MOHAWK RIVER BASIN
TOWN OF GERMAN FLATTS
HERKIMER COUNTY, NEW YORK

ILI ON RESERVOIR
NO. 1 DAM
NY 00186

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

DEPARTMENT OF THE ARMY
NEW YORK DISTRICT, CORPS OF ENGINEERS
26 FEDERAL PLAZA
NEW YORK, NY 10278

JULY 1981
DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.
This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization.

Examination of available documents and visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life or property. However, the dam has some deficiencies which require further investigation and remedial work.
The downstream slope of the dam is about 1.5H:1V, which is considerably steeper than that of similar dams designed in accordance with modern standards of practice. Therefore, it is recommended that a stability investigation of the embankment, with particular attention to the steepness of the downstream slope, be started within 6 months after receipt of this report by the Owner. Any necessary remedial work should be completed within 18 months after receipt of this report by the Owner. The investigation and the design and construction observation of any remedial work should be done by a qualified, registered professional engineer.

Hydrologic and hydraulic analysis indicates that the PMF overtops the embankment. The 1/2 PMF, however, does not overtop the embankment. Therefore, in accordance with Corps of Engineers' screening criteria for review of spillway adequacy, spillway capacity is considered "inadequate", but not seriously inadequate.
PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The Phase I Investigation does not include an assessment of the need for fences, gates, no-trespassing signs, repairs to existing fences and railings and other items which may be needed to minimize trespass and provide greater security for the facility and safety to the public. An evaluation of the project for compliance with OSHA rules and regulations is also excluded.
# ILION RESERVOIR NO. 1 DAM, NY 00186

**PHASE I INSPECTION REPORT**

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Identification No.: NY 00186
Name of Dam: Ilion Reservoir No. 1 Dam
State Located: New York
County: Herkimer
Municipality: Town of German Flatts
Watershed: Mohawk River Basin
Stream: Offstream of tributary of Steele Creek
Date of Inspection: June 4, 1981

ASSESSMENT

Examination of available documents and visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life or property. However, the dam has some deficiencies which require further investigation and remedial work.

The downstream slope of the dam is about 1.5H:1V, which is considerably steeper than that of similar dams designed in accordance with modern standards of practice. Therefore, it is recommended that a stability investigation of the embankment, with particular attention to the steepness of the downstream slope, be started within 6 months after receipt of this report by the Owner. Any necessary remedial work should be completed within 18 months after receipt of this report by the Owner. The investigation and the design and construction observation of any remedial work should be done by a qualified, registered professional engineer.

Hydrologic and hydraulic analysis indicates that the PMF overtops the embankment. The 1/2 PMF, however, does not overtop the embankment. Therefore, in accordance with Corps of Engineers' screening criteria for review of spillway adequacy, spillway capacity is considered "inadequate", but not seriously inadequate.

Because of other deficiencies, the following additional investigations should be started within 6 months after receipt of this report by the Owner. The investigations should be performed by a qualified, registered professional engineer.
1) Investigate the seepage at the downstream toe of the dam.

2) Investigate the cracked and displaced condition of the retaining wall at the downstream toe of the dam.

Any remedial work deemed necessary as a result of these investigations should be completed within 18 months after receipt of this report by the Owner. A qualified, registered professional engineer should design and observe the construction of any necessary remedial work.

The following remedial work should be completed by the Owner within 12 months after his receipt of this report. Where engineering assistance is indicated, the Owner should engage a qualified, registered professional engineer. Assistance by such an engineer may also be useful for some of the other work.

1) Institute a program to visually inspect - not just casually look at - the dam and its appurtenances at least once a month.

2) Repair the deteriorated spillway outlet structure and repair the lesser deterioration of some of the stone masonry on the spillway structure itself.

3) Remove trees, brush, and their root systems from the slopes of the embankment and to a distance of 20 feet downstream from the toe in accordance with specifications and field observation of the work by an engineer. Fill resulting holes with properly selected, compacted fill. Continue to keep these same areas and the crest of the dam clear by cutting, mowing, and cleanup at least annually.

4) Backfill animal burrows on the slopes of the embankment with properly selected, compacted fill.

5) Prepare written routine operation and maintenance procedures for the dam and its appurtenances.

6) Institute a program of comprehensive technical inspection of the dam and its appurtenances by an engineer on a periodic basis of at least once every two years.

7) Develop an emergency action plan outlining action to be taken to minimize the downstream effects of an emergency, together with an effective warning system.
Overview Photo - Illion Reservoir No. 1 Dam from upstream - 6/4/81
1.1 GENERAL

a. Authority

The National Dam Inspection Act, Public Law 92-367, August 8, 1972, authorized the Secretary of the Army through the Corps of Engineers to initiate a national program of dam inspection throughout the United States. The New York District of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within New York State. C. T. Male Associates, P.C., has been retained by the New York District to inspect and report on selected dams in the State of New York. Authorization and notice to proceed was issued to C. T. Male Associates, P.C., under a letter from Michael A. Jezior, LTC, Corps of Engineers. Contract No. DACW51-81-C-0014 has been assigned by the Corps of Engineers for this work.

b. Purpose of Inspection

The purpose of the inspection program is to perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public, and thus permit correction in a timely manner by non-Federal interests.

1.2 DESCRIPTION OF PROJECT

a. Location

The dam is located offstream of an unnamed tributary of Steele Creek about 1.7 miles southwest of the Village of Ilion. The dam at its maximum section is at Latitude 42 degrees - 59.6 minutes North, Longitude 75 degrees - 3.3 minutes West.

Access to the dam is from Interstate 90 (New York State Thruway) to the north, then west via State Route 5S to the Village of Ilion, then south from Ilion via State Route 51 to Spinnerville Gulf Road (County Route 15), then south via Elizabethtown Road (County Route 105) to the dam. The dam and reservoir are located on the west side of the road (see Vicinity Map, and Drainage Area Map Appendix C-5).
b. Description of Dam and Appurtenances

Ilion Reservoir No. 1 Dam is an earthen embankment about 40 feet high, 270 feet long, and 12 feet wide at the crest, with upstream and downstream slopes of 2H:1V and 1.5H:1V, respectively. There is hand-placed riprap on the upstream slope up to an elevation about 2 feet above reservoir level. Available design drawings indicate that the dam has a stone masonry core wall and puddle core, and that the embankment consists of "fine selected material" on the upstream side and "coarse material" on the downstream side. Both abutments appear to be soil and there are no outcrops of bedrock in the vicinity of the dam.

There is a low earth dike, about 5 feet high and 30 feet long, in a saddle on the perimeter of the reservoir near the right abutment of the dam. The dike has a crest width of about 12 feet and upstream and downstream slopes of about 2H:1V. The top of dike is about at the same elevation as the top of dam.

The dam has an overflow spillway located on the shore of the reservoir near the right abutment. The spillway consists of a 5-foot-wide by 1-foot-high opening into a stone masonry and concrete vault with a slate slab on top. A culvert of unknown size exits the structure and runs about 300 feet down a steep slope to a stone masonry outlet structure. The outlet structure is located next to a ditch which runs along Elizabethtown Road.

The dam has two 16-inch-diameter cast iron pipes which exit from the toe of the dam. One of these pipes is an outlet pipe and the other is a blowoff. There are two valves on the outlet pipe, one located on the downstream slope in a valve box and another located downstream of the dam in a concrete vault with a manhole cover. The outlet pipe runs to the filter plant where it connects with a raw water supply main. The blowoff discharges into the bottom level of the filter plant control building. The valve on the blowoff is located here, with the operating handwheel for the valve located on the top floor of the filter plant control building.

The incoming supply line to the reservoir consists of a 10-inch pipe from Ilion Reservoir No. 2 which connects to an 8-inch pipe from Ilion Reservoir No. 3. Flow in this line can be controlled by 3 valves in series on the pipe near the reservoir. Flow into the pipe can also be controlled with valves at the upstream reservoirs.
c. **Size Classification**

In accordance with Recommended Guidelines (Reference 1), Ilion Reservoir No. 1 Dam is classified as "intermediate" in size because its height is about 40 feet (within the 40 to 100-foot range). The maximum storage capacity at top of dam is 63 acre-feet.

d. **Hazard Classification**

In accordance with Recommended Guidelines (Reference 1), Ilion Reservoir No. 1 Dam is classified as having a "high" hazard potential. This is because it is judged that failure of the dam would significantly increase flows downstream which could cause loss of more than a few human lives and appreciable property damage. Downstream development that could be damaged or destroyed by a dam failure includes: the water filtration plant with its various buildings located immediately downstream; portions of Spinnerville Gulf Road (County Route 15) and State Route 51; and the hamlet of South Ilion, with many dwellings, through which the unnamed tributary of Steele Creek runs about 1800 feet downstream of the dam (vertical drop from the dam to the hamlet is about 200 feet).

e. **Ownership**

The dam was originally constructed for the present owner in 1893. The dam and reservoir are owned by:

Village of Ilion Board of Water Commissioners  
P.O. Box 330  
Morgan Street  
Ilion, NY 13357

Attn: Charles R. Baker, Water Superintendent  
(315) 895-7711

f. **Operator**

Day-to-day operation of the dam is the responsibility of the Village Water Department. The heads of the department are the following:

Charles R. Baker, Water Superintendent  
Edward C. Allston, Assistant Water Superintendent  
(same address and phone as Owner above, for both)

Also, the Filter Plant Operator, Michael McCormack, (315) 894-9144, operates the reservoir appurtenances.

g. **Purpose**

The dam was originally constructed as a raw water supply impoundment for the Village of Ilion. It is still used for this purpose.
h. Design and Construction History

The dam was designed in 1891 and 1892 for the Village of Ilion. The designer was the Stanwix Engineering Company, Rome, New York, which is no longer in business. Data concerning the original design can be found in Appendices F2, F3, and G. The dam was constructed by a Mr. J. J. Rumsey of Fostoria, Ohio, whose business status is unknown.

There is no knowledge or record of any other construction, modification, or major repair of the dam. Refer to Section 2 of this report, as well as to the Engineering Data Checklist in Appendix F2, for a complete discussion of the design and construction history. Selected plans and other engineering data are included in Appendices F3 and G.

i. Normal Operating Procedures

The water filtration plant is located at the dam site. The Filter Plant Operator records the water level several times daily and the dam appurtenances are operated frequently. All of the valves on the outlet pipe at the dam are normally open and the blowoff is usually closed. Normal pool level is about one foot below the spillway crest. The raw water supply pipe to the reservoir is normally open.

