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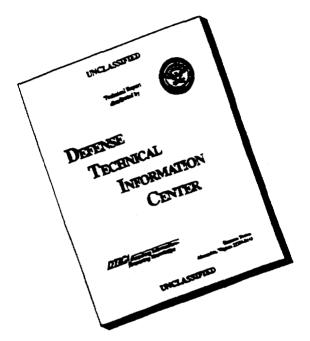
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CRITERIA FOR INCAPACITATING SOLDIERS WITH FRAGMENTS AND FLECHETTES (U)

By William Kokinakis Joseph Sperrazza

JANUARY 1965



U. S. ARMY MATERIEL COMMAND
BALLISTIC RESEARCH LABORATORIES
ABERDEEN PROVING GROUND, MARYLAND

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BALLISTIC RESEARCH LABORATORIES

REPORT NO. 1269

JANUARY 1965

CRITERIA FOR INCAPACITATING SOLDIERS WITH FRAGMENTS AND FLECHETTES (U)

William Kokinakis Joseph Sperrazza

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BALLISTIC RESEARCH LABORATORIES

REPORT NO. 1269

WKokinakis/JSperrazza/mec Aberdeen Proving Ground, Md. January 1965

CRITERIA FOR INCAPACITATING SOLDIERS WITH FRAGMENTS AND FLECHETTES (U)

(CONFIDENTIAL)

ABSTRACT

Presented are estimates of the conditional probabilities, P_{hk} that single, random hits with a standard series of homologously shaped, steel flechettes, which tumble within a soldier, will incapacitate the soldier. The functional dependence of P_{hk} on the weight, m of the flechette and its initial striking velocity, v_{o} is given by

$$P_{hk} = 1 - e^{-a(mv_0^{3/2} - b)^n}$$

where e is the base of the natural logarithm and a, b and n are parameters whose values are determined from the tactical situation and time at which the incapacitation is to ensue. The analysis was based on experimental data produced by the Biophysics Division, Medical Directorate, Chemical Research and Development Laboratories (CRDL), Edgewood Arsenal.

The Edgewood experiments demonstrate that within "ballistic" simulants of the human anatomy; i.e., gelatin or goats, relatively quick tumbling occurs with the standard series of flechettes for striking velocities greater than 3000 fps. It is suggested that the weight of the flechette should not exceed about 13 grains else the tumbling will occur too late after entrance and that only a small portion of the flechette's energy will be deposited within the target.

Also presented are estimates of the conditional probability that single, random hits with chunky (spheres or cubes), steel fragments will incapacitate a soldier. Although these latter criteria appear in other Ballistic Research Laboratories (BRL) publications, they are included for purposes of consolidation.

(UNCLASSIFIED)

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A NOTE ON CLASSIFICATION

The plan of the experiments, including the types of targets used, is CONFIDENTIAL. The functional dependence of P_{nk} or the variables m and v_{o} and <u>unspecified numerical values</u> of the parameters a, b, n is classified CONFIDENTIAL; on the other hand, when numerical values are given for a, b, n the relation is classified SECRET.

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INTRODUCTION

The U. S. Army program on wound ballistics was started about 1950 as a cooperative effort among three, then Army Technical Services:

Ordnance Corps, Chemical Corps and Medical Services. Its main purpose was, and still is, to develop casualty criteria for infantry soldiers struck by penetrating missales such as unstabilized fragments, bullets and arrow-like missales termed flechettes. Presently the program is continuing under auspices of the Army Materiel Command, with the cooperation of the Medical Services.

The study involves two distinct phases: (1) the conduct of appropriate experiments and the assessment of hypothetical wounds in terms of incapacitation — this phase is carried out by the Biophysics Division, CRDL, Edgewood Arsenal, and (2) the formulation of criteria for incapacitation in terms of missile parameters — this phase is carried out by the BRL. The reader is referred to BRL Report No. 996^{1*}, dated October 1956 for a general description of the work and for the formulation of the earlier criteria that were developed for chunky steel fragments **. Those criteria were based on experiments with 0.85-grain spheres and 2.0- and 16.0-grain cubes.

In BRL Report No. 996, the dependence of P_{hk} on the weight (m) and striking velocity (v_o) for steel fragments was found to be as follows:

$$P_{hk} = 1 - e^{-a(mv_0^{3/2}-b)^n}$$

where m is weight of fragment, \mathbf{v}_0 is the striking velocity, e the base of the natural logarithm and a, b and n are parameters whose values

Superscript numbers denote references found on page 28.

The steel fragments are presumed to be generic to those generated by the detonation of high explosive shell.

depend on time after wounding and tactical role. Reported were values of a, b and n associated with each of four tactical roles and seven post-wounding times. However, of the total of 28 combinations, four had been selected as being represent tive of all of them:

Case	Standard	Representative of
1	Defense ≤ 30 Seconds	Defense ≤ 30 Seconds
2	Assault ≤ 30 Seconds	Assault ≤ 30 Seconds Defense ≤ 5 Minutes
3	Assault ≤ 5 Minutes	Assault ≤ 5 Minutes Defense ≤ 30 Minutes Defense ≤ 12 Hours
14	Supply ≤ 12 Hours	Supply ≤ 12 Hours Supply ≤ 24 Hours Supply ≤ 5 Days Reserve ≤ 30 Minutes Reserve ≤ 12 Hours Reserve ≤ 24 Hours

The effectiveness of weapons of the artillery type are evaluated, in general, using the criterion for Case 3 and weapons of the personal type (rifles, hand grenades, etc.) are evaluated using the criterion for Case 1.

Data obtained later with a 225-grain steel cube were in accord with the general rules proposed in BRL Report No. 996.

Subsequent reevaluations of all previous medical assessments of the incapacitating potential of the steel fragments resulted in revised criteria which were published in BRL Technical Note No. 12973. However, the main purpose of that note was to suggest tentative criteria of the incapacitating potential of an homologous series of steel flechettes pending the completion of experiments with the homologous series 4,5,6.

^{*} The four significant tactical roles considered in this study are described in Appendix A.

The provisional estimates of the wounding potential of the flechettes were restricted to those that remained stable in the simulants of human targets (gelatin or goats); it was observed that when the striking velocity was less than about 3000 fps, tumbling within target did not occur whereas if the striking velocity exceeded 3000 fps, the flechette tumbled relatively quickly and deposited more energy in the target than did the more stable flechette, and therefore produced grosser wounds.

It is the purpose of the present study to report the casualty criteria for tumbling flechettes and to include, under one cover, the latest criteria for fragments and non-tumbling flechettes. (This publication supersedes and/or compliments casualty criteria previously published in the following BRL Reports: Report No. 996¹, Technical Note Nos. 1297³, 1235⁷, 1437⁸, and 1486¹⁰, and Memorandum No. 1420⁹.) The criteria pertain to single, random hits averaged over the whole body or averaged over the major separate parts of the anatomy such as the head and neck, thorax, abdomen, pelvis, and arms and legs. The latter breakdown should be useful to designers of body armor, helmets, and other protective devices.

(CONFIDENTIAL) EXPERIMENTAL PROCEDURE

For each combination of missile and striking velocity the procedure for establishing the size (depth and lateral extent) of a hypothetical wound tract in a soldier first involves firing the missile into different types of anatomical components of goats. Measurements are made of the retardation in velocity of the missile while penetrating different thicknesses of the components. Supplementary experiments include the determinations of physical damage to especially critical components. In general, the tissue models are obtained from Angora goats. However, human skulls and limbs are occasionally used for the experiments. Firings are also made into whole, live goats and complete descriptions of each wound tract are obtained by autopsy. All these data serve as inputs to

To account for protection that could be offered by clothing, body armor, etc., retardation firings are also carried out with such materials.

medical assessors who then estimate physiological effects in soldiers subjected to the many hypothetical wounds that could arise from random strikes. It is the purpose of the remainder of this section to describe briefly the assessing technique.

To aid in the identification of the various tissue and organs that lie in the many different paths of a missile's trajectory (wound tract), and to combine these structures with degree of traumatic damage a "bookkeeping" procedure was set up, as typified by the example illustrated in Table I. The combinations of anatomical components struck and the degree of damage are called "wound classes".

TABLE I

(UNCLASSIFIED) Typical Wound Classes

Symbol	Description
B ₂	SKULL; severe fragmentation or depressed fracture
$B_{a7}V_{2}$	BONE; with concurrent cardiovascular wound
$B_{L1}V_{1}$	BONE; with concurrent cardiovascular wound
H	HAND; any wound at this velocity
K ₂	URETER, URETHRA and URINARY BLADDER; puncture wound with leakage
NaV2	NERVE; with concurrent cardiovascular damage
P ₇	LUNG; puncture with small blood loss

The reader is referred to the referenced CRDL Reports 4, 5, and 6 for a complete description of the procedure.

In Table I, the subscript 2 of B_2 denotes severity of the bone wound. The subscript L of $B_{Ll}V_l$ denotes bone damage affecting the legs and V identifies it as a combination wound involving vascular damage as well. The subscript l of V_l indicates the degree of incapacitation and is based on vascular size, location of vessel and wound size. And so on until there are described all the possible wound classes that a specific missile can produce. The number of wound classes varies with the type, weight, and striking velocity of missile.

The next step in the procedure is to relate wound classes with the decrement in task performance of the soldier. Because of the intimate dependence of performance on the behavior of the limbs, incapacitation arbitrarily was related to behavior of the limbs. Table II lists a total of 16 disability (or functional groups) which consider different combinations of limb deficits that can occur from practical considerations. The deficit either could be one in which loss of fine muscular coordination of a limb occurs or one in which total loss of the limb occurs. A limb need not necessarily be hit to become disabled. For example, a hit on certain parts of the spinal cord could render all extremities inoperable.

Of crucial significance to the study are the judgments made by the medical assessors on the relationships between behavior of the limbs and the ability of the wounded "enemy" soldier to carry out his assigned task. Table III represents the best estimates of these relationships and are based on a consensus of opinion of medical assessors and of combat personnel. Each discrete level of disability refers to, "on the average", the decrease in effectiveness of the enemy soldier. Some of the readers of this report might wish to defer reading the next several pages and turn to subsequent paragraphs which define the term $P_{\rm hk}$ (page 16).

Only six discrete post-wounding times ranging from one-half a minute to five days are considered in the assessments. Generally, as post-time wounding increases, the deleterious effects of a wound accumulate and the wound is assigned to a functional group associated with a higher level of incapacitation.

Some examples of the change in functional group with time are given in Table V. Table V is illustrative only and applies to a 7.2-grain steel flechette striking the bare skin of the "enemy" soldier at a velocity of 2000 fps. There are very few exceptions to the cumulative effects of the wound. For instance, let us examine wound class $B_{a7}^{\ V}_2$. After 24 hours, this wound class falls into Functional Group XIII which rates 100% incapacitation for all tactical roles; but at five days this wound class falls into Functional Group VIII, which rates 75% incapacitation for three of the four tactical roles. The significance here is that the wound, if left unattended would start to heal after 24 hours.

(UNCLASSIFIED) The Relation Between Functional Group and Behavior of Each Extremeity

Functional Group	Arms*	Legs*
I	N,N	N,N
II	N,N	N,F
III	N,N	F,F
IV	N,N	N,T
V	N,N	T,T
VI	N,F	N,N
VII	F,F	N,N
VIII	N,T	N,N
IX	T,T	N,N
X	F,F	F,F
XI	F,F	F,T
XII	F,F	T,T
XIII	F,T	F,F
XIV	T,T	T,T
VX	N,N	F,T
XVI	N,F	F,F

TABLE II

Code: N No effect on extremity

F Loss of fine muscular coordination (weakness) of extremity

T Total loss of extremity function
* No attempt is made to differentiate between the right and left limbs

TABLE III

(CONFIDENTIAL) Fercent Disability Vs. Functional Group for Four Tactical Situations (U)

	Each *	Functional		Percent Di	sability	
Arm	Leg	Groups	<u>Assault</u>	<u>Defense</u>	Reserve	Supply
N,N	N,N	I	0	0 '	0	. 0
N,N	N,F	II	50	25	75	25
N,N	F,F	III	75	25	100	50
N,N	N,T	IV	100	50	100	100
N,N	T,T	Λ	100	50	100	100
N,F	N,N	VI	50	25	75	25
F, F	N,N	VII .	75	50	100	50
N,T	N,N	VIII	75	75	100	75
T,T	N,N	IX	100	100	100	100
F,F	F,F	X	75	75	100	75
$\mathbf{F}_{,\bullet}\mathbf{F}$	F,T	XI	100	75	100	100
F,F	T,T	XII	100	75	100	100
F,T	F,F	XIII	100	100	100	100
T,T	T,T	XIV	100	100	100	100
N,N	F,T	VX	100	50	100	100
N,F	F,F	XVI	75	50	100	75

Codes: N No effect

F Loss of fine muscular coordination

T Total loss of extremity function

^{*} No attempt is made to differentiate between the right and left limbs.

Table IV is a rearrangement of Table III.

TABLE IV

(CONFIDENTIAL) Functional Groups Vs. Percent Disability for Four Tactical Situations (U)

Percent	Functional Group						
Disability	Assault	Defense	Reserve	Supply			
0	I	I	I .	I			
25	-	II,III,VI	_	II,VI			
50	II,VI	IV,V,VII XV,XVI	. -	III, VII			
75	III,VII,VIII,	VIII,X,XI, XII	II,VI	VIII, X,XVI			
100	IV,V,IX,XI, XII,XIII,XIV, XV	IX,XIII, XIV	III,IV,V, VII,VIII, IX,X,XI, XII,XIII, XIV,XV,XVI	IV,V, IX,XI, XII, XIII, XIV,XV			

TABLE V

(C) Effect of Post-Wounding Time on Assignment of Functional Group (U)

				Functi	onal Gr	oup	
Wound	Description	30	5	30	12	24	5 .
Class		sec.	min.	min.	hr.	hr.	days
B ₂	SKULL; severe fragmentation, or depressed fracture	XIV	XIV	XIV	XIV	XIV	XIV
B _{a7} V ₂	BONE; with concurrent cardiovascular wound	VI	X	XIV	XIII	XIII	VIII
$^{\mathrm{B}}_{\mathrm{Ll}}^{\mathrm{V}}_{\mathrm{l}}$	BONE; with concurrent cardiovascular damage	IV	VX.	XI	XI	XI	XI
H	HAND; any wound at this velocity	VI	VI	VI	VI	VI	VI
К2	URETER, URETHRA, AND URINARY BLADDER; puncture wound with leakage	I	I	I '	X	VIV	VIX
$^{\mathrm{N}}_{\mathrm{a}}^{\mathrm{V}}_{\mathrm{2}}$	NERVE; with concurrent cardiovascular damage	VI	X	XIV	X	X	VI
P ₇	LUNG; puncture with small blood loss	I	III	X	X	X	XIV

One might wish to cross-reference Table V with Tables III or IV to determine the relation between wound class and percent disability associated with tactical role and post-wounding time.

The wound classes describe the degree of traumatic damage which occurs in the anatomical structures. To determine specific portions of a soldier's anatomy which are vulnerable to the missile's penetration; the anatomical cross-sectional charts in the text 11 by Eycleshymer and Shoemaker were chosen as standard. These charts, which consider an "average man" to be 69 inches in height and 155 pounds in weight, "slice" our theoretical soldier into 108 horizontal cross sections. Section 1, starting with the top of the head, through Section 18, are 1.2 cm. thick; the remaining sections are 2.6 cm. thick. The process of horizontal scanning, for six equiangular rotations starting with the anterior as zero degrees, can result in as many as 100,000 trajectories for each missile at each velocity. Until recently, personnel of the Biophysics Division accomplished the task by hand; the time required to project one missile at three velocities was roughly two months. A computer program has been written by BRL 12, and the BRLES Computer can now perform the same task in one hour.

The projections are made only for horizontal trajectories through an erect soldier. The soldier is assumed to be standing in the standard anatomical position on the balls of his feet with his arms at his side and palms facing forward. It is further assumed that no part of his body shields any other. The trunk is projected with the extremities removed, and the arms and legs are projected as though removed from the trunk. However, the BRL presently is programming the anatomy so that trajectories other than normal can be evaluated. Hopefully, this project will be completed within the next few months.

