

Best Available Copy



CONTENTS

Page

S STRUCTURE CON

وود بر ا

For	'exord	
Abs	lract	
1.	Introduction	1
3.	Solutions of the Membrane System	2
3.	Behavior of Membrane Solutions as $S \rightarrow O$	5
4.	Natural Frequencies for a Free-Edged Hemisphere	7
5.	Discussion	10
ó.	References	15

ABSTRACT

worker the street of the street

;

In this paper the meabrane solutions for non-symmetric vibration of a spherical dome are studied. The solutions are written in a convanient form, and it is shown how these reduce to the familiar membrane and inextensional solutions in the static limit. This information enables one to perceive several difficulties in finding inextensional frequencies by numerical means and to suggest ways around these difficulties. Also membrane frequencies are found for circumferential wave numbers up through eight by direct calculation and compared with several different approximations. One type of approximation, due to Jeffreys and Jeffreys, gives quite good results. It is seen that earlier work agrees well with these results except for a few frequencies which are not found at all in the present calculations.

.

÷

. *

4. 1. A REAL AND A DECEMBER OF A DECEMBER

i,

11.1.1

1. In roduction

It is dyring the behavior of tents and parachates it is pertinent to start the vibrations of this shells. In this paper we shall focus our attention on the non-symmetric vibration of this spherical shells. Within the classical this-shell theory the governing system of equations is of eighth order, and solutions in the form of Associated Legendre Functions have been found by Kalnins and Wilkinson¹ and Prasad². Four of these solutions are of bending type and can often be approximated with the aid of the asymptotic methods used by the writer^{3~5}. Although we shall make some remarks about these solutions, our main concern here is with the remaining four solutions, which are of membrane type.

We shall first write down these four solutions in various forms that are useful and shall describe some approximations that are applicable in several limiting cases. Then in Section 3 we shall present formulas showing how these dynamic solutions reduce to the familiar static membrane and inextensional solutions as the dimensionless frequency, Ω_{-} , tends to zero. It is helpful to have this information, in particular, to know what linear combinations of the Legendre Function solutions approach the inextensional solutions as $\Omega \rightarrow 0$, before one tries to deduce inextensional frequencies and modes from the Legendre Function solutions. This new information should help in evading the difficulty that has been experienced (see $Hwang^6$) in making these computations. Section 4 contains results about membrane natural frequencies for hemispheres with free-edges. These results are compared with each other and also with the earlier calculations of Naghdi and Kalnins⁷. The results are discussed in Section 5.

1. Steffer of the Metbrane System

The low membrane solutions will be designated as $\mathfrak{A}_{j}^{\mathfrak{m}}$ and have been given in terms of Associated Legendre Functions by Naghdi and Kalnins⁷. We shall use slightly modified versions of their solutions, which are convention studying the limit as $\mathfrak{A}_{=>0}$.

shells of revolution) and

$$\lambda = (1 - \Omega^{2}) / [1 + (1 + \nu)\Omega^{2}]$$

$$(n + \frac{1}{2})^{2} = (3/2)^{2} + (1 + \nu)\Omega^{2} [3 - (1 - \nu)\Omega^{2}] / (1 - \Omega^{2})$$

$$(k + \frac{1}{2})^{2} = (3/2)^{2} + 2 (1 + \nu)\Omega^{2}$$
(3)

(I)

where \mathcal{D} is Poisson's Ratio. The functions Z_n^m and Z_n^m are related to the Associated Legendre Functions by e.g.

$$Z_{n}^{m}(\cos \phi) = (-2)^{m} n! \frac{\Gamma(n-n+1)}{\Gamma(n+n+1)} P_{n}^{m}(\cos \phi)$$
$$= \sin^{m} \phi F[1+n+n, n-n; n+1; \frac{1}{2}(1-\cos \phi)]$$

where $F(\ldots)$ denotes the hypergeometric function. We shall also use the representation $\int = (2\pi n^{1/2})^{1/2} \mathbb{P}\left[-n, n^{1/2}, n^{1/2}, \frac{1}{(1-\cos^{2})}\right]$ (3)

when we be derived from the definition by a familiar property of the hopes constrict function.

