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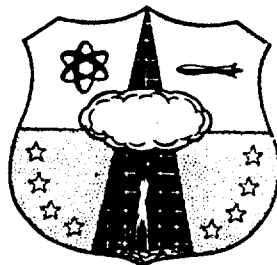
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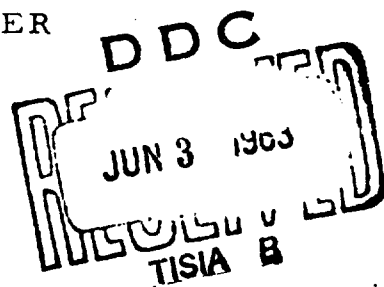
STATIC STABILITY TESTS ON A 0.098 SCALE
STANDARD LAUNCH VEHICLE (SLV)-1B
WITH 4-SQUARE-FOOT FIN AREA

TECHNICAL DOCUMENTARY REPORT NO. AFSWC-TDR-63-21

February 1963



Test Directorate
AIR FORCE SPECIAL WEAPONS CENTER
Air Force Systems Command
Kirtland Air Force Base
New Mexico



Project No. 620-850B-7043

(Prepared under Contract No. AF 29(601)-5603
by C. E. Ziegler, Vought Aeronautics, Division
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ABSTRACT

The purpose of the tests performed in the Chance Vought high-speed wind tunnel was to obtain force data to evaluate the static stability characteristics of the SLV-1B with 4-square-foot fins.

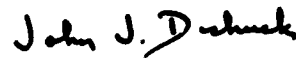
The model was instrumented with a six-component internal strain gage balance and two base pressure probes to determine the forces on the model. The model was then placed in the tunnel and tested in the Mach number range of 0.6 through 5.0, and a Reynolds number range of 6 million/ft. to 20 million/ft. The model attitude was varied from -10 to +10 degrees in the pitch plane.

The results obtained were force and moment data in the body axes; these results are presented in tabulated form with selected coefficients presented in plotted form.

PUBLICATION REVIEW

This report has been reviewed and is approved.


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DCS/Plans & Operations

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1. INTRODUCTION.

This report presents data obtained from tests in the Chance Vought high-speed wind tunnel on a 0.098 scale model of the Standard Launch Vehicle (SLV)-1B with 4-square-foot fins. The test was conducted during the period from 16 October through 20 October 1962. Results are presented in tabulated form with selected coefficients presented in plotted form. A data analysis presentation is also included in section 8.

The model consisted of the same basic parts as the Scout Derivative Model (reference 1). The only changes were in the nose shape and the fin location. Tests were run on the complete body and also on the second stage. Provisions were included for the removal and adjustment of the fins. There were no fins on the second stage.

2. SUMMARY.

a. General information.

High-speed wind tunnel test No.	89
Customer's test designation	None
Test dates	16-22 Oct 1962
Model	Standard Launch Vehicle -1B
Model scale	098
Test dynamic pressure	900-2500 psf
Mach numbers	0.6, 0.8, 1.0, 1.2, 2.0, 3.0, 4.0, 5.0
Test Reynolds number.	6 million/ft. to 20 million/ft. nominal
Test authorization	Contract No. AF 29(601)-5603
Occupancy hours	21 hrs. 9 min.
Number of runs	29
Customer representative	D. E. Poucher
Wind tunnel test engineer	C. E. Ziegler

b. Test objectives.

To determine the static stability characteristics of the model in the Mach number range of 0.6 to 5.0.

3. NOMENCLATURE.

Forces and moments tending to produce a climbing right turn, clockwise roll maneuver are positive. Directions assume the model to be at $\varphi = 0$ and the observer to be viewing upstream.

Coefficient data are presented in the body and stability axes.

PNT		Data sequence number, (card number)	
ALPHA		Angle of attack in the pitch plane of the model, corrected for deflection, positive nose up.	degrees
N	C_N	Normal force coefficient, body axes	$\frac{\text{normal force}}{qS}$
PM	C_m	Pitching moment coefficient, body axes	$\frac{\text{pitching moment}}{qSc}$
Y	C_Y	Side force coefficient, body axes	$\frac{\text{side force}}{qS}$
YM	C_n	Yawing moment coefficient, body axes	$\frac{\text{yawing moment}}{qSb}$
RM	C_l	Rolling moment coefficient, body axes	$\frac{\text{rolling moment}}{qSb}$
A	C_A	Axial force coefficient corrected to the equivalent of free stream static pressure acting on the base body axes	$C_{AU} - C_{AB}$
AU	C_{AU}	Axial force coefficient as recorded uncorrected for base pressure effects	$\frac{\text{axial force}}{qS}$
AB	C_{AB}	Axial force coefficient due to base pressure	$\frac{(P_B - P_S) S_B}{qS}$
L	C_L	Lift force coefficient, stability axes	$\frac{\text{lift force}}{qS}$
D	C_D	Drag force coefficient corrected to the equivalent of free stream static pressure acting on the base, stability axes	$\frac{\text{drag force}}{qS}$

CP	Center of pressure, positive upstream, inches from sta 25.5 for B ₃ configuration and 14.1 for B ₄ configuration	$\frac{C_m(c)}{C_N}$
TO	Free stream stagnation temperature	degrees Rankine
Po	Free stream stagnation pressure	psia
PS	Free stream static pressure	psia
Q q	Free stream dynamic pressure	psf, psi
M	Free stream Mach number	
RN/L	Reynolds number per foot	
S	Reference area, sq. in.	7.2576
c	Reference length, in.	3.038
b	Reference length, in.	3.038
S _B	Base pressure correction area, sq. in.	4.909 (B ₃) 4.909 (B ₄)

Body nomenclature

B ₃	Complete body less fins
B ₄	B ₃ less first stage
F ₂	Fins
Δ _F	Fin cant angle

4. DESCRIPTION OF FACILITY.

The Chance Vought Corporation high-speed wind tunnel is an atmospheric-exhaust, blow-down tunnel with a 4- by 4-foot test section size. The Mach number range of the tunnel is from 0.5 to 5.0. Air is stored in six tanks, with a total volume of 28,000 cubic feet, at a maximum pressure of 600 psia and a nominal temperature of 100 degrees Fahrenheit.

The circuit utilizes both supersonic and transonic test sections, each 4 by 4 feet in cross section and slightly over 5 feet long. For supersonic operation

a single-peak variable diffuser is placed downstream of the supersonic test section. For transonic operation the variable diffuser is removed from the circuit and replaced with a porous-wall, transonic-test section with 22 percent wall porosity. The transonic plenum is pumped by ejector action of the main tunnel airstream acting on controllable ejector flaps located downstream of the test section. Adjustable choking flaps, also located downstream of the test region, are utilized for subsonic Mach number adjustment. Figure 1 shows the general tunnel arrangement and identifies various areas within the facility.

5. MODEL AND INSTRUMENTATION.

The model tested was a 0.098 scale model of the Standard Launch Vehicle-1B with 4-square-foot fins. The model consisted of two basic bodies and two tail configurations. One body configuration was the second stage of the missile and was approximately 25 inches long. The other body configuration was the second stage with a first stage added to give it a total length of 49.09 inches. The fins were the same as those used on the Scout Derivative model described in reference 1. One set of fins had zero incidence angle and the other set had 3 degrees incidence angle to produce positive roll. Figures 2 and 3 show the installation of the two body configurations in the tunnel. Figure 4 shows the dimensions of the two bodies and the fins, and the orientation for each component.

Model forces were measured by the VB-13 six-component internal strain gage balance mounted on sting configuration number 1 with sting extension CVS54377 (reference 2). Figures 5 and 6 show the general arrangement and identify the sting sections. Two static pressure probes were located in the cavity of the body to measure base pressure. Each probe was connected to a separate pressure transducer to provide a backup system.

In addition to force balance and base pressure transducer outputs, tunnel parameters were also recorded. These parameters consisted of angle of attack, stagnation and static pressures, and stagnation temperature.

6. TEST PROCEDURES.

Preliminary preparations for the test included calibration of the VB-13 balance and the base pressure transducers. The sting and extension were

1. STORAGE TANK
2. MDCING HEADER
3. GATE VALVE
4. CONTROL VALVE
5. ENTRANCE CONE
6. STILLING CHAMBER
7. VARIABLE NOZZLE
8. TEST SECTION
9. SUPERSONIC DIFFUSER
10. SUBSONIC DIFFUSER
11. EXHAUST MUFFLER
12. COOLING TOWER
13. CONTROL ROOM
14. OFFICE
15. MODEL ROOM
16. AIR COMPRESSOR AND AIR DRYING ROOM

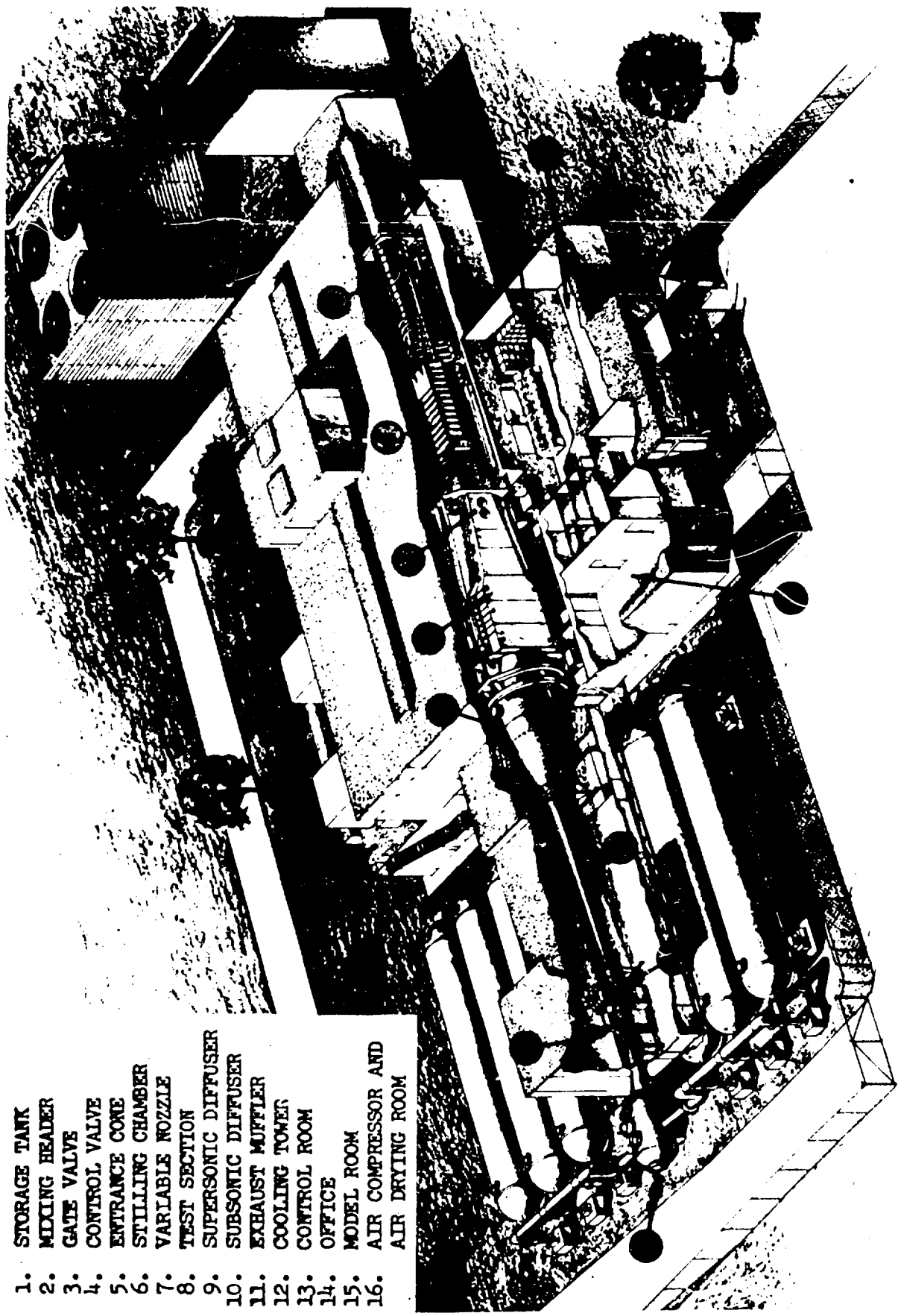


Figure 1. Chance-Vought high-speed wind tunnel.

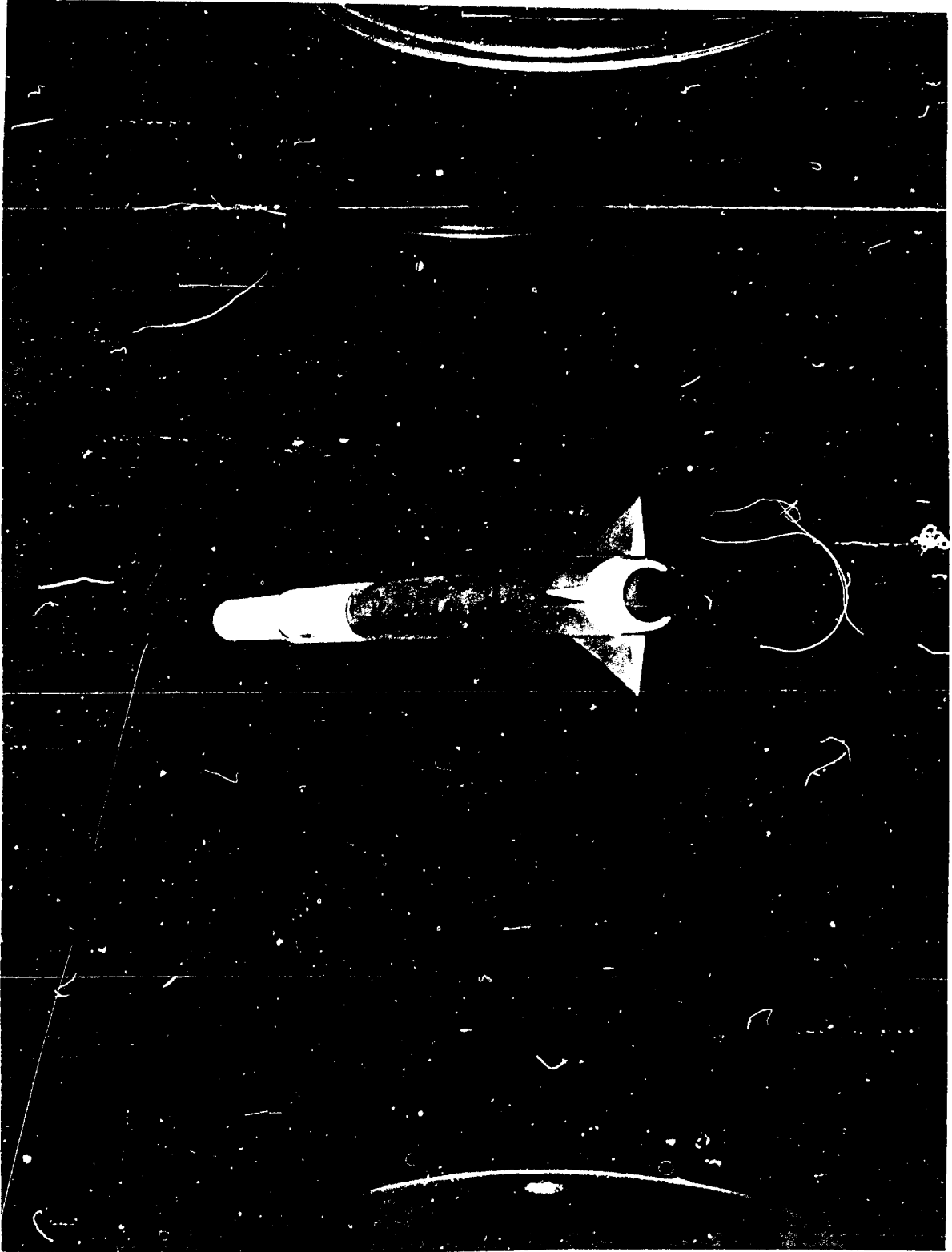


Figure 2. SLV-1B Model mounted in tunnel.

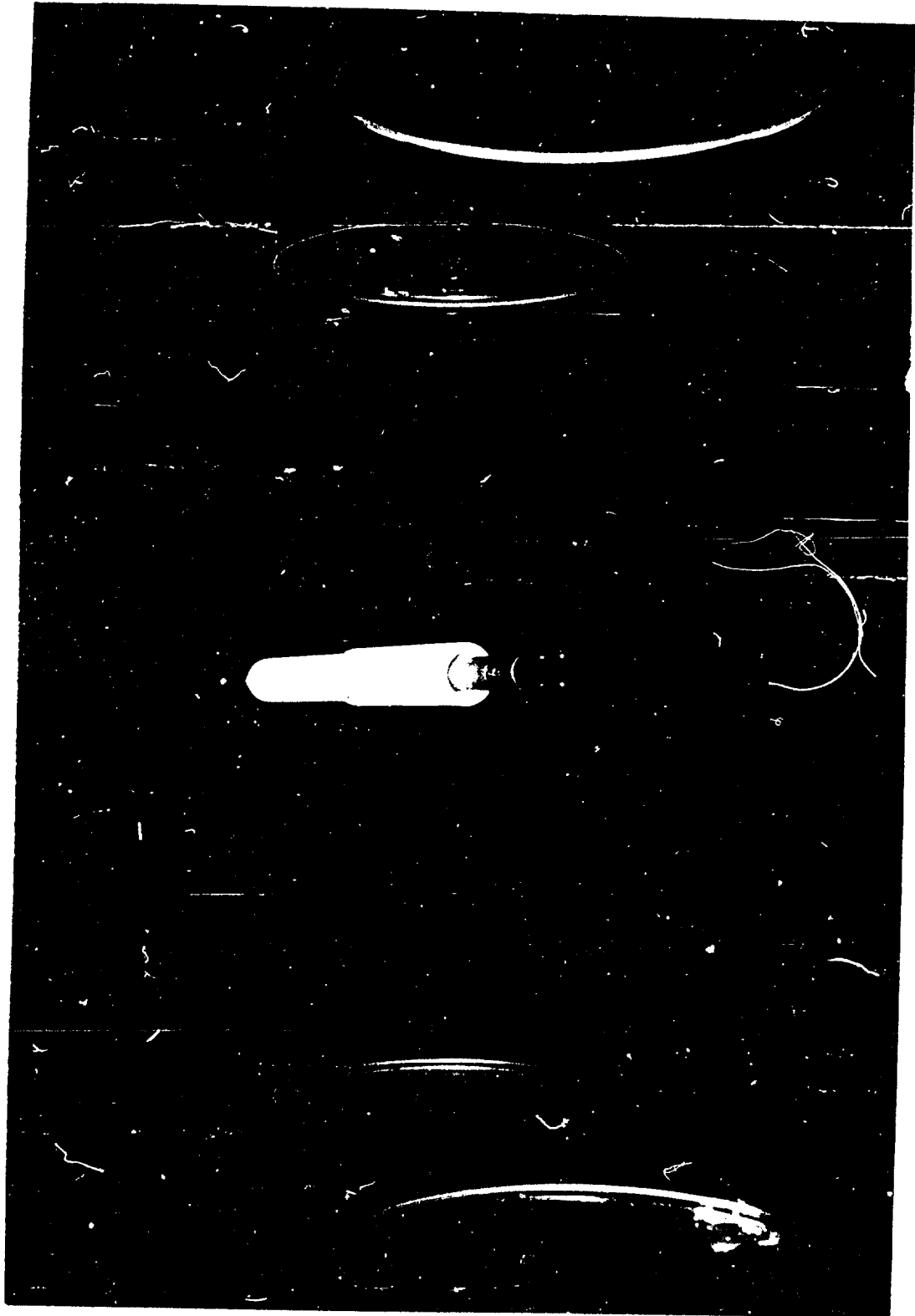
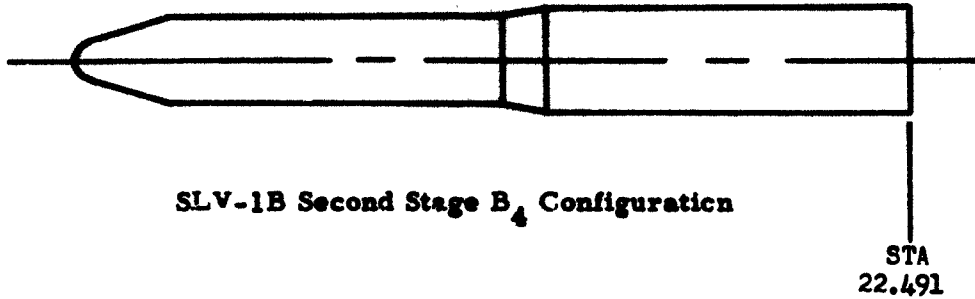


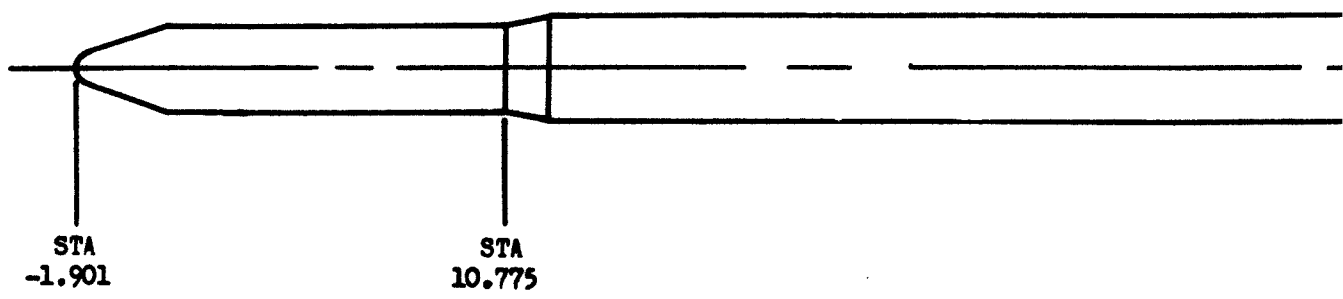
Figure 3. Second stage of SLV-1B mounted in tunnel.



SLV-1B Second Stage B₄ Configuration

STA
22.491

SKETCH OF THE SLV-1B MODEL

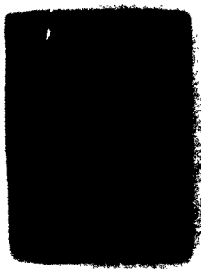


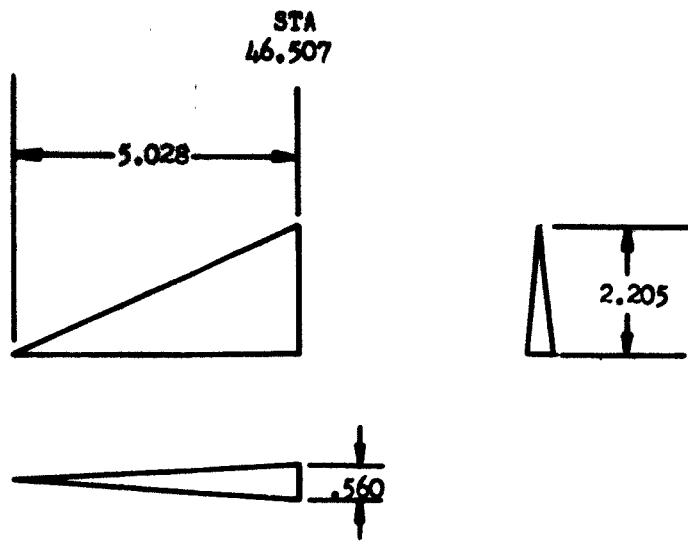
STA
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STA
10.775

SLV-1B B₃F₂ Configuration

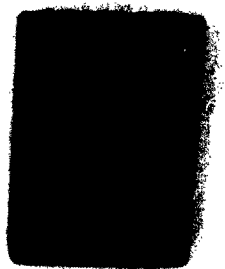
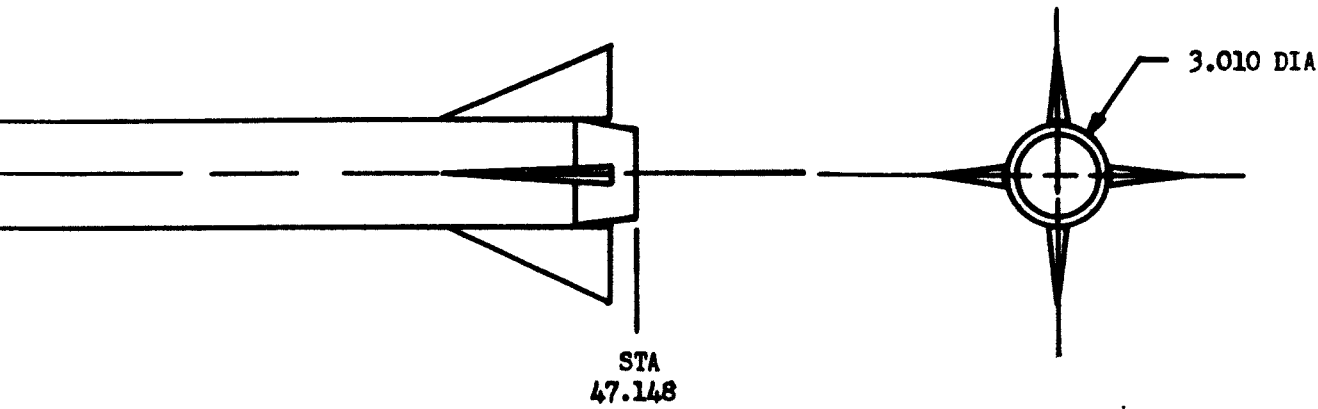
Figure 4. Dimensions of model.

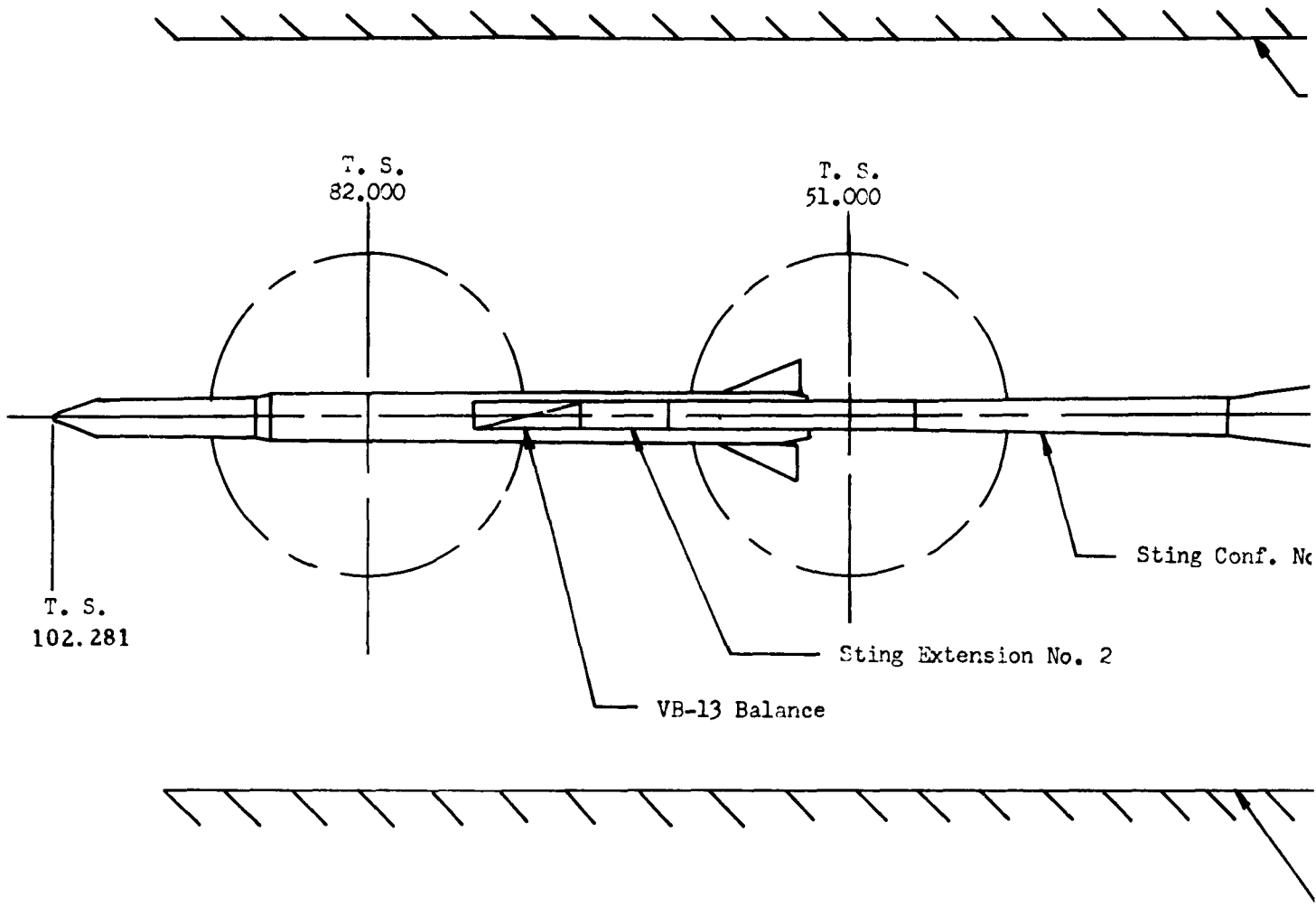




SLV-1B F₂ Fins

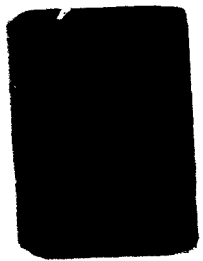
Note: The fin with the 3 degree cant angle is the same as the fin above except it is aligned at a 3 degree angle with the body axes.

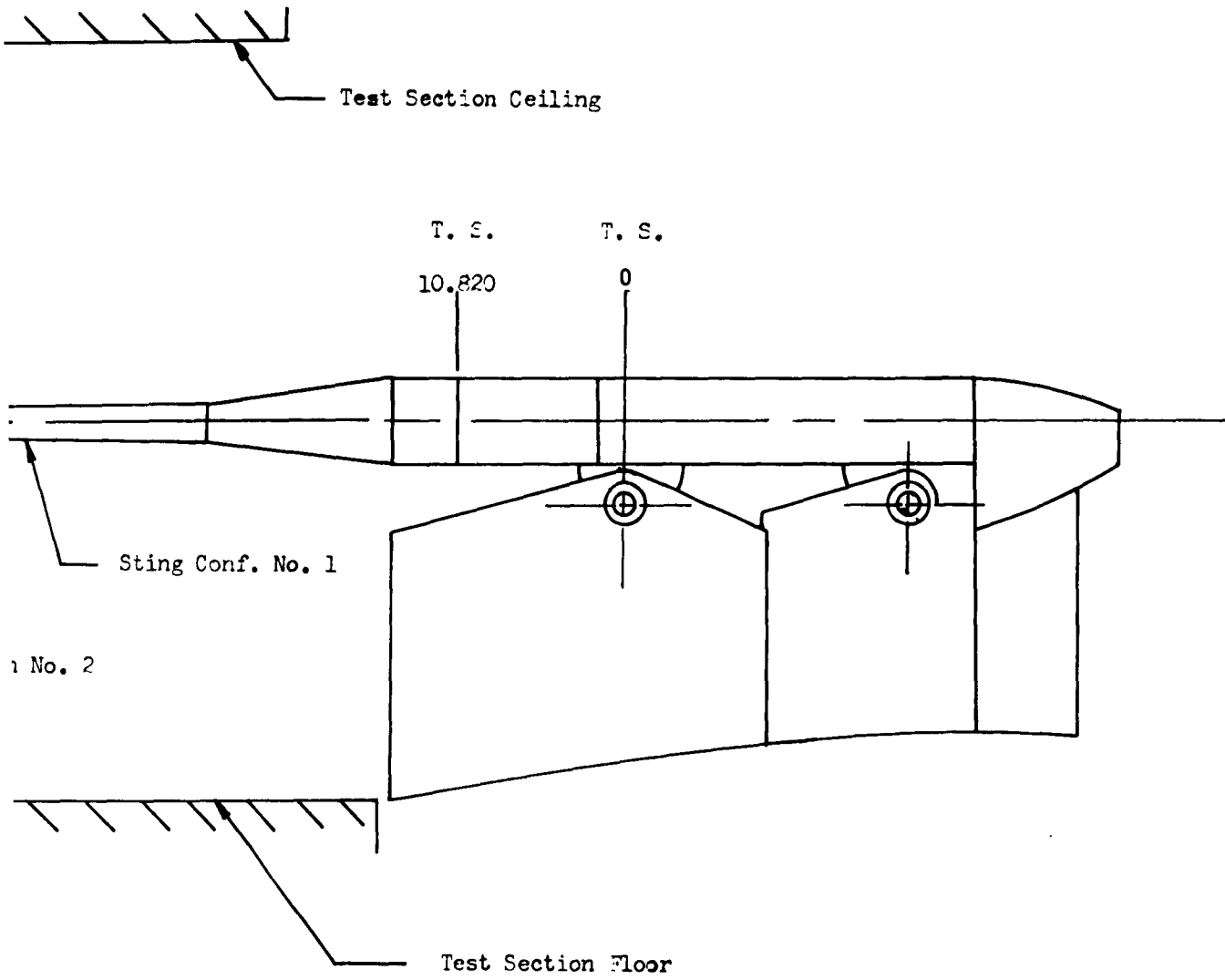




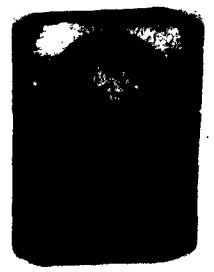
SLV-1B Installation Ske

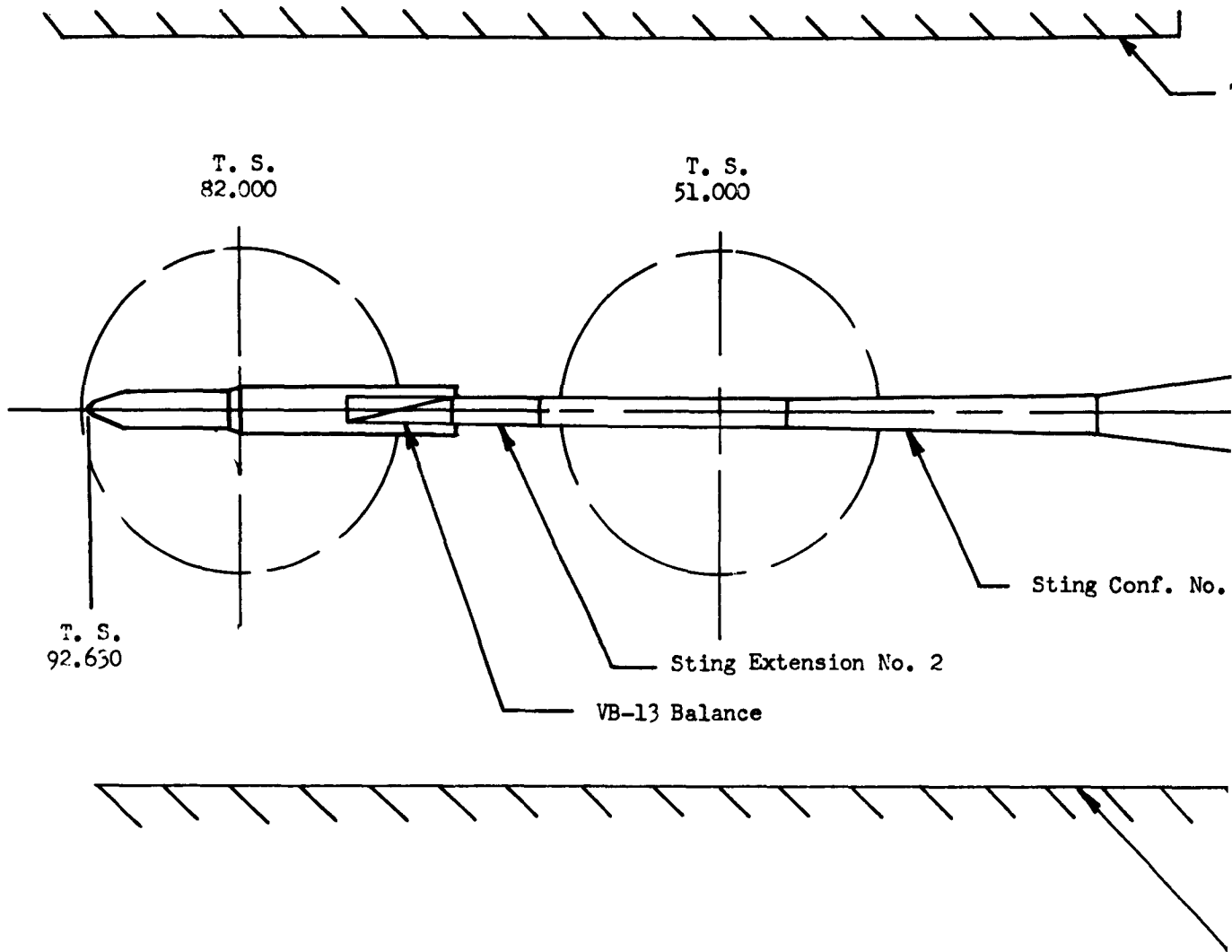
Figure 5. SLV-1B Installation sketch.





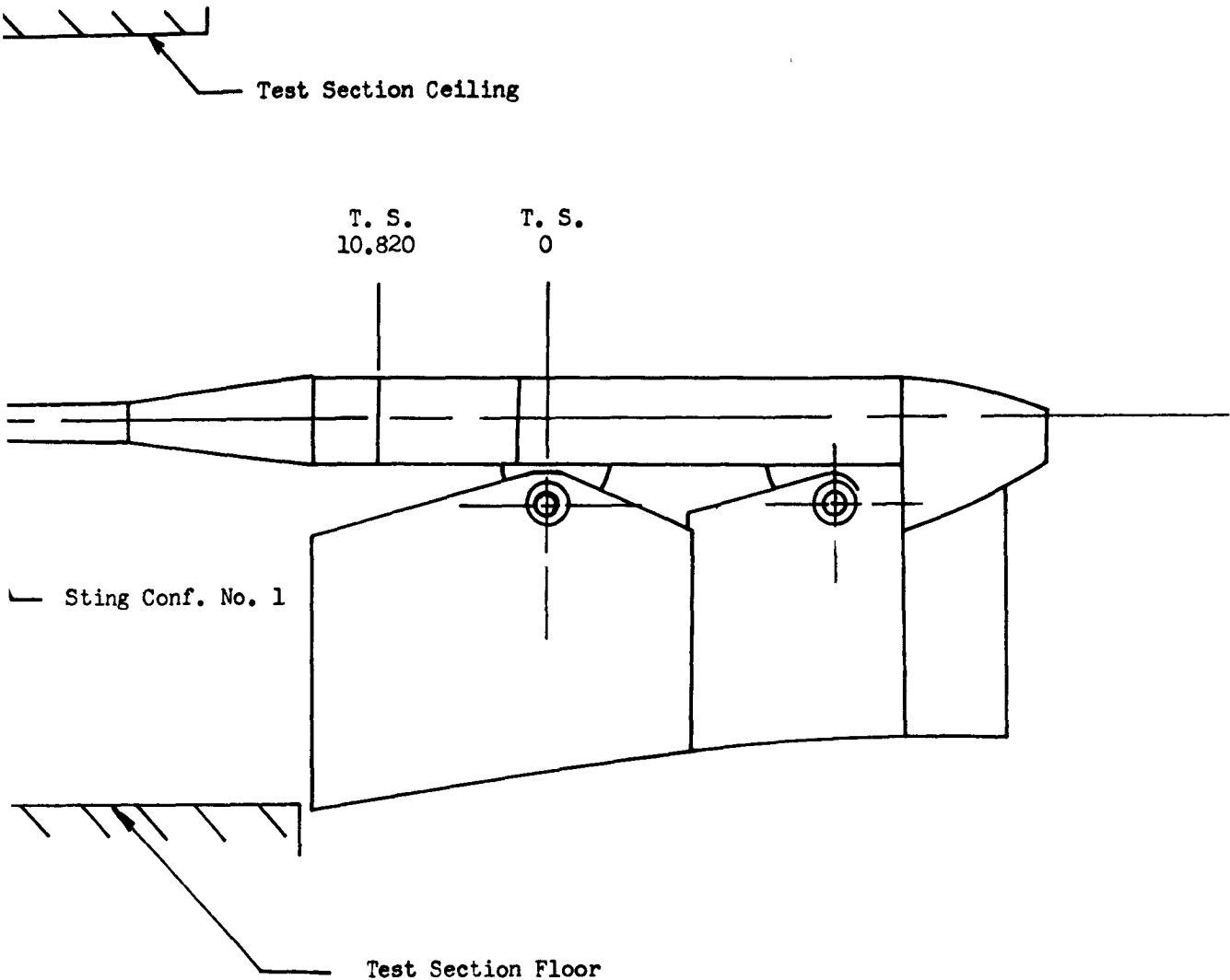
LV-1B Installation Sketch





SLV-1B Second Stage Install

Figure 6. SLV-1B Second stage installation sketch.



Second Stage Installation Sketch



also calibrated for load deflections. Following installation of the model in the tunnel, additional load checks were made to ensure that the balance and data systems were functioning properly.

For test runs the tunnel was started with the model at zero angle of attack. When the flow was established the model was pitched to the maximum negative angle of attack, then back through zero to the maximum positive angle of attack, and returned to zero before the termination of the run. The angle of attack range through which the model was pitched was from a negative 10 degrees to a positive 10 degrees.

The test was conducted in the Mach number range of 0.6 to 5.0 and a dynamic pressure range of 900 to 2,500 psf.

Data cards were sampled before and after each run to obtain "wind on" and "wind off" data. Tare cards were also sampled before each run to permit a correction for model weight tare effects.

Data were sampled at the rate of 10 times per second for the body-alone and second-stage configurations, and 5 times per second when the fins were on the body. The data were digitized and recorded on magnetic tape. At the conclusion of each run, data cards were punched from the tape. The data cards were checked after each run to ensure satisfactory results. After the cards were accepted, the model and/or Mach number was changed. On-the-line data plotting was done by analog computer data reduction to parallel and check digitized data.

7. DATA REDUCTION.

Static force data were reduced by digital computer to obtain nondimensional force and moment coefficients about the body axes. A complete description of the data reduction procedure is presented in reference 3.

All coefficients were corrected for model weight tares, and angle of attack was corrected for sting and balance deflection. Axial force data are presented in three coefficient forms: axial force corrected for base pressure (C_A), axial force uncorrected for base pressure (C_{AU}), and axial force due to base pressure (C_{AB}).

Pitching moment was referenced to station 25.5 for the B₃ configurations and to station 14.1 for the B₄ configuration.

To present some means of determining data accuracies, static accuracies of the VB-13 balance are presented. The tabulated accuracies were obtained by computing a "root mean square" deviation between the applied and calculated loads over the maximum load range.

Results are as follows:

<u>Component</u>	<u>Load</u>	<u>Coefficient</u>
Normal force	0.74 lb.	0.0163
Side force	0.44 lb.	0.0097
Axial force	0.35 lb.	0.0077
Rolling moment	0.59 in-lb.	0.0043
Pitching moment	0.74 in-lb.	0.0054
Yawing moment	0.44 in-lb.	0.0032

8. DATA ANALYSIS.

The experimental data show that the vehicle's first-stage static margin is approximately 15 inches less than originally estimated at Mach 3.8, which, for the nominal 76° trajectory, is the critical point. It appears that this is due to the fin effectiveness which is considerably lower than estimated. The vehicle's drag is higher transonically and lower supersonically than the original estimates. Fin rolling moment characteristics are generally as estimated except for lowered transonic effectiveness. At first-stage separation of the flight article, the nose cone and heat shield are jettisoned, exposing the payload. A model of this second stage was not available for these wind tunnel tests. The second stage as referred to in these tests consists of the vehicle forebody forward of body station 238.5 and is not representative of the actual vehicle second stage. This configuration was tested in an attempt to further define the body-alone center of pressure location and load distribution. The vehicle's second-stage static margin is more negative than estimated while the drag is less than estimated.

a. Wind tunnel tests.

The model tested was a 0.098 scale version of the SLV-1B. Transonic and supersonic tests were made on the first-stage configuration (with and without fins) and supersonic tests were made on the second-stage configuration to confirm the vehicle's estimated aerodynamic characteristics. The test runs on the first stage with and without fins were made to determine the fin effectiveness.

A standard six-component force balance was used to obtain normal force, pitching moment, axial force and rolling moment (yaw and yawing moments were negligible). The axial force (zero lift drag) data have been corrected to zero base drag.

The center of pressure locations are determined using the pitching moment and normal force derivatives; therefore, c.p. is directly effected by errors in both of these derivatives. The normal force and pitching moment errors are a function of several things; one of these being whether or not the normal force vector acts between the balance strain gages. For total vehicle tests, where the c.p. is well aft of the nose and between the balance strain gages, the c.p. location can be determined with ± 4 to 6 inches for the full-scale vehicle. However, for body-alone tests, where the c.p. is close to the nose of the vehicle and well outside of the balance strain gages this error can be increased by as much as a factor of 6. For these reasons, the center of pressure data for the body alone (and consequently the fin alone) from these tests should be used with caution. The values of normal force are much less sensitive to this effect than the computed values of center of pressure.

The test data for total vehicle $C_{N\alpha}$ are below predicted values at Mach numbers below Mach 4.0. The maximum variation is 18% at Mach 0.6. At Mach numbers from 3 to 5 the disagreement between predicted and measured is within the usual accuracy of prediction methods.

The experimental body-alone data are greater than estimated supersonically and less than estimated transonically. Part of the disagreement between experiment and prediction for the full first-stage configuration is due to this fact.

The C_{N_a} S of the fin plus carryover was determined by subtraction of body-alone C_{N_a} S from total-vehicle C_{N_a} S. Test data were consistently below the predicted values by 6% to 27% with the greatest disagreement occurring between Mach 2.0 to 3.0.

Test points produced a smooth curve with no unexpected variations in the pitching moment derivative.

The test data have been corrected by using a calculated friction drag and adding to that the pressure drag obtained from the wind tunnel and the calculated drag for six explosive bolt fairings.

Corrected wind tunnel data for the total vehicle are higher subsonically and transonically but lower supersonically than the estimates. The maximum variations were a 20% increase over the estimated data at Mach 1.0 and a 14% decrease below the estimated data at Mach 5.0.

Body-alone test data agree very well with the estimated data.

Zero lift fin drag, $(C_{D_oS})_{fin}$, was obtained by subtracting the C_{D_oS} of the body alone from the C_{D_oS} of the total vehicle. The fin drag was underestimated subsonically and transonically and overestimated supersonically.

The c.p. variation for the total vehicle and body alone were computed from experimentally determined C_{m_a} and C_{N_a} values.

The test data (essentially rigid body) values of center of pressure for the total vehicle have the same trend as the predictions but indicate that the vehicle is less stable supersonically than estimated. The maximum decrease in static margin is about 15 inches or 0.484 body diameter. The maximum decrease in rigid body static margin occurred at Mach 3.8 and dropped from 35 inches of static margin to 20 inches.

In view of the problems of measuring the body-alone center of pressure no firm comments may be made concerning the disagreement between the experimental and predicted values. Since the body alone data are also used in determining the fin center of pressure the same caution must be taken when evaluating or using the fin center of pressure data.

Wind tunnel data and estimates for rolling moment coefficient are in generally good agreement. Test data did not show the predicted sharp peak transonically and are about 17% below the estimate in this region; for speeds in excess of Mach 2.0, test data are slightly higher. Supersonically the maximum difference between test and predicted values occurs at Mach 5.0 and is about 9.5%.

b. Second stage.

Second-stage aerodynamic data parameters were determined experimentally from Mach 2.0 to 5.0. The experimental normal force data agree very well with the predicted value at Mach 2.0. However, as the velocity increases, the test results show a gradual increase while the predicted value is constant for speeds in excess of Mach 3.0. The difference between the two values is a maximum of 25% at Mach 5.0.

A negative static margin of 75 inches was predicted at the Mach number for second-stage ignition; test data showed this negative static margin to be about 100 inches. In the range from Mach 3.0 to Mach 5.0, the maximum difference between test and prediction occurred at Mach 3.0 where the experimental static margin was 17% greater than predicted.

The experimental drag was lower than estimated over the entire test range. The maximum difference between predicted and measured drag occurred at Mach 4.0 where the test data were 14% below the predicted values.

9. CONCLUSIONS AND RECOMMENDATIONS.

The following conclusions may be derived from the wind tunnel tests on the SLV-1B model.

a. First stage.

The vehicle's normal force parameter is generally less than estimated with the largest differences occurring at transonic speeds. This difference arises partly from the body-alone characteristics and partly from the fin characteristics.

The rigid body center of pressure is forward of the estimates, thus resulting in a less stable rigid vehicle than estimated. This difference amounts

to about 15 inches decrease in static margin at a Mach number of 3.8. It appears that the primary reason for this effect lies in a lower fin effectiveness than estimated.

The test data show that the vehicle's zero lift drag parameter is less supersonically and greater transonically than the estimated values. Differences between fin-measured and estimated drags essentially account for these differences.

Estimated center of pressure variations due to the flexibility for the nominal 76° trajectory, when added to test data, show the vehicle to be unstable above Mach 3.0.

b. Second stage.

Normal force and zero lift drag force parameter estimates differed from test data by a maximum of 25 and 14% respectively between Mach 3.0 and 5.0. The parameters were under- and over-estimated respectively and the differences increased with Mach number.

Test data gave values for center of pressure 25 inches forward of the predicted location for an increase in the negative static margin of 33% at Mach 3.0. The difference decreases as Mach number increases resulting in a 15-inch difference at Mach 4.0.

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APPENDIX I

HIGH-SPEED WIND TUNNEL RUN LOG

HIGH SPEED WIND TUNNEL RUN LOG

RUN No.	CONFIGURATION	MACH NO.	Q PSFA	α RANGE DEGREES	ϕ	Δ F	COMMENTS
1	B ₃	1.2	1440	+10 to -10	0	-	
2	B ₃ ^F ₂	"	"	"	"	0	
3	"	"	"	"	"	3	
4	"	1.0	"	"	"	"	
5	"	.8	1300	"	"	"	
6	"	.6	900	"	"	"	
7	"	"	"	"	"	0	
8	"	.8	1300	"	"	"	
9	"	1.0	1440	"	"	"	
10	B ₃	"	"	"	"	-	
11	"	.8	1300	"	"	-	
12	"	.6	900	"	"	-	
13	"	2.0	1440	"	"	-	
14	B ₃ ^F ₂	"	"	"	"	0	
15	"	"	"	"	"	3	
16	"	3.0	"	"	"	"	
17	"	"	"	"	"	0	
18	B ₃	"	"	"	"	-	
19	"	4.0	"	"	"	-	
20	B ₃ ^F ₂	"	"	"	"	0	
21	"	"	"	"	"	3	
22	"	5.0	"	"	"	"	
23	"	"	"	"	"	0	

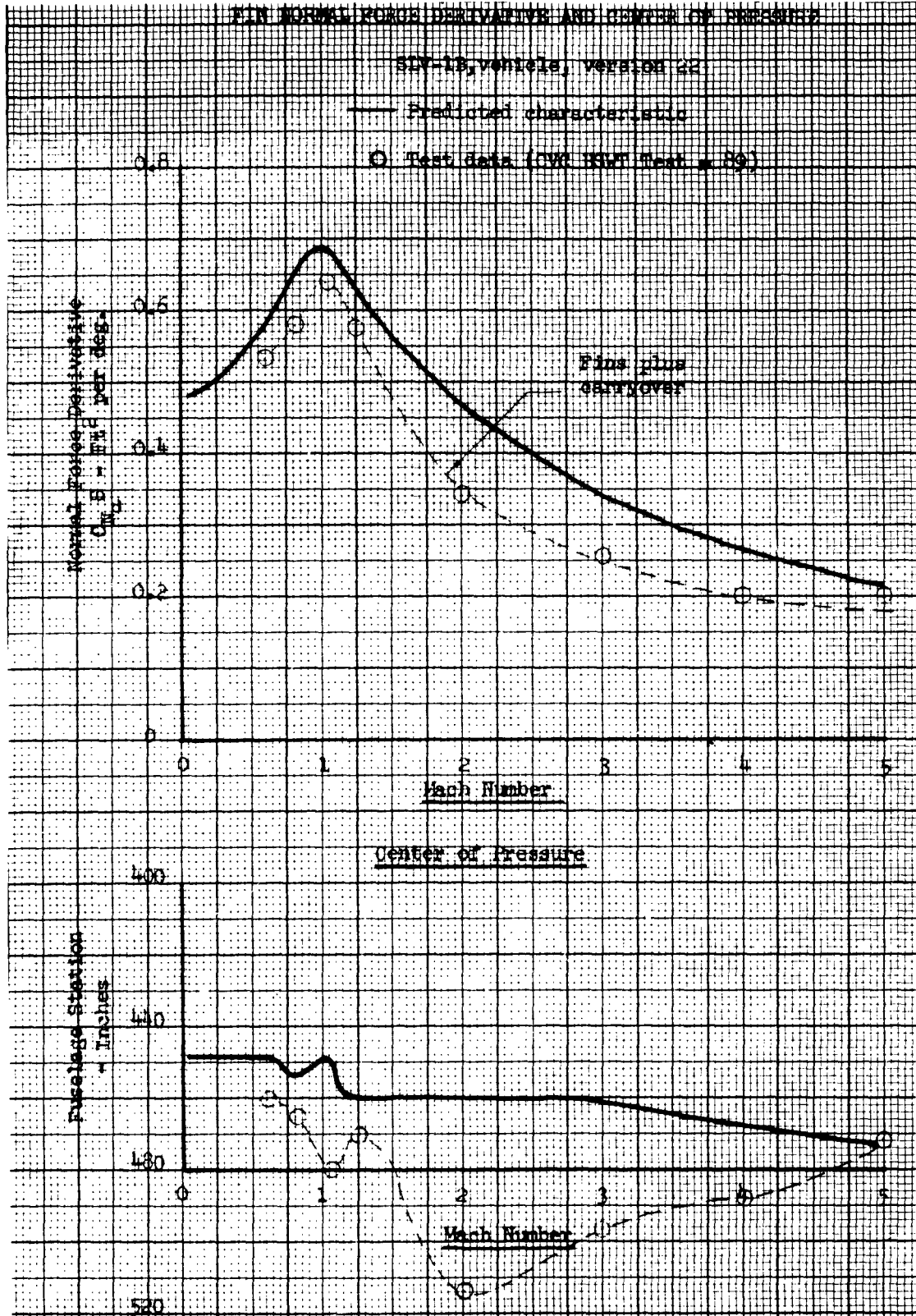
HIGH SPEED WIND TUNNEL RUN LOG (cont'd)

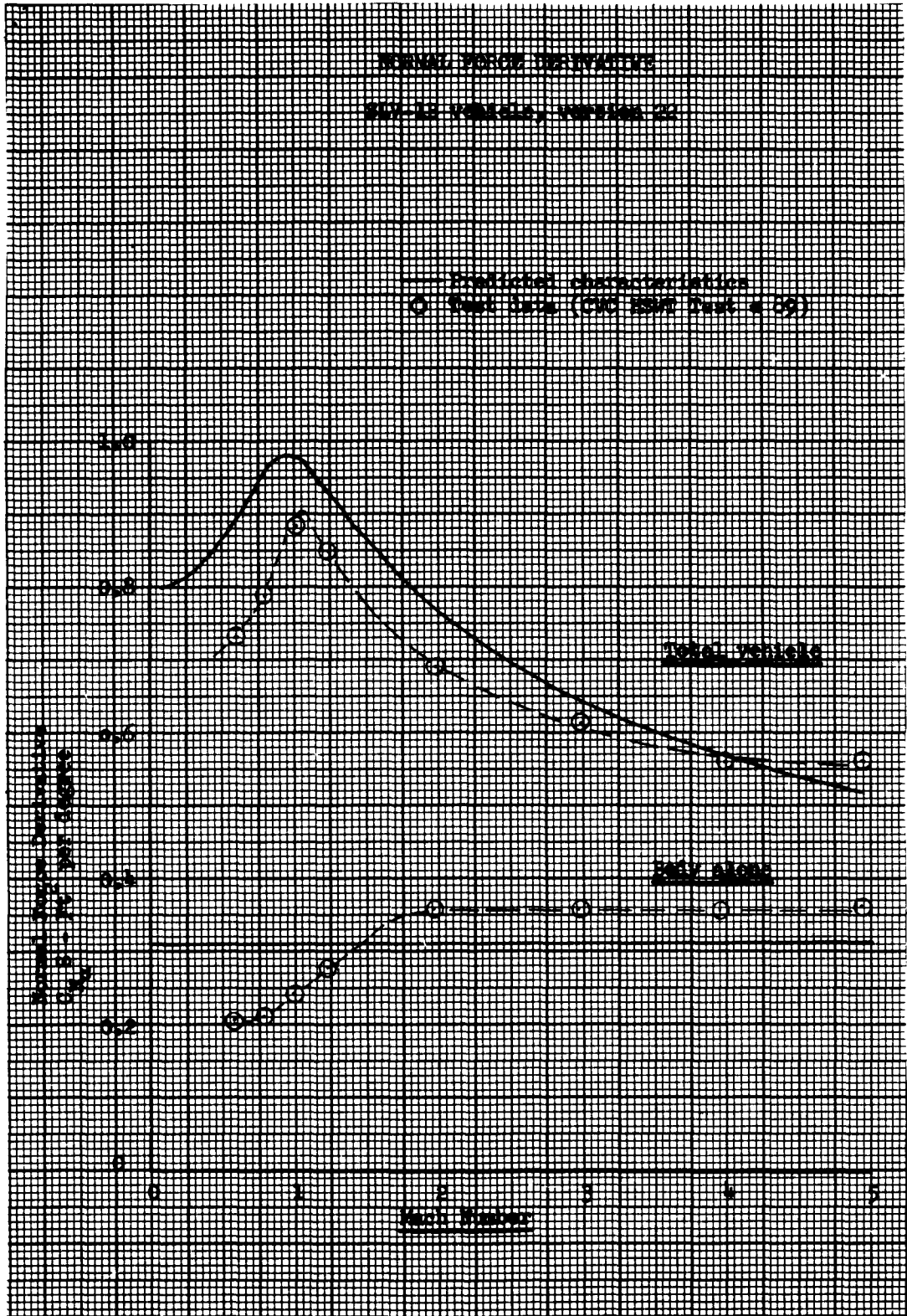
RUN NO.	CONFIGURATION	MACH NO.	Q PSFA	α RANGE DEGREES	ϕ	ΔF	COMMENTS
24	B ₃	5.0	1440	+10 to -10	0	-	
25	B ₄	"	"	"	"	-	
26	"	4.0	2500	"	"	-	
27	"	3.0	"	"	"	-	
28	"	2.0	"	"	"	-	
29	B ₃ ^F ₂	.6	900	"	"	0	Rerun of 7

