UNCLASSIFIED

AD NUMBER

AD460199

LIMITATION CHANGES

TO:

Approved for public release; distribution is unlimited.

FROM:

Distribution authorized to U.S. Gov't. agencies only; Administrative/Operational Use; DEC 1964. Other requests shall be referred to Office of Naval Research, 875 North Randolph Street, Arlington, VA 22203-1995.

AUTHORITY

ONR ltr, 10 Aug 1965

THIS PAGE IS UNCLASSIFIED

UNCLASSIFIED AD_460199

DEFENSE DOCUMENTATION CENTER FOR SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION ALEXANDRIA, VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

05824-2-T

THE UNIVERSITY OF MICHIGAN

COLLEGE OF LITERATURE, SCIENCE, AND THE ARTS DEPARTMENT OF GEOGRAPHY

Technical Report No. 2

Geographical Coordinate Computations

General Considerations

W. R. TOBLER

Under contract with:

Department of the Navy Office of Naval Research Geography Branch Washington, D. C.

Contract No. Nonr 1224(48), Task No. 389-137

Administered through:

GED BY: L

7.

60

December 1964

DDC

ROBUNE

MAR 3 1 1965

SUBIVE

DDC-IRA E

OFFICE OF RESEARCH ADMINISTRATION - ANN ARBOR

GEOGRAPHICAL COORDINATE COMPUTATIONS

Part I

General Considerations

Technical Report No. 2

ONR Task No. 389-137 Contract Nonr 1224 (48)

Office of Naval Research Geography Branch

W. R. Tobler Department of Geography University of Michigan Ann Arbor, Michigan

December, 1964

This report has been made possible through support and sponsorship by the United States Department of the Navy, Office of Naval Research, under ONR Task Number 389-137, Contract Nonr 1224(48). Reproduction in whole or in part is permitted for any purpose by the United States Government.

\$

REPORT AVAILABILITY NOTICE

The following report has been issued by the University of Michigan under Contract Nonr-1224(48), ONR Task No. 389-137, sponsored by the Geography Branch of the Office of Naval Research. Copies are available from the Defense Documentation center for Scientific and Technical Information.

GEOGRAPHICAL COORDINATE COMPUTATIONS

Part I

General Considerations

By W. R. Tobler

Technical Report Number 2

December, 1964

ABSTRACT

Part I provides a discussion of the usefulness of coordinate models for studies of geographically distributed phenomena with comments on specific coordinate systems and their relevance for the analysis and inventorying of geographical information. Appendices include equations for conversion from the Public Land Survey system into latitude and longitude and to rectangular map projection coordinates. Part II considers map projections in greater detail, including estimates of the errors introduced by the substitution of map projection coordinates for spherical coordinates. Statistical computations of finite distortion are related to Tissot's Indicatrix as a general contribution to the analysis of map projections.

ACKNOWLEDGEMENTS

The preparation of this report has been facilitated by the assistance of several individuals. The University of Michigan Computation Center contributed in the numerical processing, and the University's Office of Research Administration and the Geography Branch of the Office of Naval Research both provided valuable administrative advice and support. Messrs E. Franckowiak, D. Kolberg, F. Rens, and R. Yuill, graduate students in the Department of Geography, contributed in several ways and were largely responsible for the illustrations and computer programs. The project has also benefited greatly from discussions with Professors R. Berry, L. Briggs, D. Marble, and J. Nystuen.

INTRODUCTION

In recent years there has been a rapid increase in the use of formal mathematical and statistical methods for the analysis of terrestrial distributions. Such procedures have been found to be of considerable assistance in fields such as city and regional planning, demography, ecology, geography, geology, and regional science. The present study is concerned with only one of the several mathematical strategies which have been utilized for such analyses; the "coordinate model". This term is taken to include that class of studies which specifically refers to the location of observational phenomena by some system of coordinates.

As an example, a technique associated with contemporary theories in geology consists of estimating the departures of empirical geological observations from a "regional trend". Here one has a collection of numerical observations (z_i) at specific terrestrial locations (x_i, y_i) , i = 1,2, ..., n. The procedure begins by estimating a specific portion of the locational trend of the observations as a least squares equation $\hat{z} = f(x, y)$. The trend is then subtracted from the observations to obtain the residual, which is subsequently interpreted in terms of geological theory. In this instance the recording of locations in some system of coordinates is an essential prerequisite for the analysis. There are many other such examples. The coordinate model is widely used, and is enjoying increasing popularity since the advent of electronic computers, which permit facile manipulation of the metricized locations. The researcher now also has available to him a rapidly increasing amount of information recorded in terms of coordinates; the U.S. Bureau of the Census, for example, now provides population statistics in terms of latitude and longitude coordinates. It is difficult to over-estimate the usefulness of this manner of recording information since a large number of the analytical methods designed for the analysis of distributions assume the existence of a system of coordinates.

As a system of locational labels the specific coordinates employed for the recording of observations are not of direct or inherent interest, but rather only what they enable one to deduce regarding interrelations among the phenomena observed. In this sense the particular coordinate system utilized is irrelevant. On the other hand, computations may often be simplified by the choice of a convenient coordinate notation. From a scientific point of view descriptions of phenomena and their interrelations are often simplified by appropriate formalizations involving a "natural" coordinate system for that phenomena; the use of geomagnetic coordinates in the study of terrestrial magnetism, for example. The present study, however, considers only systems which appear to be of practical utility for the large scale recording of terrestrial observations, with some emphasis on systems available in the United States.

The actual surface of the earth can be referred to as the topographic surface. This bumpy two-dimensional surface is difficult to describe in all its detail. Theoretically it is possible to introduce a system of coordinates on this surface such that ground distances, etc., between all points can be calculated. In practice this is not attempted. As an approximation to the topographic surface the geodesist utilizes a surface of constant gravitational potential, the geoid. This bumpy but rather smooth surface is still too complicated for practical computations. A further simplification is made by assuming the earth to have the shape of an ellipsoid, generally an ellipsoid of revolution. Geodetic coordinates are then defined for positions on this ellipsoid. An even simpler model of the topographic surface is to consider the earth to be a perfect sphere. One can continue thusly, finally arriving at the assumption that the earth is a flat plane. Each of these assumed models of the earth has its advantages and disadvantages since realism may lead to extreme cumbrousness. In practical terms, the following (somewhat contradictory) criteria seem appropriate:

a) The coordinates should permit accurate and economical formulae for computation. The highest level of precision available today can be achieved only through the use of geodetic formulae. These formulae are fairly complicated. Computational simplicity can be obtained, with a consequent reduction in accuracy, by employing spherical formulae. Further computational simplicity can be achieved by the use of plane coordinates based on an appropriate map projection, again with some loss of accuracy.

Computational simplicity is important for two reasons. The cost and time required for computation, particularly when large amounts of information are to be processed, can be reduced by significant amounts through the use of simplified formulae. In addition, the number of persons and agencies who can effectively make use of the information is significantly increased by the use of simplified formulae.

It is more difficult to discuss accuracy, upon which the level of computational simplificty depends, since the degree of precision required in particular studies varies considerably. There is no reason to employ a method which results in accuracies greater than required or greater than those with which the information was recorded. An objective of this study has been to estimate the accuracy obtainable by employing several alternate methods. This allows the individual researcher to choose the simplest computational method which yields the requisite level of accuracy.

b) A rapid and accurate method of determining the coordinates of a position should be available. In general a system of coordinates which requires a carefully executed geodetic survey can be considered highly accurate, but relatively slow. A system which enables one to read coordinates from an aerial photograph or map (either manually, mechanically, or electronically) is more rapid but the accuracy is dependent on the map scale. The convenience of this method is also dependent on the availability of maps or photographs to which the coordinate system has been affixed. Between the extremes of geodetic surveying and map scaling are a number of intermediate systems, including automatic navigation devices which permit virtually instantaneous, in situ position determination, with fair accuracy. Emphasis in this study is on map scaling procedures.

c) The coordinates should be widely available and should be equally convenient for use at a local, national, and international level. This objective arises since most types of information collected at a national level are used both nationally and locally. Census records provide a good example. National use of local records also is increasing. The accuracy requirements at these two levels generally differ, however. At the local level an accuracy of fifty feet may be insufficient, whereas at the national level an accuracy of five miles may suffice.

TERRESTRIAL COORDINATE SYSTEMS

There are many locational coordinate systems in use throughout the world. Emphasis in the current discussion is on systems available in the United States.

Geodetic Coordinates:

ê

Geodetic latitude and longitude provide the traditional method of identifying locations on the surface of the earth. The earth is assumed to be an oblate spheroid and the geodetic coordinates are based on actual measurement (triangulation) between sets of locations on the topographic surface. These values are then adjusted to fit an ellipsoid representative of the region in question. Different ellipsoids are employed for the several continents of the world, with an International Ellipsoid in use for world-wide computations. Geodetic coordinates, based on the Clarke Ellipsoid of 1866 (1927 adjustment), are indicated on maps published by the U.S. Geological Survey and by the U.S. Coast and Geodetic Survey. Latitude and longitude scaled from such maps are geodetic coordinates, but such scaling will not yield the same accuracy as when the positions are established in the field by an expensive first order geodetic survey.

Computations employing geodetic coordinates usually take into account the ellipsoidal shape assumed for the earth. The relevant formulae are fairly complicated. For precise geodetic work it is necessary to carry approximately fifteen significant digits. Experience with a digital computer, however, indicates that, once programmed, the ellipsoidal formulae do not require appreciably more effort than the simpler spherical formulae. A floating point program with seven significant digits (as employed) for this study) yielded values which differed less than 100 meters from more precise values over a range of 6000 kilometers.

Assumptions required to apply geodetic computations to the surface of the earth are that (a) the geodetic latitudes and longitudes are known without error, (b) the ellipsoid chosen is representative of the region in question, and (c) the points involved lie on the surface of the ellipsoid (roughly, at sea level). On the other hand, this is the most accurate system available. The actual proportional error in distance, based on misclosures of the U.S. continental triangulation network, appears to be on the order of

$$\frac{1}{20000}$$
 p1/3

where D is the computed distance in miles on the Clarke Ellipsoid of

1866 (1927 adjustment). The differences between the several ellipsoids in use throughout the world are small; on the order of three kilometers per 6000 miles. Connections of this length on one ellipsoidal datum are rare and the figure given does not take into account the fact that the relation between the several datums in actual use are not yet known in detail; in other words, distances between positions whose geodetic coordinates are referred to different ellipsoids may be in error by a larger figure.

Astronomic Coordinates:

Astronomic latitude and longitude are based on celestial observations and may depart from geodetic coordinates by as much as two kilometers at any point, due to departure of the geoid from the ellipsoid. Astronomical observations are usually available only for isolated points, and will not be considered in this report.

The U.S. Public Land Survey

The Public Land Survey system is based on a set of six mile squares numbered as townships north and south of a base parallel, and as ranges east and west of a base meridian. These six mile squares are then subdivided into 36 sections, each one mile square, and numbered in serpentine fashion. Each section can be further subdivided into quarter-sections, each one sixteenth of a mile in area. Several systems similar to the Public Land Survey exist in various parts of the United States; these are not considered here.

Strictly speaking, the Public Land Survey is an areal identification scheme and not a metrical coordinate system, though it is often regarded as such. As a partitioning of areas the system does not differ from county or census units, except that the elemental areas are roughly of equal size and are labeled in a more convenient fashion. The system is not complete, in the sense that it is defined only for certain portions of the western United States. In these areas large amounts of information have been (and continue to be) collected and recorded in terms of Sections, Townships, and Ranges. These collections of information provide a valuable source of raw data for research workers. The Public Land Survey, however, was not designed for the analytical manipulations usually required in research work. For example, statistical analyses of spatial distributions may require calculation of the average location (and its variance, and so on) of phenomena. For such computations the distances between observed locations may be needed. The distance between the SW2, Sec. 25, T5S, R7W, Willamette Meridian, and the NEZ, Sec. 2, T6N, R8E, Black Hills Meridian, is not immediately apparent, nor is there any simple formula which can be employed to obtain this difference. Observations recorded in the Public Land Survey System, however, can be convered to a coordinate system having the requisite metrical properties. This is because the Public Land Survey has many of the topological ordering properties of a coordinate system. The most direct and convenient conversion is to latitude and longitude. This can be effected in several ways. The system of Townships and Ranges is shown on U.S. Geological Survey topographic maps and approximate

coordinates could be scaled from there maps. A more convenient procedure is to attempt a direct calculation. The equations for such a conversion are given in the Appendix, along with an estimate of their validity. The errors are fairly small so that they might be of little consequence when working with observations from the entire United States. The urban researcher working within one city, on the other hand, might find these errors intolerable.

