TITLES AND ABSTRACTS
"GEOLOGIE UND BAUWesen"
(GEOLOGY AND CIVIL ENGINEERING)
1944 to 1962

Klaus W. John

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Titles and Abstracts

Geology and Civil Engineering
1946-1962

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INTRODUCTION

PROFESSOR STINI'S ENGINEERING GEOLOGY

It can safely be asserted that Professor Terzaghi founded the classic soil mechanics with the publication of his book "Erbaumechanik" in 1925. At about the same time, Professor J. Stini of Wien, Austria, also originated a unique approach to engineering geology, which since has developed in a distinctly different fashion as compared to conventional geology applied to technological problems.

From the very beginning Stini's engineering geology emphasized the importance of the structure of rock masses, as given by its plane-fabrics features, such as jointing, bedding, and schistosity. Stini's work on statistical surveys of geological discontinuities greatly contributed toward techniques of determining and evaluating the anisotropy of rock masses.

Stini's concepts gave birth to "geomechanics" (or rock mechanics as generally designated in English-speaking countries) as developed and practiced in the Central European Alpine countries since the 1920's. Professor Stini actively participated in this development until his death in 1957. Since then, Dr. L. Müller, of Salzburg, Austria, has provided this group with a leadership that is conscious of the need for further methodical evolution. The "Salzburg School of Rock Mechanics" emerged from this more recent development. In this endeavor Dr. Müller has actively been supported by the late Professor L. Föppl, F. Pacher, and others.

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This development of geomechanics and rock mechanics, covering about four decades, ultimately resulted in initiation of the International Society of Rock Mechanics by Dr. Müller.

"GEOLOGIE UND BAUWESEN"

The most important work of Professor Stini is unfortunately not presented in his books. His book, "Technische Geologie," published in 1925, does not, in his own opinion, represent modern engineering geology. True engineering geology, as advocated by Stini's Austrian School, is much better documented in his three-hundred odd papers than in his books.

A considerable number of Stini's papers have been published in "Geologie und Bauwesen" (Geology and Civil Engineering) which was founded by him in 1929. The principal objective of this periodical originally was to further the relationship between civil engineering and geology. With increasing progress this mutual, beneficial collaboration expanded to include engineering mechanics, geophysics, mining engineering, application of engineering geology to biology (termed "engineering biology" in European usage), and others.

In May 1963, in connection with forming of the International Society of Rock Mechanics, the periodical was renamed Felsmechanik und Ingenieurgeologie - Rock Mechanics and Engineering Geology - Journal of the International Society of Rock Mechanics. Thus, the new name goes hand-in-hand with an increased internationalization of its contents.

THE LANGUAGE BARRIER

The work published by Stini and Müller, and their disciples, represents a vast treasure of concepts, ideas, methods, and experiences, supported by case histories, in the fields of engineering geology, rock mechanics, and geotechnical engineering. All of this, because it is almost exclusively published in German, remained relatively unknown in the English-speaking world.

The compiler of the present titles and abstracts attempted earlier to summarize the concepts of the "Salzburg School of Rock
Mechanics in a paper in the English language." The interest in the particular subject, expressed in the discussion and request for more information, suggested that additional effort might well be justified to overcome the language barrier and to disseminate some of the information contained in "Geologie und Bauwesen" in the English language.

PRESENT COVERAGE

The titles and abstracts as given here represent an attempt only to cover the most recent publications.

Volumes 16 (First Postwar) to 23 (1946 to 1957)

For this period, only the titles, original and translated, and authors of all 135 papers contained in "Geologie und Bauwesen" are included.

Volumes 24 to 28 (1958 to 1962)

This period concludes the publication of the original "Geologie und Bauwesen." Of the 90 papers published, short abstracts are given in addition to the titles and authors as indicated above.

The present collection was discontinued with the issuance of the renamed version of the publication in May 1963. Commencing at that time, each edition of the new journal contains English-language abstracts for all papers.

LIMITATIONS

It is well realized that the present coverage omits, or touches too lightly, many important contributions, particularly a considerable number of earlier papers by Stini and Müller. It is hoped that this series of titles and abstracts can be completed at a later date.

CLASSIFICATION

All entries, titles, and titles and abstracts were listed under one of the following subject groups. Although in many cases such a rigid classification is difficult to achieve, it is believed that it generally aids in reviewing the material presented in "Geologie und Bauwesen."

1. Engineering Geology
2. Geohydrology and Hydrology
3. Engineering Mechanics
4. Rock Mechanics
5. Testing and Test Results
6. Tunnels and Underground Excavations
7. Dam and Rock Abutments
8. Slopes and Landslides
9. Rock Bolting and Rock Anchors
10. Soil Mechanics
11. Geophysics
12. Miscellaneous Titles

Within the subject headings (numbers), titles and abstracts are listed in chronological sequence. The resulting index numbers are used in Section III - AUTHORS' INDEX. Unless indicated to the contrary, the original articles appeared in the German language.
II. TITLES AND ABSTRACTS

1. ENGINEERING GEOLOGY

1.01 Are Dirt Roads Feasible in the Hungarian Lowland, Considering the Geological and Hydrological Conditions? (Kann die Erdstrasse im Hinblick auf die geologisch-hydrologischen Grundlagen als die Bauweise für die Ungarische Tiefebene angesehen werden?)

L. Hauser Vol. 16, No. 2, 1947, pp. 49 - 63

1.02 Suggestions for an Engineering Geological River Map (Anregungen zu einer flussbaugeologischen Karte)

K. Bistritschan Vol. 16, No. 2, 1947, pp. 64 - 64

1.03 Houskeeping, also in Engineering Geology (Haushalten, auch in der Ingenieurgeologie)

G. Beurle Vol. 16, No. 2, 1947, pp. 76 - 77

1.04 On the Knowledge of the Deep Canyons (Zur Kenntnis der Tiefenrinnen)

J. Stini Vol. 16, Nos. 3/4, 1948, pp. 96 - 105

1.05 Hydrological and Engineering Geological Observations at the French Atlantic Coast (Hydrologische und baugeologische Beobachtungen an der französischen Atlantikküste)

K. Bistritschan Vol. 17, No. 4, 1950, pp. 109 - 119

1.06 On the Occurrence of Building Stones in the Upper and Lower Pinz Provinz (Über die Bausteinvorkommen des Ober und Unterpinzgaues)

A. Haiden Vol. 17, No. 4, 1950, pp. 126 - 142
1.07 Engineering Geological Map of the River Enns - Part One (Flussbaugéologische Karte der Enns - 1. Teil)
K. Bistritschan Vol. 18, No. 1, 1950, pp. 1 - 8

1.08 On Geotechnical Investigations of River Power Plants (Über die Baugrunduntersuchung an Flusskraftwerken)
H. Seelmeier Vol. 13, No. 1, 1950, pp. 9 - 17

1.09 Engineering Geological Annotations on Modern Dam Construction (Baugeologische Randbemerkungen zum neuezeitlichen Talsperrenbau)
J. Stini Vol. 18, No. 1, 1950, pp. 18 - 29

1.10 On the Weathering Phenomena of Marl and Clay Slates of the Flysch Zone of Scheibbs (Über Verwitterungerscheinungen bei Mergeln und Tonschiefern der Flyschzone von Scheibbs)
W. T. Schmidt Vol. 18, No. 1, 1950, pp. 44 - 46

1.11 Engineering Geological Measurements of Dip Angles and their Evaluation (Baugeologische Fallwinkelmessungen und ihre Auswertung)
J. Stini Vol. 18, No. 2, 1951, pp. 65 - 82

1.12 A "Dot Reaction" to Characterize Rock Structures (Eine Tüpfelreaktion zur Kennzeichnung von Gesteinsstrukturen)
H. Häusler Vol. 18, No. 3, 1951, pp. 186 - 194

1.13 On the Relations Between Joints and the Valley System of the Mountain Region of Graz (Über die Zusammenhänge zwischen Klüftung und Talnetz im Grazer Bergland)
H. Flügel Vol. 18, No. 3, 1951, pp. 195 - 200
1.14 Annotations on the Problem of the Forming of Caves (Randbemerkungen zur Frage der Entstehung der Höhlen)
J. Stini Vol. 18, No. 4, 1951, pp. 228 - 235

1.15 Engineering Geological Observations at Reconstruction Projects (Baugeologische Beobachtungen bei Wiederaufbauvorhaben)
E. Schröder Vol. 18, No. 4, 1951, pp. 236 - 242

1.16 Engineering Geological Map of the River Enns - Part Two (Flussbaugeologische Karte der Enns - 2. Teil)
K. Bistritschan Vol. 19, No. 1, 1952, pp. 29 - 30

1.17 Geotechnics or Geology (Geotechnik oder Geologie)

1.18 The New Austrian Code on Building Stones (Die neue österreichische Gesteinsnormung)
A. Kieslinger Vol. 20, No. 1, 1953, pp. 1 - 5

1.19 Representation of Geological Planes in Engineering Plans (Die Darstellung geologischer Flächen in Bauplänen)
L. Müller Vol. 20, No. 1, 1953, pp. 6 - 10

1.20 The Geological Profile of the Old Semmering Tunnel (Das geologische Profil des alten Semmeringtunnel)
W. J. Schmidt Vol. 20, No. 1, 1953, pp. 10 - 13

1.21 Comparison of the Geotechnical Conditions at the Old and the New Semmering Tunnel (Vergleich der technisch-geologischen Verhältnisse beim alten und neuen Semmeringstunnel)
W. J. Schmidt Vol. 20, No. 1, 1953, pp. 19 - 24
1.22 A Contribution on Structures Protective Against Avalanches
(Ein Beitrag zum Lawinenschutzbau)

K. Killian
Vol. 20, No. 1, 1953, pp. 24 - 27

1.23 Engineering Geologist or Geological Engineer (Ingenieurgeologie
oder Geologingenieur)

J. Stini
Vol. 20, No. 1, 1953, pp. 28 - 33

1.24 Geologic-genetic Considerations in Geotechnical Problems
(Geologisch-genetische Gesichtspunkte bei Baugrundfrageen)

G. Keller
Vol. 20, No. 2, 1953, pp. 41 - 55

1.25 Examples of Geotechnical Maps (Beispiele ingenieur-geologischer
Baugrundkarten)

A. Graupner
Vol. 20, No. 2, 1953, pp. 77 - 82

1.26 Geotechnics as Related to Geology, Civil Engineering, and Geophysics
(Die Geotechnik in ihrer Beziehung zur Geologie, Bautechnik und
Geophysik)

K. Keil
Vol. 20, No. 3, 1953, pp. 177 - 186

1.27 Engineering Geology (Ingenieurgeologie)

K. Keil
Vol. 20, No. 3, 1953, pp. 187 - 190

1.28 To the Knowledge of Deep Canyons, a Supplement (Zur Kenntnis
der Tiefenrinne, eine Ergänzung)

E. M. Winkler
Vol. 21, No. 3, 1955, pp. 110 - 114

1.29 Engineering Geological Map of the River Enns (Flussbaugeologische
Karte der Enns)

K. Bistritschan
Vol. 21, No. 3, 1955, pp. 123 - 128
1.30 A Geotechnical Map of the City of Göttingen (Eine geologische Baugrundkarte der Stadt Göttingen)
M. P. Gwinner
Vol. 22, No. 1, 1956, pp. 49 - 53

1.31 Remarks on Engineering Geological Evaluation of Borings (Bemerkungen zur baugeologischen Untersuchung von Bohrungen)
H. Häusler
Vol. 22, No. 1, 1956, pp. 61 - 65

1.32 Near East UNESCO Symposium on Applied Geology in Ankara, Turkey (Nahost-UNESCO-Symposion für Angewandte Geologie in Ankara)
K. Bistritschan
Vol. 22, No. 2, 1956, pp. 130 - 134

1.33 Core Drilling in Civil Engineering Explorations (Die Kernbohrung als Schürfbohrung im Bauwesen)
H. Seelmeier
Vol. 22, No. 2, 1956, pp. 135 - 140

1.34 Engineering Geological Observations at the Sariyar Power Plant in Turkey (Baugeologische Beobachtungen beim Kraftwerk Sariyar-Türkei)
K. Bistritschan
Vol. 22, No. 3, 1956, pp. 221 - 223

1.35 Engineering Geological Reports on Tunnels (Tunnelbaugeologische Gutachten)
E. E. Hensolt
Vol. 23, No. 3, 1957, pp. 139 - 160

1.36 Geological Survey and Prediction During Construction of Hydro-power Plant Prutz-Imst in Tyrol (Geologische Aufnahme und Voraussage beim Kraftwerksbau Prutz-Imst der TiWAG (Tirol))
The 7.7-mile (12.3 km) long pressure tunnel of the Hydro-power Plant Prutz-Imst at the Inn River, Austria, was completed in 1956. The results of the engineering geological exploration, which were based on superficial outcrops only, are compared with the actual findings during construction. The tunnel penetrated quartz phyllite and phyllite gneiss
with complex rock structures. The overburden ranged up to 3300 ft (1000 m) in depth. The difficulties of extrapolating geological data from surface observations to the tunnel location are discussed. Generally good correlation was found during construction. Details on the rock structure are given. The advantage of using stereo maps for evaluation of geological features is stressed. The penstock and the underground powerhouse, 162 by 83 ft (50 by 25 m) in plan and 60 ft (18 m) high, were located in jointed limestones and dolomites. The excavation was orientated so that the geostatistical influence of the predominant joints was minimized. The metamorphic rocks proved highly impermeable. The limestone at the powerhouse location was highly permeable, resulting in up to 37 GPS (140 l/sec) flow at individual locations.

