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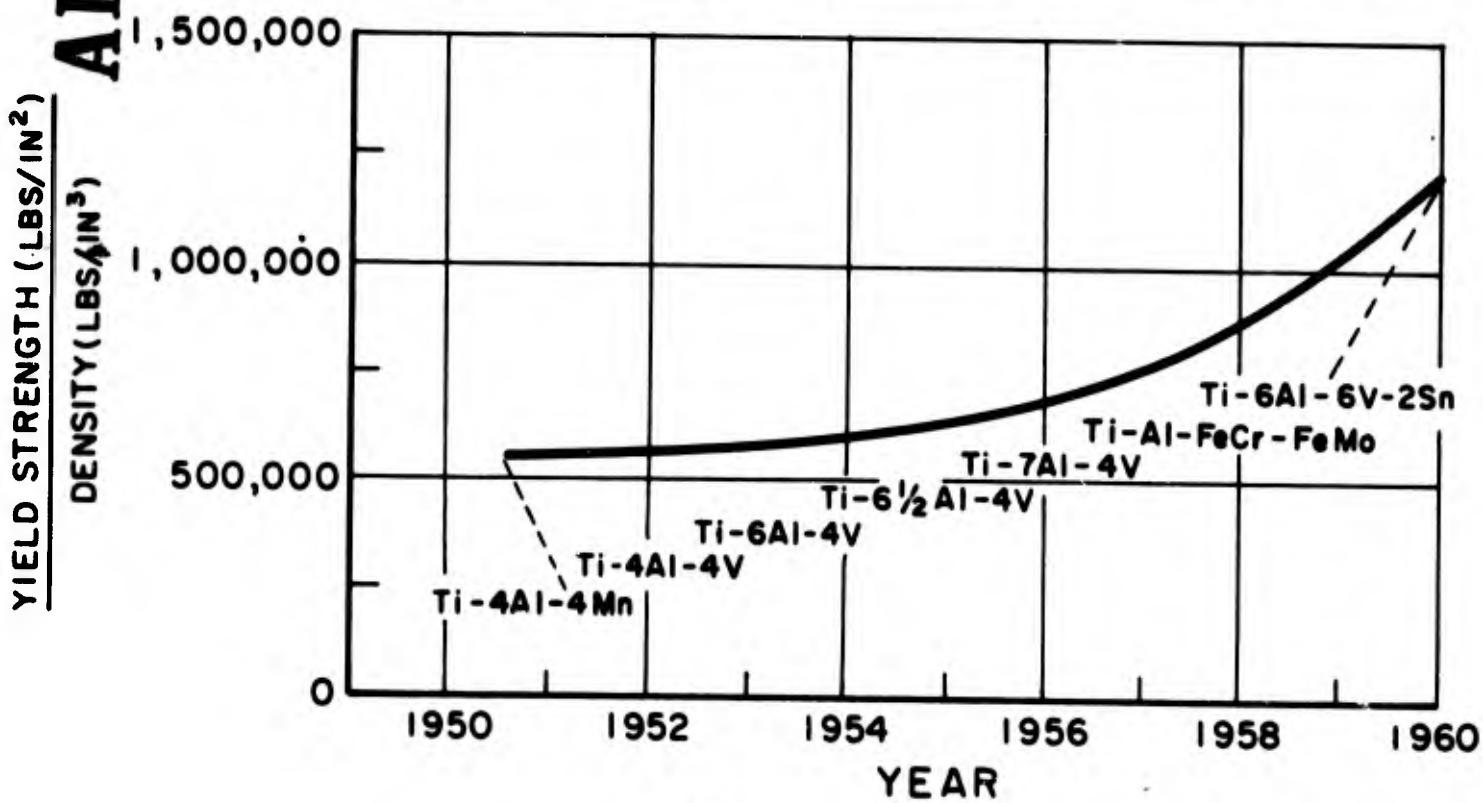
# WATERTOWN ARSENAL LABORATORIES

## Monograph Series

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THE Ti-6Al-6V-2Sn-0.5Fe-0.25Cu  
ALPHA-BETA TYPE ALLOYS UTILIZED AT WATERTOWN ARSENAL



By

R. M. COLTON

F. J. RIZZITANO

12-13 SEPTEMBER 1960

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**THE Ti-6Al-6V-2Sn-0.5Fe-0.25Cu ALLOY AND OTHER  
ALPHA-BETA TYPE ALLOYS UTILIZED AT WATERTOWN ARSENAL**

By

**R. M. COLTON  
F. J. RIZZITANO**



**Abstract of  
Technical Presentation to be given at  
New York University  
Sixth Titanium Metallurgy Conference  
Lecture No. 11**

**12-13 SEPTEMBER 1960**

THE Ti-6Al-6V-2Sn-0.5Fe-0.25Cu ALLOY AND OTHER  
ALPHA-BETA TYPE ALLOYS UTILIZED AT WATERTOWN ARSENAL

ABSTRACT

I Introduction

During the past four or five years Watertown Arsenal has been actively engaged in the development, evaluation and exploitation of medium and high strength alpha-beta type titanium alloys. A large portion of the development work has been carried out at New York University under the auspices of Watertown Arsenal. At the present time several experimental alloys have exhibited yield strengths in excess of 200,000 psi while maintaining good ductility and toughness. Figure 1 lists a number of the most promising alloys evaluated and their corresponding mechanical property values.

The development and evaluation of the alloys were predicated on existing and contemplated Ordnance Corps material requirements for weapons systems.

Several of the alpha-beta alloys studied, including the Ti-6Al-6V-2Sn-0.5Fe-0.25Cu alloy developed at New York University, the Ti-Al-FeCr-FeMo developed at Titanium Metals Corporation of America, and the Ti-6Al-4V alloy initially studied at Watertown Arsenal are currently being utilized in such weapons systems.

II Mechanical Properties

Figure 2 shows the versatility of the Ti-6Al-6V-2Sn-0.5Fe-0.25Cu alloy. It is useful as a medium (130,000-169,999 psi yield strength) as well as a high (170,000-189,999 psi yield strength) strength material requiring toughness and ductility.

III Ordnance Corps Utilization of Alpha-Beta Type Titanium Alloys - Experimental Applications

1. Current Applications

a. Gun Components - Ti-6Al-6V-2Sn-0.5Fe-0.25Cu at 170,000 psi yield strength.

Figure 3 - Barrel Extrusion and Machined Barrel

Figure 4 - Chamber Expanded Extrusion and Nozzle Forging

Figure 5 - Table II Typical Metallurgical Properties of Above Forgings and Extrusions Processed for Alpha-Beta Type Titanium Alloys

b. Ammunition Components - Ti-6Al-6V-2Sn-0.5Fe-0.25Cu at 170,000 psi yield strength and Ti-6Al-4V at 140,000 psi yield strength.

Figure 6 - Reverse Extrusions

Figure 7 - Reverse Extrusions

Figure 8 - Closed Die Forgings

Figure 9 - Reverse Extrusions

Figure 10 - Closed Die Forgings

Figure 5 - Table II Typical Metallurgical Properties of Above  
Forgings and Extrusions Processed for Alpha-Beta  
Type Titanium Alloys

c. Vehicular Systems - Ti-7Al-4V at 150,000 psi yield strength and  
Ti-6Al-4V at 130,000 psi yield strength.

