A procedure for calculating groundwater flow lines

Charles J. Daly
**Title:** A Procedure for Calculating Groundwater Flow Lines

**Author(s):** Charles J. Daly

**Performing Organization:** U.S. Army Cold Regions Research and Engineering Laboratory, Hanover, NH 03755

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**Abstract:**

A methodology for the calculation of flow lines in steady or unsteady two-dimensional velocity fields is described. Although the principal application is intended to be determining fluid particle trajectories in groundwater flow, components of the methodology are relevant to more general problems of fluid flow. Two alternative numerical procedures form the core of the methodology. Each employs the method of characteristics to solve for the advection of fluid particles. The first uses an efficient, fourth-order Runge-Kutta, predictor-corrector algorithm based upon a constant time step. The second uses a fifth-
order Runge-Kutta algorithm incorporating an embedded fourth-order result. This latter alternative includes automatic time-step modification and guarantees a prescribed level of accuracy. Several utility routines are provided in support of the method of characteristics. There is a two-dimensional spline calculation procedure for the analytic description of flow-field parameters, steady potential, and potential gradient. Spline interpolation subroutines enable the user to incorporate function and gradient evaluations directly into computer program code. There is also a routine for calculating average linear velocity for those flow situations where Darcy's law is appropriate. A plotting routine features an option for producing flow-line map overlays to a user-supplied scale.
PREFACE

This report was written by Dr. Charles J. Daly, Hydrologist, Earth Sciences Branch, Research Division, U.S. Army Cold Regions Research and Engineering Laboratory, Hanover, New Hampshire. Funding for the final phase of this investigation was provided through DA Project 4A161102AT24, Task A, Work Unit 006, Chemistry of Freezing and Frozen Soils.

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A PROCEDURE FOR CALCULATING GROUNDWATER FLOW LINES
by
Charles J. Daly

Any continuous mathematical function of spatial coordinates \( \vec{x} \) and time \( t \) can constitute a field. Fields may be scalar, vector, or tensor, e.g. hydraulic head \( h(\vec{x},t) \), velocity \( \vec{v}(\vec{x},t) \), and stress \( \tau(\vec{x},t) \) respectively. The scalar field is the most elementary type. Components of vector and tensor fields are themselves scalar fields.

The principles of classical physics generally suffice to describe the motion of a group of individual rigid objects. For example, the velocity of the center of mass of the \( i \)th object in a group can be specified as a function of time:

\[
\vec{v}_i(t) = (v_{x_1}(t), v_{y_1}(t), v_{z_1}(t)).
\]

(1)

In considering fluid flow, however, the same principles of classical physics can not be applied to the uncountable number of molecules contained in even a small volume of fluid. Instead, the field approach is employed, and the velocity of fluid particles is specified by the velocity vector field:

\[
\vec{v}(\vec{x},t) = (v_x(\vec{x},t), v_y(\vec{x},t), v_z(\vec{x},t)),
\]

(2)

that is, a fluid particle located at point \( \vec{x}_0 \) at time \( t_0 \) has velocity \( \vec{v}(\vec{x}_0,t_0) \).

The significance of the velocity vector field can be appreciated from two perspectives. The first, called the Eulerian viewpoint, focuses attention on specific spatial locations \( \vec{x}_p \) and observes the velocity of particles moving past those locations. The velocity field is revealed by the set of observations:

\[
\vec{v}(\vec{x}_p,t) \quad \text{p = 1,2,3, \ldots}
\]

(3)
The second perspective, called the Lagrangian viewpoint, focuses on a number of specific particles moving with the flow. Over time each particle follows a trajectory, or flow line, defined by the locus of points:

$$\mathbf{x}_k(t) = (x_k(t), y_k(t), z_k(t)) \quad k = 1, 2, 3, \ldots$$

(4)

Monitoring the velocity of each moving particle would give the set of data again revealing the velocity field:

$$\mathbf{v} \left( \mathbf{x}_k(t), t \right) \quad k = 1, 2, 3, \ldots$$

(5)

The intent of this report is to describe a methodology for determining the flow lines of particles carried along as part of a moving fluid. It is natural then to adopt the Lagrangian viewpoint of the velocity field.

OVERVIEW OF MODELING

Figure 1 is a schematic of the flow-line calculation procedure as applied to the case of steady ground-water flow. The system is assumed to be governed by Darcy's law and the mass conservation principle. The main components are:

1) the spline generator and function subroutines,
2) the average linear velocity calculation subroutine,
3) the flow-line determination routines, and
4) the flow-line plotting routine.

Figure 2 illustrates the results of applying the procedure in Figure 1. The composite map, in this case a flow net, could be used to predict the trajectory of ground-water contamination and the propagation rate of a contamination front. (In practice one must also consider the importance of sorption and mechanical dispersion on the transport (Daly 1983).)

In the sections that follow, each component in the complete methodology of Figure 1 is described, documented, and then demonstrated.

SPLINE GENERATING PACKAGE

Description

Consider the two-dimensional domain, shown in Figure 3, defined by $1 \leq x \leq x_N$ and $y_1 \leq y \leq y_M$. Let $D$ denote the domain and $\partial D$ its boundary. Values of a function $f(x, y)$, whose analytic form is unknown, are given at a
Figure 1. Schematic of modeling procedure for two-dimensional steady groundwater flow.
Figure 2. Results of model application shown in Figure 1.
number of points in \( D \) and on \( \partial D \). These points are arranged so that one point is located at the intersection of every vertical \( (x = \text{constant}) \) and every horizontal line \( (y = \text{constant}) \). Each point arranged in this fashion is called a knot. (Regular placement of the knots, as in Figure 3, is not essential to the derivation of a spline interpolate. This assumption does lead, however, to the relatively simple calculation procedure described later.)

Let the approximating expression for the unknown function \( f(x,y) \) be designated by \( S(x,y) \). The particular form of \( S(x,y) \) depends on the set of functions from which it is to be constructed. A variety of so-called basis functions are available for this purpose. In cases where the smoothness of \( f(x,y) \) can be estimated, some justification can be made for the selection of particular basis functions. If \( f(x,y) \) is believed to vary smoothly, it would appear to be more advantageous to construct \( S(x,y) \) from functions exhibiting this property (Rivlin 1969, Schultz 1973).

A spline is a composite function. For domain \( D \) of Figure 3, a bicubic spline interpolate \( S(x,y) \) will be composed of \((N-1) \times (M-1)\) bicubic polynomials. (The polynomials are bicubic since they contain powers of both \( x \) and \( y \) up to order three.) Each individual polynomial is valid only in and on the boundary of a particular subrectangle of \( D \). Thus there is a one-to-one correspondence between the polynomials and the subrectangles.
Each of the constituent bicubic polynomials has the same general formula. This formula can be illustrated by writing the equation of the polynomial associated with the isolated subrectangle of Figure 4. In total, \((N-1) \times (M-1)\) of these equations must be written to define the entire spline. For the subrectangle of Figure 4, the polynomial is:

\[
s(x, y) = f(x_i, y_j)C_i(x)C_j(y) + f(x_i, y_{j+1})C_i(x)C_{j+1}(y) \\
+ f(x_{i+1}, y_j)C_{i+1}(x)C_j(y) + f(x_{i+1}, y_{j+1})C_{i+1}(x)C_{j+1}(y) \\
+ \frac{\partial f}{\partial x}(x_i, y_j)D_i(x)C_j(y) + \frac{\partial f}{\partial x}(x_{i+1}, y_j)D_i(x)C_j(y) \\
+ \frac{\partial f}{\partial y}(x_i, y_j)C_i(x)D_j(y) + \frac{\partial f}{\partial y}(x_{i+1}, y_j)C_i(x)D_j(y) \\
+ \frac{\partial^2 f}{\partial x \partial y}(x_i, y_j)D_i(x)D_j(y) + \frac{\partial^2 f}{\partial x \partial y}(x_{i+1}, y_j)D_i(x)D_j(y) \\
+ \frac{\partial^2 f}{\partial x^2}(x_i, y_j)D_i(x)D_j(y) + \frac{\partial^2 f}{\partial x^2}(x_{i+1}, y_j)D_i(x)D_j(y). \tag{6}
\]

The interpolating functions \(C_i\), \(C_{i+1}\), \(D_i\), and \(D_{i+1}\) are defined by the following generalized formulas:

\[
C_i(\theta) = \frac{(\theta - \theta_{i+1})^2}{(\Theta_i - \theta_{i+1})^2} + \frac{2(\theta - \theta_i)(\theta - \theta_{i+1})^2}{(\Theta_i)^3} \tag{7}
\]
Evaluation of the interpolating functions and their derivatives at the knots yields the important results:

\[ C_i(\theta_i) = C_{i+1}(\theta_{i+1}) = \frac{\partial D_i(\theta_i)}{\partial \theta} = \frac{\partial D_{i+1}(\theta_{i+1})}{\partial \theta} = 1 \]  
\[ C_i(\theta_i) = C_{i+1}(\theta_{i+1}) = \frac{\partial D_i(\theta_{i+1})}{\partial \theta} = \frac{\partial D_{i+1}(\theta_i)}{\partial \theta} = 0 \]  
\[ D_i(\theta_i) = D_{i+1}(\theta_{i+1}) = D_i(\theta_{i+1}) = D_{i+1}(\theta_i) = 0 \]  
\[ \frac{\partial C_i(\theta_i)}{\partial \theta} = \frac{\partial C_{i+1}(\theta_{i+1})}{\partial \theta} = \frac{\partial C_i(\theta_{i+1})}{\partial \theta} = \frac{\partial C_{i+1}(\theta_i)}{\partial \theta} = 0. \]

The last four equations can be used to show that the function \( s(x,y) \) has the following properties: the values \( s, \partial s/\partial x, \partial s/\partial y, \) and \( \partial^2 s/\partial x^2 \partial y \) are equal to the corresponding values \( f, \partial f/\partial x, \partial f/\partial y, \) and \( \partial^2 f/\partial x^2 \partial y \) at each of the knots \( (x_i,y_j), (x_i,y_{j+1}), (x_{i+1},y_j), \) and \( (x_{i+1},y_{j+1}) \).

