

UNCLASSIFIED

AD 4 6 3 8 9 6

DEFENSE DOCUMENTATION CENTER

FOR

SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION ALEXANDRIA, VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

1

AD NO. 463896
DDC FILE COPY

463896

6 DEFORMATION PROCESSING OF ANISOTROPIC METALS.

11 Jan 1965

12 [3] p.

AVAILABLE COPY WILL NOT PERMIT FULLY LEGIBLE REPRODUCTION. REPRODUCTION WILL BE MADE IF REQUESTED BY USERS OF DDC.

Prepared under Navy, Bureau of Naval Weapons

15 Contract N0w 65-0124-d

9 Progress Report No. 3,

DDC
JUN 2 1965
DDC-IRA E

1 Nov [redacted] -31 Dec [redacted] 1964,

10 by D. H. AVERY AND W. A. BACKOFEN.

21263

5 Metals Processing Lab., Cambridge, Mass. Inst. of Tech.,

J.

DEFORMATION PROCESSING OF ANISOTROPIC METALS

D. H. Avery and W. A. Backofen

During the past report period [↓] ~~elevated-temperature tensile tests have~~ ~~been~~ carried out on the alloy Zircaloy 4. As in the case of the Ti alloy 2.5 Sn-4 Al (~~Report No. 1~~), a very sharp maximum in strain rate sensitivity, ^{α/β - beta} ~~m~~, was found at or near the ~~α-β~~ transus, ~~Figure 1~~. Elongation values, ~~Figure 2~~, again correlated with strain rate sensitivity; however the maximum value of 220% was not as striking as in the titanium alloy.

Values of strain ratio, R , were high in Zircaloy 4 (approximately 4 at RT) and decreased with increasing testing temperature. For temperatures below 600°C, R was relatively constant with strain. In the range 600° to 800°C, R was found to increase remarkably after the onset of necking. In this temperature range necking occurred only in the width direction, leading to chisel-edged fractures showing 100% reduction in width and R values approaching infinity. ←

A sheet of HPS-20, cross-rolled sintered beryllium has been ordered. This material should be characterized by strong anisotropy with [0002] along the sheet normal and high R values. One of the principle problems in beryllium technology lies in the very limited bend ductility at ordinary temperatures. Since sheet bending is a plane-strain operation, high R values and plane strain strengths would naturally be expected to impair ductility. Temperature dependence of deformation in plane strain will be of immediate experimental concern.

