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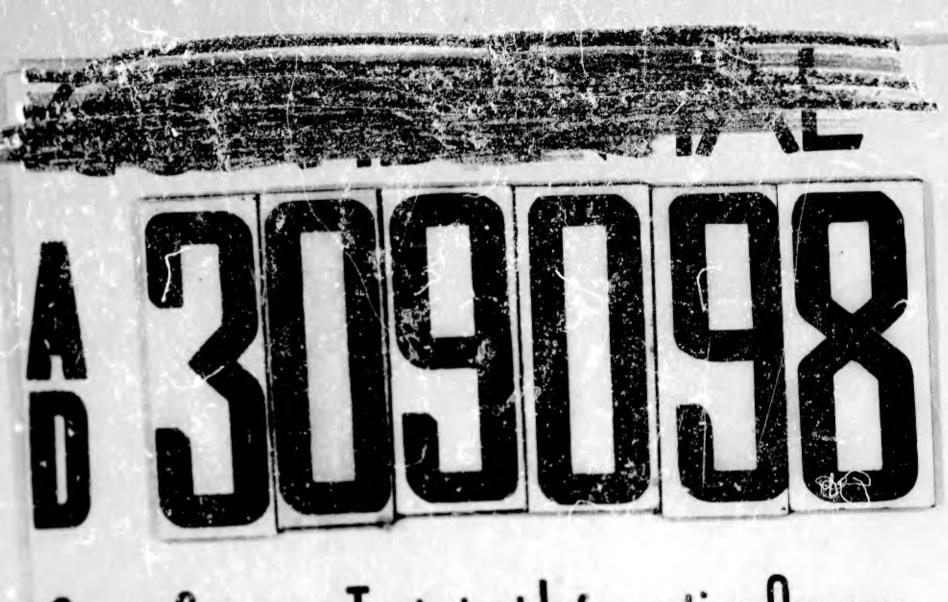
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IN SECURITY PROGRAM REGULATION

DATED - JULY 1972

DOD 5000.1R & EXECUTIVE ORDER 11652 (EXECUTIVE ORDER 10501 AMENDED)

Defease Decomentation Center Defease Supply Agency Cameron Station Alexandria. Virginia 22314

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# Armed Services Technical Information Agency

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ELECTRONIC CONTROL AND GUIDANCE DIVISION

REPORT ON

TESTS OF GUN DATA COMPUTER, T29E2 (U)

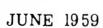


First Report On Ordnance Project No. TR5-5047

(D. A. Project No. 514-03-001)



E. P CASSIDY







Aberdeen Proving Ground

Maryland

U. S. ARMY ORDNANCE
DEVELOPMENT AND PROOF SERVICES
ABERDEEN PROVING GROUND
MARYLAND

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TESTS OF GUN DATA COMPUTER, T29E2 (U)

First Report on Project No. TR5-5047

Dates of Test: July 1957 to October 1957

#### ABSTRACT (G)

The Gun Data Computer, T29E2, Serial Number 1, was subjected to accuracy, ruggedness, environmental, mechanical, electrical, reliability, and maintainability tests to determine if it would satisfy engineering requirements. The gun data computer satisfied all engineering requirements except those pertaining to extremetemperature tests. The Gun Data Computer, T29E2, Serial Number 1, is satisfactory for "user" tests at normal temperature. It is recommended that the gun data computer be modified as detailed in the body of this report before being considered for complete "user" tests.

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#### 1. (U) INTRODUCTION

The Gun Data Computer T29E2, is a modified version of the Gun Data Computer T29E1. Both computers perform the same functions as the Gun Data Computer, T29, which they supersede, by determining values of deflection, quadrant elevation, and fuze time for the 105-mm howitzers, M2 and M2Al. The Gun Data Computer, T29E2, differs from the T29 and T29E1 in that it may also be adapted for use with the 155-mm howitzer, M1A2, by means of four interchangeable units. The operator performs the functions of and replaces the horizontal control operator, vertical control operator, and computer, described in FM6-40, dated January 1951. In addition to the elimination of the foregoing personnel, the computer makes the artillery fire direction center more efficient by reducing computation errors arising from stress and fatigue of personnel, and by permitting the use of less highly trained personnel than could previously be used in fire direction centers.

#### 2. (U) DESCRIPTION OF MATERIEL

The Gun Data Computer, T29E2, is a transportable, electromechanical instrument capable of computing fire control data for the 105-mm howitzers, M2 and M2A1, and a 155-mm howitzer, M4A2. The computer is part of a fire direction system consisting of a power generator, power conversion unit, one, two, three or six computers, one gunnery officer's console, and a plotting board. For a more detailed description of Gun Data Computer, T29E2, see Reference 1.

#### 3. (C) DETAILS OF TEST

#### 3.1 Procedure

3.1.1 Accuracy Tests. The problems used to check the computer accuracy are listed in Appendix A.

Three types of problems were used for both the 105-mm and 155-mm trajectories. The first tw groups, geometry and ballistic problems, were used to check the performance of the computer in computing the effects of nonstandard meteorological and ballistic conditions. All ballistic and meteorological inputs, except the one involved in the particular test problem, were kept to standard conditions during the test. The third group, miscellaneous problems, includes both high and low angle computations in which the effects of nonstandard meteorological and ballistic effects are cumulative.

- 3.1.2 Ruggedness Tests. The computer, power conversion unit, and ballistic changeover units were mounted securely to the bed of a truck and transported over a 10-mile gravel course. Typical problems were solved before and after the road tests and the results compared with established standards.
- 3.1.3 Mechanical Tests. Tests were conducted to determine if the input controls would be damaged should their limits be inadvertently exceeded. Through the performance of all tests, frequent visual inspections for mechanical failures were made.
- 3.1.4 Electrical Tests. The computer was inspected for shock hazards as well as for overload protection devices.

#### 3.1.5 Environmental and Storage Tests

- 3.1.5.1 High-Temperature Tests. The computer was placed in a test chamber and the temperature raised to \$\frac{125}{\text{OF}}\$. The computer required approximately two hours to reach a stable temperature of \$\frac{167}{\text{OF}}\$ in the \$\frac{125}{\text{OF}}\$ ambient temperature. The exact time could not be determined because of a generator shutdown for refueling. Operational tests were performed on the computer at \$\frac{167}{\text{OF}}\$. The air temperature was then raised to \$\frac{160}{\text{OF}}\$ and the computer was stored at this temperature for a period of four hours with the full impact of solar radiation of an intensity of 360 Btu/sq ft/hr.
- 3.1.5.2 Low-Temperature Tests. The computer was placed in a test chamber and the temperature lowered to -40°F. After an exposure of 72 hours without the benefit of solar radiation, the computer was energized and allowed to warm up for a period of 30 minutes. A test problem was then inserted at 10-minute intervals and all computer outputs recorded for each stage.

At the conclusion of the above test the air temperature was lowered to -80°F for an exposure time of 72 hours. The computer was then allowed to return to room temperature and was checked for malfunctioning and physical damage.

- 3.1.6 Reliability and Maintainability. Throughout the performance of all tests, a log was kept of computer operation. All failures, replacement of parts, and data pertinent to reliability and maintainability were recorded.
  - 3.2 Results

#### 3.2.1 Accuracy lests

- 3.2.1.1 Geometry Problems. The answers obtained by solving the geometry problems with the Gun Data Computer 72982, Serial Number 1, are shown in Appendix 8. The average error in azimuth was approximately two mils for the 105-mm and approximately three mils for the 155-mm trajectories.
- 3.2.1.2 Ballistic Problems. The average error in quadrant elevation (Q.E.) for the 105-am low-angle, normal-trajectory ballistic problems was 1.35 mils with approximately 83 per cent of the answers being within specifications. For the 155-am low-angle, normal-trajectory ballistic problems the average error was 0.68 mil with approximately 94 per cent of the answers being within specifications. The average error for the 105-am high-angle, normal-trajectory ballistic problems was 1.79 mils with approximately 81 per cent of the answers being within specifications. For the 155-am high-angle, normal-trajectory ballistic problems the average error was 1.21 mils with approximately 84 per cent of the answers being within specifications. Detailed results are contained in Appendix B.
- 3.2.1.3 Miscellaneous Problems. The difference between the computer outputs and the correct test directive answers to the problems are listed in Appendix B.
- 3.2.2 <u>Ruggedness Tests</u>. The answers to a test problem inserted into the computer before and after 10 miles of road testing on the Munson gravel course are contained in Appendix B. None of the changes in answers exceeded the maximum permissible errors.

### 3.2.3 Environmental and Storage Tests

3.2.3.1 High-Temperature Tests. The computer required approximately two hours to reach a stable temperature of /167°F in a /125°F ambient temperature. The exact time could not be determined because of a generator shutdown for refueling.

The errors in test problem answers, after the computer had stablized for 2 hours in a \$\frac{125}{9}\$F ambient temperature, are listed in Appendix B. All seven range errors were greater than 10 meters; four out of seven azimuth answers were greater than 1 mil; three out of seven fuze errors were greater than 1/10 second; all seven Q.E. answers were greater than 1 mil.

After the computer was stored for 4 hours at a \$150°F ambient temperature with the full impact of solar radiation of an intensity of 360 Btu/sq ft/hr and then brought back to room temperature, two deficiencies were noted:

- a. The paint on the Front of the 105-mm fuse unit had blistered in the intense heat.
- b. The rear portion of the weight-of-projectile potentiometer had become open-circuited.
- 3.2.3.2 Low-Temperature Tests. The computer required approximately three hours to reach a stable temperature of \$\frac{200}{100}\$ in an ambient temperature of \$\frac{-400}{100}\$. This temperature reading was obtained from a thermocouple temperature measuring device placed just inside the rear panel of the computer behind the amplifier bank. The exact time of reaching this stabilizing temperature could not be determined because of a 5-minute generator shutdown for refueling.

The errors in the test problem answers, after the computer was allowed to warm up for 3 hours and 20 minutes in a -40°F ambient temperature, are listed in Appendix B. Six out of seven range answers were greater than 10 meters; four out of seven azimuth answers were greater than 1 mil; two out of seven fuze errors were greater than 1/10 second; three out of seven Q.E. errors were greater than 1 mil.

After the computer had been stored at -73°F for a period of 72 hours and brought back to room temperature, it was found that the plastic sheathing on the cable connecting the meterological panel to the main frame had become brittle and cracked in the extreme cold.

- 3.2.4 Mechanical Tests. Tests were made to exceed the operating limits of the input controls to determine if the controls would be damaged should the limits be inadvertently exceeded. The results of this test failed to show any damage to the controls.
- 3.2.5 <u>Electrical Tests</u>. All power and lighting circuits were found to be properly fused.
- 3.2.6 Reliability and Maintainability. The following failures were noted during the course of the tests:
  - a. An open wire developed on the 105-mm quadrant elevation unit.
  - b. The paint on the front of the 105-mm fuze unit had blistered in the intense heat of the high-temperature test.
- c. The rear portion of the weight-of-projectile potentiometer had become open-circuited during the high-temperature test.

4. (c) concludions

Gun Data Computer, Thin, Berial Busher 1, atisfied all engineering requirements except those pertaining to extreme-temperature tests.

Gun Data Computer, T2922 is satisfactory for "user" tests at normal temperatures.

#### 5. (C) RECOMMENDATIONS

Heaters should be installed on all Gun Data Computers, T29E2, intended for extreme cold weather operation.

The existing weight-of-projectile potentione ter should be replaced by one which is more reliable and unaffected by large temperature changes.

A more flexible type sheathing should be used to replace the present plastic sheathing on the cable from the met panel.

lights on the fuze unit indicator should be placed in a more easily accessible position.

All servos containing limit stops should be equipped with slip clutches.

SUBMITTED:

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SP3, Ord Corps

Test Director

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Chief, Research and Engineering

Projects Branch

SAUL TARAGIN

Chief, Electronic Control and

Guidance Division

APPROVED:

H. A. NOBLE

Assistant Deputy Director

for Engineering Testing

Development and Proof Services

#### REFERENCES

- 1. Notes on Development Type Material, FCDD-294, Gun Data Computer, T29El, Pelock Instrument Corporation, College Point, Long Island, New York.
- 2. FM 6-40 Field Artillery Gunnery dated January 1950.
- 3. FT, Howitzer, 105-mm, M2Al and M4, FT 1054-4, dated July 1951.
- 4. FT, Howitzer, 155-mm, MM and M1, FT 155 Q-2, dated April 1944.

#### APPENDICES

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WAR DEPARTMENT OFFICE OF THE CHIEF OF ORDHANCE

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SUBJECT: Test Directive - Gun Data Computer, TOOD (U)

TO:

Cormanding General Aberdeen Proving Ground Maryland

ATTN: ORDGB-AA-DMPS

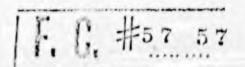
- 1. This pertains to Ordnance Project TR 5-5047 Priority 1C.
- 2. Objective: To determine whether Gun Data Computer, T29E2 is suitable for submissior to the U.S. Army Artillery Board as an item proposed for standardization.
  - 3. Materiel Required:
    - a. Gun Data Computer, T29E2
    - b. Power Conversion Unit
    - c. Dummy Gunnery Officers Console
    - d. Set of Cabling
    - e. 3 kw 3 ph 400 cycle Engine Generator.

Items a through d with necessary spare parts will be furnished by Frankford Arsenal. Item e is available at your proving ground.

- 4. Technical Characteristics: Gun Data Computer, T29E2 has been developed to furnish output data for conducting firing missions with the 105mm Howitzer M2A2, FT 105-H-4 and the 155mm Howitzer M1A2, FT 155-Q-2. One set each of the following interchangeable units are furnished for each weapon:
  - a. Range Unit

b. Fuze Unit





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- c. Main Control and Charge Switch Units
- d. Nuzzle Volocity Unit
- e. Quadrant Elevation Unit.
- 5. Status: The items listed in paragraph 3 above are expected to be ready for shipment to your proving ground approximately 1 June 1957.

#### 6. Test Procedure:

a. Service Contract: In the event of a major malfunction due to tests being performed, Frankford Arsenal is to be notified immediately. Major repairs will be made by personnel of the contractor, Belock Instrument Company. Your proving ground is authorized to make minor repairs as may be necessary.

#### b. Reference Materiel:

- (1) Test Directive Gun Data Computer T29El, Chief of Ordnance to your proving ground, dated 3 November 1954, file 00/40-23715.
- (2) Notes on Dev. Type Mat. Gun Data Computer T29E2 (with shipment).
  - (3) Appendix A, in 4 parts (inclosed).
  - (4) Appendix B, in 4 parts (inclosed).
- c. Engineering: The data listed in references 6b(3) & (4) above were used by the contractor in conducting acceptance tests. [These data should be checked by your proving ground prior to their use in engineering test problems.) Test problems should include intermediate data as well as the data shown in the inclosed appendices.

#### d. Accuracy:

- (1) The accuracy tests are divided into four parts.
- (a) Geometry Tests: These tests check the Computer accuracy in solving the Azimuth and Range for the three conditions of the Target Grid System for Field Artillery. In addition, the replot portion of the Computer is fully checked.

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Subject: Test Directive - Cun Data Computer, T29.2 (U)

- (b) Ballistic Tests: Thes tests check Computer accuracy in solving for Quadrant Elevation under both normal and abnormal conditions of meteorology, muzzle velocity and projectile weight, for targets both above and below the level of the weapon.
- (c) Combined Tests: These tests combine the problems of a and b above and check the Computer accuracy for a "real" problem with extreme abnormalities including the effects of jump, drift and cross wind. Problems are included for both high and low angle fire.
- (d) Other Accuracy Tests: These tests check the Computer accuracy for the following items:
  - 1 Percentage Range Correction
  - 2 Percentage Fuze Correction
  - 3 Range Spread
  - 4 Fuze
  - 5 Fuze-type Spots.

Note: When testing the Computer for accuracy, all inputs must be checked for proper settings. Unless otherwise specified, these are the settings for standard conditions using center range and P.D. fuze. Geometric and muzzle velocity settings are zero unless otherwise specified. The operator should check to insure that the proper Main Control Unit, Fuze Unit, Q.E. Unit and Muzzle Velocity Unit are being used to conform to the ballistics of the weapon being tested.

- (2) The Geometry Test Problems of Appendix A, Part 1, shall be inserted with the Computer set for standard ballistic and meteorological conditions. The Q.E. and Fuze units are disengaged. The "Survey" position of the Compute Switch is to be used to obtain Range and Azimuth. Upon completion of each problem, the Easting, Northing and Height Replot data is obtained.
- (3) The Normal Trajectory Test Problems of Appendix A, Part 2, for the 105mm Howitzer are inserted with the Computer, set for standard ballistic and meteorological conditions. The range may be inserted using either the Observer Distance or Northing inputs. The range will be read from the range output dial. The height is inserted via the Height input unit. The "Survey" position of the Compute Switch is required. The Quadrant Elevation readings will be recorded. Upon completion of these problems, the

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Normal Trajectory Test Problems of Appendix B, Part 1, for the 155mm Howitzer will be inserted. The test will be conducted in a manner similar to that given above. Noth Quadrant Elevation and Puze readings will be recorded.

- (4) The Abnormal Effect Trajectory Problems of Appendix A, Part 2, for the 105cm Howitzer will be inserted into the Computer. All ballistic and meteorological effects shall be set at standard conditions except for the particular effect under consideration. When inserting meteorological data, all ten lines of the Meteorological Panel shall have the same setting. Range and hold data are inserted as in paragraph 3. The "Survey" position of the Compute Switch is used and the Quadrant Elevation readings are recorded. The Wind Test Problems shall be inserted in such a manner that the Azimuth indication shall be zero mila. For the purposes of this test, a 50 mph Pius Wind shall be considered a Rear Wind and a 50 mph Minus Wind shall be considered to be a Head Wind. The Plus Wind shall be inserted as a 50 mph South Wind on all lines of the Meteorological Panel and the Minus Wind shall be inserted as a 50 mph North Wind on all lines of the Meteorological Panel. Upon completion of these problems, the Abnormal Effect Trajectory Test Problems of Appendix B, Part \_, for the 155mm Howitzer will be inserted. The test will be conducted in a manner similar to that given above. Both Quadrant Elevation and Fuze readings will be recorded.
- (5) The Combined Effects Trajectory Test Problems of Appendix A, Part 3, for the 105mm Howitzer shall be inserted in the Computer. The "Compute" position of the Compute Switch is required. All ballistic and meteorological effects except those specifically noted shall be set at standard conditions. Range, Azimuth, Fuze and Quadrant Elevation shall be recorded. Upon completion of these problems, the Combined Effects Trajectory Test Problems of Appendix B, Part 3, for the 155mm Howitzer shall be inserted. The test will be conducted in a manner similar to that used above.
- (6) The Fuze Test Problems of Appendix A, Part 4, for the 105mm Howitzer shall be inserted in the Computer. Height is set at zero, and all ballistic and meteorological effects are set for standard conditions. Both Fuze and Quadrant Elevation readings will be recorded. Upon completion of these problems, the Fuze Test Problems of Appendix B, Part 4, for the 155mm Howitzer shall be inserted in the Computer. This test shall be conducted in a manner similar to that given above.
- (7) A random selection of several problems from each charge listed in F.T. 105-H-4 shall be used to check the 105mm ballistics with respect to Weight of Projectile, Cross Wind, Drift, and Jump. Jump data to be used is for the 105mm Howitzer M2Al in Carriage M2A2. A random selection

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of several problems from each charge listed in F.T.

to check the 155cm ballistics with respect to Drift

Jump data to be used is for the 155cm Howitzer H1

percentage Range and Puse Corrections will both be
maximum values to insure proper operation. The The se
settings will be tested to insure that a 25 ft. charmen have a target
is being inserted. The Range Spread settings will

\*2C and \*1C to insure that a lange Charge is -10C, respectively.

(8) Accuracy of the Computer Outputs shall be as follows:

Quadrant • 1 mil or the equivalent Elevation - permissible range error.

Range - 

+ 10 meters, + .1% of maximum range or + ½ probable error, whichever is greatest.

Fuze - + .1 seconds for low angle fire; + .2 seconds for high angle fire.

Azimuth - + 1 mil or the equivalent range error.

Discretion will be used when evaluating the results of tests involving problems with large height of target and/or large abnormal ballistic and meteorological conditions since data on probable error for these circumstances are not available. The Q.E. answers to the problems listed in Appendices A and B, Part 2, which lie between the answer listed and the ENIAC value shall be considered acceptable. In Appendix B, Part 2, neither the Fuze answers or the answers for those problems in the 900 or 1200 mil sections will be used in determining the acceptability of the Gun Data Computer T29E2. It should be noted that the basic meteorological and ballistic settings for the problems of Appendices A and B, Part 2, are to be inserted using the F.A. Voltage Test Set in conjunction with the Computer Null Meter.

#### e. Stability:

- (1) The Computer shall be left in the "Standby" condition for a period of thirty minutes. Any changes in Quadrant Elevation, Range, Fuze or Azimuth shall be noted when the switch is thrown to "Compute" at the end of this time.
- (2) The Computer shall remain energized for a period of eight continuous hours during the conduct of the Acceptance Test. The test problem will be inserted at the end of this time and the answers recorded.

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- (3) The Computer will be tested for proper shielding of sensitive components by bringing the operators body or some foreign object close to these components when the instrument is in the case during the solution of a problem.
- (4) The Computer shall be struck by hand to similate bumps which it may receive during normal usage. This will be done during the solution of a problem.
- f. Interchangeability: The ease and facility with which the units listed, paragraph & above, can be inserted and removed is to be determined.
- g. Ruggedness: The Computer, Power Conversion Unit and set of Changeover Ballistic Units shall be securely fastened to the body of a truck and the vehicle then driven at moderate speeds over unimproved dirt roads and/or streets for a distance of ten miles. These units shall then be set up indoors, carefully inspected for physical damage, energized and the test problems inserted.
- h. Ease of Operation: During the conduct of all tests, ease of setting knobs and reading results shall be noted. All dials shall be inspected for proper range of marking, convenient division and adequate lighting. The number of men required to move the Computer will be noted.
- i. Ease of Maintenance: The Computer shall be examined for ease of replacing subassemblies and lights, location and accessibility of test points and cable receptacles.
- j. Shock Hazards: Throughout all tests, the Computer and Power Conversion Unit shall be examined for existing shock hazards. In no case will electrical connection between the cases of these units and either side of the power source be permitted.
- k. Overload Protection Devices: All handwheels greater than two inches in diameter shall contain clutches to prevent damage to the instrument due to turning the handwheel past the limit stops. (All servos containing limit stops shall have similar protection to prevent damage to the servo motor. All power and lighting circuits shall be properly fused.)

#### 1. Environmental Tests:

(1) Storage: The equipment must be capable of safe storage without permanent impairment due to the effects of extreme temperature. The required temperatures for storage purposes are:

Lower limit - 80°F. for at least 3 days duration
Upper limit - 160°F. for periods of 4 hours a day.

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- (2) Operation: The equipment will be tested to insure acceptable performance within a temperature range from 125°F (plus minimum exposure of 4 hours with full impact of solar radiation, 360 BTU/SqFt/Nr) to 40°F (minimum exposure of 3 days without benefit of solar radiation). Where up time required to reach operating temperature is to be recorded. All temperature testing will be continued until the internal temperature of the computer has been stabilized. The time required after energizing the computer for it to reach a condition of efficient and accurate operation is to be determined.
- 7. Reports: Correspondence and reports pertaining to these tests are Confidential. Remorandum reports will be required at the conclusion of accuracy tests and at the conclusion of ruggedness tests. These reports are to be submitted to the Chief of Ordnance, Attn: ORDTR.
- 8. Funding: Program Schedule 7040-5400-10 SEA No. 575 and Work Schedule 8040-5400-10-575 SEA No. 575 provide program authority for conducting engineering tests of Computer T29E2.
- 9. Testing Period: Gum Data Computer T2922 is to be thoroughly tested as outlined above. Tests are to be completed 3 months from receipt date at your proving ground.

FOR THE CHIEF OF ORDNANCE:

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WILLIAM W. FOSTER Lt Col, Ord Corps Assistant

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				1. 1. 1	And the			
	. 1	e fa	1 0			0	Y	
					4,	R	H	-
			300.2		200	2313	•	1996
	2811				200	3392		200 2
4					2,0	4/70		
			499,3		- 500	4673		477.4
			1		500	6724		500.0
12			2 2 3 *		500	7052	9749	500.2
15			9701.		1000			10:2.5
15					- 100.	7029	9918	157.2
7 =	lane.	76.5	9:97		1000	1076	9827.	998.9
		.11.					YI	
	1240	73	1990		200	2890	203	200.5
	1757	9796	100.0		, 200	4265	9987	201.0
100	2416	9749	193.8		200	4868	7518	261.0
-500	o i Ca.	195	4924		500	6:69	77/	499.6
" 1°	3511	19	54.11		500	8167	9976	4999
1.	3835	9812	500.4		500	8472	9761	499.9
13 0	3268	723	905:7		1000	3155	782	999.2
-1000	3758	10	197.6		1000	8600	9985	199.5
1,000	3683	9543	999.7		1000	8677	9837	4904
		ZII						
						.لا ـ	111.	
100	1579	80	179.2		200	3661	299	201.5
201	2048	9916	2001		200	5442	9998	202.2
- 200	2555	9772	200.4		200	6003	1826.	202.2
. 4.7.0	257/	576	501.1		500	3589	754	498.1
- 800	4194	10	500.1		-500	9838	9975	498.4
500	4366	9902	497.8		500	9972	9175	498.4.
- 1005	3774	923	978.6		1000	10640	636	1000.7
1.00	4457	9976	999.3		9.1000	10393	9752	999.8
1000	1518	7866	949.4		1000	10473	9789	199.6
	11	7						
20%	1767	117	199.6					
-200	2629	7971	199.9					
200 .	3415	9762	200.0					
-566	3079	125	500.5					
-500	5205		500.1					
500	×452		502.0					
1000	4918	80%	9717					
-1000	5433		1005.2					
1000	5449	4	000,3	A-10	)			
	,	/		Y T(				

### APPENDIX A

PART 2

ABRORMAL EFFECTS TRAJECTORIES

105 mm Rowltzer

In 4, taray 413-51/21957

A-11

105 MM Q DEAL LLEVATION CHE K

CH	ARGE :	+ 30 F	6	CHARGI VI - 50 MIC					
0	R	<b>P</b>	40	٥	R	H			
200	1124	63	199 5	200	2 4 5 8	2 37	2000		
200	1.571	5	177.4	200	4400	9121	201.4		
200	2317	4779	200 "	200	1753	1985	201.6		
500	1752	+60	5 (	500	7017	752	1995		
500	3372	74+1	500.0	500	#39T	7	+151		
500	169	9729	+98.2	500	8562	9885	4 18.7		
10.	2435	760	10020	1000	3+34	799	999.7		
. 200	3444	19 =.	996.3	1000	370-	332	171.5		
1500	3553	9923	995, 9	1 ~	2467	9937	999.5		

CH	ARGE V	+ 50 F/S	5		CHARGE	VIL +50	F/S
*	R	18		0	R	H	01
200	2963	121	177.8	200	3111	342	199.0
200	4049	9899	2009	200	5656	9997	202.5
200	4575	9735	201,2	200	6106	9844	202.6
500	5094	891	502.4	500	83/1	752	498.6
500	7300	9091	502.2	500	10107	7	498.1
1000	7045	740	1001.8	500	101241	9865	499.0
1000	7421	94	1001.10	1000	10188	799	1000.9
1000	75 45	486+	999.7	1000	10681	332	999.6
				1000	10735	9857	999.5

# 105MN QUAURANT ELEVA ION CHECK

	OHARG	£ 3 .	10 7/1	«		CHA	est Y	- 50 1/2
0	K	~	•			•	k H	e, "
200	730	4.5	201-3	3	2	00 /01	10 14	2018
200	14 14	1171	200-3		20	336	e 447	1 199.5
210	2117	9738	197.1		3	37	2 983	3 /181
300	1908	355	+ 71.2.		5	65 60	193	4916
500	2000	9978	417.7		01	631	97 491	4994
1000	3097	7775	501.2		51	0 63	67 4373	4990
1000	291+	1953	196.6		100	58	11 903	196.7
1000	3051	9132	910.2		100	E 649	5 9918	9166
					/ 87	0 651	12 783	0 946.6
	CHARGE	П - 3	OF/s			Cri	(GE 27)	- 50F/S
0	R	. H	*		4	K	н	e'
200	1187	C3	201.2		200	1619	207	200.8
200	1571	5	200.3		201	4 24		200,8
200	2317	9779	191.3		20	r 478	4 1792	200,6
500	1752	460	996.9		2.00	632	0 /84	497.7
600	3372	9941	50.5		500	762	١١١	501,1
500	3681	9728	501.8		21 25	3//	9919	5 m.7
1000	29+5	760	994.7		375	786	6 9825	1000.7
1000	3498	9931	1000.1		1000	838	3 755	1000.7
1000	3553	9783	1000.3					
						CHA	RGE VII	-50 F/s
					0	R	H	.01
					200	2952	308	201.5
					200	5231	9999	201.9
					210	5902	9793	201.8
					500	1989	895	997.5
					510	9570	9974	498.7
					1000	9837	9713	499.0
					1000	9754	643	1001.2
					1000	10132	9917	1001.2
					100	10158	9864	999.7

1 - 5 MM GONEDENHALELE-ATION CHECK

PLUS TAPE WILL

		I					V.	
3	. 8	12	6		*		H	•
20	)	7 1			31	1772	171	1711
3 81	1510	709	3 1		4	36.0	1566	111.5
	2239	1750	1900		3 80	45.24	1700	1916
* = =	1671	7.1	4 : 1-1		200	<b>**</b> 0" <b>*</b> ₹"	904	5010
5 -	3127	216-	· 4177		2.00	67.00	7947	521
300	. 33 .2	10 7	50 3		2.10	72 51	7775	500.0
1600	- 2411	71.	100% 6		,	6764	9 5	171.1
1000	17 33	56	10-6-0			7210	7174	1900.0
1818	3 473	1737	191.3		100	74/2	1719	131 -
		II					71	
:0	12 45	73	201.3		20-	266.	231	1116
2	1944	7971	232-		1 .1	960 100	1151	2000
		14	177			31 11	1290	21111
50	2146	44-	471.3		2 100	7235	116	501.4
600	3569	24	1. 7 4 .4		• •	A191	9751	499.8
500	3.101	4877	200. 4		5 15	1 53	974	479.4
10000	3354	73'	1717		221	8742	773	1000.4
12.0	3712	11:1	777.1			9281	9.9%	774.9
1010	3/2	175%	978.1		9.9.4.1	7340	9010	177.3
		Ш				<i>Y</i>	J.T.	
200	1366	754	2007		13	3012	32 K	147.9
200	2292	4963	200.3		200	5653	5	201.3
200	2969	9846	211.4		2000	6254	91135	201.9
500	2404	595	501.0		41	9020	840	497.0
500	42.6	15	447.8		5.65	10516	9976	497,4
500	4618	9799	501.0		300	10662	7973	977.5
1 mo	4111	702	1004.0		1000	10.72	850	1002.7
1 17971	4534	6 +	1000.0		1350	11186	1955	1005,3
1070	4652	9884	1001.5		100	1127+	7777	10013
	.71	<b>Z</b>	p					
200	2022	95	200.6					
200	2506	21	200.3					
200	3451	9762	200.1					
5 ೧೭	31//	730	501.0					
5 60	5337	9962	499.7					
5 00	5531	9831	499 1					
1 allen	5042	830	997.0					
1000	5658	9930	999.5					
1000	5774	9126	979.5	A-14				