The first four terms in each bicubic polynomial, represented by eq 6, are known since \( f(x,y) \) is given at every knot. The spline determination problem is then to estimate the remaining 12 terms in the equation of each bicubic polynomial. These unknowns are the values of \( \partial f/\partial x, \partial f/\partial y, \) and \( \partial^2 f/\partial x^2 \partial y \) at the four corners of every subrectangle. They are found by observing continuity and differentiability conditions at the knots. Since the joint edges of two adjacent subrectangles share common knots, the polynomials in each of these adjacent elements share common unknowns. This fact suggests the solution of simultaneous equations for the unknowns, and this is exactly the method used.
The algebra involved in obtaining the system of equations is quite cumbersome, although the procedure is relatively simple to explain. The procedure consists of four steps.

**Step 1**

The equation of the bicubic polynomial in each subrectangle is differentiated twice with respect to \( x \). This yields a set of equations for \( \frac{\partial^2 s(x,y)}{\partial x^2} \), one equation for each subrectangle of domain \( D \).

A continuity requirement is imposed on the determination of \( \frac{\partial^2 s}{\partial x^2} \) at each knot in \( D \). Since a given knot usually belongs to more than one subrectangle, there is in general more than one equation for the determination of \( \frac{\partial^2 s}{\partial x^2} \) at a knot. Continuity requires that all of these determinations be equal. Observing the continuity conditions along a single horizontal \( y = y_j \) yields a complete set of equations for \( \frac{\partial f}{\partial x} \) at each interior knot on that line. (The values of \( \frac{\partial f}{\partial x} \) must be given at the end points of that line.) Each horizontal line is considered in succession until \( \frac{\partial f}{\partial x} \) has been determined at every knot in \( D \).

Let subscripts \( i \) and \( j \) be used to refer to the point \( (x_i,y_j) \); for example, \( f_{i+1,j} = f(x_{i+1},y_j) \). The systems of equations solved for the values \( \frac{\partial f}{\partial x} \) along the horizontals can then be written:

\[
\frac{\Delta x_{i+1}}{\Delta x} \frac{\partial f_{i+1,j}}{\partial x} + 2(\Delta x_{i+2} + \Delta x_i) \frac{\partial f_{i+1,j}}{\partial x} + \Delta x_i \frac{\partial f_{i+2,j}}{\partial x} =
3\left[ \frac{\Delta x_{i+1}}{\Delta x_i} (f_{i+1,j} - f_{i,j}) + \frac{\Delta x_i}{\Delta x_{i+2}} (f_{i+2,j} - f_{i+1,j}) \right]
\]

where \( 1 \leq i \leq N-2, 1 \leq j \leq M, \) and \( \Delta x_i = x_{i+1} - x_i \).

**Step 2**

A procedure similar to that used in Step 1 is used to determine \( \frac{\partial f}{\partial y} \) at every knot in \( D \). First, the equation of each bicubic polynomial is differentiated twice with respect to \( y \), yielding a set of equations for \( \frac{\partial^2 s(x,y)}{\partial y^2} \). The separate determinations of \( \frac{\partial^2 s}{\partial y^2} \) at a knot must be equal. Observing this requirement along a single vertical line \( x = x_i \) gives a complete set of equations for \( \frac{\partial f}{\partial y} \) along that line.

Given the values of \( \frac{\partial f}{\partial y} \) at the end points of each vertical line enables the solution of each set of simultaneous equations; thus the values \( \frac{\partial f}{\partial y} \) at every knot are obtained. The systems of equations can be constructed from:
Step 3

The equations of the bicubic polynomials that are valid along the vertical boundaries of D are differentiated to produce equations for \( \partial^3 s(x,y)/\partial x \partial y^2 \). Along each of these vertical boundaries the value of \( \partial^3 s/\partial x \partial y^2 \) must be continuous at the knots. This results in two systems of equations, one for each boundary. When the values \( \partial^2 f/\partial x \partial y \) are given at the four corners of D, these two systems can be solved for all other values of \( \partial^2 f/\partial x \partial y \) on the vertical boundaries.

The equations are of the form:

\[
\Delta y_{j+1} \frac{\partial^2 f_{i,j+1}}{\partial x \partial y} + 2(\Delta y_{j+1} + \Delta y_j) \frac{\partial^2 f_{i,j+1}}{\partial x \partial y} + \Delta y \frac{\partial^2 f_{i,j+2}}{\partial x \partial y} =
3 \left[ \frac{\Delta y_{j+1}}{\Delta y_j} \left( \frac{\partial f_{i,j+1}}{\partial x} - \frac{\partial f_{i,j}}{\partial x} \right) + \frac{\Delta y_j}{\Delta y_{j+1}} \left( \frac{\partial f_{i,j+2}}{\partial x} - \frac{\partial f_{i,j+1}}{\partial x} \right) \right]
\]

(17)

where \( 1 \leq i \leq N \), \( 1 \leq j \leq M-2 \), and \( \Delta y_j = v_{j+1} - v_j \).

Step 4

The equations of all the bicubic polynomials are differentiated to give \( \partial^3 s(x,y)/\partial x^2 \partial y \) in each subrectangle. Continuity of \( \partial^3 s/\partial x^2 \partial y \) along each horizontal line leads to a set of simultaneous equations for \( \partial f/\partial x \partial y \) at all the interior points of each line. The necessary values \( \partial f/\partial x \partial y \) at the ends of each horizontal line were obtained in Step 3.

The equations to be solved can be written:

\[
\Delta x_{i+1} \frac{\partial^2 f_{i+1,j}}{\partial x \partial y} + 2(\Delta x_{i+1} + \Delta x_i) \frac{\partial^2 f_{i+1,j}}{\partial x \partial y} + \Delta x_i \frac{\partial^2 f_{i+2,j}}{\partial x \partial y} =
3 \left[ \frac{\Delta x_{i+1}}{\Delta x_i} \left( \frac{\partial f_{i+1,j}}{\partial y} - \frac{\partial f_{i,j}}{\partial y} \right) + \frac{\Delta x_i}{\Delta x_{i+1}} \left( \frac{\partial f_{i+2,j}}{\partial y} - \frac{\partial f_{i+1,j}}{\partial y} \right) \right]
\]

(19)

where \( 1 \leq i \leq N-2 \) and \( 1 \leq j \leq M \).

Since each part of the calculation procedure involves the solution of simultaneous tridiagonal equations, it is relatively easy to compute the
spline by Gaussian elimination. Moreover, if it is recognized that the tridiagonal matrices of Steps 1 and 4, as well as those of Steps 2 and 3, are identical, the number of Gauss elimination procedures can be cut in half. (This is equivalent to the statement that if \( A \hat{x} = \hat{b} \) and \( A \hat{y} = \hat{c} \) are to be solved for \( \hat{x} \) and \( \hat{y} \), then \( A^{-1} \) need be determined only once.)

**Documentation**

This section documents the two-dimensional spline interpolating package implemented in Fortran IV. Subroutines within the package are able to return interpolated values of a function and its first partial derivatives. The interpolating functions are defined within a domain covered by a rectangular grid in the \( x, y \) plane. Values of the function to be interpolated are known at the grid intersections on and within the boundary of the domain. Values of the first derivatives are known for grid intersections on the boundary, and values of the second derivative \( \frac{\partial^2 f}{\partial x \partial y} \) are known at the four corners of the domain.

Using the complete interpolation package is a two-step process. First, the user creates a file containing raw input data and runs the CREATE program to create a binary file containing spline data. Employing the spline data, interpolating functions may then be called from the user's own Fortran programs like any other Fortran real-valued function. The raw input data file must contain the following information in the order shown using free-formatting conventions:

\[
\begin{align*}
N, M \\
x_1, x_2, x_3 \ldots x_N \\
y_1, y_2, y_3 \ldots y_M \\
f(x_1, y_1), f(x_2, y_1), f(x_3, y_1) \ldots f(x_N, y_1) \\
\vdots \\
\vdots \\
\vdots \\
f(x_1, y_M) \ldots f(x_N, y_M) \\
\frac{\partial f}{\partial x} (x_1, y_1) \ldots \frac{\partial f}{\partial x} (x_1, y_M) \\
\frac{\partial f}{\partial x} (x_N, y_1) \ldots \frac{\partial f}{\partial x} (x_N, y_M) \\
\frac{\partial f}{\partial y} (x_1, y_1) \ldots \frac{\partial f}{\partial y} (x_N, y_1)
\end{align*}
\]
where \( N \) and \( M \) are integers denoting the number of vertical and horizontal lines in the grid. Though \( N \) and \( M \) must be integers, the other data may take any legal single-precision real value (\( N \) and \( M \) must both be \( \geq 4 \)). \( x_i \) and \( y_i \) need not be regularly spaced; the grid can be made finer in areas where greater resolution is required.

Two additional inputs, \( XYSC \) and \( FSSCALE \), allow for data scaling. The scaling parameters allow for more convenient input of raw data. Their function is most clearly explained by Table 1. If \( XYSC \) and \( FSSCALE \) are omitted, their default value is 1.0.

Execution of CREATE generates the spline data file subsequently referenced by the interpolation functions. The CREATE program is designed to operate through the intermediary of an interactive terminal. It asks for the name of the raw data file and the name of an output file in which to store the binary spline data it generates. If all goes well, CREATE will terminate with the message 'normal termination.' Minor code revisions can easily be made to alter CREATE input/output functions. The CREATE program listing is provided in the appendix.

The interpolation functions \( SPLINE \), \( DSDX \), and \( DSDY \) return the value of the spline \( S \) and its first partial derivatives. Calls to the functions may be incorporated into Fortran code, as in the following examples evaluated at \( x = X_1, y = Y_1 \):

\[
\begin{align*}
\text{HEIGHT} &= \text{SPLINE} \,(X_1,Y_1,N) \\
\text{XSLOPE} &= \text{DSDX} \,(X_1,Y_1,N) \\
\text{YSLOPE} &= \text{DSDY} \,(X_1,Y_1,N) \\
\text{GRADM} &= \text{SORT} \, (\text{DSDX} \,(X_1,Y_1,N)^2 + \text{DSDY} \,(X_1,Y_1,N)^2)
\end{align*}
\]

Each of the interpolation functions requires the spline data file that CREATE produced. Before calling any of the functions, spline data must be read into a COMMON block single call to subroutine \( \text{SPLOAD} \):

\[
\text{CALL SPLOAD } (<\text{infil})
\]

where \(<\text{infil}\>\) is the Fortran unit number assigned to the spline data file. The parameter \( n \) specifies one of up to three separate spline data file locations in COMMON, i.e. \( n \) may be chosen by the user as equal to either 1,
Table 1. Function of XYSC and FSCALE.

