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APPARATUS AND METHOD FOR CALIBRATING VOLTAGE SPIKE WAVEFORMS

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) JOSEPH M. MUHITCH employee of the United States Government and citizen of the United States of America, (2) EDWARD W. WILBUR, JR., citizen of the United States of America, residents (1) Exeter, County of Washington, State of Rhode Island and (2) Bristol, County of Bristol, State of Rhode Island, have invented certain new and useful improvements entitled as set forth above of which the following is a specification:

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APPARATUS AND METHOD FOR CALIBRATING VOLTAGE SPIKE WAVEFORMS

STATEMENT OF GOVERNMENT INTEREST

The invention described herein may be manufactured and used by or for the Government of the United States of America for governmental purposes without the payment of any royalties thereon or therefor.

CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

This patent application is co-pending with one related patent applications entitled APPARATUS AND METHOD FOR CALIBRATING VOLTAGE SPIKE WAVEFORMS FOR THREE-PHASE ELECTRICAL DEVICES AND SYSTEMS (Attorney Docket No. 83342), by the same inventor as this application.

BACKGROUND OF THE INVENTION

(1) Field of the Invention

The present invention generally relates to an apparatus and method for calibrating voltage spike waveforms that are used to test survivability and compatibility of an electrical device.

2. Description of the Prior Art

Many electrical devices, both military and commercial-off-the-shelf ("COTS"), have specifications that are incomplete with regard to compatibility and survivability. This problem is exacerbated when COTS devices are integrated with devices configured in accordance with military specifications such as onboard electronics of a submarine or other naval vessel. Vendors typically do not perform tests or evaluations on the compatibility and survivability characteristics of electrical devices.

What is needed is a technique for efficiently and inexpensively testing the compatibility and survivability of electrical devices.

Prior art systems and techniques for testing electrical devices with voltage spike waveforms and voltage spike suppression devices are disclosed in U.S. Patent Nos. 4,307,342, 5,463,315, 5,525,926, 5,623,215 and 6,088,209. However, such prior art systems and techniques do not address the aforementioned problem or meet the aforementioned need.

SUMMARY OF THE INVENTION

It is therefore an object of the present invention to provide an apparatus and method for calibrating voltage spike waveforms that are used to test the survivability and

compatibility characteristics of electrical equipment including military and commercial off-the-shelf electrical devices.

It is another object of the present invention that the aforesaid apparatus and method be relatively inexpensive to implement.

Other objects and advantages of the present invention will be apparent from the ensuing description.

Thus, the present invention is directed to, in one aspect, an apparatus for calibrating voltage spikes used in testing an electrical device, comprising an input for receiving a voltage spike, and power supply inputs for receiving power for energizing an electrical device under test. The power supply inputs comprise a high voltage input, a common input and a ground input. The apparatus further comprises a plurality of outputs comprising a high voltage output, a common output, and a ground output. The plurality of outputs are configured for connection to corresponding high voltage, common and ground inputs of the electrical device under test. The power supply common and ground inputs are connected to the common and ground outputs, respectively. The apparatus further comprises a circuit for connecting and disconnecting the power supply high voltage input to and from, respectively, the high voltage output, selecting a pair of the plurality of

outputs, transforming the voltage spike into a predetermined voltage spike waveform, and applying the predetermined voltage spike waveform to the selected pair of outputs.

In a related aspect, the present invention is directed to a method of testing an electrical device, which includes providing an electrical device under test having high voltage, common and ground inputs, providing a power source for energizing the electrical device under test wherein the power source has high voltage, common and ground outputs, and connecting the common and ground outputs of the power source to the common and ground inputs of the electrical device under test. The method further comprises selecting a pair of the plurality of inputs of the electrical device, connecting the power supply high voltage input to the high voltage input of the electrical device under test if the selected pair comprises the high voltage and common inputs of the electrical device, generating a voltage spike, transforming the voltage spike into a predetermined voltage spike waveform, and applying the predetermined voltage spike waveform to the selected pair of inputs of the electrical device under test.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing features of the present invention will become more readily apparent and may be understood by

referring to the following detailed description of an illustrative embodiment of the present invention, taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a block diagram showing a testing system that utilizes the apparatus of the present invention;

FIG. 2 is a schematic diagram of one embodiment of the apparatus of the present invention; and

FIG. 3 is a schematic diagram of a capacitive circuit shown in FIG. 2.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is directed to a single-phase voltage spike waveform calibrator for performing a voltage spike test on single-phase electrical devices and equipment under test.

