TECHNICAL REPORT 231-14

ON THE SURFACE WAVE PATTERN OF SUBMERGED BODIES ARRESTED IMPULSIVELY FROM UNIFORM MOTION

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By

C. C. Hsu

November 1966

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## NOTATION

f	Depth of submergence measured from the centerline of the body
$F_{\lambda}$	Function of $\theta$ as defined
F	Froude number based on depth
g	Gravitational acceleration
G	Function of $\kappa$ , $\theta$ and $\tau$ as defined
L	Distance between source and sink
Гi	Strength of point source
M n	Function of t, source strength
M '	Function of t, source strength
Mı	Source strength
Ma	Sink strength
R <i>I</i> ,	Real part
R <sub>n</sub>	Radial distance of source or sink, M
<b>R</b> <sub>n</sub>	Image of R
R1	$\sqrt{x^2 + y^2}$
Ra	$\sqrt{(x+l)^2 + y^2}$

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S	Surface
S '	Arbitrary surface enclosing singularities
t	Time
to	Initial reference time
U	Uniform free-stream speed
x,y,z	Rectangular Cartesian coordinates
$\mathbf{x}_{n}, \mathbf{y}_{n}, \mathbf{z}_{n}$	Position of source or sink
δ <sub>c</sub>	Angle between line of motion and straightline radiating from the origin
91	$= \tan^{-1} (y/x)$
95	$= \tan^{-1} \frac{y}{x+l}$
ζ	Surface elevation
ζο	Disturbance due to original motion
ζ <sub>3.</sub>	Disturbance caused by the stopping action
۲ <sub>1</sub>	Initial unsteady surface disturbance
θ	Angle
$\boldsymbol{\theta}_{\lambda_1}$	$= -1/4 \left[ \cot \delta_{\lambda} - \sqrt{\cot^2 \delta_{\lambda} - 8} \right]$
θ. Λ <b>2</b>	$= -1/4 \left[ \cot b_{1} + \sqrt{\cot^2 b_{1} - 8} \right]$

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κ	Dummy variable
κ <sub>o</sub>	$= g/U^2$
Φ	Total velocity potential
Фо	Velocity potential due to the prescribed singularities
Φ <sub>O</sub>	Image of $\phi_0$
<b>~</b> ຍ	$= \mathbf{x} \cos \theta + \mathbf{y} \sin \theta  \cdot$
$\widetilde{\omega}_{1}$	= $[x + U(t-\tau)] \cos \theta + y \sin \theta$
ີ ພ <sub>2</sub>	$= [x + l + U(t-\tau)] \cos \theta + y \sin \theta$
ũ	= $(x-x_n) \cos \theta + (y-y_n) \sin \theta$

#### ABSTRA CT

In this report a theoretical study on the surface wave pattern of submerged bodies arrested impulsively from uniform motion has been carried out. Seen from above, the waves appear to pass through the suddenly stopped body, fading away in the foremost portion of the pattern. The extent of this disappearing wave front in advance of the stopped body is approximately equal to 1/2 Ut, where U is the constant speed which the body originally possessed, and t the time elapsed since the sudden alteration in motion took place. If the transient effect is negligible, i.e., for a sufficiently long time t, except for the disappearing wave front, the group of steady regular waves, produced by the initially moving submerged body, advances into still water within a V-shaped region as if no changes had taken place (see Figure 2). The front portion of this wave pattern becomes blunter as the elapsing time increases, due to the disappearing wave front. The location of the motionless body may be determined from the wave pattern by simple arithmetic calculations.

#### INTRODUCTION

When a small obstacle is moved forward through still water, the surface is covered with a wave pattern fixed relative to the obstacle. On the upstream side the wavelength is short and the force governing the disturbance is principally surface tension. On the downstream side the waves are longer and are governed principally by gravity. If at some instant a sudden alteration in the motion takes place, very interesting questions

arise as to what form the surface disturbance will take in response to such abrupt changes. In this report the surface wave pattern of a submerged body arrested impulsively from uniform motion is studied. The analysis is based on the usual assumptions that the fluid is ideal and very large in extent and the disturbance is infinitesimal. It has been found possible to make calculations in this case, and the results illustrate various points of interest.