<table>
<thead>
<tr>
<th>Input to CREATE</th>
<th>factor</th>
<th>data in file</th>
</tr>
</thead>
<tbody>
<tr>
<td>( x )</td>
<td>XYSC</td>
<td>( x )</td>
</tr>
<tr>
<td>( y )</td>
<td>XYSC</td>
<td>( y )</td>
</tr>
<tr>
<td>( \frac{\partial f}{\partial x} )</td>
<td>FSCALE</td>
<td>( \frac{\partial f}{\partial x} )</td>
</tr>
<tr>
<td>( \frac{\partial f}{\partial y} )</td>
<td>FSCALE</td>
<td>( \frac{\partial f}{\partial y} )</td>
</tr>
<tr>
<td>( \frac{\partial^2 f}{\partial x \partial y} )</td>
<td>FSCALE</td>
<td>( \frac{\partial^2 f}{\partial x \partial y} )</td>
</tr>
</tbody>
</table>

2, or 3. Thus, the same program code can call upon up to three spline functions.

SPLOAD, SPLINE, DSDX, and DSDY are listed in Appendix A, and a sample, called PROGRAM, demonstrates the use of these routines.

AVERAGE LINEAR VELOCITY ROUTINE

Description

The velocity field is an essential input to the calculation of fluid particle trajectory. For so-called laminar flow in porous media, this information is supplied by the average linear velocity, that is, an average velocity of the particles being carried along through the pores:

\[
\vec{v}^* = -\frac{K}{\phi} \nabla h
\] (20)

where \( K \) is the medium hydraulic conductivity, \( \phi \) is the effective porosity, and \( \nabla h \) is the gradient of hydraulic head \( h \).

Equation 20 presents a somewhat idealized view of fluid flow in porous media. The actual speed of particles moving through the void spaces ranges from near zero at the grain boundaries to many times the magnitude of \( \vec{v}^* \) in the larger spaces between grains. This phenomenon accounts for some of the observed smearing of sharp solute fronts in porous media flows. It appears, however, that the effect is less consequential given only the approximate descriptions of the hydraulic head, hydraulic conductivity, and effective porosity fields that are normally available.
Fortran program FG is written to supply the Cartesian components of a two-dimensional velocity field according to eq 20. Used in conjunction with a program called MAIN, FG requires spline data files for h (n=1), k (n=2), and \( \varphi \) (n=3). Listings of programs MAIN and FG are included in Appendix A.

FLOW-LINE DETERMINATION ROUTINES

Description

The equation of continuity for two-dimensional flow is:

\[
\frac{\partial}{\partial x} (\rho v_x) + \frac{\partial}{\partial y} (\rho v_y) + \frac{\partial \rho}{\partial t} = 0
\]

(21)

where \( \rho \) is fluid density and \( t \) is time. Using the characteristics approach and assuming constant density, eq 21 becomes the linked system of ordinary differential equations:

\[
\begin{align*}
v_x &= \frac{dx}{dt} \\
v_y &= \frac{dy}{dt} \\
\frac{d\rho}{dt} &= -\rho \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right)
\end{align*}
\]

(22)

The first two equations define a flow line, while the last simply states the assumption that fluid density is constant along a flow line. The problem of determining the flow line becomes one of solving the joint equations

\[
f(x,y,t) = \frac{dx}{dt} = v_x \quad \frac{dy}{dt} = v_y = g(x,y,t)
\]

(23)

for \( x(t) \) and \( y(t) \).

Two alternative methods for solving eq 23 are proposed.

Method 1

A fourth-order Runge-Kutta technique is used to start the procedure, which is continued by a more efficient predictor-corrector scheme. The numerical solution method starts at point \( (x_0, y_0) \) at time zero. Using a time step \( \Delta t \), successive points \( (x_n, y_n) \) along the trajectory of the particle, which began at point \( (x_0, y_0) \), are obtained. The Runge-Kutta algorithm for accomplishing this is
\[ x_{n+1} = x_n + \frac{1}{6} (a_1 + 2a_2 + 2a_3 + a_4) \] (24)

\[ y_{n+1} = y_n + \frac{1}{6} (b_1 + 2b_2 + 2b_3 + b_4) \] (25)

where:

\[ a_1 = \Delta t f(x_n, y_n, t_n) \] (26)

\[ b_1 = \Delta t g(x_n, y_n, t_n) \] (27)

\[ a_2 = \Delta t f(x_n + \frac{a_1}{2}, y_n + \frac{b_1}{2}, t_n + \frac{\Delta t}{2}) \] (28)

\[ b_2 = \Delta t g(x_n + \frac{a_1}{2}, y_n + \frac{b_1}{2}, t_n + \frac{\Delta t}{2}) \] (29)

\[ a_3 = \Delta t f(x_n + \frac{a_2}{2}, y_n + \frac{b_2}{2}, t_n + \frac{\Delta t}{2}) \] (30)

\[ b_3 = \Delta t g(x_n + \frac{a_2}{2}, y_n + \frac{b_2}{2}, t_n + \frac{\Delta t}{2}) \] (31)

\[ a_4 = \Delta t f(x_n + a_3, y_n + b_3, t_n + \Delta t) \] (32)

\[ b_4 = \Delta t g(x_n + a_3, y_n + b_3, t_n + \Delta t) \] (33)

and \( f \) and \( g \) are defined in eq 23.

Runge-Kutta algorithms belong to the set of self-starting numerical solution methods. Self-starting means that the determination of all successive points \((x_n, y_n)\) requires only the starting point \((x_0, y_0)\). In other words, calculation of \( x_n \) and \( y_n \) depends only on the known values \( x_{n-1} \) and \( y_{n-1} \). The set of nonself-starting methods requires the values \((x_n, y_n)\) to be given at more than one point along the trajectory. For example, a fourth-order predictor-corrector algorithm, called Milne's method, requires the values \( x_0, x_1, x_2, x_3, y_0, y_1, y_2, \) and \( y_3 \) to calculate successive values of \( x_n \) and \( y_n \).

In addition to the question of starting values, the efficiency of the calculation procedure is an important factor in selecting a numerical method. It turns out that Milne's algorithm is significantly more efficient than the Runge-Kutta method, although both are fourth-order accurate. Method 1 takes advantage of the Runge-Kutta self-starting feature and the efficiency of Milne's method. Given a starting point \((x_0, y_0)\), the Runge-Kutta procedure is used to obtain \((x_1, y_1)\), \((x_2, y_2)\), and \((x_3, y_3)\). At that stage the necessary starting values are available for Milne's method, which is then used to generate succeeding points.
Milne's predictor-corrector method consists of two steps. First, predicted estimates of $x_{n+1}$ and $y_{n+1}$ are calculated. Let these be denoted $x^*_{n+1}$ and $y^*_{n+1}$. Second, the predicted values are corrected to obtain the final values $x_{n+1}$ and $y_{n+1}$ at the end of a time step. The algorithm is

\[
x^*_{n+1} = x_{n-3} + \frac{4\Delta t}{3} \left[ 2x'_{n} - x'_{n-1} + 2x'_{n-2} \right]
\]

\[
y^*_{n+1} = y_{n-3} + \frac{4\Delta t}{3} \left[ 2y'_{n} - y'_{n-1} + 2y'_{n-2} \right].
\]

Then

\[
x_{n+1} = x_{n-1} + \frac{\Delta t}{3} \left[ x^*_{n+1} + 4x'_{n} + x'_{n-1} \right]
\]

\[
y_{n+1} = y_{n-1} + \frac{\Delta t}{3} \left[ y^*_{n+1} + 4y'_{n} + y'_{n-1} \right]
\]

where:

\[
x'_{n} = f(x_{n}, y_{n}, t_{n})
\]

\[
y'_{n} = g(x_{n}, y_{n}, t_{n}).
\]

Consideration of the Runge-Kutta and Milne algorithms shows that Milne's method requires only two evaluations of $f$ and $g$ per time step, whereas Runge-Kutta requires four. This makes Milne's method more efficient.

Nonself-starting methods typically assume constant $\Delta t$, whereas self-starting methods allow for change of $\Delta t$ at each time step. For problems in which the frequent change of $\Delta t$ is desirable, exclusive use of a self-starting method, such as a Runge-Kutta algorithm, is advised.

**Method 2**

The algorithms of Method 1 do not permit the stepwise estimation of accuracy, nor do they allow for time-step modification in response to algorithm performance. Method 2, however, incorporates both of these features.

Consider the following Runge-Kutta algorithm from Sarafyan (1966):

\[
x^{(4)}_{n+1} = x_{n} + \frac{1}{6} (a_{1} + 4a_{3} + a_{4})
\]
\[ x^{(6)}_{n+1} = x_n + \frac{1}{336} \left( 14a_1 + 35a_4 + 162a_5 + 125a_6 \right) \]  
(41)

\[ y^{(4)}_{n+1} = y_n + \frac{1}{6} \left( b_1 + 4b_3 + b_4 \right) \]  
(42)

\[ y^{(6)}_{n+1} = y_n + \frac{1}{336} \left( 14b_1 + 35b_4 + 162b_5 + 125b_6 \right) \]  
(43)

\[ a_1 = \Delta t f(x_n, y_n, t_n) \]  
(44)

\[ b_1 = \Delta t g(x_n, y_n, t_n) \]  
(45)

\[ a_2 = \Delta t f(x_n + a_1/2, y_n + b_1/2, t_n + \Delta t/2) \]  
(46)

\[ b_2 = \Delta t g(x_n + a_1/2, y_n + b_1/2, t_n + \Delta t/2) \]  
(47)

\[ a_3 = \Delta t f(x_n + a_1/4 + a_2/4, y_n + b_1/4 + b_2/4, t_n + \Delta t/2) \]  
(48)

\[ b_3 = \Delta t g(x_n + a_1/4 + a_2/4, y_n + b_1/4 + b_2/4, t_n + \Delta t/2) \]  
(49)

\[ a_4 = \Delta t f(x_n - a_2 + 2a_3, y_n - b_2 + 2b_3, t_n + \Delta t) \]  
(50)

\[ b_4 = \Delta t g(x_n - a_2 + 2a_3, y_n - b_2 + 2b_3, t_n + \Delta t) \]  
(51)

\[ a_5 = \Delta t f(x_n + 7a_1/27 + 10a_2/27 + a_4/27, \]
\[ y_n + 7b_1/27 + 10b_2/27 + b_4/27, t_n + 2 \Delta t/3) \]  
(52)

\[ b_5 = \Delta t g(x_n + 7a_1/27 + 10a_2/27 + a_4/27, \]
\[ y_n + 7b_1/27 + 10b_2/27 + b_4/27, t_n + 2 \Delta t/3) \]  
(53)

\[ \xi = x_n + \frac{1}{625} \left( 28a_1 - 125a_2 + 546a_3 + 54a_4 - 378a_6 \right) \]  
(54)

\[ \eta = y_n + \frac{1}{625} \left( 28b_1 - 125b_2 + 546b_3 + 54b_4 - 378b_5 \right) \]  
(55)

\[ a_6 = \Delta t f(\xi, \eta, t_n + \Delta t/5) \]  
(56)

\[ b_6 = \Delta t g(\xi, \eta, t_n + \Delta t/5). \]  
(57)