-/-

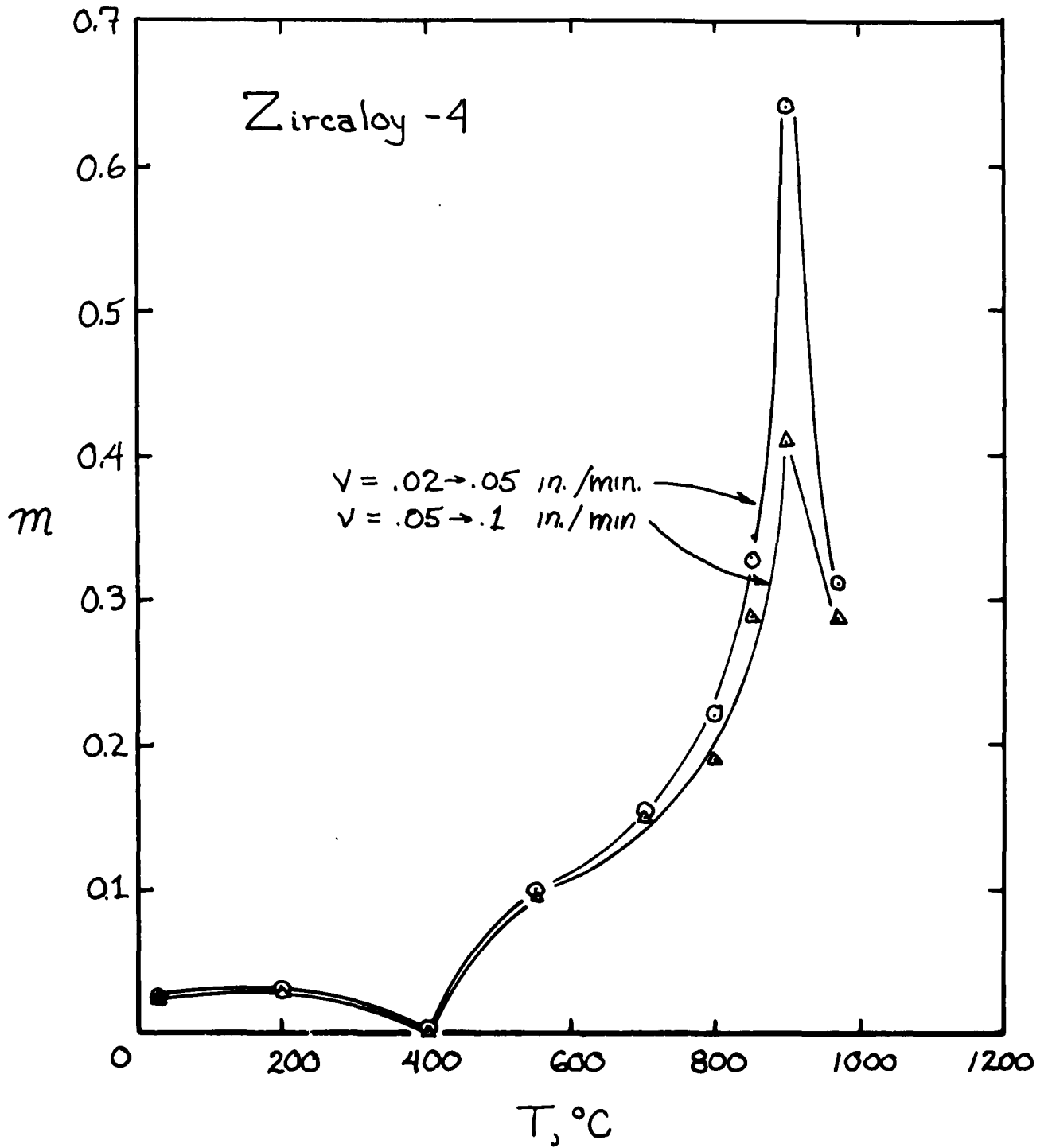


Figure 1. Strain Rate Sensitivity, m , Values versus Temperature for Zircaloy 4 at Two Pulling Velocities. m is the exponent in the empirical expression $\sigma = k\epsilon^m$.