A useful pair of asymptotic formulas for $P_n^{\pi}(\cos \beta)$ when $n \in \bot$ m are both large and

$$x \neq n \sin \beta$$
 (6)

has been given by Jeffreys and Jeffreys⁸. From them we derive the following asymptotic formulas for $2n^{m}$:

$$\sum_{n}^{n} \sim \sum_{n}^{n} (N-n\cos\beta)^{-n-\frac{1}{2}} (N-n\cos\beta)^{-n} = \sum_{n}^{-\frac{1}{2}} \sin^{2}\beta$$
(7)

where

$$\sum_{n}^{n} (\pi^{2} - n^{2} \sin^{2} \beta)^{\frac{1}{2}}$$

$$\sum_{n}^{n} = 2^{n} \frac{n! n!}{(n+n)!} (2\pi)^{-\frac{1}{2}} (\frac{\pi^{2} - n^{2}}{n})^{n+\frac{1}{2}} (\pi+n)^{n}$$

a<asind:

$$Z_{n}^{\pi} \sim D_{n}^{\pi} N^{\frac{1}{2}} \sin \tilde{\varphi}_{n}^{\pi} \qquad (8)$$

where

$$\begin{aligned} x &= x_{n} = (n^{2} \sin^{2} f - n^{2})^{\frac{1}{2}} \\ y_{n}^{(1)} - x^{2} \frac{n!}{(n+n)!} \frac{n!}{(n+n)!} (\frac{1}{(n+1)!} - \frac{n!}{(n+1)!} (\frac{n!}{(n+1)!})^{n/2} \\ \tilde{e}_{n}^{(1)} &= (n+\frac{1}{2}) \frac{1}{p} - n \propto +\frac{1}{2} \pi \\ \tilde{e}_{n}^{(1)} &= (n+\frac{1}{2}) \frac{1}{p} - n \propto +\frac{1}{2} \pi \\ \tilde{e}_{n}^{(1)} &= arc \cos \left[n \cos f / (n^{2} - \pi^{2})^{\frac{1}{2}} \right], \quad 0 \leq p \leq \pi \\ \tilde{e}_{n}^{(1)} &= arc \cos \left[n \cot f / (n^{2} - \pi^{2})^{\frac{1}{2}} \right], \quad 0 \leq q \leq \pi \end{aligned}$$

Accelerate accelerate points of interest about these solutions that is can execute action further effort. First, the writer has previously observed that in the actional effect case (m=0) the torsionless membrane solutions, $\sum_{i=1}^{n}$ and $\sum_{i=1}^{n}$, are not necessarily accurate approximations to solutions of the complete (i.e., membrane plus bending) system when $\sum_{i=1}^{n}$. This defect of the membrane approximation was also shown to be symptomatic of the occurrence of a transition point (of infinite order) in the asymptotic approximations to the bending solutions when $\sum_{i=1}^{n}$. The singularity in (2) when $\sum_{i=1}^{n}$ is evidence that this diffisolution for k, (3), contains no such singularity, and we conclude that the rensional membrane solutions $\sum_{i=1}^{m}$ and $\sum_{i=1}^{m}$, are free of this defect at $\sum_{i=1}^{m}$.

Second the asymptotic formulas (7) and (8) for Z_n^m are valid when n and m are both large and are of course equally applicable to the function Z_X^m . These asymptotic representations suffer from a transition point at $\phi = \phi_t$, where

$$\sin \beta_{\rm f} = \pi/n$$

(9)

It is worth dwelling on the differences between this transition point and the one described above, where $\Omega = 1$.