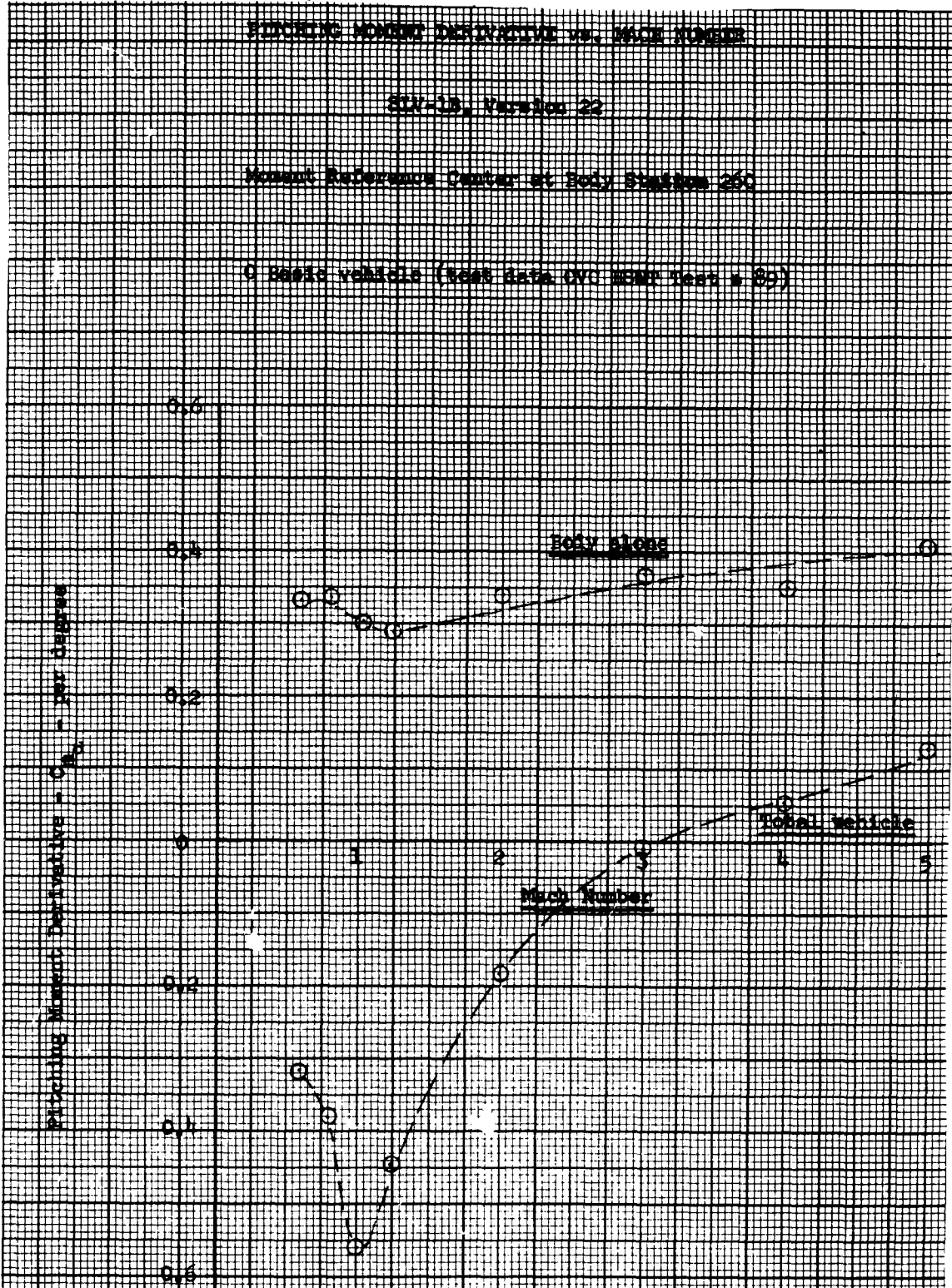
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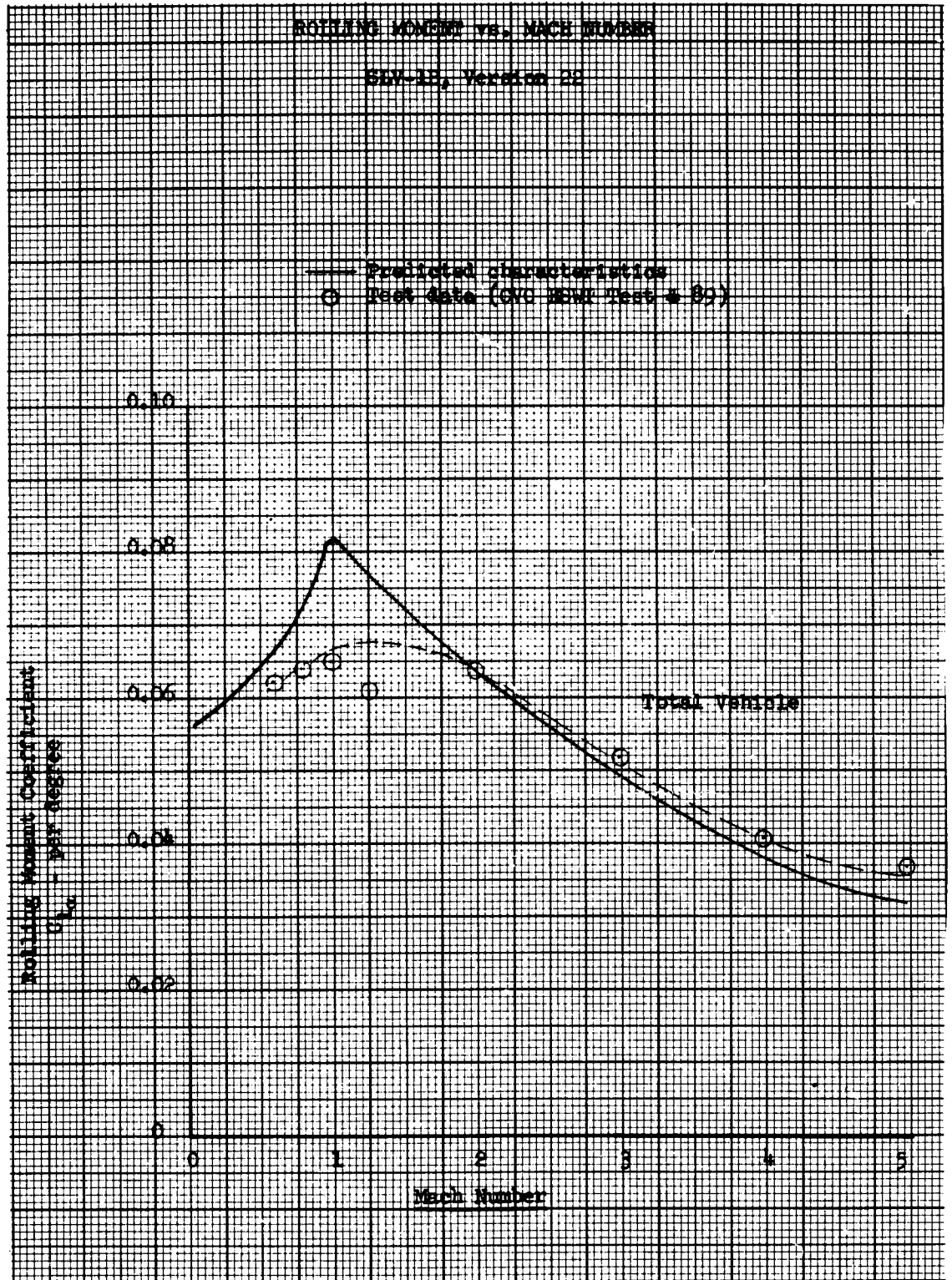
APPENDIX II

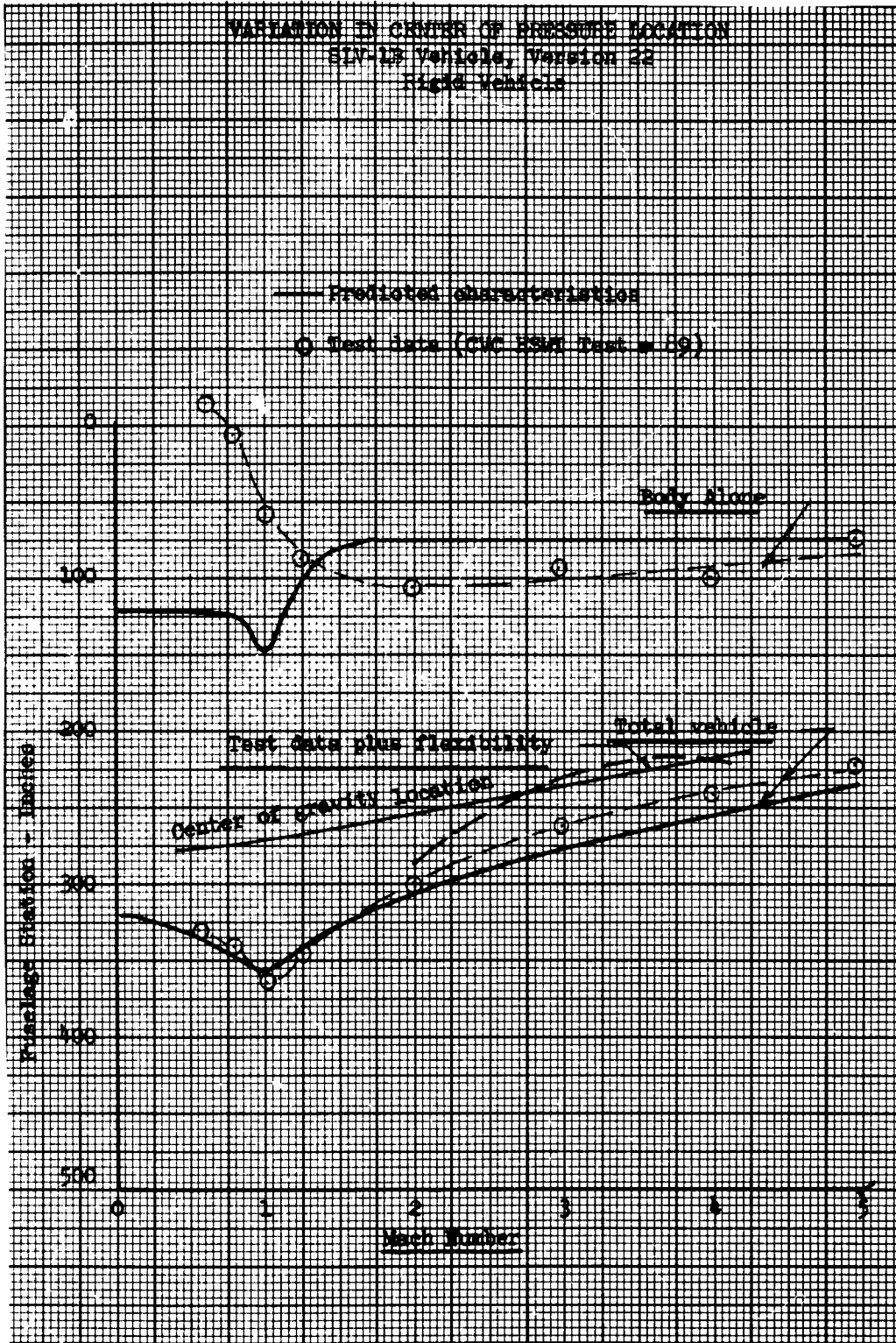
ANALYSIS PLOTTED DATA

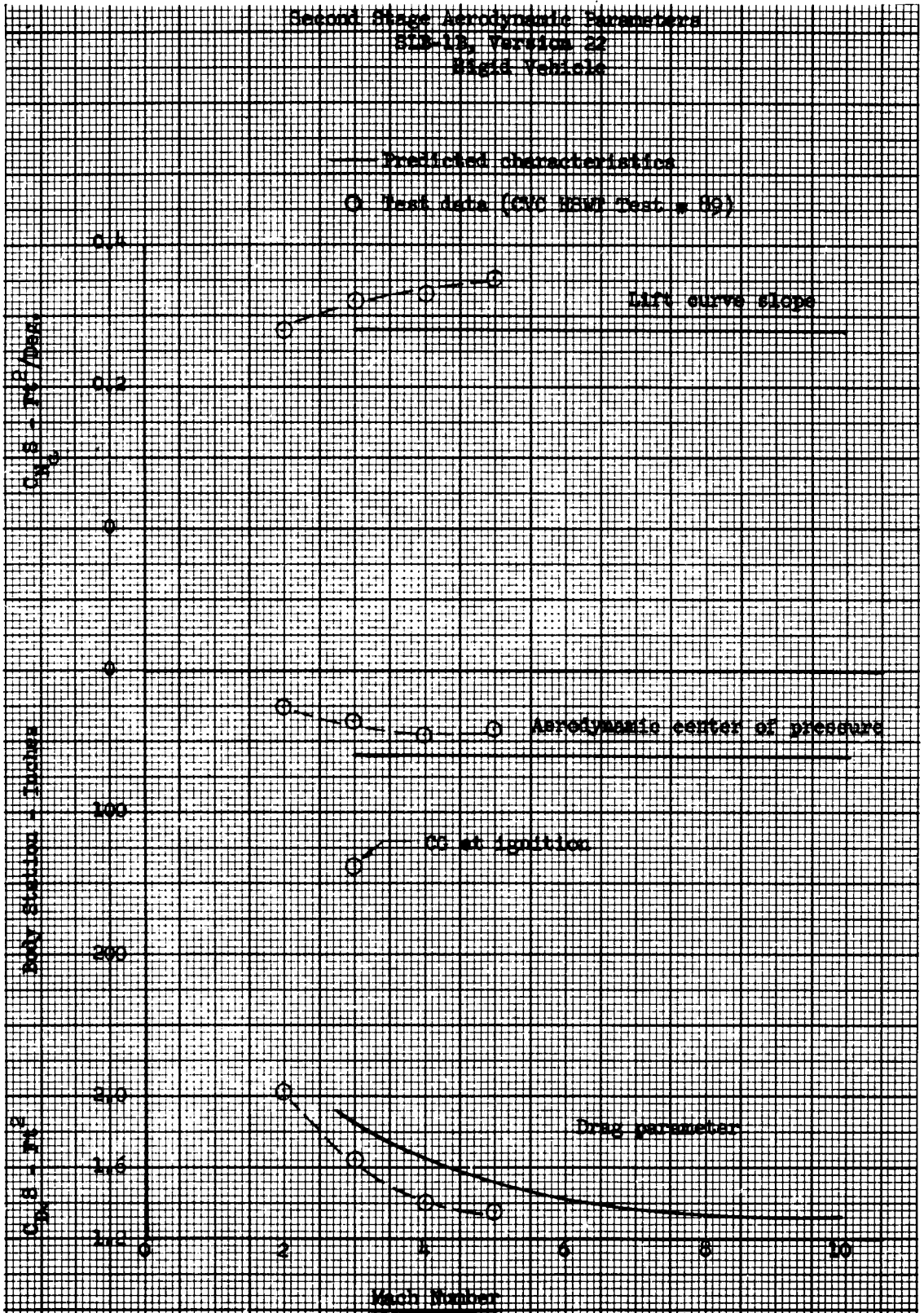


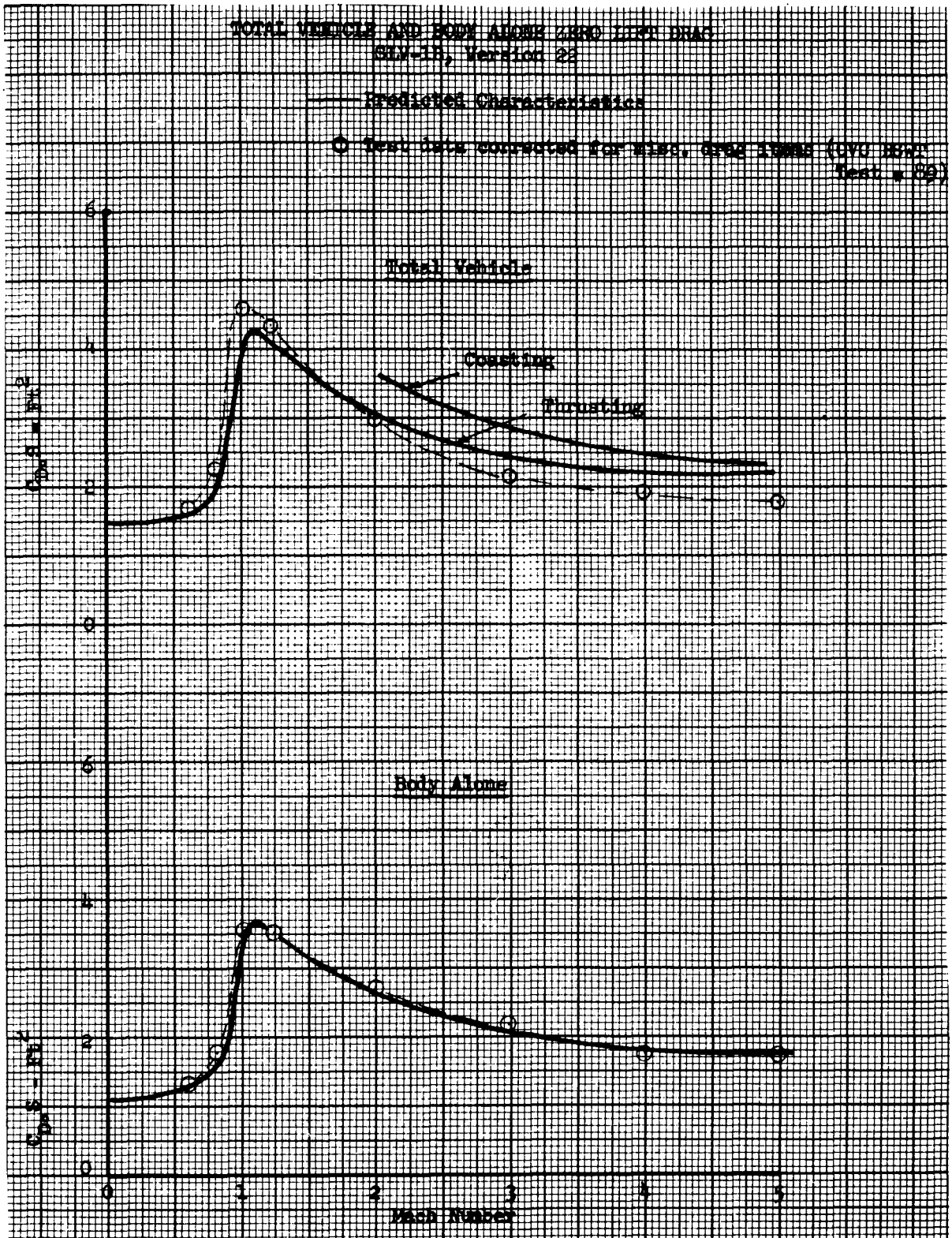


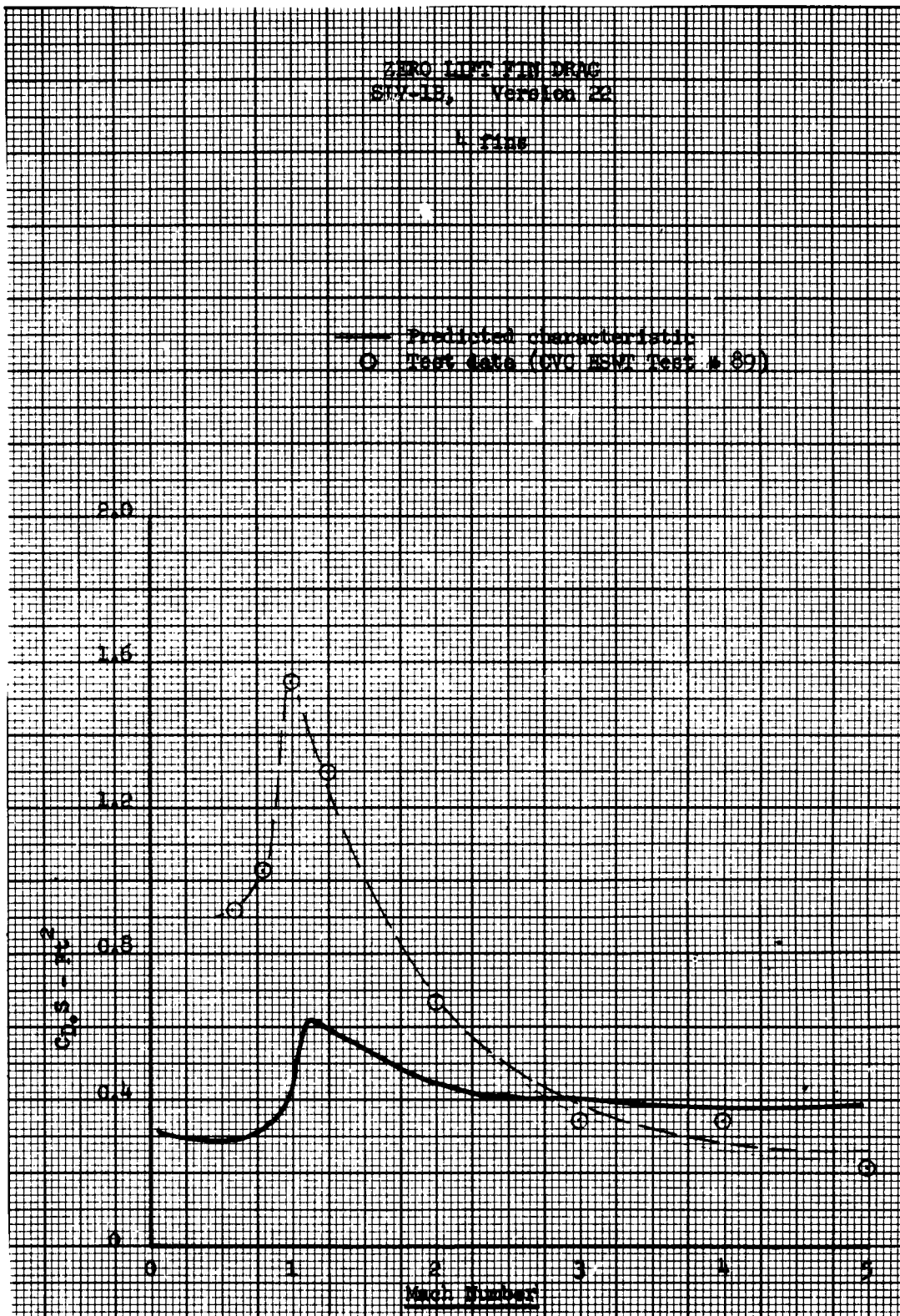












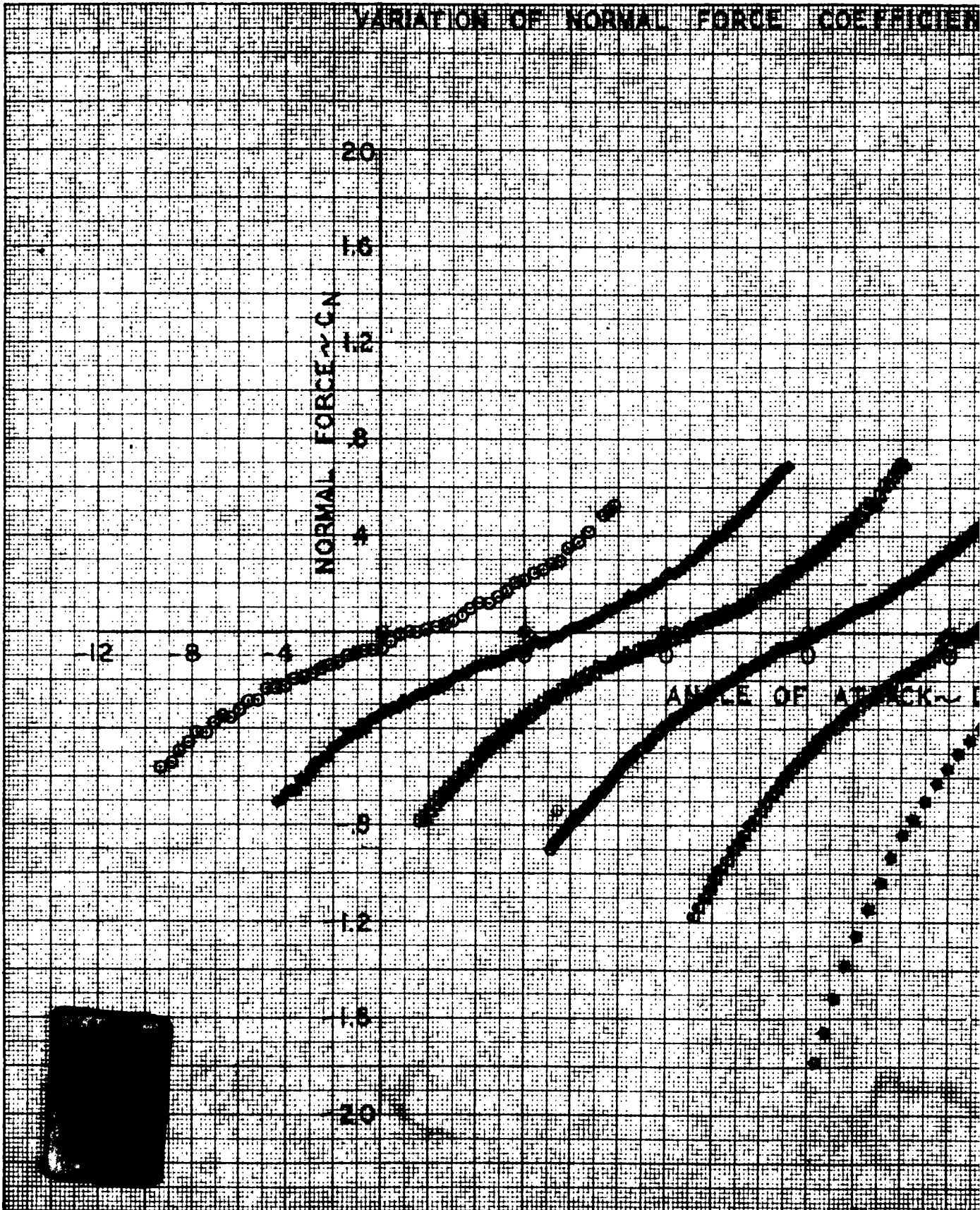
TDR-63-21

APPENDIX III

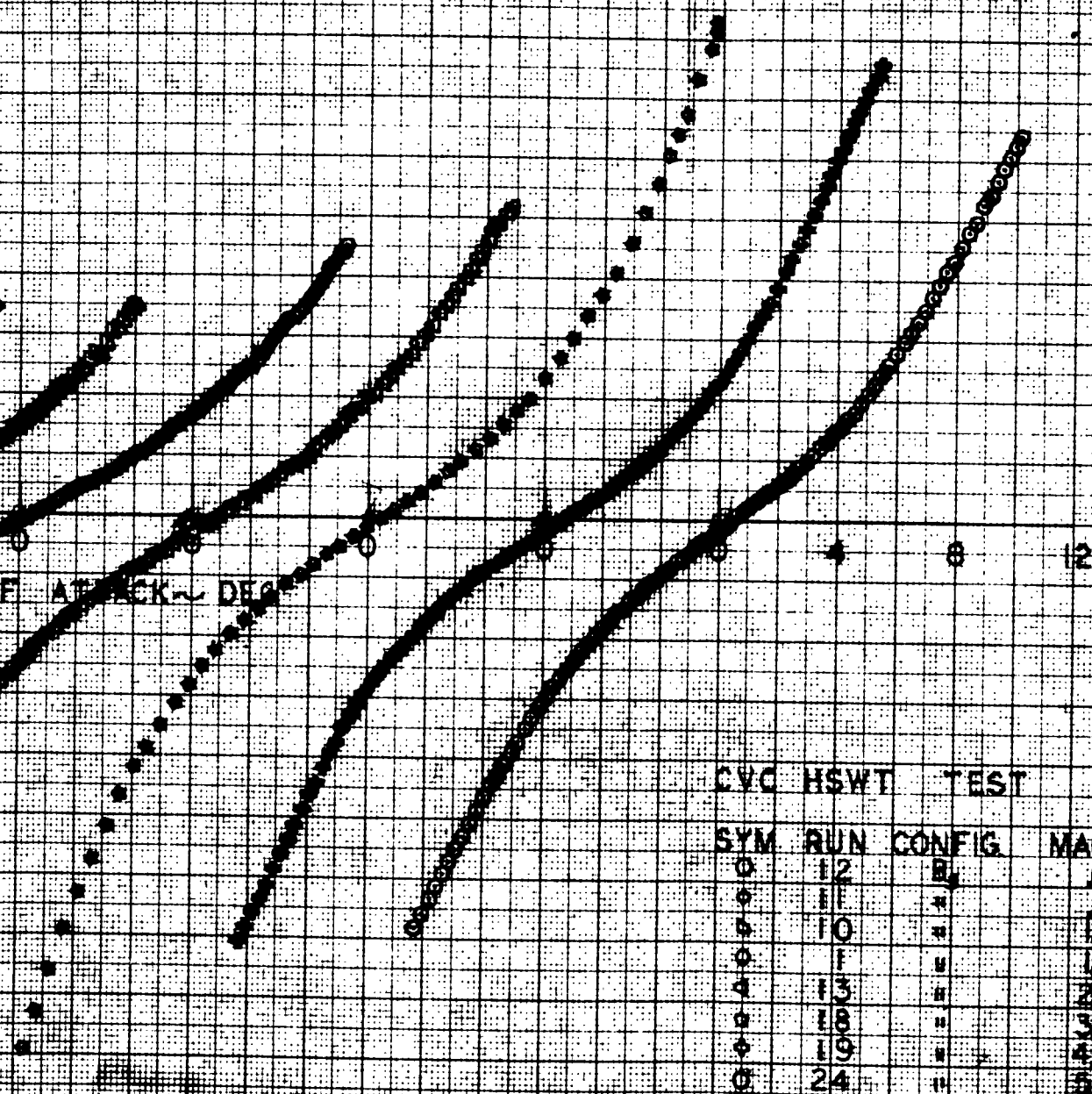
TEST RUNS - PLOTTED DATA

PLOTTED DATA INDEX

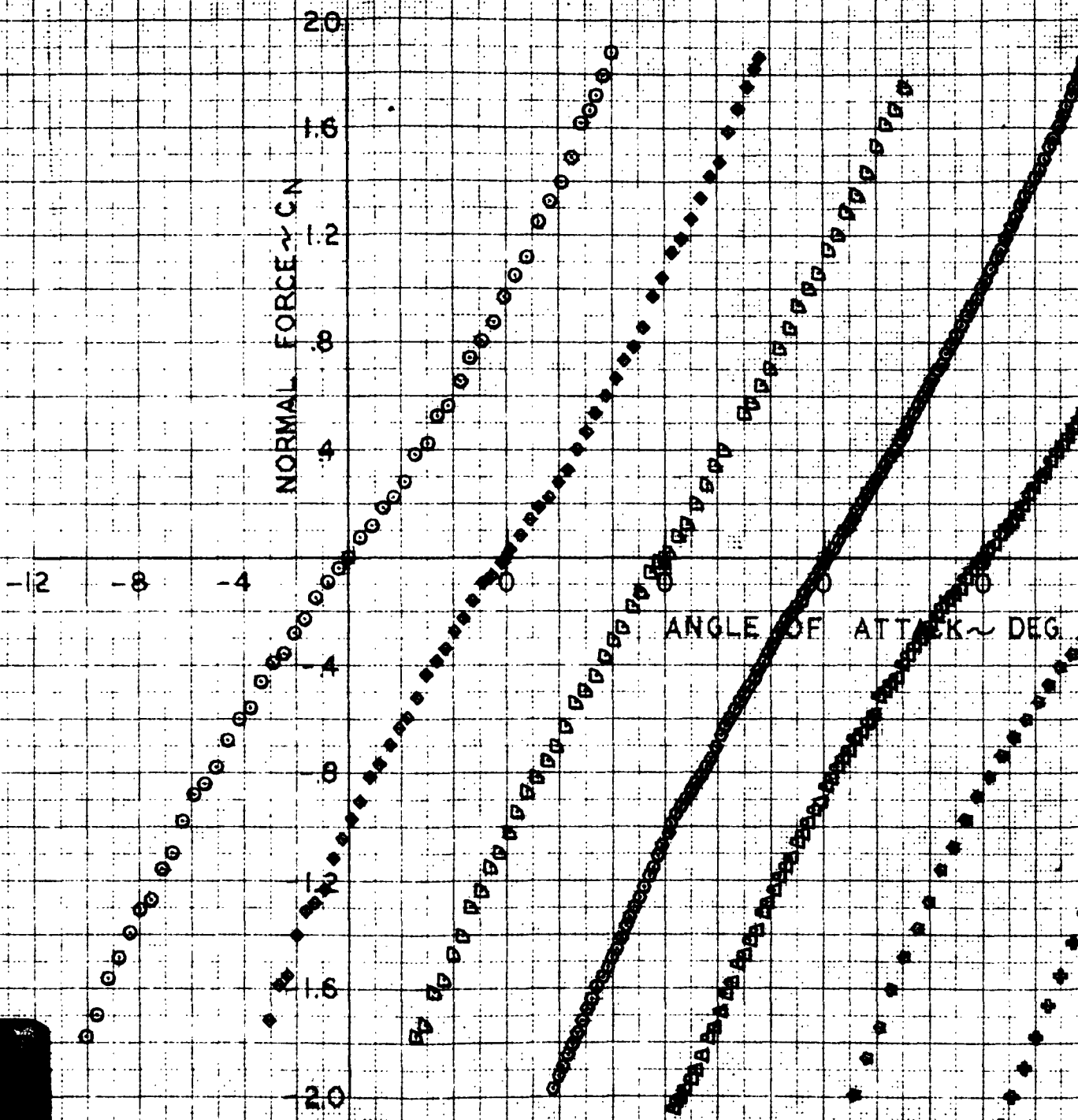
Run No.	Conf.	M	Δ_F	Page Number			
				C_F/α	C_m/α	C_l/α	C_A/α
12	B ₃	0.6	-	35	39	43	47
11		0.8	-				
10		1.0	-				
1		1.2	-				
13		2.0	-				
18		3.0	-				
19		4.0	-				
24	5.0	-					
29	B ₃ F ₂	0.6	0	36	40	44	48
8		0.8	"				
9		1.0	"				
2		1.2	"				
14		2.0	"				
17		3.0	"				
20		4.0	"				
23	5.0	"					
6	B ₃ F ₂	0.6	3	37	41	45	49
5		0.8	"				
4		1.0	"				
3		1.2	"				
15		2.0	"				
16		3.0	"				
21		4.0	"				
22	5.0	"					
28	B ₄	2.0	-	38	42	46	50
27		3.0	-				
26		4.0	-				
25		5.0	-				

