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ACQUISITION COORDINATE COMPUTATION
FOR TRACKING AND SURVEILLANCE SENSORS
PROGRAM DOCUMENT

TECHNICAL DOCUMENTARY REPORT NO. ESD-TDR- 65-160

December 1964

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R. G. Schinnerer
D. R. Thompson

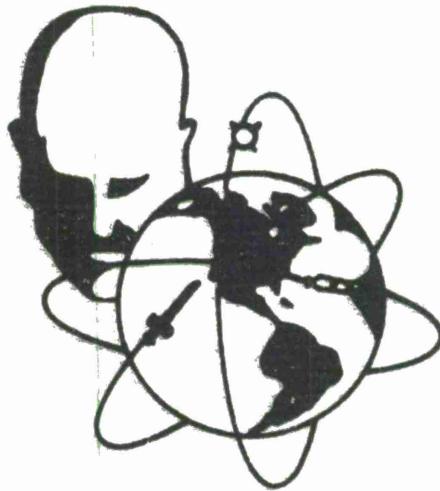
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Prepared under Contract No. AF 19(628)- 3438 by Aeronutronic,
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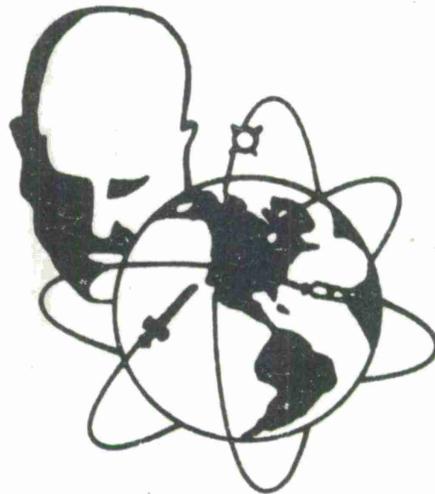
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FOREWORD

Aeronutronic Publication Report No. U-3011

ACQUISITION COORDINATE COMPUTATION
FOR TRACKING AND SURVEILLANCE SENSORS
PROGRAM DOCUMENT

ABSTRACT

A computer program has been developed to calculate acquisition coordinates of earth satellites for three types of sensors: planar fan, horizontal fan and tracker. The program is equipped to consider the special requirements of phased array trackers, such as the AN/FPS-85. Included in the document are the program description, formulation, operating instructions, flow diagrams, and test cases.

Publication of this technical documentary report does not constitute Air Force approval of its findings or conclusions. It is published only for the exchange and stimulation of ideas.

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SECTION 1

INTRODUCTION

The Observing Schedule Program (OBSERV) is programmed for the Philco 2000 computer and is to be part of the B-3 Semi-Automatic Program System (SPS) at the SPADATS Center in Colorado Springs, Colorado. It functions in conjunction with the Executive Program and receives its input from the Schedule, SEAI and FAN input tapes.

OBSERV has been developed to compute sets of acquisition coordinates for stations with fixed beam surveillance devices and sensors that can track satellites. The capability to handle phased array trackers of the AN/FPS-85 type has also been included. For surveillance devices, the program computes the time and coordinates of beam penetration by all satellites requested on the input tape. For tracking devices, the program calculates acquisition coordinates at evenly spaced intervals of time, as specified by the input, during the periods that a satellite is within the tracker coverage.

The primary mode of operation for one specified sensor is the computation of acquisition coordinates of specified satellites in the current satellite population. The results are then presented for each station in chronological order. Data listed for each time point include the identification and the acquisition coordinates of the satellite currently being observed. Satellite positions are computed using the simplified general perturbations technique used in other SPS programs (Hilton, 1963). Flexibility in the program is provided by various input and output control options. The program has been designed for maximum computational efficiency. This will result in a significant reduction in the computer time required for each case.

In addition to the features mentioned above, the program may also be used to simulate sensor-satellite patterns.

SECTION 2

PROGRAM DESCRIPTION

The program OBSERV is designed to calculate acquisition coordinates for sensors of three primary types: planar fan, horizontal fan and tracker. The overall program functions are shown schematically in Figure 1 and are described in the following subsections.

2.1 INITIALIZATION

The initialization consists of two basic parts: (1) initialization for each sensor and (2) initialization for each satellite being processed for the given sensor.

a. Initialization by Sensor

In this section the time limits for acquisition coordinate computation are established, the topocentric coordinate system for this station is computed from the azimuth and elevation angle of the boresight vector (if required), and the sidereal time at the station is computed at the "beginning reference time."

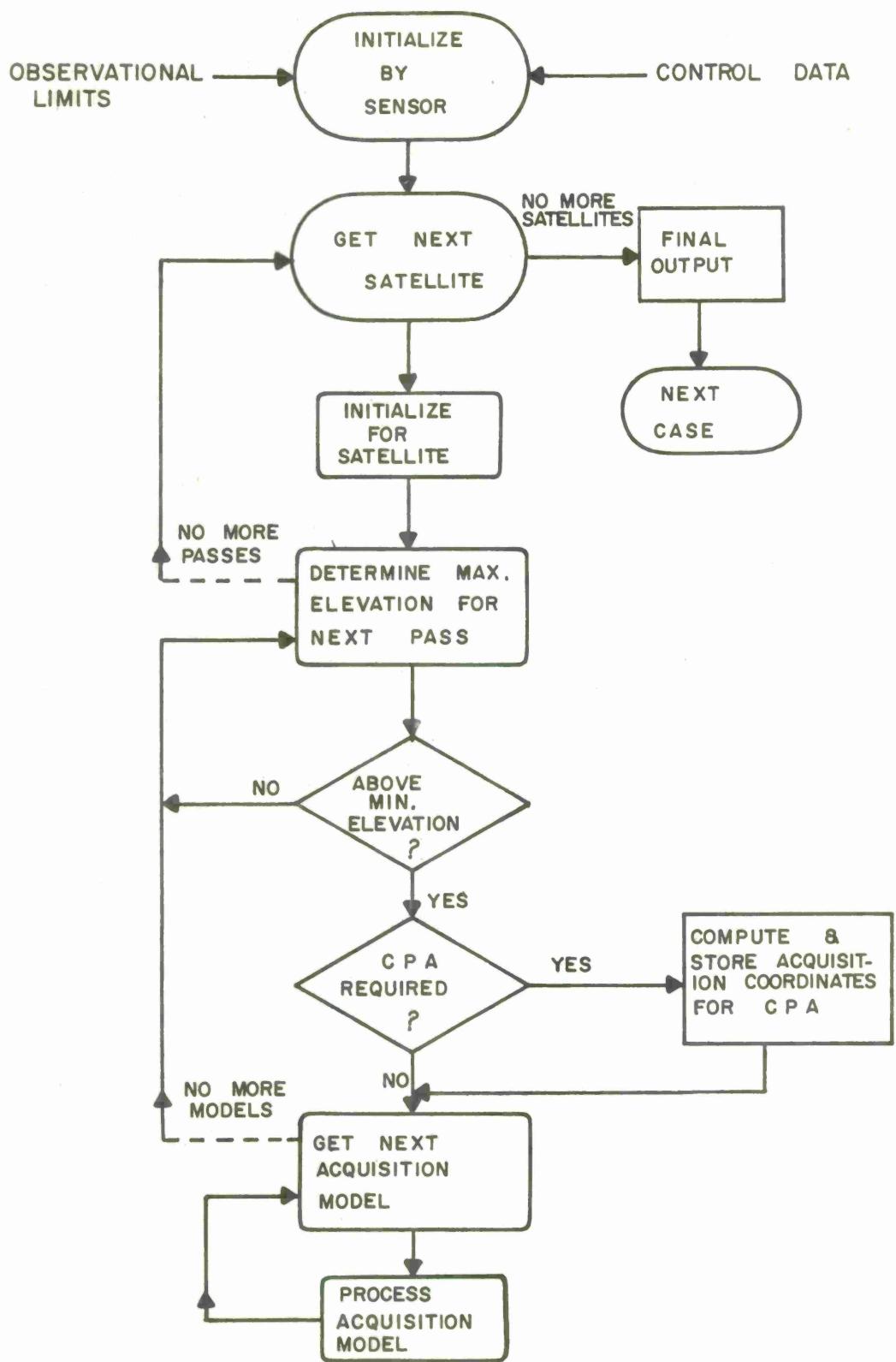


FIGURE 1 OBSERV PROGRAM FUNCTIONS

The time limits and the azimuth and elevation angles of the boresight vector are obtained from the input control card.

b. Initialization by Satellite

The orbital elements for each satellite are obtained from the system subroutine NXTELM. Using these, the calculations shown in Section 3.2 are performed. The minimum elevation angle, h_{min} , is obtained from either the fan card or the tracker card depending on the radar type being processed.

2.2 PRELIMINARY ACQUISITION COMPUTATIONS

This section is entered once for each revolution of the satellite falling within the requested time limits. The formulation given in Section 3.3 is used to obtain the time at which the satellite is at a maximum elevation angle with respect to the sensor. If the point of maximum elevation is below the horizon of the sensor, the calculations are performed again for the next revolution, unless the upper time limit has been passed. If the point of maximum elevation is above the sensor's horizon, a return is made to the main program to test the point against the minimum observable elevation angle. If it is above, the calculation continues to obtain the acquisition points required; if not, a return is made to the beginning of the subroutine to try again on the next revolution.

If acquisition coordinates for the closest point of approach (CPA) are requested, they are computed at the time of maximum elevation.

2.3 ACQUISITION MODELS

The term "Acquisition Model" denotes a mathematical scheme which describes the manner in which a sensor effects satellite acquisition. Four such acquisition models are contained in this program (see Figure 2). They are: (1) the subroutine PACQUI, designed for planar fan radars; (2) the subroutine HACQUI, used for horizontal fan radars; (3) the subroutine TACQUI, a generalized tracker acquisition model; and (4) the subroutine TACQUII, a specialized subroutine used by TACQUI to obtain acquisition times for phased array trackers. Each acquisition model is successively processed for one pass before the next pass is considered.

Each case may contain as many as thirty acquisition models for one station; however, only one tracker model may be used. The acquisition types need not be ordered.

a. Subroutine PACQUI

This subroutine uses iteration by halving to calculate the topocentric coordinates of the satellite at the time of fan penetration. It then checks to ensure that the satellite is within the observational limits of the fan. If it is, the acquisition coordinates are stored for output.

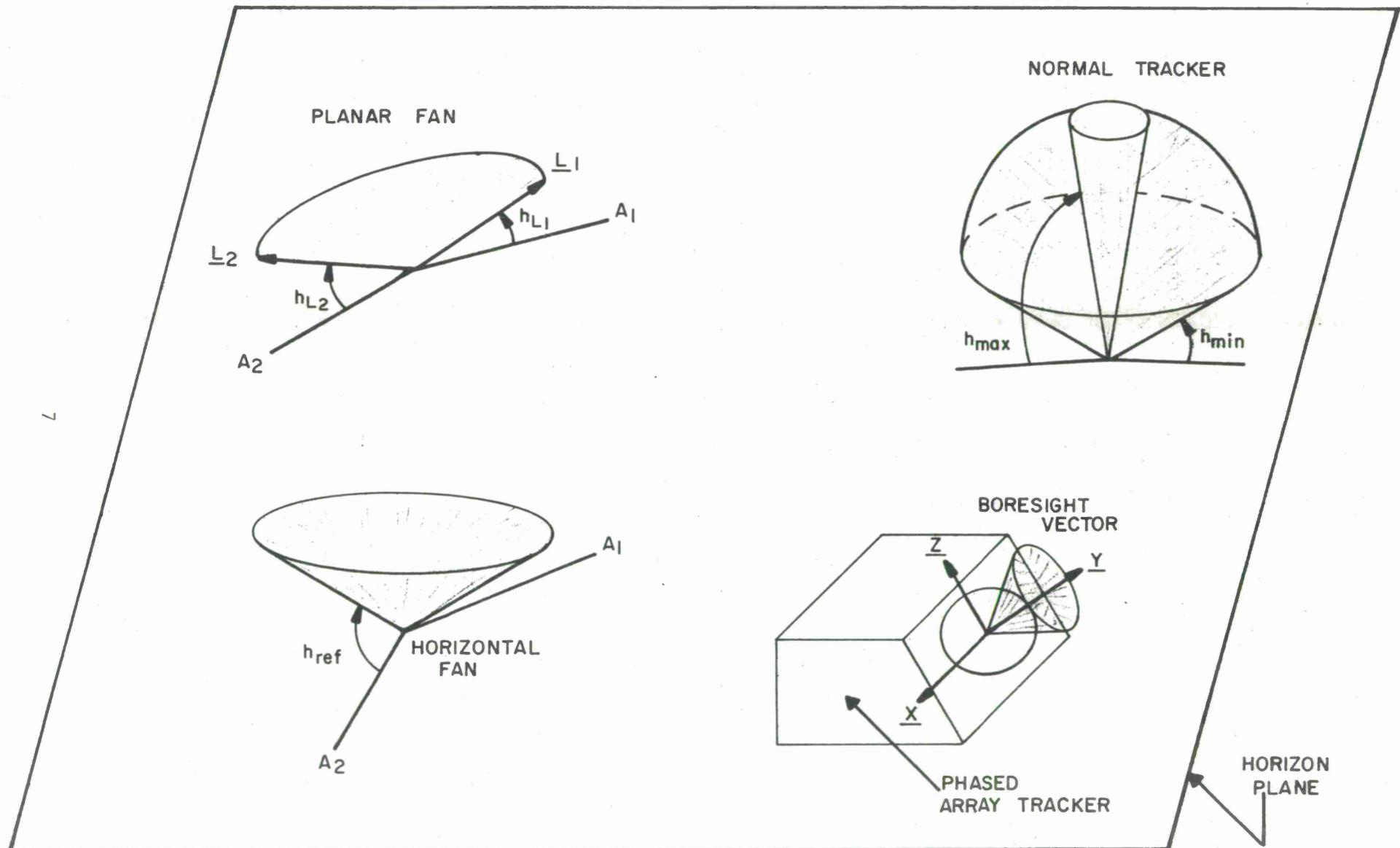


FIGURE 2 RADAR COVERAGE ASSUMED BY THIS PROGRAM

b. Subroutine HACQUI

The horizontal fan acquisition model calculates the points at which the satellite penetrates a cone which forms a constant angle with the horizon. If the points are within the azimuthal and range limits of the fan, they are stored for output. The maximum observable range is assumed to vary linearly between the angular limits of the fan.

c. Subroutine TACQUI

This subroutine makes use of either HACQUI or TACQUII (as required) to obtain the time span during which the satellite is observable by the tracker. It then computes the acquisition coordinates specified by the input tracker card: either a specified number of points per pass (ranging from two to eight), or a specified time interval between points.

Tracking limits for a normal tracker are determined by a vertical cone whose side forms an angle with the horizon equal to the minimum elevation angle. If the elevation angle of any point for a normal tracker is greater than the maximum, the point is rejected. No azimuth limits are assumed.

The tracking limits of a phased array tracker are determined by the minimum elevation angle, the limiting values of the direction cosines relative to the reference vectors normal to the boresight, and the maximum off-boresight angle.

d. Subroutine TACQUI1

This subroutine is used by subroutine TACQUI for phased array trackers. It uses iteration by halving to determine the acquisition coordinates and the times when the satellite enters and exits the coverage limits of the radar. Acceptable entry and exit points are stored for output.

2.4 FINAL OUTPUT

After every requested satellite has been processed through the acquisition models for one station, the accepted acquisition points are sorted either by time or by order of satellite appearance and output as shown in Figure 10.

The available output options are:

- (1) The fan number may be output.
- (2) The units of range and range-rate may be obtained in either nautical or MKS units.
- (3) The direction cosines with respect to the topocentric reference system may be obtained.
- (4) The point of maximum elevation may be computed as an acquisition point.
- (5) The output points may be restricted to the ascending half of each pass.

SECTION 3

FORMULATION

The acquisition coordinate computation program employs a simplified General Perturbations theory to calculate positions and velocities of the satellite. The formulation for this theory is given in the reference: Hilton, 1963. The remaining program formulation is detailed in the following subsections.

3.1 INITIALIZATION FOR EACH SENSOR

The following calculations are performed once for each station requiring acquisition coordinates:

- (1) Compute the topocentric reference triad from the boresight azimuth and elevation:

$$\underline{x} = \begin{cases} x_{xh} &= \sin A_B \\ x_{yh} &= \cos A_B \\ x_{zh} &= 0 \end{cases} \quad (1)$$

$$Y \left\{ \begin{array}{l} y_{xh} = -\cos h_B \cos A_B \\ y_{yh} = \cos h_B \sin A_B \\ y_{zh} = \sin h_B \end{array} \right. \quad (2)$$

$$Z \left\{ \begin{array}{l} z_{xh} = \sin h_B \cos A_B \\ z_{yh} = -\sin h_B \sin A_B \\ z_{zh} = \cos h_B \end{array} \right. \quad (3)$$

- (2) Compute the sidereal time at the station at the "beginning reference time"

$$\theta_i = (\dot{\theta} - 360) D + \dot{\theta} F + \theta_{gr_0} + \lambda_E \quad (4)$$

where D and F are, respectively, the days and fraction of a day of the "beginning time" into the reference year; θ_{gr_0} is the Greenwich sidereal time at the start of the year, λ_E is the east longitude of the observing station and $\dot{\theta}$ is the rotation rate of the earth.

3.2 INITIALIZATION FOR EACH SATELLITE

The following calculations are performed once for each satellite.

- (1) Enter the XYZI subroutine to compute the time independent initial parameters required for the ephemeris subroutine, XYZSB.

- (2) Calculate the epoch Greenwich sidereal time, θ_o :

$$\theta_o = \theta_i + \dot{\theta} (t_o - t_B) \quad (5)$$

where θ_i is from equation (4) and $(t_o - t_B)$ is the difference between the epoch time, t_o , and the input "beginning time" t_B .

- (3) Compute $\sin \dot{\theta}$ and $\cos \dot{\theta}$:

$$\sin \dot{\theta} = \sin \left\{ (\dot{\Omega} - \dot{\theta}) \Delta t_1 \right\} \quad (6)$$

$$\cos \dot{\theta} = \cos \left\{ (\dot{\Omega} - \dot{\theta}) \Delta t_1 \right\} \quad (7)$$

$$\text{where } \dot{\Omega} = -\frac{3}{2} J_2 \frac{a^2 e}{p^2} n \cos i \quad (8)$$

$\dot{\Omega}$ is the rotation rate of the earth and
 Δt_1 is 5 minutes

- (4) Compute K_1 , the critical value for $Z \cdot W$, above which visibility of this satellite is not possible for this station (see Figure 3).

$$K_1 = q_2^{-1} \cos h_{\min} \left\{ (q_2^2 - \cos^2 h_{\min})^{1/2} - \sin h_{\min} \right\} \quad (9)$$

where q_2 , the geocentric apogee distance, is given by:

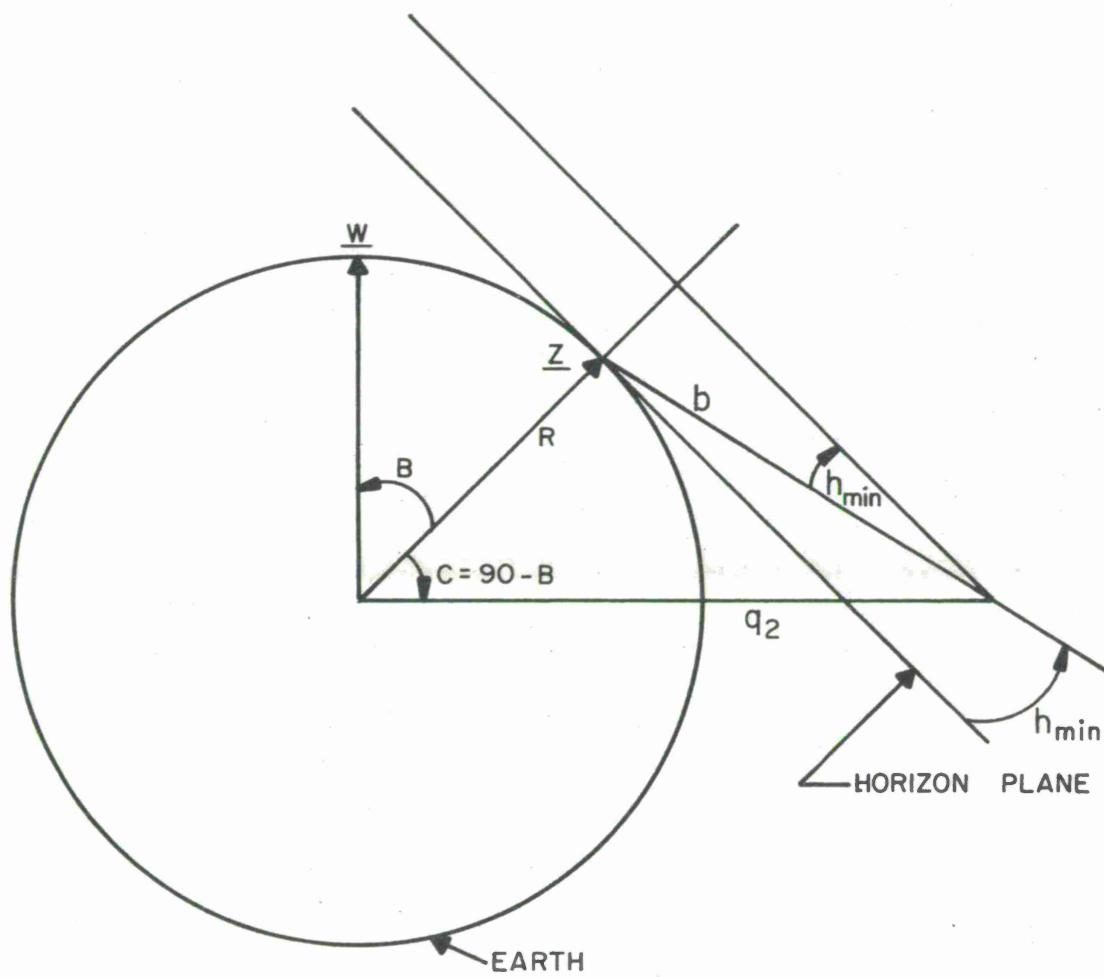
$$q_2 = a(1 + e) \quad (10)$$

- (5) Compute the revolution number at the "beginning time":

$$N_B = N_o + I \left\{ \frac{n}{2\pi} (t_B - t_o) \right\} \quad (11)$$

where N is the epoch revolution number and I represents the integral part of the bracketed quantity

- (6) The quantity t_L , used in later calculations, is set equal to zero at this point.
 (7) The quantity ϵ , also used in later calculations, is set equal to 1/2 of the beamwidth of the sensor.



$$\underline{Z} \cdot \underline{W} = \sin C$$

$$q_2 \sin C = b \cos h_{\min}$$

$$q_2 \cos C = R + b \sin h_{\min}$$

ELIMINATING b TO SOLVE FOR $\sin C$ FROM THESE TWO EQUATIONS GIVES THE CRITICAL VALUE OF $\underline{Z} \cdot \underline{W}$ GIVEN BY EQUATION(9). THE ASSUMPTION IS MADE THAT THE EARTH IS SPHERICAL AND THEREFORE THAT $R = 1$.

\underline{Z} IS A UNIT VECTOR DIRECTED TOWARD THE OBSERVERS ZENITH

\underline{W} IS A UNIT VECTOR IN THE DIRECTION OF ORBITAL ANGULAR MOMENTUM

FIGURE 3 DERIVATION OF CRITICAL VALUE FOR $\underline{Z} \cdot \underline{W}$

3.3 COMPUTATION OF t AND $L_{zh_{max}}$ FOR EACH PASS

This calculation is used to determine the point of maximum elevation angle of the satellite with respect to the sensor.

- (1) Set t_i equal to t_L and initialize for $\underline{Z} \cdot \underline{W}$ computation as follows:

$$\dot{\theta}_t = \dot{\theta}_o + \dot{\theta}(t_i + t_B - t_o) \quad (12)$$

$$\dot{\Omega} = \dot{\Omega}_o + \dot{\Omega}(t_i + t_B - t_o) \quad (13)$$

Compute the sine and cosine of $\Omega - \theta_t$

- (2) Iterate on $\underline{Z} \cdot \underline{W}$ as follows: if $t_i + t_B > t_F$ return to main program; otherwise,

$$t_{i+1} = t_i + \Delta t_1 \quad (14)$$

$$\sin(\Omega - \theta_t)_{i+1} = \sin(\Omega - \theta_t)_i \cos \Delta + \cos(\Omega - \theta_t)_i \sin \Delta \quad (15)$$

$$\cos(\Omega - \theta_t)_{i+1} = \cos(\Omega - \theta_t)_i \cos \Delta - \sin(\Omega - \theta_t)_i \sin \Delta \quad (16)$$

$$\underline{Z} \cdot \underline{W}_{i+1} = \sin(\Omega - \theta_t)_{i+1} \cos \phi \sin i + \sin \phi \cos i \quad (17)$$

where t_F is the final time for which look angles are required and ϕ is the station latitude.

if $|\underline{Z} \cdot \underline{W}_{i+1}| \geq K_1$ continue the iteration; otherwise,

- (3) Set t_i equal to $t_{i+1} - \Delta t_1$ and iterate on \dot{L}_{zh} as follows:

- (a) Enter the XYZSB subroutine to obtain the position and velocity of the satellite at time $t_i + t_B$

- (b) Compute ρ , $\dot{\rho}$ and $\dot{\rho}_h$ from equations (29) through (31).

- (4) Compute \dot{r}_{zh} , the zenithal component of the range velocity and \dot{L}_{zh} , the zenithal components of \dot{L} .

$$\dot{r}_{zh} = (\dot{x} + \dot{\theta}y) \cos \phi \cos \theta + (\dot{y} - \dot{\theta}x) \cos \phi \sin \theta + \dot{z} \sin \phi \quad (18)$$

$$\dot{L}_{zh} = \frac{1}{\rho} (\dot{r}_{zh} - \frac{F}{\rho} r_{zh})$$

$$\text{where } \theta = \theta_o + \dot{\theta} (t_i + t_B - t_o) \quad (19)$$

if $L_{zh} \leq 0$ add Δt_2 to t_i ($\Delta t_2 = 25$ min. at present) and continue the iteration; otherwise, enter the following iteration on \dot{L}_{zh} :

add Δt_2 to t_i

- (5) Enter the XYZSB subroutine to obtain the position and velocity of the satellite at time $t_i + t_B$

- (6) Compute \dot{L}_{zh} as above

if $L_{zh} > 0$ continue the iteration; otherwise, set

$\Delta t_{i-1} = 25$ minutes and $N = 0$ and enter the following iteration on \dot{L}_{zh} :

- (7) Iterate to obtain the point of maximum elevation:

$$\text{set } \Delta t_i = -\frac{1}{2} |\Delta t_{i-1}| \quad (20)$$

$$t_{i+1} = t_i + \Delta t_i \quad (21)$$

$$N = N + 1 \quad (22)$$

Enter the XYZSB subroutine and compute \dot{L}_{zh} as above.

If N is less than 7 test $\dot{L}_{zh} : 0$; if $\dot{L}_{zh} < 0$ set $\Delta t_{i+1} =$

$\frac{1}{2} |\Delta t_i|$ and continue iteration; if $\dot{L}_{zh} \geq 0$ set

$\Delta t_{i+1} = -\frac{1}{2} |\Delta t_i|$ and continue iteration.

(8) If $N = 7$ compute \dot{L}_{zh} as follows:

$$\ddot{L}_{zh} = (\dot{L}_{zh_i} - \dot{L}_{zh_{i-1}}) / \Delta t \quad (23)$$

(9) Test the quantity $\frac{\dot{L}_{zh}}{\ddot{L}_{zh}}$: if

$$|\frac{\dot{L}_{zh}}{\ddot{L}_{zh}}| < |\frac{\Delta t}{2}| \text{ set } t_{i+1} = t_i - \frac{\dot{L}_{zh}}{\ddot{L}_{zh}} ; \text{ otherwise, set} \quad (24)$$

$$t_{i+1} = t_i + \frac{\dot{L}_{zh}}{|\dot{L}_{zh}|} \left| \frac{\Delta t_i}{2} \right| ; \text{ then compute } \underline{\rho}_h \text{ and } \dot{\rho} \quad (25)$$

as follows:

$$\theta = \theta_o + \dot{\theta} (t_{i+1} + t_B - t_o) \quad (26)$$

$$X = (X/\cos \theta) \cos \theta \quad (27)$$

$$Y = (X/\cos \theta) \sin \theta \quad (28)$$

where $X/\cos \theta$ is a station coordinate function obtained as input.

$$\underline{\rho}_h \left\{ \begin{array}{l} \rho_{xh} = (x + X) \sin \phi \cos \theta + (y + Y) \sin \phi \sin \theta - (z + Z) \cos \phi \\ \rho_{yh} = -(x + X) \sin \theta + (y + Y) \cos \theta \\ \rho_{zh} = (x + X) \cos \phi \cos \theta + (y + Y) \cos \phi \sin \theta + (z + Z) \sin \phi \end{array} \right. \quad (29)$$

$$\rho = (\rho_{xh}^2 + \rho_{yh}^2 + \rho_{zh}^2)^{1/2} \quad (30)$$

$$\dot{\rho} = \frac{1}{\rho} \left\{ (x + X) (\dot{x} + y \dot{\theta}) + (y + Y) (\dot{y} - x \dot{\theta}) + (z + Z) \dot{z} \right\} \quad (31)$$

$$\text{Set } t_L = t_{i+1} + \Delta t_1 + \Delta t_2 \quad (32)$$

- (10) Test ρ_{zh} : if $\rho_{zh} > 0$, exit to next computation; otherwise return to the beginning of this section 3.3.(1) with the new t_L . If $\rho_{zh} \leq c(\sin h_{\min} - \epsilon)$, also return to the beginning of this section with the new t_L .

3.4 COMPUTATION OF THE MAXIMUM ELEVATION

If the point of maximum elevation (CPA) is required, compute A and h as follows:

$$A = \tan^{-1} \frac{\rho_{yh}}{\rho_{xh}} ; \quad 0 \leq A \leq 2\pi \quad (33)$$

$$h = \sin^{-1} \frac{\rho_{zh}}{\rho} \quad (34)$$

where ρ and ρ_{zh} are available from the previous section at the time of closest approach.

3.5 DETERMINATION OF THE REQUIRED ACQUISITION MODEL

Test the radar type to determine which acquisition model is required:

Planar fans use PACQUI formulation.

Horizontal fans use HACQUI formulation.

Trackers use TACQUI formulation.

3.6 PACQUI FORMULATION

Acquisition model for planar fans

- (1) Compute $\underline{E} \cdot \underline{N}$, where \underline{N} is a unit vector normal to and above the plane of the fan.

$$f_{N_1} = \underline{E} \cdot \underline{N} \quad (35)$$

Set $t_1 = -10$ minutes and $t_2 = t_i$

(2) Start iteration to make $\underline{\rho} \cdot \underline{N}$ change sign:

(a) If $\rho_{zh} \geq 0$ continue the iteration with (c); otherwise,

(b) If this is the first time through, set $t_i = t_2$ and exit, if this is not the first time through, set $\underline{\rho} \cdot \underline{N}$ equal to ρ_{N_1} , $\Delta t = +10$ and $t_{i+1} = t_2$; then go to step (d) to obtain the descending observation time.

(c) If $|\underline{\rho} \cdot \underline{N}| \leq \rho_c$ go to the next subsection; otherwise,

$$(d) \quad t_{i+1} = t_i + \Delta t \quad (36)$$

$$\rho_{N_3} = \underline{\rho} \cdot \underline{N} \quad (37)$$

(e) Compute ρ , ρ and $\underline{\rho}_h$ from equations (29) through (31).

(f) Compute $\underline{\rho} \cdot \underline{N}$ and test $|\underline{\rho} \cdot \underline{N}_1| < 0$; if > 0 continue the iteration with (a) above; otherwise, go to the next subsection.

(3) Iterate, by halving, to determine the time when the satellite passes within the observational limits of the fan.

$$(a) \quad \Delta t_{i+1} = \frac{\rho_{N_3} (\underline{\rho} \cdot \underline{N})}{|\rho_{N_3} (\underline{\rho} \cdot \underline{N})|} - \frac{\Delta t_i}{2} \quad (38)$$

$$(b) \quad t_{i+1} = t_i + \Delta t_{i+1} \quad (39)$$

$$\rho_{N_3} = (\underline{\rho} \cdot \underline{N}) \quad (40)$$

(c) Compute ρ , ρ and $\underline{\rho}_h$ from equations (29) through (31). (41)

(d) Compute $\underline{\rho} \cdot \underline{N}$ and test: if $|\underline{\rho} \cdot \underline{N}| \leq \rho_c$ go to the next subsection; otherwise return to (a) above to continue the iteration.

- (4) Test the observation with respect to the angular limits of the fan: if $(\underline{L} \cdot \underline{L}_1)(\underline{L} \cdot \underline{L}_2) \geq (\underline{L} \cdot \underline{L}_2)$, the observation is within the angular limits of the fan; otherwise, return to 3.6(2)(a).

$$\underline{L} = \frac{\rho}{\rho}; \underline{L}_1 \text{ and } \underline{L}_2 \text{ are unit topocentric vectors defining the angular limits of the fan.} \quad (43)$$

- (5) If range limits are specified perform the following test: if $\rho \leq \rho_{\max 1} + \rho'_{\max} \cos^{-1}(\underline{L} \cdot \underline{L}_1)$ the range is observable.

$\rho_{\max 1}$ is the maximum observable range along \underline{L}_1

ρ'_{\max} is the derivative of maximum observable range with respect to the angle $\cos^{-1}(\underline{L} \cdot \underline{L}_1)$. It is assumed linear for this program and is given by:

$$\rho'_{\max} = \frac{\rho_{\max 2} - \rho_{\max 1}}{\cos^{-1}(\underline{L}_1 \cdot \underline{L}_2)} \quad (45)$$

- (6) If the satellite is observable and the time of observation falls within the requested time limits, then perform the following calculations if illumination information is required.

- (a) Compute the sun's true longitude, ℓ_\odot , at time $\frac{(t_B + t_i)}{1440} = T$:

$$\ell_\odot = L_\odot + n_\odot T + 1.91 \sin(n_\odot T - M_\odot) \quad (47)$$

where n_\odot is the mean motion of the sun in degrees per day

L_\odot is the mean longitude of the sun at time T , given by

$$L_\odot = L_{\odot 0} + n_\odot T; L_{\odot 0} \text{ is the mean longitude of the sun at the beginning of the epoch year.} \quad (48)$$

$$M_Q = L_{Q_0} + n_Q T - \pi_Q; \pi_Q \text{ is the sun's longitude of perifocus} \quad (49)$$

- (b) Calculate the geocentric unit vector toward the sun, \underline{L}_Q :

$$\underline{L}_Q \left\{ \begin{array}{l} L_{x_Q} = \cos \delta_Q \cos \alpha_Q \\ L_{y_Q} = \cos \delta_Q \sin \alpha_Q \\ L_{z_Q} = \sin \delta_Q \end{array} \right. \quad (50)$$

$$\text{where } \alpha_Q = \ell_Q - 2.47 \sin 2 \ell_Q \quad (51)$$

$$\delta_Q = \tan^{-1} (0.4336635 \sin \alpha_Q) \quad (52)$$

- (c) Calculate and test the elevation angle of the sun, h_Q

$$h_Q = \sin^{-1} \left(-\underline{L}_Q \cdot \frac{\underline{R}}{R} \right) \quad (53)$$

where $\frac{\underline{R}}{R}$ is a unit vector from the station to the geocenter.

If $h_Q > -5^\circ$, no visual points may be calculated.

If $h_Q < -5^\circ$ the calculation continues to determine if the satellite is illuminated.

- (d) It has already been established that the satellite is above the sensor's horizon. The Earth's shadow is assumed cylindrical. See Figure 4.

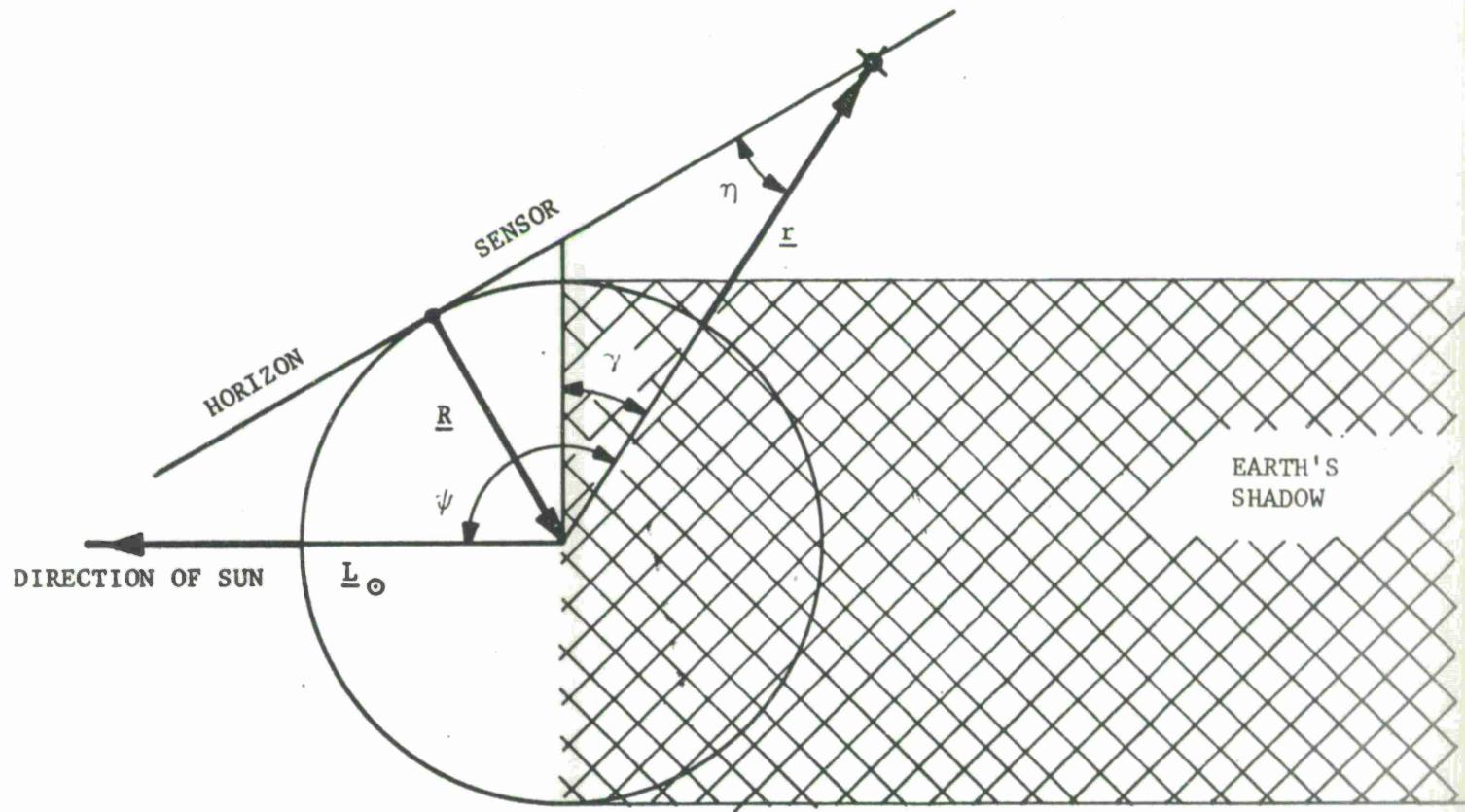
$$\cos \psi = \frac{1}{r} (\underline{L}_Q \cdot \underline{r}) \quad (54)$$

- (e) If $\cos \psi$ is positive, the satellite is illuminated. If $\cos \psi$ is negative, the satellite may still be illuminated. This is determined from γ and η as follows.

$$\gamma = \psi - 90^\circ \quad (55)$$

$$\eta = \sin^{-1} \left(\frac{R}{r} \right) \quad (56)$$

If $\gamma + \eta > 90^\circ$, the satellite is not visible, if $\gamma + \eta \leq 90^\circ$, the satellite is illuminated.



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FIGURE 4. POSITION OF SATELLITE WITH RESPECT TO THE EARTH'S SHADOW

- (7) If either the satellite is not observable or this is the first time through, and $t_i < t_2$; then set

$$\underline{\rho} \cdot \underline{N} = \rho_{N_1} \quad (57)$$

$$t_i = t_2 \quad (58)$$

$$\Delta t = 10 \text{ min} \quad (59)$$

and return to 3.6(3)(b). Otherwise, continue with the next subsection after storing the acquisition coordinates for output.

3.7 HACQUI FORMULATION

Acquisition model for horizontal fans

- (1) Set $t_2 = t_i$ and $\Delta t = -10 \text{ min}$.
- (2) Iterate to make ρ_{zh} approach $\rho \sin h_{ref}$. $\cos h_{ref}$ and $\sin h_{ref}$ are available from the acquisition buffer (input quantities)
 - (a) If $|\rho_{zh} - \rho \sin h_{ref}| \leq \rho \epsilon \cos h_{ref}$ go to (4) below; otherwise, continue with (b).
 - (b) Set $K_3 = 1$ and $t_{i+1} = t_i + \Delta t$
 - (c) Compute ρ , ρ and $\underline{\rho}_h$ from equations (29) through (31).
 - (d) If $\rho_{zh} > \rho \sin h_{ref}$ return to (a) above; otherwise, continue with (3).
- (3) Iterate to obtain the time of fan penetration

$$(a) \Delta t_{i+1} = \frac{K_3 (\rho_{zh} - \rho \sin h_{ref})}{|K_3 (\rho_{zh} - \rho \sin h_{ref})|} \cdot \frac{\Delta t_i}{2} \quad (63)$$

$$(b) K_3 = \rho_{zh} - \rho \sin h_{ref} \quad (64)$$

$$t_{i+1} = t_i + \Delta t_{i+1} \quad (65)$$

(c) Compute ρ , $\dot{\rho}$ and $\underline{\rho}_h$ from equations (29) through (31).

(d) If $|\rho_{zh} - \rho \sin h_{ref}| > \rho \in \cos h_{ref}$ return to (a); otherwise, continue with (4). (66)

(4) Compute A and h from ρ and $\underline{\rho}_h$:

$$A = \tan^{-1} \frac{\rho_{yh}}{\rho_{xh}} \quad (67)$$

$$h = \sin^{-1} \frac{\rho_{zh}}{\rho} \quad (68)$$

(5) If this is a tracker to (8); otherwise, continue with (6).

(6) If $(A_2 - A_1)(A - A_1)(A_2 - A) \geq 0$ the observation is within the angular limits of the fan so continue with (7). A_1 and A_2 are the azimuthal limits of the fan.

If $t_i < t_1$ and $t_i < t_2$, set $T_1 = t_i$, $\Delta t = 10$ min and $t_i = t_2$, then return to 3.7(2)(b); otherwise exit.

(7) If $\rho \leq \rho_{max1} + \rho'_{max}(A - A_1)$ the range is observable so continue with (8).

ρ_{max1} is the maximum observable range in the A_1 direction

ρ'_{max} is the derivative of maximum range with respect to $(A - A_1)$. It is assumed linear and is given by:

$$\rho'_{max} = \frac{\rho_{max2} - \rho_{max1}}{A_2 - A_1} \quad (69)$$

If $\rho > \rho_{max1} + \rho'_{max}(A - A_1)$ and $t_i < t_2$, set $T_1 = t_i$, $\Delta t = 10$ min and $t_i = t_2$, the return to 3.7(2)(b); otherwise exit.

(8) If the satellite is observable and the time of observation is within the requested time limits; then, if required, test for solar illumination using equations (46) through (56). If this is the first time through and $t_i < t_2$, set $T_1 = t_i$, $\Delta t = 10$ min and $t_i = t_2$, then return to 3.7(2)(b); otherwise, set $T_2 = t_i$ and $t_i = t_2$ and exit to the next subsection. In either case, store the acquisition coordinates for output.

3.8 TACQUI FORMULATION

Acquisition model for trackers

- (1) If a maximum range is specified test ρ , if $\rho > \rho_{\max}$ exit, otherwise continue with (2).
- (2) If this is a phased array tracker, go to TACQUII (3.9). Otherwise, set $A_1 = 0$, $A_2 = 2\pi$ and go to HACQUI (3.7).
- (3) If only the ascending half of the pass is required, set $T_2 = t_2$.
- (4) Test the points per pass integer, P :

If $P = 9$, an output interval, Δt , is specified, so go to (5); otherwise set

$$\Delta t = \frac{T_2 - T_1}{P - 1} \quad (70)$$

$$t_i = T_1 \quad (71)$$

and go to (6).

- (5) Set $N = \text{integral part of } (T_2 - T_1)/2\Delta t$ and

$$t_i = \frac{1}{2} (T_2 + T_1) - (N + 1) \Delta t \quad (72)$$

- (6) If this is a phased array, go to (8).

- (7) If ascending points only are required, set

$$T_2 = T_2 + \Delta t \quad (73)$$

- (8) Compute ρ , A , h and $\dot{\rho}$, for output, at each time point between T_1 and T_2 required by (4) or (5) above.

3.9 TACQU11 FORMULATION

Acquisition model for phased array trackers

(1) Set $K_1 = 1$ and go to AFILT3 (3.10)

(a) if this observation passes the tests in AFILT3 or is marginal and visible, go to (4).

(b) if this observation fails the tests in AFILT3 or is marginal but not visible as described by equations 98-100, go to (2).

(2) Set $K_1 = -1$, $t_2 = t_i$, $K_3 = -1$ and $\Delta t = -0.2 \text{ min}$ (75)

(3) Iterate to check for visible points on this pass

(a) Set $t_{i+1} = t_i + \Delta t$ (76)

(b) Compute ρ , $\dot{\rho}$ and $\underline{\rho}_h$ from equations (29) through (31).

(c) If $\rho_{zh} > 0$ go to (d); if ≤ 0 and $t_i < t_2$, set

$t_i = t_2$, $\Delta t = 0.2$ and $K_1 = +1$ and go to (a). (77)

(d) Go to AFILT3

If the satellite fails the tests in AFILT3, return to (a).

If it passes the tests, set $t_2 = t_i$ and go to (e).

If it is marginal, set $t_2 = t_i$ and go to (8).