1.3 PERTINENT DATA

a. Drainage Area (acres) 35.6

b. Discharge at Dam Site (cfs)
   Spillway (W.S. at top of dam) 42
   Outlet Pipe (maximum flow to filter plant) 1.5
   Blowoff (normally closed - estimated potential w/W.S. at Spillway Crest) 40
   Maximum Known Flood Unknown

c. Elevation (feet - NGVD)
   All elevations are based on elevations provided by the Owner (see Appendix F3-11) and from plans in Appendix G. They are assumed to be in feet above mean sea level NGVD (National Geodetic Vertical Datum of 1929). The elevations appear consistent with current USGS mapping.
   Top of Dam 732
   Design High Water Unknown
   Spillway Crest 728.5
   Normal Pool 727.5
   Entrance Invert of Outlet Pipe 700 +
   Entrance Invert of Blowoff 693 +
d. Reservoir Length (feet) - at spillway crest  400+

e. Reservoir Surface Area (acres)

<table>
<thead>
<tr>
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<th>Top of Dam</th>
<th>Spillway Crest</th>
<th>Normal Pool</th>
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<td>3.5+</td>
<td>2.7+</td>
<td>2.5</td>
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f. Reservoir Storage (acre-feet)

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<th>Top of Dam</th>
<th>Spillway Crest</th>
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<td>63</td>
<td>50</td>
<td>46</td>
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g. Dam

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<tr>
<td>Type</td>
<td>Earthen embankment.</td>
</tr>
<tr>
<td>Length</td>
<td>About 270 feet.</td>
</tr>
<tr>
<td>Height</td>
<td>About 40 feet.</td>
</tr>
<tr>
<td>Top Width</td>
<td>About 12 feet.</td>
</tr>
<tr>
<td>Side Slopes</td>
<td>Upstream - About 2H:1V. Downstream - About 1.5H:1V.</td>
</tr>
<tr>
<td>Zoning</td>
<td>&quot;Fine selected material&quot; in upstream half of embankment; &quot;coarse material&quot; in downstream half of embankment.</td>
</tr>
<tr>
<td>Impervious Core</td>
<td>Stone masonry core wall, with &quot;puddle&quot; against the upstream side of the wall.</td>
</tr>
<tr>
<td>Cutoff</td>
<td>Stone masonry core wall and puddle core extend 5 feet below original ground surface.</td>
</tr>
<tr>
<td>Grout Curtain</td>
<td>Unknown.</td>
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h. Spillway

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<tbody>
<tr>
<td>Type</td>
<td>Earthen embankment.</td>
</tr>
<tr>
<td>Length of Weir</td>
<td>About 5 feet.</td>
</tr>
<tr>
<td>Upstream Channel</td>
<td>Reservoir immediately upstream of overflow. Normal water level is one foot below overflow crest.</td>
</tr>
<tr>
<td>Downstream Channel</td>
<td>Culvert of unknown size from vault, about 300 feet down steep slope to stone masonry outlet structure at ditch near road.</td>
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i. Outlet Works

1) Outlet Pipe

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<tr>
<td>Size</td>
<td>16-inch diameter.</td>
</tr>
<tr>
<td>Description</td>
<td>Cast iron pipe from reservoir to filter plant.</td>
</tr>
<tr>
<td>Control</td>
<td>Valve in valve box on downstream slope and valve downstream of dam in concrete vault.</td>
</tr>
</tbody>
</table>

1-5
2) Blowoff
Size - 16-inch diameter.
Description - Cast iron pipe from reservoir discharging into bottom of filter plant control building.
Control - Valve in bottom of filter plant control building with handwheel control on upper level of building.
SECTION 2
ENGINEERING DATA

2.1 DESIGN DATA

a. Geology

There was no geologic information available in the data for this site. The following information was obtained from current geologic maps and publications for this region (References 26 and 27), as well as from the site visit.

Ilion Reservoir No. 1 Dam is located in the southern New York Section of the Appalachian Plateaus Province and lies on the northern slope of the dissected plateaus of that province. Bedrock in the vicinity of the reservoir consists of shales and siltstones of Upper Ordovician age. No maps are available showing the surficial geology.

b. Subsurface Investigations

No records of subsurface investigations are available for this dam site.

c. Dam and Appurtenances

The dam was designed in 1891 and 1892 by the Stanwix Engineering Company, Rome, New York, which is no longer in business. Some drawings concerning the original design can be found as Appendices G-1 to G-6.

Available design drawings call for a stone masonry core wall extending about 5 feet into the original ground with "puddle" about 5 feet wide against the upstream side of the core wall. The embankment material upstream of the puddle is described on the drawings as "fine selected material," and the embankment material downstream of the core wall is described as "coarse material."

2.2 CONSTRUCTION HISTORY

a. Initial Construction

The dam was constructed in 1892 and 1893 by J. J. Rumsey of Fostoria, Ohio, whose present business status is unknown. No records concerning the actual construction of the dam are known to exist.

A brief review of the construction history, as can be determined from the available data and the Owner, can be found on Appendix F2-2.
b. Modifications, Repairs, and Maintenance

There is no knowledge or record of any reconstruction, modification, or major repair of the dam. Some of the appurtenances are, however, different than some appearing on the original design drawings (see Appendices G-1 & G-3).

c. Pending Remedial Work

There are no known plans for any remedial work at the dam.

2.3 OPERATION RECORD

a. Inspections

There is no known record of inspection of the dam by the Owner.

The only inspection report found for the dam was one done by the NYS-DEC, dated October 19, 1971 (see Appendix F3-1). The report indicated that the dam was in satisfactory condition and received routine maintenance.

b. Performance Observations

Other than the observations made in the one inspection report found (see Appendix F3-1), there are no other known records of performance observations.

c. Water Levels and Discharges

The Filter Plant Operator checks and records the reservoir level several times each day in the plant daily log book. The daily log book has been kept for many years. Rainfall is measured from the period of April to November at the reservoir. The measurements are taken by the Filter Plant Operator and are available from 1948 to the present.

d. Past Floods and Previous Failures

There are no known past floods at or previous failures of the dam.

2.4 EVALUATION

a. Availability

As listed on Appendix F1, various engineering data and records are available in the files of the Owner and the Dam Safety Section of the NYS-DEC. This data was reviewed, and copies of the records significant to the dam are included in chronological
order in Appendices F3 and G. Appendix F2, Checklist for General Engineering Data and Interview with Dam Owner, also contains pertinent engineering information.

b. Adequacy

Available data consisted of some design/construction drawings, an inspection report, and data from the Owner on the dam and its history. Such data as design calculations, specifications, complete design drawings, record drawings, complete data on foundation and embankment soils, and operation and performance data were not available. The lack of such in-depth engineering data does not permit a comprehensive review. Therefore, the available data was not adequate by itself to permit an assessment of the dam.

c. Validity

It is not possible to determine on the basis of the visual inspection alone whether the embankment section was built in accordance with the design drawings. The elevation of the top of the dam is about 1/2 a foot higher than the elevation for top of dam shown on Appendix G-4. The design drawings (see Appendix G-1, G-3 and G-4) also show some appurtenances which are different than some which presently exist.
SECTION 3
VISUAL INSPECTION

3.1 FINDINGS

a. General

Ilion Reservoir No. 1 Dam was inspected on June 4, 1981. The inspection party (see Appendix B-1) was accompanied by: Mr. Charles Baker, Water Superintendent; Mr. Edward Allston, Assistant Superintendent; and Mr. Michael McCormack, Filter Plant Operator, all representing the Owner. The weather was cloudy and warm. The water surface was about 1.4 feet below the spillway crest, or at about EL 727.1, at the time of the inspection. The Visual Inspection Checklist is included as Appendix B, while selected photos taken during the inspection are included as Appendix A and as the Overview Photo at the beginning of this report. Appendix A-1 is a photo index map.

b. Dam and Dike

1) Dam

There were no major sloughs or slides evident on the embankment.

Crest - The crest of the dam is covered with grass which is kept mowed (see Photo A-2A). Many tree roots extend across the top of the crest, from trees on the downstream slope to the upstream side of the crest (see Photo A-2B). The crest appears to be well maintained and shows no signs of settlement, cracking, or horizontal movement.

Upstream Slope - The upstream slope of the dam is covered with handplaced riprap up to an elevation about 2 feet above the water surface in the reservoir, and the riprap is in good condition. Above the riprap, the upstream slope is covered with grass which is kept mowed (see Photo A-3A).

Downstream Slope - The downstream slope of the dam is about 1.5H:1V, which, for a dam of this height (about 40 feet) is considerably steeper than that of similar dams designed in accordance with modern standards of practice. No evidence of creep or sloughing of the slope was observed. The downstream slope is covered with large evergreen trees up to about 18 inches in diameter (see Photos A-3B and A-4A). There are many small (2 to 3-inch-diameter) animal burrows on the downstream slope and one large burrow at Sta 1+80 about 10 feet below the crest of the dam. At the downstream toe of the dam, in the deepest section of the valley, where the
toe of the embankment is retained by a stone masonry and concrete retaining wall, there is a soft, wet area with some standing water next to the base of the retaining wall. This retaining wall is cracked in several places and displaced downstream (see Photo A-4B).

Abutments - Both abutments of the dam appear to consist of soil. No bedrock outcrops were observed in the vicinity of the dam. Trees are growing on the contact between the downstream slope of the dam and the left abutment. Along the contact between the downstream slope and the right abutment, trees are growing on the downstream slope and grass, which is kept mowed, is growing on the abutment itself (see Photo A-5A).

2) **Dike**

On the south side of the reservoir, near the right abutment of the dam, there is a low dike built across a saddle in the reservoir perimeter (see Photo A-5B). The dike is covered with grass, which is kept mowed, and appears to be in good condition. The upstream slope of the dike is riprapped up to an elevation about 2 feet above the level of water in the reservoir.

c. **Appurtenant Structures**

1) **Reservoir Supply Line**

The incoming supply line to the reservoir consists of a 10-inch pipe from Ilion Reservoir No. 2 which connects with an 8-inch pipe from Ilion Reservoir No. 3. This supply pipe was not observable. The Owner, however, indicated that the line is regularly used and that all of the valves on it are operable.

2) **Outlet Pipe and Blowoff**

The 16-inch cast iron outlet pipe from the dam discharges at the filter plant. The outlet pipe is controlled by 2 valves, one in a valve box on the slope (see Photo A-7A) and another in a concrete vault downstream of the dam (see Photos A-6A and A-6B). The valve on the dam slope does not close fully and is only operated every 2 or 3 years. The valve in the vault is well maintained and operable. The vault itself is also in good condition. The only portion of the outlet pipe observable is the portion through the vault and it appears to be in good condition.

Only the downstream end of the blowoff and the valve on the blowoff, both located in the lower level of the filter plant control building (see Photo A-7B), were observable. The building is in good condition, with some sediment deposited in the bottom due to the operation of the blowoff. The handwheel on the valve is located
on the top floor of the filter plant control building, is used regularly, and is in good condition (see Photo A-8A). The valve and downstream end of the pipe are rusted but still function adequately (see Photos A-8B and A-9A).

3) **Spillway**

The only parts of the spillway observable were the upstream wall of the stone masonry and concrete vault with the overflow opening (see Photo A-9B) and the downstream stone masonry spillway outlet structure (see Photo A-10A). The culvert between these structures was not observable. The upstream vault wall is eroding at the waterline and there is leakage into the vault through the stone masonry. The spillway outlet structure is falling apart. The stone masonry is displaced and many joints are loose.

d. **Reservoir Area**

A minor amount of organic silty soil is washing into the reservoir from the adjacent slope at the northwest corner of the reservoir, but there is no evidence of significant sedimentation in the reservoir or of slope stability problems around the perimeter of the reservoir. Photo A-10B shows the reservoir, as well as the aerator structure in the reservoir.

e. **Downstream Channel**

The spillway from the reservoir discharges through a buried pipe, into a ditch along Elizabethtown Road in Spinnerville Gulf. This gulf is parallel to the small valley on which the dam is located. There is no channel in which water flows downstream of the dam itself. In the deep section of the valley downstream of the dam, there are several water treatment structures and the ground is covered with grass which is kept mowed. No evidence of seepage was observed downstream of the soft, wet area immediately next to the toe of the dam.

3.2 **EVALUATION**

Many large trees growing on the downstream slope and on the left abutment of the dam could lead to seepage problems and internal erosion (piping) of the embankment if any of the trees blow over and pull out their roots or if any of the trees die and their roots rot.

The downstream slope of the dam is steeper than that of similar dams designed in accordance with modern standards of practice and should be evaluated to determine whether it has an adequate factor of safety against failure.
A wet, soft area with standing water near the downstream toe of the dam may indicate a seepage problem which would adversely affect the stability of the dam if not remedied.

The cracked and displaced retaining wall at the downstream toe of the dam is a cause for concern.

Animal burrows on the downstream slope, depending on how deep they extend into the embankment, could become a focus of seepage and piping.

The deteriorated spillway outlet structure could collapse and restrict spillway discharge flows. Also, the deterioration of some of the stone masonry on the spillway structure itself could, in time, seriously weaken the structure if allowed to continue.
SECTION 4
OPERATION AND MAINTENANCE PROCEDURES

4.1 OPERATION PROCEDURES

There are no written operation procedures for the dam.

Ilion Reservoir No. 1 is used as part of the public water supply for the Village of Ilion. The valves on the outlet pipe are normally open and the valve on the blowoff is normally closed. Normal pool level is usually about at EL 727.5 or about a foot below the spillway crest. The raw water supply pipe to the reservoir is normally open. Reservoir levels are adjusted daily as water is treated and enters the Village distribution system. The maximum daily outflow from the reservoir is reported to be about 1.0 mgd (about 1.5 cfs).