It is hoped that anthropological differences that exist among diverse ethnic groups will not affect materially the adequacy of the criteria (P_{hk}) that finally are derived. For example, we are assuming tacitly that ratios of vulnerable areas to presented areas are independent of size of the individual. Actually, we recognize that smaller statured individuals should be more susceptible to wounding because they enjoy less protective tissue such as skin, muscle, etc. But when computing the expected number of casualties that could be produced by a weapon, one must account for the probability that the enemy soldier will be struck. But, the smaller the soldier, the lower the hit probability. Hence an increased P_{hk} is compensated to some extent by a decreased probability of being hit. A study of this kind, at the present time, is unwarranted.

In the projection process, the entire body is surveyed and divided into six major anatomical subdivisions; head and neck, thorax, abdomen, pelvis, 2 arms and 2 legs. The arms are further subdivided into upper arms and elbows, lower arms, wrists and hands and the legs are subdivided into upper legs and knees, lower legs, ankles and feet. This subdivision allows incapacitation data to be obtained for major subdivisions, as well as for an average for the entire body.

The Biophysics Division of CRDL present their results in the form of tables as illustrated by Tables VI and VII for a 7.2-grain steel flechette striking the bare torso at a velocity of 2000 fps. The enemy soldier is considered to be in an assault role. Table VI pertains to the post-wounding time of five minutes and is restricted to the thorax. It lists values of the areas of critical components vulnerable to the attack by the given fragment at the residual velocity of the fragment after penetrating through any protective anatomical components. The cross sections 19-27 refer to Eycleshymer and Shoemaker cross-sectional anatomy chart numbers, 19-27. Table VII is restricted to the thorax, abdomen, and lower legs and lists percent incapacitations for six post-wounding times. Data such as in Table VII can be summarized to yield average incapacitations for the entire body.

Table VIII presents such a summary for the whole body. Listed are the percent incapatitation, disability groups, percent of body area subjected to incapacitation, and the time after wounding. Again the 7.2-grain steel flechette with a striking velocity of 2000 fps is illustrated for the assault role.

Averaged over six different directions. It is to be pointed out that for each direction sufficient trajectories are introduced into each slice so that complete overlapping exists between adjacent trajectories. The first direction is for strikes perpendicular to the anterior; each successive direction is at multiple integers of 60°.

TABLE VI

(UNCL) Mean Vulnerable Areas (cm²) of Some Critical Components of the Thorax

Anatomical Cross Sections: 19-27

Wound Class (Critical Component)	Vulnerable <u>Area</u>
Ba.,	26.8
Bv ₇	1.7
Na	4.8
$_{ m N\Gamma}$ 5	1.3
P ₇	134.0
v_2	21.1
v_{1_4}	184.5

TABLE VII

(SECRET) Percent Incapacitation for Selected Anatomical Regions with a 7.2-Grain Steel Flechette at 2000 fps (U)

Tactical Role: Assault

		Percent of Total Body Area that is					
Subdivision %	% Incapac-		Subjec	et to Inc	apacita	ation	
Total Body Area		30 Sec.	5 Min.	30 Min.	<u>12 Hr.</u>	24 Hr.	5 Days
Thorax 12.8	0	9.9	3.1	2.6	2.9	3.0	3.4
	25	_	-			-	·
	50	2.3	2.3	2.3	1.8	1.8	1.8
	75	0.1	6.9	3.5	4.1	3.5	3.1
	100	0.5	0.5	4.4	4.0	4.5	4.5
Abdomen 10.5	0	10.1	7.2	3.8	2.0	2.0	5.7
	25	-	-	-	-	_ '	-
	50	_			-	-	-
	75	-	2.9	4.7	3.3	5.8	0.3
	100	0.3	0.3	2.0	5.2	2.7	4.4
Lower Legs 10.2	0	4.5	4.1	3.4	4.1	4.3	4.5
	25	***	_	_ `	-		- '
	50°	0.2	<0.1	<0.1	<0.1	<0.1	0.2
	75		0.6	. 1.0	0.6	0.3	
	100	5.5	5.6	5.8	5.5	5.5	5.5
				*			•

TABLE VIII

(SECRET) Percent Incapacitation for the Whole Body with a 7.2-Grain Steel Flechette at 2000 fps (U)

Tactical Role: Assault

% Incapaci-	Disability						S	
tation	Group	30 Sec.	5 Min.	30 Min.	12 Hr.	24 Hrs.	5 Days	
None - 0	I	57.9	41.4	34.6	33.9	35.6	40.6	
Mild - 25	-	-		-	. -	-	-	
Moderate - 50	II,VI	24.8	21.2	21.2	9.9	10.0	10.3	
Severe - 75	III,VII, VIII,X,XVI	1.3	21.0	17.4	18.7	16.8	8.1	
Total - 100	IV,V,IX,XI XII,XIII, XIV,XV	16.0	16.3	26.8	37.5	37.6	41.0	

The numbers in the table represent the percentage of the average projected body area (averaged over 6 directions) which, if hit, would result in a particular percentage level of incapacitation. Thus, the conditional probability, P_{hk} , that a random hit results in an incapacitation is taken to be:

$$P_{hk} = \frac{\Sigma(P_i A_i)}{\Sigma A_i}$$

 P_i is the average incapacitation associated with the hits on a subdivision whose average subtended area is A_i . ΣA_i is the total presented area of the body. Thus, for the post-time wounding of 5 minutes we estimate from Table VIII the following value for P_{hk} :

$$P_{hk} = (0 \times 0.414) + (.25 \times 0) + (.50 \times 0.212) + (.75 \times 0.210) + (1 \times 0.163)$$

 $P_{hk} = 0.43$

The term "probability of incapacitation" is a misnomer here. Actually, what is derived is an estimate of an <u>average level</u> of <u>incapacitation</u> that could be imposed on a soldier as a result of a <u>random</u> hit with a particular missile at a specific striking velocity. If we were dealing with a dichotomy, that is, if a hit either incapacitated ($P_i = 100\%$) or did not

incapacitate (P_i = 0%), then P_{hk} would represent the probability of incapacitation. For the moment let us admit the concept of a dichotomy. Then, if an assessor evaluated a hit at an intermediate level of incapacitation, say P_i = 25%, it would mean that he was uncertain to the extent of 25% that the hit would result in no incapacitation; or conversely, he was uncertain to the extent of 75% that the hit would result in full incapacitation.

But in our case this is not what the assessor means when he assesses a hit at an intermediate level of incapacitation. For example, if he associates with a specific wound the level $P_i = 25\%$, he means that the soldier would not be able to perform 25% of his duties.

We must realize that the assessments are subjective and depend on clinical and field experience of the medical officer(s). Because of potential errors of subjectivity a conservative approach was adopted in the procedure for making assessments. Along each hypothetical wound track only that anatomical component that would constitute the highest incapacitation is considered in the establishment of the wound class; either individual or synergistic effects of all other components in the tract are not included.

When weapons systems analysts or designers evaluate the lethality of a fragmenting shell the usual thing to do is to estimate the number of casualties that would be caused under a specific set of conditions. Briefly, the expected number of casualties can be found from the following expression:

$$E(C) = \int \int \sigma(x,y) P_k(x,y) dxdy$$

where $\sigma(x,y)$ is the areal density of troops at a specific point (x,y) on the ground, and $P_k(x,y)$ is the probability that a soldier located in the elemental area dxdy will be incapacitated. $P_k(x,y)$ takes into account the number of hits on the soldier and the probability that each hit will cause an incapacitation. Neglecting synergistic effect of multiple

wounds and assuming that \mathbf{P}_{hk} is relatively small for each hit, then \mathbf{P}_k can be computed from the binomial expansion.

$$P_k = 1 - (1 - P_{hk_1}) (1 - P_{hk_2}) \cdots (1 - P_{hk_i}).$$

The reader is referred to BRL Technical Note No. 1511 for a more detailed description of the formulation of E(C).

(CONFIDENTIAL) RESULTS AND DISCUSSION

Tables IX and X summarize some of the physical characteristics of the steel fragments and the homologous series of steel flechettes used for the experiments.

TABLE IX

(UNCLASSIFIED)	Character	Characteristics of Fragments			
Missile	Weight grams	Dimension cm.	Presented Area * sq. cm.		
**Sphere, 0.85 gr.	0.055	0.236 (Diameter)	0.044		
***Cube, 2.1 gr.	0.136	0.282 x 0.282 x 0.216	0.101		
***Cube, 16.0 gr.	1.06	0.505 x 0.513 x 0.518	0.393		
***Cube, 225 gr.	14.7	1.22 x 1.22 x 1.27	2.30		

^{*} For Cubes: Presented Area = $\frac{Surface\ Area}{4}$

Commercially available ball bearings

^{***} ASTM 1020 Steel -- note that the "cubes" actually were rectangular parallelepipeds.

TABLE X (UNCLASSIFIED) Characteristics of WP Flechettes

			Shaft		Fir	ıs	Frontal Presented
Missile	Weight grams	Length cm.	Diameter cm.	No.	Span cm.	Thickness cm.	Area sq. cm.
1.72 gr.	0.112	1.71	0.114	. 4	0.287	0.018	0.0164
7.2 gr.	0.464	2.75	0.180	4	0.450	0.030	0.0416
15.2 gr.	0.982	3.40	0.236	14	0.594	0.043	0.0745

Estimates of the probability of incapacitation ($P_{\rm hk}$) were made at three striking velocities for each of the four fragments and three flechettes. The 0.85-grain sphere, the 2.1-grain cube and 16.0-grain cube were evaluated at nominal striking velocities of 1000, 3000, and 5000 fps; those for the 225-grain cube were 500, 1000, and 2500 fps. The three flechettes were evaluated at nominal striking velocities of 500, 2000, and 4000 fps.

A relationship which, on the average, yielded a good fit to the experimental data for the whole body was:

$$P_{hk} = 1 - e^{-a(mv^{3/2} - b)^n}$$

where different values of the parameters a, b, n were associated with each different combination of tactical role and post-wounding time. Further, we a priori assumed that the same relationship held for each of the major body sections. Thus, if P_{hkj} is this conditional probability for the jth part, and r_j is the relative presented area of the jth part, then

$$P_{hk} = \Sigma(r_j P_{hk_j})$$
.

^{*} Made by Whirlpool Corporation of Hardened 1060 steel.

^{**}Including fin area.

A least square procedure (as discussed in Reference 1) was set up to determine the best values of a, b, and n. Actually, some judgment on the ballistic limits of skin and clothing helped to establish the value of the threshold parameter, b. Note that when MV $_{0}^{3/2}$ = b then P_{hk} = 0.

The tables in Appendix B list values of the parameters a, b and n for four tactical roles (Defense \leq 30 seconds, Assault \leq 30 seconds and \leq 5 minutes and Supply \leq 1/2 day) for the helmeted, nude soldier, and for the soldier clothed in the American winter uniform (with helmet) and boots; these relations are plotted in Appendix C.

The transformation of the criteria from the nude soldier to the clothed soldier was accomplished quite simply by subtracting from the striking velocity the average velocity lost by the missile while traversing the clothing and/or boots. Table XI is a tabulation of these losses in velocity.

The criteria (which include various levels of incapacitation, i.e., 25%, 50%, 75%, 100%) are not stringent enough when applied to the design and/or evaluation of "personal" type weapons such as pistols, hand grenades, cannister ammunition, anti-personnel mines, rifles, etc. Because of close engagement ranges associated with such weapons their effectiveness should be based only on hits that would cause complete incapacitations. In this instance P_{hk} is defined as the probability that a random, penetrating hit will result in a complete loss in the ability of the soldier to fight. Hence, Appendix B includes values of the parameters for 100% incapacitation for Defense \leq 30 seconds, Assault \leq 30 seconds, and Assault \leq 5 minutes.

At striking velocities of approximately 3000 fps, both the 1.7-and 7.2-grain flechettes started tumbling, that is, rotated end-over-end rapidly, shortly after penetrating tissue. The average depth of tissue penetration to tumbling was 4.1 and 5.0 cm respectively for the 1.7 and 7.2. On the other hand, the 15.2-grain flechette at 4000 fps yawed violently after approximately 8.0 cm of travel in tissue but usually did

TABLE XI

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Retardation Data (U)

		Loss in Velocity (fps)						
Missile Weight Grains	Striking Velocity fps	Clothinga	Boots	Helmet	Ba Clothing a	<u>Boots</u>	imit (fps) Helmet	Skin in Situ
	,			SPHERE			· · · · · · · · · · · · · · · · · · ·	
.85	1000 3000 5000	390 175 325	175 c ¹⁵⁰ 270	1000 2072 3088	902	593	2757	281
				CUBES				
2.1	1000 3000 5000	320 287 441	190 e255 485	1000 1954 2040	850	567	2892	310
16	1000 3000 5000	135 150 250	100 150 220	1000 870 1550	605	419	1457	206
225	500 1000 2500	70 34 934	43 25 25 25	500 2380 323	349	237	758	155
				FLECHETTES	· · · · · · · · · · · · · · · · · · ·			•
1.7	500 2000 4000	c ^{N.A.} 48 25	N.A. N.A. N.A.	500 2000 794	474	433	C [₫] 2473 R=2694	202
7.2	500 2000 4000	^c 65 60 25	N.A. N.A. N.A.	500 325 245	361	305	C [₫] 871 R=966	172
15.2	500 2000 4000	c 69 45 9 20	N.A. N.A.	500 273 190	351	257	C=912 R=912	181

a. Six-layer winter uniform.

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b. Helmet with nylon liner.

c. Derived by interpolation or extrapolation

d. C = Crown, R = Rim.

not tumble end-over-end as did the 1.7- and 7.2-grain flechettes. Thus, a distinction is made in that the 15.2-grain flechette is not considered to be a "tumbler" in the strict sense of the word.

The above suggests that weight is a limiting factor in attaining desirable tumbling qualities, at least for the series of flechettes tested. However, this is only valid if restricted to homogeneous materiel, as a few experiments with an 18-grain bimetallic flechette show that tumbling can occur early in the target even at velocities lower than 2000 fps.

The L/D (length over diameter) ratio probably plays a role in inducing tumbling. The L/D ratios of the 1.7 and 7.2 (150 and 153) are slightly higher than that of the 15.2 (144). But, a short 10-grain experimental flechette with an L/D = 126 has proved to be a good early tumbler.

Another cause of early and rapid tumbling of flechettes in tissue and gelatin, is the inducement of bending and distortion of the flechette upon impact with the target at the higher velocities. Such distortions have been observed for the 1.7 and 7.2 flechettes as well as other experimental flechettes of 13 grains and less. On the other hand, bending and distortion of the 15-grain flechette was not as extensive.

Tumbling characteristics are also affected by the shape of the nose of the flechettes and its hardness. Blunt nose flechettes usually are quite stable in the target even at velocities greater than 3000 fps. Also the noses of soft steel flechettes (30-40 Rockwell) become blunted (flatten out) at high striking velocities and the flechettes are relatively stable.

Generally speaking, in order to qualify as a good tumbler, a homologous flechette should weigh no more than 13 grains, be of mild steel and possess a sharp point. Actually, it has been found that an acute, compound point is most desirable.

In view of the previous comments, wound ballisticians and weapon systems analysts are cautioned not to consider a flechette in the tumbling category solely on the basis that its striking velocity approaches or

exceeds 3000 fps. However, once a flechette has been defined as a tumbler, in the strict sense, the values of a, b and n given in the tables are applicable.

The 15.2-grain flechette was not considered to be a tumbler and therefore was not included in the analysis. The criteria are based specifically on incapacitations derived for the 1.7- and 7.2-grain flechettes at 4000 fps. It is suggested that the criteria for tumbling flechettes be limited to apply to weights between 1.7 and 13 grains and for striking velocities exceeding 3000 fps.

Because of insufficient datum points the values of the parameter b for the tumbling flechettes were chosen arbitrarily to be equal to those for the non-tumbling flechette. The dashed portion of the curves for the tumbling flechettes merely connect the values b with those solid portions of the curve which are supported by data.

When we account for all levels of incapacitation (0, .25, .50, .75, and 1.00) the wounding potential of the tumbling flechette is in general about 10% greater than that for the steel fragments. However, for some anatomical subdivisions, the tumbler is not as potentially incapacitating. In the arms, for example, the P_{hk} for tumblers is less than that for fragments because the flechette must penetrate some minimum distance before tumbling occurs. Hence, in the case of the upper extremities, the flechette is well into or through an arm before any appreciable tumbling occurs. In contrast, the P_{hk} 's for tumblers are greater for lower extremities than those of the fragment, because within the larger cross-sectional area of the legs, there is a sufficient tract length in which the flechette may tumble and thus be more effective.

