LASER PHOTOGRAPHIC TECHNIQUE FOR DIRECT PHOTOGRAPHY IN AN AEROBALLISTIC RANGE

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ARO, Inc.

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ABSTRACT

A front-lighted photographic system employing a giant-pulse ruby laser as a light source has been developed and installed in the 1000-ft hypervelocity Range G of the von Kármán Gas Dynamics Facility. Preliminary results indicate that this photographic technique provides an excellent method for in-flight examinations of model integrity, surface condition, and for accurate in-flight measurements of model profile dimensions (±0.002 in.) and their changes that might be produced by erosion or ablation.
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SECTION I
INTRODUCTION

Schlieren and shadowgraph techniques have been used extensively in aeroballistic ranges as means of examining hypervelocity projectiles and their flow fields. With these techniques, models appear in silhouette in the resultant photographs. Very little information regarding the actual condition of model surfaces, other than gross effects, can be gained. Radiation from heavily ablating models tends to fog portions of schlieren and visible-light shadow photographs, thus obliterating even model profile information. Under certain aeroballistic range conditions, high aerodynamic density gradients near the nose regions of the models produce considerable distortion in visible-light shadow photographs of such models. These distortions result primarily from refraction effects; in some cases, the luminosity of these nose cap regions is also sufficient to produce fogging of the film.

The Q-switched ruby laser has characteristics which make it an excellent light source for use in a front-lighted photographic technique for obtaining photographs of models in flight within aeroballistic ranges. The short time duration of the laser pulse effectively "stops" motion, the high intensity provides adequate film exposure, and the monochromaticity allows filtering of unwanted light.

A brief description of the laser photographic technique developed and employed successfully in the 1000-ft hypervelocity range (Armament Test Cell, Hyperballistic (G)) of the von Karman Gas Dynamics Facility (VKF) is given, and some initial results are presented herein.

SECTION II
DESCRIPTION

2.1 OPTICAL ARRANGEMENT

The direct-photographic system is shown schematically in Fig. 1 (Appendix). The beam from a pulsed ruby laser is diffused by a ground glass, and a portion of the diffuse light is directed by a 47-mm focal length (f. 1.) lens into a 508-mm f. 1. collimating lens. This expanded beam (approximately 5 in. in diameter) is used to illuminate models in flight. A white cardboard diffusing screen is placed perpendicularly to the expanded beam. This diffusing screen serves to delineate the model.
The camera (4- by 5-in. Graflex®) is mounted directly above the laser, and the optical axis of the camera forms an angle of approximately 15 deg with the laser beam. The camera employs a 360-mm f. 1. lens. The lens is stopped down (f/D = 25) to produce a 4-in. depth of field. A greater depth of field may be obtained by stopping the camera lens more, provided sufficient light intensity is available. A narrow bandpass filter (maximum transmission = 60 percent at λ₀ = 6943 Å, Δλ₁/₂ = 15 Å) at the camera lens severely attenuates light other than that at the laser wavelength. This allows operation of the camera in an open-shutter mode, since there is little or no 6943 Å background light.

A red-sensitive film (Kodak S0243®) is used. This film has an ASA emulsion speed rating of 1.6 and a resolution of 500 lines/mm.

Both the camera lens and the collimating lens are mounted in range ports in such a manner that the lenses serve also as vacuum-tight windows.

This system is customarily installed in Range G at an axial location 64 ft from range entrance. (Other such systems are available at other locations.)

2.2 LASER SYSTEM

The laser system employed in the front-lighted photographic technique is a pulsed ruby laser, Korad Corporation Model K-1CQ. The laser is operated in the Q-switched mode using a pockels cell. Characteristics of the laser system are as follows:

- Peak power: ~50 MW
- Energy output: 1.09 J
- Pulsewidth (FWHM): 22 nsec
- Beam divergence (0.5 angle, 0.5 power): ~4 mrad
- Wavelength: 6943 Å
- Linewidth: 0.1 Å

SECTION III
PRELIMINARY RESULTS

Photographs have been obtained of several model configurations at velocities from 4600 to 20,000 ft/sec. These heretofore unavailable photographs enable valuable in-flight examinations of model integrity and surface condition.
Figure 2 shows a laser photograph of a model which was damaged during launching. This photograph shows quite clearly the location and extent of a small area of damage along the edge of the model. This slight model damage was not evident in visible-light shadowgrams, X-ray shadowgrams, or schlieren photographs. Surface damage such as that depicted in Fig. 2 can significantly alter the aerodynamic behavior of a model and its flow field.

