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VELOCITY REDUCTION METHOD TO REDUCE THE
FLOW-INDUCED NOISE OF TOWED SENSOR SYSTEMS

STATEMENT OF GOVERNMENT INTEREST

The invention described herein may be manufactured and
used by or for the Government of the United States of America
for governmental purposes without the payment of any royalties
thereon or therefor.

BACKGROUND OF THE INVENTION

(1) Field of the Invention

This invention generally relates to a velocity reduction
method for reducing the flow-induced noise of towed sensor
systems. More particularly, the invention relates to a method
for reducing the tow velocity of a hydrophone system while
keeping the tow vessel speed constant and therefore reducing
the flow-induced noise received by the hydrophones without
affecting ship trajectory or operation. By reducing the flow-
induced noise, higher quality data can be obtained.

(2) Description of the Prior Art

Arrays of pressure sensors are used in both commercial
and military systems for the reception of sound waves in
water, air, or other fluids. The array is a multi-sensor
system which allows for the simultaneous acquisition of
signals from spatially separated locations. Commercial towed
systems use hydrophone arrays to locate oil deposits beneath
the ocean floor. Military systems use pressure sensor arrays
to locate and classify acoustic targets (e.g., a ship or
submarine in water or a tank in air). A fundamental
limitation of towed systems of pressure sensors is the flow-
induced noise. This non-acoustic noise is generated by
pressure fluctuations at the solid/fluid interface of the
structure containing the sensors. Some part of the noise is
transmitted through the structure and received by the pressure
sensors. The resulting unwanted noise is termed, "self-noise"
because it is the resulting noise of the system in the absence
of any acoustic signals. The flow-induced noise is directly
related to the speed of the array system relative to the
surrounding fluid. Turbulence scaling has shown that the
magnitude of the direct flow noise is proportional to the
velocity cubed ($U_0^3$) when a fully developed turbulent boundary
layer is present.

By reducing or eliminating the self-noise induced by the
flow of fluid relative to the pressure sensors, performance of
the pressure sensors (e.g., detection range or signal-to-noise
ratio) can be maximized. The following patents, for example,
disclose various attempts at noise control in arrays:
Specifically, Paslay et al. disclose a water borne means for making seismic surveys of underwater deposits of oil by seismic signals received by a plurality of detecting devices disposed within an elongated flexible streamer. The streamer is slightly positively buoyant when immersed in the water and is provided with a plurality of weights suspended therefrom at intervals and adapted to cause the streamer assembly to be neutrally buoyant when towed through the water at a high rate of speed by a moving vessel whereby the streamer slowly sinks through the water at the points of connection with the weights as the forward end of the streamer is momentarily brought to rest during the towing operation and the sections of the streamer intermediate the weights slowly rise within the water. An arrangement is thus provided in which only the forward end of the streamer is momentarily brought to rest, the remainder of the streamer continuing forward movement as a shot is fired and the entire length of the streamer is maintained in tension during the reception of the seismic signals whereby fortuitous noises of spurious character caused
by a release of the towing strain within the streamer and
extraneous noise signals from the lead-in connecting the
streamer and the vessel are prevented from being picked up by
the detecting devices. Accordingly, the patent to Paslay et
al. describes a system in which the array is designed to stop
and physically touch the ocean floor. The weighted streamer
is used to sink the array when its motion is minimized, thus
the array is not maintained at a constant depth.

The patent to Cryar discloses a method and apparatus for
continuous marine seismic surveying, in which a seismic
impulse source is transported along the surface of a marine
body and produces seismic impulses at intervals, the
reflections of which from the marine bottom and sub-bottom
strata are detected and recorded to produce a profile of the
subsurface conditions. Accordingly, Cryar describes the
simultaneous deployment and retrieval of two hydrophones or
groups of hydrophones (an array) such that one is "always at a
condition of minimum movement in the water." However, there
is no consideration or understanding in Cryar of the effect
that the negatively buoyant tow cable therein will have on the
system, and two separate arrays must be used.

