**Physical and Acoustical Properties of Surface Sediment from Venezuela Basin: A Data Report**

Kevin Briggs
Michael Richardson

Naval Ocean Research and Development Activity
Ocean Science Directorate
NSTL, Mississippi 39529

**Physical and Acoustic Properties of Surface Sediment from Venezuela Basin**

Physical and acoustic properties of surface sediments collected with a 0.25-m² box core were measured from 45 stations in the Venezuela Basin. Samples were collected from three locations representing different sedimentary provinces in addition to transects between the locations. Location 1 (15°07'N, 69°22'W) was on the eastern slope of the Beata Ridge in 3950 m water depth. Sediments were pelagic foraminifera ooze. Location 2 (13°45'N, 67°45'W) was in...
the central Venezuela Basin in 5050 m water depth. Sediments consisted of interbedded turbidite and pelagic sediments. Location 3 (13°30'N, 64°45'W) was on the western flank of the Aves Ridge in 3500 m water depth. Sediments were predominantly hemipelagic in origin.

Values of porosity, grain size, percent CaCO3, organic carbon and nitrogen, shear strength, color, compressional wave velocity, and attenuation were determined from 6.1 cm inside diameter cylindrical subcores. X-radiographs of 36 x 44 x 3 cm rectangular acrylic subcores were made to determine sedimentary/biological structure. Probes used to measure shear strength and compressional wave velocity were occasionally inserted into whole box cores for additional measurements. The color of freshly collected sediments from whole box cores was also noted.

In this report we present the entire data set in table form. Methods of collection and subsequent laboratory and computational analysis are presented in detail. The data presented here will be the subject of more detailed analysis in future publications.
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Kevin Briggs
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Ocean Science Directorate
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January 1984
EXECUTIVE SUMMARY

Physical and acoustic properties of surface sediments collected with a 0.25-m$^2$ box core were measured from 45 stations in the Venezuela Basin. Samples were collected from three locations representing different sedimentary provinces in addition to transects between the locations. Location 1 (15°07'N, 69°22'W) was on the eastern slope of the Beata Ridge in 3950 m water depth. Sediments were pelagic foraminifera ooze. Location 2 (13°45'N, 67°45'W) was in the central Venezuela Basin in 5050 m water depth. Sediments consisted of interbedded turbidite and pelagic sediments. Location 3 (13°30'N, 64°45'W) was on the western flank of the Aves Ridge in 3500 m water depth. Sediments were predominantly hemipelagic in origin.

Values of porosity, grain size, percent CaCO$_3$, organic carbon and nitrogen, shear strength, color, compressional wave velocity, and attenuation were determined from 6.1 cm inside diameter cylindrical subcores. X-radiographs of 36 x 44 x 3 cm rectangular acrylic subcores were made to determine sedimentary/biological structure. Probes used to measure shear strength and compressional wave velocity were occasionally inserted into whole box cores for additional measurements. The color of freshly collected sediments from whole box cores was also noted.

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ACKNOWLEDGMENTS

The authors wish to acknowledge the assistance of the ships' captains and crews of the R/V GYRE (cruise 79G7), USNS LYNCH (cruise 708-80), and USNS BARTLETT (cruise 1301-82). We also wish to thank all of the scientific colleagues who participated in the aforementioned cruises. Without their support a project of this scope would have been impossible. Thanks to David C. Young, Frank Carnaggio, and James Matthews for designing and fabricating the compressional wave velocity probes. Special thanks are extended to Skidaway Institute of Oceanography and Steve Bishop, in particular, for use of the CHN analyzer and to NAVOCEANO for the training and use of the Micromeritics Particle Size Analyzer. We thank Richard Ray for the compilation of data exhibited in Appendix A and David K. Young for careful review of the manuscript. This work was supported by Program Element 61153N; Ralph R. Goodman and James E. Andrews, Program Managers.
# CONTENTS

<table>
<thead>
<tr>
<th>Section</th>
<th>Page</th>
</tr>
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<tbody>
<tr>
<td>LIST OF ILLUSTRATIONS</td>
<td>iv</td>
</tr>
<tr>
<td>LIST OF TABLES</td>
<td>iv</td>
</tr>
<tr>
<td>I.  INTRODUCTION</td>
<td>1</td>
</tr>
<tr>
<td>II. MATERIALS AND METHODS</td>
<td>1</td>
</tr>
<tr>
<td>A. SITE SELECTION</td>
<td>1</td>
</tr>
<tr>
<td>B. FIELD COLLECTION</td>
<td>3</td>
</tr>
<tr>
<td>C. FIELD ANALYSIS</td>
<td>7</td>
</tr>
<tr>
<td>D. LABORATORY ANALYSIS</td>
<td>15</td>
</tr>
<tr>
<td>III. RESULTS</td>
<td>18</td>
</tr>
<tr>
<td>IV. REFERENCES</td>
<td>19</td>
</tr>
<tr>
<td>APPENDIX A—SEDIMENT ACOUSTIC AND PHYSICAL PROPERTY DATA FROM BOX CORES COLLECTED IN THE VENEZUELA BASIN</td>
<td>21</td>
</tr>
<tr>
<td>APPENDIX B—FREQUENCY HISTOGRAMS OF GRAIN SIZE DISTRIBUTION DATA FOR SEDIMENTS COLLECTED IN BOX CORES FROM THE VENEZUELA BASIN</td>
<td>19</td>
</tr>
<tr>
<td>APPENDIX C—X-RADIOGRAPHS OF SEDIMENTS COLLECTED FROM THE VENEZUELA BASIN</td>
<td>233</td>
</tr>
<tr>
<td>APPENDIX D—COLOR DESCRIPTIONS OF CORES</td>
<td>253</td>
</tr>
<tr>
<td>APPENDIX E—COMPRESSIONAL WAVE VELOCITY PROBE DATA</td>
<td>257</td>
</tr>
<tr>
<td>APPENDIX F—SEDIMENT SHEAR STRENGTH MEASURED WITH HAND-HELD VANE SHEAR PROBE</td>
<td>263</td>
</tr>
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</table>
ILLUSTRATIONS

Figure 1. Location of sampling sites in the Venezuela Basin 2
Figure 2A. MK III box corer ready to deploy 6
Figure 2B. Deployment of box corer from rear U-frame of USNS BARTLETT 6
Figure 2C. Retrieval of box corer containing bottom sediment sample 6
Figure 2D. Subcoring of box core sample after detachment of box core and spade from box corer with aid of cart 6
Figure 3. Block diagram of compressional wave velocity probe measuring system 10
Figure 4. Line drawing of compressional wave velocity probes 10
Figure 5. Block diagram of sediment core compressional wave velocity and attenuation measuring system 13

TABLES

Table 1. Location, depth, date, and time of collection for the 68 box core stations occupied in the Venezuela Basin 4
Table 2. Listing of subcores collected from 45 box core samples obtained for physical/acoustic properties analysis 8
I. **INTRODUCTION**

This report presents data on the horizontal and vertical distribution of surface sediment physical and acoustic properties. The data was collected in an investigation of the effects of biological processes on the physical and acoustic properties of deep-sea sediments. Results from the biological collections will be included in subsequent reports. The entire data set on the following sediment properties is printed in the form of tables: porosity, grain size distribution, percent calcium carbonate (CaCO₃), organic carbon and nitrogen, shear strength, color, and sedimentary/biological structure, sediment compressional wave velocity, and attenuation. Methods of collection and subsequent laboratory and computational analysis are presented in detail. The data presented here will be the subject of more detailed analysis in future publications. The purpose of the report is to make the bulk of the sediment data available as rapidly as possible to others involved with this study.