Figure 11 - Tank Track Components

d. Rapid Fire Weapons

Figure 12 - Gatling Gun Indexing and Holding Bracket

Figure 5 - Table II Typical Metallurgical Properties of Above  
Forgings and Extrusions Processed for Alpha-Beta  
Type Titanium Alloys

## 2. Future Applications

a. Rocket Motor Casings and Missiles

b. Armor

## IV Processing and Fabrication of Components

### 1. Forging

a. Closed Die

b. Open Die

c. Ring Rolling

### 2. Extrusion

a. Forward

b. Reverse

### 3. Cold Forming

a. Shear Spinning

b. High Energy Rate Forming

c. Tube Reducing

### 4. Joining

a. Fusion Welding

b. Pressure Welding

Figure 13 - Pressure Welding Equipment

Figure 14 - Pressure Welding in Operation

Figure 15 - Pressure Welded Ammunition Component

Figure 16 - Mechanical Properties of Pressure Welded Ammunition Component - Weld and Base Material

Figure 17 - Macrostructure of Pressure Welded Joint

Figure 18 - Microstructure of Pressure Welded Joint

V Design and Testing Considerations for High-Strength Titanium Applications

1. Notch Sensitivity

Figure 19 - Effect of Notch Radius on Impact Values for V-Notch Charpy Impact Specimens Tested at -40°F

2. Testing of Thin Sections

Figure 20 - Effect of V-Notch Charpy Specimen Size on Impact Level Tested at -40°F

3. Ring and Cylinder Tests

Figure 21 - Compression Test on Thin-Walled Pressure Welded Cylinder - 93% Weld Efficiency

Figure 22 - Compression Test on Thin-Walled Pressure Welded Cylinder - 100% Weld Efficiency

VI Future Plans at Watertown Arsenal

1. Fabrication of Pressure Welded Rocket Motor Casings

2. Continued Evaluation of High Strength Alpha-Beta Type Titanium Alloys  
(Extensive data on most phases discussed in this presentation are available upon request at Watertown Arsenal.)

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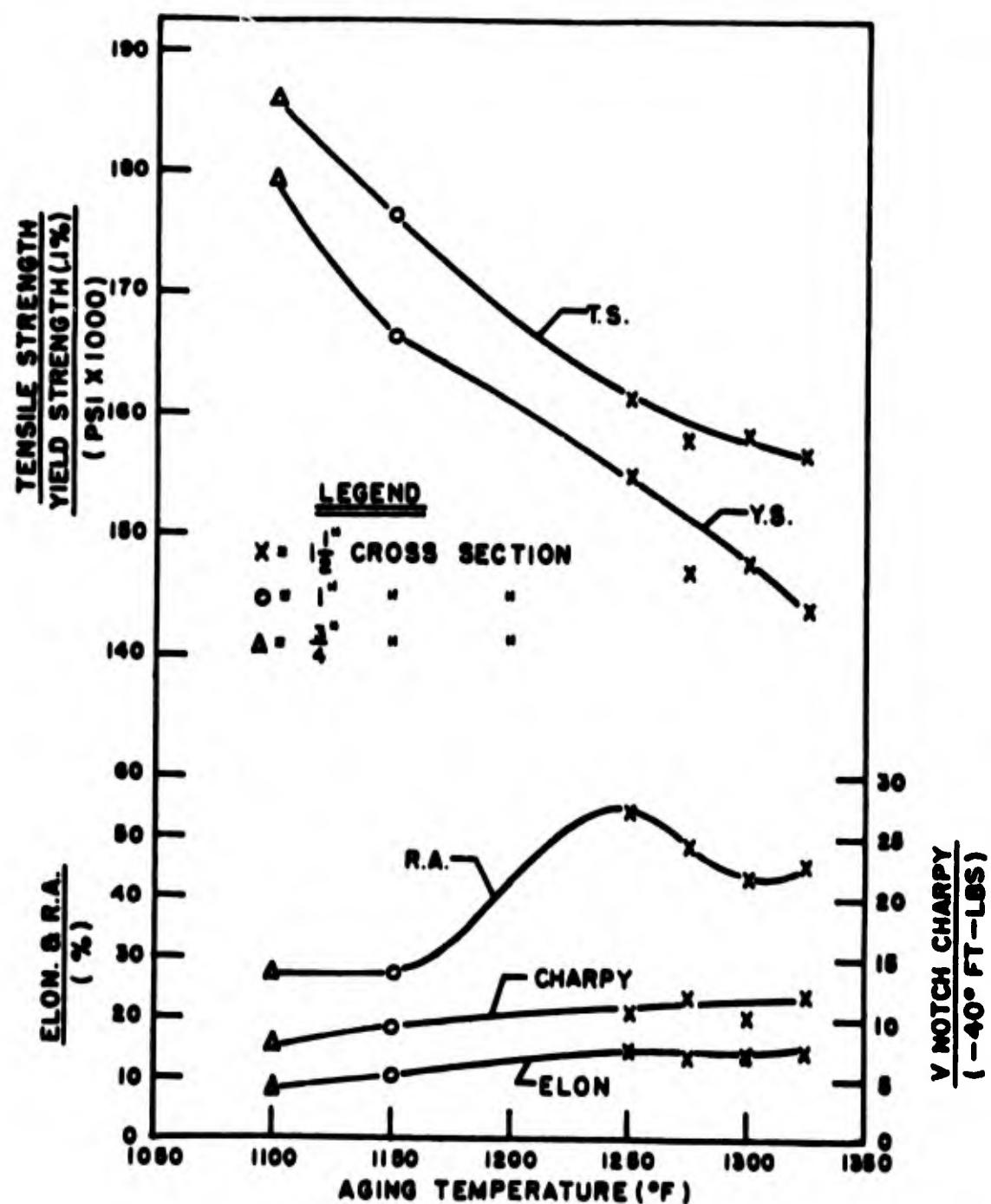
Figure 21 - Compression Test on Thin-Walled Pressure Welded Cylinder - 93%  
Weld Efficiency

Figure 22 - Compression Test on Thin-Walled Pressure Welded Cylinder - 100%  
Weld Efficiency

**PROMISING HIGH STRENGTH ALPHA-BETA TYPE  
TITANIUM ALLOYS**

ALLOY COMPOSITION	YIELD STRENGTH (.1% OFFSET) (PSI)	ELON. (%)	R. A. (%)	V-NOTCH IMPACT AT -40°F (FT-LBS)
Ti-Al-V-Sn-Zr-Cu-Mn	208,500	7.9	17.8	6.9
	197,500	9.7	25.3	7.7
	181,500	14.1	42.0	9.9
Ti-Al-V-Sn-Zr-Fe-Ni	204,000	7.1	21.6	8.4
	198,500	8.1	33.6	9.6
	178,000	10.8	35.2	10.7
Ti-Al-V-Sn-Zr-Cu-Fe	203,000	7.2	26.1	9.6
	188,000	11.8	37.1	9.9
	185,000	9.7	34.2	11.0
Ti-Al-V-Sn-Zr-Cu-Fe-Cr-Mo	203,000	6.8	23.0	8.6
	197,000	10.9	32.1	7.7
	182,500	12.8	46.1	12.3

**FIGURE 1**



AGING TEMPERATURE VERSUS MECHANICAL PROPERTIES OF  
Ti-6V-2Sn TITANIUM ALLOY AT VARIOUS CROSS SECTIONAL  
THICKNESSES ( DATA REPORTED BY FACILITY E )