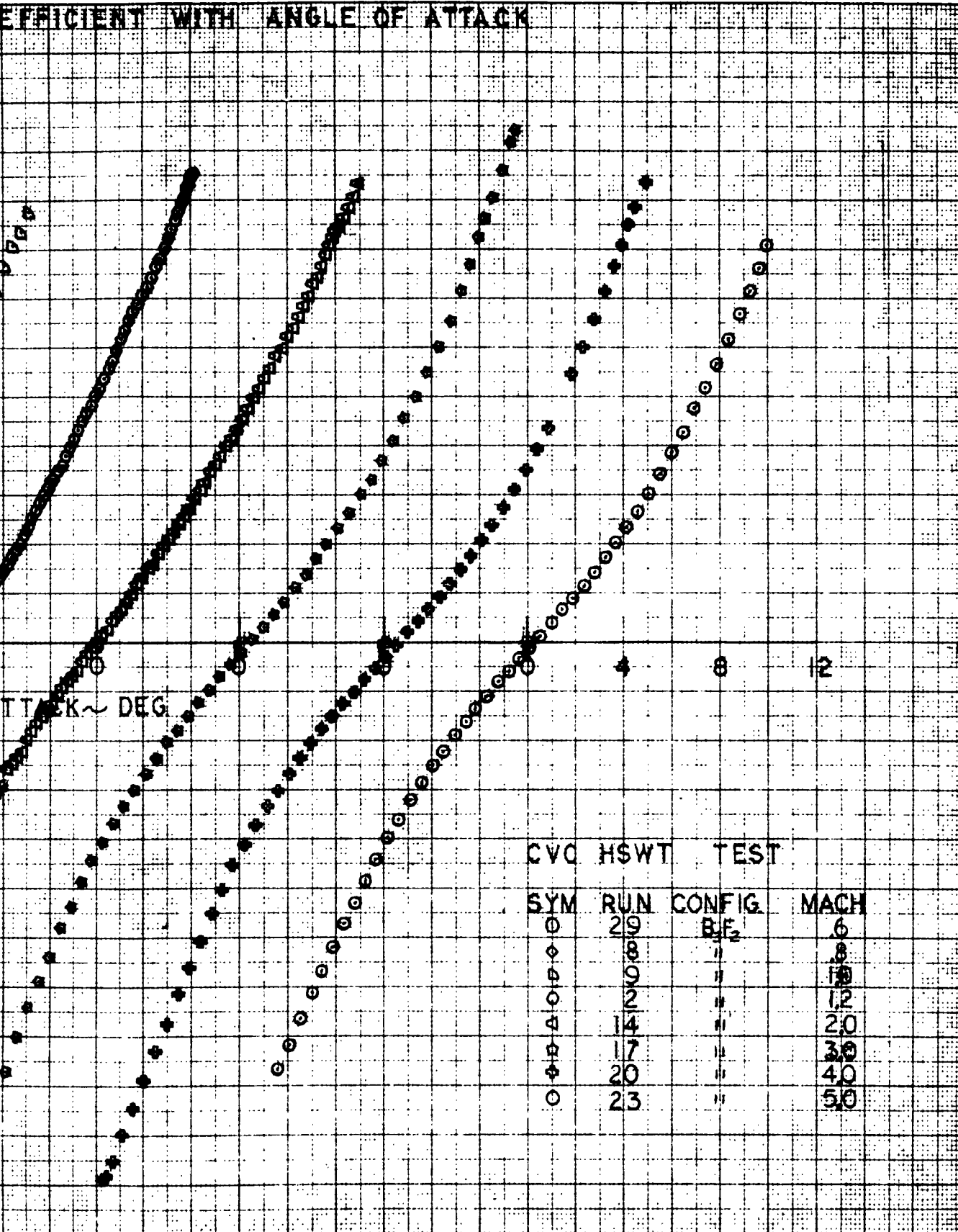


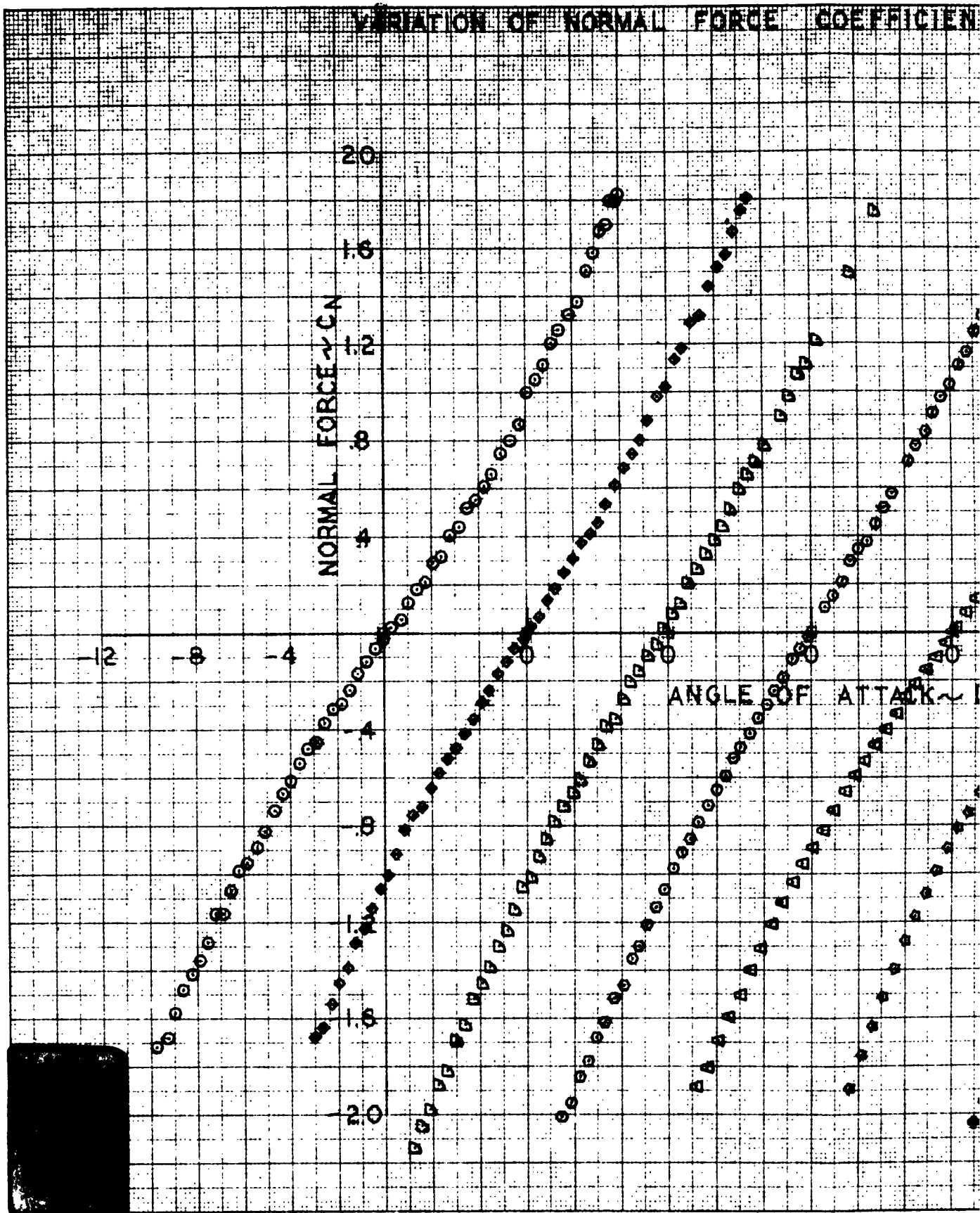
COEFFICIENT WITH ANGLE OF ATTACK



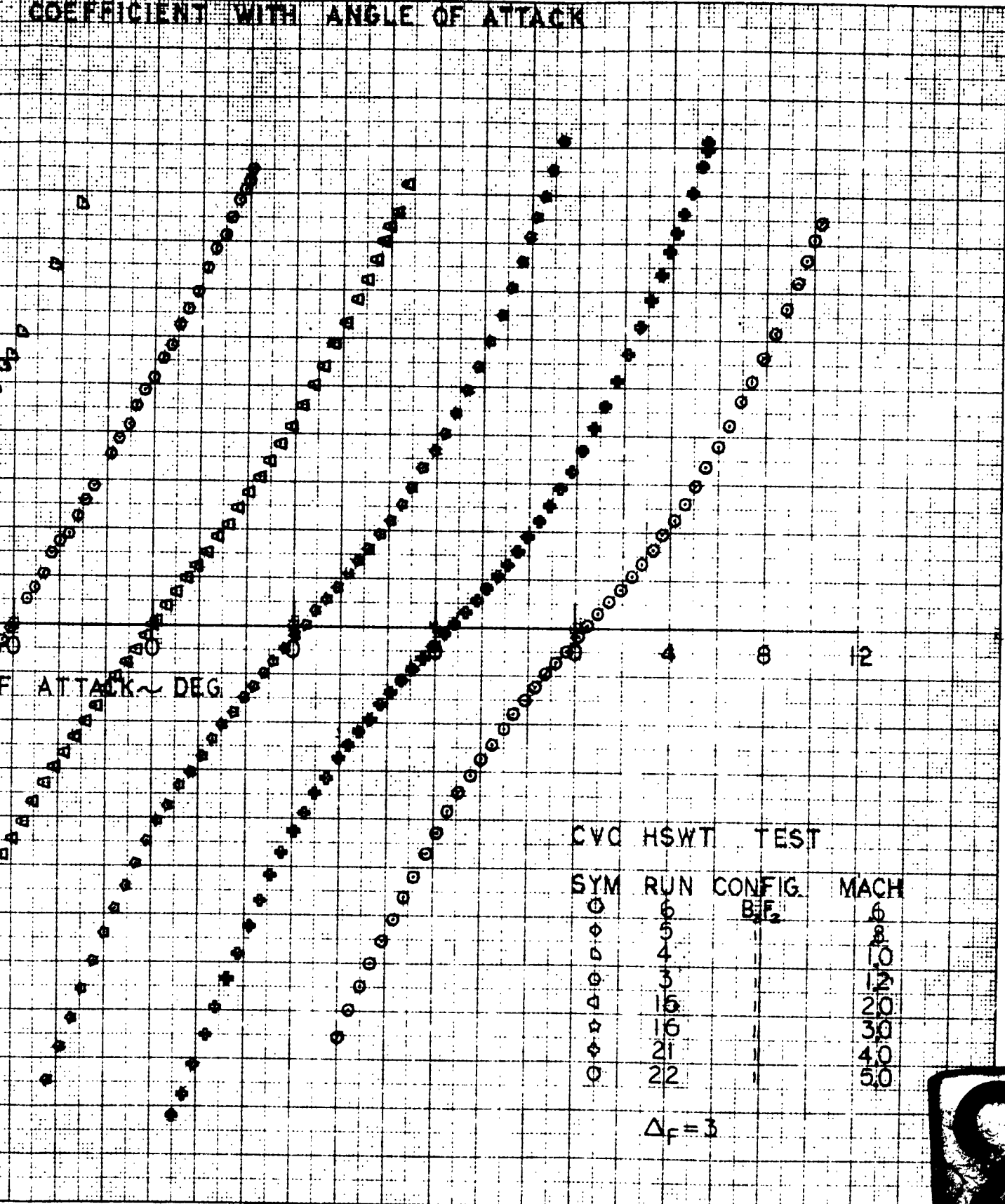
VARIATION OF NORMAL FORCE COEFFICIENT



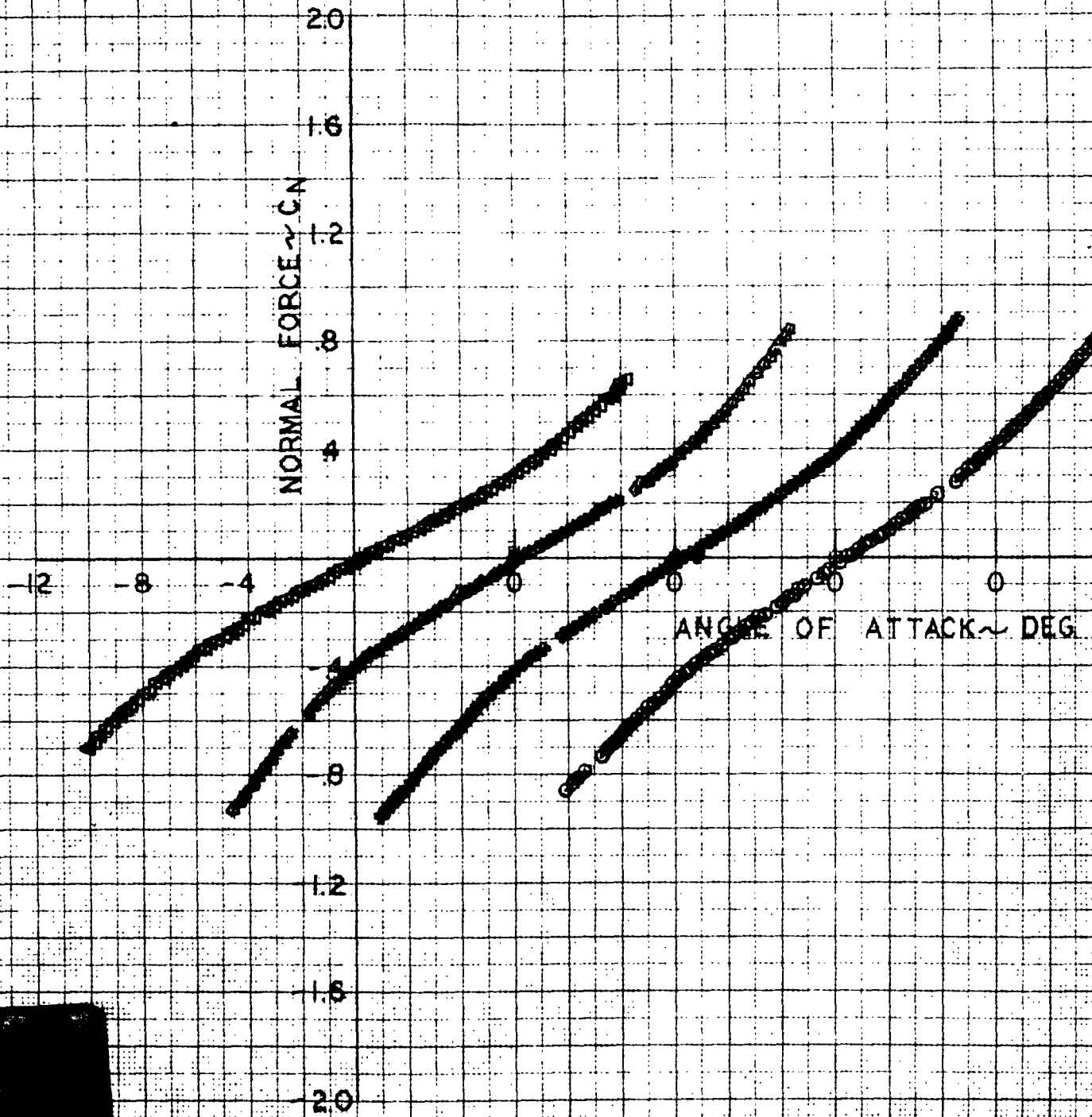




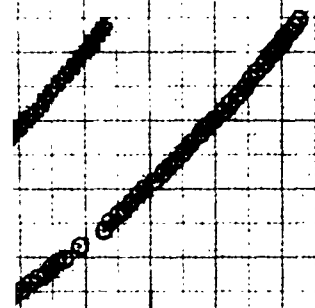
COEFFICIENT WITH ANGLE OF ATTACK



VARIATION OF NORMAL FORCE COEFFICIENT WITH



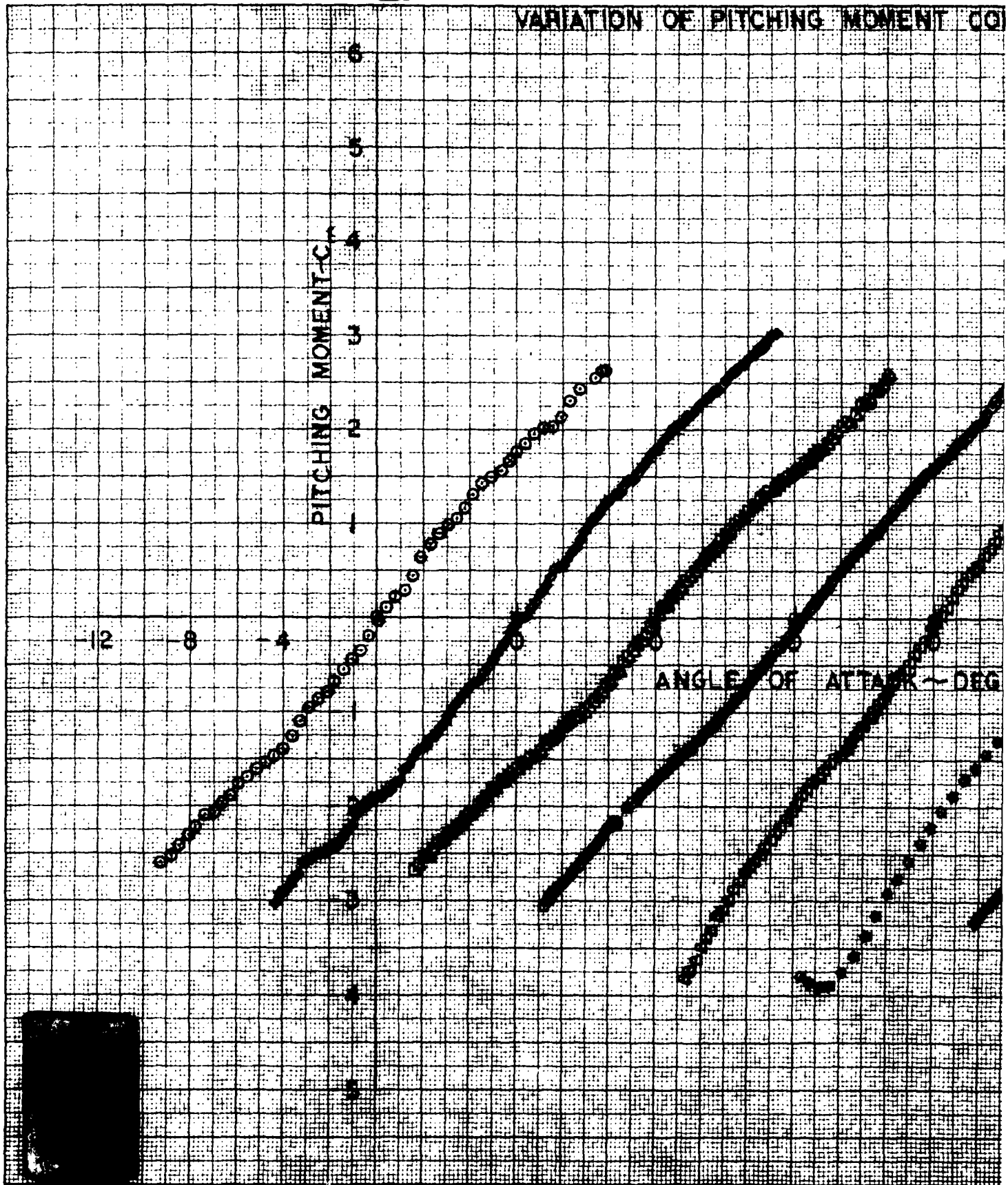
EFFICIENT WITH ANGLE OF ATTACK



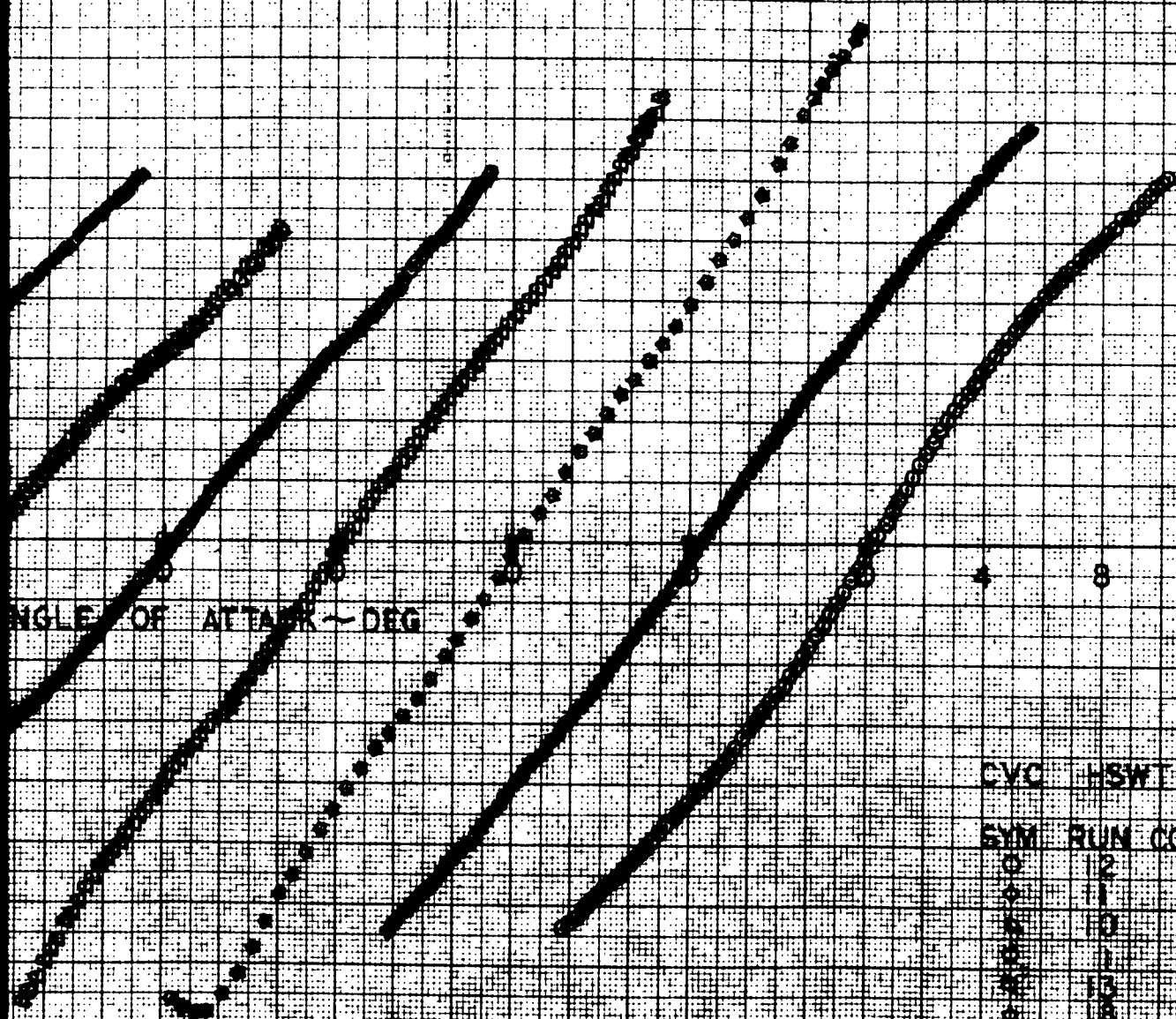
ATTACK ~ DEG

CVC	HSWT	TEST	
SYM	RUN	CONFIG	MACH
4	28	B.	20
4	27	*	30
4	26	*	40
0	25	*	50





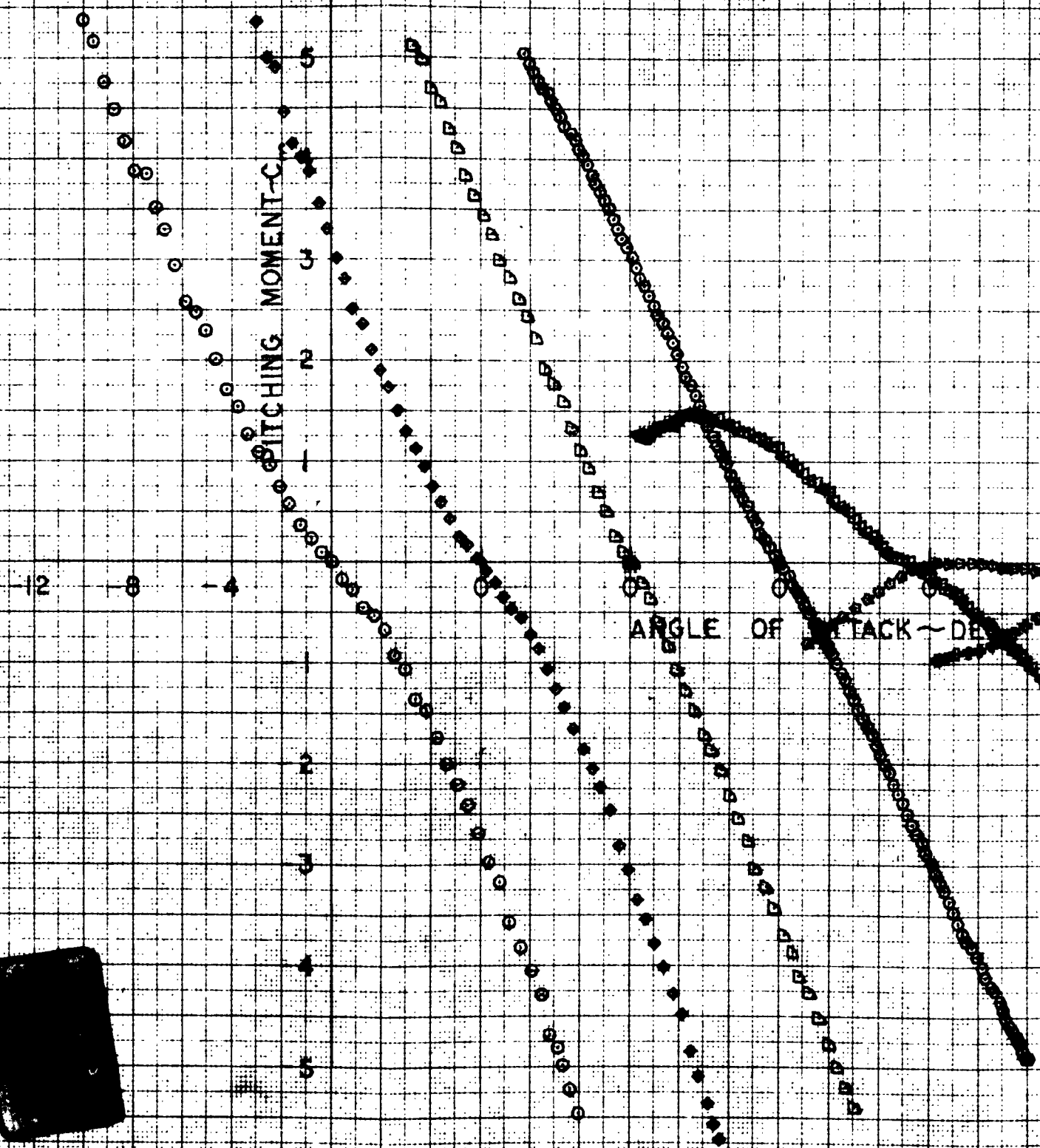
OF PITCHING MOMENT COEFFICIENT WITH ANGLE OF ATTACK



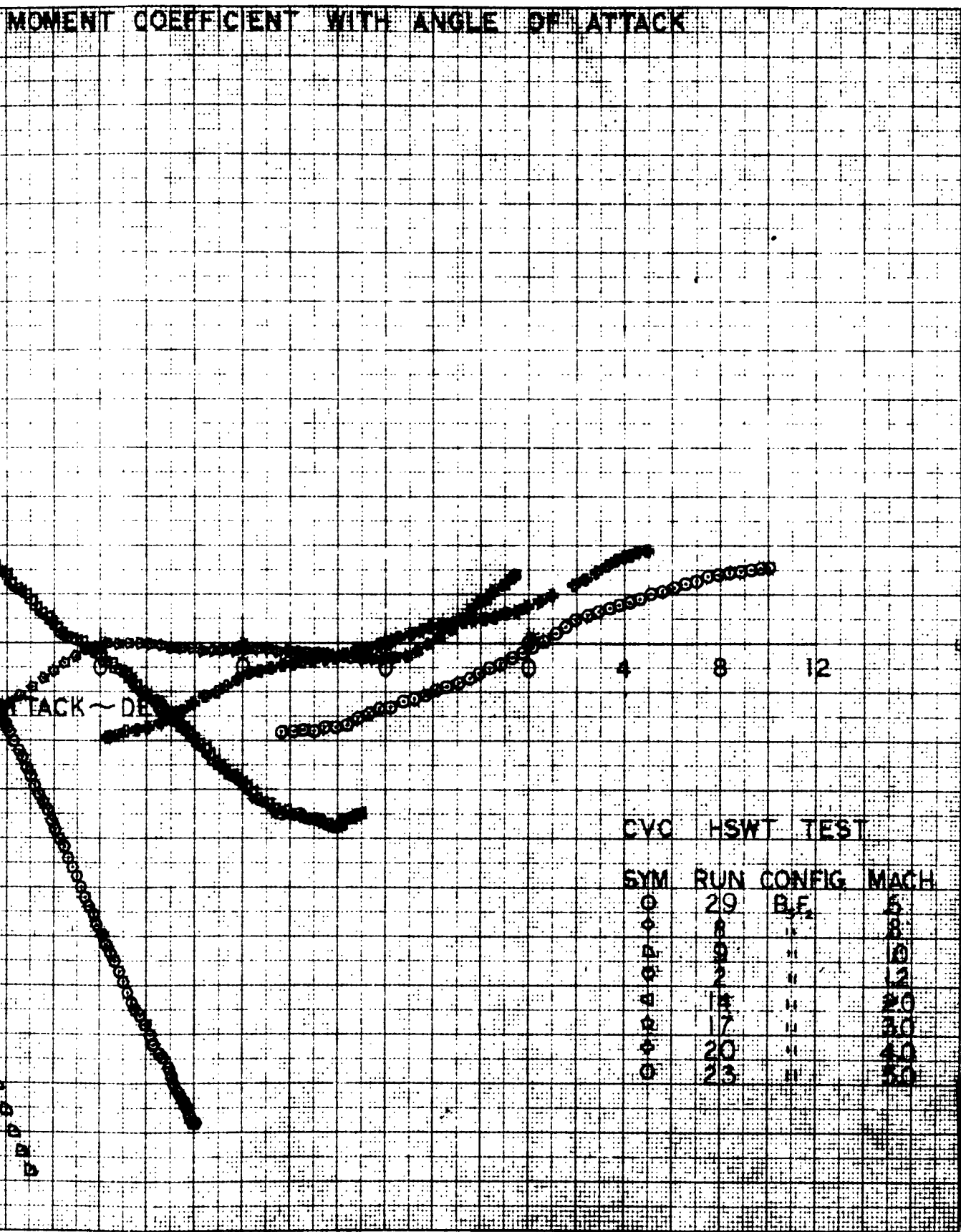
ANGLE OF ATTACK ~ DEG

CVC	HSWT	TEST
10	12	8
11	11	8
12	10	8
13	11	8
14	13	8
15	19	8
16	19	8
17	24	8

VARIATION OF PITCHING MOMENT COEFFICIENT

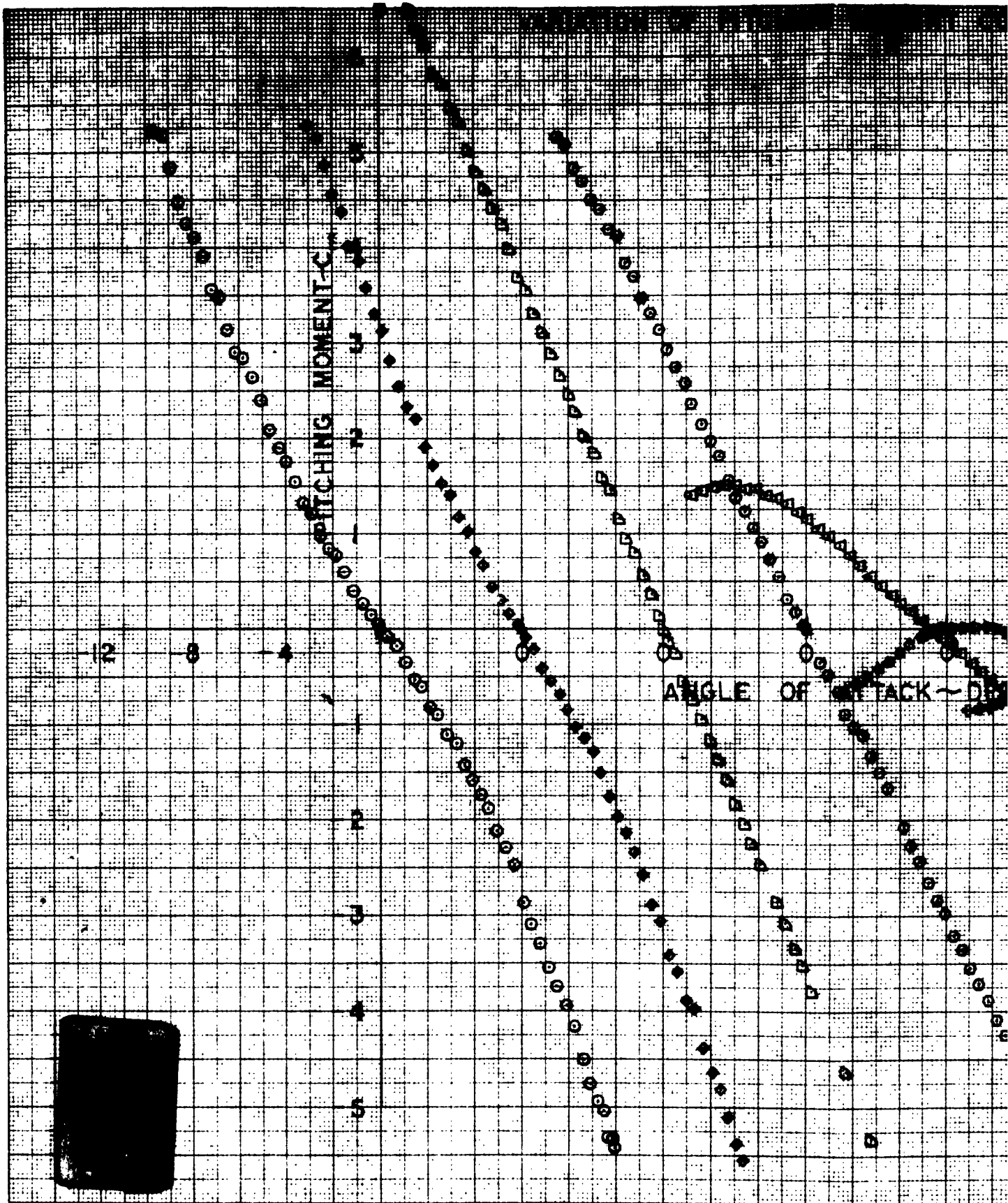


MOMENT COEFFICIENT WITH ANGLE OF ATTACK

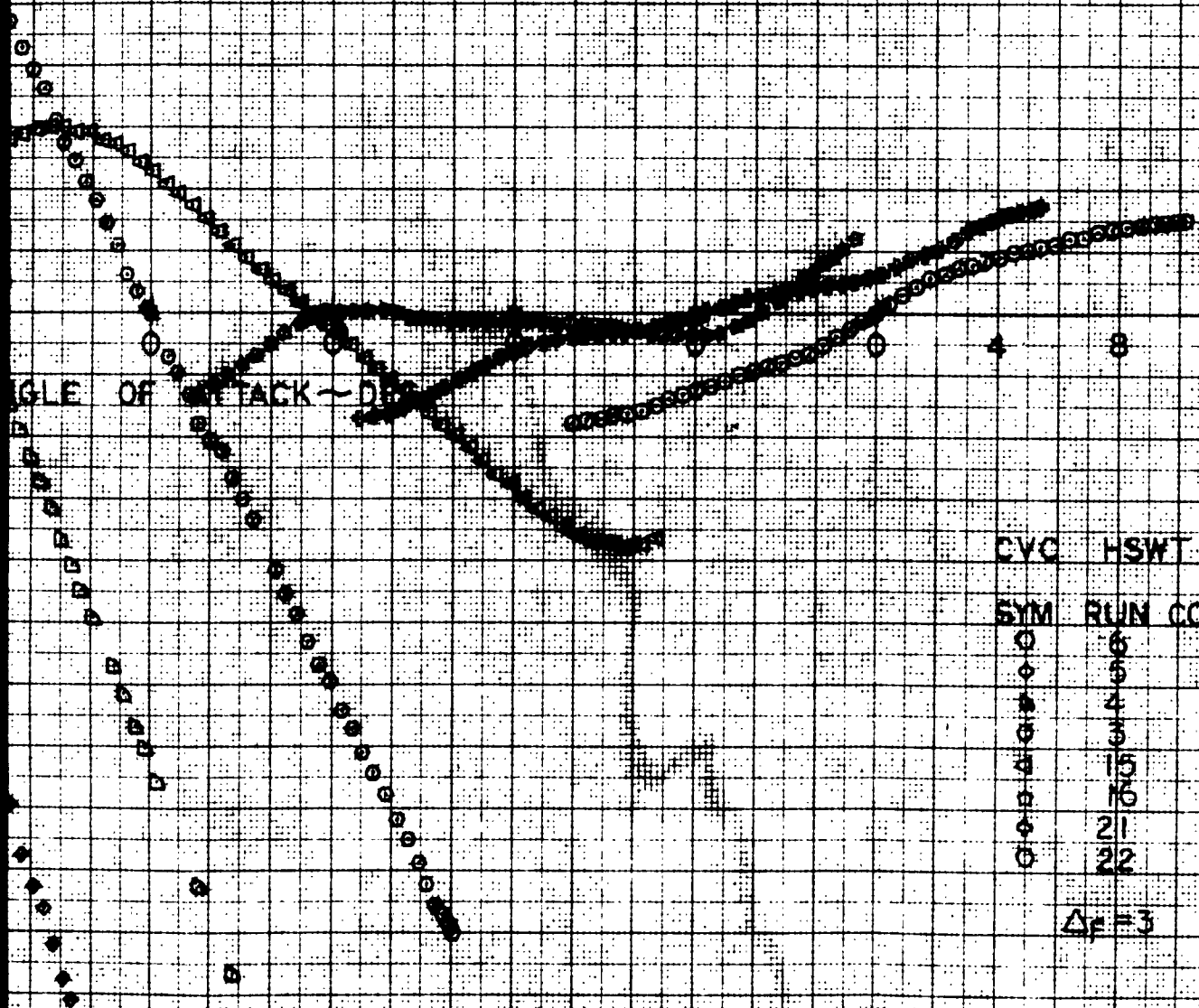


CYC	HSWT	TEST	
SYM	RUN	CONFIG	MACH
○	29	B.F.	5
◇	8	"	8
□	9	"	10
○	2	"	12
○	14	"	20
○	17	"	30
○	20	"	40
○	23	"	50





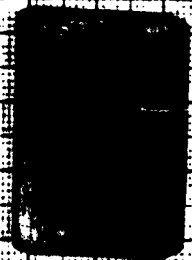
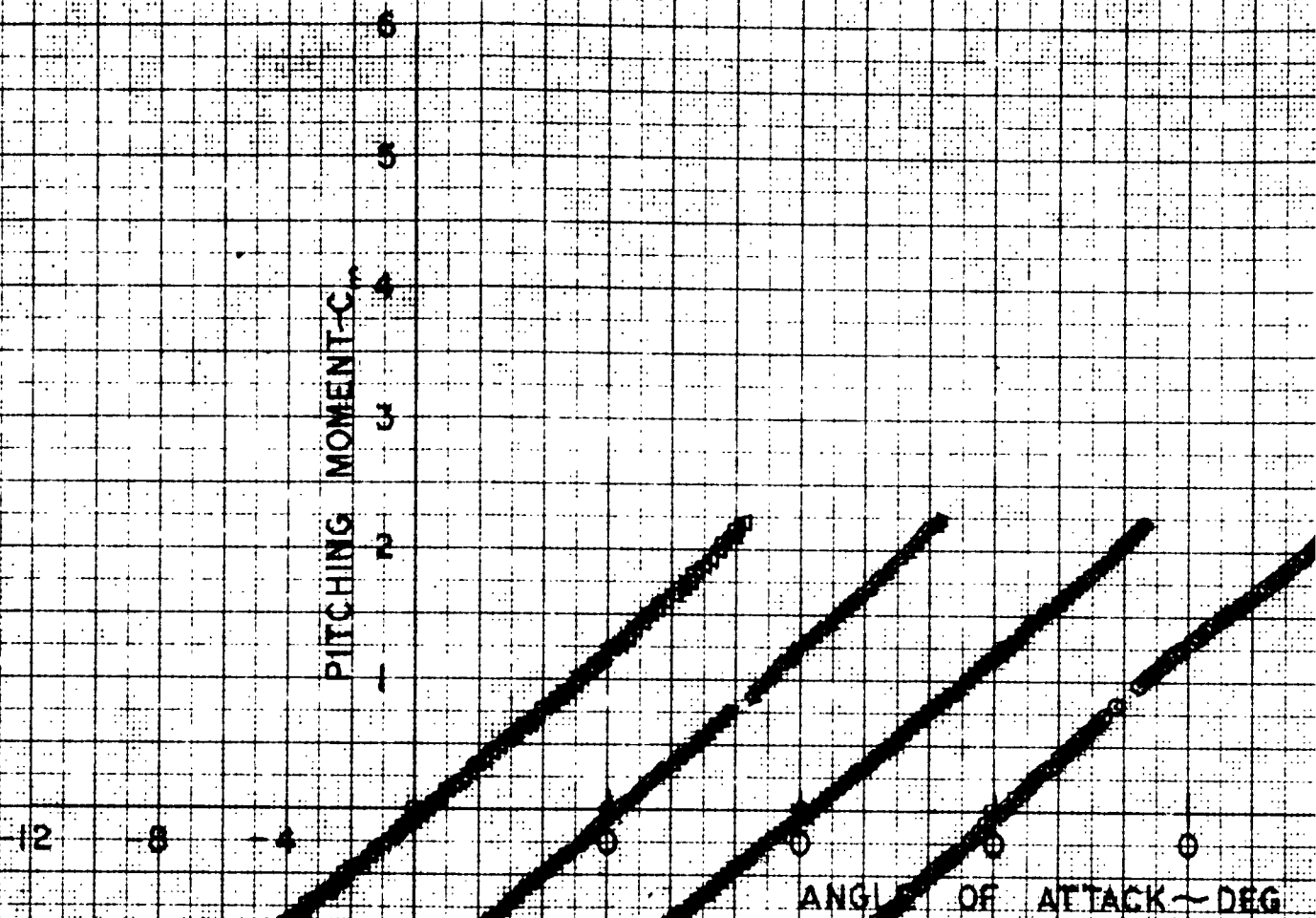
ANGLE OF ATTACK - DEGREE



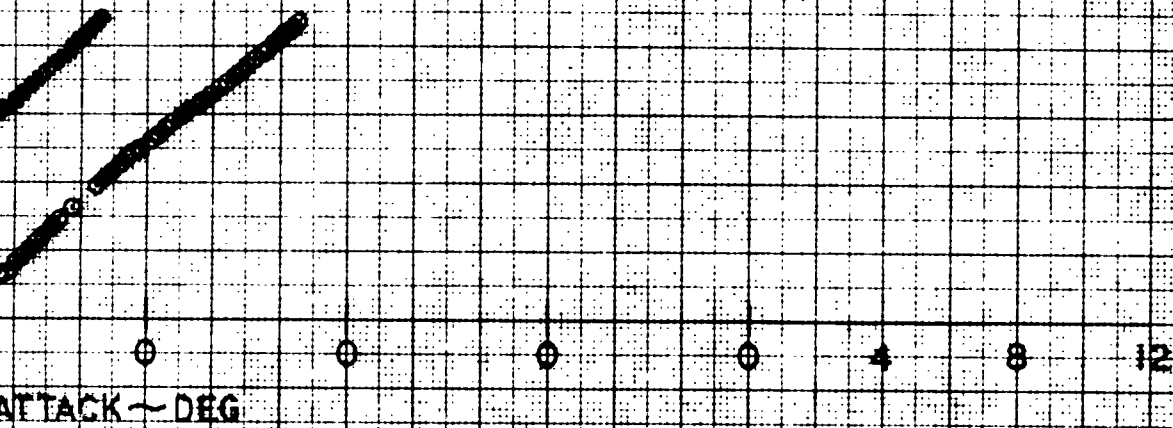
CVC	HSWT
SYM	RUN CON
0	6
0	9
0	4
0	3
0	15
0	16
0	21
0	22

$\Delta r = 3$

VARIATION OF PITCHING MOMENT COEFF

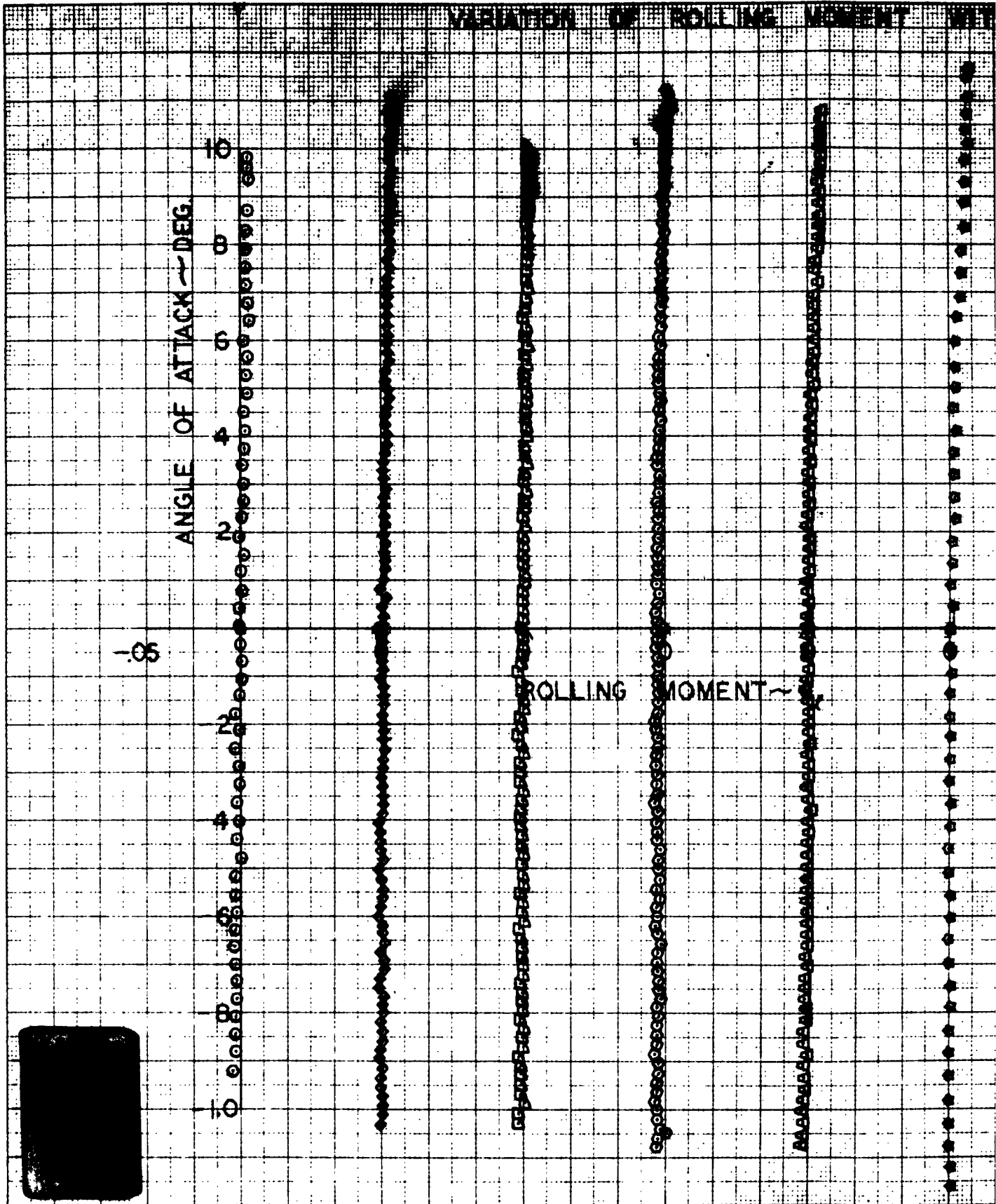


MOMENT COEFFICIENT WITH ANGLE OF ATTACK

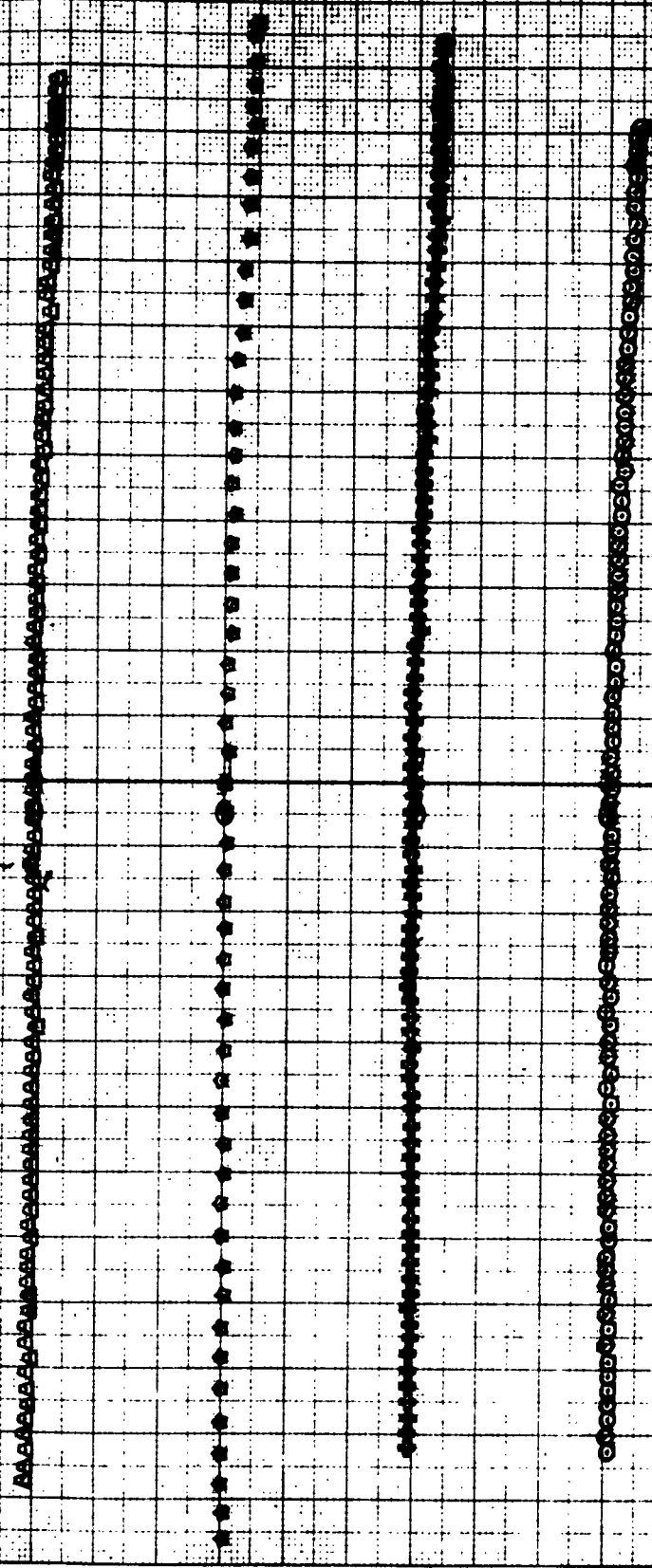


CVC	HSWT	TEST
SYM	RUN	CONFIG
4	28	B*
4	27	II
4	26	*
0	25	II





MOMENT WITH ANGLE OF ATTACK



.05 .10 .15 .20 .25

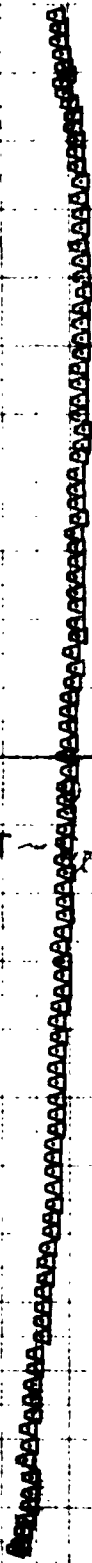
CVC	HSWT	TEST	
SYM	RUN	CONFIG	MACH
○	12	B ₃	6
◇	11	*	8
◊	10	*	10
◐	1	*	12
◑	13	*	20
◒	18	*	30
◓	19	*	40
◔	24	*	50

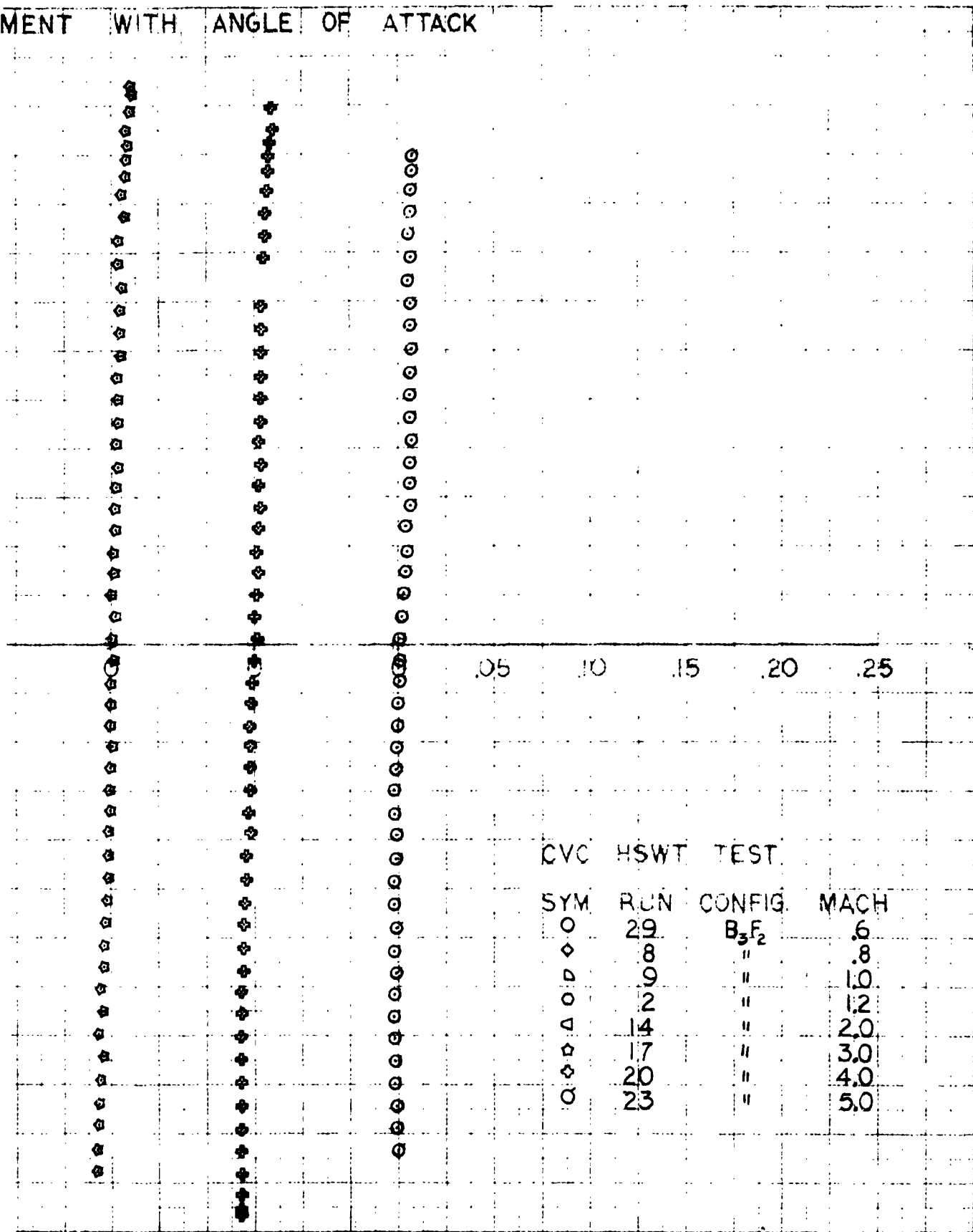


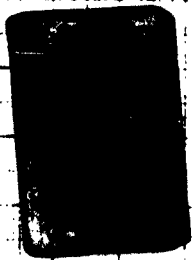
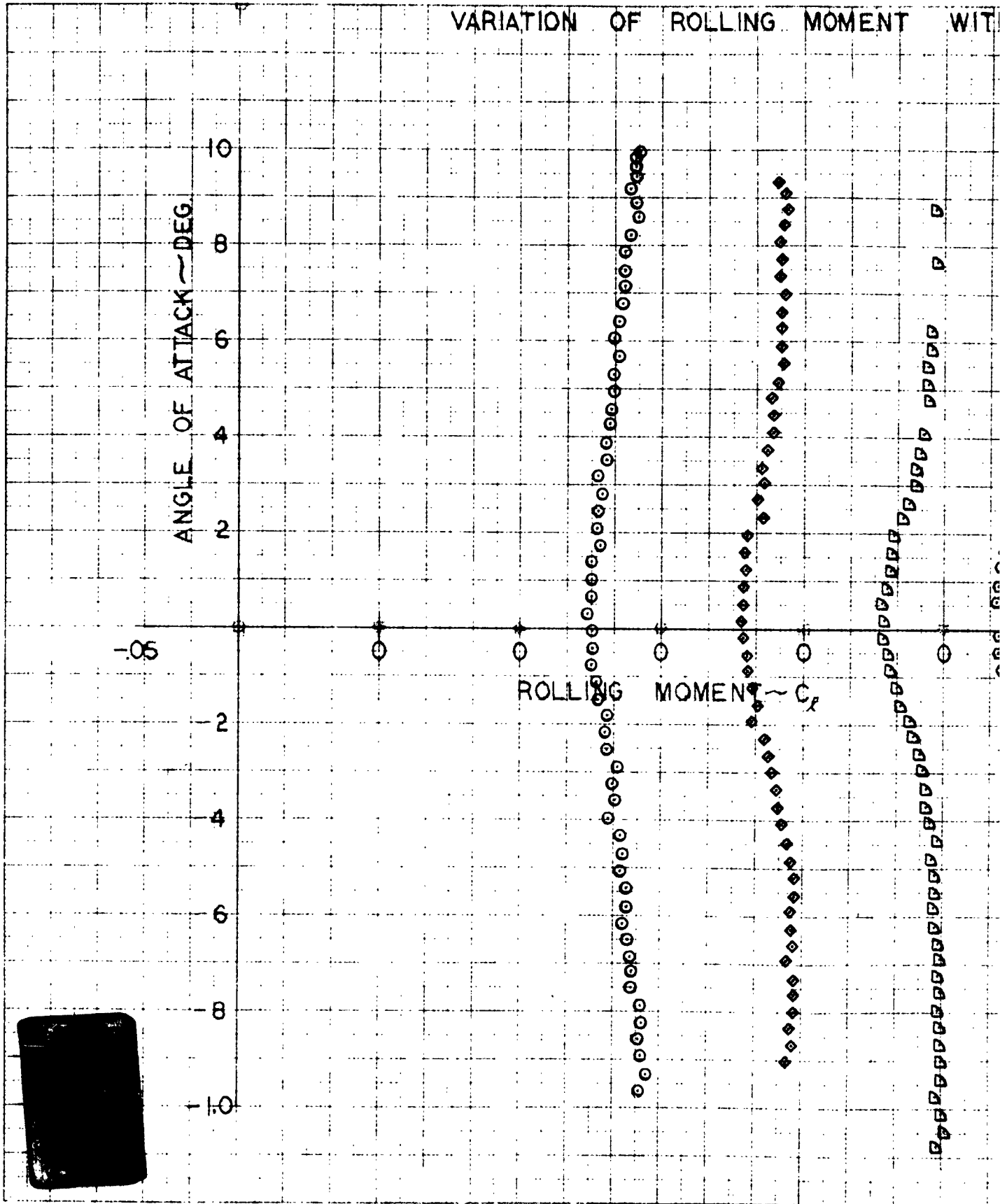
VARIATION OF ROLLING MOMENT WITH AN

ANGLE OF ATTACK ~ DEG.

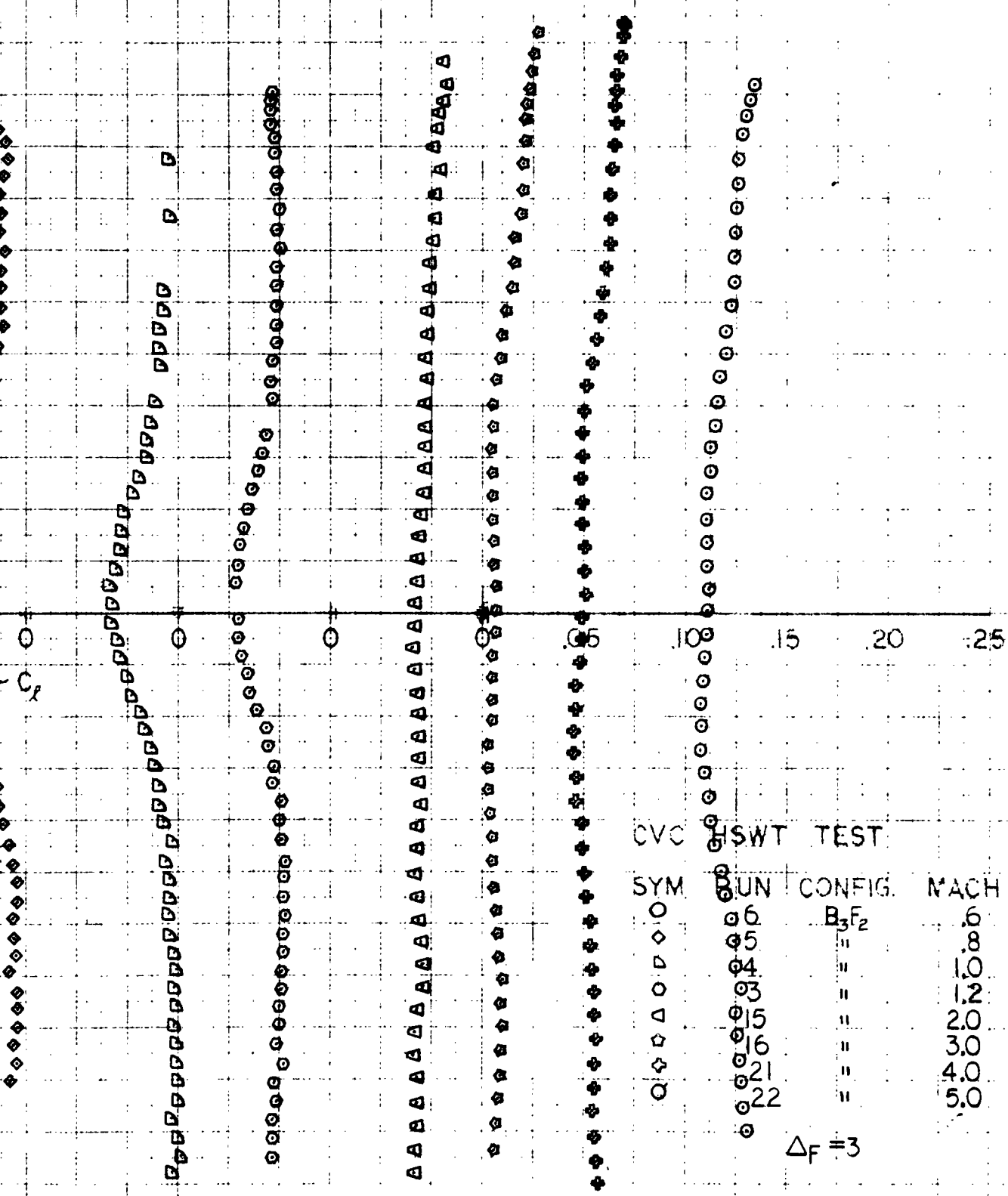
-05







MOMENT WITH ANGLE OF ATTACK



CVC SWT TEST

SYM	CONF.	MACH
○	B ₃ F ₂	.6
◇	"	.8
△	"	1.0
☆	"	1.2
□	"	2.0
⬠	"	3.0
⬡	"	4.0
⊙	"	5.0

$\Delta F = 3$



VARIATION OF ROLLING MOMENT WITH A

ANGLE OF ATTACK ~ DEG.

-05

10

ROLLING MOMENT ~ C_r



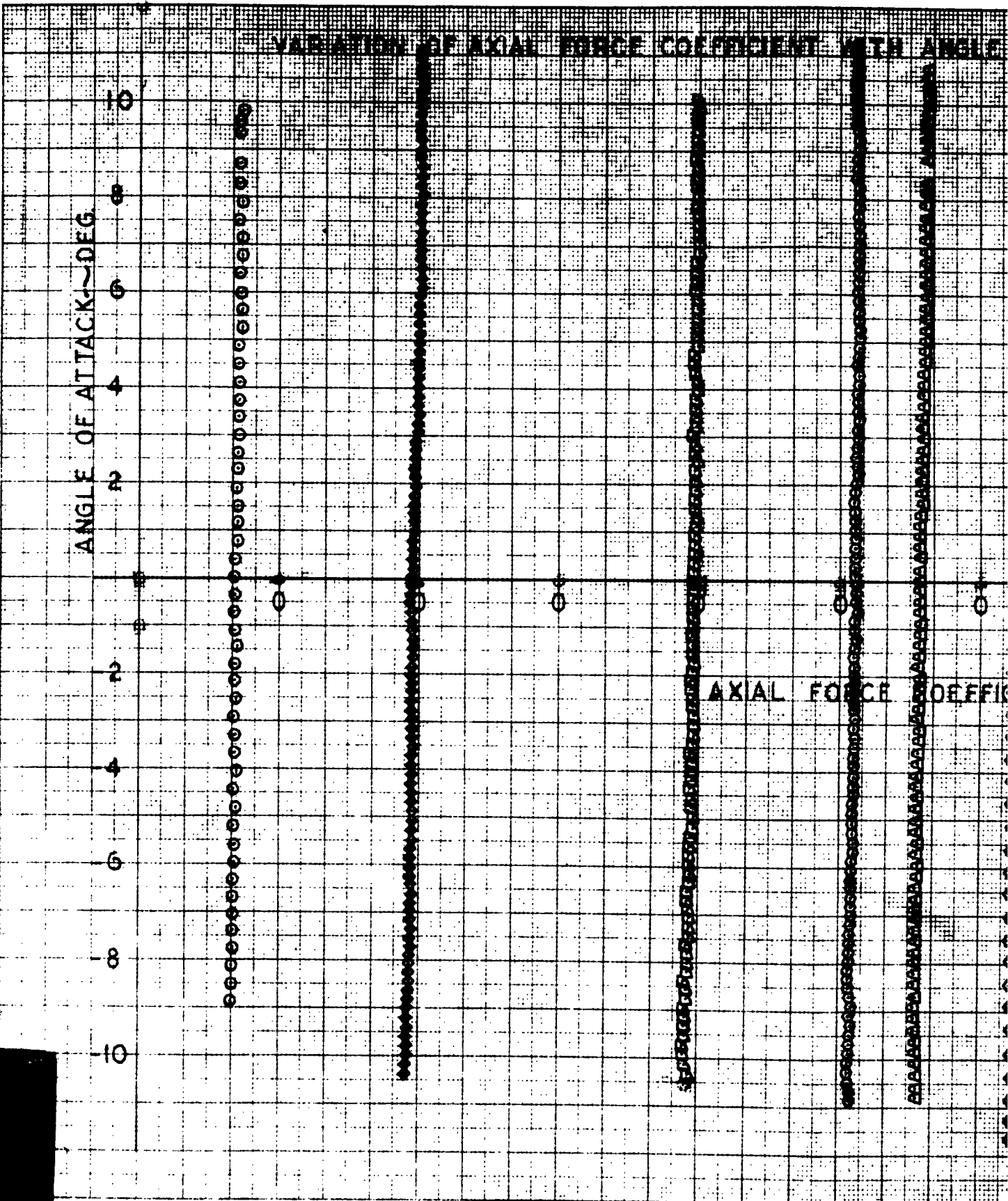
MENT WITH ANGLE OF ATTACK

0 0 0 .05 .10 .15 .20 .25

CVC HSWT TEST

SYM	RUN	CONFIG	MACH
4	28	B ₁	20
☆	27	↓	30
◇	26	•	40
○	25	■	50





ANGLE OF ATTACK

COEFFICIENT

.2 .4 .6 .8 1.0

CVC HSWT TEST

SYM	RUN	CONFIG	MACH
○	12	B ₃	6
◇	11	"	8
◊	10	"	10
○	1	"	12
△	13	"	20
☆	18	"	30
⊕	19	"	40
⊙	24	"	50

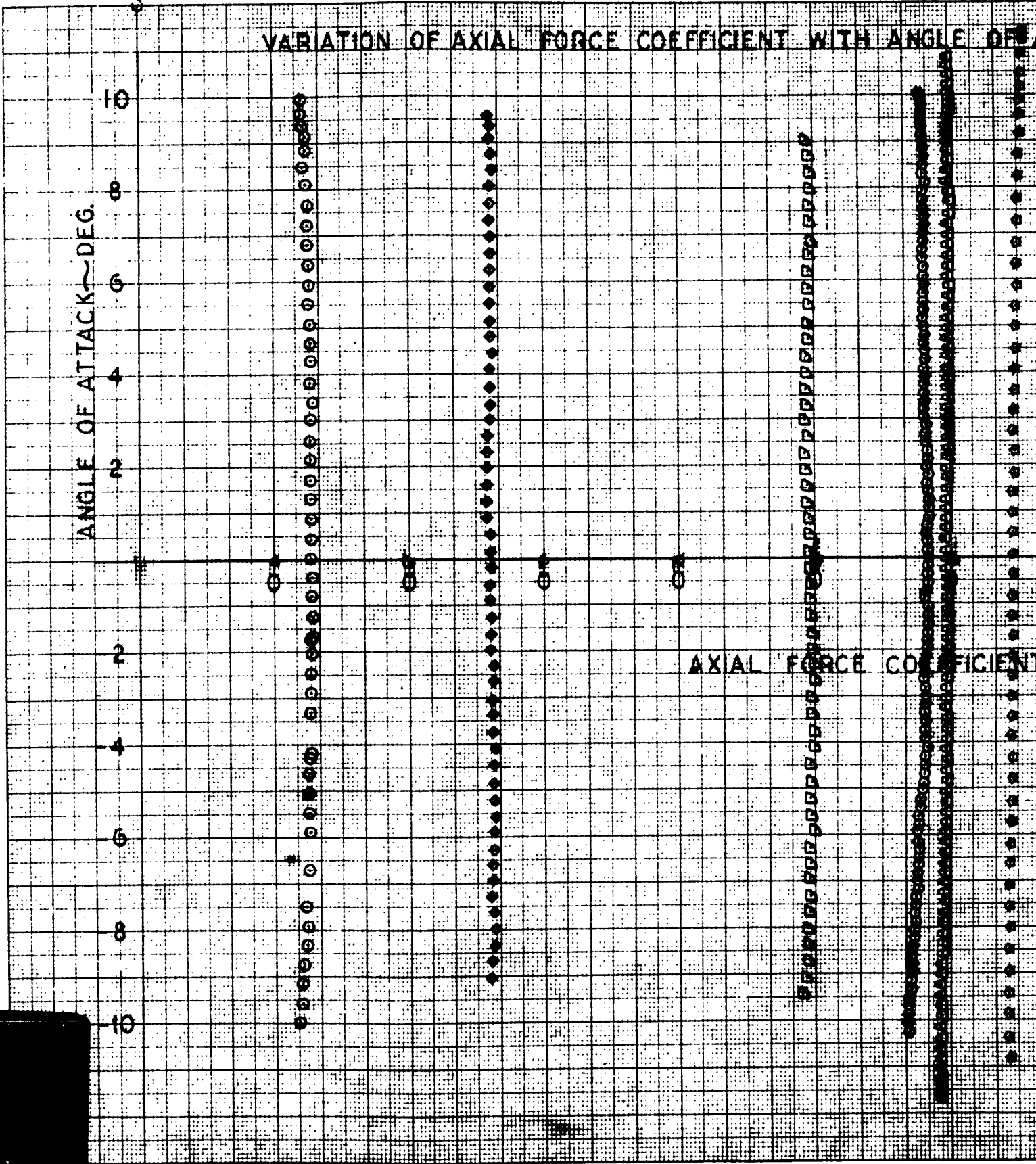


VARIATION OF AXIAL FORCE COEFFICIENT WITH ANGLE OF

ANGLE OF ATTACK ~ DEG.

10 8 6 4 2 0 2 4 6 8 10

AXIAL FORCE COEFFICIENT



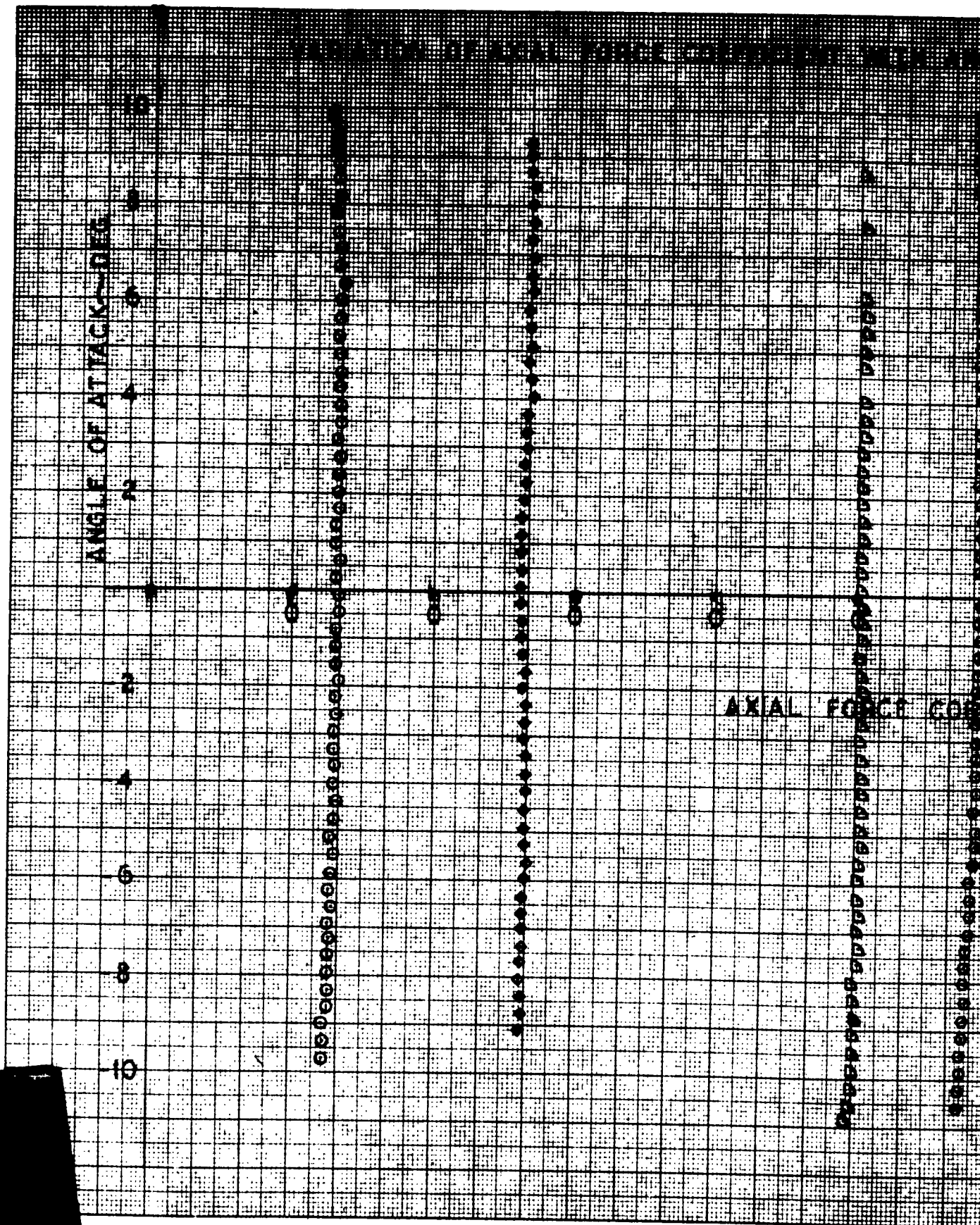
COEFFICIENT WITH ANGLE OF ATTACK

AL FORCE COEFFICIENT C_{A}

CVC HSWT TEST

SYM	REIN	CONFIG	MACH
0	25	B/E	5
1	25	"	8
2	25	"	10
3	25	"	12
4	14	"	20
5	17	"	30
6	20	"	40
7	23	"	50





AXIAL FORCE COEFFICIENT - C_A

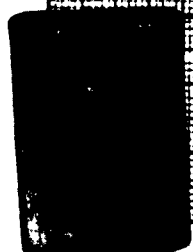
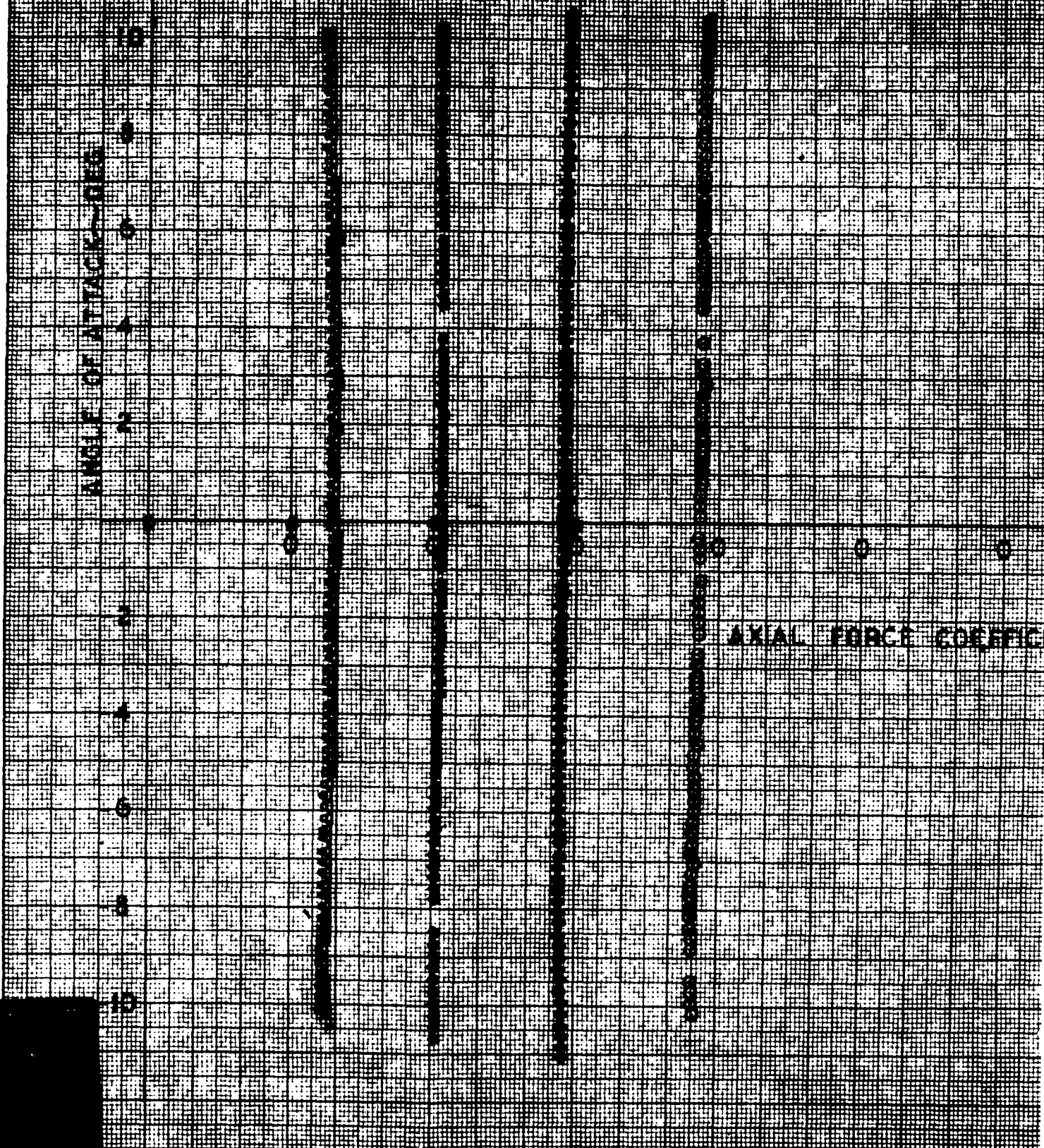
CVC HSWT TEST