The GEOREF and Marsden Squares Systems

The GEOREF System is used by the U.S. Air Force to identify locations. It is a modification of latitude and longitude in which letters are substituted for the numerical values. Every combination of letters is taken to represent a quadrilateral bounded by latitude and longitude. In this sense the system is a partitioning of area rather than a true coordinate system. The same results can be achieved by using latitude and longitude with a convention regarding the quadrant in which the quadrilateral of area lies. The system has certain advantages in applications which require error-free rapid verbal communications (e.g. radio). The system is shown on maps published by the U.S. Air Force.

The Marsden Squares system employed by the National Oceanographic Data Center is similar to the GEOREF System in that a numbering of latitude and longitude quadrilaterals is substituted for the geodetic coordinates. There are many other such systems available, including the World Aeronautical Chart designations and the International Millionth Map of the World system. The advantage of these systems is largely one of bookkeeping. Such systems are not further considered in this report.

THE SPHERICAL ASSUMPTION

The various computations are simplified if it is assumed that the earth is a sphere. The results of such computations do not differ by large amounts from the corresponding ellipsoidal values - the polar flattening of the earth, after all, is quite small. On the basis of a number of computations it appears that a reasonable and convenient rule of thumb is that the flattening of the earth can be taken as an <u>approximate</u> upper bound on the percentage error of measures calculated on a spherical as compared to an ellipsoidal assumption. This is about one part in 300. An even safer estimate is that the error will be less than one percent. For some purposes this is intolerably large, but for the majority of requirements it is far more accurate than are the data or theories now available. Detailed numerical differences between an ellipsoid and sphere for distances and angles also have recently been published. Computation of the differences for a random sample of 200 pairs of points within the continental United States resulted in the following values:

Distance Differences (miles)	Angular differences (degrees)
Average: 0.046	Average: 0.006
Standard Deviation: 1.896	Standard Deviation: 0.083
Minimum: -3.788	Minimum: -0.150
Maximum: 4.871	Maximum: 0.159

A second sample might yield somewhat different results, but the sample is probably representative for the country as a whole. As expected, the differences depend on both the distance and on the direction of the point pairs. A comparison of surface areas is given in the accompanying table.

In performing these computations it has been assumed that the earth is a sphere whose radius is equal to the <u>equatorial</u> radius of the Clarke Ellipsoid of 1866, and that the geodetic latitude and longitude can, without modification of their numerical values, be considered to be spherical coordinates. These assumptions have the advantage of extreme simplicity. A slight improvement in accuracy can be obtained if they are not retained. For example, the spherical radius employed might be the average radius of terrestrial ellipsoid in the vicinity of the area of interest, rather than the equatorial radius. It can be proven that the average radius at any latitude is the geometric mean of the radii of curvature along the meridian and normal to the meridian. This average radius is given in the accompanying tables. Conversion of geodetic latitude to spherical latitude can also be accomplished in a large number of ways. Four of the simpler methods are illustrated in the figure. Mathematical treatments can be found in works on geodesy and map projections.

THE PLANE ASSUMPTION

It often is convenient to employ plane coordinates for the inventorying of analysis of terrestrially distributed phenomena. In particular, many of the numerous statistical and analytical methods which have been devised for the analysis of two dimensional distributions assume the existence of a system of Cartesian coordinates. As a very simple example, suppose that an objective is to compute the average location and the locational variance of a set of discrete phenomena on the surface of a sphere. One can proceed in several ways:

- a) Record the observations in latitude and longitude and then perform the calculations using the spherical formulae for average and variance.
- b) Plot the distribution on a map, assign arbitrary rectangular coordinates to the map, record the observations in these coordinates, and then perform the calculations using the plane formulae for the average and variance.

COMPARISON OF AREAS FOR A ONE DEGREE ZONE OF LONGITUDE WITHIN THE UNITED STATES

(Values in square miles, rounded to the nearest square mile)

Ellipsoidal Area	Spherical Area*
4265	4282
4228	4244
4189	4205
4150	4164
4109	4123
4067	4080
4024	4035
3979	3990
3934	3943
3887	3895
3839	3846
3789	3796
37 39	3744
3687	3692
3634	3638
3581	3583
3526	3528
3469	3471
3412	3413
3354	3354
3295	3294
3234	3232
	Ellipsoidal Area 4265 4228 4189 4150 4109 4067 4024 3979 3934 3887 3839 3789 3739 3687 3634 3581 3526 3469 3412 3354 3295 3234

*Radius equal to equatorial radius of Clarke ellipsoid of 1866.

#

CLARKE ELLIPSDIO OF 1866

,1

	EAN RADIUS DIUS OF THE PARALLEL	-5837 6378-2064 -6656 6372-1767 -9106 6354-0986	• 3100 6281 9481 • 6000 6281 9481 • 4672 6162 2714	••••••••••••••••••••••••••••••••••••••		-5687 5066-5297 -4106 4892-8360 -2824 4709-7877 -1696 4317-7242 -0579 4317-0079		-1223 2703-0712 -5218 2447-915 -9612 1923-9953 -9612 1923-8953 -9610 1384-9715 -1656-0388 -9610 1384-9715 -1656-0388 -1928-02388 -1928-0217 -1011-2173 -1012-012 -1112-2173 -1122-2173 -112
II IN KILOMETERS	RADIUS ME Normal Rad To The Merioian	78.2064 6356. 78.2474 6356. 78.3703 6356.	79.2274 6357 79.2178 6358	80.1591 0.500 80.7330 6361. 81.3699 6362. 82.0652 6364.	85.3198 6370.	86.2209 6372. 87.1439 6374. 88.0815 6376. 89.0268 6378.	90.9114 6381. 91.8364 6383. 92.7403 6385. 93.6163 6387. 94.4577 6389. 95.2581 6390.	96.0112 6392. 97.3516 6394. 97.9316 6394. 98.8422 6396. 98.8812 6399. 99.2451 6399. 99.2451 6399. 99.7369 6399. 99.8610 6399.
RAO	RADIUS DF THE Merioian	6335-0344 63 6335-1569 63 6335-5231 63	6336.1704 63 6336.9745 63 6339.3456 63 6339.3456 63	6340.8549 63 6342.5659 63 6344.4656 63 6346.5398 63	6356.2540 63 6351.1485 63 6356.2540 63	6358.9457 63 6361.7029 63 6364.5051 63 6367.3308 63 6370.1588 63	6372.9570 6372.9570 6375.7345 6375.7345 6381.0624 6383.5820 6385.9794 63	6388.2357 63 6390.23139 6392.23139 6392.25146 63 6395.5226 63 6395.8391 63 6396.8391 63 6399.4057 63 6399.4057 63 6399.7780 63
	RAGIUS DF THE Parallel	3963.2258 3959.4791 3948.2459	3929.5463 3903.4138 3869.8950 3829.0502	3780-9528 3725-6892 3663-3592 3594-0755	3435.1618 3435.1618 3245.8212	3148.1893 3040.2613 2926.5205 2807.1780 2480	2002.430 2552.5869 2417.8147 2278.3928 2134.3928 1986.6619 1834.9064	1679.6072 1521.0611 1359.5722 1195.4507 1195.4507 1029.0127 860.5796 860.5796 519.0344 346.5839 173.4605
ILES	MEAN Raoius	3949.7901 3949.8410 3949.9932	3950.2456 3950.5964 3951.0429 3951.5818	3952.2090 3952.9200 3953.7092 3954.5709	3958.6052 3958.6852 3957.5233 3958.6052	3959.7227 3960.8672 3962.0303 3963.2029	3965.5413 3965.5413 3965.6893 3967.8113 3968.8988 3969.9435 3970.9373	3971.8727 3972.7423 3974.2581 3974.8925 3975.4380 3975.4380 3975.2454 3976.5013
RADII IN M	RADIUS Normal To The Meridian	3963.2258 3963.2513 3963.3276	3963.4543 3963.6303 3963.8542 3964.1245	3964.4391 3964.7957 3965.1915 3965.6236	3966.5832 3966.5832 3967.1036 3967.6458	3968.2058 3968.7792 3969.3619 3969.9492	39710-2369 3971-6950 3972-2567 3972-8010 3973-3239	3974.2891 3974.7242 3975.4824 3975.4824 3975.6229 3976.0724 3976.6042 3976.6042 3976.6042
	RADIUS OF THE Merician	3936.4000 3936.4761 3936.7036	3937.0810 3937.6055 3938.2731 3939.0788	3940.0167 3941.0799 3942.2603 3943.5491	3944.9368 3946.4128 3947.9662 3949.5852	3951.2578 3952.9710 3954.7122 3956.4680	3959.9222 3959.9702 3963.3709 3963.3709 3966.5660 3966.5660	3969.4577 3970.7614 3971.9566 3973.9856 3974.8036 3974.8036 3976.6297 3976.6297
	LATITUDE	2.5 5.0	7.5 10.0 12.5 15.0	17.5 20.0 22.5	27.5 30.0 32.5 35.0	442°0 442°0 1000	, , , , , , , , , , , , , , , , , , ,	65.0 67.0 72.0 882.0 882.0 882.0 875.0 882.0 875

INTERNATIONAL ELLIPSOID

	RADIUS OF THE Parallel	6378.3380 6372.3079 6354.2286 6324.1325 6282.0734	6228.1266 6162.3890 6084.9787 5996.0350 5895.7188 581.7139 5661.7139	5528-4503 5384-6633 5230-6160 5066-5909	4517.09.8555 4517.7655 4517.7653 4517.7653 4517.7653 4517.7653 3891.1271 3666.7440 3495.3020 3495.3020 3477 2188.0242 1923.8944 1923.8944 1923.8944 1923.8944 1923.8944 1111.2153 835.3047	557.1726 279.1575 .0001
METERS	MEAN RAOIUS	6356.8619 6356.9434 6357.1866 6357.5902 6358.1509	6358.8647 6359.7260 6360.7286 6361.8650 6363.1266 6363.1266	6367.5637 6369.2233 6370.9526 6372.7388	6376.42/3 6378.3016 6382.0394 6382.0394 6383.8742 6389.059 6389.6676 6392.1592 6393.5493 6393.5493 6393.5493 6393.5493 6399.6664 6393.5493 6399.68234 6399.8234 6399.8234	6399.5573 6399.8040 6399.8864
RADII IN KILO	RADIUS Normal To The Meridian	6378.3380 6378.3787 6378.5008 6378.7032 6378.9846	6379.3425 6379.7746 6380.8774 6381.8474 6381.4800 6381.4800 6382.1707	6383.7046 6383.7046 6384.5364 6385.4031 6386.2982	6389.0849 6399.0849 6390.0249 6390.0249 6390.0241 6392.7731 6392.7731 6392.7731 6395.2737 6395.2737 6395.2737 6395.2737 6395.2737 6395.2737 6399.4781 6399.8721 6399.5175	6399.7219 6399.8452 6399.8864
	RADIUS OF THE MERIOIAN	6335.4584 6335.5801 6335.9437 6336.5471 6336.5471	6338.4526 6339.7405 6341.2397 6342.9391 6344.8260 6344.8260 6344.8260	6351.4638 6353.9470 6356.5349 6359.2083	6364.7301 6367.5367 6370.3453 6370.3453 6370.3453 6370.3453 6381.1750 6381.1750 6381.1750 6381.6775 6381.0573 6394.0157 6395.5365 6395.5365 6395.5365 6395.5365 6395.5365 6396.9837	6399.3928 6399.7629 6399.8864
	RAOIUS Of the Parallel	3963.3075 3959.5606 3948.3267 3929.6259 3903.4916	3869.9707 3829.1233 3781.0223 3725.7560 3653.4225 3663.4225	3718-0169 3435.2129 3345.8680 3250.1476 3148.2274	2926.5501 2807.2036 2682.6050 2417.8295 2417.8295 278.4045 2134.5934 1986.6685 1834.9109 1679.6100 1521.0625 1359.5725 1359.5725 1359.5725 1359.5725 1359.5725 1359.5725 519.0333	346.5831 173.4601 .0001
LES	MEAN RADIUS	3949.9630 3950.0136 3950.1647 3950.4155 3950.7639	3951.2074 3951.7426 3952.3656 3953.0717 3953.8557 3953.8557	3955.6127 3956.6127 3958.7185 3959.8284	3962.1203 3963.2849 3965.64503 3965.6476 3965.6475 3965.7476 3965.7476 3967.8619 3976.8619 3972.75511 3971.8957 3971.8954 3977.8856 3975.4366 3975.28856	3976.4926 3976.6458 3976.6971
RADII IN MI	RADIUS Normal To The Merioian	3963.3075 3963.329 3963.4087 3963.5345 3963.7093	3963.9317 3964.2002 3964.5127 3964.8668 3965.2599	3966.1510 3966.6422 3967.6591 3957.6976 3958.2538	3969.4020 3969.9854 3971.5689 3971.1484 3971.1492 3972.8177 3972.8177 3972.8177 3973.3370 3973.3370 3975.1238 3975.1238 3975.4807 3975.4678 3975.4678	3976.5948 3976.6715 3976.6971
	RADIUS OF THE MERICIAN	3936.6635 3936.7391 3936.9650 3937.3400 3937.3409	3938.5240 3939.5240 3940.2558 3941.3118 3942.4842 3943.7644	3945.1426 3946.6087 3948.1517 3949.7598 3951.4209	3954.8520 3956.5960 3956.5960 3966.0743 3961.7822 3965.0704 3965.0704 3966.6253 3966.6253 3966.6253 3966.6253 3966.6253 3966.6253 3971.9791 3972.9942 3973.9942 3974.8066 3974.8066	3976.3904 3976.6203 3976.6971
	LATITUDE	0.00.00	22.0 22.5 25.5 25.0 25.0	27.5 30.0 32.5 37.5	44400000000000000000000000000000000000	85.0 87.5 90.0