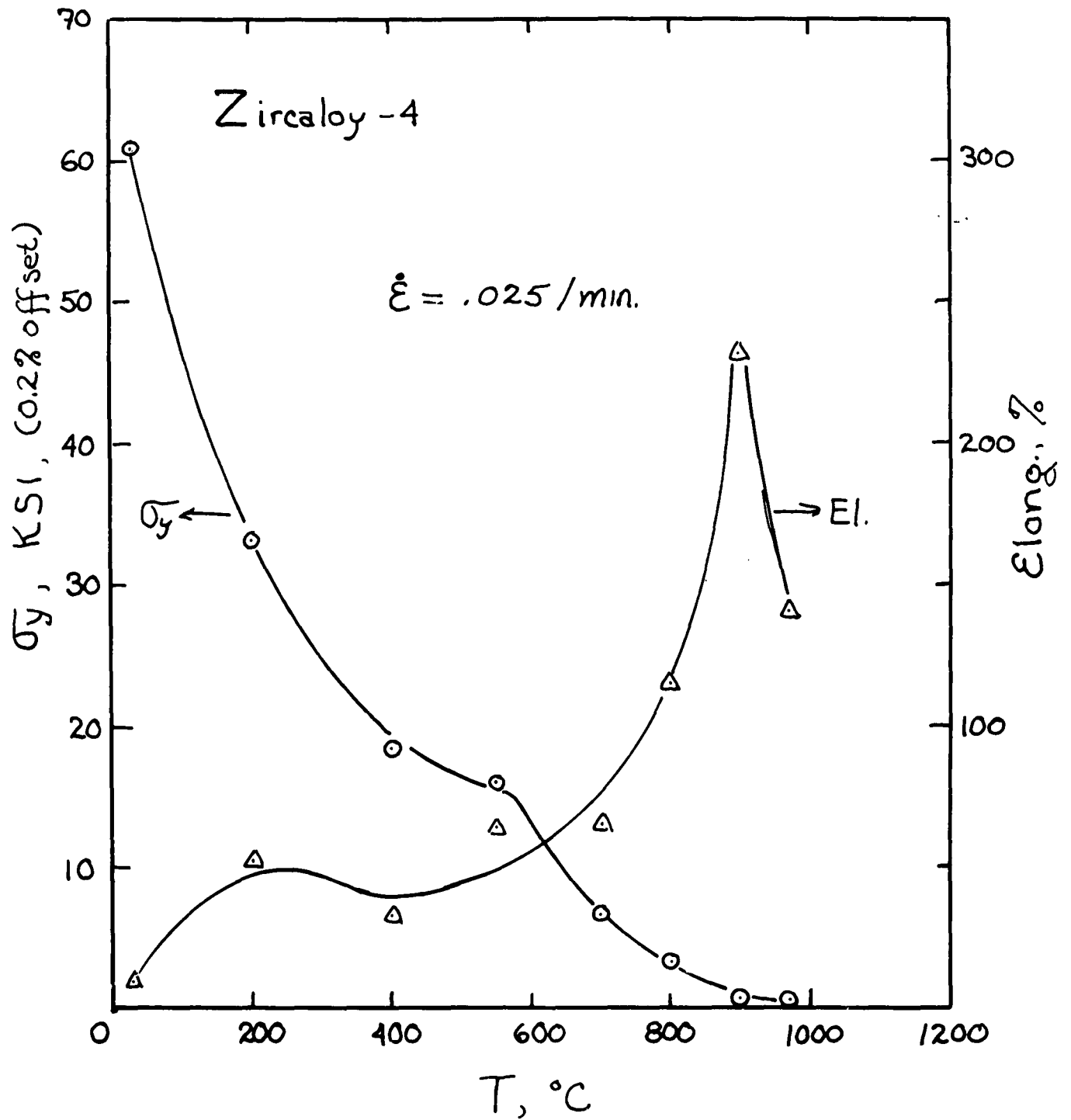


Figure 2. 0.2% Offset Yield Strength and Percent Elongation versus Temperature for Zircaloy 4. $\dot{\epsilon} = 0.025 \text{ min}^{-1}$.

DISTRIBUTION LIST

Contract N0w 65-0124-d, M.I.T.

Effect of Crystallographic Textures of Several
Anisotropic Metals on Design and Operation of
Deformation Processing Systems

<u>ADDRESSEE</u>	<u>NUMBER OF COPIES</u>
Chief, Bureau of Naval Weapons (DLI-31) Department of the Navy Washington 25, D. C.	2
Chief, Bureau of Naval Weapons (RRMA-24) Department of the Navy Washington 25, D. C.	4
Chief, Bureau of Naval Weapons (PID-24) Department of the Navy Washington 25, D. C.	1
Bureau of Naval Weapons Fleet Readiness Representative, Atlantic U. S. Naval Air Station Norfolk 11, Virginia	1
Bureau of Naval Weapons Fleet Readiness Representative, Pacific U. S. Naval Air Station North Island San Diego 35, California	1
Bureau of Naval Weapons Fleet Readiness Representative, Central Wright-Patterson Air Force Base Dayton, Ohio	1
Commanding Officer (MAP) Aeronautical Systems Division Air Force Materials Laboratory Plans and Programs Office (Mr. H. Jonson) Wright-Patterson Air Force Base, Ohio	1
Headquarters, Army Materials Command (Dr. Peter Kosting, AMC-RD-RD-CM) Washington 25, D. C.	1

DISTRIBUTION LIST

Contract N0w 65-0124-d, M.I.T.