The most obvious difference between the two kinds of transition points is this. The transition point for Ω =1 shows itself as a singularity in the relation (2) between n and Ω and does not involve m, whereas the present transition point is determined by the relation (9) between m and n and does not show itself as a singularity of any

..... It we compare the membrane system of equations with the conplace e_1 (i.e., for a sphere we see $\frac{5}{100}$ that (i) the membrane system has a stationary when 2=1 but the complete system does not, and (ii) neither cost - 1 of a singularity at points given by (9). We conclude that the - w truty in the performe equations for 2=1 implies that some of the conforme solutions are then poor approximations to complete solutions. The obsence of such a singularity at $p = p_{\rm p}$ means that the present transition point does not significantly affect the accuracy of the membrane solutions as approximations to complete solutions but merely affects the accuracy of the asymptotic formulas, (7) and (8), as approximations to the membrane solutions. Alternatively, we may say that, when 2=1, bending effects intrude into the membrane equations, or that there is serve schange of bending and stretching energies, but bending does not affect what happens at $p=p_1$. The shortcouings of the approximations (7) and (8) near ϕ_{t} can be overcome entirely within the scope of the merbrane theory, without considering bending effects.

Υ.,

3. D. M. vior of Membrane Solutions as 200.

We consider first the passage to the static limit, S=0. In this case $n \rightarrow 1$ and $k \rightarrow 1$ and

 $Z_{1}^{m} = \sin^{m} \not\in \bar{r} [\underline{m}+2, \ m-1; \ m+1; \ \frac{1}{2}(1-\cos \not)]$ = $[2^{m} / (1 + m)] (m + \cos \not) \tan^{m} \frac{1}{2} \not\land$ $Q_{1}^{m} = (-\sin \not)^{m} \ d^{m} Q_{1}^{o} (x) / dx^{m} , \ x = \cos \not$ $Q_{1}^{o} (x) = \frac{1}{2} x \ln (1 + x) / (1 - x) - 1$

Love⁹ gives the solutions \sum_{m}^{m} (j=1,2,3,4) to the statical membrane solutions, with the following displacements:

$$\begin{array}{l} x_{1}^{(0)} : x_{1}^{(0)} = \cos \beta & x_{1}^{(0)} : u_{2}^{(0)} = -\cos \beta + \sin \sin \beta + \sin \beta +$$

ó

Is at simply and χ_2^{m} are those corresponding to right bary of a control of an inextensional motions for mW2, and the solutions $\chi_1^{(m)}$ are those for which the stress resultants $n_{M}^{(m)}$, $n_{CO}^{(m)}$ and $n_{CO}^{(m)}$ is a control identically. The relations between $\chi_1^{(m)}$ and the limits associated of the vibrational solutions $\chi_1^{(m)}$ are found by comparing bemaviors of y=0 and $\beta = \frac{1}{2}T$. The results are

$$\begin{array}{c} \underbrace{S_{1}^{0} \times S_{2}^{0}}{}, & j=1,2,3,4 \\ -\underbrace{(S_{1}^{1} + S_{3}^{1}) \rightarrow X_{1}^{1}}{}, & \underbrace{S_{1}^{1} - S_{3}^{1} \rightarrow X_{2}^{1}}{} \\ -\underbrace{(S_{2}^{1} + S_{4}^{1}) \rightarrow X_{3}^{1}}{}, & \underbrace{S_{2}^{1} - S_{4}^{1} \rightarrow X_{4}^{1}}{} \end{array} \right\}$$
(10)

and for r > 2

$$\begin{array}{c} -(1+\pi) \ 2^{-\pi} \ (S_{1}^{-\pi} + S_{3}^{-\pi}) \rightarrow S_{1}^{-\pi} \\ B_{2} \ (S_{1}^{-\pi} - S_{3}^{-\pi}) \ + \frac{2(-1)^{m}}{(\pi-2)!} \ (C_{2}^{-\pi} - S_{3}^{-\pi}) \rightarrow S_{2}^{-\pi} \\ \frac{2^{-m+1}}{\pi(n-1)} \ (S_{1}^{-\pi} - S_{3}^{-\pi}) \rightarrow S_{3}^{-\pi} \\ B_{-} \ (S_{1}^{-\pi} + S_{3}^{-\pi}) \ + \frac{4(-1)^{m+1}}{(n+1)!} \ (S_{2}^{-\pi} + S_{4}^{-\pi}) \rightarrow S_{4}^{-\pi} \\ B_{2} \ = 2^{-\pi} (\pi^{-1} + 1) \left[\pi + \frac{(-2^{\pi}\pi)^{-\frac{1}{2}}}{(\pi-2)!} \ (S_{2}^{-\pi+1} + \frac{1}{2}) \right] \\ \mu_{4} \ = -2^{-\pi+1} \ \pi^{-1} \ \left[(m-1)^{-1} + \frac{(-2)^{\pi}\pi^{-\frac{3}{2}}}{(2-2\pi)!} \ (m-1)^{-1} + \frac{(-2)^{\pi}\pi^{-\frac{3}{2}}}{(2-2\pi)!} \ (13) \end{array} \right]$$