c) Record the observations in latitude and longitude, apply a transformation to obtain rectangular coordinates, and then perform the claculations using the plane formulae for the average and variance.

Procedure (a) has the disadvantage of being more complicated. A sufficiently small portion of the earth's surface can be considered a plane and the additional complication introduced by the use of spherical versions of the statistical formulae may not be warrented. Somewhat similar problems have been investigated in the field of land surveying and are reported in most works on geodesy. Procedures (b) and (c), above, are mathematically equivalent since maps are made by transforming latitude and longitude to plane coordinates via a map projection. Hence a study of the numerical differences between computations on a plane and on the earth becomes a study of map projection distortions.

The official map producing agencies of the various countries of the world have recognized the advantages of rectangular coordinates for local purposes and save the map user the trouble of assigning his own system of rectangular coordinates. They do this by publishing maps which have the official plane coordinates printed directly on the maps. Two map projection systems of this type are available in the United States, and comparable systems exist in most other countries of the world. The use of these systems is not restricted to calculations; they might also be used to record and index information in terms of the plane coordinates, perhaps scaled from topographic maps. The systems now available have several features in common. The coordinates are usually given as rectangular coordinates, often chosen so that all values are positive. More importantly, the errors in computing as though the earth were a plane disk can be evaluated. This implies that the region within which one can perform plane computations with a specified level of precision can be defined on an a priori basis. If the allowable error is small, the region must be small or several map projection systems (called zones) must be used within the region. In the latter event conversion between zones may be required. This conversion may be directly from zone to zone or may involve reconversion to geodetic coordinates as an intermediate step. There are certain advantages in using a conformal map projection for such a system since the scale errors are then independant of direction and a scale factor can be applied to improve the accuracy of short lengths . The two systems employed in the United States are:

1) The State Plane Coordinate System: This system comprises approximately 120 zones covering the entire United States, with the orientation toward individual states. The accuracy within each zone is one part in 10,000. The larger states therefore require several zones. The zones overlap, with boundaries between zones lying along minor civil divisions (usually counties). The Lambert Conformal Conical projection and the Transverse Mercator projection are employed (with only one exception),

7

depending on the shape of the individual states. This system is admirably suited to the needs of the local land surveyor and has been officially adopted by many local governmental units. In many states it has legal status, is used for land ownership, and appears on large scale maps. Conversion tables are available and simple to use for any particular zone. Conversion between zones, and especially between states, is somewhat more inconvenient. The location of the zones occasionally is awkward. In Washington state, for example, the two merging metropolitan areas of Seattle and Tacoma each lie in a separate zone. The system of State Plane Coordinates appears on all recent U.S. geological Survey topographic maps.

2) The Transverse Mercator System:

Known as the Universal Transverse Mercator grid system (UTM) this system is employed by the U.S. Army. The UTM grid extends to eighty degrees north and south latitude, beyond which a Polar Stereographic grid is employed. The UTM grid extends around the world in sixty north-south zones, each covering six degrees of longitude with an overlap of one half degree. The accuracy within each zone is one part in 2500. Since different areas of the world are based on distinct ellipsoidal datums, separate tables are required for various parts of the world. Procedures are available for converting directly from one zone to adjacent zones. The zonal nature of the system is occasionally inconvenient. An alphanumeric partitioning of areas is available in the system. The UTM grid appears on all Army Map Service topographic maps, on some foreign maps, and on all recent U.S. Geological Survey topographic maps.

Both of the foregoing systems have several advantages. They can be employed for virtually all computations without serious error. Further, any information recorded in either of these systems can be related to geodetic coordinates and hence to information collected anywhere else in the world. Also, these coordinates are already shown on published maps, and most photogrammetric firms are sufficiently familiar with these systems to add them to aerial photographic or maps compiled by photogrammetric methods. The disadvantages of these systems stem largely from their advantages. The very refinement required to provide coordinates of high accuracy restrict these systems to relatively small portions of the earth's surface and the transformation equations, either between zones, or to and from geodetic coordinates, are relatively complicated. These difficulties can be circumvented in several ways.

When a map projection system is to be used soley for computational purposes, and not necessarily to be indicated on published maps, the choice of a particular projection depends on the type of computation contemplated. The systems cited above are so refined that they yield a stated level of accuracy for virtually all computations. This is a restriction which narrows the range of suitable projections and results in projection which require fairly involved computations. For a given

problem there may be a specific projection which is computationally much simpler but which yields results which are of equal accuracy. For example, a problem which requires interpolation between two points on a sphere might be attacked by using the gnomonic projection (see Appendix) since all great circles are straight lines on this projection; linear interpolation in gnomonic coordinates will yield a point lying on the arc connecting the two given points. Similarly, problems involving circles on a sphere may be attacked using the stereographic projection. In other situations computational simplicity and speed may be more important than a few tens of meters of accuracy. Kao, for example, has recently shown that the geometric (perspective) projections are especially well suited for calculation by digital computer, particularly when large amounts of locational information are required within fractions of a second (i.e., in real time problems). Clearly the choice depends on the nature of the problems and the volume of the information to be processed. Computer calclation of distance and direction on a sphere (or ellipsoid) may, in many instances, be easier than attempting to convert to plane coordinates. On the other hand a more complicated problem, as for example, occurs in weather prediction, may advantageously be solved by the use of an appropriate map projection. In this instance the problem is to construct contour-type maps of the entire northern hemisphere from information received from locations scattered within this region. Rather than attempting to solve the contour interpolation problem on a sphere, the Weather Bureau employs stereographic map projection coordinates with a local correction for the projection distortion and solves the problem in plane coordinates.

If one has information recorded in latitude and longitude simple conversions to map projection coordiantes are available. For example, one can pretend that these are already the ordinate and abscissa of a plane coordinate system. The resulting projection is known as the square projection. Computations performed in this manner will differ from the true values by amounts which depend on the size of the region and on the latitude. Another simple, but slightly better, conversion is to multiply all the abscissas (longitudes) by a constant equal to the cosine of the average latitude of the region in question (the square projection with a standard parallel; also known as the rectangular projection). Such a procedure might for example, by employed in urban analysis, depending on the size of the area. Another alternative would be to transform to rectangular coordinates by converting all values into distances north and east (that is, measured along a parallel) from some arbitrary point within the region. This yields the sinu-The equations for all of the above projections are soidal projection. extremely simple. Somewhat more refined, but also more complicated, solutions take into cosideration the shape of the area of concern. Albers' equal area conical projection with standard parallels at 29° 30'N and 45° 30'N, and Lambert's conformal conical projection with standard parallels at 33°N and 45°N, for example, are two systems which might be suitable



SQUARE PROJECTION





Standard parallels at 60N and 60S

for the continental United States. The distance error in computing with these latter systems is not likely to exceed fifty miles.

The use of latitude and longitude, while advantages from the point of view of long run national needs, entails some local difficulties. In the process of recording it may be necessary to interpolate between curved lines, and the system of minutes and seconds is awkward (Decimal degrees are more convenient). The complete number of digits required to specify a given location in its world context is excessively large for local use, and the north-south and east-west designation is often superflouous (a mathematical convenience is obtained if south latitudes and west longitudes are considered negative). Finally, and perhaps most important, it is often difficult to determine the latitude and longitude of a particular spot.

The direct recording and storage of geographical information in terms of rectangular coordinates circumvents some of these difficulties, but introduces others. The majority of the electro - mechanical data reduction devices (specifically, coordinate readers) which are now on the market utilize rectangular coordinates. These instruments reduce the teduim of coordinate reading, even when the desired result is latitude and longitude coordinates. In this case the inverse map projection equations are required. Curiously, these are not widely available in the literature on the subject of map projections (with a few exceptions) since the previous technology prohibited their extensive use.

If the objective of the study does not include subsequent conversion to latitude and longitude, a convenient procedure is to draw arbitrary rectangular (or polar) coordinates on whatever maps or aerial photographs are available. One advantage is that this can be done by persons with no training and with virtually no intellectual effort or financial expenditure. When the map used is accurate and at a "sufficiently large" scale these arbitrary coordinates may be employed as are the map projection coordinates discussed above. If the information collected has no permanent value, this procedure is perfectly satisfactory.

A disadvantage is that the errors introduced are not known. The limits within which a certain level of accuracy obtains is uncertain an one never knows whether the system can be extended to include a neighboring territory. A second major disadvantage is that it may not be possible to use information collected for one study in a second study which either (a) encompasses a larger area than the original study, or (b) which is subsequent in time to the original study, especially if the original map has been lost, or (c) which requires a higher level of accuracy than the

the original study. One can imagine the difficulty of analyzing the greater metropolitan area of Kansas City if Kansas City, Missouri and Kansas City, Kansas, used two different and unrelated grid systems. Or if each bureau of a city government employed a distinct system of coordinates. The actual occurance of situations of this very nature in the field of civil engineering is what gave impetus to the establishment of the system of State Plane Coordinates by the U.S. Coast and Geodetic Survey in the 1930's.

Conversion between arbitrary map coordinates can be effected with relative ease if the relation between the two systems is known, or if both systems are related to latitude and longitude by known inverse equations. If the relation between systems is not known it is theoretically possible to estimate the relation if the coordinates of a sufficient number of points are accurately known in both systems (see Appendix). Such conversions may occasionally be required but are expensive.

A final distinction should be made between coordinates and areas. Coordinates describe points, not areas, and one must distinguish between an real recording unit such as a census tract and between the coordinate system used to pinpoint some centroid taken to represent that areal unit. Areal information recording units are extremely numerous and differ widely in size and shape. As a consequence it is often necessary to convert from one areal unit (e.g. census tract) to other areal units (school district, political precint, and so on). These areal conversions differ somewhat from the coordinate conversions discussed in this report. In general, specification of the areal boundaries must be included in the mathematical conversion statements. There are then again several procedures, of varying accuracy and complexity, which may be employed for the conversions.