FIGURE 2

FORWARD EXTRUSIONS

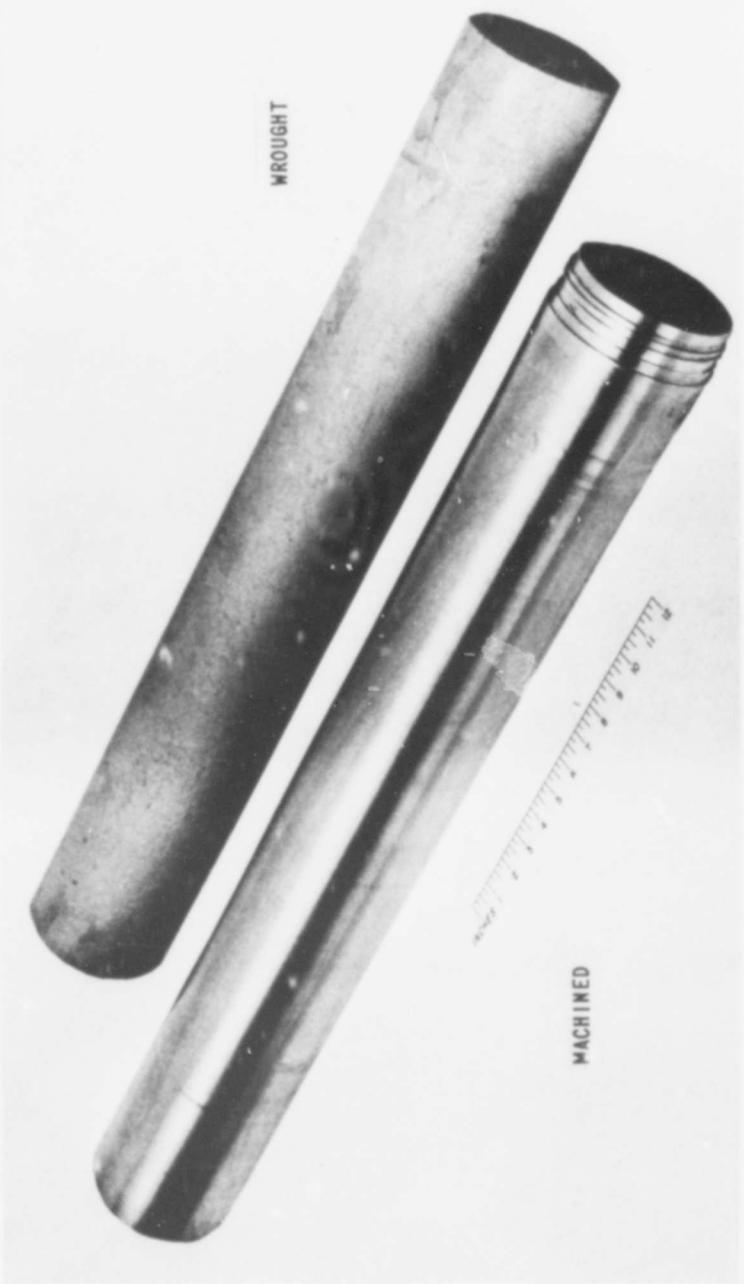


FIGURE 3



EXPANDED FORWARD  
EXTRUSION

FORGING

FIGURE 4

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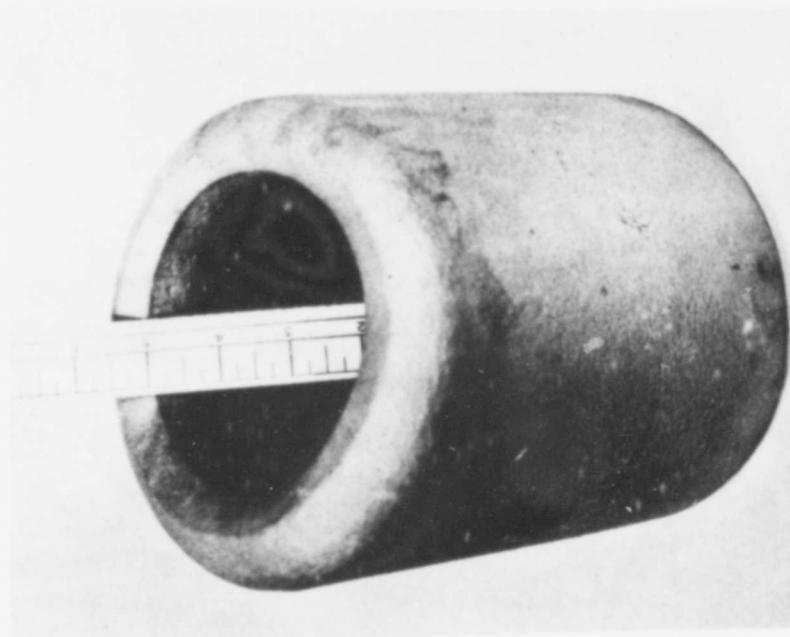








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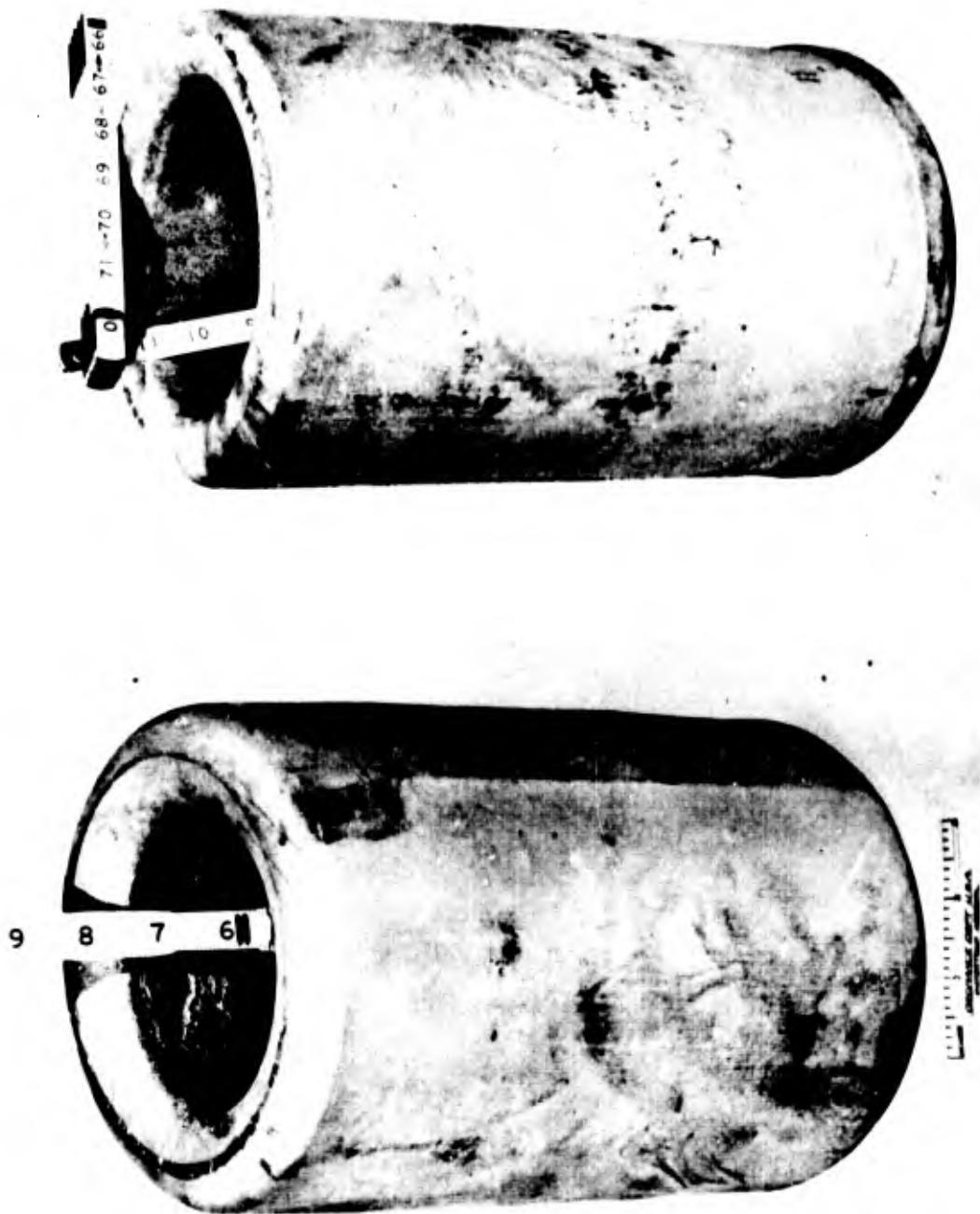