At the time of the inspection the reservoir level was about 1.4 feet below the spillway crest.

4.2 MAINTENANCE OF DAM AND OPERATING FACILITIES

There are no written maintenance procedures for the dam.

The microstrainer building and office of the water treatment plant is located adjacent to the right abutment of the dam and is manned daily. The Filter Plant Operator checks the reservoir level visually several times daily and records the level in the daily log. The dam crest, dike, and areas immediately around the reservoir are mowed on a regular basis. The riprap around the reservoir is regularly cleaned of brush.

Prior to winter the reservoir is drawn down about a foot by opening the blowoff and closing off the supply pipe to the reservoir. The reservoir is drawn down to prevent ice damage to the riprap. The reservoir is refilled to its normal level each spring.

The blowoff is used regularly to control sediment deposition in the reservoir. In the spring the water level is allowed to rise to about 1 inch over the spillway crest so that the debris on the reservoir surface can be skimmed off.

The valves on the supply line to the reservoir are used regularly. The valve on the outlet pipe, nearest the dam, does not close completely and is only operated every two or three years. The valve on the outlet pipe in the concrete vault is exercised at least once a month.
4.3 EMERGENCY ACTION PLAN AND WARNING SYSTEM

There is no emergency action plan and warning system for the dam.

4.4 EVALUATION

Maintenance of the dam and appurtenances is generally satisfactory. However, the problems associated with conditions near the downstream toe (wet area and displaced retaining wall at toe) and the growth of trees on the dam should be remedied. The operation and maintenance procedures should be organized in writing for ready reference.

The Owner should develop an emergency action plan outlining action to be taken to minimize the downstream effects of an emergency, together with an effective warning system.
SECTION 5
HYDRAULICS AND HYDROLOGY

5.1 DRAINAGE AREA CHARACTERISTICS

Hlon Reservoir No. 1 and its dam are located about 400 feet offstream of an unnamed tributary of Steele Creek. Steele Creek flows to the north and discharges into the Mohawk River about 2 miles from the dam site.

The total drainage at the dam is only 0.06 square miles (38.1 acres), of which about 7% (2.5 acres) is actual reservoir surface at the normal pool elevation, one foot below the spillway crest. The topography of the drainage area is characterized by slopes of from 10% to 20%. Elevations in the drainage area vary from EL 727.5 to EL 920. (See Appendices C-5 and C-6).

5.2 ANALYSIS CRITERIA

The U.S. Army Corps of Engineers Hydrologic Engineering Center's Program HEC-1 DB (Reference 3) was used to develop the test flood hydrology and perform the reservoir routing.

The purpose of this analysis was to evaluate the dam and spillway with respect to their surcharge storage and spillway capacity. Accordingly, it was assumed that the water surface was at the normal pool level, EL 727.5, which is about one foot below the spillway crest, at the start of the flood routing. The Filter Plant Operator maintains reservoir levels at or below EL 727.5 at all times by controlling inflow to and outflow from the reservoir. It was assumed that the supply pipe to the reservoir and the outlet pipe and blowoff from it were closed, since their capacities are small and all can be controlled by Water Department personnel.

If the 10-inch supply pipe was assumed open throughout the flood, it is considered that its inflow would be more than matched by outflow through the 16-inch outlet pipe. Also, the 16-inch blowoff could be operated to provide additional discharge capacity in an emergency. Therefore, the result would be even better than for the completely closed condition of the supply and outlet works as modeled.

A constant base flow of 2 cfs per square mile was chosen to represent average conditions in the drainage area and was inputted into the program for all subareas.

The index PMP (probable maximum precipitation) inputted to the HEC-1 DB program was 19.2 inches for a 24-hour duration all-season storm over a 200-square-mile basin, according to HMR 33.
(Reference 4). Maximum 6-hour, 12-hour, 24-hour, and 48-hour precipitation for the actual size of the drainage area (same for 10 square miles or less) were inputted to the program as percentages of the index PMP in accordance with HMR 33. A storm reduction coefficient was then applied internally by the program in order to transpose or center the storm over the actual total drainage area. Thus, the corrected 48-hour PMP for the actual total drainage area became 21.8 inches. All rainfall was distributed using the Standard Project Storm arrangement embedded in the program.

Appendix C-7 summarizes the subarea, loss rate, and unit hydrograph data inputted to the program. Only two subareas were used. Subarea 1 consists of all the drainage area around the reservoir, and Subarea 2 consists of just the reservoir surface. For the land in Subarea 1, loss rates were assumed to be 1.0 inch initially and a constant 0.1 inch per hour thereafter. Snyder unit hydrograph parameters were chosen for average conditions. A conservative standard lag time was computed. The program uses the inputted lag time and Snyder peaking coefficient to solve by iteration for approximate Clark coefficients which are then used to calculate the runoff hydrograph.

For the reservoir surface making up Subarea 2, loss rates were set to zero so that rainfall would equal rainfall excess, or runoff. Assuming no delay in the rainfall/runoff response, a constant unit hydrograph for a rainfall duration equal to the HEC-1 DB calculation interval was developed per Appendix C-7 and inputted to the program.

The floods selected for analysis were the PMF (probable maximum flood) and 1/2 PMF. Floods as ratios of the PMF (e.g., 1/2 PMF) were taken as ratios of runoff, not of precipitation. Peak inflow for the PMF is about 211 cfs or 3,517 csm (cfs per square mile). Peak outflow is reduced slightly by reservoir routing to about 209 cfs (3,483 csm). For 1/2 PMF the peak inflow is about 106 cfs (1,767 csm) and the routed peak outflow is about 41 cfs (683 csm).

5.3 RESERVOIR CAPACITY

Storage capacity data for the reservoir was developed using USGS contour mapping (see Appendix C-5) and a known capacity at normal pool, EL 727.5, of 46 acre-feet (15 million gallons, see Appendix F3-5). Area measurements inside contour elevations were obtained from the USGS mapping, and the capacity of the reservoir at various elevations was then computed by hand using the method of conic sections. The computations appear on Appendix C-6.

At the spillway crest, EL 728.5, the reservoir has a capacity of 50 acre-feet. At the top of dam, EL 732, the reservoir has a capacity of 63 acre-feet. Surcharge storage between the spillway crest and top of dam amounts to 13 acre-feet, or about 4.1 inches.
of runoff from the 38.1-acre drainage area. Therefore, the reservoir has some capacity to attenuate peak inflow.

5.4 SPILLWAY CAPACITY

The dam has a 5-foot-wide by 1-foot-high inlet opening to a vault on the upstream end of a long culvert which discharges to a ditch about 300 feet from the right abutment of the dam.

The discharge capacity of the spillway was taken to be the capacity of the inlet opening of the vault on the upstream end of the culvert. The inlet opening of the spillway was assumed to act as a sharp-crested weir for depths of flow less than or equal to one foot and as an orifice for depths of flow greater than one foot. The spillway discharge computations are presented on Appendix C-8. With water 3.5 feet over the crest of the spillway (i.e., water level at top of dam) the spillway discharges about 42 cfs.

For the service spillway crest at EL 728.5 and the top of dam at EL 732, total discharge computations are summarized on Appendix C-9. Total discharge from the dam is the sum of the discharge from the spillway, plus flow over the dam for the overtopping condition. As discussed previously in Section 5.2, the supply pipe to and the outlet and blowoff pipes from the reservoir were all assumed to be closed. The hand-computed discharges for the spillway were inputted directly to the HEC-1 DB program.

With the reservoir level at the top of dam, EL 732, the total discharge from the dam is just the capacity of the spillway, or about 42 cfs.

5.5 FLOODS OF RECORD

There are no known records of past flood discharges at the dam.

5.6 OVERTOPPING POTENTIAL

The results of the overtopping analysis using the HEC-1 DB program are summarized in Table 5.1. The overtopping analysis computer input and output for the PMF and 1/2 PMF are included starting on Appendix C-10.

As noted from Table 5.1, the PMF overtops the dam by about 0.3 of a foot maximum with duration of overtopping of about 3.3 hours. The 1/2 PMF does not overtop the dam, but instead results in minimum freeboard of about 0.1 of a foot. Peak inflows are 211 cfs for the PMF and 106 cfs for 1/2 PMF. Peak outflow is 209 cfs for the PMF and is reduced significantly by reservoir routing to 41 cfs for 1/2 PMF. Time to maximum stage, or the time from the start of the 48-hour storm to peak outflow, is about 40 hours for the PMF and about
TABLE 5.1
ILION RESERVOIR NO. 1 DAM

OVERTOPPING ANALYSIS

CONDITIONS
Total Drainage Area = 0.06 square miles
Start Routing at Normal Pool EL 727.5
Top of Dam EL 732
Total Project Discharge Capacity at Top of Dam = 42 cfs ±
due to spillway. Outlet pipe and blowoff assumed closed.
Some values rounded from computed results.

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<tr>
<th>INFLOW</th>
<th>PMF</th>
<th>1/2 PMF (a)</th>
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<tbody>
<tr>
<td>48-hour Rainfall (inches)</td>
<td>21.8</td>
<td>12.8 (b)</td>
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<tr>
<td>48-hour Rainfall Excess (inches) (c)</td>
<td>18.2</td>
<td>9.1 (d)</td>
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<tr>
<td>Peak Inflow (cfs)</td>
<td>211</td>
<td>106</td>
</tr>
<tr>
<td>Peak Inflow (csm)</td>
<td>3,517</td>
<td>1,767</td>
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<table>
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<tr>
<th>OUTFLOW</th>
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<tbody>
<tr>
<td>Peak Outflow (cfs)</td>
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<td>41</td>
</tr>
<tr>
<td>Peak Outflow (csm)</td>
<td>3,483</td>
<td>683</td>
</tr>
<tr>
<td>Time to Peak Outflow (hours)</td>
<td>40.3</td>
<td>42</td>
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<tr>
<td>Maximum Storage (acre-feet)</td>
<td>64</td>
<td>63</td>
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<tr>
<td>Max. W.S. Elevation (feet-NGVD)</td>
<td>732.3</td>
<td>731.9</td>
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<tr>
<td>Minimum Freeboard (feet)</td>
<td>overtopped</td>
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<tr>
<td>Maximum Depth over Dam (feet)</td>
<td>0.3</td>
<td>not overtopped</td>
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<tr>
<td>Duration of Overtopping (hours)</td>
<td>3.3</td>
<td>n/a</td>
</tr>
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</table>

(a) One-half of PMF total runoff, including base flow. For PMF base flow = 2 cfs per square mile = < 1 cfs.
(b) Approximation assuming total losses are the same as for the PMF.
(c) Rainfall Excess = Rainfall for the Reservoir Surface. For the rest of the drainage area, losses are assumed to be 1.0 inch initially and 0.1 inch per hour thereafter.
(d) Equal to one-half of PMF value.
42 hours for 1/2 PMF. The peak portion of the inflow and outflow hydrographs for the PMF and 1/2 PMF are shown by the computer plots on Appendices C-16 and C-17.

5.7 EVALUATION

The PMF overtops the embankment. The 1/2 PMF, however, does not overtop the embankment. Therefore, in accordance with Corps of Engineers' screening criteria for review of spillway adequacy, spillway capacity is considered "inadequate", but not seriously inadequate.
SECTION 6
STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

The following visual observations, which are discussed in detail in Section 3, are indicative of potential long-term stability problems at the Ilion Reservoir No. 1 Dam:

1) Steepness of the downstream slope.
2) Trees growing on the downstream slope and left abutment.
3) Seepage near the downstream toe of the dam.
4) Animal burrows on the downstream slope of the dam.

