminous base

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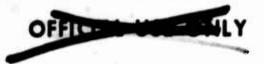
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8	CONCORDE	FAA	12	31	9.5			12	31	12	31		
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Paveme	CON- CORDE	<u>450</u> 12.5						410 14					
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w.	DC-8 -55	<u>650</u> 12	<u>650</u>				445 12.5	8 + 7	<u>960</u> 12.5			
Induced Pavement Stress/Required Thickness	B-707	<u>625</u> 11.5	<u>625</u>				<u>430</u> 12	8 + 6	<u>935</u> 12			
uired T	DC-8 -63	<u>687</u> 12.5	<u>687</u> 9.5				<u>475</u> 13	8 + 7.5	<u>1,020</u> 13			
ss/R.eq	L-500	475	475				<u>330</u> 9.5	8 + 2	710 9.5			
nt Stre	B-747	11	<u>600</u> <u>8.5</u>				<u>405</u> 11	8 + 5	<u>925</u> 11			
Paveme	L-2000B-2707CORDE B-747	<u>690</u> 12.5	<u>690</u> 9.5				<u>475</u> 13	8 + 7.5	1,020 13			
l paonbu	B-2707	613 11.5	<u>613</u>				<u>421</u> 11.5	9 + 8	<u>920</u> 12			
Ir	L-2000	<u>698</u> 14	<u>698</u> 10				<u>488</u> 14	8 + 10	1,015 14.5			
	Allowable Stress	400	550				350	400	407			
Pavement	Subgrade Rating " _k "	400	400				600	400	320			
Rigid Pa	ess	12	12				12	12	12			
	Concrete Subbas ThicknessThickne	8	œ				10	8 + 3 ⁽¹⁾	6			
ort:	Miami	9R-27L, 12-30 Critical	9R-27L, 12-30 Noncritical				Term. Apron	Term. Apron	Small Area			
Airport:	4			sken	Runy		8	norq	A bue	s ke	wixe.	L

Note: (1) -8 inches of concrete with 3-inch bituminous overlay

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	DC-8-55	ACBR	5 7	9	2	9	~	9	~	~				
	DC.	FAA	11.5	6	11.5	6	11.5	6	11.5	11.5				
	B-707	CBR	2	9	7	6	7	9	2	2				
	н В	FAA	11	6	11	6	11	6	=	=				
	1-63	CBR	7.5	6.5	7.5	6.5	7.5	6.5	7.5	7.5				
Pavcment Thickness	DC-8-63	FIL	11.5	6	11.5	6	11.5	6	11.5	11.5				
Thicl		CBR	2	•	2	9	2	9	2	2				
nent '	L-500	FAA	8	6.5	80	6.5	œ	6.5	æ	8				
aven	-747	ACBR	2	9	2	9	2	9	2	2				
ed P	B-7	FAAC	10	8	10	∞	10	80	10	10				
Required	RDE	CBR	7.5	6.5	7.5	6.5	7.5	6.5	7.5	7.5				
Ч	CONCORDE	FAAC	12	9.5	12	9.5	12	9.5	12	12				
		CBR	2	•	2	\$	2	9	2	7				
	B-2707	FAAC	10.5	8.5	10.5	8.5	10.5	8.5	10.5	10.5				
	000	CBR	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2	80	2	8	7	8	8				
	L-2000	FAA	11.5	6	11.5	6	11.5	6	11.5	11.5				
	radc ing	BR	60	60	60	60	60	60	60	60				
nent	Subgra Ratin	FAA	Fa	F a	F) B	ы Ц	Fa	Fa	Fa	Fa				
Javen	Trick	less	26 min.	21 min.	22 min.	12 min.	22 min	21 min	14 min	20 min				
ble F	Total S. h. Thick	baser	<u> </u>							6				
Flexible Pavement		faceBase baseness FAAC								12				
	1.12	face								2				
ort:	Miami		9R-27L Critical	9R-27L Noncrit.	9L-27R Critical	9L-27R Noncrit.	12-30 Critical	12-30 Noncrit.	Taxiways	Aprons				
Airport:					бүбу	VnuA			S	norq	y pu	5 8 Y 5	WİXE	L

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PRC R-890 55

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	60									<u> </u>	<u> </u>
s	DC-8 -55					450					
Induced Pavement Stress/Required Thickness	B-707					<u>435</u> 16					
ired T	DC-8 -63					<u>475</u> 17					
ss/Requ	L-500					<u>350</u> 13.5					
nt Stre:	B-747					<u>400</u> <u>15</u>					
aveme	CON- CORDE					<u>475</u> 17					
duced I	B-2707					$\frac{430}{16}$					
In	L-2000B-2707CORDE B-747					<u>545</u> 20					
	Allowable Stress					295					
Pavement	Subgrade Rating A					250					
Rigid Pa	e s										
	Concrete Subbas ThicknessThickne	•				12					
ort:	Philadelphia					All Rigid					
Airport:	Р		sken	Muny		s	pron	A bri	s ys	wixe'	L



1													
	L-20	FAAC	18.5	15				18.5					
	ubgrade Rating	CBR	20	20				20					
	Subgrade Rating	FAA CBR	F2	F2				F2					
			24.5	24.5				23					
	Total S., b. Thick	baseness	10	10				80					
		faceBase	11	11				12					
	5.17	face	3.5	3.5				3					
	Philadelphia		9L-27R Critical	9L-27R Noncrit.				All Flex.					
	ቪ				sysy	nun A		S	pron	A bru	5 E Y 5	wixe'	L
			5	-	5 · · ·								
				0	FFIC		 SE	UN	L.,	4			

Airport:

		~				1		_		
	8-55	CBF	19	17			19			
	DC-8-55	FAACBR	17.5	14			17.5			
	:0	CBR	19	17			19			
	B-707	FAA	17	13.5			17			
. "	3-63	CBR	20	18			20			
Pavement Thickness	DC-8-63	FAA CBR	18	14.5			18			
Thicl		CBR	19	17			19			
nent	L-500	FAA	11.5	6			11.5			
aver	B-747	AACBR	18	16			18			
	В-	FAA	18	14.5			18			
Required	RDE	CBR	20	18			20			
H	CONCORDE	FAA	185	15			18.5			
			18	16			18			
	B-2707	FAACBR	16.5	13.5			16.5			
	L-2000	CBR	24	22			24			
		FAA	18.5	15			18.5			
	grade ting	CBR	20	20			20			
ment	Subg Rat	FAA	F2	F2			F2			
Pave	Total Sub-Thick	basquess	24.5	24.5			23			
Flexible Pavement	Cub.		10	10			8			
Flex		eBase	11	11			12			
		e	5	ŝ						

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PRC R-890 57

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	j.	R		S.				 1				T	T
-	-8-55	CBR	24	21.	31	28		 31	54	24			
	DC-	FAA	25	20					25	17.5			
	-707-	CBR	24	21.5	31	28		31	24	24			
	B-7	FAA	24.5	9.5				1	4.5	2		<u>†</u>	T
	-63	CBR	25	22.5 1		30		 m	5	5			t
ness	DC-8-6	AA	26.5	21 2	m	<u> </u>		m.	6.52	8 2		 	┢
Thicknes		CBRF	5	Ŀ.	33	30		 m	5 2	5 1			-
	L-500	FAAC	6 2	13 22		<u> </u>		~	6 2	2 2			-
Pavement	7	BRF.							1				┢
	B-74	AACI	22	50	28	25		 28	22	22			┢
Required		щ	21	5 17				 	21	15			
Req	CUNCORDE	ACBR	5 25	22.	32	29		 32	5 25	5 25			
191	ğ	FAA	26.	21				 	26.	18.			
	-2707	CBR	5 23	21	30	27		30	5 23	5 23			
	B-	FAA	23.5	19					23.	15.5			
	-2000	CBR	32	29	41	37		 41	32	32			
	L	FAA	27	22					27	18.5			
	rade ing	CBR	15	15	10.6	10.6		10.6	15	15			
nent	Subgra Rating		F4	F4					F4	F2			
aver	r ot al	less	26	23	37	37		37	23	37			
ble ['] F	Sub Thick	baseness FAA CI	6.	œ	24	24		 24	8	24	0 I		
Flexible [.] Pavement			12	10	10	10		 10	10	10			
	Sur-	faceBase	5	5		3 1		3 1	5	3			
ort:	Portland			.1 .	10L-28R Critical	10L-28R Noncrit.			10R-28L Taxiway	All Aprons			
Airport:	ሲ				sysv	MunA		s	pron	A bri	e ske	wixe'	L

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	10	~	-vi	_	-										PRC
	-8-55	FAACBR	21.						24						1.1
	DC-	FAA	14					9	17.5						
	- 707	CBR	21.5						24						
	B-7	FAA	13.5						17 12						1
	-63	CBR	23		1				25.5					<u>†</u>	1
ness	DC-8-63	FAA	4.5						18			<u> </u>		1	1
Thicknes		CBR	22.5 1						25						1
lent 7	L-500	FAAC	6						11.52						į
Pavement	-747		20						22 1						ň.,
	B-7.	FAACBR	14.5						18						
Required	UE	-	22.5						25						
Я	CONCORDE	FAACBR	15 2						8.5				-		actual thickness
			51						23 1						thicl
	B-2707	FAACBR	3.5						16.5						ctual
	000	CBR	29 1						32 1						×
	L-2000	AA	15						18.5						of 1.5
	rade ng	baseness FAA CBR F	15 min.						15 min.1						actor
nent	Subgrade Rating	FAA	F2						F2						ase f
aver	T ot al	less	23	-					23 min.						ted b
bleH	(1)	basq	4						4						trea
Flexible ⁵ Pavement		Sase	15						15 min.						ment
	511F	faceBase	4						4						00
011:	San Francisco		10L-28R, 1R-191 10R-281 (Noncrit						All Flex.						: (1) Includes cement treated base factor
Airport:	Sai				вүби	MunA			. 5	pron	A bri	e ske	wixe	T	Note:

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PRC R-890 60

-			-	-	 -			-		_	
s	DC-8 -55	360				<u>360</u> 14					
hicknes	B-707	<u>350</u>				<u>350</u> 14					
Induced Pavement Stress/Required Thickness	DC-8 -63	<u>385</u> 15				<u>385</u> 15					
ss/Req	L-560	<u>275</u> 11				<u>275</u> 11					
nt Stre	B-747	<u>320</u> 13				<u>320</u> 13					
aveme	CON- CORDE	<u>380</u> 15				<u>380</u> 15					
duced I	L-2000B-2707CORDE B-747	<u>340</u> 13.5				<u>340</u> 13.5					
ų	L-2000	<u>430</u> 16.5				<u>430</u> 16.5					
	Allowable Stress	325				325					
Rigid Pavement	Subgrade Rating "k"	400				400					
Rigid Pa		6				6					
	Concrete Subbase ThicknessThickness	13				13					
ort:	San Francisco	10 L-28R, 1 0R-28 L IR-19 L (Critical)				All Rigid					
Airport:	Sa		sken	NUUA		8	vordy	∦ put	s s ke	wixe'	L