O. Schmidegg
Vol. 24, No. 1, 1958, pp. 22 - 29

1.37 Are Engineering Geological Surveys to Include a Detailed Investigation of the Water Contained in Joints of In-situ Rock Masses?
(Soll die baugeologische Geländeaufnahme auch eine eingehende Untersuchung der Kluftwasserverhältnisse im Felsgebirge einschließen?)

Any engineering geological investigation of underground structures of some importance should include a careful study of the ground water conditions by means of borings. Knowledge of the position of the phreatic line of the water in joints and faults of the rock mass is important for design and construction of pressure tunnels, dams and their reservoirs, and remedial measures for unstable slopes. The point of the paper is supported by numerous outlines of case histories.

J. Stini
Vol. 24, No. 1, 1958, pp. 31 - 36

1.38 Utilization of New Type of Spatial Model in Applied Geology
(Über die Anwendung eines neuartigen räumlichen Modellies in der praktischen Geologie)

Spatial models, which illustrate the inhomogeneities and anisotropies of rock masses, are utilized for design of dams, large underground openings, and mine workings. A model showing contour lines and geological features by a system of wires bent accordingly is preferred over a model utilizing continuous horizontal plates, because of the difficulties in adjusting to new findings. The model of a dam site with the dam in place allows convenient observation of the change
in relation between predominant geological features and the direction of the dam thrust as the structure is rotated or otherwise modified.

A. Fuchs Vol. 24, No. 2, 1958, pp. 118 - 120

1.39 The Pressure Tunnel of the Hydropower Plant Altenmarkt at the Enns River (Der Triebwasserstollen des Ennskraftwerkes Altenmarkt)

Several alternate alignments of a pressure tunnel, approximately one mile long, to be constructed in Austria, were studied in order to avoid unfavorable geological conditions. Using his extensive knowledge of the region and judgment, J. Stini proposed an alignment which was considerably longer than the direct route, but which probably would not penetrate critical zones composed of slate with gypsum. Subsequent detailed investigations confirmed the advantages of the alignment as selected in the preliminary investigation.


1.40 Possibilities and Limitations of Geological Predictions, Discussed Using the Example of the Loibl Tunnel (Möglichkeiten und Grenzen der geologischen Voraussage, erörtert am Beispiel des Loibltunnels)

In southeastern Austria a highway tunnel, approximately one mile long (1.6 km), was to be driven through highly faulted rock masses of the Triassic period. Comprehensive geological explorations provided important information for the design engineers. The selection of the most favorable tunnel alignment, including the location of the tunnel entrances, was based upon geological surface observations. Findings during construction proved the geological predictions to be correct, except for a 370-ft (110 m) zone where less stable rock was encountered. In this zone the geological conditions were too complex to be extrapolated from surface surveys only.

F. Kahler Vol. 24, No. 3/4, 1959, pp. 165 - 170
1.41 Weathering of Rock (Rahmenverwitterung)

The type of grain bond of rocks, either indirect bond in sandstones or direct bond such as in granite or marble, determines the mechanics of weathering. The scaling of plane surfaces of building stones often commences at the center and progresses to the edges. This effect is believed to be due to more rapid drying near the edges of the surface. The center remains moist longer, which initiates the weathering effect. Some geological analogies to this process are given. Numerous photos illustrate the exfoliation of different types of rock due to weathering.

A. Kieslinger Vol. 24, No. 3/4, 1959, pp. 171 - 186

1.42 Significance of Glacial Formations of the Alps for the Design of Pumping-Storage Plants, Presented Using the Hydropower Plant Weissach, Algau (Die Bedeutung der alpinen eiszeitlichen Bildungen für die Planung von Speicher-Kraftwerken, dargestellt am Weissach-Kraftwerk im Allgäu)

At the site of the proposed arch dam, a hydropower plant in southern Germany, molasse rock was encountered at one abutment and till at the other, indicating an epigenetic valley. When resistivity measurements did not provide definite results, five core borings were drilled which disclosed the considerable depth and horizontal extent of the moraine deposit at one abutment. The proposed dam had to be modified to an earthfill dam utilizing the moraine material. The pressure tunnel, approximately three miles (5 km) long, is to penetrate different types of molasse material. The proposed alignment was lowered by 133 ft (40 m) in order to avoid a trench filled with lake deposits of rock flour. Geological conditions resulted in placing the penstock and the powerhouse underground instead of on the till and clayey materials on the surface. The original design concept, which was developed without thorough geological information, had to be modified essentially because of the adverse geological conditions found later.


1.43 From the Working Day of an Engineering Geologist (Aus dem Alltag eines Baugeologen)

The author, a geologist by trade, has come to engineering geology through soil mechanics. His professional activity encompasses the entire field of geotechnics, foundation investigations in both soil and rock, subgrade design for
highways, tunnel design, and slope stability studies. Several examples illustrate particular geotechnical problems, some in considerable detail. Principal aspects of geotechnical consulting on a commercial basis in Switzerland are discussed briefly.

A. Von Moos


During construction of the "thermal adit," 1.5 miles long (2.4 km), with overburden ranging up to 3450 ft (1035 m), near Badgastein, Austria, temperatures of the rock mass were observed which could not be explained by the deep overburden. From the tunnel entrance the temperature gradually increased to 111°F at Station 1.0 mile (1.6 km). The temperature then decreased in spite of the further increase of the overburden depth, resulting in temperatures considerably higher than the theoretical temperatures as would be determined by the geothermal gradient. Uranium minerals were found in the rock masses; the air in the adit also proved to be highly radioactive. The general phenomenon was investigated in a comprehensive hydrogeological and geophysical study. The thermal source and the considerable influence of major joints on the temperature propagation were derived from the pattern of temperature distribution. It is concluded that in spite of the subject experience, the standard concept of predetermining the temperatures in drifts by means of geothermal gradient is adequate.

F. Scheminzky and J. Stini

1.45 The Pressure Tunnel of the Hydropower Plant Hieflau at the Enns River (Der Triebwasserstollen des Ennskraftwerkes Hieflau)

A detailed account of a carefully planned and executed engineering geological exploration and control of a 3.7-mile-long pressure tunnel in Styria, Austria, is given. The alignment of the tunnel is parallel to the slope of a mountain massif consisting of limestone with some dolomite. The conditions are generally favorable for construction. A detailed geological survey of the tunnel alignment was conducted during
construction. The results of this survey are presented in the paper. In the center portion of the tunnel, local over-stressing of the rock after excavation was observed. This overstressing was due to the combination of considerable over-burden height with unfavorable orientation of the principal jointing. The penetration of a buried channel, approximately 80 ft (25 m) wide and filled with gravel, proved to be somewhat difficult. Numerical data are given on construction processes, which are believed typical for European construction techniques.

H. Seelmeier
Vol. 24, No. 3/4, 1959, pp. 242 - 257

1.46 The Significance of Concepts of Historical Geology for Rock Mechanics (Die Bedeutung der historischen Denkwweise in der Geologie für die Geomechanik)

In rock mechanics, the genetic concept of the geology is often neglected, although it could provide valuable technical information. The importance of the paleogeographical and paleoclimatic conditions for the petrofabrics of the rock material is stressed. The influence of tectonic processes on the technological properties of the in-situ rock is obvious. Morphological concepts also should be considered. In many phases of geotechnics, the relation between the structure of a rock mass and geological processes which cause them is not clearly recognized. The time factor in geological processes is very important.

K. H. Heitfeld
Vol. 25, No. 2/3, 1960, pp. 191 - 202

1.47 Geomorphology and Petrofabrics of Basalt (Formen und Strukturen des Basaltes)

The history of the origin of tertiary basalt is not yet completely understood. The differentiation between origin by extrusion and origin by intrusion is not yet possible. Based on the author's observation of the eruption of the Kilauea Iki volcano on Hawaii in November, 1952, the different patterns and petrofabrics of basalts and their origin are analyzed. In conclusion, petrofabrics of both extrusion and intrusion materials are described in detail. The paper represents a detailed account of primarily geological interest.

E. Schenk
Vol. 26, No. 4, 1961, pp. 258 - 272
1.48 Mapping of In-situ Rock for Geotechnical Purposes (Die Kartierung von Festgesteinen für geotechnische Zwecke)

A method for classifying in-situ rock according to its geotechnical properties is given. The following features are considered: rock type, elasticity and deformability, reaction upon stress relief, homogeneity, compactness, properties in connection with the ground water, and excavation and crushing characteristics. Many examples of this classification system are given. Codes for degrees of bedding, jointing, and faulting are introduced. Color codes for different types of rock are also proposed.

A. Graupner Vol. 26, No. 4, 1961, pp. 273 - 288

1.49 Engineering Geological Investigation at the Wag-Plateau (Bau-geologische Erkundungen auf der Waghochfläche)

The principal aspects of an engineering geological investigation of the site of the upper reservoir of a pumped-storage hydropower plant in Styria, Austria, are given. Large-scale percolation tests in shafts served to determine the permeability of the terrace materials. Since the sands and gravels of the higher terrace were not deemed satisfactory, the bottom of the reservoir was located in the silty and cemented gravel of the lower terrace. In addition, the geologic history of the site is outlined.

E. Fischer and G. Spaun Vol. 27, No. 2, 1961, pp. 37 - 44

1.50 The Statistical Significance of Data on Rock Structure in Applied Geology (Die statistische Bedeutung von Strukturdaten in der angewandten Geologie)

Knowledge of the petrofabrics of the rock substance and the structure of in-situ rock is important for other than pure research purposes. Particularly, data on the structure of rock masses are of great significance in engineering geological work. The development of research on fabrics is reviewed briefly; reference is made to Exner, W. Schmidt, and Sanders. The mathematical relation between the number of observations, the area of the equal-area projection, and the area of the unit area after Kamb are given. This relation should give previous investigations on petrofabrics and rock structures more statistical significance.

M. Kirchmayer Vol. 28, No. 1, 1962, pp. 55 - 57
1.51 On the Necessity and Scope of Geological Investigations in Dam Construction (Über Notwendigkeit und Ausmass geologischer Untersuchungen im Talsperrenbau)

The scope of the explorations of dam sites within the slate ranges of the Rhine Valley has expanded during the past decades. Although detailed geological maps of the subject area were already available, geological investigations of the earlier hydropower projects consisted essentially of general geological reports only. Only since 1945 have comprehensive geotechnical investigations, based on borings, been performed at future dam sites. These explorations resulted in more definite information, particularly on the permeability of the dam foundations. Three examples of dam projects subject to earlier investigations illustrate some of the shortcomings of the more general geological approach based on outcrops only. In conclusion, the following methods of modern geotechnical explorations are reviewed: geophysics investigations, drilling methods, logging of bore holes, geochemical investigations, ground water observations, water pressure tests, and rock mechanics tests.

H. W. Koenig and K. H. Heitfeld

Vol. 28, No. 1, 1962, pp. 63 - 76
2. GEOHYDROLOGY AND HYDROLOGY

2.01 The Flood Catastrophe in Salzburg in July 1946 (Die Salzburger Hochwasserkatastrophe Juli 1946)

2.02 The Measurement of Water Temperature as a Means to Determine Relations Between Springs and Open Flows (Die Wasserwärmemessung als Hilfsmittel bei der Bestimmung von Zusammenhängen zwischen Quellen und offenen Gerinnen)
J. Stini Vol. 16, No. 3/4, 1948, pp. 92 - 95

2.03 Investigations on Artesian Wells in the Styrian Basin, Considering Their Importance to the Tertiary Geology (Erhebungen über artesische Wasserbohrungen im steirischen Becken, unter Berücksichtigung ihrer Bedeutung für die Tertiargeologie)

2.04 Annotations on the Theory of Erosion (Einige Vorbemerkungen zur Theorie der Erosion)
G. Stratil-Sauer Vol. 18, No. 1, 1950, pp. 30 - 43

2.05 On the Determination of the Permeability of Soil Masses by Means of Settling Tests (Einges über die Bestimmung der Bodendurchlässigkeit durch Absitzversuche)
T. Lipcik and L. Müller Vol. 18, No. 2, 1951, pp. 102 - 111

2.06 The Surface Blanket of Flood Deposits (Die Lessdecke)
G. Stratil-Sauer Vol. 18, No. 3, 1951, pp. 123 - 142
2.07 The Deep Erosion of the Salzach River in the General Area of the City of Salzburg (Die Tiefenerosion der Salzach im weiteren Bereich der Stadt Salzburg)
K. Bistritschan and K. Fiebinger Vol. 18, No. 4, 1951, pp. 243 - 246

2.08 The Sensitivity of Ground Water Basins to Increased Extraction (Die Empfindlichkeit von Grundwasserbecken gegenüber gesteigerten Entnahmen)
G. Keller Vol. 19, No. 1, 1952, pp. 55 - 65

2.09 Flow Velocity at the River Bottom and Sediment Transportation (Sohlengeschwindigkeit und Geröllbewegung)

2.10 Blasting in Boreholes to Increase the Yield of Wells (Torpedierung zur Erhöhung des Wasserandranges in Grundwasserbohrungen)
G. Keller Vol. 19, No. 3, 1952, pp. 201 - 216

2.11 Storage of Water in Karst Caves (Wasserspeicherung in Karstohlförmen)
J. Stini Vol. 19, No. 4, 1952, pp. 258 - 273

2.12 A Tertiary Torrent in the Granitz Valley, Eastern Carinthia, and the History of its Region (Ein teriärer Wildbach im Granitztal (Ostkärnten) und die Geschichte seiner Landschaft)
P. Beck-Mannagetta Vol. 20, No. 3, 1953, pp. 139 - 144

2.13 Considerations on the Formation of Thermal Springs (Gedanken über die Bildung von Warmquellen (Thermen))
J. Stini Vol. 20, No. 3, 1953, pp. 212 - 228
2.14 Displacement of Rivers and Problems at the River Mouths (Flussverdrängung und Mündungsprobleme)
J. Putzinger Vol. 21, No. 1/2, 1954, pp. 51 - 60

2.15 Criteria of the Formation of Compensation Profiles (Kriterien der Kompensationsprofilbildung)
J. Putzinger Vol. 21, No. 1/2, 1954, pp. 61 - 67

2.16 On the Causes of Meandering of Rivers (Über die Ursachen des Schlingerns der Flüsse)

2.17 Does the Variation in Yield of Springs in Limestone Terrain Reflect the Quality of the Drinking Water? (Spiegeln die Schüttungsschwankungen der Quellen im Kalkgebirge die Güte des Trinkwassers wider?)

