EXTENDING THE CAPABILITIES
OF THE NATICK TERRAIN ANALYSIS
SYSTEM

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RESEARCH, DEVELOPMENT AND ENGINEERING CENTER
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### Extending the Capabilities of the Natick Terrain Analysis System

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### Abstract

The Natick Terrain Analysis System (TAS) was developed to satisfy the need for a more scientific method of designing camouflage patterns and coloration based on actual terrain reflectance data. This report describes the three phase expansion of the TAS. Phase I extended the TAS capabilities to acquire and process reflectance data to 900 nm, and to predict the appearance of a scene through an image intensifier or with three dye, false color, infrared sensitive film. Phase II added the capability to quantify the brightness of targets in imagery recorded through an image intensifier or thermal imager, and determine a probability of detection of a target against the background. Phase III allows the user to interactively create camouflage patterns and overlay the patterns on a scene to perform a subjective analysis of its effectiveness.
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This report of the three phases of the Natick Terrain Analysis System was prepared by Arthur Gold of Decilog, Inc., Melville, NY under U.S. Army Natick RD&E Center contract DAAK60-86-C-0085, funded by Program Element 11162786, Project AH98. The work was performed during the period July 1986 to March 1990.

Project Officer at Natick was Lisa B. Hepfinger, Individual Protection Directorate.
EXTENDING THE CAPABILITIES OF THE NATICK TERRAIN ANALYSIS SYSTEM

1. Introduction.

The Natick Terrain Analysis System\textsuperscript{1-3} was designed to satisfy the need for a more scientific method of designing camouflage patterns and coloration based on actual terrain reflectance data. This report describes the three-phase expansion of the Terrain Analysis System to include reflectance data in the near-infrared, to allow for the analysis of video data obtained through an image intensifier or thermal imager, and for the interactive creation and evaluation of camouflage patterns.

The Phase I effort can be subdivided into six tasks:

a. Modify the Video Data Processing software to allow for wavelengths in the range of 720 nanometers (nm) to 900 nm.

b. Convert the 400-900 nm data to $L^*$ values using published photocathode sensitivities and nighttime illumination data.

c. Plot the reflectance curve of a single pixel representative of each clustered domain.

d. Produce varying density symbol plots of the clustered domains.

e. Model three dye, false color, infrared film.

f. Plot the clustered domains on the IA-100 printer.

The Phase II effort can be subdivided into two tasks:

a. Quantify the brightness of nighttime imagery recorded on 3/4" video cassettes from an image intensifier.

b. Quantify emitted radiation in the 8-14 micrometer spectral band taken by a thermal imaging radiometer.
The Phase III effort can be subdivided into four tasks:

a. Cluster a CIELAB\textsuperscript{1} data file and generate a data file that can be used as a background scene.

b. Interactively create camouflage patterns.

c. Overlay patterns onto background scenes.

d. Calibrate the color monitor.

Each of these tasks will be discussed in the following sections. All of the software has been implemented and tested on the existing Terrain Analysis System.

2. Phase I.

   a. Video Data Processing Software Modifications

   The EXPOSE routine creates a disk file of reflectance values for the wavelength being processed. The name that the EXPOSE routine assigns to the resultant disk file is in the format DLI:SCI\textsubscript{xxx}.yyy, where "\text{xxx}" is a three digit user assigned scene number and "\text{yyy}" is the wavelength number. The section of code that does range checking was modified to accept for the additional values between 720 and 900 nm.

   The EXPOSE routine corrects the video signal level of each pixel within the scene area being processed for any nonuniformities in the camera tube. This corrected value is then converted to reflectance by using the reflectance target calibration curve built into the module. The reflectance curves of the calibrated targets have been expanded to include 720-900 nm data.

\textsuperscript{1} 1976 International Commission on Illumination (CIE) L* a* b* (CIELAB). L* is a measure of lightness (0 = black, 100 = white); a* = a measure of redness (positive axis) or greenness (negative axis); b* = a measure of yellowness (positive axis) or blueness (negative axis).
The EX2DB routine, which combines the exposure files into a data base file, has been expanded to allow for the creation of a data base file that contains 27 wavelengths in the range of 380 to 900 nm.

b. Convert 400-900 nm Data to \( L^* \) Values

A new software module has been written that permits the user to calculate \( L^* \) coordinates for the image of a terrain scene as displayed on near-infrared viewing devices such as image converters, image intensifiers and low light level video imaging systems. The user selects the desired 400-900 nm scene data file and specifies an illuminant and the spectral response of the photocathode of the imaging device.

