Coherent detection of orbital angular momentum in radio

The angular momentum propagated by a beam of radiation has two contributions: spin angular momentum (SAM) and orbital angular momentum (OAM). SAM corresponds to wave polarisation, while OAM-carrying beams are characterized by a phase which is a function of azimuth. We demonstrate experimentally that radio beams propagating OAM can be generated and coherently detected using ordinary electric dipole antennas. The results presented here could pave the way for novel radio OAM applications in technology and science, including radio communication, passive remote sensing, and new types of active (continuous or pulsed transmission).

 photon orbital angular momentum, radio phase modes, electromagnetic radiation

b. ABSTRACT

The views, opinions and/or findings contained in this report are those of the author(s) and should not contrued as an official Department of the Army position, policy or decision, unless so designated by other documentation.

14. ABSTRACT

15. SUBJECT TERMS

photon orbital angular momentum, radio phase modes, electromagnetic radiation
Coherent detection of orbital angular momentum in radio

ABSTRACT

The angular momentum propagated by a beam of radiation has two contributions: spin angular momentum (SAM) and orbital angular momentum (OAM). SAM corresponds to wave polarisation, while OAM-carrying beams are characterized by a phase which is a function of azimuth. We demonstrate experimentally that radio beams propagating OAM can be generated and coherently detected using ordinary electric dipole antennas. The results presented here could pave the way for novel radio OAM applications in technology and science, including radio communication, passive remote sensing, and new types of active (continuous or pulsed transmission) electromagnetic measurements.
Coherent detection of orbital angular momentum in radio

L. K. S. Daldorff,1 S. M. Mohammadi,2 J. E. S. Bergman,3 B. Isham,4,* M. K. T. Al-Nuaimi,5 K. Forozesh,6 and T. D. Carozzi7

1University of Michigan, 2455 Hayward Street, 4129 SRB, Ann Arbor, Michigan 48109, USA
2Department of Electrical and Computer Engineering, Interamerican University of Puerto Rico, 500 Dr. John W. Harris Road, Bayamón, Puerto Rico 00957, USA
3SIT AB, Östervgen 11, 169 53 Solna, Sweden
4Department of Electrical and Computer Engineering, Interamerican University of Puerto Rico, 500 Dr. John W. Harris Road, Bayamón, Puerto Rico 00957, USA
5Department of Electrical and Computer Engineering, University of Technology, P.O.Box 55505, 12906 Baghdad, Iraq
6Department of Electrical and Electronic Engineering, University of Technology, P.O.Box 55505, 12906 Baghdad, Iraq
7Onsala Space Observatory, SE-439 92 Onsala, Sweden
(Dated: August 31, 2014)

The angular momentum propagated by a beam of radiation has two contributions: spin angular momentum (SAM) and orbital angular momentum (OAM). SAM corresponds to wave polarisation, while OAM-carrying beams are characterized by a phase which is a function of azimuth. We demonstrate experimentally that radio beams propagating OAM can be generated and coherently detected using ordinary electric dipole antennas. The results presented here could pave the way for novel radio OAM applications in technology and science, including radio communication, passive remote sensing, and new types of active (continuous or pulsed transmission) electromagnetic measurements.

PACS numbers: 41.20.-q, 41.20.Jb, 07.57.Hm, 07.57.Kp,

As early as 1909 the wave motions associated with a revolving shaft were studied by Poynting, who suggested, by analogy, that circularly-polarised light should carry angular momentum (OAM) [2]. In 1936 Beth reported on an optical experiment [1] in which he verified Poynting’s prediction. Since then others have studied electromagnetic OAM [2? , 3], however it is only recently that electromagnetic OAM has been extensively studied and utilized, both theoretically [4? –6] and experimentally, at visible [7? , 8], millimeter and microwave [9? –12], and radio wavelengths [13? ]. OAM has also been studied in electron beams [14].

In addition to energy and linear momentum, electromagnetic waves can propagate angular momentum to infinity. The total electromagnetic angular momentum has mode numbers \( j = s + l \), where \( s \) and \( l \) are mode numbers, respectively, of the electromagnetic spin and orbital angular momentum[15]. Classically, spin angular momentum manifests itself as wave polarisation, where mode numbers \( s = \pm 1 \) correspond to right- and left-hand circularly polarised modes and \( s = 0 \) to linearly-polarised modes. Similarly, OAM-carrying beams are characterized by a phase which is a function of azimuth, and OAM mode numbers \( l \) are classically manifested by a change in phase of \( l \times 360° \) around any arbitrary circle centred on the beam axis [7, 11].