Referring to FIG. 1, there is shown a testing system that utilizes single phase voltage spike calibrator 10 of the present invention. Calibrator 10 receives and calibrates voltage spikes that are generated and provided by voltage spike generator ("VSG") 12. The system shown in FIG. 1 effects particular tests on the electrical device or unit under test ("UUT") 14 wherein each test entails providing a predetermined voltage spike waveform into UUT 14. UUT 14 can be any type of single phase electrical device. UUT 14 includes high voltage input 16, common input

18 and ground input 20. Specifically, calibrator 10 transforms the voltage spike provided by VSG 12 into particular voltage spike waveforms that are required for complete survivability and compatibility testing of UUT 14.

Three standard tests are commonly utilized. In the first test, calibrator 10 transforms the voltage spike provided by VSG 12 into a first predetermined voltage spike waveform which is applied to the high voltage input 16 and common input 18 of UUT 14. This test is referred to as the line-to-line test. In the second test, calibrator 10 transforms the voltage spike outputted by VSG 12 into a second predetermined voltage spike waveform which is applied to the high voltage input 16 and ground input 20 of UUT 14. This test is referred to as the high-to-ground test. In the third test, calibrator 10 transforms the voltage spike provided by VSG 12 into a third predetermined voltage spike waveform which is applied to the common input 18 and ground connector 20 of UUT 14. This third test is referred to as the common-to-ground test. In each of these aforesaid tests, each of the first, second, and third predetermined voltage waveforms may have the same or different waveform characteristics, e.g. peak voltage, overshoot, rise time, fall time, etc.

Referring to FIG. 1, power supply 22 provides a supply voltage and current to the UUT 14. Power supply 22 includes

high voltage output 24, common output 26 and ground connector 28 that are inputted into attenuator 30. Attenuator 30 is connected between power supply 22 and calibrator 10 and attenuates high voltage spikes in order to prevent such spikes from being applied to power supply 22. Specifically, attenuator 30 is configured to attenuate the high frequency components of the voltage spike outputted by VSG 12. For example, attenuator 30 is configured to attenuate a voltage spike having a peak voltage of 1000 volts so as to yield a voltage spike having a peak voltage of 300 volts. Attenuator 30 includes high voltage line 32, common line 34 and ground line 36 that are connected corresponding to high voltage, common and ground inputs, respectively, calibrator 10. Attenuator 30 is well known in the art and is therefore not discussed in detail.

Calibrator 10 includes high voltage input 38, common input 40 and ground input 42 that are connected to high voltage line 32, common line 34 and ground line 36, respectively, of attenuator 30. Calibrator 10 further comprises high voltage output 44, common output 46 and ground output 47. Common input 40 is connected to common output 46. Ground input 42 is connected to ground output 47. Calibrator 10 further includes high voltage input 48 and common input 49 that are connected to the high voltage and common outputs, respectively, of VSG 12.

Referring to FIG. 2, calibrator 10 further includes switch 50 that comprises a plurality of groups 50a-h of switch contacts. Group 50a comprises switch contacts SW1-11, SW1-12, SW1-13, and SW1-14. Switch contact SW1-11 is connected to high voltage output 44 of calibrator 10. Switch contact SW1-12 is an open circuit. Switch contact SW1-13 is connected to switch contact SW1-14 and both switch contacts SW1-13 and SW1-14 are connected to one end of fuse 52. The other end of fuse 52 is connected to high voltage input 38.

Group 50b of switch contacts comprises switch contacts SW1-21, SW1-22, SW1-23 and SW1-24. Switch contact SW1-21 is connected to VSG high voltage input 48. Switch contact SW1-22 is connected to high voltage output 44. Switch contact SW1-23 is connected to switch contact SW1-24. Group 50c of switch contacts comprises switch contacts SW1-31, SW1-32, SW1-33 and SW1-34. Resistor R1 is connected between switch contact SW1-24 and switch contact SW1-31. In one embodiment, resistor R1 has a resistance of about one ohm. Switch contact SW1-32 is an open circuit. Switch contact SW1-33 is connected to high voltage output 44. Switch contact SW1-34 is connected to common output 46.

Group 50d comprises switch contacts SW1-41, SW1-42, SW1-43, and SW1-44. Switch contact SW1-41 is connected to node 60 of capacitive circuit 62. Capacitive circuit 62 is

described in detail in the ensuing description. Switch contact SW1-42 is an open circuit. Switch contact SW1-43 is connected to one end of fuse 63. The other end of fuse 63 is connected to common input 40. Switch contact SW1-44 is connected to one end of fuse 52.