As eqs 40 through 43 indicate, the Sarafyan algorithm is an embedded Runge-Kutta scheme, that is, the same information used to calculate the fifth-order result \( x_{n+1}^{(6)} \) can be used to calculate an embedded fourth-order result \( x_{n+1}^{(4)} \) with essentially no extra effort. When, after a given time
step $\Delta t$, $x_{n+1}^{(6)}$ and $x_{n+1}^{(4)}$ agree to $m$ significant digits, $x_{n+1}^{(6)}$ must be accurate to that number of digits. This feature of the embedded algorithm is used to increase or decrease the time step so as to balance efficiency and accuracy.

Cartesian coordinates $(x,y)$ along a flow line are calculated at points in time separated by time steps. The degree of detail desired for plotting a flow line will determine a selected maximum time step $\Delta T$, chosen independently of accuracy considerations. For each interval $(t, t + \Delta T)$, Method 2 automatically determines a constant $\Delta t$ that will guarantee that every successive result within the interval is accurate to a specified number of significant digits $m$. The rule for dividing the interval $(t, t + \Delta T)$ requires that

$$
\Delta T = 2^k \Delta t \quad (58)
$$

where $k$ may equal 0, 1, 2, 3, or 4. When accuracy consistently exceeds $m+1$ significant digits throughout a time interval $\Delta T$, the time step $\Delta t$ is doubled (but never exceeds $\Delta T$).

Documentation

The approaches of both Methods 1 and 2 are implemented in the form of the Fortran subroutines listed in Appendix A. The two subroutines are fully interchangeable, and operate in conjunction with the MAIN and FG programs.

MAIN serves to supply either method with necessary inputs. Execution of MAIN asks the user to give the file names of spline data files for $h$, $K$, and $\psi$, as previously described. It then asks for an input file name containing data on time-step size, scale, flow region boundaries, and origins for the flow lines to be calculated. Finally, MAIN asks for a file name in which to output the computed points along the flow lines. The input file has the following free-format structure:

\[
\begin{align*}
\Delta t & \quad \text{(or } \Delta T \text{ for Method 2); time step} \\
XYSC; & \quad \text{scaling factor for } x \text{ and } y \text{ data} \\
x_1, x_n, y_1, y_m; & \quad \text{flow boundaries} \\
x_0, y_0; & \quad \text{origin of flow line } 1 \\
& \quad \text{...} \\
& \quad \text{...} \\
& \quad \text{...} \\
x_0, y_0; & \quad \text{origin of flow line } 2 \\
\end{align*}
\]
The scale factor multiplies all $x_0, y_0$ data and flow boundary data in the file. The MAIN program is designed to continue reading origins until it encounters an end-of-file. Calls from MAIN to either Method 1 or 2 subroutines include passing $x_0, y_0$ and $\Delta t$ ($\Delta T$). Either subroutine outputs flow-line point data to the specified file at intervals $\Delta t$ ($\Delta T$). Calls to subroutine FG originate from Method 1 or 2 routines.

FLOW-LINE PLOTTING

Description

A plotting routine, listed in Appendix A, can be used to display output from the method of characteristics solvers. Plot scale is set by the user at the time of plot execution. This scaling feature, used with transparent drawing films or tracing papers, enables the user to produce flow-line overlays at the scale of an appropriate base map (see Fig. 2).

Documentation

Program SPLIT is designed to be executed interactively. The user must provide the name of a file that contains output from either method of characteristics and a plot scale.

Coordinate data stored in the flow-line file are given at the actual base map scale, i.e. multiplied by scaling factor XYSC (see Documentation, above). That data may be in feet, meters, miles, etc. The scale factor for plotting (SCALE) has the interpretation:

1 inch of plotting paper = (SCALE) units of the base map

If coordinate data are expressed in feet, then SCALE = 2000 gives a plot for which 1 in. of paper equals 2000 ft.

Symbols are drawn showing the location of a fluid particle at time intervals whose duration is printed on the plot. The user can choose to have symbols drawn at every Nth point of the flow line by specifying N; all points are plotted, but only every Nth is given a symbol.

APPLICATION

The flow line calculation and plotting package is demonstrated by considering a potential groundwater contamination problem at the hypothetical site shown in Figure 5.
Figure 5. Base map for demonstration site.

Figure 6 is a contour map of steady water-table elevations (in feet above MSL) in the study area. A water-table contour map may be constructed by interpreting static water levels at a number of wells, by observing topographic and stream elevation data, and by considering the drainage behavior of the study region. The persistence of runoff after rainfall events is an indicator of the depth to the water table in the vicinity of streams; sustained baseflows generally indicate a high water table.

Often it can be assumed that although water table elevations may gradually change, the hydraulic gradient remains fairly constant (steady state or quasi-steady state). This may be a valid assumption over considerable lengths of time, up to many decades.
Figure 6. Water table contours in ft above MSL.

For the purpose of demonstration, hydraulic conductivity was chosen to vary over the study area from 30 ft/day in the south to 50 ft/day in the north. Effective porosity was selected as 0.1 throughout the study area. In actual practice, field surveys should be conducted to define clearly the spatial variability of these quantities.

Raw data files for head, conductivity, and effective porosity were prepared. In the case of hydraulic head, data were specified on a uniform grid $\Delta x = \Delta y = 2000$ ft. Far less detailed grids were required to describe $K$ and $\theta$. The three raw data files were analyzed by CREATE to generate spline data files.
Flow lines were calculated using Method 1, $\Delta t = 365.25$ days, and Method 2, $\Delta t = 2922$ days. Occasionally, Method 2 required shorter time steps of 1461 and 730.5 days to maintain accuracy to three significant digits. Outputs of both methods were in very close agreement, comparing the values of $x$ and $y$ coordinates at time steps of 2922 days (the interval between outputs using Method 2). The results of Method 2 are plotted in Figure 7. Boxes around the data points locate fluid particles along stream lines at time intervals of 2922 days. An overlay of Figure 7 on the base map can be used to trace contaminant transport in the study area; the composite map is shown as Figure 8.
SUMMARY

A set of Fortran computer programs for the calculation of flow lines in two-dimensional velocity fields has been described, documented, and demonstrated. The approach has been shown to have useful application to the prediction of contaminant transport in groundwater flow systems.

LITERATURE CITED


This routine reads a file of raw data, analyses it, and generates an output file of spline data.

```
COMMON /SFL/ F(5, 50), /* f(x,y) 
1 DPDX(X(50, 50)), /* df/dx (x,y) 
1 DPDY(Y(50, 50)), /* df/dy (x,y) 
1 X(50), /* x grid values 
1 Y(50), /* y grid values 
1 DELX(50), /* delta x along grid 
1 DELY(50), /* delta y along grid

INTEGER*2 INFILE /* logical unit # of input file 
INTEGER*2 OUTFILE /* logical unit # of output file
PARAMETER INFILE = 5 /* only file unit we open 
PARAMETER OUTFILE = 5

MNEMONIC CODES FOR CRREL FILE CALLS 
INTEGER*2 JIREAD, JSWRIT, JSRDWR, JSCL0S, JSFRWD, JSRWND

PARAMETER 
1 JIREAD = 1, /* READ 
1 JSWRIT = 2, /* WRITE 
1 JSRDWR = 3, /* READ AND WRITE 
1 JSCL0S = 4, /* CLOSE FILE 
1 JSDELE = 5, /* DELETE FILE 
1 JSFRWD = 6, /* MOVE FORWARD ONE FILE (MAG TAPE) 
1 JSRWND = 7, /* REWIND

OPEN input file 
GET filename from user 
CALL GFILES(INFILE, JIREAD, *Spline data infile*, 1F)

GET data from infile 
READ(INFILE*) NX, NY /* x,y dimensions 
READ(INFILE*) (X(I), I=1, NX) /* read x values 
READ(INFILE*) (Y(I), I=1, NY) /* read y values 
READ(INFILE*) ((X(I,J), I=1, NX), J=1, NY) /* f(x,y) at knots 
READ(INFILE*) (DPDX(I,J), J=1, NY) /* df/dx at left side 
READ(INFILE*) (DPDX(I,J), J=1, NX) /* df/dx at right side 
READ(INFILE*) (DPDY(I,J), J=1, NX) /* df/dy at bottom 
READ(INFILE*) (DPDY(I,J), I=1, NY) /* df/dy at top 
READ(INFILE*) DPOXY(1,1), DPOXY(NX,1) /* df/dy at corners 
1 DPOXY(1, NY), DPOXY('X, NY)

READ scaling factors from the file (if present) 
READ(INFILE*, END=4) XYS C
GO TO 1 
4 XYS = 1.0 
1 READ(INFILE*, END=6) FSCALE 
GO TO 5 
6 FSCLAE = 1.0

CLOSE input file 
CALL FFILES(INFILE, JSCL0S)
```
C USE COORDINATE SCALE FACTOR TO SCALE INPUT X'S AND Y'S
C AND FUNCTION SCALE FACTOR FOR F AND ITS DERIVATIVES
DO 2 I=1,NX
2  X(I)=X(I)*XYSC
DO 3 I=1,NY
3  Y(I)=Y(I)*XYSC
DO 9 J=1,NY
9   F(I,J)=F(I,J)*SCALE
DO 8 I=1,NX
8   FDX(I,J)=DFDX(I,J)*SCALE/XYSC
DO 7 I=1,NX
7   FDY(I,J)=DFDY(I,J)*SCALE/XYSC
DO 6 I=1,NX
6   F(I,J)=F(I,J)*SCALE/XYSC
DO 3 J=1,NY
3   XDFX(I,J)=XDF(I,J)*SCALE/XYSC
DO 2 J=1,NY
2   YDFY(I,J)=YDFY(I,J)*SCALE/XYSC
DO 1 J=1,NY
1   XDFX(NX,J)=XDFX(NX,J)*SCALE/XYSC
DO 7 J=1,NY
7   YDFY(NX,J)=YDFY(NX,J)*SCALE/XYSC