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Settle Concrete Subgrade Numerical Lood DC-8 bit DC-8 bit	Air	Airport:		Rigid Pa	Pavement		I	Induced Pavement Stress/Required Thickness	avemer	it Stres	s/Requ	uired Tl	nicknes	D
		Seattle	Concrete Thickness	ss	I O I	Allowable Stress	L-2000	B-2707	CON- CORDE		L-500	DC-8 -63	B-707	DC-8 -55
Ib-34 $8 + 5^{(1)}$ 300 550 $8 + 5$ $8 + 2$ $8 + 3$ $8 + 4$ $8 + 2.5$ Noncritical $6 + 8^{(1)}$ 300 550 $6 + 8$ $6 + 6$ $6 + 5$ $6 + 5$ $6 + 5$ $6 + 5$ $6 + 6$ $6 + 5$ 7 $6 + 5$ 7 $6 + 5$ 7 $6 + 5$ 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		16-34 Critical	12		300	400	<u>511</u> 15	<u>406</u> 12	<u>450</u> 13	<u>380</u> 11.5	<u>325</u> 10	<u>455</u> 13	<u>420</u> 12.5	<u>430</u> 12.5
I6-34 $6 + 8(1)$ 300 550 $6 + 8$ $6 + 5$ $6 + 5$ $6 + 5$ $6 + 7.5$ $6 + 6$ Noncritical $6 + 8(1)$ 300 550 $6 + 8$ $6 + 5$ $6 + 5$ $6 + 6.5$ $6 + 6$ $7 - 5$ $6 + 7$ $7 - 5$ $7 - 5$ $6 + 7$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$ <td< td=""><th></th><td>16-34 Noncritical</td><td>+</td><td></td><td>300</td><td>550</td><td>+</td><td>+</td><td>3 + 3.5</td><td>+</td><td>(+ 8</td><td>8 + 4</td><td>8 + 2.5</td><td>8 + 3.5</td></td<>		16-34 Noncritical	+		300	550	+	+	3 + 3.5	+	(+ 8	8 + 4	8 + 2.5	8 + 3.5
Term. Apron. 10 300 400 $\frac{13}{15}$ $\frac{566}{12}$ $\frac{480}{15}$ $\frac{400}{13}$ $\frac{520}{125}$ Taxiway 3 10 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{450}{135}$ $\frac{455}{135}$ $\frac{455}{125}$ $\frac{420}{1255}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{450}{135}$ $\frac{455}{125}$ $\frac{420}{135}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{450}{135}$ $\frac{455}{125}$ $\frac{420}{125}$ Holding Aprons 12 300 400 $\frac{511}{12}$ $\frac{456}{12}$ $\frac{455}{12}$ $\frac{420}{12}$ $\frac{12.5}{12}$ $\frac{12.5}{12.5}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{456}{12}$ $\frac{456}{12}$ $\frac{420}{12}$ $\frac{12.5}{12.5}$ $\frac{450}{12.5}$ $\frac{455}{12.5}$ $\frac{420}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{420}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{450}{12.5}$ $\frac{400}{12.5}$ </td <th>sken</th> <td>16-34 Noncritical</td> <td>6 + 8⁽¹⁾</td> <td></td> <td>300</td> <td>550</td> <td>+</td> <td>+ 6</td> <td>+</td> <td>-2 +</td> <td></td> <td></td> <td>6 + 6</td> <td>6+6.5</td>	sken	16-34 Noncritical	6 + 8 ⁽¹⁾		300	550	+	+ 6	+	-2 +			6 + 6	6+6.5
Term. Apron, 10 300 400 $\frac{613}{15}$ $\frac{506}{12}$ $\frac{480}{13}$ $\frac{400}{13}$ $\frac{570}{10}$ $\frac{520}{13}$ Taxiway 3 10 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{450}{13}$ $\frac{406}{13}$ $\frac{450}{10}$ $\frac{455}{13}$ $\frac{420}{13}$ Taxiway 6 and 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{455}{10}$ $\frac{420}{13}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{106}{12}$ $\frac{13}{15}$ $\frac{12.5}{10}$ Holding Aprons 12 12 12 12 12 12 12	vun M													
Term. Apron. In In In In In In In Taxiway 3 10 300 400 $\frac{513}{15}$ $\frac{506}{12}$ $\frac{565}{12}$ $\frac{480}{10}$ $\frac{400}{13}$ $\frac{570}{13}$ $\frac{520}{13}$ Taxiway 3 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{570}{13}$ $\frac{455}{10}$ $\frac{420}{13}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{13}{13}$ $\frac{12.5}{12.5}$ Holding Aprons 12 300 400 $\frac{511}{15}$ $\frac{406}{12}$ $\frac{455}{13}$ $\frac{455}{10}$ $\frac{420}{13}$ Holding Aprons 12 300 400 $\frac{511}{12}$ $\frac{12}{12}$ $\frac{12}{10}$ $\frac{13}{13}$ $\frac{12.5}{12.5}$														
Term. Apron. 10 300 400 570 520 520 11.5 10 13 12.5 Taxiway 3 10 12 300 400 15 12 13 12.5 420 520 12.5 Taxiway 6 and 12 300 400 511 406 450 380 325 420 12.5 Holding Aprons 12 300 400 511 406 450 380 325 420 Holding Aprons 12 12 12 12 10 13 12.5 Holding Aprons 12 300 400 511 12 11.5 10^{2} 12^{2} 420 Holding Aprons 12 10^{2} 12^{2}														
Taxiway 6 and 12 300 400 511 406 450 380 325 455 420 Holding Aprons 12 12 12 12 13 11.5 10 13 12.5 Holding Aprons 12 12 12 12 12.5 12.5 12.5 Holding Aprons 11 15 16 1 1 13 12.5 Holding Aprons 12 12 12 12 12 12.5 12 Holding Aprons 11 16 16 16 16 16 17 12.5 Holding Aprons 12 12 12 12 12 12.5 12.5 Holding Aprons 16 16 16 16 16 16 16 17 12.5 Holding Aprons 12 12 12 12 12 13 12.5 12.5 12.5 Holding Aprons 16 16 16 16 16 16 16 16 16 16 16 <t< td=""><th>S</th><td>Term. Apron, Taxiway 3</td><td>10</td><td></td><td>300</td><td>400</td><td><u>613</u> <u>15</u></td><td><u>506</u> 12</td><td><u>565</u> 13</td><td><u>480</u> 11.5</td><td><u>400</u></td><td><u>570</u> 13</td><td><u>520</u> 12.5</td><td><u>540</u> 12.5</td></t<>	S	Term. Apron, Taxiway 3	10		300	400	<u>613</u> <u>15</u>	<u>506</u> 12	<u>565</u> 13	<u>480</u> 11.5	<u>400</u>	<u>570</u> 13	<u>520</u> 12.5	<u>540</u> 12.5
A bns εγεωίχεΤ	bron	Taxiway 6 and Holding Aprons	12		300	400	<u>511</u> 15	<u>406</u> 12	<u>450</u> 13	<u>380</u> 11.5	<u>325</u> 10	<u>455</u> 13	420 12.5	<u>430</u> 12.5
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WIXET	e ske													
	wixe'													
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Note: (1) Rigid pavement with bituminous overlay

PRC R-890 61





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ŝ	DC-8 -55	<u>335</u> 11	<u>335</u> 11	<u>450</u> 8.5		 	<u>335</u> 11					
hicknes	B-7 07	<u>325</u> 11	<u>325</u> 11	<u>440</u> 8.5			<u>325</u> 11					
uired T	DC-8 -63	<u>350</u> 11.5	<u>350</u> 11.5	<u>475</u> 9			<u>350</u> 11.5					
ss/Requ	L-500	<u>260</u> 8.5	260 8.5	<u>345</u> 6.5			<u>260</u> 8.5					
nt Stree	B-747	<u>295</u> 10	<u>295</u> 10	<u>395</u> 8			<u>295</u> 10					
Induced Pavement Stress/Required Thickness	L-2000B-2707CORDE B-747	<u>350</u> 11.5	<u>350</u> 11.5	<u>475</u> 9			<u>350</u> 11.5					
duced 1	B-2707	<u>323</u> 10.5	<u>323</u> 10.5	<u>425</u> 8	1		<u>323</u> 10.5					
Ir	L-2000	420 13	<u>420</u> 13	540 9.5			420 13					
	Allowable Stress	500	500	680			500					
Pavement	Subgrade Rating "k"	260	260	260			260					
Rigid Pa	e s s	6	9	9			6					
	Concrete Subbas ThicknessThickne	15	15	12			15					
ort:	Dulles	All Critical	Interior 100 ft. Noncritical	Outer 25 feet Noncritical			llA					
Airport:				sken	NunA		S	norq	А риз	e ske	wixe'	L





Rating Allowable L-2000B-2707 "k" Stress 300 390 est 12 + 5 12 + 0 300 467 12 + 2 12 + 0	Concrete Subbase Thickness Thickness 12 + 3 8 12 + 3 8
e at	300
	300
420 14	300
420 8	300





Rigid Pavement Suborad	sub <i>e</i>	ent		Ĩ	duced F	aveme	nt Stres	s/Requ	lired T	Induced Pavement Stress/Required Thickness	л С
Concrete S ThicknessT	Concrete Subbasc ThicknessThickness	Rating "k"	Allowable Stress	L-2000B-2707CORDE	3-2707	CON-	B-747	L-500	DC-8 -63	B-7 07	DC-8 -55
	30	300	400	$\frac{511}{14}$	<u>406</u> 12	<u>450</u> 13	<u>380</u> 11.5	<u>325</u> 10	<u>455</u> 13	<u>420</u> 12.5	<u>430</u> 12.5
	8	300	545	<u>613</u> 11.5	<u>506</u> 9.5	570 10.5	<u>480</u> 9	<u>400</u> 7.5	<u>570</u> 10.5	<u>525</u> 9.5	<u>535</u> 10
	8	300	400	$\frac{511}{14}$	<u>406</u> 12	<u>450</u> 13	<u>380</u> 11.5	<u>325</u> 10	<u>455</u> 13	<u>420</u> 12.5	<u>430</u> 12.5
~	8	300	545	<u>613</u> 11.5	<u>506</u> 9.5	570 10.5	<u>480</u>	<u>400</u> 7.5	570 10.5	<u>525</u> 9.5	<u>535</u> 10
									- 11		
∞		300	400	<u>511</u> 14	<u>406</u> 12	<u>450</u> 13	<u>380</u> 11.5	<u>325</u> 10	<u>455</u> 13	<u>420</u> 12.5	<u>430</u> 12.5
80		300	400	$\frac{613}{14}$	<u>506</u> 12	<u>570</u> 13	<u>480</u> 11.5	400 10	570 13	<u>525</u> 12.5	<u>535</u> 12.5



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	DC-8-55	FAACBR	25.5	20.5											
		CBRF	2	~											
	B-707	FAAC	24.5	19.5								-			
	63	BRF	2					<u> </u>							
ness	DC-8-63	FAACBR	26.5	1											
ľhick		CBRF	2	~ ~											
Jent 7	L-500	FAA CBR	16	13											
Required Pavement Thickness	147	CBR													
red F	B-747	FAACBR	21	17											
Requi	RDE	CBR													
щ	CONCORDE	FAA CBR	26.5	21											
	B-2707	FAACBR								_					
	B-	₹A/	23.5	19.5			<u> </u>								
	L-2000	ACBR		2											
		RFAA	27	21.											
٦t	Subgrade Rating	ACBR													
'emei	al Sul	s FA	F4	F.4					_						
Flexible Pavement	Total S., h. Thick	baseness FAA	2 17	2 17											
exible	Ű	seba													
F١		faceBase	3 12	3 12											
	i V	[a,	m	m											
ort:		Pittsburgh	28L, Critical	28L, Critical											1
Airport:		Pitt			syav	van A			S	pron	A bri	e eve	wixe	L	

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Air	Airport:		Rigid Pa	Pavement		In	Induced Pavement Stress/Required Thickness	aveme	nt Stres	s/Requ	lired T	hicknes	s
Mi	Minneapolis	Concrete Subbas ThicknessThickne	e s	Subgrade Rating "k"	Allowable Stress	L-2000	L-20003-2707CORDE B-747	CON- CORDE	B-747	L-500	DC-8 -63	B-707	DC-8 -55
	29L - 11R, Critical	11		300	368	<u>560</u> 16	<u>450</u> 13	<u>500</u> 14.5	<u>420</u> 12.5	<u>360</u> 11	<u>500</u> 14.5	470 13.5	<u>475</u> 14
	29L-11R, Noncritical	6		300	438	<u>685</u> 14	575 11.5	<u>645</u> 12.5	<u>530</u> 11	<u>450</u>	650 12.5	590 11.5	<u>610</u> 12
sken	29L - 11R, Noncritical	12		300	438	<u>511</u> 14	<u>406</u> 11.5	450 12.5	<u>380</u> 11		<u>455</u> 12.5	<u>420</u> 11.5	430 12
un A													
	Apron and Taxiways	12		300	368	$\frac{511}{16}$.	<u>406</u> 13	<u>450</u> 14.5	<u>380</u> 12.5	<u>325</u> 11	455 14.5	420 13.5	<u>430</u> 14
norq													
A bri													
e ske													
wixe'													
L													



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		Kigid Pa	d Pavement		Ĩ	duced F	avemen	it Stres	s/Requ	iired T	Induced Pavement Stress/Required Thickness	0
υĘ	Concrete Subbase ThicknessThickness	Subbase Thickness	Subgrade Rating "k"	Subgrade Rating Allowable "k" Stress	L-2000B-2707CORDE B-747	8-2707	CON-		L-500	DC-8 -63	B-707	DC-8 -55
	13		185	400	<u>555</u> 17	<u>4.22</u> 13.5	<u>460</u> 14.5	<u>390</u> 13	$\frac{350}{11.5}$	<u>460</u> 14.5	<u>430</u> 14	<u>440</u> 14
						·						
										•		
Holding Areas	13		185	400	<u>555</u> 17	<u>422</u> 13.5	<u>460</u> 14.5	<u>390</u> 13	<u>350</u> 11.5	<u>460</u> 14.5	<u>430</u> 14	440 14
Terminal Apron	13 + 3 ⁽²⁾		185	400	13+7	13 + 0	13+2.5	13+0	13+0	13 + 2.5	13 + 2	13 + 2

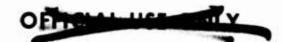
Notes: (1) Four-hundred feet, south end only

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(2) Thirteen inches of Portland Cement concrete with a 3-inch bituminous overlay

PRC R-890 67



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	5.5	3R				_			-		<u> </u>	—	—	
	DC-8-	FAACBR	5	9.5	9.5				Ŀ.					
	DQ	RFA	11.5	6	6				11.			 		
]	B-707	CBR												
	B-	FAA	11	6	6				11					
	-63	CBR					1							
Pavement Thickness	DC-8-63	FAACBR	1.5	9.5	9.5				11.5					
hick														
ent T	L-500	FAACBR		6.5	Ŀ.									
vem	-		0	6	ف									
	B-747	FAACBR		∞										
Required	<u> </u>		10						10	<u>-</u>				
Requ	CONCORDE	AACBR					L	 						
	NO	FAA	12	10	10				12					
	207	CBR												
ļ	B-2707	FAACBR	11	6	5				11					
	00	CBR												
	L-2000	FAAC	11.5	9.5	9.5				11.5					
	a b i d e	R									_			
nt	Subgrade Rating	FAA CB	ष मि	Fa	Fa				гa					
eme		L.			H									
Par	Total Sub-Thick-	baseness	13	13	11				13					
Flexible Pavement	duy S		(1)	(1)	(1)				(1)					
Fley		faceBase	10	6	80				10					
	5.1	face	3	4	3				3					
				(2) ical	(3) ical				75					
		~	29-11 Critical	29-11 (2) Noncritical	29-11 Noncrit				All Taxiways					
Airport:		Oakland	29- Cri	29-11 Noncr										
Air		Oal			sken	un X			S	pron	A bui	e ske	WIXE	T

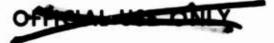
(2) Center 75 feet of noncritical section of runway 29-11.(3) Outer 37.5 feet on each side of noncritical section.