Huckabay et al. disclose a continuous marine seismic
surveying system whose intent is to improve the signal-to-
oise ratio in continuous marine seismic surveying by
periodically stopping or slowing the motion of the towed
detector member, so that during a portion of the survey
operating cycle the hydrophone array can be dead in the water.
During this portion of the cycle, the requisite function of
transducing the returned pressure waves can take place with little or no noise interference generated in the hydrophones. The system has the capability of conducting a continuous survey of an area from a craft moving at a substantially constant speed. Although Huckabay et al. describe the basic concept of "stopping or slowing" the motion of the towed array to improve a signal-to-noise ratio, only the use of a neutrally buoyant array or "streamer" is described. Accordingly, Huckabay et al. fail to recognize or address the effect of a non-neutrally buoyant tow cable on the array shape.

Thigpen et al. disclose a marine seismic cable handler which is a hydraulically-powered yo-yo reel for handling a marine seismic cable in shallow water. At the beginning of a recording episode, a partially reeled-in seismic cable is released to drift to a standstill behind a ship. Data are recorded. The cable is then accelerated to match the ship's velocity. Following the initial acceleration, the cable is super-accelerated as it is partially reeled in. A microprocessor adjusts a dwell time between recording episodes to compensate for small variations in the ship's velocity. It is acknowledged that the patent to Thigpen et al. describes the basic concept of deploying the tow cable to decelerate the array to a standstill and mentions the need for maintaining a constant array depth; but proposes achieving these results via chains or buoys and does not describe a system using a neutrally buoyant tow cable.
Thigpen '083 discloses a seismic timing control system for optimizing the acoustic signal-to-noise ratios during a useful maximal-length recording cycle within the time frame of a minimal-length recording episode. To implement the method, during an intermittent-tow seismic operation, the noise level due to cable manipulation during an entire recording episode is monitored. A quiet-window of a desired length is established by adjusting the length of the interval during which the seismic cable is at rest. The initiation of a recording cycle is adjusted relative to the quiet window to take maximum advantage of the quiet period. Although Thigpen '083 describes the basic concept of deploying the tow cable to decelerate the array to a standstill and mentions the need for maintaining a constant array depth, these results are again obtained by provided chains or buoys to the array. Thigpen '083 does not describe a system using a neutrally buoyant tow cable.

Thigpen '245 discloses a constant tensioner for a seismic marine cable or towed seismic cable, wherein the instantaneous towing force and the instantaneous cable displacement relative to a fixed shipboard reference are continuously measured and sampled. A microprocessor associated with a servo controlled capstan device uses those measurements to pay out cable or to retrieve cable in response to an increase or decrease in the instantaneous towing force. The microprocessor also tries to minimize the average cable displacement. Accordingly, Thigpen '245 describes a system to maintain constant tow cable tension via deployment and retrieval of the tow cable. This system is
only for small displacement and not the gross motions needed to effect flow-induced noise reduction.

The patent to Savit discloses a method for maintaining a substantially constant tension on a towed seismic cable, wherein the instantaneous towing force and the instantaneous cable displacement relative to a fixed shipboard reference are continuously measured and sampled. A microprocessor associated with a servo controlled capstan device uses those measurements to pay out cable or to retrieve cable in response to an increase or decrease in the instantaneous towing force. The microprocessor also tries to minimize the average cable displacement. As with Thigpen '245, Savit is primarily describing a system to maintain constant tow cable tension via deployment and retrieval of the tow cable and is thus only for small displacement.

The patent to Bjerkoy discloses a method for conducting seismic surveys in waters covered with ice. Seismic impulses are actuated under water and reflected signals are detected by a streamer cable towed behind a vessel in order to avoid the source of noise located outside of the seismic system due to the ice-breaking operation of the vessel. The vessel is stopped during active survey and the streamer cable is hauled in with a speed corresponding to the desired propulsion speed of the cable during detection. After detection, the vessel again resumes ordinary operational speed and the streamer is paid out with a speed which maintains the desired advancing speed of the system. Bjerkoy is therefore confined to the
retrieval of an array when the tow vessel is not moving. This
method cannot be used for a continuously moving vessel.

Vali et al. disclose a reduced noise fiber optic towed
array and method of using the same wherein the fiber sensors
are connected in parallel, and the optical fiber cable is paid
out from the towing ship at a velocity about equal to but
opposite to the velocity of the towing ship. Turbulence and
acceleration noise is reduced due to the manner in which the
fiber cable is paid out, and crosstalk between sensors is
eliminated. Although Vali et al. describe the basic concept
of paying out the tow cable to reduce the array velocity to
zero, a negatively buoyant tow cable as used therein will
cause the front end of the array to sink dramatically when the
speed of the array is reduced to zero or near-zero.