Another phenomenon, which appears unique at first glance, is concerned with the performance of the non-tumbling flechette in the pelvic region. In all tactical roles, the non-tumbling flechette has a higher probability of incapacitating in the pelvic subdivision than the chunky fragment, at least for the lower and mid-range values of the parameter $mv^{3/2}$. This occurs because bone structures are more dense in this region

of the body and the flechette's superior ability to penetrate bone allows it to get to other organs, such as blood vessels and arteries, with more residual velocity (energy). The smaller fragments are either stopped completely or lose most of their energy in traversing the bone. Additionally, a stable flechette becomes unstable after penetrating or glancing off bone, and in the assessment procedure, is considered a tumbler after striking bone.

Early, during the animal experimental firings with flechettes, it was found that the superior penetrating ability of the missile would allow it to reach every major organ within the human body at velocities of 3000 and 4000 fps, and, unless bone were encountered, any of the three flechettes could traverse the body even at 500 fps. As a result, in projecting flechettes through anatomical cross sections in order to determine the fraction of the total mean presented body area vulnerable to specific gradations of wounding, it was possible in many instances to identify wound classes without recourse to the stepwise process of tissue retardation. In the case of fragments, however, the wound tracts were incrementally evaluated to determine velocity decay as the missile encountered and perforated each type of tissue and organ.

In projecting the imaginary wound tracts through the cross-sectional anatomy charts, personnel of the Biophysics Division credited the larger missiles at the higher velocities with wound tracts greater than the actual width of the missile. Table XII shows the increase in mean presented area of the body which resulted when projection was performed to account for missile size.

WILLIAM KOKINAKIS

JOSEPH SPERRAZZA

(UNCLASSIFIED) TABLE XII

Wt. of Missile grains	Missile Bite	Mean Presented Body Area
	FRAGMENTS	
0.85	0.0	5144
2.1	0.4	5310
16.0	0.8	5481
225.0	1.6	5837
	FLECHETTES*	
1.7 at 500 + 2000 fps	0.0	5144
at 4000 fps	0.3	5144
7.2 at 500 + 2000 fps	0.2	5312
at 4000 fps	0.5	5312
15.2 at 500 + 2000 fps	0.3	5396
at 4000 fps	0.5	5396

^{*} At the tumbling velocity of 4000 fps, the larger missile bite was considered only after the flechette commenced tumbling. Prior to start of tumble, the smaller missile bite was used.

(UNCLASSIFIED)

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APPENDICES

- (UNCLAS) A. DEFINITION OF TACTICAL SITUATIONS
- (SECRET) B. INDEX AND TABLES OF PARAMETERS (a, n, b) FOR CURVES OF $P_{\rm hk}$ (U)
- (SECRET) C. INDEX AND CURVES OF P VERSUS PROJECTILE WEIGHT AND STRIKING VELOCITY $^{\rm hk}(U)$

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APPENDIX A

(UNCLASSIFIED) DEFINITION OF TACTICAL SITUATIONS

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Assault: For purposes of data application, the tactical situation of assault is considered to be strictly on a company operations level requiring each participating soldier to engage in the maximum type of physical activity. It is postulated that a typical standard type of assault action would be taking place. Two platoons, with one held in reserve, will attack an enemy position at point x approximately 200 -300 yards from the initial positions of the attacking platoons. The standard procedure of one platoon attacking frontally with the other platoon on the enemy's flank is considered to prevail in such an operation. Each platoon gives cover fire while its partner advances. Certainly no more than 48 hours and probably much less will be allowed for such an operation either to succeed or fail before regrouping prior to another attempt. In such a situation one can readily realize the host of physical activities which would occur. However, an attempt has been made to choose what is considered to be the most important physical requirements necessary for the average advancing assault soldier. In this situation, locomotion forward to meet the enemy is more than implied. Out of various standard forms of locomotion such as crawling, walking, dragging or running, running was considered to be the form most necessary for such an engagement. This choice was substantiated as being closest to reality in informal discussions with Field Forces representatives. In addition to being able to run, the soldier must be able to load, aim, and fire a rifle or carbine in the accustomed manner. To be able to see, hear, think, and communicate with others are also requirements in an active stress situation.

<u>Defense</u>: Again the company level of operations has been chosen. This situation is considered to be static, with men well dug in, and having maximum shelters for protection.

It is postulated that locomotion in such a situation is much less a compelling requirement than in assault. The total distance over which the defensive soldier is likely to move is approximately 10 to 20 feet, but mobility such as crawling or walking with difficulty was considered to be entirely adequate as a form of movement. In addition, the soldier is required to load and fire his rifle, but fr n a fixed position requiring less upper extremity dexterity than in the assault situation. The requirements of being able to see, hear, think, and communicate with others still exists.

Supply: The supply situation offers considerably more difficulty in the evaluation of human incapacitation, for one finds it difficult to delineate specific work requirements in such a field of diverse activities. An attempt was made to choose only one specific work situation. This choice is one of a soldier who is standing in an ammunition line receiving light loads from his right and passing them on to the man to his left. The implication here is that he must assume a standing position, utilize his arms, but not engage in any sort of locomotion. This was considered to be somewhat a realistic front line supply situation engaged in at one time or another by a typical supply "ammo" bearer. Although only one typical situation was chosen as an illustrative example of the supply situation, one can, from a much broader sense, evaluate incapacitation in this stress situation. If one considers supply situations far in the rear of actual combat, one could consider just about all extremity disability as totally incapacitating, as an injured man would likely report to some dispensary for treatment soon after injury.

Reserve: Our reserve situation implies a company of men ready to be either committed to an assault or defensive situation as already described. However, prior to commitment, this type of reserve pool is considered physically inactive. It is considered that any wound of even a relatively innocuous type will produce a greater degree of incapacitation than the same wound sustained during an assault or defensive situation. This reasoning is based on the assumption that men who sustain wounds while in a reserve pool are much less likely to be committed by their company commanders to the above circumstances.

APPENDIX B

(SECRET) INDEX AND TABLES OF PARAMETERS

(a, n, b) FOR CURVES OF P

hk

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INDEX OF TABLES

			'
Table	Projectile	Tactical Role	Part of Body
I	Fragment	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Nude, entire and each anatomical subdivision.
II	Fragment	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Clothed, entire and each anatomical subdivision.
III	Stable Flechette	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Nude, entire and each anatomical subdivision.
IV	Stable Flechette	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Clothed, entire and each anatomical subdivision.
V	Tumbling Flechette	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Nude, entire and each anatomical subdivision.
VI	Tumbling Flechette	Defense ≤ 30 seconds Assault ≤ 30 seconds Assault ≤ 5 min. Supply ≤ 12 hours	Clothed, entire and each anatomical subdivision.
VII	Fragment, Stable and Tumbling Flechette	100% Incapacitation for Defense ≤ 30 seconds, Assault ≤ 30 seconds, & Assault ≤ 5 min.	Nude, entire
VIII	Fragment, Stable and Tumbling Flechette	100% Incapacitation for Defense ≤ 30 seconds, Assault ≤ 30 seconds, & Assault ≤ 5 min.	Clothed, entire
IX	Fragment, Stable and Tumbling Flechette	100% Incapacitation for Defense ≤ 30 seconds	Clothed, entire and each anatomical subdivision.

TABLE I

(SECRET) Parameters (a,n,b) for Curve of Phk

Steel Fragments (U)

(Soldier is assumed to be nude)

Part of Body	<u>a</u>	n	Ъ	<u>r*</u>
	Defense ≤	30 sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	8.7026 x 10 ⁻³ 2.1001 x 10 ⁻³ 7.3623 x 10 ⁻⁴ 6.8001 x 10 ⁻⁶ 1.4293 x 10 ⁻³ 6.3251 x 10 ⁻⁴ 1.6788 x 10 ⁻³	• 36023 • 27000 • 46494 • 74407 • 42552 • 46675 • 41356	26,500 26,780 26,780 23,500 26,780 26,700 26,500	.0651 .1304 .1065 .1156 .2045 .3778
	Assault ≤	30 sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	7.5501 x 10 ⁻³ 1.2809 x 10 ⁻² 5.0675 x 10 ⁻⁴ 1.5833 x 10 ⁻⁵ 5.1702 x 10 ⁻³ 3.4535 x 10 ⁻⁴ 1.4992 x 10 ⁻³	.37518 .31650 .50878 .72599 .36032 .57226 .45492	26,500 26,700 26,780 23,500 26,780 26,400 26,500	
	Assault ≤	5 min.		*.
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	8.1464 x 10 ⁻³ 2.2652 x 10 ⁻² 2.1028 x 10 ⁻³ 1.5984 x 10 ⁻⁴ 3.6001 x 10 ⁻³ 4.3226 x 10 ⁻⁴ 2.0785 x 10 ⁻³	• 38955 • 28542 • 44292 • 58732 • 40015 • 56420 • 44545	26,500 26,700 26,780 23,500 26,500 25,800 25,800	
	Supply ≤ 1	12 hrs.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	4.5911 x 10 ⁻² 3.7620 x 10 ⁻² 1.0607 x 10 ⁻¹ 4.9274 x 10 ⁻³ 5.9909 x 10 ⁻⁴ 3.6130 x 10 ⁻⁴ 3.4423 x 10 ⁻³	.27078 .26330 .20885 .38392 .53665 .56185 .41845	26,780 26,780 25,800 23,500 23,500 23,500 23,500	

* r is ratio of the presented area of a Part to the entire body.

TABLE II

(SECRET) Parameters (a,n,b) for Curve of $P_{\rm hk}$

Steel Fragments (U)

(Soldier with helmet and winter clothing)

Part of Body	a	<u> </u>	<u>d</u>	r*
	Defense ≤ 30	sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	2.6648 x 10-4 1.7955 x 10-2 5.1602 x 10-4 4.0293 x 10-6 8.4126 x 10-4 5.3116 x 10-4 8.8771 x 10-4	• 57884 • 27859 • 48523 • 77314 • 45662 • 47749 • 45106	20,000 45,000 43,500 36,500 30,500 31,400 31,400	.0651 .1304 .1065 .1156 .2045 .3778
	Assault ≤ 30	sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	2.1063 x 10 ⁻⁴ 1.0479 x 10 ⁻² 3.4436 x 10 ⁻⁴ 1.0015 x 10 ⁻⁵ 3.1468 x 10 ⁻⁴ 3.0833 x 10 ⁻⁴ 7.6442 x 10 ⁻⁴	•59981 •32779 •53050 •75050 •39054 •57749 •49570	20,000 40,500 42,000 41,000 30,000 30,000 31,000	
	Assault ≤ 5	min.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	2.1641 x 10 ⁻⁴ 1.9060 x 10 ⁻² 1.7401 x 10 ⁻³ 1.0855 x 10 ⁻⁴ 2.1247 x 10 ⁻³ 3.5277 x 10 ⁻⁴ 1.0454 x 10 ⁻³	.62684 .29474 .45191 .60862 .43224 .57631 .48781	20,000 44,000 45,000 39,000 31,100 30,000 31,000	
	Supply ≤ 12	hrs.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	6.0806 x 10 ⁻⁴ 3.2873 x 10 ⁻² 9.2431 x 10 ⁻² 4.0060 x 10 ⁻³ 3.6448 x 10 ⁻⁴ 3.1099 x 10 ⁻⁴ 2.1973 x 10 ⁻³	.55367 .27050 .21660 .39513 .56628 .57085 .44350	20,000 45,000 43,500 40,500 29,000 29,000	
* r is ratio	of the presented area of a	Part to the en	tire body.	

TABLE III

(SECRET) Parameters (a,n,b) for Curve of Phk

Non-Tumbling Flechett: (U)

(Soldier is assumed to be sude)

		•	
a	<u>n</u>	<u>b</u>	<u>r*</u>
Defense ≤ 3	o sec.		
4.4497 x 10 ⁻⁵ 1.8074 x 10 ⁻⁶ 9.9419 x 10 ⁻⁵ 4.7265 x 10 ⁻⁵ 3.5068 x 10 ⁻⁴ 6.2746 x 10 ⁻⁵ 5.5791 x 10 ⁻⁵	.71730 .85827 1.01934 .60399 .45248 .57247 .59839	17,000 0 0 11,000 0 10,000 10,000	.0651 .1304 .1064 .1156 .2045 .3778
Assault ≤ 30	sec.		
4.4106 x 10 ⁻⁵ 5.3687 x 10 ⁻⁶ 2.1914 x 10 ⁻⁶ 2.5449 x 10 ⁻⁴ 1.2913 x 10 ⁻³ 9.5249 x 10 ⁻⁵ 1.0590 x 10 ⁻⁴	.71887 .80156 .81548 .53045 .39877 .60084 .58983	17,000 10,000 0 15,000 16,000 10,000	
Assault ≤ 5	min.		
1.3627 x 10 ⁻⁴ 2.1605 x 10 ⁻³ 6.3702 x 10 ⁻⁴ 2.0479 x 10 ⁻³ 7.2379 x 10 ⁻⁴ 1.9488 x 10 ⁻⁴ 6.4241 x 10 ⁻⁴	.67313 .43596 .51350 .43161 .47249 .57565	18,000 15,000 0 15,000 16,000 15,000 14,000	
Supply ≤ 12	hrs.		
1.5786 x 10-4 3.5758 x 10-3 4.7248 x 10-4 2.3060 x 10-3 5.5160 x 10-4 5.4716 x 10-4 1.2127 x 10-3 presented area of a	.66436 .40604 .57593 .44704 .48814 .50490 .46380 Part to the en	18,000 18,500 11,000 18,000 17,000 18,000 17,000 tire body.	
	Defense ≤ 30 4.4497 x 10-5 1.8074 x 10-8 9.9419 x 10-8 4.7265 x 10-5 3.5068 x 10-4 6.2746 x 10-5 5.5791 x 10-5 Assault ≤ 30 4.4106 x 10-5 5.3687 x 10-6 2.1914 x 10-6 2.5449 x 10-4 1.2913 x 10-3 9.5249 x 10-5 1.0590 x 10-4 Assault ≤ 5 1.3627 x 10-4 2.1605 x 10-3 6.3702 x 10-4 2.0479 x 10-3 7.2379 x 10 1.9488 x 10-4 6.4241 x 10-4 Supply ≤ 12 1.5786 x 10-4 5.5758 x 10-3 4.7248 x 10-4 5.5758 x 10-3 5.5160 x 10-4 5.4716 x 10-4 1.2127 x 10-3	Defense ≤ 30 sec. 4.4497 x 10-5 1.8074 x 10-6 1.8074 x 10-8 9.9419 x 10-8 1.01934 4.7265 x 10-5 3.5068 x 10-4 6.2746 x 10-5 5.5791 x 10-5 5.5791 x 10-5 5.5791 x 10-5 5.5839 Assault ≤ 30 sec. 4.4106 x 10-5 2.1914 x 10-6 2.1914 x 10-6 2.1914 x 10-6 2.1914 x 10-6 2.5449 x 10-4 1.2913 x 10-3 9.5249 x 10-5 1.2913 x 10-3 9.5249 x 10-5 1.0590 x 10-4 58983 Assault ≤ 5 min. 1.3627 x 10-4 2.1605 x 10-3 4.3596 6.3702 x 10-4 5.1350 2.0479 x 10-3 4.3161 7.2379 x 10-4 1.9488 x 10-4 5.7565 6.4241 x 10-4 5.7565 6.4241 x 10-4 5.7593 2.3060 x 10-3 4.7248 x 10-4 5.57593 2.3060 x 10-3 5.5160 x 10-4 5.4716 x 10-4 5.0490 1.2127 x 10-3 4.6380	Defense ≤ 30 sec. 4.4497 x 10 ⁻⁵ .71730 .17,000 1.8074 x 10 ⁻⁶ .85827 0 9.9419 x 10 ⁻⁸ 1.01934 0 4.7265 x 10 ⁻⁵ .60399 11,000 3.5068 x 10 ⁻⁴ .45248 0 6.2746 x 10 ⁻⁵ .57247 10,000 5.5791 x 10 ⁻⁵ .59839 10,000 Assault ≤ 30 sec. 4.4106 x 10 ⁻⁵ .71887 17,000 5.3687 x 10 ⁻⁶ .80156 10,000 2.1914 x 10 ⁻⁶ .81548 0 2.5449 x 10 ⁻⁴ .53045 15,000 1.2913 x 10 ⁻³ .39877 16,000 9.5249 x 10 ⁻⁵ .60084 10,000 1.0590 x 10 ⁻⁴ .58983 11,000 Assault ≤ 5 min. 1.3627 x 10 ⁻⁴ .67313 18,000 2.1605 x 10 ⁻³ .43596 15,000 6.3702 x 10 ⁻⁴ .51350 0 2.0479 x 10 ⁻³ .43161 15,000 7.2379 x 10 ⁻⁴ .57565 15,000 6.4241 x 10 ⁻⁴ .57565 15,000 6.4241 x 10 ⁻⁴ .57565 15,000 6.4241 x 10 ⁻⁴ .57564 18,000 Supply ≤ 12 hrs. 1.5786 x 10 ⁻⁴ .66436 18,000 3.5758 x 10 ⁻³ .40604 18,500 4.7248 x 10 ⁻⁴ .57593 11,000 2.3060 x 10 ⁻³ .48814 17,000 5.4716 x 10 ⁻⁴ .48814 17,000 5.4716 x 10 ⁻⁴ .48814 17,000