C Open output file
C Get filename from user
CALL GFILE$(&OUTFIL,J&WRIT,*Output file name *,16)
C Call spline to generate matrix values
CALL SPLNXY(NX,NY)
C Write matrices to output file
WRITE (OUTFIL) (F(I,J),I=1,NX,J=1,NY)
WRITE (OUTFIL) (DFDX(I,J),I=1,NX,J=1,NY)
WRITE (OUTFIL) (DFDY(I,J),I=1,NX,J=1,NY)
WRITE (OUTFIL) (XDFX(I,J),I=1,NX,J=1,NY)
WRITE (OUTFIL) (YDFY(I,J),I=1,NX,J=1,NY)
XYM1=NX-1
NYM1=NY-1
WRITE (OUTFIL) (DELX(I),I=1,XYM1)
WRITE (OUTFIL) (DELY(I),I=1,NYM1)
C Close output file
CALL FILESS(OUTFIL,J&CLOSE)   /* close output file
C Print message to terminal indicating normal termination,
CALL TNOU (*normal termination *,16)
999 CALL EXIT
END

SUBROUTINE SPLNXY(NX,NY)
C BY C.J. DALY
COMMON /SPL/ F(50,50), DF0X(50,50), DF0Y(50,50), DF0XY(50,50)
 Y(50), Y(50), DELX(50), DELY(50)
DIMENSION TRIAX(50), TRIYX(50), TRIXY(50)
DIMENSION TRIU(5), TRIY(5), TRIYL(5)
DIMENSION RHS(5), DGTX(5), DFYX(5)

C Compute coefficients for the spline. Note that Gaussian
C elimination is carried out for the tridiagonal matrices
C before proceeding to Steps One through Four.

NXM1 = NX - 1
NXM2 = NX - 2
NXM3 = NX - 3
NYM1 = NY - 1
NYM2 = NY - 2
NYM3 = NY - 3

C Compute delta x and delta y.
DO 1 I = 1, NYM1
   DELX(I) = X(I+1) - X(I)
   GO TO 2
2 CDFLY(I) = Y(I+1) - Y(I)

C Fill tridiagonal matrices for all four Steps.
DO 3 I = 1, NYM2
   TRIUXU(I) = DELX(I)
   TRIXU(I) = (DELX(I+1) + DELX(I)) / 2
   GO TO 4
4 TRIYU(I) = DELY(I)

C Perform pivoting of tridiagonal matrices, downward.
C Save pivot values for all four Steps.
DO 5 I = 1, NYM3
   TRIXL(I+1) = TRIXU(I+1) / TRIXU(I)
   TRIY(I+1) = TRIYU(I+1) / TRIYU(I)
   GO TO 6
6

C Perform pivoting of tridiagonal matrices, upward.
C Save pivot values for all four Steps.
DO 7 I = 1, NYM2
   TRIUX(U(I)) = TRIUXU(I)/TRIYD(I)+1)
   GO TO 8
8 TRIY(I) = TRIY(I)/TRIY(I)+1)

C Compute and save ratios for efficiency.
DO 9 I = 1, NYM2
9 DGTX(I) = DELX(I)/DELX(I+1)
   GO TO 10
10 DFYX(I) = DELY(I)/DELX(I+1)

C Perform Step One.
DO 11 J = 1, NY
   DO 12 I = 1, NYM2
      RHS(I) = 3.0 * ((F(I+1,J)-F(I,J))/DGTX(I) +
     1 (F(I+2,J)-F(I+1,J))/DGTX(I))
   12 CONTINUE
      RHS(I) = R*(S*(NXM2) + TRIUXU(NYM3)*DFYX(NX,M,)+)
     1 RHS(I) = +RHS(I) - TRIYL(I)*DFYX(I,J)
   DO 12 I = 1, NYM3
RHS(I+1) = RHS(I+1) + TRIY(U(I+1) * RHS(I)
DO 14 I = 1,NXM3
II = NXM2 - I
14 RHS(I1) = RHS(I1) + RHS(I1+1) * TRIY(U(I1)
DO 15 I = 2,NXM1
DFDX(I,J) = RHS(I-1) / TRIYD(I-1)
11 CONTINUE

C Perform Step Two.
DO 16 I = 1,NX
DO 17 J = 1,NYM2
RHS(J) = 3.0 * ((F(I,J+1)-F(I,J))/QTXY(J) +
(F(I,J+2)-F(I,J+1))/QTXY(J))
17 CONTINUE
RHS(1) = RHS(1) - TRIY(L(1)*DFDY(I,1)
RHS(NYM2) = RHS(NYM2) - TRIYU(NYM2)*DFDY(I,NX)
DO 18 I = 1,NYM3
RHS(J+1) = RHS(J+1) + RHS(J) * TRIY(L(J+1)
DO 19 J = 1,NYM3
JJ = NYM2 - J
19 RHS(JJ) = RHS(JJ) + RHS(JJ+1) * TRIYU(JJ)
DO 20 J = 2,NYM1
DFDY(I,J) = RHS(J-1) / TRIYD(J-1)
16 CONTINUE

C Perform Step Three.
DO 26 INDEX = 1,2
IF (INDEX.EQ.1) I = 1
IF (INDEX.EQ.2) I = NX
DO 21 J = 1,NYM2
PHS(J) = 3.0 * ((DFDX(I,J+1)-DFDX(I,J))/QTXY(J) +
(DFDX(I,J+2)-DFDX(I,J+1))/QTXY(J))
RHS(1) = RHS(1) - TRIY(L(1)*DFDY(I,1)
RHS(NYM2) = RHS(NYM2) - TRIYU(NYM2)*DFDY(I,NX)
DO 22 J = 1,NYM3
RHS(J+1) = RHS(J+1) + TRIY(L(J+1) * RHS(J)
DO 23 J = 1,NYM3
JJ = NYM2 - J
23 RHS(JJ) = RHS(JJ) + RHS(JJ+1) * TRIYU(JJ)
DO 24 J = 2,NYM1
DFDY(I,J) = RHS(J-1) / TRIYD(J-1)
26 CONTINUE

C Perform Step Four.
DO 28 J = 1,NY
DO 29 I = 1,NYM2
PHS(J) = 3.0 * ((DFDY(I+1,J)-DFDY(I,J))/QTXY(I) +
(DFDY(I+2,J)-DFDY(I,J+1))/QTXY(I))
RHS(1) = RHS(1) - TRIY(L(1)*DFDY(I,1)
RHS(NYM2) = RHS(NYM2) - TRIYU(NYM2)*DFDY(INX,J)
DO 30 I = 1,NXM3
RHS(I+1) = RHS(I+1) + TRIY(L(I+1) * RHS(I)
DO 31 I = 1,NXM3
II = NXM2 - I
31 RHS(I1) = RHS(I1) + RHS(I1+1) * TRIYU(I1)
DO 32 I = 2,NXM1
32 DFDY(I,J) = RHS(I-1) / TRIYD(I-1)
28 CONTINUE
RETURN
END
SPLINE

C Spline interpolating function package

C *** SPLOAD ***

SUBROUTINE SPLOAD (INFILE, K)
C Reads spline data into one of three (K = 1, 2, or 3)
C locations in COMMON.

COMMON/SPL/ NX(3), NY(3), /* number of x,y indices
  1 F(50,50,3); /* function values at interstices
  1 DFDX(50,50,3), /* df/dx at interstices
  1 DFDY(50,50,3), /* df/dy at same
  1 DFDXY(50,50,3), /* df/dxdy at same
  1 X(50,3), /* x values of vertical grid lines
  1 Y(50,3), /* y values of horiz. grid lines
  1 CELX(50,3), /* delta x along grid
  1 CELY(50,3), /* delta y along grid

INTEGER INFILE /* data file for spline function

REWIN INFILE
C read data file into common
IF(K.GT.3.OR.K.LT.1)K=1
READ (INFILE) NX(K), NY(K)
KX=NX(K)
KY=NY(K)
KXM1=KX-1
KYM1=KY-1

READ (INFILE) ((F(I,J,K),I=1,KX),J=1,KY)
READ (INFILE) ((DFDX(I,J,K),I=1,KX),J=1,KY)
READ (INFILE) ((DFDY(I,J,K),I=1,KX),J=1,KY)
READ (INFILE) ((DFDXY(I,J,K),I=1,KX),J=1,KY)
READ (INFILE) (X(I,K),I=1,KX)
READ (INFILE) (Y(I,K),I=1,KY)
READ (INFILE) (CELX(I,K),I=1,KXM1)
READ (INFILE) (CELY(I,K),I=1,KYM1)

REWIN INFILE

999 RETURN
END

C *** SPLINE ***

FUNCTION SPLINE (X1,Y1,Y) /* Returns Real
C Function spline(x,y) returns spline interpolating function value at (x,y).