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irp	Airport:		Rigid Pa	Pavement		In	duced F	avemai	nt Stres	ss/Requ	iired T	Induced Pavement Stress/Required Thickness	10
Ч	Phoenix	Concrete Subbase ThicknessThickness	Subbase Thickness	Subgrade Rating "k"	Allowable Stress	L-2000	L-2000B-2707CORDE B-747	CON- CORDE		L-500	DC-8 -63	B-707	DC-8 -55
	8R-26L Critical Ends	12(1)		300	350	<u>511</u> <u>16.5</u>	<u>406</u> <u>13.5</u>	<u>450</u> 14.5	<u>380</u> 13	<u>325</u> 11.5	<u>455</u> 14.5	420 14.0	<u>430</u> 14.0
,													
vanA													
	Aprons (Portion)	12(1)		300	350	<u>511</u> 16.5	406 13 . 5	450 14.5	<u>380</u> 13	<u>325</u> 11.5	<u>455</u> 14.5	420 14.0	430 14.0
orqA													
Note:	Ξ	20' x 25' slabs, outer edge considered equivalent to a		which ar nch overa	edges of which are 14 inches thick, tapered to 11-inch thickness in interior. to a 12-inch overall thickness.	s thick, ss.	taperec	l to 11-	inch thi	ickness	in inter		This is



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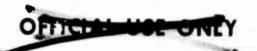
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' i				-				_	 					
		DC-8-55	CBR	20					22	22				
		DC-	FAA	11					4					
		707	CBR	20					22	22				
		B-707	FAA	Ξ					 4	14				
	•	-63	CBR	21					 5	23				
	uess	DC-8-63	FAA	12		<u> </u>			15	15				
	Pavement Thickness		CBR	20					22	22				
	aent	L-500	FAA						10	10 2				
	aven	-747		18					20					
		B-7	FAACBR	9.5					 12	12				
	Required	RDE	CBR	21					 23	23				
	Я	CONCORDE	FAA	12					15	15				
			CBR	19					21	21				
		B-2707	FAA	1					13.5	13.5				
		000	CBR	24					27	27				
		L-2000	FAA	12					15	15				
		rade ing	CBR	17					17	17				
	ment	Subgra Ratin	FAA	F 1					F l	F1				
	Pavel	Total Thick-	ness	19					19	17				
	Flexible Pavement	Total Subgrade	base	. 6	in .				6	5				
	Flex		Base	10					10	6				
		Sur-	faceBase	3					3	3				
	ij		nix	8R - 26L Noncritical					Taxiways	Terminal Apron (Por)				
	Airport:	i	Phoenix	18 N		sken	Vuu X			⊢ ∡ uo⊥d	A bus	: sle	wixs'	L
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			T	1		1	r			T	T	T
s s	DC-8 -55	<u>380</u> 13.5	ļ				<u>380</u> 13.5					
hickner	B-707	<u>375</u> 13.5					<u>375</u> 13.5					
Induced Pavement Stress/Required Thickness	DC-8 -63	$\frac{410}{14}$					410 14					
ss/Requ	L-500	<u>305</u> 11					<u>305</u> 11					
nt Stre	B-747	<u>345</u> 12.5					<u>345</u> 12.5					
aveme	L-2000B-2707CORDE B-747	400 14					<u>400</u> 14					
I paonp	B-2707	<u>372</u> 13					$\frac{372}{13}$					
Ir	L-2000	<u>487</u> 14.5					<u>487</u> 14.5					
	Allowable Stress	400					400					
Pavement	Subgrade Rating "k"	200					200					
Rigid Pa	e s :			-								
	Concrete Subbase ThicknessThickness	14					14					
ort:	St. Louis	30L-12R					All					
Airport:			sken	vanA				pron	A bri	e ske	WİX6	L

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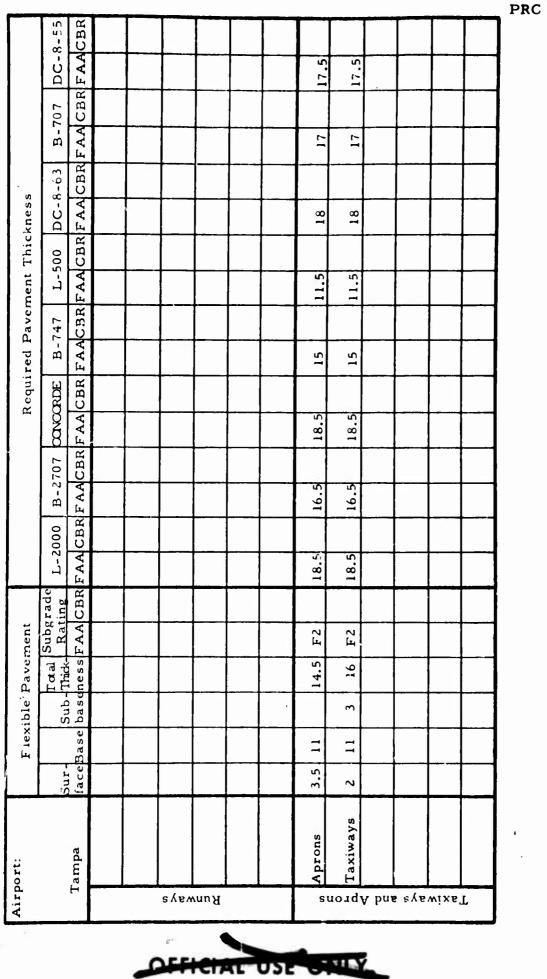
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			OF	-				_				
o.	DC-8 -55	428 13	<u>536</u> 10				<u>388</u> 13					
hicknes	B-707	<u>416</u> 12.5	<u>520</u> 5.5				<u>380</u> 12.5					
Induced Pavement Stress/Required Thickness	DC-8 -63	<u>455</u> 13	<u>570</u> 10.5				<u>410</u> 13					
ss/Req	L-500	<u>326</u> 10	<u>399</u> 7.5				<u>300</u> 10					
nt Stre	B-747	$\frac{379}{11.5}$	<u>480</u> 9				$\frac{340}{11.5}$					
Paveme	CON- CORDE	<u>450</u> 13	<u>567</u> 10.5				$\frac{410}{13}$					
l baoubr	L-2000B-2707CORDE B-747	<u>406</u> 12	<u>506</u> 10				$\frac{367}{12}$					
Ir	L-2000	<u>511</u> 15	<u>613</u> 11.5				<u>468</u> 15					
	de Allowable Stress	400	540				400					
avement	Subgra Ratin "k"	300	300				300					
Rigid Pavemen	Subbase Thickness											
	Concrete Subbase ThicknessThickness	12	10				13	_				
ort:	Tampa	Critical	Noncritical				Apron					
Airport:				sken	uny		S	bron	A but	s ys s	wixe.	L
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PRC R-890 73

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Induced Pavement Stress/Required Thickness Airport: Induced Pavement Stress/Required Thickness New Orleans Concrete Subbase Rubbase Rubbase Rubbase Rubbase Rubbase Rubbase Induced Pavement Stress/Required Thickness New Orleans Concrete Subbase Rubbase Rubbase			-				_		,				_
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	S	DC-8 -55	428	<u>536</u>				<u>428</u> 11.5	<u>675</u> 16.5	<u>550</u> 16.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	hicknes	B-707	<u>416</u> 11.5	<u>520</u>				<u>416</u> 11.5	<u>668</u> 16.5	<u>540</u> 16.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	uired T		<u>455</u> 12	<u>570</u> 9.5				<u>455</u> 12	720 17.5	<u>585</u> 17.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	ss/Req	L-500	<u>326</u> 9	<u>399</u>				<u>326</u> .9	<u>510</u> 14.5	<u>446</u> 14.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	nt Stre	B-747	<u>379</u> 10.5	<u>480</u> 8.5				$\frac{379}{10.5}$	<u>600</u> 15.5	<u>502</u> 15.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	Paveme	CON- CORDE	<u>450</u> 12	<u>567</u> 9.5				<u>450</u> 12	$\frac{715}{17.5}$	<u>577</u> 17.5			
Rigid Pavement Corleans Concrete Subbase Rating Allowable L-200 Thickness Thickness Subgrade Allowable L-200 10 L-200 10 10 12 36-58(1) 300(2) 450 $\frac{511}{13.5}$ 10 12 36-58(1) 300(2) 450 $\frac{613}{13.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 36-58(1) 300 600 $\frac{613}{10.5}$ 10 12 24-44(2) 300 800(3) $\frac{708}{20}$ iways 12 1 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$ tions 12 15 200 300(3) $\frac{708}{20}$	nduced	B-2707	<u>406</u> 11	<u>506</u> 8.5				406 11	<u>642</u> 16.5	<u>534</u> <u>16.5</u>			
Rigid PavementOrleansConcrete SubbaseSubgrade Rating "k"10Thickness Thickness36-58(1)300(2)101236-58(1)30010101036-58(1)3001010101036-58(1)30010101036-58(1)300101224-44(2)300111224-44(2)3001212152001212152001212152001212152001212152001312152001412152001515200161115200	II	L-2000	511 13.5	<u>613</u> 10.5				<u>511</u> 13.5	<u>778</u> 20	708 20			
Rigid PavementOrleansConcrete SubbaseSubgrade Rating "k"10Thickness Thickness36-58(1)300(2)101236-58(1)30010101036-58(1)3001010101036-58(1)30010101036-58(1)300101224-44(2)300111224-44(2)3001212152001212152001212152001212152001212152001312152001412152001515200161115200		Allowable Stress	450	600				450	300 ⁽³⁾	300 ⁽³⁾			
Rigid POrleansConcrete Subbase10ThicknessThickness101236-58(1)101236-58(1)101036-58(1)10101036-58(1)101224-44(2)0ns9110ns1215tions1215tions1215	ivement	Subgrade Rating "k"	300 ⁽²⁾	300				300	200	200			
Orleans 10 tical 10 critical critical critical critical ons tion	Rigid Pa	Subbase Thickness	36-58 ⁽¹⁾	36-58 ⁽¹⁾				24-44 ⁽²⁾	11	15			
Orleans 10 tical 10 critical critical critical critical ons tion		Concrete Thickness						12	6	12			
avewang anorgA bas avewixeT	ort:		28-10 Critical	28-10 Noncritical				Taxiways	Aprons Portion	Aprons Portions			
	Airp		1		sysw	nun A		8	rpron	y pue	ske	wixa]	L

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Notes: (1) Subbase is provided by previous pavements with their subbases and leveling course.

(2) Upgraded to account for subbase courses.(3) Estimated. Allowable stress would be 400

Estimated. Allowable stress would be 400 psi if k were 300.