The \( L^* \) coordinate for each scene pixel in the display is computed in a manner analogous to the calculation of the visual tristimulus value, \( Y^4 \). Because the near-infrared viewing devices present an image that varies just in lightness, \( Y \) and its corresponding lightness value, \( L^* \), are the only values that need to be calculated. These values are calculated in the following manner.

A relative photocurrent, \( i \), emitted by the photocathode of the imaging device at each pixel location is calculated from equation (1):

\[
i = \int_{400}^{900} S(\lambda)R(\lambda)I(\lambda)\,d\lambda \text{ amps} \tag{1}
\]

where

\( \lambda \) is the radiation wavelength (micron)
\( S(\lambda) \) is the spectral response of the photocathode (amps/watt)
\( R(\lambda) \) is the pixel reflectance spectrum (from the data base file)
\( I(\lambda) \) is the scene illuminant spectrum (watts/m\(^2\)-micron)

The \( Y \) tristimulus value on the display is then assumed to be \( G_i \), where \( G \) is an arbitrary constant that represents the overall luminous gain of the imaging device. The constant cancels out in the computation of the color coordinates.
The tristimulus value $Y_n$ of the white object stimulus is then computed from equation (2):

$$Y_n = G_{i_n}$$

where:

$$i_n = \int_{400}^{900} S(\lambda)I(\lambda)d\lambda$$

This is the signal that would be generated at the photocathode by the image of a perfectly diffuse white target. (Reflectance = 1.0 at all wavelengths.)

The $L^*$ coordinate for each pixel is computed from equation (3):

$$L^* = 116 \left( \frac{Y}{Y_n} \right)^{1/3} - 16$$

These $L^*$ values can then be clustered to obtain $L^*$ domains for the displayed image using the existing clustering routines.

c. Plotting of a Single Pixel vs. Wavelength

The software module REI-EC plots the spectral reflectance curves of the pixels closest to the centroids of each domain. The user is given three choices for the scale of the reflectance axis - 1.0, 0.5 or 0.2. All reflectance curves are plotted on the same 8.5" x 11" sheet of paper.

This software has been modified to plot the additional points in the range 720 to 900 nm.

d. Varying Density Symbol Plots

A capability has been provided to produce varying density symbol plots where the density of the plotted symbol is related to the $L^*$ value of the clustered domain. The user has the option of plotting any or all of the domains on the same plot or of separating them into individual plots of each domain. These plots, as well as all others produced by the TAS software, can
be output on the Hewlett Packard Model 7550A plotter currently attached to the
TAS. The Hewlett Packard Model 7220 plotter originally attached to the TAS
could also be used with no change in software.

e. Three Dye, False Color, Infrared Film

In order to provide for a three-dimensional clustering process based on the
spectral sensitivity of three dye, false color, infrared (IR) film, a new
software routine has been written that calculates color values associated with
each dye for each pixel in the scene. The existing clustering routine, CLUSTR,
properly handles these new data.

It is desirable to have the capability to evaluate camouflage against the
countermeasure of False Color IR Film. This type of film is exemplified by
Kodak Ektachrome IR Film. The film contains three layers of emulsion, which
are sensitive to the entire visual and near-IR spectrum to about 900 nm. It is
normally exposed through a Wratten Number 12 filter, which has a sharp low
wavelength cut off at 500 nm.

Upon development, the exposed silver halide in each layer results in the
appearance of a proportionate quantity of each dye. If precisely processed in
EA-5 chemicals, the appearance of the film will be proportional to the
sensitivities.

Program FILM reads the reflectance values from the data base image. It
then calculates the amount of energy that would be incident on the film at each
20 nm interval, based on the user-specified illuminant. Using the film
sensitivity curves, the program then calculates the effective processed dye
value for each of the three dyes. (This is analogous to the CIE values.)
These three values are then stored in a file for clustering.

f. Domain Plots on the Digital Letterwriter 100

The Digital Letterwriter 100 is a dot matrix printer that is capable of
producing graphic outputs. A program has been written that displays the
clustered domains on the printer as (up to) 5 different densities of dot
patterns. This produces the effect of a grey scale representation of the
clustered domains. The user is able to specify the relative dot density associated with each plotted domain.