We extend the radio angular momentum technique [2, 5, 6, 9, 10, 12, 13, 16? –19] by actively generating OAM radio beams having a variety of mode numbers using a simple antenna array [5], and by using a phase-coherent technique to detect and verify the transmitted modes [19]. The results presented here demonstrate that radio beams propagating OAM can be generated [5, 6] and coherently detected [19] using ordinary electric dipole antennas. This could potentially pave the way for novel radio OAM applications in technology and science, including radio communication, radio and radar remote sensing, ionospheric radio diagnostics, and radio astronomy. Note that, using current technology, it is only at radio frequencies that coherent measurements of electromagnetic fields, i.e. measurement of both amplitude and phase, may be performed.

An antenna array of \( N \) identical sources at angular frequency \( \omega \) and equal amplitudes has the array factor

\[
\Psi = \sum_{n=1}^{N} \exp[-i(\vec{k} \cdot \vec{x}_n - \phi_n)],
\]

where \( \vec{k} \) is the wave vector, \( \vec{x}_n \) is the position, \( \phi_n \) is the phase of the \( n \)th emitter, and \( i \) represents \( \sqrt{-1} \[6, 20–22\]. When the emitters are electric dipoles with dipole moments \( \vec{d} \), the electromagnetic energy density \( u = \varepsilon_0 (|\vec{E}|^2 + c^2 |\vec{B}|^2)/2 \), where \( \vec{E} \) and \( \vec{B} \) are the electric and magnetic fields, becomes

\[
u = \frac{k^2 |\vec{k} \times \vec{d}|^2 |\Psi|^2}{\varepsilon_0 (4\pi r)^2} + O(r^{-3}),
\]

where \( \varepsilon_0 \) is the vacuum permittivity and \( r = |\vec{x}| \) is the radial distance from the centre of the array, where \( \vec{x} \) is the position vector. The total angular momentum density is defined as \( \vec{h} = \vec{x} \times \vec{g} \), where \( \vec{g} = \varepsilon_0 \text{Re}(\vec{E} \times \vec{B}^*) \) is the linear momentum density. In our case we have linearly-polarised dipoles, i.e. \( \vec{d} \times \vec{d} = 0 \) and \( s = 0 \), so that the total angular momentum \( j = l + s = l \). Hence, only the OAM contributes to the total angular momentum.
characteristic of OAM beams\[7\]. The phase factor varies the size of the array.

The fields will be from the phasing of the elements and the geometry of the array, not the individual antenna elements, so long as the elements are much smaller than the size of the array.

We have used a circular array of \( N = 6 \) elements placed in the \( xy \) plane with emitters distributed equidistantly around the perimeter of a circle of radius \( a \) as shown in fig. 1, and phased such that \( \phi_n = 2\pi ln/N \), with \( l \) an integer. The array factor becomes

\[
\Psi_l = N(-i)^l \exp(i\varphi) J_l(ka \sin \theta),
\]

where, \( \theta \) and \( \varphi \) are the spherical polar and azimuthal angles, respectively, and \( J_l \) is the Bessel function. The array factor \( \Psi_l \) contains the phasor \( \exp(i\varphi) \) which is a characteristic of OAM beams\[7\]. The phase factor varies around the beam axis and the OAM number, \( l \), corresponds to a Fourier component. Thus, by measuring the phase of a single field component, the OAM modes can be separated by a spatial Fourier transform about the \( z \) axis\[23\].

An array of \( N = 6 \) folded half-wavelength dipole antennas was constructed, as shown in the inset in fig. 1. The antennas were fed with equal amplitudes and with phase shifts of \( \delta\phi = 0^\circ, \pm 60^\circ, \) and \( \pm 120^\circ \) between consecutive elements, such that the array generated beams carrying OAM modes \( l = 0, \pm 1, \) and \( \pm 2 \), respectively. The radiation patterns of the simulated beams are shown in fig. 2. In the simulations, ordinary dipoles were used instead of folded dipoles for simplicity.

As can be seen in the phase plots in the upper panels of fig. 3, when looking up the beam towards the transmitting array (\textit{i.e.} towards the page in fig. 3), the lines of constant phase spiral out from the beam axis counterclockwise for \( l > 0 \) (right-handed) and clockwise (left-handed) for \( l < 0 \). One complete turn at constant radius around the beam axis changes the phase of the field components by \( l \times 360^\circ \). Accordingly, for the measurements presented here, the phase of \( E_y \), which is the strongest electric field component, was measured at a constant radius from the beam axis \[19\].