II. **MATERIALS AND METHODS**

A. **Site Selection**

Three locations representing different sedimentary provinces in the Venezuela Basin were selected for study (Fig. 1). Location 1 was on the eastern part of the Beata Ridge (15°07'N, 69°22'W) in 3950 m water depth. Sediments were pelagic foraminifera ooze. Location 2 was in the central Venezuela Basin in 5050 m water depth and centered about 13°45'N, 67°45'W. Sediments were interbedded turbidite depositions and pelagic sediments. Location 3 was on the eastern flank of the Aves Ridge in a hemipelagic sedimentary province in 3500 m water depth and centered about 13°30'N, 64°45'W.

A total of 99 stations were occupied consisting of: 19 box cores, eight trawls, and one dredge haul at location 1; 23 box cores and nine trawls at location 2; 18 box cores and eight trawls at location 3; three box cores along a transect between locations 1 and 2; five box cores along a transect between locations 2 and 3; and five trawls collected about 130 km north of location 2. A listing of the depth, latitude, longitude, date, and time (GMT) of each box core sample is
Figure 1. Location of sampling sites in the Venezuela Basin.
presented in Table 1. Data pertinent to the trawl and dredge hauls will be presented in subsequent publications.

Samples were collected on three oceanographic cruises. Stations 1-6 were occupied from the R/V GYRE, cruise 79G7, which departed Panama City, Panama, on 10 November 1979 and terminated at Santo Domingo, Dominican Republic, on 26 November 1979. Stations 7-19 were occupied from the USNS LYNCH, cruise 708-80, which departed Roosevelt Roads, Puerto Rico, on 2 July 1980 and returned on 28 July 1980. Stations 20-99 were occupied from the USNS BARTLETT, cruise 1301-82, which departed Roosevelt Roads, Puerto Rico, on 14 October 1981 and returned on 8 December 1981.

B. Field Collection

Sediments were collected with the 0.25-m² MK III box corer depicted in Figure 2A-D. The design and function of the box corer were essentially the same as the box corer described by Hessler and Jumars (1974) with two exceptions: (1) the safety bar holding the release bolt was triggered by the downward fall of the column through the frame sleeve that released a lever holding the safety bar (this safety acted to prevent accidental triggering of the spade arm on deck or while the box corer was in transit to the bottom), and (2) spring-loaded doors at the top of the core box replaced the screened vents and flapper valves. A pinger, fastened on the wire 25 m from the box corer, was used to monitor sample collection on a Line Scan Recorder. Box core descent was approximately 50 m/min until the sampler was 50 m from the bottom. The box core was then lowered into the bottom as slowly as weather conditions permitted (10-25 m/min). The box core was retrieved at 50-75 m/min.

The box cores containing undisturbed surface sediment with overlying water together with the attached spade arm were carefully removed from the coring device. Cylindrical subcores (6.1-cm inside diameter and 46-cm length) and/or 36 cm (width) x 3 cm (thickness) x 44 cm (length) acrylic subcores were used to collect subsamples of the sediment. Extreme care was exercised to obtain relatively undisturbed subsamples with the sediment-water interface preserved intact within the subcores. In order to obtain undisturbed samples of the pelagic and turbidite layers at location 2, a second set of subcores was taken after manual removal of overlying sediment layers that had high shear strength and resistance to core penetration.
Table 1. Location, depth, date, and time of collection for the 68 box core stations occupied in the Venezuela Basin. Station listings do not include the 30 trawl hauls and dredge haul.

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* = macrofauna box core
Figure 2A. MK III box corer ready to deploy

Figure 2B. Deployment of box corer from rear U-frame of USNS BARTLETT

Figure 2C. Retrieval of box corer containing bottom sediment sample

Figure 2D. Subcoring of box core sample after detachment of box core and spade from box corer with aid of cart
One to 24 subcores were collected from each box core (except from stations 11, 12, and 13 which were disturbed samples). A listing of subcores by type of analysis is presented in Table 2. Some subcores were used for more than one type of analysis (e.g. compressional wave velocity and shear strength). Because of the dual-use of subcores, there will appear to be a disparity between the total number and the sum of the individual subcores. Those collected for analyses by workers outside of NORDA (i.e. benthic foraminifera: Barun Sen Gupta, LSU; meiofauna: Donald Woods, U. of Alabama; muramic acid: David White, FSU; microfaunal lipids: H. Rodger Harvey, U. of Georgia; radionuclide distribution: David Schink and Norman Guinasso, Texas A&M) will be the subject of subsequent publications.

C. Field Analysis

Sediment acoustic measurements were made utilizing three different types of apparatus: probes inserted into undisturbed box cores, USI-103 transducer-receiver head with the USI-103 sediment velocimeter, and USI-103 transducer-receiver head with different electronic components.

Replicate series of compressional wave velocity measurements were made at 0.5-cm intervals in four undisturbed box cores using the probes described in Figures 3 and 4. A Tektronix PG 501 Pulse Generator was used to trigger a Tektronix FG504 Function Generator and a Hewlett Packard 1743A dual-time interval Oscilloscope (Fig. 3). The Tektronix FG504 Function Generator drove the compressional wave transducer with a 70-kHz sine wave triggered for 10 μsec duration every 2 msec. The electrical energy was transferred into mechanical energy using a piezoceramic thin sheet transducer (12.7-mm long, 2.5-mm wide, and 0.25-mm thick) cut from a G1195 series thin sheet manufactured by Gulton Industries. The transducer was epoxied at one end into a 15-mm long, 10-mm wide window machined into a 2.4-mm thick Phenolic Sheet and potted with Scotch Cast 8 (Fig. 4).