SELECT REFERENCES

0. S. Adams, <u>Latitude Developments Connected with Geodesy and</u> <u>Cartography</u>, Coast and Geodetic Survey Special Publication No. 67 (Washington, Government Printing Office, 1921), 132 pp.

R. Bachi, "Standard Distance Measures and Related Methods for Spatial Analysis", <u>Papers</u>, Regional Science Assn., X(1962), pp. 83-132.

G. V. Bagratuni, "On the Accuracy of Distances and Azimuths obtained from the solution of the Inverse Geodetic Problem," AERDL-T-1081, 1961.

H. P. Bailey, "Two Grid Systems that Divide the Entire Surface of the Earth into Quadrilaterals of Equal Area", <u>Transactions</u>, American Geophysical Union, XXXVII (1956), pp. 628-635.

B. Berry, "Sampling, Coding, and Storing Flood Plain Data", <u>Agriculture</u> <u>Handbook</u> No. 237, U.S. Department of Agriculture, Washington, 1962, 27 pp.

B. Berry, et. al., "Geographic Ordering of Information: New Opportunities", <u>The Professional Geographer</u>, 16, 4 (July 1964) pp. 36-40.

W. Bowie and O. S. Adams, <u>Grid System for Progressive Maps in</u> the United States, U.S. Coast and Geodetic Survey Special Publication #59 (Washington, Government Printing Office, 1919), 227 pp.

R. M. Brooks, <u>Coordinate Transformation Formulas</u>, Pacific Missile Range Technical Note. 3280-220, 1962.

R. A. Bryson, "Fourier Analysis of Spatial Series," in <u>Quantitative</u> <u>Geography</u>, W. L. Garrison, ed., Forthcoming.

Bureau of Land Management, <u>Manual of Instructions for the Survey</u> of the Public Lands of the United States (Washington, Government Printing Office, 1947), 613 pp.

J. D. Carroll, Jr., <u>Chicago Area Transportation Study</u>, Final Report, Vol. I: Survey Findings (Chicago, CATS, 1959) 126 pp.

D. Clark, <u>Plane and Geodetic Surveying</u>, Vol. II, 4th ed., London, Constable and Co., 1951.

Coast and Geodetic Survey, <u>Plane-Coordinate Systems</u>, Serial 562 (Washington, Government Printing Office, 1948) 5 pp.

F. H. Collins, <u>Coordinate Transformation</u>, Technical Report NAVTRADEVCEN 1907-7315, 1963. R. L. Creighton, J. D. Carroll, Jr., and G. S. Finney, "Data Processing For City Planning", <u>Journal</u> (American Institute of Planners), XXV, 2 (1959), pp. 96-103.

C. H. Deetz, and O. S. Adams, <u>Elements of Map Projection</u>, Coast and Geodetic Survey Special Publication No. 68, 5th ed. (Washington, Government Printing Office, 1945), 60 pp.

S. C. Dodd and F. R. Pitts, "Proposals to Develop Statistical Laws of Human Geography", <u>Proceedings</u>, IGU Regional Conference in Japan (Tokyo, Kasai, 1959), pp. 302-309.

F. Fiala, <u>Mathematische Kartographie</u>, (Berlin, Verlag Technik, 1957), 316 pp.

G. A. Ginzburg, "A Practical Method of Determining Distortion On Maps", <u>Geodezist</u>, 10 (1935), pp. 49-57.

D. I. Good, "Mathematical Conversion of Section, Township, and Range Notation to Cartesian Coordinates", <u>Bulletin 170, part 3,</u> State Geological Survey of Kansas, 1964, 30 pp.

N. D. Haasbrock, <u>Investigation of the Accuracy of Plotting and</u> <u>Scaling-off</u>, Netherlands Geodetic Commission, Delft, 1955.

T. Hagerstrand, "Statistika Primaruppgifter, Flygkartering Och 'Data Processing' - Maskiner: Ett Kombineringsprojekt", <u>Meddelanden Fran Lunds Geografiska Institution</u>, Nr. 344 (Lund, University of Lund, 1955), pp. 233-255.

E. T. Homewood, "The Computation of Geodetic Areas...", <u>Empire</u> Survey Review, XIII, 101, pp. 309-321.

A. J. Hoskinson and J. A. Duerksen, <u>Manual of Geodetic Astronomy</u>, Coast and Geodetic Survey Special Publication No. 237 (Washington; Government Printing Office, 1947), 219 pp.

G. L. Hosmer, Geodesy (New York, Wiley, 1946).

B. R. Ingalls, <u>Washington's Extended Use of State Plane Coordinates</u> (Olympia, Bureau of Surveys and Maps, 1957), 11pp.

R. C. Kao, "Geometric Projections of the Sphere and the Spheroid", The Canadian Geographer, v. 3. (Autumn 1961), pp. 12-21.

R. C. Kao, <u>Geometric Projections and Radar Data</u>, (Santa Monica, System Development Corp., 1959), 47 pp.

R. C. Kao, "The Use of Computers in the Processing and Analysis of Geographic Information", <u>The Geographical Review</u>, 53(1963). pp. 530-547.

W. C. Krumbein, "Trend Surface Analysis of Contour-type Maps with Irregular Control-Point Spacing," <u>Journal of Geophysical Research</u>, Vol. 64, 7 (July 1959), pp. 823-834.

W. D. Lambert, <u>Effect of Variations in the Assumed Figure of the</u> <u>Earth on the Mapping of a Large Area</u>, Coast and Geodetic Survey Special Publication No. 100, Serial No. 258 (Washington, Government Printing Office, 1924), 35pp.

W. D. Lambert, "The Distance between two Widely Separated Points on the Surface of the Earth", Journal, Washington Academy of Sciences, XXXII,5, (1942), pp. 125-130.

E. A. Lewis, "Parametric Formulas for Geodesic Curves and Distances on a Slightly Oblate Earth", Air Force Cambridge Research Laboratories, April 1963, 37 pp.

A. Libault, <u>Les Measures sur les Cartes et leur Incertitude</u>, Paris, 1961.

K. A. MacLachlan, "The Coordinate Method of O and D Analysis", Highway Research Board <u>Proceedings</u>, 29th Annual Meeting (Washington National Research Council, 1949) pp. 349-367.

F. J. Marschner, "Structural Properties of Medium and small scale maps", <u>Annals</u>, Association of American Geographer, XXXIV, 1, pp. 1-46.

F. J. Marschner, <u>Boundaries and Records</u>....(Washington, Farm Economics Research Division, Department of Agriculture, 1960), 73 pp.

H. C. Mitchell and Lansing G. Simmons, <u>The Plane Coordinate Systems</u>, Coast and Geodetic Survey Special Publication No. 235, (Washington, Government Printing Office, 1945) 62 pp.

F. Moser, "A Computer Oriented System in Stratigraphic Analysis", Ann Arbor, Institute of Technology, 1963.

D. Neft, "Statistical Analysis for Areal Distributions", Ph.D. Thesis, Columbia University, 1962, 286 pp.

S. Nordbeck, Location of Areal Data For Computer Processing, Lund Studies in Geography, Series C, 2, 1962, 41 pp.

J. O'Keefe "The New Military Grid of the Department of the Army", Surveying and Mapping VIII, 4 (1948), pp. 214-216. W. C. Krumbein, "Trend Surface Analysis of Contour-type Maps with Irregular Control-Point Spacing," <u>Journal of Geophysical Research</u>, Vol. 64, 7 (July 1959), pp. 823-834.

W. D. Lambert, <u>Effect of Variations in the Assumed Figure of the</u> <u>Earth on the Mapping of a Large Area</u>, Coast and Geodetic Survey Special Publication No. 100, Serial No. 258 (Washington, Government Printing Office, 1924), 35pp.

W. D. Lambert, "The Distance between two Widely Separated Points on the Surface of the Earth", Journal, Washington Academy of Sciences, XXXII,5, (1942), pp. 125-130.

E. A. Lewis, "Parametric Formulas for Geodesic Curves and Distances on a Slightly Oblate Earth", Air Force Cambridge Research Laboratories, April 1963, 37 pp.

A. Libault, <u>Les Measures sur les Cartes et leur Incertitude</u>, Paris, 1961.

K. A. MacLachlan, "The Coordinate Method of O and D Analysis", Highway Research Board <u>Proceedings</u>, 29th Annual Meeting (Washington National Research Council, 1949) pp. 349-367.

F. J. Marschner, "Structural Properties of Medium and small scale maps", <u>Annals</u>, Association of American Geographer, XXXIV, 1, pp. 1-46.

F. J. Marschner, <u>Boundaries and Records</u>....(Washington, Farm Economics Research Division, Department of Agriculture, 1960), 73 pp.

H. C. Mitchell and Lansing G. Simmons, <u>The Plane Coordinate Systems</u>, Coast and Geodetic Survey Special Publication No. 235, (Washington, Government Printing Office, 1945) 62 pp.

F. Moser, "A Computer Oriented System in Stratigraphic Analysis", Ann Arbor, Institute of Technology, 1963.

D. Neft, "Statistical Analysis for Areal Distributions", Ph.D. Thesis, Columbia University, 1962, 286 pp.

S. Nordbeck, Location of Areal Data For Computer Processing, Lund Studies in Geography, Series C, 2, 1962, 41 pp.

J. O'Keefe "The New Military Grid of the Department of the Army", Surveying and Mapping VIII, 4 (1948), pp. 214-216.

J. A. O'Keefe, "The Universal Transverse Mercator Grid and Projection", <u>The Professional Geographer</u>, N. S., IV, 5 (1952), pp. 19-24.

W. D. Pattison, <u>Beginnings of the American Rectangular Land</u> <u>Survey System</u>, 1784-1800, Research paper no. 50 (Chicago; Department of Geography, University of Chicago, 1957), 248 pp.

F. R. Pitts, "Committee on the Utilization of Stored Data Systems", <u>The Professional Geographer</u>, 16, 4 (July, 1964) pp. 41-44.

Radio Technical Comission for Aeronautics, "Coordinate System Aspects of Position Identification", Journal of the Institute of Navigation, Vol. 8, #1, Spring 1961, pp. 48-58.

W. F. Reynolds, <u>Relation Between Plane Rectangular Coordinates</u> and <u>Geographic Positions</u>, Coast & Geodetic Survey Special Publication #71, (Washington, G. P. P., 1936), 90 pp.

E. Schmid, <u>Transformation of Rectangular Space Coordinates</u>, U.S. Coast and Geodetic Survey Technical Bulletin No. 15 (Washington, Government Printing Office, 1961), 13 pp.

A. I. Shevanova, "On the Accuracy of Small-Scale Maps," Geodesy and Cartography, (OTS, JPRS, L-1389-D.). 1957, pp. 36-44.

L. G. Simmons, "How Accurate is First-Order Traingulation?", Coast and Geodetic Survey Journal, 3 (April, 1950), pp. 53-56.

B. W. Sitterly and J. A. Pierce, "Simple Computation of Distances over the Earth", <u>Journal</u>, Institute of Navigation, 1, 4 (Dec. 1946), pp. 62-67.

E. M. Sodano, "General Non-Iterative Solution of the Inverse and Direct Geodetic Problems" paper presented at 1963 IGU meeting. Berkeley, California.

State of Washington, <u>Laws of Washington</u>, Laws of 1945, Chapter 168, (S. B. 83), "Washington Coordinate System" (Olympis, State Printer, 1945) 2 pp.

P. Thompson, <u>Numerical Weather Analysis and Prediction</u>, MacMillan, New York, 1961, 170 pp.

W. R. Tobler, "A Comparison of Spherical and Ellipsoidal Measures", The Professional Geographer, XVI, 4 (1964), pp. 9-12.

W. R. Tobler, "A Polynomial Representation of Michigan Population," 1963 Papers, Michigan Academy of Science, Arts, and Letters, XLIX (1964), pp. 445-452. U.S. Air Force, <u>World Geographic Reference System</u> (GEOREF), Air Force Regulation No. 96-5, (Washington, Department of the Air Force, 1956), 7 pp.