SYM	RUN	CONFIG	MACH
0	6	B ₁ F ₂	6
0	7	"	8
0	8	"	10
0	9	"	12
0	15	"	20
0	16	"	30
0	21	"	40
0	22	"	50

$\Delta x = 3$



VARIATION OF AXIAL FORCE COEFFICIENT WITH ANGLE



RIGHT WITH ANGLE OF ATTACK

ALL FORCE COEFFICIENT - C_A

CVG HSWT TEST

SYM	RUN	CONFIG	MACH
0	26	0	2.0
1	27	1	2.6
2	26	1	3.0
3	26	1	3.5

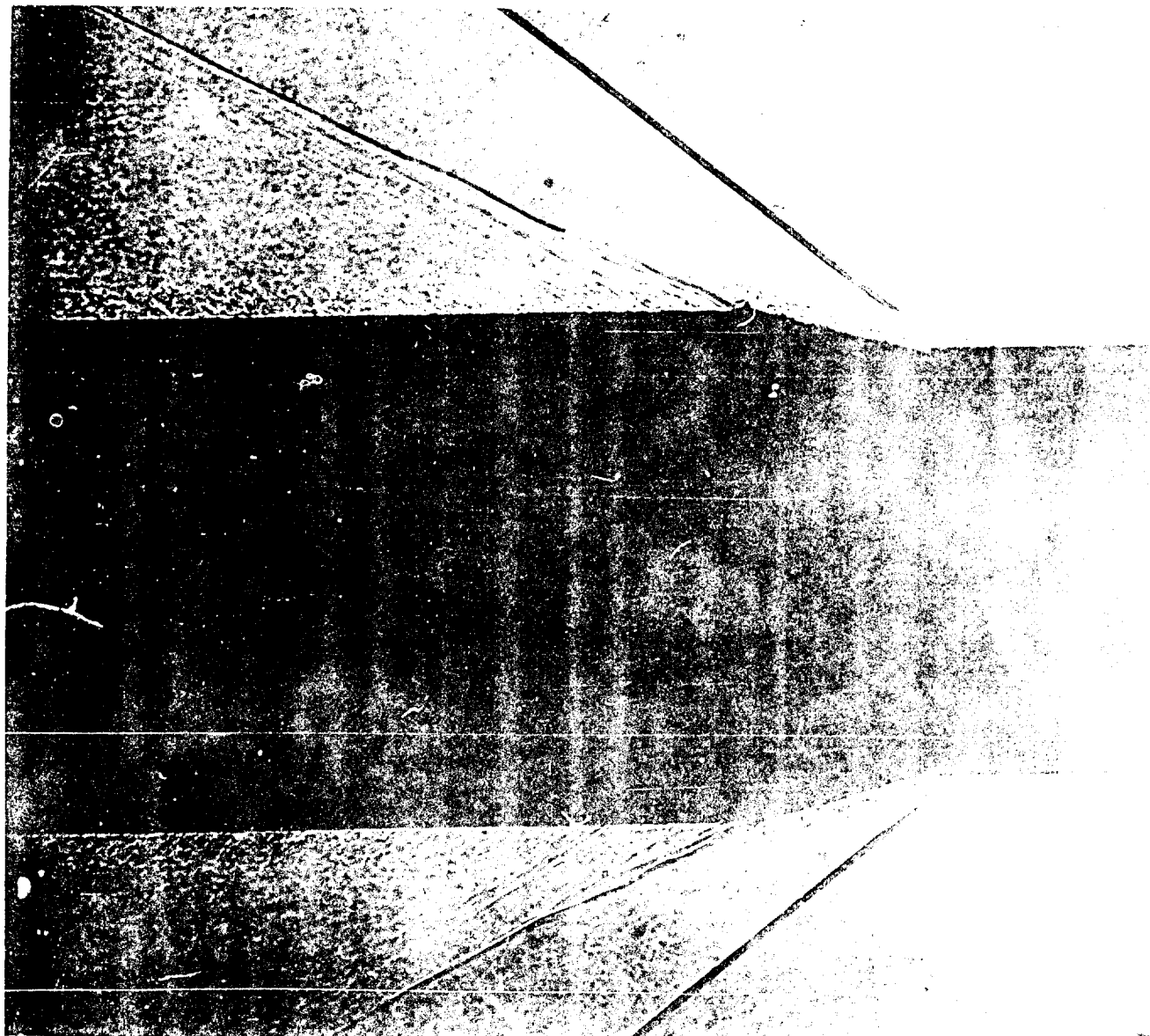


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APPENDIX IV

SCHLERIN PHOTOGRAPHS

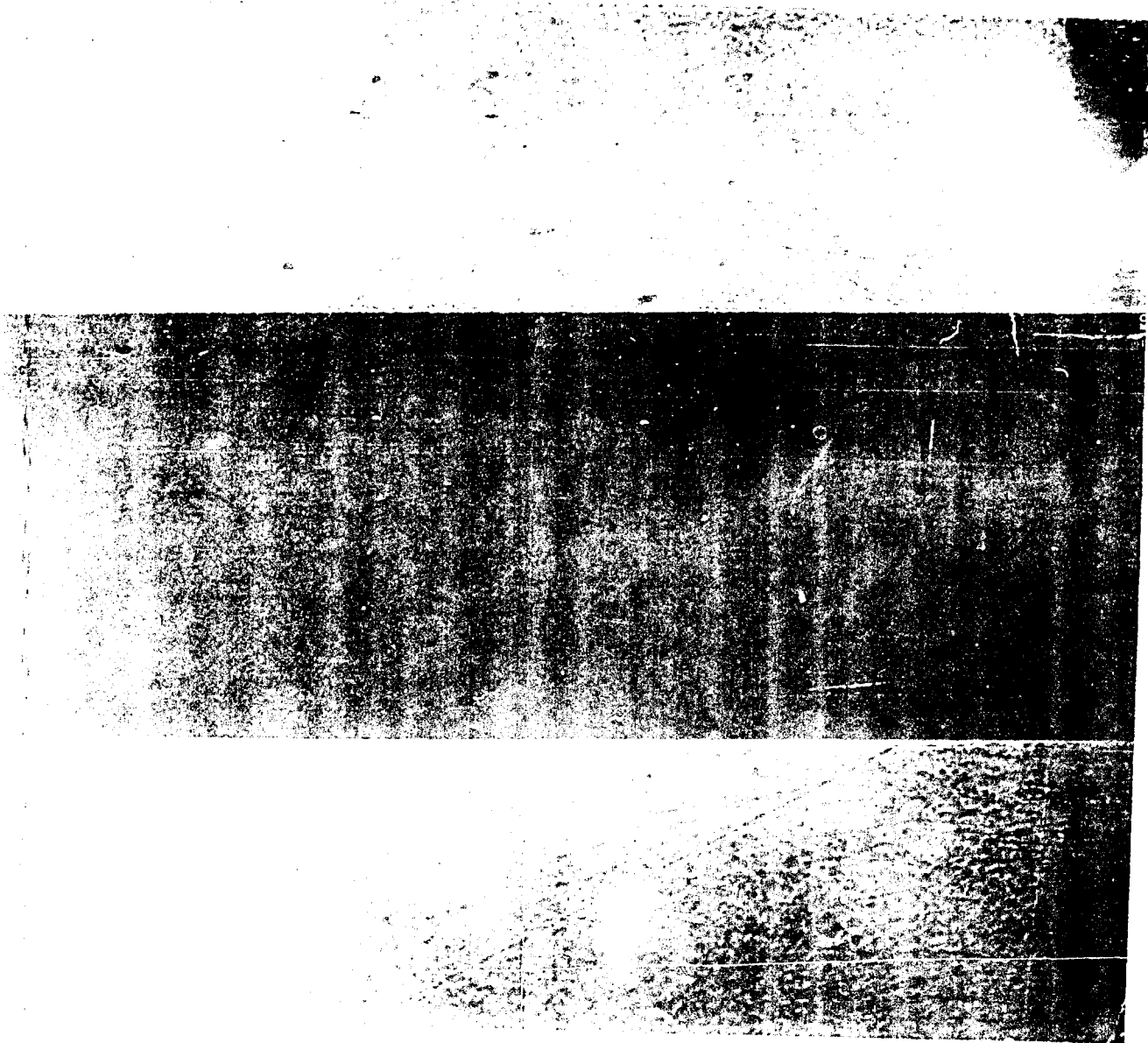
TDR-63-21



1

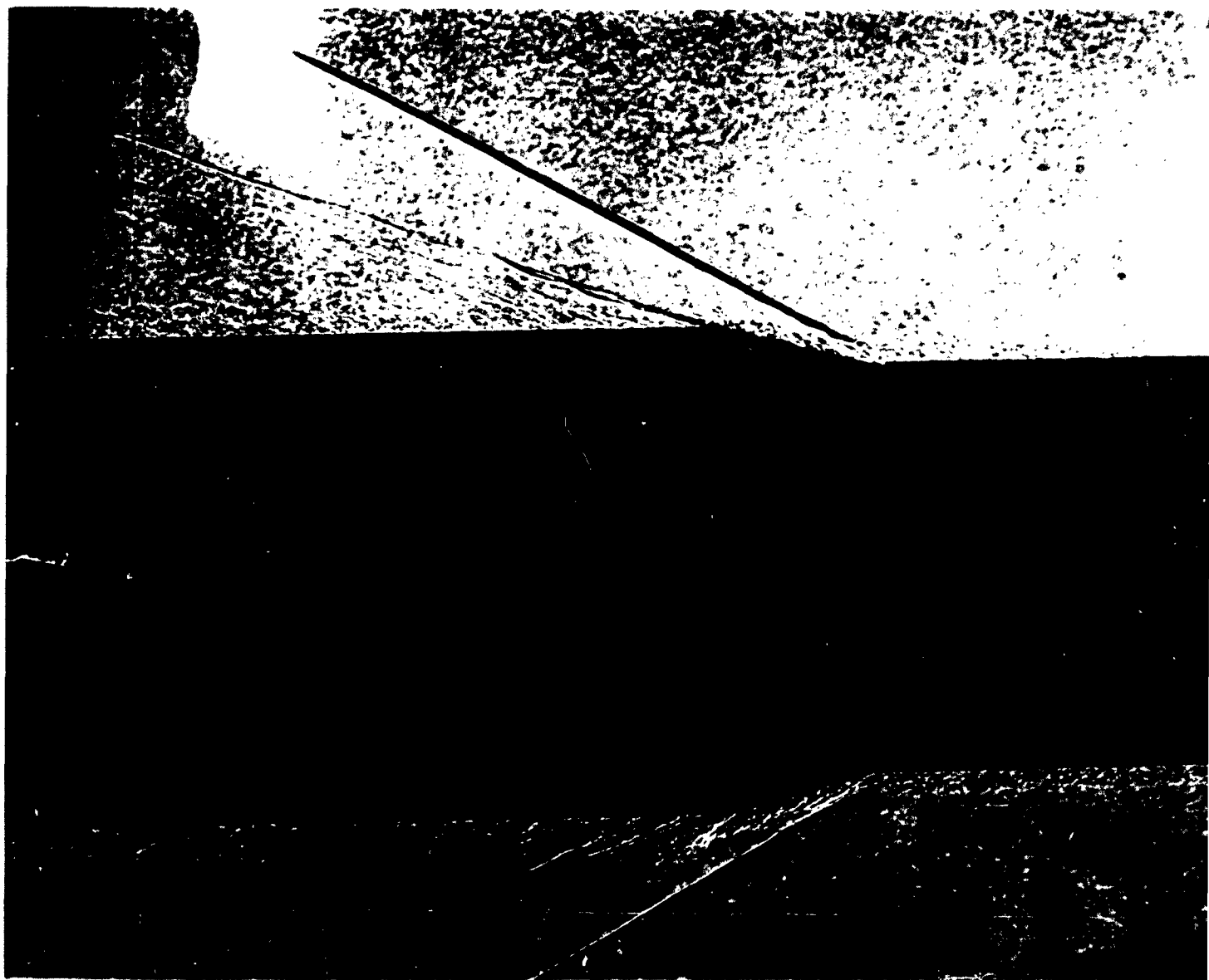


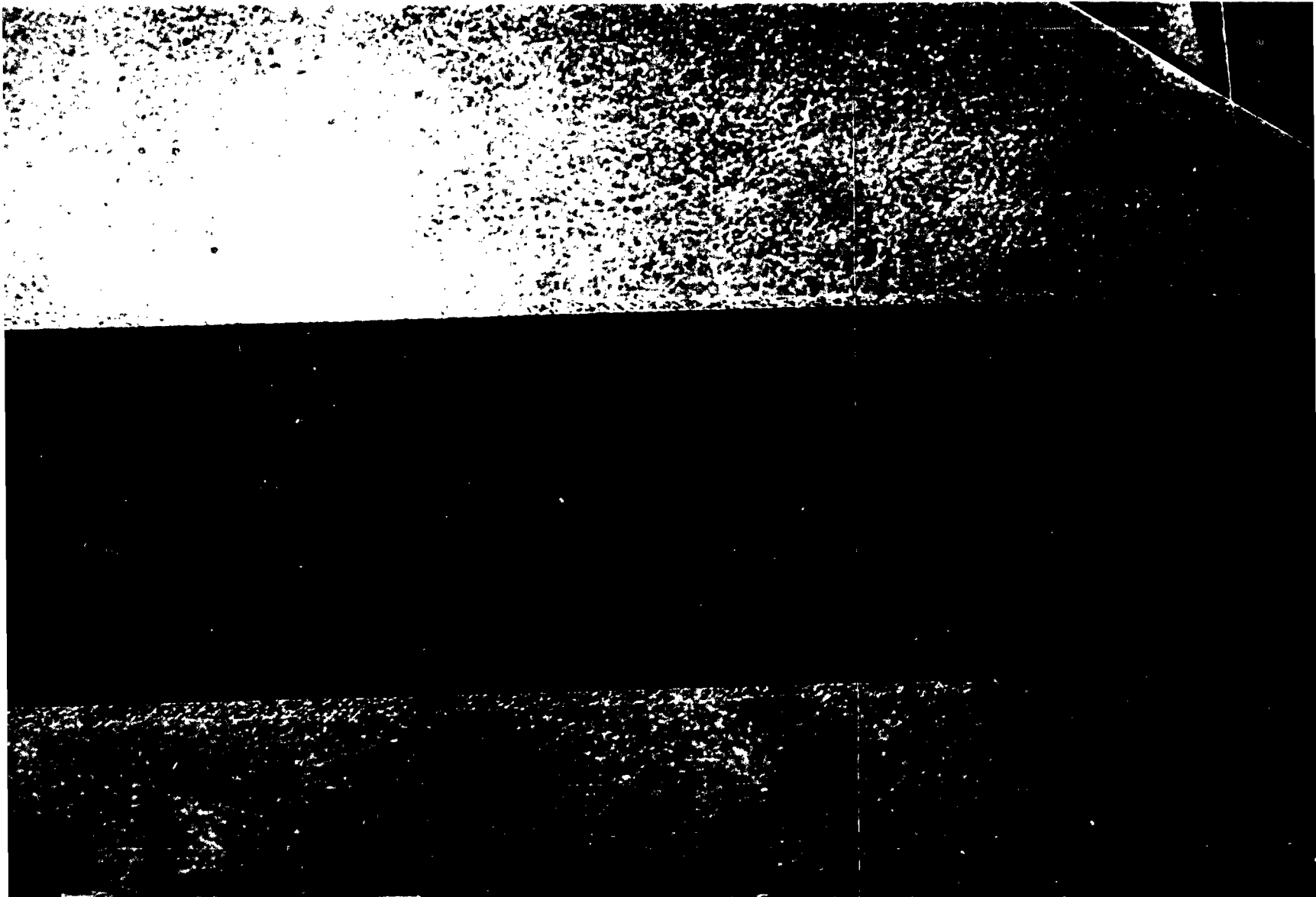
2



3

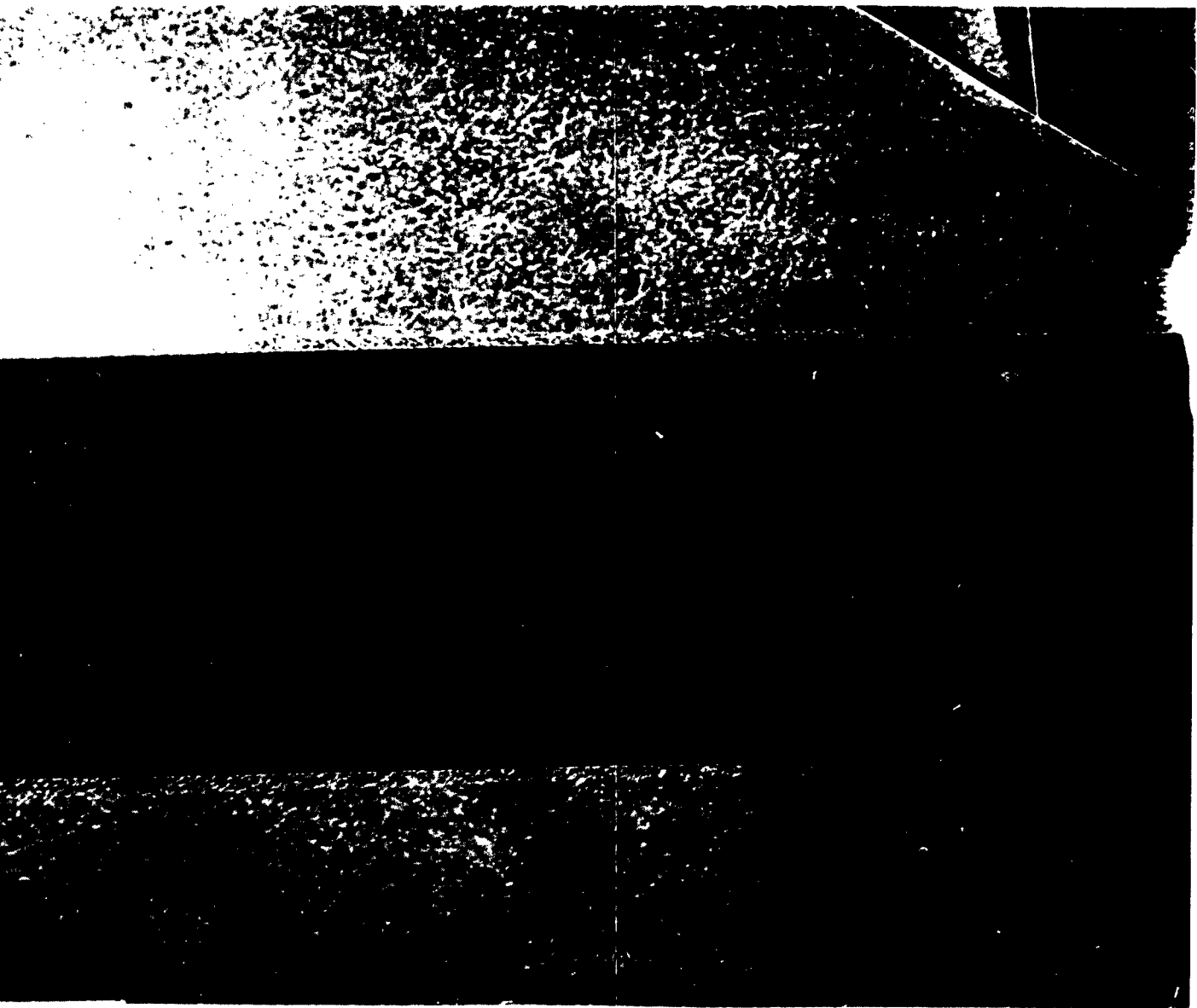
TDR-63-21





Rm 27
March 3, 0

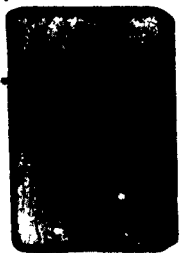
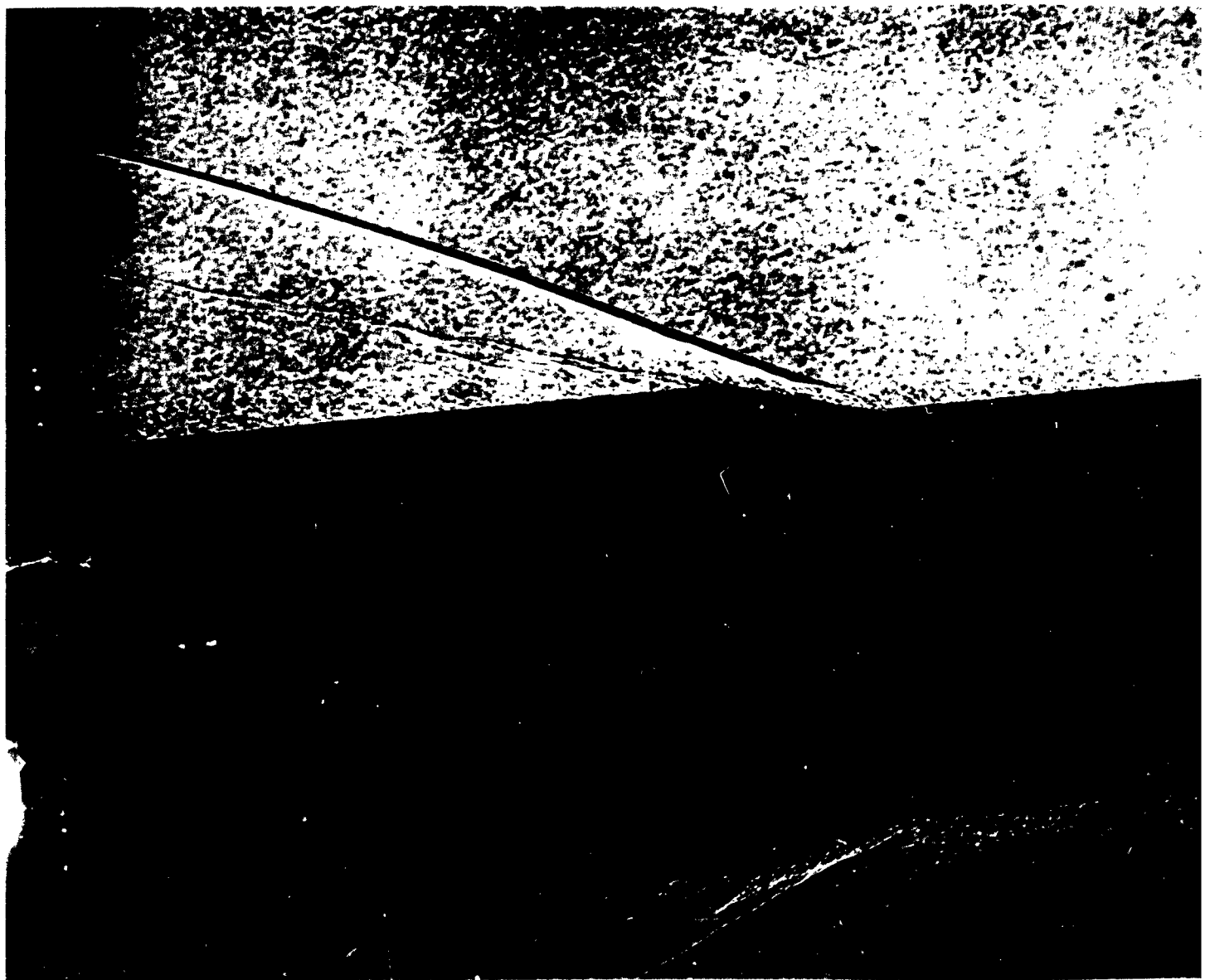


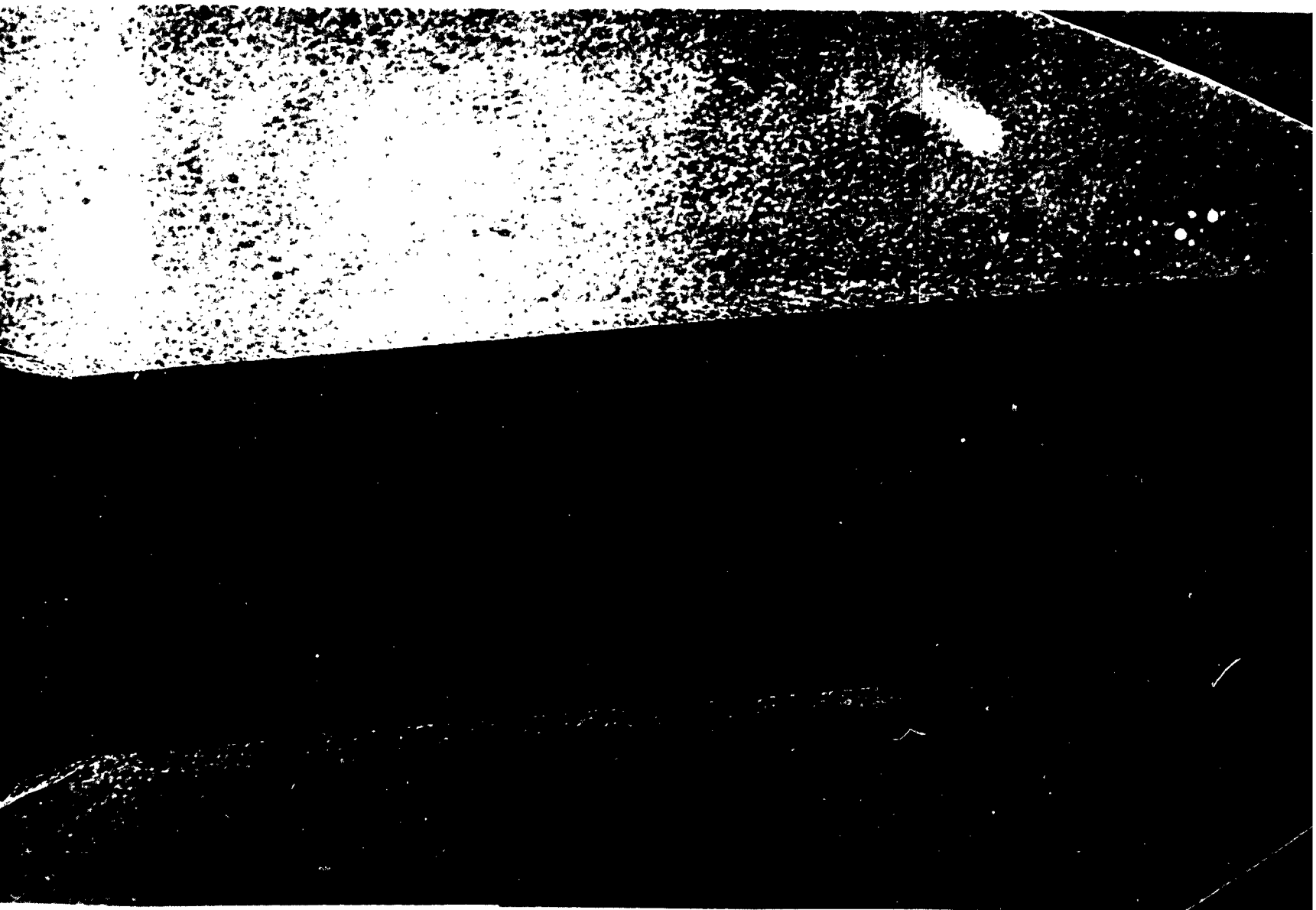


h 27
ch 3.0

3

TDR-63-21





Run 26
March 4, 0





Run 26
March 4 '0

3

APPENDIX V

TABULATED DATA

MSMT TEST 09

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 001 MACH NO 1.247 RN/L 07374596 Q 1485 PSF TO 563

COEFFICIENTS

ALPHA	V	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.12	C.0045	-00.041	0.0032	0.6276	0.6276	0.6276	0.7674	0.0161	-0.0576	-0.0048	0.1397	-27.817	024.42	005
00.14	C.0080	-00.032	0.0365	0.6273	0.6273	0.6273	0.7638	0.0126	-0.0580	-0.0050	0.1365	-12.037	024.45	006
-11.21	-C.9598	-03.181	-0.8206	0.7968	0.7968	0.7968	0.7972	0.1082	0.0691	-0.0049	0.1752	10.069	024.38	007
-10.02	-C.9300	-03.141	-0.7942	0.7870	0.7870	0.7870	0.7936	0.0974	0.0592	-0.0042	0.1748	10.263	024.32	008
-10.79	-C.9043	-03.065	-0.7719	0.7801	0.7801	0.7801	0.7934	0.1030	0.0733	-0.0045	0.1716	10.298	024.35	009
-10.63	-C.8779	-03.014	-0.7482	0.7728	0.7728	0.7728	0.7930	0.1025	0.0575	-0.0054	0.1714	10.429	024.38	010
-10.43	-C.8577	-02.952	-0.7315	0.7641	0.7641	0.7641	0.7893	0.1150	0.0372	-0.0032	0.1704	10.457	024.45	011
-10.22	-C.8344	-02.893	-0.7114	0.7570	0.7570	0.7570	0.7878	0.1167	0.0347	-0.0045	0.1690	10.555	024.51	012
-10.03	-C.8113	-02.846	-0.6909	0.7522	0.7522	0.7522	0.7866	0.1087	0.0406	-0.0049	0.1662	10.658	024.58	013
-09.84	-C.7890	-02.805	-0.6714	0.7465	0.7465	0.7465	0.7863	0.1061	0.0324	-0.0062	0.1655	10.801	024.61	014
-09.64	-C.7672	-02.751	-0.6522	0.7416	0.7416	0.7416	0.7865	0.1019	0.0521	-0.0051	0.1646	10.895	024.55	015
-09.45	-C.7498	-02.701	-0.6376	0.7362	0.7362	0.7362	0.7874	0.1016	0.0584	-0.0054	0.1658	10.945	024.45	016
-09.25	-C.7257	-02.635	-0.6160	0.7322	0.7322	0.7322	0.7874	0.0976	0.0497	-0.0043	0.1639	11.032	024.32	017
-09.03	-C.7033	-02.563	-0.5969	0.7248	0.7248	0.7248	0.7854	0.0999	0.0426	-0.0036	0.1634	11.071	024.26	018
-08.86	-C.6774	-02.525	-0.5727	0.7240	0.7240	0.7240	0.7868	0.0926	0.0482	-0.0063	0.1597	11.323	024.16	019
-08.65	-C.6667	-02.471	-0.5656	0.7148	0.7148	0.7148	0.7817	0.0814	0.0460	-0.0051	0.1601	11.261	024.16	020
-08.46	-C.6425	-02.406	-0.5443	0.7079	0.7079	0.7079	0.7775	0.0800	0.0523	-0.0047	0.1575	11.375	024.26	021
-08.27	-C.6141	-02.337	-0.5186	0.7019	0.7019	0.7019	0.7757	0.0855	0.0451	-0.0047	0.1556	11.563	024.38	022
-08.08	-C.5952	-02.278	-0.5021	0.6979	0.6979	0.6979	0.7761	0.0777	0.0571	-0.0043	0.1557	11.628	024.45	023
-07.90	-C.5689	-02.226	-0.4782	0.6935	0.6935	0.6935	0.7755	0.0735	0.0412	-0.0046	0.1539	11.890	024.51	024
-07.71	-C.5515	-02.166	-0.4630	0.6904	0.6904	0.6904	0.7755	0.0695	0.0412	-0.0028	0.1535	11.931	024.51	025
-07.53	-C.5317	-02.116	-0.4455	0.6874	0.6874	0.6874	0.7764	0.0755	0.0187	-0.0041	0.1533	12.092	024.48	026
-07.34	-C.5149	-02.083	-0.4310	0.6841	0.6841	0.6841	0.7755	0.0745	0.0328	-0.0040	0.1521	12.288	024.45	027
-07.13	-C.4942	-02.022	-0.4128	0.6810	0.6810	0.6810	0.7748	0.0640	0.0085	-0.0052	0.1503	12.431	024.42	028
-06.95	-C.4802	-01.978	-0.4012	0.6770	0.6770	0.6770	0.7738	0.0632	0.0080	-0.0052	0.1503	12.512	024.42	029
-06.77	-C.4679	-01.931	-0.3911	0.6750	0.6750	0.6750	0.7735	0.0592	0.0069	-0.0054	0.1494	12.540	024.35	030
-06.59	-C.4492	-01.883	-0.3746	0.6721	0.6721	0.6721	0.7728	0.0615	0.0068	-0.0035	0.1481	12.731	024.38	031
-06.35	-C.4273	-01.834	-0.3556	0.6681	0.6681	0.6681	0.7707	0.0574	-0.0016	-0.0050	0.1460	13.039	024.42	032
-06.22	-C.4114	-01.793	-0.3416	0.6632	0.6632	0.6632	0.7686	0.0533	0.0115	-0.0061	0.1463	13.218	024.51	033
-06.03	-C.3932	-01.746	-0.3255	0.6628	0.6628	0.6628	0.7695	0.0545	-0.0100	-0.0046	0.1445	13.486	024.51	034
-05.83	-C.3835	-01.697	-0.3180	0.6614	0.6614	0.6614	0.7700	0.0583	-0.0106	-0.0046	0.1443	13.446	024.48	035
-05.63	-C.3624	-01.664	-0.2990	0.6612	0.6612	0.6612	0.7714	0.0593	-0.0176	-0.0031	0.1427	13.948	024.42	036
-05.43	-C.3493	-01.615	-0.2881	0.6602	0.6602	0.6602	0.7711	0.0590	-0.0108	-0.0052	0.1412	14.049	024.35	037
-05.24	-C.3385	-01.572	-0.2798	0.6556	0.6556	0.6556	0.7685	0.0652	-0.0171	-0.0034	0.1412	14.108	024.35	038
-05.01	-C.3183	-01.518	-0.2623	0.6520	0.6520	0.6520	0.7646	0.0548	-0.0340	-0.0041	0.1380	14.485	024.48	039
-04.84	-C.3031	-01.472	-0.2491	0.6503	0.6503	0.6503	0.7651	0.0579	-0.0484	-0.0039	0.1381	14.730	024.55	040
-04.62	-C.2926	-01.435	-0.2412	0.6485	0.6485	0.6485	0.7661	0.0505	-0.0215	-0.0035	0.1391	14.896	024.55	041
-04.43	-C.2751	-01.403	-0.2255	0.6505	0.6505	0.6505	0.7666	0.0502	-0.0147	-0.0048	0.1355	15.461	024.51	042
-04.26	-C.2809	-01.323	-0.2334	0.6491	0.6491	0.6491	0.7659	0.0432	-0.0022	-0.0051	0.1359	14.307	024.45	043
-04.06	-C.2510	-01.298	-0.2058	0.6461	0.6461	0.6461	0.7646	0.0459	0.0053	-0.0053	0.1347	15.704	024.48	044
-03.84	-C.2370	-01.239	-0.1941	0.6455	0.6455	0.6455	0.7660	0.0428	-0.0355	-0.0043	0.1349	15.888	024.45	045
-03.65	-C.2269	-01.197	-0.1864	0.6421	0.6421	0.6421	0.7631	0.0419	-0.0035	-0.0059	0.1341	16.024	024.42	046
-03.46	-C.2130	-01.147	-0.1745	0.6424	0.6424	0.6424	0.7631	0.0282	-0.0069	-0.0042	0.1350	16.363	024.35	047
-03.27	-C.2032	-01.088	-0.1668	0.6422	0.6422	0.6422	0.7644	0.0276	0.0144	-0.0054	0.1328	16.275	024.32	048
-03.05	-C.1891	-01.029	-0.1553	0.6384	0.6384	0.6384	0.7627	0.0406	0.0021	-0.0037	0.1334	16.532	024.29	049
-02.86	-C.1789	-00.977	-0.1471	0.6399	0.6399	0.6399	0.7637	0.0434	0.0238	-0.0049	0.1320	16.593	024.29	050
-02.67	-C.1565	-00.921	-0.1270	0.6378	0.6378	0.6378	0.7615	0.0284	0.0054	-0.0049	0.1303	17.866	024.32	051
-02.50	-C.1567	-00.869	-0.1291	0.6359	0.6359	0.6359	0.7610	0.0430	0.0007	-0.0043	0.1313	16.838	024.38	052
-02.29	-C.1422	-00.824	-0.1169	0.6362	0.6362	0.6362	0.7633	0.0395	-0.0080	-0.0041	0.1323	17.609	024.48	053
-02.12	-C.1312	-00.769	-0.1078	0.6353	0.6353	0.6353	0.7608	0.0357	-0.0021	-0.0047	0.1299	17.803	024.48	054
-01.96	-C.1248	-00.712	-0.1032	0.6331	0.6331	0.6331	0.7612	0.0357	-0.0171	-0.0056	0.1321	17.324	024.45	055

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 001 MACH NO 1.247 RN/L 07374596 Q 1485 PSF TD 563

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
-01.77	-0.1144	-0.650	-0.0948	0.6336	0.6304	0.7616	0.0382	0.0114	-0.0045	0.1312	17.266	024.51	056
-01.56	-0.0996	-0.588	-0.0825	0.6308	0.6283	0.7596	0.0417	-0.0318	-0.0043	0.1313	17.933	024.58	057
-01.37	-0.0820	-0.535	-0.0669	0.6328	0.6310	0.7616	0.0345	-0.0195	-0.0039	0.1306	19.850	024.55	058
-01.18	-0.0680	-0.478	-0.0550	0.6343	0.6331	0.7649	0.0315	-0.0498	-0.0041	0.1318	21.339	024.42	059
-00.99	-0.0549	-0.409	-0.0540	0.6313	0.6302	0.7614	0.0344	-0.0497	-0.0038	0.1312	19.162	024.51	060
-00.81	-0.0582	-0.358	-0.0494	0.6330	0.6292	0.7604	0.0305	-0.0365	-0.0040	0.1312	18.701	024.51	061
-00.62	-0.0552	-0.317	-0.0484	0.6343	0.6338	0.7630	0.0235	-0.0240	-0.0044	0.1292	17.452	024.45	062
-00.41	-0.0446	-0.266	-0.0401	0.6320	0.6317	0.7611	0.0302	-0.0520	-0.0048	0.1294	18.144	024.42	063
-00.22	-0.0380	-0.216	-0.0355	0.6331	0.6330	0.7634	0.0299	-0.0454	-0.0044	0.1305	17.301	024.32	064
-00.06	-0.0352	-0.158	-0.0345	0.6323	0.6323	0.7634	0.0329	-0.0381	-0.0046	0.1311	13.630	024.29	065
-00.15	-0.0207	-0.113	-0.0224	0.6313	0.6314	0.7625	0.0257	-0.0327	-0.0037	0.1311	16.565	024.29	066
00.31	-0.0144	-0.037	-0.0178	0.6314	0.6314	0.7621	0.0259	-0.0481	-0.0045	0.1307	07.782	024.35	067
00.53	-0.0005	0.016	-0.0063	0.6319	0.6319	0.7630	0.0322	-0.0330	-0.0040	0.1311	-97.437	024.35	068
00.72	0.0100	0.084	0.0021	0.6313	0.6312	0.7650	0.0284	-0.0346	-0.0033	0.1338	25.493	024.32	069
00.91	0.0205	0.136	0.0104	0.6326	0.6323	0.7645	0.0212	-0.0294	-0.0050	0.1321	20.200	024.35	070
01.11	0.0312	0.204	0.0190	0.6311	0.6307	0.7638	0.0243	-0.0584	-0.0038	0.1331	19.862	024.42	071
01.27	0.0417	0.255	0.0277	0.6313	0.6305	0.7631	0.0139	-0.0608	-0.0044	0.1326	18.568	024.51	072
01.46	0.0519	0.297	0.0359	0.6298	0.6287	0.7646	0.0135	-0.0527	-0.0042	0.1360	17.384	024.61	073
01.68	0.0658	0.381	0.0473	0.6298	0.6291	0.7653	0.0196	-0.0615	-0.0039	0.1372	17.611	024.64	074
01.87	0.0724	0.439	0.0518	0.6318	0.6297	0.7663	0.0194	-0.0694	-0.0042	0.1365	18.423	024.67	075
02.06	0.0857	0.492	0.0639	0.6358	0.6331	0.7698	0.0089	-0.0651	-0.0044	0.1367	17.239	024.64	076
02.25	0.0943	0.538	0.0692	0.6400	0.6368	0.7734	0.0187	-0.0784	-0.0037	0.1366	17.323	024.51	077
02.41	0.1012	0.599	0.0744	0.6382	0.6345	0.7700	0.0212	-0.0568	-0.0030	0.1361	17.986	024.42	078
02.63	0.1074	0.655	0.0783	0.6363	0.6321	0.7690	0.0173	-0.0509	-0.0035	0.1369	18.540	024.51	079
02.81	0.1221	0.701	0.0908	0.6397	0.6344	0.7711	0.0102	-0.0599	-0.0035	0.1367	17.437	024.48	080
03.00	0.1293	0.745	0.0958	0.6438	0.6379	0.7740	0.0098	-0.0535	-0.0030	0.1361	17.511	024.42	081
03.19	0.1436	0.815	0.1080	0.6429	0.6359	0.7741	0.0126	-0.0609	-0.0031	0.1382	17.248	024.38	082
03.40	0.1508	0.868	0.1126	0.6471	0.6393	0.7753	0.0022	-0.0634	-0.0037	0.1360	17.481	024.35	083
03.59	0.1653	0.904	0.1252	0.6448	0.6357	0.7731	0.0016	-0.0637	-0.0036	0.1374	16.613	024.35	084
03.75	0.1830	0.965	0.1410	0.6458	0.6352	0.7748	-0.0024	-0.0581	-0.0033	0.1397	16.014	024.38	085
03.94	0.1893	0.1022	0.1452	0.6465	0.6350	0.7759	0.0005	-0.0640	-0.0031	0.1409	16.408	024.42	086
04.13	0.2037	0.1083	0.1573	0.6507	0.6377	0.7767	0.0035	-0.0657	-0.0032	0.1390	16.154	024.42	087
04.31	0.2194	0.1133	0.1619	0.6518	0.6378	0.7762	-0.0037	-0.0603	-0.0023	0.1383	16.358	024.45	088
04.56	0.2247	0.1185	0.1737	0.6498	0.6340	0.7766	-0.0041	-0.0682	-0.0026	0.1426	16.026	024.45	089
04.72	0.2396	0.1239	0.1864	0.6541	0.6365	0.7798	-0.0009	-0.0972	-0.0024	0.1433	15.713	024.42	090
04.89	0.2531	0.1298	0.1977	0.6576	0.6383	0.7814	-0.0016	-0.0766	-0.0028	0.1431	15.583	024.45	091
05.11	0.2648	0.1355	0.2068	0.6607	0.6397	0.7839	-0.0056	-0.0709	-0.0025	0.1442	15.556	024.35	092
05.28	0.2837	0.1413	0.2236	0.6630	0.6396	0.7837	-0.0062	-0.0788	-0.0028	0.1441	15.136	024.29	093
05.48	0.2980	0.1458	0.2357	0.6639	0.6384	0.7845	-0.0136	-0.0734	-0.0028	0.1460	14.857	024.29	094
05.65	0.3133	0.1507	0.2490	0.6664	0.6387	0.7865	-0.0074	-0.0658	-0.0028	0.1479	14.612	024.22	095
05.89	0.3225	0.1552	0.2554	0.6671	0.6374	0.7831	-0.0181	-0.0607	-0.0027	0.1457	14.617	024.32	096
06.09	0.3337	0.1594	0.2705	0.6667	0.6343	0.7840	-0.0083	-0.0667	-0.0020	0.1497	14.253	024.38	097
06.28	0.3501	0.1637	0.2786	0.6694	0.6349	0.7846	-0.0122	-0.0605	-0.0015	0.1497	14.205	024.38	098
06.48	0.3678	0.1682	0.2936	0.6743	0.6369	0.7870	-0.0127	-0.0539	-0.0019	0.1501	13.895	024.38	099
06.70	0.3886	0.1735	0.3115	0.6793	0.6383	0.7874	-0.0135	-0.0400	-0.0019	0.1490	13.560	024.42	100
06.87	0.4031	0.1788	0.3238	0.6826	0.6390	0.7886	-0.0139	-0.0477	-0.0014	0.1496	13.479	024.42	101
07.06	0.4215	0.1835	0.3393	0.6855	0.6386	0.7889	-0.0178	-0.0558	-0.0019	0.1503	13.231	024.38	102
07.26	0.4335	0.1871	0.3497	0.6862	0.6365	0.7875	-0.0212	-0.0494	-0.0016	0.1510	13.113	024.48	103
07.48	0.4541	0.1922	0.3674	0.6901	0.6365	0.7872	-0.0215	-0.0427	-0.0019	0.1508	12.861	024.51	104
07.65	0.4719	0.1985	0.3831	0.6929	0.6358	0.7871	-0.0216	-0.0431	-0.0019	0.1513	12.778	024.51	105
07.84	0.4902	0.2033	0.3987	0.6982	0.6372	0.7892	-0.0152	-0.0352	-0.0009	0.1520	12.597	024.48	106

MSWT TEST 09

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 001 MACH NO 1.247 RN/L 07374596 Q 1485 PSF TD 563

10/17/62

COEFFICIENTS

ALPHA	M	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
08.04	0.5075	02.075	0.4133	0.7024	0.6376	0.7890	-0.0152	-0.0498	-0.0009	0.1513	12.420	024.51	107
08.26	0.5183	02.146	0.4216	0.7039	0.6361	0.7891	-0.0189	-0.0365	-0.0001	0.1530	12.580	024.48	108
08.46	0.5435	02.218	0.4444	0.7063	0.6332	0.7886	-0.0225	-0.0447	0.0005	0.1534	12.400	024.48	109
08.63	0.5732	02.277	0.4715	0.7134	0.6346	0.7893	-0.0294	-0.0606	0.0008	0.1547	12.066	024.45	110
08.86	0.5998	02.346	0.4950	0.7192	0.6344	0.7890	-0.0299	-0.0610	0.0002	0.1546	11.882	024.38	111
09.06	0.6255	02.403	0.5173	0.7287	0.6382	0.7910	-0.0300	-0.0616	0.0006	0.1528	11.672	024.35	112
09.25	0.6486	02.446	0.5374	0.7352	0.6393	0.7919	-0.0268	-0.0756	-0.0003	0.1526	11.455	024.32	113
09.44	0.6627	02.490	0.5494	0.7358	0.6357	0.7913	-0.0237	-0.0681	0.0005	0.1555	11.417	024.32	114
09.61	0.6792	02.523	0.5641	0.7369	0.6324	0.7896	-0.0275	-0.0472	0.0007	0.1571	11.284	024.35	115
09.75	0.6952	02.565	0.5790	0.7420	0.6332	0.7882	-0.0276	-0.0473	-0.0000	0.1550	11.191	024.38	116
09.92	0.7156	02.623	0.5960	0.7454	0.6316	0.7871	-0.0243	-0.0474	0.0011	0.1555	11.123	024.45	117
10.06	0.7390	02.652	0.6173	0.7507	0.6313	0.7884	-0.0243	-0.0477	0.0003	0.1570	10.990	024.51	118
10.18	0.7531	02.697	0.6294	0.7565	0.6334	0.7901	-0.0278	-0.0350	0.0009	0.1566	10.878	024.51	119
10.32	0.7706	02.750	0.6449	0.7597	0.6319	0.7914	-0.0276	-0.0360	0.0009	0.1595	10.841	024.51	120
10.41	0.7896	02.787	0.6627	0.7624	0.6301	0.7905	-0.0273	-0.0511	0.0009	0.1604	10.722	024.58	121
10.53	0.8001	02.839	0.6712	0.7672	0.6317	0.7916	-0.0337	-0.0605	0.0010	0.1600	10.779	024.58	122
10.59	0.8243	02.868	0.6933	0.7770	0.6364	0.7959	-0.0371	-0.0690	0.0012	0.1595	10.571	024.51	123
10.67	0.8317	02.897	0.7001	0.7760	0.6330	0.7950	-0.0339	-0.0545	0.0014	0.1620	10.582	024.48	124
10.76	0.8414	02.941	0.7080	0.7814	0.6356	0.7953	-0.0304	-0.0830	0.0008	0.1597	10.617	024.42	125
10.86	0.8477	02.949	0.7133	0.7810	0.6326	0.7931	-0.0341	-0.0548	0.0006	0.1605	10.568	024.42	126
11.01	0.8720	02.978	0.7347	0.7901	0.6353	0.7953	-0.0342	-0.0626	0.0019	0.1600	10.377	024.35	127
11.15	0.8802	03.018	0.7416	0.7894	0.6312	0.7993	-0.0308	-0.0696	0.0018	0.1622	10.416	024.32	128
11.24	0.8990	03.054	0.7586	0.7953	0.6322	0.7934	-0.0339	-0.0852	0.0007	0.1612	10.320	024.38	129
11.30	0.9082	03.095	0.7665	0.7986	0.6329	0.7945	-0.0339	-0.0577	0.0024	0.1615	10.353	024.42	130
11.39	0.9124	03.095	0.7702	0.7971	0.6294	0.7918	-0.0305	-0.0568	0.0008	0.1624	10.305	024.48	131
11.39	0.9131	03.103	0.7701	0.8008	0.6330	0.7945	-0.0403	-0.0380	0.0014	0.1615	10.326	024.55	132
11.42	0.9171	03.122	0.7740	0.8003	0.6313	0.7948	-0.0335	-0.0515	0.0019	0.1635	10.343	024.55	133
11.42	0.9310	03.143	0.7871	0.8054	0.6336	0.7962	-0.0337	-0.0517	0.0019	0.1626	10.256	024.48	134
11.42	0.9319	03.146	0.7875	0.8081	0.6361	0.7964	-0.0336	-0.0592	0.0023	0.1623	10.255	024.45	135
00.05	0.0413	-00.025	0.0407	0.6422	0.6422	0.7693	0.0121	-0.0515	-0.0047	0.1271	-01.813	024.42	137
00.05	0.0340	-00.043	0.0334	0.6416	0.6415	0.7668	0.0190	-0.0498	-0.0059	0.1253	-03.821	024.38	137

MSWT TEST 89

 CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 002 MACH NO 1.244 RN/L 07456231 Q 1484 PSF TO 558

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
-10.17	0.0243	-0.086	0.0219	0.8362	0.8361	1.0274	0.0279	-0.1014	-0.0031	0.1913	-10.787	024.48	006
-10.57	-2.0571	05.192	-1.8752	1.1651	0.8014	1.0128	0.0430	-0.1354	-0.0041	0.2114	-07.668	024.42	007
-10.23	-1.9719	05.118	-1.8397	1.1535	0.8020	1.0137	0.0493	-0.1615	-0.0046	0.2117	-07.706	024.38	008
-10.02	-1.9239	04.951	-1.7546	1.1434	0.8061	1.0149	0.0515	-0.1593	-0.0036	0.2088	-07.774	024.38	009
-09.87	-1.8900	04.868	-1.7240	1.1267	0.8043	1.0138	0.0466	-0.1076	-0.0043	0.2095	-07.818	024.42	010
-09.66	-1.8460	04.782	-1.6847	1.1174	0.8054	1.0132	0.0523	-0.0902	-0.0030	0.2077	-07.825	024.45	011
-09.51	-1.8079	04.708	-1.6499	1.1034	0.8051	1.0131	0.0377	-0.0765	-0.0030	0.2080	-07.870	024.48	012
-09.30	-1.7673	04.658	-1.6129	1.0938	0.8063	1.0144	0.0368	-0.0605	-0.0039	0.2080	-07.912	024.48	013
-09.11	-1.7213	04.577	-1.5713	1.0866	0.8118	1.0181	0.0293	-0.0677	-0.0048	0.2062	-08.007	024.42	014
-08.93	-1.6748	04.496	-1.5282	1.0724	0.8100	1.0162	0.0280	-0.0516	-0.0031	0.2062	-08.079	024.42	015
-08.75	-1.6415	04.423	-1.4986	1.0640	0.8138	1.0166	0.0408	-0.0905	-0.0015	0.2048	-08.156	024.42	016
-08.57	-1.5948	04.339	-1.4560	1.0536	0.8133	1.0173	0.0371	-0.1251	-0.0029	0.2041	-08.186	024.45	017
-08.37	-1.5612	04.265	-1.4261	1.0398	0.8111	1.0155	0.0326	-0.1164	-0.0027	0.2044	-08.247	024.51	018
-08.19	-1.5245	04.188	-1.3924	1.0327	0.8141	1.0167	0.0318	-0.0936	-0.0049	0.2028	-08.299	024.51	019
-08.04	-1.4882	04.104	-1.3593	1.0272	0.8184	1.0188	0.0275	-0.0925	-0.0034	0.2005	-08.346	024.48	020
-07.86	-1.4581	04.042	-1.3322	1.0174	0.8174	1.0182	0.0304	-0.1115	-0.0045	0.2008	-08.378	024.45	021
-07.65	-1.4136	03.946	-1.2922	1.0123	0.8207	1.0207	0.0260	-0.0964	-0.0031	0.2000	-08.422	024.38	022
-07.48	-1.3688	03.841	-1.2504	0.9985	0.8175	1.0172	0.0316	-0.0716	-0.0031	0.1997	-08.481	024.42	023
-07.31	-1.3356	03.756	-1.2202	0.9910	0.8198	1.0167	0.0375	-0.0681	-0.0062	0.1969	-08.525	024.45	024
-06.14	-1.3004	03.676	-1.1877	0.9850	0.8217	1.0210	0.0299	-0.0674	-0.0040	0.1972	-08.543	024.42	025
-06.97	-1.2637	03.587	-1.1545	0.9808	0.8256	1.0219	0.0325	-0.0794	-0.0030	0.1954	-08.588	024.35	026
-06.79	-1.2273	03.511	-1.1210	0.9708	0.8236	1.0172	0.0317	-0.0630	-0.0047	0.1936	-08.623	024.38	027
-06.60	-1.1839	03.397	-1.0809	0.9644	0.8250	1.0200	0.0274	-0.0619	-0.0033	0.1950	-08.692	024.35	028
-06.45	-1.1544	03.314	-1.0542	0.9579	0.8273	1.0223	0.0198	-0.0821	-0.0024	0.1950	-08.716	024.35	029
-06.28	-1.1083	03.209	-1.0110	0.9508	0.8262	1.0194	0.0294	-0.1000	-0.0034	0.1932	-08.722	024.38	030
-06.11	-1.0684	03.120	-0.9745	0.9443	0.8280	1.0212	0.0248	-0.0696	-0.0025	0.1932	-08.797	024.38	031
-05.89	-1.0241	03.021	-0.9340	0.9343	0.8253	1.0171	0.0274	-0.0885	-0.0018	0.1919	-08.872	024.48	032
-05.77	-0.9898	02.924	-0.9016	0.9260	0.8253	1.0151	0.0329	-0.0850	-0.0026	0.1898	-08.962	024.61	033
-05.56	-0.9537	02.822	-0.8691	0.9233	0.8280	1.0184	0.0188	-0.0781	-0.0010	0.1904	-08.975	024.61	034
-05.37	-0.9295	02.751	-0.8477	0.9157	0.8272	1.0194	0.0283	-0.1096	-0.0008	0.1922	-08.991	024.64	035
-05.19	-0.8993	02.643	-0.8205	0.9135	0.8302	1.0202	0.0275	-0.0866	-0.0013	0.1900	-08.991	024.67	036
-05.01	-0.8699	02.536	-0.7936	0.9083	0.8303	1.0193	0.0200	-0.0783	-0.0004	0.1890	-08.929	024.74	037
-04.85	-0.8417	02.459	-0.7678	0.9076	0.8349	1.0237	0.0264	-0.0895	-0.0001	0.1888	-08.858	024.61	038
-04.66	-0.8110	02.371	-0.7404	0.9064	0.8382	1.0248	0.0229	-0.0822	-0.0018	0.1859	-08.877	024.55	039
-04.46	-0.7801	02.274	-0.7123	0.9004	0.8410	1.0268	0.0259	-0.0592	-0.0013	0.1858	-08.881	024.45	040
-04.27	-0.7477	02.174	-0.6828	0.9004	0.8424	1.0282	0.0327	-0.0787	-0.0037	0.1858	-08.857	024.32	041
-04.09	-0.7062	02.061	-0.6441	0.8963	0.8429	1.0280	0.0399	-0.1198	-0.0013	0.1851	-08.832	024.22	042
-03.88	-0.6625	01.942	-0.6040	0.8942	0.8460	1.0278	0.0184	-0.0570	-0.0006	0.1819	-08.865	024.19	043
-03.72	-0.6268	01.839	-0.5708	0.8854	0.8426	1.0227	0.0215	-0.0622	-0.0022	0.1801	-08.906	024.22	044
-03.52	-0.5975	01.756	-0.5448	0.8808	0.8419	1.0242	0.0316	-0.0736	-0.0026	0.1823	-08.914	024.26	045
-03.34	-0.5668	01.658	-0.5169	0.8760	0.8410	1.0227	0.0212	-0.0813	-0.0010	0.1817	-08.929	024.32	046
-03.16	-0.5345	01.552	-0.4872	0.8723	0.8407	1.0264	0.0276	-0.0573	-0.0012	0.1817	-08.929	024.32	047
-02.99	-0.5075	01.459	-0.4628	0.8719	0.8437	1.0261	0.0614	-0.1115	-0.0021	0.1824	-08.822	024.35	048
-02.81	-0.4801	01.349	-0.4392	0.8698	0.8445	1.0274	0.0275	-0.0908	-0.0002	0.1824	-08.736	024.35	049
-02.61	-0.4488	01.246	-0.4102	0.8631	0.8405	1.0214	0.0205	-0.0800	-0.0004	0.1809	-08.519	024.48	050
-02.46	-0.4230	01.155	-0.3865	0.8578	0.8382	1.0211	0.0207	-0.1245	-0.0014	0.1829	-08.433	024.55	051
-02.28	-0.3891	01.072	-0.3555	0.8596	0.8422	1.0260	0.0309	-0.1148	-0.0014	0.1829	-08.295	024.51	052
-02.10	-0.3522	00.976	-0.3211	0.8537	0.8389	1.0235	0.0271	-0.0936	-0.0003	0.1846	-08.373	024.51	053
-01.95	-0.3228	00.871	-0.2939	0.8571	0.8448	1.0289	0.0135	-0.0597	-0.0002	0.1835	-08.416	024.48	054
-01.77	-0.2888	00.780	-0.2626	0.8550	0.8465	1.0296	0.0137	-0.0736	-0.0007	0.1844	-08.199	024.38	055
				0.8550	0.8465	1.0296	0.0204	-0.0647	-0.0002	0.1830	-08.205	024.35	056

MSWT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 002 MACH NO 1.244 RN/L 07456231 Q 1484 PSF TD 558

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
-31.59	0.2661	00.711	-0.2424	0.8548	0.8478	1.0298	0.0204	-0.0500	-0.0012	0.1820	-08.111	024.35	057
-31.62	0.2353	00.634	-0.2163	0.8526	0.8470	1.0286	0.0175	-0.0934	-0.0017	0.1816	-08.109	024.35	058
-31.24	0.2122	00.556	-0.1937	0.8517	0.8473	1.0289	0.0313	-0.1121	-0.0036	0.1816	-07.966	024.35	059
-31.34	0.1849	00.462	-0.1695	0.8505	0.8473	1.0290	0.0213	-0.1060	-0.0011	0.1817	-07.590	024.38	060
-30.84	0.1617	00.383	-0.1492	0.8457	0.8434	1.0266	0.0283	-0.1114	-0.0013	0.1832	-07.205	024.45	061
-30.69	0.1277	00.284	-0.1175	0.8474	0.8459	1.0301	0.0315	-0.0886	-0.0018	0.1842	-06.757	024.45	062
-30.52	0.1049	00.231	-0.0972	0.8503	0.8494	1.0318	0.0314	-0.0884	-0.0012	0.1825	-06.690	024.48	063
-30.34	0.0746	00.147	-0.0695	0.8483	0.8478	1.0313	0.0349	-0.0945	-0.0016	0.1835	-05.991	024.48	064
-30.17	0.0479	00.071	-0.0454	0.8497	0.8496	1.0316	0.0283	-0.1025	-0.0018	0.1821	-06.475	024.48	065
30.31	0.3176	00.311	-0.0178	0.8502	0.8502	1.0319	0.0282	-0.1164	-0.0012	0.1818	-01.922	024.51	066
30.19	0.0057	00.058	0.0029	0.8476	0.8476	1.0291	0.0349	-0.1217	-0.0013	0.1815	-30.978	024.55	067
30.39	0.0332	00.134	0.0274	0.8473	0.8471	1.0299	0.0343	-0.1217	-0.0016	0.1828	-12.279	024.51	068
30.54	0.0641	00.217	0.0561	0.8454	0.8469	1.0278	0.0242	-0.1215	-0.0021	0.1829	-10.261	024.61	069
30.73	0.0950	00.284	0.0843	0.8490	0.8478	1.0306	0.0307	-0.1198	-0.0026	0.1828	-08.081	024.58	070
30.90	0.1112	00.347	0.0978	0.8524	0.8507	1.0324	0.0338	-0.1117	-0.0020	0.1816	-09.470	024.55	071
31.11	0.1431	00.432	0.1266	0.8542	0.8516	1.0345	0.0336	-0.1113	-0.0021	0.1829	-09.173	024.45	072
31.26	0.1749	00.509	0.1560	0.8555	0.8519	1.0348	0.0266	-0.1120	-0.0017	0.1829	-08.843	024.38	073
01.47	0.2107	00.618	0.1889	0.8546	0.8495	1.0324	0.0295	-0.0890	-0.0021	0.1829	-08.916	024.32	074
01.62	0.2382	00.695	0.2142	0.8544	0.8480	1.0313	0.0257	-0.0815	-0.0019	0.1833	-08.862	024.32	075
01.83	0.2625	00.753	0.2353	0.8578	0.8498	1.0313	0.0289	-0.0806	-0.0017	0.1815	-08.679	024.28	076
01.98	0.2865	00.827	0.2571	0.8558	0.8464	1.0286	0.0357	-0.1146	-0.0019	0.1822	-08.770	024.29	077
02.16	0.3173	00.918	0.2851	0.8605	0.8491	1.0290	0.0421	-0.1050	-0.0019	0.1799	-08.787	024.32	078
32.33	0.3451	01.011	0.3104	0.8614	0.8481	1.0265	0.0385	-0.1046	-0.0030	0.1784	-08.899	024.32	079
32.53	0.3770	01.111	0.3353	0.8600	0.8442	1.0243	0.0349	-0.1056	-0.0020	0.1802	-08.952	024.35	080
02.73	0.3975	01.175	0.3573	0.8618	0.8440	1.0245	0.0349	-0.1323	-0.0025	0.1805	-08.976	024.32	081
02.88	0.4395	01.286	0.3965	0.8648	0.8438	1.0247	0.0308	-0.1282	-0.0024	0.1809	-08.887	024.38	082
03.05	0.4683	01.370	0.4229	0.8635	0.8397	1.0215	0.0336	-0.1148	-0.0018	0.1818	-08.888	024.31	083
03.23	0.5063	01.473	0.4581	0.8685	0.8413	1.0231	0.0298	-0.1282	-0.0013	0.1818	-08.838	024.58	084
03.41	0.5375	01.549	0.4865	0.8719	0.8414	1.0242	0.0363	-0.1334	-0.0014	0.1828	-08.753	024.58	085
03.58	0.5693	01.634	0.5155	0.8768	0.8428	1.0249	0.0292	-0.1196	-0.0019	0.1821	-08.720	024.55	086
03.76	0.5975	01.721	0.5411	0.8793	0.8420	1.0243	0.0287	-0.0975	-0.0015	0.1824	-08.748	024.51	087
03.93	0.6310	01.826	0.5717	0.8858	0.8445	1.0264	0.0284	-0.1111	-0.0016	0.1819	-08.791	024.45	088
04.11	0.6615	01.915	0.5995	0.8876	0.8424	1.0240	0.0284	-0.1171	-0.0021	0.1816	-08.795	024.48	089
04.31	0.6978	02.018	0.6324	0.8948	0.8448	1.0267	0.0280	-0.1091	-0.0026	0.1819	-08.783	024.45	090
04.49	0.7216	02.094	0.6555	0.8966	0.8427	1.0250	0.0278	-0.1225	-0.0018	0.1823	-08.816	024.45	091
04.65	0.7612	02.210	0.6905	0.9008	0.8419	1.0253	0.0342	-0.1274	-0.0011	0.1834	-08.820	024.45	092
04.83	0.7950	02.301	0.7212	0.9078	0.8439	1.0279	0.0306	-0.1203	-0.0018	0.1839	-08.794	024.38	093
05.01	0.8300	02.392	0.7532	0.9119	0.8426	1.0255	0.0266	-0.1056	-0.0012	0.1829	-08.755	024.38	094
05.19	0.8667	02.503	0.7872	0.9146	0.8397	1.0255	0.0333	-0.1178	-0.0018	0.1851	-08.774	024.35	095
05.37	0.9011	02.608	0.8181	0.9241	0.8431	1.0263	0.0260	-0.1033	-0.0023	0.1829	-08.792	024.38	096
05.55	0.9340	02.694	0.8482	0.9279	0.8414	1.0261	0.0285	-0.1011	-0.0024	0.1847	-08.770	024.35	097
05.76	0.9638	02.775	0.8744	0.9345	0.8420	1.0267	0.0311	-0.1058	-0.0009	0.1848	-08.748	024.38	098
05.92	1.0048	02.888	0.9125	0.9422	0.8431	1.0292	0.0268	-0.0972	-0.0017	0.1861	-08.731	024.35	099
06.10	1.0334	02.987	0.9362	0.9457	0.8406	1.0276	0.0223	-0.0809	-0.0013	0.1869	-08.781	024.42	100
06.31	1.0737	03.085	0.9749	0.9529	0.8400	1.0284	0.0246	-0.0851	-0.0008	0.1884	-08.730	024.48	101
06.49	1.1147	03.178	1.0125	0.9610	0.8403	1.0270	0.0149	-0.0662	-0.0006	0.1866	-08.661	024.51	102
06.67	1.1459	03.254	1.0405	0.9675	0.8400	1.0280	0.0230	-0.0937	-0.0003	0.1881	-08.624	024.51	103
06.86	1.1904	03.356	1.0814	0.9778	0.8417	1.0300	0.0221	-0.0939	-0.0005	0.1884	-08.566	024.48	104
07.04	1.2351	03.468	1.1226	0.9870	0.8419	1.0306	0.0210	-0.0848	-0.0006	0.1887	-08.530	024.45	105
07.22	1.2706	03.575	1.1545	0.9965	0.8435	1.0308	0.0234	-0.0820	-0.0006	0.1872	-08.549	024.45	106
07.40	1.3100	03.679	1.1903	1.0064	0.8447	1.0340	0.0193	-0.0809	-0.0002	0.1893	-08.531	024.38	107

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 002 MACH NO 1.244 RN/L 07456231 Q 1484 PSF TO 558

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
07.56	1.3456	-03.752	1.2231	1.0118	0.8421	1.0305	0.0217	-0.0641	-0.0006	0.1884	-08.472	024.42	108
07.77	1.3748	-03.607	1.2484	1.0192	0.8410	1.0301	0.0277	-0.0616	-0.0003	0.1891	-08.412	024.45	109
07.96	1.4137	-03.905	1.2839	1.0273	0.8397	1.0288	0.0233	-0.0460	0.0010	0.1891	-08.392	024.45	110
08.13	1.4440	-04.009	1.3098	1.0414	0.8456	1.0345	0.0156	-0.0240	0.0009	0.1890	-08.434	024.35	111
08.32	1.4836	-04.112	1.3465	1.0456	0.8398	1.0327	0.0182	-0.0215	0.0009	0.1918	-08.421	024.29	112
08.50	1.5287	-04.204	1.3876	1.0573	0.8406	1.0324	0.0069	0.0071	0.0010	0.1900	-08.355	024.19	113
08.69	1.5610	-04.243	1.4159	1.0686	0.8425	1.0325	0.0133	0.0019	0.0009	0.1900	-08.258	024.16	114
08.87	1.5975	-04.340	1.4584	1.0802	0.8424	1.0328	0.0088	0.0107	0.0001	0.1904	-08.202	024.16	115
09.03	1.6481	-04.432	1.4961	1.0866	0.8384	1.0300	0.0112	0.0080	0.0005	0.1916	-08.170	024.19	116
09.16	1.6816	-04.510	1.5269	1.0946	0.8376	1.0299	0.0075	-0.0220	0.0001	0.1923	-08.148	024.22	117
09.31	1.7185	-04.587	1.5603	1.1043	0.8372	1.0288	0.0135	-0.0263	-0.0030	0.1916	-08.109	024.26	118
09.45	1.7499	-04.640	1.5886	1.1139	0.8380	1.0306	0.0160	-0.0101	0.0001	0.1926	-08.056	024.26	119
09.58	1.7910	-04.701	1.6265	1.1246	0.8382	1.0311	0.0122	-0.0383	-0.0003	0.1929	-07.975	024.29	120
09.69	1.8076	-04.739	1.6412	1.1283	0.8361	1.0302	0.0188	-0.0506	-0.0017	0.1940	-07.965	024.32	121
09.79	1.8482	-04.837	1.6785	1.1419	0.8398	1.0335	0.0110	-0.0358	0.0003	0.1936	-07.950	024.26	122
09.87	1.8628	-04.851	1.6919	1.1433	0.8363	1.0300	0.0104	-0.0205	0.0003	0.1937	-07.912	024.35	123
09.95	1.8893	-04.899	1.7163	1.1503	0.8364	1.0301	0.0169	-0.0610	-0.0003	0.1937	-07.877	024.42	124
10.03	1.9075	-04.917	1.7328	1.1547	0.8352	1.0308	0.0129	-0.0326	0.0003	0.1956	-07.832	024.42	125
10.08	1.9112	-04.919	1.7363	1.1521	0.8302	1.0269	0.0161	-0.0456	-0.0004	0.1967	-07.819	024.51	126
10.22	1.9358	-04.981	1.7574	1.1629	0.8328	1.0302	0.0154	-0.0299	-0.0014	0.1974	-07.817	024.55	127
10.35	1.9600	-05.026	1.7776	1.1760	0.8375	1.0344	0.0043	-0.0262	-0.0003	0.1969	-07.790	024.45	128
10.49	1.9938	-05.092	1.8081	1.1862	0.8373	1.0349	0.0040	-0.0016	0.0004	0.1976	-07.758	024.42	129
10.57	2.0157	-05.138	1.8269	1.1987	0.8433	1.0372	0.0071	-0.0005	0.0014	0.1939	-07.743	024.35	130
10.62	2.0263	-05.158	1.8368	1.1993	0.8402	1.0331	0.0064	0.0293	-0.0003	0.1929	-07.734	024.35	131
10.67	2.0301	-05.163	1.8400	1.1985	0.8370	1.0314	0.0061	0.0367	0.0001	0.1944	-07.727	024.38	132
10.68	2.0398	-05.172	1.8505	1.1949	0.8314	1.0287	0.0087	0.0666	0.0004	0.1973	-07.703	024.45	133
10.70	2.0594	-05.211	1.8675	1.2079	0.8400	1.0343	-0.0014	0.0509	0.0005	0.1943	-07.687	024.42	134
10.73	2.0639	-05.212	1.8726	1.2053	0.8363	1.0330	0.0022	0.0370	0.0007	0.1968	-07.672	024.42	135
10.73	2.0663	-05.216	1.8740	1.2083	0.8382	1.0358	0.0053	0.0451	0.0005	0.1976	-07.669	024.42	136
-00.04	-0.0062	-00.035	-0.0056	0.8513	1.0276	1.0276	0.0210	-0.0677	-0.0012	0.1763	17.263	024.32	137
-00.02	-0.0024	-00.051	-0.0022	0.8471	0.8471	1.0247	0.0347	-0.0791	-0.0030	0.1776	64.373	024.45	138

HSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 003 MACH NO 1.243 RN/L 07052099 Q 1477 PSF TO 580