4. Numeral Precuencies for a Free-Edged Hemisphere

In this section we shall use the formulas of Section 3 to obtain easilyties of the membrane natural frequencies for a hemispherical

 $\frac{1}{2} = \frac{1}{2} \left[\frac{1}{2} + \frac{1}{2} \right]^2 = 0$ (12)

$$\sum_{n=1}^{m} = \frac{dZ_{n}^{-m}(\cos \beta)/d\beta}{Z_{n}^{-m}(\cos \beta)} | \frac{d\beta}{dT/2} , \qquad \sum_{k=1}^{m} = \frac{dZ_{k}^{-m}(\cos \beta)/d\beta}{Z_{k}^{-m}(\cos \beta)} | \frac{d\beta}{dT/2}$$

$$= 1 + (1 + \frac{1}{2}) \frac{dZ_{k}^{-2}}{dT/2}$$

II the representation (5) is used, the frequency condition can be writted

 $\sum_{n=0}^{\infty} P(-n, n+1; n+1; 1), \quad P_{dn} = P(-n+1, n+2; m+2, 1)$ (1) or $P_{1,n} = P_{1,n}$ are defined on roughly,

 ∞ (i) (i) and multiple basis of a trial-and-error culturation α done frequencies for m40. The results are accurate to three β α of the figures and are presented in Table 1 and Figure 1. For α on we also present the results given by Naghdi and Kalmins⁷.

One interesting result is very easily derived from (15). If $m_{2} = m_{1} = m_{2} = m_{1}$, all the hypergeometric functions in (15) are approximatchy unity, and (15) reduces approximately to

 $n(n+1) + k(n+1) - 4 \left[1 + (1+2)\Omega^2 \right] \rightarrow 0$

Contains, this with (2) and (3), we obtain $\Omega^{2} \left[1 + (1-2)\Omega^{2} \right] / (1-\Omega^{2}) = 0$

a relation which cannot be satisfied for real, non-zero values of \Im . We conclude that no membrane frequencies (i.e., no natural frequencies which notes of membrane type) can be found when $\pi \gamma \gamma \Omega$. Since this has been derived solely on the basis of the membrane solutions, we must observe that it does not preclude the occurrence of bending and incutencional frequencies, nor does it rule out the transitional freque dies near $\Omega_{n} = 1$.

It is also helpful to see what is obtained if we combine the approximate formulas (7) and (a) for both n and k with the frequency relation (14). The asymptotic formulas for $dZ_n^m/d/may$ be obtained on or definerationing the asymptotic relation for Z_n^m (which is the defined in this case though not in general), or by using the

relation

$$dr_n^m/dy = (n-m+1)\csc y P_{n+1}^m - (n+1)\cos y P_n^m$$

together with the asymptotic relation for Z_n^m . The frequency equation assumes different forms in three regions, as follows:

- 1-

(21)

(i) n>kyn	
$(m-1in^{-1})^2 - (M_n - \frac{1}{2}nM_n^{-1})(M_k - \frac{1}{2}iM_k^{-1}) = 0$	(17)
(ii) kymyn	
$(m-14n^{-1})^2 \tan_2^{-11}(k-m+1)$	
$-(N_{n} - \frac{1}{2}nN_{n}^{-1})(N_{k} - \frac{1}{2}kN_{k}^{-1}) = 0$	(18)
(iii) kynym	
(n-Hn ⁻¹) ² tan ¹ / ₂ TT(k-m+1) tan ¹ / ₂ TT (n-m+1)	
$\frac{1}{n} \left(N_{n} - \frac{1}{2}nN_{n}^{-1} \right) \left(N_{k} - \frac{1}{2}kN_{k}^{-1} \right) = 0$	(19)

Natural f^{μ} encies may be estimated easily in the various regions with the aid of these formulas. The results of these computations are compared with the calculations based on the accurate frequency equation (15) in Table I.