(e) Set $\Delta t_{i+1} = \frac{1}{2} K_3 \Delta t_i$ and go to (7). (78)

(4) Set $t_2 = t_i$, $K_3 = +1$ and $\Delta t = -10 \text{ min}$ (79)

(5) Set $t_{i+1} = t_i + \Delta t$. (80)

Compute ρ , $\dot{\rho}$ and $\underline{\rho}_h$ from equations (29) through (31).
Go to AFILT3

If the satellite passes the tests in AFILT3, return to the beginning of 3.9(5).

If it fails the tests, go to 3.9(6).

If it is marginal, go to 3.9(8).

(6) Set $\Delta t_{i+1} = -\frac{1}{2} K_3 \Delta t_i$ and $K_3 = -1$ (81)

(7) Iterate to obtain the times of marginal visibility

(a) Set $t_{i+1} = t_i + \Delta t_{i+1}$

(b) Compute ρ , $\dot{\rho}$ and $\underline{\rho}_h$ from equations (29) through (31).

(c) Go to AFILT3

If the satellite passes the tests in AFILT3 go to 3.9(3)(e).

If it fails the tests go to 3.9(6).

If it is marginal go to 3.9(8).

(8) Compute A and h from equations (67) and (68) and:

If this is the first time through set

$$T_1 = t_i \quad (83)$$

$$t_i = t_2 \quad (84)$$

$$\Delta t = 10K_1 \quad (85)$$

$$K_3 = 1 \quad (86)$$

and go to 3.9(5); otherwise, if $t_i > T_1$ set $T_2 = t_i$; if $< T_1$ set (87)

$$T_2 = T_1 \quad (88)$$

$$T_1 = t_i \quad (89)$$

and exit.

3.10 AFILT3 FORMULATION

Determine whether the satellite is visible, invisible or marginally visible to the sensor at this time.

(1) Test against minimum elevation angle

(a) Set $\delta = \rho_{zh} - \rho \sin h_{min}$ and (90)

$E = \rho \epsilon \cos h_{min}$ (91)

U_{max} , V_{max} , $\cos \psi_{max}$, $\sin h_{min}$, and $\cos h_{min}$ are stored from input into the FANTAB buffer.

(b) Go to AFILT31 (3.11)

(2) Test against maximum off boresight angle

(a) Set $\delta = \underline{\rho} \cdot \underline{y} - \rho \cos \psi_{\max}$ (92)

$E = \rho \epsilon \sin \psi_{\max}$ (93)

(b) Go to AFILT31

(3) Test against minimum angle from z axis

(a) Set $\delta = \rho U_{\max} - |\underline{\rho} \cdot \underline{z}|$ (94)

$E = \rho \epsilon (1 - U_{\max}^2)^{1/2}$ (95)

(b) Go to AFILT31

(4) Test against minimum angle from x axis

(a) Set $\delta = \rho V_{\max} - |\underline{\rho} \cdot \underline{x}|$ (96)

$E = \rho \epsilon (1 - V_{\max}^2)^{1/2}$ (97)

(b) Go to AFILT31

3.11 AFILT31 FORMULATION

Subroutine used by AFILT3

(1) If $\delta \geq 0$ the satellite is visible (98)

(2) If $\delta < 0$ the satellite is invisible (99)

(3) If $|\delta| < E$ the satellite is marginally visible (100)

SECTION 4

OPERATING INSTRUCTIONS AND COMPUTER REQUIREMENTS

The OBSERV module is programmed for the Philco 2000 computer. This section describes the tape setup, deck setup, input options and output formats.

4.1 GENERAL

This program has two modes of execution: (1) in conjunction with the Semi-Automatic System job-schedule mode of operation, where the normal operating procedures required for this mode are described in Section 2 of reference 3; and (2) the manual mode of operation which obtains input from the console typewriter instead of the SCHEDULE TAPE.

Input quantities are to specify which sensor is to be provided acquisition coordinates, which satellites are to be observed and the time period which calculations are to cover. The data are calculated and stored in core and on magnetic tape for one satellite at a time. Note that any or all types of acquisition models can be combined in the same case.

For one satellite, output data for the visual passes only and all the predictions for one pass may be printed in chronological order without being mixed with predictions for other satellites.

Due to changes in system operating procedures, OBSERV has become somewhat like a main sequence program, which reverses the original design specifications. Therefore, the program has been modified so that it may be run in the manual mode. In this mode the program may be called big using the console typewriter. The input is the same as for option 0 in the schedule tape mode except that the base day and base message numbers are typed in. Most of the changes are primarily concerned with input data processing.

4.2 TAPE SETUP

Tape assignments are displayed in Figure 5. When OBSERV is run in the manual mode of operation the SCHEDULE TAPE (logical 2) is not used.

4.3 DECK SETUP

For both modes of operation (schedule and manual), the FAN TAPE (logical 0) is generated from punched cards on the Philco 1000 in read-code mode with sense option on. Nine types of cards are used (see Figure 6):

<u>CARD TYPE</u>		<u>CONTENT</u>
1		"FANCARDS" Card
2		Control Card
3		Fan/Tracker Card
4		"FROM" Address Card
5		"INFO" Address Card
6		"TO" Address Card
7		"ALL", "ALL BUT", or "ONLY" Card
8		ENDCASE Card
9		ENDSCHED Card

Explanation of card types:

<u>TYPE</u>	<u>DESCRIPTION</u>
1	Used as the Tape Identifier. See Figure II-1
2	Must always be used and specifies data about the sensor, the calculations and the output. Fields 11 and 12 are used in the headings of the printed output. See Figure II-2

<u>Logical Unit</u>	<u>Tape Identification</u>	<u>Description</u>
0	FANCARDS	FAN TAPE - Input
1	70/BINMST	SPS B-2 Master
2	70 Δ SCHTP	SCHEDULE TAPE - Input (Not required in manual mode)
4	70 Δ SEAII	Sensor, Element Acquisition Information Communication Files
7 (write ring in)	SCRATCH	SCRATCH
8 (write ring in)	SCRATCH	SCRATCH
9 (write ring in)	SCRATCH	SCRATCH
11 (write ring in)	70 ØUTPUT	OUTPUT

FIGURE 5. TAPE SETUP FOR OBSERV

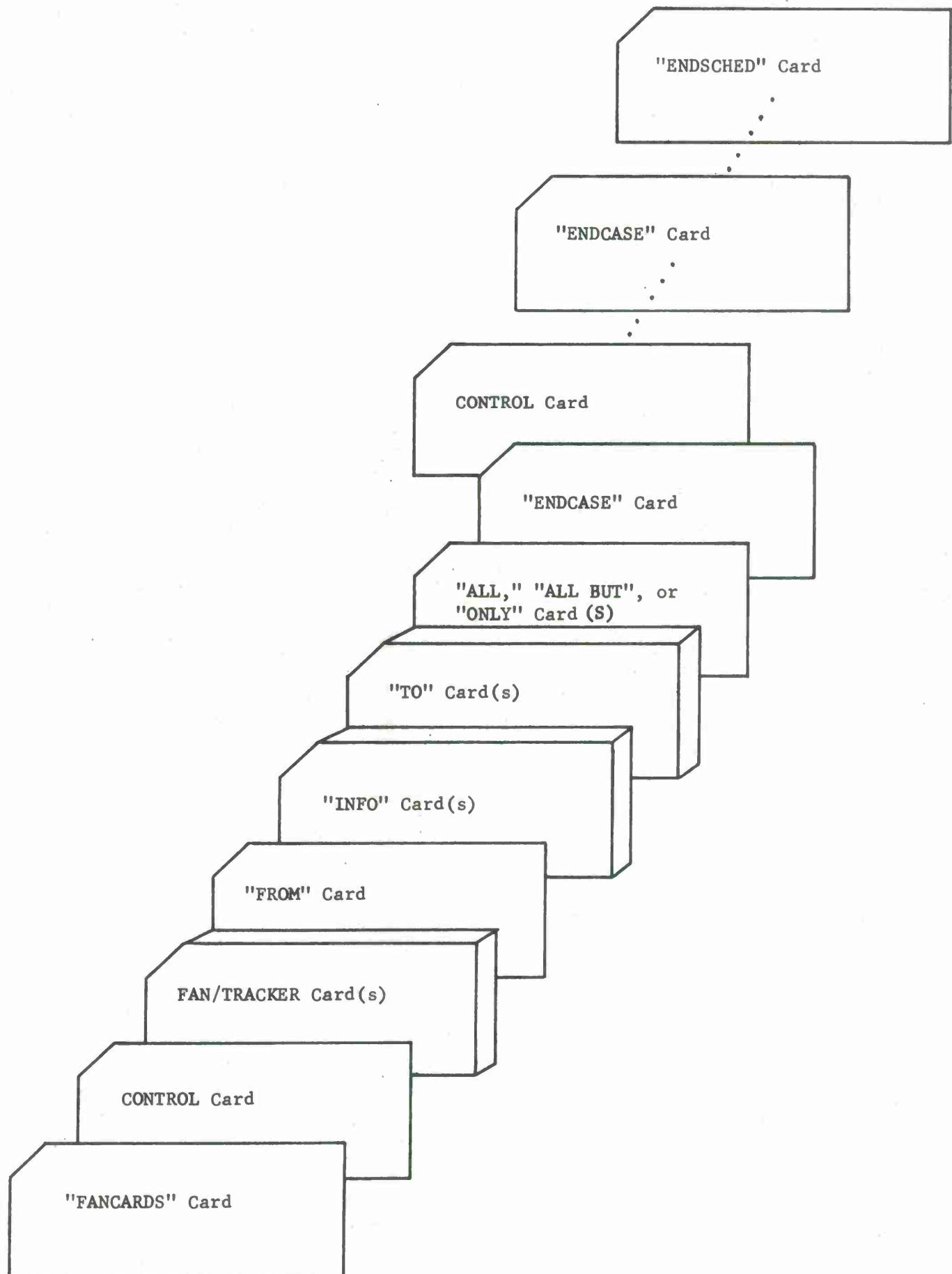


FIGURE 6. DECK SETUP FOR FAN TAPE - (LOGICAL 0)

<u>Type</u>	<u>Description</u>
3	FAN Card - used to specify data for fixed beam surveillance sensors. As many as two fixed beams or fans may be specified on one card. A maximum of fifteen cards, specifying no more than 30 beams can be used. See Figure II-3.
4,5,6	TRACKER Card - used to specify data for a sensor with tracking capability. This card, one per sensor, must have a "Δ-99.0" punched in the first field. Any number 2 thru 8 points may be specified per satellite pass. If 9 is indicated-points are spaced Δt apart. See Figure II-4.

<u>Type</u>	<u>Description</u>
7	Specifies the satellites to be used. The ALL card indicates <u>all</u> satellites are to be used in the run. The ALL BUT card indicates <u>all but</u> the satellites specified in the variable field beginning in Column 9 are to be run. The ONLY card indicates <u>only</u> the ones specified in the variable field are to be run. The satellite numbers are specified by five digit numerics separated by commas. A range of satellites may also be specified. For example, assume satellites 00004, 00005, 00006, 00007, are to be run. This may be specified on an ONLY card in one of two ways: ONLY 00004, 00005, 00006, 00007, ONLY 00004 - 00007
	Data can continue on subsequent cards, the data beginning in Column 1. See Figure II-6.
8,9	Both cards have 11-8-2 punch in Column 9 for END BLOCK Control and both are the same as those used on Schedule Tape jobs. END CASE - separates each group of Case Data Cards. ENDSCHED - the last card in the deck.

The required order of cards to be used for the FAN Input Data

Tape is as follows:

<u>TYPE</u>	<u>CONTENT</u>
1	"FANCARDS" Card
2-7	Case Data Cards

<u>Type</u>	<u>Content</u>
8	END CASE Card
2-7	Case Data Cards
8	END CASE Card
.	.
.	.
.	.
.	.
.	.
9	ENDSCHED Card

The Case Data Cards are arranged in the following order:

<u>TYPE</u>	<u>CONTENT</u>	<u>COMMENT</u>
2	Control Card	One per case
3	Fan/Tracker Cards	One Tracker card and/or any number of fan cards the total not to exceed 30 fans.
4	"FROM" Card	One per case
5	"TO" Card	Up to nine per case with limitation that the sum of "TO" and "INFO" Cards cannot exceed nine.
6	Either "ALL", "ALL BUT" or "ONLY"	One per case; additional satellite specifiers can follow "ALL BUT" and "ONLY" Cards.

For schedule mode of operation the SCHEDULE TAPE (logical 2) is generated from punched cards in the same manner as the FAN TAPE is generated (see Figure 7). The cards are as follows:

- ID Card
- JOB Card
- REM Card (optional)
- SPS JOB Card
- Parameter (Base-Time) Card
- Data Cards (for options 1, 2, 3, 4, and 5 only) -
Element, Sensor, etc.
- ENDOFJOB Card

The ID, JOB, REM, ENDOFJOB, ENDSCHED and the END CASE Cards are described in Section 5.4 of reference 3.

The parameter (Base-Time) Card is depicted in Figure II-7

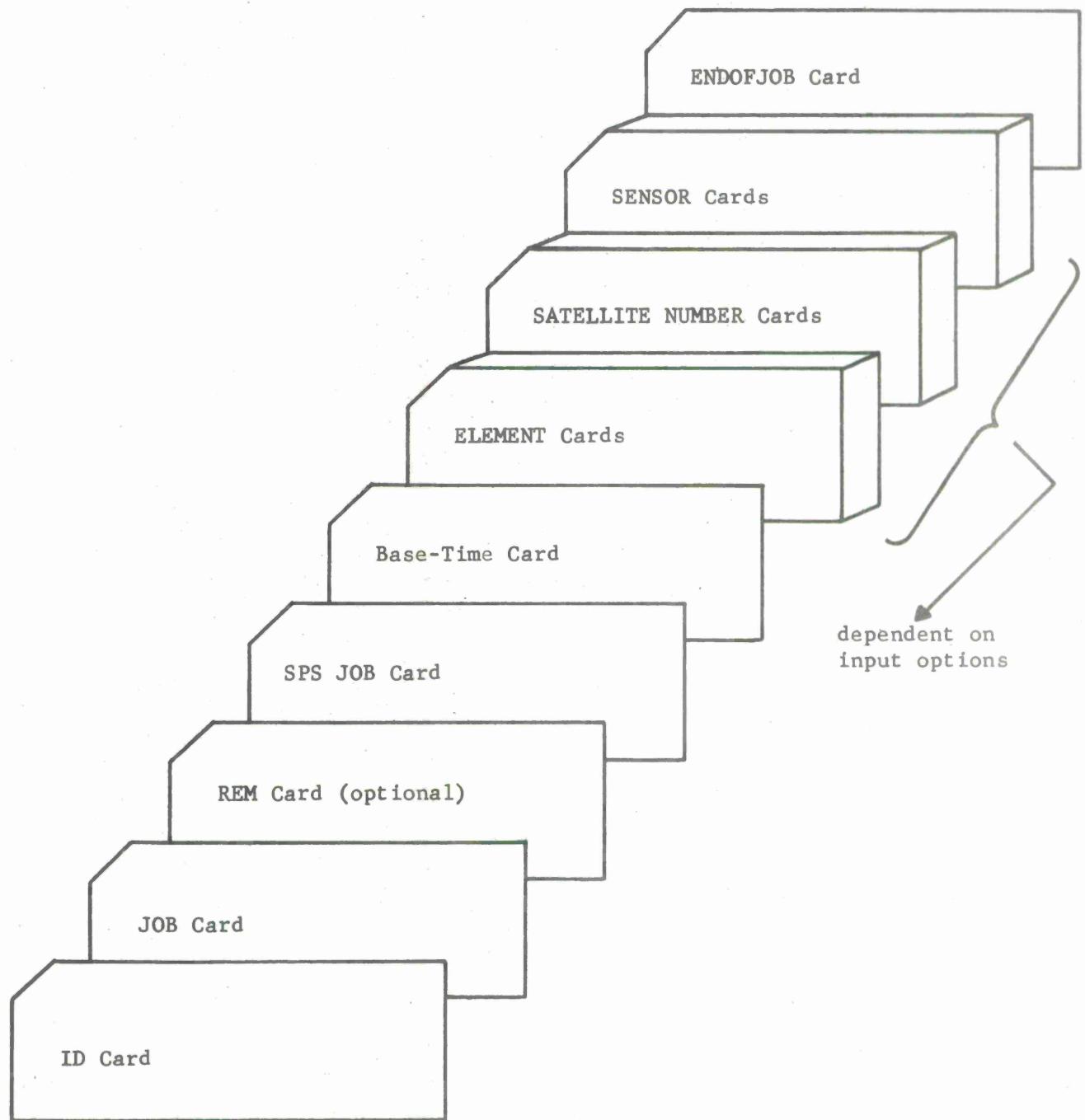


FIGURE 7. DECK SETUP FOR SCHEDULE TAPE - (LOGICAL 2)

4.4 INPUT OPTIONS

The program allows six input options while in the schedule tape mode of operation. The input option designates whether required data will come from the input tape or from standard system files.

TABLE I INPUT OPTIONS

INPUT OPTION	<u>Tape 4 (SEAI)</u>		<u>Tape 2 (SCHEDULE)</u>			
	<u>E-FILE</u>	<u>S-FILE</u>	<u>PARAMETER</u>	<u>ELEMENT</u>	<u>SATELLITE</u>	<u>SENSOR</u>
0	*	*	Yes	No	No	No
1		*	Yes	Yes	No	No
2	*	*	Yes	No	Yes	No
3			Yes	Yes	No	Yes
4	*		Yes	No	Yes	Yes
5	*		Yes	No	No	Yes

*Use of these files is implied with this option.

- Notes:
- (1) Parameter card - This card specifies the base day and base message number.
 - (2) E-File - This file on the SEAI tape contains the elements of all satellite orbits.
 - (3) S-File - File on the SEAI tape which contains the coordinates of all the sensors.
 - (4) Element Cards - Each set of six cards contains the elements of any given satellite orbit.
 - (5) Satellite Number Cards - These cards contain the numbers of satellites whose elements are to be obtained from the E-File.
 - (6) Sensor Cards - These cards contain the coordinates of any one sensor.

Descriptions of the cards and tape files mentioned above can be found in Sections 5.4 and 5.5 respectively, of reference 3.

A description of each option follows:

- 0 - The elements of those satellite orbits on the E-File which are specified on the ALL, ALLBUT or ONLY card will be used in calculations. The coordinates of the sensor specified on the Control Card will be obtained from the S-File.
- 1 - The elements introduced by the Element Cards will be used in calculations. All other operations are the same as option 0.
- 2 - Those elements specified on the Satellite Number Cards will be read from the E-File and used for calculations. All other operations are the same as option 0.
- 3 - Operations are similar to option 1 except that the sensor coordinates are obtained from the Sensor Card.
- 4 - Operations are similar to option 2 except that the sensor coordinates are obtained from the Sensor Card.
- 5 - The elements of those satellite orbits on the E-File which are specified on the ALL, ALLBUT or ONLY card will be used in calculations. The sensor coordinates are obtained from the Sensor Card.

4.5 OUTPUT

a. Options

- (1) -0- Specifies the generation of the output on printed copy and teletype tape.
- (2) -1- Output is produced on printed copy only. Note that the information on the printed copy and the teletype tape are in the same order; however, the direction cosine printout is optional on hard copy but is not available for the teletype tape. When run in manual mode, option 0 is automatically specified. In the schedule mode, column 18 of the SPSJOB card specifies the option (0 or 1).

b. Format

Figure 8 shows the general format of the output with heading information. FAN number is optional on both hard copy and teletype tape; also, when requested for a tracker, FAN number prints "T" and for point of maximum elevation "***". Every

SAT. SUMMARY FOR STA - XXX

NNNNN,

DECAYING

NNNNN,

100 DAYS PAST EPOCH

NNNNN,

SAT.NO./SET NO.

NNNNN/SSSS.

△△△
PP SSS TTTT VVVV (up to 9 addresses)

DE RRRR MMMM C

CCCr

P DD/HHMMZ

FM SENDING STATION ADDRESS

TO STATION ADDRESS

INFO STATION ADDRESS

CLASSIFICATION (see below) DDD HHMM.FF

LOOK ANGLE SCHEDULE FOR STATION ADDRESS

SAT	XXXX	TIME	ELEV	AZMTH	RANGE	R-RATE	FAN No.	DIRECTION	COSINES			
								U	V	W		
DAY	DDD	DD/MM/YY		(XX)								
NNN	NNNNN	HHMM.FF	±	EE.E	AAA.A	RRRRR	±	RR.R	NN	±.UUU	±.VVV	±.WWW
...
...

NO MORE DATA

DD/HHMMZ MMM RRRR

Classification Format

UNCLAS ISPADATLAS

CONFIDENTIAL ISPADATLAS

SECRET ISPADATLAS

SECRETNOFORN ISPADATLAS

SECRET RELEASABLE OUTSIDE SSO CHANNELS ISPADATLAS

XXX = Station ID Number

NNNNN = Satellite Number

NNNNN = 000 if no Satellites qualify for these two categories

Hard Copy Only

SSSS = Element Set Number

△△△ = TTY Heading for each message or after every 100 lines if TTY is requested with addressing Priority and To and INFO Station Route Addresses

RRRRR = Sending Station Route Address; MMMM = Message Number; C = A or D

CCC = ZNR if unclassified

Current Time

Route Addresses may also be included

Current Time

XXXX = ELEM or REV

XX = KM or NM

Hard Copy and TTY output

Data Within Period

Current Time; Month; Sending Station Route Address

TTY Wrapup

NOTES: Underlined quantities are of fixed format and are printed as shown.

This Format is subject to change without notice in order to comply with Military Network changes.

FIGURE 8 OBSERVING SCHEDULE PROGRAM OUTPUT FORMAT

effort has been made to ensure that teletype headings conform with the procedure presently established for use within the military networks. The RANGE may print "0" kilometers - this indicates that the actual range was greater than 16,383 km. and could not be contained in the internal packed format.

c. Satellite Summary

The satellite summary output routine has been retained which lists the satellites being used and their corresponding element set numbers. This is printed on the hardcopy only. Special comments are printed if the predictions are more than one hundred days from epoch or if the satellite has reached decay conditions during the prediction.

d. Diagnostic Error Comments

The program may print any one of a number of diagnostic error comments some of which indicate an error in the input and others which indicate a malfunction of the program or the machine.

They are nearly all self-explanatory and are intended to aid the user in the full utilization of the program. The comments which might appear are as follows:

- (1) "CASE REJECTED - BASE TIME CARD MISSING OR IN ERROR".

The entire job is rejected because of a faulty card or because the base time or message number was typed incorrectly.

- (2) "CASE REJ-INP ERR - STA XXX" The current case only is rejected for one of the following stated reasons:

"ERROR ON ALL BUT OR ONLY CARDS".

"FAN PARAMETER (REQUEST) CARD MISSING (NO R IN COLUMN 79)."

"CHECK INPUT DATA FOR ILLEGAL CHARACTERS IN FIELDS."

"STA. NO. ON R AND F CARDS DIFFER."

"FAN CARDS MISSING (NO F IN COLUMN 79)."

"ADDRESS CARD MISSING"

"PRIORITY NOT PUNCHED IN PARAMETER (REQUEST) CARD."

"MORE THAN THIRTY RECORDS IN F TYPE CARDS"

"ALL, ALL BUT, OR ONLY CARDS MISSING"

"ROUTING DATA MISSING"

"TOO MANY ROUTE CARDS"

- (3) "ERROR ON TRACKER CARD. CARD REJECTED" A tracker card is rejected for one of the following reasons:

"ONLY 1 TRACKER CARD ALLOWED"

"LIMITS ON BORESIGHT ANGLES WRONG"

"POINTS PER PASS WRONG"

"DELTA T IS ZERO"

"MAX. RANGE IS WRONG"

"MIN. ELEV. GREATER THAN 90"

- (4) "ERROR IN FAN RECORD. RECORD REJECTED" A single fan record is rejected for one of the following reasons:

"FAN TYPE NOT H OR P"
"FAN ENDS TOO CLOSE TO COLINEAR"
"ELEVATION GREATER THAN 89 DEG"
"AZIMUTH LIMITS ARE EQUAL"
"MAX. RANGE IS WRONG"
(5) "SUBROUTINE ERROR FROM LOCATION XXXXX"
(6) "EXPONENT OVERFLOW FROM LOCATION XXXXX"

After printing either of the above two comments,
the program continues processing at the next logical
point.

4.6 PROGRAM NOTES

a. Case Bypass Option

Toggle 47 in the on position causes the program to type the sensor
about to be processed and wait for a "STOP" or a "GO" type-in from the
operator. A "STOP" will cause the case to be bypassed. A "GO" will
cause the case to be run.

b. Point of Maximum Elevation

The point of maximum elevation is the first point calculated. If
the range at the point of maximum elevation exceeds the maximum range
of the tracker, the entire pass is rejected. If this point falls within
the maximum range, the entire pass is retained.

c. Use of the ALL, ALL BUT, and ONLY cards.

One of these cards must be present in every set of Case Data Cards
that is used to generate the Fan Input Data Tape. The content of this
card is important only for input options of zero and five, because
Element and Satellite Number Cards are not used. Therefore, it becomes
necessary to specify which satellites are desired from the E-File.¹
This is accomplished by using an ALL, ALL BUT or ONLY card as described
in Section 4.3a.

For input options 1, 2, 3 and 4, the Schedule Tape contains either
Element or Satellite Number Cards to specify which satellites are to be
used. Because this tape overrides the Fan Input Data Tape, any one of
the ALL, ALL BUT or ONLY cards can be used since it will not be read.
Therefore, whichever card is used may either be blank or contain satellite
numbers.

¹ Refer to Table 1 in Section 4.4

d. Use of the Satellite Summary

The information printed on the Satellite Summary is dependent on the input option. This information is particularly helpful when using input option zero. For this input, the summary lists only those satellites available on the E-File of all those requested on the ALL, ALL BUT or ONLY Cards.

However, for options 1, 2, 3, and 4 the summary prints out all the satellites on the Element or Satellite Number Cards.

e. Acquisition Buffer

Depending on the type of sensor, the acquisition buffer (Figure I-1) holds the respective constants for processing planar fans, horizontal fans, and trackers.

f. Operational Sequence

The B-3 system is initialized by depressing the "load" button on the console. This rewinds the system tape, reads the first block into core and executes a jump to cell 0.

EXECMOD1 and EXECMOD2 are then loaded into core and the tape on logical 4 is checked for proper I.D. "NEXT FUNCTION" is then typed on the console typewriter. The operator can respond to this comment in several ways. He may type "MANUAL", "EXEC", or "WRAPUP". "WRAPUP" will wrap up the output tape and rewind it in lock-out.

(1) Manual Mode

If the operator types "MANUAL" the system will request the program I.D. (OBSERV). After typing in the I.D. the system will execute the object program, which in turn will request the "BASE DAY" and "BASE MESSAGE NO." via the required input console typewriter. The operator must be certain that the data has been prestored onto a tape mounted on logical 0. Upon completion of the program, the system will again type "NEXT FUNCTION".

(2) Schedule Mode

If the operator types "EXEC" and toggle 24 is on, then the schedule tape mounted on logical unit 2 will be processed. A schedule tape program is requested by using an "SPSJOB" card. Such a request causes the system to load EXECMOD3 into core. EXECMOD3 then converts the input data and places it in the proper buffers. It then returns control to EXECMOD2 which loads the object program and executes it. When all the jobs on the schedule tape have been completed, the system again types "NEXT FUNCTION".

SECTION 5

PROGRAM TEST CASE

The test case included in this section illustrates many of the features of the modified program. The input data are shown in Figure 9 and the output in Figure 10.

The satellites which were used exhibit a wide variety of characteristics. Satellite 00001 has a period of approximately 20 hours and a small eccentricity; satellite 00002 has a very high eccentricity (0.7); and satellite 00003 a very low inclination (1.0°). Satellite 00004 has a very small perigee height; satellite 00005 has a high drag; and satellites 00006 and 00007 have typical direct and retrograde orbits, respectively. The sensor used is located at 30° north latitude and 90° west longitude.

The acquisition model is a complex one consisting of a composite of each of the different types. It contains the following:

- (1) A phased-array tracker configuration with the boresight oriented at an elevation of 45° and azimuth of 180° . The limits imposed are 1° in elevation, 60° in α and β , (α and β are respectively, the compliments of the angles between the range vector and the primary and tertiary topocentric reference vectors) and 70° in off-boresight angle.

- (2) A horizontal fan at an elevation of 5° extending only within the tracker limits
- (3) A series of five planar fans which form a crude "S" centered about the boresight vector. This figure ranges in azimuth from 140° to 220° and in elevation from 25° to 65° .

PLANAR FANS

Fan #	Beg. Elev.	Beg. Az	End. Elev.	End. Az
1	65°	140°	65°	220°
2	65°	220°	45°	220°
3	45°	140°	45°	220°
4	45°	140°	25°	140°
5	25°	140°	25°	220°

- (4) The point of maximum elevation is also requested and is printed regardless of elevation or azimuth.

No range test is requested, nor is a visual only test or up-pass only. It is requested that the passes not be interlaced.

The output shows the acquisition data for all satellites except 00001 and 00003. Satellite 00001 has a large period and was not positioned correctly for acquisition during the period of interest. Satellite 00003 has too low an inclination for the sensor location.

The output data for satellite 00002 shows the advantage of using maximum elevation as opposed to closest approach. One may note from the range-rate values that frequently such a satellite does not have a closest approach point during a complete pass.

The pass which satellite 00007 makes on revolution 994 illustrates well the use of the composite acquisition model. Observe that it rises through the lower tracker boundary, penetrates the horizontal fan, passes through 3 segments of the "S" configuration, reaches maximum elevation, and finally leaves the tracker coverage at one of the "corners".

The pass which satellite 00006 makes on revolution 899 illustrates the program's ability to detect very short passes. (Note that the

point of maximum elevation is not within the tracker coverage.) The period of time during which the satellite is within the tracker coverage is only .63 minutes.

		JOB	OBSERV TEST CASE								
		REM	AS IN DOCUMENTATION								
SPSJOB	OBSERV	30									
250	25									BP	
0333	300000	900000	300							S	
1	00001	U 10	0000	166.8	100	4250		000000	0	10E	
2	00001	38644.00000000	30.0000	254.9999	59.9999	.0009999	9.9999			10E	
3	00001	1.19841762	.0000000000	-.02001	.03912	0000000				10E	
4	UU001	0000000000								10E	
5	00001	5.86986988	0000000000	0000000000						10E	
6	UU001	12015844+4	0000000	31023	200	100	5021921			10E	
1	00002	U 20	0000	0 41.1	200	4245		000000	0	20E	
2	00002	38639.00000000	334.9999	40.0000	44.9999	.69999999	40.0000			20E	
3	UU002	2.42731506	.0000000001	-.31076	.39231	-23567-9				20E	
4	00002	0000000000								20E	
5	00002	3.66666663	-2880464-8	282854-17						20E	
6	00002	59324807+3	-09999-9	642	200	100	41012 4			20E	
1	00003	U 30	0000	0 6.1	300	4240		000000	0	30E	
2	00003	38634.00000000	354.9999	30.0000	35.0000	.0009999	.9999			30E	
3	UU003	16.26752414	.000004304	-8.94240	17.88071	-35249-6				30E	
4	UU003	0000000000								30E	
5	00003	1.03103103	-3637922-6	-734870-11						30E	
6	UU003	88519923+2	-09999-8	191	300	100	40902 3			30E	
1	00004	U 40 58 ALP	1 0000	0 6.3	400	4235		000000	0	40E	
2	00004	38629.00000000	354.9999	30.0000	35.0000	.0009999	40.0000			40E	
3	UU004	15.81261142	.000003953	-6.40843	8.09006	-33305-6				40E	
4	00004	0000000000								40E	
5	00004	1.05105104	-3504045-6	-379921-11						40E	
6	00004	91066551+2	-09999-8	321	400	100	40828 7			40E	
1	00005	U 50 58 BET	2 0000	0 6.5	500	4245		000000	0	50E	
2	00005	38639.00000000	325.0000	59.9999	134.9999	.0009999	30.0000			50E	
3	UU005	15.15600388	.001740700	-6.56358	10.42109	-15298-3				50E	
4	UU005	0000000000								50E	
5	00005	1.08108107	-1655527-3	-5019476-6						50E	
6	UU005	95011852+2	-50000-6	512	500	100	4090714			50E	
1	UU006	U 60	0000	0 6.9	600	4230		000000	0	60E	
2	UU006	38624.00000000	245.0000	74.9999	269.9999	.0200000	79.9999			60E	
3	UU006	14.33633205	.000147327	-1.15575	-2.82611	-13427-4				60E	
4	UU006	0000000000								60E	
5	UU006	1.12244899	-1537982-4	-2945666-8						60E	
6	UU006	10044410+3	-50000-7	658	600	100	4082323			60E	
1	UU007	U 70	0000	0 6.9	700	4230		000000	0	70E	
2	UU007	38624.00000000	245.0000	74.9999	269.9999	.0200000	99.9999			70E	
3	UU007	14.33633205	.000147327	1.15575	-2.82611	-13427-4				70E	
4	UU007	0000000000								70E	
5	UU007	1.12244899	-1537982-4	-2945666-8						70E	
6	UU007	10044410+3	-50000-7	658	700	100	4082323			70E	
ENDOFJOBR											
ENDSCHEDR											

FIGURE 9 Input Data for Test Case (1 of 2)

FANCARDSP
 333 0.0 1.0 .08196411 ORR 0 0 1 0 1 1 45 180 0 RP
 -99.0 1.09 1 2.0 .8662 .8662 70.0 333 FP
 5.0 120.0 240.0 HH FP
 65.0 140.0 65.0 220.0 1P 65.0 220.0 45.0 220.0 2PFP
 45.0 140.0 45.0 220.0 3P 45.0 140.0 25.0 140.0 4PFP
 25.0 140.0 25.0 220.0 5P FP
 AERONUTRONIC DIV. PHILCO CORP. PHILCO FROM 333A
 SPACETRACK R AND D FACILITY 496L SPO ESD AFSC 496LSPO TO 333A
 FIRST AEROSPACE CONTROL SQUADRON ADC ONEAERO INFO 333A
 ONLY 00001-00007
 END CASER
 ENDSCHEDR

FIGURE 9 (2 of 2)

BEGIN SCHED. TAPE

JOB OBSERV TEST CASE
REM AS IN DOCUMENTATION
SPSJ08 OBSERV 30

START OBSERV
01-04-04 04.0

AERONUTRONIC DIV. PHILCO CORP.
SPACETRACK R AND D FACILITY 496L SPO ESD AFSC
FIRST AEROSPACE CONTROL SQUADRON ADC

PHILCO FROM 333A
496LSPO TO 333A
ONEAERO INFO 333A

SAT. SUMMARY FOR STA-333

00001-00007

DECAYING

00000

100 DAYS PAST EPOCH

00000

SAT.NO./SET NO.

00001/0010 00002/0020 00003/0030 00004/0040 00005/0050 00006/0060 00007/0070

*0

RR 496LSPO ONEAERO *0
DE PHILCO 25H 04/0408Z *0

ZNR*

R 040408Z ZEX *0

FM AERONUTRONIC DIV. PHILCO CORP.
TO SPACETRACK R AND D FACILITY 496L SPO ESD AFSC
INFO FIRST AEROSPACE CONTROL SQUADRON ADC

AFGRNQ*

BT

FIGURE 10 Output Data for Test Case (1 of 13)

UNCLAS SPACETRACK 4 0408.80

LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	NO.	DIRECTION COSINES	
								U	V	W
	DAY 250	06/09/64								
00002	212	0030.48	21.1	248.2	0	3.2	T	.010	.866	.500
00002	212	0031.48	21.2	247.7	0	3.1	T	.006	.863	.506
00002	212	0033.48	21.3	246.9	0	3.1	T	-.002	.857	.515
00002	212	0035.48	21.4	246.0	0	3.1	T	-.010	.851	.526
00002	212	0037.48	21.5	245.3	0	3.1	T	-.016	.845	.534
00002	212	0039.48	21.5	244.5	0	3.0	T	-.024	.840	.542
00002	212	0041.48	21.6	243.8	0	3.0	T	-.030	.834	.551
00002	212	0042.03	21.6	243.6	0	3.0	T	-.032	.833	.553
00002	212	0043.48	21.6	243.2	0	3.0	T	-.036	.830	.557
00002	212	0045.48	21.5	242.5	0	2.9	T	-.045	.825	.563
00002	212	0047.48	21.5	241.9	0	2.9	T	-.051	.821	.569
00002	212	0049.48	21.4	241.4	0	2.9	T	-.057	.817	.573
00002	212	0051.48	21.4	240.8	0	2.8	T	-.063	.813	.579
00002	212	0053.48	21.3	240.3	0	2.8	T	-.070	.809	.583
00002	212	0055.48	21.2	239.8	0	2.8	T	-.076	.806	.587
00002	212	0057.48	21.1	239.4	0	2.7	T	-.081	.803	.590
00002	212	0059.48	20.9	238.9	0	2.7	T	-.089	.800	.593
00002	212	0101.48	20.8	238.5	0	2.7	T	-.094	.797	.596
00002	212	0103.48	20.7	238.1	0	2.6	T	-.100	.794	.599
00002	212	0105.48	20.5	237.8	0	2.6	T	-.105	.793	.601
00002	212	0107.48	20.4	237.4	0	2.6	T	-.111	.790	.604
00002	212	0109.48	20.2	237.1	0	2.5	T	-.116	.788	.605
00002	212	0111.48	20.0	236.8	0	2.5	T	-.122	.786	.606
00002	212	0113.48	19.9	236.4	0	2.5	T	-.127	.783	.609
00002	212	0115.48	19.7	236.2	0	2.4	T	-.132	.782	.609
00002	212	0117.48	19.5	235.9	0	2.4	T	-.138	.781	.610
00002	212	0119.48	19.3	235.6	0	2.4	T	-.143	.779	.611
00002	212	0121.48	19.1	235.4	0	2.4	T	-.148	.778	.611
00002	212	0123.48	18.9	235.1	0	2.3	T	-.154	.776	.612
00002	212	0125.48	18.7	234.9	0	2.3	T	-.158	.775	.612
00002	212	0127.48	18.5	234.7	0	2.3	T	-.163	.774	.612
00002	212	0129.48	18.3	234.5	0	2.2	T	-.168	.773	.612
00002	212	0131.48	18.1	234.3	0	2.2	T	-.172	.772	.612
00002	212	0133.48	17.9	234.1	0	2.2	T	-.177	.771	.612
00002	212	0135.48	17.7	234.0	0	2.1	T	-.181	.771	.611
00002	212	0137.48	17.4	233.8	0	2.1	T	-.187	.770	.610
00002	212	0139.48	17.2	233.6	0	2.1	T	-.192	.769	.610
00002	212	0141.48	17.0	233.5	0	2.1	T	-.195	.769	.609
00002	212	0143.48	16.8	233.3	0	2.0	T	-.200	.768	.609
00002	212	0145.48	16.5	233.2	0	2.0	T	-.205	.768	.607
00002	212	0147.48	16.3	233.1	0	2.0	T	-.209	.768	.606
00002	212	0149.48	16.1	233.0	0	1.9	T	-.213	.767	.605
00002	212	0151.48	15.9	232.9	0	1.9	T	-.217	.767	.604
00002	212	0153.48	15.6	232.8	0	1.9	T	-.222	.767	.602
00002	212	0155.48	15.4	232.7	0	1.9	T	-.225	.767	.601
00002	212	0157.48	15.1	232.6	0	1.8	T	-.230	.767	.599
00002	212	0159.48	14.9	232.5	0	1.8	T	-.234	.767	.598
00002	212	0201.48	14.7	232.4	0	1.8	T	-.238	.766	.597
00002	212	0203.48	14.4	232.3	0	1.8	T	-.243	.766	.595

FIGURE 10 (2 of 13)

UNCLAS SPACETRACK 4 0408.80
LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES		
DAY		06/09/64					NO.	U	V	W
00002	212	0205.48	14.2	232.2	0	1.7	T	.247	.766	.594
00002	212	0207.48	13.9	232.2	0	1.7	T	.251	.767	.591
00002	212	0209.48	13.7	232.1	0	1.7	T	.255	.767	.589
00002	212	0211.48	13.5	232.0	0	1.6	T	.258	.766	.588
00002	212	0213.48	13.2	232.0	0	1.6	T	.262	.767	.585
00002	212	0215.48	13.0	231.9	0	1.6	T	.266	.767	.584
00002	212	0217.48	12.7	231.9	0	1.6	T	.270	.768	.581
00002	212	0219.48	12.5	231.8	0	1.5	T	.274	.767	.580
00002	212	0221.48	12.2	231.8	0	1.5	T	.278	.768	.577
00002	212	0223.48	12.0	231.7	0	1.5	T	.282	.768	.576
00002	212	0225.48	11.7	231.7	0	1.5	T	.286	.768	.573
00002	212	0227.48	11.5	231.7	0	1.4	T	.288	.769	.570
00002	212	0229.48	11.3	231.6	0	1.4	T	.292	.769	.569
00002	212	0231.48	11.0	231.6	0	1.4	T	.296	.769	.566
00002	212	0233.48	10.8	231.6	0	1.4	T	.299	.770	.564
00002	212	0235.48	10.5	231.5	0	1.3	T	.304	.770	.562
00002	212	0237.48	10.3	231.5	0	1.3	T	.307	.770	.560
00002	212	0239.48	10.0	231.5	0	1.3	T	.311	.771	.556
00002	212	0241.48	9.8	231.5	0	1.3	T	.313	.771	.554
00002	212	0243.48	9.5	231.5	0	1.3	T	.317	.772	.551
00002	212	0245.48	9.3	231.5	0	1.2	T	.320	.772	.549
00002	212	0247.48	9.0	231.4	0	1.2	T	.325	.772	.546
00002	212	0249.48	8.8	231.4	0	1.2	T	.328	.772	.544
00002	212	0251.48	8.5	231.4	0	1.2	T	.332	.773	.541
00002	212	0253.48	8.3	231.4	0	1.1	T	.334	.773	.539
00002	212	0255.48	8.0	231.4	0	1.1	T	.338	.774	.535
00002	212	0257.48	7.8	231.4	0	1.1	T	.341	.774	.533
00002	212	0259.48	7.5	231.4	0	1.1	T	.345	.775	.530
00002	212	0301.48	7.3	231.4	0	1.0	T	.348	.775	.527
00002	212	0303.48	7.0	231.4	0	1.0	T	.352	.776	.524
00002	212	0305.48	6.8	231.4	0	1.0	T	.354	.776	.522
00002	212	0307.48	6.5	231.4	0	1.0	T	.358	.776	.518
00002	212	0309.48	6.3	231.4	0	1.0	T	.361	.777	.516
00002	212	0311.48	6.0	231.4	0	.9	T	.365	.777	.513
00002	212	0313.48	5.8	231.4	0	.9	T	.367	.778	.510
00002	212	0315.48	5.5	231.4	0	.9	T	.371	.778	.507
00002	212	0317.48	5.3	231.4	0	.9	T	.374	.778	.505
00002	212	0319.48	5.0	231.4	0	.8	T	.378	.779	.501
00002	212	0320.16	5.0	231.4	0	.8	H	.378	.779	.501
00002	212	0321.48	4.8	231.4	0	.8	T	.380	.779	.499
00002	212	0323.48	4.5	231.4	0	.8	T	.384	.779	.495
00002	212	0325.48	4.3	231.4	0	.8	T	.387	.779	.493
00002	212	0327.48	4.1	231.4	0	.7	T	.389	.780	.491
00002	212	0329.48	3.8	231.4	0	.7	T	.393	.780	.487
00002	212	0331.48	3.6	231.4	0	.7	T	.396	.780	.485

BT

FIGURE 10 (3 of 13)

*0

RR 496L SPO ONEAERO *0
DE PHILCO 26H 04/0408Z**0

ZNR*

R 040408Z ZEX *0

FM AERONUTRONIC DIV. PHILCO CORP.
TO SPACETRACK R AND D FACILITY 496L SPO ESD AFSC
INFO FIRST AEROSPACE CONTROL SQUADRON ADC

AFGRNC*

BT

UNCLAS SPACETRACK 4 0408.80

LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTHI	RANGE	R-RATE	FAN	DIRECTION	COSINES	
					(KM)		NO.	U	V	W
	DAY 250	06/09/64								
00002	212	0333.48	3.3	231.4	0	,7	T	-.400	.780	.481
00002	212	0335.48	3.1	231.4	0	,7	T	-.402	.780	.479
00002	212	0337.48	2.8	231.4	0	,6	T	-.406	.781	.475
00002	212	0339.48	2.6	231.4	0	,6	T	-.409	.781	.473
00002	212	0341.48	2.3	231.5	0	,6	T	-.411	.782	.468
00002	212	0343.48	2.1	231.5	0	,6	T	-.414	.782	.466
00002	212	0345.48	1.8	231.5	0	,6	T	-.418	.782	.462
00002	212	0347.48	1.6	231.5	0	,5	T	-.420	.782	.460
00002	212	0349.48	1.4	231.5	0	,5	T	-.423	.782	.457
00002	212	0351.48	1.1	231.5	0	,5	T	-.427	.782	.454
00002	212	0352.66	1.0	231.5	0	,5	T	-.428	.782	.452
00002	987	0037.00	11.2	93.4	2091	-,3	*♦	,096	-,979	,178
00007	987	0039.07	8.8	118.8	2232	2.5	T	-,228	-,866	,445
00007	987	0040.51	5.1	133.0	2512	3.9	T	-,417	-,728	,543
00007	987	0040.56	5.0	133.4	2522	3.9	H	-,422	-,724	,546
00007	987	0041.96	1.0	143.8	2894	4.8	T	-,558	-,591	,583
00007	988	0216.22	51.1	298.0	897	-,9	T	-,759	,554	,342
00007	988	0216.43	51.5	288.2	890	,2	*♦	,691	,591	,416
00007	988	0217.52	42.2	245.9	998	3.3	T	,261	,676	,689
00007	988	0219.52	19.5	218.9	1593	6.0	T	-,283	,592	,755
00007	988	0221.52	6.7	210.9	2360	6.6	T	-,520	,510	,685
00007	988	0221.88	5.0	210.0	2505	6.7	H	-,548	,498	,672
00007	988	0222.82	1.0	208.2	2884	6.8	T	-,611	,472	,635
00004	639	0342.48	1.0	187.1	1963	-,5.1	T	-,689	,124	,714
00004	639	0342.70	1.6	185.1	1897	-,4.9	T	-,684	,089	,724
00004	639	0343.88	5.0	171.5	1588	-,3.6	H	-,635	-,147	,758
00004	639	0344.70	7.0	159.2	1440	-,2.3	T	-,570	-,352	,742
00004	639	0345.80	8.1	139.4	1362	,0	*♦	-,432	-,644	,631
00004	639	0346.70	7.3	123.0	1416	1.9	T	-,292	-,832	,472
00004	639	0346.92	6.9	119.3	1444	2.4	T	-,259	-,866	,428
00007	989	0354.18	2.2	304.0	2929	-,3	*♦	,422	,828	-,368
00004	640	0516.56	1.0	240.0	1967	-,7.0	T	-,341	,866	,366
00004	640	0517.11	3.3	240.0	1736	-,7.0	T	-,312	,865	,394
00004	640	0519.11	17.4	240.3	911	-,6.6	T	-,123	,829	,546
00004	640	0521.01	84.0	243.0	331	-,7	*♦	,670	,093	,737
00004	640	0521.11	88.3	51.2	329	,2	T	,720	-,023	,694
00004	640	0521.66	52.1	60.2	411	4.3	T	,774	-,533	,342
00004	641	0656.99	16.6	344.9	940	,0	*♦	,856	,250	-,452
00004	642	0833.35	10.7	1.4	1199	,0	*♦	,826	-,024	-,563