3. Phase II.

a. Analysis of Image Intensifier Imagery

The TAS is now capable of accepting imagery recorded on 3/4" video cassettes taken through an image intensifier. The cassettes must be placed in the video cassette recorder (VCR) and played through the FOR.A model FA-410 digital time base corrector. This is the identical setup that is used to process multispectral scene data collected with the TAS field data acquisition system. Additional software has been written that allows the user to perform the desired types of calculations on the digitized image intensifier imagery.

The user is instructed to load the cassette into the VCR and to start the playback a few seconds prior to the beginning of the frames of interest. This gives the time base corrector a few frames in which to lock on to the video synchronization signal. The imagery is displayed on the black and white monitor so that the user is able to see what frames are being input to the TAS. When the user decides that the proper frame sequence is being displayed, a command to the software causes a single frame to be digitized and displayed on the red/green/blue (RGB) monitor (in monochrome). The VCR can then be stopped, since the frame of interest is in the TAS video memory.

A digitizing tablet has been added to the TAS hardware configuration and this tablet is used to select image areas of irregular shape. The tablet sits on a desk next to the monitor and has a "pen" attached to it. Movements of this "pen" on the tablet are reflected as movements of a cursor on the image displayed on the RGB monitor. Under instructions from the software, the user outlines areas of arbitrary shape on the digitized image intensifier image representing a target and a background.
A series of statistics are provided for each of the areas outlined. These statistics include:

- Number of pixels in outlined target
- Number of pixels in outlined background
- Average video signal level (target)
- Average video signal level (background)
- Minimum video signal level (target)
- Minimum video signal level (background)
- Maximum video signal level (target)
- Maximum video signal level (background)
- Variance of video signal level (target)
- Variance of video signal level (background)
- Number of pixels in target critical dimension
- Number of pixels in height of video image
- Probability of detection

The probability of detection, \( P_D \), is a function of the signal to noise ratio (SNR) in the image\(^5\)-\(^7\). The equations used in the software for these calculations are presented in Appendix A.

The user is also given the option of determining the relative effect on \( P_D \) that changing system characteristics produces. The user is required to specify the conditions under which data were collected (CASE 1) and the proposed new conditions (CASE 2). Data sets representing these conditions are selected from user-maintained data files. The following characteristics may be specified:

- Modulation transfer function (MTF) of the imaging system
- Spectral sensitivity of the detector system
- Atmospheric transmission
- Illuminant
- Reflectance curve characteristic of target
- Reflectance curve characteristic of background
b. Analysis of Thermal Imagery

Thermal imagery is analyzed in a manner similar to image intensifier imagery, which was discussed in section 3.a. An additional capability is provided in handling the background. The user is given the option of either outlining an area representative of a background or of specifying a temperature and emissivity. In addition to the video signal level statistics presented for image intensifier imagery, statistics are provided for the calculated temperature values.

The provided statistics include:

- Number of pixels in outlined target
- Number of pixels in outlined background
- Average video signal level (target)
- Average video signal level (background)
- Minimum video signal level (target)
- Minimum video signal level (background)
- Maximum video signal level (target)
- Maximum video signal level (background)
- Variance of video signal level (target)
- Variance of video signal level (background)
- Temperature of average video signal level (target)
- Temperature of average video signal level (background)
- Temperature of minimum video signal level (target)
- Temperature of minimum video signal level (background)
- Temperature of maximum video signal level (target)
- Temperature of maximum video signal level (background)
- Temperature equivalent of video signal level variance (target)
- Temperature equivalent of video signal level variance (background)

The probability of detection, \( P_D \), is a function of the contrast (C), contrast threshold (\( C_T \)) and the signal to noise ratio (SNR)\(^{5-8}\). The equations used by the software for these calculations are presented in Appendix B.
The user is also given the option of determining the relative effect on $P_D$ that changing system characteristics produces. The user is required to specify the conditions under which data were collected (CASE 1) and the proposed new conditions (CASE 2). Data sets representing these conditions are selected from user maintained data files. The following characteristics may be specified:

- MTF of the imaging system
- Spectral sensitivity of the detector system
- Atmospheric transmission
- Minimum detectable temperature difference
- Emissivity of the target
- Emissivity of the background

4. Phase III.

The software for the Phase III effort has been developed as a separate module (DESIGN) that is fully described in the User's Manual. All of the capabilities of the Phase III software are made available to the user through a series of menus.

a. Generation of Background Scenes.