A further simplification is possible when $\mathfrak{R}^2 \gg \mathfrak{n}^2$ or

$$(k+\frac{1}{2})^2 > (n+\frac{1}{2})^2 > m^2$$
,

in which case (19) becomes

 $\tan_{2}^{1}\pi(k-m+1)$ $\tan_{2}^{1}\pi(n-m+1) = O(m^{2}\Omega^{-2})$

whence

 $k + \frac{1}{2} \approx 2J - n - \frac{1}{2}$ (20)

 $n + \frac{1}{2} \approx 2L - n - \frac{1}{2}$

where J and L are sufficiently large positive integers. When $\Omega^2 77$, we have from (2) and (3)

$$n + \frac{1}{2} \approx \Omega (1 - \nu^2)^{1/2}$$

 $k + \frac{1}{2} \approx \Omega [2(1 + \nu^2)]^{1/2}$

Combining these with (20) and (21) we find two families of natural frequencies, given by

$$\Omega \approx (2J + m - \frac{1}{2})(1 - y^2)^{-1/2}$$
 (22)

$$\Omega \simeq (2L + m - \frac{1}{2}) \left[2(1 + \nu) \right]^{-1/2}$$
(23)

The first of these families is associated with stretching (torsionless) membrane modes, the second with torsional modes. The frequency for each branch depends linearly on m with different slopes for the two families. These predictions are shown in Table I and Figure 1.

5. Discussion

We shall comment first on the behavior of the solutions $as \Omega \rightarrow 0$ and then on the natural frequency calculations.

The formulas (10)-(13) show clearly that in the limit as $\Omega \rightarrow 0$ the dynamic membrane solutions in the form of Legendre Functions are equivalent to the familiar static membrane and inextensional solutions. We find that, as $\Omega \rightarrow 0$, two linear combinations of the dynamic solutions tend toward the static, inextensional solutions and two other combinations tend to the static membrane solutions. These linear combinations are given in (10)-(13).

We shall now point out several of the pitfalls that one may encounter in trying to calculate the inextensional frequencies for a free-edged dome from the general solution. The general solution with

Ten - Antial wave number m is (for a dome) expressed in terms of wollded Legendre Functions in the form

$$w^{m} = C_{n} P_{n}^{m} (\cos \delta) + C_{k} P_{k}^{m} (\cos \delta) + C_{b_{2}} P_{b_{3}} (\cos \delta) + C_{b_{2}} P_{b_{3}} (\cos \delta)$$

where degrees of the Legendre Functions connected with the membrane solutions, and b_1 and b_2 are the degrees connected with the bending solutions. These solutions were given explicitly by Kalmins and Wilkinson¹.

Now the inextensional frequencies are very low, i.e.,

$$\Omega^2 = 0 (h^2 / R^2) << 1$$

where h is the thickness and R the radius of the shell. We have previously pointed out⁵ that, when Ω is this small, the bending solutions are nearly statical and are both of edge-effect type. Also, we see from (2) and (3) that

$n \approx k \approx 1$

It is an inconvenient property of the Associated Legendre Function that, e.g., $P_n^{m}(\cos \beta)$ vanishes identically when m is an integer and $m \geq n$. Since inextensional solutions occur only when $m \geq 2$, we see that $P_n^{m}(\cos \beta)$ and $P_k^{m}(\cos \beta)$ will be very small for the inextensional modes. This may make it hard to evaluate C_n and C_k numerically. This difficulty can be evaded by using the solutions Z_n^{m} , Z_k^{m} , which do not become small when a and k are near unity, i.e., we may write the general solution as

$$w^{i2} = C_{n}^{d} 2_{n} \frac{m}{n} (\cos \delta) + C_{k}^{d} 2_{k} \frac{m}{n} (\cos \delta) + C_{b_{1}} \frac{m}{b_{1}} (\cos \delta) + C_{b_{2}} \frac{m}{b_{2}} (\cos \delta)$$
(25)