2.18 Geological Observations of the Flood Catastrophe in Styria in August 1958 (Geologische Beobachtungen von der steirischen Unwetterkatastrophe vom August 1958)

Excessive rainfall, up to 16 inches (400 mm) in 24 hours, resulted in extensive flooding and erosion within the Styrian part of the Eastern Alps in Austria. A detailed account of observations is given. Erosion of overburden materials resulted in considerable deposition in most brooks. The effect of poor plant cover is discussed. Hundreds of local slope failures developed because of saturation of the overburden soils. Thin overburdens proved to be more critical than thick ones.

E. Clar Vol. 24, No. 3/4, 1959, pp. 131 - 140

2.19 Leaching of Carbonic Rock (Auslaugung von Karbonatgesteinen)
Three examples of the formation of solution channels and caverns in phyllitic and limestone formations in the Central Alps (Austria) are described. The leaching is attributed
to both flowing and stagnant water. Considerable construction difficulties both in support of arch dams and tunneling resulted from these cavities.

G. Horninger Vol. 24, No. 3/4, 1959, pp. 159 - 164

2.20 Hydraulic Effects in Geodynamics

The paper presents a comprehensive treatise on the flow of surface water with related morphological processes. The dynamics of flowing water is reviewed. The equations of forces of fluids on particles are derived. River bed processes, such as turbulent flow and sediment transportation, are analyzed mathematically. Erosional and depositional processes forming slopes are illustrated by quantitative analysis. The mechanics of meandering and forming of deltas are discussed briefly. The existence of turbidity currents in oceans is discussed in the conclusion. The mathematical approach to subject problems is stressed throughout, which might also be of interest for practicing engineers and geologists who are searching for new approaches to problems related to surface flow of water. (Engl.)

A. E. Scheidegger Vol. 25, No. 1, 1959, pp. 3 - 49

2.21 Technical Changes of Subsurface Conditions Might Result in Reduced Agricultural Yields (Technische Eingriffe in den Untergrund mit landwirtschaftlichen Mindererträgen im Gefolge)

Civil engineering and mining projects, and technical measures related to them, might result in changes in the ground water conditions which, in turn, might result in reduced agricultural yields. The influence of an open pit operation in West Germany on the adjoining agriculturally utilized land, underlain by sandy soils, was investigated. Tests disclosed the hydrogeological conditions of the region. Based upon the findings, the damage claims were disproved in this particular case of permeable soils where rainfall was the principal source of soil moisture.

G. Keller Vol. 25, No. 4, 1960, pp. 248 - 255

2.22 Soils of the 'Hohen Tauern' and Their Hydrological Conditions (Böden in den Hohen Tauern und ihr Wasserhaushalt)

In connection with design and construction of the Kaprun hydropower project in Austria, a detailed analysis
was conducted of the influence of the anticipated change in ground water conditions in the soil of a sloping region and its hydrogeological conditions. A detailed account is given of location, climatic and geologic conditions, methods of investigation, soil sections, and soil mechanics and hydrological properties. The paper essentially presents data only; no definite conclusions to the particular problem are derived.

B. Ramsauer  Vol. 25, No. 4, 1960, pp. 268 - 298
3.01 On the Application of Engineering Mechanics in Structural Geology (Über die Anwendung der technischen Mechanik in der tektonischen Geologie)
H. Kastner Vol. 20, No. 2, 1953, pp. 56 - 76

3.02 The Transition from Adhesive Friction to Sliding Friction (Der Übergang von der Haftreibung zur Gleitreibung)
L. Föppl Vol. 21, No. 4, 1955, pp. 145 - 148

3.03 Disturbance of the State of Stress by Open Joints Adjacent to a Pressure Tunnel (Störungen des Spannungszustandes in der Umgebung eines Druckstollens durch Spalten)
L. Föppl Vol. 23, No. 1, 1957, pp. 4 - 8

3.04 States of Elastic Stress in Bodies with Plane Boundaries (Elastische Spannungszustände in Körpern mit ebenen Schnitten)
L. Föppl Vol. 23, No. 1, 1957, pp. 9 - 11

3.05 Photoelastic Studies of Retaining Walls, Laterally Supported by Pre-Tensioned Rock Anchors (Spannungsoptische Untersuchungen an angehefteten Stützmauern mit vorgespannten Stützankern)
G. Sonntag Vol. 23, No. 1, 1957, pp. 12 - 18

3.06 The Stressing of Rock Masses Surrounding a Slot, Depending on Its Direction as Related to the Ground Surface (Die Beanspruchung des Gebirges in der Umgebung eines Schlitzes in Abhängigkeit seiner Richtung zur Erdoberfläche)
G. Sonntag Vol. 23, No. 1, 1957, p. 19
3.07 The Strain Energy as Criterion for the Stability of a Circular Tunnel (Die Formänderungsarbeit als Kriterium für die Standsicherheit eines Stollens von kreisförmigem Querschnitt)
L. Föppl Vol. 23, No. 2, 1957, pp. 64 - 65

3.08 Bending Stress in Tunnel Linings Based on Photoelastic Studies (Biegebeanspruchung in Tunnelröhren auf Grund spannungsoptischer Untersuchungen)
G. Sonntag Vol. 23, No. 2, 1957, pp. 79 - 81

3.09 Support of Foundation Loads of Bedding Planes that Dip Downhill (Aufnahme von Fundamentkräften in talwärts fallenden Gleitschichten)

3.10 The Soil Pressure Under a Loaded Continuous Footing (Der Bodendruck unter einem belasteten Fundamentbalken)
A brief account is given of the stress distribution under continuous footings supported on an elastic medium. A formula for the stress distribution also is given. The theoretical concept was qualitatively confirmed by photoelastic experiments.
L. Föppl Vol. 24, No. 1, 1958, pp. 2 - 3

3.11 Investigation of Stability of Tunnels by Microseismic Methods (Untersuchung der Standfestigkeit von Stollen nach der Methode der kleinen Schwingungen)
The recognized fact that the stability of underground openings in competent rock decreases with increasing size of cross sections has not yet been proved physically. The stability of an infinite plate, with a circular hole punched in it and subjected to one-dimensional stresses, depends on the two states of radial and elliptic resonance of thin plates. Formulae for the stability criteria for both vibration modes are derived. In both formulae the radius of the tunnel is related to the wave lengths. Elliptic vibrations
represent the most critical condition. It is concluded that this consideration represents proof of the decreasing stability of tunnels with increasing diameter.

L. Föppl

Vol. 24, No. 3/4, 1959, pp. 147 - 158
4. ROCK MECHANICS

4.01 On the Differences of Geological and Technical Stressing (Von den Unterschieden geologischer und technischer Beanspruchungen)
L. Müller
Vol. 16, No. 3/4, 1948, pp. 106 - 161

4.02 The Technology of the Earth's Crust (Technologie der Erdkruste)
L. Müller
Vol. 17, No. 4, 1950, pp. 97 - 108

4.03 The Survey of Joints and the Orientation of Arch Dams (Kluftmessungen und Talsperrenlage)
R. Fill
Vol. 17, No. 4, 1950, pp. 114 - 125

4.04 The "Unit Rock Block" (Der Kluftkörper)
L. Müller
Vol. 18, No. 1, 1950, pp. 52 - 60

4.05 Analysis of the Residual Stress in Rock Masses (Berechnung des Gebirgsdruckes in Fels)
C. Torre
Vol. 18, No. 2, 1951, pp. 83 - 95

4.06 On the Degree of Loosening of Rocks (Über das Mass der Auflockerung von Gesteinen)
L. Müller
Vol. 18, No. 2, 1951, pp. 96 - 101

4.07 Annotation on the Formation of Cracks in Moist Mudstones (Eine Notiz zur Rissbildung an feuchten Peliten)
H. and E. Häusler
Vol. 18, No. 3, 1951, pp. 177 - 185

4.08 A Study Group for Rock Mechanics (Eine Arbeitsgemeinschaft für Geomechanik)
L. Müller
Vol. 18, No. 4, 1951, pp. 247 - 252
4.09 The Derivation of Rock Drilling Mechanisms to Two-Dimensionally Evaluated Diagrams on Effect of Drilling (Die Zurückführung der Gesteinsbohrmechanismen auf zweidimensional gewertete Bohrwirkungsbilder)


4.10 The Residual Pressure in Rock Masses and its Determination (Der Gebirgsdruck und seine Berechnung)


4.11 Improvised Investigation of the Strength of Rock Masses (Behelfsmäßige Untersuchungen der Gebirgsfestigkeit)

J. Stini Vol. 20, No. 1, 1953, pp. 34 - 36

4.12 An Example for Utilizing Structural-Analytical Methods in Engineering Geology (Eine Beispiel für die Anwendung gefügeanalytischer Arbeitsmethoden in der Baugeologie)

F. Karl Vol. 21, No. 1/2, 1954, pp. 68 - 86

4.13 The Design of the "Unit-Rock Block" (Konstruktion des Kluftkörpers)

F. Pacher Vol. 21, No. 1/2, 1954, pp. 87 - 89

4.14 The Securing of the Left Rock Abutment of the Sarobi Hydro-power Plant (Afghanistan) Against Large-Scale Rock Creep (Die Sicherung des linken Landpfeilers am Kraftwerk Sarobi (Afghanistan) gegen den Talzuschub des Gebirges)

L. Müller Vol. 21, No. 4, 1955, pp. 149 - 161

4.15 The Terminology Related to Residual Stresses in Rock Masses (Die Begriffsbildung in der Gebirgsdrucklehre)

J. Stini Vol. 21, No. 4, 1955, pp. 169 - 177
4.16 The Technical Effects of the Anisotropy in Rock (Technische Auswirkung des Gesteinsanisotropie)
L. Müller
Vol. 23, No. 1, 1957, pp. 1 - 3

4.17 Rock Mechanics Evaluation of Details of Rock Structure (Geomechanische Auswertung gefügekundlicher Details)

In-situ rock under stress behaves pseudo-plastically. It fails in a creeping manner following the direction of least resistance under a given state of stress. The failure patterns follow existing jointing in the rock mass. The terms of "residual bond" and "interlocking bond" of rock masses, and technical indices of the rock structure, are defined. The possibilities of analytical treatment are outlined. A brief account of rock mechanics exploration and analysis of geostatistical problems connected with working in a coal stratum is given. An outline of requirements for engineering geological investigations completes the paper. The paper contains an interesting table describing strengths and deformability of different types of in-situ rock.

L. Müller
Vol. 24, No. 1, 1958, pp. 4 - 21

4.18 Classification of In-situ Rock in Tunnel Construction (Gebirgsklassifizierung für den Stollenbau)

During construction of a 7.7-mile (12.3 km) long pressure tunnel in Austria, a classification for the in-situ rock was used which considered the particular conditions of tunnel driving. The in-situ rock can be classified according to the type of support and anchoring necessary for temporary support. With the wide variety of temporary support techniques, this has become increasingly difficult. Consequently, a classification system was devised which utilizes the relation between the time the unsupported opening remains stable and its width. Openings more than 13 ft (4 m) wide will remain stable in competent rock for many years. This time-span ratio decreases to five hours for five-ft (1.5 m) spans in friable rock masses and to ten seconds for six-inch (0.15 m) spans in unstable rock. The influence of the orientation of bedding, of the area of the cross section, and of the excavation and temporary support methods can be evaluated using similar time relationships.

H. Lauffer
Vol. 24, No. 1, 1958, pp. 46 - 51
4.19 Residual Stresses and Stress Relief in Rock (Restspannungen und Entspannung im Gestein)

Numerous stress relief phenomena on surficial rocks, predominantly igneous rocks, are described. In some cases large-scale scaling of flanks of mountains can be observed; in other cases thin parallel plates pop off horizontal rock surfaces. The same phenomena can be observed in steep rock slopes which result in fissuration approximately parallel to the slope line. This parallelism is sometimes obscured by subsequent erosion changing the original geomorphological form. It is believed that rock is able to store residual stresses which are ultimately relieved by volume expansion towards free surfaces. The fissuration of surficial rock due to overstressing independent of actual jointing is utilized in quarry operations.