U.S. Air Force, <u>Geodetic Distance and Azimuth Computations for</u> <u>Lines Under 500 Miles</u>, ACIC Technical Report No. 59 (St. Louis, <u>Aeronautical Chart and Information Center</u>, 1960), 77 pp.

U.S. Air Force, <u>Geodetic Distance and Azimuth Computations for</u> <u>Lines Over 500 Miles</u>, ACIC Technical Report No. 80 (St. Louis, <u>Aeronautical Chart and Information Center</u>, 1959), 83 pp.

U.S. Air Force, <u>Map Accuracy Evaluation</u>, Part I, ACIC Ref. Publication No. 2, 1962.

U.S. Army <u>The Positional Accuracy of Maps</u>, AMS Technical Report 35, 1961.

U.S. Army, <u>The Universal Grid Systems</u>, TM 5-241 (Washington, Government Printing Office, 1951), 324 pp.

U.S. Census Bureau, 'National Location Code Areas", Mimeographed, 1963.

C. A. Whitten, <u>Air-Line Distances between Cities in the United States</u>, Coast and Geodetic Survey Special Publication No. 238 (Washington, Government Printing Office, 1947), 246 pp.

J. R. Wray, "Photo Interpretation in Urban Area Analysis", in <u>Manual fo Photographic Interpretation</u> (Washington; American Society of Photogrammetry, 1960) pp. 667-716.

APPENDIX I

CONVERSION FROM THE PUBLIC LAND SURVEY SYSTEM TO LATITUDE AND LONGITUDE

The simplest conversion begins with a procedure which assumes that the Public Land Survey conforms to the exact specifications upon which it is based. The system, as is well known, does not conform to these specifications, for a number of reasons including measurement errors unavoidable in any empirical work and a certain laxity of supervision during the establishment of the system. For conversion into latitude and longitude the following notation is convenient:

- i is an index to indicate the initial point of the survey. It is necessary to distinguish at least 37 initial points in the Western United States.
- ϕ i is the latitude of the ith base parallel.



- is the equatorial radius of the ellipsoid taken to represent the earth. For the Clarke Ellipsoid of 1866, a=3963.2257 miles.
- is the eccentricity of the ellipsoid taken to represent the earth. For the Clarke Ellipsoid of 1866 e = 0.0822718542.

 M_i is the radius of the meridian at the ith initial point. M_i is given by 2.

$$M_{i} = \frac{a(1 - e^{2})}{(1 - e^{2} \sin^{2} \theta_{i})^{3/2}}$$

is the township number of the location in question, with north townships taken as positive and south townships taken as negative.

is the range number of the location in question, with east ranges taken as positive and west ranges taken as negative.

 S_n is the northing of the section in question, with the sign convention as above.

Se is the section easting, with the sign convention as above.

 Q_n is the quarter section northing, with signs as above.

Qe is the quarter section easting.

Ø is the latitude (to be found) of the location in question.

 λ_i

я

e

Т

R

is the radius of curvature perpendicular to the meridian at latitude \emptyset :

$$N_{\emptyset} = \frac{a}{(1 - e^2 \sin^2 \theta)^{1/2}}$$

 λ is the longitude (to be found) of the location in question.

The necessary equations are then:

$$\emptyset = \emptyset_i + \frac{6 T + 3 + S_n + Q_n}{M_i},$$

$$6 R + 3 + S + 0$$

$$\lambda = \lambda_{i} + \frac{1}{N_{o} \cos \emptyset}$$

The formulae are established by observing that the center of the . township in question should be six miles times the number of the township north (south) of the base parallel, minus three miles to obtain the center of the township. The section northing and easting give the distance of the center of the section from the center of the township, and the quarter-section northing and easting give the distance of the center of the quarter-section from the center of the section. For the SW 1/4, Sec. 25, T 5 N, R 17 E, one should have for example, that the center of the township is 27 miles (5 x 6 - 3) north of the initial point. S_n is -1.5 miles and Q_n is -0.25 miles. The total distance in the north-south direction from the initial point should therefore be + 25.25 miles. This distance must then be converted to the appropriate number of degrees and added to the latitude of the initial point. A further refinement, though hardly necessary, would be to iterate on the latitude obtained in the first step in order to adjust the meridional radius employed in the computation. Determination of the longitude is similar but slightly more difficult since the distances are measured along a parallel (a loxodrome, not a great circle or geodesic), whose radius varies with the latitude.

In programming the outlined procedure for a digital computer it is simplest to employ radians instead of degrees and to store a table of S_n , S_e , Q_n , Q_e , \emptyset_1 , and λ_1 . The computer can perform the assignment to the correct initial point by letter for letter examination of the name of the principal meridian. A convention is necessary to distinguish the two different initial points employed for the Fourth Principal Meridian. The method detailed assigns latitude and longitude (to about the nearest 1/4 mile) on the assumption that the Public Land Survey designations are where they should be. Of course they are not exactly there: the legal strategy is to assign to the actual locations a status of incontestable correctness, irrespective of any errors which may have been introduced

NØ

and

during the survey. To adjust the calculated values to conform to their legal positions requires detailed historical and empirical corrections, and can be quite tedious. For many research purposes, however, such a refinement may not be necessary. To obtain an order-of-magnitude estimate of the discrepancies, the actual latitude and longitude (as recorded on large scale topographic maps) of a scattered set of locations have been compared with the computed values. For a selection of 74 points within the State of Michigan the errors are as follows:

Distribution of Errors: (N = 74)

Mean: 2.849 miles

Standard deviation: 1.827 miles

Maximum: 9.339 miles

60% of the errors are less than 2 miles

93% of the errors are less than 5.5 miles

The directional errors appear evenly distributed in all directions. A random selection of points (N = 25) from other states indicates that the errors are quite comparable and of the same order of magnitude. A sample computation is as follows:

observed location:	Sw 1/4, Sec. 28, T	2 S, R 6 E,	Michigan Meridian
calculated Lat/Lon:	42° 16'07" N, 83°	44'0S" N	
observed Lat/Lon:	42 [°] 17'10" Ν, 83 [°]	44'49" W	
difference:	1'03"	41''	
difference in miles:	2.58		

direction of difference: 154.34° (E of N)

The method given above does not include an adjustment for the convergence of the meridians. Since the edges of the ranges run due north and south, the ranges become narrower as the meridians converge. To adjust for this, standard parallels are established every twenty-four miles north and south of the base parallel. The ranges are again made six miles wide at these standard parallels. The system thus is self correcting every twenty-four miles. The order of magnitude of the difference in width of ranges, separated by twenty-four miles in a north-south direction, can be established as follows: The radius of the parallel at 45° N latitude is 2807.178 miles. At a distance of 24 miles north of 45° N it is approximately 2789.834 miles. The east-west width of the northern edge of the range 24 miles north of the 45th parallel is therefore not six miles but 0.037104 miles (195.9 feet) less than six miles. On this basis the error at R 50 E, an extreme value, would be 1.86 miles. Another slight error is introduced by the topographic elevation, since the radii employed apply to a mean sea level ellipsoid.

Empirical corrections for Michigan would need to include the fact that the standard parallels are 60 (not 24) miles apart (in accord with the surveying instructions in force at the time), and that R l E is consistently too narrow from T l N to T 20 N. An adjustment for these, and other, systematic departures could be incorporated into the computer program. Conversion of the Section, Township, and Range information to latitude and longitude can be followed by conversion to map projection coordinates for map plotting or computational purposes. Direct conversion to Cartesian map coordinates also is possible but is less convenient for the entire Western United States. This is more appropriate for operations restricted to a limited area, e.g., one individual state.

APPENDIX II

1

MAP PROJECTION EQUATIONS

The following list gives the mathematical rules for the most common map projections of a <u>sphere</u>. The following notation is standard.

arphi Latitude of a point whose projection coordinates are desired.

 λ Longitude of a point whose projection coordinates are desired.

X Abscissa of a plane cartesian coordinate system.

 \vee Ordinate of a plane cartesian coordinate system.

r Radial distance of a plane polar coordinate system.

 θ Angular direction of a plane polar coordinate system.

 Ψ_{0} Latitude of the center of the map; either the point of "tangency", or a single standard parallel.

 ψ_1 Southerly standard parallel for projections having two standard parallels.

 ψ_{1} Northerly standard parallel for projections having two standard parallels.

 λ_o Longitude of the center of the map; either the point of "tangency", or the central meridian.

C The constant of the cone for conic projections.

 γ The radial distance from the origin to the image of the southerly standard parallel in plane polar coordinates.

All equations are giver for a sphere of unit radius (R = 1) and all values are assumed to be in radians. Conversion to scale can be achieved by multiplying all distances by the appropriate scale factor. North latitudes and east longitudes are taken to be positive, i.e.

$$-\frac{1}{2} \leq \varphi \leq + \frac{1}{2}$$

$$-\pi \leq \lambda \leq +\pi$$

The equations are given in their most commonly applied form. The conical projections, for example, are not given in their oblique cases.

(1) Albers' equal area conic projection with two standard parallels:

$$C = \frac{\sin \varphi_{1} + \sin \varphi_{2}}{2}$$

$$r = \left[\frac{4}{C^{2}}\left(\sin^{2}\left(\frac{\pi}{4} - \frac{\varphi_{1}}{2}\right)\sin^{2}\left(\frac{\pi}{4} - \frac{\varphi_{2}}{2}\right)\right) + \frac{4}{C}\sin^{2}\left(\frac{\pi}{4} - \frac{\varphi}{2}\right)\right]^{1/2}$$

$$\theta = C\left(\lambda - \lambda_{0}\right)$$

This puts the origin of the coordinates somewhat beyond the north pole, which is rather inconvenient. The origin can be shifted to the intersection of the southern standard parallel with the central meridian by using

$$X = r \sin \theta$$
$$Y = r_1 - r \cos \theta$$

(2) Azimuthal equidistant projection:

1

$$r = \arccos \left[\sin \varphi \sin \varphi_{0} + \cos \varphi \cos \varphi_{0} \cos (\lambda - \lambda_{0}) \right]$$
$$\theta = \arcsin \left[\frac{\cos \varphi \sin (\lambda - \lambda_{0})}{\sin r} \right]$$

The origin of the coordinates is at Ψ_{o} , λ_{o} (3) Bonne's Equal Area projection :

$$r = \varphi_{0} - \varphi + \tan\left(\frac{\pi}{2} - \varphi_{0}\right)$$
$$\theta = \frac{(\lambda - \lambda_{0})\sin\left(\frac{\pi}{2} - \varphi\right)}{r}$$

To place the origin at the intersection of the standard parallel and the central meridian use:

- $r_{1} = \tan\left(\frac{1}{2} \varphi_{0}\right)$ $X = r \sin \theta$ $Y = r_{1} r \cos \theta$
- (4) Cassini Projection

$$X = \operatorname{arc\,sin}\left[\operatorname{cos}\varphi\,\operatorname{sm}\left(\lambda - \lambda_{o}\right)\right]$$
$$Y = -\varphi_{o} + \operatorname{arc\,tan}\left[\frac{\tan\varphi}{\cos\left(\lambda - \lambda_{o}\right)}\right]$$

(5) Gnomonic Projection:

$$X = \frac{\cos \varphi \sin (\lambda - \lambda_o)}{\sin \varphi \sin \varphi_o + \cos \varphi \cos \varphi_o \cos (\lambda - \lambda_o)}$$
$$Y = \frac{\sin \varphi \cos \varphi_o - \sin \varphi_o \cos \varphi \cos (\lambda - \lambda_o)}{\sin \varphi \sin \varphi_o + \cos \varphi \cos \varphi_o \cos (\lambda - \lambda_o)}$$

$$C = \operatorname{arc} \operatorname{cos} \left[\operatorname{sin} \varphi \, \operatorname{sin} \, \varphi_{o} + \operatorname{cos} \varphi \, \operatorname{cos} \, \varphi_{o} \, \operatorname{cos} \, (\lambda - \lambda_{o}) \right]$$

$$r = 2 \, \operatorname{sin} \left(\frac{C}{2} \right)^{2}$$

$$\Theta = \operatorname{krc} \, \operatorname{sin} \left[\frac{\operatorname{cos} \, \varphi \, \operatorname{sin} \, (\lambda - \lambda_{o})}{\operatorname{sin} \, C} \right]$$