//

however, we are not out of the modes yet, for it is only a very special linear combination of Z_n^m and Z_k^m that leads to an inextensional solution. If we rewrite (25) as

$$z^{m} = \frac{1}{2} (C_{n} + C_{k}) (Z_{n} + Z_{k}) + \frac{1}{2} (C_{n} - C_{k}) (Z_{n} - Z_{k}) + C_{b_{1}} (cos) + C_{b_{1}} (cos) + C_{b_{2}} (cos)$$

we see from (12) that the first solution becomes inextensional as $(2) \rightarrow (12)$, but the accordiootation is a membrane solution. In order to obtain a mode which is predominantly inextensional we must have

$$\frac{c_n^* - c_k^*}{c_n^* + c_k^*} \leq 1$$

It is plain that, if the constants are evaluated numerically with insufficient accuracy, so that C_n ' and C_k ' are not quite equal, we may be accidentally introducing a little bit of the membrane solution. Even a little trace of the membrane solution is enough to destroy the inextensional property of the solution and prevent one from obtaining inextensional frequencies. It is possible that this difficulty can be overcome by careful calculation. If not, it may be necessary to set $C_n'=C_k$ 'throughout the calculation, temporarily discarding one membrane boundary condition. After an inextensional frequency has been found, the discarded boundary condition can be used to calculate the difference $C_n'=C_k'$, which is initially taken as exactly zero.

The results for membrane natural frequencies of a free-edge hemisphere are given Table I and Figure 1. The gross features are these:

(i) when $\frac{2}{\pi}$, there are no membrane frequencies.

(i) When $\mathcal{L} > \pi^2$, the simple asympstotic estimates (22) and (23) are fairly reliable. These predict two families of frequencies which

depend linearly on m, the slopes of the two families being different. These predictions are less accurate near points where two frequency lines cross than elsewhere, and the errors in the asymptotic estimates change sign at such points.

(iii) If S_{n}^{2} and n^{2} are of comparable size, the picture is more complicated. When Ω and n are both large, the most important analytical features are the n- and k- transition lines, i.e., the locus of points for which n and k-are respectively. These are shown in Figure 1. Below the k-line the approximate frequency condition, (17), involves no oscillatory functions, and there is merely a single frequency for each n. Between the n-and k-transition lines the frequency condition,(18), contains an oscillatory function of k, indicating that there is one family of frequencies, namely those of torsional type. Above the n-line two families of frequencies are found, corresponding to the two oscillatory functions that occur in the frequency condition (19).

Interesting information is revealed by comparisons among the various approximations given in Table I. First, we see that the approximate frequency equations, (17)-(19), give generally good agreement with the more accurate frequency equation, (15). The accuracy is poorest, of course, near the n- and k- transition lines. The simple asymptotic estimates, (22) and (23), are not as accurate as (17) and (19) but are tolerably good when $g^2 \rightarrow \pi^2$. They are very poor near or below the n-transition line.

Lust, the calculations based on (15) do not show complete a scheme is the previous results of Naghdi and Kulnins⁷. For m=1 the a society, very good. For m=2 and 3 there is good agreement for some frequencies, but the present calculations do not show certain frequencies that were build earlier. Separate hand calculations were made for each of these questionable frequencies. In no case was a frequency found. Moreover, if we plot these doubtful frequencies on Figure 1, we see that they do not fit well with the pattern of the remaining frequencies. We conclude, therefore, that the frequencies marked with a question mark in Yorks 1 are sparious.

In closing we may remark that these membrane frequencies are all high compared with the inextensional frequencies. This does not necessarily mean that they are unimportant, however. Their importance in a problem of time-dependent loading depends on whether their mode makes a significant contribution to the response of the shell. This in turn depend on the kind of applied load and its spatial distribution. It is relevant that the modes⁵ associated with most of these frequencies involve much more motion in the shell surface than mormal to it. Therefore, if experiments on shell vibration are made in which only motion normal to the surface is measured, it will be very easy to miss these modes and conclude (erroneously) that they are unimportant.