A. Kieslinger
Vol. 24, No. 2, 1958, pp. 95 - 112

4.20 Indices of the Rock Structure (Kennziffern des Flächengefüges)

The structure of in-situ rock can be technically evaluated employing statistical surveying methods. The indices of two- and three-dimensional extent of joints are defined. Their relations to field measurements and to each other are given. These two values can be determined for any set of joints; they are utilized to describe the general structure of in-situ rock. Together with the orientation of joints, these values serve to construct the unit rock block, which represents the individual rock units that theoretically compose a jointed rock mass. Data on the technical properties of joint surfaces complete the information provided by rock mechanics surveys of jointed rock masses.

F. Pacher
Vol. 24, No. 3/4, 1959, pp. 223 - 227

4.21 Rock and Geomechanics (Fels und Geomechanik)

The relationship between engineering geology and soil mechanics, particularly the necessity of close collaboration, is discussed. Soil mechanics is limited to grained soil; beyond these limits rock mechanics, as a division of geomechanics, should take over. Rock mechanics is believed to be essentially an engineering field, beyond the reach of many geologists. The importance of rock mechanics for and the acceptance by the mining industry is stressed. Rock mechanics analyses are to be supported by testing. A rock testing laboratory is desirable.

F. Kahler
Vol. 25, No. 2/3, 1960, pp. 89 - 94
4.22 Ten Years of In-situ Measurements of Rock Compression, Progress and Practical Results (Dix ans de mesures de compression interne des roches; progrès et résultats pratiques)

Electricité de France developed several methods for determining the state of stress in in-situ rock masses. Simplicity, speed, and low costs were required from the construction point of view. Different types of test arrangements based on the stress relief technique are described. A new method in which the compression is determined from friction between steel plates of known properties is proposed. A vast amount of in-situ tests resulted in improved knowledge of the stress conditions in rock masses adjoining tunnels. Four case histories of in-situ stress measurements in tunnels are given, in which considerable numerical data are presented. (French)

J. Talobre  
Vol. 25, No. 2/3, 1960, pp. 148 - 165

4.23 Do Rock Bursts Occur Periodically? (Gibt es eine Periodizität der Gebirgsschläge?)

Previous investigators concluded that there is no periodicity of rock bursts in mining. However, from statistical evaluation of observation data of an East German mine a certain relationship between the occurrence of rock bursts and the tidal cycle can be derived. This tidal cycle influences not only the ocean, but also the earth's crust. The directions of the vectors of tidal accelerations vary and are believed to be a definite influence on stress-relieving processes in the earth's crust. The paper presents hypotheses but no definite conclusions.

K. H. Höfer  
Vol. 25, No. 2/3, 1960, pp. 166 - 175

4.24 Construction in Rock and Geomechanics (Gebirgsbau und Geomechanik)

Rock and soil mechanics are believed to be comparable in their predominant interest in problems of civil engineering and mining construction. Geomechanics covers a much wider field, the mechanics of the entire earth's crust, solving tectonics problems. Geomechanics could be considered to be a division of geophysics. The determination of the dynamics of tectonic processes based on rheology, rock structure, and mechanics appears to be the principal problem. The influence of the time factor is most important from a geological point of view.

E. Clar  
Vol. 25, No. 2/3, 1960, pp. 186 - 190
4.25 Rock Mechanics in Civil Engineering and Mining Practice

Die Geomechanik in der Praxis des Ingenieur- und Bergbaues

The wide scope of rock mechanics as applied to civil engineering and mining projects is illustrated by a variety of examples. Anchored revetment walls provide an economical structural element in highway and railroad construction in mountainous countries. The knowledge in some problems related to design and construction of arch dams, particularly the effects of water contained in and flowing through jointed rock masses supporting dams, has been improved by the application of rock mechanics concepts. More information is available now on the state of stress in steep rock slopes and the mechanics of their failure. Construction of a large underground power station in faulted rock masses necessitated extensive rock anchoring. The application of rock mechanics to tectonic problems appears promising.

L. Müller Vol. 25, No. 2/3, 1960, pp. 203 - 214

4.26 Rupture and Creep in the Terminology of Geology and Mechanics

Brechen und Fliessen in der geologischen und mechanischen Terminologie

A well defined terminology for the most essential processes of rock mechanics which can be understood by both engineers and geologists is urgently required. Abstracts from mostly European rock mechanics literature are used to present definitions being used or being proposed for specific problems, such as failure in rock, structure of rock mass (jointing, fissuration, faulting), and rheology of rock (deformation and creep in relation to time). The paper, which is intended to initiate a discussion, presents a very complete list of references to European publications on particular subjects.

L. Müller Vol. 25, No. 2/3, 1960, pp. 218 - 227

4.27 On the Stress-Strain Mechanism in Rock Masses Adjoining Underground Openings

Über den Mechanismus der Bildung der sogenannten 'Trompeter's Zone'

In 1929 the "Trompeter's Zone" was defined as the zone adjoining a new underground opening in which stress relief has occurred. The validity of this concept has been discussed extensively, and modified by other researchers. In this paper three types of in-situ rock are discussed: elastic, pseudo-plastic, and plastic rock. (1) In elastic rock
subject to low stressing, a relaxation zone cannot exist. If the stressing increases beyond the ultimate strength of this rock mass, fractures develop within this overstressed zone, resulting in stress redistribution and stress reductions near the opening. (2) In pseudo-plastic rock high rates of loading may result in similar conditions. Slow or even constant stressing results in local plastification, with subsequent stress reduction. This process continues within the rock mass until equilibrium is reached. (3) The conditions for plastic rock are principally similar to the pseudo-plastic case; however, they depend on the planar structure of the rock. References to international literature on this particular subject are given.

K. H. Höfer

Vol. 26, No. 1, 1960, pp. 2 - 13

4.28 On the Problem of the Frequency of Rock Bursts in Relation to Geophysical Factors (Zur Frage der Häufigkeit der Gebirgsschläge in Abhängigkeit von den physikalischen Grössen)

In many mines, the frequency of rock bursts varies with the seasons. In the deep ore mine of Pribran, Czechoslovakia, rock bursts were recorded over a 47-year period. Rock bursts occur most frequently in spring and fall seasons. Other researchers found similar concentrations in particular seasons. Certain relationships between occurrence and frequency of rock bursts and the velocity of the earth's rotation are found by means of the statistical comparison.

R. Kvapil

Vol. 26, No. 1, 1960, pp. 33 - 37

4.29 The Similarity Between the Icecap of the Jungfraujoch and the Large Ice Sheets of Greenland and the Antarctica (Ein Parallele zwischen der Eiskalotte Jungfraujoch und den grossen Eisschildern der Arktis und Antarktis)

Displacements and deformations within and at the surface of the 100-ft-thick icecap at the Jungfraujoch were measured over a ten-year period. Time rates and deformation profiles, deformation patterns within circular tunnels, the mechanics of spalling, and the state of stress within the ice sheet were studied and observed. The equation of flow of ice is presented, which might relate the present observations with the mechanics of the extensive ice sheets of Greenland and Antarctica. The steady motion of these ice sheets in equilibrium is considered to be a continuous creep due to gravity only. The equation of the surface of the ice sheet
is given. Field measurements correlate well with the analytical results. This is a comprehensive paper with detailed observation data and includes numerous references on the subject.

R. Haefeli
Vol. 26, No. 4, 1961, pp. 191 - 213

4.30 On the Analysis of Rock Mechanics Problems Associated with Forming of Magmatogenic Ore Deposits (Gebirgsmechanische Probleme bei der Bildung magmatogener Ganglagerstätten)

Rock mechanics problems can be analyzed by two principal methods. The first method begins with the forces applied and derives the mechanical effects within the region. The second method evaluates the phenomena observed in order to determine the forces causing them. The first approach necessitates simplifying assumptions on inhomogeneity and anisotropy of the natural materials, the knowledge of the factor time, and information on the history of the rock. The results of model tests suffer particularly from the often extremely simplified assumptions. The concept of deriving the cause from the results calls for the evaluation of a process from individual states, which might not even contribute to the process of interest. The latter approach gained considerable assistance from the analytical method for evaluating observations on the rock structure. Two examples of tectonic processes illustrate the second approach.

A. Watznauer
Vol. 26, No. 4, 1961, pp. 214 - 217


Rock mechanics analyses are impeded by inelasticity, anisotropy, and jointing of the average in-situ rock. Two diametrically opposite idealizing concepts are possible: (1) rock material is an inelastic continuum to be analyzed by methods of mechanics and thermodynamics, and (2) soil masses are discontinued, to be dealt with by stochastic methods. Rock mechanics is to interpolate between these two possibilities. The stress-strain relations within a solid in relation to time are described by its "equation of state". The idealized solids are replaced by mathematical models, of which the Nakamura solid well represents viscoelastic, stress-relaxing rock masses. The equation of state applies only for small deformations; however, conditions for plastic deformation and failure also can be derived. The
different states of a stressed solid and the modes of failure are given in relation to the principal stresses. The comprehensive paper includes mathematical derivations and references to other papers on the same subject, particularly in the Eastern hemisphere.

W. Buchheim Vol. 26, No. 4, 1961, pp. 218 - 233

4.32 On the Terminology of Geomechanics (Zur Terminologie der Geomechanik)

A precise terminology is more important in engineering geology and geotechnics than in general geology. It must be understood beyond any doubt by both geologists and engineers. Clear definitions are particularly necessary to clarify the complexes of structure (joints and faults) and failure of in-situ rock. The problem of different meanings of similar terms in different languages is far from solved.


4.33 Relaxation Phenomena in the Excavation of the Rappbode Dam (Entspannungserscheinungen in der Baugrube der Rappbodetalsperre Harz)

A comparison of permeability data of the Graywacke foundation rock of the Rappbode dam in East Germany, obtained prior and after excavation, indicated that the permeability of the in-situ rock increased with the removal of the surcharge. This effect was particularly strong at the center of the valley and negligible near the slopes. Thus, it cannot be attributed to loosening by blasting. It is believed that the expansion is due to stress relief. The process was found to be reversible. It is concluded that any remedial methods such as grouting should only be conducted after at least part of the structure is applied as surcharge and the upheave due to excavation is reversed.

F. Reuter Vol. 27, No. 2, 1961, pp. 73 - 76

4.34 Remarkable Stress Phenomena in the Bleiberg-Kreuth Mine (Bemerkenswerte Gebirgs-Spannungserscheinungen im Bergbau Bleiberg-Kreuth)

A series of rock bursts in highly mylonitized limestone in a 120-ft-deep shaft within a year's time resulted in stable
conditions in an Austrian lead mine. No bursts have been observed for the last seven years. In a part of another mine, which was being reworked, spalling from the roofs and walls of tunnels was observed. This spalling is believed due to overstressing caused by the reduction of pillar sizes and increased loads. Spalling occurred but without the common explosive effect of rock bursts and with only low velocity. Up to 60 spalls per day were observed within a zone with an approximate volume of one-million cubic yards. The phenomenon was not observed beyond this limited range. After installation of additional backfill material, rock spalling ceased and a new stable state of stress was obtained.

L. Kostelka
Vol. 27, No. 2, 1961, pp. 82 - 88

4.35 Determination of the Strength Anisotropy of a Rock Body, which is Intersected by Several Sets of Joints, by Means of Computer (Ermittlung der Festigkeitsanisotropie eines Gesteinskörpers, der von mehreren Kluftscharen durchzogen wird, mit elektronischem Rechengerät)

In order to analyze the strength characteristics of partially jointed in-situ rock, prototypes were assumed, based upon previous work by L. Müller and F. Pacher. The jointing of the rock material within the mass is assumed to be distributed statistically; it is based upon the findings of a rock mechanics survey. Three types of failures are investigated; tensile failure and shear failure through rock substance, and shear failure in the direction of a set of joints. The "resistance quotient" is defined as the ratio of strength over stressing; it varies with the direction considered. A computer was programmed to determine this ratio for the different modes of failure, based upon input data on geometry of the rock structure. The paper presents only abbreviated mathematical derivations without discussion of the results.

A. Hereth and A. Schombierski
Vol. 27, No. 3/4, 1962, pp. 126 - 128

4.36 On the Development of Joints Parallel to Surface, an Attempt of a Rock Mechanics Interpretation (Über die Entstehung Oberflächenparalleler Klüfte, Versuch einer geomechanischen Erklärung)

The observations of natural overstressing phenomena and those initiated by man, combined with stress measurements
near steeply sloping surfaces of rock banks, suggest a similarity between the stress conditions adjacent to a tunnel and those adjacent to a steep rock slope. The normal stresses generally are considerably higher than could be expected from the tangential stresses. Overstressing near the surface results in spalling of rock slabs parallel to the slope. The stress concentration recedes inward, repeating the spalling process. With increasing recession the stresses decrease and develop only potential fissuration in the rock mass. The importance of fissures parallel to the slope line for the design of arch dams is stressed.