(7) Lambert's cylindrical equal area projection:

 $X = \lambda - \lambda_o$

 $\gamma = \sin \varphi$

Or, with a standard parallel:

$$x = (\lambda - \lambda_o) \cos \varphi_o$$

 $y = \sin \varphi$

(8) Lambert's conformal conic with two standard parallels:

$$C = \frac{h\cos \varphi_{1} - Ln\cos \varphi_{2}}{Ln \tan \left(\frac{\pi}{4} - \frac{\varphi_{1}}{2}\right) - Ln \tan \left(\frac{\pi}{4} - \frac{\varphi_{2}}{2}\right)}$$

$$C_{1} = \frac{\cos \varphi_{1}}{C \tan^{C} \left(\frac{\pi}{4} - \frac{\varphi_{1}}{2}\right)}$$

$$r = C_{1} \tan^{C} \left(\frac{\pi}{4} - \frac{\varphi}{2}\right)$$

$$\theta = C \left(\lambda - \lambda_{0}\right)$$

 $X = Y \sin \theta$

(9) Mercator's conformal cylindrical projection:

$$X = \lambda - \lambda_0$$

$$Y = L_n + a_n \left(\frac{\pi}{4} + \frac{\psi}{2} \right)$$

(10) Miller's Cylindrical projection:

1

$$X = \lambda - \lambda_{0}$$

$$Y = 1.25 \text{ Ln } \tan\left(\frac{\pi}{4} + \frac{2}{5}\varphi\right)$$

(11) Mollweide's equal area elliptical projection:

Define chi by $2 \psi + 2 \sin \psi = \pi \sin \psi$, then $X = 2\sqrt{2} (\lambda - \lambda_0) \cos \psi$ $\gamma = \sqrt{2} \sin \psi$

(12) Orthographic projection:

$$X = \sin \varphi \cos \varphi_{o} - \cos \varphi \sin \varphi_{o} \cos (\lambda - \lambda_{o})$$
$$Y = \cos \varphi \sin (\lambda - \lambda_{o})$$

(13) Polyconic projection (American polyconic):

$$r = ctq \varphi$$

$$\theta = (\lambda - \lambda_{o}) sin \varphi$$

$$x = r sin \theta$$

$$y = r + \varphi - r cos \theta$$

Which puts the origin at the equator.

(14) Sinusoidal equal area projection:

 $X = (\lambda - \lambda_o) \cos \varphi$ $Y = \varphi$

(15) Square projection:

3

$$\begin{aligned} \mathbf{x} &= \mathbf{\lambda} - \mathbf{\lambda}_{\mathbf{e}} \\ \mathbf{y} &= \mathbf{\Psi} \end{aligned}$$

or, with a standard parallel (also known as the rectangular projection):

$$X = (\lambda - \lambda_o) \cos \varphi_o$$
$$Y = \Psi$$

(16) Stereographic projection:

$$X = \frac{\cos \varphi \sin (\lambda - \lambda_o)}{1 + \sin \varphi \sin \varphi + \cos \varphi \cos \varphi \cos (\lambda - \lambda_o)}$$

$$Y = \frac{\sin \varphi \cos \varphi_{o} - \sin \varphi_{o} \cos \varphi \cos (\lambda - \lambda_{o})}{1 + \sin \varphi \sin \varphi_{o} + \cos \varphi \cos \varphi_{o} \cos (\lambda - \lambda_{o})}$$

(17) Transverse Mercator projection.

$$X = \frac{1}{2} Ln \left[\frac{1 + \cos \varphi \sin (\lambda - \lambda_o)}{1 - \cos \varphi \sin (\lambda - \lambda_o)} \right]$$
$$Y = \operatorname{arc} \tan \left[\tan \varphi \sec (\lambda - \lambda_o) \right]$$

APPENDIX III

LEAST SQUARES CONVERSION FROM ONE SYSTEM OF RECTANGULAR COORDINATES TO ANOTHER

Given two sets of coordinates on the same map, with a minimum of five points identified in both systems of coordinates, it is possible to convert the coordinates of one set to the other by a two-dimensional version of a least-squares "line". The procedure is most easily effected using complex numbers.

Let x,y be one set of coordinates and u,v be the other set, and let $W_j = x + iy$ and $Z_j = u + iv$, where $i^2 = -1$, be the complex numbers representing the ith point. The objective is then to find the complex constants $A = a_1 + ia_2$ and $B = b_1 + ib_2$ in the equation $\hat{W} = A + BZ$ such that the squared residual

$$\sum_{j=1}^{N} \left| \hat{w}_{j} - w_{j} \right|^{2}$$

is a minimum. The normal equations are readily obtained by differentiation. The equation can be rewritten as a pair of transformation equations by separating the real and imaginary parts, viz: Re $(\hat{W}) = \hat{x} = a_1 + b_1 u + b_2 \vee$ Im $(\hat{W}) = \hat{y} = a_2 + b_2 u - b_1 \vee$

where \hat{x} and \hat{y} are the estimates of the x,y coordinates as obtained from the known u,v coordinates. The standard error, etc., of the estimate can be obtained in a manner analogous to that employed for ordinary least squares procedures. A similar, but considerably more complicated, procedure must be employed if the two sets of coordinates do not come from the same map, or if the relation to latitude and longitude is to be estimated, or if an attempt is made to determine the map projection of an arbitrary map.

APPENDIX IV

R CLARKE ELLIPSOID OF 1866 R DISTANCE AND DIRECTION / SODANO METHOD R W. R. TOBLER / UNIVERSITY OF MICHIGAN / GEOGRAPHY SCOMPILE MAD, PUNCH OBJECT EXTERNAL FUNCTION (LT1.LG1.LT2.LG2.DIS.DIRD) R ENTRY IN RADIANS R RETURNS DISTANCE IN KILOMETERS R RETURNS DIRECTION IN DECIMAL DEGREES R ACIC TR 80, PAGES 41-47. R NECESSARY CONSTANTS VECTOR VALUES PI=314159265E-8 VECTOR VALUES TPI=628318531E-8 VECTOR VALUES ARAD=63782064E-4 VECTOR VALUES BRAD=63565838E-4 VECTOR VALUES BOVRA=9966099247E-10 VECTOR VALUES VK1=2356218428E-7 VECTOR VALUES VK2=6956258069E-5 VECTOR VALUES VK3=4986428206E-9 VECTOR VALUES VK4=-4010886986E-10 VECTOR VALUES VK5=-7994556507E-10 VECTOR VALUES VK6=3986428206E-9 VECTOR VALUES E1=17036962E-10 VECTOR VALUES E2=21769E-10 VECTOR VALUES E3=29026E-10 VECTOR VALUES E4=3628E-10 VECTOR VALUES RAD=174532925E-10 R BEGIN COMPUTATION ENTRY TO CLARKE. INDEX=1. TANB1=BOVRA*(SIN.(LT1)/COS.(LT1)) TANB2=BOVRA*(SIN.(LT2)/COS.(LT2)) COSB1=1./SQRT.(1.+(TANB1*TANB1)) COSB2=1./SQRT.(1.+(TANB2*TANB2)) SINB1=TANB1*COSB1 SINB2=TANB2*COSB2 C1=SINB1*SINB2 D1=COSB1*COSB2 DIFLON=LG2-LG1 WHENEVER DIFLON.L.O., INDEX=-1. DIFLON= . ABS . DIFLON CDIF=COS . (DIFLON) CDIS=C1+D1*CDIF SDIS=SQRT.(1.-CDIS*CDIS) CA=D1*SIN. (DIFLON)/SDIS CB=CA*CA CC=CDIS*(1.-CB)/VK3 CD=VK4*C1 CE=VK5*C1 CF=VK6*CC CG1=2.*ATAN.(SQRT.((1.-CDIS)/(1.+CDIS))) CG=CG1/SDIS CX=CA*((CG1*(VK1+CB)+SDIS*(CC+CD)+CG*(CE+CF))/VK2) DELTAL=CX+DIFLON SDELTL=SIN. (DELTAL) CDELTL=COS.(DELTAL) DEN=TANB2*COSB1-SINB1*CDELTL

```
DIR=ATN1.(SDELTL.DEN)
WHENEVER DIR.G.PI.DIR=DIR-TPI
DIRD=DIR/RAD
DIRD=DIRD#INDEX
CPHO=C1+D1*CDELTL
SPHO=SQRT.(1.-CPHO*CPHO)
CBO=D1*SDELTL/SPHO
APHO=2.*ATAN.(SQRT.((1.-CPHO)/(1.+CPHO)))
SB02=1.-CB0*CB0
C2DEL=(2.*C1/SBO2)-CPHO
C4DEL=(2.*C2DEL*C2DEL)-1.
SB04=SB02*SB02
S2PHO=SIN. (2. *APHO)
A0=1.+E1*SB02-E2*SB04
B0=E1*SB02-E3*SB04
C0=E4*SB04
DIS=BRAD*(AO*APHO+BO*SPHO*C2DEL-CO*S2PHO*C4DEL)
FUNCTION RETURN
END OF FUNCTION
```

2

APPENDIX V

R CONVERSION OF PUBLIC LAND SURVEY INFORMATION R INTO LATITUDE AND LONGITUDE R SUBROUTINES NEEDED ARE DEGRAD, RADEG, SPHERE, AVERAD R W. R. TOBLER /UNIVERSITY OF MICHIGAN / GEOGRAPHY TRC \$COMPILE MAD, PRINT OBJECT, PUNCH OBJECT, EXECUTE INTEGER MER + C1 + C2 + C3 + C4 + C5 INTEGER COMPAR .N . TWP . RNG .Q1, Q2, S . PRINC .N1 INTEGER R.S.T D'N SECE(37), SECN(37), PMERID(36), BLINE(36), RMER(36) V'S DLT(1)=43.0,43.0,35.0,31.0,36.0,61.0,64.0,34.0,40.0,40.0, 1 42.0,33.0,40.0,34.0,34.0,31.0,42.0,37.0,35.0,34.0,45.0,40.0, 2 34.0,38.0,60.0,40.0,30.0,30.0,30.0,38.0,40.0,39.0,30.0,45.0, 3 43.0 V'S MLT(1) = 59.0,22.0,1.0,52.0,30.0,49.0,51.0,38.0,59.0,0.0. 1 30.0,22.0,25.0,59.0,29.0,0.0,25.0,52.0,44.0,15.0,47.0,46.0, 2 7.0,28.0,7.0,0.0,59.0,59.0,26.0,28.0,25.0,6.0,59.0,31.0,0.0 1 27.0,38.0,2.0,27.0,32.0,31.0,28.0,54.0,56.0,35.0,13.0,11.0, 2 20.0,14.0,36.0,7.0,56.0,51.0,3.0,27.0,59.0,23.0,56.0,11.0, 3 41.0 $V^{1}S$ DLG(1)=104.0,116.0,89.0,90.0,103.0,145.0,147.0,91.0,84.0, 1 90.0,90.0,112.0,124.0,86.0,97.0,92.0,84.0,121.0,108.0,106.0, 2 111.0,111.0,116.0,86.0,149.0,97.0,91.0,88.0,84.0,89.0,109.0, 3 108.0,91.0,122.0,108.0 V'S MLG(1)=3.0,23.0,14.0,14.0,0.0,18.0,38.0,3.0,48.0,27.0, 1 25.0,18.0,7.0,34.0,14.0,24.0,21.0,54.0,31.0,53.0,39.0,53.0, 2 55.0,27.0,21.0,22.0,9.0,1.0,16.0,8.0,56.0,31.0,9.0,44.0,48.0 V'S SLG(1)=16.0,35.0,47.0,41.0,7.0,13.0,26.0,7.0,11.0,11.0, 1 37.0,19.0,10.0,16.0,49.0,55.0,53.0,47.0,59.0,12.0,33.0,27.0, 2 17.0,21.0,24.0,8.0,36.0,20.0,38.0,54.0,6.0,59.0,36.0,34.0, 3 49.0 SECE(0) = 0.0V'S SECE(1)=2.5,1.5,0.5,-0.5,-1.5,-2.5,-2.5,-1.5,-C.5,0.5, 11.5,2.5,2.5,1.5,0.5,-0.5,-1.5,-2.5,-2.5,-1.5,-0.5,0.5,1.5, 22.5,2.5,1.5,0.5,-0.5,-1.5,-2.5,-2.5,-1.5,-0.5,0.5,1.5,2.5 SECN(0)=0.0 V'S SECN(1)=2.5,2.5,2.5,2.5,2.5,2.5,1.5,1.5,1.5,1.5,1.5,1.5,1.5,1.5, 2-1 • 5 • -1 • 5 • -1 • 5 • -1 • 5 • -2 • 5 • -2 • 5 • -2 • 5 • -2 • 5 • -2 • 5 • -2 • 5 • -2 • 5 • -2 • 5 R1=63782064E-04 MILE=0.62136994 ESQR=6768658F-09 RAD=174532925E-10 T'H INITAL, FOR I=1,1,1.G.35 DLG(I) = -DLG(I)EXECUTE DEGRAD.(DLT(I),MLT(I),SLT(I),BLINE(I)) EXECUTE DEGRAD.(CLG(I),MLG(I),SLG(I),PMERID(I)) SMLT=SIN.(BLINE(I)) DUM=SQRT . (1 .- ESQR*SMLT*SMLT) DUMCUB=DUM.P.3 DUMMY=(1.-ESQR)*R1 RMER(I)=DUMMY*MILE/DUMCUB INITAL CONTINUE RIT CONS, COMPAR V'S CONS=\$53,11*\$ N = 0