Compressional waves propagated through the sediments to two compressional wave receivers that were built as identically as possible to the compressional wave transducer. The mechanical energy was transferred into electrical energy by the piezoceramic receivers, amplified (20-dB gain) by Burr-Brown 3622K Differential amplifiers, and filtered by Krohn-Hite Model 3100R Band-Pass Filters (1-1000 kHz low cut-off and high cut-off frequencies) set in the maximum flat butterworth
| STATION | 2 | 3 | 5 | 9 | 14 | 16 | 17 | 18 | 21 | 22 | 23 | 24 | 26 | 28 | 29 | 30 | 31 | 32 | 42 | 43 | 44 | 46 | 47 | 48 |
|---------|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| NORDA   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| TOTAL SUBCORES | 0 | 10 | 8 | 2 | 15 | 12 | 3 | 1 | 8 | 3 | 3 | 7 | 5 | 2 | 7 | 7 | 2 | 1 | 10 | 11 | 11 | 5 | 3 | 9 |
| Acoustic | 5 | 5 | 2 | 15 | 12 | 3 | 1 | 5 | 1 | 2 | 4 | 4 | 2 | 4 | 6 | 2 | 5 | 5 | 5 | 2 | 2 | 9 |
| Physical | 5 | 4 | 2 | 3 | 3 | 1 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 3 | 3 | 3 | 1 | 1 | 6 |
| Shear Strength | 1 | 1 | 2 | 5 | 1 | 3 | 3 | 3 | 1 | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| X-ray boxes | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Organic | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Geotechnical | 1 | 1 | 2 | 3 | 3 | 3 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Outside NORDA |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| TOTAL SUBCORES | 3 | 3 | 3 | 6 | 5 | 6 | 8 | 5 | 13 | 0 | 0 | 13 | 0 | 0 | 14 | 0 | 0 | 0 | 13 | 11 | 12 | 14 | 0 | 0 |
| Woods | 3 | 3 | 3 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| White | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Harvey | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Schink and Guinasso | 3 | 3 | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Measurements on Whole Box Cores |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| Shear strength (torque gauge) | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |

Table 2. Listing of subcores collected from the 45 box core samples obtained for physical/acoustic property analyses.
Table 2 (continued)

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Figure 3. Block diagram of compressional wave velocity probe measuring system

Figure 4. Line drawing of compressional wave velocity probes
position. The time delay (Δt) between the two, amplified, filtered, received signals was measured with the Hewlett-Packard Oscilloscope.

The first "Δt" measurement for each series was made in the water overlying the sediment-water interface. The difference in the distance between the transducer and the two receivers was calculated from the "Δt" measurement and the compressional wave velocity for sea water (calculated from MacKenzie, 1982) given temperature, salinity, and depth. Temperature and salinity of the overlying water were measured with a YSI Model 43TD temperature probe and an AO Goldberg temperature-compensated, salinity refractometer. The difference in distance between probes was assumed to remain the same during any series of measurements. Time delay (Δt) measurements were made at 0.5-cm intervals as the probes were inserted into the sediment. Simultaneous sediment temperature measurements were made with a YSI Model 43TD temperature probe. Compressional wave velocity at each depth was calculated from the difference in distance between the transducer and receivers and the measured time delay.

Values of compressional wave velocity were determined for sediment in the cylindrical core liners (stations 9, 14, 16, 17, and 18) with an Underwater Systems, Inc. (Model USI 103) Sediment Velocimeter. Time delay measurements made on distilled water through the core liner were compared to similar time delay measurements on the sediment sample to determine sediment compressional wave velocity using the following formula:

\[
V_p = \frac{V_w}{1 - \frac{\Delta t V_w}{d}}
\]  

where \(V_p\) is the measured sound velocity through sediment (m/sec); \(V_w\) is the measured sound velocity through distilled water (m/sec); \(\Delta t\) is the measured time arrival of sound through distilled water minus the time arrival through sediment (sec); and \(d\) is the inside diameter of the core in meters.

Values of sediment compressional wave velocity and attenuation were determined at 1-cm intervals in the core samples collected at stations 21-84 with an Underwater System, Inc. (Model USI-103) transducer-receiver head. A Tektronix PG501 Pulse Generator, FG504 Function Generator, Krohn-Hite 3100R Band Pass Filter
and a Hewlett Packard 1743A dual-time interval oscilloscope were substituted for the electronics unit and oscilloscope usually employed with the USI-103 Velocimeter (Fig. 5). These substitutes increased resolution of compressional wave velocity measurements and provided accurate measurement of receiver voltages required for attenuation measurements.

The temperature of the cylindrical subcores was equilibrated with laboratory temperature prior to measurement of compressional wave velocity ($V_p$). Temperature and salinity of the overlying water were measured with a YSI Model 43TD temperature probe and a Guildline Instruments 8400A laboratory salinometer.

Sediment compressional wave velocity was determined using equation 1. All sound velocities were calculated at the common temperature, salinity, and pressure ($23^\circ$C, 35 o/oo, 1 atm) suggested by Hamilton (1971). All measurements taken with the USI-103 transducer-receiver head were made at 400 kHz. Attenuation measurements were calculated as $20 \log$ of the ratio of the received voltage through distilled water versus receiver voltage through sediment. Attenuation measurements were extrapolated to a 1-m path length and reported as dB/m at 400 kHz (Hamilton, 1972). Attenuation was also expressed as a sediment specific constant ($k$):

$$a = kf^n$$  \hspace{1cm} (2)

where $a$ is the attenuation of compression waves in sediment (dB/m), $f$ is the transmitted signal frequency (kHz), and $n$ is a measure of frequency dependence. If $n$ is assumed to be one (Hamilton, 1972), then the sediment specific constant ($k$) can be used to compare sediment attenuation to other sediment physical properties such as porosity and mean grain size without regard to the frequency at which the measurements were made.

Sediment shear strength was measured directly by a hand-held vane shear device in undisturbed box core samples and with a Wykeham-Farrance laboratory vane apparatus in cylindrical subcores. The hand-held vane shear device consisted of a 0-24 inch-ounce precision torque gauge equipped with a 1.89-cm high, 1.89-cm diameter or 2.54 x 2.54 cm vane, after the design of Dill and Moore (1965). The Wykeham-Farrance laboratory vane apparatus was equipped with a 1.26-cm high, 1.26-cm diameter vane. The torque required to shear the sediment was measured with both
Figure 5. Block diagram of sediment core compressional wave velocity and attenuation measuring system.
devices. The rotation rate for the Wykeham-Farrance vane was 84°/min, whereas the hand-held vane was rotated as slowly as possible, approximately 360°/min. Sediment shear strength ($\tau_f$) was calculated from the torque required to shear the sediment (T) and the height (H) and diameter (D) of the vane using the following formula from Monney (1974):

$$\tau_f = \frac{T}{\pi \left( \frac{H^2 D}{2} + \frac{D^3}{6} \right)} \quad (3)$$

Hand-held torque measurements were made without regard to the resistance of the vane shaft to rotation in the sediment. Measurements were made every inch after additional insertion of the vane and its 50-cm shaft. Torque measurements made with the Wykeham-Farrance vane do not include the resistance of the vane shaft as part of the measurement. Sediment was extruded from the subcore after each torque measurement exposing fresh undisturbed sediment for the next measurement.

Color descriptions of collected sediment were made with the aid of Munsell® Soil Color Charts (1975). Depth profiles of hue, value, and chroma were determined for sediments after removing a side of the box core. Depth profiles of color were also determined for sediments extruded from subcores after vane shear measurement.