L. Müller Vol. 27, No. 3/4, 1962, pp. 146 - 152

4.37 The Extent of Loosening of Rock Due to Blasting (Das Ausmass der Felsauflockerung bei Sprengarbeiten)

From the experiences of the excavation blasting for the weir of the Ybbs-Persenbeug hydropower plant at the Danube River, Austria, the following conclusions are derived: Blasting resulted in a 100% increase of the effective porosity. The loosening effect generally extended to a depth of 7 ft (2 m); along distinct fissures this value increased up to 17 ft (5 m). The increase in permeability is very significant. Consequently, design assumptions should be based on tests after excavation blasting. The amount of settlement depends directly on the loosening of the rock support, thus on the method of excavation. Data on grouting work and permeability tests illustrating the conclusions of the paper are presented.

F. Makovec Vol. 28, No. 1, 1962, pp. 58 - 62
5. TESTING AND TEST RESULTS

5.01 The Bursting Effect of Water in Compression Tests on Moist Materials (Die Sprengwirkung des Wassers beim Druckversuch an wasserhaltigen Feststoffen)

Wet concrete cubes subject to unidimensional compression, under exclusion of lateral restraint at loaded surfaces, generally fail by splitting into slabs parallel to compressive load. This splitting is a result of tensile overstressing normal to direction of compression, which is believed due to the development of pore water pressure. The splitting occurs normal to the direction of the outward flow of pore water. The same mechanics apply to the bursting of saturated material due to frost action.

L. Püppl Vol. 24, No. 1, 1958, pp. 52 - 55

5.02 Experimental Investigations of the Deformation Characteristics of Rock Masses (Experimentelle Untersuchungen über die Charakteristika der Verformbarkeit der Felsen)

Data on the deformability of in-situ rock masses and their characteristics, such as inelasticity and anisotropy, are important for the design of large dams. The deformation properties of in-situ rock can be influenced greatly by grouting. The deformability of in-situ rock can be determined by local plate-load tests and pressure-chamber tests. The results of dynamic in-situ tests are often considered doubtful. Deformability of in-situ rock generally is considerably greater than that of small specimens. In Italy the behavior of dams founded on inhomogeneous, anisotropic rock masses was investigated successfully in model tests in which the principal faults and differences in deformability of the rock foundation were represented. The results of deformation tests, both in-situ and in the laboratory, are given.

G. Oberti Vol. 25, No. 2/3, 1960, pp. 95 - 113

5.03 Apparatus for Determining the Deformability of In-situ Rock for Design of Pressure Tunnels and Their Linings (Ein Gerät zur Ermittlung der Felsnachgiebigkeit für die Bemessung von Druckstollen und Druckstollenauskleidungen)
Principal data on many pressure tunnels and shafts in Europe, completed, under construction, or in planning, illustrate the trend to higher pressures (up to over 1800 psi (130 kg/cm²)). It has become necessary to utilize more and more of the support of the adjoining rock masses. Different methods for determining the deformability of in-situ rock, with principal technical data, are described in tabulated form. The method for pressure chamber tests as developed by Tiroler Wasserkraftwerke AG is described in detail. This method utilizes a test chamber with an inside diameter of 7.3 ft (2.2 m) and a length of 6.7 ft (2.0 m). The pressure is applied by flat jacks supported by rings. Examples of stress-strain curves for phyllite before and after grouting are given. A graph for the design of tunnel linings with a 9.7-ft (2.90 m) inside diameter concludes the paper. Comprehensive references to European publications on the subject are given.

H. Lauffer  
Vol. 25, No. 2/3, 1960, pp. 114 - 129

5.04 The Strength of Preconsolidated Soils (Die Festigkeit vorbelasteter Böden)

The shear strength of highly consolidated and layered tertiary marl, to be utilized for support of a hydropower plant in West Germany, was determined by large-scale in-situ testing. In earlier investigations direct-shear tests, with shear planes on the order of 14 square feet (1.3 m²), were performed. More recent work included laboratory triaxial compression tests on samples 8 inches (20 cm) in diameter and 20 inches (50 cm) in height, and also in-situ double-shear tests on a circular block, 3 ft (90 cm) in diameter. The shear strength along bedding was determined to be c = 4.5 psi (0.32 kg/cm²); ϕ = 30°; in an oblique direction to the bedding the shear strength was determined to be c = 36 psi (2.55 kg/cm²); ϕ = 41°. Technical details of test arrangements and complete test results are given.

H. Breth  
Vol. 25, No. 2/3, 1960, pp. 177 - 185

5.05 Evaluation of Statical Deformation Measurements in In-situ Rock (Auswertung von statischen Felsdehnungsmessungen)

Pressure-chamber tests and plate-load tests, to different scales, provide data on the deformability of in-situ rock. The stress-strain relations for elastic and elastoplastic rock masses are discussed; the moduli of deformation and elasticity are differentiated. A graphical method for design of linings of underground openings in rock subject to internal pressure is given. This method does not require the assumption of Poisson's
ratio. The stress distribution within rock masses adjoining openings subject to internal pressure is given for idealized rock and jointed rock under overburden pressure. The relations between moduli of deformation and elasticity, the radii of and pressures within pressure chambers are given for both elastic and elastoplastic rock masses. It is concluded that pressure-chamber tests should be conducted by applying pressures equal to those expected in the prototype. The paper presents comprehensive data and numerous stress diagrams.

G. Seeber

5.06 On the Poisson's Number of In-situ Rock Masses (Über die Querdehnungszahl des Gebirges)

Poisson's ratios of many rock types as determined by static and dynamic laboratory tests are given. The values range from 0.04 to 0.5. It is believed that, besides the petrofabrics of the rock substance and its anisotropy, the porosity is of considerable influence on Poisson's ratio. Poisson's ratio is illustrated in one example. At least in surficial, highly jointed rock this influence should not be disregarded. Formulas for determination of the modulus of elasticity by means of different types of tests are given. One- and two-dimensional stress-relief tests after Tinzelin are discussed briefly. Comprehensive references to literature on the subject of elasticity of rock and rock masses are given. (Author uses Poisson's numbers.)

H. Link
Vol. 26, No. 4, 1961, pp. 246 - 257

5.07 Principal Considerations of Large-Scale Tests on Rock Masses (Grundsätzliches über gebirgstechnologische Grossversuche)

Rock mechanics principles are considered first. The difference between rock material, such as cores, and in-situ rock masses is stressed. The strengths of in-situ rock and its anisotropy depend primarily on the structure of the rock, and to a lesser extent on its substance. Since a test body has to include a statistically valid representation of the rock structure, rock tests are to be large-scale, and consequently in-situ tests. The stress distribution within layered material is inhomogeneous. Long duration tests and alternate load tests are important to provide valid results. The direction of testing has to be selected carefully, based upon statics and also rock mechanics considerations. The rock tests at the site of the Kurobe IV dam in Japan are briefly described.

L. Müller
Vol. 27, No. 1, 1961, pp. 1 - 8
5.08 Practice of Large-Scale Rock Tests (Die Praxis der Felsgrossversuche)

Practical experiences obtained from conducting a comprehensive program of large-scale rock tests at the site of the Kurobe IV arch dam in Japan are presented. Principal types of rock tests as performed are described and illustrated. The problem of their execution, such as excavation, rock mechanics, load and measuring devices, is discussed. It is concluded that although large-scale rock tests are expensive, their results are very important for rock mechanics and design of dams.

K. W. John
Vol. 27, No. 1, 1961, pp. 9 - 19

5.09 Instrumentation for Large-Scale Rock Tests (Instrumentation für Grossversuche in Fels)

Large-scale rock tests, covering the wide range from plate-load tests to observation of the deformations of dam abutments, necessitate loading devices, instruments, and control devices. Loads up to 4400 short tons (4000 t) are applied by means of piston jacks or flat jacks. Piston or rotational pumps provide pressures up to 7000 psi (500 kg/cm²), which is to accomplish high compressive stressing in test blocks. Displacements are preferably measured by inductive gages because they have larger measuring ranges than resistance methods. Different arrangements for measuring shear deformations in bore holes have been devised, based upon inductive- and resistance-measuring methods. Measurements are recorded automatically either continuously or in point-mode. For automatic and semi-automatic pressure regulating devices, standard components are combined to serve the particular needs.

H. Steinbichler
Vol. 27, No. 1, 1961, pp. 20 - 28

5.10 On the Evaluation of Large-Scale Rock Tests (Zur Auswertung von Grossversuchen)

The purpose of large-scale rock tests is to determine strength and deformability of in-situ rock for the stress conditions to be expected in a particular case. A combined approach by means of large-scale in-situ tests, model tests, photoelastic tests, and theoretical analysis is used to determine the technical properties of in-situ rock. The state of stress and the anisotropy of the rock structure are important. The permissible stressing of a foundation rock is still to be defined; in most
cases it depends much more on the allowable deformation than on the ultimate strength of the rock.

F. Pacher
Vol. 27, No. 1, 1961, pp. 29 - 32

5.11 Stresses in the Earth's Crust as Determined by Hydraulic Fracturing Data

The knowledge of residual stress in rock masses is of great significance for engineering and geological purposes. The stresses adjacent to an oil well can be determined by means of hydraulic fracturing. It is assumed that fracturing of the material surrounding the well occurs through tensile failure under increased hydraulic pressure within the well. The pressure at which failure occurs depends on the residual stresses within the rock. The data from five wells are evaluated. Differences between principal stresses on the order of up to 2000 psi (140 kg/cm²), which agree with the conditions as derived from seismic investigations, were determined. Equations are derived and limiting assumptions are stated. (Engl.)

A. E. Scheidegger
Vol. 27, No. 2, 1961, pp. 45 - 53

5.12 On Poisson's Ratios of Rock and In-situ Rock Masses (Zur Querdehnungszahl von Gestein und Gebirge)

Poisson's ratio of rock material as determined by static tests and by dynamic methods are compared. A considerable discrepancy is observed between the results of the different types of tests. Dynamic tests result in values of 0.25 to 0.33, with siliceous and porous materials as low as 0.10. Static tests often result in values less than 0.1, frequently as low as 0.04. A relationship between Poisson's ratio and confining pressure has been proved. The influence of loosening, jointing, and porosity is definitely confirmed. In-situ tests are discussed only briefly; Poisson's ratio on the order of 0.03 to 0.1 might be used for most in-situ rocks. Comprehensive data presented in the paper were obtained from international sources, particularly from the U.S. Bureau of Mines and the U.S. Bureau of Reclamation. (Paper gives Poisson's numbers instead of Poisson's ratios.)

H. Link
Vol. 27, No. 2, 1961, pp. 89 - 100
5.13 A Large-Scale In-situ Shear Test on Undisturbed Phyllite Rock

(Ein Grosscherversuch in Phyllitgestein bei ungestörter Lagerung der Probekörper)

The support of Pier I of the "Europe-Bridge" of the Brenner-Highway in Austria was to be supported on highly jointed quartz-phyllite. Several plate-load tests were performed in exploration tunnels and shafts. Soil mechanics tests were conducted on samples of the mylonitic joint fillers. The shear strengths along horizontal joint planes of the phyllite were determined by shear tests on rock blocks 3.3 ft by 3.3 ft (1 x 1 m) in plan. The technical details of the test arrangements are described and illustrated. A sample of the stress-strain curves determined is given. A cohesion of 14 psi (1 kg/cm²) and angles of internal friction of 20° to 37° were found for the joint planes.

J. Malina

Vol. 27, No. 3/4, 1962, pp. 120 - 125


The knowledge of the moduli of deformation and elasticity is essential for any design problem involving in-situ rock. Static determinations are expensive and time consuming, and result in extrapolations that may be doubtful. Dynamic methods allow determination of the data on elasticity of small samples such as drill cores. For rock, the dynamically determined values (usually) are higher than values determined by static methods. This is believed due to the different time rates of stressing. Seismic methods rapidly and cheaply provide average values on the modulus of elasticity over large areas; however, they do not give deformation moduli. Generally, seismically determined moduli of elasticity are three to twelve times higher than those determined by means of static pressure chamber tests. The paper presents comprehensive comparative data based on international sources, particularly the U.S. Bureau of Mines and the U.S. Bureau of Reclamation. It also gives reference to international publications. (Paper gives Poisson's numbers instead of Poisson's ratios.)

H. Link

Vol. 27, No. 3/4, 1962, pp. 131 - 145
5.15 Large-Scale Field Shear Box Tests on Quick Clay

In an investigation of a major landslide in Norway, the shear strength of quick clay in a drained condition was determined by means of in-situ shear tests. The clay layer, in which the slide took place, was exposed in the rear portion of the slide; it measured less than four inches in thickness. The technical details of two in-situ shear tests on 20 inch x 20 inch (50 x 50 cm) blocks and laboratory tests on 8 inch x 8 inch (20 x 20 cm) blocks are presented. Complete stress-strain curves are included. The angle of drained shear resistance was less than $9^\circ$. The theoretical implications of this type of test were discussed by L. Bjerrum, *Fifth International Conference on Soil Mechanics and Foundation Engineering, Paris, Proceedings*, Vol. 1, pp. 23 - 28. The paper gives valuable practical hints for performance of large-scale in-situ shear tests. (Engl.)