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#### GENERAL FORMULATION

It is well known that the fluid motion caused by a submerged obstacle may be taken to be that due to an appropriate distribution of singularities over or inside its surface. The total velocity potential for a submerged body moving through an ideal fluid of very large extent in irrotational motion may be expressed as

 $\Phi = \Phi_{0} - \overline{\Phi}_{0} + \frac{1}{\pi} \int d\tau \int d\theta \int G(\kappa, \theta, \tau) e^{\kappa (z - i\widetilde{\omega})} \sin \left( \sqrt{g\kappa} (t - \tau) \right) \sqrt{g\kappa} d\kappa$ [1]

where

g is the gravitational acceleration,

is the velocity potential due to the prescribed
 singularities and depends mainly on body shape,

 $\bar{\Phi}_{a}$  is the image of  $\Phi_{a}$ 

$$G(\kappa,\theta,\tau) = -\frac{1}{4\pi} \int \left( \frac{\partial \Phi_0}{\partial n} - \Phi_0 \frac{\partial}{\partial n} \right) e^{\kappa (z + i\omega)} dS$$

- S' is an arbitrary surface enclosing the singularities
- x,y,z are the right-handed Cartesian coordinates and the origin is taken on the mean free surface with Oz vertically upwards, and

 $\widetilde{\omega} = \mathbf{x} \cos \theta + \mathbf{y} \sin \theta.$ 

The velocity potential  $\phi_0$  due to an impulsive point source or sink at  $(x_n, y_n, z_n)$  started instantaneously at time t<sub>0</sub> with a given velocity U and maintaining that speed is given by

$$o = \frac{M_n}{R_n}$$
 [2]

where

 $M_{n}(t) = \begin{cases} 0 & t \leq t_{o} \\ M_{n} = \text{ constant} & t > 0 \end{cases}$  $R_{t} = \sqrt{(x-x_{n})^{2} + (y-y_{n})^{2} + (z-z_{n})^{2}}$ 

to is the initial reference time.

The function G in this case is simply

 $c = M_n e^{\frac{x(x_n + i(x_n \cos \theta + y_n \sin \theta))}{n}}$ 

[4]

[3]

The total velocity potential due to an impulsive point source or sink can then be shown to be

$$\Phi = \frac{M_n}{R_n} - \frac{M_n}{\tilde{R_n}} + \frac{1}{\pi} \int M_n(\tau) d\tau \int d\theta \int e^{\infty} \kappa (z+z_n) \cos \kappa \tilde{\omega}_n \sin \left(\sqrt{g\kappa} (t-\tau)\right) \sqrt{g\kappa} d\kappa$$

$$-\pi o$$
[5]

where

$$\overline{R}_{n} = \sqrt{(x-x_{n})^{2} + (y-y_{n})^{2} + (z+z_{n})^{2}}$$
$$\widetilde{\omega}_{n} = (x-x_{n}) \cos \theta + (y-y_{n}) \sin \theta$$

Following the linearized dynamical condition at the free surface, the mean surface elevation may be expressed as

$$\zeta \approx \frac{1}{g} \frac{\partial \phi}{\partial t} \bigg|_{z=0}$$

$$=\frac{1}{g}\frac{\partial}{\partial t}(\phi_{0}-\bar{\phi}_{0})+\frac{1}{\pi}\int d\tau \int d\theta \int \kappa O(k,\theta,\tau)e \cos\left\{\sqrt{g\kappa}(t-\tau)\right\} d\kappa \Big|_{-\pi}$$

[6]

or

$$\zeta = R I \left\{ \frac{1}{\pi} \int_{-\pi}^{t} M_{n} d\tau \int_{-\pi}^{\pi} d\theta \int_{-\pi}^{\infty} \kappa \left( z_{n} + i\omega \right) \cos \left\{ \sqrt{g\kappa} \left( t - \tau \right) \right\} d\kappa \right\}$$
  
at z=0 [7]

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for motions due to a constant impulsive point source or sink with

 $\widetilde{\omega} = [(\mathbf{x} - \mathbf{x}_n) + \mathbf{U}(\mathbf{t} - \tau)] \cos \theta + (\mathbf{y} - \mathbf{y}_n) \sin \theta$ 

Rl denotes the real part.