TABLE IV

(SECRET) Parameters (a,n,b) for Curve of P_{hk} Non-Tumbling Flechette (U)

(Soldier with helmet and winter clothing)

Part of Body	<u>a</u>	n	b	r* _
	Defense ≤	30 sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	4.6872 x 10 ⁻⁷ 2.296\(\text{\mu}\) x 10 ⁻⁶ 1.1286 x 10 ⁻⁷ 3.6920 x 10 ⁻⁵ 3.9447 x 10 ⁻⁴ 5.0873 x 10 ⁻⁵ 3.6302 x 10 ⁻⁵	1.02621 .83907 1.00639 .61937 .44302 .58621 .62548	0 10,000 10,000 13,000 13,000 13,000	.0651 .1304 .1065 .1156 .2045
	Assault ≤	30 sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	4.8562 x 10 ⁻⁷ 4.5872 x 10 ⁻⁶ 1.6640 x 10 ⁻⁶ 2.1342 x 10 ⁻⁴ 1.1204 x 10 ⁻³ 7.0968 x 10 ⁻⁵ 7.6217 x 10 ⁻⁵	1.02534 .81054 .83381 .54075 .40774 .62031	0 13,000 10,000 18,000 18,000 12,000 13,000	
	Assault ≤	5 min.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	1.1356 x 10 ⁻⁵ 1.7359 x 10 ⁻³ 7.6605 x 10 ⁻⁴ 1.6556 x 10 ⁻³ 7.4722 x 10 ⁻⁴ 1.8186 x 10 ⁻⁴ 5.1222 x 10 ⁻⁴	.83353 .45038 .49968 .44541 .46931 .57960	14,000 18,000 10,000 18,000 20,000 18,000 17,000	
	Supply ≤	12 hrs.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	5.2662 x 10 ⁻⁶ 3.3084 x 10 ⁻³ 4.3368 x 10 ⁻⁴ 1.9224 x 10 ⁻³ 4.6218 x 10 ⁻⁴ 4.6397 x 10 ⁻⁴ 8.4626 x 10 ⁻⁴	.89243 .40998 .57984 .45788 .49925 .51530 .48828	10,000 23,000 16,000 21,000 20,000 21,000 21,000	

^{*} r is ratio of the presented area of a Part to the entire body.

TABLE V

(SECRET) Parameters (a,n,b) for Curve of Phk

Tumbling Flechette (U)

(Soldier is assumed to be nude)

Part of Body	<u>a</u>	<u>n</u>	<u>b</u>	<u>r*</u>
	Defense ≤ 30	sec.		•
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	7.8288 x 10 ⁻² 1.8084 x 10 ⁻³ 1.0632 x 10 ⁻⁴ 5.4027 x 10 ⁻⁵ 8.8893 x 10 ⁻⁴ 5.0439 x 10 ⁻⁴ 1.3140 x 10 ⁻³	.20942 .44032 .63570 .64072 .45453 .47203 .43432	17,000 0 0 11,000 0 10,000	.0651 .1304 .1065 .1156 .2045 .3778
	Assault ≤ 30	sec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	3.1926 x 10 ⁻³ 4.3175 x 10 ⁻³ 1.5864 x 10 ⁻⁴ 1.1750 x 10 ⁻⁵ 2.2264 x 10 ⁻³ 9.5436 x 10 ⁻⁵ 1.0582 x 10 ⁻³	.45325 .38696 .60210 .77044 .40824 .66420 .48464	17,000 10,000 0 15,000 16,000 10,000 11,000	
	Assault ≤ 5 m	in.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	1.1673 x 10 ⁻² 4.2752 x 10 ⁻³ 9.6232 x 10 ⁻⁵ 2.4528 x 10 ⁻⁵ 1.9517 x 10 ⁻³ 2.7056 x 10 ⁻⁴ 7.4080 x 10 ⁻⁴	.34408 .44705 .70848 .78672 .43622 .60554 .53460	18,000 15,000 0 15,000 16,000 15,000 14,000	
	Supply ≤ 12 h	rs.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	1.9271 x 10 ⁻² 2.1764 x 10 ⁻² 3.2628 x 10 ⁻² 6.1528 x 10 ⁻⁴ 3.3384 x 10 ⁻⁴ 2.5992 x 10 ⁻⁴ 2.1780 x 10 ⁻³	• 34362 • 30853 • 31087 • 57494 • 57181 • 60132 • 46169	18,000 18,500 11,000 18,000 17,000 18,000 17,000	
* r is ratio of	f the presented area of a P	art to the en	tire body.	٠

TABLE VI

(SECRET) Parameters (a,n,b) for Curve of Phk

Tumbling Flechette (U)

(Soldier with helmet and winter clothing)

Part of Body	<u>a</u>	<u>n</u>	<u>b</u>	<u>r*</u>
	Defense ≤ 30 s	ec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	1946 x 10 ⁻⁴ 1.4)08 x 10 ⁻³ 8.8912 x 10 ⁻⁵ 3.4989 x 10 ⁻⁵ 7.7820 x 10 ⁻⁴ 3.8556 x 10 ⁻⁴ 7.4970 x 10 ⁻⁴	.68954 .45192 .64639 .66768 .46262 .48819 .46969	0 10,000 10,000 13,000 10,000 13,000	.0651 .1304 .1065 .1156 .2045
·	Assault <u>≠</u> 30 s	ec.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	1.0258 x 10 ⁻⁴ 3.8183 x 10 ⁻³ 1.3279 x 10 ⁻⁴ 7.1670 x 10 ⁻⁵ 1.7001 x 10 ⁻³ 7.7319 x 10 ⁻⁵ 7.9580 x 10 ⁻⁴	.86215 .39458 .61354 .80215 .42537 .67643 .50032	0 13,000 10,000 18,000 18,000 12,000 13,000	
	Assault ≤ 5 mi	n.		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	2.8605 x 10 ⁻⁵ 9.1266 x 10 ⁻³ 4.9520 x 10 ⁻⁵ 1.6672 x 10 ⁻⁵ 1.5598 x 10 ⁻³ 2.0868 x 10 ⁻⁴ 4.6090 x 10 ⁻⁴	.80934 .35946 .75548 .81150 .45013 .62196 .56622	14,000 18,000 10,000 18,000 20,000 18,000 17,000	
	Supply ≤ 12 hr	`S•		
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	8.2092 x 10 ⁻⁵ 1.7615 x 10 ⁻² 2.6219 x 10 ⁻² 5.7651 x 10 ⁻⁴ 2.5720 x 10 ⁻⁴ 2.0107 x 10 ⁻⁴ 1.4410 x 10 ⁻³	.73511 .32171 .32207 .57612 .58841 .61712 .48872	10,000 23,000 16,000 21,000 20,000 21,000	

^{*} r is ratio of the presented area of a Part to the entire body.

TABLE VII

(SECRET) Parameters (a,n,b) for Curve of Phk (U)

(100% Incapacitation)

(Soldier is assumed to be nude)

Situation	<u>a</u>	n	<u> </u>
	Steel	Fragments	
D30 A30 A5	3.0070 x 10 ⁻⁵ 2.2516 x 10 ⁻⁵ 2.2027 x 10 ⁻⁴	.59127 .67992 .55500	66,000 57,000 26,000
	Non-Tumbl	ing Flechettes	
D30 A30 A5	5.9648 x 10 ⁻⁸ 3.3934 x 10 ⁻⁵ 1.7280 x 10 ⁻⁵	.95227 .60867 .68914	18,000 10,000 10,000
	Tumblin	g Flechettes	
D30 A30 A5	1.1515 x 10 ⁻⁵ 4.9882 x 10 ⁻⁵ 1.3910 x 10 ⁻⁵	.64957 .63553 .76009	18,000 10,000 10,000

TABLE VIII

(SECRET) Parameters (a,n,b) for Curve (Phk (U) (100% Incapacitation) (Soldier with helmet and winter clothing)

Situation	<u>a</u>	<u>n</u>	<u>b</u>
	Steel	Fragments	
D30 A30 A5	1.4411 x 10 ⁻⁵ 9.9557 x 10 ⁻⁶ 2.1078 x 10 ⁻⁴	.63345 .73159 .55514	66,000 62,000 40,000
	Non-Tumbl	ing Flechettes	
D30 A30 A 5	5.9648 x 10 ⁻⁸ 2.6133 x 10 ⁻⁵ 1.3859 x 10 ⁻⁵	.95227 .62527 .70271	18,000 14,000 14,000
	Tumblin	g Flechettes	
D30 A30 A5	1.1515 x 10 ⁻⁵ 3.665 x 10 ⁻⁵ 1.0349 x 10 ⁻⁵	•64957 •65548 •77940	18,000 14,000 14,000

TABLE IX

(SECRET) Parameters (a,n,b) for Curve of Phk

(Defense 30 seconds, 100% incapacitation) (U)

(Soldier with helmet and winter clothing)

Part of Body			•	
1 01 1 10 01	a	<u> </u>	<u>b</u>	<u>n</u>
·	<u>s</u>	teel Fragment		-
Head and Neck Thorax Abdomen Pelvis Arms Legs Entire Body	2.5119 x 10 2.9296 x 10 3.1355 x 10 2.0858 x 10 7.8606 x 10 7.5119 x 10 1.4411 x 10	93259 5 .62903 5 .62738 -47771 76824	0 50,000 310,000 245,000 245,000 1,000,000 66,000	.0651 .1304 .1065 .1156 .2045 .3778
	Non-T	umbling Flechette		
Head and Neck Thorax *Abdomen *Pelvis	5.1500 x 10 ⁻¹ 1.1659 x 10 ⁻¹	8 7 1.15801 7 .96667	0 48 , 500	.0651 .1304
*Arms				
*Legs Entire Body	5.9648 x 10 ⁻⁶	95227	18,000	
	Tum	oling Flechette		
Head and Neck Thorax *Abdomen *Pelvis *Arms	4.0546 x 10 ⁻ 3.4494 x 10 ⁻	3 .40206 5 .64419	0 48 , 500	.0651 .1304
*Legs Entire Body	1.1515 x 10	.64957	18,000	

^{*} Insufficient data points to compute these values.

APPENDIX C

(SECRET) INDEX AND CURVES OF ${\bf P}_{\bf hk}$ VERSUS PROJECTILE WEIGHT AND STRIKING VELOCITY (U)

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INDEX OF FIGURES

P_{hk} versus mv^{3/2}

for

Steel Fragments, Stable and Tumbling Flechettes

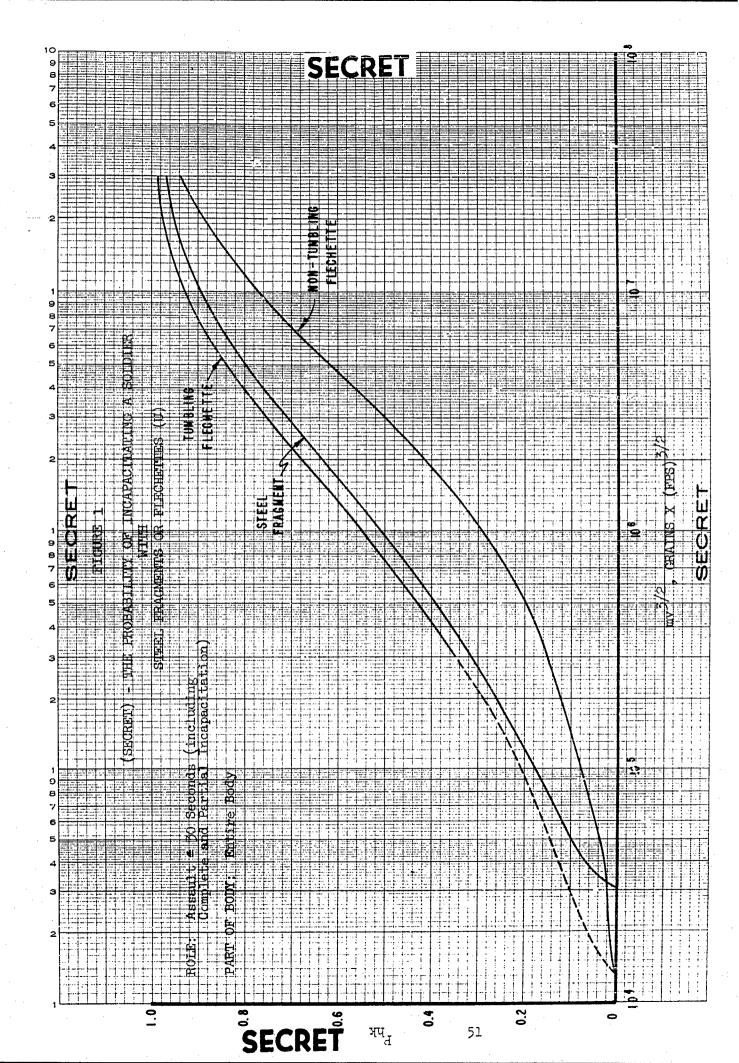
Fig. No. Part of Body Considered (Soldier is assumed to be clothed in Winter Uniform with Helmet and Boots.) Assault ≤ 30 seconds (including complete and partial incapacitation) 1 Entire Head and Neck Thorax Abdomen Pelvis Arms Legs Defense ≤ 30 seconds (including complete and partial incapacitation) 8 Entire 9 Head and Neck 10 Thorax 11 Abdomen 12 Pelvis 13 Arms Legs Assault ≤ 5 minutes (including complete and partial incapacitation) 15 Entire 16 Head and Neck 17 Thorax 18 Abdomen Pelvis 19 Arms 20