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REVERSE EXTRUSIONS

FIGURE 6

**REVERSE EXTRUSIONS**

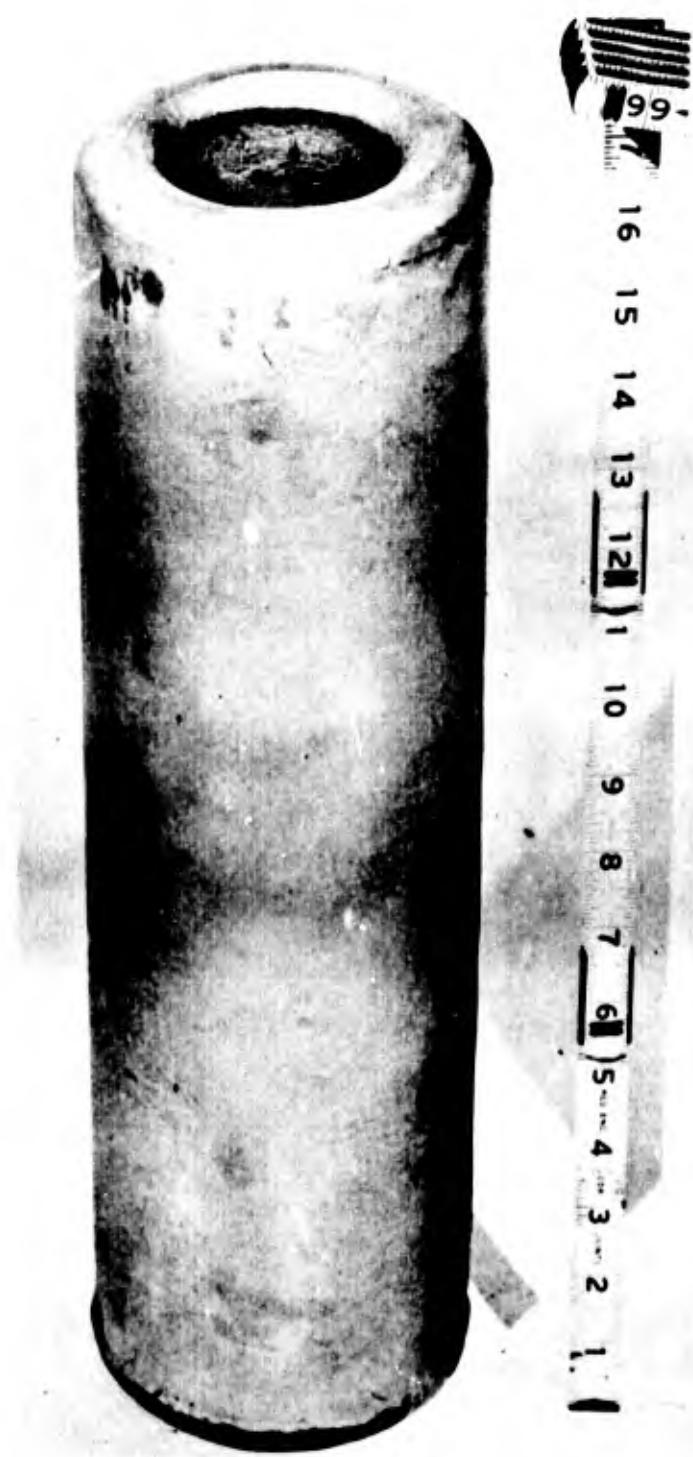


**FIGURE 7**

**CLOSED DIE FORGINGS**



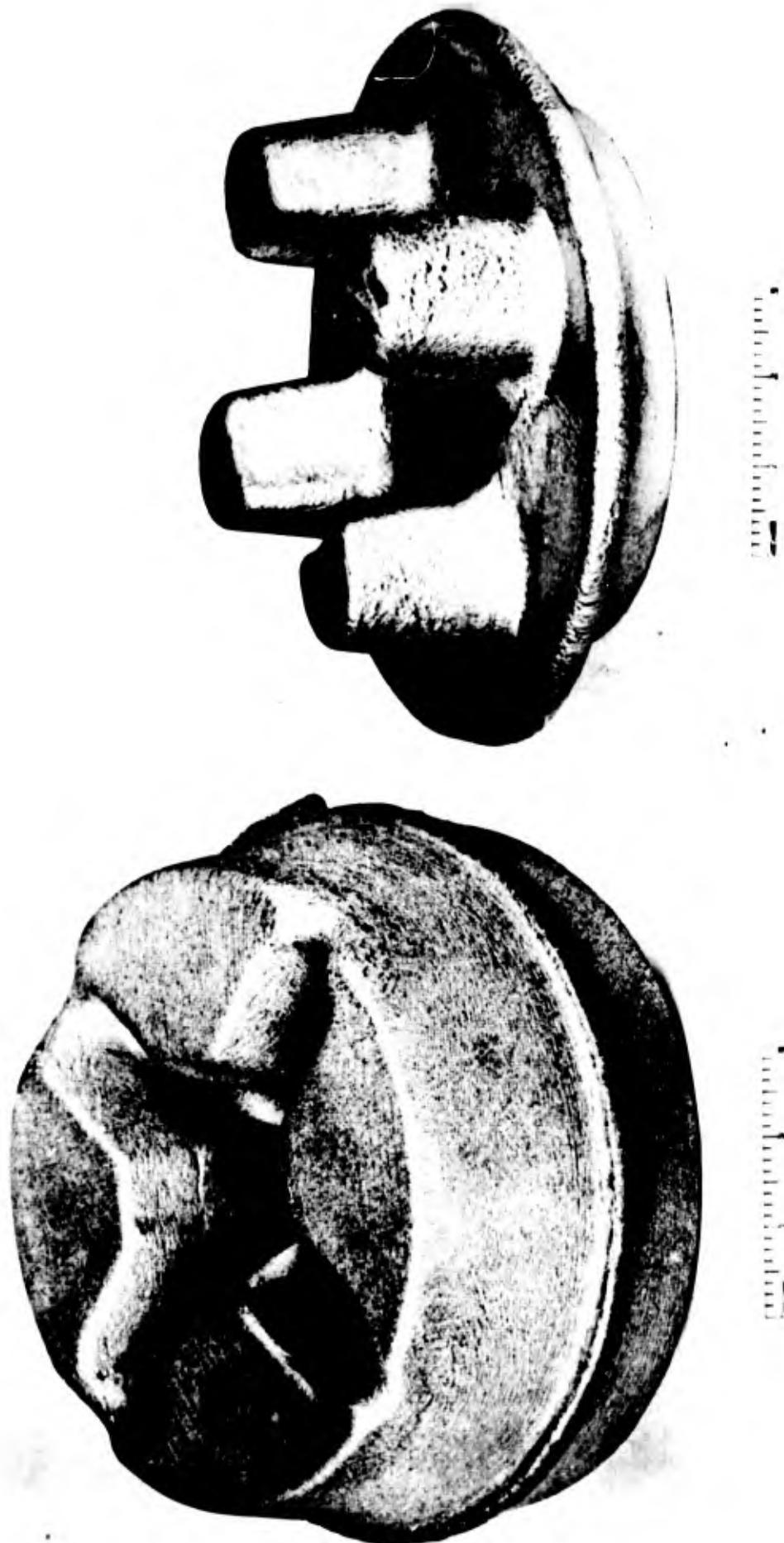
**FIGURE 8**



REVERSE EXTRUSION

FIGURE 9

**CLOSED DIE FORGINGS**



**FIGURE 10**

CAP, CENTER GUIDE



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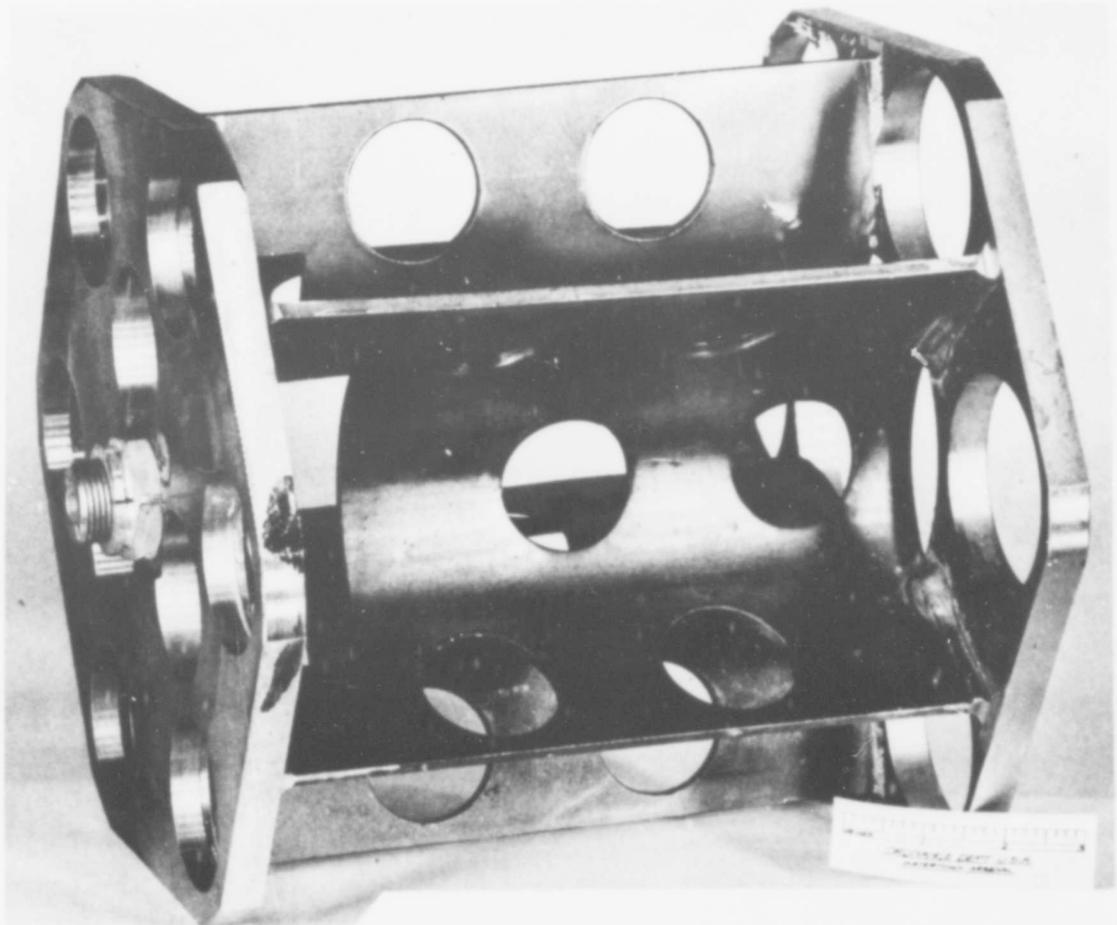


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FORGED TITANIUM TANK TRACK COMPONENTS