The Background Scene Generation routine (BAKEND) is used to create a background scene by clustering a .LAB file. The routine clusters the three-dimensional color coordinate data into a maximum of 250 domains. The initial clustering is based upon a histogramming process, which breaks the three-dimensional CIELAB color space into cubical areas that are tested to see if their pixel density is greater than a threshold value. Cubes that exceed the threshold are considered to be domains. This process is repeated, with the cubes getting larger on each pass, until there are no more than 250 domains. An optimization routine may then be used to remove any of the clustering imperfections that may have been introduced by the nonoptimal histogramming process.

The background processing software is based upon the clustering software developed in previous phases of this effort. In these prior efforts, it was
desirable to cluster the scene information into the best 3, 4 or 5 domains that could be used for the camouflage cloth. In this phase, in order to generate a realistic background scene, it was desirable to have as many domains as possible, within the hardware limitations of the display system. Since the hardware display system imposes a limit of 256 colors displayed simultaneously, and five colors need to be reserved for the camouflage pattern that is to be overlaid on the background and one color (white) reserved for textual information, the number of domains in the background scene can be no more than 250.

The BAKGND routine is not an interactive routine. The main system routine, DESIGN, requests information concerning the .IAB files to be clustered, as well as the names to use for the output files, and stores this information in the file BAKGND.DAT. This file is then read by the BAKGND routine, which runs in the background and creates the clustered scene file. An output report is printed when BAKGND has created the Background Scene file.

b. Camouflage Pattern Creation

The pattern creation module (PATTERN) is called from the main program (DESIGN) when requested by the user. The pattern creation software is actually a set of interactive modules that may be selected by the user through the menu structure. Each of the individual functions (modules) will be described below.

When the PATTERN routine is started by the DESIGN process, it initializes the color monitor to contain a blank drawing area below some descriptive information. The descriptive information depicts the color of each of the (up to) five "pens" that may be used to draw a pattern, an indication of the color of the current pen, and a chart showing the priority level of each of the colors.

One of the first options that would normally be selected is to specify the CIELAB values for each of the colors in the pattern to be drawn. The user enters the number of the color to be set and its CIELAB coordinates. The RGB values for the entered CIELAB coordinates are calculated and the box associated with the selected color is filled in with the calculated color.
Each of the colors that may be used to create the pattern has a priority level associated with it. This level is a user-assigned number between one and five, with each color having a unique number. The level can be thought of as determining in which order the color layers are applied. First level one is applied to the "fabric", and then level two is applied on top of it. This process continues until all of the (up to) five levels have been applied. The priority level, therefore, determines which color will be visible if two colors overlap on the pattern. Careful assignment of level numbers allows the user to draw overlapping patterns without trying to match the border areas.

Once this preliminary information is entered, the user may begin to draw the desired pattern. This is accomplished by telling the system which color is to be applied and then using the pen on the digitizing tablet to either draw an arbitrary closed shape or to draw a rectangle. As the pen is moved on the digitizing tablet, the outline of the shape is drawn on the color monitor in the selected pen color.

At any time during the pattern creation process, the user may select the menu option to fill in the outlines drawn. The software uses the priority level number to determine which color is visible in overlapping situations.

The system also provides an erase utility that can be used to erase selected rectangular regions of the drawn pattern.

When the pattern has been completed, or at any time during the drawing process, it may be saved to the disk. In order to correctly overlay the pattern onto a background scene, however, a scale for the pattern must be specified. This is done by using the pen to point to two locations on the pattern and entering the distance between these two points in the "fabric" (in centimeters). The system also provides the capability to save any portion of the drawing area by allowing the user to point to the upper left hand corner and lower right hand corner of the area to be saved.

Saved pattern files may be recalled for editing. The full complement of pattern creation routines described above is available to edit patterns.
c. Overlaying of Patterns onto Background Scenes.

Patterns created using this software may be overlaid onto clustered background scenes and displayed for evaluation. First, the name of the background scene is entered, and the scene is displayed on the monitor. The CIELAB coordinates of the (up to) 250 domains are translated to RGB values and the background scene is shown in color.

The user is then asked to point to the upper left hand and lower right hand corners of the section of the background that is to be overlaid by the pattern. The software scales the pattern (using the user-specified scale) to match the scale of the background scene (determined during data collection and stored as part of the file). The camouflage pattern is then painted onto the screen in the desired area. If the user-created pattern is not large enough to cover the selected area, the pattern is repeated in the horizontal and vertical directions as necessary.