FIGURE 10 (4 of 13)

UNCLAS SPACETRACK 4 0408.80
LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE	R-RATE	FAN	DIRECTION COSINES		
DAY					(KM)		NO.	U	V	W
00002	213	0851.93	1.0	197.8	8065	-6.2	T	.661	.306	.685
00002	213	0852.10	1.1	197.6	8000	-6.2	T	.660	.302	.687
00002	213	0854.10	2.5	194.3	7248	-6.3	T	.654	.247	.715
00002	213	0856.10	3.9	190.2	6489	-6.3	T	.646	.177	.742
00002	213	0857.55	5.0	186.6	5941	-6.3	H	.638	.115	.761
00002	213	0858.10	5.4	185.0	5735	-6.2	T	.635	.087	.768
00002	213	0900.10	6.7	178.1	5002	-5.9	T	.619	.033	.784
00002	213	0902.10	7.6	168.9	4322	-5.3	T	.594	.191	.781
00002	213	0903.33	7.9	161.6	3952	-4.7	**	.567	.313	.762
00002	213	0904.10	7.8	156.4	3749	-4.1	T	.546	.397	.738
00002	213	0906.10	6.2	140.2	3365	-2.1	T	.464	.636	.616
00002	213	0906.93	5.0	132.6	3284	-1.1	H	.415	.733	.538
00002	213	0908.10	2.5	121.6	3262	.5	T	.339	.851	.401
00002	213	0908.27	2.1	119.9	3269	.7	T	.326	.866	.378
00006	892	0957.33	1.0	164.7	3389	-6.0	T	.670	.264	.694
00006	892	0957.40	1.3	164.5	3363	-6.0	T	.665	.267	.697
00006	892	0958.42	5.0	161.7	3001	-5.8	H	.607	.313	.730
00006	892	0959.40	9.0	158.2	2663	-5.6	T	.538	.367	.759
00006	892	1001.40	18.9	147.1	2027	-4.8	T	.333	.514	.791
00006	892	1003.40	30.9	124.6	1551	-2.8	T	.019	.706	.708
00006	892	1005.03	36.3	92.6	1407	.0	**	.393	.805	.444
00006	892	1005.40	35.9	84.4	1416	.7	T	.471	.806	.359
00006	892	1005.48	35.8	82.9	1419	.9	T	.485	.805	.343
00004	643	1009.67	19.6	17.8	828	-0	**	.871	.288	.397
00003	582	1045.95	1.0	213.7	2496	-5.7	T	.576	.555	.601
00003	582	1047.14	5.0	206.5	2104	-5.2	H	.569	.444	.692
00005	582	1047.58	6.6	203.1	1969	-5.0	T	.565	.390	.727
00003	582	1049.58	14.0	179.8	1482	-2.8	T	.515	.003	.857
00005	582	1051.07	16.7	153.5	1351	.0	**	.403	.427	.809
00003	582	1051.58	16.4	143.7	1368	1.1	T	.347	.568	.746
00003	582	1053.22	11.7	117.8	1616	3.8	T	.180	.866	.466
00006	893	1139.13	1.0	220.2	3405	-5.5	T	.528	.645	.532
00006	893	1139.24	1.3	220.6	3370	-5.5	T	.521	.651	.553
00006	893	1140.34	5.0	225.0	3011	-5.3	H	.436	.704	.560
00006	893	1141.24	8.2	229.4	2733	-5.0	T	.355	.751	.556
00006	893	1143.24	16.1	243.6	2190	-3.9	T	.106	.861	.498
00006	893	1143.34	16.5	244.6	2165	-3.8	T	.090	.866	.492
00006	893	1146.49	25.0	285.5	1762	.0	**	.470	.873	.128
00004	644	1144.51	33.2	274.3	558	-5.2	T	.432	.834	.343
00004	644	1145.19	52.3	240.4	400	-2.1	T	.346	.532	.773
00004	644	1145.38	55.7	220.1	384	-6	2	.279	.363	.889
00004	644	1145.47	55.9	210.1	383	.1	**	.243	.281	.928
00004	644	1145.71	52.5	183.8	399	2.0	3	.131	.040	.990
00004	644	1146.74	25.8	142.6	672	5.9	5	.198	.547	.814
00004	644	1147.19	19.0	137.6	839	6.4	T	.264	.638	.724
00004	644	1148.97	5.0	129.9	1560	6.9	H	.390	.764	.513
00004	644	1149.19	3.9	129.4	1649	6.9	T	.400	.771	.496
00004	644	1149.86	1.0	128.4	1931	7.0	T	.427	.784	.451
00002	993	1147.56	15.9	63.6	2209	.0	**	.496	.861	.109

FIGURE 10 (5 of 13)

UNCLAS SPACETRACK 4 0408.80

LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES			
BAY	250	06/09/64						NO.	U	V	W
00005	583	1227.26	9.5	241.4	1759	-6.4	T	.217	.866	.451	
00005	583	1228.14	15.2	238.0	1427	-6.1	T	.176	.818	.547	
00005	583	1230.14	38.6	214.6	779	-4.0	T	.014	.444	.896	
00005	583	1231.15	52.0	168.9	636	-3	3	.130	.119	.984	
00005	583	1231.22	52.1	164.5	635	0	0	.139	.164	.977	
00005	583	1232.14	41.5	119.2	740	3.5	T	.210	.654	.727	
BT											

FIGURE 10 (6 of 13)

*0

RR 496LSPD ONEAERO *0
DE PHILCO 27H 04/0408Z*00

ZNR*

R 040408Z ZEX *0

FM AERONUTRONIC DIV. PHILCO CORP.
TO SPACETRACK R AND D FACILITY 496L SPO ESD AFSC
INFO FIRST AEROSPACE CONTROL SQUADRON ADC

AFGRMC*

BT

UNCLAS SPACETRACK 4 0408.80

LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTHI	RANGE (KM)	R-RATE	FAN	NO.	U	V	W	DIRECTION COSINES
DAY	250	06/09/64										
00005	583	1233.02	27.9	101.3	979	5.2	T	.208	-.867	.453		
00007	994	1318.05	1.0	173.1	3391	-6.4	T	-.690	-.120	.714		
00007	994	1318.52	2.7	173.7	3211	-6.4	T	-.669	-.110	.735		
00007	994	1319.08	5.0	174.4	2993	-6.4	H	-.639	-.097	.763		
00007	994	1320.52	11.8	176.8	2451	-6.2	T	-.546	-.055	.836		
00007	994	1322.52	25.4	183.1	1736	-5.6	T	-.335	.049	.941		
00007	994	1323.13	31.2	186.6	1539	-5.2	T	-.235	.098	.967		
00007	994	1324.52	48.6	202.8	1170	-3.4	T	.099	.256	.961		
00007	994	1324.60	49.9	204.6	1153	-3.3	T	.127	.268	.955		
00007	994	1325.15	57.6	219.9	1064	-2.1	T	.306	.344	.888		
00002	994	1325.90	63.3	255.6	1015	-0	*	.553	.435	.711		
00007	994	1326.52	59.8	287.0	1045	1.6	T	.715	.481	.507		
00002	994	1326.99	53.7	303.1	1107	2.7	T	.798	.496	.341		
00004	645	1319.45	3.4	240.2	1702	-2.1	T	-.309	.866	.393		
00004	645	1320.63	4.2	222.3	1623	-0	*	-.470	.671	.573		
00004	645	1321.27	4.0	212.4	1645	1.1	T	-.546	.534	.645		
00004	646	1323.09	1.0	188.2	1929	3.8	T	-.687	.143	.712		
00008	584	1409.81	29.9	267.9	934	-5.7	T	.330	.866	.375		
00005	584	1411.63	87.1	286.6	514	-3	T	.716	.048	.696		
00005	584	1411.71	88.6	43.8	513	.1	*	.719	-.017	.694		
00005	584	1413.46	31.8	87.1	894	5.6	T	.403	.7849	.342		
00007	995	1505.63	4.2	269.2	3109	-0	*	.042	.997	.062		
00005	585	1550.38	29.9	268.0	932	-5.6	T	.331	.866	.374		
00008	585	1550.52	32.1	267.0	887	-5.5	T	.344	.846	.407		
00005	585	1552.21	70.6	191.0	541	-0	*	.436	.063	.898		
00005	585	1552.28	70.4	181.7	541	.3	T	.429	.010	.903		
00005	585	1552.52	66.4	155.0	555	1.5	T	.391	-.169	.905		
00005	585	1554.52	23.5	111.4	1096	6.0	T	.045	-.854	.519		
00005	585	1554.65	22.0	110.9	1145	6.1	T	.031	-.866	.499		
00005	586	1730.54	17.8	245.5	1302	-4.3	T	-.063	.866	.495		
00008	586	1732.27	26.0	208.8	1024	-6	T	-.247	.433	.867		
00008	586	1732.49	26.2	202.8	1020	-0	*	-.273	.348	.897		
00005	586	1734.27	18.9	162.9	1257	4.0	T	-.410	-.278	.868		
00005	586	1736.27	7.9	142.0	1863	5.7	T	-.455	-.610	.649		
00005	586	1736.94	5.0	138.0	2101	6.0	H	-.462	-.667	.585		
00005	586	1738.00	1.0	133.5	2487	6.2	T	-.474	-.725	.499		
00005	587	1909.89	2.8	240.2	2308	-3.0	T	-.316	.867	.386		
00005	587	1910.88	4.4	230.0	2156	-2.0	T	-.399	.764	.507		
00005	587	1911.46	5.0	223.5	2099	-1.3	H	-.449	.686	.573		

FIGURE 10 (7 of 13)

UNCLAS SPACETRACK 4 0408.80
LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES
							NO.	U V W
	DAY 250	06/09/64						
00002	587	1912.39	5.5	212.4	2059	.1	++	.527 .533 .662
00002	587	1912.88	5.4	206.5	2067	.6	T	.563 .444 .697
00002	587	1913.49	5.0	199.4	2102	1.3	H	.603 .331 .726
00002	587	1914.88	3.0	184.5	2284	2.9	T	.667 .078 .741
00002	587	1915.87	1.0	175.7	2484	3.8	T	.693 .075 .717
00002	214	1926.27	43.9	286.9	4394	.6	T	.638 .689 .342
00002	214	1926.49	45.1	286.3	4404	.8	T	.641 .677 .361
00002	214	1928.49	55.5	280.3	4566	1.9	T	.654 .557 .511
00002	214	1930.49	64.2	271.2	4844	2.7	T	.643 .435 .630
00002	214	1932.49	70.8	257.3	5210	3.3	T	.617 .321 .719
00002	214	1934.49	74.8	237.2	5640	3.8	T	.582 .220 .783
00002	214	1936.47	76.0	214.1	6107	4.1	++	.544 .136 .828
00002	214	1936.49	76.0	213.9	6112	4.1	T	.544 .135 .828
00002	214	1938.49	75.1	194.0	6613	4.2	T	.507 .062 .860
00002	214	1940.49	73.0	180.2	7131	4.4	T	.469 .001 .883
00002	214	1942.49	70.7	171.2	7659	4.4	T	.436 .051 .898
00002	214	1943.03	70.0	169.4	7803	4.4	1	.427 .063 .902
00002	214	1944.49	68.3	165.3	8192	4.4	T	.404 .094 .910
00002	214	1946.49	66.1	161.2	8724	4.4	T	.375 .131 .918
00002	214	1948.49	64.0	158.3	9255	4.4	T	.348 .162 .924
00002	214	1950.49	62.1	156.1	9782	4.4	T	.322 .190 .927
00002	214	1952.49	60.4	154.5	10303	4.3	T	.300 .213 .930
00002	214	1954.49	58.8	153.3	10818	4.3	T	.278 .233 .932
00002	214	1956.49	57.3	152.4	11326	4.2	T	.257 .250 .934
00002	214	1958.49	56.0	151.6	11827	4.1	T	.238 .266 .934
00002	214	2000.49	54.8	151.1	12321	4.1	T	.221 .279 .935
00002	214	2002.49	53.6	150.7	12806	4.0	T	.203 .290 .935
00002	214	2004.49	52.6	150.3	13284	3.9	T	.189 .301 .935
00002	214	2006.49	51.6	150.1	13754	3.9	T	.173 .310 .935
00002	214	2008.49	50.6	149.9	14216	3.8	T	.158 .318 .935
00002	214	2010.49	49.8	149.8	14671	3.7	T	.146 .325 .935
00002	214	2012.49	49.0	149.8	15118	3.7	T	.133 .330 .935
00002	214	2013.97	48.4	149.7	15443	3.6	3	.123 .335 .934
00002	214	2014.49	48.2	149.7	15557	3.6	T	.120 .336 .934
00002	214	2016.49	47.5	149.8	15989	3.6	T	.108 .340 .934
00002	214	2018.49	46.8	149.8	0	3.5	T	.097 .344 .934
00002	214	2020.49	46.2	149.9	0	3.4	T	.087 .347 .934
00002	214	2022.49	45.6	150.0	0	3.4	T	.077 .350 .934
00002	214	2024.49	45.0	150.1	0	3.3	T	.067 .352 .933
00002	214	2026.49	44.5	150.2	0	3.3	T	.058 .354 .933
00002	214	2028.49	44.0	150.4	0	3.2	T	.049 .355 .933
00002	214	2030.49	43.5	150.5	0	3.2	T	.040 .357 .933
00002	214	2032.49	43.0	150.7	0	3.1	T	.031 .358 .933
00002	214	2034.49	42.5	150.9	0	3.1	T	.022 .359 .933
00002	214	2036.49	42.1	151.1	0	3.0	T	.015 .359 .933
00002	214	2038.49	41.7	151.3	0	3.0	T	.007 .359 .933
00002	214	2040.49	41.3	151.5	0	2.9	T	.000 .358 .934
00002	214	2042.49	40.9	151.8	0	2.9	T	.008 .357 .934
00002	214	2044.49	40.6	152.0	0	2.8	T	.014 .356 .934

FIGURE 10 (8 of 13)

UNCLAS SPACETRACK 4 0408.80
 LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTHI	RANGE	R-RATE	FAN	DIRECTION COSINES		
					(KM)		NO.	U	V	W
DAY	250	06/09/64								
00002	214	2046.49	40.2	152.2	0	2.8	T	-.021	-.356	.934
00002	214	2048.49	39.9	152.5	0	2.7	T	-.028	-.354	.935
00002	214	2050.49	39.6	152.7	0	2.7	T	-.033	-.353	.935
00002	214	2052.49	39.2	153.0	0	2.6	T	-.041	-.352	.935
00002	214	2054.49	38.9	153.2	0	2.6	T	-.047	-.351	.935
00002	214	2056.49	38.6	153.5	0	2.6	T	-.053	-.349	.936
BT										

FIGURE 10 (9 of 13)

♦0

RR 496LSPO ONEAERO ♦0
 DE PHILCO 28H 04/0408Z♦0

ZNR♦

R 040408Z ZEX ♦0

FM AERONUTRONIC DIV. PHILCO CORP.
 TO SPACETRACK R AND D FACILITY 496L SPO ESD AFSC
 INFO FIRST AEROSPACE CONTROL SQUADRON ADC

AFGRNC♦

BT

UNCLAS SPACETRACK 4 0408.80

LOOM ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTHI	RANGE	R-RATE	FAN	NO.	U	V	W	DIRECTION COSINES
					(KM)							
	DAY 250	06/09/64										
00002	214	2058.49	38.4	153.7	0	2.5	T	-.058	-.347	.936		
00002	214	2100.49	38.1	154.0	0	2.5	T	-.064	-.345	.936		
00002	214	2102.49	37.8	154.3	0	2.4	T	-.070	-.343	.937		
00002	214	2104.49	37.6	154.6	0	2.4	T	-.075	-.340	.938		
00002	214	2106.49	37.3	154.8	0	2.4	T	-.080	-.339	.937		
00002	214	2108.49	37.1	155.1	0	2.3	T	-.085	-.336	.938		
00002	214	2110.49	36.8	155.4	0	2.3	T	-.091	-.333	.938		
00002	214	2112.49	36.6	155.7	0	2.3	T	-.096	-.330	.939		
00002	214	2114.49	36.4	155.9	0	2.2	T	-.100	-.329	.939		
00002	214	2116.49	36.1	156.2	0	2.2	T	-.106	-.326	.939		
00002	214	2118.49	35.9	156.5	0	2.1	T	-.111	-.323	.940		
00002	214	2120.49	35.7	156.8	0	2.1	T	-.115	-.320	.940		
00002	214	2122.49	35.5	157.1	0	2.1	T	-.120	-.317	.941		
00002	214	2124.49	35.3	157.4	0	2.0	T	-.124	-.314	.941		
00002	214	2126.49	35.1	157.7	0	2.0	T	-.129	-.310	.942		
00002	214	2128.49	34.9	158.0	0	2.0	T	-.133	-.307	.942		
00002	214	2130.49	34.7	158.3	0	1.9	T	-.138	-.304	.943		
00002	214	2132.49	34.5	158.6	0	1.9	T	-.142	-.301	.943		
00002	214	2134.49	34.4	158.9	0	1.9	T	-.145	-.297	.944		
00002	214	2136.49	34.2	159.1	0	1.9	T	-.149	-.295	.944		
00002	214	2138.49	34.0	159.4	0	1.8	T	-.153	-.292	.944		
00002	214	2140.49	33.8	159.7	0	1.8	T	-.158	-.288	.944		
00002	214	2142.49	33.7	160.0	0	1.8	T	-.160	-.285	.945		
00002	214	2144.49	33.5	160.3	0	1.7	T	-.165	-.281	.945		
00002	214	2146.49	33.3	160.6	0	1.7	T	-.169	-.278	.946		
00002	214	2148.49	33.2	160.9	0	1.7	T	-.172	-.274	.946		
00002	214	2150.49	33.0	161.2	0	1.6	T	-.176	-.270	.947		
00002	214	2152.49	32.8	161.5	0	1.6	T	-.181	-.267	.947		
00002	214	2154.49	32.7	161.8	0	1.6	T	-.183	-.263	.947		
00002	214	2156.49	32.5	162.1	0	1.6	T	-.188	-.259	.947		
00002	214	2158.49	32.4	162.4	0	1.5	T	-.190	-.255	.948		
00002	214	2200.49	32.2	162.7	0	1.5	T	-.194	-.252	.948		
00002	214	2202.49	32.1	163.0	0	1.5	T	-.197	-.248	.949		
00002	214	2204.49	31.9	163.3	0	1.5	T	-.201	-.244	.949		
00002	214	2206.49	31.8	163.6	0	1.4	T	-.204	-.240	.949		
00002	214	2208.49	31.6	163.9	0	1.4	T	-.208	-.236	.949		
00002	214	2210.49	31.5	164.2	0	1.4	T	-.211	-.232	.950		
00002	214	2212.49	31.3	164.5	0	1.3	T	-.215	-.228	.950		
00002	214	2214.49	31.2	164.8	0	1.3	T	-.217	-.224	.950		

FIGURE 10 (10 of 13)

UNCLAS SPACETRACK 4 0408.80
 LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES
DAY		06/09/64					NO.	U V W
00002	214	2216.49	31.0	165.1	0	1.3	T	- .222 - .220 .950
00002	214	2218.49	30.9	165.3	0	1.3	T	- .224 - .218 .950
00002	214	2220.49	30.7	165.6	0	1.2	T	- .228 - .214 .950
00002	214	2222.49	30.6	165.9	0	1.2	T	- .230 - .210 .950
00002	214	2222.72	30.6	166.0	0	1.2	3	- .231 - .208 .951
00002	214	2224.49	30.4	166.2	0	1.2	T	- .234 - .206 .950
00002	214	2226.49	30.3	166.5	0	1.2	T	- .237 - .202 .950
00002	214	2228.49	30.2	166.8	0	1.1	T	- .239 - .197 .951
00002	214	2230.49	30.0	167.1	0	1.1	T	- .243 - .193 .950
00002	214	2232.49	29.9	167.4	0	1.1	T	- .246 - .189 .951
00002	214	2234.49	29.7	167.7	0	1.1	T	- .250 - .185 .950
00002	214	2236.49	29.6	167.9	0	1.1	T	- .252 - .182 .950
00002	214	2238.49	29.5	168.2	0	1.0	T	- .254 - .178 .951
00002	214	2240.49	29.3	168.5	0	1.0	T	- .258 - .174 .950
00002	214	2242.49	29.2	168.8	0	1.0	T	- .261 - .170 .950
00002	214	2244.49	29.0	169.1	0	1.0	T	- .264 - .165 .950
00002	214	2246.49	28.9	169.3	0	.9	T	- .267 - .163 .950
00002	214	2248.49	28.8	169.6	0	.9	T	- .269 - .158 .950
00002	214	2250.49	28.6	169.9	0	.9	T	- .273 - .154 .950
00002	214	2252.49	28.5	170.2	0	.9	T	- .275 - .150 .950
00002	214	2254.49	28.3	170.5	0	.8	T	- .279 - .145 .949
00002	214	2256.49	28.2	170.7	0	.8	T	- .281 - .142 .949
00002	214	2258.49	28.1	171.0	0	.8	T	- .283 - .138 .949
00002	214	2300.49	27.9	171.3	0	.8	T	- .287 - .134 .949
00002	214	2302.49	27.8	171.5	0	.8	T	- .289 - .131 .948
00002	214	2304.49	27.6	171.8	0	.7	T	- .293 - .126 .948
00002	214	2306.49	27.5	172.1	0	.7	T	- .295 - .122 .948
00002	214	2308.49	27.4	172.3	0	.7	T	- .297 - .119 .948
00002	214	2310.49	27.2	172.6	0	.7	T	- .300 - .115 .947
00002	214	2312.49	27.1	172.9	0	.6	T	- .303 - .110 .947
00002	214	2314.49	26.9	173.1	0	.6	T	- .306 - .107 .946
00002	214	2316.49	26.8	173.4	0	.6	T	- .308 - .103 .946
00002	214	2318.49	26.6	173.6	0	.6	T	- .312 - .100 .945
00002	214	2320.49	26.5	173.9	0	.6	T	- .314 - .095 .945
00002	214	2322.49	26.4	174.2	0	.5	T	- .316 - .091 .945
00002	214	2324.49	26.2	174.4	0	.5	T	- .319 - .088 .944
00002	214	2326.49	26.1	174.7	0	.5	T	- .321 - .083 .943
00002	214	2328.49	25.9	174.9	0	.5	T	- .325 - .080 .942
00002	214	2330.49	25.8	175.2	0	.5	T	- .327 - .075 .942
00002	214	2332.49	25.6	175.4	0	.4	T	- .330 - .072 .941
00002	214	2334.49	25.5	175.7	0	.4	T	- .332 - .068 .941
00002	214	2336.49	25.3	175.9	0	.4	T	- .335 - .065 .940
00002	214	2338.49	25.2	176.1	0	.4	T	- .337 - .062 .939
00002	214	2340.49	25.0	176.4	0	.4	T	- .341 - .057 .938
00002	214	2342.49	24.9	176.6	0	.3	T	- .343 - .054 .938
00002	214	2344.49	24.7	176.9	0	.3	T	- .346 - .049 .937
00002	214	2346.49	24.6	177.1	0	.3	T	- .348 - .046 .936
00002	214	2348.49	24.4	177.3	0	.3	T	- .351 - .043 .935
00002	214	2350.49	24.3	177.6	0	.2	T	- .353 - .038 .935

FIGURE 10 (11 of 13)

UNCLAS SPACETRACK 4 0408.80
 LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTH	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES		
DAY						NO.	U	V	W	
00002	214	2352.49	24.1	177.8	0	.2	T	-.356	-.035	.934
00002	214	2354.49	24.0	178.0	0	.2	T	-.358	-.032	.933
00002	214	2356.49	23.8	178.2	0	.2	T	-.361	-.029	.932
00002	214	2358.49	23.7	178.5	0	.2	T	-.363	-.024	.931
00006	899	2040.63	13.3	69.9	1979	.2	**	.399	.914	-.074
00006	899	2045.37	2.9	119.8	2726	4.7	T	-.315	-.867	.387
										BT

FIGURE 10 (12 of 13)

♦0

RR 496LSPO ONEAERO ♦0
 DE PHILCO 29H 04/0408Z♦0

ZNR♦

R 040408Z ZEX ♦0

FM AERONUTRONIC DIV. PHILCO CORP.

TO SPACETRACK R AND D FACILITY 496L SPO ESD AFSC

INFO FIRST AEROSPACE CONTROL SQUADRON ADG

AFGRNO♦

BT

UNCLAS SPACETRACK 4 0408.80

LOOK ANGLE SCHEDULE FOR OBSERV TEST SENS

SAT	REV	TIME	ELEV	AZMTHI	RANGE (KM)	R-RATE	FAN	DIRECTION COSINES
DAY	250	06/09/64						
00006	899	2045.68	1.9	121.9	2817	4.9	T	.350 -.849 .397
00006	899	2046.00	1.0	123.8	2910	5.0	T	.381 -.831 .406
00006	900	2221.88	42.1	284.7	1005	-1.8	T	.607 .718 .341
00006	900	2222.41	43.8	266.1	973	-2.1	**	.455 .720 .524
00006	900	2223.37	38.7	234.4	1045	-2.6	T	.121 .635 .763
00006	900	2224.51	27.3	212.2	1302	-4.7	5	.207 .474 .856
00006	900	2225.37	19.7	203.2	1570	-5.5	T	.374 .371 .850
00006	900	2227.37	7.3	192.6	2295	-6.4	T	.595 .216 .774
00006	900	2227.88	5.0	191.0	2492	-6.4	H	.630 .190 .753
00006	900	2228.86	1.0	188.6	2874	-6.6	T	.687 .150 .711

NO MORE DATA

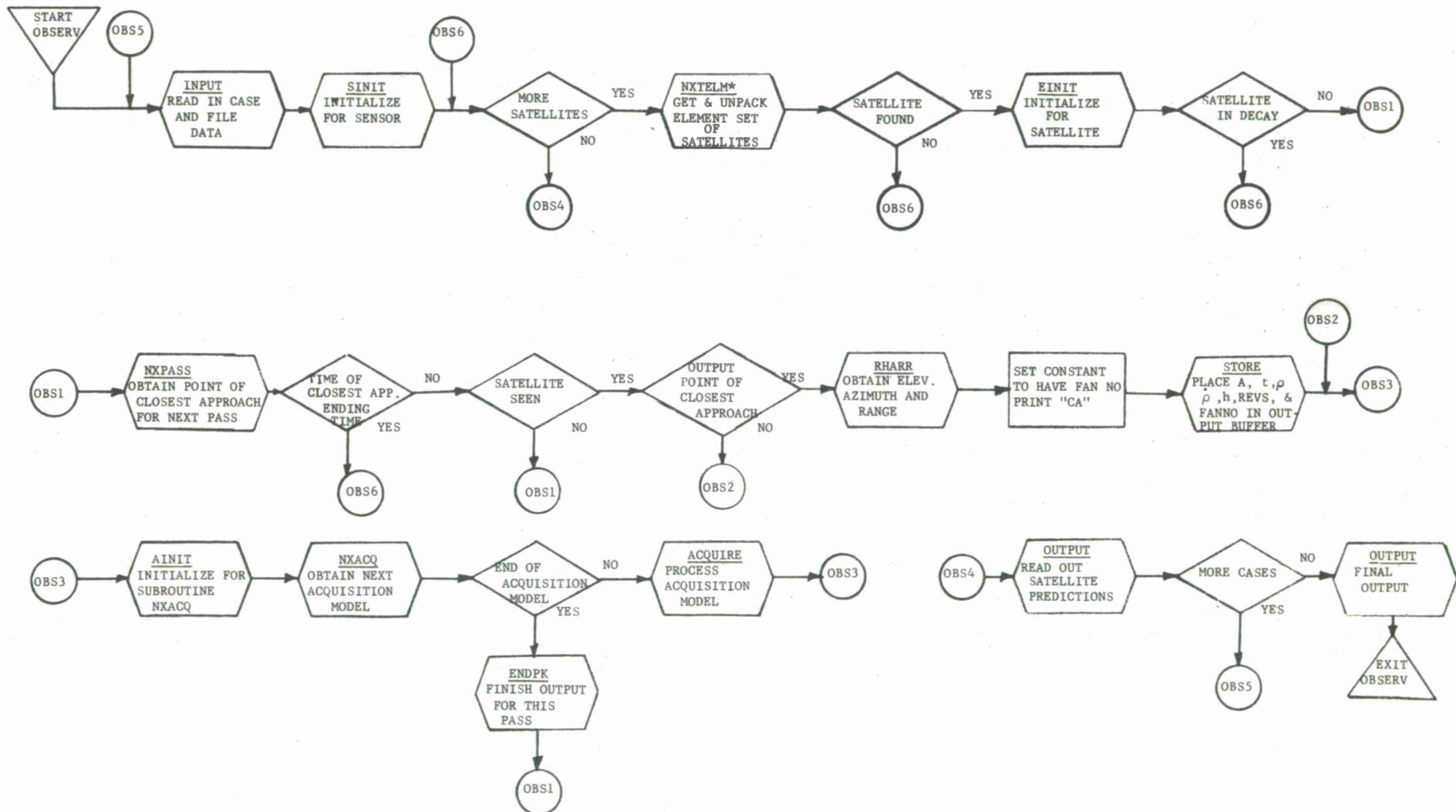
BT

FIGURE 10 (13 of 13)

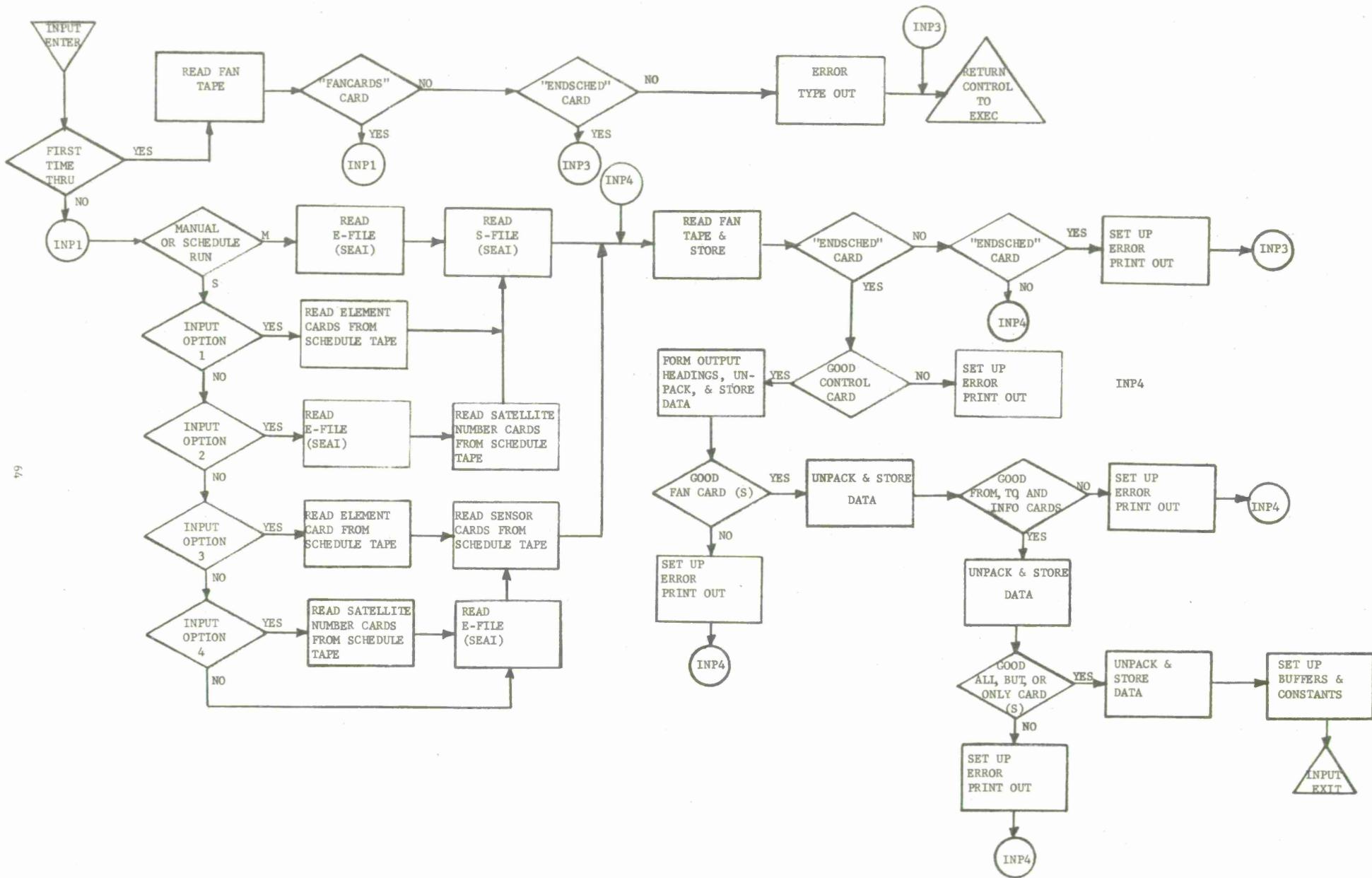
SECTION 6

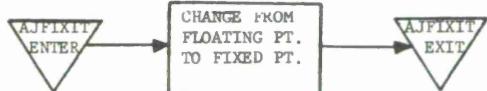
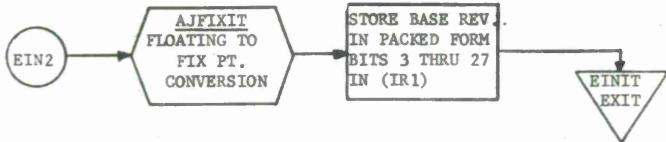
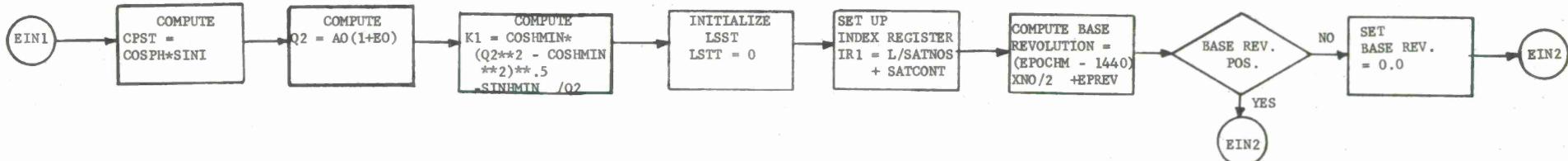
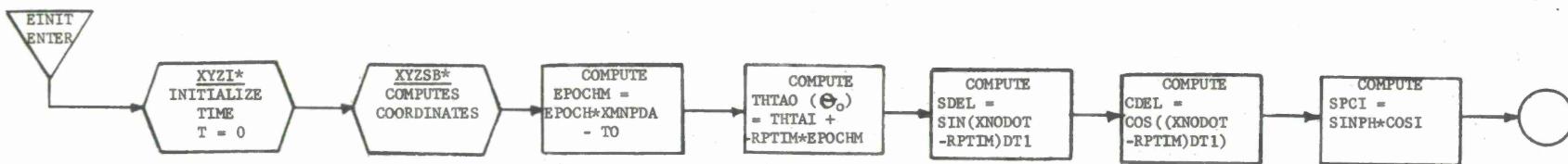
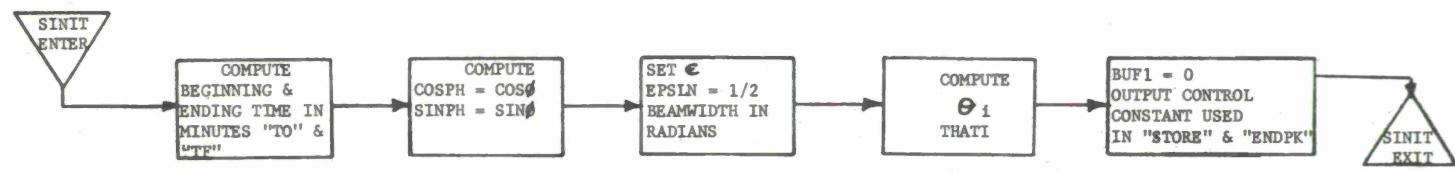
FLOW DIAGRAMS

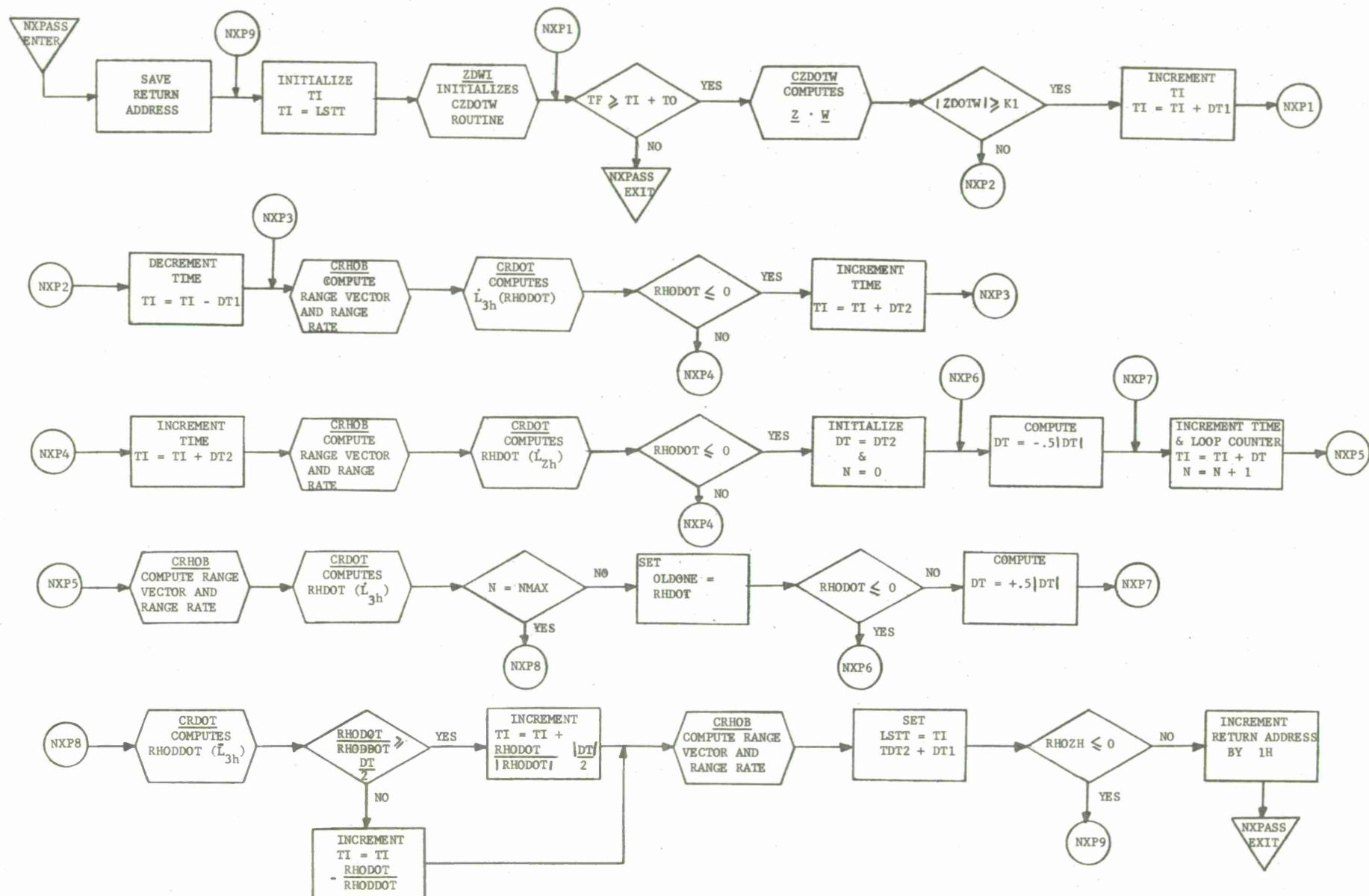
The following flow diagram displays the logical flow and computational procedures used in the program. Standard symbols are maintained throughout.