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.19	0.0339	-0.127	0.0311	0.8435	0.8434	1.0379	0.0314	-0.1226	0.1818	0.1945	-11.423	024.32	005
00.19	0.0342	-0.144	0.0314	0.8428	0.8426	1.0376	0.0246	-0.1236	0.1813	0.1949	-12.785	024.32	006
-10.84	-2.0920	35.280	-1.9315	1.1933	0.8143	1.0288	0.0014	0.1793	0.1954	0.2125	-07.668	024.45	007
-10.33	-2.0174	35.170	-1.8331	1.1777	0.8230	1.0357	0.0010	0.1741	0.1969	0.2126	-07.785	024.45	008
-10.16	-1.9531	35.092	-1.7773	1.1545	0.8229	1.0345	0.0068	0.1418	0.1966	0.2116	-07.920	024.35	009
-09.80	-1.8457	34.844	-1.6777	1.1307	0.8277	1.0396	-0.0019	0.1308	0.1966	0.2109	-07.973	024.38	010
-09.44	-1.7804	34.701	-1.6207	1.1073	0.8265	1.0356	0.0004	0.1196	0.1989	0.2091	-08.022	024.42	011
-09.08	-1.6813	34.510	-1.5292	1.0855	0.8306	1.0393	0.0053	0.1446	0.1982	0.2087	-08.169	024.42	012
-08.72	-1.6147	34.412	-1.4697	1.0691	0.8340	1.0417	0.0035	0.1278	0.2017	0.2076	-08.300	024.32	013
-08.33	-1.5152	34.199	-1.3776	1.0500	0.8394	1.0452	-0.0058	0.1606	0.1992	0.2058	-08.419	024.26	014
-07.97	-1.4643	34.125	-1.3347	1.0284	0.8334	1.0382	0.0005	0.1269	0.1998	0.2048	-08.559	024.26	015
-07.62	-1.3545	33.851	-1.2316	1.0087	0.8365	1.0384	-0.0150	0.1154	0.2004	0.2019	-08.637	024.26	016
-07.28	-1.3015	33.702	-1.1847	0.9970	0.8389	1.0412	0.0041	0.1208	0.2013	0.2022	-08.662	024.22	017
-06.93	-1.2111	33.484	-1.1003	0.9848	0.8447	1.0437	-0.0044	0.1466	0.2006	0.1990	-08.738	024.16	018
-06.57	-1.1377	33.321	-1.0333	0.9723	0.8478	1.0461	0.0015	0.0656	0.2020	0.1982	-08.867	024.13	019
-06.22	-1.0636	33.142	-0.9654	0.9587	0.8484	1.0446	-0.0002	0.0835	0.2021	0.1962	-08.975	024.19	020
-05.86	-0.9781	32.939	-0.8868	0.9399	0.8445	1.0389	0.0122	0.0458	0.2031	0.1944	-09.129	024.35	021
-05.50	-0.9132	32.748	-0.8275	0.9354	0.8518	1.0443	0.0007	0.0548	0.2024	0.1925	-09.143	024.42	022
-05.13	-0.8547	32.577	-0.7747	0.9297	0.8567	1.0473	0.0034	0.0302	0.2025	0.1905	-09.158	024.32	023
-04.82	-0.7881	32.358	-0.7131	0.9227	0.8596	1.0491	0.0068	0.0115	0.2034	0.1895	-09.090	024.32	024
-04.39	-0.7177	32.154	-0.6503	0.9060	0.8535	1.0399	0.0132	0.0077	0.2009	0.1863	-09.119	024.35	025
-04.02	-0.6523	31.971	-0.5904	0.9029	0.8592	1.0451	0.0097	-0.0055	0.2003	0.1859	-09.180	024.35	026
-33.66	-0.5927	31.823	-0.5398	0.8927	0.8564	1.0423	0.0235	-0.0521	0.2008	0.1859	-09.295	024.29	027
-03.31	-0.5215	31.556	-0.4710	0.8880	0.8593	1.0441	0.0132	-0.0581	0.1973	0.1848	-09.063	024.32	028
-02.98	-0.4779	31.382	-0.4326	0.8823	0.8586	1.0448	0.0203	-0.0838	0.1982	0.1862	-08.787	024.32	029
-02.57	-0.4195	31.226	-0.3807	0.8745	0.8566	1.0432	0.0197	-0.0676	0.1947	0.1866	-08.880	024.38	030
-02.24	-0.3548	31.063	-0.3210	0.8723	0.8591	1.0461	0.0263	-0.0935	0.1942	0.1869	-09.077	024.35	031
-01.90	-0.3017	30.923	-0.2731	0.8675	0.8580	1.0429	0.0124	-0.0872	0.1890	0.1849	-09.297	024.35	032
-01.55	-0.2431	30.735	-0.2197	0.8674	0.8612	1.0464	0.0157	-0.1057	0.1861	0.1852	-09.185	024.45	033
-01.18	-0.1869	30.553	-0.1692	0.8663	0.8626	1.0469	0.0135	-0.0971	0.1846	0.1844	-08.994	024.32	034
-00.83	-0.1104	30.306	-0.0979	0.8654	0.8639	1.0445	0.0291	-0.1141	0.1816	0.1826	-08.431	024.22	035
-00.48	-0.0680	30.183	-0.0608	0.8603	0.8597	1.0428	0.0350	-0.1260	0.1800	0.1830	-08.162	024.22	036
-00.13	-0.0174	30.044	-0.0154	0.8619	0.8618	1.0473	0.0184	-0.1268	0.1795	0.1855	-07.634	024.35	037
00.57	0.1039	-00.342	0.0954	0.8615	0.8605	1.0446	0.0240	-0.1141	0.1787	0.1841	-10.011	024.42	038
00.93	0.1518	-00.484	0.1378	0.8636	0.8613	1.0455	0.0203	-0.0995	0.1803	0.1842	-09.681	024.29	040
01.31	0.2112	-00.655	0.1914	0.8677	0.8631	1.0462	0.0302	-0.0961	0.1812	0.1832	-09.424	024.22	041
01.64	0.2949	-00.889	0.2700	0.8717	0.8636	1.0442	0.0196	-0.1173	0.1829	0.1806	-09.154	024.19	042
02.00	0.3453	-01.024	0.3149	0.8743	0.8627	1.0446	0.0227	-0.1220	0.1845	0.1819	-09.012	024.26	043
02.38	0.3757	-01.113	0.3398	0.8722	0.8573	1.0410	0.0188	-0.0924	0.1870	0.1836	-09.003	024.35	044
02.73	0.3514	-01.331	0.4099	0.8804	0.8599	1.0414	0.0184	-0.1046	0.1897	0.1815	-08.959	024.32	045
03.08	0.3157	-01.504	0.4685	0.8898	0.8633	1.0447	0.0287	-0.1445	0.1923	0.1813	-08.857	024.29	046
03.43	0.2704	-01.675	0.5229	0.8931	0.8602	1.0402	0.0319	-0.1639	0.1938	0.1800	-08.842	024.26	047
04.13	0.2104	-02.067	0.6464	0.9119	0.8629	1.0448	0.0110	-0.1874	0.1968	0.1819	-08.837	024.38	049
04.46	0.1726	-02.245	0.7034	0.9165	0.8590	1.0427	0.0306	-0.1923	0.1960	0.1836	-08.908	024.42	050
04.85	0.1297	-02.425	0.7542	0.9234	0.8563	1.0399	0.0339	-0.2049	0.1975	0.1836	-08.880	024.35	051
05.22	0.1111	-02.653	0.8294	0.9365	0.8572	1.0416	0.0434	-0.2287	0.1985	0.1844	-08.845	024.38	052
05.55	0.1279	-02.841	0.8873	0.9509	0.8606	1.0457	0.0455	-0.2389	0.1986	0.1851	-08.852	024.35	053
05.95	0.1027	-02.975	0.9334	0.9610	0.8591	1.0492	0.0439	-0.2215	0.1990	0.1901	-08.794	024.38	054
06.31	1.1101	-03.208	1.0090	0.9756	0.8588	1.0499	0.0385	-0.2390	0.1989	0.1911	-08.779	024.38	055
06.68	1.1651	-03.346	1.0574	0.9882	0.8586	1.0496	0.0406	-0.2370	0.1990	0.1910	-08.724	024.29	056
07.04	1.2501	-03.556	1.1349	1.0094	0.8627	1.0523	0.0423	-0.2618	0.2003	0.1896	-08.638	024.22	057

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 003 MACH NO 1.243 RW/L 07052099 Q 1477 PSF TD 580

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
07.41	1.3160	-03.724	1.1941	1.0231	0.8606	1.0516	0.0369	-0.2518	0.1993	0.1910	-08.597	024.22	058
07.40	1.3098	-03.894	1.2600	1.0418	0.8611	1.0518	0.0382	-0.2262	0.1998	0.1906	-08.512	024.22	059
08.17	1.4901	-04.093	1.3532	1.0596	0.8565	1.0522	0.0397	-0.2855	0.1994	0.1958	-08.345	024.29	060
08.52	1.5497	-04.230	1.4262	1.0748	0.8517	1.0468	0.0442	-0.2862	0.1988	0.1951	-08.225	024.42	061
08.87	1.5284	-04.444	1.4748	1.0977	0.8571	1.0511	0.0422	-0.2541	0.1980	0.1940	-08.300	024.38	062
09.19	1.7012	-04.622	1.5427	1.1165	0.8559	1.0505	0.0336	-0.2248	0.1975	0.1947	-08.254	024.26	063
09.45	1.7721	-04.782	1.6075	1.1354	0.8561	1.0519	0.0355	-0.2565	0.1959	0.1958	-08.199	024.29	064
09.71	1.8167	-04.853	1.6464	1.1493	0.8551	1.0493	0.0413	-0.2609	0.1956	0.1942	-08.116	024.32	065
09.90	1.8500	-04.920	1.6756	1.1598	0.8546	1.0481	0.0339	-0.2756	0.1962	0.1935	-08.079	024.29	066
10.03	1.9028	-05.003	1.7244	1.1751	0.8567	1.0509	0.0370	-0.3317	0.1966	0.1942	-07.983	024.28	067
10.22	1.9354	-05.081	1.7527	1.1872	0.8575	1.0500	0.0325	-0.3094	0.1969	0.1925	-07.976	024.22	068
10.49	1.9936	-05.188	1.8045	1.2043	0.8558	1.0493	0.0312	-0.3074	0.1959	0.1935	-07.906	024.22	069
10.62	2.0250	-05.230	1.8337	1.2080	0.8492	1.0458	0.0296	-0.2813	0.1944	0.1966	-07.846	024.42	070
10.68	2.0194	-05.216	1.8276	1.2061	0.8467	1.0432	0.0326	-0.2514	0.1941	0.1966	-07.868	024.48	071
10.73	2.0542	-05.270	1.8595	1.2204	0.8528	1.0492	0.0360	-0.3077	0.1956	0.1965	-07.794	024.45	072
00.09	0.0227	-00.131	0.0213	0.8627	0.8626	1.0421	0.0354	-0.1518	0.1798	0.1795	-17.518	024.22	073
00.09	0.0105	-00.099	0.0092	0.8619	0.8619	1.0411	0.0248	-0.1169	0.1784	0.1792	-28.599	024.38	074

MSMT TEST 89

RUN 004 MACH NO 1.018 RWL 07407903 Q 1422 PSF TO 583

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PD	PMT
00.18	0.0413	-00.011	0.0385	0.8946	0.8944	1.0616	0.0250	-0.0933	0.1929	0.1672	-00.809	026.38	006
-08.90	-1.7228	05.434	-1.5837	1.1500	0.8942	1.0814	0.1084	-0.0698	0.2189	0.1871	-09.617	026.22	000
-11.12	-2.1091	06.582	-1.9789	1.2980	0.8921	1.0931	-0.0182	0.2488	0.2216	0.2011	-09.121	026.25	008
-11.11	-2.2099	06.653	-1.9958	1.3050	0.8959	1.0987	-0.0254	0.2813	0.2217	0.2028	-09.146	026.41	009
-10.74	-2.1106	06.346	-1.9264	1.2750	0.8975	1.0973	-0.0144	0.2244	0.2212	0.1997	-09.135	026.54	010
-09.55	-1.8360	05.781	-1.6605	1.1967	0.9046	1.0996	-0.0098	0.1967	0.2224	0.1950	-09.566	026.38	011
-08.12	-1.4979	05.003	-1.3338	1.1162	0.9136	1.1037	-0.0066	0.1210	0.2228	0.1900	-10.180	026.29	012
-06.62	-1.1561	04.080	-1.0431	1.0397	0.9124	1.0949	-0.0089	0.0506	0.2197	0.1824	-10.721	026.25	013
-05.05	-0.8065	03.080	-0.7230	0.9837	0.9132	1.0888	-0.0122	0.0347	0.2184	0.1756	-11.601	026.19	014
-03.31	-0.4912	02.088	-0.4377	0.9396	0.9127	1.0767	0.0100	-0.0360	0.2135	0.1640	-12.912	026.25	015
-01.59	-0.1779	01.061	-0.1524	0.9174	0.9129	1.0731	0.0231	-0.0593	0.2010	0.1634	-18.131	026.32	016
-00.46	0.0223	00.341	0.0296	0.9141	0.9143	1.0766	0.0226	-0.0513	0.1923	0.1623	-66.519	026.35	017
-00.05	0.0632	00.079	0.0640	0.9102	0.9102	1.0746	0.0203	-0.0682	0.1904	0.1644	03.786	026.29	018
00.14	0.0669	-00.041	0.0627	0.9097	0.9095	1.0728	0.0389	-0.1557	0.1934	0.1632	-01.896	026.25	019
00.18	0.0694	-00.123	0.0666	0.9078	0.9076	1.0682	0.0285	-0.1481	0.1878	0.1606	-05.397	026.41	020
00.23	0.0656	-00.125	0.0620	0.9095	0.9092	1.0674	0.0633	-0.1640	0.1885	0.1582	-05.749	026.40	021
00.20	0.0701	-00.124	0.0668	0.9117	0.9114	1.0777	0.0217	-0.1433	0.1895	0.1663	-05.393	026.38	022
00.21	0.0622	-00.376	0.0580	0.9128	0.9126	1.0787	0.0254	-0.1522	0.1914	0.1661	-03.757	026.22	023
00.23	0.0586	-00.077	0.0549	0.9073	0.9070	1.0758	0.0184	-0.1461	0.1924	0.1688	-03.988	026.22	024
00.23	0.0590	-00.111	0.0554	0.9108	0.9106	1.0806	0.0256	-0.1371	0.1926	0.1700	-05.730	026.25	025
00.20	0.0706	-00.142	0.0674	0.9031	0.9028	1.0731	0.0463	-0.1394	0.1910	0.1703	-06.120	026.41	026
00.20	0.0544	-00.094	0.0512	0.9021	0.9019	1.0764	0.0358	-0.1196	0.1927	0.1745	-05.267	026.45	027
00.21	0.0629	-00.094	0.0597	0.9084	0.9082	1.0816	0.0340	-0.1426	0.1950	0.1734	-04.518	026.38	028
00.21	0.0758	-00.109	0.0675	0.9010	0.9007	1.0722	0.0433	-0.1496	0.1926	0.1714	-04.691	026.29	029
00.20	0.0639	-00.112	0.0606	0.9041	0.9038	1.0748	0.0441	-0.1954	0.1942	0.1710	-05.325	026.22	030
00.13	0.0258	00.002	0.0238	0.8982	0.8982	1.0701	0.0397	-0.1355	0.1922	0.1719	00.278	026.38	031
-00.59	-0.1019	00.393	-0.0925	0.9093	0.9083	1.0828	0.0405	-0.1405	0.1953	0.1745	-11.630	026.29	032
-01.64	-0.2806	00.970	-0.2547	0.9089	0.9013	1.0754	0.0301	-0.1180	0.1998	0.1741	-10.501	026.35	033
-02.80	-0.4915	01.676	-0.4469	0.9252	0.9023	1.0789	0.0268	-0.0666	0.2097	0.1767	-10.358	026.25	034
-04.10	-0.7219	02.443	-0.6555	0.9538	0.9045	1.0804	0.0097	-0.0702	0.2147	0.1759	-10.287	026.35	035
-05.48	-0.9877	03.293	-0.8964	0.9993	0.9091	1.0876	0.0165	-0.0168	0.2187	0.1785	-10.119	026.29	036
-06.85	-1.2575	04.087	-1.1412	1.0435	0.8999	1.0901	0.0175	0.0414	0.2202	0.1901	-09.873	026.32	037
-08.18	-1.5449	04.893	-1.4318	1.0644	0.8957	1.0869	0.0126	0.0530	0.2237	0.1912	-09.616	026.29	038
-09.31	-1.8169	05.619	-1.6479	1.0786	0.8964	1.0929	-0.0087	0.1474	0.2232	0.1965	-09.394	026.38	039
-10.17	-1.9977	06.091	-1.8580	1.0923	0.8961	1.0959	-0.0043	0.1649	0.2236	0.1999	-09.283	026.45	040
-10.69	-2.1134	06.427	-1.9320	1.2126	0.8923	1.0903	0.0035	0.1786	0.2242	0.1980	-09.148	026.38	041
-10.89	-2.1521	06.465	-1.9446	1.2836	0.8930	1.0921	-0.0042	0.2034	0.2239	0.1991	-09.127	026.25	042
-10.96	-2.1778	06.542	-1.9684	1.2894	0.8914	1.0889	-0.0224	0.2934	0.2212	0.1974	-09.177	026.32	043
-11.32	-2.2183	06.617	-2.0063	1.3027	0.8952	1.0956	-0.0029	0.2248	0.2248	0.2005	-09.062	026.38	044
-11.32	-2.1938	06.557	-1.9824	1.2969	0.8941	1.0941	-0.0063	0.1667	0.2231	0.2001	-09.080	026.41	045
-10.78	-2.1376	06.513	-1.9342	1.2702	0.8861	1.0840	-0.0078	0.1664	0.2223	0.1978	-09.256	026.29	046
-10.47	-2.0464	06.296	-1.8695	1.2531	0.8961	1.0936	-0.0085	0.2020	0.2260	0.1975	-09.347	026.22	047
-10.11	-1.9778	06.142	-1.7893	1.2301	0.8987	1.0942	-0.0117	0.1424	0.2240	0.1955	-09.435	026.19	048
-09.76	-1.8748	05.829	-1.6951	1.2044	0.8995	1.0958	-0.0050	0.1382	0.2212	0.1963	-09.445	026.32	049
-09.40	-1.8184	05.729	-1.6466	1.1871	0.9022	1.0977	-0.0090	0.1377	0.2254	0.1955	-09.572	026.38	050
-09.31	-1.6929	05.472	-1.5308	1.1552	0.9011	1.0959	-0.0065	0.1192	0.2249	0.1948	-09.820	026.32	051
-08.68	-1.6272	05.323	-1.4722	1.1386	0.9033	1.0959	-0.0024	0.1401	0.2237	0.1926	-09.933	026.25	052
-08.31	-1.5183	05.028	-1.3720	1.1122	0.9024	1.0941	0.0007	0.1150	0.2244	0.1918	-10.062	026.32	053
-07.96	-1.4522	04.809	-1.3138	1.0908	0.8988	-0.0034	0.0802	0.0802	0.2233	0.1903	-10.160	026.41	054
-07.58	-1.3840	04.622	-1.2522	1.0817	0.9071	1.0941	0.0059	0.0438	0.2236	0.1870	-10.465	026.41	055
-07.24	-1.2996	04.417	-1.1746	1.0668	0.9104	1.0969	-0.0063	0.0665	0.2226	0.1866	-10.325	026.35	056

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 004 MACH NO 1.018 RN/L 07407903 Q 1422 PSF TO 583

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
-06.87	-1.2326	04.249	-1.1152	1.0482	0.9073	1.0938	-0.0037	0.0261	0.2239	0.1866	-10.474	026.25	057
-06.56	-1.1480	03.997	-1.0364	1.0358	0.9106	1.0949	-0.0092	0.0384	0.2234	0.1843	-10.579	026.25	058
-06.23	-1.0512	03.699	-0.9465	1.0171	0.9085	1.0924	0.0245	0.0245	0.2214	0.1839	-10.690	026.25	059
-05.82	-1.0101	03.557	-0.9131	1.0042	0.9066	1.0879	0.0133	-0.0009	0.2204	0.1813	-10.698	026.32	060
-05.51	-0.9250	03.323	-0.8335	0.9938	0.9092	1.0865	0.0084	-0.0195	0.2206	0.1773	-10.913	026.38	061
-05.14	-0.8518	03.116	-0.7663	0.9882	0.9156	1.0884	0.0033	-0.0084	0.2208	0.1728	-11.114	026.38	062
-04.80	-0.7804	02.900	-0.7011	0.9759	0.9137	1.0865	0.0091	-0.0398	0.2195	0.1728	-11.290	026.35	063
-04.41	-0.7166	02.667	-0.6441	0.9679	0.9155	1.0860	0.0119	-0.0648	0.2222	0.1735	-11.306	026.29	064
-04.05	-0.6596	02.469	-0.5934	0.9591	0.9148	1.0860	0.0044	-0.0339	0.2184	0.1712	-11.374	026.29	065
-03.71	-0.6089	02.283	-0.5485	0.9510	0.9135	1.0837	0.0185	-0.0443	0.2164	0.1702	-11.389	026.35	066
-03.33	-0.5283	02.025	-0.4743	0.9420	0.9128	1.0830	0.0219	-0.0633	0.2156	0.1702	-11.648	026.35	067
-02.95	-0.4606	01.852	-0.4133	0.9306	0.9082	1.0783	0.0142	-0.0403	0.2143	0.1702	-12.214	026.35	068
-02.59	-0.3858	01.601	-0.3442	0.9279	0.9113	1.0822	0.0142	-0.0526	0.2120	0.1709	-12.602	026.29	069
-02.24	-0.3276	01.468	-0.3218	0.9215	0.9083	1.0779	0.0144	-0.0661	0.2088	0.1697	-12.471	026.29	070
-01.92	-0.2738	01.161	-0.2429	0.9257	0.9171	1.0871	0.0181	-0.0922	0.2069	0.1700	-12.887	026.25	071
-01.59	-0.2024	00.951	-0.1770	0.9168	0.9115	1.0812	0.0176	-0.0748	0.2023	0.1697	-14.282	026.29	072
-01.21	-0.1546	00.805	-0.1353	0.9096	0.9065	1.0770	0.0425	-0.1212	0.2000	0.1705	-15.828	026.32	073
-00.84	-0.0913	00.583	-0.0779	0.9119	0.9106	1.0815	0.0317	-0.1058	0.1974	0.1709	-19.304	026.29	074
-00.50	-0.0465	00.383	-0.0385	0.9115	0.9111	1.0808	0.0325	-0.1639	0.1964	0.1697	-25.022	026.25	075
-00.18	0.0212	00.139	0.0241	0.9141	0.9142	1.0839	0.0286	-0.1393	0.1933	0.1697	-20.017	026.25	076
00.18	0.0824	-00.123	0.0795	0.9097	0.9095	1.0785	0.0392	-0.1415	0.1932	0.1690	-04.545	026.32	077
00.54	0.1231	-00.252	0.1164	0.9085	0.9073	1.0782	0.0248	-0.1059	0.1921	0.1709	-06.218	026.29	078
00.86	0.2104	-00.544	0.1967	0.9084	0.9053	1.0747	0.0422	-0.1451	0.1948	0.1694	-07.863	026.29	079
01.24	0.2686	-00.739	0.2489	0.9153	0.9097	1.0790	0.0349	-0.1598	0.1969	0.1694	-08.361	026.29	080
01.59	0.3306	-00.953	0.3051	0.9204	0.9116	1.0809	0.0523	-0.1699	0.1978	0.1694	-08.734	026.29	081
01.97	0.3882	-01.163	0.3567	0.9204	0.9076	1.0766	0.0520	-0.1827	0.1990	0.1690	-09.078	026.32	082
02.32	0.4441	-01.361	0.4069	0.9267	0.9095	1.0792	0.0517	-0.1669	0.2033	0.1697	-09.309	026.25	083
02.65	0.5137	-01.568	0.4714	0.9273	0.9046	1.0754	0.0479	-0.1953	0.2060	0.1709	-09.272	026.29	084
03.02	0.5991	-01.822	0.5504	0.9392	0.9089	1.0794	0.0507	-0.1996	0.2097	0.1705	-09.239	026.32	085
03.36	0.6577	-02.035	0.6029	0.9517	0.9147	1.0849	0.0506	-0.2204	0.2101	0.1702	-09.399	026.32	086
03.71	0.7119	-02.230	0.6513	0.9586	0.9144	1.0861	0.0575	-0.2325	0.2121	0.1717	-09.518	026.32	087
04.08	0.7793	-02.461	0.7122	0.9685	0.9153	1.0892	0.0609	-0.2528	0.2138	0.1739	-09.594	026.29	088
04.77	0.8997	-02.856	0.8206	0.9849	0.9132	1.0878	0.0667	-0.2552	0.2163	0.1746	-09.575	026.25	090
05.11	0.9835	-03.070	0.8983	0.9971	0.9131	1.0933	0.0682	-0.2571	0.2161	0.1802	-09.483	026.29	091
05.50	1.0739	-03.341	0.9812	1.0146	0.9160	1.0984	0.0596	-0.2771	0.2156	0.1824	-09.451	026.22	092
05.86	1.1180	-03.514	1.0186	1.0263	0.9170	1.1006	0.0583	-0.2874	0.2185	0.1836	-09.550	026.25	093
06.25	1.2129	-03.779	1.0565	1.0383	0.9118	1.0945	0.0627	-0.2870	0.2175	0.1847	-09.465	026.29	094
07.59	1.4934	-04.621	1.3578	1.1042	0.9126	1.1022	0.0702	-0.2788	0.2228	0.1896	-09.401	026.22	098
08.77	1.7507	-05.316	1.5918	1.1637	0.9072	1.1010	0.0675	-0.3021	0.2198	0.1937	-09.224	026.25	101
09.08	1.8288	-05.517	1.6624	1.1862	0.9089	1.1014	0.0577	-0.2234	0.2171	0.1926	-09.165	026.25	102
09.37	1.8628	-05.602	1.6911	1.1928	0.9016	1.0953	0.0680	-0.2647	0.2197	0.1937	-09.136	026.25	103
09.55	1.9343	-05.776	1.7582	1.2077	0.8992	1.0959	0.0770	-0.2665	0.2180	0.1968	-09.072	026.25	104
09.76	1.9811	-05.891	1.8005	1.2190	0.8961	1.0894	0.0650	-0.2862	0.2176	0.1933	-09.034	026.32	105
09.92	2.0032	-05.927	1.8182	1.2318	0.9002	1.0962	0.0688	-0.3447	0.2198	0.1959	-08.988	026.32	106
10.07	2.0712	-06.093	1.8827	1.2436	0.8951	1.0873	0.0675	-0.3280	0.2185	0.1922	-08.938	026.25	107
10.30	2.1173	-06.178	1.9225	1.2563	0.8897	1.0827	0.0812	-0.3540	0.2200	0.1930	-08.865	026.22	108
10.50	2.1649	-06.306	1.9650	1.2773	0.8977	1.0922	0.0620	-0.3243	0.2179	0.1945	-08.849	026.22	109
10.58	2.1590	-06.306	1.9589	1.2712	0.8900	1.0825	0.0463	-0.2625	0.2183	0.1925	-08.874	026.38	110
10.50	2.1767	-06.354	1.9748	1.2804	0.8951	1.0907	0.0462	-0.3482	0.2184	0.1956	-08.868	026.58	111
10.50	2.1832	-06.367	1.9810	1.2826	0.8962	1.0918	0.0390	-0.3552	0.2194	0.1956	-08.868	026.58	112
00.342	-00.348	00.348	0.0334	0.8960	0.8960	1.0614	0.0295	-0.0868	0.1928	0.1655	-04.223	025.74	103

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 005 MACH NO 0.805 RN/L 07579055 Q 1277 PSF T J 590

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.19	-0.3318	-00.125	0.0302	0.4816	0.4815	0.4992	0.0307	-0.0400	0.1915	0.3177	-11.987	029.99	006
-10.44	-0.3349	36.383	-1.9136	0.8440	0.4832	0.5112	-0.0244	0.3198	0.2153	0.3281	-09.530	029.96	007
-09.39	-1.8937	06.117	-1.8291	0.8156	0.4825	0.5089	0.0362	0.2956	0.2148	0.3264	-09.561	029.96	008
-09.77	-1.8549	05.807	-1.7461	0.7902	0.4824	0.5111	0.0016	0.2581	0.2200	0.3287	-09.511	029.99	009
-09.42	-1.7740	05.573	-1.6700	0.7733	0.4896	0.5150	0.0075	0.2581	0.2175	0.3254	-09.544	029.96	010
-09.34	-1.6779	05.291	-1.5800	0.7477	0.4901	0.5155	0.0061	0.2214	0.2172	0.3254	-09.580	029.99	011
-08.69	-1.6412	05.155	-1.5478	0.7353	0.4929	0.5167	-0.0058	0.1799	0.2234	0.3238	-09.542	030.05	012
-08.34	-1.5825	04.868	-1.4548	0.7103	0.4917	0.5149	-0.0205	0.2391	0.2193	0.3232	-09.588	029.99	013
-08.00	-1.4566	04.566	-1.3724	0.6867	0.4891	0.5112	-0.0099	0.1845	0.2237	0.3222	-09.536	030.05	014
-07.65	-1.3905	04.372	-1.3127	0.6725	0.4918	0.5158	-0.0154	0.1663	0.2236	0.3240	-09.552	029.86	015
-07.32	-1.2857	04.019	-1.2122	0.6548	0.4951	0.5177	-0.0211	0.1389	0.2207	0.3226	-09.496	029.83	016
-06.93	-1.2262	03.855	-1.1577	0.6378	0.4935	0.5143	-0.0110	0.1533	0.2167	0.3208	-09.552	029.80	017
-06.62	-1.1425	03.584	-1.0780	0.6222	0.4938	0.5162	-0.0124	0.1255	0.2196	0.3224	-09.530	029.80	018
-06.28	-1.0617	03.311	-1.0311	0.6086	0.4953	0.5165	-0.0066	0.1643	0.2187	0.3212	-09.475	029.96	019
-05.90	-1.0050	03.132	-0.9485	0.5983	0.4977	0.5167	-0.0075	0.1421	0.2188	0.3191	-09.467	030.09	020
-05.58	-0.9183	02.827	-0.8652	0.5894	0.5016	0.5245	-0.0018	0.2013	0.2207	0.3229	-09.354	030.02	021
-05.21	-0.8184	02.555	-0.7680	0.5683	0.4962	0.5198	-0.0093	0.1926	0.2213	0.3236	-09.507	029.83	022
-04.87	-0.7536	02.325	-0.7087	0.5595	0.4974	0.5189	-0.0135	0.1613	0.2191	0.3215	-09.373	029.80	023
-04.47	-0.7225	02.204	-0.6815	0.5514	0.4966	0.5190	-0.0135	0.1432	0.2167	0.3224	-09.269	029.83	024
-04.08	-0.6426	01.925	-0.6354	0.5441	0.4996	0.5187	-0.0022	0.1280	0.2142	0.3191	-09.098	029.92	025
-03.75	-0.5806	01.717	-0.5468	0.5357	0.4988	0.5168	-0.0020	0.0964	0.2125	0.3180	-08.985	030.02	026
-03.37	-0.5223	01.533	-0.4922	0.5267	0.4968	0.5179	-0.0018	0.0752	0.2113	0.3211	-08.917	029.99	027
-03.01	-0.4784	01.407	-0.4518	0.5178	0.4934	0.5157	-0.0063	0.0707	0.2095	0.3224	-08.933	029.83	028
-02.66	-0.4180	01.184	-0.3945	0.5148	0.4959	0.5157	-0.0060	0.0134	0.2074	0.3198	-08.603	029.80	029
-02.30	-0.3577	01.019	-0.3376	0.5097	0.4958	0.5143	-0.0063	-0.0235	0.2052	0.3186	-08.651	029.83	030
-01.94	-0.2892	00.806	-0.2725	0.4996	0.4901	0.5068	-0.0101	0.0081	0.1989	0.3167	-08.469	030.09	031
-01.61	-0.2370	00.671	-0.2230	0.5031	0.4966	0.5138	-0.0189	-0.0565	0.2014	0.3171	-08.599	030.09	032
-01.24	-0.1678	00.445	-0.1572	0.4914	0.4879	0.5074	-0.0069	0.0017	0.1990	0.3195	-08.056	029.92	033
-00.89	-0.1177	00.302	-0.1102	0.4876	0.4858	0.5046	-0.0236	-0.0533	0.1956	0.3188	-07.794	029.83	034
-00.56	-0.0630	00.159	-0.0582	0.4882	0.4876	0.5068	-0.0278	-0.0687	0.1957	0.3192	-07.646	029.86	035
-00.18	-0.0248	00.051	-0.0253	0.4849	0.4848	0.5039	-0.0039	-0.0057	0.1939	0.3191	-05.829	029.92	036
00.17	0.0249	-00.090	0.0255	0.4821	0.4820	0.4989	-0.0189	-0.0066	0.1924	0.3169	-10.145	029.99	037
00.50	0.0681	-00.215	0.0638	0.4858	0.4853	0.5040	-0.0031	-0.0200	0.1934	0.3187	-09.589	029.99	038
00.88	0.1365	-00.414	0.1291	0.4859	0.4839	0.5016	-0.0219	-0.0308	0.1938	0.3177	-09.233	029.89	039
01.24	0.1858	-00.555	0.1752	0.4901	0.4862	0.5049	-0.0012	0.0006	0.1949	0.3187	-09.075	029.89	040
01.96	0.2519	-00.691	0.2382	0.4926	0.4858	0.5039	-0.0044	-0.0220	0.1937	0.3181	-08.338	029.96	041
01.96	0.3090	-00.847	0.2920	0.4994	0.4891	0.5066	-0.0074	-0.0198	0.1960	0.3175	-08.330	030.02	042
02.32	0.3749	-01.032	0.3546	0.5078	0.4930	0.5113	-0.0147	-0.0509	0.2039	0.3183	-08.365	029.96	043
02.70	0.4120	-01.143	0.3885	0.5085	0.4897	0.5090	-0.0019	-0.0177	0.2036	0.3194	-08.426	029.89	044
03.05	0.4506	-01.290	0.4317	0.5181	0.4944	0.5137	-0.0134	-0.0562	0.2041	0.3193	-08.542	029.83	045
03.37	0.5353	-01.508	0.5054	0.5236	0.4930	0.5116	-0.0161	-0.0526	0.2032	0.3186	-08.558	029.96	046
03.74	0.6144	-01.762	0.5807	0.5342	0.4952	0.5133	-0.0277	-0.0531	0.2064	0.3181	-08.712	029.96	047
04.05	0.6894	-01.970	0.6475	0.5535	0.5058	0.5245	-0.0269	-0.1694	0.2086	0.3187	-08.734	030.02	048
04.41	0.7430	-02.137	0.7319	0.5574	0.5013	0.5207	-0.0141	-0.1215	0.2092	0.3194	-08.739	029.86	049
04.81	0.8024	-02.341	0.7578	0.5633	0.4977	0.5152	-0.0251	-0.1412	0.2080	0.3175	-08.862	029.89	050
05.15	0.8821	-02.584	0.8335	0.5792	0.5021	0.5202	-0.0200	-0.1303	0.2133	0.3181	-08.900	029.96	051
05.53	0.9802	-02.877	0.9274	0.5908	0.4988	0.5202	-0.0271	-0.1843	0.2136	0.3204	-08.917	029.96	052
05.89	1.0210	-03.056	0.9646	0.5988	0.4966	0.5159	-0.0266	-0.2231	0.2126	0.3193	-09.094	029.96	053
06.28	1.1355	-03.414	1.0736	0.6253	0.5042	0.5229	-0.0232	-0.1836	0.2133	0.3221	-09.135	029.89	054
06.61	1.1835	-03.590	1.1180	0.6338	0.5009	0.5229	-0.0139	-0.2375	0.2133	0.3221	-09.215	029.99	055
06.97	1.2907	-03.887	1.2197	0.6598	0.5069	0.5278	-0.0007	-0.2411	0.2152	0.3209	-09.150	029.99	056

MSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 005 MACH NO 0.805 RN/L 07579055 Q 1277 PSF TO 590

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
07.36	1.3155	-03.969	1.2405	0.6649	0.5005	0.5214	0.0177	-0.2117	0.2123	0.3209	-09.165	029.96	057
07.72	1.4395	-04.376	1.3586	0.6948	0.5061	0.5277	0.0107	-0.2309	0.2133	0.3216	-09.235	029.86	058
08.07	1.5210	-04.644	1.4355	0.7106	0.5019	0.5234	0.0045	-0.2590	0.2124	0.3214	-09.275	029.83	059
08.43	1.5721	-04.817	1.4812	0.7287	0.5036	0.5232	0.0062	-0.2277	0.2136	0.3196	-09.308	029.89	060
08.76	1.6690	-05.111	1.5737	0.7459	0.4975	0.5205	-0.0128	-0.1820	0.2151	0.3231	-09.304	029.96	061
09.09	1.7572	-05.378	1.6562	0.7707	0.4992	0.5236	0.0050	-0.2249	0.2153	0.3244	-09.298	029.89	062
09.35	1.8084	-05.562	1.7035	0.7851	0.4980	0.5217	0.0040	-0.2796	0.2115	0.3237	-09.343	029.86	063
09.55	1.8454	-05.673	1.7365	0.8012	0.5020	0.5256	-0.0052	-0.2775	0.2162	0.3237	-09.359	029.89	064
09.73	1.9218	-05.905	1.8097	0.8170	0.4995	0.5232	-0.0153	-0.2573	0.2112	0.3237	-09.335	029.89	065
09.91	1.9654	-06.057	1.8499	0.8318	0.5012	0.5261	-0.0208	-0.2385	0.2130	0.3249	-09.362	029.89	066
09.98	1.9701	-06.073	1.8548	0.8268	0.4928	0.5194	-0.0009	-0.2608	0.2102	0.3266	-09.365	029.86	067
10.33	2.0423	-06.306	1.9395	0.8602	0.4986	0.5251	-0.0310	-0.2668	0.2107	0.3265	-09.289	029.92	068
10.48	2.0709	-06.352	1.9455	0.8677	0.4993	0.5264	-0.0074	-0.2968	0.2191	0.3271	-09.318	029.86	069
10.48	2.0938	-06.462	1.9691	0.8662	0.4937	0.5207	-0.0200	-0.2966	0.2093	0.3271	-09.376	029.86	070
10.50	2.1003	-06.491	1.9749	0.8694	0.4949	0.5208	-0.0043	-0.3177	0.2075	0.3259	-09.390	029.86	071
10.53	2.1222	-06.552	1.9959	0.8755	0.4961	0.5214	-0.0174	-0.2667	0.2068	0.3253	-09.380	029.92	072
10.58	2.1266	-06.579	1.9997	0.8763	0.4963	0.5225	-0.0252	-0.2776	0.2096	0.3282	-09.399	029.89	073
10.40	2.0314	-06.397	1.9576	0.8643	0.4967	0.5232	-0.0155	-0.3133	0.2082	0.3265	-09.337	029.89	074
00.01	0.0014	-00.058	0.0012	0.4709	0.4709	0.4927	0.0283	-0.0675	0.1918	0.3217	-30.097	029.89	075

MSWT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUV 006 MAC-4 MD 0.605 RN/L 06617933 Q 0902 PSF TD 594

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.17	0.3266	-0.130	0.0254	0.3910	0.3909	0.6019	0.0109	-0.0169	0.1844	0.0110	-14.859	031.41	006
-10.67	-2.0160	06.051	-1.9132	0.7344	0.3675	0.3888	-0.0656	0.4281	0.2138	0.0213	-09.119	031.34	007
-10.37	-1.8705	05.637	-1.7734	0.7008	0.3703	0.3896	-0.0434	0.3021	0.2180	0.0194	-09.156	031.44	008
-10.04	-1.8778	05.655	-1.7841	0.6944	0.3728	0.3912	-0.0337	0.3009	0.2227	0.0183	-09.159	031.31	009
-09.68	-1.7190	05.224	-1.6316	0.6579	0.3742	0.3927	-0.0314	0.3439	0.2129	0.0185	-09.232	031.28	010
-09.32	-1.6867	05.175	-1.6240	0.6415	0.3731	0.3902	-0.0375	0.3430	0.2167	0.0170	-09.321	031.31	011
-08.95	-1.5776	04.843	-1.5010	0.6095	0.3686	0.3895	-0.0512	0.3505	0.2140	0.0209	-09.326	031.25	012
-08.60	-1.4817	04.478	-1.4080	0.5989	0.3815	0.3983	-0.0407	0.2864	0.2117	0.0168	-09.182	031.28	013
-08.25	-1.4164	04.247	-1.3468	0.5822	0.3828	0.3934	-0.0254	0.2937	0.2140	0.0166	-09.108	031.31	014
-07.90	-1.3613	04.096	-1.2960	0.5645	0.3810	0.3958	-0.0143	0.2523	0.2127	0.0147	-09.141	031.28	015
-07.53	-1.2848	03.906	-1.2237	0.5472	0.3822	0.3918	-0.0148	0.2635	0.2081	0.0097	-09.236	031.31	016
-07.19	-1.1664	03.558	-1.1091	0.5278	0.3849	0.3966	-0.0213	0.2901	0.2087	0.0117	-09.266	031.41	017
-06.88	-1.1667	03.484	-1.1128	0.5169	0.3800	0.3934	-0.0142	0.2097	0.2084	0.0134	-09.071	031.41	018
-06.52	-1.0699	03.141	-1.0189	0.5072	0.3883	0.3984	-0.0034	0.2055	0.2058	0.0102	-08.919	031.34	019
-06.18	-0.9862	02.909	-0.9393	0.4803	0.3824	0.3947	-0.0156	0.2532	0.2044	0.0123	-09.063	031.31	020
-05.83	-0.9555	02.849	-0.9112	0.4815	0.3864	0.3939	-0.0140	0.1337	0.2060	0.0075	-09.057	031.34	021
-05.44	-0.8916	02.638	-0.8505	0.4744	0.3915	0.3975	-0.0201	0.1482	0.2058	0.0059	-08.988	031.28	022
-05.08	-0.8226	02.402	-0.7854	0.4588	0.3835	0.3917	-0.0191	0.0895	0.2033	0.0082	-08.670	031.37	023
-04.71	-0.7371	02.090	-0.7025	0.4500	0.3908	0.3986	-0.0080	0.1014	0.2044	0.0079	-08.613	031.28	024
-04.34	-0.6672	01.897	-0.6354	0.4444	0.3950	0.4056	-0.0086	0.0754	0.2027	0.0107	-08.637	031.28	025
-03.97	-0.6121	01.757	-0.5836	0.4317	0.3903	0.3976	-0.0013	0.1262	0.1973	0.0073	-08.720	031.31	026
-03.61	-0.5405	01.543	-0.5147	0.4267	0.3934	0.4017	0.0013	0.1057	0.1998	0.0083	-08.673	031.28	027
-03.26	-0.4814	01.316	-0.4586	0.4157	0.3880	0.3954	0.0014	0.0943	0.1985	0.0075	-08.307	031.41	028
-02.90	-0.4508	01.212	-0.4306	0.4122	0.3899	0.4005	0.0246	0.0182	0.2010	0.0106	-08.164	031.41	029
-02.54	-0.3737	00.982	-0.3559	0.4038	0.3928	0.4013	0.0076	0.0182	0.1963	0.0085	-07.984	031.31	030
-02.18	-0.3141	00.854	-0.2990	0.4038	0.3921	0.3985	-0.0068	-0.0148	0.1935	0.0064	-08.257	031.25	031
-01.85	-0.2950	00.779	-0.2821	0.4065	0.3972	0.4031	0.0176	-0.0462	0.1959	0.0059	-08.024	031.28	032
-01.49	-0.2365	00.599	-0.2262	0.3973	0.3913	0.3972	0.0104	0.0043	0.1913	0.0059	-07.694	031.31	033
-01.12	-0.1672	00.400	-0.1595	0.3947	0.3915	0.4006	-0.0206	-0.0132	0.1899	0.0090	-07.264	031.25	034
-00.76	-0.1148	00.272	-0.1096	0.3944	0.3929	0.4016	0.0245	0.0027	0.1872	0.0087	-07.184	031.28	035
-00.41	-0.0642	00.149	-0.0614	0.3987	0.3982	0.4042	0.0239	-0.0183	0.1802	0.0059	-07.039	031.28	036
-00.06	0.0252	00.049	-0.0247	0.3995	0.3995	0.4070	0.0008	-0.0198	0.1874	0.0076	-05.870	031.31	037
00.30	0.0251	-00.076	0.0231	0.3914	0.3912	0.3988	0.0045	0.0432	0.1868	0.0076	-09.258	031.28	038
00.55	0.0510	-00.179	0.0464	0.3985	0.3980	0.4031	0.0268	-0.0116	0.1866	0.0052	-10.665	031.34	039
01.01	0.1276	-00.354	0.1207	0.3921	0.3899	0.3959	0.0207	-0.0227	0.1868	0.0059	-08.425	031.28	040
01.40	0.1847	-00.529	0.1751	0.3941	0.3898	0.3978	0.0202	-0.0565	0.1875	0.0080	-08.701	031.28	041
01.73	0.2104	-00.607	0.1984	0.3997	0.3936	0.3978	0.0082	-0.1113	0.1913	0.0043	-08.759	031.28	042
02.09	0.2927	-00.831	0.2780	0.4068	0.3964	0.4032	0.0073	-0.0206	0.1903	0.0068	-08.623	031.34	043
02.44	0.3168	-00.903	0.2997	0.4071	0.3940	0.4041	0.0293	-0.0629	0.1907	0.0101	-08.660	031.41	044
02.80	0.4082	-01.109	0.3884	0.4166	0.3971	0.4034	0.0174	-0.0635	0.1928	0.0063	-08.250	031.37	045
03.18	0.4433	-01.201	0.4209	0.4163	0.3923	0.3982	0.0338	-0.1175	0.1902	0.0059	-08.227	031.34	046
03.53	0.5213	-01.430	0.4957	0.4306	0.3993	0.4044	0.0222	-0.1532	0.1947	0.0052	-08.335	031.34	047
03.88	0.5544	-01.587	0.5263	0.4331	0.3965	0.4043	0.0157	-0.1057	0.1945	0.0078	-08.699	031.37	048
04.26	0.6111	-01.737	0.5802	0.4381	0.3939	0.4040	0.0146	-0.0811	0.1972	0.0101	-08.636	031.37	049
04.57	0.6633	-01.885	0.6296	0.4484	0.3869	0.4083	0.0255	-0.0904	0.1979	0.0115	-08.634	031.21	050
04.93	0.7479	-02.122	0.7113	0.4588	0.3939	0.4011	0.0076	-0.1022	0.1987	0.0072	-08.621	031.21	051
05.30	0.8014	-02.289	0.7618	0.4660	0.3916	0.3997	0.0342	-0.0737	0.1986	0.0080	-08.678	031.28	052
05.69	0.8687	-02.475	0.8252	0.4796	0.3955	0.4054	0.0342	-0.1413	0.2013	0.0099	-08.654	031.31	053
06.05	1.0016	-02.867	0.9542	0.4995	0.3961	0.4061	0.0499	-0.1701	0.1993	0.0100	-08.696	031.28	054
06.41	1.0549	-03.102	1.0033	0.5185	0.4033	0.4156	0.0723	-0.2470	0.2013	0.0123	-08.933	031.28	055
06.77	1.1167	-03.303	1.0627	0.5208	0.3919	0.4156	0.0488	-0.2587	0.2030	0.0099	-08.986	031.34	056

MSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 006 MACH NO 0.605 RW/L 06617933 Q 0902 PSF TD 594

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PHI
07.13	1.2063	-03.555	1.1482	0.5397	0.3930	0.4029	0.0593	-0.3130	0.2062	0.0099	-06.952	031.34	057
07.47	1.2635	-03.750	1.2023	0.5491	0.3881	0.3995	0.0420	-0.2918	0.2039	0.0114	-09.017	031.28	058
07.88	1.3274	-03.953	1.2623	0.5614	0.3830	0.3944	0.0408	-0.2661	0.2037	0.0114	-09.048	031.28	059
08.22	1.3790	-04.165	1.3089	0.5847	0.3917	0.4039	0.0506	-0.2259	0.2068	0.0122	-09.176	031.34	060
08.60	1.5087	-04.511	1.4336	0.6102	0.3889	0.4015	0.0373	-0.2136	0.2113	0.0126	-09.083	031.31	061
08.91	1.5836	-04.765	1.5044	0.6281	0.3876	0.3975	0.0401	-0.2056	0.2099	0.0099	-09.141	031.31	062
09.20	1.6753	-04.952	1.5920	0.6492	0.3864	0.3947	0.0350	-0.2450	0.2073	0.0083	-08.980	031.31	063
09.45	1.6974	-05.043	1.6114	0.6567	0.3831	0.3930	0.0485	-0.2555	0.2098	0.0099	-09.026	031.34	064
09.66	1.8008	-05.316	1.7103	0.6837	0.3870	0.3993	0.0465	-0.2750	0.2103	0.0123	-08.968	031.31	065
09.84	1.7993	-05.345	1.7089	0.6764	0.3744	0.3867	0.0399	-0.2269	0.2103	0.0122	-09.024	031.34	066
09.97	1.8243	-05.419	1.7317	0.6862	0.3761	0.3869	0.0392	-0.2374	0.2123	0.0108	-09.024	031.37	067
10.17	1.8761	-05.571	1.7795	0.7050	0.3796	0.3881	0.0352	-0.3126	0.2066	0.0085	-09.021	031.37	068
10.43	1.9373	-05.803	1.8352	0.7309	0.3865	0.3965	0.0596	-0.3449	0.2112	0.0099	-09.100	031.31	069
10.54	1.9520	-05.845	1.8507	0.7248	0.3741	0.3837	0.0481	-0.4013	0.2070	0.0097	-09.096	031.31	070
10.58	1.9538	-05.926	1.8509	0.7315	0.3791	0.3888	0.0424	-0.4356	0.2098	0.0097	-09.214	031.31	071
10.56	1.9525	-05.963	1.8509	0.7255	0.3741	0.3864	0.0533	-0.3777	0.2098	0.0123	-09.278	031.31	072
10.62	1.9806	-05.927	1.8782	0.7301	0.3716	0.3839	0.0291	-0.1941	0.2127	0.0123	-09.092	031.31	073
10.33	1.9048	-05.649	1.8043	0.7237	0.3884	0.3998	0.0384	-0.3285	0.2115	0.0114	-09.009	031.28	074
-00.31	0.0124	-00.079	0.0124	0.3868	0.3868	0.3935	0.0155	0.0685	0.1827	0.0066	-19.396	031.31	070

HSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 007 MACH NO 0.603 RN/L 06930194 Q 0899 PSF TD 572

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.20	-0.0060	00.024	-0.0073	0.3758	0.3758	0.3668	0.0109	-0.0214	0.0021	-0.0090	-12.354	031.54	004
00.19	0.0210	-00.104	0.0197	0.3791	0.3791	0.3764	0.0119	-0.1133	0.0321	-0.0026	-15.038	031.60	005
00.13	-0.0013	-00.028	0.0001	0.3683	0.3683	0.3695	0.0338	-0.1100	0.0321	-0.0026	-15.038	031.44	006
-10.90	-2.0433	06.081	-1.9418	0.7219	0.3416	0.3574	0.0127	0.0451	0.0031	0.0157	-09.042	031.41	007
-10.62	-1.9480	05.878	-1.8503	0.7024	0.3494	0.3617	0.0059	0.0860	0.0024	0.0123	-09.166	031.31	008
-10.29	-1.8495	05.647	-1.7569	0.6765	0.3519	0.3678	0.0137	0.0364	0.0019	0.0159	-09.275	031.25	009
-09.91	-1.7918	05.425	-1.7041	0.6572	0.3664	-0.0100	0.0926	-0.0017	-0.0017	0.0122	-09.198	031.34	010
-09.58	-1.7434	05.336	-1.6600	0.6404	0.3553	0.0059	0.0386	0.0028	0.0028	0.0101	-09.299	031.37	011
-09.23	-1.6237	04.915	-1.5447	0.6176	0.3618	0.3693	0.0318	-0.0300	0.0051	0.0076	-09.197	031.31	012
-08.86	-1.5906	04.787	-1.5166	0.5979	0.3574	0.3673	0.0310	-0.0388	0.0058	0.0099	-09.143	031.31	013
-08.52	-1.5647	04.517	-1.4944	0.5783	0.3653	0.3719	0.0439	0.0186	0.0025	0.0066	-09.369	031.28	014
-08.14	-1.5336	04.277	-1.4700	0.5492	0.3583	0.3618	0.0135	0.0874	0.0021	0.0035	-09.460	031.41	015
-07.80	-1.2732	03.914	-1.2113	0.5390	0.3697	0.3749	0.0352	0.0629	0.0007	0.0052	-09.339	031.34	016
-07.43	-1.2318	03.743	-1.1738	0.5249	0.3687	0.3772	0.0301	0.0406	0.0042	0.0085	-09.224	031.31	017
-07.10	-1.1553	03.459	-1.1015	0.5039	0.3640	0.3691	0.0350	0.0201	0.0040	0.0051	-09.097	031.44	018
-06.76	-1.0476	03.152	-0.9864	0.4937	0.3730	0.3788	0.0352	-0.0349	0.0054	0.0058	-09.140	031.54	019
-06.44	-1.0100	03.072	-0.9616	0.4853	0.3744	0.3804	0.0291	-0.0225	0.0028	0.0060	-09.241	031.54	020
-06.08	-0.8841	02.693	-0.8390	0.4730	0.3785	0.3825	0.0176	-0.0320	0.0033	0.0040	-09.245	031.37	021
-05.74	-0.8432	02.482	-0.8006	0.4655	0.3831	0.3836	0.0280	-0.0032	0.0023	0.0035	-08.943	031.37	022
-05.35	-0.8180	02.375	-0.7788	0.4568	0.3823	0.3851	0.0058	0.0062	0.0028	0.0028	-08.821	031.31	023
-05.00	-0.7360	02.143	-0.7003	0.4396	0.3769	0.3821	0.0047	0.0331	0.0010	0.0052	-08.869	031.31	024
-04.63	-0.6803	01.977	-0.6475	0.4324	0.3787	0.3827	0.0160	-0.0103	0.0027	0.0041	-08.828	031.21	025
-04.26	-0.6471	01.853	-0.6175	0.4233	0.3732	0.3765	-0.0008	-0.0117	0.0028	0.0033	-08.701	031.31	026
-03.90	-0.5551	01.559	-0.5309	0.4097	0.3762	0.3774	0.0266	0.0617	0.0033	0.0012	-08.532	031.31	027
-03.53	-0.4311	01.196	-0.4095	0.4051	0.3819	0.3831	0.0200	-0.0577	0.0022	0.0012	-08.424	031.37	028
-03.15	-0.4066	01.096	-0.3875	0.4008	0.3814	0.3772	0.0195	-0.0328	0.0020	0.0042	-08.188	031.37	029
-02.80	-0.3194	00.874	-0.3031	0.3905	0.3773	0.3794	0.0134	-0.0428	0.0019	0.0021	-08.315	031.37	030
-02.44	-0.2810	00.723	-0.2671	0.3894	0.3795	0.3778	0.0247	-0.0627	0.0023	0.0017	-07.786	031.41	032
-02.08	-0.2426	00.618	-0.2309	0.3891	0.3819	0.3803	0.0296	-0.0486	0.0017	0.0017	-07.737	031.44	033
-01.75	-0.1676	00.366	-0.1583	0.3847	0.3807	0.3769	0.0292	-0.0341	0.0019	0.0038	-06.638	031.47	034
-01.40	-0.1116	00.245	-0.1049	0.3788	0.3769	0.3769	0.0408	-0.1018	0.0023	0.0000	-06.640	031.41	035
-00.86	-0.0753	00.174	-0.0709	0.3809	0.3801	0.3856	0.0064	-0.0246	0.0008	0.0036	-07.012	031.28	036
-00.31	-0.0367	00.099	-0.0347	0.3800	0.3798	0.3777	-0.0046	-0.0726	0.0013	0.0021	-08.195	031.31	037
00.35	0.0065	00.001	0.0062	0.3779	0.3779	0.3775	0.0171	-0.0564	0.0032	0.0004	00.332	031.31	038
00.40	0.0519	-00.153	0.0493	0.3800	0.3797	0.3783	0.0394	-0.0862	0.0009	0.0014	-08.947	031.31	043
00.76	0.1021	-00.301	0.0971	0.3820	0.3807	0.3786	0.0110	-0.0770	0.0025	0.0021	-08.965	031.34	040
01.12	0.1459	-00.374	0.1385	0.3830	0.3802	0.3785	0.0221	-0.0983	0.0046	0.0017	-07.789	031.41	041
01.48	0.1905	-00.474	0.1806	0.3850	0.3802	0.3778	0.0279	-0.1430	0.0020	0.0024	-07.536	031.41	042
01.84	0.2360	-00.576	0.2236	0.3912	0.3838	0.3821	0.0271	-0.0606	0.0025	0.0017	-07.438	031.31	043
02.23	0.3044	-00.750	0.2894	0.3924	0.3809	0.3804	0.0263	-0.0469	0.0045	0.0004	-07.481	031.28	044
02.56	0.3458	-00.867	0.3287	0.3924	0.3773	0.3752	0.0040	-0.0720	0.0029	0.0021	-07.613	031.34	045
02.91	0.4223	-01.092	0.4026	0.4000	0.3791	0.3756	0.0206	-0.1369	0.0037	0.0035	-07.858	031.37	046
03.28	0.4726	-01.235	0.4499	0.4082	0.3818	0.3808	0.0370	-0.0987	0.0011	0.0010	-07.937	031.31	047
03.63	0.5318	-01.424	0.5071	0.4065	0.3736	0.3771	0.0252	-0.1091	0.0009	0.0035	-08.136	031.34	048
03.99	0.5790	-01.565	0.5520	0.4081	0.3687	0.3739	0.0249	-0.1303	0.0021	0.0051	-08.211	031.41	049
04.34	0.6031	-01.681	0.5727	0.4235	0.3790	0.3804	0.0192	-0.0963	0.0038	0.0014	-08.470	031.37	050
04.68	0.7404	-01.998	0.7075	0.4324	0.3732	0.3739	0.0236	-0.1036	0.0045	0.0007	-08.198	031.41	051
05.07	0.8172	-02.278	0.7804	0.4510	0.3803	0.3810	0.0449	-0.0846	0.0020	0.0007	-08.468	031.41	052
05.43	0.8596	-02.441	0.8206	0.4514	0.3717	0.3757	0.0564	-0.1290	0.0055	0.0040	-08.628	031.41	053
05.77	0.9125	-02.604	0.8656	0.4706	0.3808	0.3836	0.0339	-0.1536	0.0053	0.0028	-08.669	031.37	054

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 007 MACH NO 0.603 RN/L 06930194 Q 0899 PSF TO 572

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
06.15	1.0056	-02.099	0.9595	0.4821	0.3764	0.3794	0.0220	-0.1522	0.0071	0.3030	-08.757	031.44	055
06.52	1.0889	-03.170	1.0387	0.5020	0.3809	0.3832	0.0160	-0.1509	0.0037	0.0023	-08.845	031.41	056
06.91	1.1354	-03.303	1.0814	0.5163	0.3805	0.3836	0.0210	-0.1138	0.0046	0.3030	-08.839	031.37	057
07.24	1.2259	-03.558	1.1687	0.5282	0.3767	0.3802	0.0374	-0.1672	0.0047	0.3036	-08.816	031.31	058
07.60	1.2745	-03.772	1.2136	0.5404	0.3752	0.3804	0.0206	-0.1682	0.0049	0.3052	-08.991	031.31	059
07.96	1.3915	-04.088	1.3272	0.5566	0.3673	0.3741	0.0073	-0.0604	0.0045	0.3068	-08.925	031.34	060
08.35	1.3988	-04.187	1.3296	0.5730	0.3738	0.3816	0.0307	-0.1510	0.0088	0.0078	-09.053	031.34	061
08.69	1.5033	-04.445	1.4303	0.5821	0.3693	0.3811	0.0232	-0.1124	0.0073	0.3118	-08.983	031.34	062
09.02	1.5372	-04.873	1.5584	0.6262	0.3743	0.3826	0.0311	-0.1363	0.0036	0.3083	-09.042	031.28	063
09.30	1.6455	-04.918	1.5648	0.6267	0.3656	0.3746	0.0242	-0.0649	0.0073	0.3090	-09.081	031.31	064
09.53	1.7689	-05.227	1.6838	0.6544	0.3666	0.3772	0.0153	-0.0009	0.0085	0.3106	-08.977	031.31	065
09.74	1.7522	-05.191	1.6631	0.6568	0.3657	0.3733	0.0214	-0.0238	0.0074	0.3075	-09.000	031.34	066
09.89	1.8836	-05.522	1.7920	0.6882	0.3701	0.3779	0.0127	0.0167	0.0087	0.3078	-08.905	031.34	067
10.02	1.8367	-05.441	1.7442	0.6842	0.3703	0.3779	0.0196	-0.0196	0.0098	0.3076	-08.999	031.31	068
10.26	1.9115	-05.643	1.8159	0.6995	0.3650	0.3749	0.0176	-0.0151	0.0108	0.3099	-08.968	031.34	069
10.47	1.9764	-05.790	1.8787	0.7093	0.3561	0.3684	0.0162	0.0117	0.0077	0.3123	-08.901	031.31	070
10.57	1.9831	-05.831	1.8835	0.7168	0.3591	0.3673	0.0095	0.0479	0.0065	0.3082	-08.933	031.34	071
10.59	2.0145	-05.987	1.9138	0.7251	0.3609	0.3716	0.0093	0.0267	0.0064	0.3107	-09.028	031.28	072
10.57	1.9632	-05.796	1.8644	0.7107	0.3566	0.3655	0.0217	-0.0326	0.0055	0.3090	-08.969	031.31	073
10.55	4.8840	-14.298	4.8301	0.6997	-0.2068	0.8946	-0.0362	0.0633	0.0199	1.1015	-08.894	027.15	074
10.47	1.9934	-05.841	1.8918	0.7328	0.3769	0.3844	-0.0013	0.0332	0.0108	0.3075	-08.901	031.34	075
-00.01	0.0071	-00.027	0.0072	0.3763	0.3763	0.3744	0.0510	0.0975	0.0025	-0.3019	-11.448	031.31	076
-00.01	0.0071	-00.027	0.0071	0.3708	0.3708	0.3720	0.0395	-0.0871	0.0025	0.3012	-11.379	031.34	077
00.02	-0.0042	-00.030	-0.0043	0.3720	0.3720	0.3732	0.0464	-0.1702	0.0065	0.3012	21.941	031.28	078

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 008 MACH NO 0.808 RN/L 07667581 Q 1304 PSF TD 594