J. N. Hutchinson and E. N. Rolfsen

Vol. 28, No. 1, 1962, pp. 31 - 42
6.01 Engineering Geological Annotations on the Underground Excavations in Austria During the Last Years (Baugeologische Randbemerkungen zu den Hohlraumbauten der letzten Jahre in Österreich)

J. Stini Vol. 16, No. 1, 1946, pp. 1 - 45

6.02 The Influence of Surficial Impacts on Shallow Underground Excavations in Granular Rock Masses (Der Einfluss obertägiger Erschütterungen auf oberflächennahe Hohlräume in rolligem Gebirge)

L. Hauser Vol. 16, No. 3/4, 1948, pp. 86 - 91

6.03 The Upheave of the Floor During Construction of the New Semmering Tunnel (Die Sohlenhebungen beim Bau des neuen Semmeringtunnels)

W. J. Schmidt Vol. 20, No. 1, 1953, pp. 13 - 18

6.04 Geological Considerations on the Experiences Gained During Construction of the New Semmering Tunnel (Geologische Gedanken zu den Bauерfahrungen beim neuen Semmeringtunnel)

F. Kahler Vol. 20, No. 3, 1953, pp. 129 - 132

6.05 Had the Construction of the Tunnel through the Karawanken Range to be that Difficult? (Musste der Bau des Karawankentunnels so schwierig sein?)

F. Kahler Vol. 20, No. 3, 1953, pp. 198 - 211

6.06 Extensive Zones of Mylonite Impede Driving of the Förolach Erbstollens Tunnel (Lake Presseg, Gail Valley) (Breite Mylonitzonen als Vortriebshindernis am Beispiel des Förolacher Erbstollens (Pressegger See, Gailtal)

F. Kahler Vol. 21, No. 3, 1955, pp. 115 - 120
6.07 The Stressing of the Linings of Penstock Shafts in Anisotropic Rock Masses (Die Beanspruchung von Druckschachtpanzerungen im anisotropen Gebirge)

E. Tremmel

Vol. 23, No. 2, 1957, pp. 66 - 78

6.08 Seismic Vibrations in Rock Masses Adjoining Underground Powerhouse (Schwingungen im Untergrund eines Kavernenkrafthauses während eines Erdbebens)

Japan's first underground powerhouse was constructed in central Japan from 1952 to 1955. Its dimensions are 117 ft by 57 ft (35 x 17 m) in plan and 103 ft (31 m) high; the overburden depth ranges from 127 to 286 ft (38 - 86 m). It is located in coarse-grained granite. Previous observations indicate that the seismic intensities in tunnels are approximately half of those at the surface as long as the periods are less than one second. Periods on the order of four seconds resulted in equal intensities both at the surface and underground. Little damage due to earthquakes is generally observed in tunnels. Since the cavern was designed with a seismic acceleration factor of 0.12, a complete lining reinforced by rock bolts was believed necessary. After completion of the structure, an earthquake occurred which had an epicenter approximately 112 miles (180 km) from the site. The seismograms confirmed the intensities underground to be approximately one-half of those at the surface.

S. Okamoto and T. Mizukoshi

Vol. 24, No. 2, 1958, pp. 113 - 117

6.09 Overbreak in Tunnels and Drifts (Der Mehrausbruch in Tunneln und Stollen)

In most construction jobs in rock, overbreak cannot be avoided completely; however, it can be reduced to a certain extent. Terminology and geometrical relations used in tunnel engineering are discussed in some detail. Unavoidable geological overbreak and avoidable overbreak are differentiated. The geological factors resulting in overbreak are reviewed, and the influence of the rock structure and the state of stress in the rock mass is emphasized. Technical factors, such as direction of tunnel, cross section, vibrations during construction, techniques of drilling and blasting, and temporary support, are discussed. Overbreak volumes can approximately be predicted based upon data on the rock structure. Recommendations on how to prepare definite specifications for
construction of tunnels are given. Comprehensive paper based upon European conditions—of considerable practical value.

L. Müller
Vol. 24, No. 3/4, 1959, pp. 204 - 222

6.10 Gastein and the Inrush of Warm Water into the Pressure Tunnel of Lend (Gastein und der Warmwassereinbruch in den Lender Druckstollen)

The construction of a pressure tunnel penetrating limestone, located approximately 12 miles (20 km) from the thermal springs of Badgastein, Austria, was not supposed to affect the latter. The inrush of 160 GPS (620 l/sec) into the tunnel during construction came as a surprise, and became the subject of a comprehensive investigation. Geological explorations of continuous fault zones and joints, and hydrogeological and chemical studies proved that the warm water flowing into the tunnel actually originated from the same source as the thermal springs of Badgastein. Water seepage from the pressure tunnel into the adjoining rock might have a long-range effect on the thermal springs. The positive seal of the lining of the pressure tunnel in the zone of influx during construction was deemed advisable.

J. Stini
Vol. 24, No. 3/4, 1959, pp. 258 - 265

6.11 Survey of Tunnel Sections by Means of Intersecting Light Beams (Lichtschnitt-Profilmessung in Stollen)

A simple apparatus for efficient and accurate surveying of tunnel sections was developed in Austria. A projector produces a disc of light which intersects the wall of the underground opening. The resulting illuminated band representing a section is photographed, corrected for perspective, and brought to the desired scale. The final tracing is reproduced on translucent paper. The very precise results can be utilized for differentiation between geological and avoidable overbreak in construction of tunnels.

F. Koppenwallner
Vol. 25, No. 1, 1959, pp. 50 - 58

unvollkommenen Zu Spannungsübertragung im zerklüfteten Gebirge auf die Beanspruchung von Druckschachtpanzerungen)

A modification of existing methods for the design of pressure tunnels and their linings which considers the anisotropy of the deformability of in-situ rock due to its structure is proposed. The modulus of elasticity in the direction of the maximum principal stresses is assumed to be reduced in order to allow the application of the theory of elasticity. This paper presents complete formulae which allow immediate application.

E. Tremmel Vol. 25, No. 2/3, 1960, pp. 228 - 232

6.13 An Unsuccessful Tunnel Heading (Ein gescheiterter Stollenvortrieb)

A detailed diary of an unsuccessful Austrian tunnel project covering the period from 1924 to 1942 is given. A medium-sized tunnel was planned to penetrate a massif consisting of Triassic limestone with considerable Tertiary overburden. Several attempts did not succeed in penetrating a complex fault zone because of adverse water conditions which resulted in temporary water influx of up to 53 GPS (200 l/sec). Safety precautions prevented serious accidents. It is concluded that the tunnel could have been completed if comprehensive drainage measures had been taken.

F. Kahler Vol. 25, No. 4, 1960, pp. 243 - 247

6.14 The Relation of the Geologist to New Methods of Tunnel Support (Die Stellung des Geologen zu den neuen Methoden der Stollensicherung)

Increased construction speed, new methods of support, and new equipment have resulted in new approaches to geological field work. Many conventional methods of tunnel construction have become outdated, and new methods with large tunnel sections and large-scale blasting have been successfully introduced. Gunite linings, with and without reinforcement, and rock bolting, often combined with protective chain-link mesh, serve as highly efficient temporary support. From a geological point of view it is desirable to minimize the time period between initial excavation and installation of the final lining. This paper essentially contains general discussions.

F. Kahler Vol. 26, No. 1, 1960, pp. 14 - 17
6.15 The Breaking of the Conduit Tunnel Caused by the Development of the Gypsum Mine

A pressure tunnel of a hydropower plant penetrating tuffaceous sandstone and shale was severely damaged by cracking of the concrete lining and settlements in the invert grade. A gypsum mine is located approximately 200 ft (60 m) below and 330 ft (100 m) in a horizontal direction from the tunnel. Initial investigations did not detect surface subsidence. Subsequent surveys, however, which were carried out over a one-year period, did show subsidence of the surface. The subsidence problem was analyzed utilizing the method by Bals (Germany) in which the amount of subsidence is expressed in terms of the height of the mine works. Coefficients of subsidence, of duration, and of extent are used. The results of the analyses correlated well with the measurements both in the tunnel and at the surface. Paper presents detailed observation data. (Engl.)

H. Tanaka and A. Kitano
Vol. 26, No. 1, 1960, pp. 18 - 32

6.16 Excavation of Highway Tunnels in Particularly Difficult Rock Types (Ausbruch von Autobahntunneln in ganz besonders schwierigen Bergarten)

Along the route of the Autostrada del Sole in Italy, two highway tunnels were constructed in an old landslide area. Layered material consisting of plastic clays and sandstone was penetrated. To reduce the cross section of the tunnel, twin tunnels, each 33 ft (10 m) in inside diameter, were constructed. All tunnels were completely lined by concrete approximately three-ft (90 cm) thick. Initially, the multiple-drift (Austrian) method of tunnel construction was employed. For the second of the twin tunnels, the heading-bench method was used. In the latter method, temporary support was obtained by a layer of gunite applied immediately after excavation. A second layer was applied after steel ribs and chain-link wire were installed. The total thickness of the gunite liner ranged from 8 to 12 inches (20 - 30 cm). The latter method resulted in a 25% reduction of the thickness of the final lining.

A. Zanon
6.17 The Fractured Zone of the Kurobe Transportation Tunnel

The 2.8-mile-long (4.5 km) access tunnel to the site of the Kurobe IV dam in Japan was constructed under considerable difficulties. The tunnel penetrates fine- to coarse-grained blocky biotite granite. After one mile, a fractured and saturated fault zone was encountered, resulting in severe deformation of timbering and influx of water (175 GPS, 660 l/sec). This zone, approximately 267 ft (80 m) wide, was penetrated only after four drainage tunnels were constructed parallel to the main tunnel. In addition, numerous drainage borings were drilled in order to dewater the rock masses adjoining the tunnels. Chemical grouting (Hydrock) was used extensively for stabilization of the finely fractured rock of the fault zone and for reduction of the water seepage. The paper presents a detailed account of the construction work. (Engl.)

K. Haga
Vol. 26, No. 2, 1961, pp. 60 - 78

6.18 Application of Microseismic Methods in Construction of Tunnels
(Application de la microsismique a la construction de galleries)

Microseismic tests in tunnels and other underground excavations, before or after the lining is installed, provide information on the properties of in-situ rock adjoining the openings. The zone in which the stressing has been relieved because of over-stressing and subsequent fracturing can be determined by continuous measurements of the dynamic modulus of elasticity and Poisson's ratio. The results also assist in defining homogeneous zones adjoining the opening, which is important for extending the results of other rock tests. The method substitutes technological measurements for empirical estimates. The method described here has been applied at 187 underground structures since 1955. (French)

M. F. Bollo
Vol. 26, No. 2, 1961, pp. 79 - 86

6.19 The Northern Portal of the Klammstein-Tunnel (Das Nordportal des Klammstein-Tunnels)

The northern portal of the Klammstein-Tunnel near Badgastein, Austria, was designed so that its statical function is expressed in its form. The portal partially cantilevers beyond an almost vertical rock face into loose river deposits. Part of the portal is founded directly on bedrock, and the outermost portion is supported by a concrete pedestal extending to bedrock. The entire portal was to support heavily jointed rock masses above. The horizontal thrust due to lateral
rock pressure is countered by horizontal, prestressed rock anchors. The architectural design resembles that of a shallow shell, arranged in an oblique angle to the axis of the highway and resting against the face of the rock massif.

L. Müller
F. Pacher
Vol. 26, No. 2, 1961, pp. 87 - 92

6.20 From the Practice of Tunnel Engineering, Some Experiences on True Rock Pressure (Aus der Praxis des Tunnelbaues, einige Erfahrungen über echten Gebirgsdruck)

In North Iran, the lining of a one-track railroad tunnel, which penetrated expansive phyllite, failed one and one-half years after completion. The tunnel had been completed only after considerable difficulties; construction was by the Belgium method. Considerable lateral deformations were experienced during construction. The concrete lining in the high pressure zone ranged from three to four feet (approximately 1 m) in thickness. Over a length of 667 ft (200 m), the lining roof was sheared off at the 11:00 o'clock and 1:00 o'clock points of the perimeter (12:00 o'clock would be the center of the roof arch). The failure occurred where the axis of the curved tunnel was about parallel to the vertical lamination of the rock. The mechanics of the shear failure and the resulting stresses are reconstructed. The destruction of a protective tunnel in clay by aerial bombing and the failure of a test adit in shale also are examined. An example is given of the difficulties of securing of gunite linings by rock bolting in soft, unstable rock.