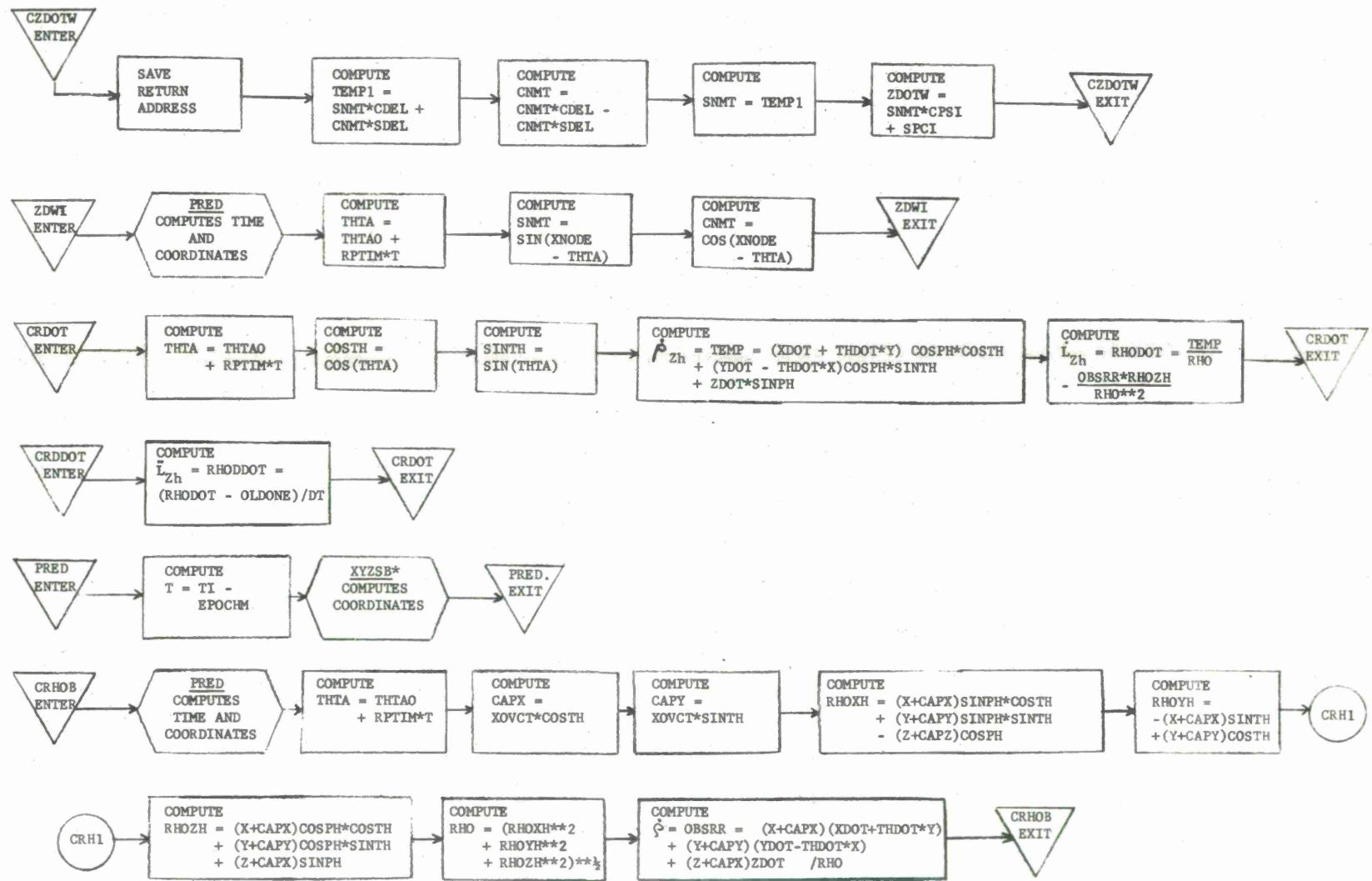


*B-2 SYSTEM SUBROUTINE

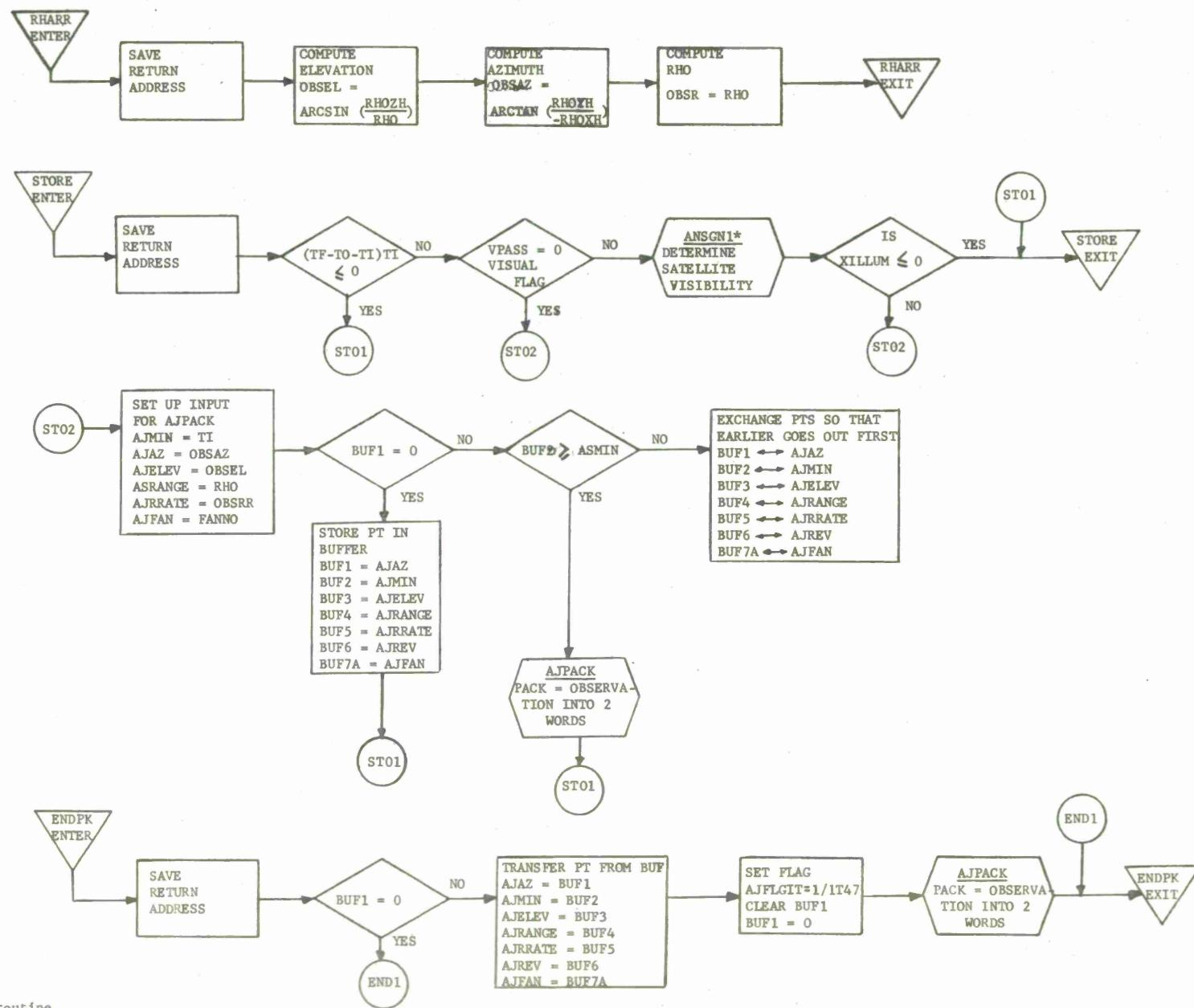




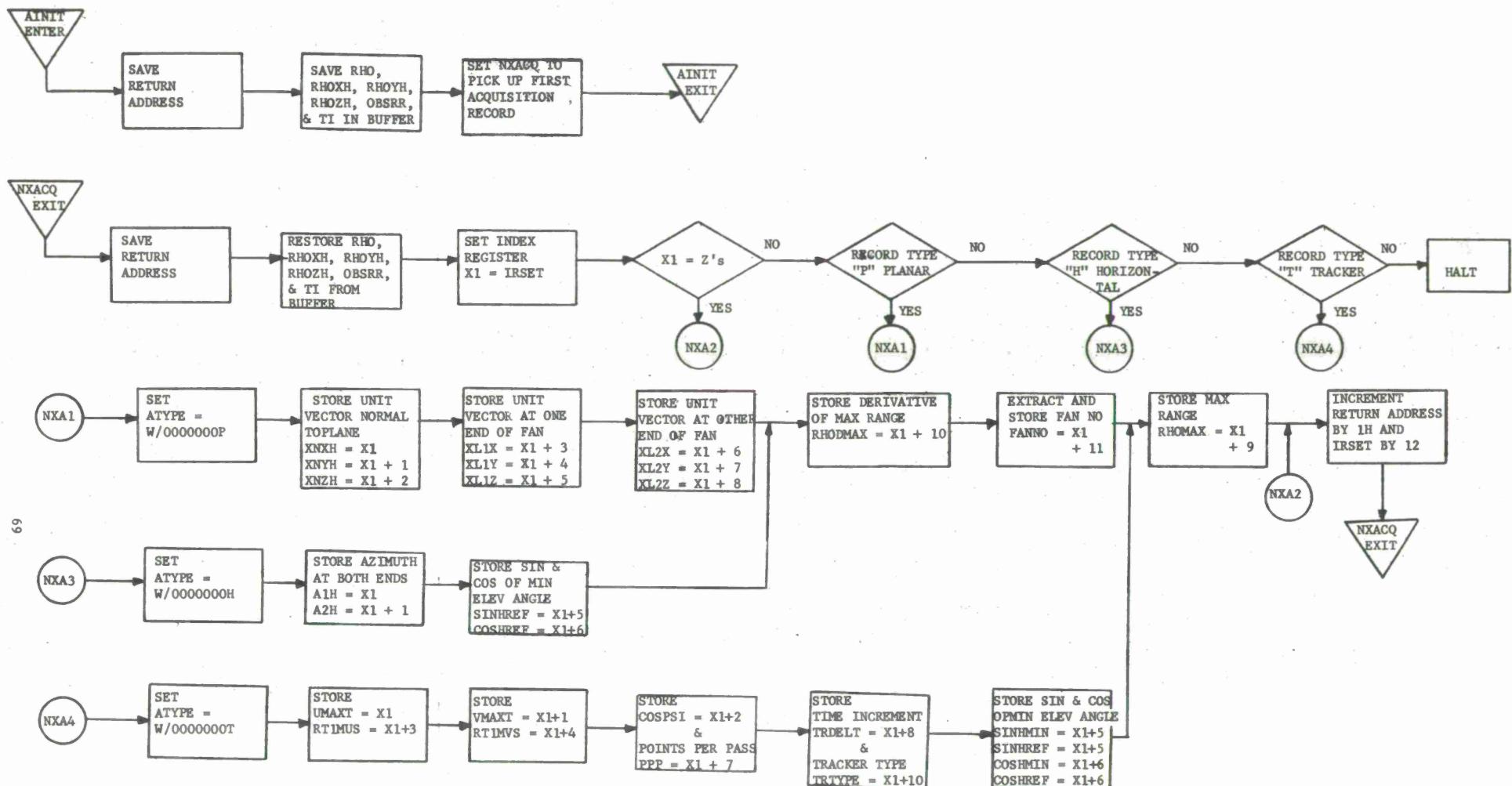


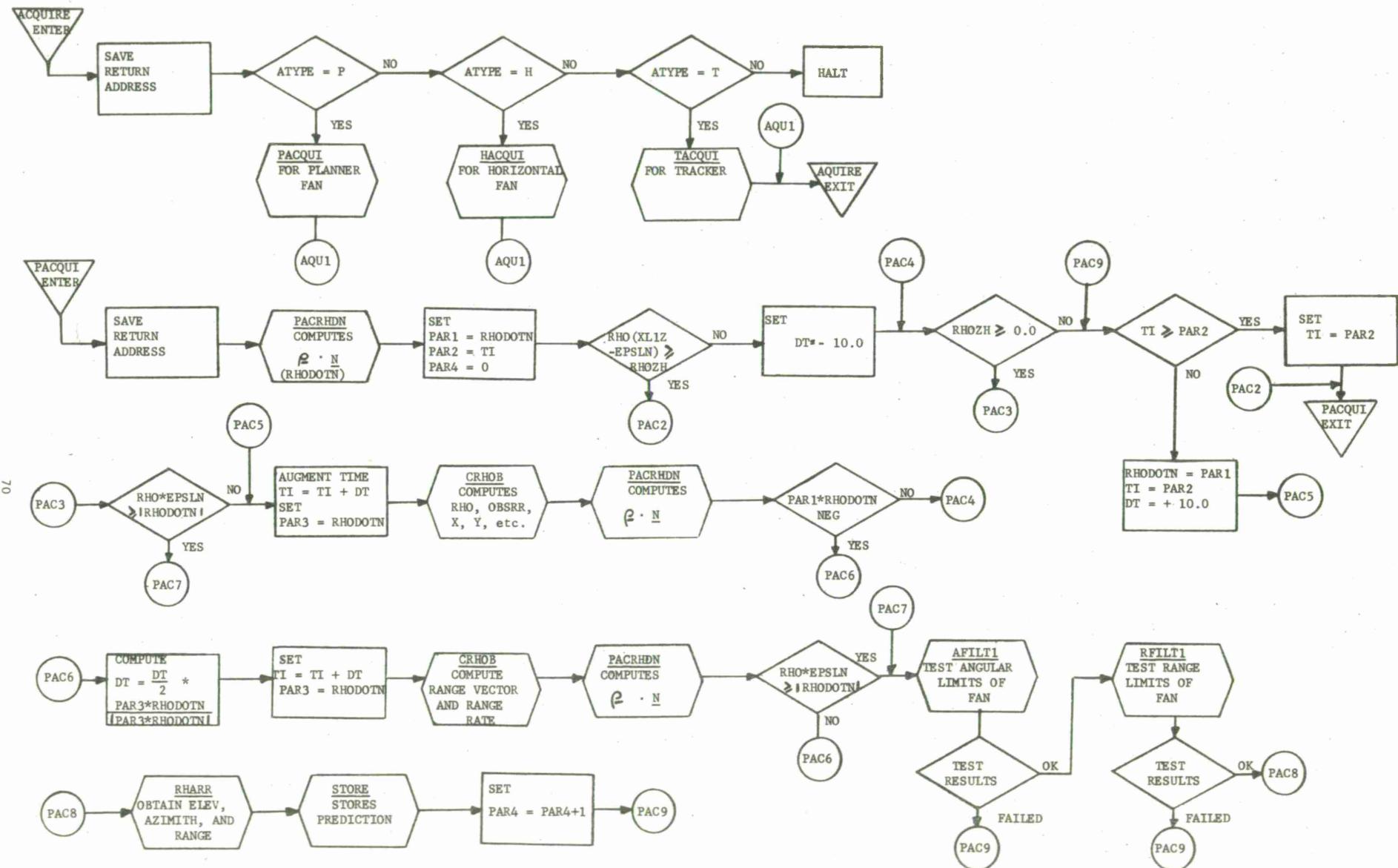


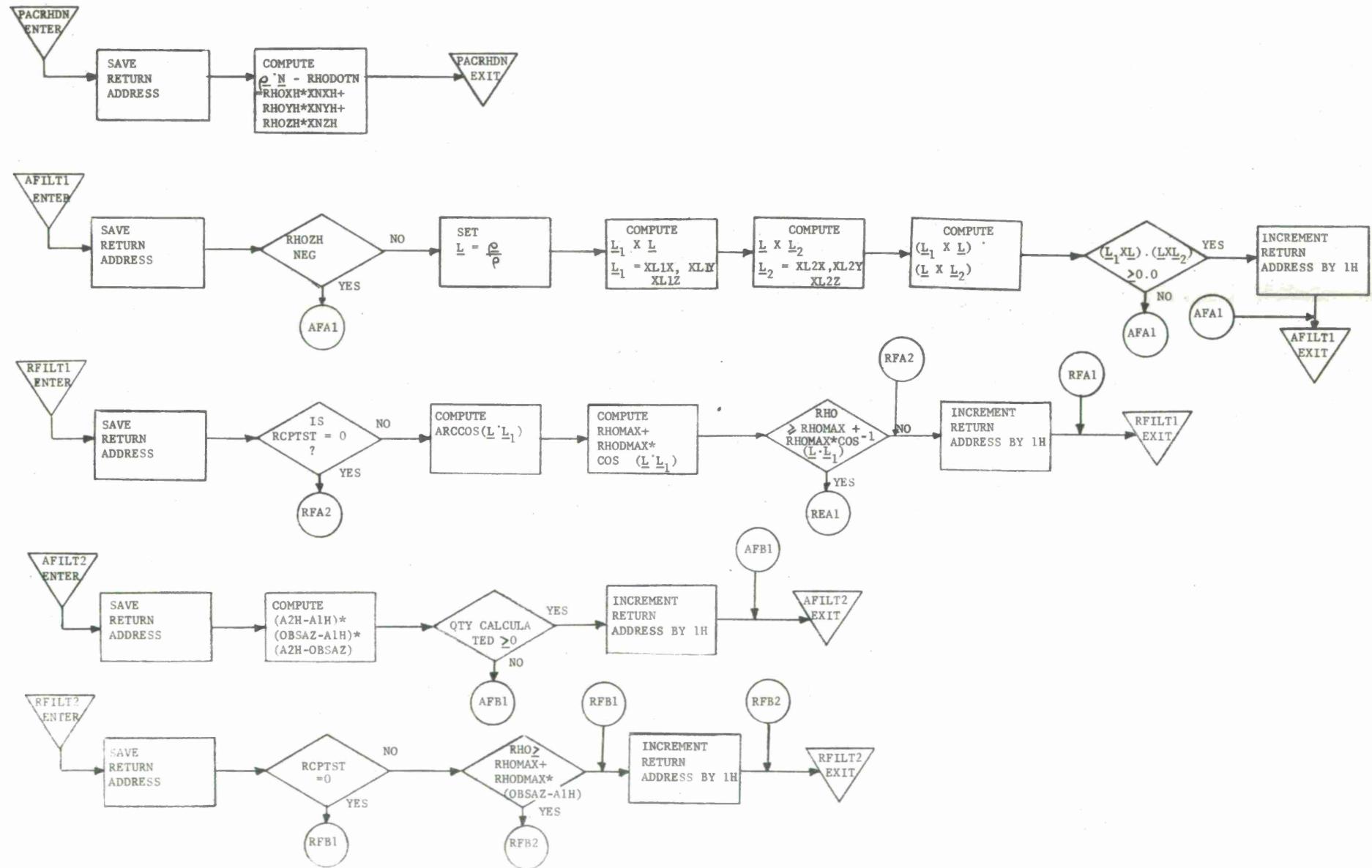
* B-2 System Subroutine

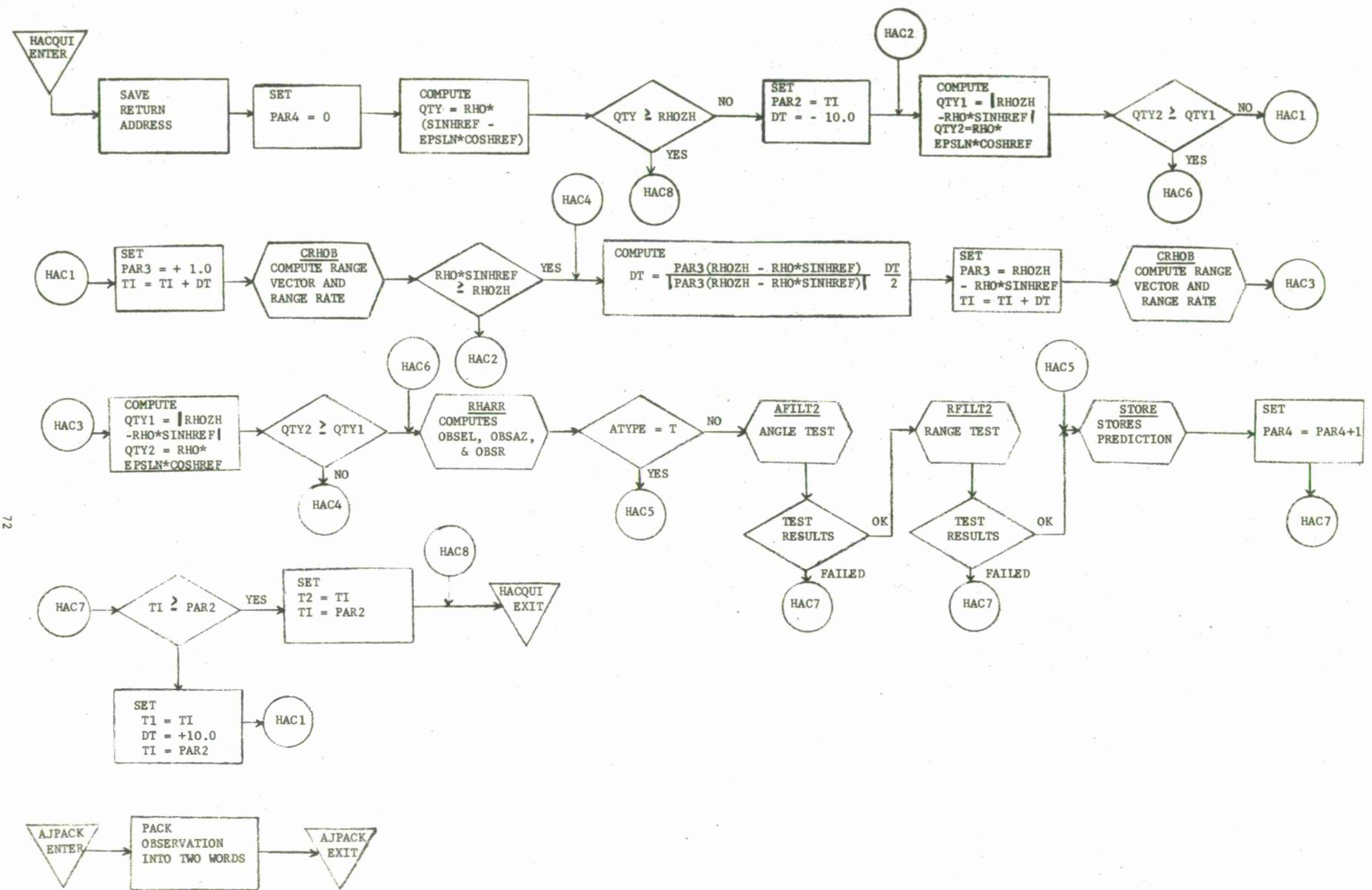


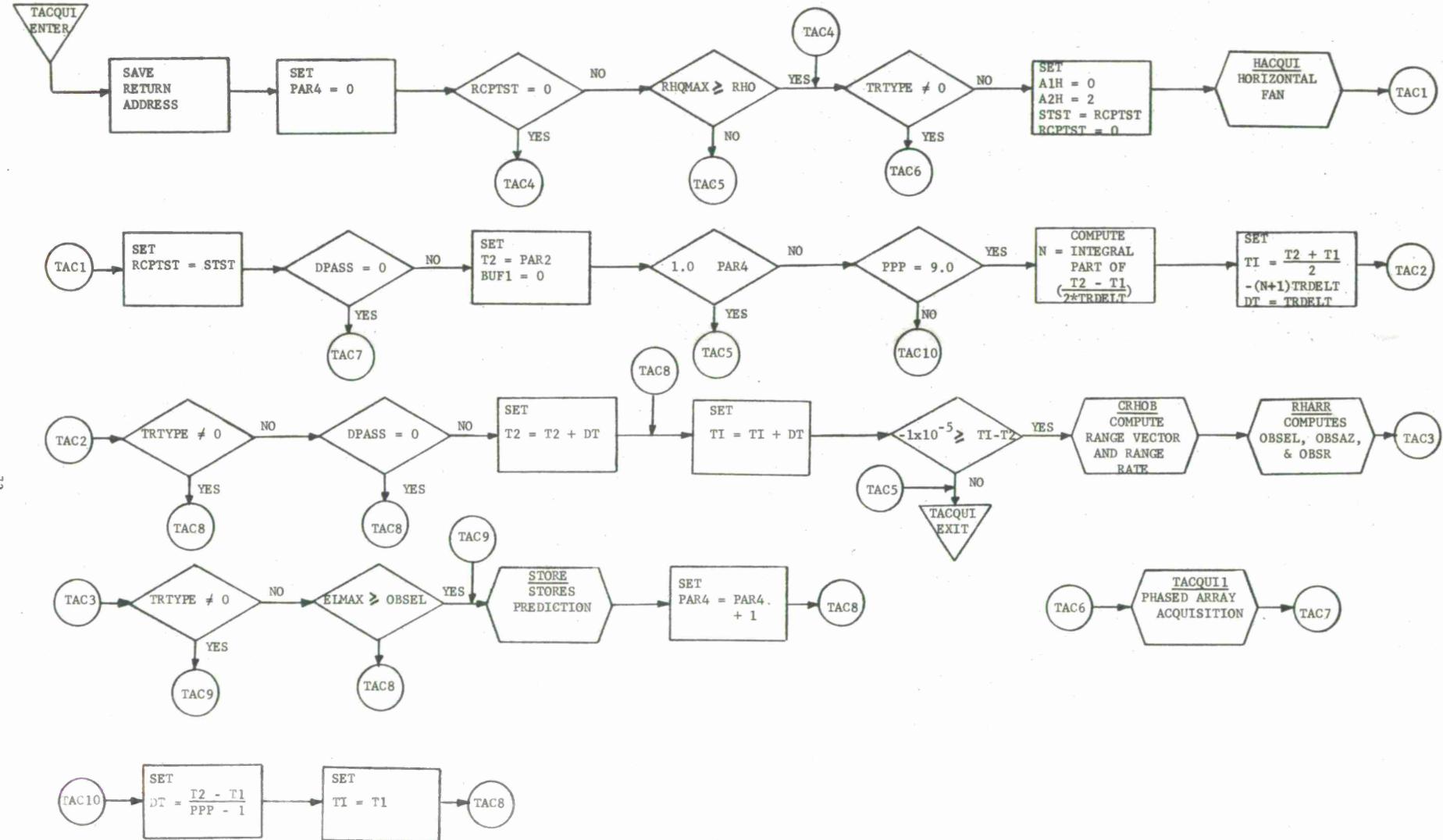
*B-2 System Subroutine

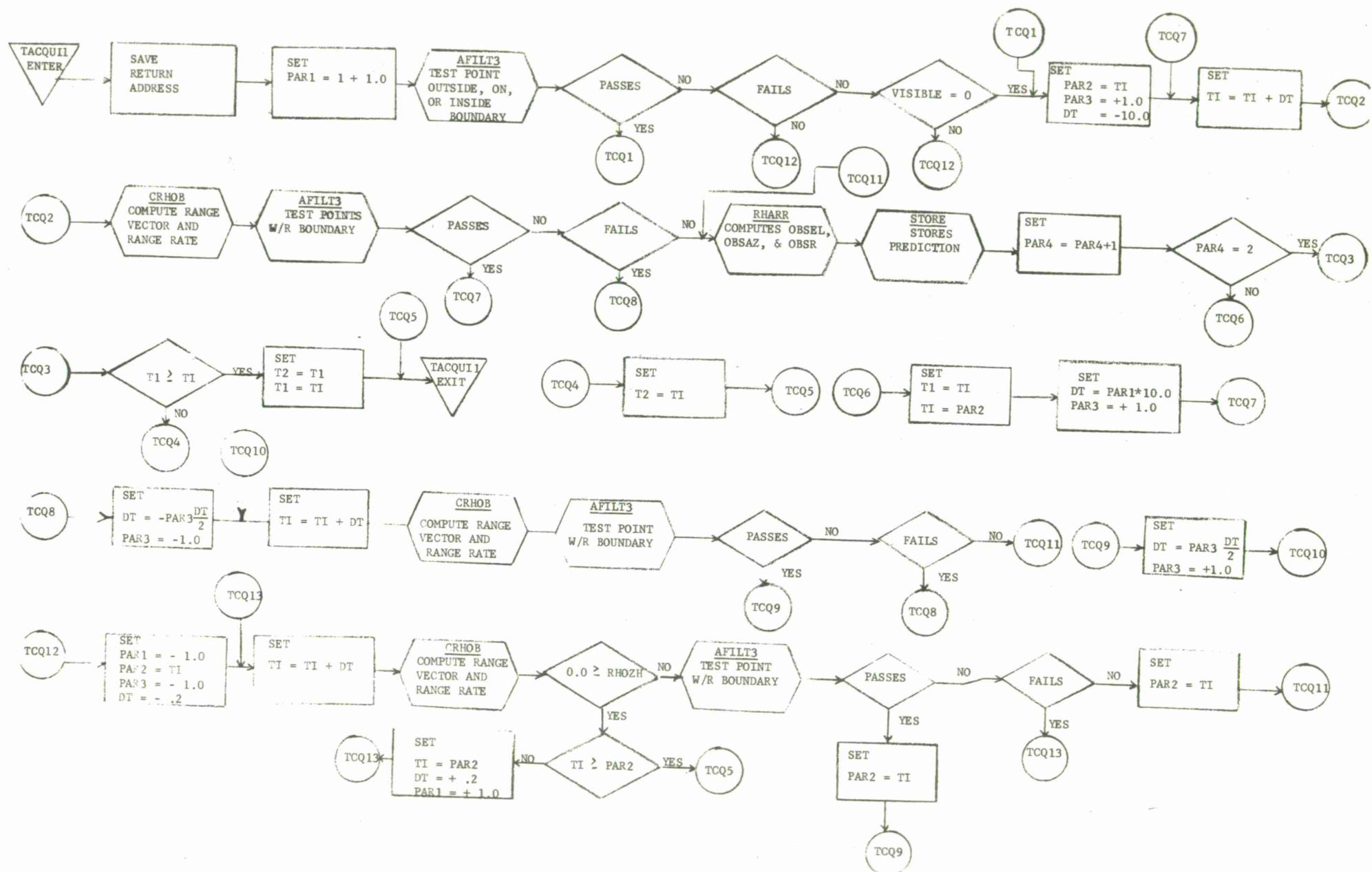


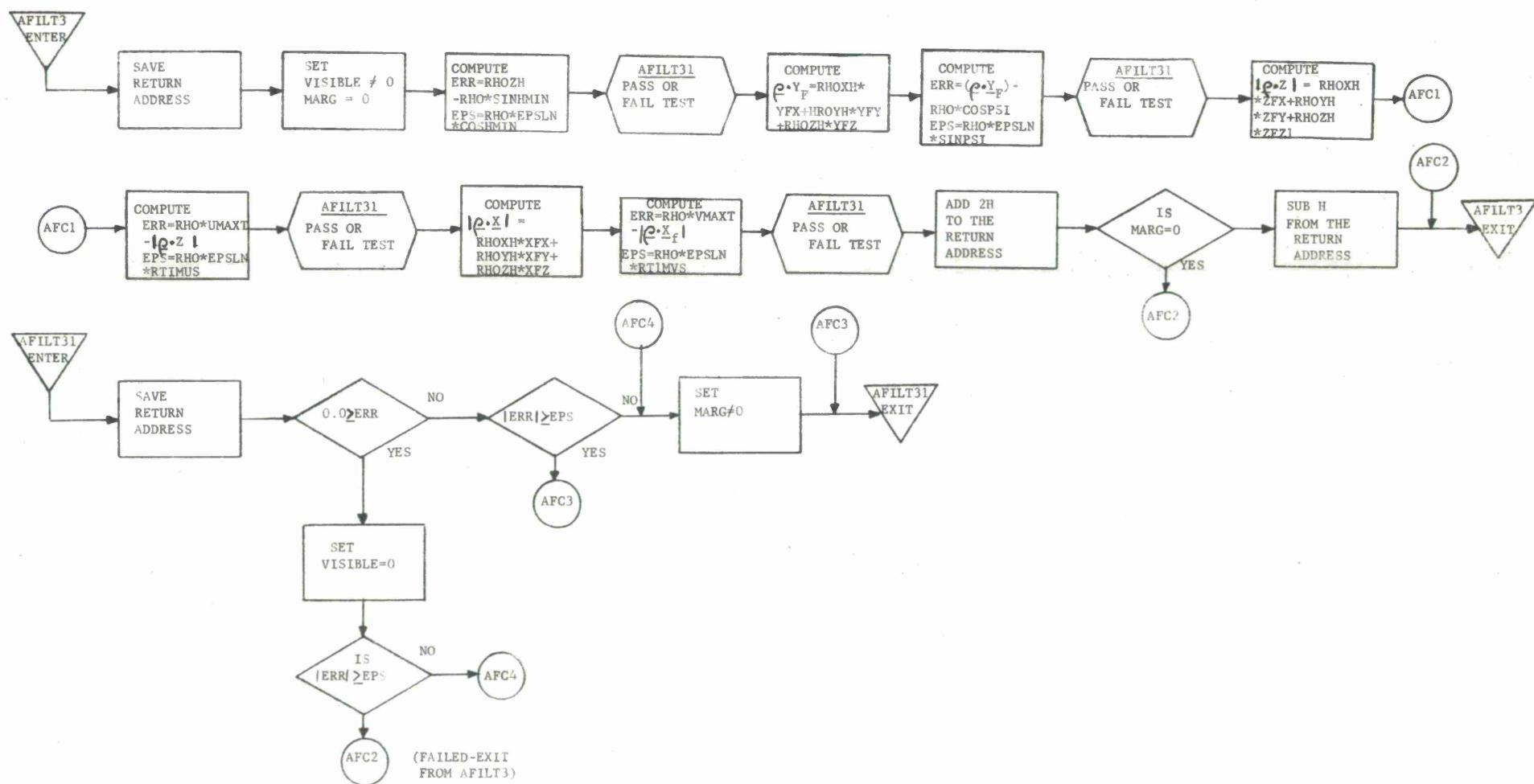


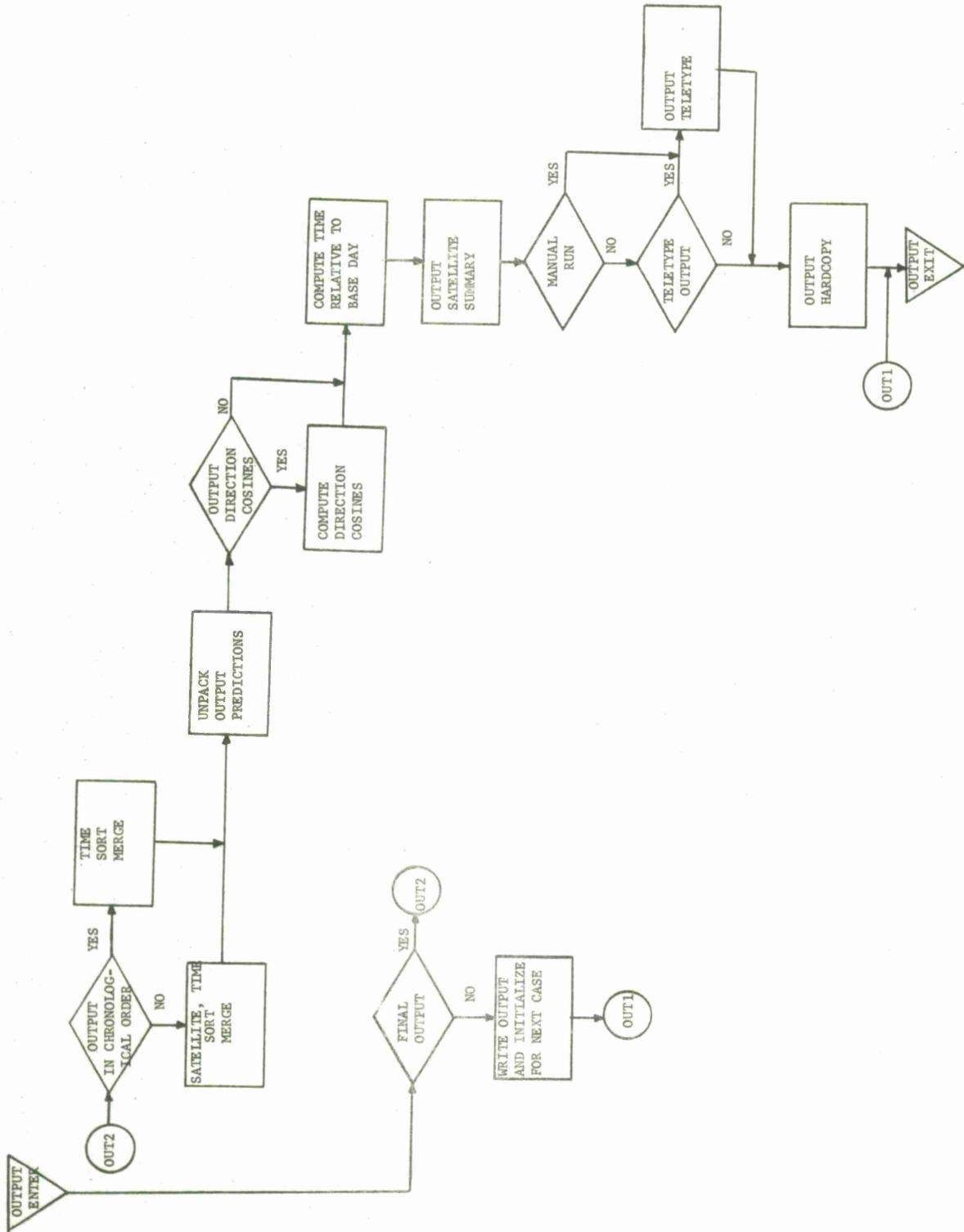












APPENDIX I

FILE FORMATS

Word

1	48 bit floating point
2	48 bit floating point
3	48 bit floating point
4	48 bit floating point
5	48 bit floating point
6	48 bit floating point
7	48 bit floating point
8	48 bit floating point
9	48 bit floating point
10	48 bit floating point
11	48 bit floating point
12	N Δ Δ Δ Δ Δ Δ P

XNX }
XNY } Unit vector normal to plane
XNZ }
XL1X }
XL1Y } Unit vector at one end of fan
XL1Z }
XL2X }
XL2Y } Unit vector at other end of
XL2Z } fan (note: $XL1Z \leq XL2Z$)
RHOMAX - Maximum range at first end
of fan
RHODMAX - Derivative of maximum
range

N - Fan Number (BCD); P - identification

a. FANTAB - Planar Fan

FIGURE I-1. FORMAT FOR ACQUISITION BUFFER

Word

1	48 bit floating point
2	48 bit floating point
3	
4	
5	
6	48 bit floating point
7	48 bit floating point
8	
9	
10	48 bit floating point
11	48 bit floating point
12	N Δ Δ Δ Δ Δ Δ H

A1H } Azimuth (coverage goes
A2H } from A1H clockwise to
A2H)

SINHREF sine at constant elevation
COSHREF cosine of constant elevation

RHOMAX - Maximum range at first end
of fan
RHODMAX - Derivative at maximum range
N - Fan Number (BCD) H - identification

b. FANTAB - Horizontal Fan

1	48 bit floating point
2	48 bit floating point
3	48 bit floating point
4	48 bit floating point
5	48 bit floating point
6	48 bit floating point
7	48 bit floating point
8	48 bit floating point
9	48 bit floating point
10	48 bit floating point
11	48 bit fixed point
12	Δ Δ Δ Δ Δ Δ Δ T

UMAXT }
VMAXT }
COSPSI } Not used for normal
RT1MUS }
RT1MVS }
SINHMIN sine of minimum elevation
COSHMIN cosine of minimum elevation
PPP points per pass
TRDELT Δt (minutes)
RHOMAX Maximum range
TRTYPE Tracker type 1 = Phased
array 0 = normal
T = identification

c. FANTAB - Tracker

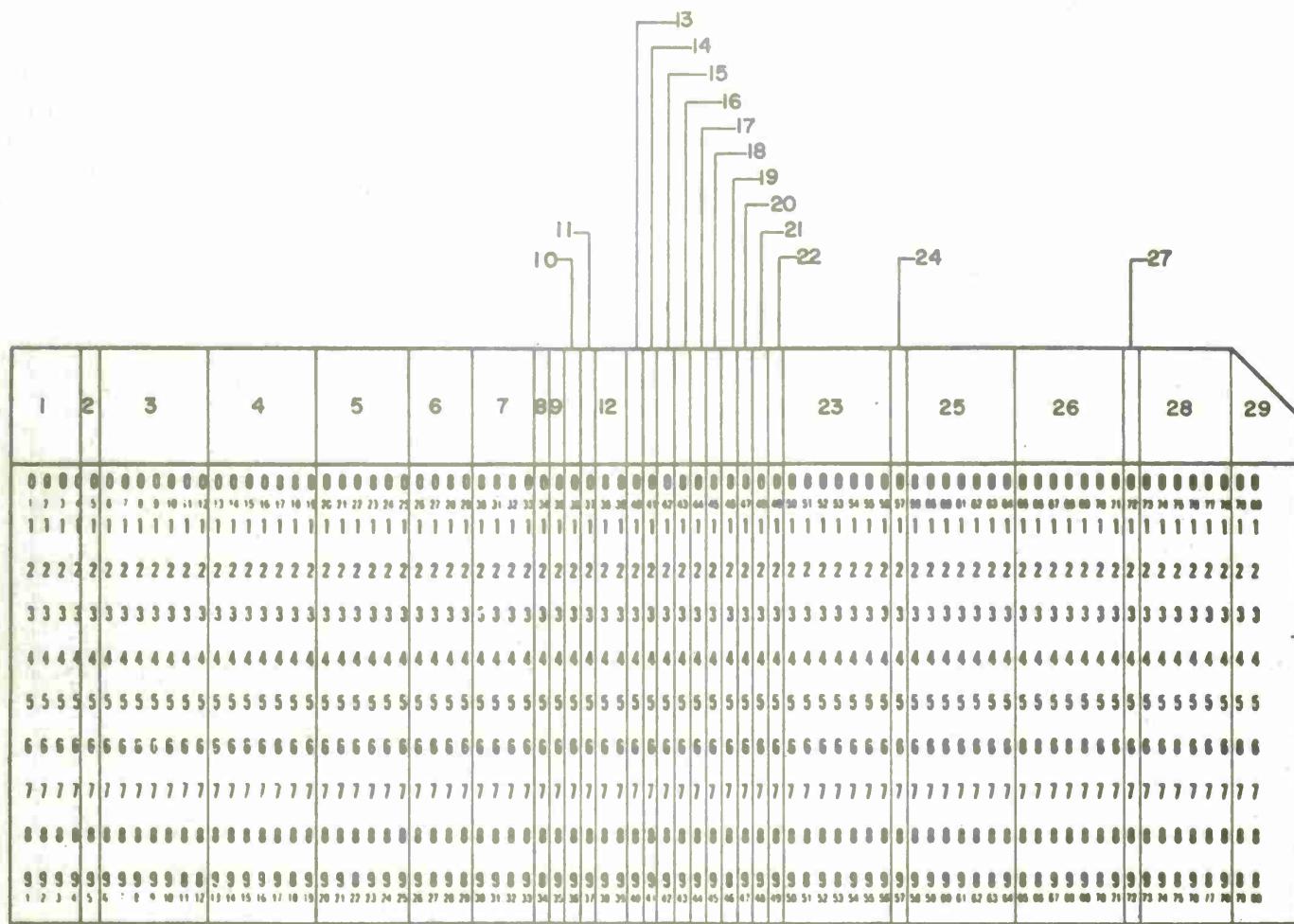
FIGURE I-1. FORMAT FOR ACQUISITION BUFFER (continued)

APPENDIX II

CARD FORMATS

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-8	"FANCARDS"
2	9	End of block character: 11-8-2 punch

FIGURE II-1. FAN INPUT DATA TAPE IDENTIFIER



<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-4	Sensor number right adjusted
2	5	Not used
3	6-12	Beginning time - days since base time
4	13-19	End time - days since base time
5	20-25	Not used
6	26-29	Beamwidth - degrees
7	30-33	Year
8	34	Output indicator for fan number column on output. 0: No fan number 1: Fan number
9	35	Output indicator for units of range and range rate. 0: Nautical units 1: MKS Units

FIGURE II-2. CONTROL CARD

<u>Field</u>	<u>Column</u>	<u>Contents</u>
10	36	Not used
11	37	Classification indicator 0: Unclassified 1: Confidential 2: Secret 3: Secret/No form 4: Secret/Releasable outside SSO channels
12	38-39	Priority - printed on output message
13	40	Not used
14	41	Visual pass indicator 0: All passes 1: Visual passes only
15	42	Not used
16	43	Down pass indicator ¹ 0: Complete pass computed 1: No points after closest point of approach
17	44	Not used
18	45	Point of maximum elevation 0: No 1: Yes
19	46	Not used
20	47	Maximum range test for point of closest approach 0: No test 1: Test
21	48	Not used
22	49	Interlace inhibit 0: Interlace predictions ² 1: No mixture of predictions ³
23	50-56	Not used
24	57	Direction cosines print out 0: No print out 1: Print out
25	58-64	Elevation angle of the boresight in degrees ⁴
26	65-71	Boresight azimuth in degrees ⁴
27	72	Element number option 0: Print revolution number 1: Print element number

1 For trackers only

2 Output in strictly chronological order

3 Same as (2) but satellite passes are not mixed

4 These fields are needed only if the tracker card indicates an FPS type tracker and/ or it is desired to print direction cosines

FIGURE II-2. CONTROL CARD (Continued)

<u>Field</u>	<u>Column</u>	<u>Contents</u>
28	73-78	Not used
29	79-80	"RP" - must contain these two letters as ID

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	17			
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56	57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75	76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94	95 96 97 98 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56	57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75	76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94	95 96 97 98 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56	57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75	76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94	95 96 97 98 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99	99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99 99

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1, 9	1-6, 40-45	Elevation angle at start of fan (h_1) - in degrees
2, 10	7-12, 46-51	Azimuth at start of fan (A_1) - in degrees
3, 11	13-18, 52-57	Maximum range at start of fan ($\rho_{1\max}$) - in kilometers
4, 12	19-24, 58-63	Elevation angle at end of fan (h_2) - in degrees
5, 13	25-30, 64-69	Azimuth at end of fan (A_2) - in degrees
6, 14	31-36, 70-75	Maximum range at end of fan ($\rho_{2\max}$) - in kilometers
7, 15	37-38, 76-77	Fan number (BCD)
8, 16	39, 78	Fan type "H" - Constant elevation azimuth scan "P" - Planar fan
17	79-80	"FP" - must contain these two letters as ID.

FIGURE II-3. FAN CARD

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
7	8	9	10	11	12	13	14	15	16	17	10	26	21	22	23	24
7	8	9	10	11	12	13	14	15	16	17	10	26	21	22	23	24
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
8	9	10	11	12	13	14	15	16	17	10	19	20	21	22	23	24
25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41
42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58
59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-6	"Δ-99.0" An elevation of -99° signifies a request for acquisition coordinates for a tracking device
2	7-18	Not used
3	19-24	Minimum elevation - degrees - floating point
4	25	Points per pass 2-8: 2-8 points per pass 9: points every delta T (field 8)
5	26	Not used
6	27	Tracker type Δ or 0: Normal tracker 1: FPS-85 tracker
7	28-30	Not used
8	31-36	Time increment in minutes - (needed only if points per pass = 9)
9	37-42	Limiting value of the SIN of the boresight oriented angle α - $\sin \alpha$ - floating point boresight oriented
10	43-48	Limiting value of the SIN of the angle β - $\sin \beta$ - floating point
11	49-54	Limiting value of the off-boresight angle, ψ , in degrees

FIGURE II-4. TRACKER CARD

<u>Field</u>	<u>Columns</u>	<u>Contents</u>
12	55-60	Maximum observable range - floating point kilometers
13	61-66	Maximum elevation angle to be used for normal tracker only - if blank, 90° is assumed
14	67-72	Not used
15	73-75	Sensor number
16	76-78	Not used
17	79-80	"FP" - must contain these two letters as ID.

FIGURE II-4. TRACKER CARD (Continued)

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-64	Station address - 64 BCD characters (can also include the routing address, even though this will be repeated in Columns 65-72)
2	65-72	Routing address - 6 or 7 BCD characters
3	73-80	Card identifier, one of the following: FROMXXXA, TO△XXXA, or INFOXXXA; XXX is sensor number

FIGURE II-5. ADDRESS CARD

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-8	ALL ΔΔΔΔ ALL BUT Δ ONLY ΔΔΔΔ.
2	9-80	<ol style="list-style-type: none"> 1. Not used for ALL Cards 2. For "ALL BUT" and "ONLY" Cards - This field contains five -digit satellite identifiers, separated by commas and/or two five -digit satellite identifiers separated by a minus.