Induced Pavement Stress/Required Thickness	Eubgrade Rating Allowable L-2000B-2707CORDE B-747 L-500 -63 B-707 -55	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $				$400 \qquad \frac{470}{15} \qquad \frac{366}{12} \qquad \frac{407}{13} \qquad \frac{340}{11.5} \qquad \frac{300}{10} \qquad \frac{410}{13} \qquad \frac{375}{12.5} \qquad \frac{385}{12.5}$					
Rigid Pavement	Concrete Subbase Rating ThicknessThickness "k"	13 300	12 300				13 300					
Airport:	Puerto Rico	Critical	Noncritical	sken	vanA		All	norq	A but	2 ske	WİX6'	L



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S	DC-8 -55	<u>428</u> 12.5	<u>536</u> 10				<u>1000+</u> 14.5	428 12.8	<u>472</u> <u>13.5</u>			
Induced Pavement Stress/Required Thickness	B-707	<u>416</u> 12.5	<u>520</u> 9.5				<u>1000+</u> 14.5	<u>416</u> 12.5	<u>460</u> 13.5			
uired T	10-8 -63	<u>455</u> 13	<u>570</u> 10.5				<u>1000+</u> 15.5	<u>455</u> 13	<u>500</u> 14.5			
ss/Req	L-500	<u>326</u> 10	<u>399</u> 7.5				<u>850</u> 12	<u>326</u> 10	$\frac{367}{11}$			
nt Stre	B-747	$\frac{379}{11.5}$	<u>480</u> 9				$\frac{1000+}{13.5}$	$\frac{379}{11.5}$	<u>418</u> 12.5			
Paveme	CON- CORDE	<u>450</u> 13.5	<u>567</u> 10.5			_	<u>1000+</u> 15	<u>450</u> 13.5	4 <u>95</u> 14			
iduced]	L-2000B-2707CORDE B-747	<u>406</u> 12	<u>506</u> 9.5				<u>1000+</u> 1	<u>12</u>	<u>451</u> 13			
Ir	L-2000	$\frac{511}{15}$	<u>613</u> 12				1000+ 17.5	511 15	<u>578</u> 16.5			
	Lbgrade Rating Allowable "k" Stress	400	550				350	400	400			
Rigid Pavement	Subgrade Rating "k"	300	300				250	300	200			
Rigid Pa		36	36				∞	24	8			
	Concrete Subbase ThicknessThickness	12	10				5	12	12			
Airport:	Denver	17L-35R Critical	17L-35R Noncritical				8R-26L Taxiway	17L-35R Taxiway	Apron			
Air				slen	nn A		8	norq	A bus	s s k e	wixe'	L

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	8-55	CBR													9
	DC-8-	FAAC	21.5	17					21.5					1	1
	07	CBR					†								
	B-707	FAA	20.5	16.5					20.5				1		
•	-63		~~~~						- ~				†		ĺ
ness	DC-8-63	FAACBR	22	17.5					22						
hick		CBRF											<u> </u>		
ent T	L-500	FAAC	16	13					16						
Pavement Thicknes	47	BRF													
ed P	B-747	FAACBR	18	14.5					18						
Required	Ш	_				-									
Ŗ	CONCORDE	FAA CBR	22.5	18					22.5						Į
			~						<u>_</u> N						
	B-2707	FAACBR	20	16					20						
	000	CBRI													
	L-2000	FAA	23	18.5					25						
	rade ng	К													
nent	Subgrade Rating	baseness FAACB	F3	F3					F3						
aven	Total	iess]	31	26					29						
ble [:] F	4.5	baser	15	10					15						
Flexible [:] Pavement			10	10					11						
		faceBase	9	6					3						
ort:		Denver	8R-26L Critical	8 R- 26L Noncritical					All						
Airport:					sken	van H			S	pron	A bri	e sys	WİXG	Т	

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OF UNLY DC-8 -55 <u>650</u> 14.5 505 14.5 375 14.5 Induced Pavement Stress/Required Thickness B-707 630 <u>485</u> 14.5 <u>365</u> 14.5 DC-8 -63 395 <u>685</u> 15 530 L-500 380 <u>292</u> 12 480 L-2000B-2707CORDE B-747 <u>330</u> 13.5 <u>570</u> 13.5 445 <u>675</u> 15 <u>530</u> <u>390</u> 15 <u>475</u> 14 350 14 <u>605</u> 14 460 735 600 Subgrade Rating Allowable "k" Stress 350 350 350 **Rigid Pavement** 250 250 250 τŋ Concrete Subbase ThicknessThicknes 9 inches 11 inches 14 inches 9L-27R Noncritical 9L-27R Critical Atlanta Apron Airport: enorgh bas evewixeT Runays NLY

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	DC-8-55	CBI													· · · · · · · · · · · · · · · · · · ·	9
	DC-	FAACBR							29							
	07	FAACBR FAACBR FAACBR FAACBR														
	B-707	AA			<u> </u>				28							
	63	BRF														
s S	DC-8-63	AAC														
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t Th	L-500	ACB							8							
men		RFA.		ļ	ļ				18							
Pave	B-747	CBF														
R .quired Pavement Thickness	в-	FAA							25							
inbr	RDE	CBR														
a a	CONCORDE	FAACBR							31							
	B-2707	FAACBR							28							
	\vdash	CBRF						_								
	L-2000	FAAC							32							
-	200						_							-		
r I	Subgrade Rating	ACE							5							
emei	Sul R	sFA) F5							
Pav	Tota	basquess FAA CBR							29							
Flexible [.] Pavement	بر ن	base							20							
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ITEM	L-2000	B-2707	CON- CORDE	B-747	Т-500	DC-8 -63	B-707	DC-8 -55
Anchorage International				No overlay	No overlays required			
Atlanta								
Runway 9L-27R, critical section	10 \$133	5 \$ 66	6.5 \$86	\$ 53	2 \$27	6.5 \$ 86	\$80 \$80	\$80 \$80
Runway 9L-27R, noncritical section	11 \$585	8 \$4 25	9 \$4 78	7 \$370	5 \$265	9 \$4 78	8 \$4 25	8 \$4 25
Rigid Apron Section	\$600	01	2 \$200	01	01	2 \$200	01	01
Cleveland Hopkins International								
Taxiways	3 \$96	0 1	О 1	0 1	01	0 1	0 1	0 1
Terminal Apron	6 \$264	2 \$88	\$ \$176	01	0,	\$ \$ 176	3 \$132	3 \$132
Detroit Metropolitan Wayne County								
Runways, critical sections	8 \$176	3 \$66	\$ 88	2 544	0 1	4 \$88	3 \$66	3 \$66
Runways, noncritical	5 \$475	2 \$ 190	2.5 \$237	01	0 1	2.5 \$ 237	2 \$190	2 2 2
Taxiways and Apron	9 \$2,000	5 \$ 1, 120	\$1, 340	3.5 \$780	01	6 \$1,340	5 \$ 1,120	5 \$1,120
Dulles International, Washington				No overla	No overlays required	P		
Friendship International, Baltimore				No overla	No overlays required	U		



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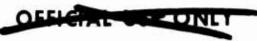


ITEM	L-2000	B-2707	CON- CORDE	B-747	L-500	DC-8 -63	B-707	DC-8 -55
Greater Pittsburgh								
Runway 28R-10L, critical section	3 \$20	01	2 \$13	0 1	0 ;	\$13	0 1	0 1
Runway 28R-10L, noncritical	2.5 \$157	0 ;	01	01	01	01	0 i	01
Taxiways and Holding Aprons	\$140	0 1	2 \$93	01	0 1	2 \$ 93	0 1	01
Terminal Apron	6.5 \$182	3 \$82	5 \$140	2.5 \$70	01	5 \$140	4 \$112	\$ 112
Honolulu International		1						
Runway 8-26, critical & Taxiway A *	7 \$50 4							
Terminal Apron, rigid	6 \$4 20	2 \$140	3 \$210	0 1	0 1	3 \$210	2 \$140	2.5 \$175
John F. Kennedy International								
Runway 13R-31L, critical	3 \$70	01	01	0 1	0 1	0 1	0,	0 1
Rigid pavement, 13 inch	4.5	01	2 \$773	01	0 1	2.5 \$965	0 1	01
Flexible pavement, 22 inch ⁺	8 \$3, 040	0 ;	2 \$760	Ċ I	2 \$760	2 \$760	0 1	••
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No cost using FAA methodology.
 + CBR method - no FAA data available.

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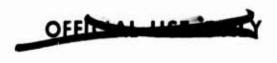
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ITEM	L-2000	B-2707	CON- CORDE	B-747	Г-500	DC-8 -63	B-707	DC-8 -55
Lambert - St. Louis Municipal Runway 12R-30L, critical section, and applicable taxiways and apron areas	4 \$545	0	0 1	0 1	0 1	0 1	0 1	0 1
Logan International, Boston				No overla	No overlays required			
Los Angeles International								
Runway 25L-7R, Critical portion, flexible construction *	4 .5 \$ 58	0 1	0,	0 1	0 1	0 1	0 1	01
Runway 25L-7R, noncritical flexible construction *	14 \$1,680	5 \$600	6 \$ 720	2 \$240	8 \$960	7 \$840	6 \$720	\$ \$ 720
Rigid pavement, 12 inch critical, including rigid aprons & taxiways	4.5 \$1,210	0 1	2.5 \$675	01	01	2.5 \$675	01	0 1
Taxiway 2J *	25 \$7	10 \$ 3	\$ 3	\$ 2	18 \$5	51	6 E	6 E
Taxiway 53J & portion of K *	18 \$1,780	8 \$790	9 \$880	5 \$880	11 \$1, 090	10 \$990	9 \$880	9 \$880
Terminal Apron, flexible *	4.5	01	0 1	0 1	01	0 1	0 1	01
* No overlave required using FAA								

* No overlays required using FAA methodology



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W	L-2000 B-2707	B-2707	CON- CORDE	B-747	L-500	DC-8 -63	B-707	DC-8 -55
Metropolitan Oakland International								
Rigid holding areas and south 400 ft of runway 29-11	7 \$10	01	2.5 \$4	0 1	0 1	2.5	\$3 2	\$ 3
Terminal apron, rigid	4 \$268	01	0 1	0 1	0 1	0 1	0 1	01
Miami International								
Terminal Apron, 8 inch rigid with 3 inch overlay	7 \$547	3 \$234	4.5 \$350	2 \$156	01	4.5 \$350	3 \$234	4 \$ 312
Terminal Apron 10 inch rigid	6 \$4 50	2.5 \$188	5 \$375	2 \$150	01	5 \$375	3 \$225	\$300

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ITEM	L-2000	B-2707	CON- CORDE	B-747	L-500	DC-8 -63	B-707	DC -8 -55
Minneapolis-St Paul International	(
Runway 29L-11R, 11 inch critical	888 \$	3°2 \$39	6 \$ 66	2.5 \$28	0 1	\$66 \$66	\$44	\$55 \$55
Runway 29L-11R, 9 inch, noncritical	8 \$532	\$ 266	\$400	3 \$200	01	\$ \$ 400	4 \$266	5 \$ 333
Runway 29L-11R, 12 inch noncritical	3 \$ 100	0 1	0 1	0 1	0 1	0 1	01	0 1
Aprons and Taxiways	\$ \$ 1,140	2 \$380	4 \$760	01	0 1	4 \$ 760	2.5 \$475	3 \$570
New Orleans International								
Apron, 9 inch concrete	18 \$684	12.5 \$475	14 \$532	11 \$4 18	о \$ 342	14 \$532	12.5 \$475	12.5 \$4 75
Apron, 12 inch concrete	13 \$494	7 \$266	9 \$342	6 \$228	\$ \$ 152	9 \$ 342	7 \$266	7 \$266
O'Hare International Airport, Chicago								
Runway 14R-32L, critical, taxiways and apron (rigid)	7 \$1,750	0 1	2 \$500	0 1	0 1	\$500	01	2 \$500
Runway 14R-32L, noncritical (rigid)	6 \$636	01	212 \$	01	0 1	3 \$318	2 \$212	2 \$212





ITEM	L-2000	B-2707	CON- CORDE	B-747	L-500	DC-8 -63	B-707	DC-8 -55
Philadelphia International Rigid Taxiways and Apron	12 \$1,820	6.5 \$985	8 \$1,210	5 \$757	2.5 \$379	8 \$1,210	6.5 \$985	7.5 \$1,140
Portland International Runway 10R-28L Both critical and noncritical *	3 \$196	01	0 1	0 1	0 1	0	0 ;	0 ;
Taxiway adjacent to 10R-28L *	9 9 \$	01	01	01	0 1	0 1	0 1	0 1
Puerto Rico International Runway 7-25, critical plue tariways and aprone	3 \$360	0 1	0 1	0 1	0 1	0 ;	01	0 1
San Francisco International Rigid Pavement, 13 inch	5.5 \$253	0 1	\$138	0 1	0 1	3 5 138	2 \$ 92	2 2 8
Flexible Pavement, noncritical *	\$ 35 4	010	0 1 0	0 1 0	0 1 0	010	0 1 0	010
Flexible taxiways and apron areas *	\$2, 450	> 1	5 1	• •	> 1)		• •

No overlay required using
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ITEM	L-2000	B-2707	CON- CORDE	B-747 L-500	L-500	DC-8 -63	B-707	DC-8 -55
Seattle - Tacoma International								
Runway 16L-34R, critical and Taxiway 6 and holding apron	5 \$83	0 1	2 \$33	01	0 1	\$ 33	0 (01
Aprons and Taxiways, 10 inch	8 \$600	3 \$ 225	5 \$375	2.5 \$188	0 1	5 \$375	\$300	\$ \$300
Sky Harbor Municipal, Phoenix								
Runway 8R-26L, critical	7 \$189	2.5 \$68	4 \$108	2 \$54	0 1	\$ 1 08	3 \$81	3 \$81
Runway 8R-26L, noncritical *	4 \$304	0 1	01	0 1	0 1	01	0 1	0 1
Flexible taxiways and holding areas *	6 \$ 421	0,	3 \$ 210	01	2 \$ 140	3 \$ 210	2 \$140	2 \$ 140
Flexible portion of terminal apron *	8 \$ 361	3 \$135	5 \$ 225	2 \$90	4 \$180	5 \$ 225	4 \$180	4 \$ 180
Rigid portion of terminal apron	7 \$315	2.5 \$113	\$ \$ 180	2 \$90	0 1	\$ \$180	3 \$135	3 \$135