COEFFICIENTS

ALP-4	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00-22	0.3314	00.088	0.0296	0.4676	0.4675	0.4785	0.0198	-0.0848	-0.0022	0.3110	-08.458	030.54	005
00-22	0.7457	00.123	0.0439	0.4709	0.4707	0.4846	0.0280	-0.1647	0.0012	0.3139	-08.170	030.57	006
-10-76	-2.0481	06.609	-2.0233	0.8593	0.8666	0.8694	-0.0163	-0.1169	0.0049	0.3228	-09.346	030.44	000
-10-39	-2.0474	06.402	-1.9292	0.8308	0.8692	0.8925	-0.0182	-0.0259	0.0032	0.3233	-09.350	030.44	008
-10-06	-1.9383	06.105	-1.8262	0.8022	0.8728	0.8935	-0.0185	-0.0385	0.0031	0.3227	-09.568	030.54	009
-09-71	-1.8403	05.796	-1.7334	0.7809	0.8773	0.8980	-0.0112	-0.0618	0.0028	0.3207	-09.569	030.47	010
-09-37	-1.7783	05.563	-1.6765	0.7627	0.8796	0.9004	0.0031	-0.0932	0.0037	0.3208	-09.504	030.41	011
-09-02	-1.7166	05.361	-1.6208	0.7395	0.8763	0.8954	0.0276	-0.0490	0.0010	0.3191	-09.680	030.47	012
-08-54	-1.5868	04.999	-1.4764	0.7144	0.8814	0.9011	0.0061	-0.0373	0.0011	0.3197	-09.571	030.63	013
-08-29	-1.5538	04.906	-1.4673	0.7057	0.8868	0.9057	0.0206	-0.0669	0.0050	0.3190	-09.593	030.50	014
-07-94	-1.4029	04.463	-1.3220	0.6773	0.8881	0.9065	0.0022	-0.0176	0.0022	0.3184	-09.666	030.41	015
-07-60	-1.3136	04.149	-1.2382	0.6523	0.8828	0.9016	0.0043	-0.0750	0.0036	0.3188	-09.595	030.34	016
-07-27	-1.2847	04.009	-1.2138	0.6377	0.8791	0.8961	0.0003	-0.0970	0.0029	0.3170	-09.681	030.44	017
-06-90	-1.2328	03.871	-1.1660	0.6261	0.8815	0.9005	-0.0086	-0.0875	0.0039	0.3190	-09.539	030.47	018
-06-57	-1.1173	03.549	-1.0549	0.6068	0.8822	0.9018	-0.0001	-0.0436	0.0005	0.3196	-09.650	030.38	019
-06-23	-1.0438	03.296	-0.9852	0.5936	0.8831	0.9029	0.0138	-0.0380	0.0024	0.3198	-09.593	030.44	020
-05-85	-0.9735	03.013	-0.9163	0.5790	0.8826	0.9012	0.0124	-0.0409	0.0058	0.3187	-09.431	030.54	021
-05-55	-0.9072	02.808	-0.8555	0.5754	0.8900	0.9071	0.0083	-0.0712	0.0043	0.3172	-09.402	030.44	022
-05-18	-0.8148	02.506	-0.7676	0.5577	0.8861	0.9037	0.0265	-0.0156	0.0070	0.3176	-09.342	030.44	023
-04-82	-0.7692	02.346	-0.7260	0.5451	0.8822	0.8981	0.0225	-0.0146	0.0084	0.3159	-09.266	030.54	024
-04-42	-0.6950	02.101	-0.6556	0.5357	0.8835	0.8984	0.0222	-0.0118	0.0059	0.3149	-09.185	030.57	025
-04-06	-0.6328	01.897	-0.5968	0.5308	0.8873	0.9028	0.0146	-0.0108	0.0051	0.3156	-09.108	030.41	026
-03-73	-0.5954	01.732	-0.5627	0.5206	0.8829	0.8978	-0.0005	-0.0361	0.0033	0.3149	-08.837	030.41	027
-03-34	-0.5198	01.501	-0.4957	0.5123	0.8828	0.8971	0.0108	-0.0397	0.0031	0.3142	-08.771	030.41	028
-03-01	-0.4344	01.285	-0.4385	0.5043	0.8822	0.8948	0.0022	-0.0062	0.0032	0.3126	-08.987	030.54	029
-02-63	-0.3846	01.118	-0.3619	0.5018	0.8846	0.8969	0.0021	-0.0124	0.0024	0.3122	-08.829	030.47	030
-02-27	-0.3375	00.946	-0.3180	0.4999	0.8869	0.9003	0.0063	-0.0506	0.0037	0.3134	-08.518	030.41	031
-01-94	-0.2740	00.749	-0.2576	0.4883	0.8793	0.8920	0.0020	-0.0328	0.0019	0.3127	-08.299	030.44	032
-01-59	-0.2253	00.591	-0.2119	0.4866	0.8805	0.8933	0.0217	-0.0851	0.0022	0.3128	-07.968	030.41	033
-01-24	-0.1587	00.434	-0.1483	0.4843	0.8810	0.8920	0.0208	-0.0669	0.0027	0.3111	-08.300	030.47	034
-00-86	-0.0924	00.242	-0.0853	0.4791	0.8778	0.8905	0.0053	-0.0836	0.0002	0.3127	-07.956	030.44	035
-00-54	-0.0699	00.171	-0.0654	0.4760	0.8753	0.8875	0.0282	-0.0867	0.0039	0.3122	-07.433	030.50	036
-00-16	-0.0167	00.032	-0.0153	0.4792	0.8792	0.8871	0.0164	-0.1028	0.0017	0.3079	-05.876	030.63	037
00-17	0.0319	00.088	0.0305	0.4799	0.8798	0.8890	0.0160	-0.1021	0.0005	0.3092	-08.362	030.60	038
00-56	0.0851	00.213	0.0804	0.4805	0.8797	0.8910	0.0154	-0.0695	0.0014	0.3113	-07.499	030.38	039
00-92	0.1429	00.349	0.1353	0.4755	0.8733	0.8866	0.0152	-0.0091	0.0018	0.3133	-07.420	030.34	040
01-25	0.1901	00.467	0.1798	0.4750	0.8709	0.8835	0.0223	-0.1140	0.0027	0.3126	-07.469	030.41	041
01-64	0.2249	00.553	0.2113	0.4788	0.8726	0.8837	0.0259	-0.1285	0.0029	0.3111	-07.470	030.47	042
01-99	0.2819	00.727	0.2653	0.4829	0.8734	0.8851	-0.0022	-0.0662	0.0030	0.3117	-07.833	030.50	043
02-35	0.3268	00.869	0.3072	0.4857	0.8727	0.8856	0.0170	-0.1025	0.0046	0.3129	-08.075	030.50	044
02-70	0.3738	01.071	0.3810	0.4930	0.8745	0.8856	0.0043	-0.0696	0.0057	0.3112	-08.055	030.57	045
03-05	0.4689	01.270	0.4428	0.5017	0.8774	0.8887	0.0237	-0.1541	0.0054	0.3112	-08.230	030.50	046
03-25	0.5382	01.453	0.5092	0.5113	0.8806	0.8924	0.0151	-0.1138	0.0063	0.3118	-08.200	030.41	047
03-75	0.6032	01.659	0.5705	0.5179	0.8795	0.8917	0.0066	-0.1129	0.0086	0.3123	-08.355	030.44	048
04-12	0.6691	01.868	0.6330	0.5252	0.8783	0.8911	0.0174	-0.1083	0.0072	0.3127	-08.481	030.44	049
04-68	0.7360	02.062	0.6950	0.5394	0.8834	0.8956	0.0047	-0.0595	0.0073	0.3123	-08.512	030.44	050
04-84	0.8069	02.243	0.7435	0.5455	0.8808	0.8942	-0.0108	-0.1015	0.0087	0.3134	-08.658	030.44	051
05-18	0.8581	02.467	0.8112	0.5559	0.8804	0.8955	0.0116	-0.0873	0.0076	0.3151	-08.735	030.38	052
05-56	0.9739	02.821	0.9229	0.5711	0.8789	0.8961	-0.0044	-0.1513	0.0093	0.3172	-08.800	030.44	053
05-92	1.0436	03.059	0.9886	0.5842	0.8790	0.8962	-0.0136	-0.1172	0.0105	0.3172	-08.905	030.41	054
06-28	1.1381	03.363	1.0786	0.6024	0.8808	0.8992	-0.0092	-0.0441	0.0105	0.3184	-08.976	030.41	055

MSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 008 MACH NO 0.808 RN/L 07667581 Q 1304 PSF TD 594

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
06.64	1.1897	-03.550	1.1259	0.6166	0.4823	0.4990	-0.0024	-0.1045	0.0126	0.3167	-09.065	030.44	056
07.00	1.2643	-03.789	1.1962	0.6321	0.4816	0.5000	-0.0123	-0.0769	0.0133	0.3184	-09.105	030.41	057
07.36	1.3415	-04.026	1.2691	0.6465	0.4785	0.4985	-0.0103	-0.0934	0.0128	0.3200	-09.117	030.44	058
07.72	1.4224	-04.292	1.3451	0.6665	0.4798	0.4991	-0.0322	-0.0606	0.0129	0.3193	-09.167	030.41	059
08.10	1.4751	-04.488	1.3928	0.6829	0.4798	0.4980	-0.0379	-0.0320	0.0117	0.3181	-09.244	030.44	060
08.43	1.5900	-04.846	1.5018	0.7121	0.4842	0.5047	-0.0252	-0.0550	0.0092	0.3205	-09.259	030.41	061
08.79	1.6748	-05.115	1.5814	0.7327	0.4825	0.5046	-0.0239	-0.0316	0.0069	0.3221	-09.278	030.44	062
09.12	1.7581	-05.369	1.6600	0.7513	0.4787	0.5013	-0.0373	-0.0614	0.0068	0.3226	-09.278	030.41	063
09.37	1.8248	-05.581	1.7224	0.7698	0.4790	0.5016	-0.0239	-0.0380	0.0073	0.3226	-09.291	030.41	064
09.60	1.8669	-05.732	1.7615	0.7803	0.4756	0.4993	-0.0369	-0.0202	0.0063	0.3237	-09.327	030.44	065
09.78	1.8921	-05.830	1.7883	0.7876	0.4731	0.4974	-0.0300	-0.0087	0.0052	0.3243	-09.360	030.41	066
09.93	1.9447	-05.971	1.8336	0.8033	0.4750	0.4991	-0.0429	-0.0075	0.0052	0.3242	-09.328	030.44	067
10.06	2.0114	-06.177	1.8976	0.8190	0.4749	0.5015	-0.0444	-0.0039	0.0051	0.3266	-09.329	030.41	068
10.35	2.0714	-06.338	1.9522	0.8435	0.4761	0.5003	-0.0577	-0.0019	0.0053	0.3242	-09.296	030.44	069
10.51	2.0997	-06.415	1.9785	0.8465	0.4715	0.4985	-0.0235	-0.0181	0.0000	0.3270	-09.282	030.44	070
10.51	2.1161	-06.478	1.9945	0.8505	0.4726	0.4985	-0.0513	0.0104	0.0033	0.3259	-09.300	030.41	071
10.58	2.1428	-06.558	2.0195	0.8582	0.4727	0.4992	-0.0517	-0.0130	0.0028	0.3265	-09.298	030.34	072
10.61	2.1332	-06.551	2.0106	0.8529	0.4683	0.4957	-0.0513	-0.0372	0.0062	0.3275	-09.330	030.44	073
10.52	2.1237	-06.563	2.0015	0.8537	0.4737	0.4985	-0.0475	-0.0361	0.0035	0.3247	-09.389	030.41	074
10.43	2.0816	-06.423	1.9624	0.8387	0.4708	0.4977	-0.0275	-0.0058	0.0022	0.3269	-09.369	030.47	075
10.04	0.5100	-00.037	0.0396	0.4635	0.4774	0.4774	0.0244	0.1190	0.0011	0.3140	-11.298	030.38	076
00.07	0.0143	-00.055	0.0138	0.4627	0.4627	0.4766	0.0357	-0.1081	0.0003	0.3139	-11.641	030.41	077

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 009 MACH NU 1.021 RN/L 07307857 Q 1450 PSF TD 597

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
00.27	0.0333	-0.114	0.0291	0.8803	0.8801	1.0614	0.0252	-0.0765	-0.0017	0.1613	-10.398	026.73	005
00.25	0.0171	-00.066	0.0134	0.8684	0.8684	1.0264	0.0326	-0.0909	-0.0021	0.1560	-10.774	026.64	006
-10.46	-2.0922	36.283	-1.9001	1.2323	0.8676	1.0261	0.0457	-0.1574	-0.0022	0.1691	-09.123	026.83	007
-10.12	-1.9911	36.056	-1.8069	1.2081	0.8717	1.0588	0.0340	-0.0977	-0.0041	0.1872	-09.240	026.80	008
-09.76	-1.9112	35.895	-1.7351	1.1865	0.8752	1.0615	0.0329	-0.0963	-0.0007	0.1863	-09.371	026.70	009
-09.38	-1.7718	05.551	-1.6257	1.1510	0.8759	1.0591	0.0280	-0.0930	-0.0003	0.1852	-09.516	026.63	010
-09.05	-1.7312	05.455	-1.5713	1.1438	0.8795	1.0650	0.0273	-0.0701	0.0000	0.1855	-09.573	026.83	011
-08.67	-1.6090	05.121	-1.4574	1.1161	0.8836	1.0668	0.0259	-0.1158	0.0033	0.1832	-09.668	026.83	012
-08.32	-1.5651	04.908	-1.4203	1.1035	0.8864	1.0684	0.0245	-0.0616	-0.0029	0.1820	-09.682	026.73	013
-07.97	-1.4674	04.704	-1.3303	1.0813	0.8864	1.0673	0.0295	-0.0986	-0.0008	0.1809	-09.740	026.77	014
-07.61	-1.4025	04.561	-1.2724	1.0664	0.8804	1.0671	0.0244	-0.0817	-0.0002	0.1786	-09.880	026.77	015
-07.27	-1.2968	04.296	-1.1716	1.0474	0.8807	1.0682	0.0258	-0.0975	-0.0015	0.1775	-10.080	026.77	016
-06.91	-1.2369	04.113	-1.1193	1.0288	0.8866	1.0620	0.0311	-0.0852	-0.0007	0.1753	-10.118	026.86	017
-06.57	-1.1897	03.841	-1.0391	1.0170	0.8913	1.0613	0.0258	-0.0874	-0.0014	0.1700	-10.158	026.96	018
-06.24	-1.0932	03.636	-0.9899	1.0036	0.8900	1.0621	0.0212	-0.0837	-0.0017	0.1721	-10.136	026.90	019
-05.85	-1.0201	03.436	-0.9230	0.9989	0.8955	1.0724	0.0231	-0.1011	-0.0012	0.1729	-10.233	026.64	020
-05.55	-0.9462	03.247	-0.8534	0.9799	0.8927	1.0726	0.0179	-0.0905	-0.0020	0.1758	-10.446	026.51	021
-05.16	-0.8690	03.005	-0.7849	0.9672	0.8923	1.0548	0.0264	-0.0908	-0.0008	0.1625	-10.504	026.67	022
-04.82	-0.8133	02.827	-0.7373	0.9596	0.8943	1.0550	0.0184	-0.0955	-0.0007	0.1607	-10.533	026.70	023
-04.42	-0.7560	02.619	-0.6830	0.9460	0.8905	1.0500	0.0166	-0.0548	0.0002	0.1595	-10.553	026.83	024
-04.06	-0.7015	02.437	-0.6361	0.9460	0.8986	1.0590	0.0269	-0.0731	-0.0001	0.1634	-10.554	026.70	025
-03.72	-0.6275	02.221	-0.5677	0.9390	0.9002	1.0571	0.0094	-0.0811	-0.0003	0.1569	-10.751	026.64	026
-03.34	-0.5391	01.932	-0.4860	0.9263	0.8964	1.0529	0.0121	-0.0695	-0.0002	0.1565	-10.887	026.83	027
-02.99	-0.4326	01.777	-0.4453	0.9197	0.8922	1.0522	0.0082	-0.0470	0.0006	0.1599	-10.957	026.90	028
-02.61	-0.4376	01.587	-0.3961	0.9204	0.9015	1.0599	0.0117	-0.0808	0.0006	0.1584	-11.020	026.80	029
-02.26	-0.3058	01.327	-0.3300	0.9127	0.8990	1.0588	0.0089	-0.0646	-0.0008	0.1598	-11.028	026.73	030
-01.93	-0.3048	01.111	-0.2744	0.9067	0.8970	1.0659	0.0309	-0.0742	-0.0008	0.1689	-11.077	026.70	031
-01.61	-0.2582	00.938	-0.2330	0.9004	0.8935	1.0618	0.0253	-0.0743	-0.0016	0.1683	-11.035	026.70	032
-01.21	-0.1799	00.701	-0.1611	0.8951	0.8913	1.0577	0.0335	-0.0859	-0.0016	0.1662	-11.836	026.77	033
-00.86	-0.1250	00.510	-0.1116	0.8917	0.8899	1.0567	0.0385	-0.1058	-0.0030	0.1668	-12.396	026.83	034
-00.52	-0.0507	00.259	-0.0427	0.8939	0.8934	1.0635	0.0331	-0.1205	-0.0022	0.1701	-15.497	026.73	035
-00.20	-0.0115	00.098	-0.0085	0.8896	0.8895	1.0567	0.0060	-0.0652	-0.0025	0.1672	-25.662	026.80	036
00.18	0.0194	00.003	0.0166	0.8889	0.8888	1.0558	0.0316	-0.0753	-0.0011	0.1670	00.514	026.86	037
00.53	0.0842	00.205	0.0760	0.8877	0.8869	1.0557	0.0522	-0.0774	-0.0013	0.1688	-07.383	026.73	038
00.89	0.1291	00.364	0.1154	0.8876	0.8857	1.0504	0.0309	-0.1015	-0.0014	0.1647	-08.568	026.77	039
01.22	0.2032	00.585	0.1864	0.8901	0.8860	1.0526	0.0334	-0.0912	-0.0019	0.1666	-08.662	026.80	040
01.59	0.2750	00.827	0.2503	0.8917	0.8844	1.0499	0.0329	-0.1110	-0.0016	0.1655	-09.134	026.77	041
01.95	0.3475	01.065	0.3174	0.8921	0.8808	1.0452	0.0353	-0.0931	-0.0016	0.1644	-09.315	026.77	042
02.27	0.4034	01.270	0.3683	0.8938	0.8785	1.0448	0.0380	-0.1047	-0.0007	0.1663	-09.565	026.83	043
02.67	0.4614	01.467	0.4197	0.9041	0.8836	1.0506	0.0301	-0.0600	-0.0013	0.1670	-09.659	026.77	044
03.01	0.5370	01.717	0.4899	0.9072	0.8802	1.0475	0.0433	-0.0990	0.0002	0.1673	-09.714	026.80	045
03.34	0.5792	01.866	0.5269	0.9143	0.8821	1.0523	0.0289	-0.1002	0.0001	0.1703	-09.786	026.77	046
03.68	0.6440	02.074	0.5859	0.9229	0.8834	1.0517	0.0291	-0.0833	-0.0010	0.1684	-09.783	026.73	047
04.03	0.7094	02.315	0.6458	0.9285	0.8808	1.0536	0.0376	-0.0940	0.0013	0.1728	-09.914	026.73	048
04.38	0.7855	02.545	0.7139	0.9384	0.8811	1.0557	0.0333	-0.0918	0.0017	0.1746	-09.868	026.77	049
04.70	0.8572	02.773	0.7805	0.9557	0.8873	1.0595	0.0319	-0.1100	0.0019	0.1720	-09.829	026.80	050
05.10	0.9414	03.039	0.8587	0.9676	0.8873	1.0630	0.0438	-0.1253	0.0036	0.1756	-09.807	026.73	051
05.49	1.0061	03.230	0.9165	0.9802	0.8880	1.0662	0.0420	-0.1141	0.0028	0.1781	-09.754	026.70	052
05.85	1.0639	03.433	0.9680	0.9904	0.8866	1.0651	0.0392	-0.0572	0.0028	0.1785	-09.802	026.60	053
06.21	1.1525	03.701	1.0495	1.0085	0.8890	1.0690	0.0408	-0.1028	0.0038	0.1800	-09.756	026.80	054
06.57	1.2083	03.871	1.0986	1.0211	0.8887	1.0712	0.0323	-0.0863	0.0031	0.1825	-09.732	026.73	055

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 009 MACH NO 1.021 RM/L 07307867 Q 1450 PSF TD 597

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	EM	AB	CP	PO	PMT
06.88	1.2917	-04.108	1.1754	1.0409	0.8926	1.0724	0.0262	-0.0596	0.0037	0.1799	-09.662	026.77	056
07.30	1.3336	-04.274	1.2294	1.0556	0.8909	1.0715	0.0210	-0.0567	0.0040	0.1807	-09.594	026.80	057
07.66	1.4379	-04.525	1.3061	1.0761	0.8925	1.0742	0.0223	-0.0441	0.0043	0.1817	-09.560	026.73	058
08.02	1.5370	-04.773	1.3974	1.0983	0.8925	1.0741	0.0233	-0.0455	0.0027	0.1816	-09.434	026.70	059
08.38	1.6186	-05.002	1.4709	1.1208	0.8944	1.0753	0.0174	-0.0264	0.0020	0.1809	-09.388	026.73	060
08.74	1.6749	-05.194	1.5201	1.1350	0.8908	1.0761	0.0195	-0.0066	0.0027	0.1853	-09.422	026.77	061
09.08	1.7568	-05.395	1.5955	1.1490	0.8829	1.0726	0.0064	0.0027	0.0022	0.1857	-09.329	026.77	062
09.34	1.8352	-05.550	1.6673	1.1704	0.8842	1.0720	0.0152	-0.0065	-0.0017	0.1878	-09.187	026.73	063
09.60	1.8751	-05.654	1.7018	1.1818	0.8814	1.0696	0.0385	-0.0152	0.0007	0.1882	-09.161	026.67	064
09.78	1.9458	-05.846	1.7679	1.1984	0.8809	1.0687	0.0087	0.0204	0.0020	0.1878	-09.127	026.70	065
09.94	1.9803	-05.957	1.7979	1.2117	0.8826	1.0660	0.0182	-0.0047	0.0025	0.1835	-09.139	026.77	066
10.09	2.0173	-06.072	1.8322	1.2187	0.8789	1.0651	0.0017	0.1279	0.0028	0.1861	-09.145	026.73	067
10.26	2.0568	-06.149	1.8651	1.2356	0.8802	1.0634	0.0261	0.0452	0.0032	0.1832	-09.082	026.73	068
10.50	2.1132	-06.254	1.9180	1.2458	0.8748	1.0580	0.0172	0.0909	0.0010	0.1833	-08.991	026.80	069
10.65	2.1351	-06.312	1.9371	1.2562	0.8784	1.0640	0.0098	0.1203	0.0026	0.1835	-08.981	026.70	070
10.68	2.1471	-06.363	1.9483	1.2571	0.8754	1.0591	0.0097	0.0914	0.0023	0.1837	-09.004	026.73	071
10.68	2.1426	-06.334	1.9443	1.2520	0.8701	1.0559	0.0063	0.0901	0.0030	0.1848	-08.980	026.77	072
10.83	2.1517	-06.320	1.9532	1.2583	0.8764	1.0608	0.0068	0.0680	-0.0011	0.1844	-08.923	026.77	073
00.10	0.0127	-00.016	0.0112	0.8749	0.8749	1.0416	0.0567	-0.1516	-0.0027	0.1667	-03.848	026.73	074
00.10	0.0327	-00.079	0.0312	0.8781	0.8780	1.0465	0.0496	-0.1234	-0.0032	0.1685	-07.386	026.67	075

HSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 013 MACH NO 1.017 RM/L 07236308 Q 1444 PSF TD 600

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.34	-0.2258	00.073	0.0222	0.5923	0.5921	0.6525	0.0113	-0.0098	-0.0003	0.3603	06.608	026.83	005
00.34	-0.0301	30.258	0.0265	0.5983	0.5982	0.6575	0.0115	-0.0171	-0.0037	0.3594	05.809	026.64	006
-10.83	-0.8357	-02.853	-0.7106	0.7336	0.5870	0.6969	0.0915	0.0785	-0.0013	0.1099	10.370	026.80	007
-10.64	-0.8399	-02.758	-0.7167	0.7335	0.5886	0.6914	0.0879	0.0987	-0.0043	0.1028	09.976	026.77	008
-10.47	-0.8118	-02.725	-0.6921	0.7222	0.5844	0.6840	0.0877	0.0937	-0.0026	0.0996	10.198	026.73	009
-10.28	-0.7854	-02.624	-0.6578	0.7186	0.5879	0.6885	0.0800	0.0750	-0.0035	0.1005	10.422	026.70	010
-10.09	-0.7686	-02.626	-0.6568	0.7077	0.5821	0.6817	0.0757	0.0668	-0.0032	0.0997	10.379	026.67	011
-09.86	-0.7448	-02.541	-0.6349	0.6962	0.5771	0.6785	0.0888	0.0315	-0.0001	0.1013	10.366	026.64	012
-09.67	-0.7212	-02.525	-0.6139	0.6899	0.5769	0.6796	0.0771	0.0968	-0.0020	0.1026	10.639	026.61	013
-09.48	-0.6895	-02.461	-0.5845	0.6859	0.5803	0.6787	0.0800	0.0664	-0.0019	0.0984	10.845	026.64	014
-09.27	-0.6741	-02.404	-0.5719	0.6815	0.5805	0.6798	0.0796	0.0505	-0.0020	0.0993	10.834	026.67	015
-09.10	-0.6457	-02.374	-0.5455	0.6768	0.5819	0.6775	0.0719	0.0486	-0.0025	0.0955	11.168	026.73	016
-08.91	-0.6344	-02.299	-0.5370	0.6710	0.5797	0.6750	0.0677	0.0545	-0.0031	0.0953	11.009	026.77	017
-08.70	-0.6081	-02.277	-0.5128	0.6692	0.5840	0.6764	0.0634	0.0608	-0.0012	0.0924	11.374	026.77	018
-08.51	-0.5951	-02.227	-0.5024	0.6642	0.5826	0.6717	0.0627	0.0680	-0.0007	0.0911	11.370	026.73	019
-08.32	-0.5720	-02.203	-0.4822	0.6558	0.5791	0.6711	0.0687	0.0765	-0.0002	0.0920	11.701	026.77	020
-08.13	-0.5574	-02.148	-0.4690	0.6578	0.5849	0.6743	0.0653	0.0525	-0.0023	0.0894	11.707	026.77	021
-07.95	-0.5332	-02.101	-0.4471	0.6534	0.5853	0.6729	0.0677	0.0996	-0.0014	0.0821	12.515	026.77	022
-07.77	-0.5068	-02.059	-0.4231	0.6476	0.5845	0.6701	0.0670	0.0519	-0.0013	0.0876	11.973	026.83	023
-07.58	-0.4941	-02.011	-0.4128	0.6426	0.5825	0.6679	0.0593	0.0652	-0.0008	0.0853	12.346	026.86	024
-07.40	-0.4681	-01.971	-0.3885	0.6432	0.5878	0.6721	0.0554	0.0709	-0.0024	0.0853	12.790	026.83	025
-07.22	-0.4593	-01.907	-0.3819	0.6403	0.5873	0.6728	0.0583	0.0710	-0.0013	0.0855	12.610	026.80	026
-07.01	-0.4480	-01.837	-0.3710	0.6372	0.5871	0.6692	0.0537	0.0996	-0.0014	0.0854	12.515	026.77	027
-06.85	-0.4285	-01.806	-0.3556	0.6325	0.5856	0.6709	0.0473	0.0610	-0.0006	0.0854	12.008	026.70	028
-06.64	-0.4122	-01.747	-0.3419	0.6280	0.5842	0.6643	0.0471	0.0457	-0.0015	0.0801	12.871	026.73	029
-06.46	-0.3940	-01.729	-0.3256	0.6256	0.5850	0.6652	0.0507	0.0314	-0.0022	0.0802	13.335	026.70	030
-06.26	-0.3944	-01.694	-0.3279	0.6281	0.5886	0.6701	0.0512	0.0237	-0.0026	0.0815	13.048	026.54	031
-06.10	-0.3732	-01.647	-0.3085	0.6249	0.5886	0.6676	0.0508	0.0155	-0.0005	0.0790	13.405	026.61	032
-05.90	-0.3543	-01.607	-0.2922	0.6191	0.5857	0.6636	0.0398	0.0358	-0.0015	0.0779	13.782	026.61	033
-05.71	-0.3408	-01.562	-0.2808	0.6168	0.5858	0.6618	0.0434	0.0059	-0.0014	0.0760	13.922	026.70	034
-05.51	-0.3216	-01.538	-0.2636	0.6164	0.5882	0.6640	0.0497	0.0363	-0.0018	0.0758	14.529	026.73	035
-05.32	-0.3105	-01.485	-0.2545	0.6163	0.5901	0.6645	0.0464	0.0201	-0.0003	0.0743	14.532	026.73	036
-05.15	-0.2925	-01.467	-0.2379	0.6201	0.5962	0.6678	0.0426	0.0488	-0.0014	0.0715	15.238	026.70	037
-04.90	-0.2742	-01.433	-0.2224	0.6166	0.5953	0.6636	0.0459	0.0274	-0.0007	0.0682	15.881	026.64	038
-04.70	-0.2709	-01.345	-0.2215	0.6113	0.5911	0.6607	0.0354	0.0245	-0.0004	0.0696	15.087	026.67	039
-04.53	-0.2568	-01.311	-0.2092	0.6104	0.5919	0.6587	0.0349	0.0668	-0.0008	0.0668	15.510	026.64	040
-04.31	-0.2405	-01.288	-0.1957	0.6037	0.5873	0.6576	0.0384	0.0318	-0.0015	0.0703	16.011	026.73	041
-04.11	-0.2220	-01.229	-0.1789	0.6070	0.5926	0.6604	0.0345	0.0599	-0.0017	0.0678	16.820	026.73	042
-03.95	-0.2223	-01.161	-0.1810	0.6062	0.5923	0.6610	0.0455	0.0166	-0.0020	0.0687	15.863	026.77	043
-03.76	-0.2114	-01.125	-0.1719	0.6072	0.5947	0.6605	0.0345	0.0364	-0.0022	0.0658	16.163	026.77	044
-03.57	-0.1954	-01.101	-0.1582	0.6020	0.5910	0.6576	0.0415	0.0154	-0.0013	0.0666	17.122	026.83	045
-03.38	-0.1930	-01.056	-0.1576	0.6049	0.5946	0.6610	0.0452	0.0081	-0.0002	0.0684	16.616	026.77	046
-03.20	-0.1744	-01.054	-0.1408	0.6058	0.5970	0.6607	0.0416	0.0150	-0.0002	0.0636	18.359	026.73	047
-02.98	-0.1675	-01.002	-0.1363	0.6038	0.5958	0.6565	0.0306	0.0425	-0.0019	0.0607	18.164	026.73	048
-02.79	-0.1449	-00.965	-0.1158	0.6027	0.5944	0.6537	0.0204	0.0107	-0.0017	0.0593	20.232	026.70	049
-02.60	-0.1491	-00.896	-0.1121	0.5962	0.5900	0.6516	0.0271	0.0113	-0.0003	0.0616	18.253	026.77	050
-02.44	-0.1467	-00.845	-0.1213	0.5987	0.5930	0.6518	0.0343	0.0048	-0.0011	0.0588	17.502	026.73	051
-02.23	-0.1318	-00.802	-0.1088	0.5960	0.5913	0.6508	0.0206	0.0163	-0.0008	0.0595	18.491	026.83	052
-02.06	-0.1253	-00.732	-0.1040	0.5939	0.5898	0.6488	0.0276	0.0022	-0.0014	0.0590	17.748	026.86	053
-01.87	-0.1113	-00.678	-0.0919	0.5963	0.5930	0.6515	0.0315	-0.0127	-0.0020	0.0585	18.501	026.86	054
-01.68	-0.1087	-00.594	-0.0912	0.5996	0.5967	0.6529	0.0395	-0.0788	-0.0001	0.0563	16.594	026.80	055

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 013 MACH NO 1.017 RN/L 07236308 Q 1444 PSF TD 600

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
-31.50	-0.0912	-0.574	-0.0757	0.5960	0.5939	0.6529	0.0285	-0.0291	-0.0002	0.3590	19.130	026.73	056
-31.31	-0.1016	-0.456	-0.0881	0.5966	0.5944	0.6509	0.0107	0.0334	-0.0014	0.3565	13.624	026.73	057
-31.09	-0.0790	-0.415	-0.0678	0.5920	0.5906	0.6484	0.0183	-0.0176	-0.0014	0.3578	15.955	026.77	058
-30.91	-0.0695	-0.362	-0.0602	0.5925	0.5915	0.6495	0.0179	0.0265	-0.0030	0.3580	15.807	026.73	059
-30.72	-0.0674	-0.293	-0.0599	0.5941	0.5933	0.6514	0.0142	0.0549	-0.0013	0.3581	13.195	026.70	060
-30.53	-0.0557	-0.255	-0.0502	0.5920	0.5915	0.6504	0.0259	-0.0329	-0.0007	0.3589	13.883	026.77	061
-30.35	-0.0577	-0.169	-0.0541	0.5947	0.5944	0.6519	0.0188	-0.0055	-0.0004	0.3575	08.912	026.73	062
-30.16	-0.0476	-0.099	-0.0459	0.5940	0.5939	0.6522	0.0195	-0.0433	-0.0004	0.3583	06.297	026.64	063
-30.03	-0.0331	-0.060	-0.0334	0.5923	0.5923	0.6510	-0.0051	-0.0182	-0.0010	0.3587	05.481	026.64	064
-30.22	-0.0262	0.027	-0.0284	0.5943	0.5944	0.6520	0.0274	-0.1099	-0.0002	0.3576	-03.122	026.67	065
-30.60	-0.0246	0.113	-0.0288	0.5929	0.5931	0.6515	0.0150	0.0131	-0.0003	0.3584	-13.964	026.73	066
-30.79	-0.0315	0.118	-0.0377	0.5945	0.5946	0.6514	0.0113	-0.0026	0.0003	0.3588	-31.567	026.77	067
-30.98	-0.0141	0.234	-0.0223	0.5965	0.5967	0.6511	0.0215	-0.0314	0.0003	0.3544	-50.176	026.73	068
-31.17	0.0234	0.310	0.1112	0.5946	0.5945	0.6524	0.0206	-0.0096	0.0007	0.3578	94.640	026.77	069
-31.36	0.0183	0.395	0.0041	0.5990	0.5989	0.6554	0.0137	-0.0561	0.0012	0.3565	40.196	026.73	070
-31.55	0.0370	0.433	0.0209	0.5974	0.5987	0.6568	0.0095	-0.0280	0.0002	0.3581	65.347	026.70	071
-31.74	0.0460	0.485	0.0259	0.5973	0.5967	0.6538	0.0086	-0.0281	0.0002	0.3571	35.529	026.67	072
-31.93	0.0547	0.536	0.0346	0.5973	0.5958	0.6541	0.0113	-0.0435	-0.0004	0.3600	33.461	026.70	073
-32.12	0.0537	0.622	0.0315	0.5986	0.5970	0.6554	0.0106	-0.0298	0.0006	0.3584	35.203	026.73	074
-32.34	0.0646	0.674	0.0402	0.5991	0.5969	0.6547	0.0067	-0.0456	0.0005	0.3577	31.707	026.73	075
-32.52	0.0754	0.711	0.0489	0.6027	0.5999	0.6583	0.0131	-0.0305	0.0009	0.3584	28.660	026.73	076
-32.68	0.0868	0.747	0.0588	0.6006	0.5972	0.6571	0.0059	-0.0613	0.0005	0.3599	26.152	026.73	077
-32.87	0.0857	0.832	0.0557	0.6007	0.5972	0.6571	0.0088	-0.0545	0.0002	0.3599	29.495	026.83	078
-33.08	0.0955	0.880	0.0635	0.5974	0.5931	0.6541	0.0079	-0.0252	-0.0004	0.3610	27.989	026.73	079
-33.27	0.1065	0.934	0.0722	0.6039	0.5988	0.6604	0.0076	-0.0338	0.0009	0.3616	26.640	026.83	080
-33.45	0.1179	0.987	0.0816	0.6055	0.5995	0.6606	0.0006	-0.0797	0.0003	0.3611	25.432	026.80	081
-33.62	0.1327	1.026	0.0946	0.6077	0.6005	0.6617	0.0068	-0.0641	0.0010	0.3612	23.501	026.77	082
-33.83	0.1552	1.068	0.1147	0.6089	0.5999	0.6627	0.0023	-0.0432	0.0012	0.3628	20.993	026.73	083
-34.01	0.1630	1.127	0.1206	0.6109	0.6010	0.6656	0.0087	-0.0428	0.0017	0.3647	20.994	026.64	084
-34.20	0.1676	1.167	0.1233	0.6103	0.5997	0.6671	-0.0020	-0.0672	0.0016	0.3674	21.150	026.54	085
-34.38	0.1812	1.196	0.1351	0.6083	0.5962	0.6636	-0.0062	-0.0531	0.0014	0.3674	20.058	026.64	086
-34.58	0.1914	1.264	0.1432	0.6090	0.5956	0.6628	-0.0069	-0.0463	0.0010	0.3673	20.069	026.67	087
-34.77	0.2054	1.297	0.1551	0.6120	0.5970	0.6665	-0.0072	-0.0400	0.0003	0.3695	19.183	026.73	088
-34.93	0.2171	1.336	0.1646	0.6169	0.6005	0.6702	-0.0109	-0.0560	0.0002	0.3697	18.698	026.70	089
-35.16	0.2352	1.371	0.1801	0.6206	0.6019	0.6714	-0.0080	-0.0558	0.0013	0.3695	17.715	026.73	090
-35.35	0.2493	1.407	0.1920	0.6228	0.6032	0.6751	-0.0117	-0.0333	0.0014	0.3719	17.144	026.77	091
-35.51	0.2565	1.461	0.1974	0.6243	0.6025	0.6734	-0.0024	-0.0264	0.0019	0.3710	17.302	026.73	092
-35.74	0.2835	1.503	0.2218	0.6284	0.6031	0.6757	-0.0064	-0.0495	0.0012	0.3726	16.107	026.70	093
-35.93	0.2899	1.534	0.2263	0.6274	0.6007	0.6755	-0.0067	-0.0574	0.0005	0.3749	16.074	026.77	094
-36.12	0.3054	1.557	0.2399	0.6273	0.5982	0.6747	-0.0108	-0.0579	0.0005	0.3765	15.485	026.73	095
-36.29	0.3189	1.588	0.2511	0.6332	0.6019	0.6795	-0.0075	-0.0584	0.0015	0.3776	15.123	026.80	096
-36.51	0.3362	1.637	0.2661	0.6342	0.6004	0.6813	-0.0149	-0.0600	0.0003	0.3813	14.790	026.86	097
-36.70	0.3468	1.672	0.2744	0.6367	0.6004	0.6851	-0.0153	-0.0463	0.0011	0.3847	14.649	026.90	098
-36.90	0.3695	1.731	0.2941	0.6457	0.6057	0.6892	-0.0196	-0.0407	0.0022	0.3834	14.230	026.86	099
-37.11	0.3861	1.775	0.3080	0.6494	0.6063	0.6882	-0.0170	-0.0478	0.0030	0.3819	13.976	026.80	100
-37.28	0.4091	1.800	0.3291	0.6519	0.6049	0.6874	-0.0143	-0.0472	0.0023	0.3825	13.366	026.77	101
-37.50	0.4260	1.847	0.3435	0.6543	0.6039	0.6888	-0.0082	-0.0390	0.0004	0.3848	13.174	026.67	102
-37.50	0.4322	1.913	0.3478	0.6553	0.6011	0.6858	-0.0156	-0.0553	0.0021	0.3847	13.446	026.70	103
-37.86	0.4560	1.975	0.3636	0.6574	0.6007	0.6876	-0.0194	-0.0568	0.0029	0.3869	13.158	026.64	104
-38.06	0.4703	2.028	0.3814	0.6607	0.6007	0.6880	-0.0162	-0.0493	0.0027	0.3873	13.103	026.64	105

HSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 310 MAC4 NO 1.017 H/L 07236308 U 1444 PSF TO 600

10/17/62

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AR	CP	PO	PNT
08.28	0.4874	02.076	0.3959	0.6637	0.5998	0.6878	-0.0232	-0.0659	0.0032	0.0880	12.942	026.70	107
08.47	0.5162	02.078	0.4220	0.6708	0.6012	0.6880	-0.0271	-0.0443	0.0025	0.0868	12.226	026.73	108
08.67	0.5355	02.155	0.4385	0.6770	0.6031	0.6912	-0.0242	-0.0152	0.0028	0.0880	12.227	026.70	109
08.87	0.5355	02.600	0.4367	0.6747	0.5994	0.6880	-0.0453	-0.0344	0.0035	0.0886	12.822	026.67	110
09.06	0.5719	02.281	0.4702	0.6834	0.6008	0.6907	-0.0528	-0.0009	0.0025	0.0899	12.116	026.70	111
09.26	0.6097	02.323	0.5056	0.6896	0.5995	0.6909	-0.0181	-0.0379	0.0039	0.0914	11.573	026.70	112
09.46	0.6238	02.411	0.5167	0.6946	0.6002	0.6931	-0.0219	-0.0249	0.0038	0.0929	11.741	026.70	113
09.63	0.6455	02.430	0.5358	0.7012	0.6017	0.6955	-0.0326	-0.0050	0.0035	0.0938	11.436	026.73	114
09.79	0.6679	02.466	0.5558	0.7066	0.6018	0.6959	-0.0325	-0.0420	0.0022	0.0941	11.220	026.73	115
09.94	0.6879	02.526	0.5735	0.7133	0.6036	0.6965	-0.0607	-0.0404	0.0046	0.0929	11.157	026.70	116
10.10	0.7033	02.582	0.5870	0.7148	0.6008	0.6977	-0.0502	-0.0757	0.0022	0.0969	11.153	026.70	117
10.24	0.7351	02.583	0.6164	0.7226	0.6014	0.6970	-0.0474	-0.0311	0.0033	0.0956	10.675	026.73	118
10.33	0.7414	02.636	0.6220	0.7219	0.5987	0.6958	-0.0587	0.0400	0.0045	0.0971	10.801	026.73	119
10.47	0.7579	02.657	0.6375	0.7212	0.5934	0.6930	-0.0443	-0.0604	0.0055	0.0996	10.651	026.73	120
10.55	0.7819	02.688	0.6583	0.7352	0.6022	0.7021	-0.0271	-0.0361	0.0042	0.0998	10.366	026.70	121
10.66	0.7823	02.722	0.6581	0.7325	0.5981	0.6970	-0.0486	-0.0175	0.0035	0.0990	10.572	026.67	122
10.72	0.8041	02.735	0.6788	0.7374	0.5983	0.6980	-0.0524	-0.0255	0.0038	0.0998	10.334	026.61	123
10.75	0.7933	02.756	0.6667	0.7417	0.6044	0.7037	-0.0513	-0.0637	0.0030	0.0994	10.555	026.67	124
10.92	0.8094	02.789	0.6809	0.7431	0.6007	0.7013	-0.0380	-0.0100	0.0036	0.1006	10.469	026.70	125
11.01	0.8258	02.822	0.6960	0.7469	0.6003	0.7022	-0.0382	-0.0185	0.0036	0.1019	10.381	026.73	126
11.15	0.8388	02.866	0.7068	0.7516	0.6007	0.7069	-0.0277	-0.0118	0.0046	0.1061	10.378	026.70	127
11.30	0.8598	02.896	0.7252	0.7587	0.6020	0.7068	-0.0302	-0.0782	0.0029	0.1048	10.232	026.73	128
11.41	0.8788	02.903	0.7430	0.7609	0.5989	0.7034	-0.0486	-0.0142	0.0029	0.1045	10.034	026.73	129
11.44	0.8887	02.934	0.7517	0.7657	0.6014	0.7037	-0.0516	-0.0380	0.0049	0.1023	10.031	026.73	130
11.50	0.8897	03.010	0.7519	0.7670	0.6016	0.7052	-0.0447	-0.0236	0.0034	0.1036	10.278	026.70	131
11.54	0.8969	03.029	0.7587	0.7676	0.6004	0.7054	-0.0343	-0.0221	0.0031	0.1051	10.259	026.70	132
11.54	0.9202	03.017	0.7813	0.7733	0.6014	0.7079	-0.0343	-0.0368	0.0051	0.1065	09.959	026.70	133
11.54	0.9224	03.014	0.7830	0.7757	0.6034	0.7093	-0.0240	-0.0131	0.0043	0.1059	09.926	026.73	134
11.52	0.9284	03.014	0.7873	0.7763	0.6035	0.7094	-0.0239	-0.0278	0.0043	0.1059	09.885	026.73	135
11.52	0.9338	03.016	0.7940	0.7800	0.6057	0.7116	-0.0275	-0.0066	0.0005	0.1059	09.813	026.73	136
00.20	0.0607	00.047	0.0587	0.6005	0.6002	0.6567	0.0143	-0.0093	0.0007	0.0565	02.331	026.67	137
00.19	0.0413	00.025	0.0393	0.6007	0.6006	0.6561	0.0175	-0.0367	-0.0007	0.0556	01.861	026.64	138

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 011 MACH 0.003 RN/L 07497218 Q 1292 PSF TO 602

10/17/62

COEFFICIENTS

ALPHA	M	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.34	0.0251	00.024	0.0234	0.2927	0.2925	0.3008	0.0147	0.0027	0.0090	0.0083	02.894	030.28	005
00.34	0.0247	00.043	0.0230	0.2900	0.2898	0.2984	-0.0007	0.0017	-0.0014	0.0086	05.277	030.31	006
-11.05	-0.7806	-03.098	-0.7142	0.4159	0.2713	0.3063	0.0783	0.1752	-0.0007	0.0350	12.050	030.34	008
-10.86	-0.7751	-03.009	-0.7102	0.4122	0.2709	0.3053	0.0891	0.1758	-0.0019	0.0344	11.793	030.41	009
-10.86	-0.7353	-03.088	-0.6748	0.4057	0.2737	0.3070	0.0777	0.1502	-0.0013	0.0333	12.707	030.34	010
-10.49	-0.7410	-03.001	-0.6788	0.4034	0.2731	0.3051	0.0774	0.1238	0.0001	0.0321	12.304	030.38	011
-10.31	-0.7077	-03.039	-0.6476	0.3939	0.2716	0.3047	0.0802	0.1413	-0.0006	0.0331	13.045	030.44	012
-10.12	-0.6989	-02.945	-0.6381	0.3914	0.2731	0.3050	0.0716	0.1382	-0.0001	0.0319	12.836	030.54	013
-09.94	-0.6698	-02.926	-0.6121	0.3877	0.2763	0.3057	0.0708	0.1444	0.0004	0.0293	13.270	030.54	014
-09.74	-0.6600	-02.870	-0.6038	0.3831	0.2754	0.3050	0.0708	0.1385	-0.0001	0.0296	13.209	030.44	015
-09.54	-0.6402	-02.783	-0.6059	0.3777	0.2719	0.3024	0.0779	0.1541	-0.0005	0.0307	12.804	030.38	016
-09.35	-0.6117	-02.741	-0.5886	0.3723	0.2765	0.3050	0.0621	0.1112	-0.0012	0.0285	12.814	030.31	017
-09.17	-0.6181	-02.599	-0.5644	0.3699	0.2793	0.3069	0.0771	0.0707	0.0003	0.0256	12.816	030.34	018
-08.98	-0.5770	-02.578	-0.5271	0.3624	0.2760	0.3033	0.0751	0.1541	-0.0016	0.0273	13.571	030.31	019
-08.79	-0.5524	-02.587	-0.5034	0.3595	0.2764	0.3046	0.0752	0.1039	-0.0007	0.0262	14.062	030.28	020
-08.60	-0.5452	-02.517	-0.4974	0.3566	0.2782	0.3020	0.0744	0.1287	-0.0001	0.0239	14.028	030.25	021
-08.39	-0.5283	-02.513	-0.4821	0.3518	0.2777	0.3032	0.0778	0.1295	0.0001	0.0255	14.453	030.25	022
-08.21	-0.5202	-02.489	-0.4749	0.3514	0.2800	0.3045	0.0620	0.1522	-0.0014	0.0245	14.535	030.15	023
-08.03	-0.4905	-02.484	-0.4488	0.3443	0.2785	0.3018	0.0773	0.0940	-0.0000	0.0232	15.398	030.21	024
-07.85	-0.4783	-02.441	-0.4356	0.3427	0.2800	0.3027	0.0762	0.1288	0.0001	0.0227	15.507	030.25	025
-07.66	-0.4638	-02.428	-0.4222	0.3400	0.2804	0.3027	0.0754	0.1366	0.0004	0.0221	15.905	030.31	026
-07.49	-0.4476	-02.344	-0.4075	0.3339	0.2779	0.3011	0.0788	0.1201	-0.0002	0.0232	16.044	030.34	027
-07.31	-0.4349	-02.285	-0.3974	0.3354	0.2821	0.3020	0.0699	0.1509	-0.0016	0.0199	15.890	030.34	028
-07.10	-0.4175	-02.228	-0.3795	0.3301	0.2807	0.3000	0.0656	0.1067	-0.0000	0.0184	16.351	030.28	034
-06.92	-0.4216	-02.086	-0.3846	0.3302	0.2815	0.2987	0.0775	0.0837	0.0008	0.0172	15.031	030.41	029
-06.76	-0.3899	-02.087	-0.3542	0.3246	0.2806	0.2991	0.0770	0.1172	-0.0011	0.0184	16.105	030.38	031
-06.58	-0.3875	-01.995	-0.3524	0.3272	0.2846	0.3015	0.0497	0.0902	0.0009	0.0168	15.642	030.34	032
-06.35	-0.3471	-01.993	-0.3338	0.3199	0.2810	0.3000	0.0808	0.1095	-0.0003	0.0190	16.497	030.31	033
-06.22	-0.3595	-01.935	-0.3269	0.3181	0.2808	0.2991	0.0691	0.1067	-0.0000	0.0184	16.351	030.28	034
-06.01	-0.3499	-01.927	-0.3186	0.3156	0.2805	0.2988	0.0692	0.0817	-0.0016	0.0183	16.735	030.31	035
-05.82	-0.3315	-01.918	-0.3013	0.3139	0.2817	0.2990	0.0885	0.0438	-0.0009	0.0173	17.573	030.38	036
-05.63	-0.3314	-01.855	-0.3020	0.3139	0.2828	0.3000	0.0729	0.0402	0.0001	0.0172	17.012	030.41	037
-05.44	-0.3152	-01.852	-0.2867	0.3138	0.2851	0.2991	0.0755	0.1072	-0.0005	0.0139	17.845	030.41	038
-05.24	-0.3178	-01.745	-0.2905	0.3128	0.2850	0.2997	0.0610	0.0706	-0.0003	0.0146	16.874	030.38	039
-05.04	-0.2896	-01.745	-0.2636	0.3079	0.2836	0.2993	0.0527	0.1025	-0.0019	0.0157	18.301	030.31	040
-04.85	-0.2979	-01.624	-0.2730	0.3068	0.2826	0.2966	0.0490	0.0669	-0.0007	0.0140	16.555	030.38	041
-04.65	-0.2773	-01.581	-0.2534	0.3052	0.2837	0.2960	0.0489	0.0583	0.0002	0.0123	17.320	030.38	042
-04.46	-0.2644	-01.513	-0.2416	0.3032	0.2835	0.2957	0.0481	0.0822	-0.0011	0.0123	17.386	030.44	043
-04.26	-0.2619	-01.442	-0.2402	0.3017	0.2830	0.2965	0.0527	0.0329	-0.0009	0.0134	16.728	030.41	044
-04.07	-0.2545	-01.404	-0.2337	0.3026	0.2853	0.2960	0.0565	0.0334	-0.0016	0.0107	16.762	030.38	045
-03.88	-0.2393	-01.366	-0.2197	0.2984	0.2852	0.2952	0.0476	0.0982	-0.0000	0.0124	17.341	030.34	046
-03.69	-0.2371	-01.294	-0.2184	0.2982	0.2836	0.2965	0.0363	0.0873	-0.0002	0.0129	16.581	030.28	047
-03.50	-0.2190	-01.265	-0.2011	0.2999	0.2871	0.2940	0.0323	0.0693	0.0005	0.0089	17.544	030.31	048
-03.31	-0.2118	-01.187	-0.1951	0.2959	0.2842	0.2947	0.0556	0.0482	-0.0005	0.0106	16.757	030.31	049
-03.12	-0.2048	-01.130	-0.1890	0.2950	0.2843	0.2943	0.0473	0.0796	-0.0009	0.0101	17.031	030.31	050
-02.92	-0.1884	-01.050	-0.1736	0.2937	0.2844	0.2945	0.0478	0.0289	0.0002	0.0101	16.926	030.31	051
-02.73	-0.1815	-00.972	-0.1679	0.2902	0.2819	0.2919	0.0471	0.0614	0.0001	0.0101	16.244	030.31	052
-02.54	-0.1734	-00.911	-0.1608	0.2897	0.2823	0.2918	0.0433	0.0433	0.0009	0.0095	15.960	030.34	053
-02.33	-0.1641	-00.831	-0.1545	0.2889	0.2824	0.2916	0.0351	0.0742	-0.0003	0.0095	15.209	030.38	054
-02.16	-0.1533	-00.787	-0.1425	0.2890	0.2846	0.2936	0.0270	0.0601	0.0005	0.0090	15.606	030.44	055
-02.00	-0.1458	-00.751	-0.1358	0.2880	0.2831	0.2916	0.0352	0.0484	0.0000	0.0085	15.655	030.41	056

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 011 MACH MD 0.803 RN/L 07497218 Q 1292 PSF TD 602

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
-01.82	-0.1374	00.710	-0.1283	0.2895	0.2853	0.2933	0.0239	0.0290	0.0002	0.0080	15.705	030.44	057
-01.61	-0.1299	00.672	-0.1218	0.2903	0.2868	0.2926	0.0391	0.0315	0.0013	0.0059	15.717	030.44	058
-01.42	-0.1310	00.596	-0.1238	0.2899	0.2868	0.2926	0.0199	0.0351	0.0005	0.0059	13.824	030.44	059
-01.24	-0.1238	00.540	-0.1176	0.2895	0.2869	0.2905	0.0355	0.0211	0.0006	0.0036	13.241	030.38	060
-01.05	-0.1225	00.447	-0.1172	0.2861	0.2839	0.2931	0.0388	0.0711	-0.0010	0.0092	11.085	030.34	061
-00.86	-0.1104	00.388	-0.1062	0.2855	0.2838	0.2924	0.0276	0.0433	-0.0003	0.0086	10.469	030.28	062
-00.67	-0.0985	00.307	-0.0952	0.2819	0.2808	0.2899	0.0191	0.0738	0.0003	0.0091	08.465	030.34	063
-00.46	-0.0906	00.248	-0.0884	0.2790	0.2783	0.2878	0.0273	0.0414	-0.0012	0.0095	08.315	030.34	064
-00.30	-0.0830	00.170	-0.0815	0.2815	0.2810	0.2901	0.0161	0.0133	-0.0005	0.0091	06.238	030.34	065
-00.11	-0.0839	00.095	-0.0833	0.2821	0.2819	0.2904	0.0350	0.0162	-0.0002	0.0085	03.426	030.44	066
00.07	-0.0769	00.037	-0.0772	0.2813	0.2814	0.2911	0.0352	0.0157	-0.0001	0.0097	01.448	030.38	067
00.23	-0.0597	00.016	-0.0609	0.2882	0.2885	0.2954	0.0277	-0.0112	0.0008	0.0069	00.699	030.38	068
00.44	-0.0383	00.010	-0.0405	0.2827	0.2830	0.2927	0.0125	-0.0474	-0.0002	0.0097	00.766	030.38	069
00.63	-0.0479	00.102	-0.0510	0.2836	0.2841	0.2927	0.0127	-0.0570	0.0015	0.0086	06.483	030.34	070
00.82	-0.0450	00.160	-0.0490	0.2839	0.2846	0.2936	0.0039	0.0073	-0.0009	0.0091	10.802	030.34	071
01.01	-0.0418	00.273	-0.0469	0.2869	0.2876	0.2927	0.0149	-0.0086	0.0010	0.0051	19.850	030.34	072
01.23	-0.0258	00.333	-0.0320	0.2858	0.2864	0.2938	0.0178	0.0162	0.0019	0.0074	39.183	030.38	073
01.42	-0.0185	00.429	-0.0256	0.2855	0.2860	0.2940	0.0092	0.0301	0.0016	0.0080	70.414	030.41	074
01.59	-0.0154	00.506	-0.0233	0.2860	0.2865	0.2934	0.0124	0.0467	0.0010	0.0069	99.723	030.38	075
01.78	0.0019	00.527	-0.0071	0.2887	0.2888	0.2951	0.0127	-0.0036	0.0019	0.0064	44.418	030.41	076
01.96	0.0101	00.549	-0.0002	0.2897	0.2896	0.2965	0.0047	0.0031	0.0009	0.0069	64.420	030.38	077
02.15	0.0184	00.608	0.0076	0.2886	0.2877	0.2951	0.0164	-0.0453	0.0017	0.0074	00.332	030.34	078
02.34	0.0219	00.681	0.0101	0.2886	0.2879	0.2958	0.0083	-0.0554	0.0009	0.0079	94.680	030.38	079
02.55	0.0339	00.741	0.0110	0.2889	0.2877	0.2967	-0.0080	-0.0344	0.0015	0.0090	64.524	030.38	080
02.74	0.0369	00.832	0.0229	0.2927	0.2912	0.2970	-0.0162	-0.0366	0.0011	0.0057	68.504	030.47	081
02.90	0.0489	00.909	0.0341	0.2929	0.2908	0.2955	0.0028	-0.0752	0.0020	0.0047	56.462	030.47	082
03.12	0.0600	00.988	0.0439	0.2983	0.2955	0.2991	0.0016	-0.1016	0.0011	0.0036	50.024	030.44	083
03.28	0.0675	01.052	0.0505	0.2979	0.2945	0.3004	0.0003	0.0468	-0.0002	0.0059	47.340	030.41	084
03.49	0.0890	01.075	0.0707	0.3025	0.2976	0.3028	0.0042	0.0055	0.0014	0.0052	36.722	030.38	085
03.65	0.0879	01.165	0.0690	0.2988	0.2938	0.3012	0.0003	-0.0294	0.0023	0.0074	40.245	030.41	086
03.84	0.1008	01.225	0.0807	0.3024	0.2963	0.3032	0.0035	-0.0883	0.0027	0.0069	36.918	030.41	087
04.05	0.1132	01.249	0.0922	0.3021	0.2948	0.3033	-0.0041	-0.0642	0.0032	0.0085	33.516	030.38	088
04.23	0.1205	01.301	0.0983	0.3041	0.2960	0.3006	-0.0279	-0.0439	0.0023	0.0046	32.817	030.41	089
04.44	0.1461	01.317	0.1227	0.3073	0.2969	0.3055	-0.0254	0.0254	0.0015	0.0086	27.382	030.34	090
04.61	0.1624	01.396	0.1182	0.3062	0.2957	0.3055	-0.0053	-0.0746	0.0029	0.0097	28.787	030.31	091
04.80	0.1502	01.454	0.1248	0.3093	0.2978	0.3077	0.0016	-0.0830	0.0038	0.0079	29.402	030.28	092
04.99	0.1662	01.454	0.1399	0.3089	0.2956	0.3051	-0.0145	-0.0187	0.0030	0.0096	26.572	030.31	093
05.16	0.1687	01.523	0.1412	0.3126	0.2987	0.3059	-0.0110	-0.0188	0.0023	0.0072	27.422	030.34	094
05.38	0.1803	01.600	0.1517	0.3125	0.2969	0.3064	-0.0118	-0.0033	0.0024	0.0095	26.965	030.38	095
05.57	0.2012	01.663	0.1714	0.3151	0.2970	0.3077	-0.0163	-0.0132	0.0038	0.0107	25.108	030.38	096
05.77	0.2047	01.733	0.1738	0.3157	0.2966	0.3079	-0.0160	-0.0795	0.0029	0.0113	25.725	030.44	097
05.96	0.2297	01.781	0.1925	0.3199	0.2977	0.3090	-0.0368	-0.0097	0.0032	0.0113	23.567	030.41	098
06.13	0.2464	01.804	0.2129	0.3255	0.3009	0.3122	-0.0177	-0.0313	0.0029	0.0113	22.234	030.41	099
06.32	0.2416	01.880	0.2070	0.3265	0.3017	0.3142	-0.0336	-0.0266	0.0026	0.0125	23.636	030.41	100
06.54	0.2542	01.925	0.2184	0.3272	0.3002	0.3144	-0.0187	-0.0080	0.0026	0.0142	23.011	030.38	101
06.73	0.2718	02.015	0.2350	0.3275	0.2977	0.3124	-0.0312	-0.0193	0.0025	0.0147	22.504	030.31	102
06.93	0.2914	02.045	0.2532	0.3327	0.2997	0.3137	-0.0315	-0.0362	0.0026	0.0140	21.319	030.34	103
07.12	0.2988	02.079	0.2596	0.3325	0.2978	0.3134	-0.0277	-0.0524	0.0029	0.0156	21.135	030.38	104
07.31	0.3153	02.142	0.2745	0.3383	0.3006	0.3151	-0.0364	-0.0218	0.0034	0.0145	20.640	030.34	105
07.53	0.3443	02.164	0.3022	0.3413	0.2988	0.3144	-0.0332	-0.0215	0.0037	0.0156	19.096	030.38	106
07.70	0.3521	02.222	0.3090	0.3424	0.2988	0.3152	-0.0298	-0.0214	0.0030	0.0173	19.177	030.38	107

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 011 MACH NO 0.803 RN/L 07497218 Q 1292 PSF TU 602