COMMON /SPL/ X(3), NY(3), /* number of x,y indices
  1 F(50,50,3), /* function values at interstices
  1 DFDX(50,50,3), /* df/dx at interstices
  1 DFDY(50,50,3), /* df/dy at same
  1 DFDXY(50,50,3), /* df/dxdy at same
  1 X(50,3), /* x values of vertical grid lines

27
SPLINE

1 Y(56:3), /* y values of horizontal grid lines
1 DELX(56:3), /* delta x along grid
1 DELY(56:3), /* delta y along grid

REAL XI,YI /* interpolating function arguments
INTENGINE I,J /* sub-rectangle indices

C Define interpolating functions

CX(XI,I,K) = (((XI-X(I+1,K))**2)/DELX(I,K)**2)+
1 ((XI-X(I+1,K))**2)/(DELX(I,K)**2))

CX1(XI,I,K) = (((XI-X(I+1,K))**2)/DELX(I,K)**2)-
1 ((XI-X(I+1,K))**2)/(DELX(I,K)**2))

CY(YI,I,K) = (((YI-Y(I+1,K))**2)/DELY(I,K)**2)+
1 ((YI-Y(I+1,K))**2)/(DELY(I,K)**2))

CY1(YI,I,K) = (((YI-Y(I+1,K))**2)/DELY(I,K)**2)-
1 ((YI-Y(I+1,K))**2)/(DELY(I,K)**2))

DX(XI,I,K) = (XI-X(I+1,K))*(XI-X(I+1,K))**2/DELX(I,K)**2

DX1(XI,I,K) = (XI-X(I+1,K))*(XI-X(I+1,K))**2/DELX(I,K)**2

DY(YI,I,K) = (YI-Y(I+1,K))*(YI-Y(I+1,K))**2/DELY(I,K)**2

DY1(YI,I,K) = (YI-Y(I+1,K))*(YI-Y(I+1,K))**2/DELY(I,K)**2

C Make sure the point is on the map

IF(XI.GT.3.OR.YI.LT.1)K=1

KY=NX(K)

IF (XI.LT.X(I+1,K)) OR (XI.GT.X(K+K)) GOTO 777

IF (YI.LT.Y(J+1,K) OR (YI.GT.Y(K+K)) GOTO 777

C Determine I and J

NXM1 = KX - 1

NYM1 = KY - 1

DO 10 J = 1,NYM1

IF (XI.LE.X(I+1,K)) GOTO 15

C exit with X(I,K) <= XI <= X(I+1,K)

10 CONTINUE

15 DO 20 J=1,NSM1

IF (YI.LE.Y(J+1,K)) GOTO 23

C exit with Y(J,K) <= YI <= Y(J+1,K)

20 CONTINUE

C Calculate spline interpolate

30 SPLINE = F(I,J,K)*CX(XI,I,K)*CY(YI,J,K) +
1 F(I+1,J,K)*CX(XI+1,I,K)*CY(YI,J,K) +
1 F(I,J+1,K)*CX(XI,I,K)*CY(YI+1,J,K) +
1 F(I+1,J+1,K)*CX(XI+1,I,K)*CY(YI+1,J,K) +
DFOX(I,J,K)*DX(XI,I,K)*CY(YI,J,K) +
DFOX(I+1,J,K)*DX(XI+1,I,K)*CY(YI,J,K) +
DFOX(J+1,K)*DX(XI,I,K)*CY(YI,J,K) +
DFOX(I,J+1,K)*DX(XI,I,K)*CY(YI+1,J,K) +
DFOY(I,J,K)*DX(XI,I,K)*DY(YI,J,K) +
DFOY(I+1,J,K)*DX(XI+1,I,K)*DY(YI,J,K) +
DFOY(J+1,K)*DX(XI,I,K)*DY(YI,J,K) +

28
!DFOY(I+J+1,K)*CX(X1,I+1,K)+
1 1 DFDY(I+J+1,K)*UX(X1,I+1,K)*DY(Y1,I+1,J)+
1 DFDY(I+J+1,K)*CY(X1,I+1,K)*DY(Y1,I+1,J)+
1 DFDY(I+J+1,K)*DX(X1,I+1,K)*DY(Y1,I+1,J)+
1 DFDY(I+J+1,K)*DX(X1,I+1,K)*DY(Y1,I+1,J)+

RETURN
C ERROR: here if point out of bounds

WRITE (1,1310) X1,Y1
1310 FORMAT('SPLINE ARGUMENTS OUT OF RANGE: *1P2E16.6')
STOP

C *** DS/DX ***

FUNCTION DSDX(X1,Y1,K)

Returns the partial w.r.t X of the spline interpolating function

COMMON /SPL/ NX(3),NY(3), /* number of x,y indices
1 F(50,503), /* function values at interstices
1 DFDX(50,503), /* df/dx at interstices
1 DFDY(50,503), /* df/dy at same
1 DFDX(50,503), /* df/dx at same
1 X(50,3), /* x values of vertical grid lines
1 Y(50,3), /* y values of horizontal grid lines
1 DELX(50,3), /* delta x along grid
1 DELY(50,3), /* delta y along grid

REAL X1,Y1 /* function arguments
INTEGER I,J /* subrectangle indices

C Define interpolating sub-functions ( p for partials)

PDYX(X1,I+1,K) = 2*(X1-X(I+1,K))/DELX(I+1,K)*2 +
1 2*(X1-X(I+1,K))/DELX(I+1,K)*2/DELX(I+1,K)*2 +
1 4*(X1-X(I+1,K))*(X1-X(I+1,K))/DELX(I+1,K)*2 +

PCX1(X1+1,K) = 2*(X1-X(I+1,K))/DELX(I+1,K)*2 -
1 2*(X1-X(I+1,K))*2/DELX(I+1,K)*2 -
1 4*(X1-X(I+1,K))*(X1-X(I+1,K))/DELX(I+1,K)*2 +

PDX1(X1,I+1,K) = 2*(X1-X(I+1,K))*(X1-X(I+1,K))/DELX(I+1,K)*2 +
1 (X1-X(I+1,K))*2/DELX(I+1,K)*2 +
1 4*(X1-X(I+1,K))*(X1-X(I+1,K))/DELX(I+1,K)*2 +
1 (X1-X(I+1,K))*2/DELX(I+1,K)*2 +

PCY(Y1+1,K) = (((Y1-Y(I+1,K))**2)/DELY(I+1,K)**2) +
1 ((Y1-Y(I+1,K))*(Y1-Y(I+1,K))**2)/DELY(I+1,K)**3)
C Make sure the point is on the map
IF(K*GT.3.OR.K*LT.1)K=1

KX=NX(K)
KY=NY(K)
IF(x1.LT.x(K)*OR*x1.GT.x(KK)) GOTO 777
IF(y1.LT.y(K)*OR*y1.GT.y(KK)) GOTO 777

C Determine I and J
NXM1 = KX - 1
NYM1 = KY - 1

DO 1C I = 1:NXM1
  IF(x1.LE.x(I+1,K)) GOTO 15
  C exit with X(I,K) <= X1 <= X(I+1,K)
  CONTINUE
15 00 2C J=1:NYM1
  IF(y1.LE.y(J+1,K)) GOTO 30
  C exit with Y(J,K) <= Y1 <= Y(J+1,K)
  CONTINUE
20 33

C Calculate ds/dx interpolate
C
DSDX = F(I,J,K)*PCX(Y1,J,K)*CY(Y1,J,K) +
  F(I+1,J,K)*PCX(Y1,J,K)*CY(Y1,J,K) +
  F(I+1,J+1,K)*PCX(Y1,J+1,K)*CY(Y1,J+1,K) +
  DFDX(I,J,K)*PCX(Y1,J,K)*CY(Y1,J,K) +
  DFDX(I+1,J,K)*PCX(Y1,J+1,K)*CY(Y1,J+1,K) +
  DFDX(I+1,J+1,K)*PCX(Y1,J+1,K)*CY(Y1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1,J,K)*DY(Y1,J,K) +
  DFDY(I+1,J,K)*PCX(Y1,J+1,K)*DY(Y1,J+1,K) +
  DFDY(I+1,J+1,K)*PCX(Y1,J+1,K)*DY(Y1,J+1,K) +
  DFDX(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDX(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDY(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDX(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDY(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDX(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDY(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDX(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDY(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDX(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDX(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(I,J+1,K)*PCX(Y1+1,J,K)*DY(Y1+1,J,K) +
  DFDY(I+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +
  DFDY(Y1+1,J+1,K)*PCX(Y1+1,J+1,K)*DY(Y1+1,J+1,K) +

RETURN

C ERROR: here if point out of bounds

777 WRITE (1010) X1,Y1
1010 FORMAT(*SDSX ARGUMENTS OUT OF BOUNDS: *1P2E16.6)
STOP

END

C *** DS/DY ***
FUNCTION SDDY (X1,Y1,K) /* returns real

C Returns the partial w.r.t. Y of the spline interpolating function

COMMON /SPL/ NX(3),NY(3), /* number of x,y indices
1 FL(50,50,3), /* function values at interstices
1 DFDX(50,50,3), /* df/dx at interstices
1 DFDY(50,50,3), /* df/dy at same
1 X(50,3), /* x values of vertical grid lines
1 Y(50,3), /* y values of horiz. grid lines
1 DELY(50,3), /* delta x along grid
1 DELX(50,3) /* delta y along grid

REAL X1,Y1 /* function arguments
INTEGER J,J /* subrectangle indices

C Define interpolating sub-functions (p for partials)

PCY(Y1,I+K) = 2*(Y1-Y(I+1,K))/DELY(I,K)**2 +
1 2*(Y1-Y(I+1,K))**2/DELY(I,K)**3 +
1 4*(Y1-Y(I+1,K))*(Y1-Y(I+1,K))/DELY(I,K)**3

PCY(Y1,I+K) = 2*(Y1-Y(I+1,K))/DELY(I,K)**2 -
1 2*(Y1-Y(I+1,K))**2/DELY(I,K)**3 -
1 4*(Y1-Y(I+1,K))*(Y1-Y(I+1,K))/DELY(I,K)**3

PCY(Y1,I+K) = 2*(Y1-Y(I+1,K))*(Y1-Y(I+1,K))/DELY(I,K)**2 +
1 (Y1-Y(I+1,K))**2/DELY(I,K)**3

P[Y1(Y1,K)] = 2*(Y1-Y(I,K))*(Y1-Y(I,K))/DELY(I,K)**2

CX(X1,I+K) = (((X1-X(I+1,K))**2)/DELX(I,K)**2)+
1 (((X1-X(I+1,K))**2)/DELX(I,K)**2)+
1 (((X1-X(I+1,K))**2)/DELX(I,K)**2)

CX(X1,I+K) = (((X1-X(I+1,K))**2)/DELX(I,K)**2)-
1 ((X1-X(I+1,K))**2)/DELX(I,K)**2-
1 ((X1-X(I+1,K))**2)/DELX(I,K)**3

DX(X1,I+K) = (X1-X(I+1,K))**2/DELX(I,K)**2

DX(X1,I+K) = (X1-X(I+1,K))**2/DELX(I,K)**2

C Make sure the point is on the map

IF K GT 3 OR (X1<0 OR X1>1) GOTO 777
X = NX(K)
Y = NY(K)
IF (X1<X(I+1,K)) OR X1 GT X(KX*K)) GOTO 777
IF (Y1<Y(I+1,K)) OR Y1 GT Y(KY*K)) GOTO 777