* No overlay required using
 FAA Methodology

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DC-8 -55	0 5.5 \$421	N C 0 1 0 1 \$
B-707	0 - 5 - 5 - 5 - 5 - 5	0,0,0,
DC-8 -63	\$142 \$142 0 5673	2 2 2 2 3 8 5 2 4 8 5
L-500	0 1 0 1	0 1 0 1 0 1
B-747	0 1 0 1 0 1	0,0'0,
CON- CORD	2.5 \$178 0 - 5505	\$27 \$0 \$108 \$108
B-2707	0 - - - - 5337	013101
L-2000	\$355 \$355 \$238 \$1,780	\$68 \$150 \$108 \$108
ITEM	Stapleton International Airport (Denver) Runway 17L-35R (critical areas) and adjacent taxiway, rigid Runway 17L-35R, noncritical, rigid Apron area, concrete	Tampa International Critical portion of runway Noncritical portion Flexible Taxiways

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VII. MODIFICATIONS TO POTENTIAL SST AIRPORTS AND ESTIMATES OF NON-AIRLINES COSTS

A. Summary of Airport Pavement Strengthening Costs

The pavement overlay costs for each of the airports considered were determined in the previous section. These costs are summarized for aircraft at all of the airports in Exhibit 3. This exhibit indicates the costs for each aircraft under the assumption that no modifications have been accomplished for any previous aircraft; in other words, it is as though each aircraft were to be put into service on presently existing pavements. Exhibit 4 presents these results graphically. Results are in accordance with present knowledge concerning the commercial jets now in use; i.e., that some precent airport pavements require immediate strengthening. Also, the similar configuration of the Boeing and Douglas models which comprise (for the most part) the existing jet family results in closely parallel costs, with the DC-8-55 requiring a slightly higher level of overlays than the B-707-320. The stretched jets (DC-8-60 series) will stress all pavements to a greater extent than current models.

The results of the analysis regarding the high-capacity jets (B-747, L-500) are paradoxical in a sense, because they require even fewer modifications than present jets, despite their great size and weight. This is because of favorable flotation characteristics which more than offset the weight differential. Load per tire is low; one aircraft has 28 tires, and the other has 18.

The Concorde, which is being built by the British and French as a potential SST competitor, is similar in weight and landing gear configuration to the DC-8-63. Dual-tandem spacings are somewhat more narrow, but are also slightly longer. Modification costs attributable to this aircraft are somewhat less than those of the Douglas stretched jet.

The SST models in the American competition vary markedly in their configurations and in the costs of required pavement strengthening.





AIR POR TS	DC - 8 - 55	B-707	DC -8-63	B-747	L-500	CONCORDE	B-2707	L-2000
Anchorage	0	0	0	0	0	0	0	0
Atlanta	5 0 5	505	564	423	292	564	491	718
Cleveland	1 32	132	176	0	0	176	88	360
Detroit	1376	1376	1665	824	0	1665	1376	2651
Dulles, Washington	0	0	0	0	0	0	0	0
Friendship, Raltimore	0	0	0	0	0	0	0	0
Greater Pittsburgh	112	112	246	20	0	246	84	499
Honolulu	175	140	210	0	0	210	140	924
John F. Kennedy, New York	0	0	1725	0	760	1533	0	4850
Lambert-St. Louis	0	0	0	0	0	0	0	545
Logan, Boston	0	0	0	0	0	0	0	0
Los Angeles	1603 (0)	1603	2509 (675)	1122 (0)	2055 (0)	2278 (675)	1393	5342 (1210)
Metropolitan Oakland	5	ŝ	4	0	0	4	0	278
Miami	612	459	725	306	0	725	422	266
Minneapolis	958	785	1226	228	0	1226	685	1860
New Orleans	741	741	874	646	494	874	741	1178
O'Hare, Chicago	212	212	818	0	0	712	0	2386
Philadelphia	1140	985	1210	757	379	1210	985	1820
Portland	0	•	0	0	0	0	0	256
Puerto Rico	0	0	0	0	0	0	0	(0) 360
San Francisco	56	92	138	0	0	138	0	3057 (253)
Seattle - Tacoma	300	300	408	188	0	408	225	683
Sky Harbor, Phoenix	536	536	723	234	320	723	316	1590
(i	(017)	(917)	(227)	(144)	(0)	(288)	(181)	(204)
Stapleton, Denver	421	421	815	0	0	683	337	2373
Tampa	27	0	113	0	0	135	0	326
TOTAL	\$9445 (7522)	\$8402 (6479)	\$14149 (11880)	\$4798 (3536)	\$4300 (1925)	\$13506 (11468)	\$7283 (5755)	\$33456 (24674)
Notes: (1) Costs are in thousands of dollars	ands of dollars.							

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Costs are in thousands of dollars. For rigid pavements, the Westergaard analysis was used. For flexible pavement, both Corps of Engineers and FAA procedures were used, according to the availability of subgrade test results. If both were available at a single airport, the Corps of Engineers requirement was included in the cost analysis, and the cost results via the FAA method (usually lower) were placed in parentheses.

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EXHIBIT 3 - PAVEMENT STRENGTHENING COSTS

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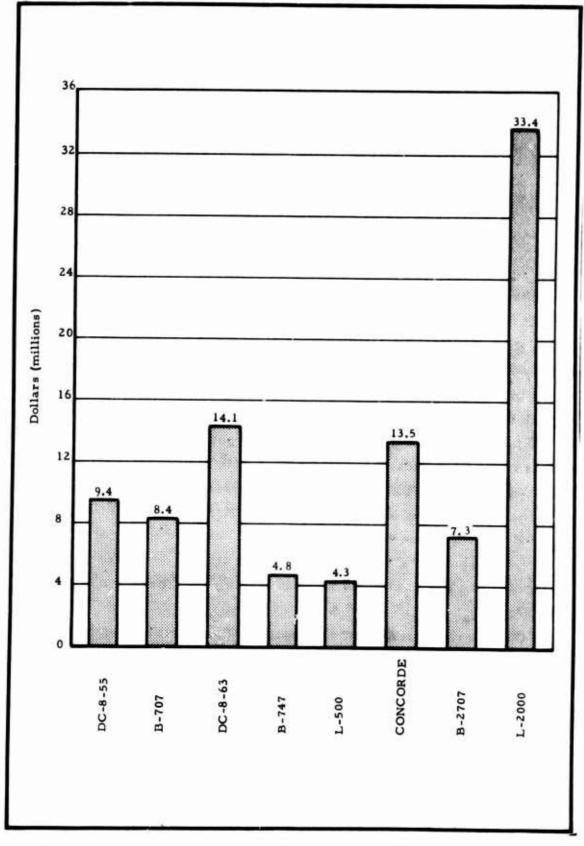


EXHIBIT 4 - PAVEMENT STRENGTHENING COSTS (BY AIRCRAFT) FOR POTENTIAL SST AIRPORTS AS THEY EXIST IN 1966

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B. Summary of Other Pavement Costs at Selected Airports

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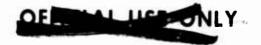
In addition to the strengthening of pavements now in existence, the requirement for which is occasioned by the great weight of future aircraft, certain new pavement costs can be allocated to future aircraft as a consequence of their increased length and wingspan. These include the widening of fillet radii at runway and taxiway intersections, increases in the size of holding aprons to accommodate larger airplanes, widening of terminal aprons and consideration of underlying structures.

1. Fillets

The inside portion of a turn being attempted by a large jet aircraft is important in that the landing gear must not be permitted to run off the pavement. This is normally avoided by paving an area in the angle formed by the intersecting runways or taxiways, the new edge being a circular curve the center of which is equidistant from the edge of the intersecting pavement lanes. The area encompassed by this curve is called a fillet. FAA standards currently call for fillets with a radius of 100 feet at a 90° intersection. Some airport pavements already incorporate these standards, while others still have them in the planning stage. It is notable that this standard is considerably in excess of requirements (including appropriate margins for pilot error) for current jets. However, some of the large aircraft considered in this study are not able to negotiate a 90° turn within such standards unless dangerously small margins are permitted between landing gear tires and edges of pavements.

Considering the extreme forward seating position of future SST pilots in relation to the landing gear, it is concluded that greater margins of safety are warranted for the larger aircraft than for present jets. The requirements set forth here for fillet radii are therefore considered to be absolute minimums for safe operation.

Evaluation of intersection fillet radii was accomplished through use of a scale model of the landing gear of each of the eight aircraft in the study. The scale used was 1 inch = 25 feet. Using each model, simulation of operations was conducted at intersections of (a) two 75-foot





taxiways, and (b) a 75-foot taxiway and a 150-foot runway. Angles of intersection of 90° , 45° , and 135° were considered for each intersection. In cases where an airport has important intersections not fitting any of these situations, separate simulations were accomplished.

In order to compensate for possible pilot error, and to encourage conditions under which normal turns can be conducted by large aircraft without undue delay and nervous strain, the following ground rules were established:

- At no time during the turn should the center line of a main or nose gear be allowed to be closer than 20 feet to the pavement edge.
- Prior to initiation of the turn itself, the nose and main gear may not leave their position astride the centerline of the pavement.

• A maximum nose wheel turning angle of 50° is permitted.

The requirement for fillet radii is a function of (a) the wheelbase of an airplane, and (b) the tread between the centerlines of the main gear. In the case of the B-2707 and B-747, the wheelbase used is the distance between the nose wheels and the centerline between forward and aft main gear, and the tread is based on the outside bogies. However, certain allowances were made where the requirement was on the margin, due to the fact that the steerable rear bogies can effectively shorten the turning length.

The results of the simulations, incorporating the appropriate safety margins, are shown in Exhibit 5.

Costs of the fillet enlargements at the various airports have been allocated to each aircraft in accordance with its requirements and are shown in Exhibit 6.

In computing these costs, only those intersections associated with the major runway or runways and the major taxiways likely to be used by the larger jets were considered. These are based on the areas included in the analysis of costs of pavement strengthening. In addition, a specific route from runway to terminal apron was assumed, and only the fillets of insufficient radius along that route were considered in the costing.



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EXHIBIT 5 FILLET REQUIREMENTS

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Ground rules:

- No bogie & closer than 20 feet to edge⁽¹⁾
 50° max nose wheel steer angle
 - Nose gear must remain on G of pavement prior to turn
 - Nose gear must never be closer than 20 feet to pavement edge

75' taxiway to 75' taxiway (90°)

B-2707	150' radius
L-2000	125' radius
Concorde	25' radius
B-747	100' radius
DC-8-63	50' radius
L-500	50' radius
B-707	25' radius
DC-8-55	25' radius

150' Runway to 75' taxiway (90°)

B-2707	100' radius ⁽²
L-2000	75 ['] radius
Concorde	0
B-747	50' radius
L-500	25' radius
DC-8-63	25' radius
B-707	0
DC-8-55	0

75' taxiway to 75' taxiway (135°)

B-2707	100' radius
L-2000	75' radius
Concorde	25' radius
B-747	50' $radius$ ⁽²⁾
L-500	25' radius
DC-8-63	50' radius
B-707	25' radius
DC-8-55	25' radius



EXHIBIT 5 (Continued)

75' taxiway to 75' taxiway (45°)

B-2707	200' radius
L-2000	150' radius
Concorde	25' radius
B-747	150' radius
L-500	25' radius
DC-8-63	25' radius
B-707	25' radius
DC-8-55	25' radius
L-500 DC-8-63 B-707	25' radius 25' radius 25' radius

150' Runway to 75' taxiway (135°)

B-2707	75' radius
L-2000	50' radius
Concorde	0
B-747	50' radius
L-500	0
DC-8-63	25' radius
B-707	0
DC-8-55	0

150' Runway to 75' taxiway (45°)

B-2707	75' radius
L-2000	0
Concorde	0
B-747	0
L-500	0
DC-8-63	0
B-707	0
DC-8-55	0

- Notes: (1) Except B-747, which has tread between outside bogies of 435", thus being within 19'5" of edge of a 75' taxiway when stationary.
 - (2) B-2707 slightly overlaps 20' limit with outside bogies. However, if wheelbase is shortened slightly to allow for steerable rear bogies (to rear wheels of front bogies or 1417'') the 150' and 100' radii are negotiated within the ground rules. Also applies to B-747 in case of 50' radius on 135° turn.