Imagine now the fluid motion to have been generated instantaneously at time t by a constant impulsive point source or sink and to be arrested instantaneously at a later time  $t_1$ . The impulsive point source or sink in this case may be described as

$$M_{n}(t) = \begin{cases} 0 & t \leq t_{0} \\ M_{n} = \text{constant} & t_{0} < t < t_{1} \\ 0 & t \geq t_{1} \end{cases}$$
[8]

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Since the problem in the present study is assumed to be linear, condition [8] may be rewritten as the sum of

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$$M_{n}(t) = \begin{cases} 0 & t \leq t_{o} \\ M_{n} = constant & t > t_{o} \end{cases}$$
[9]

and

$$M_{n}'(t) = \begin{cases} 0 & t \leq t_{1} \\ & & \\ -M_{n} = \text{constant} & t > t_{1} \end{cases}$$
[10]

The corresponding mean free-surface elevations can be expressed as

$$\zeta = R\ell \left\{ \frac{1}{\pi} \int_{0}^{t} M_{n} d\tau \int_{0}^{\pi} d\theta \int_{0}^{\infty} \kappa \left(z + i\tilde{\omega}\right) \cos\left(\sqrt{g\kappa}(t - \tau)\right) d\kappa \right\}$$
$$+ \frac{1}{\pi} \int_{0}^{t} M_{n}' d\tau \int_{0}^{\pi} d\theta \int_{0}^{\infty} \kappa \left(z_{n} + i\tilde{\omega}\right) \cos\left(\sqrt{g\kappa}(t - \tau)\right) d\kappa \right\}$$
$$= \zeta_{0} + \zeta_{1}$$

[11]

where

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 $\zeta_0$  is the disturbances due to the original motion

 $\zeta_1$  represents the disturbances caused by the stopping action.

Expression [11] is quite general and can be readily extended to wave motion caused by submerged bodies.

Consider the special case of a Rankine ovoid submerged in water at a given depth f (Figure 1), suddenly started from rest with a given velocity U at time t and maintaining that speed until t<sub>1</sub> at which the body is instantaneously brought to rest. For a first approximation the fluid motion resulting from the starting (or stopping) action may be taken to be that due to a point source (or sink) and a point sink (or source) of constant strength M distribution at the point (0,0,-f) and (0,l,f), respectively. The mean surface elevations in this case may be shown to be

$$\zeta = \zeta_0 + \zeta_1 \qquad [12]$$

where

$$\zeta_{o} = R \mathcal{L} \left\{ \frac{1}{\pi} \int_{0}^{t} M d\tau \int_{0}^{\pi} d\theta \int_{0}^{\infty} \kappa e^{-\kappa f} \left( \frac{i \kappa \widetilde{\omega}_{1} i \kappa \widetilde{\omega}_{2}}{e^{-e}} \right) \cos \left\{ \sqrt{g \kappa} (t - \tau) \right\} d\kappa \right\}$$
[13]

$$\zeta_{1} = -R\ell \left\{ \frac{1}{\pi} \int_{t_{1}}^{t} Md\tau \int_{d\theta}^{\pi} \int_{\kappa}^{\infty} e^{-\kappa f \left( i\kappa \widetilde{\omega}_{1} - i\kappa \widetilde{\omega}_{2} \right)} \cos \left\{ \sqrt{g\kappa} (t-\tau) \right\} d\kappa \right\}$$
[14]

respectively, with

 $\widetilde{\omega}_{1} = [x + U(t - \tau)] \cos \theta + y \sin \theta$  $\widetilde{\omega}_{2} = [x + l + U(t - \tau)] \cos \theta + y \sin \theta$ 

#### **RESULTS AND DISCUSSIONS**

In this section the surface wave pattern of a Rankine body arrested impulsively from uniform motion is to be discussed in some detail. The time  $t_0$  and  $t_1$  in the previous formulation are taken in this case as negative infinity and zero, respectively. The part  $\zeta_0$  in Equation [12] then represents the steady-state surface waves which travel, in a group, only downstream of the body and is contained within the straightlines radiating from the origin, each making with the line of motion an angle,  $\delta_c$ , approximately 19<sup>0</sup>28'. Far downstream  $\zeta_0$  may be expressed simply as

$$\zeta_{0} = 4\kappa_{0} \sum_{\lambda=1}^{2} \frac{M_{\lambda}}{U} \sec^{3}\theta_{\lambda_{1}} \exp(-\kappa_{0}f \sec^{2}\theta_{\lambda_{1}}) \sqrt{\frac{2\pi}{\kappa_{0}R_{\lambda}|F_{\lambda}''(\theta_{\lambda_{1}})|}} \cos(\kappa_{0}R_{\lambda}F_{\lambda}(\theta_{\lambda_{1}}) + \frac{\pi}{4})$$