... conces

z

35

J. P. Wilkinson and A. Kalnirs, "On Nor.symmetric Dynamic Problems of Elastic, Spherical Shells", J. App. Mech. <u>32</u>, 525-532 (1965)

-* C. Prasad, "On Vibrations of Spherical Shells", J. Acoust. Soc. Aml 30, 489-494 (1904)

E. W. ROSS, Jr., "Natural Frequencies and Mode Shapes for Axisymmetric Vibration of Deep, Spherical Shells", J. App. Nech. <u>32</u>, 553-561 (1905)

4. E. W. Ross, Jr., "Asymptotic Analysis of the Axisymmetric Vibrations of Shells", J. App. Mech. <u>33</u>, 85-92 (1966)

E. W. Ross, Jr., "Approximations in Nonsymmetric Shell Vibrations", To appear

⁰. Chintsun Hwang, "Some Experiments on the Vibration of a Hemispherical Shell", J. App. Mech. <u>33</u>, 817-824 (1966)

P. M. Naghdi and A. Kalnins, "On Vibrations of Elastic, Spherical Shells", J. App. Mech. 29, 63-72 (1962)

^{3.} H. Jeffreys and B. S. Jeffreys, "Methods of Mathematical Physics" (Cambridge at the University Press, 1950) 2nd Ed., p. 658.

9. A. E. H. Love, "A Treatise on the Mathematical Report of Elasticity", (Dover Publications, Inc., New York, 1944) 4th Ed., pp. 583-586.



-	

umanut takar tikili

* * * * * * * *

ł

·	ar and contactor of terms to be a contactor of the second s	
	concentration wave multipling and a more caped hand one	1 x
	according to many incory.	

در سرکاریس ک

1.

:

٠.

•

	Nurarico1 ^a	Asymptotic ^b	Sinple ^c Asymptotic	Re. 7 /
ŭ = 1	.876 .050 1.47 2.55 2.02 3.92 4.80 5.31 6.43 6.89	3.92 4.81 5.20 6.44 6.88	4.0. 4.72 5.27 t 6.51 6.51 6.31	.376 .950 1.47 3.56 2.92
m = 2	.916 1.21 2.31 3.18 3.84 4.60 5.66 5.99 7.06	3.26 3.83 4.57 5.69 5.97 7.06	3.41 ^t 3.67 ^s 4.65 ^t 5.77 ^s 5.89 ^t 7.13 ^t	.215 (?) .922 1.21 2.38 (?) 2.31
n = 3	.943 1.84 3.13 3.88 4.70 5.33 6.35 4.93	3.09 3,94 4.75 5.28 6.33 6.92	2.79 ^t 4.03 ^t 4.72 ^s 5.27 ^t 6.51 ^t 6.81 ^s	.740 (?) .943 1.20 (?) 1.83 2.07 (?)
m = 4	2.41 3.87 4.67 5.47 6.15 7.04	3.85 4.57 5.58 6.08 7.05	4.65 ^t 5.77 ^s • 5.89 ^t 7.13 ^t	

	Natorical ^a	Astupioteo	Simple Asymptotic ^C	$\frac{1}{1}$
r: = 5	3.44	2.81		
	4.5.	4.55	•	
	5.49		5.27	
	3.33	5.35	5.51 t	
	6.98	6.95	ó.31 ⁸	
0 = 0	5.54 5.19 6.27	3.41 5.19 6.23	t	
	5.99	7.09	7.13*	
n = 7	4.10	3.98		
	5.S2	2.01 2.01		
	7.01	· 0• 70		
r. = S	4.65	4.55		
	6.44	6.42		

â

E

based on Equation (15) based on Equations (17) - (19) based on Equations (22), (23) associated with torsional node ъ

С

t

associated with stretching node s

ļ

CT ALTONOMY OF A TONY OF TONY

14 1241

PC' ¥

> ×. 1111 i. r

۰.

î, ÷

•

÷

د در مدید در شد. در از در سه درسه رو در از در در از در از میشود. - از مراقع از



Distribution tens frequency, $\Delta = \cos(\varphi / E)^{\frac{1}{2}}$ versus differential wave number, m, for n tree equal learn phere according to membrane theory.