Group 50e comprises switch contacts SW1-51, SW1-52, SW1-53 and SW1-54. Switch contact SW1-51 is connected to VSG common input 49 and node 64 of capacitive circuit 62. Switch contact SW1-52 is connected to one end of fuse 52. Switch contacts SW1-53 and SW1-54 are open circuits.

Group 50f comprises switch contacts SW1-81, SW1-82, SW1-83, and SW1-84. Switch contact SW1-81 is connected to node 66 of capacitor network 62. Switch contact SW1-82 is connected to switch contact SW1-43 and one end of fuse 63. Switch contacts SW1-83 and SW1-84 are connected to one end of fuse 68. The other end of fuse 68 is connected to ground input 42.

Referring to FIGS. 2 and 3, capacitive circuit 62 comprises capacitor networks 80 and 82 and switch 90. Switch 90 comprises two groups of switch contacts. The first group, group 90a, comprises switch contacts SW2-11 through SW2-18, switch contacts SW2-21 through SW2-28, and switch contacts SW2-31 through SW2-38. Switch contacts SW2-13, SW2-15, SW2-17, SW2-22, SW2-25, SW2-26, SW2-32, SW2-33, and SW2-34 are open circuits. Network 80 comprises

capacitors C1, C2, and C3. Switch 90 can be adjusted to produce a resultant capacitance between nodes 64 and 66 that is based on any one of capacitors C1, C2, and C3 by themselves or in any combination with each other. Hence, the resulting capacitance exhibited by network 80 can be any one of seven possible capacitances depending upon the setting of switch 90. The seven possible resulting capacitances are shown in Table I.

Table I: Possible Resulting Capacitances

C1
C2
C3
C1 + C2
C1 + C3
C2 + C3
C1 + C2 + C3

In Table I, the sign "+" designates summation. In one embodiment, capacitor C1 has a capacitance of 5 uf (microfarads), capacitor C2 has a capacitance of 10 uf and capacitor C3 has a capacitance of 20 uf. Thus, in such an embodiment, the possible resulting capacitance is between 5 uf and 35 uf, inclusive.

Network 82 also comprises three capacitors and a second group of switch contacts that are part of switch 90. The

aforesaid switch contacts and capacitors are connected in the same manner as capacitors C1, C2 and C3 and the switch contacts of group 90a described above. Switch 90 can be adjusted to produce a resultant capacitance between nodes 60 and 66 that is based on any one of capacitors in network by themselves or in any combination with each other. The resulting capacitance exhibited by network 82 can be any one of seven possible capacitances depending upon the setting of switch 90. In one embodiment, the capacitors in network 82 have the same capacitances as capacitors C1, C2 and C3. Thus, in such an embodiment, the possible resulting capacitance is also between 5 uf and 35 uf, inclusive.

In a preferred embodiment, switch 90 is configured so that the capacitance between nodes 60 and 66, and between nodes 64 and 66 is substantially the same at all times.

Calibrator 10 further includes monitoring circuit 92 for monitoring the voltage spike waveforms that are inputted into UUT 14. Monitoring circuit 92 is discussed in detail in the ensuing description.

In order to conduct the first test, known as the line-to-line test, UUT 14 is de-energize by inactivating power supply 22. Next, calibrator circuit 10 is connected between UUT 14 and power supply 22. In a preferred embodiment, attenuator 30 is connected between power supply 22 and calibrator 10. Next, UUT 14 is energized by activating

power supply 22 and VSG 12 is connected to calibrator 10. Next, switch 50 is adjusted to implement the line-to-line test. When switch 50 is adjusted to implement the line-to-line test, each pair of switch contacts shown in each row of Table II are electrically connected together.

Table II

SW1-11	SW1-12 (open circuit)
SW1-21	SW1-22
SW1-31	SW1-32 (open circuit)
SW1-51	SW1-52
SW1-41	SW1-42 (open circuit)
SW1-81	SW1-82

For example, switch contacts SW1-11 and SW1-12 are connected together, switch contacts SW1-51 and SW1-52 are connected together, and switch contacts SW1-81 and SW1-82 are connected together. As a result of each pair of switch contacts in each row of Table II being connected together, the VSG high voltage input 48 is connected to high voltage output 44. VSG common input 49 is connected to node 64 of capacitor network 82 and node 66 is connected to common input 40 via switch contacts SW1-81 and SW1-82. Switch contact SW1-41 is connected to SW1-42 which is connected to an open circuit. Therefore, capacitor network 82 is out of the circuit.