105 MM Q CHAIT ELEVATION HECK

	I		MINI	50	MPH	WIN	0		
60	*	H	0			-	R	T H	40
200	762.	74	130.5				2236	150	200,7
210	1433	559.	154.5			200	3230	5531	1955
200	2196	317-	1991			A 167	3787	38 30	139.4
500	1062	917	503+			5.0	1333	851	504.8
500)	3030	3050	50.0				2.55	39 69	499.9
300	3175	3.551	50			6 012	5474	3916	4593
1.27	2865	772	395.0				6157	960	999.€
1000	3154	39.1	1000 6			1	6611	47	3993
						3760	6721	7924	999.4
		I						XI	
200	1234	73	190.9			200	2507	214	201.2
200	2015	3923	199.7			200	4129	2960	2015
300	2354	5759	185.			201	+641	9802	201.2
500	2154	477	499.9			500	6114	773	494.7
Enn	3457	16,	501.2			500	1597	9956	4 97.1
5.90	3766	5910	€.22₽			• ••	7739	9906	997.2
1000	317-1	708	994.6			1000	75 4 C	782	996.5
1000	3542	15+	+.A66			1000	8013	98 56	999.5
1260	3721	9827	998.9			ו מטים	8043	9804	398.7
	ב	TT.					_	V_II	
200	1353	97	198.8			200	2973	323	1993
250	2208	9967	200.0			200	5235	9993	202.3
200	2622	9846	197.1			200	5757	9821	201.9
500	2727	549	502.7			Sou	7706	910	494.7
500	41,22.	5	501.0			300	3212	9954	495.6
505	44 53 3877	9780	499.0			\$ 50°	94/7	9755	9 <b>9</b> 5,6
1050	1073	6ର3 3 <i>65</i>	992.9 9962			1000	9244	674	9 <b>99</b> ,6 999.1
1010	4341	3884 3884	797.6			1100	9585	9949 9788	999.0
7.00			771.6			1000	9655	មានភ	395.0
	II		1000						
200	1512	129	198, <del>9</del>						
200	2462	19 976:	199.7 199.4						
200	3369 3039	7/9	ED1.1						
500	5/40	9944							
510	5318	3821	501.1 499.5						
/4=0	4759	7.9/	997.6		†a				7.4
1000	5177	75	9993						
1000	5279	38/9		A-15					
				FIDE	AIT				
			10						

West to Let where yet

				* //	. 25	la A		**	
		-,-				77.7			
4								V.	
	A.	11				0		H	60
201						200	1797	/16	1313
						201	1427	9978	2001
						214	1113	7744	
310						310	7924	110	. 1
500						110	6477	16.5	600
524						rer.	6156	1750	0011
1424			117:			1974	6317	27/	1111.2
1506			7757			100%	2611	1117	. " .
1300	3337	1165	997.7			1440	6711	7142	111.6
	-	-					_1	1	
200	1136	7.3	197.5			200	2571	218	197.5
200	1633	19	1497			301	4392	7154	200.9
200	2404	977?	1996			200	4116	9912	316.4
500	1920	11:11	" 33 "			500	6345	827	506.6
500	3417	14	510.7			500	3077	9110	50:0
560	3103	1207	500 5			500	7119	9830	561.0
1:00	3238	700	979.3			1000	786/	865	447.6
1160	3/18	1285	1000,2			1000	1393	3848	97.12
.1000	3:11	9818	1606.4			1000	8443	98.31	4702
		1/1 .					· v	11	
200	1356	97	194.5			200	2986	317	206.1
200	2216	9967	200.1			-: 20	5301	9001	201.5
200	2632	9845	210.3		*	200	5908	1511	201.4
50C	2371	588	501.6			500	8424	630	500.0
500	4292	9917	5001			500	9547	9969	500,3
500	4493	9777	471.5			500	7764	9802	500,5
1000	3957	653	999.5			1000	9512	896	9963
1600	4364	14.	1000.2		,	1000	1986	16	974.6
1000	11561	9646	1100.6			1060	10062	9824	1776.6
	7	Z.							
200	1517	129	199.1.						
200 .	2475	19	199.8						
200	3392	9761	200.0						
500	3463	660	500,9						
500	5190	9944	500.5'						
500	5372	9821	50.0						
loco .	4856	762	949.1						
1000	5294	56	1000.1			A 16			
1000	5400	9860 .	1000.3			A-16			

122 1	14 9 114	3. h.	115	VH1150	EMPLE
	- 160	11111 113			

				/ / -	****		dir-dir		
	50	T					Tr		
le	R	14	o'		0	*	Y	20	
300	1134	6 ¥			2 00		174	210.0	
3	1501	1115	300 1		2 •0			200,5	
.22	2227	1755	2014		200	3744	90 70	30.5	
112	2007	387	409.7		510	+204	104	Sm 8	
500	2900	57	500.2		\$ 10	4729	47	F 3	
400	1235	1167	500 1		1 10		1767	500.3	
1506	3116	201	1116		1010	4446	735	1116	
1800	טנע	61	1947		1++0	7161	7776	118.0	
1150	2103	1775	4054		1003		1768	777.8	
	1	Т					II		
360	:314	75	211.5		200	\$211	180	201.2	
200	2040	9924	200.0		200	• 3:6	9779	201.3	
200	2427	1100	2000		200	492+		2013	
510	2533	425	127.7		5 10	6525	791	499.6	
500	7542	26	500.3		500	8+87	9796	500.0	
504	3869	9:18	360.1		1010	8466	702	994.9	
1000	7299	747	900.1		1000	8738	230	796.9	
1000	3700	195	778.4		1000	9005	9729	7 77.0	
1000	3876	9867	991.4					, , , , ,	
44.	. 7	II					ZII		
200	1364	98	2001		200	3080		200,5	
200	2236	7968	200,2		200	5692	9999	203.5	
200.	266/	7846	200,4		200	6108	9844	203.7	
500	2774	536	500,7		510	8765	878	498.5	
510	4232	18	500.1		510	10/49	9990	4 99.8	
500	4583	9792	500.1		500	10288	9888	5000	
1000	4043	718	198.2		1000	10322	898	999.9	
1000	4470	80	498.8		1000	10833	9943	917.9	
1000	4595	9864	998,3		1000	10833	9833	997.2	
	· JY	<u>r</u>	100			4.7			
200	1526	130	200.4						
200	2737.	997/	210.2						
200	3438	9762	200,3						
510	3923	583	50010						
200	5303	9966	500.1						
500	5493	1843	500,2						
1000	4781	155	991.0						
1000	5655	9955							
1000	. 6667	9150	993.6						
		-							

A-17
CONFIDENTIAL

# TOU I'M QUADRANFOENENEEV'TION CHECK

PL	US 55	O AIR	TEMP		MINUS	5	9º AIR	TEMP
		Y						
0	R	н	9	0	R	H	e3'	
200	2322	158	2005	201	22.84	152	2007	
200	3408	4	201.9	200	3314	7114	200.9	
200	3933	1870	2025	200	3857	98.0	2006	
500	4430	878	343.4	500	4415		418 8	
500	7071	9762	505.8	503	6568	1787	199.4	
1077	5348	777	7963	500	6611	9707	499.5	
10:0	70/2	9995	916.5	(10)	6367	166	999.1	
con	7155	47/3	1120	/,777	4857	51	997.3	
				1500	6777	9829	999.4	
	V	r_				VI		
200	2645	229	200.6	260	2545	217	202.3	
200	4128	9598		201.	42/4	9963	202.5	
200	4994		201.1	2011	4142	7306	201.9	
500	7065	753	5021	5 00	6776	787	497.5	
500	8450	13	5 00.7	500	7618	115	499.0	
500	8628	9891	500.4	500	8018	9824	499.6	
1000	8452	799	1000.4	1000	7854	760	999.1	
1000	8728	9940	1000.1	1079	8294	9976	999.7	
lovo	8180	9810	१०५८.।	1000	8370	9930	999.7	
	<b>Y.1</b> T							
200	3370	317	200.3	200	3032	326	201.3	
200	5235	72	201.8	200	5364	2	204.0	
200	6396	7730	202.6	200	5905	9831	203.7	
500	8758	816	500.4	500	8419	703	497.7	
500	10178	9951	500.2	500	9544	9980	498.4	
500	10405	9778	500,1	500	9675	9,979	+99.4	
1000	10216	860	1000.3	1000	9732	679	999.4	
1000	14715	9909	999./	1000	10106	9955	997.7	
1000	10769	1719	999.0	1000	10184	206	198.6	

#### APPENDIX A

PART 3

COMBINED EFFECTS TRAJECTORIES

105 mm Howitzer

F. C. # 57 57

unel, corety e J 413-51/1957

A -1.9

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105 MA LOW ANDLE TEST PROBLEM
                  COMPLES PRESCTS
       THE LINEAR OFFICE IN PETERS
THE CAME PRESENCE CAN CAN SEE AM
                                                      DA
    E A H E / M DAT AZ YA
  0 0 0 16120 160 150 6316 1316 -50 2138 HIST WTS
  0. 0 2 96500 760 374 5845 13/6 -50 1138
   0 '6 0 96500 700 274 5345 1316 -50 1125
6 6 96500 700 274 5345 1316 -50 1125
          "0 0 76 SE - 710 2 N 84 25 1316 - 50 1 128 1159 UFL
5 0 0 96500 750 274 5345 1916 -50 1 125 A164 1152