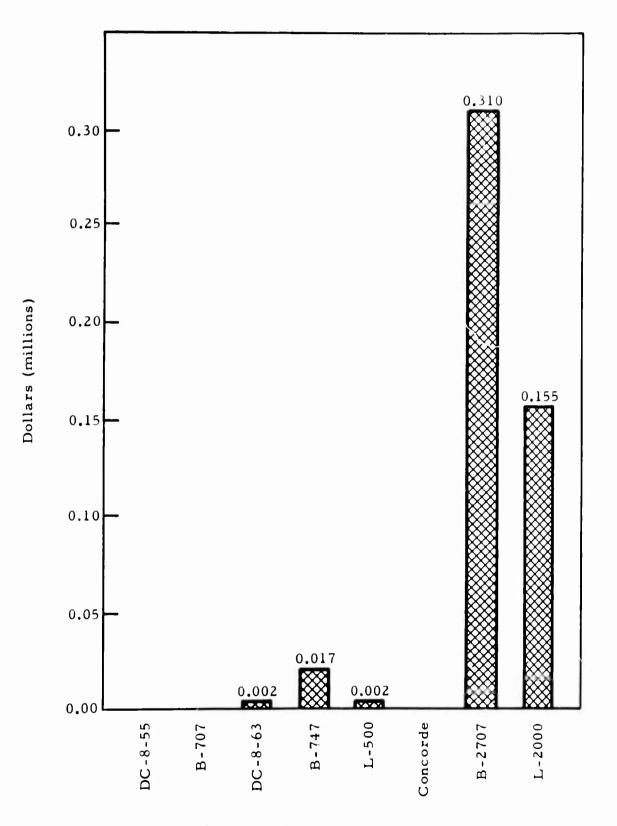


EXHIBIT 6 - FILLET MODIFICATION COSTS (BY AIRCRAFT)





The costs identified therefore represent the very minimum for operations of the larger aircraft in the study. Pavements costs were based on the thickness of adjacent existing pavement and on local prices.

When a fillet is enlarged it is necessary to move the edge lights. For costing purposes the expense of moving these lights was considered a constant of \$1,300 for each fillet altered. An additional expense associated with each fillet is the removal and renewal of the shoulders. While this cost is variable from airport to airport depending on local conditions, it is believed appropriate for the purpose of aircraft cost comparisons to base shoulder cost on the fillet paving cost. An amount equal to 30 percent of the new fillet pavement cost has been added in each case, representing the shoulder cost.

C. Conclusions Regarding Pavement and Structural Modification Costs.

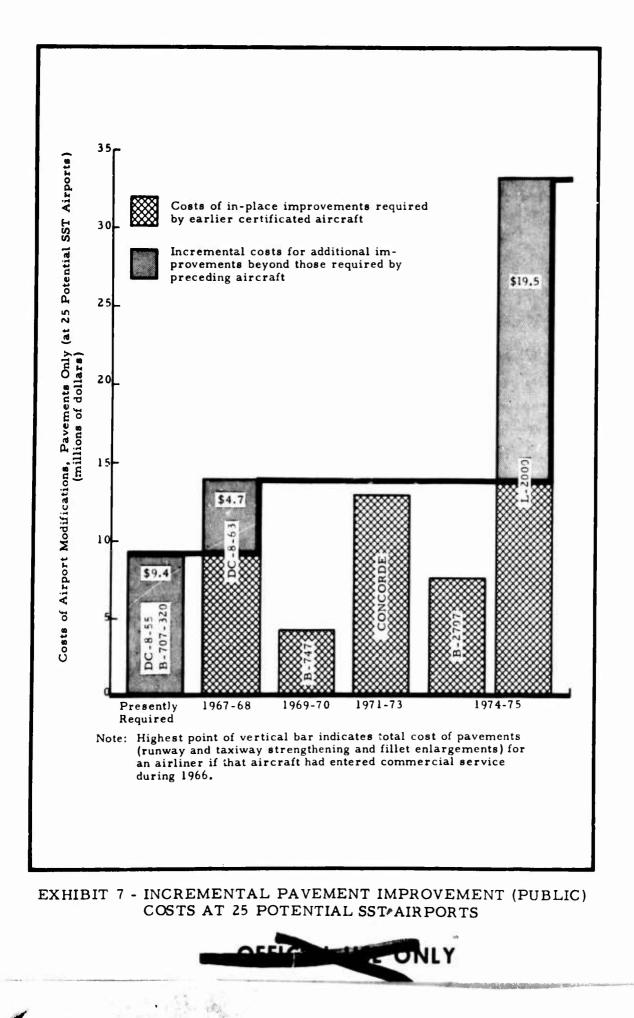
The combined costs for pavement strengthening, fillet enlargement, holding apron expansion, additions to terminal aprons, and structural modifications are shown in Exhibit 4 for each aircraft in the study on an individual aircraft basis. Exhibit 7 shows the time-phased incremental costs of airport improvement by aircraft. The assumption here is that pavements have been upgraded as required for each aircraft during the initial period of its operation.

It should be noted that present jet aircraft (DC-8-55 and B-707) are now operating in some cases on pavements which have been determined by engineering analysis to be deficient. Actual experience corroborates these findings at many airports where pavement deterioration and distress have occurred. The present jet aircraft require immediate expenditures for airport pavement improvements to meet analytical standards for unlimited stress repetitions. If these expenditures are made, costs required to qualify airports for future aircraft would be materially reduced.

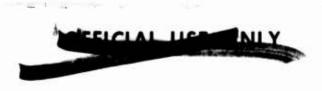
In addition to the costs associated with current jets, subsonic stretched versions require pavement modifications in the amount of \$4.7 million.







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No further costs would be incurred until the introduction of the supersonic transport, approximately in 1974.

In relation to the estimated development cost of the SST the associated pavement and structural modification costs are very small, regardless of which SST is built. This is true even if no modifications are undertaken for aircraft preceding the SST.



VII. FINANCIAL PARTICIPATION BY THE FEDERAL GOVERNMENT IN AIRPORT DEVELOPMENT

A. The National Airport Plan

1. Background

With the recognition of air transportation as a predominant feature of our modern culture and the airport as one of the basic components of the air transport system essential to manned flight, the Congress enacted the Federal Airport and Federal Aviation Acts. In response to the requirements defined within this legislation, the Federal Aviation Agency annually prepares and publishes the National Airport Plan. The Plan identifies the existing and new airports which characterize the national system of airports and recommends development for the next 5 years to meet the needs of civil aviation.¹ Inclusion of a recommended airport development or improvement in the National Airport Plan indicates that such project is eligible for consideration for Federal financial assistance under the Federal-Aid Airport Program. It does not, however, represent ability, intent, or commitment to proceed on the part of local communities or the Federal Government.

The airport development contained in the latest Plan (FY 1966-70), is based upon the requirements of the family of aircraft in use or in production at this time. It does not include any airport improvement specifically to accommodate the supersonic transport. This aircraft is not expected to require greater runway length; however, some refinements of airport improvements may be necessary. As the SST development program progresses, required airport improvements will be identified and future editions of the National Airport Plan will include such recommendations when they can be substantiated.

2. The National Airport Plan, FY 1966-1970

The National Airport Plan for FY 1966-1970 lists 4,106 existing and new airports, heliports, and seaplane facilities which characterize

¹See Exhibit 8







D.

EXHIBIT 8 - RECOMMENDED DEVELOPMENT OF 28 SELECTED AIRPORTS IN THE 1966 NATIONAL AIRPORT PLAN

			0	URRENT		FORECAST	
METROPOLITAN AREA	HUS TYPE	AIRPORT	BASED AIRCRAFT	ENPLANED PASSENGERS (Mudeds)	RUNTAY CODE(2)	RUHWAY CODE	RECOMMENDED DEVELOPMENT
Anchorage	м	International ⁽¹⁾	103	1,703	10	10	Obstruction removal, expand parking apron, relocate entrance road with aircraft overpass, paving, mainte- nance equipment building, in runway lighting, re- habilitate field lighting system, miscellaneous.
Atlanta	L	Atlanta ⁽¹⁾	31	24,489	10	10	Land; construct runway and taxiway extensions; con- struct holding and terminal aprons; lighting; miscellaneous.
Cleveland	L	Cleveland- Hopkins ⁽¹⁾	141	12,853	9	10	Land (including land for ALS); expand apron; extend runway and taxiways; construct holding aprons; con- struct runway and taxiways; overlay runway; lighting; relocate FAA Facilities; miscellaneous.
Dallas	L	Love Fletd ⁽¹⁾	164	20,989	8	x	(No forecast, pending CAB decision in Dallas/Fort Worth Regional Airport Investigation.)
Fort Worth	S	Greater Southwest International ⁽¹⁾	18	454	9	x	(No forecast, pending CAB decision in Dallas/Fort Worth Regional Airport Investigation.)
Detroit	L	Metropolitan Wayne County ⁽¹⁾	135	10,165	10	11	Land; extend runways and taxiways; construct addi- tional taxiways, aprons and service roads; lighting; ro locate nav-aids; construct maintenance building; miscellaneous.
Washington, D.C. ⁽³⁾	L	Dulles International	20	4,082	11	11	Improve existing facilities.
Baltimore	м	Friendship International ⁽¹⁾	110	5,610	9	11	Land; site preparation, including grading for Runway 33L taxiway extension, and for R/W 15L-33R includin parallel taxiway; pave, mark and light R/W 33L and parallel taxiway extension with holding pad; extend R/ 33L In-runway lighting; airport fencing; approach clearing; road relocation or tunnel.
Pittaburgh	L	Greater Pitteburgh ⁽¹⁾	14	12,675	10	11	Land; extend parallel taxiway to 10L end of runway 10L-28R; extend runway 5-23, including parallel taxi- way; extend runway 10L-28R, including parallel taxi- way; reconstruct taxiway parallel to runway 5-23; re- construct terminal apron; lighting; miscellaneous.
Honotulu	м	International ⁽¹⁾	116	8,481	12	10	Extend runway; construct apron and taxiway; lighting; miscellaneous.
Hous on	L	Intercontinental ⁽¹⁾	0	9,467	9	9	Extend runway and taxiways, enlarge apron; lighting; miscellaneous. (This airport will ultimately accom- modate community's scheduled air carrier service.)
New York	L	John F. Kennedy International ⁽¹⁾	9	51,312	11	10	Construct aprons, access road, fire and crash building high speed exit taxiways; install in-runway lighting.
St. Louis	L	Lambert-St. Louis Municipal ⁽¹⁾	195	11,961	10	10	Land; construct runway extension, taxiways, apron an service roads; lighting; miscellaneous.
Boston	L	Logan International ⁽¹⁾	31	21,140	9	10	Land; prepare site for future airport development; con- struct heliport, additional taxiways, blast pad, plane parking apron and holding apron, extend runways and taxiways, pave holding apron. runway extension and associated taxiways. expand aprons, enlarge runway exits; lighting; miscellaneous.
Los Angeles - Long Beach	L	International ⁽¹⁾	16	39,423	11	11	Land; extend runway and taxiway; construct runway, taxiways and aprons; lighting; obstruction removal; miscellaneous.
San Francisco- Oakland	L	Metropolitan Oakland International ⁽¹⁾	300	783	10	10	Construct taxiway and apron; lighting; fire and rescue building; miscellaneous.



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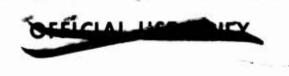


EXHIBIT 8 (Continued)

			c	URRENT		FORECAST	
METROPOLITAN AREA	HUB TYPE	AIRPORT	BASED	ENPLANED PASSENGERS (Mundreds)	RUNWAY CODE	RUNWAY CODE	RECOMMENDED DEVELOPMENT
Miami	L	International ⁽¹⁾		17,382	10	10	Land, strengthen runway and taxiways. lighting, miscellaneous.
Kansas Citv	L	Mid-Continent International ⁽¹⁾	0	0	9	9	Land: construct runways, taxiways, terminal and holdin; aprons (including general aviation areas); construct parallel entrance road, fire station; lighting; miscellaneous.
Minneapolis- St. Paul	1.	Minneapolis-St. Paul International (Wold-Chamber- lain) ⁽¹⁾	39	10,594	10	10	Land; reconstruct and extend runway; construct taxi- ways and apron; lighting; miscellaneous.
New Orleans	L	International ⁽¹⁾	0	8,958	8	9	Overlay runway and construct taxiways; lighting; miscellaneous,
Chicago	Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system Image: Second system <						
Philadelphia	L	International ⁽¹⁾	76	12,359	9	10	taxiways; construct parallel taxiway extension to run- way 27R; extend runway 17-35; extend parallel taxiway serving runway 17-35 including holding apron; construct extension to runway 9L-27R, including parallel taxiway
Portland	м	International ⁽¹⁾	76	5,014	н	10	Land; extend runway and taxiway; lighting; obstruction removal, miscellaneous.
San Juan	Ŀ		65	9,912	10	10	
San Francisco - Oakland	L	International ⁽¹⁾	61	24,893	10	10	ways and apron; lighting; fire and rescue building;
Seattle	L	Seattle - Tacoma International ⁽¹⁾	0	8,547	11	11	Construct taxiway; reconstruct taxiway; lighting; obstruction removal; miscellaneous.
Phoenix	М	Sky Harbor Municipal ⁽¹⁾	474	6,237	9	11	Land; extend runways and taxiways; construct and resurface taxiways, enlarge terminal aircraft apron; construct holding apron; lighting; miscellaneous.
Denver	L	Stapleton Inter - national Airport(1)	:100	13,173	11	12	Construct general aviation area: strengthen runway; lighting; miscellaneous.
Tampa-St. Petersburg	L	International ⁽¹⁾	56	6,230	н	10	Land, extend runways, construct taxiways and apron, lighting, miscellaneous,

Notes: (1) Airport has Federal Agreement (FAAP, etc.)