Next, switch 90 is adjusted to exhibit a desired resulting capacitance between nodes 64 and 66. The actual desired resulting capacitance is appropriate for conducting the line-to-line test. As a result, the resulting capacitance exhibited by capacitor network 82 transforms the voltage spike generated by VSG 12 into a particular voltage spike waveform having particular required waveform characteristics.

Next, VSG 12 is activated to output a voltage spike into high voltage and common inputs 48 and 49, respectively. Capacitor network 80 transforms the voltage spike into the desired voltage spike waveform as described in the foregoing description. Switch 50 is adjusted so that the aforementioned predetermined voltage spike waveform is applied to the high voltage output 44 and common output 46 of calibrator 10 which in turn causes the predetermined voltage spike waveform to be applied to the high voltage and common inputs 16 and 18, respectively, of UUT 14. Monitoring circuit 92 enables the actual waveform that is inputted into the UUT 14 to be monitored and evaluated to ensure that the waveform inputted into the UUT 14 is the proper waveform for the particular test being conducted. If after reviewing the waveform with monitoring circuit 92, switch 90 can be adjusted to provide a different resulting capacitance between nodes 64 and 66.

In order to conduct the high-to-ground test, switch 50 is adjusted so that each pair of switch contacts shown in each row of Table III are electrically connected together.

Table III

SW1-11	SW1-13
SW1-21	SW1-23
SW1-31	SW1-33
SW1-51	SW1-53 (open circuit)
SW1-41	SW1-43
SW1-81	SW1-83

For example, switch contact SW1-11 and SW1-13 are connected together, switch contacts SW1-51 and SW1-53 are connected together, and switch contacts SW1-81 and SW1-83 are connected together. As a result of each pair of switch contacts in each row of Table III being connected together. As a result of the pairs of switch contacts shown above being connected together, the VSG high voltage input 48 is connected to one end of resistor R1. The other end of series resistor R1 is connected to high voltage output 44 via switch contacts SW1-31 and SW1-33. The high voltage input 38 is connected directly to high voltage output 44 via switch contacts SW1-13 and SW1-11. VSG common input 49 is connected to node 64. Node 66 is connected to ground input 42 via switch contacts SW1-81 and SW1-83. The common input

40 is connected to node 60 via switch contacts SW1-41 and SW-43.

Next, switch 90 is configured to exhibit the desired resulting capacitance for capacitor networks 80 and 82 suitable for high-to-ground test. Since switch contact SW1-41 is connected to SW1-43, which is connected to common input 40, and switch contacts SW1-81 and SW1-83 are connected together, the resulting capacitance of capacitor network 82 is connected between common input 40 and ground input 42, and the resulting capacitance of capacitor network 80 is connected between VSG common input 49 and ground input 42. Next, the VSG 12 is activated to output a voltage spike into high voltage and common inputs 48 and 49, respectively. The resulting capacitances exhibited by capacitor networks 80 and 82 transform the voltage spike generated by VSG 12 into a particular voltage spike waveform having a particular waveform characteristics. The setting of switch 50 causes this particular voltage spike waveform to be applied to high voltage output 44 and ground output 47. As a result, the waveform is applied to high voltage and ground inputs 16 and input 20, respectively, of UUT 14.

Monitoring circuit 92 allows for the waveform that is inputted into the UUT 14 to be monitored and evaluated to ensure that the waveform inputted into the UUT 14 is the proper waveform for the particular test being conducted.

In order to conduct the common-to-ground test, switch 50 is adjusted so that each pair of switch contacts shown in each row of Table IV are electrically connected together.

Table IV

SW1-11	SW1-14
SW1-21	SW1-24
SW1-31	SW1-34
SW1-51	SW1-54 (open circuit)
SW1-41	SW1-44
SW1-81	SW1-84

High voltage input 38 is connected to high voltage 44, the VSG high voltage input 48 is connected to one end of resistor R1, the other end of resistor R1 is connected to common output 46 via switch contacts SW1-31 and SW1-34, and node 66 is connected to ground input 42. The high voltage input 38 is connected to high voltage output 44 via switch contacts SW1-11 and SW1-14. The high voltage input 38 is also connected to node 60 of capacitor network 60 via switch contacts SW1-41 and SW-44. Thus, the resulting capacitance of capacitor network 82 is connected between high voltage input 38 and ground input 42, and the resulting capacitance of capacitor network 80 is connected between the VSG common input 49 and ground input 42. Next, switch 90 is adjusted