The downstream slope of the dam is about 1.5H:1V, which is considerably steeper than the downstream slope of similar dams designed in accordance with modern standards of practice. An analysis of the stability of the embankment should be made to determine whether it has an acceptable factor of safety against slope failure.

b. Design and Construction Data

Available drawings (see Appendices G-1 to G-4) indicate that the design called for a stone masonry core wall extending about 5 feet into the original ground, "puddle" about 5 feet wide against the upstream side of the core wall, "fine selected material" in the section of the embankment upstream of the core wall and puddle, and "coarse material" in the section of the embankment downstream of the core wall. No construction records are available and it is not possible to determine on the basis of the visual inspection alone whether the dam was built in conformance with these design drawings.

c. Operating Records

The inspection report dated October 19, 1971 by the NYS-DEC (see Appendix F3-1) noted the presence of trees on the downstream slope.

d. Post-Construction Changes

No records of post-construction changes pertinent to structural stability are available for this dam.
e. **Seismic Stability**

This dam is in Seismic Zone 2. According to the Recommended Guidelines (Reference 1), a seismic stability analysis is not required.

6.2 **STABILITY ANALYSIS**

A structural stability analysis is not required because there are no gravity structures at this dam to analyze.
SECTION 7
ASSESSMENT AND RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

Visual inspection of Ilion Reservoir No. 1 Dam revealed the following deficiencies which affect the safety of the dam:

1) Trees growing on the downstream slope and left abutment.

2) Seepage occurring next to the downstream toe of the dam.

3) A downstream slope of about 1.5H:1V, which is considerably steeper than that of similar dams designed in accordance with modern standards of practice and which may not have an acceptable factor of safety against failure.

4) Animal burrows on the downstream slope.

5) A cracked and displaced retaining wall at the downstream toe of the dam.

6) The deteriorated structural condition of the spillway outlet structure, as well as lesser deterioration of the spillway structure itself.

Hydrologic and hydraulic analysis indicates that the PMF overtops the embankment. The 1/2 PMF, however, does not overtop the embankment. Therefore, in accordance with Corps of Engineers' screening criteria for review of spillway adequacy, spillway capacity is considered "inadequate", but not seriously inadequate.

b. Adequacy of Information

Available information, together with that gathered during the visual inspection, is considered adequate for this Phase I inspection.

c. Need for Additional Investigations

The following detailed engineering investigations should be performed by a registered professional engineer qualified by training and experience in the design of dams:
1) Investigate the stability of the embankment section, with particular attention to the steepness of the downstream slope.

2) Investigate the seepage at the downstream toe of the dam.

3) Investigate the cracked and displaced condition of the retaining wall at the downstream toe of the dam.

d. Urgency

The investigations recommended above in Section 7.1c should be started within 6 months after receipt of this Phase I Report by the Owner.

Any remedial work deemed necessary as a result of these investigations should be completed within 18 months after receipt of this report by the Owner.

Measures recommended below in Section 7.2a should be completed within 12 months after receipt of this report by the Owner.

7.2 RECOMMENDED MEASURES

The following work should be performed by the Owner. Where engineering assistance is indicated, the Owner should engage a registered professional engineer qualified by training and experience in the design of dams. Assistance by such an engineer may also be useful for some of the other work.

a. Complete Within 12 Months

1) Institute a program to visually inspect - not just casually look at - the dam and its appurtenances at least once a month.

2) Repair the deteriorated spillway outlet structure and repair the lesser deterioration of some of the stone masonry on the spillway structure itself.

3) Remove trees, brush, and their root systems from the slopes of the embankment and to a distance of 20 feet downstream from the toe in accordance with specifications and field observation of the work by an engineer. Fill resulting holes with properly selected, compacted fill. Continue to keep these same areas and the crest of the dam clear by cutting, mowing, and cleanup at least annually.

4) Backfill animal burrows on the slopes of the embankment with properly selected, compacted fill.
5) Prepare written routine operation and maintenance procedures for the dam and its appurtenances.

6) Institute a program of comprehensive technical inspection of the dam and its appurtenances by an engineer on a periodic basis of at least once every two years.

7) Develop an emergency action plan outlining action to be taken to minimize the downstream effects of an emergency, together with an effective warning system.

b. Complete Within 18 Months

The following remedial work should be completed by the Owner. A qualified, registered professional engineer should design and observe the construction of the remedial work.

1) Appropriate modifications as a result of the stability investigation of the embankment.

2) Appropriate modifications as a result of investigating the seepage at the downstream toe of the dam.

3) Appropriate modifications as a result of investigating the cracked and displaced condition of the retaining wall at the downstream toe of the dam.
APPENDIX A

PHOTOGRAPHS
PHOTOS NOT LOCATED

PHOTO 7B - FILTER PLANT CONTROL BUILDING
PHOTO 8A - HANDWHEEL FOR BLOWOFF, IN TOP LEVEL OF FILTER PLANT CONTROL BUILDING.
PHOTO 8B - VALVE ON BLOWOFF, IN BOTTOM OF FILTER PLANT CONTROL BUILDING.
PHOTO 9A - END OF BLOWOFF, IN BOTTOM OF FILTER PLANT CONTROL BUILDING.
PHOTO 10A - OUTLET STRUCTURE AT DOWNSTREAM END OF CULVERT FROM SPILLWAY.
A-2A  Top of dam looking from left abutment - 6/4/81

A-2B  Tree roots across top of dam at about Sta 2+20. (Many other tree roots across top of dam at other locations) - 6/4/81
A-3A  Upstream slope of dam with hand-placed riprap, looking from left abutment. Note microstrainer / treatment plant office building and entrance to spillway in background - 6/4/81

A-3B  Contact between downstream slope and right abutment, with trees on slope and grass on abutment - 6/4/81
A-4A  Downstream slope of dam viewed from left abutment - 6/4/81

A-4B  Stone masonry wall at downstream toe of dam - 6/4/81
A-5A  Downstream slope of dam near toe viewed from above right abutment. Softener building is at middle right of photo - 6/4/81

A-5B  Downstream side of dike - 6/4/81
A-6A  Vault for downstream valve on outlet pipe - 6/4/81

A-6B  Downstream valve on outlet pipe, inside vault - 6/4/81
A-7A  Valve box on downstream slope of dam for upstream valve on outlet pipe - 6/4/81

A-7B  Filter plant control building. Doorway is entrance to ladder to lower level. End of blowoff and blowoff valve located on bottom level and handwheel for valve located on top level - 6/4/81
A-8A  Top level of filter plant control building with removable handwheel and stem on blowoff valve operating nut - 6/4/81

A-8B  Blowoff valve in bottom of filter plant control building - 6/4/81
A-9A  Downstream end of blowoff valve in bottom of filter plant control building - 6/4/81

A-9B  Upstream end of spillway - 6/4/81
A-10A Outlet structure at downstream end of pipe from spillway - 6/4/81

A-10B View of reservoir from center of dam. Note aerator to right of center in photo - 6/4/81
APPENDIX B

VISUAL INSPECTION CHECKLIST
### PHASE I

**VISUAL INSPECTION CHECKLIST**

#### 1. BASIC DATA

##### a. General

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<td>Fed. I.D. #</td>
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<td>DEC Dam No.</td>
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<td>Tributary of</td>
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<tr>
<td>Latitude (N)</td>
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<tr>
<td>Longitude (W)</td>
<td>75° 3.3'</td>
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<tr>
<td>Weather Conditions</td>
<td>OVERCAST &amp; WARM</td>
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<tr>
<td>Reservoir Level at Time of Inspection</td>
<td>1.4' BELOW SPILLWAY CREST, EL 727.1</td>
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</tbody>
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##### b. Inspection Personnel (*Recorder*)

- THOMAS BENNETTUM - CTM, *
- EDWIN VOPELAK JR. - CTM, RONALD C. HIRSCHFELD - GEI

##### c. Persons Contacted (Including Title, Address & Phone No.)

- CHARLES R. BAKER, WATER SUPERINTENDANT HOME (315) 694-2348 OFFICE (315) 695-7711
- EDWARD C. ALLISON, ASST. WATER SUPERINTENDANT (315) 695-7711 BOARD OF WATER COMMISSIONERS, MORGAN ST.
- MICHAEL MCCORMACK, FILTER PLANT OPERATOR (315) 694-9144 ADDRESS FOR ABOVE: P.O. BOX 350, ILLION, NY 13357

##### d. History

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<tr>
<td>Designer</td>
<td>STANWIX ENGINEERING CO.</td>
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<tr>
<td>Constructed By</td>
<td>J. J. RUMSEY, FOSTORIA, OHIO</td>
</tr>
<tr>
<td>Owner</td>
<td>VILLAGE OF ILLION BOARD OF WATER COMMISSIONERS</td>
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<tr>
<td></td>
<td>MORGAN ST, P.O. BOX 350, ILLION, NY 13357</td>
</tr>
</tbody>
</table>
2. EMBANKMENT
   a. Characteristics
      GEI 1) Embankment Material Design drawing shows "fine selected material" in upstream shell and "coarse material" in downstream shell.
      GEI 2) Cutoff Type Design drawing shows stone-masonry core wall and "puddle" core extending 5 feet below original ground surface.
      GEI 3) Impervious Core Design drawing shows stone-masonry core wall and "puddle" core.
      GEI 4) Internal Drainage System None observed.
      GEI 5) Miscellaneous No comments.

   b. Crest
      GEI 1) Vertical Alignment Good
      GEI 2) Horizontal Alignment Good
      GEI 3) Lateral Movement No evidence of lateral movement observed
      GEI 4) Surface Cracks None observed
      GEI 5) Miscellaneous No comments

   c. Upstream Slope
      GEI 1) Slope (Estimate H:V) 2H:IV
      GEI 2) Undesirable Growth or Debris, Animal Burrows None observed
      GEI 3) Sloughing, Subsidence or Depressions No evidence of sloughing, subsidence, or depressions observed
GEI 4) Slope Protection Riprap up to an elevation about 2 feet above reservoir level.

GEI 5) Surface Cracks or Movement at Toe Not visible beneath water surface

GEI d. Downstream Slope

GEI 1) Slope (Estimate - H:V) 1.5H:1V

GEI 2) Undesirable Growth or Debris, Animal Burrows, Large trees cover entire downstream slope. One large animal burrow at Station 2+80 about 10 feet below crest of dam. Many small (2 to 3-inch diameter) animal burrows over entire downstream slope.

GEI 3) Sloughing, Subsidence or Depressions

No evidence of sloughing, subsidence, or depressions observed.

GEI 4) Surface Cracks or Movement at Toe None observed.

GEI 5) Seepage None observed

GEI 6) External Drainage System (Ditches, Trenches, Blanket)

None observed

GEI 7) Condition Around Outlet Structure Not applicable

GEI 8) Seepage Beyond Toe Very soft, wet area with some standing water at downstream toe of dam in deepest section of valley.
4586  Name of Dam  Iliam Reservoir No. 1 Dam  Date  June 4, 1981

GEI  1) Erosion at Contact  None observed

GEI  2) Seepage Along Contact  None observed

3. DRAINAGE SYSTEM
GEI  a. Description of System  None observed

GEI  b. Condition of System  Not applicable

GEI  c. Discharge from Drainage System  Not applicable

4. INSTRUMENTATION (Monumentation/Surveys, Observation Wells, Weirs, Piezometers, Etc.)
GEI  None observed

5. RESERVOIR
GEI  a. Slopes  Some soil washing into west end of reservoir from adjacent slope.

GEI  b. Sedimentation  No evidence of significant sedimentation observed

GEI  c. Unusual Conditions Which Affect Dam  None observed
6. AREA DOWNSTREAM OF DAM

a. Downstream Hazard (No. of Homes, Highways, etc.) FILTER PLANT BUILDINGS IMMEDIATELY D/S. SEVERAL DWELLINGS LOCATED IN THE HAMLET. OF SOUTH ILLON + SPINNERSVILLE GULF ROAD LOCATED 1800 FEET D/S

GEI b. Seepage, Growth No seepage observed beyond about 20 feet from downstream toe.

GEI c. Evidence of Movement Beyond Toe of Dam. 

GEI d. Condition of Downstream Channel NONE. RESERVOIR IS OFFSTREAM SPILLWAY DISCHARGES TO DITCH 300' FROM RIGHT ABUTMENT ALONG ELIZABETH TOWN ROAD.