(2) Runway Codes: 8 = 8,000-8,999 ft; 9 = 9,000-9,999 ft; 10 = 10,000-10,999 ft; 11 = 11,000-11,999 ft; 12 = 12,000-12,999 ft.

(3) The airports and heliports shown serve the Washington, D.C. metropolitan area. Development of these facilities is performed under authority other than the Federal Airport Act and costs are not included in the plan.

Source: (a) Federal Aviation Agency, 1965 National Airport Plan FY 1966-1970



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the national airport system and are thus considered crucial to national air accessibility. Almost four-fifths of the airports (the term airports includes heliports and seaplane facilities) in the Plan are existing and comprise about one-third of the 9,490 of record. For a detailed breakdown by state see Exhibit 9.

Privately-owned airports are not eligible for Federal financial assistance under the Federal-Aid Airport Program (FAAP). All of the locations for which the Civil Aeronautics Board has authorized scheduled air carrier service based on a determination of public convenience and necessity are included in the Plan.

The annual national growth rate in air carrier and general aviation activity requires a continued reappraisal of the system of airports to assure that the National Airport Plan reflects these increasing demands and requirements.

A need for improvements before 1970 is anticipated at about 88 percent of the locations in the national system. The cost of improvements is estimated at \$975 million. The cost of building new airports, heliports, and seaplane facilities is estimated at \$304 million, with the airports accounting for \$293 million. For a detailed cost breakdown by state, see Exhibit 10.

The Plan is concerned primarily with the requirements of civil aviation and recognizes that in some instances military airports might also serve civil aviation, thus avoiding unnecessary duplication of facilities. If there is a military airport in an area where the establishment of a new airport or extensive development to an existing airport is contemplated, the military airport must be declared undesirable for joint civilian use before the new project will be considered for inclusion in the Plan.

Whereas the locations and development shown in the Plan indicate eligibility under the FAAP, there is no assurance, even with sponsor availability, that a specific location or the magnitude of development described will receive FAAP financial aid. Financial limitations or



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	GA Com.		- <u> </u>	
unction	GA Busn.		8 0 7 7 8 9 0 8 9 0 9 9 9 9 9 9 9 9 9 9 9 9 9 9	
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	Site Undecided		w.c.c	
	Total GA		776613382887733 7766613882733 776661388	
	Total AC/GA		- <u>~</u> 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2	
	Total		88888888888888888888888888888888888888	
	State		Alabama Arizona Arizona Arizona Arkansas California Colorado Connecticut Delaware Dist. of Col. Florida Georgia Hawaii Illinois Indiana Kentucky Louisiana Maryland Michigan Minesota Miseissippi Misesota Miseouri Miseouri Miseouri	

EXHIBIT 9 - NATIONAL AIRPORT PLAN STATISTICAL SUMMARY







	GA GA Com. Pers			42 11	ۍ 4	3 10	7 17		29 47	_			35 32	-		11	4	2	34 8	29 7	75 114	16 11	1 12			6 32				220
unction	GA GA Busn. Con	-		29	9		9	25	4	60	-	33	40	16	10	1	0	19	19	47	- 19	4	2		_		23	_	00	201 1 102
tical Fu	AC Heli.			0	0	0	0	0	٢	0	د	0	0	0	0	•	0	0	0	0	•	0	0	0	0				, o	
Aeronautical Function	AC Cargo			0	0	0	0	0	د [.]	0	•	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0		, c	0	
4	AC Local			10	2	0	٣	6	16	11	2	9	œ	10	œ	2	0	m	9	4	19	2	1	ŝ	2	11	a	<u>،</u>	1	
	AC Trunk			2	2	7	I	1	œ	4	4	9	ĉ	5	6	1	1	4	٣	ŝ	11	1	m	4	-	- 2	1	، ر	n u	346
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	Fed. Agree.	0	Numbers	72	13	11	6	33	35	38	34	25	69	38	51	m	'n	28	49	42	145	24	10	27	2	37	12	29		710 6
	No Devel. Recom.			22	7	1	0	1	2	ŝ	-	ĥ	ŝ	0	0	0	0	ŝ	5	2	76	4	0	0	0	5	0	23	2	419
	Site Undecided			1	0	m	12	2	39	01	ŝ	42	8	00	30	Ś	0	6		0	39	0	2	19	0	10	14	11	2	497
	Total GA			82	13	14	30	53	80	72	56	79	107	47	100	13	4	52	61	83	268	31	15	47	•	54	23	20	24	2 054
	Total AC/GA			12	4	2	4	10	24	15	9	12	11	15	17	m	-	2	6	6	30	m	4	6	m	13	10	17	10	108
	Total			94	17	21	34	63	104	87	62	16	118	29	117	16	Ś	59	20	26	298	34	19	56	m	67	33	87	34	3.855
	State			Nebraska	Nevada	New Hampshire	New Jersey	New Mexico	New York	North Carolina	North Dakota	Ohio	Oklahoma	Oregon	Pennsylvania	Puerto Rico	Rhode Island	South Carolina	South Dakota	Tennessee	Texas	Utah	Vermont	Virginia	Virgin Islands	Washington	West Virginia	Wisconsin	W yoming	Total Aimonte

EXHIBIT 9 (Continued)



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								Tur	Turbojet		4	Aeronautical	tical F	Function			
State	Total	Total AC/GA	T otal GA	Site Undecided	No Devel. Recom.	Fed. Agree.	Priv.	Ser	Service w Antic.	AC Trunk	AC Local	AC Cargo	AC Heli.	GA Busn.	GA Com.	GA Pers.	
L						Numbers	of	Heliports									-
California Connecticut Dist. of Col. Florida Illinois Indiana Michigan New Jersey New York	0 ~ 20 - N + NN	0 × 0 0 ~ - C 0 Å Å	1- N - 21- ON + OO	v. 0 0 0 → 0 0 0 0 0 0		0000000-0	2000m0000-	00000000000		0000000000	00000000000	00000000000	0 0 0 m m 0 0 0 0 0 0 1 m 0 0 0 0 0 0 m m 0 0 0 0 0	~ ~ ~ ~ 0 0 0 0 0	0001-000400	c c c c c c c c c c c c c c c c c c c	
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					Nur	Numbers of S	Scaplane	Facilitie	ies	4			1				
Alaska California Florida Maine Minnesota	6 7 	~ 0 0 0 0 x		-0-00	2032	~~ 0 0 0 -		00000	00000	00000		00000	00000	0000-	00-100	000-0	
Total Seaplane	+6	83	11	~	76	α.	13	0	0	0	83	0	0	-	6	1	
Total All	4,106	1,003	3,103	515	515	2,035	436	20	88	245	639	Г	119	1.237	1,135	730	

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PRC R-890 107

Source: (a) Federal Aviation Agency, National Airport Plan

(Continued)	
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EXHIBIT	



State	Land Acquisition	Site Preparation	Paving	Lighting	Safety Buildings	Misc.	Total
Alabama	\$ 2,369	ø	,02	2	T	\mathbf{c}	,05
Alaska	697	,87	6,44	96	87	1,53	.39
Arizona	1,488	-	,23	9	2	4	,31
Arkansas	543	, 75	,92	0		$\mathbf{\omega}$,83
California	40,047	7	,10	Ś	1,296	-	,49
Colorado	81				0		2
Connecticut	1,988	1,895	•	577	220		8,466
Delaware	0				60	69	6
Dist. of Columbia	0	0	0	0	0	0	0
Florida	7,601	.95	82	,58	437	6	7,58
Georgia	10,064	1,466	34	9	100	2	6
Hawaii	260	,00	03	,13	67	0	5,29
Idaho	581	410	70	6	160	6	,74
Illinois	30,749	,74	,79	4	9		42
Indiana	1,042	1,194	66	8	50	2	,69
Iowa	402	2	94	ŝ	243	2	,66
Kansas	392	46	,12	0	\sim		,88
Kentucky	2,537	S	41	2	60		,62
Louisiana	118	2	82	\mathbf{c}	125		,14
Maine	230	~	,98	9	S		,20
Maryland	1,025	,61	,16	8	0	,42	,41
Massachusetts	1,955	-	21	6	ŝ	3	,66
Michigan	7,671	,05	59	,64	9	,31	9,84
Minnesota	542	8	.97	4	~	2	,79
Mississippi	862	61	2,830	0	219	270	σ
Missouri	1,530	1,674	,48		9	6	,55
							~ 1

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EXHIBIT 10 - SUMMARY OF ESTIMATED REQUIRED AIRPORT DEVELOPMENT COST BY ITEM BY STATE, FISCAL YEARS 1966-1970⁽¹⁾

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PRC R-890 109

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	Land	Site			Safety			
	Acquisition	Preparation	Paving	Lighting	Buildings	Misc.		Total
1	\$ 240	6	0		ъ С	4	÷	.85
	3,024	δ	,22	0	25	38		.58
	69	135	\mathbf{c}	\mathbf{c}		0		08
New Hampshire	185	0	,00	2		8		47
	1,780	\sim	,88	0		6	-	.46
	763	4	,59	4	6	6		,82
	12,941	,66	,10	α	0	0	∞	0,50
North Carolina	1,114	4	,72	9	4	6		,22
North Dakota	60	7	,68	0		ŝ	_	48
	3,196	,30	,43	6	8	4	2	4,56
	863	2,626	3,662	386	160	198		7,895
	184	,30	,10	6		\sim		88
Pennsylvania	2,275	,11	:23	0		9	2	2,13
	756	,02	,07	S		S		,29
Rhode Island	500	∞	, 1 4	4		T		,89
South Carolina	105	45	44	œ	0			,03
South Dakota	270	8	9	4		8		,28
	541	\sim	,83	~			_	,42
	215	,12	,34	7		2		,99
	16	4	2	S				,42
	75	9	4	0				,28
	400	9	,98	6	4	S		,20
Virgin Islands	1,221	,16	2	4	60			,67
	820	4	,85	2		\mathbf{c}		,04
West Virginia	397	13,259	,04	2	2	9		.61
	945	,36	\mathbf{c}	7		6		,13
	54	4	3	9		ŝ		,05
Grand Totals	\$148,283	\$207,470	\$269,527	\$44,447	\$13,271	\$46,144	\$72	9,142

Airports Used by Both Scheduled Airlines and General Aviation

OFFICIAL USE ONLY.

EXHIBIT 10 (Continued)



	Grand Total	<pre>\$ 16,529 \$ 27,156 15,783 15,783 15,783 15,783 15,783 16,559 16,780 1,431 39,781 42,083 17,470 31,301 31,301 31,301 31,301 31,302 31,30 31,302 31</pre>
	Total	<pre>\$ 7,477 7,477 7,472 5,481 5,481 5,481 5,481 5,481 5,430 8,314 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,236 1,255</pre>
on Only	Misc.	<pre>\$ 934 263 321 321 3284 3,284 1,013 209 1,003 377 922 434 1,003 377 922 450 514 514 2504 514 264 504 504 504 1,112 264 283 281 132 281 281 281 281 281 281 281 281 281 28</pre>
Airports Used by General Aviation Only	Safety Buildings	<pre>\$ 0 124 124 927 927 927 336 35 35 35 35 00 1,300 1,300 1,300 248 24 24 24 24 333 90 2,000 2,000</pre>
ied by Gen	Lighting	<pre>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$</pre>
irports Us	Paving	<pre>\$ 3,197 3,124 2,715 16,069 2,715 2,715 2,715 2,715 2,726 2,726 2,726 1,195 2,726 2,195 4,195 2,275 2,275 4,195 2,275 2,275 2,275 2,275 2,275 2,275 2,275 2,275 2,275 2,293 2,275 2,275 2,275 2,293 2,275 2,293 3,275 2,293 3,275 2,293 3,275 2,293 3,275 2,293 3,275 2,293 3,275 2,27</pre>
A	Site Preparation	<pre>\$ 1,780 1,785 1,785 1,785 8,843 8,843 8,843 8,843 8,843 8,843 1,351 6,239 6,239 6,239 6,239 6,239 821 821 821 821 861 1,352 1,352 1,352 1,352 1,352 1,352 1,352 1,032 1,0</pre>
	Land Acquisition	<pre>\$ 821 122 20,183 20,183 1,582 1,582 1,582 3,826 3,826 3,826 3,826 3,825 1,941 1,172 3,522 3,057 3,676 3,676 3,676 3,627 419 1,172 1,172 412 1,172 412 1,172 412 1,172 412 1,172 412 1,172 412 1,172 412 1,172 412 1,172 41 41 412 41 4</pre>
	State	Alabama Alaska Arizona Arizona Arkansas California Colorado Connecticut Dist. of Columbia Florida Georgia Hawaii Idaho Illinois Indiana Idaho Illinois Indiana Kentucky Louisiana Maryland Maryland Maryland Michigan Minnesota Mississippi Mississippi Missouri Montana Nebraska Nevada New Hampshire

EXHIBIT 10 (Continued)



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EXHIBIT 10 (Continued)