FIGURE II



GATLING GUN BARREL INDEXING AND HOLDING BRACKET  
Ti-6Al-4V & Ti-4Al-4V

FIGURE 12

PRESSURE WELDING EQUIPMENT

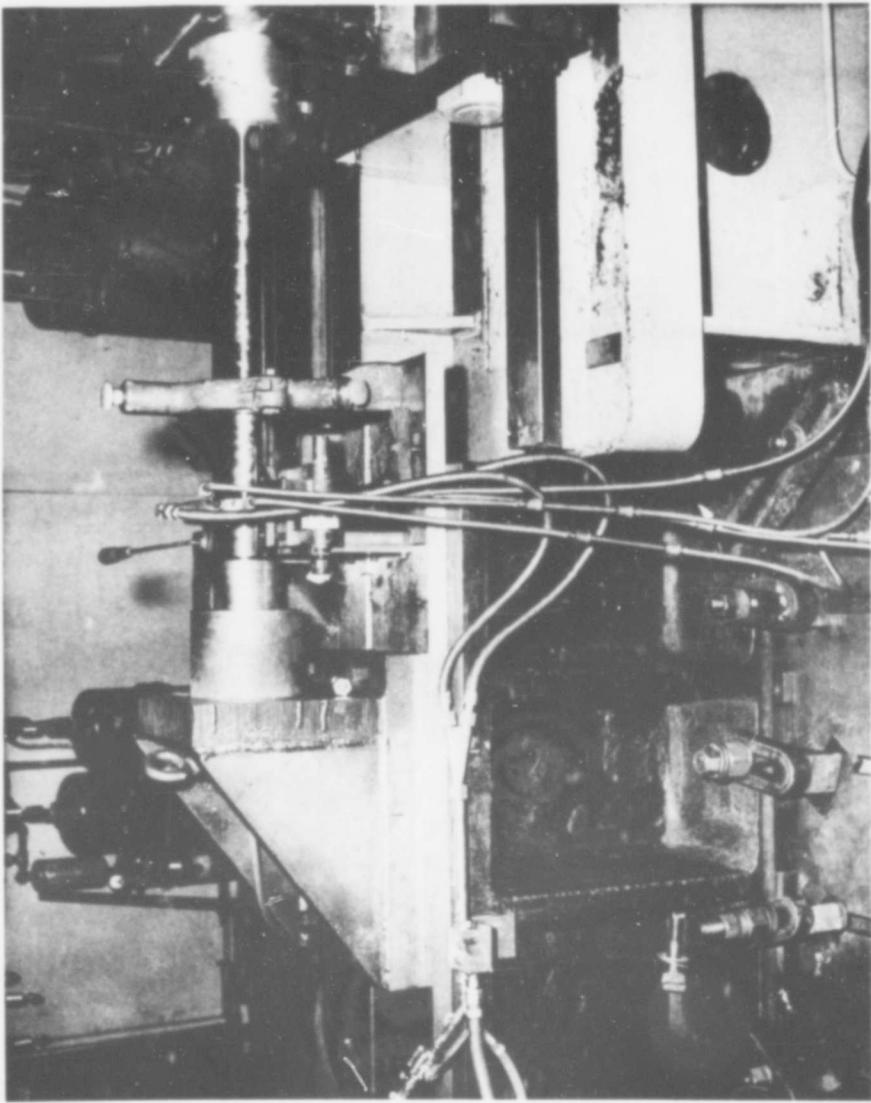


FIGURE 13

PRESSURE WELDING IN OPERATION

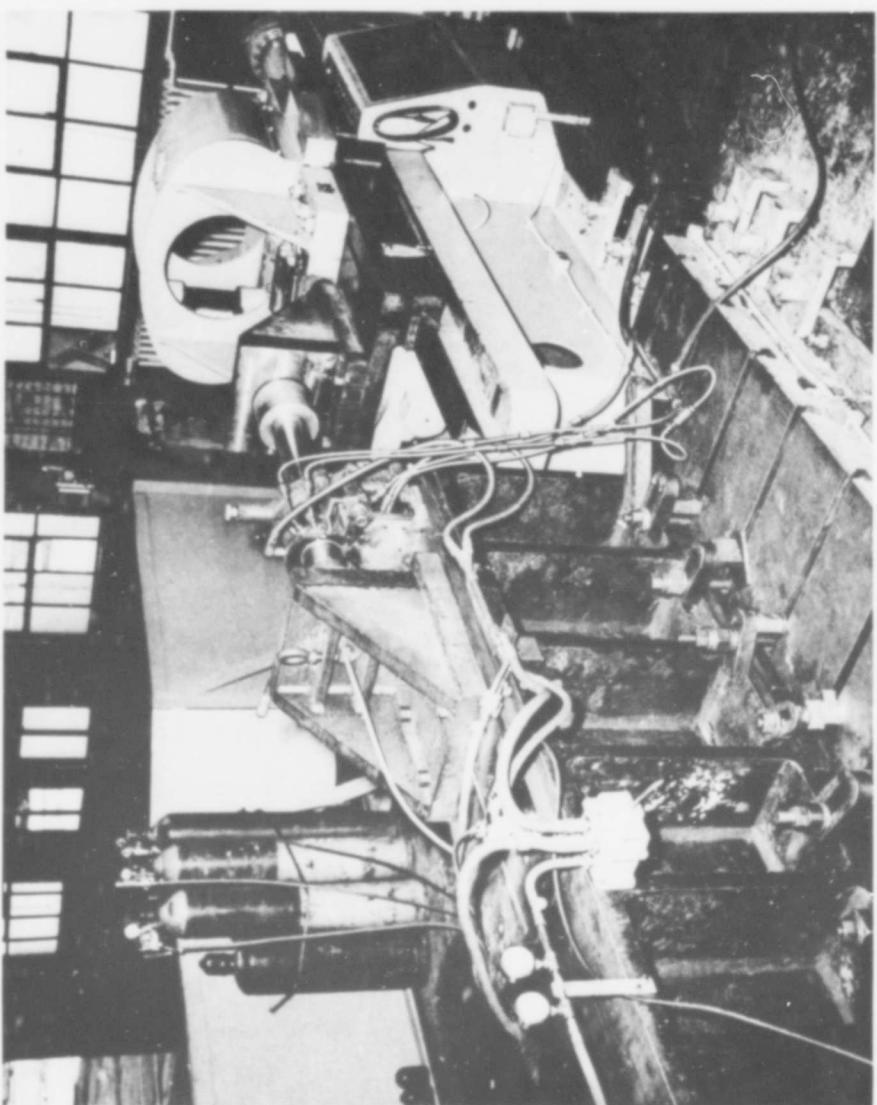


FIGURE 14

PRESSURE WELDED AMMUNITION COMPONENT

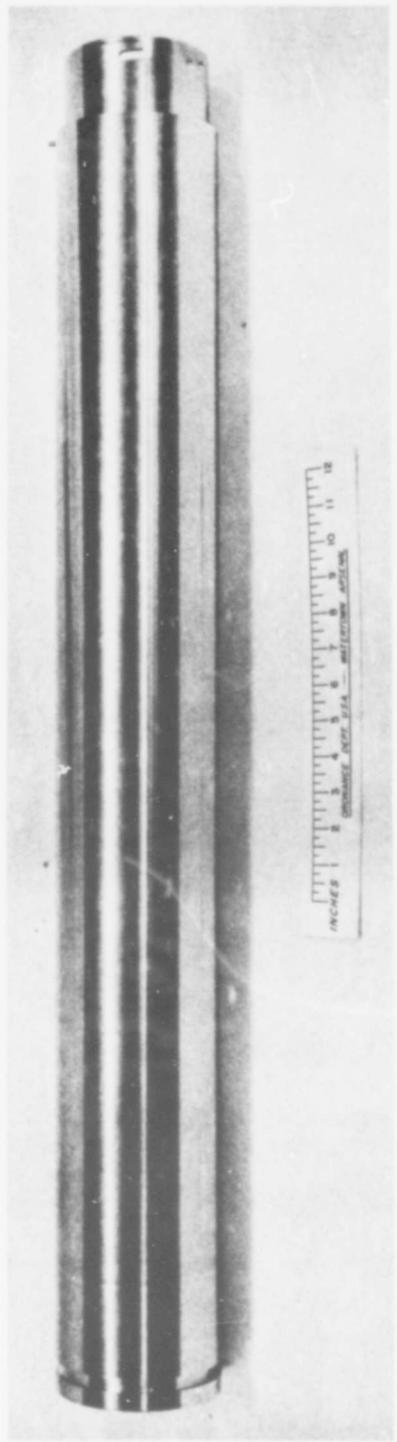


FIGURE 15

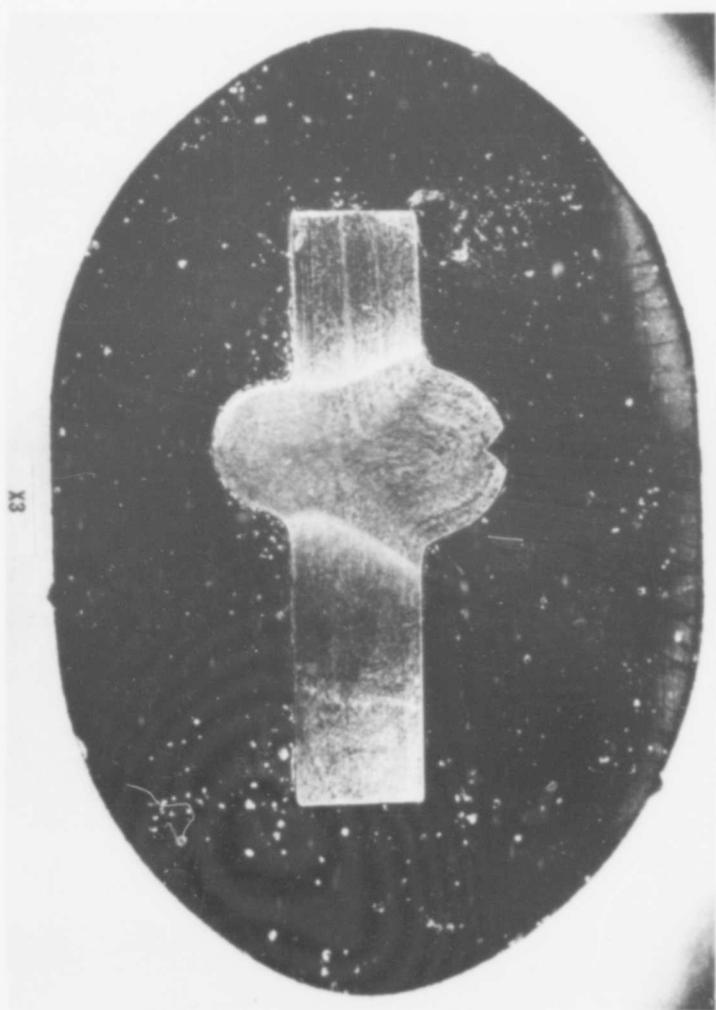
**MECHANICAL PROPERTIES OF PRESSURE WELDED  
AND INTEGRAL ADAPTER TYPE AMMUNITION-COMPONENT**

<u>Location</u>	<u>Yield Str.</u> <u>.1% Offset</u> <u>(Psi x 1000)</u>	<u>Elong.</u> <u>(%)</u>	<u>R.A.</u> <u>(%)</u>	<u>V-Notch Charpy</u> <u>Impact at -40°F</u> <u>(ft - lbs)</u>
Cylinder-Adapter	172,750	8.6	21.2	6.7
Cap End	174,000	7.2	27.2	6.1
*Welded Area (Min. Prop.)	145,000	9.0	20.0	9.0

\*Increased wall thickness at welded area to allow for slight degradation in mechanical properties resulting from welding operation.