7. SPILLWAY(S) (Including Discharge Channel)

a. General 5' WIDE BY 1' HIGH OPENING INTO STONE MASONRY + CONCRETE VAULT W/ SLATE SLIP ON TOP, FROM IT IS CULVERT OF UNKNOWN SIZE. CULVERT IS OVER 300' LONG DOWN STEEP SLOPE TO STONE MASONRY OUTLET STRUCTURE AT DITCH ALONG ELIZABETH TOWN ROAD.

b. Condition of Service Spillway UNOBSERVABLE EXCEPT FOR INTAKE OPENING OF VAULT + D/S OUTLET STRUCTURE.

INTAKE OPENING + VAULT - EROSION OF VAULT WALL AT WATERLINE + SOME LEAKAGE INTO VAULT THROUGH STONE MASONRY. OUTLET STRUCTURE - STONE MASONRY IS DETEORATED + STRUCTURE FALLING APART AT JOINTS

c. Condition of Auxiliary Spillway N/A
Condition of Discharge Channel: Outlet structure is at ditch along Elizabethtown Road—appears to be adequate, although there is some brush in ditch.

8. Reservoir Drain/Outlet - Outlet Pipe (Raw water main from reservoir to filter plant)
   a. Type: Pipe ✓ Conduit □ Other □
   b. Material: Concrete □ Metal ✓ Other □
   c. Size: " CIP □ Length □
   d. Invert Elevations: Entrance □ Exit □
   e. Physical Condition (Describe)
      Unobservable ✓
      1) Material □
      2) Joints □ Alignment □
      3) Structural Integrity □
      4) Hydraulic Capability: Good
   f. Means of Control: Gate □ Valve ✓ Uncontrolled □
      Operation: Operable ✓ Inoperable □ Other □
      Present Condition (Describe) 1 valve near dam head to operate (in valve box). 4 does not close fully. Operated every 2 or 3 years. Valve in vault operated w/ valve wrench, used regularly, well maintained.
   g. Other Outlets (water mains, diversion pipes) 16" CIP Blowoff Valve w/ handwheel in filter plant control building. Valve operable, used regularly, discharges into bottom of filter plant control bldg. Some rust on valve covering.
9. STRUCTURAL
   a. Concrete Surfaces Poured Concrete & Stone Masonry
      Wall at toe is only structural element of
      Dam which is not earth

   b. Structural Cracking Stone Masonry Wall - About 6 Vertical
      (cracks in wall. Concrete (slab) portion of wall
      is part of extension of concrete vault at toe which is used
      in retention. Today not dam is in good condition

   c. Movement - Horizontal & Vertical Alignment (Settlement)
      Dam retaining wall tilts 0.5

   d. Junctions with Abutments or Embankments Not applicable

   e. Drains - Foundation, Joint, Face Not applicable

   f. Water Passages, Conduits, Sluices Only Spillway, 16"
      outlet & 16" blowoff (see 7.2.8.)

   g. Seepage or Leakage Not applicable
h. Joints - Construction, etc. Joints of stone masonry.

WALL AT TOE IN GOOD CONDITION


GEI i. Foundation Not applicable


GEI j. Abutments Not applicable


k. Control Gates NONE KNOWN.


l. Approach & Outlet Channels BLOWOFF DISCHARGES INTO BAY OF FILTER PLANT CONTROL SLOP. OUTLET PIPE SUPPLIES RAW WATER TO FILTER PLANT. CULVERT FROM SPILLWAY DISCHARGES TO DITCH NEAR ELIZABETH TOWN ROAD. NARROW CHANNEL OF RESERVOIR 3' LONG X 3' WIDE UP TO MOUTH OF SPILLWAY

m. Energy Dissipators (Plunge Pool, etc.) NOT APPLICABLE


n. Intake Structures NOT OBSERVABLE


o. Stability


p. Miscellaneous 2 PIPES FEED INTO RESERVOIR, ONE HAS AERATOR ON ITS DISCHARGE END.
10. APPURtenANT STRUCTURES (Power House, Lock, Gatehouse, Service Bridge, Other)
   a. Description:

   OUTLET PIPE CONTROL VAULT - CONCRETE VAULT W/ 
   MANHOLE COVER THAT CONTAINS OUTLET PIPE CONTROL VALVE (REPLACED?))
   FILTER PLANT CONTROL BLDG. - HANDBUILD FIRE BLOWOFF
   VAPOR FLOE, BLOWOFF DISCHARGE END Y VALVE IN BOTTOM OF BLDG.
   BLDG IS STONE/NAISWIRY

   b. Condition:
   OUTLET PIPE CONTROL VAULT - GOOD CONDITION
   FILTER PLANT CONTROL BLDG. - GOOD CONDITION, SOME SEEPAGE
   FROM PIPING IN ROOM 1; BLDG.

11. MISCELLANEOUS MECHANICAL/ELECTRICAL EQUIPMENT
   a. Description: N/A
   
   b. Condition:

12. OTHER
## APPENDIX C

HYDROLOGIC AND HYDRAULIC ENGINEERING DATA
CHECKLIST AND COMPUTATIONS

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<th>Description</th>
<th>Page</th>
</tr>
</thead>
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<td>C-1</td>
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<tr>
<td>Drainage Area Map</td>
<td>C-5</td>
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<tr>
<td>Elevation - Area - Storage Computations &amp; Drainage Area</td>
<td>C-6</td>
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<tr>
<td>Drainage Area Data for HEC-1 DB Model</td>
<td>C-7</td>
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<td>C-8</td>
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<td>Overtopping Analysis</td>
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<td>Computer Input</td>
<td>C-10</td>
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<tr>
<td>Computer Output - Complete</td>
<td>C-11</td>
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<tr>
<td>Inflow and Outflow Hydrograph Plots</td>
<td>C-16</td>
</tr>
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</table>

PHASE I INSPECTION

HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA CHECKLIST

Name of Dam: ILION RESERVOIR #1 DAM
Fed. Id. #: NY00186

1. AREA-CAPACITY DATA

<table>
<thead>
<tr>
<th>Elevation (ft.)</th>
<th>Surface Area (acres)</th>
<th>Storage Capacity (acre-ft.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>a. Top of Dam</td>
<td>732</td>
<td>3.5 ±</td>
</tr>
<tr>
<td>b. Design High Water (Max. Design Pool)</td>
<td>UNKNOWN</td>
<td></td>
</tr>
<tr>
<td>c. Auxiliary Spillway Crest</td>
<td>N/A</td>
<td></td>
</tr>
<tr>
<td>d. Pool Level with Flashboards</td>
<td>N/A</td>
<td></td>
</tr>
<tr>
<td>e. Service Spillway Crest</td>
<td>728.5</td>
<td>2.7 ±</td>
</tr>
<tr>
<td>NORMAL Pool</td>
<td>727.5</td>
<td>2.5</td>
</tr>
</tbody>
</table>

2. DISCHARGES

| a. Average Daily | (MAX DAILY FLOW = 1MGD) | < 1.5 Est. |
| b. Spillway @ Top of Dam |                   | 42 |
| c. Spillway @ Design High Water |                | UNKNOWN |
| d. Service Spillway @ Auxiliary Spillway Crest Elevation | (FLOW NOT CURRENTLY CLOSED) | N/A |
| e. Low Level Outlet | (W/ W.S. @ SPILLWAY CREST | 0 |
| f. Total (of all facilities) @ Top of Dam |                      | 42 |
| g. Maximum Known Flood |              | UNKNOWN |
| h. At Time of Inspection |                      | < 1.5 Est. |
3. **TOP OF DAM**

   **Type:** EARTH EMBANKMENT  
   **Elevation:** 732

   a. **Type:** EARTH EMBANKMENT  
   b. **Width:** 12'  
   **Length:** 270' 

   c. **Spillover:** 5'WIDE X 1' HIGH ORIFICE W/ CULVERT D/S OF ORIFICE  
   d. **Location:** ON RIGHT SHORE OF RESERVOIR D/S OF RIGHT ABUTMENT

4. **SPILLWAY**

   **SERVICE**
   a. **Elevation:** 728.5

   **AUXILIARY**
   a. **Elevation:** N/A

   b. **Type:** CULVERT  
   **Width:** 5'WIDE BY 1' HIGH OPENING IN CULVERT D/S  
   **Type of Control:** Uncontrolled

   c. **Type:** STONE MASONRY WALL W/ CULVERT D/S  
   **Size/Length:** ____________________________

   d. **Invert Material:** STONE MASONRY  
   **Anticipated Length of Operating Service:** ____________________________

   e. **Controlled:** Type  
   **Number:** ____________________________

   f. **Flashboards; gate**  
   **Size/Length:** ____________________________

   g. **Chute Length:** ____________________________

   h. **Height Between Spillway Crest & Approach Channel Invert (Weir Flow):** 5'
5. **OUTLET STRUCTURES/EMERGENCY DRAWDOWN FACILITIES**
   a. Type: Gate ___ Sluice ___ Conduit ✓ Penstock ___
   b. Shape: TWO CAST IRON PIPES - OUTLET PIPE & BLOWOFF
   c. Size: BOTH 16" DIA
   d. Elevations: Entrance Invert OUTLET PIPE - EL 700 BLOWOFF - EL 693
      Exit Invert: UNKNOWN
   e. Tailrace Channel: Elevation N/A

6. **FLOOD WATER CONTROL SYSTEM**
   a. Warning System: NONE
   b. Method of Controlled Releases (mechanisms): OUTLET PIPE
      VALVE (NORMALLY OPEN) SUPPLIES RAW WATER TO FILTER PLANT
      BLOWOFF CAN BE OPERATED AS WELL

7. **CLIMATOLOGICAL GAGES**
   a. Type: NON-RECORDING RAIN GAGE OPERATED BY VILLAGE WATER DEPT.
   b. Location: AT FILTER PLANT NEAR RESERVOIR
   c. Period of Record: 1948 TO PRESENT
   d. Maximum Reading: UNKNOWN Date

8. **STREAM GAGES**
   a. Type: WATER-STAGE RECORDER * USGS GAGE # 01346000
   b. Location: WEST CANADA CREEK AT KAST BRIDGE, N Y
      LAT: 43° 04' 08" LONG: 74° 59' 26"
      26 MILES NORTH OF DAM
   c. Period of Record: CONTINUOUS FROM 1920 TO PRESENT, OTHERS FROM 1913
   d. Maximum Reading: 23,300 CFT 41.9 CU. FT. DATE MARCH 26, 1918

9. **OTHER**
   * HINCKLEY RESERVOIR LOCATED 4/5
10. DRAINAGE BASIN CHARACTERISTICS

a. Drainage Area  0.06 SQUARE MILES (38.1 ACRES)

b. Land Use - Type  WOODLAND W/ GRASS AROUND RESERVOIR

c. Terrain - Relief  SLOPES AVERAGING 10% TO 20%

d. Surface - Soil  GLACIAL TILL?

e. Runoff Potential (existing or planned extensive alterations to existing surface or subsurface conditions)
  NONE KNOWN.

f. Potential Sedimentation Problem Areas (natural or man-made; present or future)
  SEEPAGE FROM NATURAL SLOPE ABOVE LEFT SHORE
  OF RESERVOIR IS DEPOSITING SEDIMENTS INTO RESERVOIR ALONG LEFT SHORE

g. Potential Backwater Problem Areas for Levels at Maximum Storage Capacity (including surcharge storage)
  NONE KNOWN.

h. Dikes - Floodwalls (overflow & non-overflow) - Low Reaches Along the Reservoir perimeter
  LOW AREA OF NATURAL GROUND - DIKE ON RIGHT SHORE OF RESERVOIR U/S FROM DAM
  Location  RESERVOIR U/S FROM DAM
  Elevation  

i. Reservoir  
  SPILLWAY CREST
  Length @ Maximum Design Pool  400'± (feet)
  Length of Shoreline (@ Service Spillway Crest)  1200'± (feet)
**ELEVATION - AREA - STORAGE COMPUTATIONS**

**RESERVOIR VOLUME:** Computed by method of conic sections

\[ \Delta V_{12} = \frac{1}{3} (A_1 + A_2 + \sqrt{A_1 A_2}) \]

<table>
<thead>
<tr>
<th>ELEVATION (5)</th>
<th>AREA (6)</th>
<th>VOLUME (5E2 - FEET)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(NGVD - FT)</td>
<td>(ACRES)</td>
<td></td>
</tr>
<tr>
<td>Normal Pool</td>
<td>693 (1)</td>
<td>0</td>
</tr>
<tr>
<td>Spillway Crest</td>
<td>727.5 (1,2)</td>
<td>46 (4) 15 MILLION GALLONS</td>
</tr>
<tr>
<td>Top of Dam</td>
<td>728.5</td>
<td>50 Est.</td>
</tr>
<tr>
<td></td>
<td>732 (3)</td>
<td>63 by program</td>
</tr>
<tr>
<td></td>
<td>740</td>
<td>93</td>
</tr>
</tbody>
</table>

(1) FROM PLAN OF EMBANKMENT DATED 1892 (SEE APPENDIX G-4)

(2) FROM DATA PROVIDED BY OWNER (SEE APPENDIX F-3-11)

(3) FROM DATA PROVIDED BY OWNER (SKETCH WHICH APPEARS AS APPENDIX G-9)

(4) FROM DATA PROVIDED BY OWNER (SEE APPENDIX F-3-5)

(5) RELATIVE ELEVATION DIFFERENCES BETWEEN NORMAL POOL, SPILLWAY CREST, AND TOP OF DAM MEASURED IN FIELD. ALL ELEVATIONS ASSUMED NGVD.