FIGURE II-6. ALL, ALL BUT, or ONLY CARD

1	2	3	4	5	6
0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
1 2 3 4 5 6 7	8 9 10 11 12 13 14	15 16 17 18 19 20 21	22 23 24 25 26 27 28	29 30 31 32 33 34 35	36 37 38 39 40 41 42
1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1
2 2 2 2 2 2 2	2 2 2 2 2 2 2	2 2 2 2 2 2 2	2 2 2 2 2 2 2	2 2 2 2 2 2 2	2 2 2 2 2 2 2
3 3 3 3 3 3 3	3 3 3 3 3 3 3	3 3 3 3 3 3 3	3 3 3 3 3 3 3	3 3 3 3 3 3 3	3 3 3 3 3 3 3
4 4 4 4 4 4 4	4 4 4 4 4 4 4	4 4 4 4 4 4 4	4 4 4 4 4 4 4	4 4 4 4 4 4 4	4 4 4 4 4 4 4
5 5 5 5 5 5 5	5 5 5 5 5 5 5	5 5 5 5 5 5 5	5 5 5 5 5 5 5	5 5 5 5 5 5 5	5 5 5 5 5 5 5
6 6 6 6 6 6 6	6 6 6 6 6 6 6	6 6 6 6 6 6 6	6 6 6 6 6 6 6	6 6 6 6 6 6 6	6 6 6 6 6 6 6
7 7 7 7 7 7 7	7 7 7 7 7 7 7	7 7 7 7 7 7 7	7 7 7 7 7 7 7	7 7 7 7 7 7 7	7 7 7 7 7 7 7
8 8 8 8 8 8 8	8 8 8 8 8 8 8	8 8 8 8 8 8 8	8 8 8 8 8 8 8	8 8 8 8 8 8 8	8 8 8 8 8 8 8
9 9 9 9 9 9 9	9 9 9 9 9 9 9	9 9 9 9 9 9 9	9 9 9 9 9 9 9	9 9 9 9 9 9 9	9 9 9 9 9 9 9
1 2 3 4 5 6 7	8 9 10 11 12 13 14	15 16 17 18 19 20	21 22 23 24 25 26	27 28 29 30 31 32	33 34 35 36 37 38

<u>Field</u>	<u>Column</u>	<u>Contents</u>
1	1-7	Base Time - day number in year and fraction, decimal punched in Column 4
2	8-11	Not used
3	12-16	Message number, right adjusted
4	17-78	Not used
5	79	B
6	80	P

FIGURE II-7. BASE TIME CARD

SET 39 \$
 JMP START \$
 SET M/52500 \$

 SAME ORIGIN,START \$
 START JMP (P)+2 \$
 NOP \$
 HLT \$
 HLT \$
 TMD W/FANGARDS \$
 TDM SYSNAME \$
 TMA P/SYSTAB,T39 \$
 JMP TAPCK \$
 TMA P/SYSTAB+7,T39 \$
 JMP TAPCK \$
 TMA P/SYSTAB+8,T39 \$
 JMP TAPCK \$
 TMA P/SYSTAB+9,T39 \$
 JMP TAPCK \$
 TMA N/11T15;P/SYSTAB,T39 \$
 JMP PANT.PINT \$
 CM PHAIN \$
 TMD C/TJML,EREXIC/JMP,ER10 \$
 TDM 0 \$
 TDM 3 \$
 TMD C/HLTL,EBLOCS \$
 TDM ILOCES \$
 CM NOELMS \$
 CM AJDNCNT \$
 TMA EXLOD \$
 JAZ (P)+2H \$
 JMP GO ON \$
 TMD 1/1T6 \$
 TDM CARDTYP \$
 CM NOTTY \$
 TMD W/ BP \$
 TDM CONBUF+9 \$
 TAG1 TMA C/HLT,181C/HLT,TAGA \$
 JMP FLEX \$
 TMQ W/ 0 \$

 TAG3 CD
 JMP TCMR \$
 TDA \$
 TMD 0/72T47 \$
 JAED TAG1 \$
 TMD 0/32T47 \$
 JAED TAG2 \$
 AQ \$
 SLA 6 \$
 TAQ \$
 JMP TAG3 \$
 TMQ CONBUF \$
 TMA C/HLT,181C/HLT,TAG7 \$
 JMP FLEX \$
 TMQ W/ 0 \$

 TAG4 CD
 JMP TCMR \$
 TDA \$
 TMD 0/72T47 \$

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JAED TAG2+1H \$
 TMD 0/32T47 \$
 JAED TAG5 \$
 AQ \$
 SLA 6 \$
 TAQ \$
 JMP TAG4 \$
 SRQ 6 \$
 TQM CONBUF+1 \$
 JMP GO ON \$
 TAG6 0/321A/BASE DAS \$
 A/Y\$ \$
 A/ 10/52T11S \$
 TAG7 0/321A/BASE-MES \$
 A/SSAGE NOS \$
 A/ 10/52T11S \$
 GO ON TMD L/CONBUF \$
 TDXLC ,3 \$
 TMA 9,3 \$
 THD W/ BP \$
 JAED (P)+2H \$
 JMP CASE REJ \$
 TMA 0,3 \$
 THD W/ \$
 JAED CASE REJ \$
 TMQ 0/000001717171717 \$
 ETA 1,3 \$
 JAZ CASEREJ \$
 TAM AJMSGNO \$

 L TMA (P)+2 \$
 JMP XSRCH \$
 JAZ CASE REJ \$
 JMP LOAD \$
 HLT \$
 TIJL (P)+1H \$
 ICOZ 7+128+7 \$
 CAM BASE \$
 A/CASE REJECTED-BAS \$

 A/SE TIME CARD MISS \$

 A/SING OR IN ERRORS 48 \$

 CASEREJ TMA N/6T15;P/(P)-6,T39 \$
 JMP PANT \$
 TMA N/48T15;P/(P)-7,T39 \$
 JMP FLEX \$
 TMA N/10T15;P/CONBUF,T39 \$
 JMP PANT \$
 JMP PANT.FINISH \$
 JMP MANEXIT \$

 L BUFA SET (P)+128\$ \$
 BUFB SET (P)+128\$ \$
 START6 TJM READX\$ \$

APPENDIX III
 PROGRAM LISTING

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JMP    BUF022$          TMA    C/HLT,SATNOS      $
RD6A   TJM    READXS      AM     NOELM           $
TMD    TIOS             AM     N/1T15          $
TDXLC  0,3$            TAM    IEEND           $
TMD    C/HLT,0;C/HLT,SYSTABS  SRA    24$           $
JMP    SYSIOS          TAM    TEMP1$          $
TMD    C/HLT,BUF01,C/HLT,BUF01$  TMA    NOELMS          $
AIXJ   0,3$            TMQ    4/112/0132/1$      $
BUF022 TIJ    BUFBS        EIS    4S1 BS          $
TJM    TIOS             SRA    24$           $
L READ   TMA    1/110010001T47$      TMQ    28/112/018/1$      $
R JMP    SYS$            EIS    4A 10D1$          K125
TIO    TIO              S     TMA    C/HLT,0;C/HLT,ORIGIN-1 $      $
JMP    SYSNOS          SM    TEMP1$          $
READYX  JMP    (P)$          SLA    17$           $
BUF01   TIJ    BUFAS          EI    D/0$           $
TJM    TIOS             TAM    AJNMBLK$          $
JMP    READ$            TMA    IEENDS          $
LOAD   TMQ    1/1T3$          SCD    4LMAX$          $
ETA    CARDTYP$          TDM    4RMAX$          $
JAZ    LOADES           SM    N/2T15$          $
JMP    LOADSNO          TAM    4LMAX2$          $
LOADE  TMQ    1/1T7$          JMP    START6$          $
ETA    CARDTYP$          CASATTB TJM    NXTCASES          $
JAZ    LOADS$            TMD    CASXX$          $
TMQ    1/1T0$            TDXLC  C/HLT,SATTB;C/HLT,SATNOS$      $
JMP    ELMLODS          TDXRC  ,3$           $
LOADSNO JMP    CASATTB      TMA    MASKSATS          $
TMA    NUMELMS          SLA    ,3$           $
SLA    24$              TAM    MASKBLS          $
TAM    NOELMS          JAED   ELEND$          $
TESTSN  TMQ    1/1T8$          TMO    1/1T0$          $
ETA    CARDTYP$          EA    MASK1$          $
JAZ    LOADE7$           TETD   ,4$           $
LSNCO   TMD    C/HLT,L.BLOC;C/HLT,STYPES  AIXO   1,3$           $
TDXLC  ,3$              TDM    AIXO           $
TDXRC  ,4$              TMD    1,4$           $
TMD    ,3$              AIXO   CASPP$          $
TMD    ,4$              TMO    1/1T0$          $
AIXO   1,3$              EA    MASK1$          $
AIXOL  1,4$              TETD   ,4$           $
JNO    (P)-5HS          TETD   AIXO           $
CA     S                JAED   ELEND$          $
TMQ    STYPES           TMO    1,4$           $
SLQ    12$              TETD   LOAD A3$          $
SLAQ   18$              TETD   LOAD A4+1H$      $
TAM    STYPES           TETD   4A10$          $
TMA    MASKBLS          TETD   LOADA7-1H$      $
SLAQ   18$              TETD   C/HLT,ELOC;C/HLT,SATNOS$      $
TAM    STAIDS          TETD   ,3$           $

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```

LOADE7 TMA    C/HLT,SATNOS      $
TMA    NOELM           $
AM     N/1T15          $
TAM    IEEND           $
SRA    24$           $
TAM    TEMP1$          $
TMA    NOELMS          $
TMQ    4/112/0132/1$      $
EIS    4S1 BS          $
SRA    24$           $
TMQ    28/112/018/1$      $
EIS    4A 10D1$          $
TMA    C/HLT,0;C/HLT,ORIGIN-1 $      $
SM    TEMP1$          $
SLA    17$           $
TMQ    16/0132/1$      $
EI    D/0$           $
TAM    AJNMBLK$          $
TMA    IEENDS          $
TAM    4LMAX$          $
SCD    24$           $
TDM    4RMAX$          $
SM    N/2T15$          $
TAM    4LMAX2$          $
JMP    START6$          $
JMP    NXTCASES          $
CASATTB TJM    CASXX$          $
TMD    C/HLT,SATTB;C/HLT,SATNOS$      $
TDXLC  ,3$           $
TDXRC  ,4$           $
CASPP  TMQ    MASKSATS          $
ETA    ,3$           $
ETD    MASKBLS          $
JAED   ELEND$          $
TMO    1/1T0$          $
EA    MASK1$          $
TAM    ,4$           $
AIXO   1,3$           $
AIXO   1,4$           $
JMP    CASPP$          $
ELEND  CA    S           $
TAM    ,4$           $
CASXX  JMP    (P)$          $
LOADO  TIJ    LOAD A3$          $
TIJ    TETD   LOAD A4+1H$      $
TETD   4A10$          $
TETD   LOADA7-1H$      $
OPTION  TMD    C/HLT,ELOC;C/HLT,SATNOS$      $
TDXLC  ,3$           $
TDXRC  ,4$           $
CQ    S           $
JMP    ELMLODS          $
TMA    NUMELMS          $
TMO    18/1T29          $
TMD    D/400B39$          $

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JAGD	ECYCLES\$
NOCYCLE	ETA ,3\$
ETD	MASKZ\$
JAED	NOMORE\$
SRA	18
TAM	,4\$
AIXO	16,3\$
AIXO	1,4\$
JMP	NOCYCLE
ASGN	PASSONE,M/37545
NOMORE	TMQ 24/1T47
ETA	,3
ETD	MASKZ
JAED	(P)+4H
THQ	18/1T29
ETA	,3
JMP	NOMORE-5H
CM	,4
TMA	NUMELMS
SLA	24\$
AMS	NOELMS
JMP	TESTSNSS
ECYCLE	DRANA+ 400
ETD	16,3\$
SRD	18
TDM	1,4\$
TMA	D/400B15\$
AMS	NOELMS
TMD	C/HLT,EBLOCS
TDXLC	,3\$
JMP	OPTION0+3HS
L 4S1	TJM 4S1 B+2H
	TMA 1/1
	JMP (P)+3H
4S1 A	TJM 4S1 B+2H
	CA
	THQ 12/0;36/1
	TMD C/HLT,SATNOSS
	TDXLC ,1
L 4S1 B	RPTA 1000\$
	EIS 1,1\$
	JMP
4S2	TJM (P)-1H
	TMD C/HLT,BUFA+120\$C/HLT,BUFB+120\$
	AIXOL ,3
	JOF (P)+3H
	AIXOR ,3
	JNO (P)+2H
	JMP RD6AS
	TMA ,3
	TMD W/END CASE
	JAED 4S2-1H

CN K-160

\$

R 4S3	TMD W/ENDSCHED
	JAED (P)+4H
	TMA N/1T16
	AHS 4S2-1H
	JMP 4S2-1H
	TIJ 4S3 A
	TJM NXTCASE
	JMP 4S2-1H
	TJM (P)+4H
	TMA W/END CASE
	RPTAN 12
	TMD 10,3
	JAED
	TMA W/ENDSCHED
	RPTSN 13
	TMD 10,3
	JAED 4S3 A
	JMP RD6AS
	JMP 4S3+1H
	A/END FAN INPUTS
4S3 A	TMA N/13T15;P/(P)-2,T39
	JMP FLEX
	JMP PANT.ALLFIN
	TIJ NXTCASE1+1HS
	TJM NXTCASE1S
	JMP NXTCASE+1H
4S4	TJM 4S4 A=1H S BIT 47=1,ERROR
	CD \$ 46=1,COMMA
	SIXO 1,0 \$ 45=1,DASH
	JOF 4S4 A \$ 44=1,ENDCASE
	TMQ 4T11
	CA
	SLAQ 6
	TMQ 4T11
	TMD 0/60T47
	JAED 4S4+1
	TMD W/0000000,
	JAED (P)+2S
	TMD W/0000000-
	JAED (P)+2S
	JMP 4S4 A=1
	TMD 1/1T46
	JMP (P)+2
	TMD 1/1T45
	JMP (P)+1
	TMD 1/1T47
	DORMS 4T9
	SRAQ 6
	JMP
4S4 A	AIXO 1,3
	SIXO 1,1
	JNO (P)+2
	JMP 4S2
	JMP (P)+3

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TIXZ 10,1
 TIXZ 9,0
 THD ,3
 TDM 4T11
 JMP 4S4+1H
 TMD 1/1T44
 JMP 4S4 A=3H
 4S4 3 TJM 4S4 B3+5H
 CM 4T9
 CM 4T6
 TIXZ 5,2 \$
 JMP 4S4
 TMA 4T6
 SLAQ 6
 TAM 4T6
 TMA 4T9
 JAZ 4S4 B3
 4S4 31 TMD N/10T15
 AIXO 0,1
 JOF 4S4 B2
 SIXO 1,3
 AIXO 1,1
 JOF (P)+2H
 JMP (P)-3H
 4S4 32 TMQ 30/18/18/0
 TMA STAN
 EIS 4S4 B3-1
 TMA N/16T15IP/4S4 B3-3,T39\$
 JMP FLEX
 JMP PANT,SPACE
 TMA N/3T15IP/4S4 B3-3,T39
 JMP PANT
 TMQ 4T9
 SRQ 3
 JQO NXTCASE
 AIXO 10,3
 JMP 4S2
 JMP NXTCASE
 JMP (P)-3H
 W/ERROR ON
 W/ ALL BUT
 W/ OR ONLY
 W/ CARDS
 W/CASE REJ
 W/-INP ERH
 W/-STA XXX
 4S4 33 SIXO 1,2
 JNO 4S4 B+4H
 JMP 4S4
 TMA 4T9
 JAZ (P)+2H
 JMP TMA N/4T15IP/4S4 B3-7,T39
 JMP PANT

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JMP 4S4 B1
 4BCDADD TJM (P)+6H
 AM W/000WWWWX
 TAQ
 ES W/
 SRD 3
 SD
 JMP
 * 0/7777777777777777
 0/60606060603254
 JMP
 4HEAD TJM (P)-1H
 TIJ PANT,TPANTAS
 TJM 4OUT1+2H S
 TMA N/2T15IP/(P)-8H,T39S
 JMP 4OUT 1 \$ LINE 1
 TMD L/StADR+20 \$ LINE 2
 TDXLG ,7
 JMP 4HEAD 4
 TMD C/HLT,StADR+301C/HLT,8
 TDM 4SAVE 02
 TMQ W/DE
 TQM DUM
 TIXZ 18,1
 JMP 4OUT 5
 TMQ STADR+1
 JMP 4OUT 5D
 JMP 4OUT 5B
 TIXZ 48,1 \$ LINE 3
 TMQ AJMSGNO
 CA
 SLAQ 6
 JAZ (P)+2H
 JMP (P)+3H
 SIXO 6,1
 JMP (P)-5H
 SRAQ 6
 TQM DUM
 JMP 4OUT 5
 TIXZ 12,1S
 TMQ W/H
 TQM DUM
 JMP 4OUT 5
 TIXZ 48,1S
 TMQ STADR+10\$
 TQM DUMS
 JMP 4OUT 5\$
 JMP 4OUT 5C
 JMP 4HEAD 4
 TMA AJMSGNO
 JMP 4BCDADD
 TAM AJMSGNO
 R TMA CLSFY \$ LINE 4 IF UNCLAS

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JAZ (P)+4H
JMP (P)+5H
A/ZNR80/3232323254
TMA N/1T151P/(P)-2H,T39
JMP 4OUT 1
TMD L/STADR+40
TDXLC ,7
JMP 4HEAD 4 S LINE 5(4)
JMP 4HEAD 4 S FM LINE
JMP 4HEAD 4 S TO LINE
THA ,7
TMD W/
JAED (P)+2H
JMP (P)-4H
THA C/HLT,1;C/HLT,AFGRNCS
JMP 4OUT 1
JMP 4HEAD=1H

AFGRNC A/AFGRNC10/3254
4HEAD 4 TJM 4OUT 1+5H
TMD N/9T15
TDXRC ,7
TDA
AIXO 10.7
JMP 4OUT 1+1H

4OUT 1 TJM (P)+5H
TAD
JMP PANT.TPANTA
TAD
JMP PANT
JMP

L 4OUT 2 TJM (P)-1H \$ INSERT 0/32 IF HALF WORD BLANK
TDXLC ,4
TDXLC ,0
SIXO 10.0
TDXLC,0
TDXLC,2
TIXZ 1,1
TMQ 24/1:24/0
ETA ,2
ETD W/
JAED 4OUT 2A-2H \$
SRQ 24
ETA ,2
ETD W/
JAED 4OUT 2B
AIXO 1,2
TMD N/10T15
AIXO 1,1
JNO 4OUT 2+7H
TMD 0/32
TDM ,2
4OUT 2A SIXO 1,2
JMP 4OUT 2C

CD

TDXLC,1

TDXRC,0

TDA

TDM 9,0

4OUT 2B JMP 4OUT 2C
JMP 4OUT 2A+2H

4OUT 2C TJM (P)+5H
TMQ 6/1T47
ETA W/
ETD ,2
JAED (P)+2H
JMP
TMA ,2
EI 8/011010
TAM ,2
JON (P)-4H
JQO (P)+1H
SLQ 6
JMP 4OUT 2C+2H

4C1 W/SAT. SUM
W/MARY FOR
W/ STA-XXX
4C2 W/DECAYING
4C3 W/100 DAYS
A/ PAST EPOCH \$
4C4 W/SAT.NO./
W/SET-NO.
\$

4SAVE02S

TMD 4SAVE 02
TDXLC ,2
TDXRC ,0
TDM 4SAVE 02
JMP
4OUT 5 TJM (P)-1H
TMD 4SAVE 02
TDXLC ,2
TDXRC ,0
TDM 4SAVE 02
TMQ DUM
SLAQ 6
TQM DUM
JMP (P)+5H
4OUT 5A CD
SIXO 6,1
JNO (P)=6H
JMP 4OUT 5-5H
TMQ 42/1:6/0
EIS ,2

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CD
SIXO 1,0
JNO (P)+4H
AIXO 1,2
TIXZ 8,0
JMP 4OUT 5A
SLA 6
TAM .2
JMP 4OUT 5A
4OUT 5B TJM 4OUT 5-1H
TIXZ 6,1
TMD W/
JMP (P)+4H
4OUT 5C TJM 4OUT 5-1H
TIXZ 48,1
TMD 7/011010\$1/101100
TDM DUM
JMP 4OUT 5+1H
4OUT5D TJM 4OUT5+1H S
TQA S
TIXZ 0,1 S
TIXZ M/60,0S
SRAQ 6S
TQD S
SRD 10 S
SIXO ,0S
JOF (P)+3H S
AIXO 6,1S
JMP (P)+2H S
SLQ 6 S
JAZ (P)+2H S
JMP (P)-9H S
TQM DUM S
JMP 4OUT5+1HS

S
4SMRYX S
TMD 4SMRYX\$
TDXLC ,6S
JMP (P)S
4SUM4RYTJM (P)-1HS
TXDLC ,6S
TDM 4SMRYX\$
TIJ 4OUT1+3H
TJM 4OUT1+2H
JMP PANT.PAGE
JMP 4CLEAR
TMA STAN
TMO 30/1:18/0
EIS 4C1+2
TMA N/3T15;P/4C1,T39
JMP 4OUT1
JMP PANT.SPACE
TIJR 4NXTTEL+6HS

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JMP 4SET
JMP PANT.SPACE
JMP PANT.SPACE
JMP 4CLEAR
TMA N/1T15;P/4C2,T39
JMP 4OUT1
JMP PANT.SPACE
TIJR 47
TJM 4NXTTEL+6HS
JMP 4SET
JMP PANT.SPACE
JMP PANT.SPACE
JMP 4CLEAR
TMA N/3T15;P/4C3,T39
JMP 4OUT1
JMP PANT.SPACE
TIJR 46
TJM 4NXTTEL+6HS
JMP 4SET
JMP PANT.SPACE
JMP PANT.SPACE
JMP 4CLEAR
TMA N/2T15;P/4C4,T39
JMP 4OUT1
JMP PANT.SPACE
TMD C/HLT,SATNOS S
TDXLC ,1S
TMD L/4BFR\$
TDXLC ,0S
CSM D/1B47\$
TAM 4T13S
CM 4T14S
NXTSET TMO 18/1T47S
ETA ,1S
JAZ NONXSETS END OF SATNOS TABLE
TMO ,1S
JQN (P)+3HS CHECK THIS SATELLITE
AIXO 1,1S
J NXTSETS
TAM SATNS
JMP NXTELM\$
NOP S
TMO 18/1T47 S
ETA SATN
JMP BIN8CDS
TMD BCDSATS
TDM 4T7S
TMA ELNOS
JMP BIN8CDS
TMD BCDSATS
TDM 4T8S
TMA D/1B47\$
AMS 4T13S
JAZ SATONES
J SATTWOS
GET.EL. SET NO.
CONVERT TO BCD
EL SET NO. IN BCD

* THERE WILL BE 4 GROUPS OF THE FOLLOWING PER LINE OF
* OUTPUT FOR SATNO./ELNO. EACH GROUP CONTAINS 3 WORDS
* (SSSSS/EE) ,(EE SSSS) ,(S/EEEE)

* FIRST SAT. IN GROUP

SATONE	TMA	4T7\$	(000SSSS)
	TMQ	0/61T5\$	SLASH
	SLAQ	6\$	(000SSSS/)
	TMQ	4T8\$	(0000EEE)
	SLQ	24\$	(EEEE0000)
	SLAQ	12\$	(EE000000)=Q
	TAM	0,0\$	(SSSSS/EE)=A
	SLAQ	12\$	(000000EE) =A
	TMQ	MASKBLS	
	SLAQ	12\$	
	TAM	1,0\$	(0000EE) =A
	AIXO	1,0\$	
	AIXO	1,1\$	
	J	NXTSETS	

* SECOND SAT. IN GROUP

SATTWO	TMA	0,0\$	(0000EE)
	TMQ	4T7\$	(000SSSS) =Q
	SLQ	18\$	(SSSS000) =Q
	SLAQ	24\$	(EE SSSS) =A
	TAM	0,0\$	
	SLAQ	6\$	
	TMQ	0/61T5\$	SLASH
	SLAQ	6\$	
	TMQ	4T8\$	
	SLQ	24\$	
	SLAQ	24\$	(S/EEEE00)
	TMQ	MASKBLS	
	SLAQ	12\$	(S/EEEE)
	TAM	1,0\$	(S/FEEE)
	AIXO	2,0\$	
	AIXO	1,1\$	
	CSM	D/1B47\$	
	TAM	4T13\$	
	TMA	D/1B47\$	
	AMS	4T14\$	
	TMD	D/4B47\$	
	JAED	(P)+2H\$	
	J	NXTSETS	
	CM	4T14\$	
	TMA	N/12T15;P/4BFR,T39\$	
	JMP	4OUT1\$	
	JMP	4CLEAR\$	
	TMD	L/4BFR\$	
	TXDLC	0,0\$	
	J	NXTSETS	

* END OF SATNOS TABLE

NONXSETCD	\$
TXDLC	0,0\$
TDA	\$
SM	C/HLT,4BFRIC/HLT,0\$
TAM	4T7\$
JAZ	4SUMMRY-3HS
TMA	4T13\$
JAZ	SET00\$
J	SET11\$

* FIRST SAT. IN GROUP

SET00	TMA	0,0\$	(0000EE)
	TMQ	MASKBLS	
	SLAQ	24\$	(EE)
	TAM	0,0\$	
	J	SETEND\$	

* SECOND SAT. IN GROUP

SET11	TMA	4T7\$	
	AM	P/4BFR,T39\$	
	J	SETEND+1\$	
SETEND	TMA	4T7\$	
	AM	C/HLT,13C/HLT,4BFR\$	
	JMP	4OUT1\$	
	JMP	4SUMMRY-3HS	
BINBCD	TJM	BINDONES	BIN.SAT. NO. IN (A)
	CM	BCDSATS	
	TAO	\$	
	TIKZ	0,2	\$
NXTCHARCA		\$	
BINDONEJAEQ	(P)\$		BIN.NO. NOW CONVERTED TO BCD
	DAO	D/10\$	
	SLA	0,2	\$
	AMS	BCDSATS	
	AIXO	6,2	\$
	JMP	NXTCHAR\$	

L 4CLEAR	TJM	(P)+7H	
	TMD	L/4BFR	
	TXDRC	,3	
	TMD	W/	
L	RPTA	11	
	TDM	1,3	
	SIXO	11,3	
	JMP		
L	TAO		
	TMA	1/1T16	
	AMS	(P)+1	
	TOA		
	JMP		

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4NXTTEL TJM (P)-1H
 TMO 18/1T47\$
 ETA .1
 JAZ 4NXTTEL-1HS
 TMD .1
 AIXO 1,1\$
 SCD
 JDP (P)-6H
 JMP 4NXTTEL-5H
 4SET TJM 4SET3-1H
 TMD C/HLT,SATNOS \$
 TDXLC ,1\$
 TMD L/4BFR
 TDM 4T6
 CSM D/1B47\$
 TAM 4T13\$
 CM 4T14\$
 JMP 4NXTTEL
 NOP
 TAM 4T7
 4SET 1 JMP 4NXTTEL
 JMP 4SET 2
 TAM 4T8
 TMA 4T7
 AM D/1B47\$
 TMD 4T8\$ SAT,NOS. CONSECUTIVE ?
 JAED 4SET 3S YES
 TMA 4T7\$
 JMP BINBCDS
 JMP 4COMMA
 JMP 4SET1
 4SET2 TMA 4T7\$
 JMP BINBCDS
 JMP 4BLANKS
 TMA 4T6\$ 4BFR+? IN BOTH HALVES
 TDXLC ,0\$
 SM C/HLT,4BFR\$
 TAM 4T7\$
 TMD C/HLT;C/HLT,4BFR\$ BUFFER EMPTY ?
 JAED (P)+2HS MAYBE
 J GROUPCKS NO
 TMA 4T13\$
 JAN 4SET3-1HS BUFFER IS EMPTY
 J GROUPCKS AT LEAST 1 SATNO. TO PRINT
 TMA D/12B15\$
 INSERT TMO 1/1B15/0:32/1\$
 EIS SLAQ\$
 J ASBLS\$
 GROUPCKTMO JQO AS20R4\$ 2ND OR 4TH SATNO. IN GROUP
 AS00R2 JQO AS3\$ 3RD
 J AS1\$ 1ST
 AS20R4 JQO SLAQ+2HS 4TH
 J AS2\$ 2ND
 AS1 TMA D/12B15\$ FIRST SAT. IN GROUP

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J INSERTS
 AS2 TMA D/24B15\$ SECOND SAT. IN GROUP
 J INSERTS
 AS3 TMA D/36B15\$ THIRD SAT. IN GROUP
 J INSERTS
 ASBL TMA ,0\$
 TMQ MASKBL\$
 L SLAQ SLAQ 0\$
 TAM ,0
 TMQ 15/1T15\$
 ETA 4T7\$
 AM C/HLT,13C/HLT,4BFR\$ NO. WORDS TO PRINT IN LEFT
 * HALF OF A REG. STARTING
 ADDRESS IN RIGHT HALF
 JMP 4OUT 1
 JMP
 4SET 3 TMA 4T7\$
 JMP BINBCDS\$
 JMP 4DASH\$
 JMP 4NXTTEL
 JMP 4SET 2
 TAM 4T8
 TMA 4T7
 TDM 4T9
 AM D/1B47\$
 TAM 4T7
 TMD 4T8
 JAED 4SET3+3H \$
 THD 4T9
 TDM 4T7
 JMP 4SET2-4H \$
 4SLASH TMQ //
 TJM 4DONE\$
 JMP INSERTAS
 4BLANK TMQ W/
 TJM 4DONE\$
 JMP INSERTAS
 4COMMA TMQ W/
 TJM 4DONE\$
 JMP INSERTAS
 4DASH TMQ W/-
 TJM 4DONE\$
 INSERTATMA BCDSATS SAT.NO. IN BCD AT T47
 SLAQ 6\$
 TAM 4T7\$
 JMP 4HALF
 4RESET TMD 4T8\$
 TDM 4T7
 4DONE JMP (P)\$
 4HALF TMD 4T6\$ 4BFR TO
 TDXLC ,0\$ 0X
 TMA 4T14\$ GROUP COUNT
 TMD D/3B47\$
 JAED SAT13\$ LAST SAT. ON THE LINE-13TH.
 TMA D/1B47\$

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AMS 4T13S COUNTS NO. IN GROUP

TAQ \$

JQO SAT20R4\$

SAT002 JQO SAT3S

J SAT1S

SAT20R4JQO SAT4S

J SAT2S

SAT1 TMD 4T7\$ FIRST SAT. IN GROUP
(0011111,)

TDM ,0\$ X0 NOT INCREMENTED HERE

J 4RESETS

SAT2 TMA ,0\$ SECOND SAT. IN GROUP
(0011111,)

TMQ 4T7\$
TDM 1,0\$
SLQ 12S
SLAQ 12S
TAM ,0\$
AIXO 1,0\$
J ASEENDS

SAT3 TMA ,0\$ (0022222,) =A
TMQ 4T7\$ THRD. SAT IN GROUP
TDM 1,0\$ (0033333,)
SLQ 12S (33333,00) =Q
SLAQ 24S (222,3333) =A
TAM ,0\$ (222,3333) =ABUF+1 IST TIME

AIXO 1,0\$
J ASEENDS

SAT4 TAM ,0\$ (11111,22)
TMA ,0\$ (0033333,)

TMQ 4T7\$ 4TH AND LAST SAT IN GROUP

SLQ 12S

SLAQ 36S (3,44444,) =A

TAM ,0\$

AIXO 1,0\$

TMA D/1847\$

AMS 4T14S

CSM D/1847\$

TAM 4T13S

J ASEENDS

SAT13 TMA 4T7\$ LAST=13TH. SAT. ON LINE

TMQ MASKBL\$

SLAQ 12S

TAM ,0\$ XXXXX, **

CM 4T14S

TMA N/10T15:P/4BFR,T39\$

JMP 4OUT1\$

JMP 4CLEAR\$

TMD L/4BFR\$

SETBFRTDM 4T6\$

JMP 4HALF=3HS

ASEND LD \$

TXDLC ,0\$

JMP SETBFERS

BCDSAT \$

4T13 \$

4T14 \$

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REWIND TJM (P)+4H
JMP SYS
TIO ABUF
JMP SYSNO
JMP

NXTCASE JMP PANT.FINISH
CM PHAIN \$ OR 4S3 A
TMA N/7T23JH/BAT47
JMP REWIND
TMA N/8T23JH/BAT47
JMP REWIND
TMA N/9T23JH/BAT47
JMP REWIND

NXTCASE1 JMP (P)+3HS
JMP SATLODS
JMP MANEXIT \$

• RESET

CM PASSONES CN K=160
CQ S CN K=160
JMP ELMLODS CN K=161

TMD W/ MORE \$

TDM AJMRDTAS

TIJ AJINSHR+1H \$

TJM AJINSHR \$

TMD W/ SAT R

TDM AJLN12

TMD W/EV TI

TDM AJLN12+1

TMD C/JMP, SYS; C/TIO, AJBFFX

TDM AJWT89+1

TIJ AJPKITA+3H

TJM AJPKITA-1H

TIJ AJDYCK

TJM AJDLOOP

TIJ GLOP-TGLOP

TJM AJCLU+3H

TIJ GLOP-GLOP

TJM AJHDU+3H

TMD C/ICOZ, 27+128+1IC/TMA, AJELEV

TDM AJFWL6

TMD C/ICOZ, 34+128+1IC/TMA, AJAZ

TDM AJFWL7

TIJ AJDAYSS \$

TJM AJ1OUT \$

TMD C/HLT, 17+128+17IC/TMA, AJUNS

TDM AJFCL

TMD C/HLT, 34+128+34IC/TMA, AJCONS

TDM AJFCF

TDM AJFSC

TMD C/HLT, 22+128+22IC/TMA, AJSCS

TMD C/HLT, 34+128+34IC/TMA, AJNFS

```

TDM AJNF
TMD C/HLT,54+128+54;C/TMA,AJACN2S
TDM AJACN1
TMD W/ $ 
TDM AJBFFR $ 
JMP PANT.PAGE $ 

```

```

* READ SENSOR FILE
READSN$ JMP SNSGETS
TMD C/HLT,SBLOCS
TDXLC ,3S
TMD IEENDS
TDXLC ,4$ 

```

```

R RPTAA 9$ 
TMD 1,3$ 
TMD 1,4$ 
SIXO 9,3$ 
TMA ,3$ 
TMD MASKBLS
JAED (P)+3HS
AIXO 9,3$ 
JMP (P)-8HS

```

```
* CASE BY PASS OPTION
```

```

4A 1 JMP RD6AS
TMA ,3
TMD W/ENDSCHED
JAED 4S3 A
TMD W/END CASE
JAED 4A 1
TAM 4A3-1
TMA N/12T15;P/4A3-2,T39
JMP FLEX
TTD
SCD 1
JDP 4A 4
JMP 4A 2
4A 1A JMP 4S3
JMP RD6AS
TMA ,3
JMP 4A 1+6H
4A2 JMP STOPGOS
JMP 4A 4$ 
JMP 4A 1A$ 
A/STATION XXXX$ 

```

```

4A3 A/JANS
A/FEB$ 
A/MARS
A/APRS
A/MAYS
A/JUNS
A/JUL$ 

```

```

A/AUGS
A/SEPS
A/OCTS
A/NOVS
A/DECS

```

```
* ERROR OUTPUT
```

```

AJERRORNOP
TMA N/6T15;P/AJERR7,T39
JMP PANT
TMA N/10T15
TDXRC ,3
JMP PANT
TMD 4S4 B3-2
TMD 4T9
JMP 4S2
JMP 4S4 B2
AIXO 10,3
JMP (P)-3H

```

```
* DETERMINE TIME
```

```

4A 4 JMP AKLOK
TQM ZULUT
SLQ 12
TQM TFN
TMD L/4A3=1
TDXLC ,0
SRAQ 7
CA
SLAQ 7
TMD D/64
JAGD (P)+7H
SLA 8
TAD
ADXN 0,0
TMD 0,0
TDM MONTH
JMP (P)+3H
SM D/54
JMP (P)-7H
JMP FKLOK
JMP FYKLOK
JMP AJFIXIT
TAM DFN

```

```
* PROCESS CONTROL CARD
```

```

TIJ 4S2
TJM AJERROR+8H
TMQ 12/1T47
ETA 9,3
TMD W/000000RP

```

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JAED (P)+3H
 TMA N/7T15IP/AJERR1,739
 JMP AJERROR+1\$
 TMA C/HLT/C/TIJI,AJSRFHR
 JMP XSRCH
 JAZ AJERROR

 TMA 8,3
 SLA 35
 JAP 4A 4AA
 TMD C/HLT,17*128+17;C/TMA,AJUN1\$
 TDM AJFCL
 TMD C/HLT,34*128+34;C/TMA,AJCON1\$
 TDM AJFCF
 TMD C/HLT,22*128+22;C/TMA,AJSC1\$
 TDM AJFSC
 TMD C/HLT,34*128+34;C/TMA,AJNF1\$
 TDM AJFNF
 TMD C/HLT,54*128+54;C/TMA,AJACN3\$
 TDM AJACN1

 4A 4AA TMA BASE
 FAM BEGT
 TMO YEAR
 JMP BKLOK
 TAM BEGT
 TDM FDAY
 THA BASE
 FAM ENDT
 JMP BKLOK
 TAM ENDT
 FSH BEGT
 TMO F/29
 JAGQF TIME OUT

 CM RSU \$
 CM RSV \$
 CM RSW \$
 TMD 0/3217/110000 \$
 TDM AJUNITS+1 \$
 TMO W/ (NM) \$
 TMA RNGFLAG
 JAZ (P)+2H
 TMO W/ (KM) \$
 TQM AJUNITS
 TMD A/E 0/3216/110000 \$
 TDM AJLN12+6 \$
 TMO W/ \$
 TMA ELFLAG
 JAZ (P)+5H
 TMD A/E FAN30/3260 \$
 TDM AJLN12+6 \$
 TQM AJUNITS+1 \$
 TMO A/ NO.30/321A/ \$
 TQM AJUNITS+2 \$
 TMD W/ \$

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TDM AJUNITS+3 \$
 TDM AJUNITS+4 \$
 TDM AJUNITS+5 \$
 TDM AJLN12+7 \$
 TDM AJLN12+8 \$
 TDM AJLN12+9 \$
 TMA DRCOSPL
 JAZ BYPASS2 \$
 TMD W/ U \$
 TDM AJUNITS+3 \$
 TMD W/ V \$
 TDM AJUNITS+4 \$
 TMD W/ W \$
 TDM AJUNITS+5 \$
 TMD W/ DIRE \$
 TDM AJLN12+7 \$
 TMD W/ CTION CO
 TDM AJLN12+8 \$
 TMD W/SINES \$
 TDM AJLN12+9 \$

 BYPASS2 TMA PRIO \$
 TMD W/
 JAED AJERROR
 CM AJ1STF
 TMA CLSFY
 SLA 8
 TAM CLSFY
 TMD N/5T39
 JAGD AJERROR

 TMA ZFX \$
 TMO ZFY \$
 JHP COMPL \$
 TDM YFX \$
 TQM YFY \$
 TAM YFZ \$
 TMO DE2RA \$
 FMMRS ZFX \$
 FMMRS ZFY \$
 FSIN \$

 S TAM XFX \$
 S FCOS ZFY \$

 S TAM XFY \$
 S TMD F/0 \$
 S TDM XFZ \$
 S FCOS ZFX \$

 S TAM ZFZ \$
 S TMO YFZ \$
 S FMMR XFY \$

TAM	ZFX	\$
FCSM	XFX	\$
FHARS	ZFY	\$
TMA	4C4+2	
JMP	(P)+5H	\$
		\$

TMD	W/ SAT EL
TDM	AJLN12
TMD	W/EM TI
TDM	AJLN12+1

• UNPACK SENSOR RECORD

CSM	D/1815\$
TAM	SATCONT\$
TMQ	1/1T8 \$
ETA	CARDTYP
JAZ	(P)+9H
TMQ	18/1T47
ETA	STAN
ETD	STAID
JAED	LOAD S0
TMD	W/N S AND
TDM	AJERR9+1
TMA	N/4T15IP/AJERR9,T39
JMP	AJERROR+1S
TMD	IEEND\$
TDXL	,4S
TMQ	18/1T47
ETA	,4
ETD	STAN
JAED	LOAD S
ETD	MASKBLS
JAED	(P)+3H
AIXO	9,4
JMP	(P)-6H
TMQ	24/0;24/1
TMA	STAN
SLA	24
EIS	LOAD S-2
TMA	N/3T15IP/LOAD S-3,T39
JMP	AJERROR+5H

A/STATION XXXX NOT ON SEAI\$3

LOAD S	TMD C/HLT,STYPES
	TDXL ,0
	CA
R	RPTAA 9
	THD 1,4
	TDM 1,0
	TMQ STYPE
	SLQ 12

SLAQ	18
TAM	STYPE
TMA	W/
SLAQ	18
TAM	STAID
LOAD S0	SLA 6
	TMO 24/1;18/0;6/1
	EIS LOAD S1-3H
	EIS LOAD S1-5H
	EIS LOAD S1-7H
	JMP LOAD S1

W/FROMXXXA
W/TO XXXA
W/INFOXXXA

• STORE FAN AND ADDRESS DATA
L HLT IREC
LOAD S1 TMD (P)
TDXL ,0
TMD W/
L RPTA 256
TDM 1,0
TMD LOAD AS
TDXRC ,0S
AIXO 10,3\$
LOAD F JMP 4S2
JMP LOAD A1
TMQ 12/1T47
ETA 9,3
ETD W/000000FP
JAED (P)+7H
SRQ 6
ETA 9,3
ETD LOAD S1-3H
JAED LOAD A
LOAD F1 TMA N/5T15IP/AJERR6,T39 \$
JMP AJERROR+5H
TMD C/HLT,AJBFFR+150JC/HLT,(P)+4HS
AIXJ 0,0
TMA N/5T15IP/AJERR5,T39 \$
JMP AJERROR+5H
R RPTAA 10
TMD 1,3
TDM 1,0
TMD W/
TDM 1,0
JMP LOAD F
R LOAD F2 TJM (P)+7H
NOP STADR+50
R RPTAA 9
THD 1,3
TDM 1,4
AIXO 1,3
AIXO 1,4

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JMP

L LOAD A THA W/
TMD AJBFFR
JAED CHKME^L
TAM ,0
TMA 9,3
TMD LOAD S1-7H
JAED (P)+3H
LOAD A1 TMA N/3T15;P/AJERR3,T39
JMP AJERROR+5H
TMD LOAD F2+1H
TDXLC ,4

TMD C/HLT,STADR+9;C/HLT,STADR-1
TDM STADR+9
JMP LOAD A7
TIXZ 18,2
TIXZ 30,1
TMA W/00000FM
JMP LOAD A9
JMP 4S2
JMP LOAD A1
TMA 9,3
TMD LOAD S1-5H
JAED (P)+2H
JMP LOAD A1
JMP LOAD A7
TIXZ 18,2
TIXZ 30,1
TMA W/00000TO
JMP LOAD A9
JMP 4S2
JMP LOAD A1
TMA 9,3
TMD LOAD S1-5H
JAED (P)+2H
JMP (P)+6H
JMP LOAD A7
JMP 4OUT 2
JMP (P)-8H
LOAD A3 TMA N/5T15;P/AJERR10,T39
JMP AJERROR+5H

LOAD A4 JMP 4S2
JMP LOAD A5
TMA 9,3
TMD LOAD S1-3H
JAED (P)+2H
JMP LOAD A5
JMP LOAD A7
TIXZ 30,2
TIXZ 18,1
TMA W/000INFO
TIJ LOAD A6+1H

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TJM LOAD A6
JMP LOAD A9
JMP 4S2
JMP LOAD A5
THA 9,3
TMD LOAD S1-3H
JAED (P)+2H
JMP LOAD A5
JMP LOAD A7
JMP 4OUT 2
JMP (P)-8H

JMP 4S2
JMP 4A20
AIXO 10,3
JMP (P)-3H
LOAD A5 TMD C/HLT,STADR+20;C/HLT,8
TDM 4SAVE 02
THA PRIO
SRQD 12
TQM DUM
TIXZ 12,1
JMP 4OUT 5
JMP 4OUT 5B
TMD L/STADR \$
TDXLC ,7
TMQ 0,7
TDM SAVE
JMP LDA5
LDA5A THA 0,7
TMD W/
JAED LDA5B
TMD SAVE
JAED LDA5B
TAM SAVE
JMP 4OUT5B
TMQ 0,7
LDA5 JMP 4OUT 5D
LDA5B TMD STADR+9
AIXOR 1,7
JNO LDA5A
JMP 4OUT 5C

TMD C/HLT,STADR+40;C/HLT,8
TDM 4SAVE 02
THA PRIO
SRQD 12
TQM DUM
TIXZ 6,1
ETA 12/1T11
ETD W/YY
JAED (P)+5H
ETD W/00
JAED (P)+3H
TIJ LOAD A6+7H

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TJM LOAD A6
JMP 4OUT 5
JMP 4OUT 5B
LOAD A6 JMP (P)+7H
TIJ (P)+6H
TJM (P)-2H
TMQ W/P
TQM DUM
TIXZ 12,1
JMP 4OUT 5
TMA ZULUT
TMQ W/Z
SRA 12
SRAQ 36
TQM DUM
TIXZ 42,1
JMP 4OUT 5
TMD W/ ZEX
TDM DUM
TIXZ 24,1
JMP 4OUT 5
JMP 4OUT 5C

TMQ ZULUT
SLAQ 12
SLA 6
SLAQ 24
SLA 6
AM 0/61T17;0/71T47
TAM DUM
TMD C/HLT, STADR+10\$C/HLT, 8
TUM 4SAVE 02
TIXZ 48,1
JMP 4OUT 5
JMP 4OUT 5B
TMD MONTH
TUM DUM
TIXZ 18,1
JMP 4OUT 5
JMP 4OUT 5B
TMQ STADR+1
JMP 4OUT 5D
JMP 4OUT 5C
JMP LOADA5-4H \$

LOAD A7 TJM LOAD F2+7H
TMA N/10T15
TXDRC ,3
JMP PANT
TMA W/
TMQ 8,3
JAED LOAD A8
TAM 8,3
TMA N/1T39
AMS STADR+9

TDXRC ,0
SIXO 1,0
JOF LOAD A8+1
TQM 0,0
JMP LOAD F2+1H
LOAD A8 TMA N/3T15JP/AJERR11,T39
JMP AJERROR+5H
TMA N/3T15JP/AJERR12,T39
JMP AJERROR+5H
\$
LOAD A9 TJM 4OUT 2-1H
TMD LOAD A9-1
TXDLC ,4
TXDLC ,0
SIXO 1,0
TXDLC ,0
SIXO 9,0
TXDRC ,0
TDM LOAD A9-1
THQ ,0
SRAQ ,2
TMA ,0
TQM ,0
NOP 5
TMD LOAD A9-1
AIXOL 1,0
JNO (P)-7H
JMP 4OUT 2+1H

* EDIT ALL, ALL BUT, OR ONLY CARDS
*
4A 10 JMP 4S1
TMA ,3
TMD W/ALL
JAED 4A 10A
TMD W/ALL BUT
JAED 4A 10A+2
TMD W/ONLY
JAED 4A 10A+3
JMP LOAD A3

* 4A 10A JMP 4S2
JMP 4A20
AIXO 10,3
JMP (P)-3H
CD
JMP (P)+3H
JMP 4S1 A
TMD 1/1
TDM 4T3
AIXO 1,3
TIXZ 9,1
TIXZ 9,0
TMD ,3

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TDM 4T 11
4A 10B JMP 4S4 B
TMD 4T6
TDM 4T5
TMO 4T9
JOO 4S4 B1
JOO 4A 10C+3H
JOO 4A 10C+6H
4A 10C TIJ 4A 10F+1H
TJM 4A 10F
JMP 4A 10D-4H
JOO (P)+1H
JOO 4A 10C
JMP 4A 10D-4H
JOO 4A 10C
JHP 4S4 B
TMO 4T9
JOO 4S4 B1
JOO (P)+3H \$
JOO 4S4 B1
JHP 4A10C \$
TMA 4T5
TMD 4T6
JAED (P)+2H
JAGD 4S4 B1
4A 10D TAO
CA
JMP FXINT
TAQ
TMA FXERCL
JAZ 4BCDADD-3H
TQA
TMD C/HLT,SATNOS
TDXLC ,4S
TMO 18/1T47\$
R 4A 10D1RPTAN 1000\$
ETD 1,4\$
JAED (P)+2H
JMP 4A 10E
SIXO 1,4\$
TMO 1/0347/1
TMA 4T3
EIS ,4
4A 10E TMA 4T5
JMP 4BCDADD
TAM 4T5
TMD 4T6
JAED 4A 10D
JAGU (P)+2H
JMP 4A 10D