Figure 16

FIGURE 17



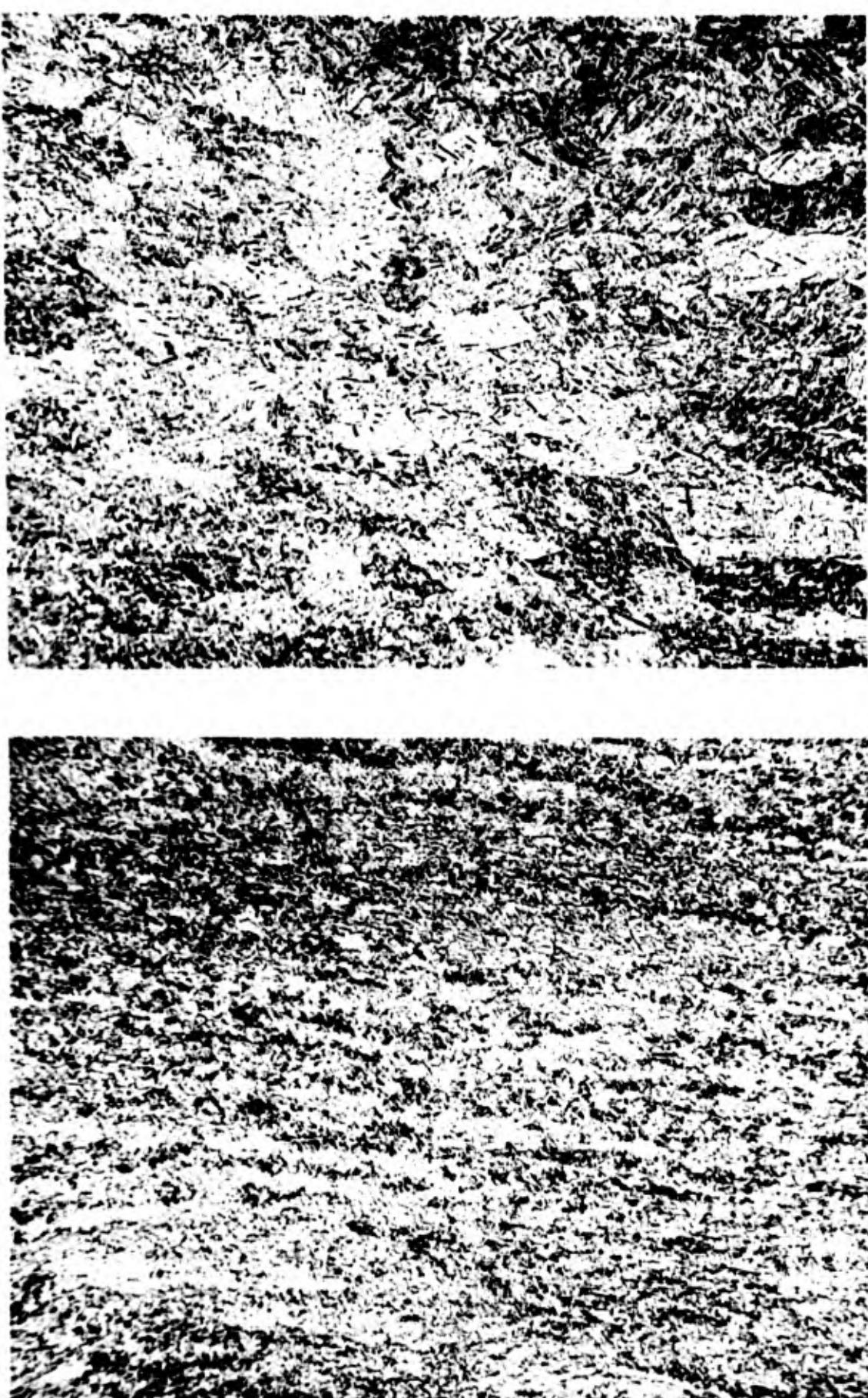
MACROSTRUCTURE OF PRESSURE WELDED JOINT

MICROSTRUCTURE OF PRESSURE WELDED JOINT AND BASE MATERIAL

X100  
BASE MATERIAL

X100  
JOINT MATERIAL