Sedimentary/biological structure was revealed by X-raying sediments collected with acrylic rectangular subcores. Rectangular cores were constructed of two 3-mm thick acrylic sheets (36 x 44 cm) separated by 6-mm thick acrylic sides (3-cm width). One face was sealed with silicone sealant and held together with stainless steel machine screws; the other face was sealed with neoprene and stainless steel machine screws. Two 19-mm diameter holes in the top of the core were used for displacement of air during core insertion. The holes were closed by means of neoprene stoppers after sediment collection. Bottom edges of the cores were beveled to improve penetration. The bottoms of the cores were sealed with rectangular acrylic boxes lined with cellular neoprene. Rubber straps held the bottoms fast to the cores.

The rectangular cores were X-rayed by placing a 35.3 x 42.8 cm sheet of Kodak AA industrial X-ray film on the back of each core and exposing it to 50 kV, 20 ma for 30 sec with a Kramex PX-20N portable X-ray unit (Rhoads et al., 1977). For
safety purposes, cores were X-rayed in a 1.6-cm thick plywood box lined with 1.6-mm thick lead sheeting.

D. Laboratory Analysis

All cylindrical core samples not extruded for sediment shear strength measurements were refrigerated or frozen for subsequent laboratory analysis. Refrigerated cores were used in determining sediment porosity, grain size, and percent calcium carbonate (CaCO$_3$). Organic and nitrogen determinations were made on sediment from frozen cores.

Cores were sectioned at 2-cm intervals by extruding the sediment with a plunger and slicing the exposed sediment off with a spatula. Immediately after sectioning, subsamples of extruded sediment for porosity determinations were placed in preweighed aluminum pans, weighed, dried in an oven at 105°C for 24 hr, cooled in a desiccator, and reweighed. Percent water was calculated by dividing the weight of evaporated water (difference between wet and dried sediment weights) by the weight of the dried solids and multiplying by 100. Using an average grain density value of 2.65 for noncarbonate sediment (location 2) and 2.70 for carbonate sediments (locations 1 and 3), porosity values were determined from tables relating porosity to water content (Lambert and Bennett, 1972). The values were not corrected for the salinity of pore water.

Grain-size analysis of sediment was accomplished essentially as described by Folk (1965). The silt and clay fractions from 4 to 10 $\Phi$ (phi), however, were determined with a Micromeritics® Model 5000 Particle Size Analyzer rather than the standard pipette method. The sediment samples were soaked overnight in 200 ml of dispersant solution (2.5 g of sodium hexametaphosphate per liter of distilled water), then disaggregated by sonicating the sample with a cell disruptor for 12 min while stirring with a magnetic stirrer. The disaggregated sample was wet-sieved with dispersant through a 62-μm screen to separate the sand-sized fraction from the silt- and clay-sized fraction. The finer fraction was collected in a 1000-ml graduated cylinder, and enough dispersant was added to fill the graduated cylinder to 1000 ml. The coarser fraction was rinsed off the screen into a beaker with distilled water and then dried.
The dried, coarser fraction was fractionated into -3 to -2, -2 to -1, -1 to 0, 0 to 1, 1 to 2, 2 to 3, and 3 to 4 φ intervals with an ATM sonic sifter and each fraction was individually weighed to determine the sand-sized particle distribution. The silt- and clay-sized fraction was thoroughly agitated by vigorous stirring and aeration. A 20-ml aliquot sample representative of the total distribution of particles in suspension was pipetted from the graduated cylinder and into a preweighed beaker, dried in an oven, and weighed. After 5 days, 20-ml aliquot samples were pipetted from the appropriate depths in the graduated cylinder and into preweighed beakers, dried, and weighed to estimate the weight of clay-sized particles in the 10 to 11, 11 to 12, and 12 to 14 φ intervals. At the conclusion of six days of settling, all particles 10 φ and coarser were near the bottom of the graduated cylinder. At this time the supernatant was slowly siphoned into another graduated cylinder, leaving the settled particles and about 200 ml of dispersant. The supernatant volume was recorded. A 20-ml aliquot sample was pipetted from the supernatant after agitation, dried, and weighed to estimate the weight of the particles finer than 10φ. Finally, the sample remaining in the graduated cylinder was sonicated and stirred for 12 minutes in a beaker prior to size determination with the Micromeritics® analyzer. This particle size analyzer determines the concentration of silt- and clay-sized particles in liquid suspension at various depths in a sample cell by means of a finely-collimated, horizontal X-ray beam. The concentration was presented in the form of a cumulative "percent-finer-than" distribution trace in relation to the Stokesian diameter of the particles.

Sediment grain size distributions were analyzed with an HP 9825A desktop computer and plotted with an HP 9862A plotter (unpublished program is available on request from MDR). Data were plotted as weight percent histograms and cumulative weight percent for all phi-sizes through 14 φ. The fraction finer than 12 φ was equally divided between the 12 to 13 φ and 13 to 14 φ intervals. Percentages of gravel (< -1.0 φ), sand (-1.0 to 4.0 φ), silt (4.0 to 8.0 φ), and clay (> 8.0φ) were tabulated. The mean phi, standard deviation, skewness, kurtosis, and normalized kurtosis were calculated according to the graphic formula of Folk and Ward (1957).

Percent CaCO₃ analysis was accomplished with a gasometric apparatus based on the design of Hulsemann (1966). Sediment subsamples were dried at 105°C for 24 hr,
ground in a mortar and pestle, and stored in a desiccator prior to analysis. A weighed portion (200-500 mg dry weight) of the subsample was added directly to a flask from the weighing paper, and the amount of sediment adhering to the paper was subtracted to obtain the exact weight. A magnetic stir bar was added to the flask, and the flask was attached to the apparatus by means of a silicone-greased, ground-glass connection and secured with a joint clamp. Next, a side arm with 5 ml of 4N hydrochloric acid (HCl) was attached in the same manner to the apparatus above the sample flask, and the system was closed off from atmospheric pressure by means of a three-way stopcock. Negative pressure in the system was created by lowering an open flask of mercury connected to a 100-ml burette. After the side arm containing the acid was rotated emptying its contents into the sample flask, the acidified sample was mixed with a magnet and heated with a Bunsen burner until the liquid bubbled up the sides of the flask. The system was allowed to come to thermal equilibrium with laboratory temperature before the mercury manometer was adjusted and the reading recorded. Barometric pressure was noted and recorded before and after each sample run. Two CaCO₃ standards were run at the beginning of the day to test for leaks in the system.

The volume of gas (CO₂) released was corrected to standard temperature and pressure and converted to carbonate as CaCO₃ by means of the formula:

\[
\frac{VP}{TW} \times 0.1605 = \% \text{CaCO}_3
\]

where \(V\) = observed volume of CO₂, \(P\) = corrected pressure, \(T\) = room temperature (°K), and \(W\) = weight of the sample in grams. Gas pressure was corrected for barometric pressure, water vapor pressure, and temperature. Duplicates from each depth in the core were analyzed. If values of duplicates differed by more than 2%, another replicate was run.