Airports Used by General Aviation Only

C+++ C	Accuration	e ;			Safety		Ē	Ę
טומוב	Acquisition	Freparation	Faving	Buingit	Buitaings	MISC.	1 0 1 a 1	Urand 1 otal
New Jersey	\$ 4,623	~	,48	-4		0	,84	7,30
New Mexico	1,007	17	,69	82	~1	62	9,34	17.17
New York	16,117	5	Г		135		,60	.10
North Carolina	2,016	02	,53	2		S	8,94	7,16
North Dakota	426	Ó	,31		0	9	,35	4,83
Ohio	6,506	50	,74	,06		5	0,96	5.52
Oklahoma	3,333	2,132	7,790	1,105	69	881	15,310	23,20
Oregon	1,003	\sim	8	4		∞	,47	7,36
Pennsylvania	11,589		,43	7		0	,43	,56
Puerto Rico	992	1	,52	Ъ		5	44	.74
Rhode Island	30	-+	,28	2	220	∞	,08	.97
South Carolina	830	9	,21	~		0	,89	.92
South Dakota	591	\sim	,28	4		7	,35	0,63
Tennessee	2,791	-	4	\sim	35	-	4,12	54
Texas	7,940	ŝ	,66	∞		9	,23	9.23
Utah	169	\sim	,06	\mathbf{c}	137	~	,30	.73
Vermont	419	0	œ	9		2	,72	00,
Virginia	3,171	4	4	6		Г	;13	,34
Virgin Islands	0		0	0	0			.67
Washington	1,129	4	,32	~	75	8	,14	1,18
West Virginia	820	2,479	2,298	632	0	280	,50	.11
Wisconsin	1,286	7	,27	Г	0	9	,69	3,83
Wyoming	107	6	6		0			3,515
Grand Totals	\$157,076	\$119,989	\$197,318	\$33,684	\$7,116	\$31,614	\$546,797	\$1,275,939

Note: (1) Costs are in thousands of dollars. Source: (a) Federal Aviation Agency, National Airport Plan

PRC R-890 111



changing techniques in evaluating aviation need may overtake and preclude carrying out the published recommendation.

The National Airport Plan reflects the requirements for air access as they apply to the individual community, which, in a broader sense is as they apply to the nation. Air access is expressed in terms of locations which require public airports and the extent of facilities required.

TISE ON

3. Federal Aviation Agency--Civil Aeronautics Board Coordination

The Federal Aviation Act of 1958 imposes on the Civil Aeronautics Board and the Federal Aviation Agency the responsibility of encouraging and developing an air transportation system properly adapted to present and future needs of air commerce. The Board is empowered to regulate the airline route structure of the United States and to determine which communities shall receive airline service. It may designate the airports through which such service is to be provided, but this decision is usually left to airline management.

The Federal Aviation Agency is charged with the development of a national system of public airports to anticipate and meet the needs of civil aeronautics. The National Airport Plan, which represents that system, includes all airports used by the certificated air carriers and suggests developments to meet their future needs. Inasmuch as future airline-oriented requirements at these airports are based on the expectation of continued airline service, the FAA must look to the Board for information regarding its actions which might affect the future status of these locations. In order to coordinate the programs of the two Agencies, the Civil Aeronautics Board reviews that portion of the National Airport Plan relating to air carrier needs.

The Board reviews the Plan as it relates to certain of its own policy considerations and those formulated in conjunction with other agencies which bear on the future development of the certificated air carrier system.

Specific requests for aid under the Federal-Aid Airport Program are coordinated with the Board to determine whether Federal funds will be allocated for development to accommodate air carrier activity.





B. Federal-Aid Airport Program¹

1. Federal Airport Act

The Federal Airport Act places statutory responsibility with the Administrator of the Federal Aviation Agency for assisting, within the limit of funds available, in producing a system of public airports adequate to anticipate and meet the needs of civil aeronautics. The primary purpose of the Federal-Aid Airport Program is to assist each community which has a substantial aeronautical requirement in developing a new airport or in bringing its existing civil airport to a standard compatible with the present and future needs of civil aeronautics so that each airport will in fact be part of "a system of public airports adequate to anticipate and meet the needs of civil aeronautics."

This Program is not limited to any class or category of public airports. However, financial assistance under the Program is available only to public agencies, such as states, counties, municipalities and other political subdivisions and agencies. Federal grants under the Act are on a matching basis; the Federal Government generally provides 50 percent of the cost of the airport development and the local public agency provides the remaining 50 percent.

2. Programmed Assistance in Airports Development

Projects considered for programming under FAAP are in one of two categories: airports used by all segments of civil aviation or airports used exclusively by general aviation.

In this summarization of the FAAP programming, only the first category is pertinent.



¹Federal Aviation Agency, Advisory Circulars AC 150/5100-1, <u>Information on Federal-Aid Airport Program (FAAP)</u>, 15 April 1965, and AC 150/5100-2, <u>Priorities Under the Federal-Aid Airport Program</u> for FY 1967, 9 May 1966

Development of airports used by both air carrier and general aviation is considered for programming, within the limitations of the National Airport Plan, on the basis of the requirements under the Federal Aviation Agency airport design criteria. (See Appendix A for reference to design criteria.)

DISE ON

a. <u>New or Replacement Airports</u>

Federal participation in the construction of new airports is considered in communities where (1) the volume of air traffic now or projected for the future exceeds the potential capacity of the existing airport; (2) the existing airport cannot economically be improved to handle its air traffic safely and adequately; (3) the area lacks an airport but facts indicate a need for one; or (4) one new airport can serve one or more communities more efficiently than existing facilities. The majority of communities can be adequately served by one properly planned, well-developed civil airport. It is desirable that new or replacement airports be located to best serve area or regional needs. Joint ownership or support by two or more communities is preferable in these cases. The following situations describe cases in which a new airport may be needed:

- An airport serving the community can no longer efficiently and safely accommodate all types of operations due to total volume. Annual air carrier operations in excess of 30,000 are used as a guide to determine when a study should be made as to whether a separate airport is needed for general aviation.
- There is no existing airport with the capacity or potential for development to serve the anticipated aeronautical requirements of the area.

b. Area or Regional Airports

Communities are urged to give careful consideration to the designation of one airport to serve two or more communities located in fairly close proximity to each other. This is for the purpose



of obtaining improved service and economy in airport development, operation and maintenance. These are important factors to be considered by sponsors in preparation of Requests for Aid under the Federal-Aid Airport Program.

c. Airports to Relieve Congestion

The Federal Airport Act authorizes a special Discretionary Fund for the development of airports the primary purpose of which is use by general aviation and which relieve congestion at airports with a high density of traffic by other segments of aviation; but which are not restricted to general aviation alone.

d. Long-Range Planning

Federal-Aid Airport Program funds are generally available only to provide long-range solutions to community airport problems. The development or improvement of a facility which may be replaced in a very few years, or other short-range solutions, will be considered only when the facts balanced against the funds required justify such a solution.

- 3. Allocation of Federal Funds
 - a. Rationale

Federal funds available for airport development under the Federal Airport Act are usually less than the Requests for Aid submitted by sponsors. Therefore, it is necessary to establish priorities to be used in allocating appropriated funds. The priorities applied in allocating these funds are listed in descending order of priority in 3. b.

According to the Federal Airport Act, projects eligible for consideration should include all types of airport development and should not be limited to any classes or categories of public airports. Within the limits of discretion permitted by the Act, the FAA uniformly applies the priorities on a national basis. In those states where the program can be supported entirely within State Apportionment Funds, allocations may be made under lower priorities than would be the case where Discretionary Funds are essential to the state program. Airports used





by general aviation are not eliminated from consideration in the Fiscal Year 1967 F gram. The application of priorities is intended to provide the greates , public benefit from available Federal funds.

b. **Priorities Schedules**

The priorities observed by the decision maker in allocating Federal funds for airport development under the Federal-Aid-Airport Program are these:

(1) Urgent safety facilities to support all-weather operations at major air carrier airports. This covers in-pavement lights, high-intensity runway edge lighting, land for the approach lighting system, and generators for standby power at "continuous power airports."

(2) Development for improved service of modern equipment now being acquired by the scheduled airlines. This covers lengthening, strengthening, widening, and marking of runways and taxiways with related land acquisition for the accommodation of new jet aircraft.

(3) Improvements to provide additional airport capacity required by scheduled airlines and air taxis such as parking aprons, secondary runways, and additional taxiways.

(4) Development at airports which accommodate a high volume of activity or tend to divert aircraft operations from the busy metropolitan area airports serving scheduled air carriers.

(5) Development for public use by general aviation at airports in medium and small communities.

(6) Development needed under the National Airport Plan not covered by the first five priorities.

C. Probable Federal Assistance beyond 1970

Federal expenditures at airports for the period 1947-1964 averaged approximately \$41million per year Public Law 88-280 approved in March 1964 provided appropriation authorizations of \$75 million for each of the years 1965, 1966, and 1967.

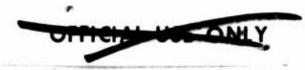
Although the Federal Government's participation in airport development has gradually increased, aviation technology and activity have grown





at a much faster rate, leaving airports generally under-equipped to cope with the magnitude of air traffic--both passenger and cargo--which will certainly be experienced beyond 1970.

Air traffic growth nine years ago began a progressively widening rift between air commerce domands upon airports and federal financial participation in airport development. As a result, airport adequacy has not kept pace with the needs. The rate of airport improvement (land acquisition, pavement, lighting, support facilities, etc.) must be accelerated in order to cope with the demand of increased air travel. It appears incontrovertible that Federal assistance must without delay be increased substantially in order to assist local, county, or state governments in meeting these demands within the context and intent of a truly national air commerce plan.





IX. CONCLUSIONS

Only minor modifications are required to qualify appropriate air terminals for SST operation. All necessary improvements fall in the pavements area; e.g., thicker concrete and larger fillets will be required. Alteration or replacement of buildings in the terminal complex cannot be attributed to the SST, but rather to continually increasing air traffic volume. Independent analysis of pavement adequacy at each of the potential SST airports considered for the two competing SST designs suggests that the SST could require improvement programs which would range from \$15 million down to zero dollars, depending on which aircraft design is selected.

In relation to the development cost of the SST, the pavement strengthening costs are very small, regardless of which SST is built. This is true even if no modifications are undertaken for aircraft preceding the SST.

The airport modifications are expected to be accomplished over a time span of several years, thus the total modification funds will not have to be available at the time the SST becomes operational.





X. RECOMMENDATIONS

During the course of the SST economic impact study, related areas which warrant further comprehensive investigation were identified. The more prominent areas are briefly described in this section.

A. Identification of Potential Gateway Airports

As part of its long-range planning, the Federal Aviation Agency should predict 10 years in advance which m; jor airports (both large and medium hubs) have the potential to become international air terminals. These long-range projections should be reviewed and updated on an annual basis with a 5-year firm plan as an implementing directive.

The short-range, 5-year projection should be the basis for FAAsponsored coordinating seminars among interested and concerned parties; e.g., Federal inspection agencies, the Post Office Department, U. S. air carriers (both scheduled and supplementary), foreign carriers, freight forwarders, and local and regional commerce, industry, and planning representatives.

B. New Airport Construction Programming

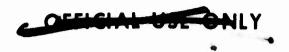
In a manner similar to that described above, the FAA should establish a continuing capability to predict airport saturation and replacement schedules. As an instrument for oversight of United States air commerce, the FAA should annually assess for each of the major hubs:

- Responsiveness to air commerce requirements in a national context
- Capability for continued growth as required by increasing passenger and freight volumes.

The FAA should further project the status of those airports for a period of 10 years into the future.

Where the requirement for a new airport is identified, the FAA should sponsor coordinating discussions with the affected communities





within the region to be served. In this manner a smooth and orderly transition would be ensured from a situation wherein an airport approaches the condition of becoming saturated or unmanageably large, to the implementation of acceptable remedies such as phase-out of the existing airport or transfer to the status of a general aviation terminal, supplementation of the existing airport(s) by the construction of an additional facility, or replacement of existing airport(s) with a new, regional service airport.

C. <u>General Acceptance of a Universal</u>, Standardized Pavement <u>Analysis Method</u>

The FAA should sponsor the development of a single, standard methodology for determining pavement requirements at airports which would receive general acceptance within the aviation community. The several evaluation techniques currently employed by airport engineers resist correlation and separately provide an unacceptable margin for error. A uniform, scientific method of measuring pavement stress capability is essential as a basis for national and international comparison of airport abilities to accept future aircraft.

D. Airport Adequacy Survey

An airport adequacy survey of foreign air terminals should be undertaken as soon as practicable after FAA adoption of a uniform airport pavement evaluation system. Potential SST airports should be examined first. These would include all major European airports, most Asian airports, and principal African, Australian, and Oceania airports. The Central American and South American airports present a particularly attractive situation because this survey would provide an opportunity for the United States to assist its southern neighbors in a demonstrably pragmatic manner. Central and South American citizens appreciate engineering assistance which, as in the case of the intercontinental jet airliner, promises technological and economic progress to the regions surveyed.





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101/101