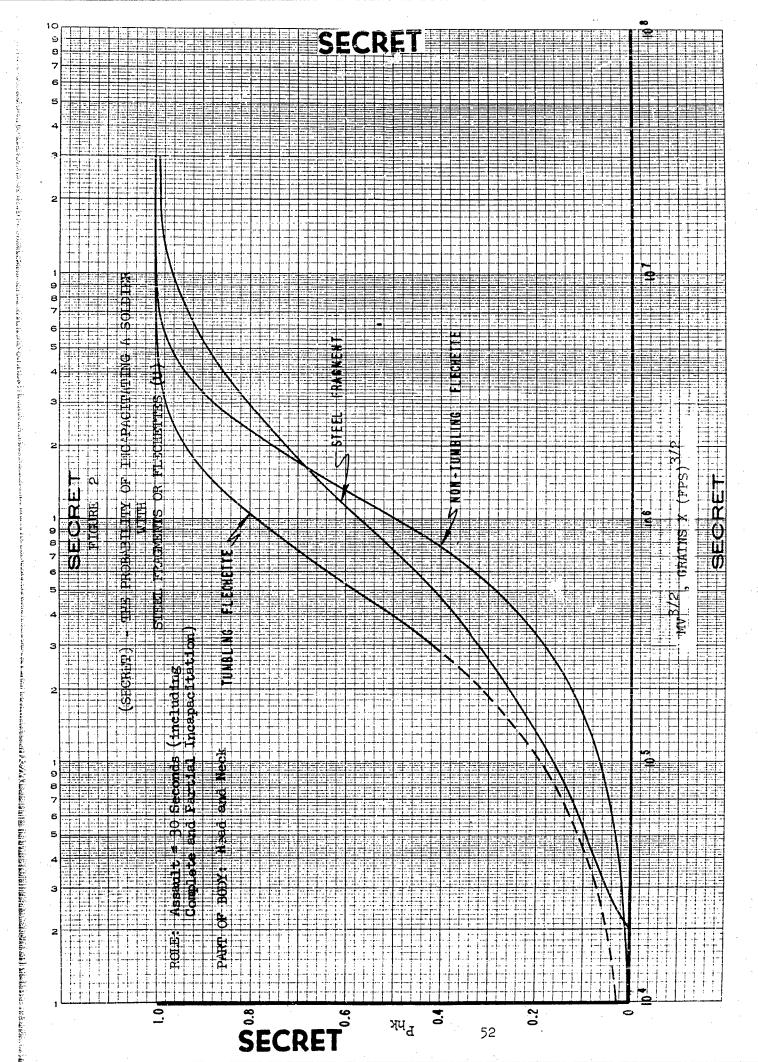
Legs

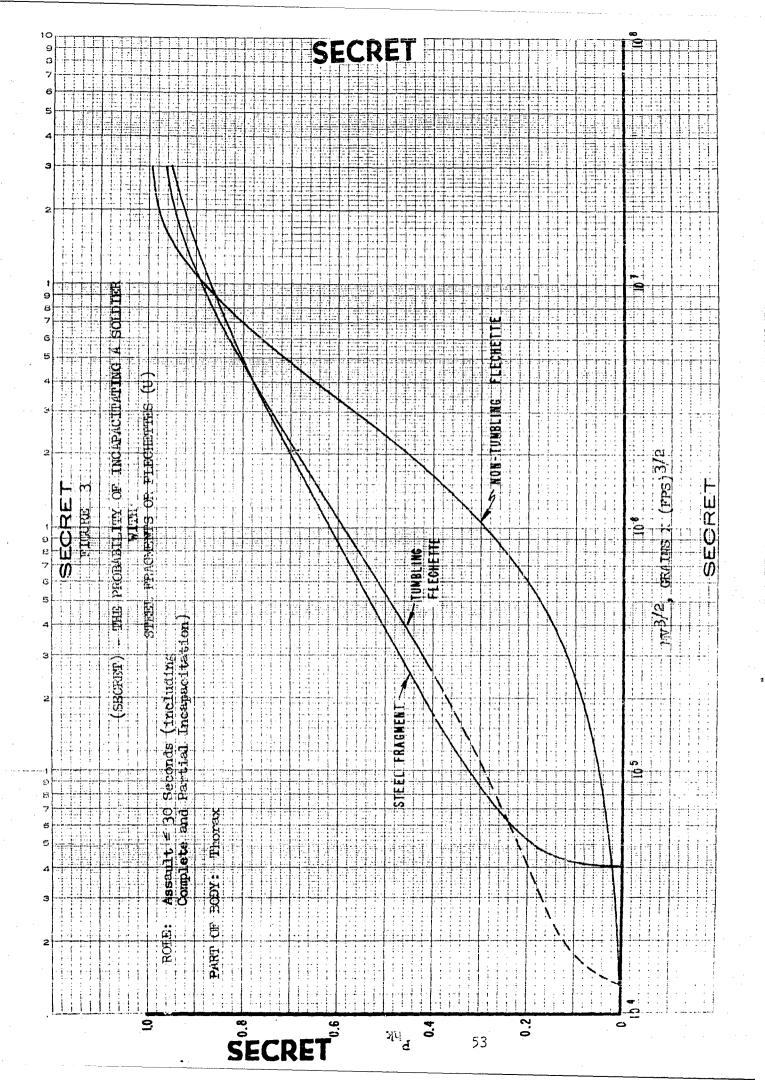
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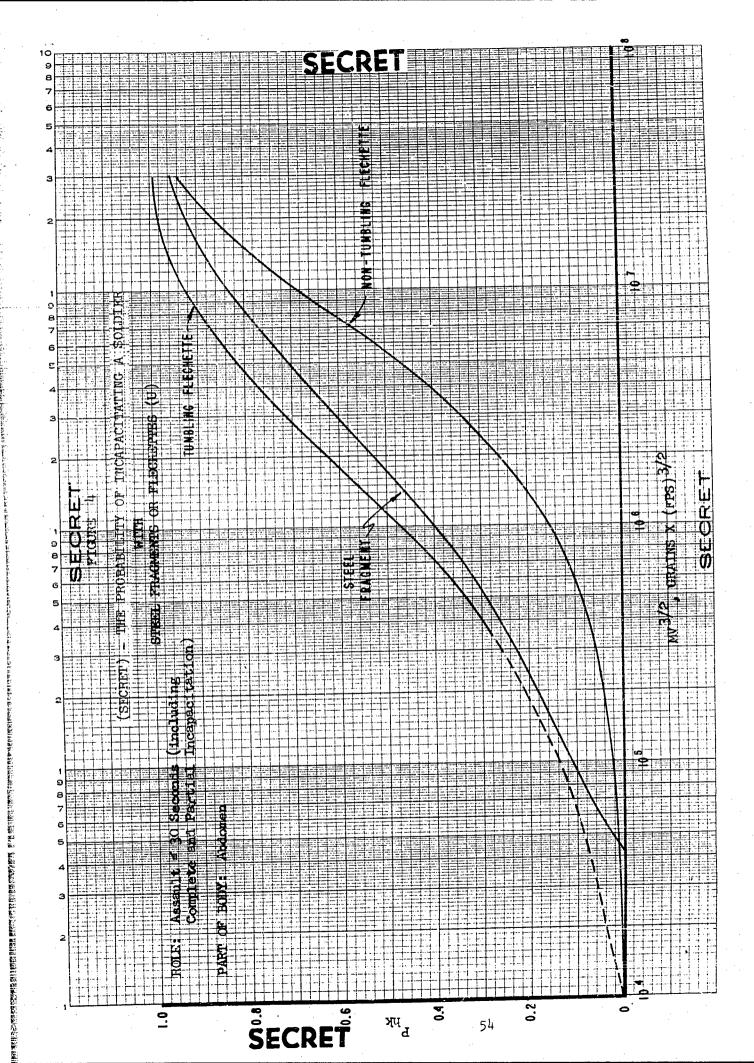
Defense < 30 seconds (100% incapacitation only)

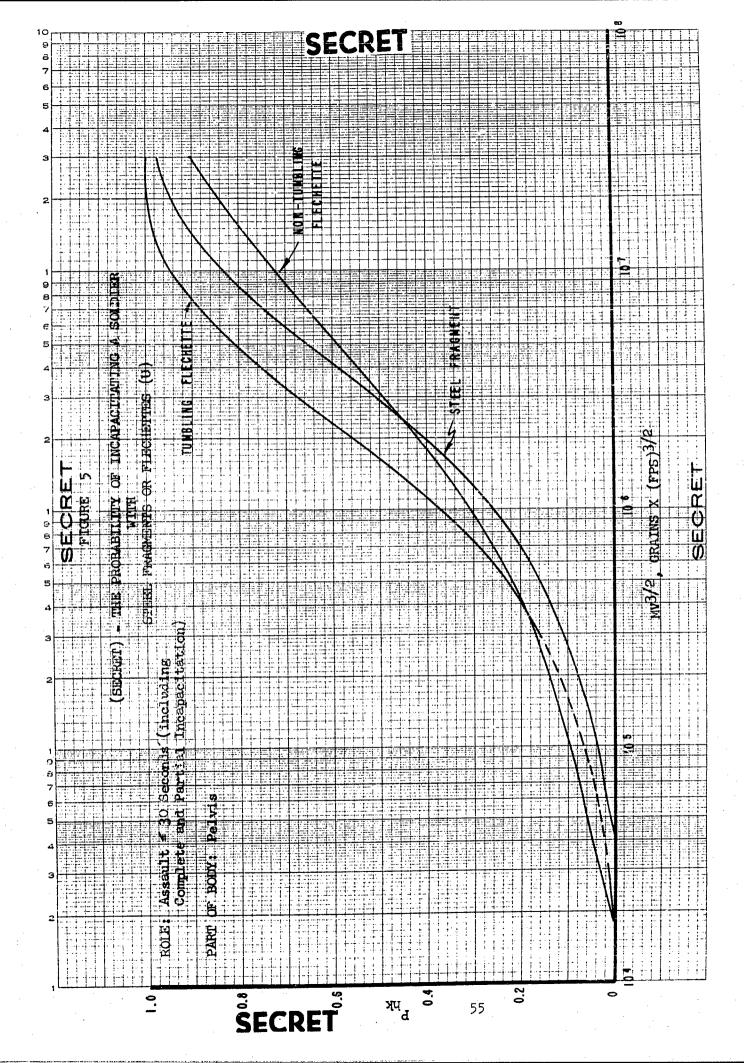
22	Entire Body
23	Head and Neck
24	Thorax
25	Abdomen, Fragment only
26	Pelvis, Fragment only
27	Arms, Fragment only
28	Legs, Fragment only
	100% Incapacitation Only
29 30 31	Assault < 30 seconds Defense < 30 seconds Assault < 5 minutes