5 0 0 0 96500 750 274 5192 3242 -50 1 125 A164 1152

6 0 0 0 8660 760 274 5095 2042 -50 1 126 A164 1162

7 0 0 0 1666 750 274 5045 7242 -50 1 126 A164 1152
    1808, NO
                             SETTINGS
      1 - - -
                                HORNIAL
    **
                           MUTTLE VILOCITY CHAINS + 30 F/S
   3
                           SOUTH WIND 40 M/+ WEST WIND SO 1: /H
    5
                           9. STD. AIL DENSITY 110%
                            AIR TEMP, O'F
                           POWCER TEMP OFF
                           PROJ WT. . 2 SQUARES
```

TEST PLL CHARGES FOR EACH PROBLEM, ADDING EACH SETTINGS

#### 105 MM COMBINED SEPECTE

#### ANSWERS TO LOW-ANGLE TEST PROBLEMS

		-		Notice III III	1	8						0.0
NORMALS				\$5-10 mag.	MV			MV WIND				
Che	A	AZ	E	QE	R	AZ	<u>F</u>	QE	8	AZ	F	96
1	2986	645	19.3	536	2186	647	18.6	471	2986	647	18.5	461
2	2989	648	16.7	422	2987	100	164	361	2989	649	16.3	37
3	2113	649	14.7	340	2993		14.5	113	2993	649	14.5	310
3	2117	650	12.7	269	2117		12.7	252	2997	650	12.7	25
5	6004	3848	25.1	435		3145	24.9	410	6004	3843	25.3	441
6	6007	1849	21.9	331		3919	21.9	322	6007	3848	22.0	35
7	6007	3850	15.2	247	1007		19.2	240	6007	3050	19.2	25
	MV.	WIN	D, DE	NS.	MV.	WIN.	D DE	VS.,	MV,	WIN	PT	VS.,
Chq.	<u>R</u>	AZ		<u>₽</u> E	R	AZ	F	QE	R	AZ	E	QE
	2986	647	18.6	466	2986	647	18.6	466	2986	647	18.7	48
4	2189	. 648	16.3	379	2989	648	16.4	380	2989	648	16.4	39
3	2973	649	14.5	312	2993	649	14.5	312	2993	649	14.6	32
4	2997	650	12.7	252.	2997	650	12.7	252	2997	650	12.7	26
5	6004	3848	25.4	454	6004	3847	25.7	468	6004		260	49
6	6007	1848	22.2	363	6007	3848	22.3	388	6007	8848	224	40
7 .	6007	3850	19.3	267	6507	3850	19.4	276	6007	3350	19.4	28

# Chq. R AZ F QE

Chq.	R	AZ	F	QE
1	2986	647	18.8	489
2	2989	648	16.5	399
3	2993	649	14.6	327
4	2997	650	12.7	262
. 5	6004	3844	26,1	500
6	6007	3849	22.4	403
٠ ٦	6007	· 3850	19.4	285

		- 10	(17)	25 6 6 1	" 1	18 6	11	. "	1.7 1 1	111	
			ce	116 111	0,0	1111	15				
	417	٠	110	* F1	F * #4	100 11	11	200			
		-	,	15111	NIE.	er	000	JA	1.6	DA	50
1	4	27	1	1	24	2 1	A2	41-			
8"	0		6	-17	21	e	0	0		-,-	0
D	.00	-	C	2374	۵		4.0	0	0	0	c
91	0	6.	6.2	21.1			6.0	4"	)	0	
	0	0.	0		-27	0	ی	43	C	0	0
C	2	0	0	6000	31	-	0	. 1	c	0	C
C	4	C	-	71:0	21	-			4	· ·	0
•	0	0	0	ye 7,3	31	C		2	o	0	C

1500 10

SETTINGS,

NOI MAL

MULTLE VELOCITY CATANGE - 20 F/2

MONTH WIND COMIN WEST WIND 20 M/4

OF, STD AIR DENSITY 90 %,

AIR TERM 118° F

FOUDLE TEMP, 130° F

FROJ WT 1 SQUAKE

THE ALL CHARGES FOR EACH PROFIETY, ADDING FACHE

105 CONDICTO CTILLES

		A	usue	2.2	10	pd 14	6.84	A 4		7651	1,1	CHL	
		NO I	MALS		1	MY				MV. WIND			
chg	. 5	AZ		38		AZ	E	SE	<u>A</u>	AZ	F	25	
1		6861	9,66		2986	. 312	28/	1 901	2984	0:77	26.7		
2	-	6343		1175	2980	6351	35	1125	2784			124	
3		6356			3990		30 .	1 1027	2440	43.2	11 2	97	
4		6359			+114		40.5	1013	4994	6364	37.7	95	
5		6349			5998		53.1	1093	5998	6355	45.4	104	
6		634+			6996		51.9	1151	6795	6314	52 5		
7	7189	6340	70.6	1196	7990	63-1	62.3	1/57		6332		1131	
	MI	, will	VD. D	ENS.			8		gan	0.0	\$* e *6		
cha.	B	AZ	E	QE									
1 :-	2985	6367	27.6	920	2985	6367	27.8	924	2985	6361	30 (	990	
2	2986	63.45	37.9	1103	2986				2986	6340	35.6		
3	3790	6360	35.0	1000	3990			995	3990	6354		1039	
4	4794	6361	39.2	9841	4977		392	955	4994			1026	
345	5998	6351	47.7	1065	5998	6351		1065	6998	6345	50.2	1094	
6	6993	6339	55.3	1115	6993		58.6	1141	6993	6330	60.5	1154	
7 .	7984	6326	64.0	1160	7984	6373	66.9	1176	7984	6373	107	1185	

MY, WIND, DENS., A.T., P. ., WT.

Chg.	R	AZ	F	<u> </u>
1	2985	6359	31.0	1007
2	2984	6338	36.5	1141
3	3989	6353	38.1	1051
4	4993	6356	42.3	1035 1
5	5995	6344	50.7	1101
6	6970	6330	60.3	1155
7	7980	6322	68.3	1185

A XTGTHTAA

FART h

FUZE

305 m Homitson

IF. C. FIF 57.

A-24

CONFIDENTIAL

CONFIDENTIAL FUZE CHECK

111/11/11/11/11/11	9 11 1123	E IN SECNOS	
	J.V.	3.1	
F - FF	F to F F	R G F	E.
11. 11. 1. 6.0	2742 11.5	4115 1996 187	13.4
12 - 156.7 19 16.2	13.7		15.7
27	618 160	5039 2447 11.0	17.5
7 16 . 16.7	4115 3017 115 185	441 - 279.3 115	11.4
St. 5 1.00 12 19.2.	4672 46 . 21.2 21.2	19.14 31C.1 . 1,5	21.5
and arrest to the	5024 4754 4 24.4	(401 343 4 23 3	23.6
7253 31 6 31.6	5/2: 49: " 25/ 25.0	Cust 371.7 25.8	25.0
200 1110 584 33.5		7315 411 ( 382	257
274 11277 70 36.1	1486 1110 -17 41.4	7772 461.6 30.	30.9
	107 17/5 461 458	7750 511.3 goe	33.7
17	7372 1145 8 47.4 47.4		
1024 2116 73 9.3		9144 936.0 1-2	
2226 273.7 11.7 11.9	.V.	Sist 12:2:	
27/ 1 3480 147 14.8°	3658 212.0 13.6 13.6	R230 1146.7 1	
22 2 4242 12.0 18.0	1115 251.1 15: 15.6	7772 1196.2 (0.1	
3666 504.5 31.0 21.0	4572 286.4 11.6 17.6	1315 11374 61.7	61.7
	5029 3.4.2 19.8 19.8	* *** .Z., Z	
4028 230,6 335 33.4	5486 365.3 12.1 22.1	- Z77.	
3658 11317 36.4 37.0	3944 410.7 24.6 24.6	5426 202.7 17.2	17.2
3200 11218 39.2 39.2	CHC1 462 1 27.4 27.5	39114 227.2. 14.0	18.9
	6615 491.9 29.3 29.3	6.161 200.1 20.8	20.8
and processes	,	61:63 279.5 32.7	22.7
2102 202.5 9.7 9.7	1215 9:3.2 48.5 48.3	7315 307.7 24.7	24.6
2276 2223 10.7 10.7	1568 1631.0 81.4 SIR	7772 3375 267	26.7
1743 2752 13.1 13.1	6401 1685.9 53.3 53.2	8130 3641 283	28.8
33.5 15.7 15.8	5944 1140,2 34,8 54.7	SCET 403.0 31.1.	31.1
3658 400.0 187 18.7		9144 4588 33.6	33.5
4/15 480.8 22.0 22.0		9201 4824 36.2	
		10038 426.5 34.1	34.0
4663 7726 37.7 37.6			
4572 961.4 38.6 38.5		10973 908.8 60.2	60.0
4115 1018 6 41.4 41.4		10516 991.6 13:4	
3658 1160.5 43.8 43.1			65.4
		9601 1078.5 67.2	67.0
			68.4
		. 3687 1151.3 69.8	64.6

APPEDIX D

PART 1

MORHAL TRAJECTORIES

155 mm Howltoer

I. C. # 5.7. 57

Souls arely e) 413. 51/2 1957

A-26

CONFIDENTIAL

155 MM GUARGENT CONFIDENTIMEON AMECE

J.	TIT.
ORH COF	6 K H E 6' F'
ne 1191 69 60 239 61	200 2017 17 80 200 1.1
21 1617 6 216 260 83	310 3612 0 11.5 200 10.7
20. 2527 9779 11 0 20 12.2	300 1414 9766 140 199 142
100 1617 219 1.0 349 9,2	ire 2111 146 110 350 122
110 2556 0 1199 550 14.2	150 8181 6 15.81 380 18.3
36. 3113 9755 17.0 350 17.3	310 KIT 1864 10,0 350 20,4
100 7 91 436 16 507 17.2	see here the 16.0 501 16.3
. 660 3316 0 1842 201 13.8	SM 1372 0 3417 500 254
500 1717 9711 11.0 501 224	500 5118 1130 21.0 Bon 27.5
100 2937 175 240 945 25.8	100 1309 113 360 889 35.1
75 3777 6 3156 900 32.0	9.00 1566 0 46.2 899 40.8
, 415 34-6 9776 BBC, 400 33.5	om 6110 9948 41.0 899 416
1080 2860 828 290 1048 29.2	1. FE 4760 SYY 40. 6 1052 40.7
1350 1400 0 11.95 1050 35.4	1016 5726 967AMID 1051 453
1000 1492 1123 16.0 1050 36.9	1650 5316 0 44.5 1051 43.7
1260 2:31 233 22.0 1200 32.0	120 3968 739 41.0 1200 44.1
1200 2694 0 37.45 1200 37.5	WOW 4352 0 47.59 1200 47.7
1203 2730 9103 34.0 12.00 38.0	120 4283 9910 48.0 1200 481
$\mathcal{I}\mathcal{L}$	
	IV.
200 1564 76 7.0 2.00 7.1	200 2329 159 1.6 250 8.2
200-2042 0 9.72 200 9.4	206 34-12 0 12.07 2:00 12.3
200 2834 9764.13,0 199 13.2	100 4213 9791 15.0 200 15.3
350 2324 256 11.0 350 11.2	250 3715 501 12.0 350 12.3
350.3273 0 . 15.78 350 16.1	350 3428 0 20.55 350 21.0
350 3701 98 09 15.0 350 18.5	350 6006 9135 23.0 350 23.5
500 2744 539 14.0 500 14.3	500 5217 758 21,0 500 21.5
500 4176 0 2192 500 22.4	· 500 6860, 0 28.45 500 29.1
500 4537 9763 24.0 500 24.4	500 7187 9783 30.0 . 500 30,7
Gen drug	900 7145 770 420 895 42.6
900 4740 0 7:49 899 36.0	700 7721 0 45.12 898 46.8
900 49/9 9738 37.0 899 37.6	960 1876 9765 47.0 899 47.9
1050 3728 457 74.0 1051 34.5	1050 3474 837 47.0 1051 48.0
1030 7232 0 37.29 1051 000	1050 (128 0 50.82 1051 51.9
1030 454 4868 40.0 1051 000	1550 6948 9958 310 1051 521
1300 2995 888 37.0 1200 : 37.0	1200 5172 778 51.0 1200 51.1
1200 3363 0, 42.07 12.00 42.1	1400 5454 0 743 1200 54.4
1200 3428 9814 43.0 1200 43.0	1200 SE16 9825 55.0 1200 55.1

# CONFIDENTIAL

177		111	
6 K H & 6' 1		6 K H 5	se' E'
200	91-2.	20 6201 430 11	19 - 12 4
26 - 1714 3 272 2000		- 1: F O 14 :	
	(7.4	101 300 45 28 31.6	
562 2534 544 157 350	150	15. 19. 15. 15.	
110 160 0 20 000	2 3 7	11 1111 0 112	
SC 264 1778 350	25.6	20 1600 4718 3000	
566 (570 412 .40 500		4.00 mee; 111 W.C	
3.0 343. 0 119 500		12.4 0 4131	
100 1617 11:1 100 505		13-13-15 41.5 436	1100 45 5
1.0 31 810 41 815	46 5	900 11/20 106 600	849 600
\$ 1604 C 31.6 818	527	4759 C 14754 C 1.55	810 676
90. 9659 9814 120 898	53.0	11: 14721 7769 (6:	178 67.7
1050 8241 110 54.6 1051	553	13. 13117 108 71.3	
1010 1857 0 11.15 1051	58.6	1.5 . 3400 0 73 89	105/ 75.7
1050 1747 9104 13.0 1051	57.4	1350 13513 9100 740	
120 (218 120 25 1500	58.1	12: 10312 614 76.0	
1200 6807 0 61.1 1200	61.7	1.1 10177 0 77.12	
Les 6887 4749. (2.0 1700	62.1	1. 18436 4125 79.0	1200 78.9
YI.			
200 4113 291 11.0 199	11,3		
200 5754 0 16.38 200			
200 (5/3 9/65 19.0 2.00	19.6		
350 5784 823 17.0 351	17.5		
350 8475 0 26.74 3.50	27,5		
350 8800 9834 28.0 350	2,8,8		
500 9193 802 110 500	31.8		
500 10497 0 36.41 500	37.4		
500 10613 9899 37.0 500	38.0		
900 11431 908 55.0 892	56.0		
900 12629 0 586 897	60.0		
900 12094 9894 57.0 898	60.5		
1050 10497 865 62.0 1052	64.0		
1050 10914 0 65.64 1052	67.0		
1050 11034 9730 66.0 1052	67.8		
1200 8345 698 67.0 17.00	67.2		
1200 8575 0 6933 1200	r c an		

1200 8575 0 6933 1200 69,4

APPENDIX B

PART 2

AGNORMAL EFFECTS TRAJECTORIES

155 mm Houltser

[F. C. # 5.7...57 enel 2° 1049 0 413-51/21757

A-29

CONFIDENTIAL

135 MM QUADRANT ELEVATION CHICK

		M	UZZLE	VILOC	ו עדו	LUS 3	0 11/50	c.			
		I						, m	1		
0	R	H	T	•	T'	0		Н	T	10	17
23/1	1013	118	5.0	227	5.3	201.4	1827	175	. 7.0	108	7.4
231.1	1999	0	1.80	231	10.4	209.4	272'0"		11.35.	107	
231.1	2792	9719		234	14.8	20%6	3795	7737	15.0	210	15.8
377. +	1564	300	8.0	376	8.5	. 341,7	2500	394	10,0	340	10.5
377.4	2976	0	15.65	377	16.7	341.7	4373	0.	10,11	342	19.1:
377.4	3566	9618	19.0	278	202	34/.7	4792	982	40.0	3.342	21.1
471.5	1844	452	10.0	472	10,6	965,4	1070	672		A 55	13.7
471.5	3470	0	19.23	472	20.5	455.0	5340	0	43.50	455	
471,5	3929	9710	22,0	471	23.4.	456,0	5629	9832	25.0		26.4
922.6	32/3	933	26.0	963	29.)	922.0	56/8	904	17.0	924	139.7
922.6	4054	0	33,45	923	35.5	922.0	6301	0:	42.17	920	44.3
922.6	4222	9746	35,0	.922	37.0	4120	6409	9034	43.0	920	45.2
401.5	2907	95A	31.0	1095	32,4	1031,5	5317	848	41.0	1034	48,8
1101.5	3461	0	37.95	1100	39.5	1031.5	5817	0	45.39	1033	4810
1101.5	3587	97/6	39,0	1100	41,1	1031.5	5884	9870	46,0	1033	
1191.4	2550	926	33.0	1185	34.1	11695	4539	7.32	45.0	1164	
1191.9	2964	0	3 8 8 8	1192	40.7	N64.5	. 4846	0	48.48	11.65	
1191.4	3040	9791	40.0	1192	41,9	1164,5	4890	1881	49.0	1165	51.5
- 1		II.									
227,1	1390	142	6,0	225	6.3	,					
227.1	2459	0	/0.73	227	11,4						
227.1	3/37	9787	14.0	228	14,8						
\$40.0	1996	305	9.0	338	9.5						
340.7	3+38	0	15.93	340	16:9		45				
340,0	4050	9723	19.0	341	20.1						
187.8	2474	601	12.0	488	12.7						
487.8	4415	0	22,24	488	23.6					*	
487.9	4734	9799	24,0	487	25.4	,					
933.1	4803	873	3210	937	34.1						
933,1	4993	0	37.73	933	39.9						
933.1	5/42	9768	39,0	932	41.2	4.					
. 440.2	2001	772	27 0	10.78	000	10					

34.0

43.8

39.5

1079,3 3981 772

1157.9 39/5 0

1079.3 4406

1157,9 3506

1079.3

0

1462 9882 4210

889

37.0 1078

38,0

42.94

44.00

41.40 10.80

1080

1154

1159 46.2

### ITS MM GUADRANT ELEV FION CHECK

			MUSSEE	VELO	CITY I	Lus 50	ft/500	c	n		
		IX	100							-	1
•	R	14	T	•	7'	•	R	H	T	•	T
2.74.6	2416	213	8.0	213	8.5	2012	2890	37+	10.0	2.06	10,6
211.6	3142		13.45.		19.3	301.2	6207	0	17.51	209.	18.5
214.6	4626			214	17.0	201.2	6125	9765		209	21.0
355.3				342	15.8	334.7	5032	673	14.0	335	14.8
355.			21,66	355	23.1	334.7	8536		26.32		27.6
355.2	1 6461			355	75.5	331.7	8975	7777	28.0	334	29.3
799.8			21.0	302	22.4	462.7	8940	306	29.0	463	30,4
797.3	.7363		21.55	497	31.5	462.7	10316	0	34.78		36.9
777 8	7677			493	330	462.7	10489	9796	36,0	463	37.7
911.6	7644			914	47.2	911,2	//844	845	57.0	906	59.6
911.6	8261		18/4	909.	_	911,2	122.79	0	60.25		6 5.0
911.6	. 8382		49.0	206	52.0	411,2	12499	9795	61.0	909	63.8
1059.4		724	. 51.4	1061	53.6	10414	10923	884	. 63,0	1	.66.6
1654.4			53.12	1060	56.8	1094.4	11349	0	66.10	1046	
1059.4				1060	57.7	1644.4	11468	9736	67,6	1046	70.4
1197,6		829	53.0	1196	55.5	1174,3	8730	772	68.0	11.94	6.7.9
1197.6		0	56,45	11.98	59.2	1174.3	8197	0	70.55	1195	72.4
1197.6	5153	1894	57.0	1198	59.8	1194,3	9030	9862	71.0	1195	72.8
		X.		P				TYT			
214,6	2692	282	80	213	8. 4	210,6	4967	529	11.0	206	11.7
24,6	4800	: 0	15,10	215	15.8	210.6	8054	.0	20,64	211	21,9
214,6	5611	9752	18.0	: 215	18,8	210.6	8736	9748	23.0	, 211	24.3
362.5	.4069	238	13.0	303	13.7	347,0	8879	842	24,0	349	25,3
3625	7/49	, '0	24.47	363	25.6	347,0	10910	0	31.17	347	32,8
362.5	7334	9812	24.0	362	27.7.	347,0	11056	9875	32.0	347	33,6
479.3	6767	861	2410	480	25.2	498.3	11970	866	37.0	498	38,9
479.3	85.65	0.	31.46	479	33.0	4983	13159	0	41,92	498	44.1
474.3	8920.	9763	33.0	479	34.6	+98.3	13409	9786	43,0	498	4-5.2
900,7	9393	879	49.0	901	51.5		14583	777	65,0	911	68.0
900.7	10010		52.87	899	_	. 915.0	15042		67.82	913	71.1
900.7	10184	9723	54,0	899		915.0	15070	97+8	68.0	913	71.2
1046.5	8614	883	55.0	109-9	58.0	. 1063.3		680	73.0	1064	77.1
-	9068	0		10 18		1063.3	-	0	. 75.23	1069	79,3
1046.5		1.674 ×		1043	62.1.		13742	9763	76.0	1064	
1176.7 .:	7	9326	1 -	1196	61.8	11837		687	77.0	1184	80.0
		, ,	62.47		64.4	1183.7	11998	0		1185	79,9
			63.0		65.0	1183.7	11379	4	80.0	1185	81.6
	, ., .	1			05,0			,			E. C. O

INSLIN DUADRANT ELEVATION CHECK

MUTTLE VELOCITY MINUS 30 40/sec

							- /	-			
		I		-	,			III			
.0	9	11	T	0	T	•	R	1-1	T	4	7'
231	760	40	4.	255	37	2016	1726	134	17.4	2.11	6.9
234	1677	0	5.78	231	1.7	201.6	2578	0	12.62	210	10.9
2.11	2367	1750	13.5	229	12.6	2:16	3336	9774	14.0	208	137
377.	12.51	450	7.0	378	6.8	3+17	2114	351	7.0	343	88
27 4	2020	2	4.37	377	14.0	3411	3562	0	16.77	341	16.7
37-, 2	2952	1756	17.3	271	165	341.7	+ 2 4 5	1814	11.0	341	1 4.7
476.5	15 44	382	7.0	470	8.7	156.0	2665	694	13.0	4.56	11.3
11.5	2943	0	17.66	472	17.2	454 8	4725	0	22./2	455	21,8
4.15	1115	7777	20.0	473	19.4	+ 05.0	5087	1786	24,0	954	23,6
		****	- 0			922.0	4880	903	3+.0	887	31.8
421 6	3455	0	39.77	924	29.0	7120	5573	0	39.59	922	38.8
922 6	3581	79 4	3210	726	31.1	122.0	6766	7732	+1.0	923	40.2
1101 5	2430	849	29.5	1102	27.0	1031.5	4306	841	40.0	1109	39.2
1.21, 5	2947	0	34.45	1100	33.2	10315	4732	0	41,45	1106	45,1
1101,5	3070	. 1737	36.0	1100	3.t.7	1031.5	4793	9686	45.0	1106	43.9
11714	: 20AD	945%	29.0	1201	28.4	1164.5	3918	876	41.0	1169	40.1
11114	2527	0	35.77	1192	34.3	1164.5	4303	. 0	45.54	1165	. 44. 2
1191.4	2606	9790	37.0	1191	35.4	1164.5	134/	9901	96.0	1165	44.7
160		-		100							
11-		. 11:									
227,1	1287	118	6.0	229	5.8			r			
227.1	2119	.0	10.03	227	9.8						
227.1	2909	9784	14,0	. 225	13,6						
3,40.0	1650	265.	8.0	341	7.8						
343.0	2971	0	14.77	3.90	14.4						
340.5	3577	9723	18.0	339	17.6						
4878	2110	519	. 11.0	488	10.8						
487,8	3825	0	20,64	488	20,2						
4578	4226	7742	23.0	489	22.5						
·		,			. \						
933,1	4343	0	35.0%	933	34.1						
933.7	4447	9841	26.0	433	35.1						
1079.3	3330	863	33,0	1084	32.3						
1077.3	3833	. 0	3845	1079	37.4						
1077.3	3879.	9905	39.0	.1079	: 37.9						
11579		820	25,0	1165	34.3						
1137.9	3408	. 0	37.42	1158	38.6	A <sub>1</sub>					
	3487	9794	41.0	1158	39.6	20					

ISSUN QUADRANT PLEVATION CHECK

MUZZLE VELOCITY MINUS 30 FO/100

		TI						Y			
1	R	H	T	0	T	4	K	H	T	0	T'
214 6	1150	183	2.6	216	6.8	201.2	334/	31/	1.0	209	8.9
246	3241	0	12 33	215	1.0	241.2	SCR+		16.50	204	167
214.6	126	7 1771	16.0	213	15.6	207.2	4177	9712		2141	19.1
333.2	285	+ +80	11.0	355	10.7	3317	4502	744	13.0	337	130
1552		0	17.72	354	19.9	334.7	7426	0	15.12	335	25.3
355.2	3516	9743	22.0	354	219	334.7	8416	1761	27,0	335	27.2
417.8	3+2	905	14.0	498	13.6	462.7	H145	#26	27.0	452	27.1
477.8	650	1 0	2 7.26	499	26.5	462.7	9722	0	31.35	163	
477.9	6676	7766	29.0	500	29.2	462.7	10/13	1731	35.0	463	35.2
411.6	6466	823	400	581	31.2	911 2	11012	753	55.0	405	54.8
911.6	7066	0	44.33	910	42.7	911.2	11578	13	57.77	701	58.1
.44.6	7/58	7940	45.0	912	43,6	911.2	11737	9732	59.0	910	59.2
1059.4	5808	8/7	45.0	1057	45.3	1014.4	10244	721	61,0	1047	61.5
1057.4	CIOR	C	49.89		47.2	1094,2	10597	0	63.60	1996	C4.0
10514	6431	9742.	50,0	1059		10+1,4	10499	9887	64.0	1095	64.4
1197.6	4716	877	49.0	1199	45.9	7/94,3	8099	850	65.0	1174	63.8
1197.6	5041	0	. 51.93	1198	. 44.4	1199.3	8389	o '	67.91	1175	66.7
1117.6	5137	9741	53.0	1197	50.4	1194.3	8398	9972	68.0	11 75	66.8
	10	V					•	VII			
214,6	2549	246	80	2.15	77	2161	4737	478	11.5	210	11.0
214.6	4350	0	11.24	215	14.2	2/06	7494	. 0	19.73		19.9
214,6	5117	9778	17.0	2.14	17.0	210.6	8149	7768	22,0.	210	22.2
362.5	3593	666	12.0	364	12.0	347,0	8002	863	122,0	350	22.1
362.5	6574	0	23.28	363	23.3	347.0	10/94	0	29.96	347	30.3
362.5	7000	9797	25.0	363	25.0	347,0	10464	1849	31.0		.31.3
479.3	5753	9/3	21,0	480	21.0	479.3	11121	9/2	35.0	497	35.4
479.3	7898	0	30.00	479	30.0		12446	0	40.46	448	41.0
479.3	8124	9355	31.0	479	31.0	498.3	12572	9877	41.0	492	41.5
900.7.	8655	750	47,0	893	46.3	915,0	13799	720	63,0	910	63.1
900.7	9188	· •	505+	900	50.1	41512	14221	0	66.57	913	65.9
900,7	9273	9869	51.0	901	50.7	915.0	1+289	9878	66.0	9:3	66.4
1046.5	7827	903	52.0	1047	51.7	1063.3	12525	804	70.0	1064	70.6
1044.5	83 03	•	55.75	1048	55.5	1063.3	12976	0	72.67	1064	73.2
1044.5	8,333	9937	56 2	1948	55.8	1063.3	12918	9878	73.0	1064	73.G
1196.7.	6318		57,0	1197	55.6	11837	10396	771	74.0	1184	72.7
1196.7	6557	0	59.58	1197	58.1	1183.7	10448	0	76.46	1185	
1196.7	6594	9887		1197	58.5	//83.7	10700	9829	77.0	1185	
1176./	6577	Y 887	20,0	1197	58,5	//83.7	10700	7827	77.0	11 65	_

ISSMM & ACKAINT ELEVATION LIECK

	3	9	PLUS	50 MP	H WI	ND(5)		m			
0	*	24	T	o' t		*	R	H	T	0'	· e'
2311	118 =	100	4.0		6.1	2016	1538	147	6.0	210	9.1.
2311	1813	0	9.40		1. 5	201.6	2764	0	11.00	210	11.3
25.	2316	1715	130		13.5	2016	3471	9799	14.0	204	149
377+	1507	276	7.5	.7 -	9.1	341.7	2437	370	10.0	5,041	10.2
372.	277+	9	14.03		11.0	341.7	4165	C	17,5%	3016	121
377. 4	3271	7747	-	378	11.5	341.7	+701	7768	20,0	392	:0.6
4715	1777	415	10.0	.472	10.2	4550	2776	640	12.0	455	12.3
4715	3245	0	1447	472	19.1	4560	6106	0	22.90	455	2 3.
+7/5	340+	7:47	2/0	474	21.7	4550	5535	. 9751	25.0	156	25.9
		,	-			122.0	54 27	8+8	34.0	921	37.4
9226	38++	0	32/8	5512	33.4	922.0	6105	0	40,97	97.0	42.7
9226	4046	9708	34.0	250	353	922.0	6243	9799	42.0	117	45.4
11515	2770	867	30.0	1097	30.9	1031.5	5/72	774	440 .	1034	+2.0
11015	3296	0	36.52	1101	37.5	1031.5	5654	0 .	44.10	1033	46,4
1101.5	.329 .	9550	37.0	1101	38.6	10345	5758	9812	45.0	1033	47.4
1191.4	2449	827	82.0	5211	32.3	11645	4363	829	13.1	1169	44.9
1191.4	2840	0	37.41	1192	38.9	1164.5	4743	0	47.10	1165	
1/71.4	2953	9700	3.90	1192	40.6	1164.5	1834	4900	480	1166	50.6
	,,,,		,		70,13						
	1.75	IL						IV		117	
22.7	1244	130	6.0	227	6.1	219.6	2058	20+	7.0	1215	7.2.
22.7	2303	0	10.44	227	10.7	214.6	37/5	•	12.94	215	13.4
22.7	3047	9761	14.0	227	19.3	214.6	4525	9769	16.0	214	1.6.0
340.0	19 23	280	7.0	340	7,2	355,2	3060	535	11.0	356	11.9
3400	3234	0	15.37	340	10, 18	355.2	5600	•	20.93	355	
370.1	3753	9774		346	18.57	355.2	6105	9775	23.0	- F 5 6	29.0
447.8	2+01	555		482	12.3	499.8	4827	881	19.0	500	19.7
487.8	9175	0	21.47	988	22,2	499.8	7020	0	2850	500	29.9
487.4	4451	9832	23.0	488	23.8	499.8	7334	9800	34,0	500	. 01.9
9331	4116	810	31.0	931	32.1	911.6	7234	888	42,0	915	**
733.1	4786	0	36,46	132	38.0	911.6	7920	0	4451	9.11;	401.6
933.1	4970	9726	38.0	931	39.6	911.6	7993	9893	47.0	911	49.5
1079.3	3742	834	35.0	1079	36.9	1059.4	6696	129	48.0	1 461	
1079.3	4241	0	40.02	1080	420	1051.4	7100	0	51.26	rcel	
1079.3	4336	9811	41.0	1080	93.0	1059.4	7190	98 23	52.00	1451	
1157.9	3400	792	37.0	1156	37.3	11976	5408	806	51.0	1195	
1157.9	3785	0	41,51	1152	43,4	1197.6	5731	0	54.41	1197	5.7.4
1157.9	3826	9033	42.0	1158	44.0	1197.6	5784	9853	55.0	11.47	, v. v. A

155 MM GU JRANT ELEVATION CHE K

				PLUS	50M+	HWI	ON				
	ę	Y H	Т	477	7'	0	<b>A</b> *	н	7	c'	T'
2146		260	1.00	212	5	210.6	+119	101	11.0	71'-	11. 15
214.6	4822	0 1	14.71	2.14	15 4	2116	711+	9	20/6	2 1 1	2.1. 1
2/16	5 724	9737	180	4	116.3	3/4.5	1556	7.913	220	2 = 1	7
362.5		711	14.0	3	19.9	3420	8707	ALAI	21.0	4.41	2.1.7
362.5		0	24.37	12.		3420	10966	0	3067	201	53.3
362.5	7717	1301	24.0	364	28.0	347.0	11331	9005	32.0	342	-4.1
779.3		850	24.0	410	2 ** 1	178.3	12294	781	37.1	497	20.1
471-3	-	0	31.38	475	23.4	198 2	1344	0	41.49	49%	459
479.3		9752	35.0	478	37.6	115.3	135/3	9902	¥2. 2	1713	4 6.0
900.7	.9582	780	49.0	194	52.2	915.0	15121	695	650	308	* 1 1
9 46,7	10159	0	52.44	842	55.9,	915.0	15524	0	67.25	710	736
900.7	10251	9564	53.0	892	56.5	915.0	15654	9782	69.0	110	7 1.
1046.5		7/3	55.0	1047	59.4	1063.3	13762	751	72,0	10 66	10.5
1046.5		0	57.82	1047	62.5	1063,3	1.11.8	0	74.45	.066	20,5
1046.5		9951	58.0	1647	.2.7	. 10633	14/95	9830	75.0	1066	84.%
11467		697	59.0	1177	\$2.	1183.7	11534	717	74.0	119,7	8 4.0
1196.7	7302	. 0	61.59	1199	500	1183.7	11795	0	78.16		. 2 7, 0
1194.7	7343	9886	62.0	1194		118217	11917	916-	77.0	1182	· · · · · · · · ·
		AI									
1.2			14.4	208	10,5						
209.2		354	10.0	209							
209.2		0	17.05	7.07	21,4						
209.2		9725		237	14.5						
334.7	5046	840	14.0 25.96	2.35							
334.7	_	0.		336	30.						
334.7		9731	28.0								
462.7	8902	873.	28.0 24.49	4 ( 3							
462.7	10426	9748	36.0	463	= 34						
462.7	11012		57.0	904		6					
	, 122.14	734	69.82	909	60						
911.2	12712	9951	60.0	107		.7					
	12743										
	11292	7//	63.0	1049					1,		
	11662	0	65.49	1048							
1040.4	11735	9851	670	1048							
1194.3		828	69.76	1193		- 3		Fire			
1194.3	9322		70.0	1179		5.9		0			
11943	1348	9925	70.0	11 79	7	5, 7					

# ISSMM QUADRANT ELEVATION CHECK

		I		Mins	\$ 50	MPH	w, No	I	, .		
49			Т	e'	T'	9	R				
- 11					6.1	201				•	T'
231	1916	. 0	1.38	_	4.5	201				10?	0.1
231	2474	777		-	19.1	201.				2.0	11.0
372	4- 1+9	1 27			3.1	3 4/.				2.09	19.0
37	4 21/4	. 0	15.0	0 372	151	34/.	•			341	16.11
377	4 32/3	174	3 18.0	377		3 11	_			392	17.6
+ 7/·	5 1775	4/3	10.0	472	12.1	458					20.0
111.5		0	18.4	3 72	18,5	455				455	22.9
17/ 5	3550	974	3 21.0	970	21.0	455				959	25.0
	1,000					922.				913	55.1
9:2.6			32.00	722	31.6	922.			10,71	.727	40.2.
9221			3 33.0	729	22.5	922.6				723	41.4
1101.			33.0	1100	27.4	15 51.				1033	38.7
1/81.5		-	35.9	1099	25.0	1031,5			4312	1037	13.1
1131.5		190		1100		1031.				1032	
11.11.4	•			1176	31.5	1/64	5 4073		. 41.0	1167	418
1191.4			37.2	7 1192	35.9	1164.	5 4 394		4691	1165	45.7.
11/14	2676	9270	3310	1) 35	36.5	1164,5	5 4469	9740	•	1165	46.2
		I					-				
227,1	1383	150	6,0					YI			
אר גנ	12268		10.42	175	5,1	214,4	700+	198	7.0	219	7.0
2271	2795	9741	14.0	227	10.5	214.6	3526	0	12.76	2.15	12.7
110.0		279	9,0	226	14.1	214.6	4537	9754	16.0	214	15.8
340.0	3165	0	15.34		9.1	355,2	2967	516	11.0	354	11,0
340,0	3670	7772	18,0	390	15,5	355.2	5212	0	20.57	355	20.9
487.8	2365	551	1200	339	18, 1	355,2	5823	9737	23.0	354	22.7
497,8	4054	0	21.41	487	1.51	499.8	4177	919	17.0	199	16.9
4374	4326	9826	23.0	488	21.5	477.8	6591	0	29.11	500	. 27. 8
	4	,		100	2.3.0	497.8	6964	9735	30.0	500	24.6
933,7	4535	0	36.33	4 52.		911.6	60 40	789	42.0	JOA "	41.1
933.1		9884	37.0	933	35.8	911.6	7887	0	46.02	913	45.3
1079.3	3548	8/0	35.0	10,82	38.5	911.6	7517	9787	47.0	919	46,3
1077.3	3979	0	39.87	10.79	34.5	1059.4	6/63	829	47,0	1059	46.0
1079.3	4076	9184		1079	37.0	1057.4	6585	0	50.83	1059	49.6