L. Von Rabcewicz
Vol. 27, No. 3/4, 1962, pp. 153 - 167
DAMS AND ROCK ABUTMENTS

7.01 Some Considerations on Modern Dam Construction in Smaller Countries (Einige Gedanken über den neuzeitlichen Talsperrenbau in kleineren Staaten)
J. Stini
Vol. 17, No. 4, 1950, pp. 143 - 151

7.02 Statics and Dam Geology (Statik und Talsperrengeologie)
J. Stini
Vol. 20, No. 2, 1953, pp. 88 - 110

7.03 Faults and Dam Construction (Verwerfungen und Talsperrenbau)
J. Stini
Vol. 20, No. 3, 1953, pp. 152 - 166

7.04 The Securing of Dam Foundations (Die Baugrundsicherung von Stauanlagen (Talsperren))
K. Keil

7.05 Faults and Dam Construction (Verwerfungen und Talsperrenbau)
J. Stini
Vol. 23, No. 1, 1957, pp. 51 - 54

7.06 Influence of Large Differences in the Moduli of Elasticity of Concrete and Rock on Design of Arch Dams (Einfluss grosser Elastizitätsunterschiede zwischen Beton und Fels auf die Berechnung einer Sperre)
O. Zerlauth
Vol. 23, No. 2, 1957, pp. 103 - 111

7.07 Some Practical Considerations of Foundation Problems of Arch Dams (Einige praktische Überlegungen zum Problem der Gründung von Staumauern)

Dams and their foundations are believed to be an inseparable static unit. The design should attempt to minimize tensile stresses of the rock abutments. Rock anchoring should be used only as a last resort. Very narrow valley sections are apt
to be unfavorable dam sites. Their rock flanks are often subject to tension normal to slopes, resulting in jointing parallel to slope lines. Any dams, and particularly arch dams, can be designed to resist major earthquakes. The advantages of arch dams over gravity dams are emphasized, because of the higher strength and load-carrying capacity of the former. Discontinuities within dams, their bases, and their foundations should be avoided. Such singularities might cause stress peaks and oversteering. Irregularities of the morphology of the valley section and of the deformability of the foundation rock essentially can be cancelled by the system of circumferential joints and foundation pads (Italian pulvino). A pulvino also reduces the undesirable restraint of the dam by the rock foundation. It reduces the problems due to deformations caused by temperature changes. Local geological discontinuities such as joints and faults should be reinforced by doweling and anchoring. A brief review of problems related to design of earth and rock fill dams concludes the paper. Comprehensive treatise by one of Europe's outstanding designers of water-retaining structures.

C. Semenza Vol. 24, No. 2, 1958, pp. 61 - 81

7.08 Examples on the Influence of the Anisotropy of In-situ Rock on the Foundations of Arch Dams (Beispiele für den Einfluss der Gebirgs-Anisotropie auf Talsperrengründungen)

Most in-situ rock masses represent discontinuous materials with inherent anisotropies of their vectorial properties and inhomogeneities of their scalar properties. Several examples are given to illustrate the effect of anisotropies in the rock abutments on the support of large arch dams. The structure of the rock mass and its orientation in respect to the dam thrust govern deformability, stress distribution, and the ultimate strength of a rock abutment. Photoelastic studies were used to investigate problems related to stress distribution in jointed rock; however, large-scale in-situ tests are necessary to determine the mechanical properties of jointed rock masses.

L. Müller Vol. 24, No. 2, 1958, pp. 82 - 94

7.09 Brief Considerations on Rupture of Arch Dam Abutment

A series of two-dimensional model tests was performed on horizontal sections through the dam and rock abutments for the design of the Kurobe IV arch dam in Japan. The stress distribution, based upon assumed elastic behavior, was investigated for homogeneous and for jointed rock abutments.
The condition of failure was investigated for homogeneous weak rock and firm rock with jointing (1) parallel to the direction of thrust and (2) parallel and normal to this direction. For homogeneous abutments the theory of elasticity appears to be applicable. The quantitative evaluation of the tests on homogeneous abutments is difficult. The simulated anisotropies of the jointed rock abutments greatly affected the failure patterns. Failure patterns and deformations observed in this test series are presented. (Engl.)

M. Takano
Vol. 25, No. 2/3, 1960, pp. 130 - 141

7.10 Rupture Studies on Arch Dam Foundation by Means of Models

Three-dimensional model tests were carried out for the design of the Kurobe IV dam in Japan. They served to investigate the influence of the structure of the rock abutment on the stability of the arch dam. The model scale was 1 : 500. The highly jointed abutment rock was represented by several alternate model structures. Homogeneous rock was represented by a compacted mixture of sand and soluble glass. Jointed rock was represented by cubes of plaster separated by clay seams. Only hydrostatic loading was applied. The dam supported on homogeneous material failed by shear through the rock adjacent to the dam. The rupture commenced in the lower third of the contact. The abutment consisting of jointed material failed along joints parallel to the dam thrust. The failure was preceded by considerable deformation in the rock mass. In subsequent tests, the orientation of the joint system was modified in order to determine the orientation of least resistance. The comprehensive paper includes numerous illustrations. (Engl.)

M. Takano
Vol. 26, No. 3, 1961, pp. 99 - 121

7.11 Observation and Surveys on the Abutments of the Vaiont Dam

The Vaiont arch dam, 875 ft (262 m) high, is situated in a very narrow valley in the North Italian mountains. The abutment rock is composed of limestone which is jointed both parallel and normal to the slope surface. Rock tests were performed both in the laboratory and in-situ. The latter comprised seismic and static tests. Stress relief measurements, plate-load tests, pressure-chamber tests, and rock-shear tests were performed to determine the technological properties of the in-situ rock. The effect of excavation blasting was observed during construction. The efficiency of grouting operations was controlled by seismic surveys of the zones being grouted. The movements due to stress redistribution during excavation were observed by seismographs. In order to observe the
deformations of the rock abutments during filling of the reservoir, a comprehensive system of stress and deformation meters were installed. The latter consists of a combination of pendulums and extensometers. A geodetic net was instituted to coordinate all measurements. Piezometers are installed to control the efficiency of grout curtain and drainages. (Engl.)

M. Pancini


7.12 The Stress Distribution in the Rock Foundation of Concrete Dams
(Das Kräftespiel im Untergrund von Talsperren)

The increased size of dams and the necessity to utilize sites rejected earlier necessitates the improvement of knowledge on stress-strain relations in rock foundations. Of all exterior forces, the buoyancy and the thrust of the water contained in the joints are the most difficult to evaluate. A concept for this evaluation is given. The stress distribution in the rock abutment depends on the rock mass being utilized for support. Increasing rock volume results in steeper thrust lines which increase the stability of the abutment. Conversely, the buoyancy acting in the supporting rock mass raises the line of thrust. The stability of abutments consisting of jointed rock depends on both stress pattern resulting from overburden weight and on the dam thrust and its relative orientation to the structure of the rock mass. Stability analysis of rock abutments should be based on large-scale rock tests. It is concluded that at the present time the rock abutment represents the weakest part of most arch dams, with resulting true factors of safety of not much more than 1.5.

L. Müller

Vol. 26, No. 3, 1961, pp. 142 - 151

7.13 Results of the First Series of Tests Performed on a Model Reproducing the Actual Structure of the Abutment Rock of the Vaiont Dam

A comprehensive model test series for the final design of the Vaiont Dam was performed by I.S.M.E.S. in Bergamo, Italy. The Vaiont Dam is of the plunging arch type, 875 ft (262 m) high and 600 ft (180 m) wide at crest elevation. The dam is located in Northern Italy. The tests were performed on a 1 : 85 scale model of the dam supported on abutments which reproduced the structure of the actual in-situ rock. The model technique is described in detail and is well illustrated. The tests were performed successfully; however, the interpretation of the results proved rather difficult. The rock

abutments deformed somewhat, particularly in the middle third of the dam height, but supported the dam satisfactorily, even under a water head increased by 133 ft (40 m) above the maximum reservoir level. (Engl.)

M. Pancini

Vol. 27, No. 3/4, 1962, pp. 105 - 119
8. SLOPES AND LANDSLIDES

8.01 Landslides in the Region of Ernstbrunn-Dörfels, Lower Austria (Erdrutschungen im Gebiete von Ernstbrunn-Dörfels, Niederösterreich)
F. Bachmayer Vol. 17, No. 1, 1949, pp. 4 - 6

8.02 Newer Views on Ground Movements and their Control by the Engineer (Neuere Ansichten über "Bodenbewegungen" und ihre Beherrschung durch den Ingenieur)
J. Stini Vol. 19, No. 1, 1952, pp. 31 - 54

8.03 New Facts and New Knowledge on the Rock Fall Region of Köfels (Neuer Sachbestand und neue Erkenntnisse über das Bergsturzgebiet von Köfels)

8.04 Downhill Dipping Beds and Dam Construction (Talauswärtsfallende Schichten und Talsperrenbau)
J. Stini Vol. 19, No. 4, 1952, pp. 254 - 257

8.05 Directions for Methodic and Economic Restoration Following Landslides (Richtlinien für eine zielgerechte und rationelle Sanierung von Rutschungen)
S. L. Rintel Vol. 20, No. 2, 1953, pp. 81 - 87

8.06 Formation of Ice in a Talus Slope (Über Eisbildung in einer Schutthalde)
G. Mutschlechner Vol. 20, No. 2, 1953, pp. 110 - 114
8.07 Expansion and Fracturing of Rock Masses and Landslides, Described in an Example from the Engineering Geological Practice (Bergzerreissung und Hangrutsche an einem Beispiel aus der baugeologischen Praxis)

H. Ascher and G. Horninger
Vol. 20, No. 2, 1953, pp. 112 - 119

8.08 Observations of Soil Movements During Improvement of the Wechsel-Highway in Eastern Styria (Beobachtungen an Bodenbewegungen anlässlich des Ausbaues der Wechsel-Bundesstrasse in der Oststeiermark)

W. Brandl
Vol. 22, No. 1, 1956, pp. 54 - 60

8.09 Hydraulic Fracturing and High-Pressure Water (on slope failures due to hydrostatic pressure) (Wassersprengung und Sprengwasser)

J. Stini and H. Petzny
Vol. 22, No. 2, 1956, pp. 141 - 169

8.10 Rock Slides at Sites of Hydropower Plants (Felsgrundbrüche im Baugelände von Wasserkraftanlagen)

J. Stini
Vol. 22, No. 3, 1956, pp. 224 - 245

8.11 The Securing of a Dam Excavation Having Slip Planes Dipping Downhill (Die Sicherung des Talsperrenaushubes mit talwärts fallenden Gleitschichten)

L. Müller and F. Pacher
Vol. 23, No. 2, 1957, pp. 82 - 98

8.12 Classification of Landslides (Klassifikation der Rutschungen)

B. Backofen
Vol. 23, No. 3, 1957, pp. 125 - 130

8.13 The Landslide at the Athletic Field of Weissenkirchen (Die Rutschung am Sportplatz bei Weissenkirchen)

H. Schwenk
Vol. 23, No. 4, 1958, pp. 169 - 175
On the Creep Phenomena on Rock Slopes and Their Indications
(Einiges über Talzuschübe und deren Vorzeichnung)

Three case histories of land creeps in natural rock slopes observed in Austria are presented: (1) A large gneiss massif creeps in the direction of its steeply dipping foliation. The traces of the creep can be clearly observed where the highly fractured slip zone was penetrated by a railroad tunnel. From a technical point of view the creeping rock massif can be considered stable since the creep occurs over a long period of time. (2) During construction of a second tunnel in a sloping region composed of phyllitic rocks, a high inflow of water was observed at a highly mylonitized fault zone also exposed at the surface. This increase in permeability is explained by the renewed movements along the fault and the resulting loosening due to tilting of rock laminae towards the valley. (3) A prominent rock massif considered for support of an arch dam was found to be separated from the adjoining rock masses by two distinct joints, partially filled with broken rock; however, no indications of present movement were found. It is concluded that engineers have to accept as stable what geologists might consider to be in a state of geological creep. The evaluation of the influence of time should depend on the length of the time period being considered.


The Use of Heavy Equipment on Steep Slopes Might be Dangerous
(Gefahren des Maschineneinsatzes in steilen Halden)

The difficulties encountered in using heavy earth-moving equipment at rather small but difficult construction jobs related to rock slopes are briefly discussed. Conditions of both safety and economy are to be met. This paper refers only to typical European construction methods in alpine countries.

F. Kahler Vol. 25, No. 1, 1959, pp. 64 - 67

Decompressed and Altered Zones in Steep and High Slopes (Zones Décomprimées et Alterées des Versants à Forte Pente)

The effects of erosion and gravity forces on steep slopes and the possibilities of seismic and statical methods of investigation are discussed. For a sloping region two principal limits are given: (1) the boundary of the zone of recognizable superficial alteration and fracturing, and (2) the generally more shallow zone of decompression or relaxation.
In addition, zones of displaced materials, with both disturbed and undisturbed rock structure, are differentiated from the overall, stable rock mass. Microseismic refraction measurements allow determination of the boundary between sound, stressed rock masses, and altered, relaxed rock masses. The extent of the different types of displaced materials also can be determined by dynamic investigations. (French)

M. F. Bollo
Vol. 26, No. 4, 1961, pp. 234 - 245

8.17 Classification of Landslide Fissures (Klassifizierung der Erdrutschrisse)

Classification and mapping of fissures developed during landslides provide valuable assistance in analyzing the mechanics of the slides. A classification of the fissures based on the type of stressing which caused the deformations is proposed. Both superficial and deep fissures are considered. The direction of the vector of total deformation in respect to the orientation of the fissure surface is the principal criterion used for this classification. The geomorphology of different types of superficial landslide fissures is discussed in detail. A graphical system for mapping landslide fissures also is proposed. Illustrative diagrams and a table for morphogenetic classification are given.