C Determine I and J

NXM1 = MX - 1
NYM1 = MY - 1

IF I = 1 OR I = NXM1
   (X1<0 OR X1>1) GOTO 15
C Exit with X(K) <= X1 <= X(I+1,K)
CONTINUE
15 DO 20 J=1, NYM1
   IF (Y1 LE Y(J+1,K)) GOTO 30
C   exit with Y(J,K) <= Y1 <= Y(J+1,K)
20 CONTINUE
BOOK  
C Calculate ds/dy interpolate
30 DSDY = F(I,J,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   F(I,J+1,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   F(I+1,J,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   DFDX(I,J,K)*DX(X11,I,K)*PCY(Y1,J+K) +  
   DFDX(I+1,J,K)*DX(X11,I,K)*PCY(Y1,J+K) +  
   DFDX(I,J+1,K)*DX(X11,I,K)*PCY(Y1,J+K) +  
   DFDX(I+1,J+1,K)*DX(X11,I,K)*PCY(Y1,J+K) +  
   DFDY(I,J,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   DFDY(I+1,J,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   DFDY(I,J+1,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   DFDY(I+1,J+1,K)*CX(X11,I,K)*PCY(Y1,J+K) +  
   DFDY(I,J,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I+1,J,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I,J+1,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I+1,J+1,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I,J,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I+1,J,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I,J+1,K)*DX(X11,I,K)*PDY(Y1,J+K) +  
   DFDY(I+1,J+1,K)*DX(X11,I,K)*PDY(Y1,J+K)
999 RETURN
C ERROR: here if point out of bounds
777 WRITE (1,1010) X1,Y1
1010 FORMAT ('DSDY ARGUMENTS OUT OF BOUNDS: *'IP2E16.6)
STOP
END
****** PROGRAM ******

Sample program for Spline Interpolating Package
It returns function value and gradient at points chosen by user

MNEMONIC CODES FOR CREATE FILE CALLS
INTEGER*2 JREAD,JWRIT,JCLOSE,JREADP,JCLOSE,JREADW,JWRITE,JREADR

PARAMETER
1 JREAD = 1  /* READ  
1 JWRIT = 2  /* WRITE  
1 JCLOSE = 3  /* CLOSE FILE  
1 JREADP = 4  /* MOVE FORWARD ONE FILE (MAG TAPE)  
1 JWRITE = 5  /* WRITE  
1 JREADW = 6  /* MOVE FORWARD ONE FILE (MAG TAPE)  
1 JCLOSE = 7  /* CLOSE FILE

INTEGER INFILE  /* fortran unit number of data file

REAL XY1, */ point we pass to spline
1 HEIGHT, */ interpolated function value
1 XSLOPE, */ ds/dx at xy
1 YSLOPE  /* ds/dy at xy

C open the data file made by CREATE
INFILE=5  /* fortran unit # of data file

C get filename from user.
CALL FILE$(INFILE,JREAD,*SPLINE FILE*,11)

C load the spline data file
Data is arbitrarily loaded into location k=1 in COMMON.
CALL SLOAD1(INFILE,1)

C close data file
CALL FILE$(INFILE,JCLOSE)

C get point from user
READ(1,*) XY1

C call interpolating functions
HEIGHT = SPLINE(XY1,1)  /* find function value at xy
XSLOPE = DSFX(XY1,1)  /* find ds/dx
YSLOPE = DSFY(XY1,1)  /* find ds/dy

PRINT 13) HEIGHT,XSLOPE,YSLOPE

13 FORMAT(1X,FL**,2,F10.5)

C print answers on terminal
GOTO 10  /* loop until user gets bored

END
Main program for 2-D particle movement in a flow field.

MNNMONIC CODE; FOR CRREL FILE CALLS

PARAMETER

INTEGER*2 J$READ,J$WRIT,J$RDWR,J$CLOS,J$FRWD,J$RWND

PARAMETER
1 J$READ = 1, /* READ
1 J$WRIT = 2, /* WRITE
1 J$RDWR = 3, /* READ AND WRITE
1 J$CLOS = 4, /* CLOSE FILE
1 J$DELE = 5, /* DELETE FILE
1 J$FRWD = 6, /* MOVE FORWARD ONE FILE (MAG TAPE)
1 J$RWND = 7, /* REWIND

INTEGER SPFILE,OUTPUT

Points along a single flow line (XP,YP)
DIMENSION XP(1000),YP(1000)

Boundaries of the flow region
COMMON BOUND/X1,XN,Y1,YM
INFILE=5
OUTPUT=6
SPFILE=7
PRINT 100

FORMAT(/1X,4H GIVE)

Read hydraulic head spline data file.
CALL GFILE$(SPFILE,J$READ, *H SPLINE INFILE *,15)
CALL SPLOAD(SPFILE)
PRINT 100

Read hydraulic conductivity spline data file.
CALL GFILE$(SPFILE,J$READ, *K SPLINE INFILE *,15)
CALL SPLOAD(SPFILE)
PRINT 100

Read effective porosity spline data file.
CALL GFILE$(SPFILE,J$READ, *PSI SPLINE INFILE *,17)
CALL SPLOAD(SPFILE)
PRINT 100

Get filename for file containing delta t, scale, flow region boundaries, and initial points of flow lines.
CALL GFILE$(INFILE,J$READ, *POINT INPUT FILE *,16)
PRINT 100

Get filename for output of flow line points.
CALL GFILE$(OUTPUT,J$WRIT, *STREAMLINE OUTPUT FILE *,22)

READ(INFILE,**DELT
READ(INFILE,**XYSC
READ(INFILE,**XYSC

Scale input flow boundary data.
X1=X1*XYSC
XN=XN*XYSC
Y1=Y1*XYSC
YM=YM*XYSC
WRITE(OUTPUT,1000)DELT
WRITE(OUTPUT,1001)X1,XN,Y1,YM
1000 FORMAT(1X,4F10.2)
C Read (X,Y), the beginning point of a flow line.
C Scale input values.
2 READ(INFILE,*,END=1)X,Y
   X=X*XYSC
   Y=Y*YSC
C Compute flow line coordinates.
   CALL STREAM(OUTPUT,Y,Y,DELT)
C Go back to read initial point for another flow line.
   GO TO 2
1 CALL FILES$(INFILE,J3CLOS)
   CALL FILES$(OUTPUT,J3CLOS)
   STOP
END
AVERAGE LINEAR VELOCITY

C Average linear velocity calculation routine.
SUBROUTINE FG(T,X,Y,F,G,OUT)
REAL K
C K = hydraulic conductivity (isotropic). COMMON location 2.
C H = hydraulic head. Spline data in COMMON location 1.
C PSI = effective porosity. COMMON location 3.
C The flow region is X1 < X < XN and Y1 < Y < YM.
COMMON/BOUND/X1,XN,Y1,YM
C Check to see if x and y are within the flow region.
IF(X.LT.X1.OR.X.GT.XN)GO TO 1
IF(Y.LT.Y1.OR.Y.GT.YM)GO TO 1
C Use spline files to compute the following.
(NDX,NDY) is the hydraulic gradient.
DNDX=DSDX(X,Y,1)
DNDY=DSDY(X,Y,1)
K=SPLINE(X,Y,2)
PSI=SPLINE(X,Y,3)
C Darcy's law for average linear velocities.
C F = x component of the average linear velocity.
C G = y component of the average linear velocity.
F=-(K*DNDX)/PSI
G=-(K*DNDY)/PSI
RETURN
C IOUT = 1 signals the crossing of a flow boundary.
I IOUT=1
RETURN
FND
METHOD 1 ALGORITHM

SUBROUTINE STREAM(OUTPUT,X,Y,DELT)

SOLVES F(X,Y,T) + C/2X + G(X,Y,T) + C/DY + DC/DT = 0

BY THE METHOD OF CHARACTERISTICS USING FOURTH ORDER
RUNGE-KUTTA AND PREDICTOR-CORRECTOR ALGORITHMS.

INTEGER OUTPUT

DIMENSION XNPM(3),YNPM(3),XNT(1001),YN(1001)

WHEN IOUT IS RETURNED AS 1, THE CHARACTERISTIC WILL BE CROSSING
A BOUNDARY OF THE FLOW REGION.

NPOINT=1
DELFT2=DELT/2.
DELT3=DELT/3.
DELFT6=DELT/6.
DELFT4=4.*DELT3
DELFT8=8.*DELT3

INITIALIZE AT THE POINT OF ORIGIN OF THE CHARACTERISTIC

XNT(1)=X
YN(1)=Y

T=0.
CALL FG(TN,XN,YN,F1,G1,IOUT)
IF(IOUT.NE.0)Go TO 1

PERFORM RUNGE-KUTTA FOR THE FIRST THREE POINTS TO GET STARTED
CLASSICAL (4,4) FORMULATION.