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
07-89	0.3683	02.260	0.3238	0.3466	0.2989	0.3173	-0.0301	-0.0466	0.0036	0.0184	18.640	030.41	108
08-08	0.3902	02.305	0.3437	0.3548	0.3029	0.3202	-0.0301	-0.0966	0.0036	0.0173	17.945	030.38	109
08-27	0.3972	02.338	0.3501	0.3530	0.2990	0.3162	-0.0495	-0.0839	0.0045	0.0172	17.882	030.41	110
08-46	0.4080	02.403	0.3574	0.3570	0.3005	0.3177	-0.0576	-0.0696	0.0041	0.0173	17.978	030.38	111
08-65	0.4355	02.409	0.3852	0.3631	0.3010	0.3199	-0.0542	-0.0528	0.0053	0.0189	16.806	030.38	112
08-87	0.4533	02.478	0.4019	0.3648	0.2966	0.3202	-0.0508	-0.0447	0.0052	0.0218	16.609	030.34	113
09-01	0.4637	02.528	0.4110	0.3665	0.2984	0.3203	-0.0547	-0.0707	0.0046	0.0207	16.565	030.28	114
09-23	0.4678	02.607	0.4336	0.3726	0.2982	0.3211	-0.0511	-0.0626	0.0044	0.0229	16.236	030.28	115
09-42	0.4988	02.622	0.4437	0.3729	0.2952	0.3197	-0.0631	-0.0318	0.0047	0.0244	15.968	030.31	116
09-56	0.5180	02.672	0.4613	0.3798	0.2979	0.3211	-0.0587	-0.0812	0.0061	0.0232	15.672	030.34	117
09-78	0.5407	02.685	0.4824	0.3846	0.2970	0.3196	-0.0706	-0.0501	0.0043	0.0226	15.087	030.41	118
09-92	0.5612	02.744	0.5010	0.3926	0.3004	0.3226	-0.0630	-0.0910	0.0054	0.0223	14.853	030.34	119
10-06	0.5758	02.778	0.5149	0.3940	0.2980	0.3219	-0.0673	-0.0507	0.0047	0.0238	14.657	030.38	120
10-20	0.5929	02.804	0.5305	0.3997	0.2994	0.3261	-0.0561	-0.0325	0.0045	0.0267	14.366	030.38	121
10-28	0.6058	02.833	0.5434	0.4039	0.3005	0.3272	-0.0488	-0.0150	0.0050	0.0267	14.184	030.34	122
10-39	0.6187	02.887	0.5520	0.4089	0.3026	0.3282	-0.0483	-0.0732	0.0056	0.0256	14.077	030.31	123
10-50	0.6333	02.858	0.5678	0.4117	0.3014	0.3275	-0.0835	-0.0709	0.0049	0.0261	13.708	030.31	124
10-58	0.6317	02.874	0.5657	0.4116	0.3007	0.3273	-0.0644	-0.0264	0.0046	0.0266	13.821	030.31	125
10-64	0.6433	02.910	0.5771	0.4123	0.2987	0.3264	-0.0760	-0.0372	0.0055	0.0277	13.742	030.34	126
10-72	0.6608	02.936	0.5938	0.4157	0.2980	0.3268	-0.0724	-0.0349	0.0057	0.0289	13.497	030.34	127
10-81	0.6880	02.953	0.5997	0.4208	0.3008	0.3285	-0.0492	-0.0321	0.0045	0.0277	13.430	030.34	128
10-95	0.6771	02.996	0.6080	0.4219	0.2988	0.3276	-0.0765	-0.0301	0.0061	0.0289	13.442	030.34	129
11-11	0.6894	03.017	0.6189	0.4257	0.2985	0.3273	-0.0572	-0.0268	0.0053	0.0289	13.297	030.34	130
11-20	0.7099	02.998	0.6386	0.4297	0.2975	0.3291	-0.0651	-0.0281	0.0058	0.0316	12.831	030.38	131
11-31	0.7206	03.012	0.6482	0.4334	0.2979	0.3278	-0.0649	-0.0365	0.0063	0.0299	12.697	030.41	132
11-34	0.7326	03.072	0.6604	0.4378	0.2994	0.3300	-0.0616	-0.0366	0.0067	0.0306	12.722	030.31	133
11-37	0.7455	03.051	0.6717	0.4411	0.3000	0.3301	-0.0577	-0.0356	0.0059	0.0300	12.435	030.34	134
11-40	0.7358	03.065	0.6626	0.4363	0.2967	0.3273	-0.0655	-0.0205	0.0054	0.0305	12.656	030.34	135
11-40	0.7357	03.127	0.6625	0.4363	0.2967	0.3277	-0.0577	-0.0039	0.0059	0.0311	12.912	030.31	136
11-43	0.7506	03.076	0.6765	0.4423	0.2993	0.3305	-0.0540	-0.0352	0.0062	0.0306	12.449	030.31	137
11-43	0.7377	03.095	0.6638	0.4395	0.2999	0.3314	-0.0649	-0.0441	0.0069	0.0321	12.746	030.28	138
00-13	0.0036	00.020	0.0029	0.2862	0.2862	0.2965	0.0031	0.0424	-0.0069	0.0103	18.909	030.28	139
00-16	0.0162	00.023	0.0154	0.2885	0.2885	0.2964	-0.0012	0.0582	-0.0013	0.0079	04.254	030.28	140

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 012 MACH NO 0.606 RN/L 06972404 Q 0900 PSF TD 569

COEFFICIENTS

ALPHA	N	M	PH	L	D	A	AU	Y	YM	KM	AB	CP	PD	PMT
00.02	-0.0120	-00.029	-0.0121	0.2077	0.2077	0.2077	0.2063	0.0111	0.0025	-0.0007	-0.3014	07.359	031.31	006
-11.38	-0.7709	-03.115	-0.7181	0.3390	0.3390	0.1907	0.2166	0.0858	0.0633	-0.0054	0.3259	12.275	031.15	007
-11.04	-0.7300	-03.031	-0.6798	0.2281	0.1919	0.1919	0.2166	0.0682	0.0236	-0.3044	0.3227	12.612	031.21	008
-10.66	-0.6890	-02.905	-0.6413	0.3177	0.1936	0.1936	0.2131	0.0546	0.1270	-0.0041	0.3196	12.810	031.25	009
-10.29	-0.6706	-02.782	-0.6259	0.3063	0.1895	0.1895	0.2132	0.0775	0.0715	-0.0035	0.3237	12.605	031.21	010
-09.92	-0.6279	-02.739	-0.5845	0.3027	0.1975	0.1975	0.2190	0.0605	0.1046	-0.0023	0.3215	13.253	031.15	011
-09.55	-0.6167	-02.617	-0.5734	0.2964	0.1971	0.1971	0.2167	0.0863	0.0866	-0.3027	0.3196	12.933	031.12	012
-09.22	-0.5659	-02.611	-0.5263	0.2901	0.2021	0.2021	0.2162	0.0550	0.0308	-0.0042	0.3161	14.017	031.15	013
-08.82	-0.5470	-02.543	-0.5101	0.2795	0.1979	0.1979	0.2150	0.0492	0.0534	-0.0030	0.3191	14.124	031.18	014
-08.45	-0.4987	-02.534	-0.4619	0.2709	0.2000	0.2000	0.2150	0.0473	0.1238	-0.3028	0.3149	14.887	031.21	015
-08.08	-0.4638	-02.329	-0.4310	0.2635	0.2003	0.2003	0.2130	0.0416	0.0978	-0.0031	0.3127	15.252	031.31	016
-07.72	-0.4221	-02.231	-0.3909	0.2583	0.2034	0.2034	0.2139	0.0291	0.1655	-0.0022	0.3105	16.062	031.37	017
-07.36	-0.4243	-02.101	-0.3951	0.2540	0.2014	0.2014	0.2143	0.0474	0.0863	-0.0019	0.3129	15.043	031.21	018
-06.99	-0.3814	-02.092	-0.3539	0.2478	0.2024	0.2024	0.2153	0.0305	0.0834	-0.3030	0.3125	16.662	031.12	019
-06.64	-0.3533	-01.975	-0.3275	0.2419	0.2026	0.2026	0.2098	0.0460	0.0968	-0.3039	0.3074	16.986	031.18	020
-06.29	-0.3614	-01.902	-0.3372	0.2402	0.2018	0.2018	0.2119	0.0471	0.0859	-0.0032	0.3101	15.980	031.08	021
-05.92	-0.3303	-01.774	-0.3074	0.2377	0.2018	0.2018	0.2108	0.0460	0.1084	-0.0016	0.3060	16.316	031.12	022
-05.57	-0.2937	-01.711	-0.2724	0.2329	0.2054	0.2054	0.2105	0.0411	0.0473	-0.3027	0.3051	17.694	031.08	023
-05.16	-0.2873	-01.619	-0.2680	0.2271	0.2021	0.2021	0.2081	0.0409	0.0467	-0.3026	0.3060	17.116	031.15	024
-04.77	-0.2379	-01.549	-0.2198	0.2264	0.2074	0.2074	0.2103	0.0354	0.0024	-0.3022	0.3029	19.780	031.18	025
-04.40	-0.2370	-01.483	-0.2208	0.2194	0.2016	0.2016	0.2049	0.0188	0.0061	-0.0019	0.3031	19.011	031.28	026
-04.02	-0.2281	-01.413	-0.2130	0.2231	0.2077	0.2077	0.2089	0.0237	0.0424	-0.3037	0.3012	18.773	031.31	027
-03.64	-0.1997	-01.267	-0.1864	0.2164	0.2058	0.2058	0.2058	0.0182	0.0284	-0.3017	0.3017	19.276	031.25	028
-03.26	-0.1922	-01.110	-0.1802	0.2159	0.2053	0.2053	0.2044	0.0396	0.0795	-0.0015	0.3009	17.544	031.15	029
-02.89	-0.1752	-00.969	-0.1648	0.2105	0.2019	0.2019	0.2054	0.0291	0.0283	-0.0008	0.3035	16.805	031.05	030
-02.49	-0.1574	-00.884	-0.1483	0.2138	0.2071	0.2071	0.2049	0.0169	0.0968	-0.0027	0.3022	17.049	031.05	031
-02.12	-0.1395	-00.801	-0.1319	0.2093	0.2043	0.2043	0.2019	0.0329	0.1109	-0.3024	0.3024	17.432	031.02	032
-01.78	-0.1280	-00.693	-0.1217	0.2057	0.2019	0.2019	0.2006	0.0172	0.0388	-0.0034	0.3013	16.454	031.08	033
-01.41	-0.1038	-00.556	-0.0987	0.2101	0.2076	0.2076	0.2042	0.0182	-0.0383	-0.0007	0.3035	16.279	031.12	034
-01.07	-0.0928	-00.448	-0.0889	0.2056	0.2039	0.2039	0.2037	0.0065	-0.0060	-0.0009	0.3001	14.663	031.15	035
-00.68	-0.0802	-00.364	-0.0778	0.2034	0.2025	0.2025	0.2009	0.0231	0.0272	-0.0004	0.3016	13.806	031.25	036
-00.31	-0.0763	-00.204	-0.0752	0.2042	0.2038	0.2038	0.1999	0.0060	0.0153	-0.0004	0.3039	08.142	031.25	037
00.05	-0.0725	-00.042	-0.0727	0.2031	0.2032	0.2032	0.2007	0.0232	-0.0306	-0.0006	0.3025	01.779	031.21	038
00.43	-0.0448	00.101	-0.0463	0.2036	0.2040	0.2040	0.2024	0.0229	-0.0206	-0.0010	0.3016	-06.875	031.18	039
00.80	-0.0154	00.218	-0.0184	0.2085	0.2087	0.2087	0.2064	0.0219	-0.0460	0.0006	0.3023	-42.937	031.21	040
01.20	0.0009	00.279	-0.0034	0.2097	0.2097	0.2097	0.2049	0.0201	0.0368	0.0002	0.3049	10.721	031.15	041
01.54	-0.0068	00.441	-0.0125	0.2095	0.2098	0.2098	0.2064	0.0090	-0.0034	0.0019	0.3034	-96.283	031.15	042
01.92	0.0085	00.639	0.0015	0.2067	0.2065	0.2065	0.2064	0.0128	0.0315	-0.0009	0.3001	29.247	031.15	043
02.32	0.0194	00.781	0.0109	0.2086	0.2080	0.2080	0.2071	-0.0044	0.0024	0.0012	0.3009	22.624	031.15	044
02.66	0.0298	00.890	0.0200	0.2114	0.2102	0.2102	0.2079	0.0004	0.0020	0.0010	0.3023	90.661	031.21	045
03.02	0.0469	00.960	0.0357	0.2138	0.2116	0.2116	0.2106	-0.0061	0.0011	0.0024	0.3011	63.459	031.12	046
03.41	0.0652	01.047	0.0525	0.2155	0.2120	0.2120	0.2107	0.0051	-0.0465	0.0011	0.3013	48.764	031.02	047
03.75	0.0932	01.158	0.0790	0.2169	0.2133	0.2133	0.2127	0.0087	0.0126	0.0024	0.3006	37.759	031.05	048
04.12	0.1185	01.298	0.1002	0.2203	0.2125	0.2125	0.2136	-0.0033	0.0027	0.0027	0.3011	34.049	031.08	049
04.52	0.1418	01.418	0.1015	0.2194	0.2108	0.2108	0.2113	-0.0131	-0.0067	0.0023	0.3006	36.382	031.25	050
04.89	0.1418	01.483	0.1233	0.2224	0.2111	0.2111	0.2121	-0.0039	0.0059	0.0039	0.3010	31.780	031.31	051
05.27	0.1664	01.554	0.1456	0.2332	0.2224	0.2224	0.2182	-0.0035	-0.0182	0.0026	0.3007	28.377	031.25	052
05.65	0.2029	01.660	0.1835	0.2367	0.2176	0.2176	0.2209	-0.0029	0.0277	0.0043	0.3032	24.843	031.15	053
06.00	0.2132	01.755	0.1894	0.2367	0.2192	0.2192	0.2182	-0.0029	0.0407	0.0022	0.3036	25.013	031.15	054
06.41	0.2399	01.850	0.2145	0.2388	0.2134	0.2134	0.2188	-0.0126	-0.0833	0.0047	0.3055	23.436	031.28	055
06.79	0.2591	01.938	0.2315	0.2471	0.2180	0.2180	0.2244	-0.0195	-0.0041	0.0036	0.3064	22.961	031.21	056

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 012 MACH NO 0.606 RW/L 06972404 Q 0900 PSF TO 569

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AR	CP	PO	PMT
07.16	0.2797	02.006	0.2502	0.2518	0.2187	0.2257	-0.0251	-0.0301	0.0032	0.0070	21.787	031.08	057
07.53	0.2929	02.033	0.2627	0.2677	0.2111	0.2193	-0.0306	-0.0204	0.0034	0.0081	21.090	031.12	058
07.92	0.3482	02.133	0.3150	0.2635	0.2176	0.2257	-0.0147	-0.0669	0.0030	0.0082	18.609	031.08	059
08.30	0.3697	02.298	0.3352	0.2635	0.2123	0.2223	-0.0160	-0.0224	0.0031	0.0100	18.886	031.15	060
08.71	0.4138	02.425	0.3768	0.2730	0.2128	0.2230	-0.0115	-0.0358	0.0042	0.0102	17.805	031.25	061
09.38	0.4848	02.547	0.4638	0.2885	0.2123	0.2263	-0.0520	-0.0221	0.0045	0.0139	15.959	031.08	063
09.62	0.5032	02.613	0.4607	0.2931	0.2120	0.2276	-0.0584	-0.0005	0.0041	0.0156	15.755	031.08	064
09.84	0.5228	02.619	0.4776	0.3061	0.2200	0.2298	-0.0415	-0.0103	0.0044	0.0098	15.219	031.12	065
10.03	0.5411	02.682	0.4958	0.3037	0.2127	0.2286	-0.0367	-0.0131	0.0048	0.0138	15.058	031.12	066
10.19	0.5573	02.760	0.5107	0.3088	0.2135	0.2242	-0.0257	-0.0217	0.0048	0.0107	15.043	031.15	067
10.46	0.5915	02.810	0.5424	0.3204	0.2166	0.2314	-0.0598	-0.0404	0.0034	0.0148	14.430	031.12	068
10.68	0.6059	02.855	0.5552	0.3255	0.2170	0.2294	-0.0548	-0.0068	0.0037	0.0124	14.316	031.15	069
10.79	0.6269	02.898	0.5756	0.3281	0.2145	0.2284	-0.0541	-0.0295	0.0044	0.0148	14.043	031.12	070
10.85	0.6481	02.891	0.5961	0.3329	0.2147	0.2295	-0.0388	-0.0030	0.0040	0.0148	13.549	031.15	071
10.88	0.6501	02.897	0.5977	0.3350	0.2162	0.2317	-0.0610	-0.0307	0.0040	0.0155	13.537	031.12	072
-00.16	-0.0246	-00.060	-0.0240	0.2124	0.2124	0.2096	0.0052	0.0500	-0.0024	-0.0027	07.430	031.05	070

MSMT TEST 09

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 09

RUN 013 MACH NO 2.010 RN/L 07297436 Q 1465 PSF TD 547

COEFFICIENTS

ALPHA	N	PM	L	O	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.37	0.2135	-0.065	0.0129	0.4740	0.4740	0.5473	-0.0021	-0.1020	-0.0020	0.0733	-16.719	028.59	006
-11.23	-1.2556	-03.990	-1.1407	0.7023	0.6668	0.5648	0.0832	0.0533	-0.0044	0.0980	09.653	028.59	007
-11.00	-1.2148	-03.948	-1.1037	0.6886	0.6635	0.5612	0.0835	0.0514	-0.0043	0.0966	09.653	028.59	008
-10.75	-1.1802	-03.828	-1.0725	0.6701	0.6602	0.5574	0.0835	0.0514	-0.0043	0.0949	09.653	028.56	009
-10.54	-1.1401	-03.736	-1.0356	0.6668	0.6600	0.5595	0.0793	0.0276	-0.0037	0.0935	09.954	028.56	010
-10.29	-1.1004	-03.627	-0.9998	0.6529	0.6639	0.5574	0.0769	0.0303	-0.0033	0.0935	10.013	028.56	011
-10.03	-1.0621	-03.489	-0.9650	0.6427	0.6648	0.5567	0.0789	0.0303	-0.0036	0.0919	10.979	028.52	012
-09.80	-1.0195	-03.400	-0.9259	0.6293	0.6626	0.5557	0.0798	0.0070	-0.0031	0.0932	10.131	028.49	013
-09.57	-0.9803	-03.307	-0.8893	0.6214	0.6648	0.5551	0.0755	0.0117	-0.0019	0.0902	10.250	028.49	014
-09.34	-0.9484	-03.163	-0.8611	0.6083	0.6605	0.5510	0.0786	-0.0125	-0.0028	0.9004	10.133	028.52	015
-09.09	-0.9004	-03.100	-0.8164	0.5965	0.6601	0.5507	0.0703	0.0214	-0.0027	0.9004	10.458	028.56	016
-08.86	-0.8762	-03.994	-0.7949	0.5891	0.6596	0.5487	0.0598	0.0025	-0.0015	0.8891	10.382	028.56	017
-08.64	-0.8430	-03.881	-0.7641	0.5828	0.6615	0.5495	0.0664	-0.0134	-0.0027	0.8880	10.382	028.62	018
-08.38	-0.7999	-02.805	-0.7242	0.5725	0.6608	0.5474	0.0586	-0.0090	-0.0026	0.8866	10.653	028.62	019
-08.17	-0.7798	-02.701	-0.7064	0.5668	0.6607	0.5458	0.0581	-0.0038	-0.0020	0.8851	10.522	028.62	020
-07.93	-0.7437	-02.643	-0.6731	0.5586	0.6604	0.5455	0.0607	-0.0112	-0.0022	0.8851	10.797	028.62	021
-07.71	-0.7084	-02.588	-0.6421	0.5519	0.6621	0.5460	0.0564	-0.0127	-0.0016	0.8849	11.101	028.59	022
-07.47	-0.6765	-02.515	-0.6107	0.5461	0.6621	0.5456	0.0588	-0.0018	-0.0018	0.8835	11.294	028.59	023
-07.26	-0.6525	-02.427	-0.5890	0.5400	0.6613	0.5433	0.0542	0.0075	-0.0019	0.8820	11.299	028.59	024
-07.02	-0.6191	-02.367	-0.5581	0.5336	0.6614	0.5436	0.0570	-0.0147	-0.0013	0.8822	11.615	028.62	025
-06.83	-0.5943	-02.276	-0.5352	0.5285	0.6611	0.5406	0.0493	-0.0169	-0.0017	0.8795	11.635	028.65	026
-06.59	-0.5661	-02.222	-0.5091	0.5261	0.6621	0.5420	0.0453	-0.0237	-0.0006	0.8776	11.927	028.62	027
-06.35	-0.5412	-02.132	-0.4868	0.5191	0.6621	0.5386	0.0480	-0.0407	-0.0012	0.8766	11.966	028.65	028
-06.13	-0.5142	-02.064	-0.4617	0.5169	0.6646	0.5394	0.0437	-0.0277	-0.0006	0.8748	12.193	028.59	029
-05.89	-0.4943	-01.979	-0.4438	0.5142	0.6659	0.5390	0.0498	-0.0349	-0.0005	0.8731	12.161	028.56	030
-05.66	-0.4700	-01.890	-0.4220	0.5076	0.6635	0.5380	0.0423	-0.0373	-0.0010	0.8746	12.216	028.56	031
-05.43	-0.4445	-01.832	-0.3986	0.5035	0.6635	0.5368	0.0415	-0.0360	-0.0010	0.8733	12.524	028.59	032
-05.20	-0.4243	-01.748	-0.3806	0.4993	0.6627	0.5357	0.0414	-0.0391	-0.0009	0.8729	12.519	028.52	033
-04.95	-0.4022	-01.711	-0.3607	0.4969	0.6639	0.5368	0.0413	-0.0395	-0.0009	0.8729	12.921	028.52	034
-04.69	-0.3842	-01.622	-0.3451	0.4919	0.6620	0.5351	0.0378	-0.0411	-0.0010	0.8731	12.821	028.56	035
-04.47	-0.3627	-01.550	-0.3254	0.4914	0.6646	0.5362	0.0377	-0.0419	-0.0009	0.8717	12.985	028.56	036
-04.24	-0.3406	-01.494	-0.3055	0.4856	0.6617	0.5336	0.0374	-0.0352	-0.0005	0.8718	13.327	028.59	037
-04.02	-0.3224	-01.457	-0.2890	0.4858	0.6643	0.5347	0.0373	-0.0355	-0.0013	0.8704	13.731	028.59	038
-03.78	-0.3082	-01.387	-0.2770	0.4841	0.6648	0.5352	0.0372	-0.0364	0.0005	0.8704	13.675	028.59	039
-03.55	-0.2903	-01.316	-0.2609	0.4819	0.6648	0.5340	0.0337	-0.0304	-0.0009	0.8691	13.767	028.62	040
-03.31	-0.2763	-01.228	-0.2489	0.4813	0.6661	0.5355	0.0336	-0.0313	-0.0009	0.8693	13.505	028.65	041
-03.08	-0.2633	-01.146	-0.2376	0.4754	0.6689	0.5377	0.0336	-0.0471	0.0001	0.8688	13.224	028.56	042
-02.84	-0.2417	-01.073	-0.2184	0.4758	0.6645	0.5348	0.0334	-0.0332	0.0001	0.8704	13.491	028.59	043
-02.61	-0.2247	-00.987	-0.2032	0.4763	0.6665	0.5365	0.0264	-0.0430	-0.0008	0.8700	13.337	028.52	044
-02.39	-0.2076	-00.899	-0.1879	0.4763	0.6681	0.5379	0.0328	-0.0427	-0.0004	0.8698	13.152	028.46	045
-02.17	-0.1863	-00.843	-0.1804	0.4752	0.6685	0.5381	0.0252	-0.0227	-0.0005	0.8698	13.754	028.46	046
-01.98	-0.1758	-00.772	-0.1595	0.4739	0.6681	0.5379	0.0285	-0.0376	-0.0003	0.8698	13.343	028.49	047
-01.74	-0.1652	-00.682	-0.1510	0.4689	0.6641	0.5360	0.0213	-0.0471	0.0003	0.8718	12.545	028.59	048
-01.52	-0.1550	-00.612	-0.1425	0.4698	0.6658	0.5362	0.0212	-0.0624	-0.0012	0.8704	11.995	028.59	049
-01.28	-0.1333	-00.556	-0.1228	0.4695	0.6666	0.5370	0.0173	-0.0637	-0.0015	0.8704	12.662	028.59	050
-01.06	-0.1229	-00.467	-0.1142	0.4700	0.6678	0.5387	0.0203	-0.0711	-0.0009	0.8710	11.541	028.68	051
-00.85	-0.1169	-00.382	-0.1099	0.4703	0.6686	0.5394	0.0132	-0.0734	-0.0005	0.8708	09.917	028.65	052
-00.61	-0.0995	-00.310	-0.0946	0.4680	0.6669	0.5390	0.0162	-0.0737	-0.0012	0.8720	09.461	028.62	053
-00.39	-0.0823	-00.222	-0.0791	0.4689	0.6684	0.5402	0.0158	-0.0748	-0.0012	0.8718	08.182	028.59	054
-00.14	-0.0607	-00.103	-0.0795	0.4684	0.6682	0.5400	0.0154	-0.0617	-0.0013	0.8718	03.865	028.59	055
00.05	-0.0590	-00.047	-0.0594	0.4681	0.6681	0.5414	0.0114	-0.0484	-0.0006	0.8733	02.430	028.59	056

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 013 MACH NO 2.010 RN/L 07297436 Q 1465 PSF TO 547

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.27	-0.0372	00.024	-0.0394	0.4682	0.4684	0.5415	0.0112	-0.0493	-0.0006	0.0731	-01.951	028.56	057
00.54	-0.0303	00.108	-0.0347	0.4687	0.4690	0.5404	0.0143	-0.0497	-0.0002	0.0715	-10.877	028.52	058
00.76	-0.0234	00.210	-0.0296	0.4688	0.4672	0.5401	0.0070	-0.0666	-0.0013	0.0729	-27.187	028.52	059
00.98	-0.0051	00.297	-0.0131	0.4674	0.4675	0.5405	0.0064	-0.0823	-0.0012	0.0729	-77.755	028.52	060
01.20	0.0133	00.367	0.0035	0.4676	0.4674	0.5406	0.0021	-0.0764	-0.0000	0.0731	83.488	028.56	061
01.42	0.0316	00.437	0.0199	0.4706	0.4699	0.5431	0.0047	-0.0695	-0.0002	0.0731	42.086	028.56	062
01.67	0.0424	00.505	0.0286	0.4735	0.4724	0.5443	-0.0026	-0.0644	-0.0031	0.0718	36.220	028.59	063
01.89	0.0627	00.575	0.0452	0.4725	0.4708	0.5443	-0.0032	-0.0725	-0.0004	0.0735	28.773	028.62	064
02.13	0.0713	00.660	0.0537	0.4733	0.4709	0.5444	-0.0073	-0.0668	-0.0010	0.0735	28.137	028.62	065
02.35	0.0936	00.752	0.0741	0.4737	0.4723	0.5441	-0.0046	-0.0817	-0.0007	0.0718	23.756	028.59	066
02.57	0.1042	00.818	0.0829	0.4777	0.4735	0.5451	-0.0054	-0.0684	0.0033	0.0717	23.848	028.56	067
02.79	0.1185	00.904	0.0953	0.4792	0.4740	0.5456	-0.0062	-0.0621	0.0000	0.0717	23.178	028.56	068
03.03	0.1369	00.957	0.1116	0.4805	0.4739	0.5458	-0.0069	-0.0557	0.0005	0.0710	21.241	028.59	069
03.25	0.1593	01.029	0.1323	0.4805	0.4722	0.5454	-0.0110	-0.0716	0.0004	0.0731	19.620	028.56	070
03.49	0.1899	01.096	0.1409	0.4812	0.4717	0.5450	-0.0081	-0.0719	0.0007	0.0733	19.598	028.59	071
03.70	0.1847	01.167	0.1536	0.4857	0.4747	0.5478	-0.0190	-0.0602	0.0031	0.0731	19.199	028.56	072
03.95	0.1991	01.252	0.1660	0.4867	0.4741	0.5488	-0.0195	-0.0760	0.0011	0.0748	19.103	028.59	073
04.14	0.2247	01.306	0.1898	0.4895	0.4746	0.5480	-0.0170	-0.0688	0.0009	0.0735	17.655	028.62	074
04.38	0.2468	01.377	0.2098	0.4927	0.4752	0.5487	-0.0211	-0.0703	0.0008	0.0735	16.944	028.62	075
04.63	0.2888	01.464	0.2293	0.4990	0.4774	0.5523	-0.0217	-0.0792	0.0022	0.0735	16.547	028.62	076
04.86	0.2873	01.536	0.2459	0.5001	0.4774	0.5522	-0.0192	-0.0721	0.0012	0.0748	16.242	028.59	077
05.05	0.3055	01.606	0.2622	0.5034	0.4783	0.5531	-0.0199	-0.0660	0.0026	0.0746	15.974	028.59	078
05.31	0.3357	01.664	0.2899	0.5094	0.4803	0.5548	-0.0242	-0.0674	0.0015	0.0746	15.059	028.56	079
05.53	0.3375	01.717	0.3095	0.5128	0.4805	0.5553	-0.0215	-0.0604	0.0022	0.0748	14.589	028.59	080
05.76	0.3716	01.801	0.3217	0.5134	0.4785	0.5549	-0.0255	-0.0693	0.0020	0.0764	14.723	028.62	081
06.01	0.4010	01.857	0.3483	0.5222	0.4829	0.5593	-0.0263	-0.0632	0.0030	0.0764	14.070	028.62	082
06.23	0.4109	01.944	0.3563	0.5217	0.4800	0.5578	-0.0268	-0.0638	0.0032	0.0778	14.371	028.62	083
06.49	0.4435	02.003	0.3834	0.5268	0.4801	0.5592	-0.0271	-0.0788	0.0034	0.0791	13.815	028.59	084
06.72	0.4690	02.094	0.4097	0.5311	0.4796	0.5587	-0.0311	-0.0656	0.0033	0.0791	13.562	028.59	085
06.94	0.4975	02.148	0.4358	0.5365	0.4799	0.5592	-0.0348	-0.0666	0.0032	0.0793	13.120	028.62	086
07.20	0.5218	02.219	0.4578	0.5400	0.4784	0.5593	-0.0283	-0.0662	0.0047	0.0809	12.919	028.65	087
07.45	0.5421	02.322	0.4754	0.5455	0.4793	0.5589	-0.0320	-0.0746	0.0034	0.0797	13.010	028.68	088
07.66	0.5786	02.397	0.5094	0.5535	0.4807	0.5618	-0.0391	-0.0841	0.0044	0.0811	12.594	028.68	089
07.91	0.6081	02.473	0.5366	0.5564	0.4775	0.5599	-0.0444	-0.0929	0.0047	0.0824	12.355	028.65	090
08.14	0.6357	02.577	0.5611	0.5662	0.4810	0.5650	-0.0432	-0.0865	0.0046	0.0840	12.317	028.68	091
08.38	0.6806	02.660	0.6033	0.5755	0.4815	0.5666	-0.0371	-0.0717	0.0052	0.0851	11.874	028.62	092
08.60	0.7060	02.753	0.6261	0.5817	0.4815	0.5665	-0.0374	-0.0731	0.0062	0.0840	11.845	028.59	093
08.86	0.7365	02.816	0.6534	0.6263	0.4826	0.5687	-0.0443	-0.0827	0.0063	0.0860	11.617	028.52	094
09.09	0.7656	02.927	0.6797	0.5976	0.4827	0.5700	-0.0440	-0.1066	0.0059	0.0873	11.614	028.49	095
09.29	0.7956	03.012	0.7075	0.6033	0.4812	0.5689	-0.0441	-0.0862	0.0055	0.0877	11.500	028.56	096
09.52	0.8308	03.121	0.7395	0.6137	0.4828	0.5770	-0.0509	-0.0681	0.0064	0.0891	11.411	028.56	097
09.67	0.8636	03.178	0.7702	0.6213	0.4830	0.5722	-0.0509	-0.0765	0.0068	0.0891	11.181	028.56	098
09.84	0.8954	03.216	0.7994	0.6302	0.4842	0.5735	-0.0546	-0.0635	0.0075	0.0893	10.912	028.59	099
10.02	0.9208	03.326	0.8222	0.6308	0.4860	0.5751	-0.0507	-0.0867	0.0064	0.0891	10.972	028.56	100
10.17	0.9677	03.385	0.8559	0.6475	0.4855	0.5761	-0.0477	-0.0856	0.0071	0.0906	10.705	028.56	101
10.29	0.9776	03.419	0.8751	0.6530	0.4862	0.5770	-0.0441	-0.0730	0.0069	0.0907	10.625	028.59	102
10.38	0.9905	03.485	0.8869	0.6593	0.4848	0.5758	-0.0437	-0.0960	0.0070	0.0909	10.399	028.62	103
10.60	1.0151	03.542	0.9089	0.6618	0.4833	0.5756	-0.0406	-0.0745	0.0073	0.0924	10.599	028.62	104
10.78	1.0350	03.680	0.9262	0.6692	0.4841	0.5765	-0.0505	-0.0646	0.0070	0.0924	10.802	028.62	105
10.99	1.0704	03.789	0.9582	0.6809	0.4858	0.5796	-0.0572	-0.0609	0.0068	0.0958	10.753	028.62	106
11.20	1.1141	03.849	0.9987	0.6819	0.4848	0.5801	-0.0540	-0.0615	0.0077	0.0953	10.476	028.62	107

MSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 013 MACH NO 2.010 RN/L 07297436 Q 1465 PSF TO 547

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
11.32	1.1311	33.953	1.0134	0.6998	0.4873	0.5811	-0.0035	-0.0780	0.0067	0.0938	10.618	028.62	108
11.44	1.1644	33.977	1.0446	0.7090	0.4877	0.5815	-0.0467	-0.0991	0.0075	0.0938	10.376	028.62	109
11.48	1.1961	34.313	1.0744	0.7196	0.4913	0.5853	-0.0466	-0.0931	0.0077	0.0940	10.193	028.65	110
11.52	1.1999	34.385	1.0778	0.7230	0.4903	0.5841	-0.0530	-0.0804	0.0074	0.0938	10.344	028.62	111
11.56	1.2275	34.096	1.1043	0.7254	0.4904	0.5841	-0.0504	-0.0804	0.0065	0.0937	10.137	028.59	112
11.59	1.2296	34.109	1.1060	0.7279	0.4909	0.5848	-0.0466	-0.0948	0.0075	0.0938	10.151	028.62	113
00.06	0.0542	-30.039	0.0537	0.4762	0.4761	0.5494	-0.0029	-0.0808	-0.0025	0.0733	-02.214	028.59	114

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 014 MACH ND 2.010 RN/L 06813357 Q 1467 PSF TD 575

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.11	0.0495	-00.192	0.0483	0.5964	0.5963	0.7060	0.0160	-0.1218	-0.0019	0.1096	-11.767	028.59	006
-11.58	-2.0147	01.245	-1.8579	0.9698	0.5773	0.7030	0.0347	-0.1348	-0.0180	0.1258	-01.817	028.62	307
-11.61	-2.0392	01.257	-1.8812	0.9766	0.5781	0.7023	0.0387	-0.1778	-0.0177	0.1242	-01.873	028.59	008
-11.63	-2.0483	01.270	-1.8902	0.9764	0.5751	0.7009	0.0426	-0.1988	-0.0196	0.1258	-01.884	028.62	009
-11.61	-2.0479	01.253	-1.8899	0.9770	0.5766	0.7024	0.0530	-0.2115	-0.0182	0.1258	-01.859	028.62	010
-11.53	-2.0232	01.224	-1.8671	0.9695	0.5767	0.7011	0.0488	-0.1753	-0.0180	0.1244	-01.838	028.65	011
-11.40	-2.0070	01.230	-1.8592	0.9631	0.5779	0.7022	0.0483	-0.1539	-0.0176	0.1243	-01.862	028.62	012
-11.23	-1.9770	01.267	-1.8269	0.9504	0.5765	0.7010	0.0442	-0.1258	-0.0169	0.1246	-01.947	028.68	013
-11.01	-1.9398	01.309	-1.7943	0.9348	0.5750	0.6994	0.0401	-0.1267	-0.0153	0.1246	-02.049	028.68	014
-10.81	-1.9063	01.353	-1.7641	0.9253	0.5779	0.7022	0.0439	-0.1995	-0.0150	0.1243	-02.156	028.62	015
-10.59	-1.8503	01.365	-1.7127	0.9080	0.5778	0.7021	0.0500	-0.1913	-0.0151	0.1243	-02.242	028.62	016
-10.36	-1.7849	01.349	-1.6515	0.8909	0.5793	0.7020	0.0493	-0.1768	-0.0169	0.1227	-02.296	028.59	017
-10.11	-1.7462	01.410	-1.6177	0.8751	0.5775	0.7015	0.0519	-0.1625	-0.0149	0.1240	-02.453	028.56	018
-09.89	-1.6858	01.457	-1.5624	0.8599	0.5789	0.7015	0.0339	-0.1297	-0.0164	0.1226	-02.625	028.56	019
-09.66	-1.6208	01.470	-1.5036	0.8431	0.5793	0.7020	0.0297	-0.1651	-0.0140	0.1227	-02.755	028.59	020
-09.44	-1.5817	01.477	-1.4655	0.8290	0.5773	0.7022	0.0360	-0.1438	-0.0144	0.1229	-02.837	028.62	021
-09.22	-1.5096	01.426	-1.3974	0.8125	0.5780	0.7008	0.0368	-0.1373	-0.0143	0.1229	-02.810	028.62	022
-08.98	-1.4761	01.434	-1.3672	0.8047	0.5813	0.7027	0.0348	-0.1365	-0.0133	0.1214	-02.931	028.62	023
-08.77	-1.4230	01.412	-1.3179	0.7908	0.5807	0.7021	0.0343	-0.1580	-0.0129	0.1214	-03.015	028.62	024
-08.52	-1.3848	01.425	-1.2831	0.7816	0.5828	0.7025	0.0337	-0.1585	-0.0112	0.1197	-03.126	028.56	025
-08.31	-1.3186	01.371	-1.2204	0.7681	0.5837	0.7035	0.0332	-0.1725	-0.0114	0.1198	-03.158	028.59	026
-08.09	-1.2849	01.362	-1.1898	0.7595	0.5844	0.7043	0.0288	-0.1369	-0.0095	0.1198	-03.221	028.59	027
-07.86	-1.2372	01.342	-1.1456	0.7483	0.5847	0.7044	0.0248	-0.1374	-0.0098	0.1197	-03.294	028.56	028
-07.65	-1.1866	01.301	-1.0979	0.7395	0.5868	0.7066	0.0277	-0.1294	-0.0093	0.1198	-03.331	028.59	029
-07.42	-1.1485	01.276	-1.0631	0.7302	0.5868	0.7051	0.0307	-0.1502	-0.0087	0.1184	-03.376	028.59	030
-07.22	-1.1147	01.268	-1.0323	0.7212	0.5858	0.7056	0.0267	-0.1363	-0.0081	0.1198	-03.454	028.59	031
-06.98	-1.0568	01.229	-0.9777	0.7105	0.5863	0.7048	0.0258	-0.1213	-0.0074	0.1185	-03.533	028.62	032
-06.78	-1.0266	01.219	-0.9500	0.7049	0.5878	0.7048	0.0221	-0.1291	-0.0072	0.1170	-03.608	028.62	033
-06.58	-0.9859	01.180	-0.9121	0.6970	0.5880	0.7049	0.0249	-0.1282	-0.0062	0.1169	-03.636	028.59	034
-06.35	-0.9380	01.137	-0.8672	0.6882	0.5882	0.7039	0.0280	-0.1560	-0.0061	0.1157	-03.684	028.65	035
-06.09	-0.9092	01.129	-0.8417	0.6808	0.5876	0.7032	0.0204	-0.1282	-0.0057	0.1156	-03.774	028.62	036
-05.91	-0.8503	01.062	-0.7850	0.6744	0.5900	0.7053	0.0232	-0.1273	-0.0057	0.1153	-03.794	028.56	037
-05.69	-0.8226	01.017	-0.7599	0.6694	0.5907	0.7047	0.0229	-0.1267	-0.0058	0.1140	-03.755	028.59	038
-05.47	-0.7798	00.975	-0.7200	0.6621	0.5935	0.7032	0.0153	-0.1201	-0.0050	0.1127	-03.799	028.62	039
-05.25	-0.7474	00.935	-0.6899	0.6589	0.5930	0.7054	0.0218	-0.1188	-0.0047	0.1124	-03.801	028.56	040
-05.03	-0.7160	00.891	-0.6614	0.6514	0.5908	0.7034	0.0213	-0.1182	-0.0048	0.1125	-03.780	028.59	041
-04.79	-0.6732	00.816	-0.6215	0.6448	0.5907	0.7019	0.0172	-0.1106	-0.0048	0.1112	-03.683	028.62	042
-04.58	-0.6496	00.787	-0.6005	0.6396	0.5896	0.7010	0.0135	-0.1108	-0.0050	0.1114	-03.662	028.65	043
-04.33	-0.6102	00.728	-0.5639	0.6345	0.5901	0.7018	0.0095	-0.0964	-0.0046	0.1117	-03.623	028.72	044
-04.11	-0.5839	00.701	-0.5401	0.6291	0.5888	0.7004	0.0193	-0.0942	-0.0040	0.1117	-03.646	028.72	045
-03.90	-0.5354	00.613	-0.4938	0.6285	0.5935	0.7034	0.0086	-0.0954	-0.0049	0.1099	-03.481	028.65	046
-03.69	-0.4971	00.555	-0.4578	0.6247	0.5940	0.7024	0.0081	-0.1020	-0.0037	0.1085	-03.395	028.65	047
-03.45	-0.4705	00.528	-0.4339	0.6211	0.5938	0.7023	0.0112	-0.1084	-0.0031	0.1085	-03.411	028.65	048
-03.22	-0.4469	00.499	-0.4131	0.6144	0.5903	0.6990	0.0141	-0.0999	-0.0034	0.1088	-03.394	028.72	049
-03.03	-0.3969	00.427	-0.3651	0.6124	0.5923	0.6997	0.0136	-0.1065	-0.0031	0.1075	-03.266	028.75	050
-02.79	-0.3628	00.368	-0.3335	0.6098	0.5928	0.7003	0.0132	-0.0987	-0.0030	0.1075	-03.083	028.75	051
-02.58	-0.3324	00.309	-0.3052	0.6086	0.5942	0.7015	-0.0008	-0.0865	-0.0030	0.1073	-02.825	028.72	052
-02.35	-0.3058	00.265	-0.2812	0.6080	0.5959	0.7029	0.0081	-0.1001	-0.0019	0.1070	-02.637	028.65	053
-02.14	-0.2791	00.222	-0.2567	0.6055	0.5955	0.7024	0.0059	-0.0929	-0.0028	0.1069	-02.413	028.62	054
-01.96	-0.2520	00.161	-0.2316	0.6012	0.5929	0.7012	0.0197	-0.1047	-0.0028	0.1083	-02.197	028.62	055
-01.73	-0.2173	00.102	-0.1993	0.6005	0.5942	0.7024	0.0231	-0.1115	-0.0024	0.1082	-01.420	028.59	056

MSWF TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 014 MACH NO 2.010 RN/L 06813357 Q 1467 PSF TD 575

10/17/62

COEFFICIENTS

ALPHA	V	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
-01.52	-0.1829	00.059	-0.1670	0.6003	0.5957	0.7037	0.0231	-0.1117	0.0026	0.1080	-00.981	028.56	057
-01.29	-0.1562	00.032	-0.1429	0.5970	0.5936	0.7030	0.0229	-0.0975	-0.0027	0.1093	-00.615	028.52	058
-01.08	-0.1370	00.019	-0.1258	0.5966	0.5941	0.7033	0.0265	-0.1046	0.0022	0.1092	-00.422	028.49	059
-00.85	-0.1174	00.006	-0.1086	0.5948	0.5931	0.7009	0.0266	-0.1267	0.0018	0.1077	-00.163	028.49	060
-00.64	-0.0974	00.001	-0.0914	0.5933	0.5927	0.7019	0.0299	-0.1261	0.0018	0.1107	05.094	028.49	061
-00.43	-0.0775	00.000	-0.0743	0.5933	0.5930	0.7036	0.0265	-0.1199	0.0010	0.1109	18.585	028.56	062
00.00	-0.0201	00.123	-0.0177	0.5915	0.5914	0.7024	0.0193	-0.0991	-0.0010	0.1096	88.532	028.59	064
00.18	-0.0047	00.136	-0.0047	0.5930	0.5930	0.7014	0.0091	-0.0796	0.0022	0.1101	-17.366	028.68	065
00.44	0.0339	00.194	0.0321	0.5914	0.5913	0.7014	0.0190	-0.0843	-0.0012	0.1105	-12.847	028.78	066
00.65	0.0874	00.266	0.0807	0.5897	0.5893	0.6988	0.0154	-0.0866	-0.0014	0.1105	-09.245	028.78	067
00.86	0.1103	00.295	0.1014	0.5939	0.5923	0.7015	0.0149	-0.0839	-0.0006	0.1092	-08.112	028.81	068
01.07	0.1297	00.324	0.1187	0.5941	0.5918	0.7010	0.0045	-0.0925	0.0001	0.1092	-07.591	028.81	069
01.28	0.1605	00.368	0.1473	0.5955	0.5920	0.7012	0.0112	-0.1127	0.0009	0.1092	-06.966	028.81	070
01.52	0.1955	00.429	0.1797	0.5996	0.5964	0.7035	0.0177	-0.1111	0.0005	0.1089	-06.459	028.75	071
01.75	0.2382	00.487	0.2198	0.6028	0.5958	0.7044	0.0138	-0.1043	0.0015	0.1086	-06.218	028.68	072
01.94	0.2659	00.533	0.2456	0.6035	0.5949	0.7047	0.0170	-0.1177	0.0009	0.1098	-06.095	028.62	073
02.20	0.3009	00.577	0.2778	0.6070	0.5959	0.7041	0.0201	-0.1242	0.0024	0.1082	-05.831	028.59	074
02.38	0.3169	00.609	0.2918	0.6092	0.5966	0.7046	0.0200	-0.1310	0.0011	0.1080	-05.837	028.56	075
02.61	0.3641	00.685	0.3366	0.6124	0.5964	0.7042	0.0228	-0.1298	0.0013	0.1077	-05.711	028.49	076
02.84	0.3951	00.729	0.3650	0.6156	0.5967	0.7045	0.0190	-0.1228	0.0015	0.1077	-05.604	028.49	077
03.05	0.4177	00.757	0.3854	0.6172	0.5958	0.7037	0.0255	-0.1213	0.0019	0.1079	-05.506	028.52	078
03.25	0.4485	00.817	0.4139	0.6198	0.5954	0.7034	0.0252	-0.1277	0.0015	0.1080	-05.534	028.56	079
03.48	0.4834	00.877	0.4461	0.6250	0.5975	0.7056	0.0214	-0.1208	0.0025	0.1080	-05.511	028.56	080
03.69	0.5137	00.923	0.4743	0.6274	0.5955	0.7052	0.0210	-0.1203	0.0025	0.1096	-05.440	028.59	081
03.89	0.5449	00.981	0.5032	0.6316	0.5960	0.7054	0.0208	-0.1269	0.0020	0.1094	-05.467	028.59	082
04.13	0.5873	01.039	0.5428	0.6378	0.5971	0.7081	0.0189	-0.1200	0.0022	0.1111	-05.374	028.59	083
04.39	0.6167	01.081	0.5692	0.6423	0.5969	0.7083	0.0200	-0.1190	0.0032	0.1114	-05.323	028.65	084
04.76	0.6517	01.143	0.6023	0.6460	0.5962	0.7091	0.0198	-0.1331	0.0040	0.1128	-05.316	028.65	085
04.98	0.6986	01.215	0.6468	0.6516	0.5956	0.7097	0.0191	-0.1180	0.0040	0.1128	-05.285	028.62	086
05.19	0.7247	01.259	0.6702	0.6572	0.5966	0.7094	0.0186	-0.1029	0.0031	0.1128	-05.276	028.65	087
05.43	0.7601	01.303	0.7029	0.6644	0.5981	0.7108	0.0113	-0.0966	0.0030	0.1127	-05.208	028.62	088
05.67	0.8024	01.361	0.7421	0.6725	0.5992	0.7133	0.0143	-0.0957	0.0032	0.1141	-05.154	028.62	089
05.91	0.8303	01.391	0.7671	0.6775	0.5983	0.7123	0.0105	-0.1033	0.0034	0.1140	-05.090	028.59	090
06.11	0.8696	01.434	0.8034	0.6859	0.5998	0.7136	0.0100	-0.1104	0.0038	0.1139	-05.011	028.56	091
06.33	0.9106	01.473	0.8418	0.6914	0.5979	0.7119	0.0128	-0.1166	0.0044	0.1140	-04.915	028.59	092
06.54	0.9527	01.530	0.8809	0.7003	0.5990	0.7130	0.0088	-0.1022	0.0041	0.1140	-04.879	028.59	093
06.78	0.9986	01.588	0.9239	0.7085	0.5987	0.7141	0.0116	-0.1012	0.0042	0.1155	-04.825	028.59	094
07.00	1.0356	01.625	0.9577	0.7162	0.5981	0.7142	0.0109	-0.0954	0.0046	0.1141	-04.768	028.62	095
07.24	1.0785	01.651	0.9975	0.7252	0.5981	0.7136	0.0103	-0.1006	0.0041	0.1155	-04.650	028.59	096
07.46	1.1180	01.704	1.0337	0.7336	0.5974	0.7146	0.0062	-0.0790	0.0042	0.1172	-04.629	028.65	097
07.69	1.1697	01.766	1.0818	0.7474	0.6006	0.7160	0.0052	-0.0568	0.0028	0.1155	-04.534	028.59	098
07.91	1.1970	01.725	1.1056	0.7558	0.6006	0.7160	0.0013	-0.0725	0.0043	0.1153	-04.377	028.56	099
08.15	1.2466	01.753	1.1519	0.7663	0.6001	0.7154	-0.0030	-0.0727	0.0041	0.1153	-04.298	028.56	100
08.37	1.2807	01.775	1.1833	0.7714	0.5958	0.7159	-0.0076	-0.0369	0.0034	0.1170	-04.152	028.62	101
08.52	1.3277	01.775	1.2262	0.7848	0.5972	0.7157	-0.0017	-0.0508	0.0035	0.1169	-04.062	028.59	102
08.74	1.3721	01.813	1.2669	0.7974	0.5986	0.7161	-0.0048	-0.0716	0.0023	0.1170	-04.014	028.62	103
08.94	1.4125	01.808	1.3036	0.8091	0.5992	0.7160	-0.0096	-0.0585	0.0018	0.1168	-03.888	028.56	104
09.11	1.4624	01.825	1.3509	0.8186	0.5970	0.7140	-0.0173	-0.0666	0.0018	0.1170	-03.792	028.62	105
09.23	1.4883	01.819	1.3737	0.8274	0.5972	0.7157	-0.0144	-0.0591	0.0015	0.1185	-03.713	028.62	106
09.37	1.5354	01.839	1.4179	0.8383	0.5964	0.7150	-0.0156	-0.0298	0.0005	0.1186	-03.638	028.65	107

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 014 MACH NO 2.010 RM/L 06813357 Q 1467 PSF TD 575

HSMT TEST 89

10/17/62

COEFFICIENTS

ALPHA	V	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
09.53	1.5808	-01.862	1.4597	0.8525	0.5990	0.7162	-0.0163	-0.0297	-0.0004	0.1172	-03.578	028.65	108
09.70	1.6199	-01.888	1.4955	0.8656	0.6012	0.7183	-0.0136	-0.0001	-0.0021	0.1170	-03.541	028.62	109
09.84	1.6458	-01.882	1.5188	0.8742	0.6018	0.7189	-0.0177	0.0209	-0.0027	0.1170	-03.473	028.62	110
09.95	1.6762	-01.875	1.5473	0.8809	0.6002	0.7173	-0.0147	-0.0168	-0.0012	0.1170	-03.398	028.62	111
10.09	1.6943	-01.859	1.5631	0.8867	0.5991	0.7173	-0.0258	0.0196	-0.0023	0.1182	-03.333	028.56	112
10.26	1.7290	-01.814	1.5944	0.8985	0.6001	0.7170	-0.0233	0.0268	-0.0034	0.1169	-03.188	028.56	113
10.46	1.7677	-01.785	1.6298	0.9092	0.5982	0.7167	-0.0276	0.0329	-0.0041	0.1185	-03.070	028.62	114
10.64	1.8137	-01.756	1.6719	0.9222	0.5969	0.7155	-0.0394	0.0741	-0.0039	0.1186	-02.941	028.65	115
10.84	1.8710	-01.741	1.7251	0.9391	0.5978	0.7165	-0.0303	0.0828	-0.0055	0.1186	-02.826	028.68	116
10.94	1.9199	-01.713	1.7711	0.9534	0.5999	0.7186	-0.0308	0.0912	-0.0043	0.1186	-02.711	028.68	117
11.03	1.9453	-01.703	1.7947	0.9602	0.5989	0.7180	-0.0315	0.0953	-0.0035	0.1190	-02.659	028.75	118
11.04	1.9406	-01.654	1.7901	0.9590	0.5985	0.7175	-0.0282	0.0954	-0.0050	0.1190	-02.589	028.75	119
11.10	1.9692	-01.638	1.8165	0.9697	0.6017	0.7204	-0.0321	0.0446	-0.0061	0.1186	-02.526	028.65	120
20.07	0.0563	-00.157	0.0556	0.5933	0.5933	0.7042	0.0226	-0.1136	-0.0018	0.1109	-08.449	028.56	121

MSMT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RJN J15 MACH N3 2.010 RN/L 07940708 Q 1463 PSF T3 561

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
00.18	0.0446	-0.2024	0.0427	0.6060	0.6059	0.7167	0.0129	-0.1161	0.1927	0.1108	-13.864	028.52	006
-11.19	-1.9747	01.359	-1.8231	0.9598	0.5877	0.7116	0.0286	-0.0359	0.1911	0.1239	-02.090	028.52	009
-10.82	-1.8677	01.411	-1.7433	0.9343	0.5903	0.7128	0.0212	-0.0632	0.1824	0.1225	-02.271	028.52	008
-10.38	-1.8088	01.452	-1.6708	0.9060	0.5900	0.7111	0.0306	-0.0877	0.1915	0.1211	-02.442	028.56	009
-09.91	-1.5937	01.486	-1.5665	0.8752	0.5925	0.7136	0.0224	-0.0678	0.1932	0.1211	-02.665	028.56	010
-09.47	-1.5955	01.507	-1.4760	0.8481	0.5937	0.7134	0.0287	-0.1106	0.1928	0.1197	-02.870	028.56	011
-08.98	-1.5049	01.511	-1.3940	0.8196	0.5918	0.7115	0.0307	-0.1100	0.1929	0.1197	-03.049	028.56	012
-08.55	-1.6010	01.473	-1.2972	0.7947	0.5930	0.7128	0.0229	-0.1256	0.1913	0.1198	-03.194	028.59	013
-08.12	-1.3099	01.468	-1.2127	0.7745	0.5956	0.7139	0.0223	-0.1620	0.1916	0.1184	-03.404	028.59	014
-07.67	-1.2130	01.435	-1.1194	0.7536	0.5975	0.7160	0.0276	-0.1169	0.1933	0.1185	-03.527	028.62	015
-07.23	-1.1188	01.375	-1.0346	0.7350	0.5990	0.7160	0.0333	-0.1156	0.1962	0.1170	-03.732	028.62	016
-06.80	-1.0359	01.308	-0.9575	0.7194	0.6011	0.7190	0.0431	-0.1500	0.1962	0.1179	-03.836	028.49	017
-06.37	-0.9577	01.220	-0.8850	0.7047	0.6023	0.7170	0.0387	-0.1644	0.1945	0.1148	-03.869	028.43	018
-05.96	-0.8932	01.152	-0.8259	0.6916	0.6021	0.7167	0.0311	-0.1796	0.1941	0.1146	-03.917	028.39	019
-05.50	-0.8228	01.040	-0.7613	0.6780	0.6019	0.7137	0.0266	-0.1714	0.1930	0.1118	-03.840	028.43	020
-05.06	-0.7392	00.978	-0.6834	0.6624	0.5996	0.7120	0.0186	-0.1569	0.1924	0.1124	-04.020	028.56	021
-04.57	-0.6641	00.883	-0.6102	0.6515	0.6038	0.7122	0.0212	-0.1625	0.1930	0.1114	-04.065	028.65	022
-04.14	-0.5941	00.772	-0.5492	0.6421	0.6038	0.7123	0.0204	-0.1613	0.1933	0.1115	-03.947	028.68	023
-03.71	-0.5317	00.668	-0.4917	0.6335	0.6003	0.7106	0.0196	-0.1672	0.1951	0.1102	-03.816	028.72	024
-03.27	-0.4665	00.541	-0.4313	0.6283	0.6027	0.7114	0.0360	-0.1847	0.1945	0.1088	-03.524	028.72	025
-02.82	-0.4033	00.450	-0.3731	0.6229	0.6038	0.7120	0.0353	-0.1989	0.1943	0.1082	-03.386	028.59	026
-02.40	-0.3388	00.355	-0.3133	0.6157	0.6020	0.7113	0.0348	-0.1982	0.1937	0.1093	-03.188	028.52	027
-01.98	-0.2664	00.270	-0.2455	0.6109	0.6021	0.7111	0.0484	-0.2024	0.1935	0.1091	-03.084	028.46	028
-01.56	-0.2122	00.189	-0.1957	0.6064	0.6008	0.7099	0.0448	-0.1947	0.1927	0.1091	-02.705	028.46	029
-00.67	-0.1538	00.091	-0.1422	0.6031	0.6003	0.7095	0.0412	-0.1867	0.1916	0.1092	-01.822	028.49	030
-00.26	-0.0443	00.000	-0.0960	0.6014	0.6003	0.7112	0.0274	-0.1662	0.1905	0.1109	-00.020	028.56	031
00.18	0.0176	00.168	0.0157	0.6028	0.6026	0.7135	0.0343	-0.1643	0.1917	0.1109	06.058	028.56	032
00.60	0.0827	00.254	0.0764	0.6038	0.6030	0.7134	0.0339	-0.1489	0.1919	0.1108	28.951	028.52	033
01.04	0.1404	00.358	0.1294	0.6049	0.6025	0.7122	0.0293	-0.1263	0.1931	0.1092	09.323	028.49	034
01.49	0.1979	00.437	0.1822	0.6063	0.6014	0.7122	0.0284	-0.1246	0.1928	0.1093	07.738	028.52	035
01.90	0.2476	00.524	0.2275	0.6090	0.6012	0.7108	0.0060	-0.0962	0.1939	0.1108	06.702	028.52	036
02.32	0.3050	00.612	0.2803	0.6135	0.6017	0.7099	0.0315	-0.0809	0.1959	0.1082	06.092	028.59	038
02.79	0.3700	00.706	0.3403	0.6198	0.6026	0.7122	0.0178	-0.0839	0.1973	0.1096	05.793	028.59	039
03.22	0.4203	00.795	0.3958	0.6260	0.6034	0.7114	0.0169	-0.0824	0.1975	0.1080	05.747	028.56	040
03.61	0.4888	00.887	0.4500	0.6317	0.6021	0.7132	0.0091	-0.0897	0.1971	0.1111	05.515	028.59	041
04.05	0.5551	00.983	0.5109	0.6440	0.6003	0.7171	0.0116	-0.0953	0.1976	0.1108	05.383	028.52	042
04.52	0.6180	01.081	0.5684	0.6521	0.6054	0.7173	0.0107	-0.1085	0.1976	0.1120	05.313	028.46	043
04.92	0.6847	01.179	0.6305	0.6590	0.6025	0.7164	0.0164	-0.0984	0.1968	0.1139	05.229	028.56	044
05.37	0.7580	01.288	0.6980	0.6733	0.6050	0.7189	0.0120	-0.1122	0.1982	0.1139	05.161	028.56	045
05.83	0.8297	01.373	0.7638	0.6877	0.6066	0.7206	0.0075	-0.1116	0.1984	0.1140	05.011	028.59	046
06.27	0.9043	01.465	0.8472	0.7046	0.6079	0.7218	0.0032	-0.1119	0.1992	0.1139	04.914	028.56	047
06.75	1.0093	01.571	0.9260	0.7208	0.6069	0.7221	0.0059	-0.1331	0.1990	0.1152	04.751	028.52	048
07.19	1.0831	01.635	0.9990	0.7352	0.6044	0.7212	0.0117	-0.1245	0.1995	0.1168	04.586	028.56	049
07.62	1.1774	01.729	1.0864	0.7583	0.6074	0.7229	0.0104	-0.1025	0.2012	0.1155	04.462	028.59	050
08.09	1.2647	01.777	1.1666	0.7790	0.6071	0.7240	0.0095	-0.1245	0.2007	0.1169	04.270	028.59	051
08.56	1.3620	01.843	1.2566	0.8021	0.6062	0.7244	0.0017	-0.1552	0.2038	0.1182	04.111	028.56	052
09.00	1.4439	01.849	1.3312	0.8259	0.6076	0.7258	0.0037	-0.1409	0.2004	0.1182	03.891	028.56	053
09.36	1.5290	01.862	1.4100	0.8473	0.6047	0.7236	0.0055	-0.1333	0.2016	0.1169	03.699	028.59	054
09.67	1.6050	01.888	1.4801	0.8692	0.6083	0.7267	0.0057	-0.1357	0.2034	0.1184	03.573	028.59	055
09.90	1.6669	01.863	1.5375	0.8862	0.6087	0.7272	0.0105	-0.1225	0.2035	0.1185	03.596	028.62	056

HSWT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 015 MACH NO 2.010 RN/L 07040708 Q 1463 PSF TO 561

10/17/62

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
10.23	1.7272	-01.864	1.5916	0.9063	0.6093	0.7275	-0.0079	-0.1372	0.2070	0.1182	-03.279	028.56	057
10.66	1.8429	-01.818	1.6982	0.9407	0.6102	0.7282	-0.0138	-0.1249	0.2053	0.1179	-02.997	028.49	058
10.93	1.9151	-01.774	1.7645	0.9631	0.6110	0.7291	-0.0188	-0.1048	0.2043	0.1181	-02.814	028.52	059
11.03	1.9694	-01.760	1.8159	0.9774	0.6119	0.7301	-0.0233	-0.0986	0.2051	0.1182	-02.715	028.56	060
11.17	1.9857	-01.754	1.8297	0.9839	0.6108	0.7292	-0.0201	-0.1126	0.2033	0.1184	-02.683	028.59	061
11.18	2.0079	-01.724	1.8509	0.9908	0.6131	0.7314	-0.0170	-0.1199	0.2039	0.1184	-02.609	028.59	062
00.14	0.3747	-00.197	0.0732	0.6048	0.6046	0.7154	0.0231	-0.1360	0.1922	0.1112	-06.004	028.62	063

HSWT TEST 89

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 016 MACH NO 2.990 RN/L 08260977 Q 1429 PSF ID 581