The measurements took place in an anechoic chamber at a frequency of 2.383 GHz (corresponding to a wavelength, \( \lambda \), of 0.126 m) and at a distance of \( z = 4.82 \) m (38.3 \( \lambda \)) from the transmitting array and hence well into the far-field region. The \( E_y \) field was measured with a half-wave dipole antenna placed at the tip of a one-meter-long rotating arm, which was mounted on a pillar.
FIG. 2. (Colour on-line) Simulated radiation patterns for the $l = 0, \pm 1, \pm 2$ radio beams. For $l \neq 0$ the beams exhibit the characteristic null along the beam axis ($\theta = 0^\circ$)[5, 6, 19, 24]. Simulations, analytical calculations, and measurements show that the $l = 0$ and $\pm 1$ beams have maxima at $\theta = 0^\circ$ and $\theta = 22^\circ$, respectively. For $l = \pm 2$, the angle of the beam varied significantly around the beam axis. This is because $l = \pm 2$ is much closer to the theoretical limit in the inequality $|l| < N/2$ for unambiguous transmission of OAM modes; the OAM beam will degrade as the limit is approached. Note also that the amplitude patterns for $l = \pm 2$ exhibit ripples. Small ripples were also present for $l = \pm 1$ but are not visible in the figure. Ripples generally appear when $|l|$ approaches the upper limit of $N/2$. The color scale and contour lines indicate power density for each beam relative to the maximum of the $l = 0$ beam; the interval between contour lines is 3.2 dB.

FIG. 3. (Colour on-line) Simulated and measured phase distributions in the OAM beam. In the upper panels the positive $z$ axis is out of the paper, in the lower panels the positive $z$ axis is oriented upwards. The upper panels show the simulated OAM beam phase distribution for the $y$ component of the electric field at the measurement plane. From left to right, the panels show the phase for $l = -2, -1, 0, 1, \text{ and } 2$, as seen looking along the beam axis toward the transmitting array, i.e. in the negative $z$ direction. The white circle indicates the position of the measurement circle. The lower panels show the measured phase of the $y$ component of the electric field. The measured phase is indicated by both colour and vertical displacement. The OAM mode is found by counting the number of branch cuts from $-180^\circ$ to $+180^\circ$, i.e. for $|l| = 0, 1, \text{ and } 2$ we have 0, 1, and 2 branch cuts, respectively. The orientation of the phase slope gives the sign of the measured OAM mode. Declining phase values when the $xy$ plane is traversed in a right-handed sense indicate a negative mode, and increasing values a positive mode. The distortions visible in the measured phase are due to increased reflection when the receiving antenna is close to the floor. The color bar at right shows phase in degrees; both the upper and lower panels use the same color scale.

mode, as can be expected from the variation of the beam maximum around the beam axis in the radiation pattern for $l = 1$ and 2 in fig. 2.

Fig. 4 shows the measured $l$ spectra, computed by means of a spatial Fourier transform about the $z$ axis (see Eq. 4 above). Only minor errors arise at the transmitting side, where the feeding network delivered a maximum phase error of $3^\circ$ and a maximum amplitude difference of 0.03 dB to the six transmitting antennas. These antennas were well-tuned and less than 2% of the power was reflected back to the transmitter. The spread in the spectrum is primarily due to the finite number of transmit antennas and the reflections in the measurement chamber. The spectra confirm that the intended OAM modes were transmitted and correctly detected.

In summary, we have generated several radio OAM modes using a circular antenna array and successfully verified these modes via measurements of a single elec-
Backscatter from OAM-modulated radar observations of rotational phenomena in the atmosphere and space. The experiment opens up new possibilities for radio communications and for radio and radar remote sensing of rotational phenomena in the atmosphere and space. Backscatter from OAM-modulated radar observations of the ionosphere can be analysed using the methods presented here to diagnose possible rotational properties of plasma processes. Artificially-induced and natural radio emissions from the ionospheric plasma [13, 25, 26] could be analyzed for possible OAM effects, lending clues to plasma processes. The large-array radio telescopes currently being designed and constructed could be used to search for signs of electromagnetic OAM arriving from astrophysical plasmas [23, 27]. Each OAM mode can act as an independent channel for transmission and reception, suggesting the possibility of increasing the information transfer rate within existing measurement and communications bands. In all applications, the reception of weak radio signals located close to an undesired strong source might be improved by orienting the central null in an OAM receiving antenna towards the undesired source. For example, radio observations of the solar corona could be performed by placing the central null in an OAM beam over the radio-bright disk of the sun.

We thank Leunart Åhlén, Walter Puccio, Sven-Erik Jansson, Farid Shiva, Thomas Oswald, Erland Cassel, Shi Cheng, and Johan Lindberg for technical support and advice. We thank Anders Rydberg and Anders Åhlén for loaning equipment and for allowing access to the new Ångström Laboratory antenna chamber, which was funded by the Knut and Alice Wallenberg Foundation. We thank the electronics lab of the Swedish Institute of Space Physics in Uppsala for granting access to their facilities, lending equipment, and for covering the electrical equipment expenses. We thank Masih Noor at the Center for Accelerator and Instrument Development for help with the CAD drawing for Figure 1 and Anders Hast and Martin Ericsson at UPPMAX for valuable help and feedback in visualizing the antenna patterns. The construction materials and personnel hours required for the experiment were privately financed by the authors. SMM thanks Interamerican University of Puerto Rico for its hospitality during part of this work. We also thank the referees for constructive and helpful comments.

* bisham@bayamon.inter.edu

[12] J. Courtial, D. A. Robertson, K. Dholakia, L. Allen, and