SUMMARY OF THE INVENTION

Therefore it is an object of this invention to provide a
system and apparatus for reducing flow-induced noise of towed
sensor systems.

Another object of this invention is to provide a system
and apparatus for reducing flow-induced noise of towed sensor
systems in which a relative velocity is reduced between a
towed array and the surrounding water.

Still another object of this invention is to provide a
system and apparatus for reducing flow-induced noise of towed
sensor systems in which a relative velocity is reduced between
a towed array and the surrounding water by providing a
neutrally buoyant towed sensor system.
A still further object of the invention is to provide a system and apparatus for reducing flow-induced noise of towed sensor systems in which a relative velocity is reduced between the towed array and the surrounding water by providing a neutrally buoyant tow cable.

Yet another object of this invention is to provide a system and apparatus for reducing flow-induced noise of towed sensor systems which is simple to manufacture and easy to use.

In accordance with one aspect of this invention, there is provided a system for reducing flow-induced noise in an underwater towed system. The system includes at least one neutrally buoyant towed array, a tow platform for defining a towed direction of the at least one towed array, a neutrally buoyant tow cable connected to the at least one towed array and the tow platform, and a deploy and retrieve apparatus for deploying and retrieving the tow cable. The deploy and retrieve apparatus is connected to both the tow cable and the tow platform. Deployment of the tow cable from the deploy and retrieve apparatus correspondingly deploys the at least one towed array, and retrieval of the tow cable with the deploy and retrieve apparatus correspondingly retrieves the at least one towed array.

BRIEF DESCRIPTION OF THE DRAWINGS

The appended claims particularly point out and distinctly claim the subject matter of this invention. The various objects, advantages and novel features of this invention will be more fully apparent from a reading of the following
detailed description in conjunction with the accompanying
drawings in which like reference numerals refer to like parts,
and in which:

FIG. 1 is a schematic view of a proposed system according
to a first preferred embodiment of the present invention;
FIG. 2 is a schematic view of a proposed system according
to a second preferred embodiment of the present invention;
FIG. 3 is a graph illustrating an estimated change in
wall pressure spectral level with a change in tow speed
according to the present invention;
FIG. 4 is a graph illustrating a tow cable deployment
rate according to the present invention; and
FIG. 5 is a graph illustrating data acquisition time as a
function of relative tow speed.

DESCRIPTION OF THE PREFERRED EMBODIMENT

In general, the present invention is directed to a system
for reducing a tow velocity of a hydrophone system while
keeping a tow vessel speed constant and therefore reducing
flow-induced noise received by the hydrophone system without
affecting either a trajectory or operation of a ship. By
reducing the flow-induced noise received by the hydrophone
system, higher quality data can be obtained.

Referring first to FIG. 1, a schematic of a first
proposed system according to the present invention, the
structure for achieving the system is relatively simple and
includes a towed system 10 such as a hydrophone system, a tow
platform 12 which determines the direction (indicated by arrow
12a) of the towed system 10, a tow cable deploy and retrieve system 14 mounted to the tow platform 12, and a tow cable 16 operatively connected to the tow cable deploy/retrieve system 14 and the towed system 10. It should be understood that generally the environment in question is an underwater environment and that the towed system 10 illustrated herein is therefore in an underwater environment and the tow platform 12 is generally situated on the surface of the water.

The towed system 10 is described herein as a hydrophone array, however, the application is suitable to any underwater towed system which is affected by flow turbulence and the noise generated therefrom. The tow platform 12 may be a barge, ship, or any other suitable surface vessel. Further, the tow cable deploy and retrieve apparatus 14 may be a pulley member or any other similar structure that is intended to reel in and reel out a length of cable 16. It will further be appreciated that the environment may be an air environment with the tow platform 12 being an airborne vehicle, or the tow platform 12 may be a submarine rather than a surface vessel.