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(picofarads). Test port 100 is connected to switch contact SW1-61 and test port 102 is connected to the junction of resistors R2 and R3. When switch 50 is configured to implement the line-to-line test, switch contact SW1-61 is connected to switch contact SW1-62, and switch contact SW1-71 is connected to switch contact SW1-72. In turn, switch contact SW1-62 is connected to high voltage output 44, and switch contact SW1-72 is connected to common output 46. When switch 50 is configured to implement the high-to-ground test, switch contact SW1-61 is connected to switch contact SW1-63, and switch contact SW1-71 is connected to switch contact SW1-73. In turn, switch contact SW1-63 is connected to high voltage output 44, and switch contact SW1-73 is connected to node 66. When switch 50 is configured to implement the common-to-ground test, switch contact SW1-61 is connected to switch contact SW1-64, and switch contact SW1-71 is connected to switch contact SW1-74. In turn, switch contact SW1-64 is connected to common output 46 and switch contact SW1-74 is connected to node 66.

Calibrator 10 further includes outputs 104 and 106 that are connected to one end of fuse 52 and one end of fuse 63, respectively. Outputs 104 and 106 are used for synchronization with other test equipment.

In one embodiment, each switch 50 and 90 is configured as a seven deck rotary switch. However, suitable switches can be used as well.

The present invention allows for one test set up for all required test conditions while UUT 14 is energized. The present invention also allows for the changing of test instrumentation while UUT 14 is energized. The present invention allows for variation of the phase in which the voltage spike is induced. This phase variation can be performed while UUT 14 is energized. It is not necessary to de-energize, rewire circuitry, and then re-energize UUT 14 in order to adjust the phase in which the voltage spike is induced.

The present invention provides a technique for testing the compatibility and survivability of electrical devices which is relatively more safe and efficient than prior art techniques. Furthermore, the present invention minimizes test set-up and reconfiguration time. Additionally, calibrator 10 can be realized inexpensively with commercially available electrical components.

Another important feature of the present invention is that calibrator 10 is portable and can be easily transported and integrated with the other devices and test equipment.

The principals, preferred embodiments and modes of operation of the present invention have been described in

the foregoing specification. The invention which is intended to be protected herein should not, however, be construed as limited to the particular forms disclosed, as these are to be regarded as illustrative rather than restrictive. Variations in changes may be made by those skilled in the art without departing from the spirit of the invention. Accordingly, the foregoing detailed description should be considered exemplary in nature and not limited to the scope and spirit of the invention as set forth in the attached claims.

Attorney Docket No. 83343

APPARATUS AND METHOD FOR CALIBRATING VOLTAGE SPIKE WAVEFORMS

ABSTRACT OF THE DISCLOSURE

An apparatus and method for calibrating single phase voltage spikes used in testing single phase electrical equipment. Capacitance is selected from a capacitor network in order to adjust the single phase voltage spike so as to produce a predetermined voltage spike waveform having particular waveform characteristics that are required to perform survivability and compatibility tests.