(6) FROM USGS TOPOGRAPHIC MAPPING APPENDIX C-5, EXCEPT AS NOTED.

**DRAINAGE AREA**

<table>
<thead>
<tr>
<th>AREA (ACRES)</th>
<th>AREA (SQUARE MILES)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Watershed direct to reservoir (Subarea 1)</td>
<td>35.6</td>
</tr>
<tr>
<td>Reservoir surface (Subarea 2)</td>
<td>2.5</td>
</tr>
<tr>
<td>@ Normal Pool El 727.5</td>
<td></td>
</tr>
<tr>
<td><strong>Total</strong></td>
<td><strong>38.1</strong></td>
</tr>
</tbody>
</table>
DRAINAGE AREA DATA FOR HEC-2 DB MODEL

SUBAREA 1: AREA TRIBUTARY DIRECTLY TO RESERVOIR
AREA = 0.056 SQUARE MILES

LOSS RATES: 1.0" - INITIALLY
0.1"/HOUR - CONSTANT LOSS RATE

UNIT HYDROGRAPH PARAMETERS: USE SNYDER METHOD

A = DRAINAGE AREA = 0.056 SQUARE MILES
L = LENGTH OF MAIN WATERCOURSE TO UPSTREAM LIMIT OF
   DRAINAGE AREA = 0.31 MILES
L_a = LENGTH ALONG MAIN WATERCOURSE TO POINT OPPOSITE
      THE CENTROID OF THE DRAINAGE AREA = 0.11 MILES
C = SNYDER'S BASIN COEFFICIENT = 7.0 ASSUMED AVERAGE
C_p = SNYDER'S PEAKING COEFFICIENT = 0.625 ASSUMED AVERAGE
k_p = STANDARD LAG IN HOURS = C_p (L/L_a)^0.5 = 0.73 HOURS

USE k_p = 0.7 HOURS

SUBAREA 2: RESERVOIR SURFACE, AREA = 0.004 SQ. MILES = 2.5 ACRES

LOSS RATES: NONE BECAUSE RAIN FALL ≈ RUNOFF FOR WATER SURFACE

UNIT HYDROGRAPH PARAMETERS:

FOR U.H. W/10 MINUTE DURATION + 1" RAIN

\[ Q = \frac{A(\text{"})}{10 \text{ minutes}} = \frac{2.5 \text{ acres} \times \frac{43,560 \text{ sq ft}}{1 \text{ acre}} \times \frac{-1 \text{ ft}}{1 \text{ inch}} \times \frac{1 \text{ minute}}{60 \text{ seconds}}}{10 \text{ minutes}} \]

\[ Q = 15 \text{ cfs} \]  

(w/o LOSS RATE)
**DISCHARGE COMPUTATIONS**

**SPILLWAY CAPACITY**

Spillway consists of: 5' wide x 1' high orifice opening on
U/S end of steep culvert pipe, size unknown.

For flow 0' ≤ 1' deep, weir flow assumed:

\[ Q = 3.33 \left( L - 0.2H \right) \left( H^{1.5} \right) \text{(REFERENCE B)} \]

W/ \[ L = \text{length}, \, 0.2H = \text{end losses + sharp-crested rectangular weir} \]

For flow > 1', orifice flow assumed:

\[ Q = \frac{2}{3} L C \left( \frac{125}{2} \right) \left( H_{0.6}^{3/2} - H_{0.3}^{3/2} \right) \text{(REFERENCE B)} \]

W/ \[ C = \text{orifice coef.} = 0.6 \]

<table>
<thead>
<tr>
<th>ELEV. (NGVD)</th>
<th>WATER DEPTH (feet)</th>
<th>QWeir (cfs)</th>
<th>QOrifice (cfs)</th>
<th>QSpillway (cfs)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Spillway Crest</td>
<td>728.5</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>729</td>
<td>0.5</td>
<td>0.6</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>729.5</td>
<td>1.0</td>
<td>16.1</td>
<td>16</td>
<td>16</td>
</tr>
<tr>
<td>730</td>
<td>1.5</td>
<td>29.2</td>
<td>24</td>
<td>24</td>
</tr>
<tr>
<td>731</td>
<td>2.5</td>
<td>34.4</td>
<td>34</td>
<td>34</td>
</tr>
<tr>
<td>Top of Dam</td>
<td>732</td>
<td>3.5</td>
<td>42</td>
<td>42</td>
</tr>
<tr>
<td>733</td>
<td>4.5</td>
<td>48</td>
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</tbody>
</table>
### Discharge Computations

#### Dam Appurtenance

<table>
<thead>
<tr>
<th></th>
<th>Elevation (NGVD)</th>
<th>Size</th>
</tr>
</thead>
<tbody>
<tr>
<td>Culvert Spillway (w/ Entrance Weir)</td>
<td>Crest EL = 728.5</td>
<td>5' Crest Length</td>
</tr>
<tr>
<td>Dam</td>
<td>Top of Dam EL = 732</td>
<td>270' Crest Length</td>
</tr>
<tr>
<td>Outlet Pipe</td>
<td>Inlet Invert EL = 700</td>
<td>16&quot; CIP</td>
</tr>
<tr>
<td>Blowoff Pipe</td>
<td>Inlet Invert EL = 693</td>
<td>16&quot; CIP</td>
</tr>
</tbody>
</table>

**For Flow Over Dam:**

\[
Q = \frac{5087}{L^1/16} \left[ \text{(Formula for Critical Flow Over Broad-Crested Weir, Ref.9)} \right]
\]

<table>
<thead>
<tr>
<th>Elevation (NGVD)</th>
<th>( H_{\text{Spillway}} ) (ft)</th>
<th>( H_{\text{Dam}} ) (ft)</th>
<th>( Q_{\text{Outlet}} ) (cf)</th>
<th>( Q_{\text{Blowoff}} ) (cf)</th>
<th>( Q_{\text{Spillway}} ) (cf)</th>
<th>( Q_{\text{Dam}} ) (cf)</th>
<th>( Q_{\text{Total}} ) (cf)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Normal Pool</td>
<td>727.5</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Spillway Crest</td>
<td>728.5</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>729</td>
<td>.5</td>
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<td>730</td>
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<td>0</td>
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<tr>
<td></td>
<td>731</td>
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<td>0</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Top of Dam</td>
<td>732</td>
<td>3.5</td>
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<td>0</td>
<td>0</td>
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<td>0</td>
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<tr>
<td></td>
<td>733</td>
<td>4.5</td>
<td>1</td>
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<td>0</td>
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<td>853</td>
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**Scale:** 80.00847
# SUB-AREA RUNOFF COMPUTATION

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<th>ISTAQ</th>
<th>ICOMP</th>
<th>IICON</th>
<th>ITAPE</th>
<th>JPLT</th>
<th>JPKT</th>
<th>INAME</th>
<th>ISTAGE</th>
<th>IAUTO</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
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<td></td>
<td></td>
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## HYDROGRAPH DATA

<table>
<thead>
<tr>
<th>INYDG</th>
<th>IUMG</th>
<th>TAREA</th>
<th>SNAP</th>
<th>TRSA</th>
<th>TRSC</th>
<th>RATIO</th>
<th>15NOW</th>
<th>ISAME</th>
<th>LOCAL</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>-1</td>
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| RES | 1 | 2 | 0 | 0 | 1 | 0 | 0 |

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# Peak Flow and Storage Summary for Multiple Plan-Ratio Economic Computations

**Flows in Cubic Feet per Second (Cubic Meters per Second)**

**Area in Square Miles (Square Kilometers)**

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APPENDIX D

STABILITY ANALYSIS

NO GRAVITY STRUCTURES TO ANALYZE
APPENDIX E
REFERENCES
REFERENCES

This is a general list of references pertinent to dam safety investigations. Not all references listed have necessarily been used in this specific report.

1. "Engineering and Design, National Program For Inspection of Non-Federal Dams", ER 1110-2-106, Dept. of the Army, Office of the Chief of Engineers, 26 September 1979, with Change 1 of 24 March 1980. Included as Appendix D of the ER is "Recommended Guidelines For Safety Inspection of Dams".


5. HMR 51, "All-Season Probable Maximum Precipitation, U.S. East of 105th Meridian for Areas from 1000 to 20,000 Square Miles and Durations from 6 to 72 Hours", U.S. Dept. of Commerce, NOAA, National Weather Service, 1974.


# Appendix F
## Available Engineering Data and Records

**Table of Contents**

<table>
<thead>
<tr>
<th>Location of Available Engineering Data and Records</th>
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<tbody>
<tr>
<td>Checklist for General Engineering Data and Interview with Dam Owner</td>
<td>F2</td>
</tr>
<tr>
<td>Copies of Engineering Data and Records</td>
<td>F3</td>
</tr>
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</table>
APPENDIX F

SECTION F1

LOCATION OF AVAILABLE ENGINEERING DATA AND RECORDS

1. Owner: Village of Ilion Board of Water Commissioners
   P.O. Box 330
   Morgan Street
   Ilion, NY 13357
   Attn: Charles R. Baker, Water Superintendent
   (315) 895-7711

   Available: Background data, drawings.


3. Construction Contractor: J. J. Rumsey, Fostoria, Ohio
   (business status unknown)

4. Agency: NYS Department of Environmental Conservation
   50 Wolf Road
   Albany, NY 12233
   Attn: George Koch, P.E., Chief, Dam Safety Section
   (518) 457-5557

   Available: Inspection report.
CHECKLIST FOR GENERAL ENGINEERING DATA
& INTERVIEW WITH DAM OWNER

Name of Dam: LION RESERVOIR NO. 1 DAM
Fed. Id. #: NY 00186

Date: 1/29/81 6/4/81
Interviewer(s): EDWIN YOPELAK JR.
THOMAS REHNEDUM

Dam Owner/Representative(s) Interviewed, Title & Phone#
CHARLES R. BAKER, WATER SUPERINTENDANT (315) 895-7711
EDWARD C. ALLSTON, ASS'T WATER SUPERINTENDANT (315) 895-7711
MICHAEL MCCORMACK, FILTER PLANT OPERATOR (315) 894-9144

1. OWNERSHIP (name, title, address & phone #)
VILLAGE OF LION
BOARD OF WATER COMMISSIONERS, MORGAN ST., PO. BOX 330,
ILION, NY 13357, (315) 895-7711

2. OPERATOR (name, title, address & phone # of person responsible for day-to-day operation)
CHARLES R. BAKER, WATER SUPERINTENDANT OFFICE - (SAME ADDRESS AS OWNER)
HOME - 157 PROSPECT ST., ILION, NY 13357 (315) 894-2348
MICHAEL MCCORMACK, FILTER PLANT OPERATOR (315) 894-9144

a. Operator Full/Part time FILTER PLANT OPERATOR & SUPT.
ARE FULL TIME EMPLOYEES.