Figure 3 shows laser photographs of lenticular models, both statically and in flight at various velocities. There is a marked difference between the appearance of the model surface in the photographs made under in-flight conditions and in the one made at static conditions. The model appears as would be expected in the static photograph (Fig. 3a); the shiny model surface reflects the laser light specularly. In each photograph of the model in flight, however, the forward portion of the model appears to reflect as a diffuse surface, and there is an apparent effect of velocity. In Fig. 3b (velocity = 4600 ft/sec), the model surface reflects specularly except for a small diffusely reflecting region on the nose, whereas, in the photographs of higher velocity models (>9000 ft/sec), the entire forward portion of the model appears in each photograph as a diffusely reflecting surface (Figs. 3c, d, and e). At 18,000 ft/sec (Fig. 3e), the nose region appears to be nonreflecting (in the direction of the camera). These phenomena were consistently observed, i.e., all photographs of these lenticular models at nominally 4600 ft/sec show the "white spot" or diffuse nose region, whereas all photographs made at higher model velocities show the entire front portion of the model to reflect diffusely. Likewise, the "dark nose" appearance was consistently obtained on shots at velocities of nominally 18,000 ft/sec.

Photographs of a 25-deg semiangle cone made under static and in-flight (19,690-ft/sec) conditions are shown in Fig. 4. Again, the reflection characteristics of the model surface appear distinctly different for the two conditions. This in-flight appearance (Fig. 4b) was observed in all laser photographs of this model configuration at velocities of nominally 20,000 ft/sec and range pressures of nominally 40 torr.

Figure 5 shows a laser photograph and a conventional visible-light, Fresnel lens shadowgram obtained during the flight of a 1-in. -diam steel sphere (velocity: 10,800 ft/sec; range pressure: 731 torr). The design of the Fresnel lens shadowgraph is described in detail in Ref. 1. Conditions of this shot were such that high aerodynamic density gradients were established in the region just forward of the sphere. These high density gradients produced intense refraction effects which seriously distorted the visible-light shadowgraph results as demonstrated in Fig. 5a. (No noticeable distortions were observed in X-ray shadowgrams
from this shot. The laser photograph (Fig. 5b) shows an apparently undistorted view of the sphere as well as the bow shock wave. The film negative of this photograph was examined on a Benson-Lehner Model 29E digitized film reader, and a measurement of the horizontal diameter was found to agree with a measurement of the vertical diameter to within 0.25 percent. This indicates that high density gradients have little distorting effect on the image recorded using the front-light laser photographic technique.

Further, this example (Fig. 5) illustrates to some extent that the front-light laser photographic system is impervious to the effects of self-luminosity. A streak resulting from the luminosity of the shock cap region is evident in the shadowgram of Fig. 5a, whereas the laser photograph of Fig. 5b was not affected at all by this self-luminosity. Under some test conditions, of course, the self-luminosity (shock cap radiation and/or radiation produced by ablation processes) is much stronger, and the resultant streaking completely obliterates shadowgraph results. Unfortunately, no intensely ablating models have been launched since the laser photographic system has become operational, and therefore, direct experimental confirmation of its ability in this regard is not yet available. The example shown in Fig. 5 does illustrate the point that the self-luminosity streaking seen in the shadowgram is not visible in the laser photo. In addition, separate experiments using calibrated photomultiplier radiometers viewing through laser wavelength filters have shown that shock cap radiation, radiation from heavily ablating nylon spheres, and radiation from ablating aluminum spheres all fall at values less than $6.5 \times 10^{-4}$ watts/steradian.