1157.9	3116.	915	36,0	1169	35.4		6704	9122	52.0	1059	60.7
1157.9	3517	, 0	41.36			1197.6	4972	715	5/,0	1200	48,8
1157.9	3563	9875	42.0	1159	40.0	1197.6	5212	0	51.07	1198	\$1.0
	-	, , , ,		1158	40.6	111116	5286	9760	55.0	1199	52.2
											- 1

### ISS MM QUADRAN CONFIDENTALON CHECK

			K.17	105	SO MPH	WIND					
		I			-1						
ér.	R	Н	T	0'	T'	0	K	H	T	-5'	Τ'
2116	2515		8 C	214	7. 7	210.6	4787	511	11.0	206	11.2
216.6	4263	0	14,20	45	14.3	2105	1560	0	20.20	211	20.2
214.6	3016	1119	17.0	214	16.8	210.4	8047	9817	22.0	210	21.9
362.5		473	13.0	362	12.8	347.0	8177	844	23.0	350	22.7
3625	6.461	0	33.46	362	22.9	117.0	10032	0	30.44	347	29.8
363.5	6812	1814	25.0	361	29.3	3+7.0	10449	9772	32.0	346	21.2
4772		868	22.0	479	21.5	+18.3	11053	846	34.0	418	35.1
4772	7726	0	30.16	430	27.3	498.3	12153	0	40.93	498	.31.7
472.3	2119	9725	32,0	480	31.0	49.9.2	12341	9793	42,0	498	40.7
700.7	8451	848	47.0	343	95.0	915.0	132 60	875	630	910	60.0
900.7	9018	0	50.87	903	492	9/5.0	13726	0	66.15	917	63.0
900.7	9175	9737	52.0	905	50.3	9/5.0	13844	4758	67.0	915	63.8
10465	7750	836	53.0	1049	51.2	1047.3	12/10	729	71.0	1063	67.3
1096.5	8154	0	56.12	1098	54.4	1063.3	12380	0	73.48	1222	69.3
1014.5	8230	.9850	57.0	1048	55.0	1062,3	12442	0	74,0	1062	64.7
1196.7	6090	374	5710	1204	54.2	1182.7	9926	733	75.0	1185	64.6
1196.7	6379	0	60.43	1202	56.9	1182,7	10130	0	77.35	1185	70.5
1196.7	6425	9845	61.0	17.01	57.9	11827	10183	9776	78.0	1185	70.7
134	VI										
209,2	3724	348	10,0	207	10.1						
209.2	5755	0	17.02	210	16.9						
201.2	6281	9823	19.0	209	18,9						
334.7	+792	816	14.0	330							
334.7	7852	0	25,55	339							
334.7	8205	9315	27.0	239							
462.7	7757	877	27.0	463							
462.7	9515	0	33,7/	. 4 63							
462.7	9799	9790	35.0	46	•						
9/1.2	107/4	848	55.0	100		5					
911.2	//2 3/	0	58.44							**	
911.2	1/3//	9852	59.0	917							
			¥ ,. •			_					

58.5

61.9

62.1

61.2

63.6

1045

1095

1044

1197

1196

9863

10855

1174.3 7792 790 66.0 1194.3 8055 9902 69.0

1049.4 10261

890

. 0

9774

61.0

6421

65.0

790 66.0

1044.4

1044.4

### ISSMM QUADRANT ELEVATION C CK

			0 8	NEIT	Y P	LUS 10	7.				
		I						7	II.		
after the	R	11	T	0	T'	6	Ŕ	н	T		T
231,1	19/9	107	5.0	230	5.1	201.6	1527	1+6	4.	209	6.1
231.	1920	0	7.39	201	9.5	219.6	3725	0	10.97	210	11.1
2311	194-	9775	13.0	230	1 1	2026	3427	77 17	140	207	14.1
377.4	1313	274	7.0	376	. 7.1	341.7	2 + 1/	366	10.3	341.	101
3774	2124	0 .	14.97	3,17	152	391.7	4076	0	17.41	342	17.7
377 +	3232	1742	19.0	.377	182	\$ 41.7	4607	7263	20,0	391	20.2
4715	1609	115	9.0	471	9.1	4550	2712	613	12.0	. 455	17.4
4715	3/75	0	19,41	972	13.6	+ 56.0	<b>→</b> 771	0	22.78	455	23.0
4715	3586	7741	21.0	472	2.1.2	455,0	5403	9739	25.0	454	24.2
						922.0	. 5250	796	36.3	913	35.7
92216	3706	0	32.10	929	32.2	922.0	5847	0	40,67	923	40. 91
722.6	34/2	9682	34,0	915	34,2	922.0	6003	774	42.0	929	47.7.
1101.5	2603	950	29,0	1098	28.9	1031.5	1873	188	39.0	1032	34.1
110/5	3/64	0	35,83	1100	35.8	1031.5	5397	0	43.80	1033	44.0
11015	3156	9796	37,0	1100	37.0	1031.5	5524	9751	15.0	1093	45.2
117:1	2212	917	31.0	1193	31.0	1164.5	9175	757	45.0	11.66	42.5
119/1-	2709	677	37,20	1192	3,7.0	1164.5	4494	0	46.77	1165	46.6
1/2/ 20	2620	4672	34.0	1192	38.6	114,5	4595	9728	+A.0	11.65	47.5
	,							1			
		エ						JV.	•		14
227.1	135	150	6.	226	6.1	214.6	2035	202	7.0	. 213	7.1.
227.	= 277	0	10,42	227	10.5	214,6	3626	. 0	12.89	214	13.1
227,	3006	9760	14,0	226	14.1.	2/7,6	4425	9764	16.0	214:	16,2
3 +0,0	1916	275	9.0	339	01.1	555.2	30/3	526	11.0:	354	11.2.
300.0	3176	0	15.32	340	15.5	355,2	5418	0	20.76	355	21.0
343.0	3487	9771	19.0	340	18.2	3 55,2	5936	9758	. 23.0	355	23.2
447.3	2373	550	12.0	488	12.2	.4,198	449;	9000	18.0 -	500	18.2
481.3	न्द्रीड.	0	21,33	482	21,6	494.8	6751	0	2831	4.99	286
1813	4354	9824	23.0	487	23.2	+97.3	.7099	9764	30.0	499	30.2
9 23,	3878	37 <b>5</b>	30.0	917	29,5	911.6	6959	794	42.0	9,02	41.7
933.1	4600	0	36.25	434	30.4	911.6	7529	0	44.60	912	46.2
433.1	4683	9870	37.0	934	37.2	911.6	7658	9797	47.0	913	47.2
1079.3	3617	793	35.0	1082	35.3	1059.4	6292	825	47.0	1059	47.1
10773	4058	C	29.78	1080	40.0	10594	6722	. 0	50.78	1000	51.04
1079.3	4/68	9767	41.0	1079	41.1	1059.4	6857	97/1	:52.0	1061	52.2
1167.9	3/90	316	34,8	1162	36.2	1197.6	5039	897	50.0	1193	49.4
1157.9	3605	0	41.25	1159	41.2	1197,6	5370	, 0	53.89	11.98	53.2
11571	3662	9854	42,0	1158	91.9	119716	5460	9725	55.1	11231	54.3
								, ,		4 " 1 "	

155 MM DUASPANT YLIVATION CHECK

DENCEY PLUS 10 %

			.V.							vir.		
	Sin	F.	-	*	~	T'	->	R	H	-	9'	7'
	211-4			2, 1	214	49 1	21016	47:7	481	11-5-	210	11.1
	3 14 -			14.54	219	148	2126	75/3	0	14 PS	211	20.0
	211 6	5170	10.5	17.7	214	172	2105	3115	7782	23.0	210	221
	360 5			15.5	260	1 % 2	3 47.0	7774	875	22.0	350	22.0
	34 5		-	24.47	3.1	770	347.9	10148	0	20.07	347	3,0.1
	14:5				362	71, 4	3420	1134-	952+	\$1.6	3.17	41.6
	4/1.3			44.6	1000	443	428 8	11267	770	34 8	497	36.0
	+71		0	3 4.51	471	2 .7	A 10.2	122.4	0	46.51	4 7 8	454
	4713	5312	???	32-7	471	32 1	4963	12.35	9707	41.3	498	40.1
	900.7	9784	715	47.	833	155	7.5.0	13598	493	43.0	909	61.7
	70.7	9395	0	5(21	201	5:.2	4.50	13910	0	65.46	913	64,6
	700.7	. 7466	79/3	52.0	201	50	715.0	14072	9647	460	914	65.1
	122.	_	577	52.0	1098	532	104:3	12:42	757	70.0	100.1	64. 3
	1144,5	2455	0	56.61	1005	56.7	1013.4	12613	. 0	72.51	1059	71.6
	1044.5	8502	7100	57.0	1098	57.1	10633	12722	9852	73.0	1064	72.0
	1196.7	6353	912	571	119	55,1	1183.7	/5243	707	71.0	1189	71.3
	1174.7	6665	0	60.43	1193	51.3	1183.7	10461	0	76.27	1185	73.0
	1174.7	6715	9849	61.0	1195	59.9	1193.7	10536	9771	77.0	1185	74.3
											1 1 63 %	
			JY.									
	409.7.	61/0	355	9,0	207	1.1						
	219.2	5800	0	16.26	212-1	17.1						
	20 %2	5.606	7.909	17.0	207							
	33+ 7	4845	805	14,0	335	14.1						
	324,7	8013	0	\$ 5,43	335							
	334.7	5414	9801	27.0	2.35	27.1						
	462.7	5143	867	27.0	45 m	27.2						
	962.7	9770	0	33.67	462	33.8						
	462.7	10073	1754	35,0	957	35.1						
	411.2.	11029	526	55,0	900	59.5						
	4/1.2	11555	0	58,33	910	58.1						
	411.2	11657	1525	59.0	911	58.7						
1	1044.4 .	10193	8/8	61.0	1047	61.1						
	1045%	10578	0	63.97	1096	63.9						
	104412	.10709	9705	6510	10196							

9705 65:0 1096 64.8 658 66:0 1196 64.5 0 68:24 1195 66.5

1/14.3 8364 0 68.24 1195 66.5 1/94.3 8434 7772 69.0 1195 67.2

1194,3 8148

1044 - 10709 9705 65:0

155 MM GUADRANTARHEAMSTON CHOPE

				DE	NEITY	MIL	105	1070				
			1						I	Γ		
	0	5	н	T	•	T'	-	R	H	T	•	TI
- 1	111	1119	108	5.0	231	51	201.4	1834	1+7	1.0	210	6.1
23		1839	0	9,41	231	9.6	2016	2762	0	11.01	210	11.2
	11-1	2672	9671	14,00	231	14.3	209.6	4170	7771	14.0	209	19.3
	77. 4	1220	276	7.0	377	7.1	3 4/.7	2+32	371	10.0	3+2	10,2
	7.4	2764	C	15.50	377	15.4	311.7	4156	0	17.58	342	18.1
	7. 4	3274	9716	18.0	378	18.4	341.7	-684	7770	23.0	341	20.6
	15	1619	4/9	9.0	472	9.2	+550	2770	642	12.0	457	12.3
	71.5	3229	0	15.49	472	19.0	455.3	5011	0	22.23	455	,23.6
	71.5	3638	9749	21.0	473	21.5	+550	6510	9754	25,0	455	25.8
	23.6	2550	9514	24.0	967	26.0	922,0	5367	870	36.0	926	37.2
	2.6	3794	0	32,23	924	33.0	122.0	6044	0	+1.38	422	
92	2.4	3985	97/4	34.0	923	39.8	922,0	6/63	9810	. 42.0 .	,,922	43.3
	4.5	2726	877	30.0	1098	30.4	1031.5	5198	802	40.0		41.4
	1.5	3240	0	26,80	1100	36.8	1031.5	. 5580	. 0 .	++24	1033	45.8
	1,5	3377	9654	39,0 .	1100	38.8	. 1131.5	5665	1840	+5.0	10,33	The second second
	1.4	2399	841	32.0	1190	. 32.2	1104.5	4175	065	43,0	1166	
	1.+	2779	0	37.09	1192	38.0	1164.5	4653	•	47,27	1165	
	1. 4	2881	9723	39.0	1192	39.5	1169.5	+716	9837 .	40.0	11.6.5	49.3
			1		120					•		b
		'	I	- 1		1			TV			
22	7,1	1342	130	4.0	. 227	6.1	24.6	2051		7.0	215	7.2
21	7,1	2300	0	10.45	227	. 10.7	214,6	369/	0	12,95	215	13.3
22	7.1	304/	9761	14.0	. 226	14.3	2/1/6	++96	9768	16.0	214	16.5
34	0.0	1930	281	9.0	340	9.2	355,2	3096	514	11.0	356	11.3
34	<b>8</b> , 0	3227	0	15.39	340	15,8	345.2	4	• • •	20.91	355	21,6
34	1.0	3739	9775	18:0	340	18.5	355.2	6060	9773	23.0	355	23.
48	7.8	2395	557	12.0	488	12.3	479.8	4800	88/	19,0	500	19,6
18	7.8	4159	0	21.50	488	22.1	499.8	6969	0	28.57		29,6
48	7.8	4427	9835	23.0	488	23.6	919.8		9798	340	479	31,1
93.	3,1	4068	8225		1930	31.7	911,6	7/53	911	43.0	917	43.9
93	13.1	4730	,0	36.54	933	37.5	911.6	7839	0	46.61		48,4
93	33,1	4899	9740	38.0	933	39.1	9/1.6	7		¥8.0	910	49,7
107	9.3	3684	854	35.0	1079	35.8	105914	6592	767	18.00	1063	50.1
107	4.3	4174	0	40.11	1080	41.2	1059.4	7001	. 0	51.41	1061	59.5
1179	9.3	1257	9829	4 1,0	1080	42.2	1059.4	7070	7859	52.0	1001	54.1
110	7.7	3333	8/34	37.0	11.57	37.6	1197, 6	5282	863		1198	52,1
	7.9	37/2	0	41.62	,1158	42,5	1197,6	5608	0	57,44	1198	55.9
	7.1	3822	9723	43.0	11 59	44.0	Ex 1177.6	5681	7900	55.0	1178	56.2

155 A	A	QUADRANT	ELEVATION	CHECK
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								6 20 4			
			DENS	ITY N	AINUS	1070					
		V							JEE		
0	8	54	T	0	7"	•	*		T	•	T'
2146	2744	254	1.0	219	9.3	246	4552	518	110	205	11.6
214.4	4641	0	14.74	215	15.3	211.6	8066	0	20.52	211	2.1.9
214,6	5181	9817	/2.0	214	17.6	2116	8776	9737	21.0	2.11	24.5
10.5	4000	707	15.0	363	13.4	3 + 7. +	8717	814	24.1	349	25.5
361.5	6992	0	24,01	362	25.0	3120	10113	0	\$1.71	347	33 2
343.5	7446	115A	24.0	362	27.0	3+20	HIEG	9069	12.0	347	34,1
177.3	6464	883	23.0	479	23.9	+14.1	12/02	8-	37.0	498	34.5
479.3	8416	0	30.76	479	323	418.3	1333+		41.15	1 498	44.8
474 2	8669	9844	32.0	479	33.4	+11.3	13507	7770	4 2. 0	498	45.9
100.7	9360	7/1	41.0	701	51.3	9/5.3	/+ 818	872	45.0	912	69.6
900.7	1871	0	5215	900	54.6	\$15.3	15346	0	C.0.07	913	72.9
700.7	10006	9794	630	299	55.4	115.3	15+94	9732	69.0	713	73.9
1046,5	8579	684	65,1	1049	57.3	1063.3	13586	772	73.0	1065	79.0
1046.5	8135	0	57.69	1049	60.6	1065.3	13 723	0	75.52	1064	31,6
1096.5	8775	9917	58,0	1049	60.9	1465.3	13984	9852	76.0	1064	82.1
1194.7	4084	723	59.0	1196	60,5	1183.7	1/276	802	77.0	1184	81.4
1196.7	7064	0	61.67	1197	63.4	1183.7	1/539.	0	79.52	1185	84.2
1194.7	7094	9908	62.0	1197	,63.8	1183.7	11586	9848	80.0	1185	84.7
		,			-			•			4
	- 7.	TI .		812 111	1-0						
209.2	3844	359	10,0	208	10.5						
2092	6/03	0	17,24	209	18.1						
209.2	. 6909	9740	20.0	209	21.0						
234.7	4994	849	. 14,0 .	336	14.6						14.7
334.7	8469	a .	26,84	335	27.4						
334,7	8993	9742	28.0	337	29.4						
462.7	87/4	879	28.0	463	29.4						
462,7	10377	. 0	34,50	462	36.3						
442.7	10744.	9748	34.0	463	37.9						
911.2	11938	779	67.0	907.	: 60.2	*1					
911,2	12444	. 0	51.18	908	63.4	,					
911.2	12612	9720	61.0	909	64.5						
10442	11007.	808	63.0.	1047	67.2						

70.1.

70.2

70.5.

72.9

65.82 1047

66.0 1047

68,0 1194

1044.2 11406 0

1044,2 :11430 9947

1194,3 8804 705

1194,3 9044 0 20.31 1195

1194,8 9118 9786 740 1195 73.6

### ISSMM QUADRANT CLEVATION CHECK

			AIR T	EMPER	ATURE	PLV:	51	F			
		I				100	Carry I	J			
4	R	H	1	0	T'			H .	T	•	
2 1/1	9.09	108	5.0	241.	5.1	2086	1511	147	6.0	207	6.1
211	1927	0	7.39	251	4.5	4086	274/	•	./0.34	210	11.2
23/./	2411	1775	13.00	130	13.2	2014	1+44	7170	14.0	209	14.2
1724	1314	276	7.0	377	7. 1	3067	2120	369	10.0	341	10.2
\$77.4	2737	. 0	15.01	272	15.3	3447	4/07		13.54	342	17.8
172.4	32 46	1743	18.0	377	19.3	1417	4638	9766	20.00	341	20,3
471.5	16/2	417	9.0	472	4.2	485,0	2753	487	12.0	455	12.2
9 74.5	2195	0	10,44	472	18.8	135.6	5019	. 0	12.8+	455	23.3
* 34.5	3606	7744	21.0	472	21.3	455.0	5+++	. 7746	260	454	25.4
5/03/	150	35		700	-	122,0	.5297	125	34.0	.915	35.1
4321	3772	0	3207	722	32.5	7220	5915	0	+0.85		+1.+
\$22.6	344	, 9695	34.0	923	34.4	922,0	6070	9775	42.0	722	
1101.5	2707	101	30.0	1097	30.1	10 3/.5		115	39.0	1032	37.5
1101.5	3195	0	35.93	1100	36,2	1081.6	5470	0	+1.77	1033	44.6
1101.5	3282	1014	37,00	1100	21:3	1031,5	. 2281	7786	45,0	1033	45.7.
1171,4	2377	8/2	320	1191	31.0	1164.5	: 4217	. 800	43.0	1165	43.2
1196. #	2738	•	37.3/	1191	37.4	1164.5	4658	0	46.97	1165	4717
1191.4	2049	9693	39.0.	1191	34.0	1164,5	4445	977/	+8.0	1165	48.4
13.0		I	30 4 1			71 -74		V.			
227.1	1318	130	6.0	227	6.1	,214.6	2047	- 204	7.0	214	7.1.
2271	2283	0	10.43	227	10.6	2 M.L	3472	0	12:94	214	13,2
227.1.	3019	9761	14,0	226	14.2	210,6	4470	9768	16.0:	214	16.4
349 = .	1921	279	9.0	340	9,2	356,2	3035	532	17.0	355	11.3
3400	3194	• '	15.35	340	15.6	355,2	5504	•	20.07	356	21.4
3440	3706	9772	18.0	340	18.3	356.2	6006	9749	23.0	355	23.5
487.0	2381	562	. 12.0	484	12.2	+91.8	4532	915	18.0	501.	. 18.4
4878 '	4105	0	21,42	488	21.2	+11.8	6870	0	28.48	500	29.2
+87.8	4381	9828	23.0	488	23,9	417.8	7/90	9787	340	499	30.7
WI Lie	20 1 20	4 1 5 1			20,9	911.6	7098	856	42,0	910	42.7
93311	4651	0	36.36	932	36.8	911.6	7676	0	. 46,86	913	47.3
933!	4724	9889	37.0	933	37.4	: 911.6	7766	9861	47.0	913	48.0
1079.3	3644	8/6	35.0	1079	35.4	1059.4	6375	.701	17,0	10.01	48.0
1079.3	4105	0	39.9/	1079	40.4	1059.4	6857	<b>6</b>	\$1.11	1061	52.2
1077.3	1205	9791	440	1079:	41.5	1059.4	6154	9789	52.0	1061	53,1
1157.9	1276	770	37.0	1158		11976	5190	772	540	1198	. H U
1157.9	3448	0	41.40	1 12	37.2	1197.6	5483	0.	5128	1198	54.5
1157.9	3496	9882	42,0	1158	41.7	11976	5644	9820	SSAO	1198	
		,	100	1158	42,3	* "	7-6				

ISS MM JABRANT THE THE N CHEC

### AIR. TEMPERATURE . PLUS ST. F

32					110	W. 25 .	·	I.		
0 R.		T	• .	L'	9	R.	H .	T	•	t'
2196 - 277/ .	257	1.0	213	7.4	2164.	4031	+ + + +	140	015	11, 3
219.6" 4719	0 .	14.03	215	15.6	3/46	7752		20.02	TIO .	20. 8
	9721	18.0	215	18,9	210.6	9341	1776	22.0.	210	22.9
362.5 4822	701	14.0	30+	.14.6	347.0"	8+67	843 .	24.0	349	23.7
342.5 7094	0	24.24	364	27.4	3474	10572	i • ,-	34 17	348	31.8.
	9785	160	.364	27.3 .	247.0	10000	9770	32.0	348.	33.9
	903	23.0	482	24.1	4113	11657	895	160	497	37.6
479,3 8502	0	3/.22	480	32.7	4143	12951	0	41.28	498	43.2
	1727	33.0	480	34.6	472.3	13186	9850	42.0	499	4 4.0
	771	41.0	890	50.3		14297	814	64,0	907	65.9
700.7 9854	0	52,40	893	54.0	915,0	14782	0	46.87	911	69.2
9007 9996	9856	640 .	.874	54.6	915.0	11802	9963	67,0	901	69.4
1046,5 8531	734	55.0	1047	57.2		19107	647	72.0	1064	75.0
1096.5 8907	0	57.91	1097	\$0, 2	10453	15382	0	74.06	1064	77.2.
146.5 9043	9711	59.0	1047	61.3	10873	13505	9700.	75.0	1054	78.2
196.7 6761.	77/	59.0	1195	59.9	1103.7	10871	636	76,0	1183	77.2
194.7 7033	0	6187	1196	G 2.9	1/03.7		0	77.95	11 54	79.4-
196.7 7044	9965	62.0	1196		11.83.7.	31/082	9982	78,0	11 84	79.4
<b>Y</b>	Γ		2							
209.2 3792	349	10.0	202	10.3						
209.2 6001	0.	17.01	209	17,8						
209.2 6592	9820	19.0	209	19,9						
334.7 . 4956	830	14.0	336	14.5						
334.7 8384	0, 1	25.83	336	27.0						
334.7 8698	9851	27.0	336	78.2						
462.7 8675	848	28.0	464	29,3						
462.7 10278	6	34.32	904	36.0						
441.7 10685	9720	36.0	464	37.7						
911.2 11766	694	57.0	901	58.7						
9/1/2 12206	ø ·	59.67	904	G1.6						
		60,0	909	67.0						
1094.4 10037	694	68.0	1046							
1044#	•	65.94	1046							
10444 /1297 9	885	46,0	1045	1 68.	7					1
	860	67.0	1199		0					
1194.3 8848	4 4 1	69-87	1199		9 .					
1/94.3 886/ 9	758	70.0	119	1 1						

A-43

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# Armed Services Technical Information Agency

ARLINGTON HALL STATION ARLINGTON 12 VIRGINIA

FOR
MICRO-CARD

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CONFIDENTIAL

### MY MM QUADLANT ELEVATION CHECK

AIR	Ten	PERATURE	MINUS	59 ° F
-----	-----	----------	-------	--------

1632 4500 1500 2760 1158	9776 275	T 6,0 1.11	7 5,1	7'	0	R	征		•	T'
1612 2500 1500 2760	9778	7.17	7 5,1							
2500 1500 2760	9775			6.1	2096			6.0	207	6.1
1500			231	1.6	2136			10.70	216	11.2
2750	274	13.0	231	12,2	209.4	100			201	142
	-/-	8,0	3,77	2.1	3+1.7	2411		10.0	241	10 2
II CA	0	15.03	478	15.0	341.7	4118	0	17.54	3,92	17.5
	9741	18.0	378	1 h y'	341, 7	4699	9766	20.0	342	20.4
1788	4/4	10.0	-172	10.7	14.0	2717	638	12.0	454	17.
3201	0	18,46	472	9,_	116.0	:037	0	22 8	450	73.9
3619	9746	21,0	473	21.9	+65 1	5964	9706	25,3	175	75.1
					9220	5319	832			365
	Ų	32./4			922.0	5962	0	10,12 .	120	41.6
		33.00	927	231	1-20	6100	478F	+1.0		427
		30.0	10 1 m	: 11.2	1031.5	5050	764	400	1934	10,8
3209	0	3518	1101	261	1031 :	5503	0	44.05	1032	14.9
3290	9823	37.3	1105	2.7.4	1611-	560+	7801	45.00		459
2383	812	32.0	11 7	32.1	1114,5	4222	819	43.0	1166	
2750	0	37.39	11-11		1/29	4534	. 0	4705		
2791.	9: 3A	38.0	11 11	381	1100	4664	9790	48.0	11.65	49.6
	IĮ.						17			
13+0	130	6.0	227	· 1	2/4.6	2014	200	7.0	215	7.1
2290	0	10.43			214.6	3544	0	12,82	214	13.0
3018	9761	14,0			214.6	4+12	9158	16.0	214	16.1
1925	280	9.0	3.70		5541	2003	521	11.0	355	11.1
3208	0	15.36	2000		30 % -	5391	0	20,67	354	20.9
3720	9774	18.0	340		355 4	5142	1797	23.0	354	23,2
2387	554	12,0	99.	•	4.79.8	4412	894	18,0	199	18.2
	0	21.45	A . C.		499.8	6764	0	2823		28.6
4100	-	23,0	488		4193	7/36	9751	30.0	•	30.4
4039	8045	31.0	1728	314	111.6	7026	803	42.0		42.4
4679	0	34,44	4 3 8	37.0	911.6	7616	0	46,00		46.8
4858	9721	38.0	932	38.6	911.6	7796	1800	47.0		17.8
3666	83!	35,0	1080	35, 6	1059.4	6356	893	47,0	1060	47.
4/28	0	39.99	1077	40,7	1059.4	6805	0	50.84		51.7
4220	9806	41.0	1074		1059.4	6437	9723	52.0		529
3307	786	37,0	1159		1197.6	5182	707	51.0		5100
3668	0	41.98	115%		119716	5442	0	53.79		51.0
3709	9890	42.00	1153		1197,6	5527	9748	55,0		55.0
	27/0 3209 3290 2383 2750 2791 3290 3218 3215 3215 3215 3215 4128 4128 4128 4128 4128 4128 4128 4128	3849 9866 3209 0 3190 9823 2383 812 2750 0 2790 0 3018 9761 115 280 3029 0 3018 9761 115 280 3208 0 3720 9771 1387 554 9128 0 4100 9821 1403 8045 14128 0 4128 0 4128 0 4128 0 4128 0 4128 0 4128 0 4128 0 4128 0	3849 986 986 986 20.0  2710 861 20.0  3209 0 3598  3290 9823 27.3  2383 812 32.0  2750 0 37.39  2791 9598 38.0  II  1340 130 6.0  2290 0 10.43  3018 9761 14,0  1315 280 9.0  3208 0 15.36  3720 9774 18.0  1387 554 12.0  4128 0 21.45  4100 9831 33.0  4128 0 31.45  4128 0 31.91  4220 9806 41.0  3307 786 37.0  41.98	3758 32.14 32.2 3849 9166 33.60 926 2710 861 20.0 16 12 3209 0 3596 1100 3190 9833 37.0 1100 2383 812 32.0 1171 2383 812 32.0 1171 2750 0 37.38 1171 2790 0 10.43 72.7 2290 0 10.43 72.7 3018 9761 14,0 22.6 1115 280 9.0 22.7 2308 0 15.36 340 3720 9774 18.0 340 3720 9831 23.0 488 4039 8045 31.0 428 4039 8045 31.0 1080 4128 0 31.91 1077 4858 9721 38.0 932 3666 83: 35.0 1080 4128 0 31.91 1077 4130 9806 41.0 1077 4120 9806 41.0 1077 4120 9806 41.0 1077	3750 32.14 32.0 384) 9866 33.0 922 23 1 27/0 861 20.0 16 12 1.2 3103 0 3596 1106 26.1 3190 9813 27.3 1105 27.4 2383 812 32.0 1131 37.5 2750 0 37.39 1131 37.5 2791. 9898 38.0 1131 37/ 11 1340 130 6.0 227 6.1 2290 0 10.43 227 10.6 3018 9761 14.0 226 19.2 3018 9761 14.0 226 19.2 3290 0 15.36 240 15.7 3208 0 15.36 240 15.7 3208 0 15.36 240 15.7 3208 0 21.45 4.8 21.9 4100 9821 23.0 488 23.5 4100 9821 23.0 488 23.5 4100 9821 23.0 488 23.5 4101 0 3645 31.0 928 31.4 4101 0 3645 31.0 928 31.4 4102 9806 4.0 1079 40.7 4120 9806 4.0 1079 40.7 4120 9806 4.0 1079 40.7 4120 9806 4.0 1079 41.7 41.7	3758 32.14 712 32.0 12.0 38.4 97.1 27.0 861 20.0 10 18 20.2 10 31.5 10 31.0 31.0 9823 27.3 1105 27.4 1611 27.5 1611 27.9 17.5 1611 27.9 17.5 17.6 17.6 17.6 17.6 17.6 17.6 17.6 17.6	37.58 32.14 31.0 51.0 51.0 51.0 51.0 51.0 51.0 51.0 5	3756 32.14 31.0 31.0 5962 0 3849 9866 33.60 926 23.1 12.0 5962 0 3210 861 20.0 16 18 20.2 18.6 5050 766 3203 0 3596 1106 36.1 18.6 5050 766 3210 9823 27.3 1102 27.4 1611 5602 18.0 2383 812 32.0 1111 37.5 1164 4584 0 23791 9698 38.0 1131 37.5 1164 4584 0 23791 9698 38.0 1131 37.7 1164 4584 0 2390 0 10.43 72.7 10.6 2146 3596 0 3028 9761 14.0 72.6 10 2146 47.2 9758 3028 0 15.36 200 15.7 3552 5397 0 3028 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 0 15.36 200 15.7 3552 5397 0 3020 9774 10.0 340 18.4 3552 5397 0 4100 9821 23.0 488 23.5 1133 7136 7157 1 4037 554 12.0 47 12.2 4998 4992 4964 0 4100 9821 23.0 488 23.5 1136 7166 7026 803 1167 0 4100 9821 23.0 488 23.5 1116 7026 803 116	3758	3758 32.14 32.0 32.14 32.0 32.0 32.0 32.0 32.0 32.0 32.0 32.0

# ISE MM QUADRANT ELEVATION CHICK

### AIR TEMPERATURE MINUS 69 . P

						C M/6	V1 67				
			3	530	100			M			
•	K	**	1	•	T'	0		н	7		-
3114		247	1.0	115	9.1	210.6	1000	509	110	205	11.5
211.6		0	17.54	215	14.6	211,4	7459	•	40.4	211	
3 M.C		1602		214	17.C	2144	8540	7748	250	210	21,1
<b>なりつ</b> 。		680		363	1 4 1	3120	8410	878	210	350	23.6
30.5		0	2356	351	.2.3,6	347.0	10441	0	50.77	347	31.9
362.5		9850		360	240	347.0	10773	1820	32,0	346	32.6
+74.3		883		977	22.1	1743	1/442	709	23.0	499	36.7
477.3	7969	0	10.18	478	34.3	4962	12 461	o	3479	498	42.0
4793	8853			478	0.56	419,3	12848	9843	+2.00	498	42.7
900.7	8735		+7,0	901	47.2	115.0	14079	757	64.0	912	65.0
900.7	9353	0	50,36	909	51.5	915,0	14509	0	66.78	915	
9047	9511			904	52.5	415.0	14541	9940	67.1	916	67.9
1045		829	53.0	1049	53.5	,0613	12784	906	21.0	1064	68.1
1145	8473	0	5639	100%	56.9	1648.3	13:67	0	74.10		72,6
10465	8549	9841	57.0	1048	57.5	10614	13272	. 1734	•	1064	75.5
1196.7	6385	844	57.0	.1198	56.5	. //83.7	10613	896		1054	76.2
1196.7	6687	0	60.23	1194	51,6	11837	10898	0	75.0	1184	74.8
1196.7	6756	9790	61.0	1138	60.4	1183.7	10990	9687	77.97	1185	77.8
							10110	1601	79.0	1185	78.7
	- \	YI									
201,2	3754	353	10.0	207	10.3						
209,2	5923	0	17.14	7.10	17.5	*					
201.2		. 9733	2,0,0	209	20,3						
3 84,7	4895	828	14.0	336	14:3						
331.7	8110	0	25,72	334	26,0						
3 34,7	8437	9836	27.0	333	27.2						
462.7	8182	904	27.0	452	27.2						
462.7	9866	. 0	33,9/	462	34.2						
442.7	10120	9821	35.0	461	35.2						
911.2	11342	68/	56.0	911	5G.8						
911,2	11771	0	58.67	913	59.6						
911.2	11822	9913	59.0	914	60.0						
1044.4	10475	665	62,0	1047	63.3						
1044,4	10794			1007	673						

65.5

66.1

65.7

68,5

64,40 1097

1047

1195

1196

1196 68.3

65,0

66,0

68.78

69,0

1044.4 10794 0

1844 10877 9829

11943 8569 9919

796

0.

1194.3 8277

155 MM	4 Uhon AN	17	ELEVAT	104	CHECK
	W	OF	PACU.	+/	SQUAKE

				~	Or.	FN EV.	-/	SOUNK	-		
	(1	SEN	BHE			.II	I. G	KEEN	BAG	-	
6	K	H	T	۵.	•	. 6	R	H	+	. 6.	· . F'
23/1		741	6.0	2110	60	2016	1524		40	201.7	6.1
2311		0	7.34	231.1	9.4	2096			11.4	207.1	
	2+85	7772	110	230.5	13.1	201.6			14.0	208.	
-77.		272	90	3748	80,7	3 41.7			10.0	341.9	
11:4		0	14.94	3772	15.1	341.7	4080		17.€	341.8	12.7
31/4		7737	150	3773	18.2	3 41.7	462		21.1	341.4	
371.5		409	100	4712	10.1	455.6	2743		12.0	485.5	
7/15		0	18.36	4720	18.6	4 5 5,0	475	1.00	22.8	455.2	Committee of the commit
	3576	4736	21,0	4725	212	4 35,1	5434	9734	25.0	465.0	
200 6		0	31.96	9231	32.3	922.0	52 86		30.0	915.6	
		7817	3300	923+	37.3	122.	5891		. 40.7	7210	41.1
	2695	833	30.0	10186	30.0	922.0	6063		42.0	216	41.5
	3174	0	3 5.79	11000	34.0	1031.5	4901		37.0	1032.5	39. 4
1131.5		9187	37.0	11000	37.2	1031.5	5446	0	43,8	1032.2	
1171.4		916	31.0	11916	30.9	1031.5	5578	9734	45.0	1032.3	45,6
	2721	0	37.17		37./	1164.5	+219	770	43.0	1165.4	43.2
11:4	2775	9852	3000	11915	37.9	11645	4 538		468	1164.7	47.0
11.		/	A1 F 3			1164.5		9737		1164.9	48.3
		FEW	ر من الله	-		777	4:14				
227.1	1332				0.6.0	209.6	1526	145	6.0	204.5	6.1
227.1	2264		10.4	227.	2 10.5	209.6	2725	0	10.1	219.4	11.1
227.1	3010		1+ -	226	3 14.2	209.6	2+38	9796	14.0	208,7	14.2
340.0	1914	276	9. 9	384.	4.1	341.7	24/3	365	10.0	341.5	10.2
340,0	3172	0	15.3	340,	15.5	341.7	4070	0	17.5	3416	128
3 + 0.0	3697	9766	18.0	337.	9 18,2	3 41.7	4622	9760	21.0	341.1	20.3
487.8	2373	547	12.0	188.	1 12.2	455,0	2747	6329	12.0	455.6	12.2
497.9	4080	٥	21.3	487	7.1.7	4 55.0	5001	0	22.8	454.7	23.2