Frozen sediment cores for organic carbon and nitrogen analysis were thawed before extruding and sectioning at 2-cm intervals. Care in sectioning and sampling the core was exercised so that organic contamination (e.g. plastic core liner) was not introduced. The samples of the cores were refrozen and stored until analysis at a later date.
Thawed sediment samples were added to preweighed, precombusted (475°C) beakers and dried at 90°C for 24 hr. After cooling in a desiccator the samples were reweighed and ground to a fine powder in a clean mortar and pestle. Calcium carbonate was removed from the samples by adding excess (approx. 110%) 4N HCl. The amount of acid added was determined a priori from percent CaCO₃ analysis of separate sediment cores. After 12 hr, the acidified samples were brought to seawater pH (8.2) by adding 8N sodium hydroxide (NaOH). A Corning Model 125 pH meter with a calomel reference electrode (ceramic-type junction) was used to monitor pH. Samples were dried at 90°C for 24-36 hr, cooled in a desiccator, then weighed to determine the reacted weight. Finally, the dried samples were ground in a clean mortar and pestle, added to clean vials, sealed, and weighed.

Immediately before weighing a subsample of finely-ground sediment for analysis, the vial was weighed again to correct for absorbed water. Any additional weight due to water absorption was added to the reacted weight value. The subsample (20,000-45,000 µg) was weighed in a precombusted (475°C) aluminum boat and loaded into a Perkin-Elmer Model 240 CHN analyzer for determination of organic carbon and nitrogen. Duplicates from each depth in the core were analyzed. Additional replicates were run if values of duplicates differed by more than 2%.

III. RESULTS

The bulk of data in this report is presented in five appendices. Appendix A contains data on the following sediment acoustic and physical properties: compressional wave velocity \( V_p \), compressional wave velocity ratio \( V_p \) ratio, compressional wave attenuation \( k \), porosity, percent calcium carbonate \( \text{CaCO}_3 \), percent organic carbon \( \text{C} \), percent organic nitrogen \( \text{N} \), shear strength, percent sand, percent silt, percent clay, mean \( \phi \) (phi), standard deviation, skewness, kurtosis and normalized kurtosis. Sample designator consists of station number followed by subcore number (e.g. 3-4 designates the fourth subcore collected at station 3).

Appendix B contains frequency histograms of grain size distribution data. Grain size data were plotted as weight percent histograms and cumulative weight curves for phi sizes -4 through 14. Also included are percentage gravel, sand,
silt, and clay and mean phi, standard deviation, skewness, kurtosis, and normalized kurtosis.

X-radiographs of sediments collected with the 36 x 44. x 3 cm rectangular subcores are presented in Appendix C. X-radiographs depict sedimentary/biological structure from eight stations and include X-radiographs from all three locations. Images are "positives" produced from the developed X-ray transparency, and thus darker areas of the X-radiograph denote areas of greater sediment density.

Color descriptions of sediments are presented in Appendix D. Color descriptions are depicted as both Munsell® hue/value/chroma designations and soil color names. The "hue" refers to red, yellow, green, blue, and purple. The "value" refers to lightness. The "chroma" refers to strength (departure from a neutral of the same lightness). All descriptions are for sediments collected with subcores except at station 31 where the color was described from a freshly opened box core.

Compressional wave velocity probe measurements are presented in Appendix E.

Appendix F contains sediment shear strength values measured with the hand-held vane shear device.

IV. REFERENCES


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Appendix A

Sediment Acoustic and Physical Property Data
From Box Cores Collected in the Venezuela Basin

Compressional wave velocity ($V_p$, m/sec), compressional wave velocity ratio ($V_p$ ratio), attenuation ($k$), porosity (%), percent calcium carbonate ($\text{CaCO}_3$), percent organic carbon ($C$), percent organic nitrogen ($N$), shear strength ($\text{g/cm}^2$), percent sand, percent silt, percent clay, mean $\phi$ (phi), standard deviation, skewness, kurtosis and normalized kurtosis for sediments collected with cylindrical subcores from box cores in the Venezuela Basin are presented. Sample designator consists of station number followed by subcore number (e.g. 3-4 designates the fourth subcore collected at station 3).
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Cruise: GYRE 79G-7   Sample: 3-6   Date: 11/15/79
Position: 15-14N; 69-14W   Depth: 3958m
Calculated for: 23.0 Deg-C   35.00 o/oo   0 m 400 kHz

| Depth (cm) | Vp (m/sec) | Vp Ratio | Attr. % | Foss. CaCO3 | C | N | Str. | Sand | Silt | Clay | Mean | Dev | Skew | Kurt | N. Kurt |
|------------|------------|----------|---------|-------------|---|---|------|------|------|------|------|------|------|------|-------|------|
| 0.0        | 1532.8     | 1.002    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 1.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      | 52.37 | 11.00 |
| 2.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 3.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 4.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 5.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 6.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 7.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 8.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 9.0        | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 10.0       | 1493.3     | 0.976    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 11.0       | 1493.3     | 0.976    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 12.0       | 1493.3     | 0.976    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 13.0       | 1493.3     | 0.976    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 14.0       | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 15.0       | 1493.3     | 0.976    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 16.0       | 1485.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 17.0       | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 18.0       | 1489.5     | 0.974    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 19.0       | 1485.6     | 0.971    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 20.0       | 1485.6     | 0.971    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 21.0       | 1481.8     | 0.969    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 22.0       | 1481.8     | 0.969    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 23.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 24.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 25.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 26.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 27.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 28.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 29.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 30.0       | 1478.1     | 0.966    |         |             |   |   |      |      |      |      |      |      |      |       |       |
| 31.0       | 1481.8     | 0.965    |         |             |   |   |      |      |      |      |      |      |      |       |       |
### Cruise: GYRE 79G-7  Sample: 3-7  Date: 11/15/79
### Position: 15-14N:69-14W  Depth: 3958m
### Calculated for: 23.0 Deg-C 35.00 σ/CO

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Position: 15-13H; 65-17W  Depth: 3958m
Calculated for: 23.0 Deg-C  35.00 o/co  0 m  460 kHz

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Calculated for: 23.0 Deg-C 35.00 c/oo  0 m 400 Khz

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Position: 13-50N; 67-39W  Depth: 5054m
Calculated for: 23.0 Deg-C  15.00 o/oo  0 m  400 kHz

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Position: 13-50N; 67-39W  Depth: 5054m
Calculated for: 23.0 Deg-C  35.00 °/oo  0 m 400 kHz

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Cruise: LYNCH 708-80  Sample: 14-15  Date: 7/23/80
Position: 13-5N;67-39W  Depth: 5054m
Calculated for: 23.0° C  35.00 o/oo  0 m 400 kHz
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Cruise: LYNCH 708-80  Sample: 14-17  Date: 7/23/80
Position: 13-50N; 67-39W  Depth: 5054m
Calculated for: 23.0 Deg-C  15.00 o/oo  0 m  400 kHz