Once the pattern is overlaid onto the background, the system allows the user to zoom the displayed image by a factor of two.

d. Monitor Calibration

As described in the above sections, background scenes and overlaid patterns are displayed in color on the monitor. The numeric color coordinates known by the software are in the CIELAB color space. The monitor needs a digital number (0-255) for each of the red, green and blue guns to display a color. Software has been provided to transform any specified L*, a* or b* coordinate into RGB values to produce a "visual match" to an object with the same L*, a*, b* coordinates. The fidelity of this conversion and subsequent display depends upon the calibration data for the color monitor.

A complete calibration procedure\textsuperscript{10} is described in the TAS Users Manual and will not be repeated here. Appendix C of this report presents a modified monitor calibration procedure. This short procedure is not as rigorous as the full calibration procedure and is useful only to display colors within a small area of CIELAB space.
5. Conclusions and Recommendations

All of the software modules for the three phases have been installed and tested. A demonstration was held at Natick using the Terrain Analysis System at the completion of each phase.

A number of limitations of the current system have become apparent as more and more requirements have been placed upon it. It is therefore recommended that the following steps be taken:

a. The number of analytical software routines that form a part of the TAS has increased dramatically over the past few contractual efforts. The slow speed of the PDP-11/23+ processor greatly hampers the user's efficiency in performing analyses. The processor should be upgraded to allow for faster and more efficient analyses.

b. The current hardware configuration has two disk drives, each of which uses removable 20 MByte cartridges. The data associated with each scene has increased dramatically as the system has been expanded into the near-IR and thermal regions. It is strongly recommended that additional disk storage be added to the system.

This document reports research undertaken at the US Army Natick Research, Development and Engineering Center and has been assigned No. NATICK.TR-90/049 in the series of reports approved for publication.
6. References


Appendix A

ANALYSIS OF IMAGE INTENSIFIER IMAGERY

Equation set
Appendix A

\[ P_D = 1 - e^{-(SNR^*-1)} \]  \hspace{1cm} \text{Ref (5)}

\[ SNR^* = SNR \times FACTF \times FACTM \]

\[ SNR = \frac{\bar{V}_T - \bar{V}_B}{\sqrt{\sigma_T^2 + \sigma_B^2}} \]  \hspace{1cm} \text{Ref (6)}

\[ \bar{V}_T = \frac{1}{N_T} \sum_{N_T} V(x, y) \]

\[ \bar{V}_B = \frac{1}{N_B} \sum_{N_B} V(x, y) \]

\[ \sigma_T^2 = \left( \frac{1}{N_T} \sum_{N_T} V^2(x, y) \right) - (\bar{V}_T)^2 \]

\[ \sigma_B^2 = \left( \frac{1}{N_B} \sum_{N_B} V^2(x, y) \right) - (\bar{V}_B)^2 \]

\[ FACTF = \frac{L_{T_2} - L_{B_2}}{L_{T_1} - L_{B_1}} \]

where:

\[ L_{I_J} = \int_{400}^{1200} S_J(\lambda) T_J(\lambda) R_{I_J}(\lambda) I_J(\lambda) d\lambda \]

and \( I = T, B \) (Target, Background)

\( J = 1, 2 \) (Case1,Case2)

\[ FACTM = \frac{MTF_2}{MTF_1} \nu \]  \hspace{1cm} \text{Ref (7)}

where:

\[ \nu = \frac{N_H}{2 \times N_{CD}} \]
The following terms were used in the previous equations:

- **PD**: Probability of Detection
- **SNR**: Signal to Noise Ratio
- **SNR***: Modified Signal to Noise Ratio
- **V(z,y)**: Digital video signal level for a pixel at coordinates (z, y)
- **VT**: Average video signal level for the outlined target
- **VB**: Average video signal level for the outlined background
- **σ_T**: Variance of the outlined target pixels
- **σ_B**: Variance of the outlined background pixels
- **FACTF**: Spectral Sensitivity and Atmospheric Factor
- **FACTM**: Modular Transfer Function (MTF) factor
- **NT**: Number of pixels in outlined target
- **NB**: Number of pixels in outlined background
- **S**: Spectral response of the detector (milli-amps/watt)
- **T**: Atmospheric Transmission (0-1)
- **R**: Reflectance (0-1)
- **I**: Illuminant (watts/cm² - micron)
- **NH**: Number of pixel heights in image
- **N_CD**: Number of pixel heights in critical dimensions of target
Appendix B
ANALYSIS OF THERMAL IMAGERY
Equation set
Appendix B

\[ P_D = 1 - e^{-(SNR^* - 1)} \]  
\[ SNR^* = |SNR * FACTH * FACTM * FACTN| \]