DO 2 IT=1,3
T1=TN+DELT
XVAL=XN+F1*DELT2
YVAL=YN+G1*DELT2

CALL FG(T1,XVAL,YVAL,F2,G2,IOUT)
IF(IOUT.NE.0)Go TO 1

XVAL=XN+F2*DELT2
YVAL=YN+G2*DELT2
CALL FG(T1,XVAL,YVAL,F3,G3,IOUT)
IF(IOUT.NE.0)Go TO 1

XVAL=XN+F3*DELT
YVAL=YN+G3*DELT
CALL FG(T1,XVAL,YVAL,F4,G4,IOUT)
IF(IOUT.NE.0)Go TO 1

XN1=XN+DELFT6*(F1+F4)+DELFT3*(G2+G3)
YN1=YN+DELFT6*(G1+G4)+DELFT3*(C2+C3)
XNT(IT+1)=XN1
YN(IT+1)=YN1
NPOINT=IT+1
XN=XN1
YN=YN1
T=TN1
CALL FG(TN,XN,YN,F1,G1,IOUT)
IF(IOUT.NE.0)Go TO 1

XNPM(IT)=F1
YNPM(IT)=G1

USE PREDICTOR-CORRECTOR METHOD FOR THE REST OF THE CHARACTERISTIC
STANDARD FOURTH ORDER MILNE FORMULATION.
METHOD 1 ALGORITHM

DO 3 IT=4,110;
  TN1=TN*DELT
  XNP1=XNT(IT-3)+DELT83*(XNPM(3)+XNPM(1))-DELT43*XNPM(2)
  YNP1=YNT(IT-3)+DELT83*(YNPM(3)+YNPM(1))-DELT43*YNPM(2)
  CALL FG(TP1,XNP1,YNP1,XPRM,YFKM,OUT)
  IF (IOUT.NE.0) GO TO 1
  XN1=XNT(IT-1)+DELT5*(XPRM*XNPM(2))+DELT43*XNPM(3)
  YN1=YNT(IT-1)+DELT5*(YPRM*YNPM(2))+DELT43*YNPM(3)
  XNT(IT+1)=XN1
  YNT(IT+1)=YN1
  NPOINT=IT+1
  XPRM(1)=XNPM(2)
  YPRM(1)=YNPM(2)
  XNPM(2)=XNPM(1)
  YNPM(2)=YNPM(1)
  CALL FG(TN1,XN1,YN1,XNPM(2),YNPM(3),OUT)
  IF (IOUT.NE.0) GO TO 1
3 CONTINUE
C THERE WILL BE NPOINTS ON THE CHARACTERISTIC LINE
1 WRITE (OUTPUT,1000)NPOINT
1000 WRITE (OUTPUT,1001)((XNT(I),YNT(I)),I=1,NPOINT)
1001 FORMAT(5(5X,2F10.2))
RETURN
END
**METHOD 2 ALGORITHM**

**SUBROUTINE STREAM (OUTPUT, X, Y, DELT)**

C SOLVES \( F(X, Y, T) \) \( \frac{DC}{DX} + \frac{DG}{DY} + \frac{DC}{DT} = 0 \)

C BY THE METHOD OF CHARACTERISTICS USING AN EMBEDDED \((k, g)\) C RUNGE-KUTTA FORM AND ACCURACY CHECK.

C INVOLVES VARIABLE TIME STEP FEATURE.

C

INTEGER OUTPUT

DIMENSION XNT(1001), YNT(1001)

PARAMETER TCL = 1.001

PARAMETER TOL = 0.0001

PARAMETER SMALL = 1.0E-13

IOUT = 0

C WHEN IOUT IS RETURNED AS 1, THE CHARACTERISTIC WILL BE CROSSING

C A BOUNDARY OF THE FLOW REGION.

NP = 1

C INITIALIZE AT THE POINT OF ORIGIN OF THE CHARACTERISTIC

XNT(1) = X

YNT(1) = Y

XNP = X

YNP = Y

TNP = T

C

C PERFORM RUNGE-KUTTA

ISTEP = 1

DO 2 IT = 1, 1000

T = DELT / ISTEP

DT2 = T / 2.

DT4 = T / 4.

DT5 = T / 5.

DT7 = T / 7.

DT36 = T / 36.

DT63 = T / 63.

DT27 = T / 27.

XNP = XNP + TNP * X

YNP = YNP + TNP * Y

TNP = TNP + T

C

C WITHIN EACH MAJOR TIME STEP \( \delta t \), RUNGE-KUTTA is

C USED AT TIME STEPS \( \delta t \) = \( \delta t \) / ISTEP.

DO 3 JT = 1, ISTEP

CALL FG(TNP, XNP, YNP, F1, G1, IOUT)

IF (IOUT .LT. 10) GO TO 1

XVAL = XNP + DT2 * F1

YVAL = YNP + DT2 * G1

TVAL = TNP + DT2

CALL FG (TVAL, XVAL, YVAL, F2, G2, IOUT)

IF (IOUT .LT. 3) GO TO 1

XVAL = XNP + DT4 * F2

YVAL = YNP + DT4 * G2

TVAL = TNP + DT4

CALL FG (TVAL, XVAL, YVAL, F3, G3, IOUT)

IF (IOUT .LT. 5) GO TO 1

XVAL = XNP + DT6 * (F1 + F2)

YVAL = YNP + DT6 * (G1 + G2)

TVAL = TNP + DT6

CALL FG (TVAL, XVAL, YVAL, F4, G4, IOUT)

IF (IOUT .LT. 7) GO TO 1

XVAL = XNP + DT8 * (F2 + F3 - F2)

YVAL = YNP + DT8 * (G2 + G3 - G2)

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METHOD 2 ALGORITHM Page 2

TVAL = TN + DT
CALL FG(TVAL, XVAL, YVAL, F4, G4, IOUT)
IF (IOUT.NE.0) GO TO 1

XVAL = XN + DT27*(7.**F1 + 12.**F2 + 546.**F3 + 54.**F4 - 378.**F5)
YVAL = YN + DT27*(7.**G1 + 12.**G2 + 546.**G3 + 54.**G4 - 378.**G5)
TVAL = TN + DT5
CALL FG(TVAL, XVAL, YVAL, F5, G5, IOUT)
IF (IOUT.NE.0) GO TO 1

XN14 = XN + DT625*(2.**F1 - 12.**F2 + 546.**F3 + 54.**F4 - 378.**F5)
YN14 = YN + DT625*(2.**G1 - 12.**G2 + 546.**G3 + 54.**G4 - 378.**G5)
T1 = TN + DT

Begin calculation for accuracy check.
XA6 = AHS(XN16)
YA6 = AHS(YN16)
IF (XA6.LT.SMALL) XA6 = SMALL
IF (YA6.LT.SMALL) YA6 = SMALL
CHECKX = ABS(XN16 - XN14) / XA6
CHECKY = ABS(YN16 - YN14) / YA6
IF (CHECKX.LT.TOLX .AND. CHECKY .LT.TOLY) GO TO 5

Here if accuracy is insufficient. Go back and start
from the beginning of the major time step with a new
cell t equal to 1/2 the current cell t.
ISTEP = ISTEP * 2
IF (ISTEP .LT. 32) GO TO 4
WRITE (1, 1302)
STOP

1302 FORMAT (1X, 5HMAX TIME STEP TOO LARGE, ABORT)

5 IF (CHECKX .LT. TOLX .AND. CHECKY .LT. TOLY) KOUNT = KOUNT + 1
XN = XN16
YN = YN16
3 TN = TN1

XI(T1+1) = XN16
YI(T1+1) = YN16
NP0INT = IT + 1

If accuracy criteria was consistently surpassed throughout
the major time step, double cell t.
IF (KOUNT .NE. ISTEP) ISTEP = ISTEP / 2
IF (ISTEP .LE. 1) ISTEP = 1
XNP = XN16
YNP = YN16
TNP = TN1
2 CONTINUE

There will be NPOINTS on the characteristic line
WRITE (OUTPUT, 1000) NPOINT
1000 FORMAT (1X, I5)
WRITE (OUTPUT, 1001) ((XNT(I), YNT(I)), I = 1, NPOINT)
1001 FORMAT (5(5X, 2F10.2))
**** SFLOT PLOTTING ROUTINE ****

ROUTINE FOR PLOTTING STREAMLINES. CREATES OVERLAYS WHEN
USED WITH APPROPRIATE SCALE FACTORS.

Mnemonic codes for corel file calls:

INTEGER JSREAD, JSWRITE, JSRDWR, JSCLOSE, JSFRWD, JSRWND

Parameter

1 JSREAD = 1 /* READ
1 JSWRITE = 2 /* WRITE
1 JSRDWR = 3 /* READ AND WRITE
1 JSCLOSE = 4 /* CLOSE FILE
1 JSDELETE = 5 /* DELETE FILE
1 JSFRWD = 6 /* MOVE FORWARD ONE FILE (MAG TAPE)
1 JSRWND = 7 /* REWIND

DIMENSION X(1:33), Y(1:22), LABEL(10)

INFILE=5
CALL GFILE(INFILE, JSREAD, *GIVE STREAMLINE INPUT FILE*, 26)
READ(INFILE, 1000) DELT
READ(INFILE, 1100) X, Y
1000 FORMAT(1X, 4F1.2)

INPUT SCALE, 1 INCH OF PAPER EQUALS (SCALE) FEET, METERS, MILES, ...

PRINT 1001
1001 FORMAT(1X*11, 2F, INPUT SCALE)
READ(1, *) SCALE
PRINT 1004
1004 FORMAT(1X*31, 2F, VERY N TH POINT, GIVE N)
READ(1, *) INCR
TINCR = DELT * INCR

INITIATE PLOT MODE.
CALL PLOTS(J)

DETERMINE FLOW REGION DIMENSIONS IN INCHES.
XLORE = (XN - X1) / SCALE
YLORE = (YN - Y1) / SCALE

DRAW OUTLINE OF FLOW REGION.
CALL PLOT(XLORE + 3, YLORE)
CALL PLOT(XLONG - 3, YLONG)
CALL PLOT(XLONG, YLONG + 2)
CALL PLOT(XLONG, YLONG - 2)
CALL PLOT(XLONG - 3, YLONG)

READ IN, AND PLOT THE STREAMLINES ONE AT A TIME.
READ(INFILE, 1002, END=1) NPONINT
1002 FORMAT(1X, 15)
X(NPONINT + 1) = X1
Y(NPONINT + 1) = Y1
X(NPONINT + 1) = SCALE
Y(NPONINT + 1) = SCALE
READ(INFILE, 1503)((X(I), Y(I)), I = 1, NPONINT)
1503 FORMAT(5X, 2F13.2)

PERFORM PLOTTING OF THE CURRENT FLOW LINE.
CALL LINE(X, Y, NPONINT + 1, INCR, S)
GO TO 2

OUT REFERENCE MARKS AND ANNOTATION ON THE PLOT.

ENCOD(18,200C, LABEL)X1.Y1

WHITE(1H(F7.1, 1H(F7.1, 2H)) )

SIZE=.16

YLOC=-.5

CALL SYMBOL(XLOC, YLOC, SIZE, LABEL'DATA1')

ENCOD(20, 2001, LABEL)TINCR

FORMAT(14H INTERVAL = F6.1)

XLOC=XLONG/2.

CALL SYMBOL(XLOC, YLOC, SIZE, LABEL'DATA2')

ENCOD(18, 2003, LABEL)XN, YM

XLOC=XLONG-1.75

YLOC=YLONG+.5

CALL SYMBOL(XLOC, YLOC, SIZE, LABEL'DATA3')

FILE(INFILE, JCLOSE)

STOP

END