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Calculated for: 23.0 Deg-C 35.00 g/oo
0 m 400 kHz

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Position: 13-45;N67-40W  Depth: 5054m
Calculated for: 23.0 Deg-C 35.00 g/oo  0 m 400 kHz

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Cruise: LYNCH 708-80  Sample: 16-4  Date: 7/24/80
Position: 13-45N 67-40W  Depth: 5054m
Calculated for: 23.0 Deg-C  35.00 d/oo  0 m  400 kHz

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Cruise: LYNCH 708-80  Sample: 16-5  Date: 7/24/80
Position: 12-45N;67-40W  Depth: 5054 m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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### Cruise: LYNCH 708-80  
Sample: 16-6  
Date: 7/24/80  
Position: 13-45N; 67-40W  
Depth: 5054m  
Estimated Temp: 23.0 Deg-C  
Estimated Salinity: 35.00 a/o  
Estimated Depth: 0 m 400 kHz

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Position:  13-45N;67-40W  Depth:  5054m  
Calculated for:  23.0  Deg-C  35.00 oeo  0 m 400 kHz  

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Cruise: LYNCH 708-80  Sample: 16-8  Date: 7/24/80
Position: 13-45N; 67-40W  Depth: 5054m
Calculated for: 23.0 Deg-C  35.00 a/o
          0 m  400 kHz

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Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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Calculated for: 23.0 Deg-C  35.00 d/oo  0 m 400 kHz

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Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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**Sample:** 24-4  
**Date:** 10/19/81  
**Position:** 15-06N; 69-24W  
**Depth:** 3936m  
**Calculated for:** 23.0 Deg-C  
**35.00 o/oo**  
**0 m 400 kHz**

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Position: 15-06N;69-24W  Depth: 3936m
Calculated for: 23.0 Deg-C  35.00 d/oo  0 m 400 kHz

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Cruise: BARTLI 1301-82  Sample: 24-7  Date: 10/19/81
Position: 15-06N;69-24W  Depth: 3936m
Calculated for: 23.0 Deg-C  35.00 g/oo
0 m  400 kHz

| Depth (cm) | Vp | Vp Ratio | Attn | k | Por. CaCO3 | C | N | Str. | Sand | Silt | Clay | Phi | Mean | Dev | Skew | Kurt | N. Kurt |
|------------|----|----------|------|---|------------|---|---|------|------|------|------|-----|-----|-----|-----|-----|------|-------|
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| 1.0        | 1517.2 | 0.992    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 2.0        | 1513.0 | 0.989    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 3.0        | 1508.9 | 0.987    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 4.0        | 1504.6 | 0.984    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 5.0        | 1500.7 | 0.981    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 6.0        | 1500.7 | 0.981    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 7.0        | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 8.0        | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 9.0        | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 10.0       | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
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| 12.0       | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 13.0       | 1499.6 | 0.981    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 14.0       | 1498.9 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 15.0       | 1498.5 | 0.980    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 16.0       | 1497.8 | 0.979    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 17.0       | 1497.8 | 0.979    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 18.0       | 1496.3 | 0.978    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 19.0       | 1495.2 | 0.978    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 20.0       | 1493.0 | 0.976    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 21.0       | 1493.0 | 0.976    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 22.0       | 1491.5 | 0.975    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 23.0       | 1491.5 | 0.975    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 24.0       | 1492.3 | 0.976    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 25.0       | 1491.2 | 0.975    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 26.0       | 1489.0 | 0.974    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 27.0       | 1491.2 | 0.975    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 28.0       | 1489.7 | 0.974    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 29.0       | 1490.8 | 0.975    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 30.0       | 1487.5 | 0.973    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 31.0       | 1485.4 | 0.971    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 32.0       | 1488.6 | 0.973    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
| 33.0       | 1488.6 | 0.973    |      |   |            |   |   |      |      |      |      |     |     |     |     |       |       |
Cruise: BARTLET 1301-02  Sample: 24-8-2  Date: 10/19/81
Position: 15-06N 69-24W  Depth: 3936m
Calculated for: 23.0° Deg-C  35.00 oo  0 m  400 kHz

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Depth: 3936 m    0 m 400 kHz

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### Sediment Properties

**Cruise:** BAKLT 1301-82  
**Sample:** 24-8-5  
**Date:** 10/19/81  
**Position:** 15-06N, 69-24W  
**Depth:** 3936m

**Calculated for:** 23.0 Deg-C 35.00 o/oo  
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### Ultrasonic Borehole Geophysical Data

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**Sample:** 29-3  
**Date:** 10/23/81  
**Position:** 15-03n65-21w  
**Depth:** 3959m  
**Temperature:** 35.00 °C  
**Depth:** 400 kHz  

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Cruise: BARTLE 1301-82  
Sample: 30-3  
Date: 10/23/81

Position: 15-09N;69-34W  
Depth: 3945m

Calculated for: 23.0 Deg-C  
0 m 400 kHz

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Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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Cruise: BARTT 1301-82  Sample: 43-2  Date: 10/29/81
Position: 14-45N; 66-52W  Depth: 449m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz
### Cruise: U.S.R.L. 1301-82  Sample: 43-3  Date: 10/29/81
Position: 14-45'68-52W  Depth: 4493m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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Cruise: BARTLT 1301-82  Sample: 44-13  Date: 10/30/81
Position: 14-19N 68-22W  Depth: 4805m
Calculated for: 23.0 Deg-C  35.00 g/oo  0 m 400 kHz

Mean: ___  Dev: ___  Skew: ___  Kurt: ___  N. Kurt: ___
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Date: 10/30/81  
Position: 14-19N, 68-22W  
Depth: 4805 m  
0 m 400 kHz

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Cruise: BARTLT 1301-82  
Sample:  48-4  
Date: 11/01/81  
Position:  13-44N; 67-48W  
Depth:  5049m  
Calculated for:  23.0 Deg-C  
0 m  400 kHz