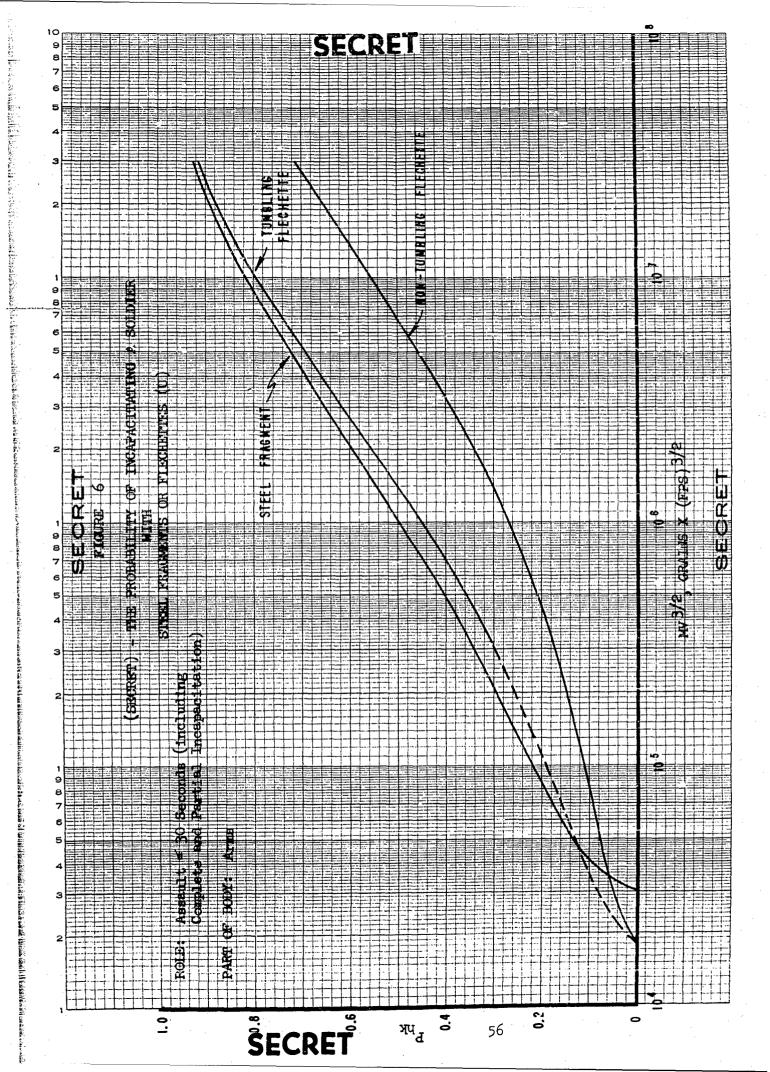


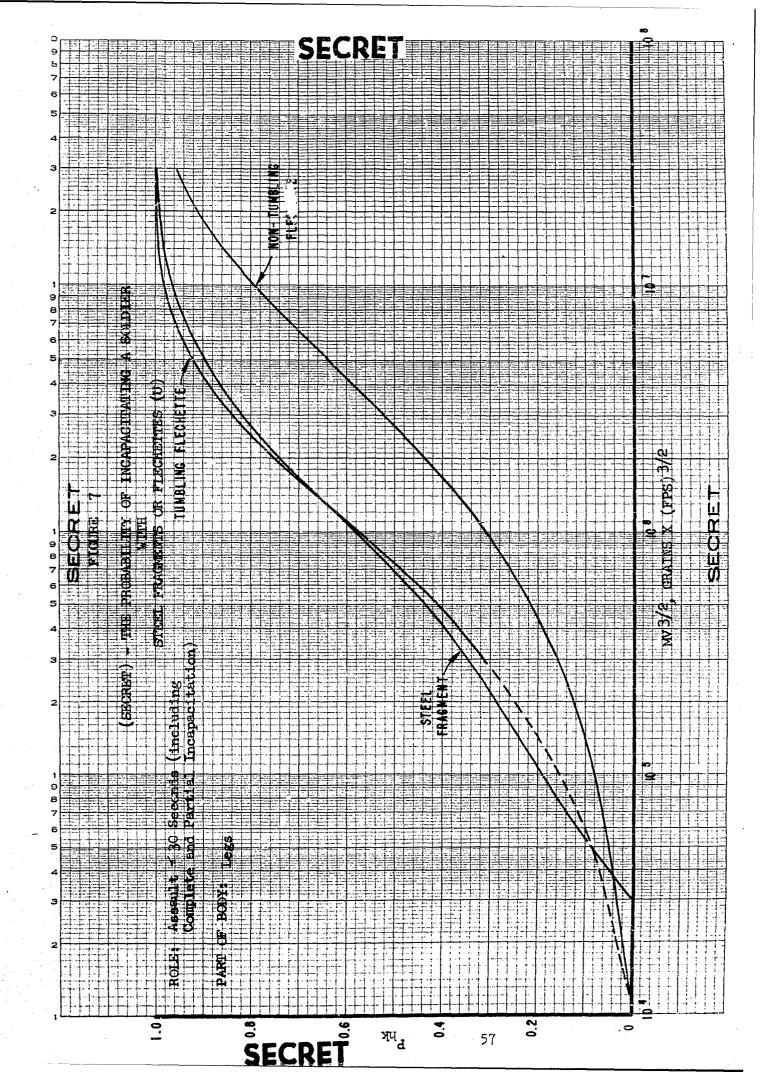


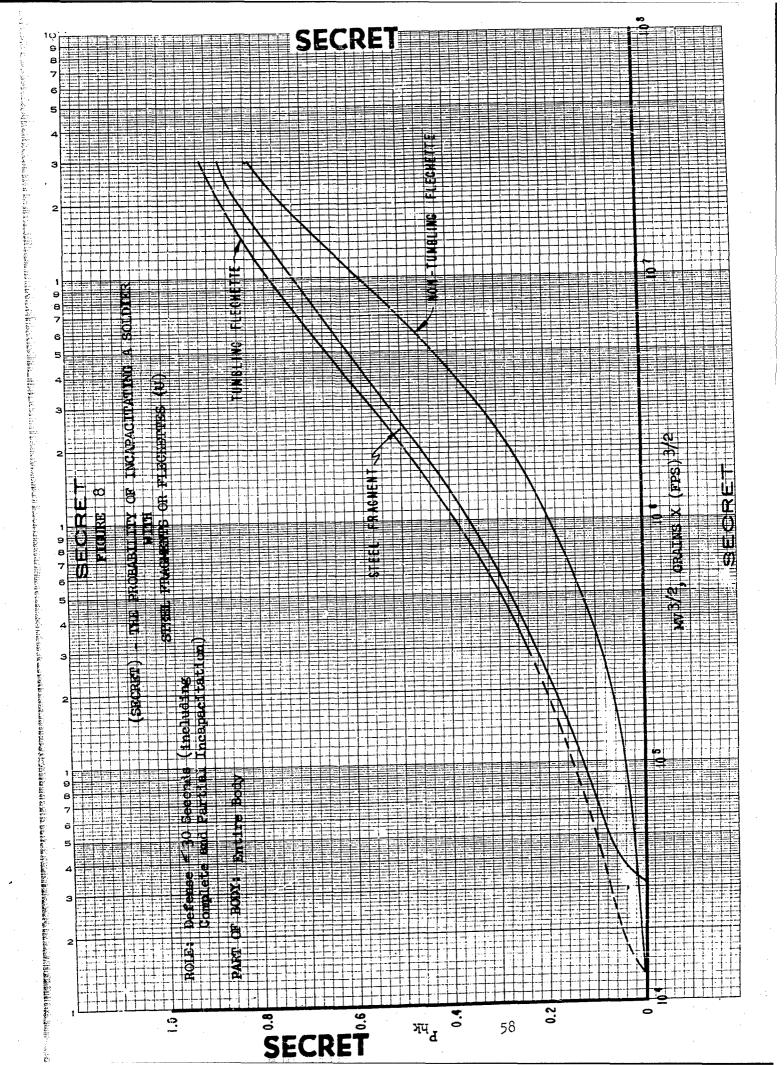


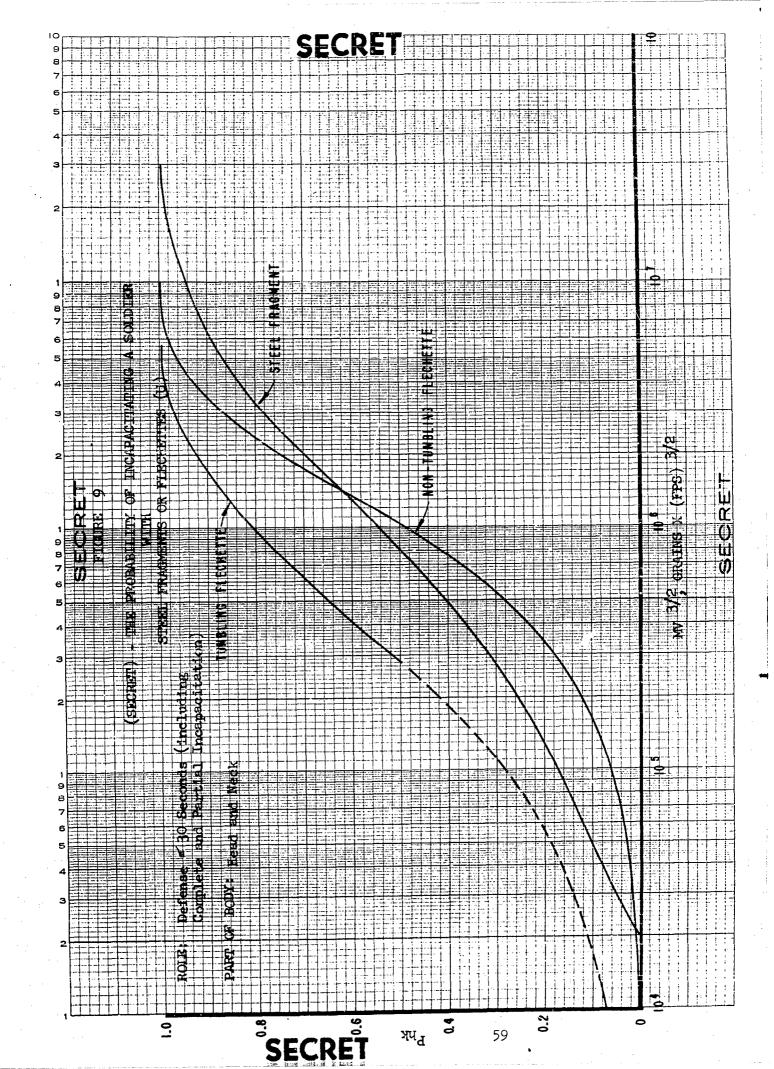


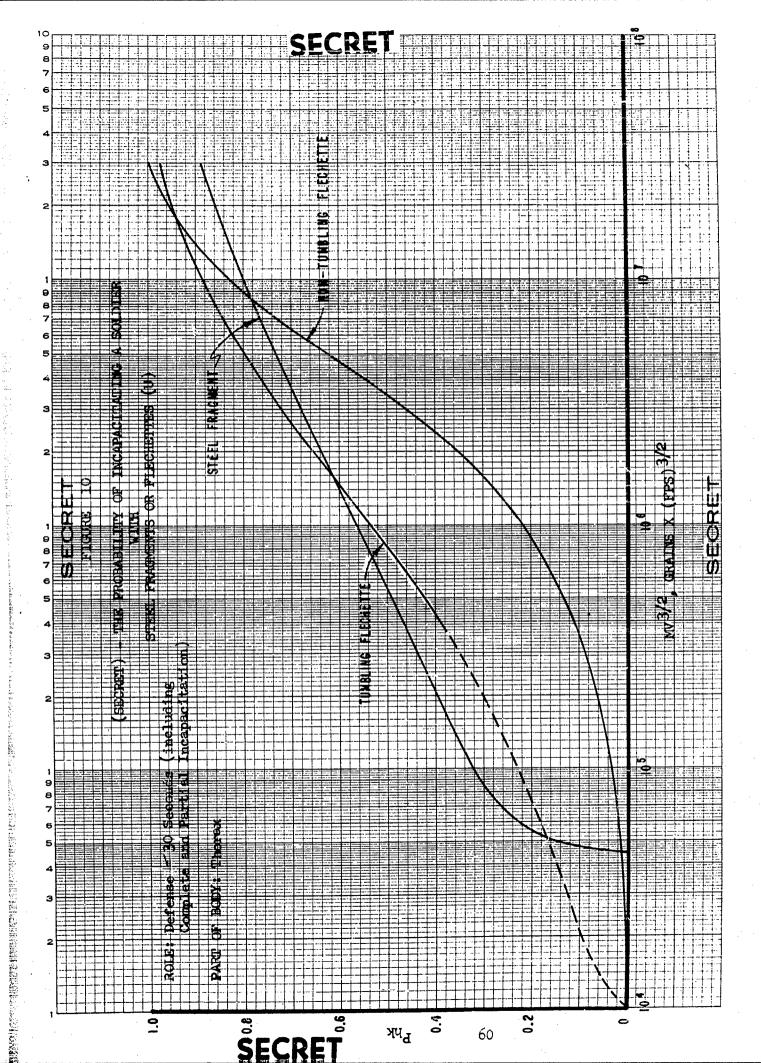


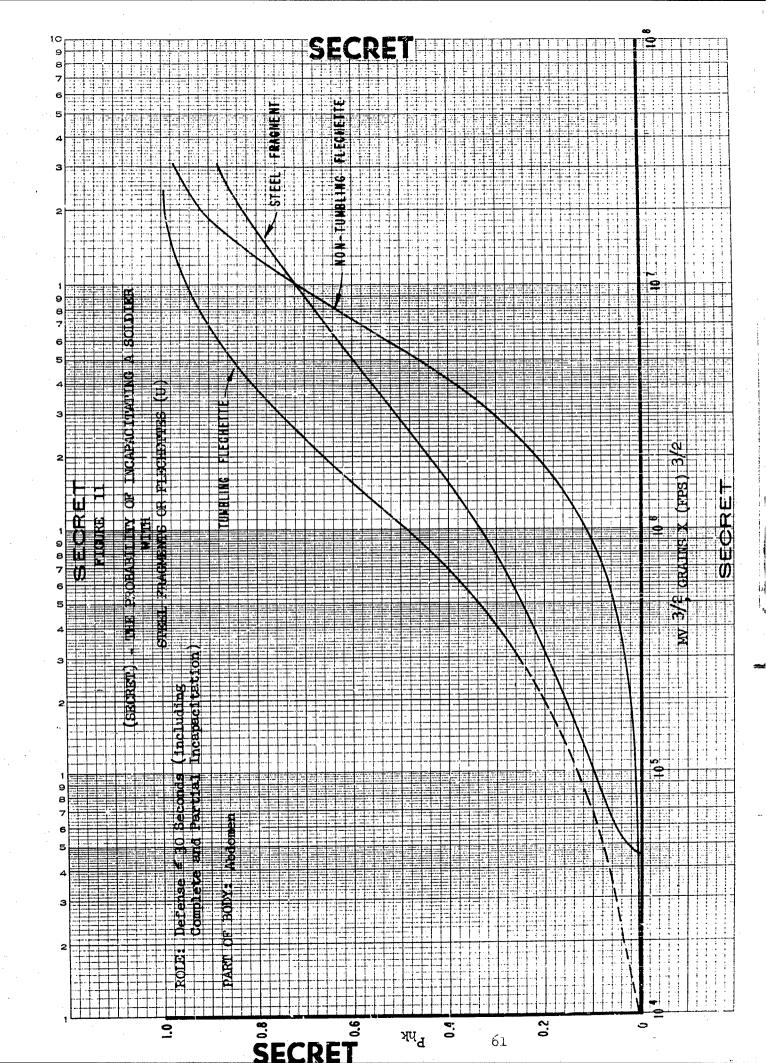


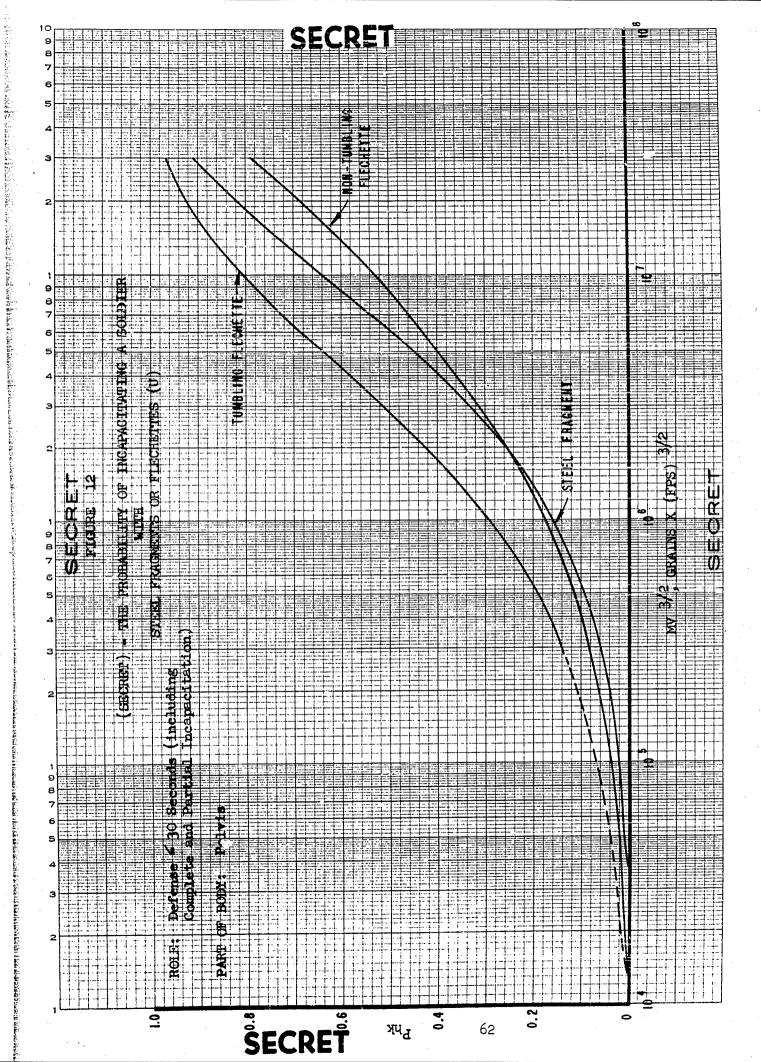


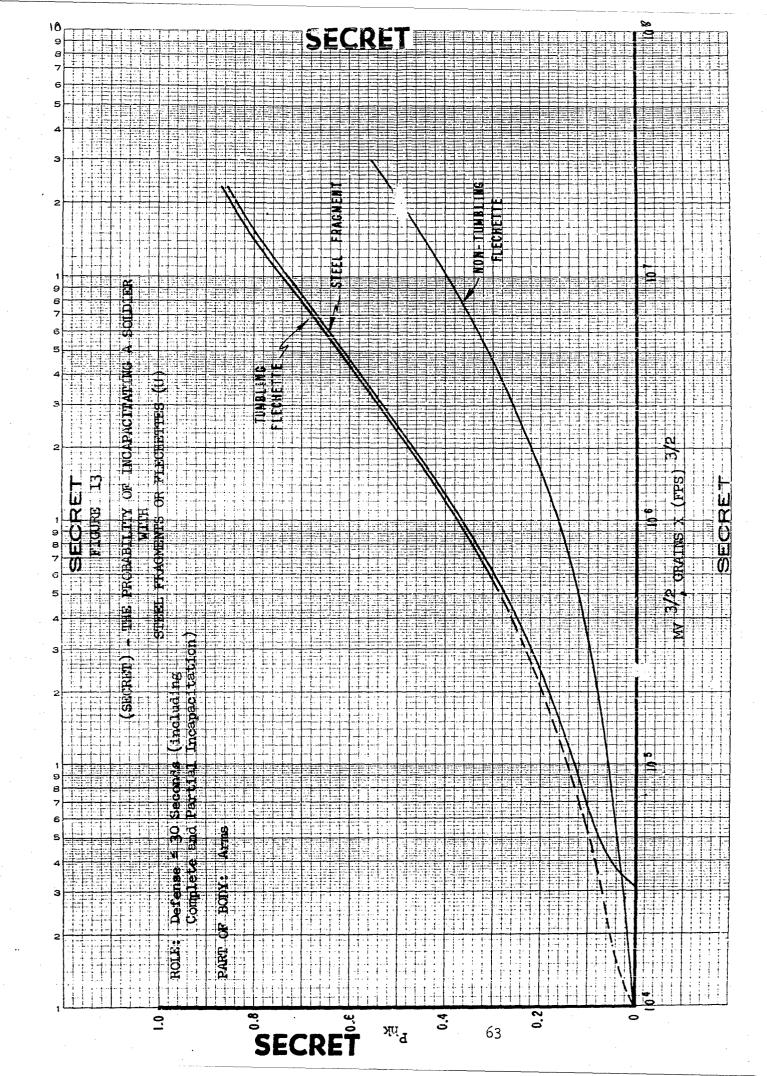


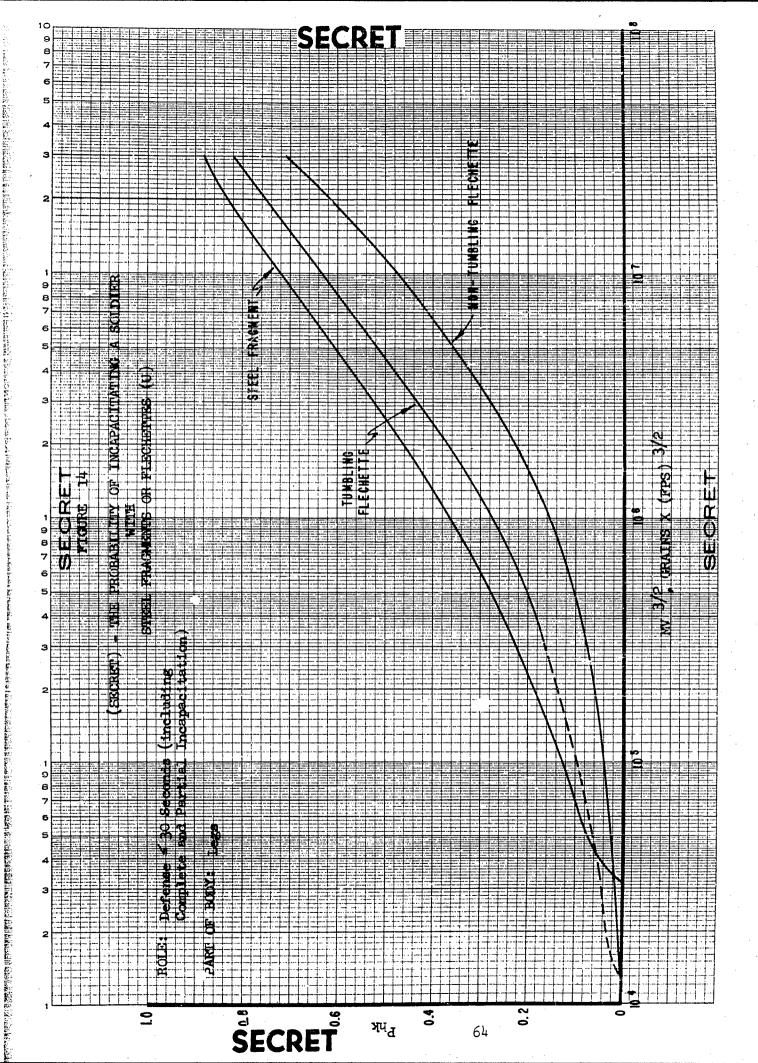


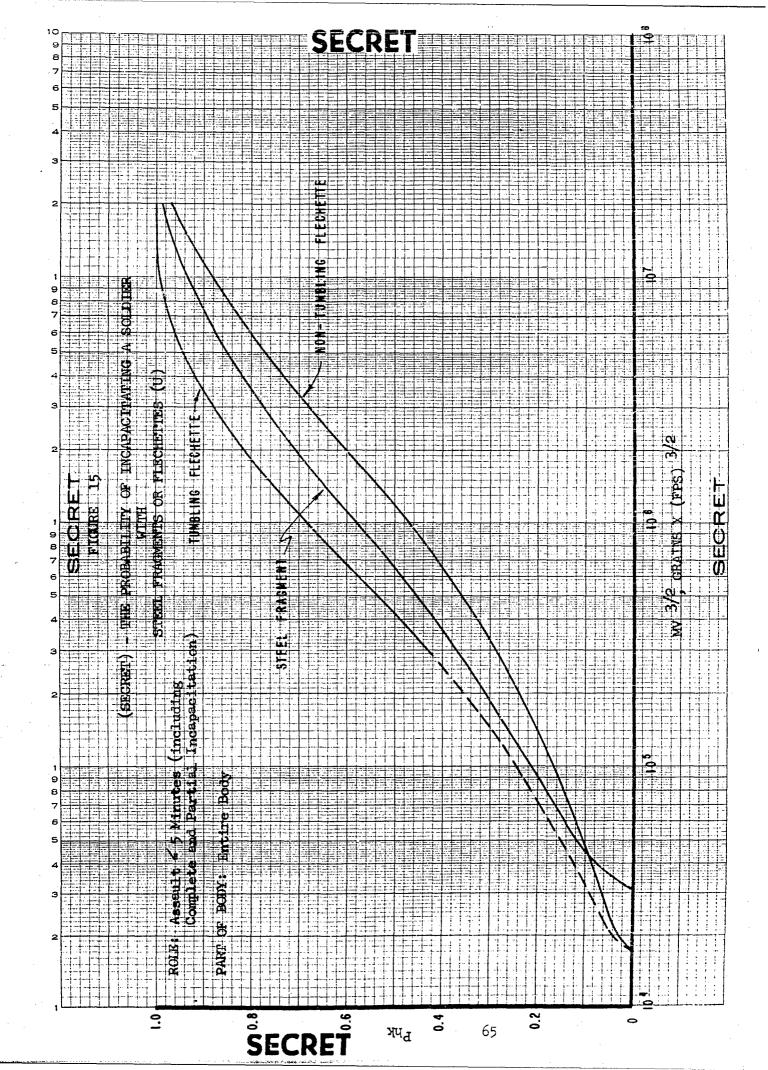


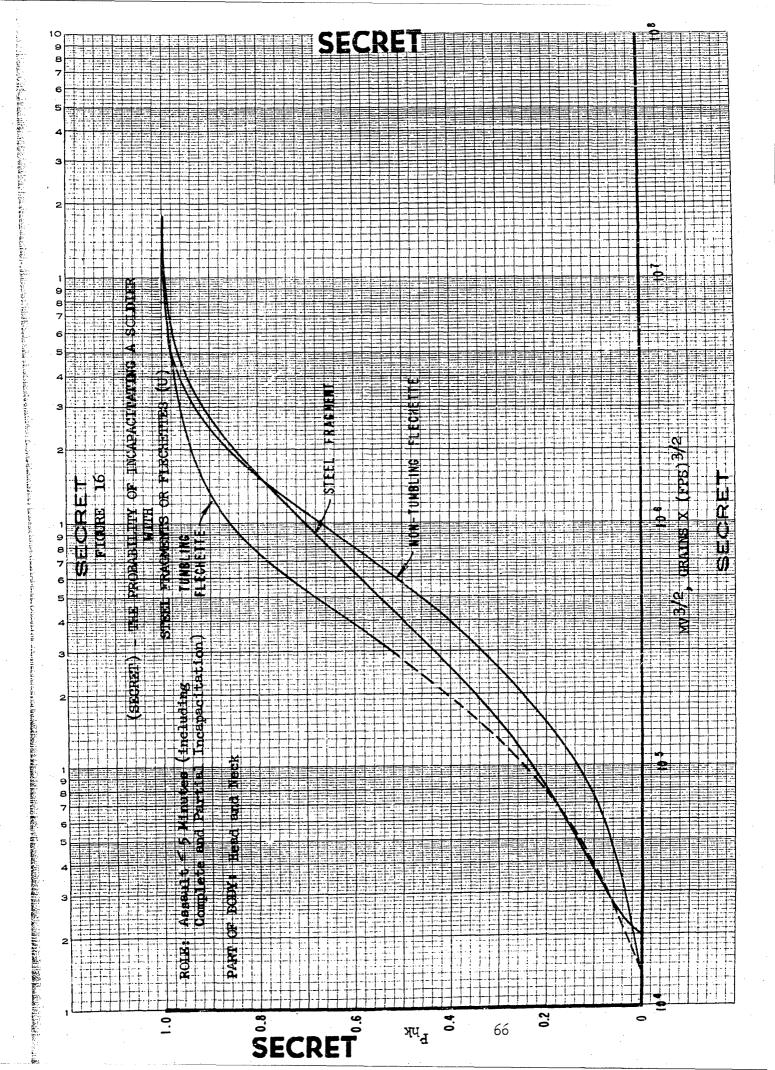


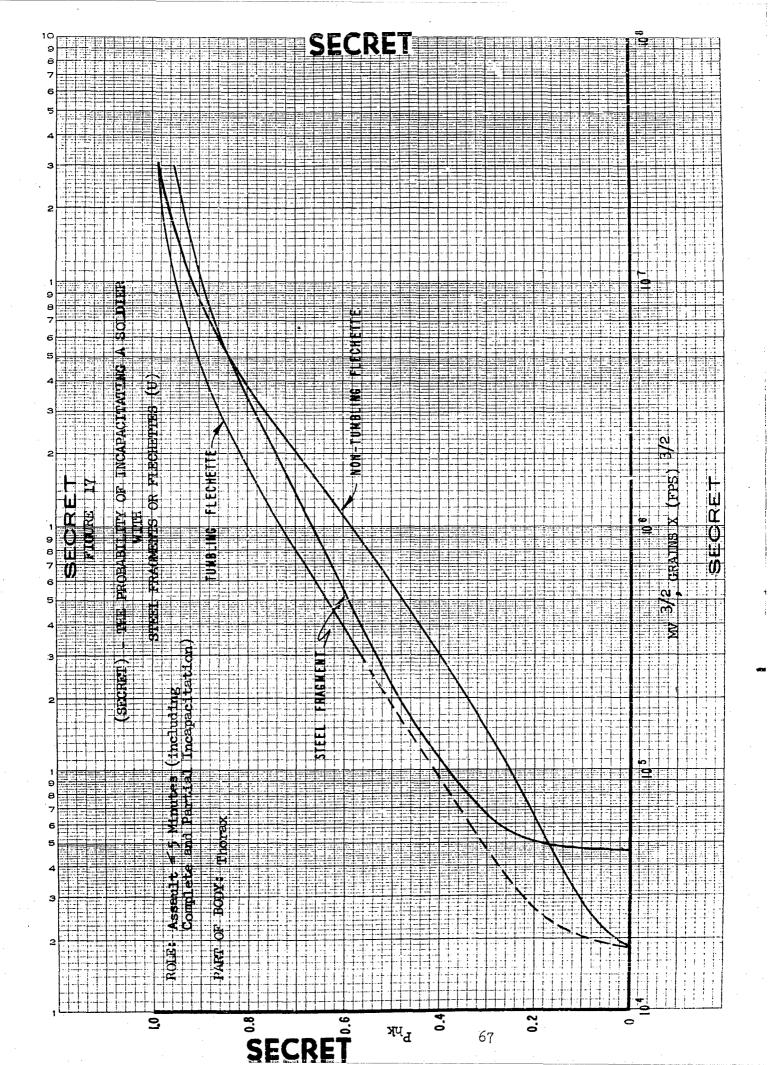


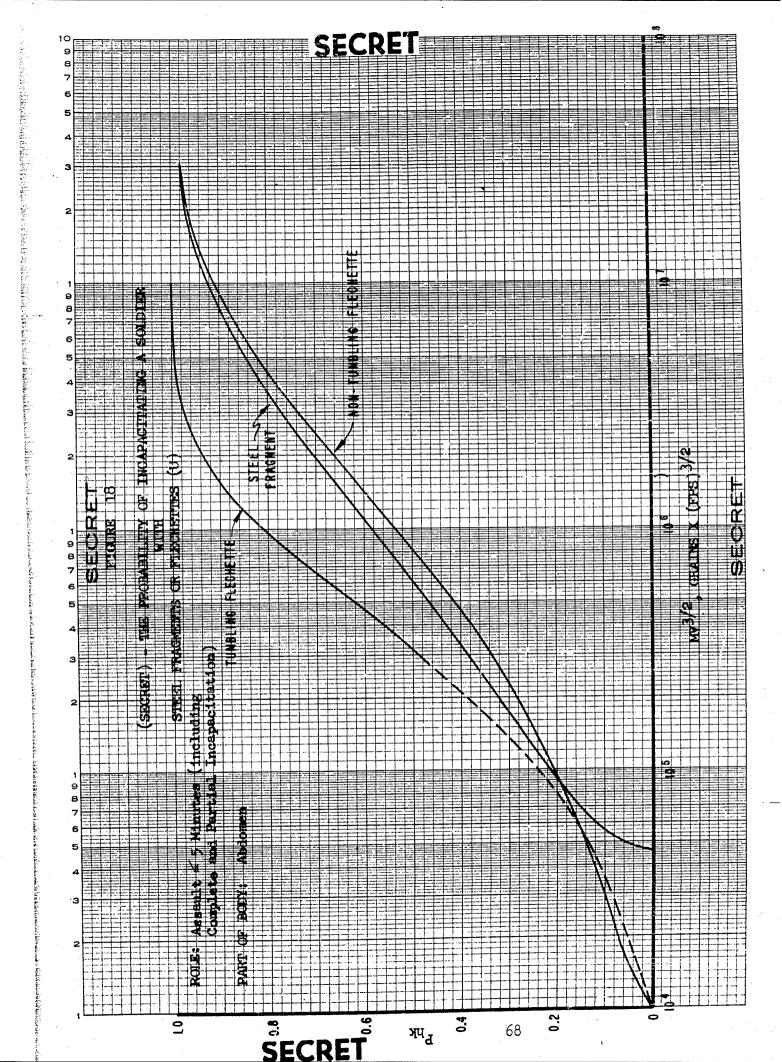


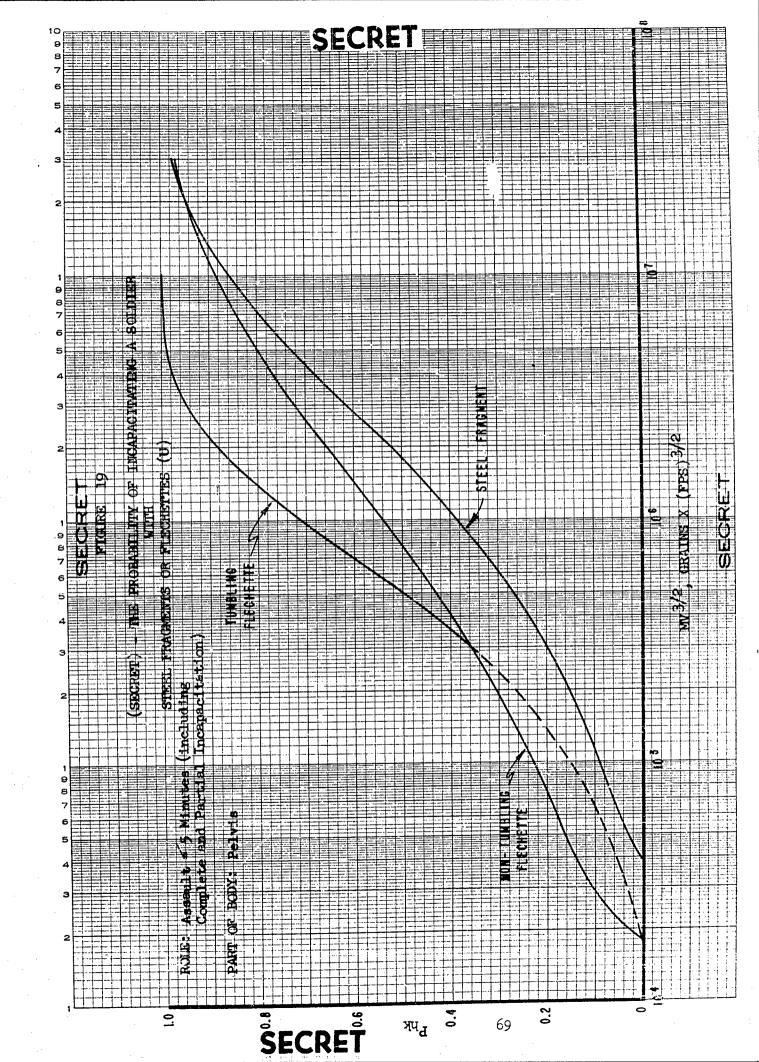


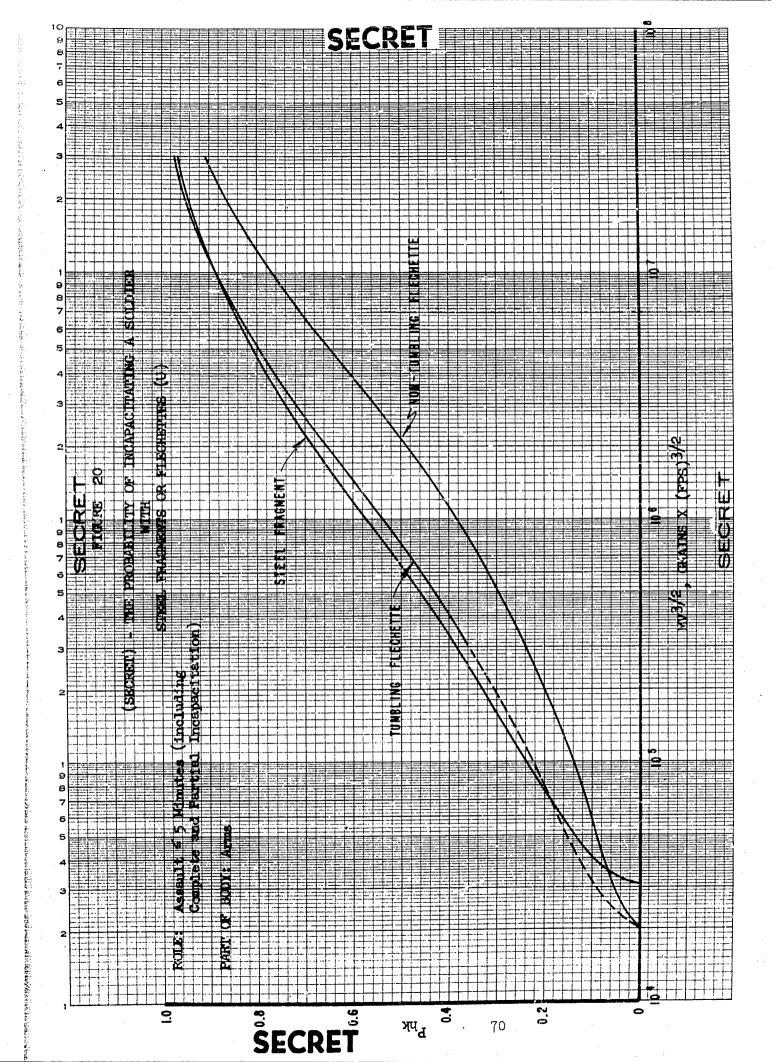