The primary source of unwanted noise in towed hydrophone systems 10 is the noise induced by the turbulent flow of fluid (e.g., water or air) over the structure containing the hydrophones. Although not specifically shown due to the variety of options available, the hydrophone system 10 may be in a cylindrical shell, a flat plate, or other comparable housing. By reducing a relative velocity between the hydrophone system 10 and the surrounding water, a magnitude of the fluctuating noise induced by the turbulent boundary layer
will be decreased. The turbulent boundary layer is defined as
the layer of fluid which passes over the surface of the
hydrophone system housing 10. The direct pressure flow noise
scales as a function of velocity cubed, so significant
reductions in flow noise are possible with modest decreases in
tow speed. The method allows for the reduction in a velocity
of the hydrophone array while maintaining a constant velocity
of the tow platform 12 (also referred to as the tow point,
e.g., a ship or tow body).

A fundamental way to decrease the flow-noise of a towed
system 10 is to decrease the tow speed. Because it is not
desirable to decrease the speed of the tow platform 12, the
speed of the towed system 10 must be decreased independently.

This can be accomplished by increasing a deployment length of
the tow cable 16 at a velocity corresponding to the desired
decrease in relative velocity of the towed system 10. For
example, if the tow platform 12 is traveling at a speed of 10
knots and the desired absolute speed of the towed system 10 of
hydrophones is 4 knots, then the relative velocity between the
tow platform 12 and the towed system 10 must be 6 knots. The
tow cable 16 must then be deployed at a speed of 10.1 feet per
second relative to the tow platform 12. In FIG. 1, rotation
of deploy/retrieve system 14 in the direction indicated by
arrow 14a, provides a relative motion of towed system 10 with
aspect to tow platform 12 as indicated by 10a.

Both the tow cable 16 and the towed system 10 are formed
so as to be neutrally buoyant, thereby preventing the
hydrophone system 10 from sinking as the tow cable 16 is
deployed. This feature of providing both a neutrally buoyant
tow cable 16 and neutrally buoyant towed system has not
previously been proposed in the art. Instead, it was thought
that the neutrally buoyant towed system 10 and the speed at
which the system was towed would compensate for non-neutrally
buoyant tow cables.

Further, any electrical connections to the hydrophone
system 10 may be maintained via a slip-ring conductor (not
shown) within the deploy/retrieve system 14. The data
connection could also be maintained through a slip-ring or
with a wireless short-range transmit/receive unit (not shown).

In FIG. 1, the towed system 10 is deployed from the tow
platform 12 until the available tow cable 16 length is
reached. Then, the array 10 is retrieved so that another
deployment cycle may begin. It should be understood that
multiple systems may be implemented so that one system is
always being deployed.

FIG. 2 illustrates another possible system where there
are actually two hydrophone systems 20, 30 connected in a
looped and neutrally buoyant tow cable 22. More specifically,
the tow cable 22 is looped around a remote tow cable
deploy/retrieve structure 24 and the tow cable 22 is a
continuous loop. The reeling structure 24 is intentionally
provided to be remote from the tow platform 12, the reeling
structure 24 having the tow cable 22 looped therearound. With
the reeling structure 24 being positioned remote from the tow
platform 12, a separate attachment line 26 is provided between
the tow platform 12 and the reeling structure 24. Although
not specifically shown, it is also contemplated that the reeling structure 24 may be mounted to the tow platform 12 as in the embodiment of FIG. 1. If the reeling structure 24 is in fact remote from the tow platform 12, the reeling structure 24 will be underwater during operation. While one system 20 is being deployed to reduce the absolute speed of deployment (indicated by arrow 20a) of that system and thus the self-noise, the other system 30 is being retrieved as indicated by arrow 30a. All remaining structure is similar to that shown in FIG. 1 and will not be repeated herein for the sake of brevity.

Turbulence research has shown that the pressure flow noise on the outside of a towed structure, such as a flat plate or a cylinder in axial flow, scales with the “free stream velocity” raised to the third power. In this case, the “free stream velocity” is the speed of the towed system 10 relative to the surrounding fluid. A typical scaling of the wall pressure frequency spectrum is

\[ \Phi(\omega) = F\left(\frac{\omega \delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \]  