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4A 10F JMP 4A 10B
TIJ 4A 10B
TJM (P)-2H
4A 20 TMD P/AJBFFR,T15\$P/FANTAB,T39
TDXLC ,3
TDXRC ,6
TIXZ ,5
CM TRFLG
CM FNCONT
TIJ FNOTAB
TJM STIKFN
TMD W/N R AND
TDM AJERR9+1
4A 21 TMA ,3
TMD W/
JAED (P)+2H
JHP AJFCARD
TMD W/ZZZZZZZ
TDM ,6
CM PHAIN
TMO W/ZZZZZZZ
TMA FANTAB
JAEO AJNORMX
TMA FANTAB+12
JAEO AJNORMX
TMD P/FANTAB,T15
TDM TEMP2
TDXLC ,4
TMD 5,4
TDM TEMP1
SRT1 AIXO 12,4
TMA 0,4
TMD W/ZZZZZZZ
JAED SRT2
TMA 5,4
TMO TEMP1
JAGOF SRT1
TAM TEMP1
CD
TDXLC ,4
TDM TEMP2
JMP SRT1
SRT2 TMD TEMP2
TDXLC ,4
TMD P/FANTAB,T15
TDXLC ,6
R DRNNAA 12
TMA 0,4
TMD 0,6
TDM 1,4
TAM 1,6

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AJNORMX	TMD	P/AJBFFR,T15
TDM		AJCOL79
TMO	BEGT	\$ DETERMINE
JMP	AJFIXIT	\$ NUMBER
SLA	17	\$ OF
TMO	F/1073741824.	\$ MINUTES
FMARS	AJHOLD	\$ EXPIRED
TMA	BEGT	\$ IN
FSM	AJHOLD	\$ BEGINNING
TMO	F/1440.	\$ DAY
FMARS	AJHOLD	\$ REQUEST.
TMA	RNGFLAG	\$ NM
JAZ	(P)+2	\$ OR
TMA	XKMPER	\$ KM
TMO	ERK2KMS	\$ CONVERSION
JMP	(P)+2	\$ FACTORS
TMA	ERK2KMS	\$ FOR
FDA	F/1.8525	\$ RANGE CNT260
TMA	XNMPER	\$ AND
TAM	AJCNV1	\$ RANGE
TQM	AJCNV2	\$ RATE.
JMP	START1	\$
AJFCARD	TMA	C/HLT,0;C/TIYL,AJSRFWE
JMP	XSRCH	S SET UP FANTAB FROM F CARDS
JAZ	AJERROR	\$ AND CHECK INPUT.
TMA	AJFNTAB	\$
FAM	F/90.0	\$
JAP	AJREGFN	\$
TMA	TRFLG	\$ INTERPRET TRACKER CARD
JAZ	(P)+3H	\$
TIXZ	1,4	\$
JMP	TRERR	\$
TMD	F/5	\$
TDM	PHAIN	\$
TIXZ	0,4	\$
TMA	C/HLT,0;C/TIYL,AJSRFWF	\$
JMP	XSRCH	\$
JAZ	THERR	\$
TMD	L/TEMPO	\$
TDXLCL	/4	\$
R	RPTAA	11
TMD	1,4	\$
TDM	1,6	\$
SIXO	11,6	\$
TMA	10,6	\$
JAZ	AJFC1	\$
TIXZ	2,4	\$
TMU	0,6	\$
FMMR	0,6	\$
FSM	F/1	\$
JAP	TRERR	\$
TAU		\$
FCSQ		\$
TMO	F/1	\$

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S	JAEQ	TRERR	\$
	FSORT		\$
	TAM	3,6	\$
	TMO	1,6	\$
	FMMR	1,6	\$
	FSM	F/1	\$
	JAP	TRERR	\$
	TAQ		\$
	FCSQ		\$
	TMO	F/1	\$
	JAEQ	TRERR	\$
	FSORT		\$
S	TAM	4,6	\$
	TMO	DE2RA	\$
	FMMRS	AJFNTAB+2	\$
	TMD	F/0	\$
	JAED	TRERR	\$
	FCOS		\$
S	TAM	2,6	\$
	FSIN	AJFNTAB+2	\$
	TAM	SINPSI	\$
AJFC1	TIXZ	3,4	\$
	TMA	7,6	\$
	TMO	F/2	\$
	JAGQF	(P)+2H	\$
	JMP	TRERR	\$
	TIXZ	4,4	\$
	TMD	F/9	\$
	JAED	(P)+2H	\$
	JMP	AJFC2	\$
	FCAMAS	8,6	\$
	TMD	F/0	\$
	JAED	TRERR	\$
AJFC2	TMA	RCPTST	\$
	JAZ	AJFC3	\$
	TIXZ	5,4	\$
	TMA	F/0	\$
	TMO	9,6	\$
	JAGQF	TRERR	\$
	FMMR	ERPKM	\$
	TAM	9,6	\$
AJFC3	TMA	AJFNTAB+1	\$
	TMO	F/90	\$
	TIXZ	6,4	\$
	JAGQF	TRERR	\$
	TMO	DE2RA	\$
	FMARS	AJFNTAB+1	\$
S	FSIN		\$
	TAM	5,6	\$

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S	FCOS	AJFNTAB+1	\$
TAM	6,6		\$
TMD	0/3710/63T47		\$
TDM	11,6		\$
TMA	ELMAX		\$
TMD	F/0		\$
JAED	(P)+4H		\$
TMO	DE2RA		\$
FMARS	ELMAX		\$
JMP	(P)+3H		\$
TMD	F/2		\$
TDM	ELMAX		\$
TJM	TRFLG		\$
AIXO	1,5		\$
AIXO	10,3		\$
AIXO	12,6		\$
JMP	4A21		\$
TRERR	TMA C/HLT, SIC/HLT, TRCOM7		\$
JMP	PANT		\$
TMA	N/10T15		\$
TXDRC	,3		\$
JMP	PANT		\$
TMD	P/TRCOM-1, T39		\$
ADXR	,4		\$
TMA	,4		\$
JMP	PANT		\$
AIXO	10,3		\$
JMP	PANT, SPACE		\$
JMP	4A21		\$
L	HLT	7	\$
L	HLT	AJERR7	\$
L TRCOM4	HLT	4	\$
	HLT	TRCOM1	\$
	HLT	4	\$
	HLT	TRCOM2	\$
	HLT	3	\$
	HLT	TRCOM3	\$
	HLT	2	\$
	HLT	TRCOM4	\$
	HLT	3	\$
	HLT	TRCOM5	\$
	HLT	4	\$
	HLT	TRCOM6	\$
TRCOM41	A/ONLY 1 TRACKER CARD ALLOWEDS		

TRCOM42 A/LIMITS ON BORESIGHT ANGLFS WRONGS

TRCOM43 A/POINTS PER PASS WRONGS

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TRCOM4 A/DELTA T IS ZEROS
 TRCOM5 A/MAX. RANGE IS WRONGS
 TRCOM6 A/MIN. ELEV. GREATER THAN 90S
 TRCOM7 A/ERROR ON TRACKER CARD. CARD REJECTEDS

L	AJSRFWFICOZ	6*128+6	\$
	TMA	AJFNTAB	\$
	ICOZ	24*128+6	\$
	TMA	AJFNTAB+1	\$
	ICOZ	25*128+1	\$
	TMA	TEMP7	\$
	JBT	27*128+1	\$
	TMA	TEMP10	\$
	ICOZ	36*128+6	\$
	TMA	TEMP8	\$
	ICOZ	42*128+6	\$
	TMA	TEMP0	\$
	ICOZ	48*128+6	\$
	TMA	TEMP1	\$
	ICOZ	54*128+6	\$
	TMA	AJFNTAB+2	\$
	ICOZ	66*128+6	\$
	TMA	ELMAX	\$
	ICOZ	60*128+6	\$
	CAM	TEMP9	\$
L	RSTSTWD	0	\$
	HLT	AJREG1	\$

AJREGFNAIXO	3,3	\$
TMD	RSTSTWD	\$
TXDLC	,3	\$
TDM	RSTSTWD	\$
AIXO	5,3	\$
TMO	1,3	\$
TMD	F/6	\$
TDM	PHAIN	\$
AJREG1	TMA	\$
	SRAQ	\$
	TQM	\$
	SRAQ	\$

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TMD	RSTSTWD	\$
SIXJ	1,3	\$
SIXO	3,3	\$
TMA	0/60T47	\$
TMQ	42/1T41	\$
EIS	4,3	\$
EIS	9,3	\$
TJM	FNFLG	\$
AJRE32 TMA	0,3	\$
TMD	W/	\$
JAED	AJREG4	\$
TIXZ	0,4	\$
TMA	C/HLT,01C/TIJL,AJSRFWD	\$
JMP	XSRCH	\$
JAZ	FNERR	\$
TMQ	AJFNTAB+6	\$
SLAQ	42	\$
SLA	30	\$
SLAQ	6	\$
TAM	11,6	\$
TIXZ	1,4	\$
TMQ	6/1T47	\$
ETA	11,6	\$
TMD	0/47T47	\$
JAED	CONVP	\$
TMD	0/30T47	\$
JAED	CONVH	\$
JMP	FNERR	\$
CONVP TMA	AJFNTAB+3	\$
TMQ	AJFNTAB	\$
JAGQF	AJREG3	\$
TQM	AJFNTAB+3	\$
TAM	AJFNTAB	\$
TMA	AJFNTAB+1	\$
TMD	AJFNTAB+4	\$
TDM	AJFNTAB+1	\$
TAM	AJFNTAB+4	\$
TMA	AJFNTAB+2	\$
TMD	AJFNTAB+5	\$
TDM	AJFNTAB+2	\$
TAM	AJFNTAB+5	\$
AJREG3 TMA	AJFNTAB	\$
TMQ	AJFNTAB+1	\$
JMP	COMPL	\$
TDM	3,6	\$
TQM	4,6	\$
TAM	5,6	\$
TMA	AJFNTAB+3	\$
TMQ	AJFNTAB+4	\$
JMP	COMPL	\$
TDM	6,6	\$
TQM	7,6	\$
TAM	8,6	\$
TMQ	3,6	\$
FMMR	6,6	\$

S	TMQ	4,6	\$
	FMAD	7,6	\$
	TMQ	5,6	\$
	FMAD	8,6	\$
	TAM	LDOTL	\$
	FCAMA	LDOTL	\$
	FSM	F/.9998477	\$
	TIXZ	2,4	\$
	JAP	FNERR	\$
	FACOS	LDOTL	\$
S	TAM	10,6	\$
	TMQ	LDOTL	\$
	FMMR	LDOTL	\$
	TMQ	F/1	\$
	FMSU	F/1	\$
	FSQRT		\$
S	TAM	2,6	\$
	TMQ	5,6	\$
	FMMR	7,6	\$
	TMQ	4,6	\$
	FMSU	8,6	\$
	FDA	2,6	\$
	TQM	0,6	\$
	TMQ	3,6	\$
	FMMR	8,6	\$
	TMQ	5,6	\$
	FMSU	6,6	\$
	FDA	2,6	\$
	TQM	1,6	\$
	TMQ	4,6	\$
	FMMR	6,6	\$
	TMQ	3,6	\$
	FMSU	7,6	\$
	FDAS	2,6	\$
	JMP	CONVOUT	\$
CONVH	TIXZ	4,4	\$
	TMQ	AJFNTAB	\$
	TMA	F/89	\$
	JAGQF	(P)+2H	\$
	JMP	FNERR	\$
	FMMR	DE2RA	\$
	TAM	AJFNTAB	\$
S	FSIN		\$
S	TAM	5,6	\$
	FCOS	AJFNTAB	\$
	TAM	6,6	\$
	TIXZ	5,4	\$
	TMA	AJFNTAB+1	\$
	TMQ	AJFNTAB+4	\$

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JAEQ	FNERR	\$	
TQM	1,6	\$	
TMO	DE2RA	\$	
FMARS	0,6	\$	
FMMRS	1,6	\$	
FSM	0,6	\$	
JAP	(P)+2H	\$	
FAM	TWOP1	\$	
TAM	10,6	\$	
CONVOUTTMA	AJFNTAB+2	\$	
TIKZ	3,4	\$	
TMO	F/0	\$	
JAEQ	FNERR	\$	
TAM	9,6	\$	
TMA	AJFNTAB+5	\$	
JAEQ	FNERR	\$	
FSM	9,6	\$	
FDAS	10,6	\$	
TMO	ERPKM	\$	
FMMRS	9,6	\$	
FMMRS	10,6	\$	
		\$	
TMD	11,6	\$	
STIKFN	TDM (P)	\$	
TMA	FNCONT	\$	
SLA	10	\$	
TMO	42/1T47	\$	
EIS	11,6	\$	
INCA	STIKFN	\$	
INCA	FNCONT	\$	
AIXO	12,6	\$	
AIXO	1,5	\$	
AJREG34	AIXO 5,3	\$	
TMA	FNFLG	\$	
JAZ	4A21	\$	
CM	FNFLG	\$	
JMP	AJREG2	\$	
COMPL	TJM COMPLX	\$	
TQM	TEMP2	\$	
TMO	DE2RA	\$	
FMARS	TEMP1	\$	
FMMRS	TEMP2	\$	
S	FCOS	\$	
		\$	
S	TAM FSIN	TEMP3 TEMP2	\$
			\$
S	TAM FCOS	TEMP2 TEMP1	\$
			\$
TAD	TEMP2	\$	
FMMR	TEMP2	\$	
TAM	TEMP2	\$	

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S	FCSM	TEMP3	\$	
	FMARS	TEMP3	\$	
	FSIN	TEMP1	\$	
			\$	
	TMO	TEMP2	\$	
	TMD	TEMP3	\$	
	COMPLX	JMP (P)	\$	
	DOTPR	TDM TJM	TEMP6 DOTPRX	\$
		TAM	TEMP4	\$
		FMMR	TEMP2	\$
		TMO	TEMP4	\$
		FMAD	TEMP1	\$
		TMO	TEMP6	\$
		FMAD	TEMP3	\$
	DOTPRX	JMP (P)	\$	
	FNERR	TJM	FNERRX	\$
		TAM	TEMP1	\$
		TMA	0/3T15	\$
		CD		\$
		TXDLC	,4	\$
		JAEQ	(P)+2H	\$
		JMP	(P)+3H	\$
		TMA	RCPTST	\$
		JAZ	FNERRX-1H	\$
		TMA	C/HLT,53C/HLT,FNCOM6	\$
		JMP	PANT	\$
		TMA	N/5T15	\$
		TXDRC	,3	\$
		JMP	PANT	\$
		TMD	P/FNCOM-1,T39	\$
		ADXR	,4	\$
		TMA	,4	\$
		JMP	PANT	\$
		JMP	PANT.SPACE	\$
		JMP	AJREG4	\$
		TMA	TEMP1	\$
	FNERRX	JMP (P)	\$	
L	HLT	7	\$	
L	HLT	AJERR7	\$	
L	FNCOM4	HLT 3	\$	
		HLT	FNCOM1	\$
		HLT	4	\$
		HLT	FNCOM2	\$
		HLT	3	\$
		HLT	TRCOM5	\$
		HLT	4	\$
		HLT	FNCOM4	\$
		HLT	3	\$
		HLT	FNCOM5	\$
	FNCOM41	A/FAN TYPE NOT H OR P\$	\$	

FNCOM2 A/FAN ENDS TOO CLOSE TO COLINEARS \$

FNCOM4 A/ELEVATION GREATER THAN 89 DEGS \$

FNCOM5 A/AZIMUTH LIMITS ARE EQUALS \$

FNCOM6 A/ERROR IN FAN RECORD. RECORD REJECTED\$

L	AJSRFWDICOZ	6*128+6	\$
TMA	AJFNTAB	\$	
ICOZ	12*128+6	\$	
TMA	AJFNTAB+1	\$	
ICOZ	18*128+6	\$	
TMA	AJFNTAB+2	\$	
ICOZ	24*128+6	\$	
TMA	AJFNTAB+3	\$	
ICOZ	30*128+6	\$	
TMA	AJFNTAB+4	\$	
ICOZ	36*128+6	\$	
TMA	AJFNTAB+5	\$	
HLT	39*128+3	\$	
CAM	AJFNTAB+6	\$	

AJ79F W/ FS
AJERR1 A/FAN PARAMETER (REQUEST) CARD MISSING (NO R IN COS)

A/L 79).\$

AJERR2 A/NO FAN CARDS AND NO MAX. ELEV. REQUESTS

AJERR3 A/ADDRESS CARD MISSING\$ 3

AJERR4 A/PRIORITY NOT PUNCHED IN PARAMETER (REQUEST) CARD.\$

AJERR5 A/MORE THAN THIRTY RECORDS IN F TYPE CARD\$

AJERR6 A/ILLEGAL CARD EXISTS AFTER F CARDS.\$

AJERR7 A/CHECK INPUT DATA FOR ILLEGAL CHARACTERS IN FIELDS.\$

AJERR9 A/STA,NO.ON R AND F CARDS DIFFER.\$

AJERR10A/ALL, ALL BUT, OR ONLY CARDS MISSING\$5

AJERR11A/ROUTING DATA MISSING\$ 3

AJERR12A/TOO MANY ROUTE CARDS \$ 3

AJSRFWRHLT	4*128+4	\$
TMA	STAN	\$
ICOZ	12*128+7	\$
TMA	BEGT	\$
ICOZ	19*128+7	\$
TMA	ENDT	\$
ICOZ	29*128+4	\$
TMA	BEAMW	\$
HLT	33*128+4	\$
TMA	YEAR	\$
JBT	34*128+1	\$
TMA	ELFLAG	\$
JBT	35*128+1	\$
TMA	RNGFLAG	\$
JBT	37*128+1	\$
TMA	CLSFY	\$
HLT	39*128+2	\$
TMA	PRI0	\$
JBT	41*128+1	\$
TMA	VPASS	\$
JBT	43*128+1	\$
TMA	DPASS	\$
JBT	45*128+1	\$
TMA	FNCPA	\$
JBT	47*128+1	\$

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TMA	RCPTST	\$
JBT	49+128+1	\$
TMA	CONTG	\$
JBT	57+128+1	\$
TMA	DRCOSFL	\$
ICOZ	64+128+7	\$
TMA	ZFX	\$
ICOZ	71+128+7	\$
TMA	ZFY	\$
JBT	72+128+1	\$
TMA	4C4+2	\$
AJSRFWHLHT	79+128+1	\$
CAM	AJCOL79	\$
AJSRFWEICOZ	6+128+6	\$
CAM	AJFNTAB	\$
TIMEOUTJM	TIMEX	\$
TMA	F/29	\$
FAM	BEGT	\$
TAM	ENDT	\$
JMP	FYKLOK	\$
TQM	TEMPO	\$
TMA	C/HLT,0;C/TIYL,TIM01	\$
JMP	GLOP.GLOP	\$
TIMEY	JMP (P)	\$
L TIM01	HLT	69+128+51
TMA	TIM02	\$
ICOZ	77+128+3	\$
CAM	TEMPO	\$
TIM02 A/REQUESTED TIME EXCEEDS 29 DAYS. END TIME CHANGED TO S		
CHKMEL	TMA	FNCPA
JAZ	(P)+4H	\$
TMD	F/0	\$
TOM	FANTAB+5	\$
JMP	LOAD A1-3H	\$
TMA	C/HLT,5;C/HLT,AJERR2	\$
JMP	AJERROR+5H	\$
MASKBL W/		
MASKSATO/777777T47		
MASK1 1/1TO		
MASK2 W/0000ZLLL		
* AJFNTABASTOR 7		
AJBFFR W/		
SET	(P)+150	\$
FNOTAB SET	(P)+30	\$
W/++		
W/T		

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OCTALA SET	(P)+50	\$
TEMP0	S	\$
TEMP1	S	\$
TEMP2	S	\$
TEMP3	S	\$
TEMP4	S	\$
TEMP5	S	\$
TEMP6	S	\$
TEMP7	S	\$
TEMP8	S	\$
TEMP9	S	\$
TEMP10	S	\$
BUF1		\$
BUF2		\$
BUF3		\$
BUF4		\$
BUF5		\$
BUF6		\$
BUF7		\$
BUF8		\$
XLSUNT		\$
ALSUN		\$
CSALS		\$
SNALS		\$
DLSUN		\$
CPT		\$
SNDLS		\$
CSDLSS		\$
SUNLK		\$
SUNLY		\$
SUNLZ		\$
SNHSN		\$
CSHSN		\$
CSAN		\$
HSUN		\$
CSPST		\$
SAVE	S	
STYPE	S	
STNM	S	
STNM2	S	
PHIRD	S	
XLAMBA	S	
OALT	S	
XOVCT	S	
CAPZ	S	
STGAR	S	
STAID	S	
AJFNFLDS		
AJCAPRQS		
RMAX	S	
BEAMW	S	
XINTRV	S	
AJSVXR1S		
AJSV34	S	
AJSV56	S	

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AJSV7 \$
AJPAGESS
AJTYSW \$
AJSMDAYS
AJHR \$
AJMIN \$
AJFRMIVS
AJSAT \$
AJAZ \$
AJREV \$
AJRANGES
AJRRATES
AJELEV \$
AJDEPRES
AJDAY \$
AJDDD \$
AJDATE \$
AJTM17 \$
AJMSGNOS
ZULUT \$
TFN \$
MONTH \$
DFN \$
AJCOL'79\$
YEAR \$
FDAY \$
BEGT \$
ENDT \$
PRIO \$
AJ1STF \$
CLSFY \$
CLAS \$
AJSSAVES
AJSTAIDS
AJFLGITS
AJSVSV \$
AJCKENDS
BASE \$
VPASS \$
DPASS \$
FCAP \$
RCPTST \$
CONTG
STAN \$
AJSTAN \$
AJKPxR3\$
ELFLAG \$
RNFLAG \$
AJHOLD \$
AJCNV1 \$
AJCNV2 \$
AJNMBLKS
AJSTBK \$
AJCHNBKS
AJDNONTS

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AJMRGSHS
4LMAX
4LMAX2
4RMAX
IEEND
ILOCE
IRSET
NOELM
PHAIN
PSATN
AJFAN
AJSAT1
ATYPE
SINHMIN
COSHMIN
TRDELT
TRFLG
PPP
TRTYPE
XL1X
XL1Y
XL1Z
XL2X
XL2Y
XL2Z
A1H
A2H
SINHREF
COSHREF
RHOMAX
RHODMAX
DRCOSFL
FANNO
FNCONT
FNFLG
UMAXT
RT1MUS
VMAXT
RT1MVS
CCPHTH
CDEL
CNMT
COSPSSI
CPSI
CSPHTH
DT
EPOCHM
EPS
EPSLN
ERR
FNCPA
K1
LDOTL
LSTT
MARG

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N
OBSAZ
OBSEL
OBSRR
OLD ONE
PAR1
PAR2
PAR3
PAR4
Q2
RHO
RHODDOT
RHODOT
RHODOTN
RHOSORO
RHOXH
RHOYH
RHOZH
RSU
RSV
RSW
SDEL
SINPSI
SNMT
SPCI
STST
T1
T2
TEM1
TF
THTAO
THTAI
TI
VISIBLE
XF_X
XF_Y
XF_Z
YF_X
YF_Y
YF_Z
ZFX
ZF_Y
ZF_Z
XILLUM
XNXH
XNYH
XNZH
ZDOTW
SATCONT

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* * * * * MAIN PROGRAM STARTS HERE * * * * *

START1 CM PHAIN
JMP INITEL
JMP SINIT
NXTTEL TMD F/1
TDM PHAIN
TMA C/HLT, SATNOS
AM SATCONT
TAD
TDXLC ,0
NXTTEL'1 TMA 0/1T15
AMS SATCONT
AIXO 1,0
TMO 1/1T0
ETA 0,0
JAN NXTTEL2
TMA 0,0
JAZ AJENDPK
JMP NXTTEL1
ETA 0,0
JAZ AJENDPK
TAM SATN
JMP NXTELM
JMP NXTTEL1
JMP EINIT
TMO XNO
TMA F/.072220521
JAGQF (P)+4H
TMD 1/1T1
DORMS 0,0
JMP NXTTEL1
TMA EPOCH
FSM ENDT
TMO F/-100
JAGQF (P)+3H
TMD 1/1T2
DORMS 0,0
START2 TMD F/3
TDM PHAIN
JMP NXPASS
JMP NXTTEL
TMO RHO
FMMR EPSLN
FMSU FANTAB+5
TMO RHOZH
JAGQF START2
TMA FNCPA
JAZ (P)+5H
JMP RHARR
TMD 0/36 T5
TDM FANNO
JMP STORE
JMP AINIT
START3 TMD F/2

\$ ERROR EXIT RETURNS TO NXCASE
\$ SET ERROR EXIT TO RETURN
\$ TO NXTTEL.
\$ GET NEXT SATELLITE TO BE
\$ PROCESSED FROM SATNOS TABLE.
\$
\$ ALL SATELLITES DONE
\$
\$ ALL SATELLITES DONE
\$ UNPACK ELEMENT SET
\$ IF SATELLITE NOT FOUND
\$ INITIALIZE FOR SATELLITE
\$
\$ SATELLITE NOT IN DECAY
\$ IRS MUST BE PRESERVED
\$ SATELLITE IN DECAY
\$
\$ NO MORE PASSES
\$
\$ SATELLITE CANNOT BE SEEN.
\$ FIXED FANS BEING PROCESSED
\$ AND CPA REQUESTED.
\$ INITIALIZE NXACQ ROUTINE
\$ SET ERROR EXIT TO RETURN

```

TDM PHAIN          S TO START3,
JMP NXACQ          S GET NEXT ACQUISITION MODEL
JMP (P)+2H          S NO MORE ACQ. MODELS
JMP START4          S NORMAL RETURN FROM NXACQ
JMP ENDPK          S FINISH UP THIS PASS
TMD F/1            S SET ERROR EXIT TO RETURN
TDM PHAIN          S TO NXTEL.
JMP START2          S GO BACK AND GET NEXT PASS.

* START4 JMP AQUIRE          S PROCESS ACQ. MODEL
  JMP START3          S GO BACK AND GET NEXT ONE.

* * * * * MAIN PROGRAM ENDS HERE * * * * *

```

```

AFEND 42S
HACQUI TJM HACQUIX
CM PAR4
FCSM EPSLN
TMQ COSHREF
FMAR SINHREF
TMQ RHO
FMAR
TMQ RHOZH
JAGQF HACQUIX
TMD TI
TDM PAR2
TMD F/10.0
TDM DT
HACQ3 TMQ RHO
FMMR SINHREF
FSM RHOZH
TAQ
FCAQAS TEMP1
TMQ RHO
FMMR EPSLN
TMQ COSHREF
FMAR
TMQ TEMP1
JAGQF HACQ1
HACQ8 TMA F/1.0$ DT = SIGN OF PAR3(RHOZH-RHO+SINHREF)
TAM PAR3
TMA DT
FAMS TI
JMP CRHOB
TMQ RHO
FMMR SINHREF
TMQ RHOZH
JAGQF HACQ2
JMP HACQ3
HACQ2 TMQ DT
TMA F/.5
FMAKS TEMP1
TMQ RHO
FMMR SINHREF
FSM RHOZH
TAM TEMP2
TMQ PAR3
FMAR
TMQ TEMP1
JAN HACQ4
FCSQ
TAQ
HACQ4 TQM DT
FCSM TEMP2
TAM PAR3
TQA
FAMS TI
JMP CRHOB
SET PAR4=0
TEST IS RHO(SIN(HREF)-EPSLN+COS(HREF)) GREATER THAN OR
EQUAL TO RHOZH
SET PAR 2=TI
SET DT=-10
TEST IS RHO+EPSLN+COSHREG GREATER
THAN OR = ABS( RHOZH-RHO+SINHREF )
TEMP1=ABS(RHOZH-RHO+SINHREF)
SUBROUTINE
TEST IF RHO+SINHREF IS GREATER
THAN OR = RHOZH
DT = SIGN OF PAR3(RHOZH-RHO+SINHREF)
TEMP1= DT+.5
TEMP2= RHO+SINHREF - RHOZH
DT
SET PAR3= RHOZH- RHO+SINHREF
SET TI=TI+DT

```

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```

TMO      RHO          TEST IF RHO+EPSLN+COSHREF > OR =
FMMR     SINHREF      ABS(RHOZH-RHO+SINHREF)
FSM      RHOZH
TAQ
FCAQAS   TEMP1        TEMP1=ABS(RHOZH-RHO+SINHREF)
TMO      RHO
FMMR     EPSLN
TMO      CUSHREF
FMAR
TMO      TEMP1
JAGOF    HACQ1
JMP      HACQ2
HACQ1    JMP      RMARR      SUBROUTINE
TMA      ATYPES      TEST FOR TRACKER TYPE
TMD      W/0000000TS
JAED     HACQ1KS
JMP      AFILT2      SUBROUTINE
JMP      HACQ6        EXIT -FAILED ANGLE TESTS
JMP      RFILT2      SUBROUTINE
JMP      HACQ6        EXIT -FAILED RANGE TEST
HACQ1K   JMP      STORES
TMA      F/1.0
FAMS     PAR4
HAC06    TMA      TI          TEST IF TI >OR= PAR2
TMO      PAR2
JAGOF    HACQ7
TAM      T1          SET TI=TI
TMD      F/10.0       SET DT=10
TDM      DT
TQM      TI          SET TI=PAR2
JMP      HACQ8
HAC07    TAM      T2          SET T2=TI
TMD      PAR2
TDM      TI
HACQUIXJMP 0          EXIT

AFILT2  TJM      AFILT2X
TMA      A2H          TEST IF (A2H-A1H)(OBSAZ-A1H)
FSM      A1H          (A2H-OBSAZ) 7 OR= 0
TAM      TEMP1
TMA      OBSAZ
FSM      A1H
TAQ
TMA      A2H
FSM      OBSAZ
FMAR
TMO      TEMP1
FMAR
JAN      AFILT2X
TMA      D/1816
AMS      AFILT2X

```

INCREMENT RETURN ADDRESS FOR
NORMAL RETURN

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```

L AFILT2XJMP 0          EXIT
RFILT2  TJM      RFILT2X
TMA      RCPTST
JAZ      RFB1
TMA      OBSAZ
FSM      A1H
TMO      RHODMAX
FMAR
FAM
TAQ
TMA      RHO
JAGOF    RFILT2X
RFB1    TMA      D/1 B16
AMS      RFILT2X
L RFILT2XJMP 0          INCREMENT BY 1H

```

TEST IS RCPTST=0
TEST IF RHO > OR= RHOMAX+
RHODMAX*(OBSAZ-A1H)

```

RFILT2  TJM      RFILT2X
TMA      RHO
JAGOF    RFILT2X
RFB1    TMA      D/1 B16
AMS      RFILT2X
L RFILT2XJMP 0          EXIT

```

```

AQUIRE  TJM      ACQUIRX
TMA      ATYPE
TMD      A/0000000PS
JAED     ACQUI1
TMD      A/0000000HS
JAED     ACQUI2
TMD      A/0000000TS
JAED     ACQUI3
HLT
ACQUI3 JHP      TACQUI
ACQUIRXJMP
ACQUI1 JHP      PACQUI
JMP      ACQUIRX
ACQUI2 JHP      HACQUI
JMP      ACQUIRX

```

SAVE RETURN ADDRESS
TEST IF ATYPE IS P(PLANAR FAN),
H(HORIZONTAL FAN),OR T(TRACKER)
PLANAR FAN

HORIZONTAL FAN

ERROR
TRACKER SUBROUTINE
EXIT
PLANAR SUBROUTINE

HORIZONTAL SUBROUTINE

```

PACQUI  TJM      PACQUIX
JMP      PACRHDN
TAM      PAR1
TMD      PAR2
TDM      PAR2
CM      PAR4
TMA      XL1Z
FSM      EPSLN
TMO      RHO
FMAR

```

SUBROUTINE COMPUTES RHO DOT N
PAR2=TI
PAR4=0
TEST IS RHO(XL1Z-EPSLN) GREATER
THAN OR EQUAL TO RHOZH

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THQ RHOZH
 JAGQF PACQUIX
 TMD F/10.0
 TDM DT
PACQ2 TMA RHOZH
 JAP PACQ1
PACQ6 TMA TI
 TMD PAR2
 JAGQF PACQ13
 TMD PAR1S
 TDM RHODOTNS
 TQM TI
 TMD F/10.0
 TDM DT
PACQ8 TMA DT
 FAMS TI
 TMD RHODOTN
 TDM PAR3
 JMP CRHOB
 JMP PACRHDN
 TMQ PAR1
 FMAR
 JAP PACQ2
PAC05 TMQ DT
 FMMR F/.5
 TAM TEMP1
 TMQ PAR3
 FMMR RHODOTN
 TMQ TEMP1
 JAP PACQ3
 FCSQ
 TAQ
PAC03 TQM DT
 TQA
 FAMS TI
 TMD RHODOTN
 TDM PAR3
 JMP CRHOB
 JMP PACRHDN
 TAQ
 FCAQAS TEMP1
 TMQ RHO
 FMMR EPSLN
 TMQ TEMP1
 JAGQF PACQ4
 JMP PAC05
PAC04 JMP AFILT1
 JMP PACQ6
 JMP RFILT1
 JMP PACQ6
 JMP RHARR
 JMP STORE
 TMA F/1.0
 FAMS PAR4
 JMP PACQ6

SET DT= -10
 TEST IF RHOZH IS POSITIVE
 TEST IF TI IS GREATER THAN OR EQUAL TO PAR2
 SET TI= PAR2
 SET DT=+10
 SET TI= TI+DT
 SET PAR3= RHODOTN
 SUBROUTINE COMPUTES RHO DOT N
 TEST IF PAR1= RHODOTN IS POSITIVE
 COMPUTE DT= SIGN(PAR3*RHODOTN)*DT/2
 TEMP1= DT/2
 SET TI= TI+DT
 SET PAR3= RHODOTN
 SUBROUTINE COMPUTES RHO DOTN
 TEST IF RHO*EPSLN IS GREATER THAN OR EQUAL TO ABS(RHODOTN) = TEMP1
 TEMP= ABS(RHODOTN)
 SUBR. TEST ANGULAR LIMITS OF FAN
 TEST FAILED
 SUAR. TEST RANGE LIMITS OF FAN
 TEST FAILED
 SUAR. COMPUTES RHO,H,A,S RHODOT
 SUAR. STORE PT FOR OUTPUT AFTER TESTIN

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PACQ1 FCAHA RHODOTN
 TAM TEMP1
 TMQ RHO
 FMMR EPSLN
 TMQ TEMP1
 JAGQF PACQ4
 JMP PACQ8
PACQ13 TMD PAR2
 TDM TI
 PACQUIXJMP 0
 PACRHONTJM PACRHDX
 TMQ RHOXH
 FMMR XNXH
 TMQ RHOYH
 FMAD XNYH
 TMQ RHOZH
 FMAD XNZH
 TAM RHODOTN
 PACRHDXJMP 0

AFILT1 TJM AFILT1X
 TMA RHOZH
 JAN AFILT1X
 TMQ RHOZH
 FMMR XL2Y
 TMQ RHOYH
 FMSU XL2Z
 TAM TEMP1
 FMMR XL1Z
 TMQ RHOZH
 FMSU XL1Y
 TAM TEMP2
 FMMR XL2X
 TMQ RHOXH
 FMSU XL2Z
 TAM TEMP3
 FMMR XL1Z
 TMQ XL1X
 FMSU RHOZH
 TAM TEMP4
 FMMR RHOYH
 TMQ RHOXH
 FMSU XL1Y
 TAM TEMP5
 FMMR XL2Y
 TMQ XL2X
 FMSU RHOYH
 TMQ TEMP5
 FMAR
 TMQ TEMP4
 FMAD TEMP3

TEST IF RHO*EPSLN IS GREATER THAN OR EQUAL TO ABS(RHODOTN)
 TEMP1= ABS(RHODOTN)
 EXIT
 COMPUTE RHO DOT N

TEST IF (L1 CROSSL) DOT(L CROSSL2)
 IS POSITIVE
 QTY TO BE TESTED = ((XL2Z*RHOYH-
 XL2Y*RHOZH)*(XL1Y*RHOZH-XL1Z*RHOYH)+
 +(XL2Z*RHOXH-XL2X*RHOZH)*(XL1X*
 RHOZH-ZL1Z*RHOXH)+(XL2Y*RHOXH
 -XL2X*RHOYH)*(XL1X*RHOYH
 -XL1Y*RHOXH))/RHO*#2

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TMQ TEMP2
FMAD TEMP1
JAN AFILT1X
TMA D/1B16
AMS AFILT1X
L AFILT1XJMP 0

RFILT1 TJM RFILT1X
TMA RCPTST TEST IF RCPTST=0
JAZ RFA1
TMO RHOXH TEST IF RHO IS GREATER THAN OR EQUAL T
FMMR XL1X $RHOMAX + RHODMAX * \text{ARCOS}(L \cdot DOT\ L_1)$
TMQ RHOYH
FMAD XL1Y
TMO RHOZH
FMAD XL1Z
FDA RHO
TQA
S FACOS
TMQ RHODMAX
FMAR
FAM RHOMAX \$
TAQ
TMA RHO \$
JAGQF RFILT1X
RFA1 TMA D/1B16
AMS RFILT1X
L RFILT1XJMP 0 EXIT

AINIT TJM AINITX
TMD RHO
TDM BUFFER
TMD RHOXH
TDM BUFFER+1
TMD RHOYH
TDM BUFFER+2
TMD RHOZH
TDM BUFFER+3
TDM OBSRR
TDM BUFFER+4
TMD TI
TDM BUFFER+5
TIJ FANTAB
TJM IRSET
AINITX JMP 0
SAVE RHO, RHOXH, RHOYH, RHOZH,
+ OBSRR

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BUFFER ASTOR 6 \$

NXACQ0 TJM NXACQX
TMD BUFFER
TDM RHO
TMD BUFFER+1
TDM RHOXH
TMD BUFFER+2
TDM RHOYH
TMD BUFFER+3
TDM RHOZH
TMD BUFFER+4
TDM OBSRR
TMD BUFFER+5
TDM TI \$
TMD IRSET
TDXLC ,1
TMA A/ZZZZZZZ\$
TMD ,1
JAED NXACQX
TMQ 0/77T47 TEST FOR RECORD TYPE
ETA 1,1
TMD A/0000000PS
JAED NXAP1
TMD A/0000000HS
JAED NXAH1
TMD A/0000000TS
JAED NXAT1
HLT 0
NXAP1 TDM ATYPE
TMD ,1
TDM XNXH
TMD 1,1
TDM XNYH
TMD 2,1
TDM XNZH
TMD 3,1
TDM XL1X
TMD 4,1
TDM XL1Y
TMD 5,1
TDM XL1Z
TMD 6,1
TDM XL2X
TMD 7,1
TDM XL2Y
TMD 8,1
TDM XL2Z
NXAH2 TMD 10,1
TDM RHODMAX
NXAT2 TMQ 0/77T5 \$

RESTORE RHO, RHOXH, RHOYH, RHOZH,
+ OBSRR

X1=L/FANTAB STORED IN IRSET

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ETA 11.1S
 TAM FANNO
 TMD 9,1
 TDM RHOMAX
 TMA D/1816
 AMS NXACQX
 TMA N/12715
 AMS IRSET
 L NXACQX JMP 0
 NXAH1 TDM ATYPE
 TMD ,1
 TDM A1H
 TMD 1,1
 TDM A2H
 TMD 5,1
 TDM SINHREF
 TMD 6,1
 TDM COSHREF
 JMP NXAH2
 NXAT1 TDM ATYPE
 TMD ,1
 TDM UMAXT
 TMD 1,1
 TDM VMAXT
 TMD 2,1
 TDM COSPSI
 TMD 3,1
 TDM RT1MUS
 TMD 4,1
 TDM RT1MVS
 TMD 5,1
 TDM SINHMIN
 TDM SINHREF\$
 TMD 6,1
 TDM COSHMIN
 TDM COSHREF\$
 TMD 7,1
 TDM PPP
 TMD 8,1
 TDM TRDELT
 TMD 10,1
 TDM TRTYPE
 JMP NXAT2

TACQJI1TJM TCQUIX
 TMD F/1.0 SET PAR1= 1.0
 TDM PAR1
 JMP AFILT3 SUBROUTINE
 JMP TCO1 FAILED EXIT
 JMP TCO2 MARGINAL EXIT
 TCQ6 TMD TI NORMAL OR PASS EXIT SET PAR2=TI

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TDM PAR2
 TMD F/1.0 SET PAR3=1.0
 TDM PAR3
 TMD F/-10.0 SET DT=-10.0
 TDM DT
 TCQ3 TMA DT SET TI=TI+DT
 FAMS TI
 JMP CRHOB SUBROUTINE
 JMP AFILT3 SUBROUTINE
 JMP TCO4 FAILED EXIT
 JMP TCO5 MARGINAL EXIT
 JMP TCO3 PASSED EXIT
 TCQ2 TMA VISIBLE TEST FOR VISIBILITY YFS = X NO=0
 JAZ TCO1 FAILS
 JMP TCO6 OK
 TCQ1 TMD F/-1.0 SET PAR1=-1.0
 TDM PAR1
 TDM PAR3
 TMD TI SET PAR2=TI
 TDM PAR2
 TMD F/-2 SET DT=-2
 TDM DT
 TCQ7 TMA DT SET TI=TI+DT
 FAMS TI SUBROUTINE
 JMP CRHOB TEST IS /> OR=RHOZH
 TMA F/0.0
 TMQ RHOZH
 JAGQF TCO8
 JMP AFILT3 SUBROUTINE
 JMP TCO7 FAILED EXIT
 JMP TCO9 MARGINAL EXIT
 TMD TI SET PAR2=TI
 TDM PAR2
 TCQ10 TMQ PAR3 SET DT=PAR3+DT+.5
 FMMR DT
 TMQ F/.5
 FMARS DT
 TMD F/1.0 SET PAR3=1.0
 TDM PAR3
 TCO11 TMA DT SET TI=IT+DT
 FAMS TI
 JMP CRHOB SUBROUTINE
 JMP AFILT3 SUBROUTINE
 JMP TCO4 FAILED EXIT
 JMP TCO5 MARGINAL EXIT
 JMP TCO10 PASSED EXIT
 TCQ5 JMP RHARR SUBROUTINE
 JMP STORE SUBROUTINE
 TMA F/1.0 SET PAR4=PAR4+1.0
 FAMS PAR4
 TMD F/2.0 TEST IF PAR4=2.0
 JAED TCO12
 TMD TI SET T1=TI
 TDM T1
 TMD F/1.0 SET PAR3=1.0

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	TDM	PAR3	
	TMA	PAR1	SET DT=PAR1+10
	TMQ	F/10.0	
	FMARS	DT	
	TMD	PAR2	SET TI=PAR2
	TDM	TI	
	JMP	TCQ3	
TCQ12	TMA	T1	TEST IS T1 > OR = TI
	TMQ	TI	
	JAGQF	TCQ13	
	TMD	TI	SET T2=TI
	TDM	T2	
TCQUIX	JMP	0	EXIT
TCQ13	TMD	T1	SET T2,T1
	TDM	T2	
	TMD	TI	SET T1=TI
	TDM	TI	
	JMP	TCQUIX	
TCQ4	TMD	PAR3	SET DT=-PAR3+DT+.5
	FMMR	DT	
	TMD	F/- .5	
	FMARS	DT	
	TMD	F/-1.0	SET PAR3=-1.0
	TDM	PAR3	
	JMP	TCQ11	
TCQ9	TMD	TI	SET PAR2=TI
	TDM	PAR2	
	JMP	TCQ5	
TCQ8	TMA	TI	TEST IS TI > OR = PAR2
	TMQ	PAR2	
	JAGQF	TCQUIX	
	TDM	TI	SET TI=PAR2
	TMD	F/.2	SET DT=.2
	TDM	DT	
	TMD	F/1.0	SET PAR1=1.0
	TDM	PAR1	
	JMP	TCQ7	
TACQUI	TJM	TACQUIX	
	CM	PAR4	SET PAR4=0
	TMA	RCPTST	TEST TS RCPTST=ZERO
	JAZ	TACQ1	
	TMA	RHOMAX	TEST IS RHOMAX >OR= RHO
	TMQ	RHO	
	JAGUF	TACQ1	
TACQUIX	JMP	0	TEST PHASED ARRAY TRTYPE=0 NO #1 YES
TACQ1	TMA	TRTYPE	
	JAZ	TACQ2	
	JMP	TACQUI1	SUBROUTINE
TACQ3	THA	F/1.0	
	TMQ	PAR4	

JAGQF	TACQUIX		
TMA	PPP	TEST IF PPP=9.0	
TMD	F/.9.0		
JAED	TACQ4		
JMP	TACQ6		
TACQ4	TMA	TRDELT	
	FAD		
	TAM	TEMP1	
	TMA	T2	
	FSM	T1	
	FDA	TEMP1	
	TQA		
	JMP	SEPSUB	
	TMO	TRDELT	
FMARS		TI	
	TMA	T2	
	FAM	T1	
	TMO	F/.5	
	FMAR		
	FSMS	TI	
	TMD	TRDELT	
	TDM	DT	
	FCSM	DT	SET DT=TRDELT
	FAMS	TI	\$
TACQ4A	TMA	DPASS	\$
	JAZ	TACQ7	\$
	TMA	TRTYPE	\$
	JAZ	(P)+2H	\$
	JMP	TACQ7	\$
	TMA	DT	\$
	FAMS	T2	\$
TACQ7	TMA	DT	SET TI=TI+DT
	FAMS	TI	
	FSM	T2	TEST IF -1E-4 > OR = TI-T2
	TAO		
	TMA	F/-0.00001	
JAGQF	TACQ8		
	JMP	TACQUIX	
TACQ8	JMP	CRHOB	SUBROUTINE
	JMP	RHARR	SUBROUTINE
	TMA	TRTYPE	TEST FOR PHASED ARRAY TRTYPE=0 NO 1YES
	JAZ	TACQ9	
TACQ10	JMP	STORE	SUBROUTINE
	TMA	F/1.0	
	FAMS	PAR4	
	JMP	TACQ7	
TACQ9	TMA	ELMAX	TEST IF ELMAX > OR = OBSEL
	TMO	OBSEL	
	JAGQF	TACQ10	
	JMP	TACQ7	
TACQ6	TMA	PPP	COMPUTE DT=(T2-T1)/(PpP-1)
	FSM	F/1.0	
	TAM	DT	
	TMA	T2	
	FSM	T1	

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```

FDAS DT
TMD T1
TDM TI
JMP TACQ4A
TACQ2 TMD F/0.0      $  

        TDM A1H  

        TMD TWOP1  

        TDM A2H  

        THD RCPTST  

        TDM STST  

        CM RCPTST  

        JMP HACQUI  

        TMD STST  

        TDM RCPTST  

        THA DPASS  

        JAZ TACQ3  

        TMD PAR2  

        TDM T2  

        CM BUF1  

        JMP TACQ3

```

SET A14=0
SET A2H=TWOP1
SET STST=RCPTST
SET RCPTST=0
SUBROUTINE
\$
\$
TEST UPASS ONLY DPASS=1 NO DPASS =0
SET T2=PAR2
\$