Fig. 1

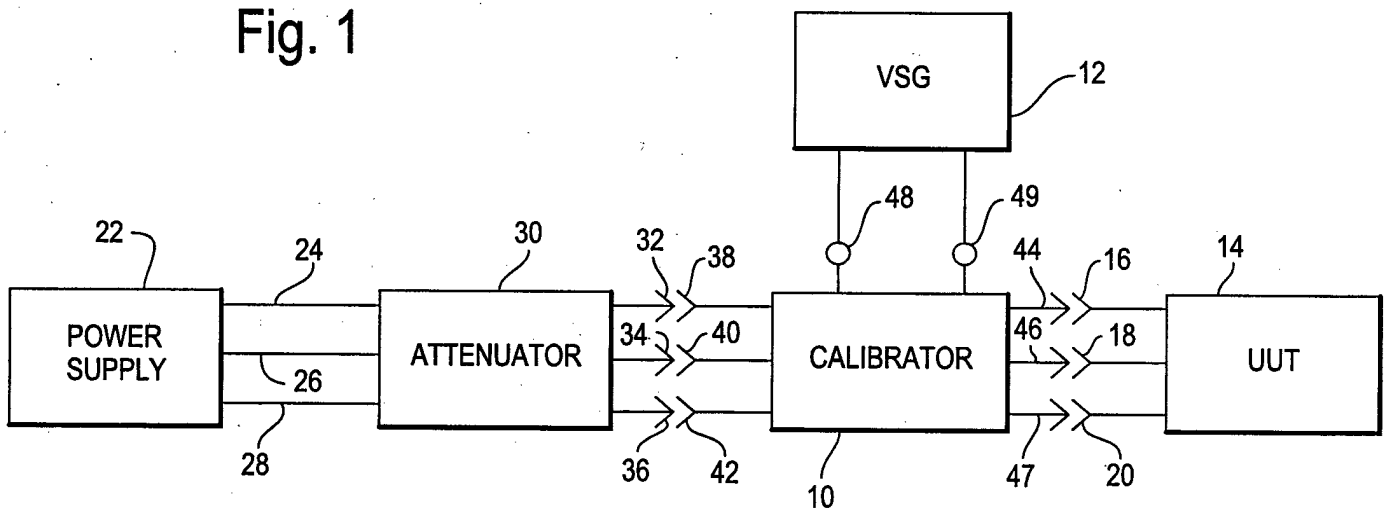
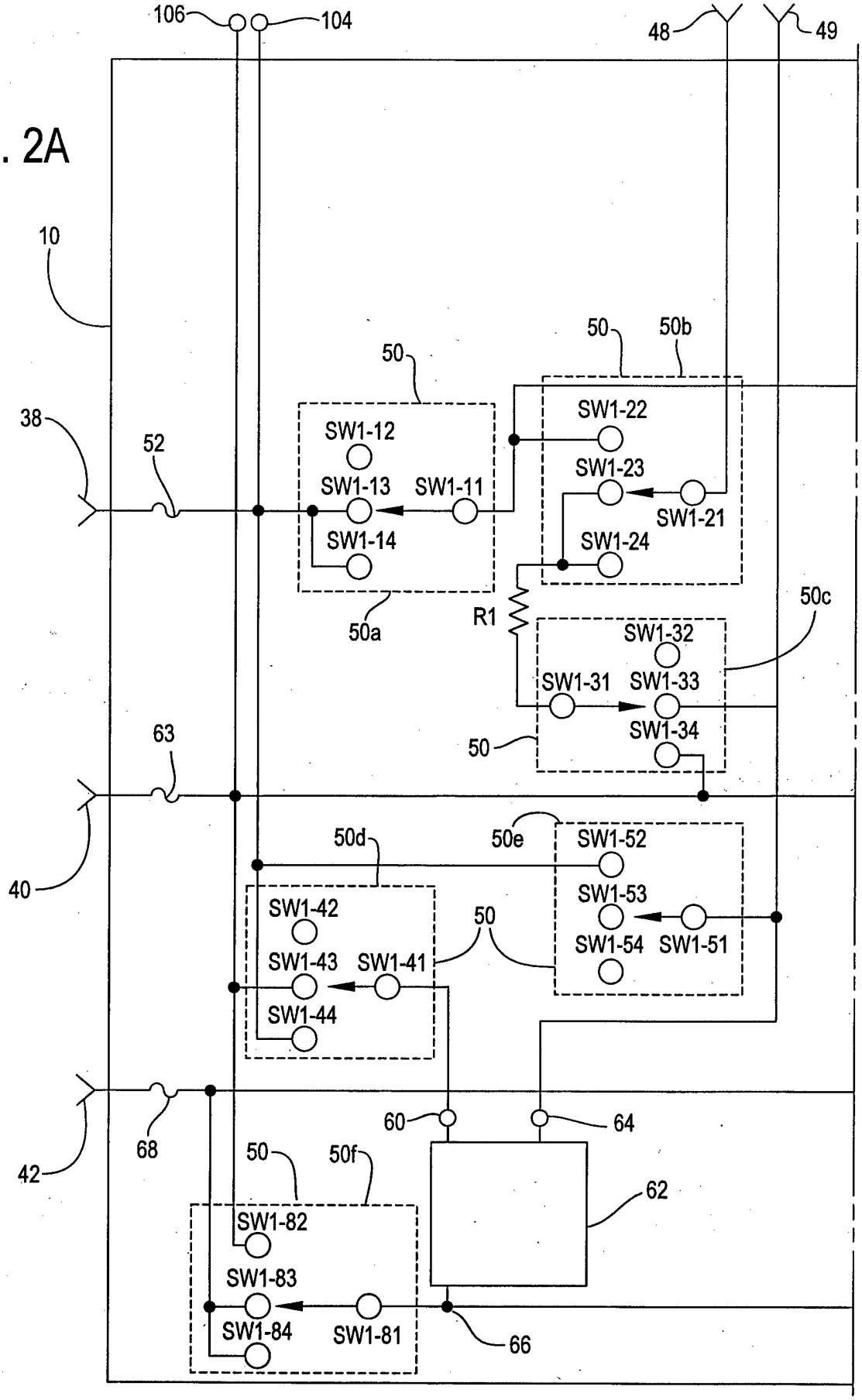