<u>ADDRESSEE</u>	<u>NUMBER OF COPIES</u>
Director National Aeronautics and Space Agency (Code RRM - Mr. Raring) Washington 25, D. C.	1
Franklin Institute Laboratory (Mr. Marvin Herman) Philadelphia 3, Pennsylvania	1
Commanding Officer U. S. Naval Air Engineering Center Aeronautical Materials Laboratory Philadelphia 12, Pennsylvania	1
Chief, Naval Research Laboratory Attn: Mr. W. Pellini, Supt. Metallurgy Dept. Washington 25, D. C.	1
Chief, Office of Naval Research Department of the Navy Washington 25, D. C. Attn: Metallurgy Division	1
Dr. R. L. Fullman Manager, Metals Studies Section Metallurgy and Ceramics Laboratory General Electric Research Laboratory Schenectady, New York	1
Mr. N. P. Pinto, V.P. The Beryllium Corporation Reading, Pennsylvania	1
Mr. Stewart Arnold Asst. Director, Materials Laboratory Army Materials Research Agency Watertown, Massachusetts 02172	1
Mr. W. W. Beaver The Brush Beryllium Corporation 17876 St. Clair Avenue Cleveland 10, Ohio	1

DISTRIBUTION LIST

Contract NOW 64-0124-d, M.I.T.

<u>ADDRESSEE</u>	<u>NUMBER OF COPIES</u>
Professor M. C. Shaw Head, Department of Mechanical Engineering Carnegie Institute of Technology Pittsburgh 13, Pennsylvania	1
Dr. W. Rostoker IIT Research Institute Technology Center 10 W. 35th Street Chicago 16, Illinois	1
Dr. G. E. Dieter, Jr. Drexel Institute of Technology 32nd and Chestnut Streets Philadelphia, Pennsylvania	1
Mr. M. Semchyshen, Supv. Metallurgical Research Research Laboratory Climax Molybdenum Company of America 14410 Woodrow Wilson Boulevard Detroit 38, Michigan	1
Mr. J. H. Keeler, Mgr. Eng. Lamp Metals and Components Dept. General Electric Corporation 21800 Tungsten Road Cleveland, Ohio	1
Dr. Volker Weiss Associate Professor of Metallurgy Syracuse University Metallurgical Research Laboratories Building D-6, Collendale Campus Syracuse 10, New York	1
Dr. Eric B. Kula Watertown Arsenal Laboratories Watertown, Massachusetts 02172	1
Thomson-Ramo-Wooldridge, Inc. TAPCO Group Materials Development Laboratory 23555 Euclid Avenue Cleveland 17, Ohio	1

DISTRIBUTION LIST

Contract NOW 64-0124-d, M.I.T.

<u>ADDRESSEE</u>	<u>NUMBER OF COPIES</u>
Materials Advisory Board National Academy of Sciences (Mr. L. L. Gould) 2101 Constitution Avenue, N. W. Washington 25, D. C.	1
Commanding Officer Aeronautical Systems Division Air Force Materials Laboratory Physical Metallurgy Branch (MAMP) Wright-Patterson Air Force Base, Ohio	1
Mr. Roger L. Whiteley Assoc. Director Mechanical Metallurgy Division Homer Research Laboratories Bethlehem Steel Corporation Bethlehem, Pennsylvania	1
Commanding Officer Aeronautical Systems Division Air Force Materials Laboratory Manufacturing Technology Metallurgical Processing Branch (MATS) Wright-Patterson Air Force Base, Ohio	1
Scientific and Technical Information Facility Attn: NASA Representative (SAK/DL) P.O. Box 5700 Bethesda, Maryland 20014	2
Commanding General Watervliet Arsenal Watervliet, New York Attn: SWEV-RDR	1
University of California Berkeley 4, California Attn: Prof. E. G. Thomsen Industrial Engineering Dept.	1

DISTRIBUTION LIST

Contract NOw 64-0124-d, M.I.T.

<u>ADDRESSEE</u>	<u>NUMBER OF COPIES</u>
Westinghouse Electric Corporation Research & Development Laboratories Beulah Road, Churchill Borough Pittsburgh, Pennsylvania Attn: Dr. J. Brown	1
Defense Documents Center Cameron Station Alexandria, Virginia	10 (20 if available)
Mr. Roger Runck Defense Metals Information Center Battelle Memorial Institute 505 King Avenue Columbus 1, Ohio	2