3. PURPOSE OF DAM
a. Past CREATE IMPOUNDMENT FOR RAW WATER STORAGE

b. Present (SAME AS ABOVE)
RESEVOIR WATER IS PRECHLORINATED & AGLEATED

4. DESIGN DATA
b. By (name, address, phone #, business status)
STANWIX ENGINEERING CO., ROME, NY
(NO LONGER IN BUSINESS)
c. Geology Reports NONE KNOWN
d. Subsurface Investigations NONE KNOWN
e. Design Reports/Computations (H&H, stability, seepage)
NONE KNOWN
f. Design Drawings (plans, sections, details) 

   YES - SEE APPENDICES G-1 TO G-8

g. Design Specifications 

   NONE KNOWN.

h. Other (see appendices F3-9 to F3-10) & GENERAL DATA ON DAM (SEE APPENDIX F3-10), BOTH FROM OWNER.

5. CONSTRUCTION HISTORY

a. Initial Construction

1) Completed When 1892-1893 

2) By (name, address, phone #, business status) 

   MR. J.J. RUMSEY  FOSTOPIA, OHIO 
   (BUSINESS STATUS UNKNOWN)

3) Borrow Sources/Material Tests NONE KNOWN.

4) Construction Reports/Photos NONE KNOWN.

5) Diversion Scheme/Construction Sequence NONE KNOWN.

6) Construction Problems NONE KNOWN.

7) As-Built Drawings (plans, sections, details) NONE KNOWN.

8) Data on Electrical & Mechanical Equipment Affecting Safe Operation of Dam N/A (ELECTRIC & FILTER PLANT)

9) Other N/A
b. Modifications (review design data & initial construction items as applicable & describe)

NONE KNOWN.

6. OPERATION RECORD

a. Past Inspections (dates, by, authority, results)

NYS-DEC INSPECTION - OCT. 19, 1971 (SEE APPENDIX F3-30)

b. Performance Observations (seepage, erosion, settlement, post-construction surveys, instrumentation & monitoring records) NONE

c. Post-Construction Engineering Studies/Reports

1961-1964 STUDY OF WATER SYSTEM BY STEARNS & WHELEN, BUT DID NOT INCLUDE STUDY OF DAM.

d. Routine Rainfall, Reservoir Levels & Discharges

- FILTER PLANT OPERATOR CHECK LEVEL SEVERAL TIMES DAILY & RECORDS LEVEL IN DAILY LOG, MANY YEARS OF RECORD.
- APR. 1 - NOV. 1 - RAINFALL AT RES #1, NEAR WATER TREATMENT PLANT, MEASURED BY PLANT OPERATOR, RECORDS FROM 1998 TO PRESENT.
e. Past Floods That Threatened Safety (when, cause, discharge, max. pool elevation, any damage) **NONE**.

**OVERFLOW SPILLWAY USED EVERY SPRING UNDER CONTROLLED CONDITIONS TO SKIM OFF RESERVOIR SURFACE. MAX FLOW ABOUT 1" OVER CREST.**

f. Previous Failures (when, cause, describe) **NONE**.

---

g. Earthquake History (seismic activity in vicinity of dam) **NONE KNOWN**.

---

7. **VALIDITY OF DESIGN, CONSTRUCTION & OPERATION RECORDS** (note any apparent inconsistencies)

**ELEVATION OF TOP OF DAM IS ABOUT 1/2 A FOOT HIGHER THAN THE ELEVATION FOR TOP OF DAM ON APPENDIX G-4.**

---

8. **OPERATION & MAINTENANCE PROCEDURES**

a. Operation Procedures in writing? **NO**. Obtain copy or describe. (reservoir regulation plan, normal pool elevation and status of operating facilities, who operates & means of communication to controller, mode of operating facilities, i.e., manual, automatic, remote)

- **FEED LINE TO RESERVOIR CONSISTS OF 10" OUTLET PIPE FROM RES #2 WHICH CONNECTS WITH 8" PIPE FROM RES #3.**

- **OBSERVING VALVES ON PIPE AT RES #2 THERE ARE 3 VALVES IN SERIES ON LINE NEAR RES #1 WHICH CAN BE OPERATED TO CONTROL FLOW INTO RES #1.**

- **VALVE ON OUTLET PIPE FROM RES #1 EXERCISED AT LEAST ONE A MONTH (VALVE IN VAULT). VALVE ON OUTLET PIPE W/ VALVE BOX IS HARD TO OPERATE; CANNOT CLOSE FULLY.**

- **OPERATION IS OPERATED EVERY 2 OR 3 YEARS.**

- **NORMALLY WATER SURFACE KEPT 1' OR MORE BELOW SPILLWAY CREST.**

b. Maintenance Procedures in writing? **NO**. Obtain copy or describe. (how crest, dike, and reservoir regularly)

- **KEEPS RAPID CREST CLEAR OF BRUSH**

- **DURING ICE FORMING WEATHER, DRAIN RESERVOIR DOWN BY OPENING BLOWOFF OR PLUGGING INTAKES. DRAW DOWN ABOUT 1' TO PREVENT RAPID DAMAGE, RESERVOIR REFILLED IN SPRING.**

- **BLOWOFF USED WEEKLY TO CONTROL SEDIMENT BUILD-UP IN RESERVOIR.**
c. Emergency Action Plan & Warning System in Writing? NO
Obtain copy or describe. (actions to be taken to minimize the D/S effects of an emergency)

WILL UTILIZE WATER DEPT. PERSONNEL TO
CONTACT IN HAZARD AREA BY GOING DOOR
TO DOOR.

9. OTHER
APPENDIX F

SECTION F3

COPIES OF ENGINEERING DATA AND RECORDS

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<p>| Inspection Report, by NYS-DEC - October 19, 1971 | F3-1 |
| History of Ilion Waterworks, by Charles R. Baker, Water Superintendent | F3-4 |
| Data on Dam Sites from Owner | F3-10 |</p>
<table>
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<th>INFORMATION</th>
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## GENERAL CONDITION OF NON-OVERFLOW SECTION

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## GENERAL CONDITION OF SP'WAY AND OUTLET WORKS

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**ILLINOIS WATER WORKS**

P3-1
DEC DAM INSPECTION REPORT CODING

1. **River Basin** - Nos. 1-23 on Compilation Sheets
2. **County** - Nos. 1-62 Alphabetically
3. **Year Approved** -
4. **Inspection Date** - Month, Day, Year
5. **Apparent use** -
   1. Fish & Wildlife Management
   2. Recreation
   3. Water Supply
   4. Power
   5. Farm
   6. No Apparent Use
6. **Type** -
   1. Earth with Aux. Service Spillway
   2. Earth with Single Conc. Spillway
   3. Earth with Single non-conc. Spillway
   4. Concrete
   5. Other
7. **As-Built Inspection** - Built substantially according to approved plans and specifications

**Location of Spillway and Outlet Works**
1. Appears to meet originally approved plans and specifications.
2. Not built according to plans and specifications and location appears to be detrimental to structure.
3. Not built according to plans and specifications but location does not appear to be detrimental to structure.

**Elevations**
1. Generally in accordance to approved plans and specifications as determined from visual inspection and use of hand level.
2. Not built according to plans and specifications and elevation changes appear to be detrimental to structure.
3. Not built according to plans and specifications but elevation changes do not appear to be detrimental to structure.

**Size of Spillway and Outlet Works**
1. Appears to meet originally approved plans and specifications as determined by field measurements using tape measure.
2. Not built according to plans and specifications and changes appear detrimental to structure.
3. Not built according to plans and specifications but changes do not appear detrimental to structure.

**Geometry of Non-overflow Structures**
1. Generally in accordance to originally approved plans and specifications as determined from visual inspection and use of hand level and tape measure.
2. Not built according to plans and specifications and changes appear detrimental to structure.
3. Not built according to plans and specifications but changes do not appear detrimental to structure.

**General Conditions of Non-overflow Section**
1. Adequate - No apparent repairs needed or minor repairs which can be covered by periodic maintenance.
2. Inadequate - Items in need of major repair.

(Items) For boxes listed on condition under non-overflow section.
1. Satisfactory.
2. Can be covered by periodic maintenance.
3. Unsatisfactory - Above and beyond normal maintenance.
DEC DAM INSPECTION REPORT CODING (cont.)

General Condition of Spillway and Outlet Works

1. Adequate - No apparent repairs needed or minor repairs which can be covered by periodic maintenance.
2. Inadequate - Items in need of major repair.

(items) For boxes listed conditions listed under spillway and outlet works.
1. Satisfactory.
2. Can be covered by periodic maintenance.
3. Unsatisfactory - Above and beyond normal maintenance.
4. Dam does not contain this feature.

Maintenance
1. Evidence of periodic maintenance being performed.
2. No evidence of periodic maintenance.
3. No longer a dam or dam no longer in use.

Hazard Classification Downstream
1. (A) Damage to agriculture and county roads.
2. (B) Damage to private and/or public property.
3. (C) Loss of life and/or property.

Evaluation - Based on Judgment and Classification in Box Nos.

Evaluation for Unsafe Dam
1. Unsafe - Repairable.
2. Unsafe - Not Repairable.
3. Insufficient evidence to declare unsafe.

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<td>3 Broome</td>
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<tr>
<td>LAKE CHAMPLAIN</td>
<td>4 Essex</td>
</tr>
<tr>
<td>DELAWARE</td>
<td>5 Essex</td>
</tr>
<tr>
<td>SUSQUEHANNA</td>
<td>6 Essex</td>
</tr>
<tr>
<td>CHEMUNG</td>
<td>7 Chemung</td>
</tr>
<tr>
<td>OSWEGO</td>
<td>8 Chemung</td>
</tr>
<tr>
<td>GENESSEE</td>
<td>9 Chemung</td>
</tr>
<tr>
<td>ALLEGHENY</td>
<td>10 Clinton</td>
</tr>
<tr>
<td>LAKE ERIE</td>
<td>11 Clinton</td>
</tr>
<tr>
<td>WESTERN LAKE ONTARIO</td>
<td>12 Cleveland</td>
</tr>
<tr>
<td>CENTRAL LAKE ONTARIO</td>
<td>13 Clinton</td>
</tr>
<tr>
<td>EASTERN LAKE ONTARIO</td>
<td>14 Cleveland</td>
</tr>
<tr>
<td>SALMON RIVER</td>
<td>15 Oneida</td>
</tr>
<tr>
<td>BLACK RIVER</td>
<td>16 Onondaga</td>
</tr>
<tr>
<td>WEST ST. LAWRENCE</td>
<td>17 Oswego</td>
</tr>
<tr>
<td>EAST ST. LAWRENCE</td>
<td>18 Oswego</td>
</tr>
<tr>
<td>RACQUETTE RIVER</td>
<td>19 Orleans</td>
</tr>
<tr>
<td>ST. RITS RIVER</td>
<td>20 Orleans</td>
</tr>
<tr>
<td>INDIAN RIVER</td>
<td>21 Orleans</td>
</tr>
<tr>
<td>LONG ISLAND</td>
<td>22 Orleans</td>
</tr>
<tr>
<td>OSKICATCHIE</td>
<td>23 Orleans</td>
</tr>
<tr>
<td>GLENN</td>
<td>24 Orleans</td>
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</table>
The first Board of Water Commissioners of the Village of Ilion, was elected at a special election, held February 21, 1891, called for this purpose by trustees of the Village, in compliance with a petition signed by a majority of the taxpayers. After their election, these men were assigned the tremendous task of determining the source of supply, the kind of works to be constructed and deciding upon its location and superintending its construction. Their operating capital was $1,000.

It was first thought that a pumping system from deep wells, would be the most practical, but after several experiments with wells in the community, it was demonstrated that the quantity of water that these wells would furnish would be so small in comparison to the quantity required and the total number of wells would be so great, as to make it extremely impractical.

The Water Board then turned their attention to the flowing springs in various locations outside the Village. The yield from these springs proved to exceed the maximum quantity, as set. The locations of these sources, or springs, were so geographically wide spread, that again their use was extremely impractical.