The bow shock wave produced by the sphere in flight in Fig. 5 is apparent in the laser photograph as well as in the shadowgram. The fact that the shock wave is visible in the laser photograph probably resulted from the diffuse reflection of light from the white background card (see Fig. 1) back through the shock wave rather than from direct reflection of the laser beam by the shock wave. This arrangement provides, in effect, a combination of a direct-photograph system and a focused shadowgraph system with a weak, diffuse light source. The focused shadowgraph technique (recording camera focused on the model) would not be expected to suffer the distortion effects produced in the conventional shadowgram (e.g., Fig. 5a). Also, the weak diffuse nature of the light source (reflections from the background card) producing these effects accounts for the fact that only very strong shock waves of the sort produced by this high velocity-high pressure sphere shot are evident in laser photographs.

The shock wave in the laser photograph (Fig. 5b) appears as a much more distinct line than is the case in the shadowgram (Fig. 5a). The
bow shock detachment distance was measured from the laser photo-
graph and was found to agree with theory (Ref. 2) to within 15 percent. 
It was impossible, of course, to make such a measurement on the dis-
torted shadowgram.

Another point of interest is that the sphere surface did not reflect 
diffusely as was observed on shots of all other model configurations at 
velocities greater than 9000 ft/sec (e. g., Figs. 2, 3, and 4). How-
ever, the range pressures on all these shots were considerably lower 
than the 731 torr for the sphere shot. The photograph of Fig. 5b shows 
only specular reflection from the shiny surface of the sphere, just as a 
static photograph did of the same sphere.

SECTION IV
IMPROVED SYSTEM

The photographs presented above were obtained with the optical 
system schematized in Fig. 1. As mentioned in Section 2.1, this 
arrangement provides only a 5-in. -diam illuminating beam or field of 
view. The beam-expanding optical arrangement was changed to that 
shown in Fig. 6. This arrangement provides a 12-in. -diam field of 
view. This larger field of view alleviated trigger synchronization 
problems, thus improving the overall reliability of the system.

A flat, green background screen was found to produce better re-

eruits than the white screen used initially. Several of the photographs 
in Figs. 2, 3, and 4 show a bright highlight reflected from the upper 
edges of the model surfaces. This effect results from the reflection of 
light from the white background card. The green background with its 
reduced reflectance to light of laser wavelength eliminates this effect, 
yet still provides good definition of the model edges. The green back-
ground, of course, eliminates the focused shadowgraph effect discussed 
earlier. (It may, therefore, be desirable in some instances to use the 
white background.)

Figure 7a shows a static photograph of a 10-deg semiangle cone 
model (Cu nose, Al base). This model configuration is shown in flight 
in Range G in Fig. 7b (velocity = 12,750 ft/sec; pressure = 49 torr) and 
in Fig. 7c (velocity = 16,500 ft/sec; pressure = 14.5 torr). Evident in 
the photograph of Fig. 7c are very small (< 0.03-in. -diam) particles in 
the near wake of the model. These photographs demonstrate very well 
the performance of the improved laser photography system.
SECTION V
ACCURACY OF LENGTH MEASUREMENTS

The initial results obtained with the laser photographic system suggest applications of a more quantitative nature. One of these concerns measurements of the nose recession of eroding or ablating hypervelocity models. Some of the laser photographic data have been analyzed for the purpose of determining the accuracy which could be expected when using this technique for length (e.g., nose recession) measurements. Photographs (negatives) chosen for this evaluation of accuracy were from those shots on which the following criteria were met:

1. The model configuration was such that there were characteristic dimensions in both the horizontal and vertical planes suitable for measurements.
2. The model attitude and flight path were such that the film record portrayed a well-focused, direct side view of the model.
3. The model was well illuminated by the laser beam so that both the length and diameter could be measured from the film.

The film negatives of laser photographs from shots fulfilling these criteria were examined on a Benson-Lehner Model 29E digitized film reader. The diameter and length of the model were determined from the photographically recorded image on each suitable film record. The length measurements were corrected for motion blur and were compared with fabrication inspection measurements of length (accurate to ±0.0001 in.). The agreement between the values measured from the film and the actual values (inspection measurements) was extremely good. This agreement was consistently within ±0.002 in. in cases where the three criteria above were met.

Criterion No. 2 cannot be met on all launchings in the aeroballistic range; however, orthogonal shadowgraph systems employed in the VKF aeroballistic ranges do produce accurate records of model attitude and flight path. Therefore, appropriate geometric correction factors can be calculated and applied to length measurements.