VSG
12
48
49
22
24
30
32
38
44
16
14
POWER SUPPLY
ATTENUATOR
34
40
CALIBRATOR
46
18
UUT
26
28
36
42
10
47
20

Fig. 2A


106
104
48
49
10
38
52
50
50b
SW1-22
SW1-12
SW1-23
SW1-13
SW1-11
SW1-21
SW1-14
SW1-24
50a
R1
50c
SW1-32
SW1-31
SW1-33
SW1-34
50
63
40
50d
50e
SW1-52
SW1-42
SW1-53
SW1-43
SW1-41
SW1-54
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SW1-83
SW1-84
SW1-81
66

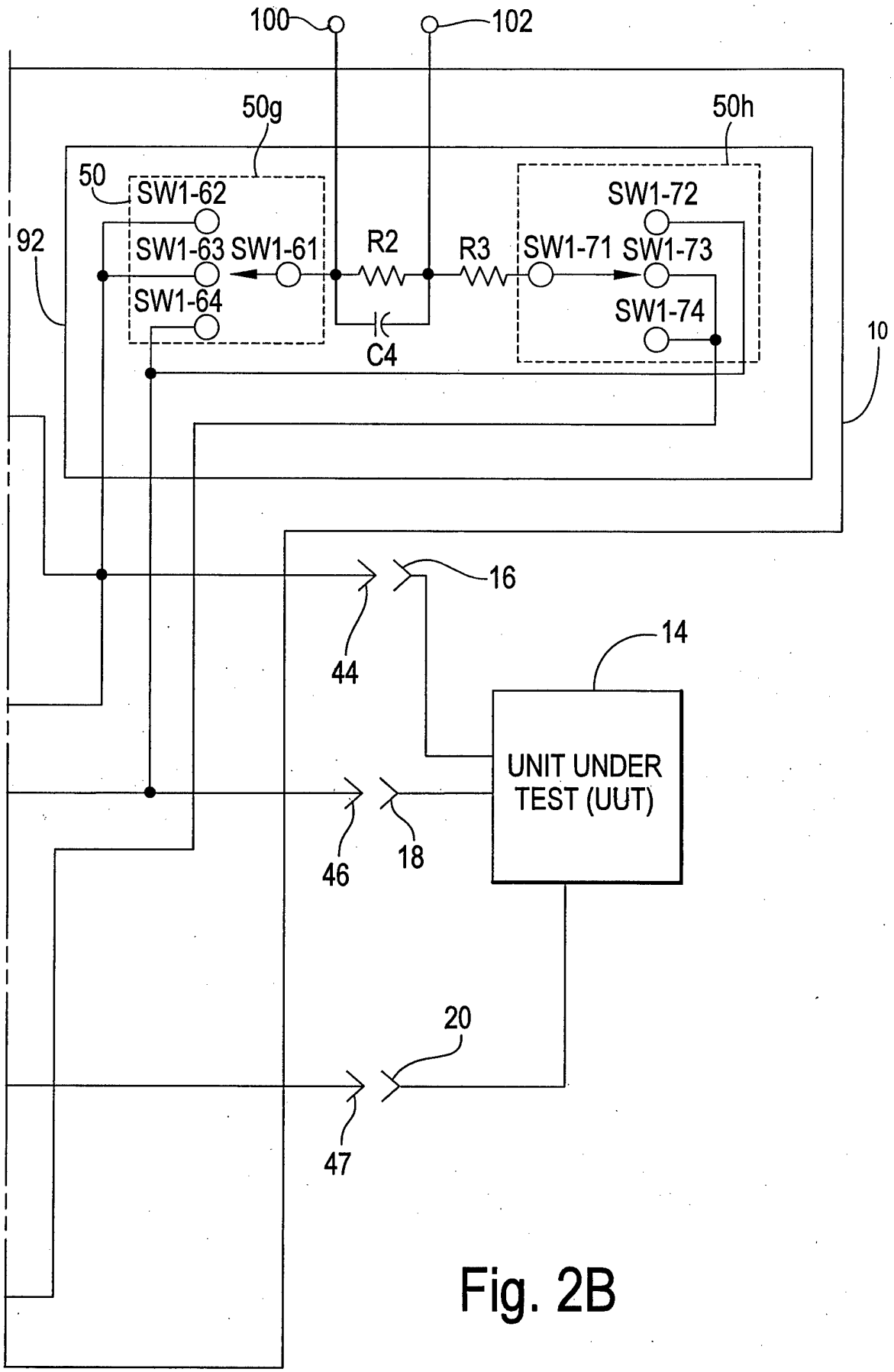
100
102
50g
50h
50
SW1-62
SW1-63
SW1-61
SW1-64
R2
R3
SW1-72
SW1-71
SW1-73
SW1-74
C4
92
10
16
44
14
UNIT UNDER TEST (UUT)
46
18
20
47