```

AFILT3 TJM AFILT3X
TJM VISIBLE
CM MARG
FCSM RHO
TMQ SINHMIN
FMAR
FAM RHOZH
TAM ERR
TMQ RHO
FMMR EPSLN
TAM TEMP1
TMQ COSHMIN
FMARS EPS
JMP AFILT31
TMQ RHO
TMA COSPSI
FMARS ERR
TMQ RHOZH
FMMR YFX
TMQ RHOYH
FMAD YFY
TMQ RHOZH
FMAD YFZ
FSMS ERR
TMA TEMP1
TMQ SINPSI
FMARS EPS
JMP AFILT31
TMQ RHOZH
FMMR ZFX

```

SET ERR= RH07H-RHO*SINHMIN
ERR
SET EPS=RHO*EPSLN*COSHMIN
TEMP1=RHO*EPSLN
EPS
SUBROUTINE
SET ERR= (RHO DOT YF)-RHO*COSPSI
ERR= RHO*COSPSI
RHO DOT YF COMPLETE
ERR
SET EPS= RHO*EPSLN*SINPSI
TEMP1= RHO*EPSLN
SUBROUTINE
SET ERR= RHO*UMAXT-ABS(RHO DOT ZF)

```

TMQ RHOYH
FMAD ZFY
TMQ RHOZH
FMAD ZFZ
TAQ
FCAQAS ERR
TMQ RHO
FMMR UMAXT
FSMS ERR
TMA TEMP1
TMQ RT1MUS
FMARS EPS
JMP AFILT31
TMQ RHOZH
FMMR XFX
TMQ RHOYH
FMAD XFY
TMQ RHOZH
FMAD XFZ
TAQ
FCAQAS ERR
TMQ RHO
FMMR VMAXT
FSMS ERR
TMQ TEMP1
TMA RT1MVS
FMARS EPS
JMP AFILT31
TMA O/2 T16
AMS AFILT3X
TMA MARG
JAZ AFILT3X
CSM O/1T16
AMS AFILT3X
L AFILT3XJMP 0

```

ERR=ABS(RHO DOT ZF)
ERR
SET EPS=RHO*EPSLN*(1-UMAXT**2)**1/2
EPS
SUBROUTINE
SET ERR=RHO*VMAXT-ABS(RHO DOT XF)
ERR=ABS(RHO DOT XF)
ERR
SET EPS=RHO*EPSLN*(1-VMAX**2)**1/2
\$
SUBROUTINE
S
EXIT
AFILT31TJM AFILX
TMA F/0.0
TMQ ERR
JAGOF AFD1
FCAQA EPS
TMQ AFILX
JAGOF AFILX
AFD2 TAM MARG
AFILX JMP 0
AFD1 CM VISIBLE
TMQ EPS
FCAMA ERR
JAGOF AFILT3X
JMP AFD2

TEST IS ZERO OR= ERR
TEST IF ABS(ERR) > OR = EPS
SET MARG NOT ZERO
EXIT
SET VISIBLE = 0
TEST IF ABS(ERR) > OR = EPS
EXIT FROM AFILT3 ROUTINE

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RHARR	TJM	RHARRX	\$
	TMA	RHOZH	\$ COMPUTE OBSEL = ARCTAN(RHOZH/RHO)
	FDA	RHO	\$
	TQA		\$
S	FASIN		\$
	TAM	OBSEL	\$ OBSEL
	TMQ	RHOYH	\$ COMPUTE OBSA7=ARCTAN(RHOYH/ =RHOXH)
	FCSM	RHOXH	\$
	JMP	ARCTAN	\$ SUBROUTINE
	TAM	OBSAZ	\$ \$
	TMD	RHO	\$ SET OBSR = RHO
	TDM	OBSR	\$
RHARRX	JMP	0	\$
STORE	TJM	STOREX	\$
	TMA	TF	\$ TEST IS ZERO > OR= TI(TF=TO-TI)
	FSM	TO	\$
	TMQ	TI	\$
	FSQ		\$
	FMAR		\$
	TAQ		\$
	TMA	F/0.0	\$
	JAGQF	STOREX	\$
	TMA	VPASS	\$ TEST IF VPASS=0
	JAZ	STO1R	\$
	JMP	ANGSN1	\$ SUBROUTINE
	TMQ	XILLUM	\$
	TMA	F/0.0	\$
	JAGQF	STOREX	\$
STO1R	TMD	TI	\$ SET UP INPUT FOR AJPACK
	TDM	AJMIN	\$ AJMIN=TI
	TMD	OBSAZ	\$
	TMD	AJAZ	\$ AJAZ=OBSAZ
	TMD	OBSEL	\$
	TDM	AJELEV	\$ AFELEV=OBSEL
	TMD	RHO	\$
	TMD	AJRANGE	\$ AJRANE=RHO
	TMD	OBSRR	\$
	TDM	AJR RATE	\$ AJRRATE=OBSRR
	TMD	FANNO	\$
	TDM	AJFAN	\$
	TMQ	T	\$
	FMMR	XNO	\$
	FDA	TWOP	\$
	TMA	EPREV	\$
	FAQS	AJREV	\$ AJREV=EPREV+T*XNO/TWOP

TMA	BUF1	S TEST IS BUF1=0
JAZ	STO2R	\$
TMA	BUF2	\$ TEST BUF2> OR= AJMIN
TMQ	AJMIN	\$
JAGQF	STO3R	\$
TQM	BUF2	\$ EXCHANGE
TAM	AJMIN	\$ BUF2=AJMIN + AJMIN=BUF2
TMD	BUF1	\$
TDM	AJAZ	\$
TAM	BUF1	\$
TAM	AJAZ	\$ AJAZ=BUF1 \$ BUF1=AJAZ
TMA	BUF3	\$
TMD	AJELEV	\$
TDM	BUF3	\$
TAM	AJELEV	\$ AJELEV=BUF3 \$ BUF3=AJELEV
TMA	BUF4	\$
TMD	AJRANGE	\$
TDM	BUF4	\$ AJRANGE=BUF4 + BUF4=AJRANGE
TAM	AJRANGE	\$
TMA	BUF5	\$
TMD	AJRRATE	\$
TDM	BUF5	\$
TAM	AJRRATE	\$ AJRRATE=BUF5 + BUF5=AJRRATE
TMA	BUF6	\$
TMD	AJREV	\$
TDM	BUF6	\$
TAM	AJREV	\$ AJREV=BUF6 + BUF6=AJREV
TMA	BUF7\$	\$
TMD	AJFAN	\$
TDM	BUF7\$	\$
TAM	AJFAN	\$
TMD	AJPACK	\$
STO3R	JMP	\$ SUBROUTINE
STOREX	JMP	\$ EXIT
STO2R	TMD	\$
	TDM	AJAZ
	TDM	BUF1=AJAZ
	TMD	AJMIN
	TDM	BUF2=AJMIN
	TMD	AJELEV
	TDM	BUF3=AJELEV
	TMD	AJRANGE
	TDM	BUF4
	TMD	BUF4=AJRANGE
	TDM	AJRRATE
	TDM	BUF5
	TMD	BUF5=AJRRATE
	TDM	AJREV
	TDM	BUF6
	TMD	BUF6=AJREV
	TDM	AJFAN
	TDM	BUF7\$
	JMP	STOREX
ENDPK	TJM	\$
	TMA	BUF1
		\$ TEST IS BUF1=0

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```

JAZ ENDPKX      S
TMD BUF1        S TRANSFER DATA FROM BU1F TO AJJS
TDM AJAZ         S
TMD BUF2         S
TDM AJMIN        S
TMD BUF3         S
TDM AJELEV       S
TMD BUF4         S
TDM AJRANGE      S
TMD BUF5         S
TDM AJRRATE      S
TMD BUF6         S
TDM AJREV         S
TMD 0/1T47        S SET FLAG AJFLGIT
TDM AJFLGIT      S
CM BUF1          S
TMD BUF7$        S
TDM AJFAN         S
JMP AJPACK        S
ENDPKX JMP 0      S

```

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```

TMO COSPH        S
FMAR             S
TMO SINPH        S
FMSU TEMP2        S
FMAD TEMP4        S TEMP4=(X+CAPX)COSTH
TAM RHOXH        S RHOXH
TMO SINTH        S COMPUTE RHOYH=(Y+CAPY)COSTH
FMMR TEMP3        S -(X+CAPX)SINTH
TMO COSTH        S TEMP3=(X+CAPX)
FMSU TEMP1        S TEMP1=(Y+CAPY)
TAM RHOYH        S RHOYH
TMO SINPH        S
FMMR TEMP5        S (Y+CAPZ)COSPH=X*SINTH+(Z+CAPZ)SINTH
TMO COSPH        S TEMP5=Z+CAPZ
FMAD TEMP2        S TEMP2=(Y+CAPY)SINTH
FMAD TEMP4        S TEMP4=(X+CAPX)COSTH
TAM RHOZH        S RHOZH
TAU              S COMPUTE RHO = (RHOXH**2+RHOYH**2
FMAR             S +(RHOZH**2)**1/2
TMO RHOXH        S
FMAD RHOXH        S
TMO RHOYH        S
FMAD RHOYH        S
TAM RHOSORD      S
S FSORT          S
TAM RHO           S RHO
TMA XDOT          S COMPUTE OBSRR=(1/P)(X+CAPX)(XDOT+THDOT
TMO THDOT         S +(Y+CAPY)(YDOT-THDNT*X)+(Z+CAPZ)
FMAD Y             S *ZDOT
TAM TEMP2          S TEMP2= XDOT+THDOT*Y
FMMR X             S
FSM YDOT          S
TMO TEMP1          S TEMP1=Y+CAPY
FMAR              S
TMO ZDOT          S
FMSU TEMP5          S TEMP5= Z+CAPZ
TMO TEMP2          S TEMP2= XDOT+ THDOT*Y
FMAD TEMP3          S TEMP3= X+CAPY
FDA RHO            S
TQM OBSRR          S OBSRR
CRH09X JMP 0        S EXIT

```

```

CRH09 TJM CRH0BX      S
JMP PRED          S
TMA THTAO         S SUBROUTINE
TMO RPTIM          S COMPUTE THTA = THTAO + RPTIM + T
FMAD T             S
TAM THTA          S
S FSIN             S
TAM SINTH          S
S FCOS THTA        S
TAM COSTH          S
TMO XOVCT          S COMPUTE CAPX = CAPX = XOVCT*COSTH
TMA COSTH          S
FMARS CAPX          S
TMA SINTH          S COMPUTE CAPY= XOVCT*SINTH
FMARS CAPY          S CAPY= QREG*XOVCT
FAM Y               S COMPUTE RHOXH= (X+CAPX)SINPH+COSTH
TAM TEMP1          S +(Y+CAPY)SINPH+SINTH -
TMO SINTH          S (Z+CAPZ)COSPH
FMARS TEMP2          S TEMP1=Y+CAPY TEMP2=(Y+CAPY)SINTH
TMA X               S
FAM CAPX          S
TAM TEMP3          S TEMP3=X+CAPX
TMO COSTH          S
FMARS TEMP4          S TEMP4=(X+CAPX)COSTH
TMA Z               S
FAM CAPZ          S
TAM TEMP5          S TEMP5= Z+CAPZ

```

```

PRED TJM PREDX          S
TMA TI              S COMPUTE T= TI-EPOCHM
FSM EPOCHM          S
TAM T               S
JMP XYZSB          S T
PREDX JMP 0          S SUBROUTINE
S EXIT

```

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CRDOT	TJM	CRDOTHX	\$
TMQ	T		\$ COMPUTE RHODOT= (XDOT+THDOT*Y)+COSPH
FMMR	RPTIM		\$
FAM	THTAO		\$ +ZDOT*SINPH
TAM	THTA		\$ THTA=THTAO+THDOT*T
S	FCOS		\$
	TAM	COSTH	\$
	TMQ	COSPH	\$
	FMMRS	CCPHTH	\$ \$ CCPHTH = COSPH*COSTH
	TMA	THTA	\$
S	FSIN		\$
	TAM	SINTH	\$
	TMQ	COSPH	\$
	FMMRS	CSPHTH	\$ \$ CSPHTH = COSPH*SINTH
	TMQ	X	\$
	FMMR	THDOT	\$
	FSM	YDOT	\$
	TMQ	CSPHTH	\$
	FMMRS	RHODOT	\$ \$ USED AS TEMP
	TMQ	Y	\$
	FMMR	THDOT	\$
	FAM	XDOT	\$
	TMQ	CCPHTH	\$
	FMAR		\$
	TMQ	ZDOT	\$
	FMD	SINPH	\$
	FSMS	RHODOT	\$ \$ RHODOT
	TMA	OBSRR	\$
	FDA	RHO	\$
	FMMR	RHOZH	\$
	FSM	RHODOT	\$
	FDA	RHO	\$
	FCSQS	RHODOT	\$
CRDOTHX	JMP	0	\$ EXIT
CRDDOT	TJM	CRDOTHX	\$
TMA	RHODOT		\$
FSM	OLD ONE		\$
FDA	DT		\$
TJM	RHODOT		\$
CRDOTHX	JMP	0	\$ EXIT

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NXPASS	TJM	NXPASSX	\$
NXPAS12TMD		LSTT	\$ SET TI=LSTT
	TDM	TI	\$
	JMP	ZDWI	\$ SUBROUTINE
NXPAS7	TMA	TI	\$ TEST IF TF IS GREATER THAN OR EQUAL TO
	FAM	TO	\$
	TAO		\$
	THA	TF	\$ TI-IF YES JMP-IF NO EXIT
	JAGQF	NXPAS1	\$
L	NXPASSX	JMP 0	\$ EXIT
NXPAS1	JMP	CZDOTH	\$ SURROUNGE
	FCAMA	ZDOTH	\$ TEST IF ABS(ZDOTH) IS GREATER THAN OR
	TMQ	K1	\$ EQUAL TO K1 -IF YES JMP
	JAGQF	NXPAS2	\$
	FCSM	DT1	\$ COMPUTE TI=TI-DT1
	FAMS	TI	\$
NXPAS6	JMP	CRHOB	\$
	JMP	CRDOT	\$ SUBROUTINE
	TMA	F/0.0	\$ TEST IF RHODOT IS GREATER THAN ZERO
	TMQ	RHODOT	\$
	JAGQF	NXPAS3	\$
NXPAS5	TMA	DT2	\$ SET TI=TI+DT2
	FAMS	TI	\$
	JMP	CRHOB	\$
	JMP	CRDOT	\$ SUBROUTINE
	TMA	F/0.0	\$ TEST IF ZERO IS GREATER THAN OR EQUAL
	TMQ	RHODOT	\$ TO RHODOT - IF YES JMP
	JAGQF	NXPAS4	\$
	JMP	NXPAS5	\$
NXPAS3	TMA	DT2	\$ SET TI=TI+DT2
	FAMS	TI	\$
	JMP	NXPAS6	\$
NXPAS2	TMA	DT1	\$ SET TI=TI+DT1
	FAMS	TI	\$
	JMP	NXPAS7	\$
NXPAS4	TMD	DT2	\$ SET DT=DT2
	TDM	DT	\$
	CM	N	\$ N=0
NXPAS9	FCSMA	DT	\$ COMPUTE DT= -.5*ABS(DT)
	TMQ	F/.5	\$
	FMARS	DT	\$
NXPAS10	FAMS	TI	\$ SET TI=TI+DT
	TMA	D/1B15	\$ SET N=N+1 FIX PT B15
	AMS	N	\$
	JMP	CRHOB	\$
	JMP	CRDOT	\$ SUBROUTINE
	TMA	N	\$ TEST IF N=NMAX NMAX=7 FOR 1ST CUT
	TMD	NMAX	\$
	JAED	NXPAS8	\$
	TMA	F/0.0	\$ TEST IF ZERO IS GREATER THAN OR EQUAL
	TMQ	RHODOT	\$ RHODOT
	TQM	OLD ONE	\$
	JAGQF	NXPAS9	\$
	FCAMA	DT	\$ SET DT= .5*ABS(DT)
	TMQ	F/.5	\$

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```

FMARS DT
JMP NXPAS10
NXPAS8 JMP CRDDOT
TMA RHODOT
FDA RHODDOT
TOM TEMP1
TMA DT
FDA F/2.0
FCAQAS TEMP2
FCAMA TEMP1
TMO TEMP2
JAGQF NXPAS11
FCSM TEMP1
FAMS TI
NXPAS14JMP CRHOB
TMA DT1
FAM DT2
FAM TI
TAM LSTT
TMA F/0.0
TMO RHOZH
JAGOF NXPAS12
TMA D/1B16
AMS NXPASSX
JMP NXPASSX
NXPAS11TMA RHODOT
TMO TEMP2
JAP NXPAS13
FCSQ
TAQ
NXPAS13FCAQ
FAMS TI
JMP NXPAS14
DT1 F/5
DT2 F/25
NMAX 0/7 T15
$ CONSTANT

```

```

EINIT TJM EINITX
JMP XYZI
CM T
JMP XYZSB
TMO EPOCH
FMMR XMNPDA
FSM TO
TAM EPOCHM
TMO RPTIM
FMAR
FAM THTAI
TAM THTAO
TMA XNUDOT
$ SURROUNGE
$ SET T=0
$ SUBROUTINE
$ COMPUTE EPOCHM= EPOCH+XMNPDA- TO
$ EPOCHM
$ COMPUTE THTAO= THTAI+RPTIM+EPOCHM
$ THTAO
$ 

```

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```

FSM RPTIM
TMO DT1
FMARS TEMP1
S FSIN
TAM SDEL
TMA TEMP1
S FCOS
TAM CDEL
TMO SINPH
TMA COSI
FMARS SPCI
TMO SINI
TMA COSPH
FMARS CPSI
TMA EO
FAM F/1.0
TMO AO
FMARS Q2
FCSM FANTAB+5
TMO FANTAB+5
FMAR
FAM F/1.0
TAM TEMP1
S FSQRT
TAM TEMP2
TMO Q2
FMMR Q2
FSM TEMP1
S FSQRT
TAM SINHMIN
FDA Q2
FMMR TEMP2
TAM K1
CM LSTT
TMD C/HLT,SATNOS
TDXLC ,1
TMD SATCONT
ADXL ,1
FCSM EPOCHM
FSM F/1440.0
FDA TWOPI
FMMR XNO
FAM EPREV
JAP (P)+2H
TMA F/0.0
TAQ
JMP AJFIXIT
SLA 30
TMO 3/1T2;30/1T47
EIS 0,1
EINITX JMP 0
$ +DT1)
$ TEMP1=(XNO*OT-THOOT)*DT1
$ COMPUTE CDEL = SIN(TMP1)
$ COMPUTE SPCI= SIN PH*COSI
$ COMPUTE CPSI = COSPH*SINI
$ COMPUTE Q2 = A0(1+EO)
$ TEMP1= COSHMIN*+2
$ TEMP2= COSHMIN
$ K1
$ SET LSTT=0
$ COMPUTE REV.NO) AT START TIME, FIX IT,
$ AND PUT INTO SATNOS TABLE
$ STORE
$ EXIT

```

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SINIT	TJM	SINITX	\$
	TMA	BEGT	\$ COMPUTE TD=REGT+XMNPDA
	TMO	XMNPD4	\$
FHARS	TO	\$	
TMA	ENDT	\$ COMPUTE TF=ENDT+XMNPDA	
FHARS	TF	\$	
TMA	PHIRD	\$ COMPUTE COSPH =COS(PHIRD)	
S	FCOS	\$	
	TAM	COSPH	\$
S	TMA	PHIRD	\$ COMPUTE SINPH= SIN(PHIRD)
	FSIN	\$	
	TAM	SINPH	\$
	TMO	BEAMW	\$ COMPUTE EPSLN=.5*BEAMW*D2R
FMMR	F/.5	\$	
TMO	DE2RA	\$ D2R= DEGREES TO RADIANS CONSTANT	
FHARS	EPSLN	\$	
CM	BUF1	\$ BUF1=0	
TMA	BEGT	\$ COMPUTE THTAI	
JMP	FYKLOK	\$ SUBROUTINE	
TAM	TOY	\$	
TQA		\$	
JMP	SEPSUB	\$ SUBROUTINE	
TAM	ORGDA	\$	
TQM	ORGTM	\$	
TMO	TOY	\$	
JMP	TLC	\$ SUBROUTINE	
TMO	ORGDA	\$	
FMMR	SIDRT	\$	
TMO	ORGTM	\$	
F MAD	SIDRT+1	\$	
FAM	THGRO	\$	
TMO	DE2RA	\$	
FMAR		\$	
FAM	XLAMBA	\$	
TAM	THTAI	\$	
SINITX	JMP	0	\$ EXIT

ZDWI	TJM	ZDWIX	\$
	FCSM	DT1	\$
FAMS	TI	\$	
JMP	PRED	\$ SUBROUTINE	
TMA	THTAO	\$ COMPUTE THTA=THTAO+THDOT+ T	
TMO	RPTIM	\$	
F MAD	T	\$	

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S	TAM	THTA	\$ THTA
	TAQ		\$ COMPUTE SNMT =SIN(XNODE-THTA)
	TMA	XNODE	\$
	FSQS	CNMT	\$ CNMT USED AS TEMP = XNODE-THTA
	FSIN		\$
S	TAM	SNMT	\$ SNMT
	TMA	CNMT	\$ COMPUTE CNMT=COS(XNODE-THTA)
	FCOS		\$
	TAM	CNMT	\$ CNMT
	TMA	DT1	\$
FAMS	TI		\$
ZDWIX	JMP	0	\$
CZDOTH	TJM	CZDOTWX	\$
	TMO	SNMT	\$ TEMP1=SNMT+CDEL+CNMT+SDEL TO COMPUTE
FMMR	CDEL	\$	
TMO	SDEL	\$	
F MAD	CNMT	\$	
TAM	TEMP1	\$ TEMP1	
FMMR	SNMT	\$ COMPUTE CNMT=CNMT+CDEL-SNMT+SDEL	
TMO	CDEL	\$	
FMSU	CNMT	\$	
TAM	CNMT	\$ CNMT	
TMO	TEMP1	\$ SET SNMT= TEMP1	
TQM	SNMT	\$	
TMA	SPCI	\$ COMPUTE ZDOTW=SNMT+CPSI+SPCI	
F MAD	CPSI	\$	
TAM	ZDOTW	\$	
CZDOTWXJMP	0		\$ EXIT

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SAME XYZSB,XYZ3 \$
ASGN DTERM, M/3752\$
SAME BJTLCE,M/3 \$
XYZI TJM (P)*3H \$
JMP BEGIN \$
JMP NTHCN \$ XYZ*1
JMP (P) \$
XYZ1 TJM XYZSWT1 \$
JMP XYZK25+1H \$
XYZ2 TJM XYZSWT2 \$
JMP (P)+4H \$
XYZ3 TJM XYZSBX \$
TIJ XYZSB3\$
TJM XYZSWT2 \$
TIJ XYZSWT1+1H \$
TJM XYZSWT1 \$
JMP XYZK25+1H \$
XYZSBG TJM XYZSBX \$
TIJ XYZSB3 \$
TJM XYZSWT2 \$
JMP XYZSB2 \$

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BEGIN TJM BEGINX\$
TMO HXOS
FMMR HXOS
TMO HYOS
FMAD HYOS
TMO HZOS
FMAD HZOS
TAM PS
TDM PO \$
S FSQRT \$
TAM RTPS
TMA F/1\$
FDA RTPS
FMMR HXOS
TAM WXS
FMMR HYOS
TAM WYS
FMMR HZOS
TAM WZS
TDM COSIS
TDO \$
FCSQ \$
FMAR \$
FAM F/1\$
S FSQRT \$
TAM SINIS
TDM XMZS
TDO \$
TMA COSIS
JMP ARCTANS
TAM XINCLS
TMA F/1\$
FDA SINIS
FMMR WXS
TAM SINOS
FMMR WYS
TAQ \$
FCSQS COSOS
TMO SINOS
JMP ARCTANS
TAM XNODEOS
TMO AXNOS
FMMR AXNOS
TMO AYNOS
FMAD AYNOS
TAM ESQS
S FSQRT \$
TAM EOS
TMA F/1\$
FSM ESQS
TAM AOS
S FSQRT \$

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TAM RTEQS\$
TMA PS
FDAS AOS
TQA \$
S FSQRT \$

TAM RTAS
TMA XNODEOS
TMO WZS
JQN (P)+2HS
FCSM XNODEOS
FAM XLOS
TAM UOS
TMO SINIS
FMMR SINIS
FDA F/.666666667\$
FCSQ \$
FAM F/1\$
FDA PS
FMMR RTEQS\$
FDA PS
FMMR P3JA02\$
FDA F/2\$
TMA F/1\$
FSQ \$
TAM XNOREV\$
FDA AOS
FMMR XKERTMS\$
FDA RTAS
TQM XNOS
FMMR XNOS
FDA PIO36\$
FMMR COS
TAM CS
BEGI4X JMP OS

DELTPI S
XNOREV S
NTHCNV TJM NTHCNX\$
TMO AOS
TMA F/1\$
FSM EOS
FMARS QOS
TMA SINIS
FDA F/-4\$
FMMR SINIS
FAM F/2\$
FSMA COSIS
FDA PS
FMMR P3JA02\$
FDA PS
TQM DELTPIS\$
TMO XM4U3\$
FMMR CS

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TAM XM4C03\$
NTHCNX JMP OS

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XYZS9X JMP (P) S
XYZK25 TJM XYZSBX S
TMA F/.06 S
TMO EO S
JAGQF (P)+3H S COMPUTE D IF E LESS THAN .06
TMA F/0 S
JMP NODTERM S SET D = 0
TMA XYZND S
FSM XNO S
THQ F/0.20061256E-2S K=66
JAGQF (P)+3H S
THQ F/13.0 S K=66
JMP (P)+5H S
THQ F/3 S
FMARS A S
FAM XYZND S
FDA A S
FMMR C S
FUA 1UVA S K=66
FMMR C S
NODTERM TAM DTERM S END COMPUTING D
TMO F/1.5 S START COMPUTING A
FMMR DTERM S
TMO T S
FMAR S
FAM C S
FMAR S
TMO F/2 S
FMAR S
FAM F/1 S
S FLOG2X \$

TMO F/-666666667\$
S FMAR \$
S F2X \$

TMO AO S
FMARS A S END COMPUTING A
S FSQRT S

TAM RTAS
TMO AS
FMARS XNS
TMA XKES
FDAS XNS
TMA F/1E-10 S K=66
TMO EO S K=66
JAGQF (P)+4H S K=66
TMA AS
TMO QOS
JAGQF (P)+7H S K=66
TMD F/0\$
TDM ES
TDM ESO S K=66
TMA A S K=66

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TDM P S K=66
JMP TAGRS S K=66
TQA S
FDA AS
TMA F/1S
FSQS ES
TDO S
FMMR ES
TAM ESQS
TMA F/1S
FAM ES
THQ QOS
FMARS PS
S FSQRT S K=66

TAM RTPS
TMA P3JA02 S
FDA PO S
FMMR XNO S
FDA PO S
TQM OMGDT S
FCSM COSI S
FMARSXNODOT S
TDO S
TMA XNODEOS
FMAD TS
TAM XNODES
XYZSWT1 JMP (P)
XYZSB2 TMA F/1S
FSM ESQS
S FSQRT S

TAM RTEQS\$
FCSM SINI S
TMO SINI S
FMAR S
TMO FLO 5 S
FMAR S
FAM FLO 4 S
FDA FLO 2 S
FMMRSOMGDT S
TMO TS
FMARS OMGASS S
FCOS S

TAM US S
TMA OMGAS S
FSIN S

TAM XLS
TMA F/0\$
TMD EOS
JAED XYZSB7\$
FCSM AYNOS
TMO XLS

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FMAR \$
 TMO US
 FMAD AXNOS
 FDA EOS
 FMMR ES
 TAM AXNS
 TMO US
 FMMR AYNOS
 TMQ XLS
 FMAD AXNUS
 FDA EOS
 FMMR ES
 TAM AYN \$
 XYZSB10 TMA SINIS
 FDA PS
 FMMR MJ3AOJ2\$
 FDA F/2\$
 TMO L3\$
 TOA \$
 FAMS AYNS
 XYZSB9 TMO T \$
 FMMR DTERM \$
 FAM C \$
 FMAR \$
 FAM F/1 \$
 FAM DELTPI \$
 FMAR \$
 TAQ \$
 FMMR XNO \$
 FAM XLO \$
 TAM XL \$
 TMA F/1\$
 FAMA COSIS
 TAM DENOMS
 TAQ \$
 FMMR F/5\$
 FSM F/2\$
 FDA DENOMS
 FMMR AXNS
 FDA F/2\$
 FMRS L3\$
 FAMS XLS
 TMQ F/0\$
 TMA WZ\$
 JAGOF XYZSB21\$
 TMA XLS
 FAM XNODES
 XYZSB22 FDA TWOPIS
 TQA \$
 JMP SEPSUB\$
 FMMR TWOPIS
 TAM US
 XYZSWT2 JMP (P)
 XYZSB21 FCSM XNODES
 FAM XLS

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JMP XYZSB22\$
 XYZSB3 TMA XNODE \$
 S FSIN \$
 TAM XNY\$
 TDM SINOS
 TMA XNODE \$
 S FCOS \$
 TAM XNX\$
 TDM COSOS
 TMO SINIS
 FMMR XNY\$
 TAM WXS
 FCSM XNX\$
 FMARS WYS
 TMO COSIS
 FCSM XNY\$
 FMARS XMXS
 FMMR XNX\$
 TAM XMY\$
 TMA RTEQS\$
 FAM F/1\$
 TAQ \$
 FMAR \$
 TMO RTEQS\$
 FMARS DENMS
 TMD US
 TDM E01\$
 XYLP CM XYZSBZ \$
 TMA E01 \$
 S FSIN \$
 TAM SINEOS
 TMA E01 \$
 S FCOS \$
 TAM COSEOS
 TDQ \$
 TMA AYNS
 FMAR \$
 TMO AXNS
 FMSU SINEOS
 TAM ESINES
 FAM US
 TAM E02\$
 FSM E01\$
 TAQ \$
 FCQA \$
 TMO TENM6\$
 JAGOF XYLPI\$
 JMP XYZLP2\$
 XYLPI TMD E02\$
 TDM E01\$
 TMA N/30T15 \$

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INCA XYZSBZ \$
JAED (P)+2H \$
JMP XYLP+1H \$

XYZLP2 TMQ SINEOS
FMMR AYNS
TMQ COSEOS
FMAD AXNS
TAM ECOS\$
TDQ \$
TMA F/1\$
FSQ \$
TMQ AS
FMARS RS
TQA \$
FDA RS
TQM ARS
THA RTAS
FDA RS
FMMR ESINES
TAM RDOTS
FMMR RTEOS\$
TAM RVDOTS
TMA RTEOS\$
FAM F/1\$
TAM SINUS
THA ESINES\$
FDAS SINUS
FCSH AXNS
TMQ SINUS
FMAD AYNS
FAM COSEOS\$
TMQ ARS
FMARS COSUS
FCSH AXNS
TQA \$
FCSH AYNS
FMAD SINUS
FAM SINEOS\$
TMQ ARS
FMARS SINUS
TMQ COSUS\$
FMMR XNX\$
TMQ SINUS
FMAD XMXS
TAM UXS
FMMR XNX\$
TMQ COSUS\$
FMSU XMXS
TAM VXS
FMMR XNYS
TMQ SINUS
FMAD XMY\$
TAM UYS
FMMR XNYS
TMQ COSUS\$

FMSU XMY\$
TAM VYS
FMMR XMZS
TAM VZS
TMQ SINUS
FMMR XMZS
TAM UZS
TMQ RS
FMMR UX\$
TAM X\$
FMMR UYS
TAM Y\$
FMMR UZS
TAM Z\$
TMQ RDOTS
FMMR UX\$
TMQ RVDOTS\$
FMAD VXS
TAM XDOTS\$
FMMR VYS
TMQ RDOTS\$
FMAD UYS
TAM YDOTS\$
FMMR UZS
TMQ RVDOTS\$
FMAD VZS
TAM ZDOTS\$
JMP XYZSBX\$

XYZSB7 TDM AYNS
TMD ES
TDM AXNS
JMP XYZSB10\$

C ARCTAN TJM ONODE8\$
TAM ONODE10\$
TQM ONODE10+1\$
THA F/0\$ NODE ACCORDING TO
TMD ONODE10\$
JAED ONODE5\$
JDP ONODE1\$ USED. THE A,Q,D REGISTERS
THA PIS
JMP ONODE3\$ ENTRY
ONODE1 TMD ONODE10+1\$
JAED ONODE8\$
JDP ONODE3\$ THE RESULT IS STORED IN
THA TWOPIS
ONODE3 TAM ONODE10+2\$
JMP ONODE7\$ 10TH. SIGNIFICANT DECIMAL DIGIT
ONODE5 TMD ONODE10+1\$
JAED ONODE8\$
JDP ONODE6\$ SUBROUTINE.....
ONODE6 THA PIOV2\$
JMP ONODE8\$
ONODE7 THA ONODE10+1\$

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```
FDA  ONODE10$  
TQA  S  
S    FATA$  
  
FAM  ONODE10+2$  
ONODE8 JMP 0$  
L ONODE10SET (P)+3$
```

* GENERALIZED SUBROUTINE TO CONVERT ANY FLOATING
* POINT NUMBER TO ITS FRACTIONAL AND INTEGRAL
* PARTS. NUMBER IN ACC. AT ENTRY, INTEGER IN ACC.,
* FRACTION IN Q REG. ON EXIT.

```
C SEPSUB TJM  SEPSUBX$  
TAM  SEPSUB3$  
FCAMA SEPSUB3$  
TMQ  1/1T1J0/43T47$  
JAGQF SEPSUB1$  
TAQ  S  
ETA  1/1T36$  
JAZ  (P)+4H$  
TMA  F/0$  
TMQ  SEPSUB3$  
JMP  SEPSUBX$  
ETA  11/1T47$  
SLA  8$  
AM   C/CAIC/SLAQN,12$  
TAM  SEPSUB2$  
SRQ  12$  
  
L SEPSUB2 CA  S  
SLAQN 12+0$  
SLA  12$  
AM   D/35$  
TAM  SEPSUB2$  
TMD  SEPSUB3$  
JDP  (P)+5H$  
FCSQ  S  
TAQ  S  
FCSH  SEPSUB2$  
JMP  (P)+4H$  
FCAQ  S  
TAQ  S  
FCAM  SEPSUB2$  
SEPSUBXJMP 0$  
SEPSUB1TMQ F/0$  
TMA  SEPSUB3$  
JMP  SEPSUBX$  
SEPSUB3$
```