START

```
N1=0
 PIT SKIP
 VIS SKIP=$1H1*$
 WIR COMPAR.GE.1
 R'T LATLON, Q1, Q2, S, T, TWP, R, RNG, C1, C2, C3, C4, C5,
1DLAT,MLAT,SLAT,DLON,MLON,SLON
V'SLATLON=$2C1,510,12,53,12,C1,53,12,C1,52,5C1,516,F3.0,
12F2.0,51,F4.0,2F2.0*$
 EXECUTE DEGRAD. (DLAT.MLAT.SLAT.RLAT)
 EXECUTE DEGRAD. (DLON, MLON, SLON, RLON)
 O'E
 R'T INDAT,Q1,Q2,S,T,TWP,R,RNG,C1,C2,C3,C4,C5
 V'SINDAT =$2C1,510,12,53,12,C1,53,12,C1,52,5C1 *$
 E'L
 N=N+1
 N1 = N1 + 1
 WIR TWP.E.SNS
 A=T*6.0-3.0
 O'R TWP.E.$S$
 A=-(T*6.0-3.0)
 0 • E
 TIO ERR
 E .L
 WIR RNG.E.SES
 B=R*6.0-3.0
 O'R RNG.E.SWS
 B=-R*6.0+3.0
 0 . E
 TIO ERR
 E+L
 WIR Q1.E.SNS
 QN=0.25
 0'R Q1.E.$5$
 QN=-0.25
 0'R Q1.E.$ $
 QN=0.0
 0 . E
 TIO ERR
 E .L
 WIR Q2.E.SES
 QE=0.25
  0 R 02.E.$W$
 QE=-0.25
  0'R Q2.E.$ $
  QE=0.0
  O'E
  TIO ERR
  EIL
  W'R C1.E.$8$
    W'R C2.E.$0$
      MER=2
    O'E
      MER=1
    E'L
  0'R C1.E.$C$
    W R C2.E.$I$
      MER=5
  0'R C2.E.$0$
    MER=6
```

.

#

\$

O'E WIR C3.E.SIS MER=3 0'E MER=4 E'L E'L 0'R C1.E.\$F\$ MER=7 0'R C1.E.\$5\$ MER=8 0'R C1.E.\$1\$ MER=9 0'R C1.E.\$4\$ WIR (C4.E.\$A\$).OR.(C5.E.\$A\$) MER=10 01E MER=11 EIL O'R C1.E.SGS MER=12 O'R C1.E.SHS W'R C3.E. \$M\$ MER=13 O'E MER=14 E'L O'R C1.E.SIS MER=15 O'R C1.E.\$L\$ MER=16 O'R C1.E.SMS WIR C2.E.SIS MER = 170'E MER = 18E'L O'R C1.E.\$N\$ W'R C2.E.SAS MER=19 0'E MER=20 E'L O'R C1.E.SPS MER=21 0'R C1.E.\$S\$ W'R C3.E.\$L\$ MER=22 0'R C3.E. \$N\$ MER=23 O'R C3.E.SWS MER = 25O'R(C3.E.\$H\$).OR.(C4.E.\$H\$).OR.(C5.E.\$H\$) MER=27 O'E MER=28 E+L 0'R C1.E.\$2\$ MER=24

-18

.

```
O'R C1.E.$6$
    MER = 26
O'R CI.E.STS
  MER=29
0'R C1.E.$U$
  WIR C2.E.SIS
    MER=31
  O'E
    MER = 32
  E'L
O'R CI.E.SWS
  WIR C3.E.SNS
    MER=35
  O'E
    MER=34
  W R C2 . E. $A$ . MER=33
  E'L
O'R C1.E.$3$
  MER=30
O'E
  T'O ERR
EIL.
A=A+SECN(S)+QN
A=A/RMER(MER)
LATIT=BLINE(MER)+A
CLAT=COS . (LATIT)
SMLT=SIN.(LATIT)
DUM=SQRT . (1.-ESQR*SMLT*SMLT)
RPAR=R1*MILE*CLAT/DUM
B=(B+SECE(S)+QE)/RPAR
LONGIT=PMERID(MER)+B
EXECUTE RADEG. (LATIT, LTD, LTM, LTS)
 EXECUTE RADEG.(LONGIT, LGD, LGM, LGS)
PIT ONE + N1
V'S ONE=$1H ////S1,14*$
P:TRI,Q1,Q2,S,T,TWP,R,RNG,C1,C2,C3,C4,C5,
1LTD, LTM, LTS, LGD, LGM, LGS
V'SRI=$1H ,2C1,10H 1/4, SEC ,12,3H, T,12,C1,3H, R,12,C1,
12H, ,S2,5C1,10H. MERIDIAN //S1,2(F5.0,F3.0,F3.0,S5),
219HCALCULATED LAT/LONG
                          *5
 WIR COMPAR.GE.1
DIFLON=LONGIT-RLON
DIFLAT=LATIT-RLAT
 EXECUTE RADEG. (DIFLAT, DLTD, DLTM, DLTS)
 EXECUTE RADEG. (DIFLON, DLGD, DLGM, DLGS)
 EXECUTE SPHERE. (RLAT, RLON, LATIT, LONGIT, RHO, ALPHA)
 EXECUTE AVERAD. (RLAT, LATIT, R1, ESQR, MRAD )
 RHO=RHO*MRAD
 ALPHA=ALPHA/RAD
 P'TR2, DLAT, MLAT, SLAT, DLON, MLON, SLON, DLTD, DLTM, DLTS, DLGD,
1DLGM, DLGS, RHO, ALPHA
 V'S R2=$1H ,2(F5.0,F3.0,F3.0,S5),17HOBSERVED LAT/LONG /51,2(F
15.0,F3.0,F3.0,S5),10HDIFFERENCE /S1,F11.4,S6,F9.4,S6,
222HMILES AND DIRECTION
                               ¥£
 PUNCH FORMAT OUT, N1, RHO, ALPHA
 V'SOUT=$15,S2,F11.4,S2,F9.4*$
 E'L
 TRANSFER TO START
 PRINT FORMAT ONE .N
```

3

ERR

-

PRINT COMMENTS THIS OBSERVATION IS INCORRECTLY RECORDEDS N1=N1-1 TRANSFER TO START E'M

AVERAD

\$COMPILEMAD,PUNCHOBJECT EXTERNAL FUNCTION (LLT,ULT,R1,ESQR,R3) R MEAN RADIUS ON ELLIPSOID R LATITUDES IN RADIANS ENTRY TO AVERAD. SMLT=SIN.((LLT+ULT)/2.) DUM=SQRT.(1.-ESQR*SMLT*SMLT) DUMCUB=DUM*DUM*DUM DUMMY=(1.-ESQR)*R1 RMER=DUMMY/DUMCUB RPAR=R1/DUM R3=SQRT.(RMER*RPAR) FUNCTION RETURN END OF FUNCTION

DEGRAD

\$COMPILEMAD,PUNCHOBJECT EXTERNAL FUNCTION (DEG,MIN,SEC,RAD) R SUBROUTINE TO CONVERT DEGREES TO RADIANS ENTRY TO DEGRAD. VECTOR VALUES RADIAN=174532925E-10 SIGN=RADIAN WHENEVER DEG.L.O., SIGN=-RADIAN RAD=SIGN*(.ABS.(DEG)+(MIN/60.)+(SEC/3600.)) FUNCTION RETURN END OF FUNCTION

1

9

RADEG

\$COMPILEMAD, PUNCHOBJECT EXTERNAL FUNCTION (RAD, DEG, MIN, SEC) R CONVERTS RADIANS TO DEGREES, MINUTES, AND DECIMAL SECONDS INTEGER I ENTRY TO RADEG. VECTOR VALUES CONS=206264806E-3 SEC= ABS (RAD) *CONS I=SEC/3600. REMAIN=SEC-(1*3600.) DEG=I*1. I=REMAIN/60. MIN=I*1. SEC=REMAIN-(I*60.) WHENEVER RAD.L.O., DEG =-DEG FUNCTION RETURN END OF FUNCTION

\$COMPILE MAD, PRINT OBJECT, PUNCH OBJECT R COMPUTES OBLIQUE SPHERICAL COORDINATES EXTERNAL FUNCTION(NLT, NLG, LAT, LON, RHO2, GA) VECTORVALUESPI=314159265E-8 VECTORVALUESTPI=628318531E-8 VECTORVALUESPIOVR2=157079633E-8 VECTORVALUESPS=0.0000001 VECTORVALUESEPS=0.0000001 SPHERE

ENTRY TO SPHERE. WHENEVERNLT.E.(90.*RAD) GA=LON-NLG RH02=PIOVR2-LAT OTHERWISE WHENEVER (LT.NE.NLT) . OR. (LG.NE.NLG) PI=314159265E-8 TPI=2.#PI PIOVR2=PI/2. EPS=0.0000001 CNLT=COS . (NLT) SNLT=SIN.(NLT) END OF CONDITIONAL WHENEVER LON.NE.LON1 DIF=LON-NLG CDIF=COS (DIF) SDIF=SIN.(DIF) END OF CONDITIONAL CLT=COS.(LAT) SLT=SIN. (LAT) Q=SLT*SNLT+CLT*CNLT*CDIF WHENEVER Q.GE.1. RH02=0. ORWHENEVER Q.LE .- 1. RHO2=PI OTHERWISE RH02=ARCCOS.(Q) END OF CONDITIONAL NUM=CLT*SDIF DEN=CNLT*SLT-SNLT*CLT*CDIF WHENEVER . ABS . DEN . L . EPS WHENEVER . ABS . NUM . L . EPS GA=0. OTHERWISE GA=PIOVR2 WHENEVER NUM.L.O.,GA=-GA END OF CONDITIONAL ORWHENEVER . ABS . NUM . L . EPS -GA=0. WHENEVER DEN.L.O., GA=PI OTHERWISE GA=ATN1. (NUM, DEN) WHENEVER GA.G.PI, GA=GA-TPI END OF CONDITIONAL LON1=LON LT=NLT LG=NLG END OF CONDITIONAL FUNCTION RETURN END OF FUNCTION

NW 1/4 SEC 04 T05S RO7W MICHIGAN

-

.