4679	7372	9819	23.0	487.4	23.3	+55,0	5442	9738	2.5.0	454,6	25.4
933.1	3894	. 974	30.0	903.5	- 11	122.0	5295	8//	36.0	918.4	36.3
933.1	4627	0	36.2	932.3	36.6	922.0	5914	0	40.8	9216	41.3
433.1	9714	9866	3 7.0	932.7	37.4	922.0	6071	7758	42.0	9219	12,6
1079.5	3634	792		108.1	35.4	1031.5	4115	899	37.0	1033.7	39,6
1071.3	4081	0	37.8	108.0	40.2.	1031,5	5460	0	43.7	10326	45:5
10793	4195	9762		108.0	47.4	1031.5	5581	9766	45.0	1022,5	45.7
1157,9	3206	878	36.0	115.9	36,2	1164,5	4214	782	430	1166.1	43.3
1157.9	3629	0	41.2	115.4	11.4	1164.5	1549	0.	46,9	1165.0	47.2
1157.9	3687	9853	12.0	115.8	42,2	1164.5	4644	9750		1165,0	43.4

155 MM SURDAMME ELEVATION CHECK

1	$\mathcal{K}$	GREEL	1 81	16			Z.	GRE	EN	PHG	
210		K		5 ,6	F'		G	- 261+		t	6.
214.					13.1		211.6	3994	3 46	1.0	314.2
, 14								7234	()	14.6	214.6
7.5 5							14 5	\$217	74:7		2 16.8
1 * 6 }		_						3756		13.0	563 4
111.4					31,1		311.5	6916		23.9	362.5
4111					3 5.4		3(1.5	7343	7722	265	2:15
9124		*			19.3		179. :	6:12	542	23.4	174.5
							111. 1	6361	2	30.7	979 1
47.14	7/6		-				77.3	7:16	7 - 14	32.0	47" :-
9/11:	703						10:1	11/4.	712	98.0	A 74.6
7/1.5	743		34.2				* a * a	75770	3	51.6	9.17
7112	775						03.7	16001	1-16	60.0	1715
1019.4						11	14:	5274	752	540	100 5,
10574			51.3				746.5	c: 64		57.0	154/9 .
1954			. 3				46 37	2137	1742	59.0	1047.7
1177.			5/2			11	7	6766	775	291	1196 2 .
1195.			* .3	1 /12, 4	537	11:	76 .	CRAT	0	629	110,00
11 37.	- 553	2 976	3 55	119.6	3.4 2	111	1 - 7	1291	7730	45.3	1/77.1
IV	W	HITE	K1. 6	,		T	z 1	VHITE	EH	· ·	
214.6	2037		7. 3		7.1	214,0			7,0	2 /4. 2	
2196	3633		12.9	219.6	13.1	211.6			12.4	2/9.6	
2 14,4	4430	7763	14.0	2/4/1-	16.2	211.6			14.0	214.1	13.1
255,2	3021	52.7	11.0	365,0	11.2	355,2		527	71.0		16.3
355,2.	5460		34,8	355,2	21,2	355,2		4	20.6	3 75,0	11.2
301.m	. 1785	9754	3 3. d	355,1	23.1	355.2			23,0	355,2	21.2
117.9	4514	705	18.0	500.1	15.74	499.8	4516	905		355,2	23,4
4776	6823	,0°	284	49916	29.8	171.6	6638	0	28.4	. 500.1	19.+
47%	7/7*	7770	30.0	497.8	30.6	197.9	7/74	7770		499,6	29.0
271.6	2012	628		706,6	ALIC	911,6	7041		30.0	477.8	30.6
911.4	7650	ರ ನ	42.8					828	42,0	906.6	42.5
711.6	7762		46 2	910.2	47.6	911.6	7450	0	46.2	9/0.2	47,0
1057,+	6368	9828 848	77.0	910.5	97.8	911.6	7762		47.0	910.5	47,6
		RE9	47,0	1060.8	47.9	1059.4	6368	869	17.0	10403	47.9
•	6931	0	51.8	1065,0	51.9	1004,4	6837	0	51,8	1060.0	51.9
	6750	9752	52,0	1059.9	329	1169.4		1752	52.0	1059.9	53.8
!!97.6 !!97.6	5173	736	51.0	1/97,6;	5/11	1197,6	5143	736	51.0	1197.6	51.1
	5465	0	5 4.1	1197.7	54,2	1197.6	5465		54.1	1/97.7	54.2
197.6	5540	<b>97</b> 80	55,5	1197.8	35,1	1197.6	5220	9806	55.0	1197.5	53,1

155 MM GUADRANT ELEVATION CHECK WY OF PROJ. + I SQUARE

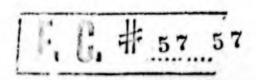
	VI U	UHITI	F 81	16	
€ 201.2	2770	H	. t	200	11.2
209.2	5717	0	פגרוו	2.19, 5	
211.2	6503	7040	19.0	219.0	
33 4.7	4710	811	14.0	826,1	
339.7	83/6	0	25.7	331.8	
334-7	4561		27.0	334.6	
462.7	9271	nie	27,0	162,6	
467.7	10050	0	34.0	162.7	
462.7	10293	94+0	35.5	40.5	
911,2	1156+	747	. 54.0	705.	
911.2	11775	0	54.1	7/6:3	
911.1	12/1+	7730	64.0	1701.Z	Y
1044.4	10587	78A	69,0	11 14.5	648
1011.4	10770	0	64.8	1144.7	46.0
1049.4	10996:	9742	65.8	1096.4	67.0
1194.3	8164	454	67.0	1174,5	67.4
1199.5	4443	0	49.2	1174.8	67.5
1174.3	8720	4750	74.6	- 1144.8	70.2
-					
V	II h	VHITE	813	( <del>-</del>	1
POG.	4843	500	11.0	208, 4	17. 3
2106	7735	. 0	20,2	211.7	20.8
210,6	6244	9810	22.0	2 10.5	22.7
347.0	ñ435.	850	23,0	247.0	23.7
347,0	10504	0 '	30.5	347.1	31,5
347.0	10888	9779	32.0	3 4 7. 0	330
498.3	11545	882	36.0	497.3	37.1
118,3	12794	. 0 .	41.0	178.1	43,5
178.3	12994	9833 .	42.6	443.4	43.3
915,0	14199	745	64.0	907.8	65,5
915,0.		0	66.6	912.2	68, 4
915,6	14687	7847	67.0	1/2.5	GA.B
10633	12880	₽73	71.0	1064,9	75.3
10663	13260	6	72.9	1063.7	74.1
1068.3	13297	4557	75.0	1063,6	772
1193,7	11694	848	75,0	1183.7.	75,5
1183.7	10976	0	778	1140.5	78.4
1163.7	10999	9125	744	11 84.5	707

### APPENDIX D

PART 3

COMBINED EFFECTS TRAJECTORIES

755 mm Rowitson



A-49

155 MM YOW ANGLE TEST PROBLEM

### COMBINED EFFECTS

ALL LINEAR DISTANCES IN METERS

ORIGIN REFERENCE OBS. CBS. LR DA DU EN HEN H DIST VA O O 0-4573 O 401 6401 -100 R500 A500 U137

	454.37		
CHARGE	OES.	*Kop	SETT INGS
	AZ	NO.	Transmitteness and those of programming and by any the end
I	1250	1	NORMAL .
11	2000	2	MUZZLE VELUCIII
III.	2250	3	300171 20172
IV.	2500	4	AIR DENSITY 110 %
V	2750	5	AIR TEMP.
YI	3250	6	POWDER TEMP
VII.	5500	. 7	PROJ. WT 5 SQUARES.
			USE GREEN BAG CHARGES I ANO II
			USE WHITE BAG CHARGES III TO VII

TEST ALL CHARGES FOR EACH PROBLEM ADDING EACH.

# 155 M. CONFIDENTIAL

### FRISHERS TO LOW AMOLE TEST INCHIEN'S

	MCKI M.S.					V			MV WIND			
C1. 5	<i>X</i>	AJ.	F	QE.	1 1	A	F	21	R	AZ	. F	6 2
1	2759	847	15.2	340	-759	846	15.0	703	2070	547	150	274
2	3268	2816	15.9	516	326.5	25/6	15.7		32.12	2821	157	287
3	4483	3056	197	354	1 0/483	3055	145	3.0	HARR	3060	116	335
./	5601	2510	21.7	346	. 5601	7:10	21,6	325	5601	3314	21.7	8-1
5	6:96	75.22	23.6	2500	2676	7522	20,5	923	: 6646	3527	38.7	347
2.0	1667	3885	28.2	351	8667	3-85	28,2	379	. 8667	3885	214	366
7	102.19	5346	30.2	,73 /	11219	5375	30.2	310	11218	5372	30. A	712
11	V 191	N.D - 1	VENS		MY H	WE D.	EVS	H. T.	1 : Y 1.	140 05	NS A.	. I.T.
1	2579	48	15.0	502	2577	1118	15.0	301	2577	843	15.0	3177
2	3268	2321	15.7	272	3268	2821	15.7	271	3268	2972.	155	316
8	44.83	3000	19.6	337	4.123	3066	196	3.00	111/85	3361	19.7	. 57
24	5:01	3315	217	347	5601	3315	21.8	204	1601	3315	214	375
5	1.61%	2527	23. 8	360	6676	3527	237	377	6:95	2528	24.0	341
. 6	7267	3686	27.5	91:	2667	3886	28.6	546	F167	3886	28.7	410
7	10218	1374	50, 5	352	16218	5374	80.3	381	10218	5374	30,7	346
				M	V WIND	DEAS	AT.	P.T. WIT.				
					2579	4118	15.0	3/3				
					3268	2822	15.8'	303				
					4453	3061	19.8	361				

2601 3215 22.0 377 6696 3528 24.1 343 2667 7286 28.7 411 102,8 5374 30.4 547

155	MM	HIGH	ANGL	E	TEST	PROBLEM
			COMBIN	vE0.	EFFE	ecrs
		o ic ra u c		de <del>v</del> o	6.4	199.00

								0				
CHRICE	6	116	IN	1:	EFER	ENCE	CES.	OFS	085	LR	DA	DU.
	E	N	H	E	N	H	DIST	AZ	VA			4
7	0	0	0	0	2313	100	0	0	0	0	0	0
II	0	0	0	0	4298	100	C	0	0	0	0	0
THE	0	0	0	0	5595	100	0	0	0	0	0	0
LIY.	0	G	0	0	6858	100	0	0	0	0	0	0
F	0	0	0	0	1617	100	 0	0	0	0	0	0
YI	0	0	0	0	10973	100	0	0	0	0	0	0
771	0	0	0	0.	13350		0	0	0	0	0	0

PROB .	SETTINES
NO	en e
1	NORMAL
2	MUZZLE VELOCITY - 30 F/S
3	NORTH WIND SO MIN ; EAST WIND 20 M/H
4	AIR DENSITY 90%
5	AIR TEMP. 1180F
6	POWDER TEMP. 130 ° F
7	WT. OF PROJ. 3 SQUARES
	USE GREEN BAG CHARGES, I TO I
,	USE WHITE BAG CHARGES IT AND VIL

TEST ALL CHARGES FOR EACH PROBLEM ADDING FACH SETTING TO THE PREVIOUS SETTING:

# ISE MA CEMPLAND EFFECTS

### ANSAIRS TO HIGH ANGLE TEST PROBLETS

	ACK.	5	480	M	V		MV			WIND		
CHS	R	RI	7 7	92	1 8	AZ	F	QE	18	AZ	F	95
	3.0	37	247	1000	21.7	31	299	1 1/2	1367	21	36.5	247
2	4278	87	31.7	1072	4210	21	17.6	410	4310		30.6	157
0.	5112	37	44 5	1644	1 1773	2	37 6	167	1372	33	26 7	915
*	5472	40	51.6	1051	6834	34	# 7.1	1313	4.87.00	36	42.1	943
-	2860	45	Stie	1045	3661	36	35.2	1011	7661	36	475	913
6	16447	42		1044	10900	37	64,8	1120	10748	39	54.0	915
7	1 12	48	155	1456	13228	~5	729	1659	13:22	41	. 4. 1	7:0
- 111	W/A	D 1	PENS		MY W	IND U	FAS	A.T.	MY NIA	O DE	NS. AT	. 1.7
1	1317	31	21.0	196	3547	30	57. F	890	3767	34	. 24.4	975
-	4.79	. 4.2	2.2	100	11279	31	31.4	813	1 4279	15	33.8	136
3	5372	36	29.4	248	5372	36	30.1	SHN	5372	38	39.7	974
* #	6833	39	45. 3	978	4133	39	45. Y	177	6732	42	47.0	1001
5	x659	41	514	471	1657	46	54.4	1007	8657	47	55.6	1020
6	10444	48	60.2	915	10943	51	626	1010	10442	52	64.11	1627
7	13316	57	76.4	1017	13314	58	71.8	1029	133/2	61	74.1	1047
	*			M	Y KIINO	DEN	S. AT.	P.T. WT.			7	
					3367	32.	= A. 8	918				
					4279	33	23.1	921				
					5572	38	39.5	968				
					4832	41	46 6	996				
					1657	47	55.5	1019				
					101412	52	64.5	1028				

APPENDIX B

PART L

FUZE

155 m nowlear

1 57.57

A-5

CONFIDENTIAL

155 711 FUZE CHECK

	and A	
raker in meri	FF & IN MILS	A IN SECONDS
$\mathcal{I}$	TV.	VI.
R & F F	R & F F'	. A OFF
1329 236.0 75 9.5	457 3138 137 13.2	5949 207.1 /7.4 17.6
2386 299.6 4.2 12.2	VIIS 246.2 15.2 15.1	6901 230.2 /9.1 19.2
2743 3696 15.2 15.2	4572 280.4 122 17.0	6158 2540 21.9 20.9
3200 4004 18.6 18.7	-5027 316.8 19.3 19.1	13/5 271.8 27.7 22.7
1313 3042 20.2 20.3	5476 356.1 21.5 21.3	7772 304.8 14.5 . 24.5
	5944 3994 23.9 23.7	\$130 331.0 26.4 ZG.4
3658 977.1 343 34.0	6401 447.6 26.5 26.2.	9677 300.6 34.3 24.4
3200 Hel. Y 370 36.4	crer co3.8 29.4 29.2	1144 34.0 30,2 30,4
2126 1163.8 37.0 37.4		9601 423.4 32,5 32.6
	7315 400.2 50.0 49.2	10058 4514 34.8 34.9
$\mathcal{I}$	6858 1652.0 52.3 51.4	10516 417.0 37.3 37.4
2286 222.8 10,6 10,6	6401 1109.2 53.9 53.0	
2743 276.0 13.0 13.0	5944 1158.6 55.2 54.2	11887 931.8 61.8 61.8
200 334.0 15.6 15.6		11430 995.4 64.6 64.6
3658 347.2 18.4 . 18.5	. <u>V</u>	10973 1643,2 16,6 66.4
4115 477.2 21.6 21.7	4572 212 6 15.0 15.0	10516 1012.8 61.1 67.8
1297 5744 23.1 23.2.	5029 239.4 16.8 16.8	10058 1117.8 69.3 69.1
	3486 267.4 18.6 18.6	1601 1149.6-70.4 70.1
1755 906.8 36.7 36.5	5944 296.6 20.5 20.4	
4572 911.6 St.6 38.2	6401 327.4 22.4 22.4	YII.
4115 1079.8 41.1 40.6	6858 360.2 24.4 29.4	1772 109.2 20.7 20.9
3658 1160,6 42.8 42.0	7315 395.4 26.6 26.6	8230 224.4 22.4 22.5
·	7772 433.6 29.0 28.9	8687 250.4 24.1 24.2
III	1230 475.8 11.5° 31.4	9144 272.2 25.9 26.0
2743 206.2 11.2 11.2	8187 524.2 34.2 34.3	1601 295,0 27.7 27.7
3200 246.8 13.3 3.3		10058 318,8 24,5 29,6
3658 2900 15.5., 15.5	9601 906.4 53.4 53.2	10516 343.8 31.4. 31.5
4/15 337.0 17.9 . 17.8	9144 916.6 56.6 56.2	10973 370.0 31.3 33.5.
4572 3892 20.5 20.4	847 1044.0 58.7 58.2	11450. 397.6 35.3 35.5
5019 448.6 23.3 23.2	1230 1092.0 60,3 59.7	11887 427.2 37.5 37.7
5395 505.0 25.9 25.8	7772.1134,2.61.6 61.0	12344 495.0 39.8 42.0
1028 6011 111		12802 493.2 42.2 . 42.4
6035 896.6 41.2 40.9		the state of the s
5486 1031.2 45.3 44.7		14630 916.4 69.1 68.5
5029 1106.0 47.2 46.5		14173 9764 72.1 71.6
4663 1156.4 48.3 47.6		13716 1620.8 74.3 73.7

1 ....

That Date

1050M Geometry Test Problems

Error

No.		AZ	East	Replot	Feight		_ 41	T	K	<u> </u>
1	2692	0	-8	2632	_6	_8	0	_8	_8	6
2	8000	0	_10	7990	96	0	0			7
3	145000	0	_14	14500	201.2	0	0	그0 그4	70	/3 0
4	2690	798	1900	1908	300.8	70	_2		0	11.2
5	8000	799	5646	5660	401.7	0	7	- 9	- 1	40.8
6	14510	799.5	10257	10253	503	40	-0.5	71	£ 3	41.7
7	2695	1597.3	2696	5	601.8		-2.7		10	43.0
g	8007	1599	8007	7	702	77	_1.0	_4	+ 5	41.8
9	14504	1599.5	14520	ó	804	- 5 - 7 - 4	-0.5	47	+ :	12.0
10	2700	2396	1919	_1903	904	Ó	_4.0	120	46	74.0
11	8016	2398	5687	-5656	805	416	-2.0		46	
12	14250	2383	10255	-9008	705			<b>430</b>	+1	45.0
13 14	2835	2840	986	-2665	590	4135	4360	4986	435	10
14	8055	3195.5	46	_8020	-906	122	4.5	746	-20	76
15 16	14500	3201	-20	_14510	_E03	O	41.0	-20	-10	73
16	2720	4008	_1938	_1914	-704	120	43.3	129	-5	_3
17	8020	4003.3	-5680	-5655	_604	120	13.3	-23	75	_1,
18	14510	4002 -	10263	-10234	-503	410	43.3	-10	_19	-3
19	2710	4807.7	-2710	10	<b>_4</b> 00	410	47.7	-10	410	0
20	8023	4804.5	-8014	22	-296	723	14.5	-14	722	_4
21	14510	4803.5 -	14504	36	-202	410	43.5	_4	436	-2
22	3480	5810	_1912	2900	_106	_	_			
23 24	8804	5601.5	-5650	5657	_106	<b>∠</b> 804	41.5	-7	ō	-6
	14495	5601.0 -	10244	10246	_106	<b>-</b> 5	41	49	47	-6
25 26	2823	6324.3	_220	2808	<b>-</b> 96			-	_	
20	14500	6301	_1420	14418	_103	0	41	41	412	-3
									,	-

#### 105 MM Georgicy Problems

						The state of the s				
Problem Number	hue	Aximuth	East.	Replot North,		1	AL	3		1
1	2690	6399.3	0	2685	0	70	_0.7	٥	15	0
2	7990	1.0	0	7990	100	_10	41.0	0	70	0
3	14502	0	15	14500	200.6	12	0	_15	0	40.8
la	2690	799.0	1902	1902	300.6	_10	_1.0	1 7	47	40.6
5	7990	\$00.0	5657	5657	401.8	10	0	0	0	41.8
6	14508	0.003	10253	10253	502.8	18.	0	0	0	12.8
7	2692	1598.3	2700	0	601.0	- 8	_1.7	0	0	41.0
8	8002	1599.6	8000	10	702.5	121	_0.4	0	120	12.5
9	14516	1600.0	14516	10	804.4	416	0	46	410	14.4
10	2698	2395.5	1923	_1900	903.0	- 2	4.5	414	19	43.0
11	8013	2398.5	5685	<b>-</b> 56 <b>5</b> 0	804.0	413	41.5	1 2.8	47	44.0
12	14260	2384.0	10253	<b>-</b> 9010	705.0	-240	<b>1</b> 6	0	<i>‡</i> 1143	45.0
13	2660	3207.0	_18.0	-2664	588.0	740	£ 7.0	_18	<i>4</i> 36	-2.0
14	8016	3196.0	50.0	_8000	-900.0	46 13	- 3.6	<b>4</b> 50	0	0
15	14514	3202.7	-20.0	-14500	_800.0	£14 14	1 2.7	_20	0	0
16	2715	4010.5	_1940	_ 1909	-704.0	£15 ↔	<b>410.</b> 5	_31	0	_4.0
17	8010	4004.3	<b>-</b> 5670	_ 5650	-605.0	110 1h	£ 4.3	_13	<i>4</i> 7	-5.0
18	14518	4003.0	10260	_10240	_502.0	41817	4 3.0	<i>4</i> 7	<b>4</b> 13	-2.0
19	2705	4808.0	_2710	15	_401.0		4 8.0	_10	15	_1.0
20	8012	4804.6	_8010	28	-301.0		£ 4.6	_10	0	2.0
21 1	4508	4803.4 _	14500	30	-203.0		4 3.4	0	30	-3.0

10500 Quadrant Elevation Check - Normale

	CHAS	GE I			c	HARCE II		
line	Helpht	0.1	Bros	Bange			Error	
952	68	201.4	11.4	1240	-			
1503	9993	201.2	11.2		73	201.0	£ 1.0	
2213	9758	200.8	40.8	1757	9996	200.0	0	
1677	419	499.0	- 1.0	2416	9799	201.0	£ 1.0	
2050	9997	501.2	4 1.2	2002	495	499.6	- 0.4	
3380	9758	502.7	1 2.7	3514	19	502.1	1 2.1	
2635	784	999.0	- 1.0	3835 3268	9812	503.5	1 3.5	
3190	43	1000.0	0	3208	723	999.0	- 1.0	
3281	9888	1000.0	Ö	3758	10	1002.0	1 2.0	
			•	3853	9843	1001.0	11.0	
	CHARG	E III						
1570	-				CH	ARGE IV		
1579 2098	80	201.0	1.0	1767	117	201 0	1	
2855	9936	200.6	40.6	2629	9991	201.2	4 1.2	
2571	9772	202.5	4 2.5	3415	9762	201.1	4 1.1	
4194	576	499.8	- 0.2	3079	725	202.6	1 2.6	
	10	500.0	0	5208	9979	499.0	- 1.0	
4366	9902	499.4	- 0.6	5432	9832	501.0	4 1.0	
3894	823	1012.0	712.0	4918	807	501.0	4 1.0	
4457	9976	1003.3	4 3.3	5433	9986	1007.0	4, 7.0	
4518	9866	1003.0	<b>→</b> 3.0	5499	9866	1003.0	7 3.0	
	CHARGE	-		7.33	7000	1002.1	£ 2.1	
	CUVKAT	•			CHA	RGE VI		
2313	156	201.0	<b>≠</b> 1.0	2890	225			
3392	1	201.0	41.0	4265	203	201.0	£ 1.0	
4170	9 <b>78</b> 8	203.0	4 3.0	4868	9987	201.0	£ 1.0	
4693	845	499.8	- 0.2	6669	9818	203.1	£ 3.1	
6724	9973	501.0	1.0		771	499.6	- 0.4	
7052	9749	501.1	7 1.1	8167	9976	500.6	4 0.6	
6540	756	1006.0	7 6.0	8472	9761	500.5	4 0.5	
7029	9918	1001.8	/ 1 @	8155	782	1002.0	1 2.0	
7076	9827	1001.5	7 1.5	8600	9985	1001.6	11.6	
			F)	8677	9837	1001.6	1.6	
	CHARGE 1	VII			CHAR	GE VII (Con	.+1 <i>a</i> \	
3661	299	202.6	126			(00)	10.11	
5442	9998	203.8	4 2.6	9972	9875	499.2	- 0.8	
6003	9826	50π°υ	4 3.8	10040	636	1004.4	7 4.4	
8589	754	498.7	4.0	10393		1001.5	7 1.5	
9838	9975	498.8	- 1.3	10473		1001.5	7 1.5	
	7717	<b>770.0</b>	- 1.2		-		F 4-7	

Line Land Chick

1191   63   199.8   -0.2   1564   76   200.0   0		Ct	rge I			Che	rge II	
1607	Bance	le (eh)	L.E.	Error	2an	ee Meleb	2 <u>C.E.</u>	Error
1607	1191	63	199.8	-0.2	156	4 76	200.0	0
2328 9779 201.1 A.1 2324 9764 200.2 70.2 1677 219 349.0 -1.0 2324 256 330.5 70.5 12590 0 350.6 70.5 30.5 70.5 70.5 30.5 70.5 70.5 30.5 70.5 70.5 30.5 70.5 70.5 30.5 70.5 70.5 30.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 7			200.0					1.0
1697 219 349.0 -1.0 2324 256 250.5 60.5 2590 0 150.0 0 1273 0 350.8 60.8 3113 9755 350.5 60.5 3271 9733 501.0 1.0 2099 436 492.0 -2.0 2744 539 499.5 -0.5 3318 0 600.4 60.4 61.0 4176 0 500.0 0 3719 9733 501.0 60.0 4537 9763 500.0 0 2039 875 1002.0 6102.0 470.0 0 901.0 41.0 3789 0 898.3 -1.7 4919 9738 90.6 60.6 3946 9776 898.4 -1.6 3728 857 1054.0 60.0 2860 828 1061.0 611.0 4252 0 1050.7 60.7 60.7 60.0 610.				21.3				
2590								
3113 9755 350.5								
2099		100						
3318 0 0 0.4 0.4 176 0 500.0 0 3719 9733 501.0 0.0 1537 9763 500.0 0 2739 875 1002.0 102.0 102.0 10.0 3789 0 876 898.4 -1.6 3728 557 1054.0 14.0 2860 828 1061.0 11.0 12.7 -1.3 12.0 9868 1050.8 12.8 12.8 12.8 12.8 12.8 12.8 12.8 12								
3719 9733 501.0 6.0 4537 9763 500.0 0 2039 875 1002.0 102.0 4740 0 901.0 1.0 3789 0 986.3 -1.7 4919 9738 90.6 1.0 386.0 9776 898.4 -1.6 3728 857 1054.0 1.0 286.0 828 1061.0 11.0 4252 0 1050.7 1.0 3400 0 1048.7 -1.3 4320 9868 1050.8 1.0 34.92 9823 1049.3 -0.7 2995 828 1208.2 1.0 2931 803 1237.0 137.0 3363 0 1200.3 1.0 2730 9903 1199.4 -0.6  Charge III  Charge IV   2027 97 199.8 -0.2 2329 159 200.5 10.3 34.54 9766 200.7 10.7 1213 9791 200.4 10.4 2873 346 350.0 0 3295 501 351.0 11.0 4191 0 350.0 0 3295 501 351.0 11.0 4191 0 350.0 0 54.28 0 350.0 0 4633 9804 350.5 10.5 6006 9735 350.2 10.2 3540 690 499.4 -0.6 5217 753 500.6 10.6 5322 0 498.8 -1.2 6860 0 500.5 10.5 5728 9730 499.0 -1.0 7187 9783 500.0 0 5309 863 901.0 11.0 71.8 770 898.6 -1.4 6006 0 900.3 10.3 7721 0 900.0 0 6110 9848 901.0 11.0 7876 9765 899.5 -0.5 4900 848 1052.8 12.8 64.74 837 1050.4 10.4 5226 9678 1100.0 150.0 6928 0 1050.0 0 613366 739 1200.5 10.5 517 778 1200.0 0 64252 0 1199.3 -0.7 5457 0 1199.0 -1.0								
2939 875 1002.0 102.0 4740 0 901.0 11.0 3789 0 996.3 -1.7 4919 9738 970.6 10.6 3946 9776 898.4 -1.6 3728 857 1054.0 14.0 2860 828 1061.0 11.0 4252 0 1050.7 10.7 10.0 0 1048.7 -1.3 4320 9868 1050.8 10.8 3492 9823 1049.3 -0.7 2995 888 1208.2 10.2 10.3 1231 803 1237.0 10.7 10.0 3363 0 1200.3 10.3 10.0 11.9 1.0 10.0 10.0 10.0 10.0 10.0		9733						0
3789 0 \$96.3 -1.7 4919 9738 90.6 \$0.6 3946 9776 898.4 -1.6 3728 857 1054.0 \$4.0 2660 828 1061.0 \$11.0 4252 0 1050.7 \$0.7 3400 0 1048.7 -1.3 4320 9868 1050.8 \$0.8 3492 9823 1049.3 -0.7 2995 828 1208.2 \$8.2 2331 803 1237.0 \$437.0 3363 0 1200.3 \$6.3 2694 0 1199.7 -0.3 3428 9814 1200.0 0  Charge III Charge IV  2027 97 199.8 -0.2 2329 159 200.5 \$0.5 2632 0 200.3 \$0.3 34.28 9814 1200.0 0  Charge III Charge IV  2027 97 199.8 -0.2 2329 159 200.5 \$0.5 2632 0 200.3 \$0.3 34.24 0 200.3 \$0.3 34.54 9766 200.7 \$0.7 4.213 9791 200.4 \$0.4 2873 346 350.0 0 3295 501 351.0 \$41.0 \$4191 0 350.0 0 54.28 0 350.0 0 0 4633 9804 350.5 \$0.5 6006 9735 350.2 \$0.2 3540 690 499.4 -0.6 5217 753 500.6 \$0.6 5322 0 498.8 -1.2 6860 0 500.5 \$0.5 5728 9730 499.0 -1.0 7187 9783 500.0 0 5309 863 901.0 \$41.0 7148 770 898.6 -1.4 6006 0 900.3 \$0.3 7721 0 900.0 0 6110 9848 901.0 \$41.0 7128 770 898.6 -1.4 6006 0 900.3 \$0.3 7721 0 900.0 0 6110 9848 901.0 \$41.0 7128 770 898.6 -1.4 6006 0 900.3 \$0.3 7721 0 900.0 0 6110 9848 901.0 \$41.0 7128 770 898.6 -1.4 6006 0 900.3 \$0.3 7721 0 900.0 0 6110 9848 901.0 \$41.0 7876 9765 899.5 -0.5 6006 9785 1100.0 \$0.0 6948 9058 1051.0 \$41.0 \$3968 739 1200.5 \$0.5 5172 778 1200.0 0 6948 9058 1051.0 \$41.0 \$3968 739 1200.5 \$0.5 5172 778 1200.0 0 69425 0 1199.3 -0.7 5457 0 1199.0 -1.0								11.0
3946 9776 898.4 -1.6 3728 847 1054.0 42.0 200 828 1061.0 11.0 4252 0 1050.7 40.7 3400 0 1048.7 -1.3 4320 9868 1050.8 40.8 3492 9823 1049.3 -0.7 2995 888 1208.2 48.2 2331 803 1237.0 437.0 3363 0 1200.3 40.3 2694 0 1199.7 -0.3 3428 9814 1200.0 0  Charge III Charge IV  2027 97 199.8 -0.2 2329 159 200.5 40.5 2632 0 200.3 40.3 34.2 0 200.3 40.3 3454 9766 200.7 40.7 4213 9791 200.4 40.4 2873 346 350.0 0 3295 501 351.0 41.0 4191 0 350.0 0 3295 501 351.0 41.0 4191 0 350.0 0 5428 0 350.0 0 4633 9804 350.5 40.5 6006 9735 350.2 40.2 3540 690 499.4 -0.6 5217 753 500.6 40.6 5322 0 498.8 -1.2 6860 0 500.5 40.5 5728 9730 499.0 -1.0 7187 9783 500.0 0 5309 863 901.0 41.0 7148 770 898.6 -1.4 6006 0 900.3 40.3 7721 0 900.0 0 5309 863 901.0 41.0 7148 770 898.6 -1.4 6006 0 900.3 40.3 7721 0 900.0 0 6110 9848 901.0 41.0 7148 770 898.6 -1.4 6006 0 900.3 40.3 7721 0 900.0 0 6110 9848 901.0 41.0 7148 770 898.6 -1.4 6006 0 900.3 40.3 7721 0 900.0 0 5386 0 1051.0 41.0 6948 9058 1051.0 41.0 3968 739 1200.5 40.5 5172 778 1200.0 0 54252 0 1199.3 -0.7 5457 0 1199.0 -1.0								
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3400 0 1048.7 -1.3 4320 9868 1050.8 40.8 3492 9823 1049.3 -0.7 2995 888 1208.2 48.2 2331 803 1237.0 437.0 3363 0 1200.3 40.3 2694 0 1199.7 -0.3 3428 9814 1200.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		828		· ·				
3/492 9823 1049.3 -0.7 2095 888 1208.2 /8.2 2331 803 1237.0 /37.0 3363 0 1200.3 /0.3 2694 0 1199.7 -0.3 34.28 9814 1200.0 0	3400	0						
2331 803 1237.0 437.0 3363 0 1200.3 40.3 2694 0 1199.7 -0.3 34.28 9814 1200.0 0  Charge III		9823					_	
2694 0 1199.7 -0.3 2730 9903 1199.4 -0.6  Charge III								
Cherge III Cherge IV  2027 97 199.8 -0.2 2329 159 200.5 \$0.5 2632 0 200.3 \$0.3 34.42 0 200.3 \$0.3 34.54 97.66 200.7 \$0.7 4.213 97.91 200.4 \$0.4 2873 34.6 350.0 0 32.95 501 351.0 \$1.0 \$41.0 \$0.350.0 0 54.28 0 350.0 0 \$0.4633 9804 350.5 \$0.5 \$0.5 \$0.6 \$0.6 \$0.7 \$0.7 \$0.7 \$0.7 \$0.7 \$0.7 \$0.7 \$0.7	2601							
2027       97       199.8       -0.2       2329       159       200.5       \$\frac{40.5}{40.3}\$         2632       0       200.3       \$\frac{40.3}{40.7}\$       3142       0       200.3       \$\frac{40.3}{40.3}\$         3454       9766       200.7       \$\frac{40.7}{40.7}\$       \$\frac{1213}{4213}\$       9791       200.4       \$\frac{40.4}{40.4}\$         2873       346       350.0       0       3295       501       351.0       \$\frac{41.0}{41.0}\$         4191       0       350.0       0       5428       0       350.0       0         4633       9804       350.5       \$\frac{40.5}{0.5}\$       6006       9735       350.2       \$\frac{40.2}{0.2}\$         3540       690       499.4       \$-0.6\$       5217       753       500.6       \$\frac{40.6}{0.6}\$         5322       0       498.8       \$-1.2       6860       0       500.5       \$\frac{40.5}{0.5}\$         5728       9730       499.0       \$-1.0       7187       9783       500.0       0         5309       863       901.0       \$\frac{41.0}{1.0}\$       7721       0       900.0       0         6110       9848       901.0       \$41	2730	9903	1199.4	-0.6	70.6 %	, A. A.	. 200.0	
2632       0       200.3       \$\frac{4}{0.3}\$       34.42       0       200.3       \$\frac{4}{0.3}\$         34.54       9766       200.7       \$\frac{4}{0.7}\$       4.213       9791       200.4       \$\frac{4}{0.4}\$         2873       346       350.0       0       3295       501       351.0       \$\frac{4}{1.0}\$         4191       0       350.0       0       5428       0       350.0       0         4633       9804       350.5       \$\frac{4}{0.5}\$       6006       9735       350.2       \$\frac{4}{0.2}\$         3540       690       499.4       -0.6       5217       753       500.6       \$\frac{4}{0.6}\$         5322       0       498.8       -1.2       6860       0       500.5       \$\frac{4}{0.5}\$         5728       9730       499.0       -1.0       7187       9783       500.0       0         5309       863       901.0       \$\frac{1}{1.0}\$       7148       770       898.6       -1.4         6006       0       900.3       \$\frac{4}{0.3}\$       7721       0       900.0       0         6110       9848       901.0       \$\frac{1}{1.0}\$       7876       9765		Cha	rge III			Cher	rge IV	