+ 
$$4\kappa_{0}\sum_{\lambda=1}^{2}\frac{M_{\lambda}}{U}\sec^{3}\theta_{\lambda_{2}}\exp(-\kappa_{0}f\sec^{2}\theta_{\lambda_{2}})\sqrt{\frac{2\pi}{\kappa_{0}R_{\lambda}|F_{\lambda}''(\theta_{\lambda_{2}})|}}\cos(\kappa_{0}R_{\lambda}F_{\lambda}(\theta_{\lambda_{2}})-\frac{\pi}{4})$$

[15]

where

1

 $\kappa_{0} = \frac{g}{y^{2}} \qquad M_{2} = -M_{1} = -M$   $R_{1} = \sqrt{x^{2} + y^{2}} \qquad R_{2} = \sqrt{(x + \ell)^{2} + y^{2}}$   $\delta_{1} = \tan^{-1} \left(\frac{y}{x}\right) \qquad \delta_{2} = \tan^{-1} \frac{y}{x + \ell}$   $F_{\lambda}(\theta) = \sec^{2}\theta \, \cos(\theta - \delta_{\lambda})$   $\theta_{\lambda_{1}} = -\frac{1}{4} \left[ \cot \delta_{\lambda} - \sqrt{\cot^{2}\delta_{\lambda} - \delta} \right]$   $\theta_{\lambda_{2}} = -\frac{1}{4} \left[ \cot \delta_{\lambda} + \sqrt{\cot^{2}\delta_{\lambda} - \delta} \right]$ 

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The part  $\zeta_1$  represents the surface disturbances due to the impulsive stopping action which may be expressed in terms of an impulsive sink and source as

$$\zeta_{1} = -R l \left\{ \frac{1}{\pi} \int_{0}^{t} M d\tau \int_{0}^{\pi} d\theta \int_{0}^{\infty} \kappa e^{-\kappa f \left( i\kappa \widetilde{\omega}_{1} - i\kappa \widetilde{\omega}_{2} \right) \cos \left( \sqrt{g\kappa} (t - \tau) \right) d\kappa} \right\}$$

$$(16)$$

It has been shown in Reference 1 that the resulting disturbance due to an impulsive source or sink may be separated into three parts:

(i) A steady local disturbance which travels both upstream and downstream and diminishes as the distance from the body increases.

(ii) A group of steady regular waves which travel downstream from the origin only as far as x = 1/2 Ut with group velocity 1/2 U.

(111) A time-dependent circular disturbance  $(\zeta_1)$  which travels both upstream and downstream and diminishes rapidly as time increases.

Since the steady disturbances expressed in Equation [16] cancel the corresponding part of  $\zeta_0$ , the resulting surface elevation  $\zeta$ may be shown to be

$$\zeta = \begin{cases} \zeta_{1}(t) & x > 0 \text{ and} \\ R \leq \frac{1}{2} \text{Ut } \cos \delta, x < 0 \\ \text{for} & [17] \\ \zeta_{0} + \zeta_{1}(t) & R > \frac{1}{2} \text{Ut } \cos \delta, x < 0 \end{cases}$$

If the time t is sufficiently long Equation [17] is approximately

$$\zeta \approx \begin{cases} 0 & x > 0 \text{ and} \\ R \leq \frac{1}{2} \text{Ut } \cos \delta, x < 0 \\ \text{for} & [18] \\ \zeta_0 & R > \frac{1}{2} \text{Ut } \cos \delta, x < 0 \end{cases}$$

The resulting surface wave pattern is shown in Figure 2. It seems that, except for the fading wave front, the group of steady waves developed by the original motion of the body will advance into still water unblemished. The extent of the disappearing wave front is, of course, dependent upon the values of U and t. The propagating wave front is seen to become blunter as t increases. It is also interesting to note that the position of the arrested body can easily be located by simple geometric or arithmetic manipulations.

Although the foregoing discussions are based on the surface wave motion due to the action of simple Rankine bodies, similar results are expected to prevail for wave motion due to arbitrary bodies, except at very low speeds in which case the effect of capillarity may become important.

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#### REFERENCE

 Hsu, C. C., "On the Surface Pattern of Submerged Bodies Started From Rest," HYDRONAUTICS, Incorporated Technical Report 231-7, April 1965.

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## FIGURE 1 - DEFINITION SKETCH

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