(1)

where \( F \) is a universal function of the non-dimensional frequency \( \omega \delta^*/U_0 \). Here \( \Phi(\omega) \) is the frequency power spectrum of the pressure fluctuation of the outside of the structure containing the hydrophones, \( \rho \) is the surrounding fluid density, \( \delta^* \) is the boundary layer displacement thickness, and \( U_0 \) is the free stream velocity. The function \( F \) is relatively
constant at low values of non-dimensional frequency (e.g. \( \omega \delta^*/U_0 < 0.1 \)). Therefore, the reduction in wall pressure power spectrum can be estimated with a reduction in free stream velocity by using equation (1) and holding \( F \) constant. For example, the ratio of the power spectra from speed 1 and 2 are,

\[
\frac{\Phi_2(\omega)}{\Phi_1(\omega)} = \frac{\left[ F\left(\frac{\omega \delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \right]_{\text{speed}_2}}{\left[ F\left(\frac{\omega \delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \right]_{\text{speed}_1}} = \frac{U_0^3|_{\text{speed}_2}}{U_0^3|_{\text{speed}_1}} = \left( \frac{U_2}{U_1} \right)^3
\]

(2)

where the right part of the equation (2) holds if the boundary layer displacement thickness and the function \( F \) do not change significantly. The power spectrum change, \( R \), in decibels (dB) is then approximated as,

\[
R \approx 10 \log_{10} \left[ \left( \frac{U_2}{U_1} \right)^3 \right] = 30 \log_{10} \left( \frac{U_2}{U_1} \right).
\]

(3)

For a tow platform speed, \( U_1 \) of 15 knots, the change in wall pressure power spectrum (from the turbulent boundary layer) is shown in FIG. 3 as a function of the difference in speed between the towed system 10 and the tow platform 12, \( U_2 - U_1 \). Negative decibel values indicate a reduction while positive values indicate an increase in power spectrum level. For example, a spectral noise reduction on the order of 14 dB is possible if the towed system velocity is decreased by 10 knots from 15 knots to an absolute speed of 5 knots.
The relative velocity between the towed system 10 and the tow platform 12 dictates that the tow cable 16 length must dynamically change as a function of time. For a steady state situation, the required deployment rate of the tow cable 16 is equal to the same relative velocity of the towed system 10.

FIG. 4 shows the cable deployment rate as a function of relative velocity. The available tow cable 16 length will dictate the time available for data acquisition unless a circular system, such as that shown in FIG. 2, is used.

FIG. 5 shows the available data acquisition time for an available tow cable 16 length of 1500 feet. For example, if the towed system 10 speed is decreased by 5 knots, 3 minutes of time are available for data acquisition.

The primary advantage of the proposed systems is the reduction of flow-induced noise in a towed system via a reduction in the velocity of the towed system 10, 20, or 30 independent of the speed of the tow platform 12. These noise reductions maximize the system performance by eliminating or significantly reducing the flow-induced noise for a particular acoustic environment. This type of feature for a towed system is not known to currently exist. Even if the flow-induced noise is eliminated, any system will still be limited to some extent by other factors such as ambient and electronic noise.

By the present invention, a system is achieved in which flow-induced noise from a towed array is substantially eliminated in a more efficient manner than previously achieved in the art.
This invention has been disclosed in terms of certain embodiments. It will be apparent that many modifications can be made to the disclosed apparatus without departing from the invention. Therefore, it is the intent to cover all such variations and modifications as come within the true spirit and scope of this invention.
VELOCITY REDUCTION METHOD TO REDUCE THE
FLOW-INDUCED NOISE OF TOWED SENSOR SYSTEMS

ABSTRACT OF THE DISCLOSURE

A system and method are disclosed for reducing flow-induced noise in an underwater towed system. The system includes at least one neutrally buoyant towed array, a tow platform for defining a towed direction of the at least one towed array, a neutrally buoyant tow cable connected to the at least one towed array and the tow platform, and a deploy and retrieve apparatus for deploying and retrieving the tow cable. The deploy and retrieve apparatus is connected to both the tow cable and the tow platform. Deployment of the tow cable from the deploy and retrieve apparatus correspondingly deploys the at least one towed array, and retrieval of the tow cable with the deploy and retrieve apparatus correspondingly retrieves the at least one towed array. The speed of deployment of the tow cable can be varied to decrease the velocity of the towed array relative to the surrounding water thus reducing flow-induced noise.
FIG. 1

FIG. 2
Change in System Speed Relative to Tow Platform $U_2 - U_1$ (Knots)

**FIG. 3**

Cable Deployment Rate (Feet/Second)

**FIG. 4**
Available Cable Deployment Length -1500 Feet

Available Acquisition Time (Minutes)

Tow System Speed Relative to Tow Platform \( U_2 - U_1 \) (Knots)

FIG. 5