34.54       9766       200.7       \$\frac{4}{0.7}\$       \$\frac{4}{213}\$       9791       200.4       \$\frac{4}{0.4}\$         2873       346       350.0       0       3295       501       351.0       \$\frac{4}{1.0}\$         4191       0       350.0       0       5428       0       350.0       0         4633       9804       350.5       \$\frac{4}{0.5}\$       6006       9735       350.2       \$\frac{4}{0.2}\$         3540       690       499.4       \$-0.6\$       5217       753       500.6       \$\frac{4}{0.6}\$         5322       0       498.8       \$-1.2\$       6860       0       500.5       \$\frac{4}{0.5}\$         5728       9730       499.0       \$-1.0\$       7187       9783       500.0       0         5309       863       901.0       \$\frac{4}{1.0}\$       7148       770       898.6       \$-1.4\$         6006       0       900.3       \$\frac{4}{0.3}\$       7721       0       900.0       0         6110       9848       901.0       \$\frac{4}{1.0}\$       7876       9765       899.5       \$-0.5\$         4900       848       1052.8       \$\frac{2}{2.8}\$       6474	2027	97	199.8	-0.2	2329	159	200.5	40.5
2873       346       350.0       0       3295       501       351.0       \$1.0         4191       0       350.0       0       5428       0       350.0       0         4633       9804       350.5       \$\frac{40.5}{0.5}\$       6006       9735       350.2       \$\frac{40.2}{0.2}\$         3540       690       \$499.4       \$-0.6\$       5217       753       500.6       \$\frac{40.6}{0.6}\$         5322       0       \$\frac{498.8}{0.8}\$       \$-1.2\$       6860       0       500.5       \$\frac{40.5}{0.5}\$         5728       9730       \$\frac{499.0}{0.9}\$       \$-1.0\$       7187       9783       500.0       0         5309       \$863       901.0       \$\frac{1}{1.0}\$       7148       770       898.6       \$-1.4         6006       0       900.3       \$\frac{40.3}{0.3}\$       7721       0       900.0       0         6110       9848       901.0       \$\frac{1}{1.0}\$       7876       9765       899.5       \$-0.5\$         4900       848       1052.8       \$\frac{2}{2.8}\$       6474       837       1050.0       0         5386       0       1051.0       \$\frac{1}{1.0}\$       6948	2632	0	200.3	10.3	31,42	0	200.3	10.3
2873       346       350.0       0       3295       501       351.0       \$1.0         4191       0       350.0       0       5428       0       350.0       0         4633       9804       350.5       \$\frac{40.5}{0.5}\$       6006       9735       350.2       \$\frac{40.2}{0.2}\$         3540       690       \$499.4       \$-0.6\$       5217       753       500.6       \$\frac{40.6}{0.6}\$         5322       0       \$\frac{498.8}{0.8}\$       \$-1.2\$       6860       0       500.5       \$\frac{40.5}{0.5}\$         5728       9730       \$\frac{499.0}{0.9}\$       \$-1.0\$       7187       9783       500.0       0         5309       \$863       901.0       \$\frac{1}{1.0}\$       7148       770       898.6       \$-1.4         6006       0       900.3       \$\frac{40.3}{0.3}\$       7721       0       900.0       0         6110       9848       901.0       \$\frac{1}{1.0}\$       7876       9765       899.5       \$-0.5\$         4900       848       1052.8       \$\frac{2}{2.8}\$       6474       837       1050.0       0         5386       0       1051.0       \$\frac{1}{1.0}\$       6948	3454	9766	200.7	10.7	4.213	9791	200.4	10.4
4633       9804       350.5       \$\forall 0.5\$       6006       9735       350.2       \$\forall 0.2\$         3540       690       499.4       \$-0.6\$       5217       753       500.6       \$\forall 0.6\$         5322       0       498.8       \$-1.2\$       6860       0       500.5       \$\forall 0.5\$         5728       9730       499.0       \$-1.0\$       7187       9783       500.0       0         5309       863       901.0       \$\forall 1.0\$       7148       770       898.6       \$-1.4\$         6006       0       900.3       \$\forall 0.3\$       7721       0       900.0       0         6110       9848       901.0       \$\forall 1.0\$       7876       9765       899.5       \$-0.5\$         4900       848       1052.8       \$\forall 2.8\$       6474       837       1050.4       \$\forall 0.4\$         5226       9678       1100.0       \$\forall 5.0\$       6928       0       1050.0       0         5386       0       1051.0       \$\forall 1.0\$       6948       9958       1051.0       \$\forall 1.0\$         3968       739       1200.5       \$\forall 0.5\$       5172       778<	2873	346	350.0		3295	501	351.0	11.0
3540       690       499.4       -0.6       5217       753       500.6       40.6         5322       0       498.8       -1.2       6860       0       500.5       40.5         5728       9730       499.0       -1.0       7187       9783       500.0       0         5309       863       901.0       41.0       7148       770       898.6       -1.4         6006       0       900.3       40.3       7721       0       900.0       0         6110       9848       901.0       41.0       7876       9765       899.5       -0.5         4900       848       1052.8       42.8       6474       837       1050.4       40.4         5226       9678       1100.0       450.0       6928       0       1050.0       0         5386       0       1051.0       41.0       6948       9958       1051.0       41.0         3968       739       1200.5       40.5       5172       778       1200.0       0         4252       0       1199.3       -0.7       5457       0       1199.0       -1.0		0	350.0	0	5428	0	350.0	0
5322       0       498.8       -1.2       6860       0       500.5       40.5         5728       9730       499.0       -1.0       7187       9783       500.0       0         5309       863       901.0       41.0       7148       770       898.6       -1.4         6006       0       900.3       40.3       7721       0       900.0       0         6110       9848       901.0       41.0       7876       9765       899.5       -0.5         4900       848       1052.8       42.8       6474       837       1050.4       40.4         5226       9678       1100.0       450.0       6928       0       1050.0       0         5386       0       1051.0       41.0       6948       9958       1051.0       41.0         3968       739       1200.5       40.5       5172       778       1200.0       0         4252       0       1199.3       -0.7       5457       0       1199.0       -1.0	4633	9804	350.5	40.5	6006	9735	350.2	10.2
5728       9730       499.0       -1.0       7187       9783       500.0       0         5309       863       901.0       \$\frac{1}{1.0}\$       7148       770       898.6       -1.4         6006       0       900.3       \$\frac{1}{0.3}\$       0       900.0       0         6110       9848       901.0       \$\frac{1}{1.0}\$       7876       9765       899.5       -0.5         4900       848       1052.8       \$\frac{2}{2.8}\$       6474       837       1050.4       \$\frac{4}{0.4}\$         5226       9678       1100.0       \$\frac{5}{5}0.0\$       6928       0       1050.0       0         5386       0       1051.0       \$\frac{1}{1.0}\$       6948       9958       1051.0       \$\frac{1}{1.0}\$         3968       739       1200.5       \$\frac{1}{0.5}\$       5172       778       1200.0       0         4252       0       1199.3       -0.7       5457       0       1199.0       -1.0		690			5217	753	500.6	10.6
5309       863       901.0       \$\frac{1}{1.0}\$       7148       770       898.6       -1.4         6006       0       900.3       \$\frac{1}{0.3}\$       7721       0       900.0       0         6110       9848       901.0       \$\frac{1}{1.0}\$       7876       9765       899.5       -0.5         4900       848       1052.8       \$\frac{1}{2.8}\$       6474       837       1050.4       \$\frac{1}{0.4}\$         5226       9678       \$1100.0       \$\frac{1}{5}0.0\$       6928       0       1050.0       0         5386       0       \$1051.0       \$\frac{1}{1.0}\$       6948       \$9958       \$1051.0       \$\frac{1}{1.0}\$         3968       \$739       \$1200.5       \$\frac{1}{0.5}\$       \$5172       \$778       \$1200.0       0         4252       \$0       \$1199.3       -0.7       \$5457       \$0       \$1199.0       -1.0		0	498.8	-1.2	6860	0	500.5	10.5
6006       0       900.3       \$\forall 0.3\$       7721       0       900.0       0         6110       9848       901.0       \$\forall 1.0\$       7876       9765       899.5       \$\forall 0.5\$         4900       848       1052.8       \$\forall 2.8\$       6474       837       1050.4       \$\forall 0.4\$         5226       9678       1100.0       \$\forall 50.0\$       6928       0       1050.0       0         5386       0       1051.0       \$\forall 1.0\$       6948       9958       1051.0       \$\forall 1.0\$         3968       739       1200.5       \$\forall 0.5\$       5172       778       1200.0       0         4252       0       1199.3       \$\forall 0.7\$       5457       0       1199.0       \$\forall 1.0\$					7187	9783	500.0	0
6110 9848 901.0 \$\frac{1}{1}.0\$ 7876 9765 899.5 \$\text{-0.5}\$ 4900 848 1052.8 \$\frac{1}{2}.8\$ 6474 837 1050.4 \$\frac{1}{2}.40.4\$ 5226 9678 1100.0 \$\frac{1}{2}.0\$ 6928 0 1050.0 0 5386 0 1051.0 \$\frac{1}{2}.0\$ 6948 9958 1051.0 \$\frac{1}{2}.0\$ 3968 739 1200.5 \$\frac{1}{2}.0\$ 5172 778 1200.0 0 \$\frac{1}{2}.0\$ 1199.3 \$\text{-0.7}\$ 5457 0 1199.0 \$\text{-1.0}\$	5309	863		<i>f</i> 1.0	7148	770	898.6	-1.4
4900       848       1052.8       \$\frac{1}{2}.8\$       \$\frac{6474}{6474}\$       \$\frac{837}{837}\$       \$\frac{1050.4}{1050.0}\$       \$\frac{40.4}{1050.0}\$         5226       9678       \$\frac{1}{100.0}\$       \$\frac{6928}{50.0}\$       \$0\$       \$\frac{1050.0}{1050.0}\$       \$0\$         5386       \$0\$       \$\frac{1}{105}\$       \$\frac{4}{105}\$       \$\frac{6948}{5172}\$       \$\frac{9058}{778}\$       \$\frac{1050.0}{105}\$       \$\frac{1}{100}\$         3968       \$\frac{739}{1290.5}\$       \$\frac{1}{200.5}\$       \$\frac{5172}{5457}\$       \$\frac{778}{278}\$       \$\frac{1}{200.0}\$       \$\frac{1}{100}\$         4252       \$0\$       \$\frac{1}{1199.3}\$       \$\frac{1}{0.7}\$       \$\frac{5}{2457}\$       \$\frac{1}{1199.0}\$       \$\frac{1}{1.0}\$	6006	0	900.3	£0.3	7721	0	900.0	0
5226 9678 1100.0 ≠50.0 6928 0 1050.0 0 5386 0 1051.0 ≠1.0 6948 9958 1051.0 ≠1.0 3968 739 1200.5 ≠0.5 5172 778 1200.0 0 4252 0 1199.3 -0.7 5457 0 1199.0 -1.0	6110				7876	9765	899.5	
5226       9678       1100.0       \$\forall 50.0\$       6928       0       1050.0       0         5386       0       1051.0       \$\forall 1.0\$       6948       9958       1051.0       \$\forall 1.0\$         3968       739       1200.5       \$\forall 0.5\$       5172       778       1200.0       0         4252       0       1199.3       -0.7       5457       0       1199.0       -1.0		848	1052.8	12.8	64.74	837	1050.4	10.4
5386 0 1051.0 \( \frac{1}{1}.0 \) 6948 9958 1051.0 \( \frac{1}{1}.0 \) 3968 739 1200.5 \( \frac{1}{1}.0 \) 5172 778 1200.0 0 \( \frac{1}{1}.0 \) 4252 0 1199.3 -0.7 5457 0 1199.0 -1.0	5226	9678	1100.0	<b>√</b> 50.0				
3968 <b>739</b> 1200.5 \$\int 0.5\$ 5172 778 1200.0 0 \\ 4252 0 1199.3 \$\int 0.7\$ 5457 0 1199.0 \$\int -1.0\$	5386	0	1051.0				1051.0	1.0
· 4252 0 1199.3 -0.7 5457 0 1199.0 -1.0	3968	739	1200.5	10.5				
	4252	0	1199.3					-1.0
	4283	9910	1200.5	10.5		9825	1199.0	-1.0

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# Curdrent Tlewtion Check.

				"formale				
	Ch	arge V				Ch	arge VI	
Sance	Heleb	e qr.	Lece		Eange	Heisht	<u>3.</u>	Error
2928	208	201.0	1.0		/110	291	201.4	1.4
4314	0	200.3			575/	0	203.3	+3.3
5234	2736	200.5	10.5		6513	9765	200.0	0
4536	594	149.8	-0.2		5784	823	353.0	13.C
6689	0	350.0	0		8475	0	350.0	0
7764	9778	350.4	10.4		0039	9834	34.9.5	-0.5
6570	912	500.5	10.5		0163	F02	501.2	11.2
8432	0	501.0	1.0		10497	0	490.0	-1.0
8679	9831	501.0	11.0		10633	9899	499.7	-1.0
9031	610	900.6	10.6		11431	908	8.500	12.8
9/01	0	900.0	0		12029	0	901.5	11.5
9659	9914	900.0	0		12094	9894	900.7	10.7
8241	810	1051.5	11.5		10497	865	1056.0	16.0
8657	0	1051.3	11.3		10914	0	1052.0	12.0
871.9	9804	1050.6	10.6		11034	9730	1052.0	1 2.0
6518	820	1199.6	-0.4		8345	698	1200.4	10.4
6807	0	1199.0	-1.0		8575	0	1200.0	0
6889	9749	1198.8	-1.2		8638	9796	1199.5	-0.5
	Che	rge VII						
5209	430	200.7	10.7					
7525	0	201.0	11.0					
8303	9728	200.6	10.6					
8434	088	353.0	13.0					
10569	0	350.2	10.2					
10884	9818	350.8	<b>≠</b> 0.8					
11539	911	499.7	-0.3					
12824	0	499.0	-1.0					
12985	9865	499.0	-1.0					
14220	806	904.1	44.1					
14704	0	899.5	-0.5					
14721	9969	901.0	1.0					
13117	708	1050.7	10.7					
13430	0	1055.0	15.0					
13513			<b>≠1.0</b>					
10372		1200.0	0					
10577		1200.0	0					
10656	9725	1199.4	-0.6					

105304 Quadrant Floration Check
(Plus Muzzle Velocity 50 ft/sec and 30 ft/sec)

	CHARGE	1 / 30 ft/	80C		CHAR	GE Y 1 50	ft/ sec
Bange	Heisht	Q.E.	Error	Banco	Peight	Q.E.	Error
1189	63	199.7	- 0.3	2963	121	202.5	1 2.5
1571	5	199.2	- 0.8	4049	9899	203.0	1 3.0
2317	9779	202.3	1 2.3	4575	9735	204.7	14.7
1752	460	500.2	40.2	5094	891	502.0	1 2.0
3372	9941	500.0	0	7300	9891	501.7	11.7
3681	9728	499.8	- 0.2	7045	790	999.0	- 1.0
2995	760	1000.0	110.0	7421	94	1001.4	11.4
3498	9981	1005.4	15.4	7545	9864	1000.6	40.6
3553	9883	1005.4	15.4				
	CHARGE	VI 4 50 ft/	вес		CHARG	E VII \$ 50	ft/sec
2653	237	201.0	11.0	3111	342	199.8	- 0.2
7400	9997	203.3	£ 3.3	5656	9997	204.2	14.2
4953	9835	201.0	1.0	6106	9844	201.0	11.0
7017	752	499.5	- 0.5	by11	752	500.2	10.2
8387	7	500.0	0	10107	7	501.5	¥ 1.5
8562	9885	500.0	0	10241	2885	500.3	40.3
8439	799	995.6	_ 4.4	10138	799	1010.0	410.0
8706	332	1002.1	4 2.1	10581	332	990.5	- 9.5
8967	9837	1000.8	40.8	10735	9857	1001.6	41.6

105MM Quadrant Elevation Check (Elmus Muzzle Velocity)

	CHANGE I (	_30f1/sec)			CHARGE II	(_30 ft/se	c)
mag	Palehi	Q.E.	Fror	Pune	Peight	ο.Σ.	Fror
730 1436 2119	68 9979 9738	200.5 200.6 197.7 496.3	4 0.5 4 0.6 - 2.3 - 3.7	1187 1571 2317 1752	63 5 9779 460	202.2 200.6 496.0	1 0.6
1908 2000 3089 2964 3051	335 9978 9785 9983 9832	1003.4 1009.0 1008.7	2 0.5 2 3.4 2 9.0 2 8.7	3372 3681 2945 3498 3553	9941 9728 760 9981 9883	500.9 503.0 1015.3 1003.4 1003.3	1 0.9 1 3.0 115.3 1 3.4 1 3.3
	CHARGE V	( _50 ft/sec	)	C	HARGE VI (	_50 ft/sec	:)
1678 3250 3752 3388 6287 6367 5899 6495 6542	161 9971 9833 893 9926 9873 903 9918 9830	202.0 201.7 200.5 496.0 499.3 499.6 1005.5 1001.7 1002.0	1 2.0 1 1.7 1 0.5 - 4.0 - 0.7 - 0.4 1 5.5 1 1.7 2 2.0	1619 4242 4784 6320 7682 8118 7866 8383	207 9951 9791 784 117 9819 9825 755	202.0 202.7 202.5 499.0 500.3 499.7 1069 878	1 2.0 1 2.7 1 2.5 - 1.0 1 0.3 - 0.3 169.0 -122.0
	CHARGE VII	( _50 ft/se	<b>c</b> )				
2952 5231 5902 7989 9570 9837 9754 10132	308 9999 9793 895 9974 9773 643 9917 9864	202.6 203.8 203.7 498.6 499.5 500.1 1001.5 1001.5	2.6 4 3.8 4 3.7 - 1.4 - 0.5 4 0.1 4 1.5 4 1.5				

165 100 10 35 15	Lievelier lec	(Flus Mussle Velocity)
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	ge II	Charl (A)				(Plus 30F)	
Errer_	S.E.	Feicht	Ethre	fre	C.5.	Height	Range
-0.1	227.0	142	1390	10.2	231.3	118	1033
1.2 .	228.3	0	2459	10.2	231.3	0	1988
10.4	227.5	9787	3137	12.5	233.8	9719	2792
-0.6	339.4	305	1996	-1.6	375.8	300	1564
12.0	342.0	0	3438	10.6	378.0	0	2976
1.7	341.7	9723	4050	10.4	377.8	9/98	3566
10.2	488.0	601	21.74	0	471.5	452	3864
10.5	480.3	0	4415	1.3	472.8	0	3470
10.2	488.0	2799	1734	/1.2	472.7	9710	3929
19.9	943.0	873	4303	1 65.0	987.6	933	3213
-0.2	932.9	0	4993	10.9	923.5	0	4054
-1.0	932.1	9768	5142	-0.4	922.2	9746	4222
-0.7	1078.6	772	3981	0.0	,	958	2907
-0.6	1078.7	0	4406	-2.1	1099.4	0	3461
-0.3	1079.0	9882	41.62	-0.7	1100.8	9716	3589
-2.5	1155.4	889	3506	-0.7	1100.0	926	2550
-0.9	1157.0	0	3915	10.6	1192.0	0	2964
-0.6	1157.3	9783	4000	0	1191.4	9791	3040
	e ,IV	Cherg			III	Charge	
	t/Sec)	( \( \frac{1}{50} \) \( \text{F} \)			t/Sec)	( / 30 F	
10.9	215.5	213	2416	-2.6	207.0	145	1837
11.7	216.3	0	3942	10.4	210.0	0	2920
12.1	216.7	9806	4626	<b>≠</b> 0.1	209.7	9739	3795
1.4	356.6	567	3420	-1.5	340.2	396	2500
12.2	357.4	0	5896	10.3	342.0	0	4373
10.2	355.4	9736	6461	40.8	342.5	9820	4792
10.2	500.0	866	54,20	-1.4	453.6	672	3070
0	499.8	0	7363	-1.4	453.6	0	5340
-1.2	498.6	9790	7677	-1.6	453.4	9832	5629
1.8	913.4	854	7644	47.0	929.0	904	5613
-5.6	906.0	0	8261	O	922.0	0	6302
-2.1	909.5	9811	8382	10.4	922.4	9834	6409
10.6	1060.0	724	7008	£5.1	1035.6	848	5317
-0.7	1058.7		7382	<i>4</i> 1.5	1033.0	0	5817
-1.6	1057.8		7484	10.2	1031.7	9870	5884
-1.5	1196.1		5597	40.1	1164.6	732	4539
-1.5	1196.1		5901	10.5	1165.0	0	4846
						9882	4890 -

#### 1559M Cundrent Tlew tion Check (Plus 50Ft/Sec Muzzle Velocity

	(250)	(7:ec)			Char	ST VI	
Benee	<u>Reichi</u>	2.2	Error	Pan	es Belshi	S.E.	Exer
2692	282	214.4		389	374	208.5	-0.7
4200	0	215,6		630		210.0	8.0
5611	9752	214.4		692		209.8	10.6
4059	738	363.6		503	-	335.4	10.7
7149	0	363.0		8531		335.0	10.3
7334	9812	347.0		647		335.0	10.3
6767	861	480.0	10.7	8960		463.5	10.8
8565	0	4.80.0	10.7	103%		462.5	-0.1
8920	9763	479.5	10.2	10689		462.5	-0.2
9393	279	900.0	-0.7	11844		912.4	11.2
10010	0	899.0	12.7	1237	0	910.2	-1.0
10184	9723	0.808	12.7	3219	9795	911.0	-0.2
8614	883	1047.4	10.9	10923	884	1049.0	14.6
9068	0	1046.3	-0.2	11349	0	1046.0	11.6
9133	9326	1046.5	0	114.68	9736	1045.2	10.8
6922	674	1195.3	-1.4	8730	772	1194.2	-0.1
7157	0	1195.4	-1.3	8987	0	1193.6	-0.7
7206	9850	1195.5	-1.2	9030	9862	1193.4	-0.9
	Char	ge, VII					
	(≠50 <sup>F</sup>	Sec)		•			
4967	529	209.0	-1.6				
8054	ó	211.6	1.0				
8736	9748	212.0	1.4				
8879	842	350.0	13.0				
10840	0	348.0	1.0				
11056	9875	350.2	13.2				
11970	866	499.0	10.7				
13159	0	497.8	-0.5				
13409	9786	497.8	-0.5				
14583	799	915.3	<i>4</i> 0.3				
15042	0	914.0	-1.0				
15070	9948	913.8	-1.2				
13360	680	1064.7	1.4				
13648	0	1063.0	-0.3				
13742	9763	1062.6	-0.7				
11082	687	1183.7	0.				
11998	0	1156.0 4					
11378	9739	1183.7	0				

	25520	querent.	Florett.	on threk	Citiese in	tele (g)	ocity)	
	(-30°	(/see)					ge II t/Sec)	
Parce	Beight	2 .	Error		Panes	Feight	QLE	Etror
260	96	233.6	12.5		1287	118	228.0	10.9
1677	0	230.4	-0.7		2119	0	227.2	10.1
23119	9750	231.1	0		5000	9781	246.7	129.6
1259	253	376.3	-2.1		1/50	265	340.2	10.2
2420	C	376.3	-1.1		2971	0	340.0	0
2952	9786	377.0	-0.4		3574	9723	340.1	10.1
1544	352	267.0	-4.5		2110	519	487.4	-0.4
2943	0	170.4	-1,1		3825	0	488.7	1.0
3305	9777	472.6	1.1		4226	9712	488.0	10.2
3455	0	923.6	1.0		4343	0	936.8	13.7
3581	9814	9-4.1.	3.1		41.1.7	9841	935.5	12.4
2430	F60	_	-		3330	863	1087.0	17.7
29/9	0	1100.4	-1.1		3833	0	1079.6	10.3
3070	9737	1099.6	-1.9		3979	9905	1057.2	-22.1
2080	2456	1286.4	0		3722	820	1168.0	18.1
2529	0	1192.0	tn.6		3408	0	1158.5	10.6
2606	9790	1190,7	-0.7		34.89	9794	1158.0	<b>≠0.1</b>
	Chara	ze III				Chor	ge IV	
	(-30 <sup>17</sup>	(Sec)				(-50°	t/Sec)	
1720	124	210.6	1.0		1950	183	217.0	12.4
2570	0	210.0	10.4		3349	0	215.0	10.4
3336	9774	210.2	10.6		4268	9721	214.6	0
2116	351	342.4	10.7		2594	480	355.8	10.6
3862	0	341.5	-0.2		5040	0	354.4	-0.8
4288	9816	342.4	<b>-</b> 0.7		5516	9783	354.5	-0.7
2665	594	454.6	-0.4		3421	905	499.0	-0.8
4725	0	454.4	-0.6		6309	0	498.8	-1.0
5089	9786	1.54.5	-0.5		6676	9756	499.0	-0.8
4880	903	918.8	-3.2		6460	823	912.4	10.8
5593	0	924.0	12.0		7066	0	911.4	-0.2
5766	9732	925.0	13.0		71 58	9860	912.3	40.7
4306	841	1111.5	0		5868	817	1058.0	-1.4
4732	O	1108.0 -	23.5		6308	0	1058.8	-0.6
4783	9885	1107.9 -			6431	9742	1058.8	-0.6
3918	876		14.5		4716	877	1198.4	40.8
4303	0	1164.5	0		5049	0	1196.8	-0.8
4341 •	c901	1164.0	-0.5		5137	9741	1196.6	-1.0

	(-50° E	Tree)			(-50°	E7Sec)	
Jan 20	Height	S.F.	From	Pence	Height.	9.5.	Errer
2549	246	215.4	M.8	3361	341	209.4	10.2
4358	0	215.1	10.5	5684	0	210.0	10.8
5117	9778	215.0	10.4	6379	9782	209.5	10.3
3193	666	363.4	10.9	1502	794	337.0	12.7
6574	0	363.0	10.5	7926	0	334.6	-0.1
7000	9797	362.4	-0.1	84.16	9761	334.3	-0.4
5753	913	4.79.3	0	F145	826	462.5	-0.2
7898	)	479.4	40.1	9722	0	462.8	1.1
8124	9855	479.3	0	10113	9731	463.2	10.5
8655	757	901.5	10.8	11092	753	914.5	13.3
9188	O	904.7	41.0	11578	0	913.4	12.2
9273	9869	904.5	13.8	11737	9732	913.4	12
7827	903	1 749.7	13.2	10244	721	1049.3	+4.9
8303	0	1048.4	1.9	10597	0	1047.0	12.6
8333	9937	1048.4	41.9	10649	9887	1046.6	12.2
6318	672	1197.3	10.6	8099	850	1194.7	10.4
6557	0	1196.5	-0.2	8389	0	1193.7	-0.6
6594	9887	1196.6	-0.1	8398	9972	1193.8	-0.5
	Charge (-50Ft/	VII Sec)					
4737	478	211.0	40.4				
7494	0	212.4	<b>√</b> 1.8				
8149	9768	211.3	10.7				
8002	863	351.0	44.0				
10194	0	347.4	10.4				
10464	9849	347.6	,40.6				
11121	912	498.6	<b>₹0.3</b>				
12146	0	498.0	-0.3				
12572	9897	498.4	<b>/</b> 0.1				
13799	720	917.5	12.5				
14221	0	917.5	12.5				
14289	9878	917.0	12.0				
12525	804	1064.0	£0.7				
12876	0	1063.4	₹0.1				
12918	9898	1063.3	0				
10396	771	1183.0	-0.7				
10648	Õ	1183.5	-0.2				
10700	9829	1183.2	-0.5				

10500 Quadrant Elevation Check (Plus Mind: 50 mph = 5)

	CHARGE	I ( 1 50 m	nh)		CHART	II ( £ 50 m	nh1
		- ( - )	h)		CAN MILE	11 ( ¥ 50 m	paj
BARRO	Height	Se Ze	Error	Proce	Height	Q. Z.	Error
766	75	204.6	14.6	1245	73	201.0	11.0
1512	9993	201.0	11.0	1845	9979	201.0	71.0
2273	9758	200.5	4 0.5	2438	9800	201.7	71.7
1691	421	498.0	- 2.0	2196	483	499.4	- 0.6
3129	9964	498.7	- 1.3	3569	24	501.4	1.4
3284	9867	501.0	41.0	3901	9817	503.4	7 3.4
2677	795	1055.6		3354	737	1010.4	710.4
3283	55	1011.2	411.2	3912	9959	1000.9	70.9
3473	9739	1007.8	47.8	3973	9857	1000.2	70.2
	CHARGE I	II ( \$ 50 m	ph)		CHARGE I	7 ( \$ 50 mp)	1)
1366	98	201.7	4 1.7	2022	95	201.2	£ 1.2
2242	9963	199.8	- 0.2	2505	21	201.1	71.1
2969	9846	242.4		3451	9762	202.7	7 2.7
5/10 J	595	498.8	- 1.2	3111	730	499.0	- 1.0
4261	15	499.4	- 0.6	5337	9962	500.0	0
4618	9789	500.0	0	553 <b>1</b>	9839	500.7	£ 0.7
4111	702	1015.6	<b>∠15.6</b>	5062	830	1007.7	7.7
4554	64	1007.0	7.0	5658	9930	1002.3	7 10 1
4652	9884	1008.0	7 8.0	5774	9726	1001.4	1 2.3 1 1.4
	CHARGE V	( 1 50 mp)	1)		CHARGE VI	( \$\frac{1}{2} 50 mph	)
1772	179	201.0	<b>≠</b> 1.0	26 <b>82</b>	231	200.5	<b>≠</b> 0.5
4508	9704	203.4	1 3.4	4690	9951	203.9	
4545	908	501.7	41.7	509 <b>7</b>	9840	204.4	7 3.9
6974	9947	501.0	1.0	7236	776	502.5	
7231	9778	504.0	14.0	8781	9980	501.4	1 2.5 1 1.4
6766	813	1001.1	↓ 1.1	9153	9726	501.5	4 1.5
7290	9976	999.2	- 0.8	8742	773	999.8	- 0.2
7418	9748	998.3	- 1.7	9281	9860	997•9	- 2.1
			·	9340	9810	993.0	- 7.0
	CHARGE V	II ( ≠ 50 m	ph)		CHARGE VII	I ( \$ 50 mp	h)
3092	328	200.7	40.7	10662	9873	503.0	£ 3.0
3653	6	203.5	4 3.5	10676	850	1001.3	7 1.3
6254	9835	204.5	4 4.5	11186	9955	999.0	- 1.0
9020	840	499.5	- 0.5	11274	9790	998.7	- 1.3
10516	9976	502.4	1 2.4	•	717-	,, -,	• ,

105001 Quadrant Elevation Check (Ninus Wind: -50 mpb - N)

	CHAS	KGE I ( _50m	ph)	CHARCE II ( -50 mph)					
Ranco	Holebt	0. 5.	Error	PORCE	Height	Q. Ic.	Irrer.		
762 1493 2196	74 9992 9758	201.7 199.8 198.0	1.7 -0.2 -2.0	1234 2015 2394	73 9928 9799	200.2 201.0 200.4	10.2		
1662 3030 3175	417 9958 9861	497.4 501.0 500.3	- 2.6 1.0 10.3 - 1.0	2154 3457 3766 3174	477 16 9510 705	499.0 502.0 501.6 1006.0	1.0 4 2.0 4 1.6 4 6.0		
2665 3154	772 9907	999.0 1012.0	112.0	3542 3721	154 9827	1003.6 1003.0	4 3.6		
	CHA RO	111 ( _50	eph)		CHARGZ 1	<b>▼ ( _50 m</b> ph)			
1353 2208 2622 2727 4122 4453 3877 4073 4341	97 9967 9846 548 5 9780 668 365 9886	199.6 201.0 201.5 500.9 501.0 500.0 1001.0 999.0	- 0.4 1 1.0 1 1.5 1 0.9 1 1.0 - 1.0 1 3.4	1512 2462 3369 3039 5140 5318 4758 5177 5279	129 19 9760 719 9944 9821 781 75 9879	200.0 200.5 201.0 1199.4 499.0 498.7 1006.8 1005.0 1004.2	0 4 0.5 4 1.0 - 0.6 - 1.0 - 1.3 4 6.8 4 5.0 4 4.2		