FIGURE 18



EFFECT OF NOTCH RADIUS ON "V" NOTCH CHARPY  
IMPACT RESISTANCE

(Ti-6Al-6V-2Sn ALLOY AT 70,000 PSI MINIMUM YIELD STRENGTH)

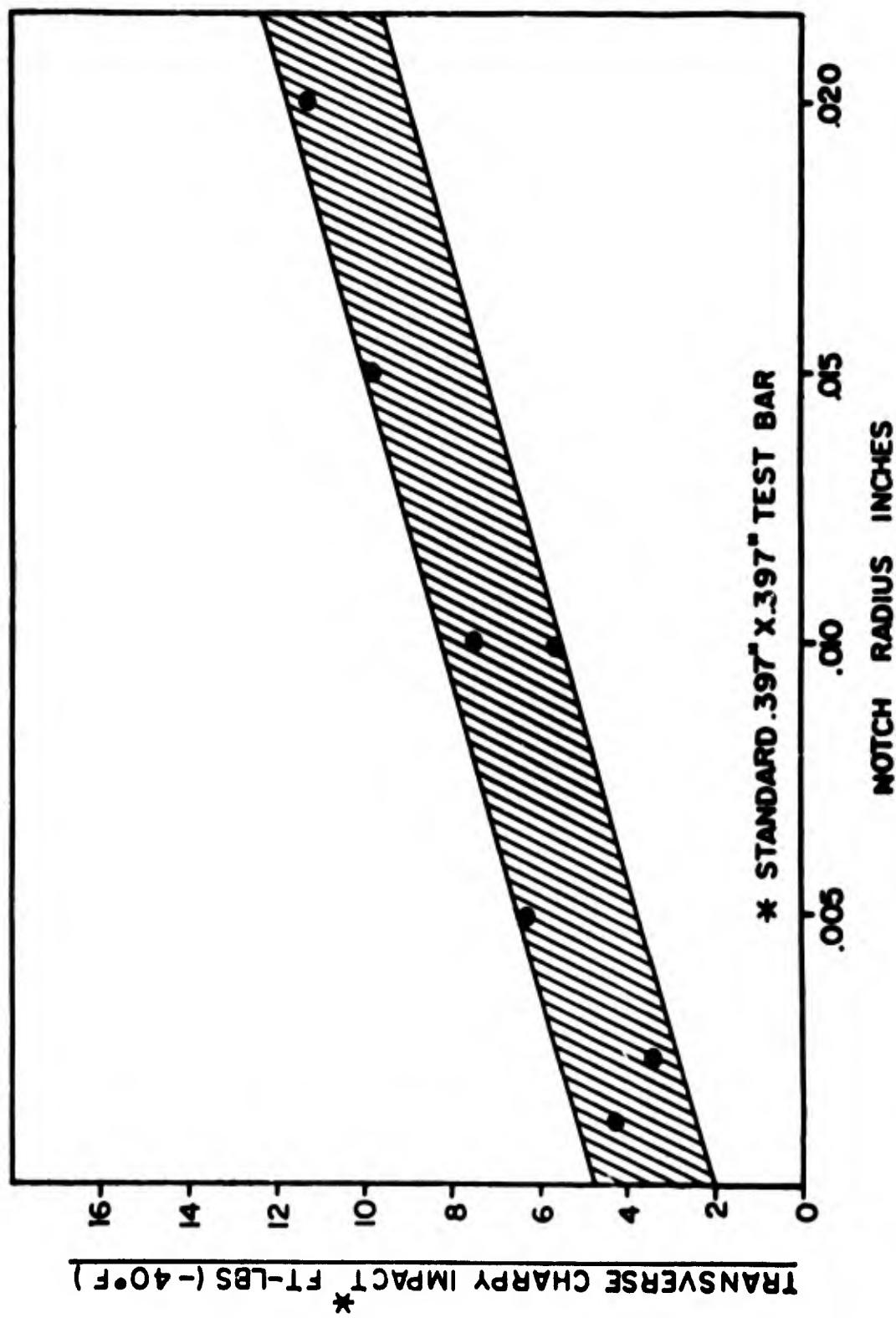
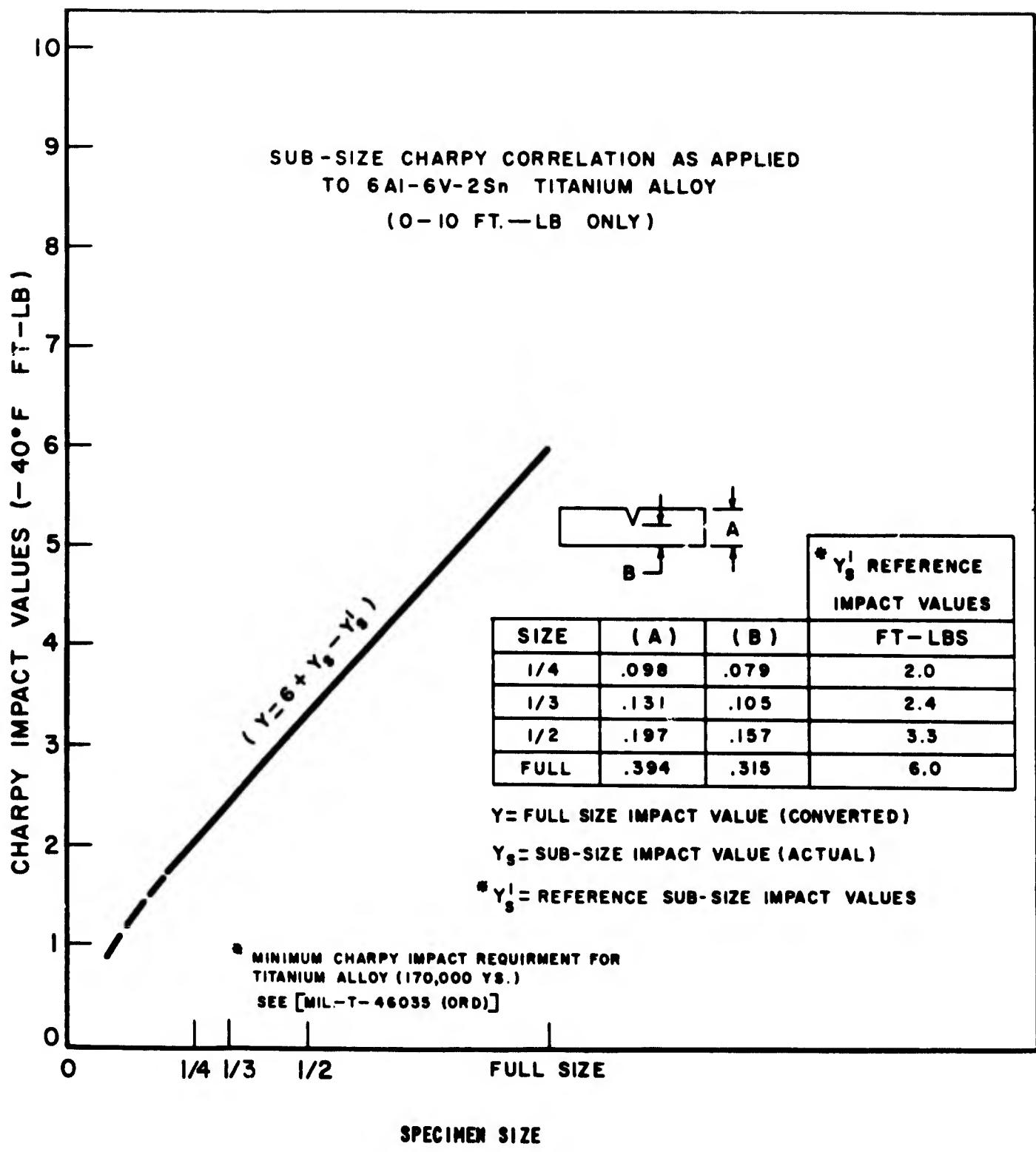