SECTION VI
CONCLUSIONS

Initial results indicate that the laser front-lighted photographic technique provides an excellent method for in-flight examination of
hypervelocity models. Laser photographs reveal in fine detail the condition of model surfaces after launching, providing information which is not available from schlieren, shadowgraph, or X-ray results. This information is frequently of value in interpreting aerodynamic and aero-
physical results. The employment of a second camera and a mirror for illumination of the "back side" of the model should allow a more complete in-flight inspection of the model surface.

The laser photographic technique is impervious to refraction and self-luminosity effects which, under some test conditions, are highly detrimental to shadowgraph, schlieren, and other photographic results. Thus, models producing high density gradients and/or ablation may be observed with no loss of clarity.

It has been shown that, under certain conditions, shock waves can be observed in the laser photographs of hypervelocity models. These preliminary results indicate that the focused shadowgraph effect could be further utilized to produce a composite picture made up of a direct photograph of the model with a shadowgram of its flow field.

Length and nose contour measurements can be accurately (±0.002 in.) extracted from laser photographic data even under conditions of ablation, self-luminosity, and high density gradients. This introduces the possibility of erosion and ablation rate studies, since it has been shown that the high density and self-luminosity usually associated with ablation should not affect the integrity of such length measurements. Several axially spaced laser photographic stations will allow detailed observation of ablation or erosion effects and accurate determinations of ablation or erosion rates.

REFERENCES


APPENDIX
ILLUSTRATIONS
NOTES:

1. Lenses L₁ and L₂ are mounted in range ports in such a manner that the lenses serve also as vacuum-tight windows.

2. Laser characteristics:
   - Output Power, 50 mw
   - Duration, 20 nsec

Fig. 1 Laser Photographic System
Material, Stainless Steel
Diameter, 2.17 in.
Length, 1.25 in.

Imprint of Sabot Joint
Damaged Edge

Model

Velocity, 18,000 ft/sec
Range Pressure, 11 torr
Exposure Duration, 20 nsec

Fig. 2 Laser Photograph of a Model in Flight within Range G, Demonstrating the Capability for Detection of Model Damage
Fig. 3 Laser Photographs of Lenticular Models

Model
Material, Stainless Steel
Diameter, 2.17 in.
Length, 1.25 in.

Range Pressures, 11 torr
Exposure Duration
(All Cases), 20 nsec
Model
Material, Al Base; Cu Nose
Base Diameter, 1.23 in.
Length, 1.08 in.

Velocity, 19,690 ft/sec
Range Pressure, 40.8 torr
Exposure Duration (Both Cases), 20 nsec

Fig. 4 Semiangle Blunt Cone (25-deg)
Self-Luminosity Streaking

a. Shadowgram

Velocity, 10,900 ft/sec
Range Pressure, 731 torr
Steel Sphere, 1-in. Diameter

b. Direct Laser Photograph

Fig. 5 Comparison of Laser Photograph and Shadowgram of a Model with High Density Gradients in the Nose Region
Lenses are mounted in range ports in such a manner that they serve also as vacuum-tight windows.

2. Laser characteristics:
   Output Power, 50 mw
   Duration, 20 nsec

Fig. 6 Improved Laser Photographic System
Model
Material, Al Base; Cu Nose
Base Diameter, 1.0 in.
Length, 2.75 in.

Fig. 7 Semiangle Cone (10-deg)

a. Static

b. In Flight at 12,750 ft/sec

Range Pressure 49 torr

Exposure Duration (All Cases), 20 nsec

Range Pressure 14.5 torr

c. In Flight at 16,500 ft/sec

≈ 0.03-in.-diam Particle
**Abstract**

A front-lighted photographic system employing a giant-pulse ruby laser as a light source has been developed and installed in the 1000-ft hypervelocity Range G of the von Karman Gas Dynamics Facility. Preliminary results indicate that this photographic technique provides an excellent method for in-flight examinations of model integrity, surface condition, and for accurate in-flight measurements of model profile dimensions ($\pm 0.002$ in.) and their changes that might be produced by erosion or ablation.
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2. Laser photography

3. Lasers - Application

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