At the September 4, 1891 special Water Board meeting, the following motion was made: "The secretary was instructed to write to the Stanwix Engineering Co., of Rome, N. Y., in regard to having their Mr. Knight come and look over the surrounding country and advise us in regard to the possible sources of water supply".

At the October 15, 1891 meeting, the written report from Mr. Knight was presented to the Water Board. This report was the beginning of the
A
593
Village of Ilion's Public Water Supply. The report called for a gravity system. The supply, was an intake on a stream being brought to an impounding reservoir of about 15 million gallons. Water from this reservoir to pass thru two (2) open slow sand filters of 300,000 gallons each, per day. The filtered water to go to a covered distributing basin (clear well) of 900,000 gallon capacity.

The engineering cost estimates for the original system are:

<table>
<thead>
<tr>
<th>System</th>
<th>Cost</th>
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</thead>
<tbody>
<tr>
<td>Supply System</td>
<td>$32,960.00</td>
</tr>
<tr>
<td>Filtering System</td>
<td>$16,000.00</td>
</tr>
<tr>
<td>Distribution System (piping)</td>
<td>$14,300.00</td>
</tr>
<tr>
<td><strong>Total</strong></td>
<td><strong>$ 93,260.00</strong></td>
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</tbody>
</table>

At a special meeting of the Water Board, held March 20, 1892, bids for the above mentioned projects, were opened. There were three bidders, with a high of $99,970. to a low of $72,326.97; This low bid was disqualified and the next low bid of $76,851.67 was accepted. The successful bidder was Mr. J. J. Rumsey of Portoria, Ohio.

In 1893, the first reservoir of 15 million gallon capacity, being fed thru an intake from a spring fed stream, was constructed. The chosen point for the reservoir was a gully on a ridge of land, about two miles south of the Village, with an elevation of 732 feet.

About 800 feet to the north of said reservoir, at an elevation of 676 feet, two (2) slow sand filters with an area of 3,040 square feet each, were constructed. Our records indicate that these slow sand filters were the third to be constructed in the United States, with Poughkeepsie, N. Y. and Hudson, N. Y. being first and second. The filters in Ilion are still in operation and are being used everyday.

The effluent from these slow sand filters was piped to a below ground clear water basin. This clearwell is 103 feet in diameter, 14 feet deep, with a ground cover of 1 1/2 feet on a reinforced concrete dome. The side walls and support columns are of poured, reinforced concrete. The capacity of this basin is 900,000 gallons and the elevation of this clearwell.
The well-full is 667 feet. This point, having an elevation of about 265 feet above our Main St., assured ample pressure by gravity, to every street in town.

The filtered water left the clearwell by a 16 inch transmission main to the newly constructed distribution system, on which customers were lined up to sign for taps to their property. Unfortunately, the sewer board had not been able to keep pace, so many applicants had to be denied the water service until the sewer had been installed.

This was the beginning of the Village of Ilion water works.

I would be very remiss as a proud department head, if I did not continue this article to the present time. Without too many details, I shall try, in chronological order, to update our system to the present.

As the population increased and industries expanded, it became necessary to increase the storage and filtration capacity to meet the demand. In 1902 - 1903, a new impounding reservoir (65 million gallons), fed by a second stream intake, was built. At the same time, two covered slow sands with 3,948 square feet each, were constructed. These filters more than doubled the original capacity. The control valves on these filters were located in the original gate house.

1913, saw the installation of a venturi meter on the distribution supply main.

In 1915, an additional intake on another stream was constructed and a transmission main laid to supply additional water to the reservoir of 1903.

In the year 1916, the use of chlorine in the water system was instituted. According to records, this process caused quite a storm.

1917 saw the addition of two more covered slow sand filters. These filters were 5,550 square feet each. The area of these two filters almost doubled the area of the existing four filters. The total filter area at this time, was about six tenths (.6) of an acre. In recent years,
one of these larger filters has been taken out of service, due to
structural failure. The present area being used is about .45% of an acre.

In 1921, work was commenced on a new reservoir, with associated
piping, to the east and south of the Village, in a natural ravine. This
project was completed in 1923 with an impounding capacity of 165 million
gallons. The total impounding capacity was now 245 million gallons.

The Ilion Water Department, in 1938 joined with The Federal Works
Progress Administration program, in the construction of a water softener
plant. The W. P. A. was to construct the building at their cost and the
Water Board, supply the softening units. These units being three in
number-Permutit Manufacturer, using zeolite resin. This plant put in
service June 3, 1939.

In 1947, a new building, designated as a chlorine house, was built
to house additional chlorinators for the purpose of pre-chlorination.

A complete survey and study of all Water Department facilities
was made by the consulting firm of Stearns & Wheler and Pitometer Associate
in 1960.

This survey led into a project of intensive renovation of and
addition to, our existing treatment plant. This project lists as follows:

1. Replacing the softeners with high exchange resins and
   associated piping.

2. Constructing a building to house a Glenfield & Kennedy
   Micro-Strainer, 7 feet 6", dia. and associated piping and laboratory.

3. Installing three (3) "diatomaceous earth filter units"
   complete with accessory equipment. These filter units are capable
   of producing 1 million gallons per day and are used to augment
   the production of our slow sand filters.

4. Complete new chlorine distribution system.

These projects completed in 1962.

In 1968, the Water Board decided it was time to eliminate the
antiquated flat rate billing system. It was decided to do this. The Village of Ilion would have to be metered 100%. The metering contract was awarded, with the Hersey Motor Co. being the successful bidder for meters and 100% remote readers. This project was successfully completed in 1969.

In the fall of 1970, contracts were bid on four (4) major projects. These are so listed:

**Contract 1. - Steele's Creek Pumping Station**
This involved (4) diverting intake dams bringing water to the pump station and pumping (if needed) into an existing reservoir. Completed in 1971.

**Contract 2. - Construction of Water Mains**
This project was to strengthen our distribution system. The contractor installed 22,345 feet of 6 inch to 16 inch size, water pipe tied into the existing system. Completed in 1971.

**Contract 3. - Prestressed Concrete Water Tanks**
Two concrete tanks were constructed on opposite ends of the distribution system. One tank has 2 million gallon capacity; the other a 0.5 million gallon capacity. Completed in 1971

**Contract 4. - Old Forge Road Pumping Station**
This was a booster station to push water into the 0.5 million gallon tank. The telemetering equipment was included in this contract. Completed in 1971.

With these projects, our water system construction comes to rest—until such time as we foresee a growing need.

I would like to say that the financing for the entire system, start to present, has come entirely from Water Department revenues.

Needless to say, the Board of Water Commissioners, its Superintendent and employees, are all proud of our water system. We adhere to the open.
door policy - if ever in Ilion, N. Y. or vicinity, please stop and look us over. It is a fine way to spend a day.

On behalf of my Board, I say,

Thank you,

CHARLES R. BAKER
WATER SUPERINTENDENT
WATERSHED DRAINAGE AREA

#1 Res. Hawke's Creek 50.0
No. 2 Intake to No. 1 Intake 0.49

#2 Res. - Hawke's Creek Intake
Source to No. 2 Intake 4.02

No. 3 Intake Litchfield Creek 2.95 (0.51 SPEC)

New Source of

#3 Res. Watershed Area 1.9

Steeles Creek Watershed
Above Hawke's Creek 21.60

Steeles Creek Watershed
Above Proposed Pumping Station 17.1

Owner

F3-10
<table>
<thead>
<tr>
<th>Date</th>
<th>Time</th>
<th>Distance</th>
<th>Rate</th>
<th>Flow</th>
<th>Depth</th>
<th>Lining</th>
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<tr>
<td>1934</td>
<td>8:00</td>
<td>1.5</td>
<td>250.0</td>
<td>1.5</td>
<td>0.80</td>
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<tr>
<td>1935</td>
<td>9:00</td>
<td>2.0</td>
<td>250.0</td>
<td>2.0</td>
<td>0.80</td>
<td>No Lining</td>
</tr>
<tr>
<td>1936</td>
<td>10:00</td>
<td>3.0</td>
<td>250.0</td>
<td>3.0</td>
<td>0.80</td>
<td>No Lining</td>
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</tbody>
</table>

Flow line: 200.0
Depth: 0.80
Lining: No Lining
## APPENDIX G
### DRAWINGS

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<tr>
<td>Profile of Dam</td>
<td>G-2</td>
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<tr>
<td>Design/Construction Drawings (no engineer named on plans) - 1892</td>
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<td>Details of Reservoir, Dwg. # 1739</td>
<td>G-3</td>
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<tr>
<td>Details of Reservoir, Dwg. # 1744</td>
<td>G-4</td>
</tr>
<tr>
<td>Design/Construction Drawings of Ilion, N.Y. Water Works, by Knight &amp; Hopkins - 1903</td>
<td></td>
</tr>
<tr>
<td>General Plan, Dwg. # 2804</td>
<td>G-5</td>
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<tr>
<td>Property and Rights of Way, Dwg. # 2811</td>
<td>G-6</td>
</tr>
<tr>
<td>Map Showing Detail in Connection with No. 1 Reservoir (no engineer named or date on plans), File 111, Map 23</td>
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<td>Water Treatment Facilities - Outside Piping:</td>
<td></td>
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<td>Water Lines, by Water Department - February 5, 1965</td>
<td>G-8</td>
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<tr>
<td>Sketch of Ilion, N.Y. Water Supply System</td>
<td>G-9</td>
</tr>
</tbody>
</table>
FROM OWNER
REDUCED TO 50% OF ORIGINAL
Cross section of Dam for the Illion Water Works
Scale 3 ft. = 1 inch

Inlet at bottom of Dam
FROM OWNER
REDUCED TO 39% OF ORIGINAL
DETAILS OF RESERVOIR
ILION, N.Y. WATERWORKS
1892
SCALE

PLAN OF BASIN AND FLOOD WATER DITCH
AT WEST END OF RESERVOIR

SECTION A-B

SECTION C-D
SECTION A-B ON SIDE EMB

SECTION C-D ON SIDE EMB

SECTION G-H ON SIDE EMB

PLAN OF OVERFLOW
SHOWING END OF FLOOD WATER CHANNEL

FRONT ELEVATION OVERFLOW

Z-W SECTIONS THROUGH OVERFLOW CHAMBER
SCALE 1/4"=1'

X-Y
DETAILS OF R. ILLION, N.Y.WAT
1892
NO 1744

SECTION & PLAN SHOWING PIPES THROUGH EMBANKMENT
SCALE 1"=12'

16" MUD PIPE
16" DELIVERY MAIN
16" MUD PIPE
FLOW LINE 2700
TAILS OF RESERVOIR
N. N. Y. WATERWORKS
1892
NO 1744

SECTION & PLAN OF FOUNTAIN
S.C. X 1/41

FLOW LINE

SECTION THRU NOZZLE
SCALE 1/41
GENERAL PLAN
ILION, N.Y. WATER WORKS
1903
Scale 1"=400'

FROM OWNER
REDUCED TO 58% OF ORIGINAL
AMENDED MAP
SHOWING
PROPERTY AND RIGHTS OF WAY
REQUIRED
FOR THE
SUPPLY SYSTEM
OF THE
ILION, NY, WATER WORKS

\[\text{(Signature)}\]

\[\text{(Date)}\]

\[\text{Charles M. Gray, President}\]

\[\text{No. 3}\]
FROM OWNER
REDUCED TO 31% OF ORIGINAL
MAP SHOWING DETAIL in connection with No. 1 RESERVOIR, ILION, NY.

Pipe line layout of filter plant at Reservoir 1

ROAD

G-7 CTM DWG NO. 81-50
NOTE:  
FOR FIRE DESCRIPTION SEE FIRE MAP SHEET 3

- - -  CHLORINE LINE

[ ] POINT OF CHLORINE APPLICATION

ILION RESERVOIR N°1
CAPACITY 15 MG

FROM OWNER
NO SCALE
Mill Act for WATER TREATMENT FACILITIES

VILLAGE OF ILION, NY
WATER TREATMENT FACILITIES

OUTSIDE PIPING WATER LINES

DATE 3-5-65

G-8 CTM DWG NO. 81-50