FIGURE 19



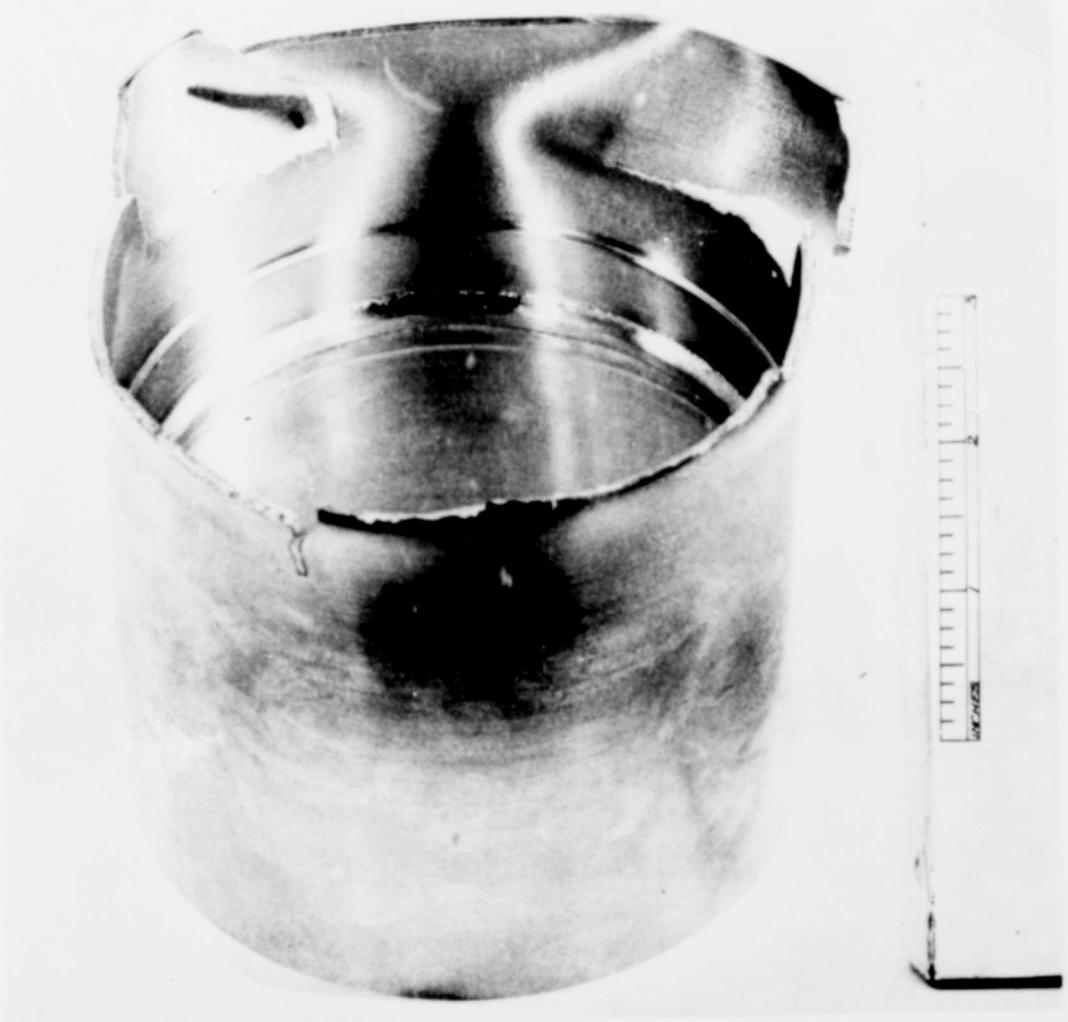
EFFECT OF V-NOTCH CHARPY SPECIMEN SIZE ON IMPACT LEVEL

FIGURE 20



COMPRESSION TEST ON THIN WALLED PRESSURE WELDED CYLINDER - 93% WELD EFFICIENCY LOAD - 197,000 LBS

FIGURE 21



COMPRESSION TEST ON THIN WALLED PRESSURE WELDED CYLINDER -  
100% WELD EFFICIENCY LOAD - 212,000 LBS

FIGURE 22