\[ SNR = \frac{V_T - V_B}{\sqrt{\sigma_T^2 + \sigma_B^2}} \]

\[ P = \begin{cases} 
\frac{1}{2} + \frac{1}{2} \left( 1 - e^{-4.2(x_t^* - 1)^2} \right)^{\frac{3}{2}} & \text{for } C^* \geq C_T \\
\frac{1}{2} - \frac{1}{2} \left( 1 - e^{-4.2(x_t^* - 1)^2} \right)^{\frac{3}{2}} & \text{for } C^* < C_T
\end{cases} \]

\[ C_T = 0.024 \times 10^{\Delta z} \]

\[ \Delta x = -\Delta y + \sqrt{\Delta y^2 + 0.484} \]

\[ \Delta y = \log_{10} \left( \frac{\theta}{4.22} \right) \]

\[ \theta = 3438 \left( \frac{NUMCD}{VIEWD} \right) \left( \frac{ACTWTH}{NUMHGT} \right) \]

\[ C^* = FACTM \times (FACTHC \times (C + 1) - 1) \]

\[ C = \left| \frac{V_T - V_B}{V_B} \right| \]

\[ V_T = \frac{1}{N_T} \sum_{N_T} V(x, y) \]

\[ V_B = \begin{cases} 
\frac{1}{N_B} \sum_{N_B} V(x, y) & \text{or} \\
\text{function of user specified } T_B \text{ and } \epsilon_B
\end{cases} \]
\[
\sigma_T^2 = \left( \frac{1}{N_T} \sum_{N_T} V^2(x,y) \right) - (\nabla_T)^2
\]

\[
\sigma_B^2 = \begin{cases} 
\left( \frac{1}{N_B} \sum_{N_B} V^2(x,y) \right) - (\nabla_B)^2 & \text{if outlined} \\
NEVD^2 & \text{if user specified} \\
\end{cases}
\]

\[
FACTM = \frac{MTF_2}{MTF_1} \left| \nu \right.
\]

where:

\[
\nu = \frac{NUMHGT}{2 * NUMCD}
\]

\[
FACTH = \frac{K_{T_2} - K_{B_2}}{K_{T_1} - K_{B_1}}
\]

\[
FACTHC = \frac{K_{T_2}}{K_{T_1}} * \frac{K_{B_1}}{K_{B_2}}
\]

where:

\[
K_{I_J} = \int_a^b S_J(\lambda) T_J(\lambda) L_J(\lambda) d\lambda
\]

and I=T,B (Target,Background)

J =1,2 (Case1,Case2)

a,b = \begin{cases} 
3, 5 \text{ for analysis} \\
\text{in 3-5 micron region} \\
8, 14 \text{ for analysis} \\
\text{in 8-14 micron region} \\
\end{cases}

Ref (7)
\[ L_I (\lambda) = \frac{2c^2 h \cdot \varepsilon_I}{\lambda^5 \left[ \exp \left( \frac{hc}{\lambda kT} \right) - 1 \right]} \]

where:

\[ 2c^2 h = 1.911 \times 10^{-16} \times 10^{30} = 1.911 \times 10^{14} \]

\[ \frac{hc}{k} = 0.014388 \times 10^6 \]

\[ T^\circ (\text{deg K}) = T^\circ (\text{deg C}) + 273.15 \]

\[ F ACT N = \left( \frac{\sigma_T^2 + \sigma_B^2}{\sigma_T^2 + \sigma_B^2 + 2 \times (NEVD_I^2 - NEVD_I^2)} \right)^{\frac{1}{2}} \]

Ref (8)

where:

\[ NEVD_I = \frac{MDTD}{1.7 \times \alpha} \]
The following terms were used in the previous equations:

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Definition</th>
</tr>
</thead>
<tbody>
<tr>
<td>PD</td>
<td>Probability of Detection</td>
</tr>
<tr>
<td>P</td>
<td>Detection probability of uncluttered targets and backgrounds</td>
</tr>
<tr>
<td>SNR</td>
<td>Signal to Noise Ratio</td>
</tr>
<tr>
<td>SNR*</td>
<td>Modified Signal to Noise Ratio</td>
</tr>
<tr>
<td>CT</td>
<td>Contrast Threshold</td>
</tr>
<tr>
<td>C</td>
<td>Contrast</td>
</tr>
<tr>
<td>C*</td>
<td>Modified contrast</td>
</tr>
<tr>
<td>NUMCD</td>
<td>Number of pixel heights in target critical dimension</td>
</tr>
<tr>
<td>VIEWD</td>
<td>Viewing distance to display device</td>
</tr>
<tr>
<td>ACTWTH</td>
<td>Size of display device (height)</td>
</tr>
<tr>
<td>NUMHGT</td>
<td>Number of pixel heights in image</td>
</tr>
<tr>
<td>V(x,y)</td>
<td>Digital video signal level for a pixel at coordinates (x,y)</td>
</tr>
<tr>
<td>V_T</td>
<td>Average video signal level for the outlined target</td>
</tr>
<tr>
<td>V_B</td>
<td>Average video signal level for the outlined background</td>
</tr>
<tr>
<td>\sigma_T^2</td>
<td>Variance of the outlined target pixels</td>
</tr>
<tr>
<td>\sigma_B^2</td>
<td>Variance of the outlined background pixels</td>
</tr>
<tr>
<td>FACTM</td>
<td>Modular Transfer Function (MTF) factor</td>
</tr>
<tr>
<td>FACTH</td>
<td>Spectral Sensitivity and Atmospheric Factor</td>
</tr>
<tr>
<td>FACTHC</td>
<td>Spectral Sensitivity and Atmospheric Factor (Contrast)</td>
</tr>
<tr>
<td>FACTN</td>
<td>Noise factor</td>
</tr>
<tr>
<td>\epsilon</td>
<td>Emissivity</td>
</tr>
<tr>
<td>N_T</td>
<td>Number of pixels in outlined target</td>
</tr>
<tr>
<td>N_B</td>
<td>Number of pixels in outlined background</td>
</tr>
<tr>
<td>S</td>
<td>Spectral response of the detector (milli-amps/watt)</td>
</tr>
<tr>
<td>T</td>
<td>Atmospheric Transmission (0-1)</td>
</tr>
<tr>
<td>N_H</td>
<td>Number of pixel heights in image</td>
</tr>
<tr>
<td>N_{CD}</td>
<td>Number of pixel heights in critical dimensions of target</td>
</tr>
<tr>
<td>NEVD</td>
<td>Noise Equivalent Video Difference</td>
</tr>
<tr>
<td>MDTD</td>
<td>Minimum Detectible Temperature Difference</td>
</tr>
</tbody>
</table>
Appendix C

Calibration of the DTAS Color Monitor for CIE L*a*b* Color Coordinates

(Modified Short Form Procedure)
Appendix C

This appendix describes a procedure to calibrate the DTAS color monitor. The user chooses four colors with known LAB coordinates that are representative of the colors that are to be displayed. Interactive software is used to play with the RGB values until a "good" visual match is obtained between these four displayed colors and the four known samples. Off-line mathematical procedures are then followed to calculate the monitor calibration matrix that can then be used by the software to convert an LAB value into the appropriate RGB values.

This procedure only produces "good" matches for LAB coordinates that fall within the area of the original four values. LAB coordinates that fall outside this region may produce totally false RGB values. The complete monitor calibration procedure described in the users manual will produce visual matches over a much greater area in LAB space.

STEP 1.

Select four color samples with known LAB coordinates that are representative of the colors that are to be displayed. Enter their LAB coordinates on lines 1-3 of the Linear Calibration Data Sheet (Figure 1).

STEP 2.

Using the monitor calibration software modules available through the DESIGN menu structure, select the option to display uniform boxes of a user specified RGB value. Adjust the RGB values until the displayed image is a "good" visual match to the first known LAB sample. Enter these values on lines 4-6 for color one (j=1). Repeat this process for the remaining three colors and enter the data in the appropriate columns in lines 4-6 of the data entry form.

STEP 3.

Using the equations shown below calculate $F_1$, $F_2$ and $F_3$ for all four colors (j=1 to 4).

$$ F_{1j} = \frac{a_j + L_j + 16}{500 + 116} \quad j=1,2,3,4 $$
\[
F_{2j} = \left( \frac{L^*_{j}+16}{116} \right)^3 \quad j=1,2,3,4
\]

\[
F_{3j} = \left( \frac{L^*_{j}+16 - \frac{b^*_j}{200}}{116} \right)^3 \quad j=1,2,3,4
\]

Enter these values on lines 7-9 of the data entry form.

STEP 4.