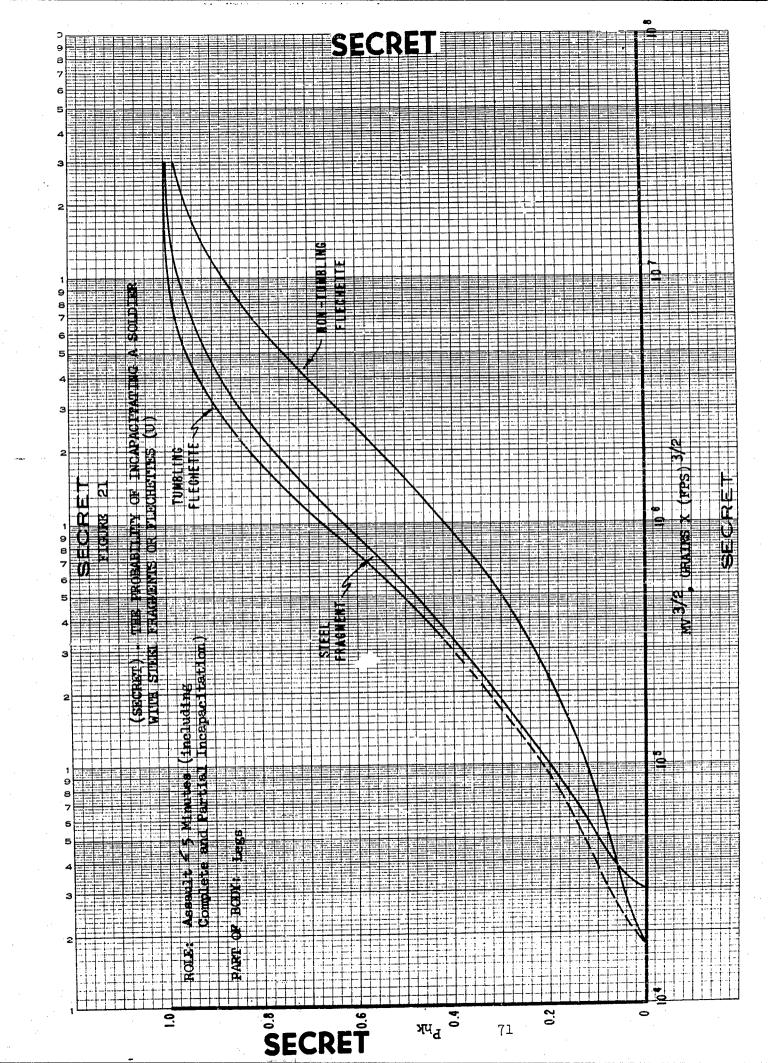








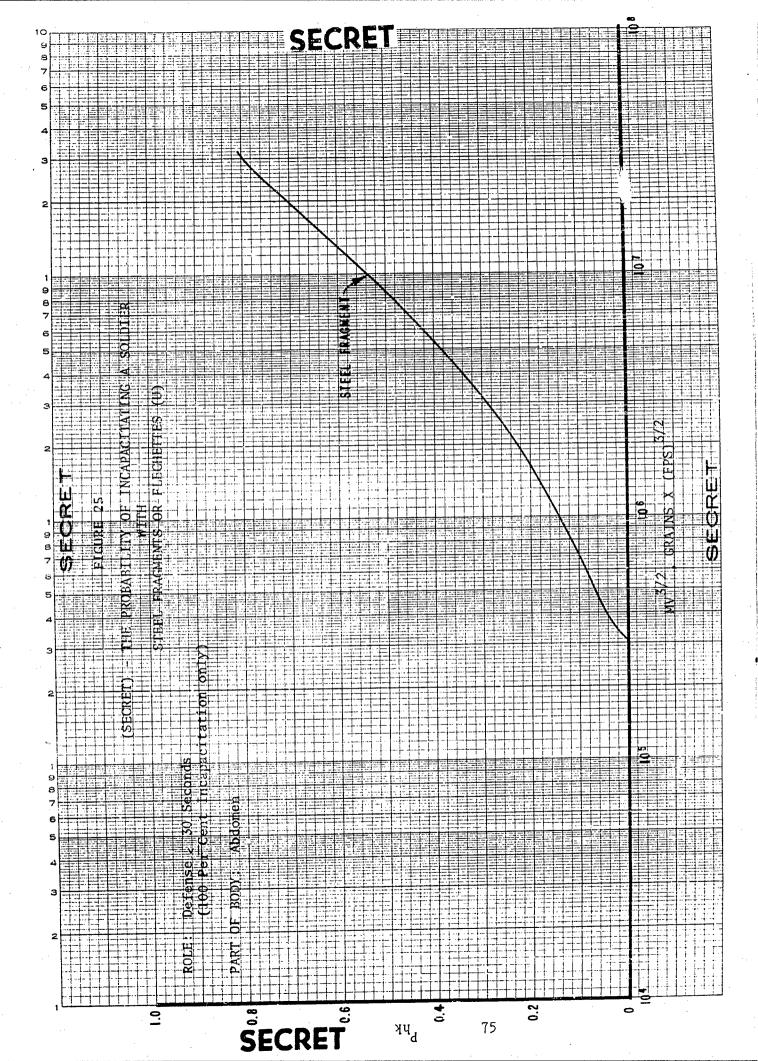


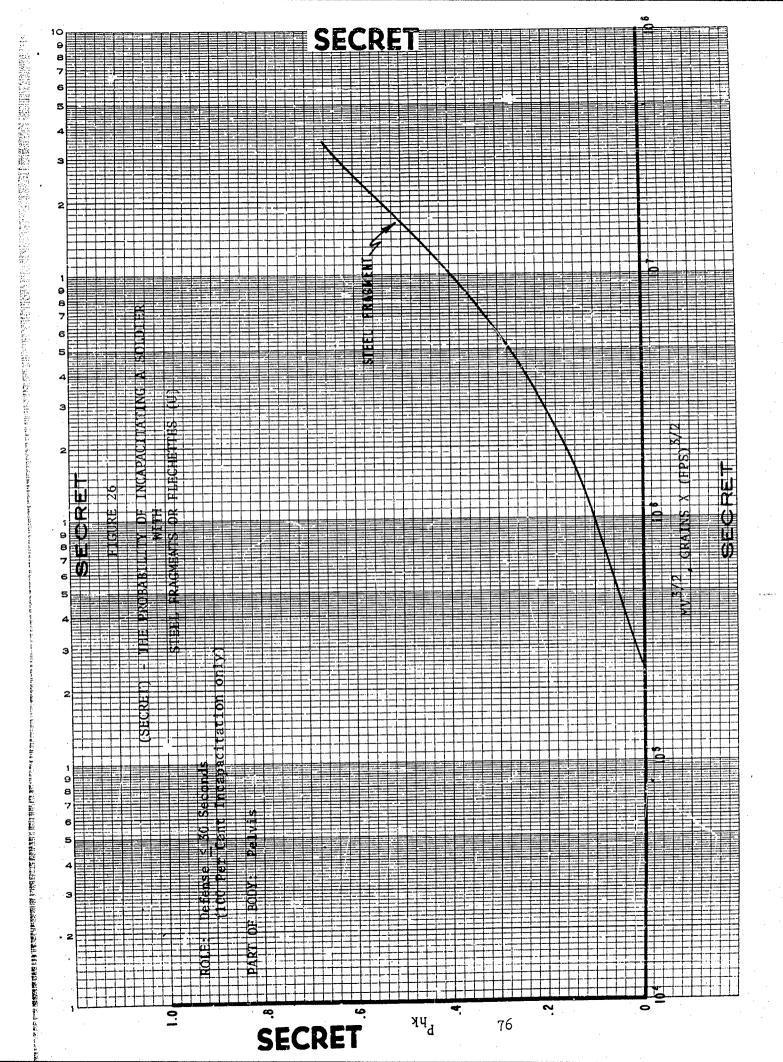


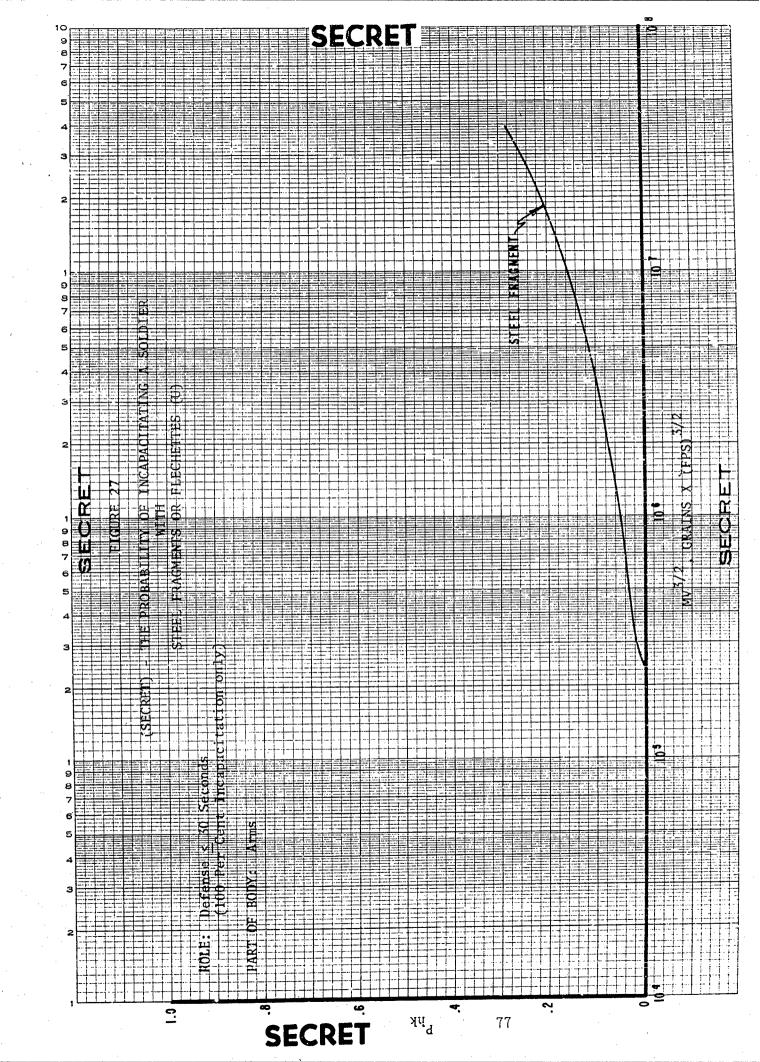
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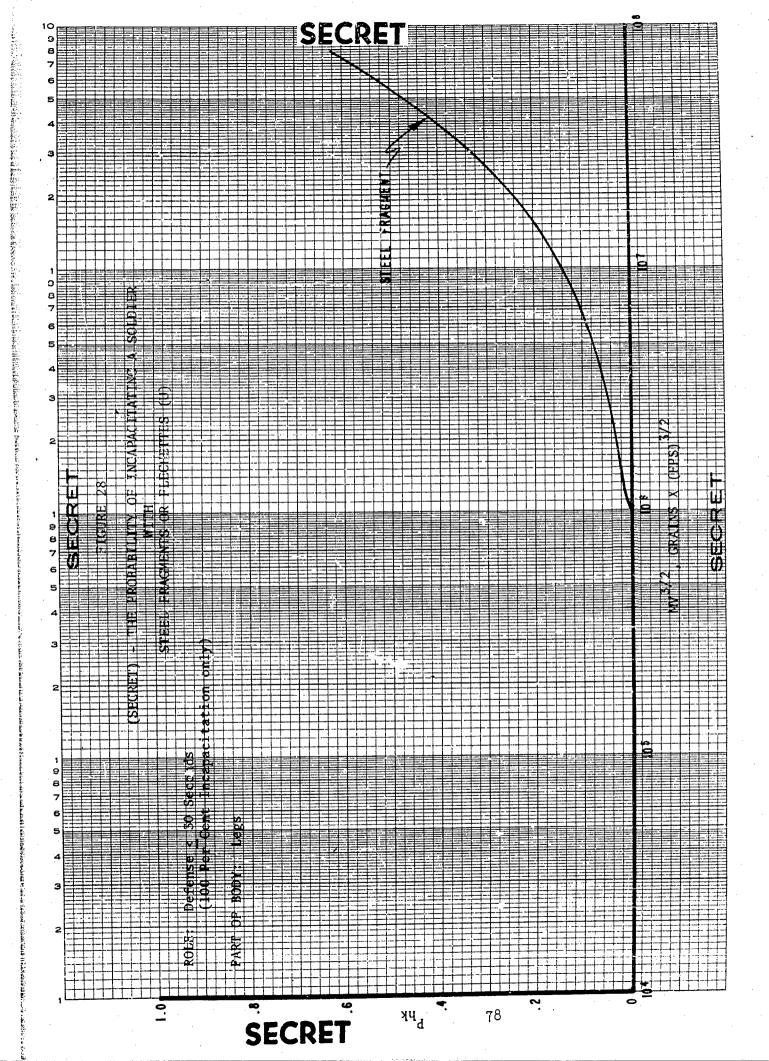
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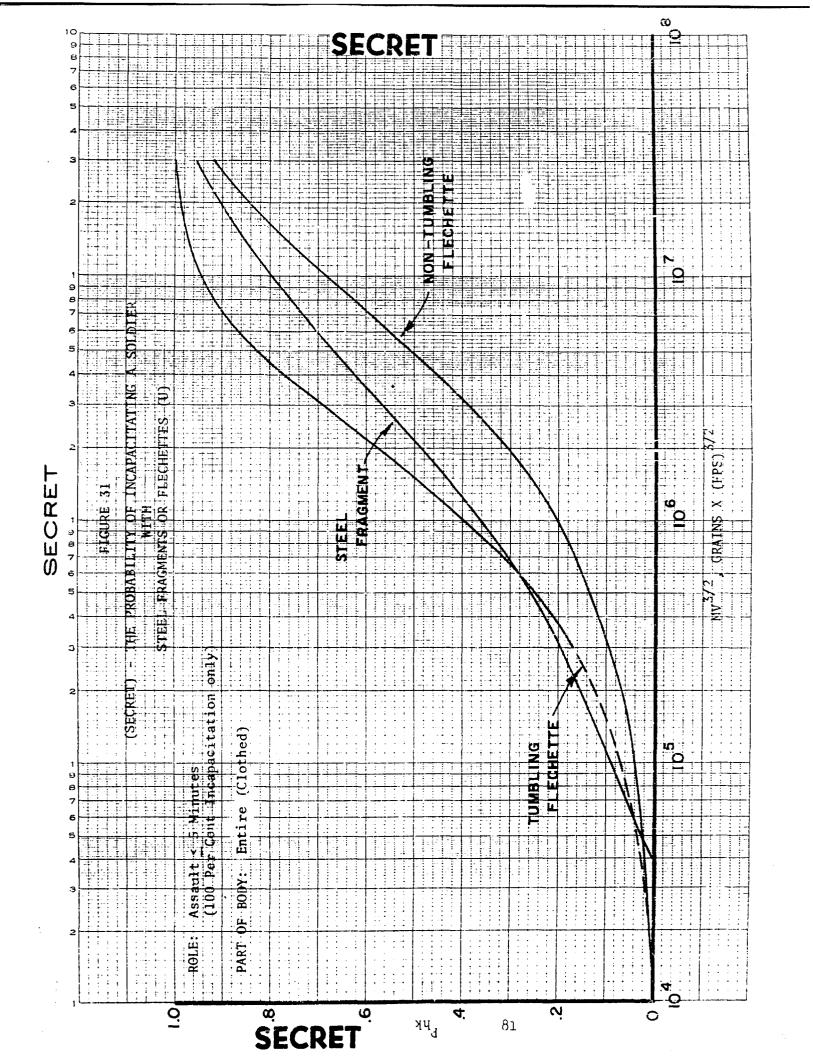








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13. ABSTRACT							

Presented are estimates of the conditional probabilities, P_{nk} that random hits with a standard series of homologously shaped, steel flechettes, will incapacitate the soldier. The functional dependence of P_{hk} on the weight, m, and initial striking velocity, v_o , of the flechette is given by an expression involving m, v_o and parameters a, b and n, whose values are determined from the tactical situation and time at which incapacitation is to ensue. Also presented are estimates, P_{hk} for chunky steel fragments. Although these latter criteria appear in other ERL publications, they are included for purposes of consolidation. (U)

Unclassified

Security Classification			LINK A		LINK B		LINK C	
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Flechettes								
Incapacitations								
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