| Depth (cm) | Vp (m/sec) | Vp Ratio | Attenu. (k) | % For. CaCO3 | % C | % N | % Shear | % Str. | % Sand | % Silt | % Clay | Mean | Dev | Skew | Kurt | Kurt |
|------------|------------|----------|-------------|--------------|-----|-----|--------|--------|--------|--------|--------|-------|------|------|------|------|------|
| 1.0        | 1506.8     | 0.985    | 0.330       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 2.0        | 1502.7     | 0.983    | 0.294       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 3.0        | 1491.7     | 0.979    | 0.232       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 4.0        | 1489.3     | 0.976    | 0.167       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 5.0        | 1489.1     | 0.971    | 0.144       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 6.0        | 1489.9     | 0.974    | 0.123       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 7.0        | 1489.6     | 0.974    | 0.112       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 8.0        | 1489.9     | 0.974    | 0.112       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 9.0        | 1490.6     | 0.975    | 0.093       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 10.0       | 1491.0     | 0.975    | 0.102       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 11.0       | 1494.7     | 0.977    | 0.114       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 12.0       | 1506.8     | 0.985    | 0.218       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 13.0       | 1506.1     | 0.985    | 0.144       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 14.0       | 1514.3     | 0.990    | 0.218       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 15.0       | 1514.7     | 0.990    | 0.391       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 16.0       | 1506.4     | 0.965    | 0.312       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 17.0       | 1506.4     | 0.965    | 0.312       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 18.0       | 1504.0     | 0.994    | 0.439       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 19.0       | 1504.0     | 0.994    | 0.439       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 20.0       | 1502.7     | 1.016    | 0.696       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 21.0       | 1502.7     | 1.016    | 0.696       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 22.0       | 1500.7     | 1.001    | 0.580       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 23.0       | 1486.7     | 0.972    | 0.083       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 24.0       | 1485.6     | 0.971    | 0.093       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 25.0       | 1485.2     | 0.971    | 0.093       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 26.0       | 1486.3     | 0.972    | 0.065       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 27.0       | 1487.4     | 0.973    | 0.056       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 28.0       | 1489.6     | 0.974    | 0.048       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 29.0       | 1492.1     | 0.976    | 0.048       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 30.0       | 1492.1     | 0.976    | 0.048       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 31.0       | 1503.1     | 0.983    | 0.102       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 32.0       | 1506.4     | 0.985    | 0.093       |              |     |     |        |        |        |        |        |       |      |      |      |      |
| 33.0       | 1494.3     | 0.977    | 0.074       |              |     |     |        |        |        |        |        |       |      |      |      |      |
Cruise: BARTLT 1301-82    Sample: 48-5    Date: 11/01/81
Position: 13-44N;67-48W    Depth: 5049m
Calculated for: 23.0 Deg-C 35.00 o/oo

| Depth (cm) | Vp m/sec | Vp Ratio | Attn. k | % For. CaCO3 | % C | % N | % Str. | % Sand | % Silt | % Clay | Phi Mean Dev | Skew Kurt N. Kurt |
|------------|----------|----------|---------|--------------|-----|-----|-------|--------|--------|--------|----------|----------------|------------------|
| 15.0       | 1525.2   | 0.997    | 0.391   |              |     |     |       |        |        |        |           |                  |
| 16.0       | 1520.7   | 0.994    | 0.391   |              |     |     |       |        |        |        |           |                  |
| 17.0       | 1520.3   | 0.994    | 0.391   |              |     |     |       |        |        |        |           |                  |
| 18.0       | 1521.1   | 0.995    | 0.370   |              |     |     |       |        |        |        |           |                  |
| 19.0       | 1529.4   | 1.000    | 0.439   |              |     |     |       |        |        |        |           |                  |
| 20.0       | 1541.8   | 1.008    | 0.604   |              |     |     |       |        |        |        |           |                  |
| 21.0       | 1553.9   | 1.016    | 0.573   |              |     |     |       |        |        |        |           |                  |
| 22.0       | 1544.9   | 1.010    | 0.531   |              |     |     |       |        |        |        |           |                  |
| 23.0       | 1541.8   | 1.008    | 0.588   |              |     |     |       |        |        |        |           |                  |
| 24.0       | 1554.7   | 1.017    | 1.066   |              |     |     |       |        |        |        |           |                  |
| 25.0       | 1499.8   | 0.981    | 1.066   |              |     |     |       |        |        |        |           |                  |
| 26.0       | 1493.2   | 0.976    | 0.278   |              |     |     |       |        |        |        |           |                  |
| 27.0       | 1486.3   | 0.972    | 0.074   |              |     |     |       |        |        |        |           |                  |
| 28.0       | 1485.9   | 0.972    | 0.065   |              |     |     |       |        |        |        |           |                  |
| 29.0       | 1485.9   | 0.972    | 0.065   |              |     |     |       |        |        |        |           |                  |
| 30.0       | 1486.7   | 0.972    | 0.048   |              |     |     |       |        |        |        |           |                  |
| 31.0       | 1488.1   | 0.973    | 0.031   |              |     |     |       |        |        |        |           |                  |
| 32.0       | 1493.2   | 0.976    | 0.048   |              |     |     |       |        |        |        |           |                  |
| 33.0       | 1503.1   | 0.983    | 0.123   |              |     |     |       |        |        |        |           |                  |
Cruise: HARTLT 1301-82  Sample: 48-6  Date: 11/01/81
Position: 13-44N;67-48W  Depth: 5049m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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Calculated for: 23.0 Deg-C  35.00 o/oo
0 m 400 kHz

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Position: 13-44N; 67-48W   Depth: 5049m
Calculated for: 23.0 Deg-C   35.00 a/co
              0 m 400 kHz

<p>| Depth (cm) | Vp  | Vp  | Attenuation | % Por. CaCO3 | % C | % N | % Str. Sand | % Silt | % Clay | % Mean | % Dev | % Skew | Kurt | N |
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| 36.0       | 1506.1 | 0.985 | 0.638       |              |     |     |             |        |        |        |       |       |      | 100 |
| 37.0       | 1531.4 | 1.001 | 0.740       |              |     |     |             |        |        |        |       |       |      | 100 |</p>
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Position: 134N;6748W  Depth: 5049m
Calculated for: 23.0 Deg-C  35.00 o/o

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Position: 13°-47N;67°-47W  Depth: 5049m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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Sample: 53-18  
Date: 11/03/81  
Position: 13-47N; 67-47W  
Depth: 5049m  
Cruise for: 23.0 Deg-C  
35.00 g/oo  
Depth: 0 m 400 kHz

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**Cruise:** BARTLE 1301-82  **Sample:** 53-19  **Date:** 11/03/81  
**Position:** 13-47N;67-47W  **Depth:** 5049m  
**Calculated for:** 23.0 Deg-C  **45.00 g/oo**  
**0 m 400 kHz**
| Depth (cm) | Vp  | Vp Ratio | Attn. k | Por. | CaCO3 | C | N | Shear | Str. | Sand | Silt | Clay | Mean | Dev | Skew | Kurt | N. Kurt |
|-----------|-----|----------|---------|------|-------|---|---|-------|------|------|------|------|------|------|-----|-------|------|---------|
| 17.0      | 1497.9 | 0.979    | 0.179   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 18.0      | 1511.7 | 0.988    | 0.400   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 19.0      | 1528.0 | 0.999    | 0.518   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 20.0      | 1537.3 | 1.005    | 0.573   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 21.0      | 1527.6 | 0.999    | 0.471   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 22.0      | 1526.5 | 0.998    | 0.439   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 23.0      | 1526.5 | 0.998    | 0.439   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 24.0      | 1552.6 | 1.015    | 0.851   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 25.0      | 1554.2 | 1.016    | 0.820   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 26.0      | 1534.6 | 1.003    | 0.765   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 27.0      | 1533.4 | 1.003    | 0.765   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 28.0      | 1550.2 | 1.014    | 0.765   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 29.0      | 1549.4 | 1.013    | 0.638   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 30.0      | 1489.5 | 0.974    | 0.391   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 31.0      | 1484.8 | 0.971    | 0.102   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 32.0      | 1484.4 | 0.971    | 0.093   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 33.0      | 1484.4 | 0.971    | 0.102   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 34.0      | 1484.1 | 0.970    | 0.102   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 35.0      | 1480.5 | 0.968    | 0.093   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 36.0      | 1485.5 | 0.971    | 0.083   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 37.0      | 1481.2 | 0.968    | 0.083   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 38.0      | 1487.7 | 0.973    | 0.133   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
| 39.0      | 1491.0 | 0.975    | 0.391   |      |       |   |   |       |      |      |      |      |      |      |      |       |       |
Cruise: BARTLT 1301-82  Sample:  53-21  Date: 11/03/81
Position: 13-47N;67-47W  Depth: 5049m
Calculated for: 23.0 Deg-C  35.00 o/oo
0 m 400 kHz