For each of the four colors \((j=1,2,3,4)\) solve the following three equations.

\[
\begin{bmatrix}
V_{ij}
\end{bmatrix}
= \begin{bmatrix}
b_{Rx} \\
b_{Gx} \\
b_{Bx} \\
D_x
\end{bmatrix} = \begin{bmatrix}
F_{i1} \\
F_{i2} \\
F_{i3} \\
F_{i4}
\end{bmatrix}
\]

Solve for \(b_{Rx}, b_{Gx}, b_{Bx}, D_x\)

\[
\begin{bmatrix}
V_{ij}
\end{bmatrix}
= \begin{bmatrix}
b_{Ry} \\
b_{Gy} \\
b_{By} \\
D_y
\end{bmatrix} = \begin{bmatrix}
F_{21} \\
F_{22} \\
F_{23} \\
F_{24}
\end{bmatrix}
\]

Solve for \(b_{Ry}, b_{Gy}, b_{By}, D_y\)

\[
\begin{bmatrix}
V_{ij}
\end{bmatrix}
= \begin{bmatrix}
b_{Rz} \\
b_{Gz} \\
b_{Bz} \\
D_z
\end{bmatrix} = \begin{bmatrix}
F_{31} \\
F_{32} \\
F_{33} \\
F_{34}
\end{bmatrix}
\]

Solve for \(b_{Rz}, b_{Gz}, b_{Bz}, D_z\)

where:

\[
V_{ij} = \begin{bmatrix}
V_{R1} & V_{G1} & V_{B1} & -1 \\
V_{R2} & V_{G2} & V_{B2} & -1 \\
V_{R3} & V_{G3} & V_{B3} & -1 \\
V_{R4} & V_{G4} & V_{B4} & -1
\end{bmatrix}
\]
STEP 5.

Now invert the $b$ matrix as shown below to yield $U$.

$$U_{ij} = \begin{bmatrix} b_{Rx} & b_{Gx} & b_{Bx} \\ b_{ Ry} & b_{ Gy} & b_{By} \\ b_{Rz} & b_{Gz} & b_{Gz} \end{bmatrix}^{-1}$$

STEP 6.

Create a disk file using the editor called MONCAL.DAT on disk 0 under UIC [1,15]. This will be a four line file that contains the following data:

- Line 1: $U(1,1)$ $U(2,1)$ $U(3,1)$
- Line 1: $U(1,2)$ $U(2,2)$ $U(3,2)$
- Line 1: $U(1,3)$ $U(2,3)$ $U(3,3)$
- Line 1: $Dx$ $Dy$ $Dz$

The format for the data is 3F10.3
LINEAR CALIBRATION DATA SHEET

<table>
<thead>
<tr>
<th></th>
<th>J=1</th>
<th>J=2</th>
<th>J=3</th>
<th>J=4</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. L*&lt;sub&gt;j&lt;/sub&gt;</td>
<td></td>
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<td>2. a*&lt;sub&gt;j&lt;/sub&gt;</td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>3. b*&lt;sub&gt;j&lt;/sub&gt;</td>
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<td></td>
<td></td>
</tr>
<tr>
<td>4. V&lt;sub&gt;Rj&lt;/sub&gt;</td>
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<tr>
<td>5. V&lt;sub&gt;Gj&lt;/sub&gt;</td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>6. V&lt;sub&gt;Bj&lt;/sub&gt;</td>
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<tr>
<td>7. F&lt;sub&gt;1j&lt;/sub&gt;</td>
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</tr>
<tr>
<td>8. F&lt;sub&gt;2j&lt;/sub&gt;</td>
<td></td>
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<td>9. F&lt;sub&gt;3j&lt;/sub&gt;</td>
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Figure 1. Data sheet for linear calibration.
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<thead>
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<td>Defense Technical Information Center</td>
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<tr>
<td>Alexandria, VA 22314</td>
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<td>Technical Library</td>
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<tr>
<td>U.S. Army Natick Research, Development and Engineering Center</td>
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<tr>
<td>Natick, MA 01760-5000</td>
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<tr>
<td>Mr. Arthur Gold</td>
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<tr>
<td>Decilog, Inc.</td>
<td></td>
</tr>
<tr>
<td>555 Broadhollow Road</td>
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<td>Melville, NY 11747</td>
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</tr>
<tr>
<td>Mr. Jerry Blimbaum</td>
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<td>Naval Coastal Systems Command</td>
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<td>Mr. Randall Williams</td>
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<td>Waterways Experiment Station</td>
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<tr>
<td>ATTN: CEMESEN-C/R. Williams</td>
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<tr>
<td>Vicksburg, MS 39180-6199</td>
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