Fig. 2B

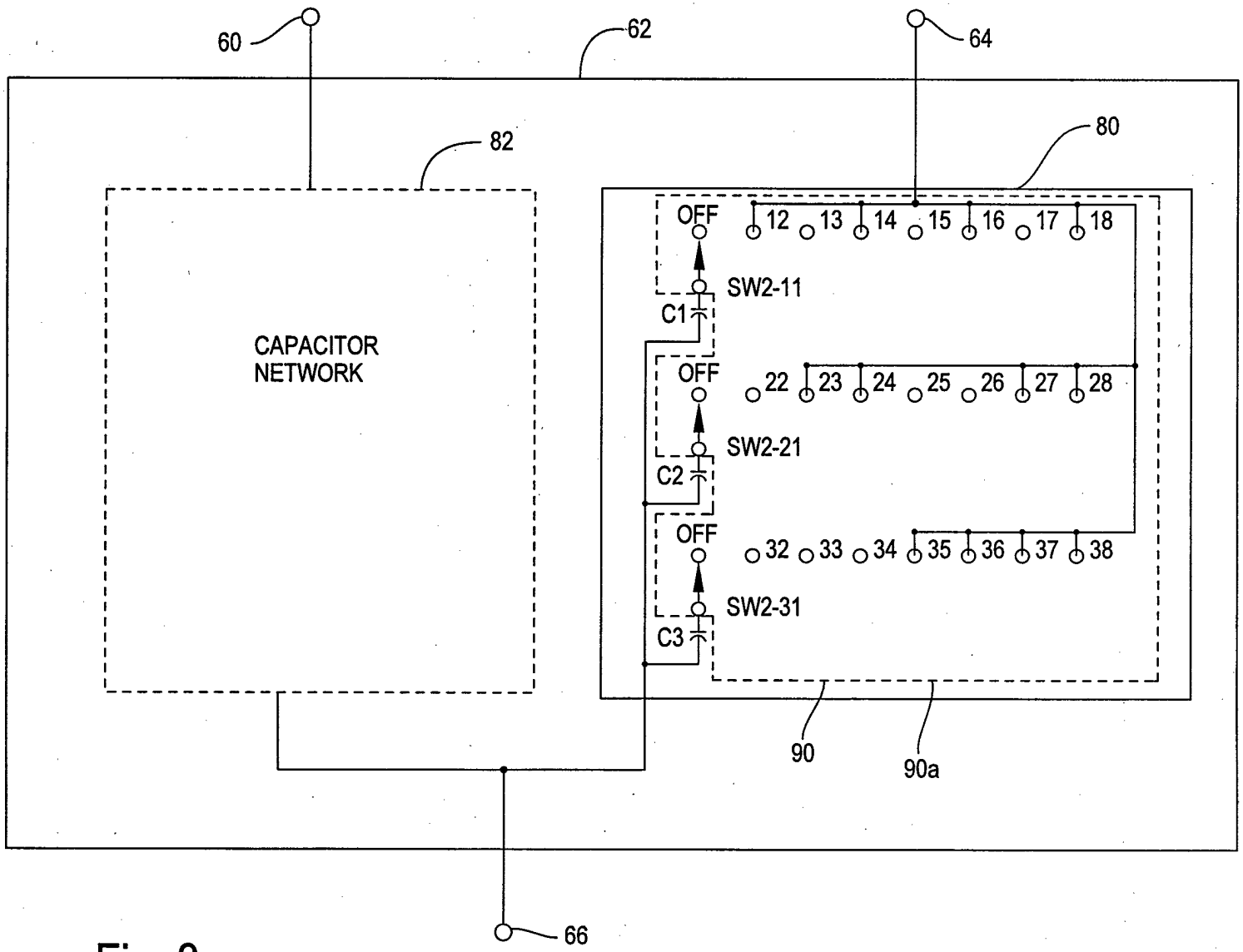
60
62
64
80
82
CAPACITOR
NETWORK
OFF
12
13
14
15
16
17
18
SW2-11
C1
OFF
22
23
24
25
26
27
28
SW2-21
C2
OFF
32
33
34
35
36
37
38
SW2-31
C3
90
90a
66

Fig. 3