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
30.16	-0.0021	-00.095	-0.0033	0.4506	0.4506	0.5269	-0.0069	-0.0108	0.1588	0.0763	39.707	057.46	006
-11.93	-2.2827	-00.913	-2.1414	0.9074	0.4452	0.5319	0.0894	-0.0904	0.1594	0.0867	01.215	057.27	007
-11.90	-2.2737	-00.893	-2.1331	0.9043	0.4450	0.5318	0.0826	-0.1217	0.1585	0.0867	01.193	057.40	008
-11.67	-2.2271	-00.858	-2.0911	0.8858	0.4444	0.5311	0.0852	-0.1366	0.1562	0.0867	01.170	057.33	009
-11.28	-2.1367	-00.803	-2.0088	0.8521	0.4427	0.5294	0.0755	-0.0869	0.1579	0.0867	01.142	057.33	010
-10.84	-2.0230	-00.735	-1.9039	0.8145	0.4424	0.5276	0.0696	-0.0965	0.1571	0.0852	01.104	057.33	011
-10.37	-1.8983	-00.673	-1.7838	0.7755	0.4417	0.5269	0.0665	-0.0829	0.1561	0.0852	01.079	057.33	012
-09.88	-1.7544	-00.573	-1.6529	0.7394	0.4402	0.5261	0.0492	-0.0801	0.1570	0.0868	00.992	057.46	013
-09.40	-1.6358	-00.496	-1.5419	0.7015	0.4402	0.5254	0.0462	-0.0595	0.1575	0.0852	00.921	057.40	014
-08.95	-1.5130	-00.409	-1.4262	0.6693	0.4393	0.5246	0.0399	-0.0623	0.1592	0.0852	00.821	057.33	015
-08.47	-1.3979	-00.332	-1.3176	0.6428	0.4418	0.5270	0.0303	-0.0653	0.1593	0.0852	00.722	057.40	016
-07.99	-1.2804	-00.238	-1.2065	0.6154	0.4417	0.5269	0.0274	-0.0449	0.1600	0.0852	00.564	057.27	017
-07.56	-1.1782	-00.147	-1.1096	0.5946	0.4435	0.5272	0.0265	-0.0537	0.1592	0.0838	00.379	057.40	018
-07.11	-1.0839	-00.083	-1.0202	0.5779	0.4473	0.5295	0.0252	-0.0325	0.1599	0.0822	00.233	057.33	019
-06.65	-0.9914	-00.028	-0.9332	0.5570	0.4451	0.5273	0.0139	-0.0353	0.1583	0.0822	00.087	057.33	020
-06.20	-0.8967	00.017	-0.8435	0.5377	0.4434	0.5267	0.0166	-0.0505	0.1582	0.0823	-00.059	057.46	021
-05.76	-0.8128	00.019	-0.7638	0.5265	0.4471	0.5264	0.0154	-0.0211	0.1575	0.0793	-00.071	057.40	022
-05.32	-0.7494	00.024	-0.7049	0.5138	0.4462	0.5256	0.0188	-0.0653	0.1597	0.0793	-00.096	057.46	023
-04.81	-0.6648	00.025	-0.6251	0.5002	0.4461	0.5253	0.0110	-0.0744	0.1550	0.0793	-00.115	057.40	024
-04.34	-0.6105	00.028	-0.5750	0.4903	0.4454	0.5217	0.0139	-0.0743	0.1552	0.0763	-00.141	057.40	025
-03.90	-0.5438	00.009	-0.5122	0.4817	0.4457	0.5235	0.0061	-0.0608	0.1545	0.0778	-00.049	057.46	026
-03.44	-0.4744	00.019	-0.4469	0.4715	0.4438	0.5216	0.0088	-0.0527	0.1534	0.0778	00.120	057.40	027
-03.01	-0.4114	00.031	-0.3875	0.4658	0.4448	0.5211	0.0084	-0.0678	0.1532	0.0763	00.228	057.46	028
-02.56	-0.3616	00.037	-0.3412	0.4642	0.4485	0.5233	0.0341	-0.0463	0.1527	0.0748	00.309	057.40	029
-02.11	-0.2992	00.058	-0.2826	0.4573	0.4466	0.5214	0.0002	-0.0694	0.1547	0.0748	00.586	057.40	030
-01.71	-0.2500	00.047	-0.2365	0.4569	0.4497	0.5244	0.0067	-0.0611	0.1550	0.0747	00.569	057.27	031
-01.26	-0.1956	00.052	-0.1857	0.4516	0.4474	0.5237	0.0060	-0.0536	0.1552	0.0763	00.808	057.33	032
-00.93	-0.1453	00.058	-0.1387	0.4494	0.4473	0.5236	0.0319	-0.0468	0.1554	0.0763	01.214	057.33	033
-00.37	-0.0914	00.063	-0.0884	0.4499	0.4494	0.5256	-0.0023	-0.0328	0.1572	0.0762	02.105	057.27	034
00.05	-0.0372	00.068	-0.0375	0.4484	0.4485	0.5263	0.0006	-0.0247	0.1565	0.0778	05.592	057.40	035
00.50	0.0049	00.059	0.0010	0.4474	0.4474	0.5237	-0.0769	-0.0188	0.1574	0.0763	-03.205	057.40	036
00.93	0.0665	00.073	0.0593	0.4511	0.4501	0.5264	-0.0079	-0.0111	0.1582	0.0763	-03.205	057.33	037
01.38	0.1126	00.085	0.1018	0.4539	0.4513	0.5262	-0.0122	-0.0116	0.1595	0.0749	-02.290	057.46	038
01.81	0.1624	00.073	0.1481	0.4547	0.4498	0.5246	-0.0133	-0.0044	0.1552	0.0748	-01.374	057.40	039
02.26	0.2201	00.077	0.2021	0.4604	0.4521	0.5269	-0.0217	-0.0166	0.1553	0.0748	-01.065	057.33	040
02.71	0.2741	00.091	0.2524	0.4648	0.4524	0.5272	-0.0189	-0.0126	0.1553	0.0748	-01.004	057.40	041
03.15	0.3238	00.096	0.2985	0.4693	0.4522	0.5270	-0.0201	-0.0099	0.1553	0.0748	-00.900	057.40	042
03.60	0.3861	00.116	0.3569	0.4775	0.4541	0.5274	-0.0141	-0.0039	0.1553	0.0733	-00.915	057.33	043
04.02	0.4406	00.130	0.4076	0.4860	0.4563	0.5295	-0.0222	-0.0023	0.1554	0.0733	-00.894	057.27	044
04.49	0.5096	00.165	0.4724	0.4937	0.4552	0.5300	-0.0267	-0.0134	0.1574	0.0748	-00.983	057.40	045
04.91	0.5783	00.164	0.5371	0.5044	0.4566	0.5315	-0.0280	-0.0212	0.1585	0.0749	-00.873	057.46	046
05.35	0.6635	00.173	0.6175	0.5218	0.4619	0.5367	-0.0298	-0.0068	0.1604	0.0748	-00.791	057.40	047
05.85	0.7327	00.174	0.6818	0.5341	0.4619	0.5367	-0.0241	-0.0135	0.1621	0.0748	-00.722	057.40	048
06.29	0.8070	00.168	0.7515	0.5483	0.4627	0.5390	-0.0361	-0.0235	0.1647	0.0763	-00.631	057.33	049
06.76	0.8919	00.150	0.8309	0.5666	0.4648	0.5411	-0.0235	-0.0514	0.1655	0.0763	-00.512	057.33	050
07.24	0.9864	00.104	0.9201	0.5844	0.4637	0.5415	-0.0294	-0.0306	0.1664	0.0778	-00.320	057.40	051
07.73	1.0882	00.049	1.0142	0.6057	0.4643	0.5421	-0.0348	-0.0623	0.1688	0.0778	-00.137	057.40	052
08.16	1.1919	00.024	1.1136	0.6312	0.4667	0.5445	-0.0362	-0.0700	0.1699	0.0778	00.062	057.27	053
08.68	1.3014	00.108	1.2157	0.6599	0.4690	0.5467	-0.0365	-0.0570	0.1704	0.0778	00.252	057.33	054
09.12	1.4144	00.209	1.3226	0.6853	0.4671	0.5479	-0.0490	-0.0380	0.1709	0.0808	00.450	057.40	055
09.55	1.5253	00.293	1.4264	0.7152	0.4686	0.5479	-0.0431	-0.0379	0.1715	0.0793	00.583	057.40	056

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 016 MACH NO 2.990 RN/L 08260977 Q 1429 PSF TO 581

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
09.85	1.6291	00.341	1.5246	0.7426	0.4709	0.5502	-0.0440	-0.0534	0.1715	0.3793	00.635	057.40	057
10.14	1.7116	00.409	1.6019	0.7654	0.4714	0.5522	-0.0445	-0.0842	0.1732	0.3808	00.726	057.46	058
10.46	1.7976	00.462	1.6817	0.7920	0.4735	0.5528	-0.0456	-0.0628	0.1739	0.3793	00.781	057.40	059
10.79	1.9085	00.529	1.7859	0.8235	0.4746	0.5539	-0.0576	-0.0284	0.1746	0.3793	00.842	057.40	060
11.21	2.0309	00.615	1.8991	0.8642	0.4785	0.5578	-0.0587	-0.0227	0.1749	0.3793	00.920	057.40	061
11.39	2.0960	00.646	1.9602	0.8832	0.4785	0.5578	-0.0595	-0.0158	0.1774	0.3793	00.937	057.40	062
11.41	2.1286	00.670	1.9897	0.8939	0.4798	0.5591	-0.0527	-0.0149	0.1769	0.3793	00.958	057.40	063
11.49	2.1458	00.649	2.0074	0.8959	0.4790	0.5583	-0.0638	0.0208	0.1767	0.3793	00.919	057.40	064
20.16	6.0589	-00.047	0.0577	0.4549	0.4547	0.5310	-0.0043	-0.0106	0.1555	0.0763	-02.439	057.33	065

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 017 MACH NO 2.990 RN/L 08177071 Q 1427 PSF TO 584

10/17/62

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PVT
10.50	1.8144	00.526	1.7011	0.7778	0.4547	0.5343	-0.0394	-0.0577	0.0075	0.3796	00.881	057.33	057
10.91	1.9240	00.592	1.8030	0.8113	0.4554	0.5350	-0.0402	-0.0588	0.0094	0.3796	00.935	057.26	058
11.25	2.0393	00.663	1.9125	0.8485	0.4597	0.5392	-0.0447	-0.0604	0.0131	0.3796	00.983	057.26	059
11.43	2.0904	00.697	1.9577	0.8655	0.4605	0.5401	-0.0418	-0.0377	0.0090	0.3796	01.012	057.33	060
11.47	2.1264	00.704	1.9926	0.8732	0.4597	0.5393	-0.0422	-0.0305	0.0103	0.3796	01.006	057.39	061
11.50	2.1520	00.702	2.0166	0.8825	0.4627	0.5408	-0.0425	-0.0304	0.0094	0.3781	00.990	057.33	062
11.51	2.1443	00.708	2.0094	0.8789	0.4607	0.5403	-0.0423	-0.0380	0.0099	0.3796	01.004	057.33	063
11.51	2.1580	00.737	2.0223	0.8842	0.4631	0.5411	-0.0354	-0.0448	0.0108	0.3781	01.038	057.26	064
00.14	0.0670	-00.063	0.0659	0.4370	0.4369	0.5135	-0.0150	-0.0021	0.0008	0.3766	-02.840	057.33	065

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 018 MACH NO 2.990 RN/L 08101905 Q 1427 PSF TO 588

10/17/62

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PVT
10.74	1.3549	03.932	1.2576	0.6607	0.3952	0.4688	-0.0202	-0.1130	0.0102	0.0736	08.815	057.33	057
11.10	1.4720	04.043	1.3682	0.6722	0.3963	0.4699	-0.0177	-0.1068	0.0096	0.0736	08.344	057.33	058
11.52	1.5746	04.182	1.4632	0.7053	0.3989	0.4740	-0.0222	-0.0727	0.0104	0.0751	08.068	057.26	059
11.69	1.6317	04.245	1.5167	0.7233	0.4013	0.4764	-0.0185	-0.1182	0.0113	0.0751	07.904	057.26	060
11.80	1.6619	04.269	1.5459	0.7304	0.4019	0.4771	-0.0225	-0.0821	0.0113	0.0752	07.804	057.39	061
11.81	1.6653	04.278	1.5481	0.7333	0.4012	0.4749	-0.0226	-0.0820	0.0104	0.0737	07.805	057.39	062
11.81	1.6711	04.292	1.5534	0.7357	0.4023	0.4760	-0.0188	-0.1041	0.0111	0.0737	07.803	057.46	063
10.20	0.0577	00.064	0.0064	0.3778	0.3776	0.4408	-0.0117	-0.0327	0.0003	0.0632	03.348	057.39	064

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

MUN 019 MACH NO 3.900 RN/L 11526396 Q 1454 PSF TD 590

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
11.51	1.2779	02.735	0.7412	2.4933	2.2930	0.3017	-0.0223	-0.0518	0.0064	-1.9913	06.766	173.27	108
11.54	1.5953	03.522	1.4946	0.6514	3.3364	0.3898	-0.0256	-0.0516	0.0093	0.3535	06.797	134.32	109
30.16	0.0364	00.032	0.0335	0.3074	0.3073	0.3549	-0.0138	-0.0613	-0.0026	0.0476	02.820	134.32	110

MSWT TEST 89

RUN 020 MACH NO 3.980 RN/L 11740779 Q 1451 PSF TO 583

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
00.26	0.0038	00.043	0.0022	0.3662	0.3661	0.4211	-0.0034	-0.0378	0.0003	0.0549	34.021	134.32	007
-11.55	-2.1687	-00.957	-2.0476	0.8086	0.3783	0.4406	0.0656	-0.0076	-0.0077	0.0623	01.341	134.32	008
-11.58	-2.1796	-00.968	-2.0575	0.8134	0.3795	0.4418	0.0660	-0.0222	-0.0069	0.0623	01.349	134.32	009
-11.27	-2.1064	-00.945	-1.9922	0.8085	0.3811	0.4418	0.0725	-0.0136	-0.0077	0.0608	01.353	134.32	010
-10.85	-2.0032	-00.913	-1.8971	0.7839	0.3764	0.4388	0.0845	-0.0157	-0.0085	0.0623	01.385	134.32	011
-10.38	-1.9907	-00.889	-1.7936	0.7017	0.3671	0.4293	0.0495	-0.0124	-0.0078	0.0623	01.428	134.32	012
-09.94	-1.7776	-00.873	-1.6867	0.6732	0.3721	0.4329	0.0543	-0.0341	-0.0071	0.0608	01.492	134.32	013
-09.46	-1.6615	-00.831	-1.5762	0.6371	0.3690	0.4298	0.0518	-0.0354	-0.0072	0.0608	01.519	134.32	014
-08.99	-1.5494	-00.781	-1.4729	0.6049	0.3674	0.4281	0.0459	-0.0300	-0.0074	0.0608	01.532	134.32	015
-08.51	-1.4266	-00.703	-1.3569	0.5717	0.3646	0.4254	0.0397	-0.0323	-0.0074	0.0608	01.498	134.67	016
-08.04	-1.3223	-00.631	-1.2582	0.5468	0.3655	0.4277	0.0269	-0.0287	-0.0069	0.0623	01.449	134.32	018
-07.58	-1.2146	-00.549	-1.1559	0.5218	0.3648	0.4256	0.0313	-0.0364	-0.0070	0.0608	01.373	134.32	019
-07.12	-1.1018	-00.507	-1.0483	0.4971	0.3633	0.4241	0.0234	-0.0390	-0.0066	0.0608	01.399	134.32	020
-06.69	-1.0063	-00.437	-0.9568	0.4809	0.3661	0.4269	0.0179	-0.0336	-0.0055	0.0608	01.319	134.98	021
-06.24	-0.9054	-00.381	-0.8602	0.4626	0.3665	0.4258	0.0168	-0.0347	-0.0055	0.0593	01.278	134.32	022
-05.76	-0.8223	-00.321	-0.7818	0.4431	0.3625	0.4233	0.0196	-0.0425	-0.0057	0.0608	01.186	134.32	023
-05.33	-0.7426	-00.287	-0.7058	0.4292	0.3618	0.4211	0.0151	-0.0366	-0.0046	0.0593	01.174	134.32	024
-04.84	-0.6664	-00.263	-0.6337	0.4152	0.3604	0.4197	0.0145	-0.0320	-0.0038	0.0593	01.197	134.32	025
-04.34	-0.6019	-00.232	-0.5728	0.4067	0.3621	0.4200	0.0068	-0.0393	-0.0042	0.0579	01.170	134.32	026
-03.87	-0.5332	-00.209	-0.5075	0.3972	0.3620	0.4184	0.0081	-0.0447	-0.0024	0.0564	01.191	134.32	027
-03.47	-0.4725	-00.188	-0.4499	0.3872	0.3593	0.4171	0.0055	-0.0480	-0.0029	0.0579	01.206	134.32	028
-03.01	-0.4112	-00.183	-0.3918	0.3817	0.3606	0.4155	0.0048	-0.0485	-0.0020	0.0549	01.353	134.32	029
-02.52	-0.3544	-00.162	-0.3382	0.3769	0.3616	0.4165	0.0046	-0.0631	-0.0020	0.0549	01.389	134.32	030
-02.09	-0.3020	-00.149	-0.2886	0.3703	0.3595	0.4144	0.0081	-0.0689	-0.0021	0.0549	01.504	134.32	031
-01.69	-0.2504	-00.120	-0.2396	0.3692	0.3620	0.4169	0.0046	-0.0880	-0.0023	0.0549	01.460	134.98	032
-01.22	-0.2016	-00.083	-0.1939	0.3643	0.3601	0.4165	0.0010	-0.0540	-0.0015	0.0564	01.245	134.32	033
-00.79	-0.1494	-00.061	-0.1443	0.3665	0.3645	0.4179	0.0043	-0.0452	-0.0008	0.0535	01.249	134.32	034
-00.34	-0.1051	-00.017	-0.1029	0.3643	0.3636	0.4186	0.0043	-0.0372	-0.0003	0.0549	00.480	134.32	035
00.10	-0.0567	00.004	-0.0574	0.3646	0.3647	0.4196	0.0041	-0.0217	-0.0007	0.0549	00.209	134.32	036
00.33	-0.0114	00.048	-0.0149	0.3669	0.3670	0.4204	0.0035	-0.0293	0.0003	0.0535	-12.693	134.32	037
00.99	0.0418	00.093	0.0355	0.3672	0.3660	0.4210	-0.0048	-0.0460	0.0007	0.0549	06.750	134.32	038
01.45	0.0873	00.128	0.0780	0.3672	0.3651	0.4200	-0.0027	-0.0389	0.0021	0.0549	04.467	134.32	039
01.88	0.1367	00.156	0.1245	0.3719	0.3676	0.4210	-0.0111	-0.0331	0.0011	0.0535	03.469	134.32	040
02.36	0.1863	00.184	0.1710	0.3754	0.3680	0.4215	-0.0124	-0.0484	0.0019	0.0535	02.994	134.32	041
02.79	0.2396	00.204	0.2215	0.3773	0.3661	0.4210	-0.0138	-0.0490	0.0027	0.0549	02.583	134.32	042
03.24	0.2967	00.216	0.2754	0.3852	0.3690	0.4225	-0.0119	-0.0414	0.0023	0.0535	02.215	134.32	043
03.66	0.3537	00.237	0.3293	0.3925	0.3707	0.4256	-0.0135	-0.0345	0.0026	0.0549	02.038	134.32	044
04.11	0.4175	00.242	0.3895	0.4034	0.3744	0.4279	-0.0150	-0.0347	0.0025	0.0535	01.764	134.67	045
04.54	0.4794	00.265	0.4483	0.4107	0.3739	0.4289	-0.0166	-0.0354	0.0032	0.0549	01.678	134.32	046
05.01	0.5516	00.297	0.5167	0.4225	0.3757	0.4306	-0.0220	-0.0366	0.0029	0.0549	01.638	134.32	047
05.46	0.6277	00.322	0.5888	0.4375	0.3795	0.4344	-0.0203	-0.0439	0.0025	0.0549	01.560	134.32	048
05.97	0.7055	00.373	0.6672	0.4514	0.3802	0.4351	-0.0224	-0.0448	0.0033	0.0549	01.604	134.67	049
06.42	0.7918	00.417	0.7442	0.4675	0.3814	0.4378	-0.0207	-0.0381	0.0030	0.0564	01.599	134.67	050
06.90	0.8780	00.478	0.8258	0.4846	0.3819	0.4383	-0.0329	-0.0269	0.0032	0.0564	01.653	134.67	051
07.38	0.9833	00.535	0.9261	0.5050	0.3818	0.4397	-0.0384	-0.0291	0.0038	0.0579	01.651	134.67	052
07.87	1.0962	00.601	1.0331	0.5312	0.3847	0.4411	-0.0335	-0.0316	0.0037	0.0564	01.666	134.67	053
08.33	1.2082	00.652	1.1390	0.5603	0.3894	0.4443	-0.0381	-0.0317	0.0049	0.0549	01.639	134.32	054
08.80	1.3210	00.727	1.2458	0.5872	0.3898	0.4462	-0.0320	-0.0321	0.0053	0.0564	01.673	134.32	055
09.26	1.4341	00.794	1.3524	0.6171	0.3915	0.4479	-0.0328	-0.0409	0.0058	0.0564	01.682	134.32	056
09.66	1.5395	00.851	1.4516	0.6463	0.3935	0.4499	-0.0441	-0.0223	0.0074	0.0564	01.680	134.32	057

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBLR 89

RUN 020 MACH ND 3.980 RN/L 11740779 Q 1451 PSF TD 583

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
09.98	1.6257	00.894	1.5328	0.6699	0.3941	0.4491	-0.0344	-0.0214	0.0072	0.0549	01.671	134.67	058
10.24	1.7093	00.914	1.6114	0.6950	0.3974	0.4538	-0.0387	-0.0153	0.0074	0.0564	01.624	134.32	059
10.50	1.7811	00.938	1.6783	0.7182	0.4003	0.4552	-0.0427	-0.0168	0.0089	0.0549	01.600	134.32	060
10.95	1.8822	00.950	1.7719	0.7499	0.3995	0.4544	-0.0364	-0.0164	0.0084	0.0549	01.533	134.67	061
11.28	1.9765	00.962	1.8594	0.7823	0.4035	0.4585	-0.0408	-0.0031	0.0090	0.0549	01.479	134.67	062
11.43	2.0218	00.981	1.9016	0.7970	0.4044	0.4594	-0.0376	-0.0176	0.0092	0.0549	01.473	134.67	063
00.19	0.0341	00.049	0.0329	0.3686	0.3685	0.4234	-0.0041	-0.0380	0.0003	0.0549	04.358	134.67	064

MSMT TEST 89

RUN 021 MACH NO 3.980 RM/L 11359327 Q 1451 PSF TO 595

10/17/62

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
-11.64	-2.1699	-00.883	-2.0470	0.8175	0.3876	0.4484	0.0950	-0.2028	0.1342	0.0608	01.236	133.98	008
-11.40	-2.1230	-00.872	-2.0044	0.8001	0.3881	0.4475	0.0834	-0.1897	0.1340	0.0593	01.247	134.32	009
-11.01	-2.0405	-00.854	-1.9295	0.7672	0.3845	0.4453	0.0816	-0.1899	0.1322	0.0608	01.271	134.32	010
-10.60	-1.9522	-00.827	-1.8483	0.7362	0.3838	0.4431	0.0761	-0.1693	0.1309	0.0593	01.286	133.98	011
-10.15	-1.8281	-00.808	-1.7325	0.6963	0.3802	0.4410	0.0664	-0.1489	0.1299	0.0608	01.342	133.98	012
-09.64	-1.7041	-00.772	-1.6168	0.6574	0.3772	0.4380	0.0569	-0.1508	0.1294	0.0608	01.377	133.98	013
-09.19	-1.5885	-00.713	-1.5078	0.6265	0.3775	0.4369	0.0540	-0.1299	0.1297	0.0593	01.363	133.98	014
-08.72	-1.4689	-00.661	-1.3949	0.5946	0.3763	0.4356	0.0478	-0.1168	0.1303	0.0593	01.367	133.98	015
-08.24	-1.3648	-00.596	-1.2972	0.5448	0.3730	0.4338	0.0382	-0.0898	0.1307	0.0608	01.326	133.98	016
-07.78	-1.2495	-00.536	-1.1876	0.4925	0.3718	0.4325	0.0321	-0.0911	0.1300	0.0608	01.303	134.32	017
-07.35	-1.1416	-00.470	-1.0847	0.5147	0.3717	0.4310	0.0296	-0.0775	0.1300	0.0593	01.251	134.32	018
-06.89	-1.0358	-00.413	-0.9837	0.4935	0.3719	0.4312	0.0182	-0.0800	0.1293	0.0593	01.212	134.32	019
-06.44	-0.9418	-00.350	-0.8941	0.4752	0.3720	0.4313	0.0206	-0.0653	0.1278	0.0593	01.130	134.32	020
-05.98	-0.8547	-00.314	-0.8114	0.4585	0.3715	0.4308	0.0127	-0.0597	0.1278	0.0593	01.117	134.32	021
-05.49	-0.7793	-00.247	-0.7405	0.4412	0.3683	0.4276	0.0122	-0.0895	0.1261	0.0593	00.965	134.32	022
-05.04	-0.6960	-00.229	-0.6608	0.4295	0.3698	0.4292	0.0147	-0.0745	0.1254	0.0593	01.000	134.32	023
-04.56	-0.6316	-00.198	-0.6002	0.4188	0.3697	0.4276	0.0141	-0.0820	0.1241	0.0593	00.953	134.32	024
-04.08	-0.5493	-00.181	-0.5216	0.4081	0.3699	0.4263	0.0135	-0.0970	0.1235	0.0564	00.998	133.98	025
-03.65	-0.4948	-00.168	-0.4704	0.3980	0.3672	0.4236	0.0128	-0.0820	0.1214	0.0564	01.033	134.32	026
-03.20	-0.4412	-00.165	-0.4201	0.3905	0.3665	0.4214	0.0159	-0.1035	0.1212	0.0549	01.138	134.32	027
-02.71	-0.3880	-00.154	-0.3702	0.3839	0.3660	0.4209	0.0119	-0.1041	0.1201	0.0549	01.203	134.32	028
-02.31	-0.3235	-00.148	-0.3083	0.3823	0.3696	0.4230	0.0077	-0.0976	0.1203	0.0535	01.389	134.32	029
-01.88	-0.2744	-00.129	-0.2622	0.3746	0.3658	0.4207	0.0072	-0.0980	0.1212	0.0549	01.425	134.32	030
-00.45	-0.2211	-00.100	-0.2119	0.3743	0.3690	0.4224	-0.0003	-0.0848	0.1213	0.0535	01.373	134.67	031
-00.95	-0.1788	-00.065	-0.1706	0.3706	0.3706	0.4241	-0.0026	-0.0777	0.1231	0.0535	01.116	134.32	032
-00.53	-0.1279	-00.037	-0.1244	0.3712	0.3701	0.4235	0.0020	-0.0708	0.1236	0.0535	00.886	134.32	033
-00.11	-0.0790	-00.010	-0.0783	0.3699	0.3699	0.4246	0.0015	-0.0639	0.1240	0.0549	00.370	134.32	034
00.35	-0.0264	00.027	-0.0286	0.3722	0.3724	0.4259	-0.0063	-0.0439	0.1258	0.0535	-03.165	134.32	035
00.80	0.0150	00.062	0.0098	0.3744	0.3742	0.4277	-0.0111	-0.0303	0.1249	0.0534	12.584	133.98	036
01.26	0.0641	00.090	0.0559	0.3752	0.3739	0.4273	-0.0124	-0.0309	0.1254	0.0535	04.247	134.32	037
01.72	0.1130	00.134	0.1018	0.3762	0.3730	0.4264	-0.0139	-0.0315	0.1244	0.0535	03.603	134.32	038
02.15	0.1654	00.154	0.1513	0.3792	0.3733	0.4267	-0.0154	-0.0172	0.1240	0.0535	02.825	134.67	039
02.60	0.2184	00.174	0.2012	0.3838	0.3743	0.4278	-0.0203	-0.0180	0.1227	0.0535	02.418	134.67	040
03.02	0.2643	00.201	0.2441	0.3896	0.3762	0.4297	-0.0216	-0.0187	0.1238	0.0535	02.311	134.32	041
03.47	0.3204	00.205	0.2970	0.3952	0.3765	0.4299	-0.0265	-0.0123	0.1245	0.0535	01.940	134.67	042
03.90	0.3810	00.218	0.3543	0.4047	0.3797	0.4331	-0.0245	-0.0195	0.1250	0.0535	01.736	134.67	043
04.37	0.4453	00.232	0.4151	0.4124	0.3795	0.4345	-0.0296	-0.0208	0.1264	0.0549	01.581	134.67	044
04.81	0.5109	00.246	0.4770	0.4239	0.3824	0.4373	-0.0279	-0.0209	0.1286	0.0549	01.466	134.32	045
05.28	0.5831	00.270	0.5452	0.4360	0.3840	0.4389	-0.0295	-0.0365	0.1311	0.0549	01.409	134.32	046
05.73	0.6548	00.303	0.6130	0.4495	0.3860	0.4409	-0.0350	-0.0234	0.1326	0.0549	01.407	134.32	047
06.18	0.7418	00.331	0.6958	0.4647	0.3881	0.4435	-0.0334	-0.0230	0.1344	0.0564	01.354	134.32	048
06.66	0.8341	00.394	0.7830	0.4861	0.3920	0.4469	-0.0318	-0.0252	0.1359	0.0549	01.434	133.98	049
07.15	0.9262	00.447	0.8703	0.5038	0.3916	0.4480	-0.0405	-0.0282	0.1377	0.0564	01.466	134.32	050
07.63	1.0279	00.495	0.9667	0.5256	0.3926	0.4476	-0.0425	-0.0224	0.1381	0.0549	01.462	134.32	051
08.09	1.1408	00.545	1.0741	0.5499	0.3933	0.4497	-0.0447	-0.0019	0.1384	0.0564	01.451	134.32	052
08.58	1.2575	00.613	1.1845	0.5783	0.3951	0.4515	-0.0492	0.0106	0.1391	0.0564	01.480	134.32	053
09.04	1.3665	00.687	1.2869	0.6080	0.3982	0.4532	-0.0536	0.0230	0.1399	0.0549	01.528	134.32	054
09.47	1.4719	00.735	1.3865	0.6344	0.3976	0.4540	-0.0578	0.0355	0.1411	0.0564	01.516	134.67	055
09.82	1.5696	00.773	1.4782	0.6632	0.4014	0.4563	-0.0658	0.0628	0.1398	0.0549	01.497	134.67	056
10.11	1.6490	00.809	1.5525	0.6872	0.4041	0.4590	-0.0632	0.0700	0.1408	0.0549	01.490	134.32	057
10.39	1.7281	00.826	1.6268	0.7097	0.4045	0.4595	-0.0641	0.0986	0.1408	0.0549	01.453	134.32	058

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 021 MACH NO 3.980 RN/L 11359327 Q 1451 PSF TO 595

10/17/62

COEFFICIENTS

ALPHA	N	PH	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
10.76	1.8148	00.854	1.7071	0.7377	0.4059	0.4594	-0.0684	0.1188	0.1428	0.0535	01.430	134.32	059
11.17	1.9247	00.870	1.8091	0.7734	0.4083	0.4632	-0.0727	0.1172	0.1443	0.0569	01.373	134.32	060
11.35	1.9964	00.885	1.8761	0.7971	0.4121	0.4656	-0.0666	0.1326	0.1447	0.0535	01.347	134.32	061
11.39	2.0252	00.891	1.9059	0.8041	0.4122	0.4657	-0.0667	0.1321	0.1443	0.0535	01.336	134.67	062
11.48	2.0493	00.897	1.9262	0.8119	0.4123	0.4673	-0.0741	0.1456	0.1451	0.0549	01.330	134.32	063
11.51	2.0532	00.898	1.9294	0.8149	0.4136	0.4671	-0.0774	0.1375	0.1454	0.0535	01.329	134.32	064
00.19	0.0418	00.034	0.0406	0.3757	0.3756	0.4290	-0.0075	-0.0367	0.1250	0.0535	02.466	134.67	065

MSWT TEST 89

10/23/62

CVO HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 022 MAOH NO 4.970 RN/L 16456655 Q 1465 PJF TO 594

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
00.27	0.0596	00.180	0.0579	0.3632	0.3629	0.4048	-0.0013	0.1853	0.1065	0.0419	09.174	301.33	006
-11.35	-1.9894	-00.937	-1.8765	0.7606	0.3766	0.4214	0.0486	-0.0584	0.1415	0.0448	01.431	300.63	007
-10.91	-1.9005	-00.928	-1.7996	0.7257	0.3728	0.4176	0.1411	-0.2425	0.1330	0.0448	01.483	300.98	008
-10.44	-1.8085	-00.883	-1.7114	0.6921	0.3706	0.4154	0.1390	-0.2289	0.1320	0.0448	01.483	300.98	009
-10.00	-1.7100	-00.878	-1.6202	0.6593	0.3680	0.4128	0.1304	-0.2163	0.1307	0.0448	01.560	300.63	010
-09.59	-1.5970	-00.861	-1.5142	0.6252	0.3652	0.4100	0.1105	-0.1688	0.1289	0.0448	01.638	300.98	011
-09.20	-1.4984	-00.848	-1.4224	0.5950	0.3635	0.4069	0.1052	-0.1681	0.1282	0.0433	01.720	300.63	012
-08.85	-1.4025	-00.819	-1.3320	0.5693	0.3625	0.4073	0.0993	-0.1206	0.1270	0.0448	01.775	300.63	013
-08.16	-1.3095	-00.815	-1.2450	0.5429	0.3606	0.4054	0.0871	-0.0939	0.1263	0.0448	01.890	300.63	014
-07.71	-1.2170	-00.778	-1.1577	0.5200	0.3599	0.4047	0.0749	-0.0822	0.1255	0.0448	01.941	300.63	015
-07.26	-1.1258	-00.741	-1.0713	0.4987	0.3593	0.4027	0.0732	-0.0910	0.1277	0.0434	02.001	300.29	016
-06.84	-1.0403	-00.688	-0.9898	0.4832	0.3619	0.4053	0.0604	-0.0352	0.1251	0.0433	02.011	300.63	017
-06.34	-0.9431	-00.650	-0.8976	0.4621	0.3602	0.4036	0.0421	-0.0027	0.1243	0.0433	02.094	300.63	018
-05.91	-0.8571	-00.606	-0.8193	0.4481	0.3617	0.4050	0.0380	-0.0041	0.1232	0.0433	02.148	300.63	019
-05.46	-0.7672	-00.578	-0.7293	0.4333	0.3620	0.4053	0.0370	0.0104	0.1196	0.0433	02.188	300.63	020
-04.97	-0.6883	-00.544	-0.6547	0.4159	0.3576	0.4009	0.0368	-0.0122	0.1182	0.0433	02.402	300.63	021
-04.49	-0.6169	-00.499	-0.5869	0.4068	0.3596	0.4030	0.0359	0.0093	0.1150	0.0433	02.436	300.98	022
-04.04	-0.5501	-00.464	-0.5231	0.4014	0.3635	0.4054	0.0287	0.0002	0.1133	0.0419	02.560	300.63	023
-03.58	-0.4903	-00.417	-0.4667	0.3931	0.3632	0.4051	0.0251	-0.0085	0.1117	0.0419	02.584	300.63	024
-03.09	-0.4227	-00.386	-0.4026	0.3838	0.3616	0.4035	0.0317	-0.0296	0.1099	0.0419	02.772	300.63	025
-02.65	-0.3591	-00.347	-0.3420	0.3781	0.3619	0.4038	0.0275	-0.0232	0.1083	0.0419	02.932	300.63	026
-02.19	-0.3026	-00.317	-0.2885	0.3728	0.3615	0.4019	0.0229	-0.0157	0.1075	0.0404	03.187	300.63	027
-01.76	-0.2468	-00.247	-0.2356	0.3687	0.3613	0.4032	0.0183	-0.0089	0.1077	0.0419	03.036	300.63	028
-01.33	-0.1908	-00.184	-0.1822	0.3699	0.3656	0.4061	0.0139	-0.0096	0.1091	0.0404	02.932	300.63	029
-00.89	-0.1460	-00.116	-0.1406	0.3683	0.3642	0.4046	0.0130	-0.0168	0.1103	0.0404	02.409	300.63	030
-00.42	-0.0977	-00.055	-0.0931	0.3598	0.3591	0.3995	0.0050	-0.0033	0.1108	0.0404	01.708	300.29	031
00.04	0.0338	00.009	0.0341	0.3582	0.3582	0.3987	0.0040	-0.0177	0.1115	0.0404	00.816	300.63	032
00.47	0.0101	00.095	0.0072	0.3592	0.3591	0.3996	-0.0001	-0.0125	0.1119	0.0404	28.419	300.29	033
01.37	0.1093	00.218	0.1006	0.3644	0.3635	0.4039	-0.0015	0.0301	0.1110	0.0404	07.760	300.63	034
02.32	0.2160	00.289	0.1493	0.3694	0.3670	0.4060	-0.0056	0.0281	0.1108	0.0390	06.059	300.63	035
02.83	0.2166	00.335	0.2016	0.3751	0.3667	0.4057	0.0107	0.0266	0.1111	0.0390	04.698	300.63	036
02.74	0.2687	00.381	0.2509	0.3775	0.3650	0.4055	0.0046	0.0320	0.1125	0.0404	04.303	300.29	038
03.20	0.3278	00.411	0.3069	0.3837	0.3660	0.4064	-0.0125	0.0514	0.1133	0.0404	03.806	300.63	039
03.62	0.3914	00.442	0.3674	0.3927	0.3687	0.4091	-0.0131	0.0281	0.1154	0.0404	03.430	300.63	040
04.08	0.4512	00.472	0.4237	0.4008	0.3697	0.4101	-0.0103	0.0219	0.1165	0.0404	03.179	300.63	041
04.56	0.5218	00.505	0.4908	0.4101	0.3697	0.4102	0.0115	0.0262	0.1173	0.0404	02.941	300.63	042
05.01	0.5963	00.530	0.5616	0.4277	0.3721	0.4125	-0.0129	0.0469	0.1195	0.0404	02.702	300.63	043
05.43	0.6749	00.565	0.6369	0.4316	0.3694	0.4113	-0.0139	0.0310	0.1203	0.0419	02.543	300.63	044
05.93	0.7608	00.595	0.7183	0.4485	0.3718	0.4137	-0.0256	0.0497	0.1218	0.0419	02.335	300.63	045
06.39	0.8477	00.620	0.8008	0.4688	0.3749	0.4153	-0.0245	0.0640	0.1239	0.0404	02.223	300.29	046
06.87	0.9491	00.633	0.8974	0.4899	0.3752	0.4156	-0.0272	0.0893	0.1242	0.0404	02.028	300.29	047
07.34	1.0315	00.676	0.9752	0.5031	0.3743	0.4162	-0.0328	0.0911	0.1244	0.0419	01.991	300.29	048
07.82	1.1313	00.705	1.0694	0.5276	0.3771	0.4176	-0.0311	0.1130	0.1249	0.0404	01.893	300.63	049
08.28	1.2325	00.718	1.1653	0.5512	0.3777	0.4181	-0.0431	0.1272	0.1256	0.0404	01.770	300.63	050
08.76	1.3352	00.740	1.2623	0.5758	0.3769	0.4188	-0.0413	0.1422	0.1259	0.0419	01.685	300.29	051
09.23	1.4426	00.746	1.3624	0.6098	0.3833	0.4237	-0.0462	0.1793	0.1282	0.0404	01.571	300.63	052
09.60	1.5362	00.758	1.4501	0.6382	0.3873	0.4278	-0.0444	0.2046	0.1301	0.0404	01.498	300.63	053
09.92	1.6227	00.768	1.5311	0.6645	0.3909	0.4313	-0.0455	0.2041	0.1319	0.0404	01.437	300.63	054
10.20	1.6940	00.783	1.5972	0.6891	0.3953	0.4343	-0.0464	0.2034	0.1345	0.0390	01.404	300.63	055
10.48	1.7639	00.781	1.6628	0.7083	0.3939	0.4344	-0.0438	0.1964	0.1370	0.0404	01.346	300.29	056

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 022 MACH NO 4.970 RN/L 16456655 Q 1465 P3F ID 594

10/23/62

COEFFICIENTS

ALPHA	N	PN	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
10.82	1.8442	00.790	1.7368	0.7364	0.3972	0.4376	-0.0555	0.2376	0.1368	0.0404	01.301	300.63	057
11.25	1.9379	00.810	1.8217	0.7753	0.4050	0.4425	-0.0535	0.2446	0.1421	0.0375	01.269	300.63	058
11.40	1.9945	00.788	1.8750	0.7918	0.4055	0.4445	-0.0577	0.2585	0.1436	0.0390	01.201	300.63	059
11.67	2.0249	00.803	1.9030	0.8022	0.4079	0.4469	-0.0546	0.2515	0.1442	0.0390	01.205	300.63	060
11.49	2.0380	00.798	1.9152	0.8085	0.4107	0.4482	-0.0551	0.2737	0.1449	0.0375	01.190	300.29	061
11.50	2.0432	00.799	1.9211	0.8063	0.4072	0.4461	-0.0515	0.2594	0.1449	0.0390	01.188	300.63	062
11.53	2.0609	00.770	1.9381	0.8103	0.4068	0.4443	-0.0553	0.2740	0.1448	0.0375	01.135	300.29	063
11.45	2.0639	00.962	1.9406	0.8155	0.4142	0.4445	-0.0346	0.2521	0.1538	0.0303	01.416	300.63	064
00.11	0.0377	00.050	0.0370	0.3591	0.3590	0.3995	-0.0108	-0.0430	0.1147	0.0404	03.996	300.29	065

MSMT TEST 89

10/23/62

CVD HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 023 MAOM NO 4-970 RN/L 16106908 Q 1465 PSF TD 602

COEFFICIENTS

ALPHA	M	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
00.29	0.0486	00.044	0.0467	0.3636	0.3634	0.4067	0.0197	-0.0480	0.0018	0.0433	02.728	300.63	006
-11.43	-1.9273	-00.942	-1.8184	0.7319	0.3570	0.4018	0.0970	-0.0081	0.0019	0.0448	01.484	300.63	007
-11.19	-1.8938	-00.931	-1.7900	0.7104	0.3495	0.3973	0.0837	0.0195	0.0012	0.0477	01.525	300.63	008
-10.80	-1.8181	-00.926	-1.7202	0.6851	0.3505	0.3968	0.0808	0.0112	0.0014	0.0463	01.548	300.29	009
-10.31	-1.7326	-00.916	-1.6414	0.6559	0.3498	0.3961	0.0755	0.0106	0.0001	0.0463	01.606	300.29	010
-09.90	-1.6338	-00.911	-1.5616	0.6241	0.3479	0.3942	0.0666	0.0166	-0.0008	0.0463	01.693	300.29	011
-09.46	-1.5300	-00.896	-1.4528	0.5895	0.3427	0.3889	0.0642	0.0164	-0.0010	0.0463	01.779	300.63	012
-09.00	-1.4254	-00.906	-1.3546	0.5596	0.3409	0.3857	0.0622	0.0092	-0.0015	0.0448	01.932	300.63	013
-08.53	-1.3368	-00.870	-1.2718	0.5330	0.3384	0.3832	0.0532	0.0148	0.0016	0.0448	01.977	300.63	014
-08.07	-1.2377	-00.866	-1.1778	0.5092	0.3387	0.3849	0.0513	0.0001	-0.0018	0.0463	02.125	300.29	015
-07.65	-1.1431	-00.836	-1.0886	0.4849	0.3376	0.3839	0.0528	-0.0142	0.0025	0.0463	02.221	300.63	016
-07.17	-1.0592	-00.776	-1.0085	0.4687	0.3391	0.3839	0.0473	-0.0229	-0.0016	0.0448	02.225	300.63	017
-06.73	-0.9701	-00.731	-0.9237	0.4498	0.3382	0.3829	0.0425	-0.0460	-0.0014	0.0448	02.290	300.63	018
-06.30	-0.8836	-00.578	-0.8412	0.4325	0.3376	0.3839	0.0344	-0.0257	-0.0023	0.0462	02.331	300.98	019
-05.82	-0.7933	-00.660	-0.7567	0.4186	0.3397	0.3860	0.0335	-0.0404	-0.0015	0.0463	02.521	300.29	020
-05.34	-0.7209	-00.610	-0.6861	0.4057	0.3401	0.3849	0.0361	-0.0400	-0.0021	0.0448	02.572	300.29	021
-04.86	-0.6413	-00.584	-0.6102	0.3936	0.3405	0.3853	0.0314	-0.0407	-0.0015	0.0448	02.746	300.63	022
-04.40	-0.5698	-00.543	-0.5421	0.3818	0.3390	0.3838	0.0341	-0.0403	-0.0013	0.0448	02.894	300.98	023
-03.93	-0.4997	-00.494	-0.4753	0.3715	0.3381	0.3829	0.0333	-0.0479	-0.0009	0.0448	03.006	300.63	024
-03.49	-0.4446	-00.449	-0.4229	0.3677	0.3413	0.3832	0.0327	-0.0482	-0.0018	0.0419	03.071	300.29	025
-03.00	-0.3768	-00.409	-0.3585	0.3600	0.3407	0.3826	0.0285	-0.0564	-0.0016	0.0419	03.297	300.63	026
-02.57	-0.3243	-00.373	-0.3087	0.3547	0.3406	0.3824	0.0246	-0.0431	-0.0009	0.0419	03.493	300.63	027
-02.13	-0.2712	-00.321	-0.2583	0.3514	0.3415	0.3820	0.0244	-0.0320	-0.0005	0.0404	03.593	300.63	028
-01.67	-0.2188	-00.281	-0.2087	0.3479	0.3417	0.3821	0.0243	-0.0319	-0.0001	0.0404	03.619	300.29	029
-01.22	-0.1576	-00.215	-0.1503	0.3442	0.3410	0.3821	0.0245	-0.0355	0.0003	0.0419	04.144	300.63	030
-00.77	-0.1163	-00.149	-0.1116	0.3462	0.3440	0.3851	0.0211	-0.0435	0.0009	0.0404	03.885	300.63	031
-00.34	-0.0630	-00.113	-0.0610	0.3447	0.3444	0.3848	0.0211	-0.0449	0.0009	0.0404	05.457	300.63	032
00.11	0.0215	00.047	0.0221	0.3467	0.3447	0.3852	0.0213	-0.0541	0.0013	0.0404	06.641	300.63	033
00.57	0.0262	00.014	0.0228	0.3427	0.3424	0.3829	0.0169	-0.0625	0.0024	0.0404	01.615	300.29	034
01.03	0.0813	00.083	0.0751	0.3446	0.3432	0.3837	0.0132	-0.0630	0.0025	0.0404	03.182	300.29	035
01.47	0.1364	00.165	0.1275	0.3490	0.3456	0.3846	0.0099	-0.0571	0.0037	0.0390	03.672	300.29	036
01.91	0.1801	00.233	0.1685	0.3514	0.3456	0.3846	0.0085	-0.0577	0.0046	0.0390	03.937	300.63	037
02.39	0.2317	00.279	0.2171	0.3541	0.3448	0.3852	0.0035	-0.0784	0.0044	0.0390	03.655	300.63	038
02.82	0.2872	00.317	0.2498	0.3602	0.3465	0.3855	0.0086	-0.0431	0.0058	0.0390	03.354	300.29	039
03.27	0.3501	00.356	0.3295	0.3699	0.3505	0.3895	0.0038	-0.0383	0.0064	0.0390	03.090	300.63	040
03.70	0.4087	00.386	0.3851	0.3774	0.3518	0.3908	0.0018	-0.0365	0.0060	0.0390	02.870	300.98	041
04.15	0.4574	00.418	0.4457	0.3851	0.3518	0.3908	-0.0031	-0.0318	0.0066	0.0390	02.685	300.63	042
04.61	0.5351	00.457	0.5050	0.3939	0.3520	0.3925	0.0018	-0.0361	0.0062	0.0390	02.596	300.63	043
05.09	0.6086	00.499	0.5748	0.4061	0.3535	0.3939	-0.0105	-0.0236	0.0064	0.0404	02.490	300.98	044
05.54	0.6810	00.535	0.6535	0.4199	0.3549	0.3953	-0.0093	-0.0159	0.0061	0.0404	02.350	300.63	045
06.02	0.7774	00.571	0.7358	0.4357	0.3562	0.3966	-0.0115	-0.0089	0.0065	0.0404	02.233	300.29	046
06.49	0.8586	00.605	0.8127	0.4524	0.3576	0.3981	-0.0167	-0.0107	0.0062	0.0404	02.148	300.98	047
06.95	0.9548	00.634	0.9042	0.4728	0.3600	0.4004	-0.0188	-0.0107	0.0060	0.0404	02.018	300.63	048
07.43	1.0403	00.678	0.9850	0.4920	0.3605	0.4010	-0.0207	-0.0040	0.0046	0.0404	01.980	300.98	049
07.91	1.1374	00.708	1.0770	0.5131	0.3601	0.4020	-0.0183	-0.0040	0.0056	0.0419	01.890	300.98	050
08.38	1.2360	00.730	1.1698	0.5394	0.3631	0.4035	-0.0193	-0.0043	0.0055	0.0404	01.794	300.63	051
08.84	1.3407	00.736	1.2685	0.5682	0.3666	0.4056	-0.0206	0.0172	0.0058	0.0390	01.668	300.63	052
09.29	1.4344	00.756	1.3566	0.5926	0.3660	0.4064	-0.0145	-0.0037	0.0057	0.0404	01.602	300.63	053
09.66	1.5282	00.777	1.4446	0.6201	0.3690	0.4094	-0.0153	-0.0188	0.0074	0.0404	01.544	300.63	054
09.97	1.6219	00.772	1.5333	0.6451	0.3699	0.4103	-0.0164	-0.0030	0.0068	0.0404	01.447	300.63	055
10.25	1.6798	00.810	1.5868	0.6650	0.3719	0.4109	-0.0168	-0.0123	0.0085	0.0390	01.446	300.29	056

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 023 MACH NO 4.97C H₂/L 161090R L 1465 PSF TO 602

10/23/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
10.51	1.7552	0.785	1.6575	0.6879	0.3741	0.4145	-0.0177	-0.0049	0.0088	0.0404	01.359	300.29	057
10.93	1.8430	0.812	1.7376	0.7218	0.3793	0.4183	-0.0185	-0.0128	0.0101	0.0390	01.339	300.63	058
11.28	1.9314	0.823	1.8192	0.7533	0.3830	0.4220	-0.0125	-0.0191	0.0100	0.0390	01.295	300.29	059
11.37	1.9778	0.825	1.8626	0.7699	0.3874	0.4249	-0.0200	0.0014	0.0099	0.0375	01.267	300.63	060
11.38	1.9967	0.829	1.9811	0.7729	0.3865	0.4240	-0.0167	-0.0052	0.0097	0.0375	01.282	300.63	061
11.46	2.0045	0.814	1.8880	0.7754	0.3848	0.4238	-0.0097	-0.0257	0.0097	0.0390	01.233	300.63	062
11.44	2.0115	0.832	1.8948	0.7784	0.3871	0.4261	-0.0135	0.0026	0.0095	0.0390	01.257	300.63	063
11.25	1.9915	0.837	1.8773	0.7703	0.3894	0.4283	-0.0166	-0.0053	0.0098	0.0390	01.277	300.29	064
00.22	0.0640	00.005	0.0627	0.3498	0.3496	0.3886	0.0128	-0.0270	0.0008	0.0390	00.255	300.63	065

HSMT TEST 89

CV6 HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 024 MAGH NO 4.970 RN/L 16399013 Q 1465 PSF TD 596

10/23/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
11.24	1.5327	03.318	1.4388	0.6237	0.3314	0.3689	-0.0016	-0.0008	0.0119	0.0375	06.577	300.63	108
11.44	1.5651	03.359	1.4686	0.6370	0.3331	0.3692	-0.0055	0.0053	0.0111	0.0361	06.517	300.63	109
11.63	1.6320	03.432	1.5311	0.6569	0.3349	0.3710	-0.0027	0.0118	0.0115	0.0361	06.389	300.63	111
11.66	1.6949	03.437	1.5525	0.6634	0.3359	0.3734	-0.0030	0.0117	0.0114	0.0375	06.311	300.63	112
11.72	1.6617	03.463	1.5588	0.6662	0.3356	0.3731	0.0040	-0.0022	0.0118	0.0375	06.332	300.63	113
11.75	1.6729	03.457	1.5691	0.6712	0.3376	0.3737	0.0037	0.0053	0.0113	0.0361	06.279	300.63	114
11.78	1.6803	03.459	1.5762	0.6736	0.3376	0.3737	-0.0031	0.0039	0.0117	0.0361	06.254	300.63	115
11.78	1.6767	03.467	1.5722	0.6741	0.3390	0.3750	0.0039	-0.0094	0.0113	0.0361	06.281	300.63	116
11.78	1.6786	03.471	1.5740	0.6750	0.3394	0.3755	0.0004	-0.0028	0.0115	0.0361	06.281	300.29	117
11.78	1.6729	03.474	1.5691	0.6700	0.3356	0.3731	0.0006	-0.0102	0.0110	0.0375	06.309	300.63	118
11.78	1.6803	03.459	1.5755	0.6768	0.3409	0.3770	0.0037	-0.0019	0.0108	0.0361	06.253	300.63	119
00.23	0.0391	00.097	0.0578	0.3115	0.3112	0.3473	-0.0052	0.0123	0.0016	0.0361	04.974	300.29	020

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 025 MACH NO 4.970 R/V/L 17345449 U 1463 PSF TD 576

10/23/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AR	CP	PO	PNT
11.42	1.0129	02.374	0.9370	0.4752	0.2802	0.3536	-0.0239	-0.0032	0.0076	0.0734	07.122	299.94	116
07.02	0.6048	01.633	0.5677	0.3988	0.2668	0.3402	-0.0163	-0.0024	0.0038	0.0734	08.204	300.29	108
00.22	0.0448	00.041	0.0437	0.2671	0.2669	0.3361	-0.0045	0.0080	0.0003	0.0692	02.774	299.94	119

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUM 026 MACH NO 3.980 RN/L 21848648 Q 2504 PSF TO 556

HSWT TEST 89

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PNT
10.88	0.8982	02.269	0.8285	0.4483	0.2839	0.3712	0.0025	-0.0402	0.0048	0.0874	07.675	230.86	108
11.06	0.9242	02.304	0.8525	0.4562	0.2843	0.3729	0.0045	-0.0413	0.0048	0.0886	07.575	230.86	109
11.29	0.9463	02.353	0.8721	0.4651	0.2854	0.3728	0.0026	-0.0424	0.0046	0.0874	07.554	231.21	110
11.47	0.9736	02.392	0.8971	0.4746	0.2867	0.3741	0.0086	-0.0436	0.0049	0.0874	07.663	230.86	111
11.62	0.9928	02.438	0.9166	0.4810	0.2869	0.3755	0.0087	-0.0448	0.0048	0.0886	07.461	230.86	112
11.72	1.0058	02.461	0.9285	0.4854	0.2871	0.3757	0.0046	-0.0454	0.0050	0.0886	07.435	230.86	113
11.78	1.0202	02.483	0.9399	0.4904	0.2882	0.3768	0.0107	-0.0460	0.0048	0.0886	07.393	230.51	114
11.81	1.0272	02.497	0.9466	0.4915	0.2873	0.3768	0.0105	-0.0412	0.0050	0.0874	07.384	230.86	115
11.85	1.0337	02.508	0.9539	0.4923	0.2862	0.3768	0.0126	-0.0465	0.0054	0.0886	07.372	230.86	116
11.87	1.0375	02.506	0.9558	0.4963	0.2890	0.3764	0.0106	-0.0416	0.0055	0.0874	07.339	230.51	117
11.88	1.0373	02.518	0.9566	0.4963	0.2890	0.3764	0.0126	-0.0418	0.0051	0.0874	07.374	230.51	118
11.87	1.0368	02.518	0.9555	0.4944	0.2872	0.3758	0.0106	-0.0466	0.0053	0.0886	07.371	230.17	119
11.90	1.0345	02.521	0.9528	0.4952	0.2881	0.3767	0.0106	-0.0419	0.0055	0.0886	07.405	230.17	120
00.14	0.0275	00.013	0.0268	0.2756	0.2755	0.3577	0.0049	-0.0087	0.0001	0.0822	01.418	221.49	121

MSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 027 MACH NO 2.990 RN/L 14158488 Q 2457 PSF TO 582

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
11.70	1.0432	02.608	0.9584	0.5161	0.3111	0.4467	0.0066	-0.0719	0.0045	0.1357	07.594	098.92	112
11.79	1.0536	02.630	0.9675	0.5217	0.3131	0.4488	0.0065	-0.0624	0.0039	0.1356	07.583	098.75	113
11.76	1.0601	02.642	0.9735	0.5251	0.3156	0.4500	0.0066	-0.0629	0.0043	0.1344	07.571	098.75	114
11.85	1.0712	02.648	0.9839	0.5271	0.3138	0.4494	0.0085	-0.0580	0.0042	0.1356	07.510	098.75	115
11.85	1.0752	02.659	0.9878	0.5280	0.3138	0.4494	0.0146	-0.0632	0.0043	0.1356	07.512	098.58	114
11.86	1.0774	02.665	0.9898	0.5294	0.3147	0.4503	0.0085	-0.0633	0.0039	0.1356	07.513	098.58	117
11.85	1.0693	02.649	0.9823	0.5258	0.3128	0.4485	0.0065	-0.0631	0.0048	0.1357	07.527	098.92	118
11.85	1.0711	02.660	0.9839	0.5270	0.3136	0.4492	0.0086	-0.0684	0.0047	0.1356	07.543	098.75	119
00.14	0.0315	00.001	0.0307	0.3183	0.3182	0.4400	0.0015	-0.0298	-0.0009	0.1218	00.089	098.75	120

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89
 RUN 028 MACH NO 2.010 RM/L 11010401 Q 2436 PSF TD 586 MSMT TEST 89

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
11.13	0.7747	02.480	0.6877	0.5173	0.3748	0.5773	0.0145	-0.0524	0.0031	0.2025	09.724	047.55	108
11.37	0.7885	02.535	0.7001	0.5179	0.3698	0.5738	0.0186	-0.0486	0.0030	0.2040	09.769	047.61	109
11.47	0.8159	02.586	0.7261	0.5242	0.3693	0.5748	0.0185	-0.0497	0.0028	0.2055	09.628	047.68	110
11.57	0.8276	02.631	0.7362	0.5308	0.3724	0.5777	0.0186	-0.0457	0.0030	0.2053	09.656	047.61	111
11.63	0.8429	02.666	0.7514	0.5301	0.3676	0.5742	0.0186	-0.0467	0.0040	0.2065	09.610	047.61	112
11.64	0.8474	02.674	0.7549	0.5353	0.3720	0.5769	0.0185	-0.0415	0.0032	0.2049	09.585	047.48	113
11.69	0.8495	02.691	0.7572	0.5331	0.3686	0.5748	0.0187	-0.0522	0.0032	0.2062	09.624	047.48	114
11.72	0.8516	02.703	0.7591	0.5330	0.3676	0.5738	0.0208	-0.0525	0.0033	0.2062	09.643	047.48	115
11.75	0.8549	02.705	0.7621	0.5348	0.3687	0.5751	0.0208	-0.0576	0.0030	0.2063	09.614	047.55	116
11.76	0.8589	02.716	0.7649	0.5402	0.3729	0.5797	0.0226	-0.0426	0.0034	0.2047	09.606	047.68	118
00.11	0.0271	00.007	0.0263	0.3916	0.3916	0.5584	0.0099	-0.0204	-0.0020	0.1888	00.742	047.48	119

HSMT TEST 89

CVC HIGH SPEED WIND TUNNEL TEST NUMBER 89

RUN 029 MACH NO 0.605 RM/L 08528337 Q 1131 PSF TO 582

10/17/62

COEFFICIENTS

ALPHA	N	PM	L	D	A	AU	Y	YM	RM	AB	CP	PO	PMT
09.99	1.8840	-05.483	1.7927	0.6833	0.3621	0.3704	0.0058	-0.0122	0.0148	0.0083	-08.842	039.18	057
10.32	1.9816	-05.765	1.8866	0.7115	0.3622	0.3687	-0.0145	0.0000	0.0137	0.0045	-08.839	039.18	058
10.48	2.0116	-05.911	1.9124	0.7207	0.3610	0.3674	0.0021	-0.0124	0.0144	0.0064	-08.826	039.21	059
10.53	1.9906	-05.809	1.8921	0.7133	0.3554	0.3611	0.0025	0.0135	0.0164	0.0057	-08.865	039.18	060
10.55	2.0740	-06.090	1.9739	0.7292	0.3554	0.3663	-0.0175	0.0348	0.0148	0.0110	-08.920	039.21	061
10.58	1.9573	-05.761	1.8591	0.7070	0.3535	0.3556	-0.0148	0.0014	0.0156	0.0021	-08.941	039.34	062
10.32	1.9106	-05.574	1.8156	0.6945	0.3579	0.3555	-0.0097	-0.0342	0.0144	-0.0024	-08.862	039.88	063
00.05	0.0057	-00.021	0.0054	0.3797	0.3796	0.3758	0.0090	-0.0457	0.0012	-0.0038	-11.290	038.92	064
00.07	-0.0095	-00.003	-0.0099	0.3794	0.3794	0.3781	0.0232	-0.0641	0.0033	-0.0013	00.925	038.56	065

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1. Simon, E. H. Static Stability Tests on a 0.098 Scale Scout Derivative Model in the Mach Number Range of 0.6 through 5.0, CVC Report 2-59710/2R653 dtd 18 Jan 62.
2. HSWT Staff. High Speed Wind Tunnel Handbook, CVC Report AER-EIR-13552 dtd Sep 62.
3. Wolfe, J. A. Data Reduction Procedures for Typical Force Tests at the Chance Vought High Speed Wind Tunnel, CVC Report AER-EOR-12978 dtd Jun 60.

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	<p>from -10 to +10 degrees in the pitch plane. The results obtained were force and moment data in the body axes; these results are presented in tabulated form with selected coefficients presented in plotted form.</p> 		<p>from -10 to +10 degrees in the pitch plane. The results obtained were force and moment data in the body axes; these results are presented in tabulated form with selected coefficients presented in plotted form.</p> 
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