> . --

ĐỘLỆI	MENT CONTROL DATA · R&D		
(Security classification of title body of ubstrac	t and indexing annotation must be entered when the overall the period of the first		
U.S. Army Natick Laboratorie	Unclassified		
Natick, Massachusetts 01760	26 GHOUP		
S REPORT TITLE			
ON MEMBRANE FREQUENCIES FOR S	SPHERICAL SHELL VIBRATIONS		
DESCRIPTIVE NOTES (Type of report and inclusiv Technical Report	e datez)		
5 AUTHOR(5) (Last name, first name, initial)			
Ross, Edward W., Jr.			
REPORT DATE	7. TOTAL NO OF PAGES 76 NO OF REFS		
May 1967	14 9		
I. CONTRACT OR GRANT NO.	90. ORIGINATOR'S REPORT NUMBER(S)		
& PROJECT NO.	67-74-OSD		
с.	95. OTHER REPORT NO(S) (Any other numbers that may be assist		
	une report)		
1 SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY U. S. Army Natick Laboratories		
	U. S. Army Natick Laboratories		
	U. S. Army Natick Laboratories Natick, Massachusetts		
13. ABSTRACT	U. S. Army Natick Laboratories Natick, Massachusetts		
ABSTRACT In this paper the membra spherical dome are studied. and it is shown how these rea solutions in the static limit several difficulties in find: and to suggest ways around th found for circumferential way and compared with several dif tion, due to Jeffreys and Jes earlier work agrees well with are not found at all in the p	U. S. Army Natick Laboratories Natick, Massachusetts ane solutions for non-symmetric vibration of a The solutions are written in a convenient form, duce to the familiar membrane and inextensional t. This information enables one to perceive ing inextensional frequencies by numerical means hese difficulties. Also membrane frequencies are ve numbers up through eight by direct calculation fferent approximations. One type of approxima- ffreys, gives quite good results. It is seen tha h these results except for a few frequencies whic present calculations.		

٠

.

T.

T

,-- -

ł

ł

,

Secondy classification

14

KEY WORDS		LINA		LINKD			
	HOLE	₩T	HOLL	M T	HOLL	43	
Analysis	8						
Continuum mechanics	8				• •		
Dynamics	8			1. A.	1	-2	
Membranes	9		i i				
Frequency	9						
Vibration	9		i i		1 1		
Elastic shells	9						
Spheres	9						
Legendre functions	10				([
Differential equations	10						
Asymptotic expansion	10				1		
Prediction	4						
Performance	4						
[ents	4			•			
Parachutes	4			•			
Parachutes	4 ICTIONS	-					

1. ORIGINATING ACTIVITY: Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (corporate author) issuing the report.

2a. REPORT SECURITY CLASSIFICATION: Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. GROUP: Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. REPORT TITLE: Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. DESCRIPTIVE NOTES: If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. AUTHOR(S): Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. REPORT DATE: Enter the date of the report as day, month, year; or month, year. If more than one date appears on the report, use date of publication.

7a. TOTAL NUMBER OF PAGES: The total page count should follow normal pagination procedures; i.e., enter the number of pages containing information.

7b. NUMBER OF REFERENCES: Enter the total number of references cited in the report.

8a. CONTRACT OR GRANT NUMBER: If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. PROJECT NUMBER: Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. ORIGINATOR'S REPORT NUMBER(S): Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

95. OTHER REPORT NUMBER(S): If the report has been assigned any other report numbers (either by the originator or by the sponsor), also enter this number(s).

10. AVAILABILITY/LIMITATION NOTICES. Enter any limitations on further dissemination of the report, other than those imposed by security classification, using standard statements such as: 「「「「「「「「「」」」」」

No. and No.

機構

No

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. SUPPLEMENTARY NOTES: Use for additional explanatory notes.

12. SPONSORING MILITARY ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring (paying for) the research and development. Include address.

13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shull end with an indication of the military security classification of the information in the paragraph, represented as (TS). (S). (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. KEY WORDS: Key words are technically neaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Menfiers, such as equipment model designation, trade name, whitary project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.