*

8

+420405 -0850800 UNION CITY MI

#

DISTRIBUTION LIST

(One copy unless otherwise noted)

Chief of Naval Research Office of Naval Research Washington 25, D.C. Attn: Geography Branch

Defense Documentation Center Cameron Station Alexandria, Virginia 22314

Director Naval Research Laboratory Washington 25, D.C. Attn: Tech. Info. Officer

Director Central Intelligence Agency Washington 25, D.C. Attn: Map Division

Commanding Officer Office of Naval Research Branch Office 230 N. Michigan Avenue Chicago, Illinois 60601

Commanding Officer Office of Naval Research Navy No. 100 Fleet Post Office New York, New York

The Oceanographer U. S. Navy Oceanographic Office Washington 25, D.C.

Commanding Officer U. S. Naval Photo Interpretation Centre 4301 Suitland Road Washington 25, D.C.

Geography Division Bureau of the Census Washington 25, D.C.

- 2 Commanding Officer Army Map Service 6500 Brooks Lane Washington 25, D.C.
 - Dr. Reid A. Bryson Department of Meteorology University of Wisconsin Madison 6, Wisconsin
 - Mr. Robert Leland Cornell Aeronautical Laboratory P. O. Box 235 Buffalo 21, New York
- 2

20

6

Dr. Richard J. Russell Coastal Studies Institute Louisiana State University Baton Rouge 3, Louisiana

Dr. Charles B. Hitchcock American Geographical Society Broadway at 156th Street New York 32, New York

Dr. Edward B. Espenshade Department of Geography Northwestern University Evanston, Illinois

Dr. Brian J. L. Berry Department of Geography University of Chicago Chicago 37, Illinois

Dr. William L. Garrison Department of Geography Northwestern University Evanston, Illinois

Dr. William C. Krumbein Department of Geology Northwestern University Evanston, Illinois

DISTRIBUTION LIST (Concluded)

Dr. Ruth M. Davis Office of Director of Defense Research and Engineering Department of Defense Washington 25, D.C.

Dr. Leslie Curry Department of Geography Arizona State College Tempe, Arizona

Dr. M. Gordon Wolman Department of Geography Johns Hopkins University Baltimore 18, Maryland

Dr. Richard C. Kao Economics Department The RAND Corporation 1700 Main Street Santa Monica, California

U. S. Navy Oceanographic Office Washington 25, D.C. Attn: Code 5005

Professor J. Ross Mackay Department of Geography University of British Columbia Vancouver, British Columbia, Canada

Professor William Bunge Department of Geography Wayne State University Detroit, Michigan

Dr. Allen V. Hershey, Head Mathematical Physics Branch Computation and Analysis Laboratory U. S. Naval Weapons Laboratory Dahlgren, Virginia Professor John D. Nystuen Department of Geography The University of Michigan Ann Arbor, Michigan

Professor M. F. Dacey Department of Regional Science University of Pennsylvania Philadelphia 4, Pennsylvania

Professor Edwin Thomas Department of Geography Arizona State College Tempe, Arizona

Professor Forrest R. Pitts Department of Geography University of Oregon Eugene, Oregon

Professor Edwin Taaffe Department of Geography The Ohio State University Columbus 10, Ohio

Dr. Lewis T. Reinwald 10002 Cedar Lane Kensington, Maryland

Dr. Duane F. Marble Department of Geography Northwestern University Evanston, Illinois

Dr. John C. Sherman Department of Geography University of Washington Seattle 5, Washington

DOC	UMENT CONTROL DATA - RAD			
(Security classification of title, body of abet	rect and indexing ennotation must be entered whe	n the overell report is cleasified)		
1. ORIGINATING ACTIVITY (Corporate author)	20. REP	ORT SECURITY CLASSIFICATION		
The University of Michigan	Un	Unclassified		
Ann Arbor, Michigan	2 5 GRC	OUP		
. REPORT TITLE				
GEOGRAPHICAL COORDINATE COMPU	TATIONS			
PART I: GENERAL CONSIDERATIC	NS			
4. DESCRIPTIVE NOTES (Type of report and inclus	ive dates)			
Technical Report No. 2				
5. AUTHOR(S) (Lest name, first name, initial)				
Tobler. W. B.				
1001019 # 10				
REPORT DATE	74. TOTAL NO. OF PAGES	Th NO OF PEEL		
December 1964	45	65		
BE. CONTRACT OR GRANT NO.	94. ORIGINATOR'S REPORT NU	JMBER(S)		
Nonr 1224(48)	05824-2-T			
b. PROJECT NO.				
- Task No. 380-137				
. Idsk No. 909-197	96. OTHER REPORT NO(3) (Ar this report)	ny other numbers that may be assigne		
d.				
Qualified requesters may obt	ain copies of this report fro	DDC.		
Qualified requesters may obt	ain copies of this report fro 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch	DDC. TIVITY esearch		
Qualified requesters may obt	ain copies of this report fro 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C.	DDC. TIVITY esearch		
Qualified requesters may obt	ain copies of this report fro 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C.	om DDC. TIVITY esearch		
Qualified requesters may obt U. SUPPLEMENTARY NOTES 3. ABSTRACT Part I provides a discus	ain copies of this report fro 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coo	om DDC. TIVITY esearch ordinate models		
Qualified requesters may obt SU SUPPLEMENTARY NOTES 33. ABSTRACT Part I provides a discus for studies of geographically	ain copies of this report from 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with construction	om DDC. TIVITY esearch ordinate models comments on		
Qualified requesters may obt U. SUPPLEMENTARY NOTES 3. ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems a:	ain copies of this report from 12 SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with or nd their relevance for the an	om DDC. TIVITY esearch ordinate models comments on malysis and in-		
Qualified requesters may obt U. SUPPLEMENTARY NOTES B3. ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in:	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with cond nd their relevance for the and formation. Appendices include	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for		
Qualified requesters may obt U. SUPPLEMENTARY NOTES B. ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in: conversion from the Public La:	ain copies of this report fro 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coo distributed phenomena with con nd their relevance for the an formation. Appendices include nd Survey system into latitude	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude		
Qualified requesters may obt SUPPLEMENTARY NOTES B. ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in: conversion from the Public La: and to rectangular map projec	ain copies of this report from 12 SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordinates of coordinates include and their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coordinates.	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map		
Qualified requesters may obt SU SUPPLEMENTARY NOTES BARSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in: conversion from the Public La: and to rectangular map projec projections in greater detail	ain copies of this report from 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordinates of the and distributed phenomena with or nd their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coordinates of the	om DDC. TIVITY essearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in: conversion from the Public La: and to rectangular map projec: projections in greater detail by the substitution of map pro-	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordinates of the and their relevance for the and formation. Appendices included ind Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for spheric	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates.		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems and ventorying of geographical into conversion from the Public Land and to rectangular map projections in greater detail by the substitution of map pro- Statistical computations of f	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coor distributed phenomena with of nd their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coor , including estimates of the ojection coordinates for sphe- inite distortion are related	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In-		
Qualified requesters may obt SUPPLEMENTARY NOTES CARSTRACT Part I provides a discus for studies of geographically specific coordinate systems and ventorying of geographical into conversion from the Public Land and to rectangular map projections projections in greater detail by the substitution of map pro- Statistical computations of f dicatrix as a general contributed	ain copies of this report from 12. SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordinates of the and their relevance for the and formation. Appendices include ind Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for sphe- inite distortion are related ution to the analysis of map	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES CARSTRACT Part I provides a discus for studies of geographically specific coordinate systems a: ventorying of geographical in: conversion from the Public La: and to rectangular map projec projections in greater detail by the substitution of map pro- Statistical computations of f dicatrix as a general contribution	ain copies of this report from 12. SPONSORING MILITARY AC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coord distributed phenomena with or nd their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for sphe- inite distortion are related ution to the analysis of map	om DDC. TIVITY essearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems at ventorying of geographical int conversion from the Public Lat and to rectangular map project projections in greater detail by the substitution of map pro- Statistical computations of f dicatrix as a general contribut	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordinates of the and distributed phenomena with condition to the analysis of the oformation. Appendices included tion coordinates. Part II coordinates of the ojection coordinates for spheric inite distortion are related ution to the analysis of map	om DDC. TIVITY esearch ordinate models comments on halysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems at ventorying of geographical int conversion from the Public Lat and to rectangular map projections in greater detail by the substitution of map pri- Statistical computations of f dicatrix as a general contribution	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with of and their relevance for the and formation. Appendices included and Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for sphe- inite distortion are related ution to the analysis of map	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES CABSTRACT Part I provides a discus for studies of geographically specific coordinate systems as ventorying of geographical in conversion from the Public Las and to rectangular map projec projections in greater detail by the substitution of map pr Statistical computations of f dicatrix as a general contribu	ain copies of this report from 12. SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordination of the usefulness of coordination of the analysis of the analysis of the analysis of the analysis of map	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems at ventorying of geographical int conversion from the Public Lat and to rectangular map projec projections in greater detail by the substitution of map pre- Statistical computations of f dicatrix as a general contribution	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordination of the usefulness of coordination of the usefulness of coordination. Appendices include and their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for spheric inite distortion are related ution to the analysis of map	om DDC. TIVITY essearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt SUPPLEMENTARY NOTES ABSTRACT Part I provides a discus for studies of geographically specific coordinate systems at ventorying of geographical int conversion from the Public Lat and to rectangular map project projections in greater detail by the substitution of map pr Statistical computations of f dicatrix as a general contribut	ain copies of this report from 12 SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with of and their relevance for the and formation. Appendices include and Survey system into latitude tion coordinates. Part II coordinates of the ojection coordinates for sphe- inite distortion are related ution to the analysis of map	om DDC. TIVITY essearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		
Qualified requesters may obt	ain copies of this report from 12. SPONSORING MILITARY ACC Office of Naval Re Geography Branch Washington, D. C. sion of the usefulness of coordistributed phenomena with condistributed phenomena with condition to the analysis of the analysis of the ojection coordinates for spherinite distortion are related ution to the analysis of map	om DDC. TIVITY esearch ordinate models comments on malysis and in- de equations for de and longitude onsiders map errors introduced erical coordinates. to Tissot's In- projections.		

X

Security Classification

Unclassified Security Classification

14-	KEY WORDS	LIN	LINKA		LINK B		LINKC	
		ROLE	WT	ROLE	WT	ROLE	WT	
	Geography							
	Coordinate conversion							
	Map projections							
	Spatial analysis						19.14	
	Information processing						=	
							-	

INSTRUCTIONS

1. ORIGINATING ACTIVITY: Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (corporate author) issuing the report.

2a. REPORT SECURITY CLASSIFICATION: Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. GROUP: Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markinga have been used for Group 3 and Group 4 as authorized.

3. REPORT TITLE: Enter the complete report title in all capital letters. Titles in all cases should be unclassified If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. DESCRIPTIVE NOTES: If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period ia covered.

5. AUTHOR(S): Enter the name(s) of author(a) as shown on or in the report. Enter tast name, first name, middle initial. If mllitary, show rank and branch of aervice. The name of the principal author is an absolute minimum requirement.

6. REPORT DATE: Enter the date of the report as dsy, month, year; or month, year. If more than one date appears on the report, use date of publication.

7a. TOTAL NUMBER OF PAGES: The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. NUMBER OF REFERENCES: Enter the total number of referencea cited in the report.

8a. CONTRACT OR GRANT NUMBER: If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. PROJECT NUMBER: Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. ORIGINATOR'S REPORT NUMBER(S): Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. OTHER REPORT NUMBER(S): If the report has been assigned any other report numbers (either by the originator or by the sponsor), also enter this number(a).

1

10. AVAILABILITY/LIMITATION NOTICES: Enter any limitations on further dissemination of the report, other than those

Imposed by accurity classification, using atandard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."

(3) "U. S. Government agencles may obtain copies of this report directly from DDC. Other qualified DDC users ahall request through

(4) "U. S. military agencies may obtain coples of this report directly from DDC. Other qualified usera shall request through

S.

T

3

(5) "All diatribution of this report is controlled. Qualified DDC users shall request through

If the report has been furnished to the Office of Technical Servicea, Department of Commerce, for aale to the public, indicate this fact and enter the price, if known.

11. SUPPLEMENTARY NOTES: Use for additional explanatory notes.

12. SPONSORING MILITARY ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring (paying for) the research and development. Include address.

13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U)

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. KEY WORDS: Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.

> Unclassified Security Classification