G. Ter-Stepanian
Vol. 28, No. 1, 1962, pp. 43 - 54
ROCK BOLTING AND ROCK ANCHORS

9.01 Annotations on Analysis and Construction of Steel Anchors in Rock (Einige Bemerkungen zur Berechnung und Ausführung von Stahlverankerungen im Fels)
S. Soretz Vol. 21, No. 4, 1955, pp. 162 - 168

9.02 Trial Operations with Rock Bolt Support in Soft Coal Deep Mining (Betriebsversuche mit Ankerausbau im Braunkohlentiefbau)
O. Fabricius Vol. 23, No. 1, 1957, pp. 20 - 40

9.03 On the Analysis of Rock Anchorings, Anchored Retaining Walls, and Revetment Walls (Über die Berechnung von Felssicherungen, verankerten Stützmauern und Futtermauern)
F. Pacher Vol. 23, No. 1, 1957, pp. 41 - 50

9.04 An Example of a Rock Bolting Job (Beispiel einer Felsnagelung)
At a gravity dam being built in Austria, in order to minimize the amount of excavation at one rock abutment without impairing construction safety, rock bolting was employed. Perfo-rock bolts 7/8 inch (22 mm) in diameter and 8 ft (2.5 m) long were installed in the rock mass above the crest of the dam being constructed. This anchorage was to secure a rock region separated from the abutment massif by distinct open joints striking parallel to the valley and dipping about 45 degrees. The installation proved to be more economical than an increase in the excavation volume. Anchoring was not utilized for final support. Technical details are given.
E. Neuhauser Vol. 25, No. 1, 1959, pp. 59 - 63
10. \textbf{SOIL MECHANICS}

10.01 The Liquid Strength of Clays (Die Zürlfließfestigkeit von Tonen)
\hspace{1cm} E. Winkler \hspace{1cm} Vol. 16, No. 3/4, 1948, pp. 162 - 172

10.02 On Impermeable Cores in Soil Masses, in Damming of Valleys, and their Significance for Construction of Dams (Über dichte Kerne in Lockermassen, als Talabschlüsse, und ihre Bedeutung für den Bau von Stauwerken)
\hspace{1cm} C. Veder \hspace{1cm} Vol. 17, No. 1, 1949, pp. 1 - 3

10.03 Do Surveys of Joints in Soil Masses Make Sense? (Haben Kluftmessungen in Lockermassen Sinn?)
\hspace{1cm} J. Stini \hspace{1cm} Vol. 18, No. 1, 1950, pp. 47 - 51

10.04 Information on the Analytical Determination of the Energy Necessary for Artificial Compaction of Soils in Cylindrical Molds (Mitteilungen über die rechnerische Ermittlung der Energiemenge für die künstliche Bodenverfestigung im zylindrischen Areal)
\hspace{1cm} E. E. Hensolt \hspace{1cm} Vol. 18, No. 3, 1951, pp. 143 - 173

10.05 A New Method to Determine the Pore Volume (Eine neue Methode zur Bestimmung des Porenvolumens)
\hspace{1cm} H. Häusler \hspace{1cm} Vol. 18, No. 3, 1951, pp. 174 - 176

10.06 On the Survey of Structures in Soil Masses (Über Gefügemessungen in Lockergesteinen)
\hspace{1cm} H. Ascher \hspace{1cm} Vol. 19, No. 2, 1952, pp. 69 - 76

10.07 Proof of Stress Distribution in Soil Masses (Nachweis der Spannungsverteilung in Lockermassen)
\hspace{1cm} L. Müller \hspace{1cm} Vol. 19, No. 4, 1952, pp. 245 - 253
10.08 Annotations on Engineering Geological Investigations of Quick Sand Strata (Einiges aus baugeologischen Untersuchungen von Schwimmsandschichten)
E. Schröder
Vol. 20, No. 3, 1953, pp. 133 - 135

10.09 The Allowable Loading and the Allowable Stressing of Foundation Soils (Die zulässige Belastung und die zulässige Beanspruchung des Baugrundes)
K. Keil
Vol. 20, No. 3, 1953, pp. 191 - 197

10.10 Annotations on Damages Due to Frost and Thawing on the Roads of the Hartberg District in Winter 1953/54 (Bemerkungen zu den Frost- und Tauschäden der Strassen des Bezirkes Hartberg im Winter 1953/54)
W. Brandl
Vol. 21, No. 1/2, 1954, pp. 44 - 47

10.11 Prevention and Repair of Frost Damage in Road Construction (Verhütung und Beseitigung von Frostschäden beim Strassenbau)
K. Keil
Vol. 22, No. 1, 1956, pp. 28 - 43

10.12 Artificial Clay (Künstlicher Ton)
K. Keil
Vol. 22, No. 1, 1956, pp. 44 - 48

10.13 Geophysics in Road Construction, Part Seven--Internal Friction (Bodenphysik im Fahrbahnbau, 7. Teil - Innere Reibung)
E. E. Hensolt
Vol. 22, No. 3, 1956, pp. 173 - 220

10.14 Geophysics in Road Construction, Part Eight--The Dynamic Evaluation of the Soil Mechanics Test (Bodenphysik im Fahrbahnbau, 8. Teil - Die dynamische Deutbarkeit des bodenmechanischen Versuches)
E. E. Hensolt
Vol. 23, No. 4, 1958, pp. 176 - 259
10.15 On the Stability of Clay slurries (Über die Stabilität von Tonschlammem)

Clay slurries are used for grouting purposes, as lubricants for caissons and similar works, and as drilling mud for rotary borings. The stability of the clay slurry suspension depends on the interparticle forces, which in turn depend on the electrolytical environment of the dispersing medium. A series of tests was performed to investigate the effect of different additives, their doses in respect to change in viscosity, and resulting increase in stability of different clay materials. Some test results are presented; however, no definite conclusions are given.

R. Jelinek and H. L. Jässberger Vol. 25, No. 1, 1959, pp. 68 - 82

10.16 Indication of Pending Failures in Gravel and Sand Pits (Anzeichen von Einsturzgefahren in Kies- und Sandgruben)

Failures of gravel or sand banks in quarries generally occur rapidly and without advance warning. In many cases scaling of slightly cemented sand layers was observed which might be interpreted as an indication of overstressing, and should be taken as a warning of an eminent failure.

F. Kahler Vol. 25, No. 4, 1960, pp. 256 - 258

10.17 Genetics of Sediments and Measuring of Grain Properties (Sedimentgenetik und Messung von Korneigenschaften)

If use is made of the different grain parameters found in the mineralogical particles of sediments, information is provided not only on genetic conditions, but also on the geological history before sedimentation. The maximum dimensions of the grains and "relative breadth" are determined by different methods described in the paper. Test data on sands and their evaluation in respect to their genesis are given. Particular features of the test results can be used for correlation of geological formations.

T. Hagerman Vol. 25, No. 4, 1960, pp. 259 - 267

10.18 The "Hydraton" Method (Das Hydratonverfahren)

The paper discusses the practical application of the "Hydraton" method invented by the author. Hydraton is a trade name
(in Germany) for in-situ clay treated with chemical additives (lime) for stabilizing purposes. Hydraton is mixed and installed similarly to concrete. Satisfying performances of past applications, particularly in construction of earth-fill dams, resulted in favorable code specifications. The permeability, potential alteration of the chemical additives, the resistance against chemical effects, surface erosion, possibility of cracking of Hydraton linings, thixotropy of Hydraton, and allowable gradient of flow within the material are discussed. A table presents complete design data for a channel lining composed of a Hydraton mixture.

K. Keil
Vol. 27, No. 2, 1961, pp. 54 - 72

10.19 Construction of Deep Foundation Excavation in Water-Bearing Soils for the Powerhouse of a Low Pressure Hydropower Plant at the Adige-River (Herstellung einer tiefen Baugrube im wasserführenden Lockergestein zur Errichtung des Krafthauses eines Niederdruckkraftwerkes an der Etsch)

The paper contains a brief account of the excavation for a hydropower plant in Northern Italy, in cohesionless gravel and sand with layers of loamy gravel 25,000 square feet (2300 m²) in area and 58 ft (17.5 m) deep. The maximum water head during excavation was 52 ft (15.5 m). From several alternates, the installation of a continuous diaphragm consisting of precast concrete elements 15 ft (4.5 m) long, with joints sealed with bentonite was selected. The concrete elements were installed as excavation proceeded. Quick conditions in local sand pockets necessitated installation of filter wells in the deep part of the excavation. The total influx into the completed excavation is on the order of 27 GPS (100 l/sec).

C. Veder
Vol. 27, No. 2, 1961, pp. 77 - 81

10.20 On the Cohesion of Sand, Accidents in Sand Pits and Their Prevention (Zur Kohäsion des Sandes, Unfälle und Unfallverhütung in Sandgruben)

The cohesion of undisturbed deposits of sands and the stability of steep slopes in sand pits are important with respect to accident prevention in quarry operations. Because soil mechanics is based on ideal conditions, its application does not always satisfy practical needs. Apparent cohesion of in-situ sands is observed in many cases; it is due to shape, surface, and gradation of grains, moisture conditions, and cementation.
Therefore, when stressed, sand deposits can react as quasi-solids with true compressive strength. Relaxation under stress results in distinct jointing, and thus sand "blocks," which might be the cause of accidents. Engineering geological investigation assists in improving safety conditions in sand pits. Comprehensive reference to international geological literature is made.

A. Kieslinger Vol. 28, No. 1, 1962, pp. 1 - 30
11.

**GEOPHYSICS**

11.01 Contributions on Geoelectrical Subsurface Investigations (Einiges über geoelektrische Baugrunduntersuchungen)

V. Fritsch
Vol. 17, No. 1, 1949, pp. 7 - 29

11.02 The Correlation of "Areal Plan" and Geoelectric in the Subsurface Diagram (Das Zusammenspiel von Arealplan und Geoelektrik im Untergrundmessbild)

E. E. Hensolt
Vol. 18, No. 4, 1951, pp. 207 - 227

11.03 Determination of Damages Caused by Impacts on Ground Surface and Structure (Die Bestimmung von Erschütterungsschäden infolge Stosswirkung auf Boden und Gebäude)

E. E. Hensolt
Vol. 19, No. 1, 1952, pp. 1 - 28

11.04 On Electrical Investigations of Borings (Über elektrische Bohrlochuntersuchungen)

H. Seelmeier


E. E. Hensolt
Vol. 21, No. 1/2, 1954, pp. 1 - 33
11.06 Geophysics in Road Construction--Part Five - Geophysical Consideration (Bodenphysik im Fahrbahnbau--5. Teil - Geophysikalische Behandlung)

11.07 Geophysics in Road Construction--Part Six - Geoelectric Plan (Bodenphysik im Fahrbahnbau--6. Teil - Geoelektrischer Plan)
E. E. Hensolt Vol. 22, No. 2, 1956, pp. 74 - 113

11.08 Influence of Radiation Energy on Properties of Rock (Einfluss der Strahlungsenergie auf die Gesteinseigenschaften)
The rheological properties of rocks are determined by their present and past environments. The effect of thermal energy is well proven. The influence of radioactivity is also a very important factor. The influence of gamma and neutron radiation is investigated in laboratory tests. After rock salt is exposed to radiation, which results in discoloring of the crystals as observed in nature, its strength decreases and its deformability increases by 250 per cent. The resistivity also decreases markedly. Similar but lesser effects are observed in carbon minerals. The effect of these changes of technical properties on the in-situ stress conditions might allow the determination of the state of stress by means of radiation measurements.
R. Kvapil Vol. 25, No. 2/3, 1960, pp. 142 - 147

11.09 The Physical Bases of the Freezing Method (Die physikalischen Grundlagen des Gefrierverfahrens)
The freezing method has been employed in shaft construction for the last 50 years. Better understanding and more economical methods now render the freezing method feasible for civil engineering projects. The physical bases of the method are reviewed; the conditions for static and flowing ground water are differentiated. Equations are given for the growth rate of frozen bodies, the influence of spacing of pipes, and for the temperature distribution in the direction of the cooling pipes. The equations provide the principal data for the design of a modern freezing system for underground excavations. The paper essentially represents a hydrodynamic and thermodynamic study. The investigations for flowing ground water conditions are not yet completed.
W. Ständer Vol. 27, No. 3/4, 1962, pp. 168 - 188
12.  MISCELLANEOUS TITLES

12.01 Annotations on Dirt Roads as Such and on Dirt Road Projects in Europe (Einige Bemerkungen über die Erdstrasse und zu Erdstrassenbauten im europäischen Raum)
L. Hauser Vol. 16, No. 1, 1946, pp. 46 - 48

12.02 The Tensile Strength of Roots (Die Zugfestigkeit von Pflanzenwurzeln)
J. Stini Vol. 16, No. 2, 1947, pp. 70 - 75

12.03 The Nature of Austrian Pozzolan and the Function of its Sulfur Trioxide in Mixtures of Pozzolan and Portland Cement (Die Natur des österreichischen Trass und die Funktion seines SO₃ in Trass-Portlandzementgemischen)

12.04 Principal Considerations on "Engineering Biology" (Grundsätzliches zur Ingenieurbiologie)
G. E. Kielhauser Vol. 20, No. 3, 1953, pp. 149 - 151

12.05 Culture, Protection of Nature, and Relation to Nature in Civil Engineering Construction (Kultur, Landschaftsschutz und Naturverbundenheit im Tiefbau)
V. Jurina Vol. 21, No. 1/2, 1954, pp. 34 - 43

12.06 Grading Equipment and Road Construction in Mountainous Areas (Räumgerate und Wegebau im Gebirge)
A. Hauser Vol. 21, No. 1/2, 1954, pp. 48 - 50

12.07 "Engineering Biology" and Building Construction (Ingenieurbiologie und Hochbau)
12.08 Damages of Buildings by Heat Originating in Manure Piles
(Bauwerksschäden durch Dungstätten als Wärmeherde)

E. Schenk

Vol. 23, No. 3, 1957, pp. 131 - 138
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