	CHARGE	▼ ( _50 mpl	h)		CHARGE VI	( _50 mph)			
2256 3290 3787 4333 6399 6478 6157 6611 6721	150 9991 9856 851 9969 9916 860 47 9824	202.1 201.0 200.7 501.5 499.3 498.8 1002.5 1004.0 1002.5	1 2.1 1 1.0 1 0.7 1 1.5 - 0.7 - 1.2 2 2.5 1 4.0 1 2.5	2507 4129 4641 6114 7597 7799 7546 8019 8043	214 9960 9802 773 9956 9806 782 9856 9806	201.0 201.9 201.0 493.2 494.4 494.3 1002.0 1002.1	1.0 1.9 1.0 -6.8 -5.6 -5.7 1.0 2.1 1.0 2.1		
	CHARGE	VII ( _50 I	mph)						
2973 5235 5727 7706 9212 9417 9244 9585 9655	323 9993 9821 910 9954 9785 674 9949	200.7 201.0 200.4 493.6 492.8 494.0 1002.0 1002.1 1002.0	10.7 10.4 - 6.4 - 7.2 - 6.0 12.0 12.0						

30000	nar et	Flow 110	n Check	(Plus	50 TH	Wind - 5	1
-							

Charge I							Cherge II			
Ferre	Eelch	e G.E.	Fror	E	ince	<u>Peleb</u>	Q.E	Fror		
1188	100	231.2	10.2	,	933	280	339.6	-0.4		
1843	0	231.2	10.2		234	0	340.7	10.7		
2518	9775	231.9	3.01		753	9774	31.1.4	12.4		
1507	276	376.1.	-1.0		101	555	86.7	-1.1		
2774	0	377.1	-0.3		175	0	488.7	10.9		
3291	7447				4.51	0832	489.2	1.4		
1799	415	1,69.5	-2.0		116	810	938.6	15.5		
3245	0	1,71.7	10.2		786	0	933.0	10.1		
3504	9747	519.0	137.5		970	9726	931.0	-2.1		
3844	0	920.1	-2.5		71.2	836	1080.5	11.2		
1016	9708	920.2	-2.4		241	0	1079.0	-0.3		
2770	867				336	9811	1079.2	-0.1		
3296	0	1099.4	-2.1		4.00	792	1157.5	-0.4		
3380	9830	1099.0	-2.5	3'	786	0	1157.1	-0.8		
21.49	827			38	526	9033	1200.0	f12.1		
2840	0	1191.7	10.3							
2953	9708	1190.7	-0.7							
	Char	ge III				Char	ge IV			
1538	147	210.4	40.8	20	)58	204	215.5	10.9		
2764	0	210.7	1.1	37	715	0	316.2	11.6		
3479	9799	210.4	40.8		525	9769	216.6	12.0		
2437	370	341.3	-0.4	30	60	535	355.8	40.6		
4165	0	342.6	10.9	56	00	0	357.0	11.8		
4701	9768	342.5	40.8	61	05	9775	357.5	12.3		
2776	640	454.3	-0.7	48	27	881	499.6	-0.2		
5106	0	455.5	£0.5	70	20	0	500.5	10.7		
5535	9751	455.0	0	73	32	9800	500.0	10.2		
5427	848	924.6	12.6	72	34	888	914.6	£3.0		
6105	0	921.0	-1.0	79	20	0	909.6	-2.0		
6243	9799	919.6	-2.4	79	93	9893	000.0	-2.6		
5172	774	1034.5	<i>f</i> 3.0	66		729	1059.7	10.3		
5654	0	1033.0	<b>≠1.</b> 5	710			1059.7	10.3		
5758	9812	1031.7	10.2	7]		0	1059.2	-0.2		
4363	829	1164.8	£0.3	540			1197.4	-0.2		
4743	0	116/.8	<b>≠</b> 0.3	57:			1195.5	-2.1		
4824	9900	1160.1	-4.4	578	34	9853	1195.4	-2.2		

1550 Quedrent Elevetion Check (Flue 50 Mon Wind - 5)

		C	herge V			Charge VI						
	Renge	Helg	ht Q.F.	Dror		Banze	Baleht	Q.E.	Error			
	3009	260	213.4	-1.2		3852	354	208.6	-0.6			
	1.822	0		0		6149	0	209.5	10.3			
	5726	9737		10.4		7036	9725	210.0	10.8			
	4389	711	363.7	10.9		5046	640	335.6	10.9			
	7286	0		13.1		8632	0	335.8	1.1			
	7717	9801	363.9	12.4		9202	9731	336.5	41.8			
	6891	250	480.0	10.7		8902	873	463.1	10.7			
	8752	0	478.5	-0.8		10626	0	462.9	10.2			
	914	9752				13012	9748	463.5	8.01			
	9582	780	895.5	-5.2		12214	734	909.7	-1.5			
	10159	0	893.8	-6.9		12712	0	904.8	-6.4			
	10251	9864	893.0	-7.7		12743	9951	905.7	-5.5			
	8799	713	1048.8	12.3		11292	711	1048.3	13.9			
	9188	0	1047.9	f.4		11662	0	1045.6	11.2			
×	9213	9951	1047.0	10.5		11735	9851	1045.5	/1.1			
	7035	697	1194.0	-2.7		9013	828	1193.4	-0.9			
	7302	0	1194.5	-2.2		9322	0	1192.5	-1.8			
	7343	9886	1194.6	-2.1		9348	9925	1192.7	-1.6			
		Ch	arge VII									
	4919	505	211.3	10.7								
	7994	0	211.5	10.9								
	8556	9813	211.5	10.9								
	8707	868	350.0	13.0								
	10966	0	350.8	13.8								
	11331	9803	349.0	12.0								
	12298	789	499.0	10.7								
	13466	0	498.2	-0.1								
	13593	9902	498.0	-0.3								
	15121	645	911.0	-4.0								
	15524	Ó	,	4.0								
	15654	9783		*********								
	13762	752	1064.4	1.1								
	14118	Õ	1063.2	-0.1								
	14195	9830	1062.7	-0.6								
	11534	717	1182.8	-0.9								
	11795	Ō	1182.8	-0.9								
	11877	9764	1182.5	-1.2								

1500	Quadrent	Flewetten	Chick	(Minus	50 !	MIN	Wind	- N)	
Charge I								-	-

RADE	Eele	15.2 at	Error	Bance	Helsh	Q.F.	Liver
1178	99	230.0	-1.1	1333	130	227.5	10.4
1816	0	231.1	0	2268	0	227.0	-0.1
27.77	9775	231.1	0	2995	9761	227.1	0
1491	274	375.9	-1.5	1911	279	340.4	10.4
2714	0	377.0	4.0-	3165	0	340.4	10.1
3213	9743	377.6	10.2	3670	9772	340.4	10.4
1774	412	469.5	-2.0	2365	551	487.2	-0.6
3158	0	477.0	-0.5	4054	0	488.2	10.4
3560	9743	470.7	-0.8	4326	9826	1.88.1	10.3
3649	0	922.8	10.2	4535	0	933.7	10.6
3744	9853	923.4	10.8	4607	9884	933.7	10.6
2635	846	1101.2	-0.3	3548	810	1080.3	/1.0
3095	0	1100.2	-1.3	3979	0	1080.0	10.7
3179	9806	1099.4	-2.1	4076	9784	1079.7	10.4
2299	203			3116	915	1157.7	-0.2
2631	0	1193.0	1.6	3517	Ó	11 58.5	10.6
2676	9870	1192.3	10.9	3563	9875	1158.3	10.4
*	Cha	rge III			Charge	IV	
1523	146	210.4	40.8	2004	198	215.6	<i>f</i> 1.0
2714	0	209.8	10.2	3526	0	218.0	12.4
3410	9797	209.4	-0.2	4337	9754	213.4	-1.2
2402	366	339.8	-1.9	2967	516	355.8	10.6
4053	0	340.5	-1.2	5272	0	355.4	10.2
4578	9762	340.8	-0.9	5820	9737	357.0	1.8
2731	634	456.4	11.4	4197	919	500.6	10.8
4940	0	456.7	£1.7	6589	Ó	500.0	10.2
5364	9740	455.8	8.04	6969	9735	497.5	-2.3
5181	815	924.1	12.1	6840	789	911.7	10.1
5772	0	924.0	12.0	7387	Ó	911.0	-0.6
5916	9764	923.4	11.4	7517	9787	916.8	15.2
4792	904	1033.8	12.3	6163	•	1059.0	-0.4
5308	0	1032.6	<i>f</i> 1.1	6580		1059.0	-0.4
5418	9774	1032.5	1.0	6704		1059.0	-0.4
4073	789	1165.5	£1.0	4972		1197.9	<b>≠</b> 0.3
4386	0	1164.4	-0.1	5212		1197.0	-0.6
4469	9760	1164.0	-0.5	5286		1198.4	40.8

#### 15500 Cunfront Flowetten Check (Nimus 50 NTH Wind - N)

	Cher	TA V	1000 7 10	WENCE IN	Charge VI					
	CD47					Charg	e 71			
Fance	Height	9.1.	Freez		Esper	Heleh!	Sala	leter_		
2555	258	214.8	10.2		3724	348	209.2	0		
4363	0	214.6	0		5755	0	210.8	11.6		
5016	9798	215.3	10.7		6289	9823	210.0	8.C		
3833	673	363.5	/1.0		4792	816	337.9	13.2		
6461	0	362.7	1.2		7852	0	335.5	8.0		
6822	9819	362.7	10.2		205	9815	333.7	-1.0		
5886	868	480.0	8.01		7957	877	462.5	0		
7726	0	479.2	0		9515	0	461.4	-1.3		
8119	9725	479.6	10.4		9799	9790	460.7	-2.0		
F451	848	89 .9	8.0-		10714	868				
9018	0	899.7	-1.0		11231	0	919.5	8.3		
9175	9735	905.5	14.8		11311	9852	918.0	16.8		
7750	836	1048.7	12.2		9863	890	1051.0	16.6		
8154	0	1048.2	1.7		10261	0	1048.0	13.6		
8220	9850	1047.7	11.2		10355	9774	1046.3	1.9		
6090	894	1199.3	12.6		7792	790	1198.0	13.7		
6379	0	1198.0	1.3		2055	9902	1195.0	10.7		
6425	9845	1197.4	10.7							
	Charg	e VII								
4787	501	210.9	10.3							
7560	0	212.2	11.6							
8047	9817	211.0	10.4							
8177	844	351.9	14.9							
10085	0	348.2	11.2							
10448	9772	347.0	0							
11053	846	499.0	10.7							
12153	0	497.6	-0.7							
12381	9793	496.7	-1.6							
13260	875	917.9	12.9							
13726	0	920.7	15.7							
13844	9758	921.2	15.7 16.2							
12100	729	1066.0	12.7							
12380	0	1064.5	1.2							
12442	0	1060.2	-3.1							
9926	733	1185.3	<b>√</b> 1,.6							
10130	0	1184.8	<i>f</i> 1.1							
10183	9796	<b>Constant</b>								

#### 105MN Quairant Elevation Check (Flue Air Density)

	CHAN	ZI(/10	S AD )	CHARGE II ( 1 105 AD)					
Base	80161	Q.E.	bre	BARRO	Bolcht	0.2.	Error		
1134	52	200.5	10.5	1236	73	201.2	11.2		
1499	9992	200.5	40.5	1633	19	200.6	40.6		
2207	9758	200.2	10.2	2406	9799	201.4	11.4		
1671	417	497.6	- 2.4	1820	497	497.6	- 2.4		
3059	9957	500.3	40.3	3487	14	502.4	1 2.4		
3207	9859	500.5	40.5	3803	9807	500.4	10.4		
3161	24	1009.0	19.0	3238	700	1008.3	18.3		
3337	9708	1006.5	4 6.5	3718	9985	1002.4	1 2.4		
				3811	9818	1002.2	1 2.2		
	CHARGE	111 ( 4 10	M AD)		CHARGE IV	( \$ 10\$ AD)			
1356	97	200.5	1 0.5	1517	129	200.4	10.4		
2216	9967	201.4	11.4	2475	19	200.6	10.6		
2632	9845	201.7	11.7	3392	9761	202.0	1 2.0		
2371	588	499.8	- 0.2	3463	660	499.6	- 0.4		
4292	9917	499.0	- 1.0	5190	9944	500.2	1 0.2		
4493	9777	498.0	- 2.0	5372	9821	500.4	10.4		
3957	653	1009.4	49.4	4856	762	1007.5	£ 7.5		
4364	14	1004.0	4.0	5294	56	1003.3	4 3.3		
4561	9646	1004.0	1 4.0	5400	9860	1003.4	1 3.3 1 3.4		
	CHARGE	V ( 10%.	AD)	-	CHARCE VI (	10% AD)			
1749	176	199.6	- 0.4	2571	218	201.0	<b>≠</b> 1.0		
3421	9988	201.0	4 1.0	4332	9954	202.4	1 2.4		
3883	9866	200.9	4 0.9	4816	9812	203.0	4 3.0		
4426	876	499.8	- 0.2	6345	827	500.2	10.2		
6677	9928	502,3	£ 2.3	8077	9910	501.0	£ 1.0		
6956	9730	501.5	1.5	8119	9880	501.1	£ 1.1		
6317	871	1006.0	4 6.0	7861	865	1003.8	4 3.8		
6887	9887	1002.0	7 2.0	8393 8443	9898	1002.1	£ 2.1		
6911	9842	1001.4	<b>≠ 1.4</b>	8443	9801	1001.7	11.7		
	CHARGE	VII ( 109	(AD)		CHARGE VII	(Cont'd)			
2986	317	201.0	4 1.0	9764	9802	500.1	4 0.1		
5301	9999	203.2	4 3.2	9512	896	1001.8	11.8		
5908	9811	203.5	<b>₹ 3.5</b>	9986	16	999.4	- 0.6		
8424	688	501.0	£ 1.0	10062	9824	1001.0	1.0		
9547	9 <b>969</b>	500.6	40.6				,		

105MM Quadrant Elevation Check (Minus Air Density)

	CHAR	SE 1 ( 105	AD)	CHARGE II ( _10% AD)					
hase.	Balchi	2.2.	Bror	Bonzo	Beight	Q. E.	Error		
1139	54	202.4	4.54	1244	74	202.7	1 2.7		
1508	9993	201.5	4 1.5	50/10	9929	202.5	1 2.5		
2229	9758	201.2	11.2	54:29	9500	203.4	7 3.4		
2007	387	499-7	- 0.3	2533	426	500.6	7 0.6		
2950	53	500.4	40.4	3542	26	503.0	7 3.0		
3255	9867	502.0	1 2.0	3869	9818	504.2	14.2		
2656	801			3299	474	1006.0	7 6.0		
3220	61	1004.9	14.9	3700	195	999.7			
3403	9745	1003.0	4 3.0	3896	9867	999.0	- 0.3 - 1.0		
	CHARGI	111 ( _105	(da		CHARGE	IA ( 70% )	LD)		
1364	98	201.5	£ 1.5	1526	130	201.2	11.2		
2236 2661	9968	201.8	41.8	2737	9971	201.3	71.3		
	9846	202.1	7 2.1	3438	9762	201.2	7 1.2		
2774	556	499.3	- 0.7	3923	553	499.6	- 0.4		
4232	18	500.3	10.3	5303	9966	501.5	₹ 1.5		
4583	9792	500.6	10.6	5493	9843	501.7	7 1.7		
4043	718	1007.0	£ 7.0	4981	855	1003.2			
4470	80	1002.0	1 2.0	5555	9955	1000.5	4 3.2		
4595	9864	1001.3	4 1.3	5667	9750	1000.0	↓ 0.5 0		
	CHARGE	▼ ( _10% AI	0)		CHARGE	VI ( _10% A	D)		
1763	174	199.4	- 0.6	3211	180	202.0	1 2.0		
3414	4	203.0	<b>≠ 3.0</b>	4366	9779	202.0	+ 2.0		
3944	9870	203.5	<b>≠</b> 3.5	4924	9824	203.0	/ 7.0		
4506	904	500.0	0	6525	891	500.3	4 3.0		
6729	47	502.1	£ 2.1	8487	9896	501.6	7 1.6		
7151	9769	503.0	4 3.0	8466	702	1000.4	70.4		
6646	835	1002.6	4 2.6	8738	230	999.8			
7151	9996	999.4	- 0.6	9005	9729		- 0.2		
7274	9768	998.7	- 1.3	yeey	71-3	999•2	_ 0.8		
	CHARGE V	II ( _10% A	D)		CHARGE	VII (Cont'd	)		
3080	333	201.5	£ 1.5	10288	9888	501.4	£ 1.4		
5592	999 <b>9</b>	205.8	£ 5.8	10322	898	1001.8			
6108	<b>७</b> ८मम	206.0	4 6.0	10833	9943		<b>≠ 1.8</b>		
8765	828	500.1	4 0.1	10833	9833	999.5	7 0.5		
10149	9990	501.5	4 1.5		Je ) )	1005.6	£ 5.6		

	Chary (/10s	e I	nt Flewetton	CHECK IN SE ALL	Charge II (/10% /.D.)						
Panee	Height	Q.F.	Error	EARPE	Beleht	S.F.	Error				
987.9	107	230.3	-0.8	1335	130	227.7	D.6				
1820	0	230.4	-C.7	2274	0	227.4	10.3				
2484	9775	231.6	10.7	3006	~760	227.6	10.5				
1313	274	375.0	-2.4	1916	278	339.7	-0.3				
2724	0	376.9	-0.5	3176	0	340.4	10.4				
3232	9742	378.0	10.6	3687	9771	341.0	1.0				
1608	415	467.7	-3.8	2373	550	487.7	-0.1				
3175	0	471.5	0	4073	0	487.1	-0.7				
3586	9741	472.2	10.7	4354	9824	488.6	10.8				
3706	0	922.6	0	3878	595	935.0	1.9				
3912	9682	923.0	10.4	4600	0	933.7	10.6				
2603	950	, , ,	,	4683	9870	936.3	13.2				
3164	0	1100.3	-1.2	3617	793	1084.0	14.7				
3256	9796	1100.0	-1.5	4058	0	1080.3	£1.0				
2292	917		2.3	4168	9767	1079.7	10.4				
2709	0	1192.2	40.8	31.90	896	1165.0	17.1				
2825	9672	1190.8	-0.6	3605 3662	9854	1158.0 1158.0	<b>%</b> :1				
	Charg				Charge (10%						
1527	146	208.6	-1.0	2035	202	213.8	-0.8				
2725	0	209.6	0	3626	0	215.2	10.6				
3425	9797	209,8	<b>√0.2</b>	4425	9764	214.7	40.1				
2411	366	341.0	-0.7	3013	526	355.8	10.6				
4076	0	341.6	-0.1	5418	0	355.0	-0.2				
4607	9763	341.2	-0.5	5936	9758	355.4	40.2				
2742	633	456.2	<b>√1.2</b>	4491	9000		_				
4971	0	456.7	£1.7	6751	0	500.8	<i>f</i> 1.0				
5403	9739	453.8	-1.2	7099	9764	498.4	-1.5				
5250	796	921.0	-1.0	6959	794	910.5	-1.1				
5847	0 *	922.2	<b>≠</b> 0.2	7529	0	913.0	1.4				
6008	9746	924.0	12.0	7658	9797	915.5	<i>+</i> 3.9				
4873	881	1029.6	-1.9	6292	825	1059.4	0				
5397	0	1031.0	-0.5	6722	0	1059.6	10.2				
5524	9751	1032.6	4.1	6857	9711	1058.7	-0.7				
4175	757	1166.5	12.0	5039	897	1197.8	10.2				
4494	0	1164.8	10.3	5370	0	1197.3	-0.3				
4595	9728	1164.5	0	5460	9725	1197.7	40.1				

	Char	x.P.)				'.D.)	
Pange	"se tobt	Car	From	lenge	Paleht	C.F.	ST.
2000	247	214.5	-0.1	3410	355	208.7	-0.5
4508	0	214.5	0	5800	0	209.8	10.6
5170	9505	211.6	0	6406	3608	209.0	-0.2
3929	(06	363.2	10.7	4845	805	335.4	10.7
6733	C	363.6	41.1	8013	0	334.3	-0.4
7048	6786	363.4	10.9	2414	9801	334.2	-0.5
6059	902	0.03,1	10.7	8148	867	461.7	-1.0
8058	0	4.79.4	<i>/</i> 0.1	9770	0	4.61.0	-1.7
۶390	9778	4.78.2	-1.1	10078	9784	463.4	1.7
8706	915	901.8	41.1	11029	836	919.2	0.3,
9348	0	903.3	12.6	11555	0	917.3	16.1
9466	9813	900.1	-0.6	11657	9825	917.4	16.2
P005	879	1050.1	13.6	10188	818	1043.2	-1.2
87,55 8502	9900	1049.3	12.8	10578	0	1048.0	13.6
		1047.4	10.9	10709	9705	104.7.0	
63 <b>53</b> 6666	842	1198.6	4.9	8148	658	1195.7	11.4
6715	9848 9848	1197.3	≠0.6 ≠0.3	836/ 8/34	97 <b>72</b>	1194.5	<b>≠</b> 0.2
	Charge		,	, , , , , , , , , , , , , , , , , , ,	7/12	11/4.5	0
4757	489	210.4	-0.2				
7513	0	211.4	<b>√</b> 0.8				
8115	9782	211.0	40.4				
7974	875	351.0	44.0				
10148	0	347.6	<b>≠</b> 0.6				
10384	9864	347.0	0				
11267	770	498.7	40.4				
12324	0	498.8	<b>≠</b> 0.5				
12435	990 <b>7</b> 688	498.4	<b>≠</b> 0.1				
13598 13990	0	914.3	-0.7				
14072	9847	917.5 915.7	12.5				
12342	757	1065.8	12.5				
12663	0	1065.4	₹2.5 ₹2.1				
12722	9852	1064.2	≠2.1 ≠2.9				
10243	709	1184.7	≠1.0 ≠1.0				
10467	0	1384.0	40.3				
10536	9771	1184.0	₹0.3				

	Cheri		sedrent Fle	vetion C	neck (Minus		eltr-101 er II	1			
	(-101				(-10% A.D.)						
Renge	Peight	G.E.	Error		Bange	Height.	CE	Error .			
991	108	230.9	-0.2		1342	130	226.8	-0.3			
1839	0	230.8	-0.3		2300	0	227.4	.0.3			
2692	9691	231.5	10.4		3041	9761	227.8	10.7			
1619	419	469.7	-1.8		2395	557	486.5	-1.3			
3229	0	473.4	-0.1		4159	0	487.8	0			
3638	9748	473.5	12.0		41,27	9835	4.88.6	10.8			
2726	877	_			3684	854	1080.5	1.3			
3240	0	1100.3	-1.2		4174	0	1079.5	10.2			
3397	9656	1101.2	-0.3		4257	9829	1079.7	10.4			
2399	841				3333	8134					
2779	0	1190.4	-1.0		3712	0	1057.5	-0.4			
2881	9723	1190.7	-0.7		3822	9723	1057.4	-0.5			
	Charg	e III				Cherg	e IV				
	(-10%	A.D.)					A.D.)				
1536	147	210.1	10.5		2051	204	215.2	406			
2762	0	210.1	10.5		3691	0	215.0	10.4			
3470	9799	210.0	40.4		4496	9768	215.0	10.4			
2770	642	455.9	10.9		4800	881	500.2	17.4			
5091	0	455.0	0		6969	0	500.2	10.4			
5510	9754	455.4	40.4		7278	9798	500.3	10.5			
5098	802	1035.7	41.2		6592	767	1061.0	1.6			
5580	0	1033.0	1.5		7001	0	1059.8	10.4			
5665	9840	1032.5	1.0		7070	9859	1059.4	0			
4275	865	1165.0	10.5		5282	863	1198.0	10.4			
4653	0	1164.1	-0.4		5608	0	1,97.1	-0.5			
4716	9837	1164.0	-0.5		5639	9908	1197.0	-0.6			

		( 1. n)				(2.0)	
Lenge	<u>Belebi</u>	Sale	DIL	Leave	Helett.	Alla,	Berge
2944	254	215.5	10.9	3844	159	208.8	-01
7175	0	215.2	10.6	(10)	0	209.8	10.6
5282	9817	214.4	8.04	6900	9740	200.5	10.3
64.64	823	479.0	-0.3	8 12	879	162.2	-0.3
8415	0	478.7	-0.6	10377	0	462.1	-0.6
8659	9844	479.2	-0.1	10744	9748	462.2	-0.5
5579	684	1048.7	12.2	11007	POR	3.8400	42.6
8935	0	1048.0	0.5	11406	0	3.6201	12.6
8975	9917	1048.0	1.5	11430	9947	1046.4	12.2
6804	723	1196.0	-0.7	FFOL	705	1193.8	-0.5
7064 7094	9908	1196.3	-0.4	90L1.	0	1193.4	-0.9
	Cher	ge VII		9113	9786	1103.3	-1.0
4952	518	207.9	-2.6				
8066	0	211.8	1.2				
8796	9737	212.2	41.6				
12102	872	498.4	<b>≠</b> 0.1				
13334	0	197.7	-0.6				
13587	9790	497.6	-0.7				
13586	772	1066.4	<b>₹3.1</b>				
13923	0	1064.3	<b>⊅1.0</b>				
13984	9852	1102 0	(0.3)				
11276	802	1183.8	<del>/0.1</del>				
11 <i>5</i> 39 11 <i>5</i> 86	0 9848	1184.1	₹0.4 ₹0.5				

105000 Quadrant Elevation Check (Plus Air Temp 1 57°F)

	CRA	3GE T ( 1 5	9°F)		CHASE	E TI ( 1 59	<sup>2</sup> 7)
Dear.	Height	Q.E.	Irror	hise	Height		Error
2322	158	201.9	4 1.9	20-5	229	200.0	0
	0430	204.3	44.3	14425	9888		7
3933	9670	205.0	4 5.0	hook	98 3h	203.0	4 3.0
	898	502.2	1 2.2	7065	753	501.5	4 1.5
7071	9762	507.0	4 7.0	8450	13	501.2	4 1.2
6548	777	1500.0	0	8628	9891	501.0	4 1.0
7012	9985	998.0	- 0.2	8452	799	1001.7	41.7
7155	9713	997.3	- 2.7	8928	9940	1000.6	10.6
				<b>8980</b>	9840	1000.4	10.4
	CHARO	E VII ( 4 5	9°r)				
3370	317	201.0	4 1.0				
5235	72	203.9	4 3.9				
6396	9730	201.0	11.0				
8758	816	501.0	4 1.0				
10178	9951	500.7	40.7				
10405	9778	500.5	4 0.5				
10216	260	1003.3	4 3.3				
10715	9909	1001.0	4 1.0				
10769	9799	1001.0	11.0				

105NM Quadrant Elevation Check (Minus Air Temp -59°7)

	CHARGE	Y ( -59° T)	1		CHARGE 7	71 ( -59° 7)	
Baba	Height	Q.E.	Error	Ranze	Beight	O. I.	Pror
2284	152	200.5	1 0.5	2545	27	203.8	13.8
33kh	3334	200.3	+ 0.3	4214	9963	501.0	
3857	9860	500.7	4 0.1	4742	9806	203.5	1 3.5
4415	864	498.0	- 2.0	7618	115	499.4	- 0.6
6568	9987	500.5	4 0.5	8048	9824	500.3	10.3
6691	9907	501.2	11.2	7854	760	1001.5	11.5
6367	866	1002.5	1 2.5	8294	9976	1002.1	1 2.1
6857	51	1001.7	11.7	8370	9830	1002.0	1 2.0
6977	9829	1001.0	£ 1.0				
	CHARGI	VII ( _59°	) <b>T</b> )				
3032	326	201.8	4 1.8				
5364	2	205.5	£ 5.5				
5905	9831	205.5	£ 5.5				
8419	703	499.0	- 1.0				
9544	9980	498.5	- 1.5				
9675	9879	498.5	- 1.5				
9732	678	1000.3	4 0.3				
10106	9955	1000.8	40.8				
10184	206		-				

155 Quadrent Tlevett n Check	(Flue 'ir Temp (9907)
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		22		and a seminar of the		magazi dan Maria		
	Cher	T or			Charge	II		
	(/590)				( \$ 59° x	T)		
Eanne	Meight	S.E.	Frror	Range	<u>Height</u>	Q.F.	Error	
					120	227 /	6 2	
989	108	231.1	0	1338	130	227.4	10.3	
1827	0	230.5	-0.6	2283	0	227.3	10.2	
2493	9775	231.0	-0.1	3019	9761	227.9	10.8	
1612	4.17	469.0	-2.5	2381	552	187.5	-0.3	
3195	0	471.7	10.2	4105	0	187.8	0	
3606	9744	472.4	1.9	4281	9828	488.0	10.2	
2704	853			3644	816	1082.1	12.8	
3195	0	1100.0	-1.5	4105	0	1079.7	40.4	
3282	9014	1099.5	-2.5	4205	9791	1079.6	10.3	
2377	812	1223.0		3296	770	1160.3	12.4	
2738	0	1191.7	10.3	3648	0	1157.9	0	
2849	9693	1190.7	-0.7	3696	9882	1157.7	-0.2	
	Cham	e III			Cherge	IV		
		0° A.T.)			( £ 59°	A.T.)		
		200 5	0.3	20.45	00/	215.0	10.4	
1531	147	209.5	-0.1	2043	204	215.0		
2741	0	210.0	10.4	3672	0	216.3	11.7	
3445	9798	209.8	10.2	4470	9768	216.0	17.4	
2753	638	454.5	-0.5	4532	915	500.8	<i>4</i> 1.0	
5019	0	4.54.5	-0,5	6870	0	499.8	0	
5444	9746	455.2	10.2	7190	9787	499.4	-0.4	
4918	915	1031.8	£0.3	6375	901	1061.0	11.6	
5470	0	1034.0	1 2.5	6854	0	1060.4	1.0	
5581	9786	1033.7	12.2	6954	9789	1060.4	£1.0	
4217	800	1166.6	12.2	5198	772	1198.5	10.9	
4558	0	1165.2	10.7	5485	0	1197.8	10.2	
4645	9771	1165.0	10.5	5544	9820	97.8	-0.1	

	155	Duedren	t Flevet	ion Che	ek(Plu	Air Temp.	(59°F)		
	Charg	e V					Charg	e VI	
	(4 59	1.7.)					( £ 59°	A.7.)	
Range	Scient	Q.E.	Fror			Pence	Height	Q.F.	Error
2971	257	214.6	0			3792	349	208.6	-0.6
4719	0	214.8	10.2			6001	0	209.6	10.4
5617	9731	215.6	1.0			6592	9820	209.6	10.4
6501	908	479.4	17.1			8675	848	462.8	0.1
8502	0	478.0	-1.3			10278	0	462.8	0.1
8913	9727	477.5	-1.8			10685	9720	462.8	0.1
8531	736	1048.5	12.0			10837	694	1041.2	-0.2
8907	0	1047.8	1.3			11172	0	1042.4	-2.0
9043	9711	1047.8	1.3	4		11247	9835	1042.0	-2.4
6761	771	1195.6	-1.1			8558	860	1194.0	-0.3
7033	0	1195.1	-1.6			8848	0	1193.3	-1.0
7044	9965	1195.4	-1.3			8861	9958	1193.4	-0.9
		e VII							
	( × 59°	(.T.A							
4825	499	210.7	40.1						
7752	0	211.3	10.7						
8343	9796	211.6	41.0						
11657	895	500.2	1.9						
12951	0	501.0	12.7						
13136	9850	501.3	<b>√3.0</b>						
13102	647	1062.2	-1.1						
13382	0	1061.5	-1.8						
13505	9700	1061.0	-2.3						
10871	636	1081.7	-2.0						
11077	0	1182.0	-1.7						
11082	9982	1184.0	<b>≠</b> 0.3						

	(-590	rge I F A.T.)			(-59	ge II F A.T.)	
Pange	Helphi	9.E.	Frror	Benge	Peleht	S.E.	Error
1184	996	-	-	1340	130	227.4	
2500	0	231.0		2290	0	227.6	
1788	9775	231.7		3028	9761	228.0	10.9
3209	414	469.4		2387	554	487.2	-0.6
3619	0	471.7		4128	0	488.7	10.9
2710	9746 861	473.4		4400	9831	4.88.4	10.6
3208	0	1122.5		3656	831	1183.2	/3.9
3290	9823	1100.3	-1.2	4128	0	1079.0	-0.3
2383	822	1099.6	-1.9	4220	9806	1079.3	0
2750	0	1224.5		3307	786	1160.6	12.7
2791	9888	1191.0	0	3668	0	1157.6	-0.3
		1191.0	-0.4	3709	9898	1157.3	-0.6
	Cher	ge III			Charge	TV	
	(-59°F	F A.T.)			(-59°F	1.T.)	
1531 2742	274	-	<b></b>	2024	200	214.0	-0.6
3449	0	210.0	10.4	3594	0	215.5	₹0.9
2757	9798	210.3	10.7	4412	9758	214.6	0
5037	638 0	454.4	-0.6	4492	894	498.0	-1.8
5464	9746	455.6	-0.4	6764	0	498.6	-1.2
5050	764	455.6	-0.4	7136	9751	498.8	-1.0
5503	0	1033.0	<i>1</i> 1.5	6356	843	1060.0	10.6
5606	9801	1031.0	-0.5	£805	0	1059.5	10.1
4232	819	1165.2	-0.9	6937	9723	1059.5	10.1
4584	0	1163.7	-0.7	5782	707	1197.6	0.
4664	9790	1164.2	-0.8	5442	0	1197.0	-0.6
•	, , , ,	1104.Z	-0.3	5527	9748	1196.7	-0.9

		15000 10	Sylvili 11 6 Au	tion Check (	"inus A	r Terr-59	°F)		
	Charge (-59°F					Chr re (-50°F	e VI		
Renge	<u>Heigh</u> t	Q.E.	Fror		Lenge	Helphi	C.F.	Fror	
2882 4458 5116 6018 7969 8353 8735 9353 9511 6385 6687 6756	247 0 9803 883 0 9743 866 0 9752 844 0 9790	215.0 215.5 215.0 480.2 479.8 902.1 903.7 903.3 1197.0 1196.0	10.4 10.5 10.4 10.9 -0.3 10.5 11.4 13.0 12.6 10.3 -0.7 -0.7		3794 5923 6714 6182 9866 10120 10475 10794 10871 8777 8544 8569	353 0 9733 904 0 9821 665 0 9829 706 0	209.2 210.3 209.5 463.0 462.5 462.5 1047.8 1046.0 1045.3 1194.3 1193.4 1193.3	0 2.1 20.3 20.2 2.4 2.6 20.9 -0.9 -1.0	
4888 7839 8560 11442 12689 12848 12784 13167 13272 10613 10898 10990	Chare (-59°) 509 0 9728 909 0 9863 905 0 9736 896 0	210.4 211.6 211.6 211.6 500.4 498.4 497.6 1063.4 1062.1 1062.4 1182.5 1182.6	-0.2 \$1.0 \$1.0 \$2.1 \$0.1 -0.7 \$0.1 -1.2 -0.9 -1.2 -1.1						

Charge	e I (Gra		vedrant	Pleasing Ores	( tere		Course)	
1 ance	Meight	C.E.	Irror		Bence	lie lebt	S.E.	Dia x
1187	981	-			1332	126	226.5	-0.6
1915	0	230.7	-0.4		2264	0	226.7	-0.4
2485	9772	231.2	1.0.		3010	9757	227.3	-0.8
1778	409	469.3	-2.2		2373	547	186.7	-1.1
3173	0	473.5	0		4080	0	187.1	-0.4
3596	9736	471.7	10.2		4372	OFIE	187.7	-0.1
2695	833	1116.54	15.0		3634	792	1082.5	13.2
3174	0	1101.5	-0.5		4081	0	1079.5	10.2
3272	9789	1100.0	-1.5		4195	9762	1079.5	10.2
2301	916	1242.2			3206	898	1162.3	Alach
2721	0	1192.3	10.9		3629	0	1157.6	-0.3
2776	9852	1191.6	10.2		3687	9853	1157.3	-0.6
Charge	III(Wh	ite Feg)			Charge	e IV (Grr	n. Beg)	
1526	145	209.3	-0.3		1524	145	209.6	0
2725	0	209.5	-0.1		2718	0	210.3	10.7
3438	9796	210.0	10.4		3433	979"	209.0	-0.6
2747	6329	454.5	-0.5		2743	637	454.3	-0.7
5001	0	455.4	10.4		4.989	0	454.6	-0.4
5442	9738	455.0	0		5434	9734	455.0	0
4915	603	1033.5	11.5		4909	889	1033.3	1.8
5460	0	1031.0	-0.5		5446	0	1033.0	1.5
5581	9766	1030.7	-0.8		5573	9754	1032.9	11.4
4214	982	1165.4	10.9		4209	770	1166.3	1.8
4549	0	1164.7	10.2		4538	0	1164.6	10.1
4644	9750	1164.3	-0.2		4638	9737	1164.4	-0.1

#### 1555 Quidrant Elevetion Check (Wt. of Froj & 1 Square)

C	herpe IV(	Grn.Feg)				Ch	arre V (C	rs. Meg)	
Pance	Petcht	<u>0.F</u> .	Imar			Purge	Felcht	Q.F.	Error
2034	201	214.9	10.3			2944	378	214.6	O
3629	0	215.2				4552	0	214.7	40.1
4444	9762	214.8				5217	9907	215.1	10.5
4510	902	499.3				6372	818	179.2	-0.2
6811	0	498.8				8207	0	478.0	-1.3