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Calculated for: 23.0 Deg-C  35.00 o/oo  0 m 400 kHz

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1.0 | 0.831 | 0.178 |
<p>| Depth (cm) | Vp (m/sec) | Vp Ratio | Attn. k | % For. CaCO3 | C | % N | % Shear | % Str. | Sand | Silt | Clay | % Phi | % Mean Dev | Skew | Kurt | N. Kurt |
|------------|------------|-----------|---------|---------------|---|-----|--------|-------|------|------|------|------|------|--------|------|------|--------|
| WATER      | 1530.4     | 1.001     | -0.015  |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 0.0        | 1529.6     | 1.000     | -0.015  |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 1.0        | 1513.3     | 0.989     | 0.140   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 2.0        | 1503.2     | 0.983     | 0.140   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 3.0        | 1503.2     | 0.983     | 0.097   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 4.0        | 1494.0     | 0.977     | 0.097   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 5.0        | 1492.6     | 0.976     | 0.097   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 6.0        | 1492.6     | 0.976     | 0.087   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 7.0        | 1491.8     | 0.975     | 0.078   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 8.0        | 1490.4     | 0.975     | 0.068   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 9.0        | 1490.4     | 0.974     | 0.050   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 10.0       | 1489.7     | 0.974     | 0.059   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 11.0       | 1489.7     | 0.974     | 0.050   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 12.0       | 1489.7     | 0.974     | 0.068   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 13.0       | 1489.7     | 0.974     | 0.050   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 14.0       | 1489.7     | 0.974     | 0.050   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 15.0       | 1492.6     | 0.976     | 0.050   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 16.0       | 1493.7     | 0.977     | 0.070   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 17.0       | 1493.3     | 0.976     | 0.078   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 18.0       | 1493.3     | 0.976     | 0.068   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 19.0       | 1493.3     | 0.976     | 0.078   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 20.0       | 1491.5     | 0.975     | 0.068   |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
| 21.0       |            |           |         |               |   |     |        |       |      |      |      |      |      |        |      |      |        |
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Cruise: HAKILT 1301-82  Sample: 69-10  Date: 11/18/81
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Calculated for: 23.0 Deg-C  35.00 o/oo
0 m  400 kHz

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Position: 13-33N; 65-24W  Depth: 3937m  
Calculated for: 23.0 Deg-C  35.00 c/oo  0 m  400 kHz  

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Position: 13-33N765-25W  Depth: 3937m
Calculated for: 23.0 Deg-C  35.00 o/oo  0 m  400 kHz

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### Data Table

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| 1.0        | 1495.9     | 0.978    | 0.164 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 2.0        | 1491.9     | 0.975    | 0.152 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 3.0        | 1490.8     | 0.975    | 0.152 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 4.0        | 1489.7     | 0.974    | 0.140 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 5.0        | 1488.6     | 0.973    | 0.140 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 6.0        | 1488.2     | 0.973    | 0.118 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 7.0        | 1487.9     | 0.973    | 0.097 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 8.0        | 1487.9     | 0.973    | 0.087 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 9.0        | 1487.9     | 0.973    | 0.087 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 10.0       | 1487.2     | 0.972    | 0.087 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 11.0       | 1486.6     | 0.972    | 0.087 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 12.0       | 1489.0     | 0.974    | 0.129 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 13.0       | 1491.2     | 0.975    | 0.190 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 14.0       | 1491.2     | 0.975    | 0.177 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 15.0       | 1487.9     | 0.973    | 0.140 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 16.0       | 1487.9     | 0.973    | 0.108 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 17.0       | 1486.4     | 0.972    | 0.087 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 18.0       | 1486.4     | 0.972    | 0.068 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 19.0       | 1486.8     | 0.972    | 0.059 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 20.0       | 1490.4     | 0.975    | 0.108 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 21.0       | 1490.4     | 0.975    | 0.097 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 22.0       | 1490.1     | 0.974    | 0.108 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
| 23.0       | 1489.3     | 0.974    | 0.129 |        |       |     |     |       |       |        |        |        |       |      |     |      |        |
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Position: 13-32W 64-44W  Depth: 3503 m
Calculated for:  23.0°C  35.00°C
0 m 400 kHz

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Calculated for: 23.0 Deg-C 35.00 o/oo 0 m 400 kHz

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APPENDIX B

FREQUENCY HISTOGRAMS OF GRAIN SIZE DISTRIBUTION DATA
FOR SEDIMENTS COLLECTED IN BOX CORES FROM THE VENEZUELA BASIN

Grain size data are plotted as weight percent histograms and cumulative weight curves for phi sizes -4 through 14. Also included are percentage gravel, sand, silt, and clay and Folk and Ward's mean phi, standard deviation, skewness, kurtosis, and normalized kurtosis. Data include three stations from location 1, five stations from location 2, three stations from location 3, three stations along a transect from location 1 to location 2, and five stations along a transect from location 2 to location 3.

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APPENDIX C
X-RADIOGRAPHS OF SEDIMENTS COLLECTED
FROM THE VENEZUELA BASIN

X-radiographs of sediments collected with X-ray boxes from intact box cores are presented. X-radiographs depict sedimentary/biological structure from eight stations and include X-radiographs from all three locations. Images are "positives" produced from the developed X-ray transparency and thus darker areas of the X-radiograph denote areas of greater sediment density.

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Color descriptions are depicted as both Munsell® hue/value/chroma designations and soil color names. The "hue" refers to red, yellow, green, blue, and purple. The "value" refers to lightness. The "chroma" refers to strength (departure from a neutral of the same lightness). All descriptions were derived from subcores except at station 31 where the color was described from a freshly opened box core.
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APPENDIX E
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261
APPENDIX F
SEDIMENT SHEAR STRENGTH MEASURED
WITH HAND-HELD VANE SHEAR PROBE

Shear strength of sediments ($\tau_p$, g/cm²) was measured in undisturbed box cores with a 1.89 x 1.89 cm or a 2.54 x 2.54 cm vane. The larger vane was used at stations 23, 28, and 31 only.
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