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```
TLC  TJM  TLC4$  
TXDLC ,1$  
TDM  TL2$  
TMD  TL1$  
TDXLC ,1$  
ETD  6/1T47$  
TDQ  S  
TMA  D/9$  
JAGO  (P)+2H$  
JMP  BJTLC E$  
MM   TL3$  
TQA  S  
SLA  8$  
TMQ  TL4$  
EIS  TLC1$  
EIS  TLC2$  
EIS  TLC3$  
R TLC1 TMD ,1$  
TMD THGROS$  
R TLC2 TMD ,1$  
TMD XLSUNOS$  
R TLC3 TMD ,1$  
TMD C3$  
TMD TL2$  
TDXLC ,1$  
TLC4 JMP S  
TL1  C/HLTR,YCONSS  
TL2  S  
1/1$ CONSTANTS MUST FOLLOW THIS WORD  
CGP  S  
MJ3A0J2F/2,1251E-3$  
10VA F/0,25 S  
DENOM S  
L3  S  
XY1  S  
TL3  D/3$  
TL4  28/1/12/0/8/1$  
* A-1 HLT REMOVED  
XYZSBZ S  
XYZND F/.072722052$  
YCONS F/98,67401$  
F/278,6797$  
F/-3,5728$  
F/99,42094$  
F/279,4267$  
F/-2,8431$  
F/99,18222$  
F/279,1879$  
F/-3,0990$  
F/98,94349$  
F/278,9491$  
F/-3,3549$  
F/98,70477$  
F/278,7104$
```

CN T-266
K-66

CN T-29

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F/-3,6100\$
F/99,45170\$
F/279,4573\$
F/-2,8811\$
F/99,21297\$
F/279,2186\$
F/-3,1370\$
F/99,39817\$
F/279,3958\$
F/-2,8850\$
F/99,15144\$
F/279,1571\$
F/-3,0610\$
F/98,91273\$
F/278,9184\$
F/-3,3169\$

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ER10	TJMR	EREKS
	TMO	EREKS
	ETA	0/4T39\$
	JAZ	EREKPS
	TIJ	PRERSS
	TJM	E3FWR1\$
	TQD	S
	TOXLC	,1\$
	SIXOL	1,1\$
	TMA	,1\$
ER11	SH	D/1B16\$
	SRA	32\$

R	RPTNN	5\$
	SRAQ	3\$
	BRO	3\$
	TOM	PRERLS
	TMA	E3WORS
	JMP	GLOP.GLOPS
ER12	TMA	PHAINS
	JAZ	NXTCASE
	TMD	F/1.0\$
	JAED	NXTELS
	TMD	F/2.0\$
	JAED	START3
	TMD	F/3.0\$
	JAED	START2
	TMO	F/5
	JAGOF	(P)•2H
	JMP	NXTCASE
	TIXZ	0,4
	JAEQ	TRERR
	JMP	FNERR
EREXP	TIJ	PRERES
	TJM	E3FWR1\$
	ETA	0/77777T15\$
	JMP	ER11\$

PRERS A/SUBROUTINE ERROR \$

PRERE A/EXONENT OVERFLOWS

PRERC A/FROM LOCATIONS

PRERL	S	
L E3WOR	HLT	\$
	TIJL	E3FWORS
	E3FWOR	HLT 17•128•17\$
	E3FWR1	TMA S
		HLT 31•128•13\$
		TMA PRERCS
		HLT 37•128•5\$
	CAM	PRERLS

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L EREX HLT S
 HLT S
 TLCE TMD SATNS
 SCD 18S
 TDM PSATNS
 TMA TWOR1\$
 JMP GLOP.GLOPS
 JMP NXTELS
 L TWOR1 HLT S
 TIJL TFWORS
 L TFWOR HLT 15+128+11\$
 TMA PRELMS
 HLT 20+128+3\$
 TMA PSATNS
 HLT 37+128+16\$
 PRTLC W/ILLEGAL S
 W/YEAR S
 PRELM A/ELEMENT NO.S

ANGSN1 TJM ANGSNX\$
 TMA TI \$
 FDA XMNPDAS
 TMA ORGDA \$
 FAM ORGTM \$
 FAQ S
 TMO C1S
 FMARS TEMS
 FAM C3S
 TMO DE2RAS
 FMAR \$
 FSIN \$

A
 TAO \$
 FMMR C2S
 FAM TEMS
 FAM XLSUNOS
 TAM XLSUNTS
 FDA RADYNS
 FMMR F/2.0\$
 FSIN \$

A
 TMO C4S
 FMAR \$
 FSM XLSUNTS
 TAO \$
 FCSM DE2RAS
 FMARS ALSUNS
 FCOS \$

A
 TAM CSALSS
 FSIN ALSUNS

TAO SNALSS

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A
 TDO S
 FMMR C5\$
 FATAN S
 TAM DLSUNS
 FSIN \$
 TAM SNDLSS
 TDM SUNLZS
 FCOS DLSUNS
 TAM CSDLSS
 TMO CSALSS
 FMARS SUNLXS
 TMO CSDLSS
 FMMR SNALSS
 TAM SUNLYS
 TMO CAPXS
 FMMR CAPXS
 TMO CAPYS
 FMAD CAPYS
 TMO CAPZS
 FMAD CAPZS
 FSQRT \$
 TAM CAPRS
 TMO CAPXS
 FMMR SUNLXS
 TMO CAPYS
 FMAD SUNLYS
 TMO CAPZS
 FMAD SUNLZS
 FDA CAPRS
 FCSQS SNHSNS
 FAM F/.0871557
 JAN ANGSN2\$
 ANGSN3 TMD F/-1.0\$
 TDM XILLUMS
 ANGSNX JMP (P)\$
 ANGSN2 TMO SUNLX
 FMMR XS
 TMO SUNLYS
 FMAD Y\$
 TMO SUNLZS
 FMAD Z\$
 TAO
 FMAR
 TMO R
 FHSU R
 THQ F/1
 JAGOF CALIL2
 JHP ANGSN3
 CALIL2 THD F/1.0\$
 TDM XILLUMS

\$ SINE 5 DEGREES

\$ \$ \$ \$ \$

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JMP ANGSNX\$

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AJPACK	TJM	AJPKXX	
	CD		\$
TXDLC	0.3X		\$
TXDRC	0.4X		\$
TDM	AJSV34		\$
TMD	AJCOL79		\$
TDXL	0.4X		\$
THA	AJHOLD		\$
FAM	AJMIN		\$
TAQ			\$
FMMR	F/100.		\$
FAM	F/.4		\$
TAQ			\$
JMP	AJFIXIT		\$
SLA	25		\$
TAM	0.4X		\$
TMA	SATCONTS		\$
SRA	19		\$
AHS	0.4S		\$
TMO	AJAZ		\$
FMMR	F/572.957795		\$
FAM	F/.4		\$
TAQ			\$
JHP	AJFIXIT		\$
SLA	1		\$
AM	AJFLGIT		\$
CM	AJFLGIT		\$
AHS	0.4X		\$
TMA	4C4+2		\$
JAZ	(P)>4H		\$
TMA	ELNO		\$
SLA	32		\$
JMP	4ELNO3		\$
TMO	AJREV		\$
JMP	AJFIXIT		\$
SLA	30		\$
TMD	C/HLT,SATNOS		\$
TDXL	>1		\$
TMD	SATCONT		\$
ADXL	>1		\$
TMO	15/1T17		\$
ES	0.1		\$
SLA	2		\$
4ELNO	3TMO	6/1T5;32/1T47	
EIS	1.4		\$
TMO	42/1T47		\$
TMA	AJFAN		\$
EIS	1.4		\$
TMO	AJRANGE		\$
FMMR	AJCNV1		\$
FAM	F/.4		\$
TAQ			\$
JMP	AJFIXIT		\$
SLA	18		\$
TMO	16/1T15		\$

BUFFER AND BL

100 X MINUTES

10 X AZ AT T4

REV NO. AT T1

RANGE AT T29
IN KM OR NM

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TMD	14/1T29	S
JAGD	(P)+1	S
JMP	(P)+1	S
CA		S
EIS	1,4X	S
TMD	AJCNV2	S
FMMA	AJR RATE	S
TAQ		S
FMMR	F/10.	S
FAM	F/.4	S
TAQ		S
JMP	AJFIXIT	S
SLA	11	S
TMD	30/1T29	S
TMD	7/1T36	S
JAGD	(P)+1	S
JMP	(P)+1	S
TDA		S
EIS	1,4X	S
TMD	AJR RATE	S
JDP	(P)+3H	S
TMD	1/1T37	S
DORMS	1,4X	S
TMD	F/572,957795	S
FMMAR	AJELEV	S
FAM	F/.4	S
TAQ		S
JMP	AJFIXIT	S
TMD	38/1T37	S
TMD	10/1T47	S
JAGD	(P)+1	S
JMP	(P)+1	S
TDA		S
EIS	1,4X	S
TMD	AJELEV	S
JDP	(P)+3H	S
TMD	1/1T0	S
DORMS	1,4	S
TMD	C/HLT,AJBFFR+128/C/HLT,AJP KITA	S
AIXJ	2,4X	S
SIXOL	128,4X	S
TMD	AJCOL79	S
TXDLC	0,4X	S
TDA		S
AM	D/1	S
TAM	AJCOL79	S
AJP KIT A TMA	N/7T23IN/1T39IH/19T47	S
JMP	SYS	S
TIO	AJBFFR	S
JMP	SYSNO	S
TMD	C/HLT,0/C/HLT,SYSTAB+7	S
JMP	SYSIO	S
JMP	(P)+2	S
AJP KIT A TMD	AJCOL79	S

10 X RRATE AT
IN KM/SEC OR
RR SIGN AT T3
10 X ELEV AT
ELEV SIGN
AT TO
OF

OUTPUT
ONTO
TAPE
(A BLOCK AT A
PACKED
PAIRS OF
DATA READY
FOR
TIME
ORDERING.

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TXDLC	0,4X	S
TDM	AJCOL79	S
TMD	AJSV34	S
TXDLC	0,3X	S
TXRC	0,4X	S
AJP KXX	JMP (P)	S
AJNODTA	TIJ AJND1 S	S
	TJM AJDLOOPS	S
	TIJ AJADREXS	S
	TJM AJCLU+3HS	S
	TIJ AJHEDEXS	S
	TJM AJHDU+3HS	S
JMP	AJDAYSS+1H	S
AJND1	JMP PANT. SPACE	S
TMD	AJTYSH	S
JDP	(P)+1	S
JMP	PANT.TSPACE	S
TMA	AJNDCH	S
JMP	GLOP.GLOP	S
TMD	AJTYSH	S
JDP	(P)+3H	S
JMP	PANT.TPANT	S
JMP	AJTYEND	S
JMP	PANT.ALLFIN	S
JMP	NXTCASE	S
AJNDCH	C/HLT,0/C/TIJL,AJNDHW	S
AJNDHW	C/HLT,9+128+8/C/CAM,AJNDAA	S
AJNDAA	A/NO DATAS	S
AJENDPK	JHP 4SUMHRY S	S
	TIJ PANT.TPANTA	S
	TJM 4OUT 1+2H	S
	JMP PANT.PAGE	S
TMA	AJCOL79 S	S
TXDLC	0,4X	S
TMD	C/HLT,AJBFFR+C/HLT;0	S
JAED	AJNDTA	S
TMD	C/HLT,AJBFFR+128/C/HLT,AJP KITB	S
AIXJ	0,4X	S
JMP	(P)+3	S
AJP KIT B TMD	47/1T47	S
TDM	0,4X	S
TDM	1,4X	S
AIXOL	2,4X	S
JMP	AJP KITB-3H S	S
SIXOL	128,4X	S
TMA	AJCOL79	S
AM	D/1	S
TAM	AJCOL79	S
TIJ	AJP KITC S	S
TJM	AJP KITA-1HS	S
JMP	AJP KFIN	S
AJP KITC	TMA N/7T23IH/8A747S	S
JMP	REWIND S	S

WORDS OF
47 ONFS
FOR
REMAINDER
OF BLOCK.

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JMP AJSRTITS
AFEND 50S
XSRCH TJM XSRCHX
CM XSRCH9
TJM XSRCH11\$
TXDLC ,1
TXDRC ,2
TDM XSRCH1
TXDLC ,3
TXDRC ,4
TDM XSRCH2
TXDLC ,5S
TXDRC ,6S
TDM XSRCH3
TAD
TDXRC ,6
XSRCH4 TMD XSRCH2
TDXLC ,3
TMO ,6
TDXRC ,5
TMD XSRCH4
TDXLC ,1
TDXRC ,4
ETD 0/177715\$
SDXL ,4
ETD 0/17778
TDM CARD.T4
ETA 0/7T8
SRD 7
JAZ XSRCH8
XSRCHC TDXLC ,2
SDXL ,1
SDXR ,3
ETD 0/17T5
SRD 10
ADXL ,3
ETA 0/1T41
JAZ (P)+2H
TJM XSRCH9
ETA 0/3T23
SLA 8
AM XSRCH10
TAM XSRCHF

L XSRCHF HLT
HLT
SIXO 2,3
TMO 2,3
TMA 1,3

L RPTN 6
SRAQ ,1
TQM XSRCHWS

L RPTN 6

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SRAQ ,2
TMA ,3
L RPTN 6
SRAQ ,1
TQM XSRCHYS
TMA XSRCH4\$
TXDLC ,4S
JAGD XSRCHGS
XSRCHJ TMO XSRCHWS
SIXOL 8,4S
JMP XSRCHHS
AIXOL 8,4S
TMA XSRCHZ\$
L XSRCHF JMP 0S
JMP XSRCHDS
TXDLC ,4S
JAED (P)+2H
JAGD (P)+3HS
TQA S
JMP XSRCHDS
TQM 1,5S
TMA XSRCHWS
XSRCHD TAM ,5S
TMA FXERCLS
JAZ XSRCHKS
TMA XSRCH9\$
JAZ (P)+2HS
JMP (P)+3HS
AIXU 1,6S
JMP XSRCHAS\$
TMD XSRCH1\$
TDXLC ,1S
TDXRC ,2S
TMD XSRCH2\$
TDXLC ,3S
TDXRC ,4S
TMD XSRCH3\$
TDXLC ,5S
TDXRC ,6S
TMA XSRCH11\$
XSRCHX JMP 0S
XSRCHG JAED XSRCHJS
JMP XSRCHHS
TQA S
TMO XSRCHWS
JMP XSRCHES
XSRCHH TJM XSRCHIS
TMA XSRCHZ\$

L RPTN 6S
SLO ,4S
RPTN 6S
SRAQ ,4S

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XSRCH1 JMP 0\$
 XSRCH2 CM XSRCH1\$
 JMP XSRCHD+3H\$

 XSRCH1 \$
 XSRCH2 \$
 XSRCH3 \$
 XSRCH4 C/HLT,0;C/HLT,16\$
 XSRCH5 C/HLT,0;C/HLT,1\$
 XSRCH6 C/TAM,XSRCH1;C/TMA,XSRCH4\$
 XSRCH7 C/JMP,FXINT;C/JMP,XSRCHD\$
 XSRCH8 C/JMP,FXFLT;C/JMP,XSRCHD\$
 XSRCH9 \$
 XSRCH10C/TMD,XSRCH6;C/TDM,XSRCHES
 XSRCH11\$
 XSRCHB TMD XSRCH5\$
 JMP XSRCHC\$
 XSRCHW \$
 XSRCHY \$
 XSRCHZ W/ \$

E AFEND \$
 AJSRIT TMA AJCOL79 \$

TDM AJCNV1\$

SLA 32

TIKZ 1,1X

SM AJNMBLK

JAZ (P)+4H

JAN (P)+3H

AIXOL 1,1X

JMP (P)-2

AM AJNMBLK

TAM AJLSTBK

CD

TXDLC 0,1X

TDM AJSVXR1

SCD 33

JDP (P)+1

JMP (P)+1

CSMS AJCNV1

TMD C/HLT,1;C/HLT,AJSRTA

AIXJ 0,1X

TMD AJLSTBK

JMP (P)+1

AJSRTA TMD AJNMBLK

TDM AJCMNBK

TMD C/HLT,AJBFFRIC/HLT,AJBFFXS

TXDLC 0,5X

TXRC 0,6X

THA N/8T23;H/BAT47 \$

JMP REWIND \$

THA N/9T23;H/BAT47 \$

JMP REWIND \$

AJSRTB JMP AJRD7

JMP AJMERGE

TMD C/HLT,0;C/HLT,AJSRTC

DETERMINE
NUMBER
OF TAPE
READS
REQUIRED.

XR1= N TIMES
AJNMBLK=MAX,C
AJLSTBK=LAST

TAPE ALTERNAT

SET UP
INPUT AND
OUTPUT BUFFER

READ AND
MERGE, IF REQ.

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SIXJ 1,1X \$ IS MERGE ALL
 TMA N/7T23;H/BAT47 \$
 JMP REWIND \$
 JMP AJCNGTM-3H \$
 AJSRTC TMD C/HLT,1;C/HLT,AJSRTB \$ NO,IS IT ONE
 SIXJ 0,1X \$ NO,CONTINUE
 TMD AJLSTBK \$ YES,SET UP FO
 TDM AJCMNBK \$ PARTIAL CORE,
 JMP AJSRTB \$
 TMD AJSVXR1 \$
 TDXLC 0,3X \$
 CM AJMRGSW \$
 AJCNGTMTMD C/HLT,1;C/HLT,AJSRTD \$ PROCESS TAPE
 AIXJ 0,3X \$ FOR PROPER
 CSM AJLSTBK \$ TIME FORMAT,
 TAM AJMRGSW \$ AJMRGSW=
 TMD AJLSTBK \$ =>,PARTIAL COR
 JMP (P)+1 \$ =>,FULL AND/OR
 AJSRTD TMD AJNHBLK \$ CORE.
 TDM AJCMNBK \$
 TDXLC 0,4X \$
 THD 4LMAX \$ IN
 TDXLC 0,5X \$ TAPE
 TMA N/8T23;N/1T39;H/91T47 \$
 JMP SYS \$ 8.
 TIO 0,5X \$
 JMP SYSNO \$
 TMD C/HLT,0;C/HLT,SYSTAB+B \$
 JMP SYSIO \$
 AIXOL 128,5X \$
 TMD C/HLT,0;C/HLT,AJSRTD+5H \$
 SIXJ 1,4X \$
 TMD AJMRGSW \$ IF PARTIAL

 L JDP (P)+8H \$
 SIXOL 128,5X \$ LENGTH BY
 TMA 47/1T47 \$ SENTINEL SEAR
 RPTAN 64 \$
 TMD 2,5X \$
 JAED (P)+2H \$
 AIXOL 2,5 \$
 SIXOL 2,5X \$
 CD \$
 TXDRC 0,5X \$
 TDA \$
 SM 4RMAX \$
 SRA 1 \$
 AM 4LMAX \$ COMMAND WORD
 L AJLEAP TAM AJSVSV \$ ADDR.(T15)IND
 SIXOL 2,5X \$
 AJINSHRJMP (P)+1H \$
 TMQ 23/1T22 \$
 ETA 0,5X \$
 TAQ CA \$
 EXTRACT FROM
 EACH PAIR (IN
 OR

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SRG 25
 DAQ D/144000
 SLO 42
 TQM AJSV34
 TAQ
 CA
 DAQ D/6000
 SLO 37
 TQM AJHR
 TAQ
 CA
 DAQ D/100
 SLO 31
 TQM AJMIN
 SLA 24
 TMQ 6/1T16
 EI AJMIN
 SLO 6
 EI AJHR
 SLO 5
 EI AJSV34
 SLA 1
 TMQ 25/1T47
 EIS 0,5X
 TMD 4LMAX2
 SIXO 2,5
 JNO AJINSMR
 AJLEAPDTMD AJSVSV
 TDXLC 0,4X
 TDXRC 0,5X
 TMA CONTG
 JAZ (P)+1
 JMP AJSATST
 JMP AJOUTPT
 AJCTAGNTMD C/HLT,0;C/HLT,AJCNGETM
 SIXJ 1,3X
 TMA CONTG
 JAZ (P)+1
 JMP AJGHPIIT
 JMP PANT-FINISH\$
 JMP NXTCASE \$
 L AJT8CD N/8T23;N/1T39;W/91T47
 C/HLT,0;C/HLT,SYTAB+8
 N/9T23;N/1T39;W/19T47
 C/HLT,0;C/HLT,SYTAB+9
 AJT9CD N/9T23;N/1T39;W/91T47
 C/HLT,0;C/HLT,SYTAB+9
 N/8T23;N/1T39;W/19T47
 C/HLT,0;C/HLT,SYTAB+8
 AJMRCH1\$
 AJMRCH2\$
 AJMRCH3\$
 AJMRCH4\$
 AJMERGETJM AJMRGX
 TMA AJCNV1

S CONVERT TO
 SS DAYS ELAPSED.
 SS HOURS.
 SS MINUTES,
 SS FRACMIN.
 SS REINSERT
 SS IN FORM.
 SS DAYS ELAPSED
 SS HOURS AT T10
 SS MIN AT T16
 SS JUMP TO FINAL
 SS OUTPUT PHASE
 SS PUT OUT HARDC
 SS AND TTY(IF RE
 SS CONTINUE
 SS OR
 SS FINISH AJJ K=1
 SS READ T8
 SS AND
 SS WRITE 9
 SS READ 9
 SS AND
 SS WRITE T8.
 SS READ
 SS AND
 SS WRITE
 SS COMMANDS.
 SS MERGE

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TMD C/HLT,AJT8CD;C/HLT,AJMRCH1
 JAN (P)+1 \$
 TMD C/HLT,AJT9CD;C/HLT,AJMRCH1 \$
 TDXLC 0,2X \$
 TDXRC 0,3X \$
 RPTAA 4 \$
 TMD 1,2X \$
 TDM 1,3X \$
 TMD 4LMAX \$
 TDXLC 0,2X \$
 TMD AJCMNBK \$
 SCD 41 \$
 TDXLC 0,3X \$
 TMD AJDNCNT \$
 TDXLC 0,4X \$
 TMD C/HLT,0;C/HLT,AJMRGIT+1H \$
 AIXJ 0,4X \$
 JMP AJCORTT \$
 JMP AJRD89 \$
 AJMRGITTMQ 47/1T47
 ETA 0,5X \$
 ETD 0,2X \$
 JAGD AJMRGA+1 \$
 TMD 0,5X \$
 TDM 0,6X \$
 TMD 1,5X \$
 TDM 1,6X \$
 TMD C/HLT,AJBFFR+128;C/HLT,AJCK6X \$
 AIXJ 2,5X \$
 SIXOL 128,5X\$
 TMD C/HLT,0;C/HLT,AJMRGA \$
 SIXJ 1,4X \$
 TDM AJMRGSW \$
 JMP AJCK6X \$
 AJMRGA JMP AJRD89 \$
 JMP AJCK6X \$
 TMD 0,2X \$
 TDM 0,6X \$
 TMD 1,2X \$
 TDM 1,6X \$
 AIXOL 2,2X \$
 TMD C/HLT,0;C/HLT,AJCK6X \$
 SIXJ 2,3X \$
 TMD 30/1T29 \$
 TDM AJMRGSW \$
 AJCK5X TMD C/HLT,AJBFFX+128;C/HLT,AJHRGB \$
 AIXJ 2,6X \$
 SIXOL 128,6X \$
 JMP AJWT89 \$
 AJMRGB TMA AJMRGSW \$
 JAZ AJMRGIT \$
 JAN AJDOTPE \$
 R AJDOCORRPTAA 2 \$
 TMD 1,2X \$
 IF OLD TAPE D
 PROCESS

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TDM	1,6X	\$	REMAINDER OF
SIXOL	2,3X	\$	
TMD	C/HLT,AJBFFX+128;C/HLT,AJDOCOR	\$	SCORE DATA
AIXJ	0,6X	\$	ONTO
SIXOL	128,6X	\$	NEW TAPE.
JMP	AJWBT89	\$	
TMD	C/HLT,0;C/HLT,AJCORTT	\$	
SIXJ	0,3X	\$	
JMP	AJREWTP	\$	
AJCORTTTMD	C/JMP,SYSC/TIO,0,2X	\$	
TDM	AJWBT89+1	\$	
CD		\$	
TXDLC	0,3X	\$	
SRD	7	\$	
TDXL	0,3X	\$	
AJMRGC	JMP AJWBT89	\$	
AIXOL	128,2X	\$	
TMD	C/HLT,0;C/HLT,AJMRGC	\$	
SIXJ	1,3X	\$	
TMD	C/JMP,SYSC/TIO,AJBFFXS	\$	
TDM	AJWBT89+1	\$	
JMP	AJREWTP	\$	IF CORE DONE,
R AJDOTPERPTAA	25	\$	
TMD	1,5X	\$	REMAINDER
TMD	1,6X	\$	OF TAPE DATA
TMD	C/HLT,AJBFFX+128;C/HLT,AJDOTPE	\$	SORTO
AIXJ	0,6X	\$	NEW TAPE.
SIXOL	128,6X	\$	
SIXOL	128,5X	\$	
JMP	AJWBT89	\$	
TMD	C/HLT,0;C/HLT,AJTAPTT	\$	
SIXJ	1,4X	\$	
JMP	AJREWTP	\$	
AJTAPTTTMD	C/JMP,SYSC/TIO,AJRFFX	\$	
TDM	AJRD89+1	\$	
JMP	AJRD89	\$	
JMP	AJWBT89	\$	
TMD	C/HLT,0;C/HLT,AJTAPTT+1	\$	
SIXJ	1,4X	\$	
TMD	C/JMP,SYSC/TIO,AJRFFR	\$	REWIND
TDM	AJRD89+1	\$	OLD AND
AJREWPTPTMA	C/HLT,0;C/HLT,SYTAB+8	\$	NEW TAPE.
TMA	N/9T23;H/8AT47	\$	
JMP	REWIND	\$	
TMA	N/9T23;H/8AT47	\$	
JMP	REWIND	\$	
TMA	AJCMNBK	\$	
AMS	AJDNCNT	\$	UPDATE BLOCK
CSMS	AJCNV1	\$	SWITCH ALTERN
CM	AJMRGSW	\$	CLEAR MERGE S
AJMRGSX	JMP (P)	\$	
L AJRD89	TJM AJRDINX	\$	
THA	AJMRCW1	\$	TAPE
JMP	SYS	\$	READ.
TIO	AJRFFR	\$	

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JMP	SYSNO	\$	
TMD	AJMRCW2	\$	
JMP	SYSSIO	\$	
AJRDINXJMP	(P)	\$	
L AJWBT89	TJM AJWBTX	\$	
TMA	AJMRCW3	\$	
JMP	SYS	\$	
TIO	AJBFFX	\$	
JMP	SYSSNO	\$	
TMD	AJMRCW4	\$	
JMP	SYSSIO	\$	
AJWBTX	JMP (P)	\$	
AJRD7	TJM AJRD7X	\$	
TMD	4LMAX	\$	
TDXL	0,2X	\$	IN
TMD	AJCMNBK	\$	RAW
TDXL	0,3X	\$	DATA
AJRD7A	TMA N/7T23;N/1T39;H/91T47	\$	FROM
JMP	SYS	\$	TAPE 7.
TIO	0,2X	\$	FILLING
JMP	SYSSNO	\$	UP AS
TMD	C/HLT,0;C/HLT,SYTAB+7	\$	MUCH CORE
JMP	SYSSIO	\$	AS
AIXOL	128,2X	\$	REQUIRED
TMD	C/HLT,0;C/HLT,AJRD7A	\$	OR
SIXJ	1,3X	\$	POSSIBLE.
TMA	AJCMNBK	\$	SORT
SLA	7	\$	
AM	4LMAX	\$	
SRA	24	\$	
AM	4LMAX	\$	
JMP	SORT-SORT	\$	
AJRD7X	JMP (P)	\$	
AJOUTPTJ	JM AJFINAL	\$	
CD	\$		
TXDLC	0,3X	\$	
TDM	AJSV34	\$	
AJ1OUT	JMP AJDAYSS	\$	
L AJDAYSSJMP	AJDAYEL	\$	
TMD	D/1	\$	
TMD	AJPAGES	\$	
TMA	CLSFY	\$	
AM	L/AJACN	\$	
TAD		\$	
TXRC	0,6X	\$	
TMD	0,6X	\$	
TDM	AJHDCY	\$	
TDM	AJTYCL	\$	
TMA	NOTTY	\$	
JAZ	AJTTY	\$	
CM	AJTYSW	\$	
JMP	(P)+3H	\$	AJTYSW+, NO T
AJTTY	CSM N/1T47	\$	=, TTY.
TAM	AJTYSW	\$	

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CD		\$
TDXL C	0,6X	\$
TDXRC	0,7X	\$
TIJ	AJCONT	\$
TJM	AJ1OUT	\$
TMD	AJTYSW	\$
JDP	(P)+1	\$
JMP	AJADR	\$
JMP	AJHEAD	\$
IF REQUESTED, TTY HEADING. HD COPY HDG.		
L AJDLOOP	AJDYCK	\$
TMD	AJSDAY	\$
JDP	AJG01	\$
TMA	AJCWJ	\$
JMP	GLOP.GLOP	\$
TMD	AJTYSW	\$
JDP	AJGO	\$
JMP	PANT.TPANT	\$
AJLOOP	TMD C/HLT,99JC/HLT,AJGO	\$
AIXJ	1,7X	\$
JMP	AJTYEND	\$
SIXOL	99,7X	\$
AFEND	80	\$
JMP	PANT.PAGE	\$
TMA	AJPAGE	\$
JMP	GLOP.GLOP	\$
TMA	D/1\$	\$
AMS	AJPAGES	\$
JMP	AJADR	\$
TIXZ	10,6	\$
TIJ	AJGOA	\$
TJM	AJHEDEX	\$
JMP	AJHDCY	\$
AJGO	TMD C/HLT,54JC/HLT,AJGOA	\$
AIXJ	1,6X	\$
SIXOL	54,6X	\$
JMP	AJHEAD	\$
AJGOA	JMP AJDLOOP	\$
AJGO1	TMQ 5/1T9	\$
ETA	0,4X	\$
SRA	1	\$
TAM	AJHR	\$
TMD	N/10T10	\$
JAGD	(P)+3	\$
TMD	C/HLT,15+128+ 2JC/TMA,AJHR	\$
TDM	AJFWL2	\$
SRA	1	\$
TAM	AJHR	\$
JMP	(P)+3H	\$
TMD	C/TCM,15+128+37JC/TMA,AJHR	\$
TDM	AJFWL2	\$
TMQ	6/1T15	\$
ETA	0,4X	\$
SRA	1	\$
TAM	AJMIN	\$
CHECK DAY ELAPSED		
IF NEW, OUTPUT		
TTY AND/OR HD COPY.		
CHECK TTY LINE COUN		
CONTINUE OR RESET		
CHECK HD COPY LINE		
CONTINUE OR RESET.		
EXTRACT		
HOURS.		
MINUTFS.		

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TMD	N/10T16	\$
JAGD	(P)+3	\$
TMD	C/HLT,17+128+ 2JC/TMA,AJMIN	\$
TDM	AJFWL3	\$
SLA	5	\$
TAM	AJMIN	\$
JMP	(P)+3H	\$
TMD	C/TCM,17+128+31JC/TMA,AJMIN	\$
TDM	AJFWL3	\$
TMQ	7/1T22	\$
ETA	0,4X	\$
SRA	1	\$
TAM	AJFRMIN	\$
TMD	N/10T23	\$
JAGD	(P)+3	\$
TMD	C/HLT,20+128+ 2JC/TMA,AJFRMIN	\$
TDM	AJFWL5	\$
SLA	12	\$
TAM	AJFRMIN	\$
JMP	(P)+3H	\$
TMD	C/TCM,20+128+24JC/TMA,AJFRMIN	\$
TDM	AJFWL5	\$
TMQ	12/1T34	\$
ETD	0,4	\$
SRD	5	\$
TDA	\$	
AM	C/HLT,0JC/HLT,SATNOSS	
TMQ	24/1316/018/1S	
EIS	SATRTS	
EIS	SATRT1	
L SATRT1	TMQ 15/1T17	\$
ETA	(P)	\$
SLA	2	\$
TMQ	10/1T15	\$
EA	1,4	\$
TAM	AJREV	\$
TMA	4C4+2	\$
JAZ	(P)+3H	\$
ETD	1,4	\$
TDM	AJREV	\$
TMQ	18/1T47S	\$
ETA	(P)	\$
TDM	AJSATS	\$
JMP	BINBCD	\$
TMD	BCDSAT	\$
SCD	30	\$
TDM	AJSAT1\$	\$
TMQ	12/1T46	\$
ETA	0,4X	\$
SLA	16	\$
TMQ	F/107374182.4	\$
FMAR		
FAM	F/.04	\$
TAM	AJAZ	\$
TMQ	5/1T5	\$

XXX00000

FL.PT.AZ,

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ETA	1,4	\$
SRA	10	\$
AM	C/THD,FNOTABJC/TDM,FANNO	\$
TAM	(P)+1	\$
L	NOP	\$
NOP		\$
TMD	ELFLAG	\$
JQO	(P)+3H	\$
TMD	W/	\$
TDM	FANNO	\$
TMD	14/1T29	\$
ETD	1,4X	\$
TDM	AJRANGE	\$
TMD	7/1T36	\$
ETA	1,4X	\$
SLA	6	\$
TMD	F/107374182.4	\$
FMAR		\$
FAM	F/.04	\$
TAM	AJR RATE	\$
TMD	1/1T37	\$
ETA	1,4X	\$
JAZ	(P)+1	\$
FCSMS	AJR RATE	\$
TMD	10/1T47	\$
ETA	1,4X	\$
SLA	17	\$
TMD	F/107374182.4	\$
FMAR		\$
FAM	F/.04	\$
TAM	AJELEV	\$
TMD	1,4	\$
JDP	(P)+1	\$
FCSMS	AJELEV	\$
TMA	DRCOSFL	\$
JAZ	BYPASS1	\$
TMA	AJAZ	\$
FSM	F/.04	\$
TAQ		\$
TMA	AJELEV	\$
JAP	(P)+3H	\$
FAM	F/.04	\$
JMP	(P)+2H	\$
FSM	F/.04	\$
JMP	COMPL	\$
TDM	TEMP1	\$
TJM	TEMP2	\$
TAM	TEMP3	\$
TMA	XFX	\$
TMD	XFY	\$
JMD	XFZ	\$
JMP	DOTPR	\$
FAM	F/.0005	\$
JAP	(P)+2H	\$

RANGE:

FL.PT.R=RATE,

FL.PT.ELEV,

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FSM	F/.0010	\$
TAM	RSV	\$
TMA	ZFX	\$
TMD	ZFY	\$
TMD	ZFZ	\$
JMP	DOTPR	\$
FAM	F/.0005	\$
JAP	(P)+2H	\$
FSM	F/.0010	\$
TAM	RSU	\$
TMA	YFX	\$
TMD	YFY	\$
JMP	DOTPR	\$
FAM	F/.0005	\$
JAP	(P)+2H	\$
FSM	F/.0010	\$
TAM	RSW	\$
BYPASS1	TMA AJCHL	\$
JMP	GLOP.GLOP	\$
TMD	AJTYSW	\$
JDP	(P)+10H	\$
TMA	0/32/42/1	\$
TMD	42/1T47	\$
TMD	ELFLAG	\$
SCD	1	\$
JDP	(P)+2H	\$
SRAQ	36	\$
TMD	LOCGB	\$
TDXL C	,1	\$
EIS	6,1	\$
JMP	PANT.TPANT	\$
AIXOL	2,4X	\$
TMD	C/HLT,01C/HLT,AJCONT	\$
SIXJ	1,5X	\$
TMD	AJMRGSW	\$
JDP	LOAD3X	\$
TMD	A/NO MORE S	\$
TDM	AJHRDTA	\$
TMA	AJCHMR	\$
JMP	GLOP.GLOP	\$
TMA	CLSFY	\$
JAZ	(P)+3H	\$
TMA	JSGP	\$
JMP	GLOP.GLOP	\$
TMD	AJTYSW	\$
JDP	(P)+1	\$
JMP	AJTYEND	\$
LOAD3X	TMD AJSV34	\$
TDXL C	0,3X	\$
AJFINAL	JMP (P)	\$
AJCONT	TMD AJTYSW	\$
JDP	(P)+1	\$
JMP	AJLOOP	\$
JMP	AJGO	\$

DECREMENT AND
CHECK COUNT.

CN-T350

CN-T350

CN-T350

CN-T350

IF DONE

FINISH

UP AND

EXIT.

OR

RETURN FOR

NEXT

DATA.

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AJDAYELTJM	AJDEXS		INITIAL ENTRY
TMO	5/1T4	\$	EXTRACT
ETA	0,4X\$	\$	
SRA	1	\$	
AJPRO	TAM AJDEPRES		DAYS
SRA	10\$	\$	ELAPSFED,
TAO	S		ADD
FMMR	F/32768\$		TO
FAM	FDAYS		FDAY
TAM	AJDAYS		AND
JMP	FYKLOKS		ENTER
CSM	D/1\$		
TAM	AJSMDAYS		
JMP	AJFIXIT	\$	SET
TAM	AJDDDS		AJSMDAY
THA	AJDAYS		SWITCH
JMP	DKLOKS		NEGATIVE.
TAM	AJDATES		
TAQ		\$	ALSO
SRA	12	\$	SAVE
SLQ	6	\$	IN
SRAQ	12	\$	AJDEPRE
TMA	AJDATE	\$	CURRENT
SLA	6	\$	DAY\$
SLAQ	30	\$	ELAPSED.
AM	0/61T1730/01T35	\$	
TAM	AJDATE	\$	
AJDEX	JMP (P)\$		EXIT,
AJDYCK	TJM AJDEX\$		NEW DATA ENTR
TMO	5/1T4	\$	
ETA	0,4X\$	\$	NEW AND OLD
SRA	1	\$	
TMD	AJDEPRES		DAY E1 APSED.
JAED	(P)+1\$		IF DIFFERENT.
JMP	AJPROS		AJPRO TO COMP
CM	AJSMDAYS		IF SAME, CLEA
JMP	AJDEXS		AJSMDAY SWITC
AJHEAD	TJM AJHEDEX	\$	HARDCOPY HEAD
JMP	PANT.PAGE	\$	
TMA	AJPAGE	\$	PAGE NUMBER
JMP	GLOP.GLOP	\$	
TMA	AJPAGES	\$	CLASSIFICATION
AM	D/1	\$	
TAM	AJPAGES	\$	LOOK ANGLE...
L AJHDSY NOP		\$	
L	JMP GLOP.GLOP	\$	DAY
TMA	AJCWI	\$	
JMP	GLOP.GLOP	\$	SAT.....R-
JMP	PANT.SPACE	\$	
TMA	C/HLT,10\$C/HLT,AJLN12	\$	
JMP	PANT	\$	
L AJHDJ	TMD C/HLT,77+128+44\$C/CAM,AJUNITSS	\$	
	TDM AJFWJ3	\$	

TMA	AJCWH	\$	
JMP	GLOP.GLOP	\$	AND
TMD	C/HLT,24+128+1\$C/CAM,AJCRLF	\$	
TDM	AJFWJ3	\$	
AIXOL	5,6X	\$	SPACE:
AJHEDEXJMP	(P)	\$	
AJADR	TJM AJADREX	\$	
	TMD AJADR=1	\$	
	TXDLC ,0	\$	
	TXDLC ,1	\$	
	TDM AJADR=1	\$	
	TXDLC ,2	\$	
	TDM AJADR=2	\$	
	JMP 4HEAD	\$	
	TMD AJADR=1	\$	
	TXDLC ,0	\$	
	TXDXRC ,1	\$	
	TMD AJADR=2	\$	
	TXDLC ,2	\$	
AJNOADRTMA	AJCWH	\$	
JMP	GLOP.GLOPS	\$	AJJ T-205
JMP	PANT.TPANTS	\$	AJJ T-205
L AJTYCL NOP		\$	AND
L	JMP GLOP.TGLOP	\$	
	TMA AJCWI	\$	A
	JMP GLOP.TGLOP	\$	
	JMP PANT.TSPACE	\$	
	TMA C/HLT,10\$C/HLT,AJLN12	\$	
	JMP PANT.TPANTA	\$	
L AJCLU	TMD C/HLT,77+128+44\$C/CAM,AJUNITSS	\$	
	TDM AJFWJ3	\$	
	TMA AJCWH	\$	
	JMP GLOP.TGLOP	\$	
	TMD C/HLT,24+128+1\$C/CAM,AJCRLF	\$	
	AJFWJ3	\$	
	TIXZ 5,7	\$	
	AJADREXJMP (P)	\$	
	AJTYENDTJM AJTNEX	\$	WRAP-UP
	TMA AJCWHM	\$	
	JMP GLOP.TGLOP	\$	
	TMA CLSFY	\$	
	JAZ JSTYEND	\$	
	TMA JSGP	\$	
	JMP GLOP.TGLOP	\$	
	JSTYENDTHA AJCWH	\$	
	JMP GLOP.GLOPS	\$	AJJ T-205
	JMP PANT.TPANTS	\$	AJJ T-205

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TMA	C/HLT,7;C/NOP,0	\$	
JMP	PANT.TSPACER	\$	AND
TMA	AJCWN	\$	
JMP	GLOP.TGLOP	\$	12 INCHES
TMA	AJCWLC	\$	OF
JMP	GLOP.TGLOP	\$	LETTER CHARA
JMP	PANT.TTYCSS	\$	AJ.I K-135
AJTNEX	JMP (P)	\$	
AJFIXITJM	AJFXEXT	\$	FIX FLT.PT.
ETD	12/1T47	\$	
CA		\$	
SCD	12	\$	
JDP	(P)+2H	\$	
JMP	AJFXEXT	\$	
SRD	4	\$	
TDXL	.2	\$	
SLAQ	1.2	\$	
AJFXEXT	JMP (P)	\$	EXIT.
AJGRPIT	TMA N/7T23;H/8AT47	\$	
JMP	REWIND	\$	
TMA	N/8T23;H/8AT47	\$	
JMP	REWIND	\$	
TMD	AJSVXR1	\$	
TDXL	0,3X	\$	
TMD	C/HLT,AJBFFR	\$	
TDXL	0,4X	\$	
AJGRPA	TMD C/HLT,1;C/HLT,AJGRPB	\$	INIT
AIXJ	0,3X	\$	
TMA	AJLSTBK	\$	AND
JMP	(P)+1	\$	
AJGRPB	TMA AJNMBLK	\$	READ
TDXL	0,7X	\$	
SLA	7S	\$	
AM	4LMAX	\$	
TDXL	0,6X	\$	INTC
TAM	AJCKEND	\$	
AJGRPC	TMA N/7T23;N/1T39;H/91T47	\$	
JMP	SYS	\$	
TIO	0,6X	\$	
JMP	SYSNO	\$	
TMD	C/HLT,0;C/HLT,SYSTAB+7	\$	
JMP	SYSIO	\$	
AIXOL	128,6X	\$	
TMD	C/HLT,0;C/HLT,AJGRPC	\$	
SIXJ	1,7X	\$	
TMD	4LMAX	\$	
TDXL	0,6X	\$	
TIXZ	0,7X	\$	
AJGRPD	TMA 0,6X	\$	IF S
TMD	47/1T47	\$	
JAED	AJGFIN	\$	FIN
CD		\$	

JAED	AJCLRLC	\$	SKIP
TMO	1/1T47	\$	LOC,
ETA	0,6X	\$	IF LA
JAEQ	(P)*1	\$	FOR T
JMP	(P)*3H	\$	AND S
JMP	AJHTBF8	\$	AND G
TMO	AJCLRLC	\$	
TMO	12/1T34	\$	
ETD	0,6	\$	
SRD	5	\$	
TDA	S		
AM	C/HLT,0;C/HLT,SATNOSS		
TMO	24/1316/0;8/1\$		
EIS	FJAMSS		
L FJAMS	TMO	18/1T47\$	
	ETD	(P)\$	
	TDM	AJSATS\$	XXX00000
	TXDLC	0,6X	REMAI
	TDM	AJSV56	POINT
	JMP	AJHTBF8	
AJGRPE	AIXOL	2,6X	
	TMA	AJCKEND	
	TXDLC	0,6X	IF AT
	JAED	AJSCHBF	OF EB
	TMA	0,6	ON TA
	JAZ	AJGRPE	
	TMO	12/1T34	
	ETD	0,6	
	SRD	5	
	TDA	S	
	AM	C/HLT,0;C/HLT,SATNOSS	
	TMO	24/1316/0;8/1\$	
	EIS	AMFJSS	
L AMFJS	TMO	18/1T47\$	
	ETA	(P)\$	
	ETD	AJSATS\$	
	JAED	(P)+1	
	JMP	AJGRPE	EBLOC
	TMO	1/1T47	SEARCH
	ETA	0,6X	
	JAEQ	(P)*1	
	JMP	(P)*3H	
	JMP	AJHTBF8	
	JMP	AJGRPX	
	JMP	AJHTBF8	
	JMP	AJGRPE	
AJGRPX	TMD	AJSV56	
	TXDLC	0,6X	
AJCLRLCAIXOL	AIXOL	2,6X	
	TMA	AJCKEND	
	TXDLC	0,6X	
	JAED	(P)*1	
	JMP	AJGRPD	
	STXOL	1,3X	

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JMP	AJGRPA	\$		
AJGFIN	TMD	47/1T47	\$	FINIS
	TDM	0,4X	\$	TRANS
	TDM	1,4X	\$	INFO
	THD	C/HLT,AJBFFR+128;C/HLT,AJGFINS		
	AIXJ	2,4X	\$	AND
	SIXOL	128,4X	\$	CLEAR
	JMP	AJWBUF	\$	NONE-I
	CM	CONTG	\$	SWITC
	TMA	N/8T23;H/8AT47	\$	
	JMP	REWIND	\$	
	TIJ	AJLEAPD	\$	
	TJM	AJINSMR	\$	
	JMP	AJCNGT M -3H	\$	
AJSCHBFTMA		N/7T23;N/1T39;H/91T47	\$	TAPE
	JMP	AJTP7	\$	SEARC
	AIXOL	1,7X	\$	FOR
	TMA	N/1T15;N/7T23;H/D1T47	\$	DATA
	JMP	AJTP7	\$	OF
	TMD	C/HLT,AJBFFX	\$	REMAI
AJSCHBGTDXL	C	0,6X	\$	POINT
	TMO	12/1T34	\$	
	ETD	0,6	\$	
	SRD	5	\$	
	TDA	\$		
	AM	C/HLT,0;C/HLT,SATNOSS		
	TMO	24/1;16/0;8/1\$		
	EIS	FJAMS1\$		
L	FJAMS1	TMO	18/1T47\$	
		(P)\$		
	ETA	AJSATS\$		
	ETD	AJSCBH	\$	AND
	JAED	AJSCBH	\$	REV
AJSCHBTDMD		C/HLT,AJBFFX+128;C/HLT,AJSCHBG+1H\$		
	AIXJ	2,6X	\$	
	SIXOL	128,6X	\$	
	TMA	N/7T23;N/1T39;H/19T47	\$	
	JMP	AJTP7	\$	
	JMP	AJSCBF	\$	
AJSCHBHTMO		1/1T47	\$	
	ETA	0,6X	\$	
	JAEQ	(P)+1	\$	
	JMP	AJSCBH	\$	
	JMP	AJWTFB8	\$	
	TMA	N/7T23;N/1T39;H/19T47	\$	
	JMP	AJTP7	\$	
AJSCHBHTMD		C/HLT,0;C/HLT,AJSCHBJ	\$	RESTO
	SIXJ	0,7X	\$	7 TO
	JMP	AJGRPX	\$	POSIT
AJSCHBJTMA		N/1T15;N/7T23;H/D1T47	\$	PRIOR
	JMP	AJTP7	\$	TO
	SIXOL	1,7X	\$	SEARC
	JMP	AJSCBH	\$	
AJSCHBKJMP		AJWTFB8	\$	

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JMP	AJSCHBD	\$		
AJTP7	TJM	AJTP7XX	\$	TAPE
	JMP	SYS	\$	READ
	TIO	AJBFFX	\$	OR
	JMP	SYSNO	\$	WRITE
	TMD	C/HLT,0;C/HLT,SYSTAB+7	\$	OR
	JMP	SYSIO	\$	SPACE
	AJTP7XXJMP	(P)		
	AJWTFB8TJM	AJBF8XX	\$	TRANS
	TMD	0,6X	\$	BUFFE
	TDM	0,4X	\$	OF
	TMD	1,6X	\$	INFO
	TDM	1,4X	\$	FROM
	CM	0,6X	\$	EBLOC
	TMD	C/HLT,AJBFFR+128;C/HLT,AJB8XX	\$	TO
	AIXJ	2,4X	\$	TAPE
	JMP	AJWBUF	\$	
	SIXOL	128,4X	\$	ROUTI
	AJBF8XXJMP	(P)		
	AJWTFBUTJM	AJWBXX	\$	TO
	TMA	N/8T23;N/1T39;H/19T47	\$	COPY
	JMP	SYS	\$	ONTO
	TIO	AJBFFR	\$	TAPE
	JMP	SYSNO	\$	
	TMD	C/HLT,0;C/HLT,SYSTAB+8	\$	
	JMP	SYSIO	\$	
	AJWBXX	JMP		
	AJSATSTTMD	AJCMNBK	\$	NO
	TDXL	0,4X	\$	SATEL
	TMD	4LMAX	\$	
	TDXL	0,5X	\$	
	TMA	N/7T23;N/1T39;H/19T47	\$	THERE
	JMP	SYS	\$	RATHE
	TIO	0,5X	\$	THAN
	JMP	SYSNO	\$	OUTPU
	TMD	C/HLT,0;C/HLT,SYSTAB+7	\$	STORE
	JMP	SYSIO	\$	INFO
	AIXOL	128,5X	\$	ON
	TMD	C/HLT,0;C/HLT,AJSATST+2	\$	SCRAT
	SIXJ	1,4X	\$	TAPE.
	JMP	AJCTAGN	\$	
	JSGP	C/HLT,0;C/TIJL,JSGP1		
	JSGP1	C/HLT,5+128+5;C/CAM,JSGP2		
E	AFEND			
	JSGP2	A/GP=310/32323235		
	AJCHW	C/HLT,0;C/TIJL,AJFWH	\$	LINE 8
	AJUNC	C/HLT,0;C/TIJL,AJFCL	\$	LINE 9 UNCLAS
	AJCONF	C/HLT,0;C/TIJL,AJFCF	\$	CONF.
	AJSEC	C/HLT,0;C/TIJL,AJFSC	\$	SECRET
	AJSNF	C/HLT,0;C/TIJL,AJFNF	\$	NO FOR
	AJCHWI	C/HLT,0;C/TIJL,AJFWI	\$	LINE 10
	AJCHWJ	C/HLT,0;C/TIJL,AJFWJ	\$	LINE 11
	AJCHWL	C/HLT,0;C/TIJL,AJFWLC	\$	
	AJCHWN	C/HLT,0;C/TIJL,AJFWNN	\$	
	AJPAGE	C/HLT,0;C/TIJL,AJPGF	\$	

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AJCWMR C/HLT,	01C/TIYL, AJFWMR \$
AJCWL C/HLT,	01C/TIYL, AJFWL \$
AJINERCC/HLT,	01C/TIYL, AJINERF \$
AJFWH4 C/HLT,	3*128+ 31C/CAM, AJLN8 \$
AJFC1 C/HLT,	17*128+171C/TMA, AJUN \$
AJFC1'1 C/TCM,	21*128+ 01C/TMA, DFN \$
AJFC1'2 C/HLT,	29*128+ 71C/TMA, TFN \$
AJFC1'3 C/HLT,	30*128+ 11C/CAM, AJCRLF \$
AJFC2 C/HLT,	34*128+341C/TMA, AJCON \$
AJFCF1 C/TCM,	38*128+ 01C/TMA, DFN \$
AJFCF2 C/HLT,	46*128+ 71C/TMA, TFN \$
AJFCF3 C/HLT,	47*128+ 11C/CAM, AJCRLF \$
AJFSC C/HLT,	22*128+221C/TMA, AJSC \$
AJFSC1 C/TCM,	26*128+ 01C/TMA, DFN \$
AJFSC2 C/HLT,	34*128+ 71C/TMA, TFN \$
AJFSC3 C/HLT,	35*128+ 11C/CAM, AJCRLF \$
AJFNF C/HLT,	34*128+341C/TMA, AJNF \$
AJFNF1 C/TCM,	38*128+ 01C/TMA, DFN \$
AJFNF2 C/HLT,	46*128+ 71C/TMA, TFN \$
AJFNF3 C/HLT,	47*128+ 11C/CAM, AJCRLF \$
AJFWI C/HLT,	24*128+241C/TMA, AJLN10 \$
AJFWT1 C/HLT,	41*128+161C/TMA, STNM \$
AJFWT2 C/HLT,	42*128+ 11C/CAM, AJCRLF \$
AJFWJ C/HLT,	7*128+ 31C/TMA, AJLN13 \$
AJFWJ1 C/TCM,	11*128+ 01C/TMA, AJDDO \$
AJFWJ2 C/HLT,	23*128+ 81C/TMA, AJDATE \$
AJFWJ3 C/HLT,	24*128+ 11C/CAM, AJCRLF \$
AJFWNN C/HLT,	17*128+171C/CAM, AJNNNN \$
AJPGF C/HLT,	60*128+ 41C/TMA, AJPG \$
AJPGF1 C/TCM,	64*128+ 01C/CAM, AJPAGES \$
AJFWLC C/HLT,	120*128+1201C/CAM, AJLTRCH \$
AJFWLR C/HLT,	14*128+131C/CAM, AJMRDTA \$
AJFWL C/HLT,	5*128+51C/TMA, AJSAT1 \$
AJFWL'1 C/TCM,	11*128+321C/TMA, AJREV \$
AJFWL'2 C/TCM,	15*128+371C/TMA, AJHR \$
AJFWL'3 C/TCM,	17*128+311C/TMA, AJMIN \$
AJFWL'4 C/HLT,	18*128+ 11C/TMA, AJDOT \$
AJFWL'5 C/TCM,	20*128+241C/TMA, AJFRMIN \$
AJFWL'6 C/ICOZ,	27*128+ 11C/TMA, AJELEV \$
AJFWL'7 C/ICOZ,	34*128+111C/TMA, AJAZ \$
AJFWL'8 C/TCM,	41*128+181C/TMA, AJRANGE \$
AJFWL'9 C/ICOZ,	48*128+11C/TMA, AJRRATE \$
HLT	54*128+2 \$
TMA	FANNO \$
ICOZ	61*128+3 \$
TMA	RSU \$
ICOZ	69*128+3 \$
TMA	RSV \$
ICOZ	77*128+3 \$
CAM	RSW \$
AJINERFC/HLT,	81*128+801C/CAM, 0,6X \$
AJNNNN A/NNNN10/77777777\$	
8/111111\$	
AJCRFLF 0/32\$	
AJLN8 A/BT10/32\$	

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AJLN10 A/ LOOK ANGLE SCHEDULE FORS

AJLN12 A/ SAT REV TIME ELEV AZMTH RANGE R-RATS

SET (P)+4 \$

AJLN13 A/DAYS

AJLN17 A/1AERO10/32\$

AJUN A/UNCLAS SPACETRACKS

AJCON A/C O N F I D E N T I A L SPACETRACKS

AJSC A/S E C R E T SPACETRACKS

AJNF A/S E C R E T N O F O R N SPACETRACKS

AJDOT 0/33\$

AJPG A/PAGES

AJMRDTAA/ MORE \$

 A/DATA10/32\$

AJUNITS SET (P)+6

L AJACN C/TMA, AJUNC1C/NOP,0 \$
 C/TMA, AJCONF1C/NOP,0 \$
 C/TMA, AJSEC1C/NOP,0 \$
 C/TMA, AJSNFC1C/NOP,0 \$
 C/TMA, (P)+11C/NOPS \$

C/HLT1C/TIYL, (P)+1\$

AJACN1 C/HLT, 54*128+541C/TMA, AJACN2\$

C/TCM, 58*128+01C/TMA, DFNS

C/HLT, 66*128+71C/TMA, TFN\$

C/HLT, 67*128+11C/CAM, AJCRLFS

AJACN2 A/S E C R E T RELEASABLE OUTSIDE SSO CHANN\$

A/ELS SPACETRACKS

AJLTRCH48/1

48/1

48/1

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42/1 10/32 \$
AJUN1 A/UNCLAS NOCC=SD \$

AJCON1 A/C O N F I D E N T I A L NOCC=SD \$

AJSC1 A/S E C R E T NOCC=SD \$

AJNF1 A/S E C R E T N O F O R N NOCC=SD \$

AJACN3 A/S E C R E T RELEASABLE OUTSIDE SSO CHANNS

A/ELS NOCC=SD \$

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* SPECIALIZED SORT ROUTINE
NAME SORT \$
SORT TJM SORTX \$
CD \$
TXDLC ,3 \$
TXDRC ,5 \$
TDM RSSV35 \$
TAD \$
TDXLC ,2 \$
SLA 24 \$
TMQ 1/1/15/0/32/1T47 \$
EIS SORT3 \$
SM N/2T15 \$
EIS SORT4 \$
SORT0 TXDLC ,2 \$
TDXLC ,5 \$
TMA 48/1T47 \$
TMQ 22/1T22/1/1T47 \$
SORT1 ETD 0,5 \$
JAGD (P)+2H \$
JMP SORT2 \$
JAED SORT2 \$
TDA \$
TXDLC ,5 \$
TDXLC ,3 \$
SORT2 TMD SORT3 \$
AIXJ 2,5 \$
TMA ,2 \$
TMD ,3 \$
TOM ,2 \$
TAM ,3 \$
TMA 1,2 \$
TMD 1,3 \$
TDM 1,2 \$
TAM 1,3 \$
TMD SORT4 \$
AIXJ 2,2 \$
TMD RSSV35 \$
TOXLC ,3 \$
TOXRC ,5 \$
SORTX JMP (P) \$
SORT3 C/HLT,03C/HLT,SORT1 \$
SORT4 C/HLT,03C/HLT,SORT0 \$
RSSV 35 END \$

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