7164	9765	499.0				P514	9800	479.3	0
6360	854	1059.6				8276	752	1049.2	12.7
6814	0	1059.1	-0.3			8664	0	1048.5	12.0
6940	9736	1059.2				8787	9742	1048.0	1.5
5186	7.50	1197.4				6566	775	1196.0	-0.7
5452	0	1.96.4	-1.2			6842	0	1196.0	-0.7
5532	9763	1196.1	-1.5			9399	9700		
770-	,,,,,	,	•						
C	harge VI(	Thite Pa	g)			Cha	rge VII(W	hite Fag	)
2037	202	214.9	10.3			3778	348	208.2	-1.0
3638	0	215.2	10.6			5927	0	209.8	10.6
4450	9763	215.4	10.8			6503	9820	209.1	-0.1
4516	905	499.3	-0.5			8201	916	462.5	-0.2
6828	Ó	498.6	-1.2			10050	0	462.0	-0.7
7174	9770	498.5	-1.3			10283	9840	462.1	-0.6
6368	869	1059.9	10.5			10587	788	1049.8	15.4
6831	O	1059.4	0			10970	0	1047.4	13.0
6950	9752	1059.6	10.2			10996	9942	1047.0	12.6
5193	736	1197.1	-0.5			8469	654	1194.4	10.1
5465	0	1196.4	-1.2			8888	0	1193.5	-0.8
5540	9780	1196.6	-1.0			8720	9750	1195.4	<b>≠1.1</b>
Ch	ørge VIII	(White H	Bag)						
4843	500	209.0	-1.6					,	
7735	0	210.8	10.2						
8294	9810	210.5	-0.1						
11545	882	498.0	-0.3						
12794	0	497.1	-1.2						
12994	9833	497,0	-1.3						
12880	873	1064.8	A.5						
13260	0	1063.3	0						
13399	9657	1062.9	-0.4						
10694	868	1182.7	-1.0	£					
10094	0	1182.9	-0.8						
10976	9925	1182.5	-1.2						
10777	774)	##O8")	-1.2						

	109	ot Pute	Check			(4	ppesdir	1)	
	CH	ANGE I				au	RGE II		France
2	09_	1	<u>r'(m)</u>	Irror, $I = I$	1	02	1	r'(Iv)	I-I
1463 1829 2286 2743 3018 3383 3200 2743	200.0 256.9 336.7 431.0 501.0 924.2 1012.4 1141.5	8.0 10.2 13.2 16.7 19.2 31.6 33.4 36.0	10.24 13.25 16.75 19.25 31.96 34.00 36.64	0 10.04 10.05 10.05 10.36 10.60 10.60	1829 2286 2743 3200 3,66 4023 3658 3200	213.5 276.0 345.7 421.2 504.3 890.0 1032.3 1141.2	9.3 11.9 14.7 18.0 21.0 33.5 36.9 39.2	8.97 11.40 13.90 16.50 19.30 29.60 32.52 34.40	-0.33 -0.50 -0.60 -1.50 -0.70 -1.50 -1.50
	CH	ARGE III				СНА	RGE IV		
2103 2286 2743 3200 3658 4115 4663 4572 4115 3658	203.5 223.5 276.3 335.0 401.5 480.4 929.4 965.1 1079.0 1162.4	9.7 10.7 13.1 15.7 18.7 22.0 37.7 38.6 41.4 43.3	9.76 10.67 13.05 15.75 18.70 22.00 37.73 38.65 41.74 43.58	40.06 -0.03 -0.05 40.05 0 40.03 40.05 40.28	2743 3200 3658 4115 4572 5029 5121 5486 5029 4572	215.6 257.6 303.3 353.3 410.0 476.4 491.7 987.5 1078.0 1147.5	11.5 13.7 16.0 18.5 21.3 24.4 25.1 43.7 46.1 47.9	11.50 13.65 16.10 18.60 21.38 24.55 25.26 43.84 46.35 48.00	0 -0.05 40.10 40.08 40.15 40.14 40.25 40.10
	CHA	RGE V							
3658 4115 4572 5029 5486 5944 6401 6675 7315 6858 6401 5944	221.0 253.8 288.8 326.8 367.6 413.6 465.5 501.2 934.1 1021.8 1087.0 1141.0	13.6 15.6 17.6 19.8 22.1 24.6 27.4 29.3 451.4 53.8	13.57 15.54 17.58 19.80 22.13 24.70 27.50 29.47 40.50 51.58 53.61 55.10	-0.03 -0.06 -0.02 0 40.13 40.10 40.10 40.17 40.10 40.18 40.31 40.30					

	1	10519K Pus	• Check				(Append	lix A)		
		HARGE YI	1			CEARGE VII				
R	90	7	r'(Ev)	Pror	R	G	7	<b>F</b> ( <u>T</u> v)	F - F	
4115 4572 5029 5486 5944 6401 6858 7315 7772 8230 9144 8687 8230 7772	197.5 224.3 252.4 281.7 312.7 345.8 381.0 419.5 462.3 512.0 907.0 1048.0 1097.8	13.9 15.7 17.6 19.5 21.5 23.6 25.8 28.2 30.8 53.6 55.6 56.6 56.7	13.80 15.60 17.60 19.46 21.46 23.62 25.90 28.30 30.88 33.80 53.30 56.52 58.87 60.67	40.10 0.04 40.02 40.10 40.10 40.20 40.10 40.20 40.10 40.37	5486 5944 6401 6858 7315 7772 8230 8687 9144 9601 10058 10973 10516	206.5 230.5 255.4 282.4 309.4 338.5 369.5 403.0 476.3 526.4 915.0 985.0 1037.6	17.2 19.0 20.8 22.7 24.7 26.7 28.8 31.1 33.6 36.2 39.1 60.2 63.4 65.6	17.14 18.90 20.80 22.66 24.66 26.76 28.90 31.18 33.50 36.17 39.26 60.57 63.76 65.94	-0.06 -0.19 0 -0.04 -0.06 -0.10 -0.03 -0.16 -0.37 -0.36 -0.34	
7315	1141.0	61.7	61.15	_0.55	9601 9144 8687	1081.0 1119.0 1152.7	67.2 68.6 69.8	67.68 68.98 70.40	10.41 10.38 10.60	

Date: 9 October 1957 Name: Cassidy

	Char	1 15	SM Fuse	Check	(4	ppendix			
R_	01	E		Pu:• Error	R	Char Q!	Z II	7.	Fu se Error
1829 2286 2743 3200 3383 3658 3200 2926	226.0 298.5 376.4 470.8 516.5 965.7 1100.0 1158.0	9.5 12.2 15.2 18.6 02.2 34.3 37.0 38.0	9.51 12.38 15.40 18.95 20.58 33.83 36.40 37.13	\$0.20 \$0.35 \$0.38 \$-0.60	2286 2743 3200 3658 4115 4297 4755 4572 4115 3658	227.0 280.6 339.3 407.1	10.6 13.0 15.6 18.4 21.6 23.1	10.70 13.10 15.73 18.62 22.04 23.30 36.17 38.05	\$0.10 \$0.10 \$0.13 \$0.22 \$0.14 \$0.20 \$-0.53 \$-0.55
	Char	ge III				Cha	urge IV		
2743 3200 3658 4115 4572 5029 5395 6035 5486 5029 4663	209.3 250.0 293.8 341.5 393.9 454.2 511.2 890.2 1033.1 1106.5 1153.8	11.2 13.3 15.5 17.9 20.5 23.3 25.9 41.2 45.3 47.2	11.15 - 13.25 - 15.48 - 17.85 - 20.45 - 23.35 / 25.97 / 40.62 - 44.82 - 46.43 - 47.05 -	0.05 0.05 0.05 0.05 0.05 0.07 0.58 0.18 0.77	3658 4115 4572 5029 5486 5944 6401 6858 7315 6858 6401 5944	215.0 246.7 287.0 316.2 355.0 397.3 414.2 499.0 991.2 1059.7 1113.3 1157.8	13.3 15.2 17.2 19.3 21.5 23.9 26.5 29.4 50.0 52.3 53.9 55.2	13.18 15.12 17.07 19.15 21.30 23.68 26.24 29.15-50.10 52.00 53.37	-0.08 -0.13 -0.15 -0.22 -0.26 0.25 -0.10 -0.30 -0.53

Charge V			15901 Fuze Check (Appendix B) Charge VI					
R	01	<u>r</u>	Fuze Error	R	٥,	E	<u>F1</u>	Fuze
4572 5029 5486 5944 6401 6858 7315 7772 8230 8687 9601 9144 8687 8230 7772	241.3 269.7 299.0 229.8 362.7 397.8 436.2	15.0 16.8 18.6 20.5 22.4 24.4 26.6 29.0 31.5 34.2 53.4 56.6 58.7 60.3 61.6	15.06 \$\forall 0.06 16.80 0 18.60 0 20.18 -0.02 22.12 \$\forall 0.02 21.50 \$\forall 0.03 28.87 -0.13 31.47 -0.03 31.32 \$\forall 0.12 52.90 -0.50 56.28 -0.32 58.47 -0.23 59.80 -0.50 60.43 -1.17	5944 6401 6858 7315 7772 8230 8687 9144 9601 10058 10516 11887 11430 10973 10516 10058	209.9 233.0 256.5 281.2 307.5 335.2 364.0 394.6 427.2 462.6 501.7 929.4 297,0 1046.0 1085.0 1117.7	19.1 20.9 22.7 24.5 26.4 23.8 30.3 32.5 34.8 37.3 61.8 64.6 66.6 68.1	19.15 20.90 22.70 24.50 26.45 28.47 30.48 32.70 35.08 37.67 61.70 64.53 66.70	0 0 0 0.05 0.17 0.18 0.20 0.28 0.37 -0.10 -0.07 0.10
	Charge	VII		9601	1145.7	70.4	68.97	-1.43
7772 8230 8687 9144 9601 10058 10516 10973 11430 11887 12344 12802 14630 14173 13716	212.1 232.4 253.7 276.0 298.8 323.0 348.1 375.0 402.8 432.4 463.9 498.5 910.0 978.5	20.7 22.4 24.1 25.9 27.7 29.5 31.4 33.3 35.3 37.5 39.8 42.2 69.1 72.1 74.3	20.57 -0.13 22.20 -0.20 23.86 -0.24 25.52 -0.38 27.41 -0.29 29.15 -0.35 31.08 -0.32 33.02 -0.28 35.20 -0.10 37.30 -0.20 39.60 -0.20 42.24 /0.04 67.92 -1.18 71.60 -0.50 74.11 -0.19					

			1590t Drift Check				
Charge I	R(H)	<u> </u>	Conpute A2	Drift	Allovat	Error ble Dry - Allow	Percentage Within 1 Mil Accuracy
	550	6397.5		-2.0	1	1.0	
	1470	6399.5	6397.0	-2.5	2	10.5	
	2750	0	6393.5	-6.5	6	10.5	
	2750	0.5	6342.5	58.0	52	16.0	3/4
Charge II	550	6390.5	6389.5	-1.0	0	A.0	
	1470	6397.0	6395.0	-2.0	2	0	
	2750	6398.5	6394.0	-4.5	4	10.5	
	3660	6399.3	6347.5				1, /1.
	,	0377.3	0347.5	-51.8	52	-0.2	17/14
Charge II		6390.0	6390.0	0	0	0	
	1470	6397.0	6395.5	-1.5	1	10.5	
	2750	6398.5	6395.7	-2.8	3	-0.2	
	5500	0.5	6363.5	-37.0	39	-2.0	3/4
Charge IV	550	6390.0	6390.0	0	0	0	
	1470	6396.7	6395.7	-1.0	ĭ	ŏ	
	2750	6398.7	6396.7	-2.0	2	ŏ	
	5950	0	6348.5	-51.8	51	10.5	4/4
Charge V	550	6390.0	6390.0	0	0	0	
	1470	6396.7	6396.0	-0.7	1	-0.3	
	2750	6398.5	6397.0	-1.5	1	10.5	
	9140	0.5	6367.0	-33.5	35	-1.5	3/4
Charge VI	550	6200 0	/ * * * * * * * * * * * * * * * * * * *				
Otter Ra AT		6390.0	6390.0	0	0	0	
	1470	6396.5	6396.0	-0.5	0	10.5	
,	2750	6398.5	6398.0	-0.5	1	10.5	
1	1000	0.5	6360.0	-40.5	42	-1.5	3/4
Charge VII	550	5390.0	6390.0	0	0	0	
	1470	6396.7	6396.5	-0.2	Ö	10.2	
	2750	6398.5	6398.0	-0.5	1	10.5	
	1700	0.5	6340.5	-6.0	58	12.0	3/4
							J/ <b>4</b>
						Total Percentage	23/28 82.0

105MM Drift Check

			Compute	r	Error		Percentage with	
CHARGE I	R	Az	Arimuth	Drift		Drift - Allow	l mil Accuracy	-
	550	6391.0	6388.5	-2.5	,	41.5		
	550	6397.0	6393.0	٥. الله	3 8	71.0		
	2750	6399.0	6391.5	-7.5	2	-0.5		
(H.A.)	1830	6398.0	6326.5	-71.5	70	μ.5	2/4	
CHARGE II	550	6391.0	6389.5	_1.5	1	40.5		
	1470	6397.0	6394.0		3	6		
	2750	6399.0		-3 -6	š	Ö		
(H.A.)	3110	6399.3	6393.0 6342.5	-56.8	57	-0.2	4/4	
CHARGE III	550 1470	6391.5	6389.7	_1.8	1	40.8		
	1470	6397.3	6394.7	-2.6	2	70.6		
	2750	6399.0	6394.0	-5.0	5	0		
(H.A.)	4570	6399.5	6369.0	-30.5	1 2 5 28	12.5	3/4	
CHARGE IV	550 1470	6391.3	6390.5	_1.5	1	<b>40.</b> 5		
		6397.3	6395.3	-2.0	2	0		
	2750	6399.0	6395.3	-3.7	2	-0.3		
(H.A.)	4570	0	6395.3 6345.0	-55	54	41.0	4/4	
CHARGE V	550 1470	6391.5	6390.7	-0.8	1	_0.2		
	1470	6397.3	6396.0	_1.3	1	40.3		
	2750	6399.0	6396.3	-2.7	3	-0.3		
(H.A.)	6398	0.3	6355.0	45.3	43	42.3	3/4	
CHARGE VI	550 1470	6391.3	6390.7	_0.6	0	40.6		
	1470	6397.3	6396.3	_1.0	1	0		
	2750	6399.0	6397.0	-2.0	2	Ö		
(H.A.)	8226	0.5	6361.0	-39.5	37	12.5	3/4	
CHARGE VII	550	6391.3	6391.0	-0.3	0	40.3		
	1470	6397.3	6396.3	_1.0	ĭ	0		
	2750	6399.0	6397.8	1.2	ī	£ŏ.2		
(H.A.)	9140	0.5	6350.0	50.5	48	¥2.5	3/4	
					Tota	1 Percentage	22/28 76.5	

### Range Spread Test (1599)

Range (C)	<u>-1C</u>	-1/20	17/20	10
1000	900	950	1050	1097
2000	1900	1950	20.8	2096
30000	2902	2951	3050	3097
6000	3900	3950	4048	4095
5000	4900	49-0	5048	5098
6000	5900	5950	6050	6098
7000	6900	6950	7050	7098
8000	7900	7950	8050	8097
9000	8900	8950	9050	9097
10000	9900	9950	10050	10097

Range Spread (105134)

Range (C)	1 3c	<u> 10</u>	<u>≯c</u>	10
1000	1049	1197	950	900
2000	2048	2096	950 1949	1998
3000	3049	3096	2950	2900
4000	4050	4097	3950	3900
5000	5049	5098	4950	4900
6000	6048	6098	5950	5900
7000	7049	7100	6951	6900
8000	8050	8098	7950	7900
9000	9049	9098	8950	8900
10000	10048	10097	9950	9900

10500 Normals (Miscellaneous Problems from SEL EDVAC Computer) Charge I

Bance	Enichi	G. E.	Q.F. Error	Corresponding R. Error
947	68	200.5	40.5	3.20
962		201.8	40.8	5.12
951.		201.2	- 0.1	0.64
1501	9993	200.7	40.7	4.50
1507		201.7	40.7	4.50
1503		201.0	40.6	2.56
2218.	9759	201.0	41.0	6.40
5555		201.5	4 0.5	3.20
. 22.18		200.5	40.3	1.92
1600	419	498.4	_ 1.6	6.03
1644		497.2	_ 1.8	6.59
1677		493.0	_ 1.9	6.95
3020	9997	500.5	10.5	1.83
3023		500.5	- 0.5	1.83
3020		500.5	40.4	1.47
3373	9758	500.7	40.7	2.56
3381		501.0	0	0
3380		501.4	11.0	3.66
2635	784	1047.0	447.0	
2636	-		41	
2635	-			
3190	43	1008.0	<b>∠</b> 8.0	21.9
3192		1007.3	1 8.4	23.9
3190		1008.0	18.2	22.5
3280	9888	1005.0		13.7
3283		1004.1	4 5.0 4 5.2 4 6.9	14.3
3281		1006.6	15.2 16.9	19.0

	10510	H Low As	gle Test Pro	blems Co	mbined	ects	(Misellaneon	m Proble	me)	
			w = 0	Ro En No	eference isting - 9 orthing - eight -	96500 750 274		Angle _5 1316 (1_ Spot _ I	154	es)
Formale	Charme	Banco	Pance Error	Arimuth	Az Error	Ture	Fue Error	Ç.E.	Q.E.Error	
	1 2 3 4 5 6 7	2980 2982 2986 2990 6010 6012 6013	-6.0 -7.0 -7.0 -7.0 46.0 45.0	648.2 650.5 652.3 653.4 3849.7 3851.7 3853.3	1 3.2 1 3.5 1 3.3 1 3.4 1 1.7 1 2.7 1 3.3	19.32 15.55 14.54 12.75 25.20 21.87 19.20	1 0.03 - 1.15 - 0.16 1 0.05 1 0.10	533.3 421.7 339.2 269.2 438.1 333.2 249.3	-2.7 -0.3 -0.8 40.2 43.1 42.2 42.3	
N/ Muzzl Velocity (30 ft/s										
()0 10/1	1 2 3 4 5 6 7	2980 2982 2985 2990 6010 6013	-6.0 -7.0 -8.0 -7.0 46.0 46.0	649.6 651.3 652.6 653.7 3850.7 3852.5 3853.4	1 2.6 1 2.3 1 3.6 1 2.7 1 2.7 1 2.7 2 3.5 1 2.4	17.10 14.20 13.40 11.90 23.83 21.25 18.70	- 1.50 - 2.20 - 1.10 - 0.80 - 1.07 - 0.65 - 0.50	468.8 382.0 313.0 252.0 412.5 324.0 242.5	-2.2 11.0 0 0 12.5 12.0 12.5	
N/ MV / V (540 - W)										
( ) . · · · · · · · · · · · · · · · · · ·	1 2 3 4 5 6 7	2980 2982 2985 2990 6010 6013 6013	-6.0 -7.0 -8.0 -7.0 46.0 46.0 46.0	649.6 651.3 652.6 653.5 3850.0 3851.5 3853.0	2.6 2.3 2.3.6 2.0 2.0 2.0 2.0 2.0 2.0	16.75 14.00 13.23 11.80 25.50 23.15 19.85	- 1.75 - 2.30 - 1.27 - 0.90 \$\delta\$ 0.20 \$\delta\$ 1.15 \$\delta\$ 0.65	459.0 376. 309.4 250.0 443.0 353.0 257.6	-2.0 -0.6 0 -2.0 -1.0 -2.6	

105MM Low Angle Test Problems Combined Effects (Miscellaneous Problems) (Cont'd)

N L MT L	Charce	Prace	Rose Error	Azimith	Ar, Trror	Pase	Luse Error	0.3.	Q.Y. Irrer
v L Air Density (110%)	1 2 3 5 7	2980 2982 2986 2989 6010 6013	-6.0 -7.0 -7.0 -8.0 /6.0 /6.0	649.8 (51.4 652.5 (7).0 3849.6 3853.6	1 2.8 1 3.4 1 3.5 1 4.0 1 1.6 1 3.8 1 3.6	16.90 14.10 13.36 11.87 26.16 23.76 20.50	- 1.70 - 2.20 - 1.14 - 0.83 \$\delta\$ 1.76 \$\delta\$ 1.56 \$\delta\$ 1.20	464.0 379.5 312.0 251.7 454.5 363.5 267.7	2.0 40.5 0 -0.3 40.5 40.5
Tomp (0°)  AT LATE  MENTALE  M	• >								
1047 (07	1 2 3 4 5 6 7	2980 2983 2985 2990 6010 6013 6013	_6.0 _6.0 _7.0 _46.0 _46.0 _46.0	649.8 651.3 652.6 653.7 3849.3 3851.0 3852.8	1 2.8 1 3.3 1 3.6 1 3.7 1 2.3 1 3.0 1 2.8	16.93 14.10 13.37 11.90 26.95 25.25 21.14	- 1.67 - 2.30 - 1.13 - 0.80 \$\frac{1}{1.25}\$ \$\frac{1}{2.95}\$ \$\frac{1}{1.74}\$	464.0 379.6 312.0 251.5 470.1 386.9 276.4	12.0 -0.4 0 -0.5 12.1 -1.1 10.4
NATAPOWDER Temp (O°F									
	1234567	2980 2983 2985 2985 2990 6010 6013	-6.0 -6.0 -8.0 -7.0 46.0 46.0 46.0	649.3 651.0 652.3 653.7 3849.3 3851.0 3853.0	2.3 2.3.0 2.3.3 2.3.7 2.3.0 2.3.0 2.3.0	17.44 14.50 13.80 12.24 28.20 25.96 21.70	- 1.26 - 1.90 - 0.80 - 0.46 / 2.20 / 3.56 / 2.30	478.2 391.7 322.0 259.4 492.8 397.7 283.7	-3.8 \$\frac{1}{0.3}\$ -1.0 -0.6 -1.2 -3.3 -1.3
NAMVAWADA ATAPTA wt.	4				9				
	1 2 3 4 5 6 7	2980 2983 2986 2988 6010 6013 6013	-6.0 -6.0 -7.0 -9.0 46.0 46.0	649.3 650.8 652.2 653.3 3848.7 3850.8 3852.8	2.8 4 3.2 4 3.3 4 2.7 4 1.8	17.75 14.75 14.00 12.40 28.54 25.95 21.70	- 1.75 - 0.60 - 0.30 \$\darklep\$ 2.44 \$\darklep\$ 3.55	398.2	-1.4 -0.5 0 -1.0 -4.8 -1.7

105MM Combined	Effects	High	Angle	Tost	Prollens	(Miscella mecus	Problems)
						Baras	

	East	ing -	0 0 0	Dbe. Diet. Dbe. Azima: Dbe. Vert. Eft_Right Drop = Add Down = Up	Angle = 0 = 0 = 0	Darge 1 2 3 4 5 6 7	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Northing 2973 2979 3986 4995 6009 7013 8013	91 91 91 91 91 91 91
Normale	Charm	Pance	Pance Error	Azimith	Az, Error	Pare	Puze Erro	ς 9,Σ,	Q.F.Erro:
	1 2 3 6 7	2978 2979 3981 4985 5990 6991 7990	- 7 - 5 - 8 - 9 - 7 - 4 1	6358.0 6361.3 6353.7 6357.0 6348.3 6343.4 6340.2	- 3.0 - 1.7 - 2.3 - 2.0 - 0.7 - 0.6 \$\darklet\$ 0.2	34.60 39.55 41.50 45.94 54.54 62.60 71.23	1 0.70 1 0.15 1 0.30 1 0.54 1 0.60 1 1.17	1067.6 1177.5 1098.3 1078.4 1132.7 1166.3 1197.5	12.5 15.3 14.4 12.7
N / Muzzle Velocity		sec)							
	1 2 3 4 5 6 7	2983 2980 3983 4985 5992 6993 7990	- 3 - 6 - 7 - 9 - 3 0	6368.0 6347.3 6362.5 6364.5 6354.0 6345.3 6341.0	- 4.0 - 3.7 - 2.5 - 1.5 - 1.0 - 0.7	32.25 33.80 40.03 44.22 53.45 62.20 70.90	\$\begin{align*} 4 3.30	971.5 1130.1 1035.5 1019.5 1097.3 1153.5 1189.0	110.5 16.1 18.5 16.5 14.3 12.5 1 2.0
N/HV/Wind (N50, W20)									
(3.70) #20)	1 2 3 4 5 6 7	2981 2980 3983 4986 5993 6995 7992	- 5 - 7 - 8 - 5 - 4	6372.3 6352.8 6367.0 6369.3 6361.0 6354.0 6347.3	<b>∠10.0</b>	30.97 33.13 38.72 42.64 51.88 60.07 69.35	4.27 4.0.13 4.92 4.94 4.94 4.57 4.95 4.965	919.0 1098.7 989.0 969.0 1050.0 1098.0 1137.0	£26.0 £7.7 £14.0 £11.0 £9.0 £8.0 £6.0

1050M High Angle Test Problems Combined Effects (Miscellaneous Problems) (Cont'd)

wheeled	Cherce	20.74	Ferce Error	ALLDIA	&r. Error	Date	Pase Lycer	Q.I.	Q.F. Error
Mir Denvi	**								
(90≸)	1 2 7 5 6 7	2982 2980 3983 4985 5992 6993 7990	- 7 - 7 - 96 - 46	6370.7 6351.0 6355.5 6367.3 6355.5 6350.0 6343.5	1 3.7 1 6.0 1 5.5 1 6.3 1 7.5 111.0 117.5	31.50 33.35 39.30 43.40 52.64 60.97 70.33	4 3.90 - 0.55 4 4.30 4 4.20 4 4.94 4 5.67 4 6.33	943.0 1110.0 1005.0 994.0 1070.8 1103.8 1164.0	123.0 17.0 18.0 18.0 15.8 15.8
ATHATATO									
Air Temp (118°F)	1 2 3 4 5 6 7	2979 2980 3980 4980 5988 6990 7985	- 6 - 6 - 10 - 14 - 10 - 3 1	6369.0 6349.5 6364.3 6366.2 6357.5 6346.0 6341.7	1 2.0 1 3.5 1 4.3 1 5.2 1 6.5 113.0 118.7	31.60 33.35 39.40 43.48 52.70 61.83 70.75	4 3.80 - 0.35 1 4.30 1 4.28 1 5.20 1 3.23 1 3.85	944.5 1110.0 1110.4 995.5 1072.0 1146.0 1180.0	120.5 17.0 112.4 110.5 17.0 15.0 14.0
KLMY LWLAD LATLP owder									
Temp()	1 2 3 5 6 7	2974 2978 3978 4980 5985 6987 7985	-11 - 8 -12 -14 -13 -1	6364.6 6345.0 6359.7 6362.5 6353.3 6344.0 6341.0	13.6 15.0 15.7 15.5 18.3 114.0 118.0	32.90 33.90 40.50 44.55 53.50 62.33 70.90	<pre></pre>	995.2 1137.5 1050.0 1032.3 1100.0 1159.0 1189.6	15.2 16.5 11.0 16.3 16.0 15.0 14.6
NAMV AWAD LATAPTAWt.									
of Proj(	2 3 4 5 6	2974 2976 3878 4980 5987 6988 7982	111 1 8 111 113 1 8 2 2 2 2	6363.0 6344.0 6355.0 6361.3 6352.3 6344.0 6341.0	1 2.0 1 5.3 1 8.3 114.0	33.34 34.03 41.25 44.90 53.67 62.38 71.00	∠ 2.34 — 2.47 ∠ 3.17 ∠ 2.60 ∠ 2.97 ∠2.18 ∠ 2.70	1012.5 1146.5 1082.4 1041.7 1104.3 1158.5 1188.0	\$\frac{1}{5.5}\$ \$\frac{1}{5.5}\$ \$\frac{1}{5.5}\$ \$\frac{1}{31.4}\$ \$\frac{1}{5.7}\$ \$\frac{1}{3.3}\$ \$\frac{1}{3.5}\$ \$\frac{1}{3.0}\$

(Miseellename Froblems Combined Effects (All Corpus)

Settings (\*1) Charries)

Facting - 0 Forthing - 0 Feight - 0

| Northing = 0 | Ohr. Disinse = 6401 | Northing = 0 | Ohr. Vot. 7: 1e = 150 | Northine = 0 | Nor

Trap-Ado-1500 Town-Up-137

Charge	( to 2 = 4 1)
1	1250
2	2000
3	2250
4	2500
5	2750
5	3250
7	5500

<u></u>	ormola	Renge		'zj=ut	h	Fuse		
Charge	Fonce	Frror	azimuth	Frror	Fuse	Error	Ç.F.	C.J. Irror
1 2 3 4 5 6 7	2757 3278 4500 5615 <b>67</b> 06 8678 10226	£2 £10 £17 £14 £10 £11 £7	848.8 2818.0 3057.0 3310.7 3522.7 3885.5 5399.0	1.8 12.0 11.0 0 10.7 10.5 13.0	15.15 15.86 19.72 21.66 23.45 28.00 29.60	-0.05 -0.04 /0.02 -0.04 -0.15 -0.20 -0.60	334.0 315.2 358.2 345.0 335.5 348.5 320.4	-6.0 -0.8 -0.5 -1.0 -0.5 -2.5 -0.6
N / Muzzle	Velocity (	30Ft/Sec	)					
1 2 3 4 5 6 7	2757 3279 4496 5615 6706 8678 10226	-2 \$11 \$13 \$14 \$10 \$11 \$7	849.4 2818.6 3057.0 3311.2 3522.8 3885.5 5399.0	\$3.4 \$2.6 \$2.0 \$1.2 \$0.5 \$1.0	13.80 14.65 18.30 20.56 22.72 27.24 38.76	-1.20 -1.05 -1.20 -1.04 -1.78 -0.96 -1.46	298.2 285.4 328.5 324.0 323.5 336.3 310.0	-4.8 -1.6 -1.5 -1.0 -0.5 -2.7

# Armed Services Technical Information Agency

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			15000	"ou that a	Test From	lema Co	-hined Ef	fects	
				(Miscellane	our F. obl	erus ) (fo	n't)	As in disputs."	
N A	39. 1.	lind	Pan 'e		/zimut		Fuze		
133	3/1年	3-5-00	Treer	1-1-uth	Freer	Time		C.E.	Q.E. Frrgr
Che	ree 1	2757	-2	850.C	/3.0				
	2	3279	/11	2821.5	10.5	13.7		294.0	-5.0
	3	4498	/15	3060.8	/0.8	15.4		286.8	-2.2
	1	5615	414	3314.4	10.4	21.2		332.8 338.2	-2.2 -2.8
	5	6705	19	3526.0	-1.0	24.30		348.2	-0.8
	6	0833	413	3884.5	-0.5	29.0		362.8	-3.2
	7	10221	+3	5379.7	16.7	28.9	,	311.5	-0.5
N 🖈	MY X W	✓ Air Den	sity (110	00/0)					
	2	2759	^	050 0	10.0				
	2	3279	0 /11	2822.0	12.3	13.78		296.7	-5.3
	3	4495	<del>/</del> 12		12.0	14.82		289.8	-2.2
	4	5615	114	3060.3 3314.0	40.3	18.75		336.8	-2.2
	5	6703	17	3524.6	-1.0 -2.4	21.62		344.3	-2.7
	5	8679	112	3834.2	-1.8	30.20		358.1 381.0	-1.9
	7	10221	43	5379.3	₹5.3	30.40		331.5	-4.0 -0.5
N /	MV ≠ W	# AD # Mir			,,,,,	,,,,,	, 0.20	<i>) . • )</i>	-0.7
	1	2760	<i>/</i> 1	850.8	12.8	13.73	-1.27	296.0	-2.0
	2	3280	12	2822.0	1.0	14.80		289.0	-2.0
	3	44,98	<i>4</i> 15	3060.8	40.8	18.70		336.6	-2.4
	4	5616	115	3313.7	-1.3	21.87		348.5	-5.5
	5	6706	10	3525.6	-2.4	25.50	12.60	368.0	<b>-9.0</b>
		8680	¥13	3884.0	-2.0	30.60	12,00	387.0	-9.0
	7	10220	74	5379.5	<i>45.5</i>	30.46	<b>≠</b> 0.16	331.8	<b>≠</b> 0.8
N / M	ny X w	AD AT,	Power T	emp (0°)					
	1	2759	Ö	850.6	12.6	77.07	-0.96	304.0	<b>5</b> 0
	2	3280	,	2821.5	-0.5	15.18	-0.62	297.4	<b>-5.0</b>
	3	4498		3060.2	3.0-	19.52		353.2	-2.6 -3.8
	4	5617		3313.7	-1.3	22.80	₹0.90	365.4	-7.6
	5	6707		3525.6	-2.4	26,22	f2.22	379,8	
	6	8679	-	3884.0	-2.0	31.40	f2.70	399.0	-11.2 -11.0
	7	10222		5379.2	£5.0	31.35		343.6	-2.4
N /	MV X W	/ 'D / AT		T of Projec		)	700,75	242.0	-~:4
	ı	2759	0			21 26	0.05	200 0	r 0
	2.	3280		850.4 2821.0	<i>4</i> 2.4 −1.0	14.15	-0.85	307.2	-5.8
	3	4498		3060.0	-1.0	15.26 19.64	-0.54	300.0	-3.0
	4	5616		3314.0	-1.0	22.94	-0.16 \$0.94	355.0	-6,0
	5	6706		3525.7	-2.3	26.30	12.20	367.7	-9.3
	6	8679		8884.0	-2.0	31.45	12.75		-13.2 -11.7
	7	10223		379.2	15.2	31.40	1.00	344.0	-3.0
			,	7.7.1.	7 7 4 65	77.110	71.00	J. L U	-2.0

B-46

### 1600 Fich Smale Port Froblems Contined Fffeets (Piecellaneous Problems)

	Satt	10.00	(A12 CM	15 (48)
--	------	-------	---------	---------

GHOLY	Con Bons	DIA COURTING		
Fasting - 0 Northing - 0 Haight - 0	Asisuth - 0 Mistance - 0 Vertical Angle - 0	form = Up = 0 left = Right = 0 left = idd = 0		

### BREET STITUS

Charge	"or thing	Sasting	Height
I	3383	9	100
II	4.298	0	100
III	5395	O	100
IV	6858	0	100
V	8687	0	100
VI	10973	C	100
AII	13350	0	100

		Normal	Range		Azimut	h	Fuze		
		Range	Fror	Azlmuth	Frrer		Frror	G.F.	Q.E. Error
Charge	1	3385	<b>/19</b>	6362.4	-76.6	34.71	10.01	1038.8	-5.2
	2	4304	£116	6363.8	~73.2	39.00	40.10	1026.5	-5.5
	3	5398	1.26	6363.0	-76.0	44.50	-0.10	1039.8	-4.2
	4	6863	<i>f</i> 31	6361.8	-78.2	51.47	-0.13	1052.4	-4.6
	5	8690	<i>‡</i> 30	6362.3	-77.7	57,84	-0.16	1042.0	-3.0
	6	10971	£24	6360.0	-82.0	66.36	-0.04	1042.6	-1.4
	7	13345	<i>f</i> 23	6355.0	-93.0	75.10	-0.40	1053.5	-2.5
		Normals	# Muzzl	e Velocity	y (-30 <sup>Ft</sup>	/Sec)			
	1	3387	<i>4</i> 20	6372.0	-56.0	32.03	,2.63	923.2	-8.3
	2	4305	125	6372.2	-55.8	36.15	12.65	922.7	-7.3
	3	54.00	127	6369.5	-62.5	42.25	12.65	963.6	-5.4
	4	6865	/31	6367.0	-67.0	49.70	12.60	997.0	-6.0
	5	8692	<i>√</i> 31	6365.2	-70.8	56.90	1.70	1012.5	-3.5
	6	10975	127	6362.5	-76.5	65.15	1.35	1018.7	-1.3
	7	13347	124	6357.3	-87.7	74.25	¥1.35	1034.2	-2.8

		22	SELIO.	2011	13,511	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 3 3	
(Fireattersons frottens)(Comft)								
N50 47 11	2017745	1 200		9 = 6	1	Faire		
	Dinne	1220	3-555	Diese	State of the last		Q. T. 1	erez
Charge I	3390	(2)	6377.1	427,2			-74.	
2	4310	100	6377.0	-51,7			n.	
3	5105	133	6973.3	-37.7	40.40		-1.0	
4	6893	110	6327.3	12.5	47.46		***	
5	6702	r-1	6272.7	-69.3	42.75	1.25 72.0	-1.0	
6	10000	110	1777.6	.67.6	60.30	M.30 000,6	41.6	
7	13370	14.0	63/17.3	-7.7	68.30	16.50 927.5	-2.5	
4 + 101 + 1	Ur Density	(900/)						
1	3390	127	6324.3	-56.7		/2 10 000 0		
2	4308	/29	6371.0	-58.0	3".43	13.20 858.7	-7.3	
3	5/03	431	(371.0	-65.0	41.70	43.30 9/3.0	-6.£ -5.0	
4	6772	139	6360.0	-90.0	48.82	13.52 972.6	-5.4	
5	8700	41.1	6368.7	-72.3	54.90	13.50 966.5	-4.5	
6	10988	144	6365.5	-82.5	63.56	13.36 984.8	-0.2	
7	13363	<i>f</i> 47	6359.3	-97.7	73.10	42.70 1014.0	-3.0	
N Y MV Y W								
1	3386	119	6373.0	-57.0	31.00	/3.20 883.7	-6.3	
3	4305	126	6373.3	-58.0	35.20	13.30 887.6	-5.4	
3 4	5400 6866	<b>√</b> 28	6370.4	-65.6	41.52	13.42 939.0	-5.0	
5	8696	√33 √3ε	6369.0 6365.3	-71.0	48.92	£3.52 974.7	-4.3	
6	10980	<i>‡</i> 37	6362.8	-100.0 -88.2	56.46	12.06 1004.4	-2.6	
7	13357	743		-100.0	64,78 73.90	\$2.18 1011.0 \$2.10 1026.7	√1.0 -2.3	
N K MV K W	≠ A.D. ≠ A				15.70	72.10 102.01	-2.,7	
					20.05	/a a m		
1 2	3386 4306	√19 √27	6370.0 6370.6		32.25	,2.85 931.0	-4.0	
3	5400	f28	6368.2		36.47	£2.67 931.2	-4.8	
4	6867	135	6366.3		42.4 <b>7</b> 49.65	<i>f</i> 2.5 <b>7</b> 970.3	-3.7	
5	8694	-37	6364.0		57.02	₹2.65 997.2 ₹1.42 1018.0	-3.8	
5	10977	135	6361.2		55.63	1.23 1028.3	-2.0 ≠1.3	
7	13355	+43			74.75	40.65 1045.2	-1.8	
N X MV X W,						70.07 1047.2	-1,0	
1	3385	<b>/</b> 18	6369.0	-63.0	16.54	17.74 945.2	<i>f</i> 27.2	Grn Bag
2	4303	124				13.80 946.3	125.3	ii ii
3	5398	<i>f</i> 26				/3.30 981.0	£13.0	ri #1
4	6866	134 137	6365.6	-75.4 5	0.00	13.40 1005.6	19.6	tt tt
5	8694	137	6364.0	-83.0 5		1.65 1020.4	41.4	11 11
6	1.0975	,			5.5%	₹1.15 1028.3	40.3	White Bag
7	13352	140	6355.5 -1	05.5 74	.73 +	10.53 1045.6	-1.4	n n

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