**AD NUMBER**

| AD411296 |

**LIMITATION CHANGES**

**TO:**
Approved for public release; distribution is unlimited.

**FROM:**
Distribution authorized to DoD only; Test and Evaluation; JUL 1963. Other requests shall be referred to Defense Atomic Support Agency, Washington, DC 20301.

**AUTHORITY**

dna ltr, 10 aug 1984
NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.
Operation
SUN BEAM
SHOT SMALL BOY

PROJECT OFFICERS REPORT—PROJECT 1.7

SHOCK SPECTRUM MEASUREMENTS (U)

F. A. Pieper, Project Officer

M. V. Barton
R. W. Sauer

Space Technology Laboratories, Inc.
One Space Park
Redondo Beach, California

Issuance Date: July 3, 1963
Inquiries relative to this report may be made to

Chief, Defense Atomic Support Agency
Washington 25, D. C.

When no longer required, this document may be destroyed in accordance with applicable security regulations.

DO NOT RETURN THIS DOCUMENT
OPERATION SUN BEAM
SHOT SMALL BOY

PROJECT OFFICERS REPORT — PROJECT 1.7

SHOCK SPECTRUM MEASUREMENTS

F. A. Pieper, Project Officer
M. V. Barton
R. W. Sauer

Space Technology Laboratories, Inc.
One Space Park
Redondo Beach, California

This document is the author(s) report to the Chief, Defense Atomic Support Agency, of the results of experimentation sponsored by that agency during nuclear weapons effects testing. The results and findings in this report are those of the author(s) and not necessarily those of the DOD. Accordingly, reference to this material must credit the author(s). This report is the property of the Department of Defense and, as such, may be reclassified or withdrawn from circulation as appropriate by the Defense Atomic Support Agency.

DEPARTMENT OF DEFENSE
WASHINGTON 25, D.C.
ABSTRACT

A total of 16 reed gages of a design which had previously been used in Operations Plumbob, Hardtack, Hardtack II, and Nougat were installed in the Small Boy Event. These gages recorded horizontal and vertical displacement shock spectra at four stations between 185 feet and 290 feet of ground zero. Some gages were placed at the surface and others at 10-foot depth. All gages yielded readable records and data is presented in both tabulated and chart form.

The gages 10 feet below the surface showed a marked attenuation at high frequencies but very little attenuation of horizontal shock at frequencies below 50 cycles per second and of vertical shock at frequencies below 25 cycles per second. A peak was noted in horizontal acceleration between 90 and 150 cycles per second at the surface and between 50 and 90 cycles at 10-foot depth. No similar peaks were noted in the vertical acceleration.

Examination of the data presented indicated that no simple scaling was possible for the ground shock which occurred. This data will have to be studied with other shock spectra data so that it may be properly weighed, and quantitative scaling rules derived.
## CONTENTS

**ABSTRACT** .......................... 5  

**INTRODUCTION** .......................... 9  
- Objective .................................. 9  
- Background ................................ 9  
- Theory .................................. 10  

**PROCEDURE** .......................... 12  
- Operations ................................ 12  
- Instrumentation .......................... 12  

**RESULTS** .......................... 13  

**DISCUSSION** ........................ 14  

**CONCLUSIONS** ......................... 15  

**REFERENCES** ......................... 38  

**TABLES** 
1. Location of Reed Gages ............... 17  
2. Frequency, Displacement Data ........ 18  

**FIGURES** 
1. Typical installation of a horizontal  
   reed gage in a protective canister  .... 20  
2. Typical installation of a vertical  
   reed gage in a protective canister  .... 20  
3. Vertical $\triangle$ and horizontal $\odot$ spectra at  
   185 feet, 10-foot depth of burial ........ 21  
4. Vertical $\triangle$ and horizontal $\odot$ spectra at  
   200 feet, 10-foot depth of burial ........ 22  
5. Vertical $\triangle$, horizontal $\odot$, and tangential $\square$  
   spectra at 200 feet, surface ............. 23  
6. Vertical $\triangle$ and horizontal $\odot$ spectra at  
   246 feet, 10-foot depth of burial ........ 24
7. Vertical $\Delta$, horizontal $O$, and tangential $\Box$ spectra at 246 feet, surface.  
8. Vertical $\Delta$ and horizontal $O$ spectra at 290 feet, 10-foot depth of burial.  
9. Vertical $\Delta$ and horizontal $O$ spectra at 290 feet, surface.  
10. Vertical acceleration versus frequency at the surface and 10-foot depth, 200-foot range.  
11. Vertical acceleration versus frequency at the surface and 10-foot depth, 246-foot range.  
12. Vertical acceleration versus frequency at the surface and 10-foot depth, 290-foot range.  
13. Horizontal acceleration versus frequency at the surface and 10-foot depth, 200-foot range.  
14. Horizontal acceleration versus frequency at the surface and 10-foot depth, 246-foot range.  
15. Horizontal acceleration versus frequency at the surface and 10-foot depth, 290-foot range.  
16. Vertical acceleration vs. frequency at 10-foot depth for ranges of 185, 200, 246, and 290 feet.  
17. Horizontal acceleration vs. frequency at 10-foot depth for ranges of 185, 200, 246, and 290 feet.  
18. Vertical acceleration versus frequency at the surface for ranges of 200, 246, and 290 feet.  
19. Horizontal acceleration versus frequency at the surface for ranges of 200, 246, and 290 feet.
SHOCK SPECTRUM MEASUREMENTS

INTRODUCTION

Objective. The objective of this project was to measure the displacement spectrum of the ground motion at ranges of 185, 200, 245, and 290 feet from ground zero, both at the surface and at a depth of 10 feet. The displacement spectrum is a plot of peak displacement versus frequency of a set of several linear fixed-frequency oscillators (of single-degree-of-freedom) resulting from the motion of the ground.

Background. The use of self-contained mechanical reed gages, capable of measuring the displacement shock spectrum in any one direction, provided an indication of the characteristics of blast-induced and ground-transmitted ground shock under conditions of low yield loading during Operation Plumbbob (Reference 1). Additional measurements, free field and in structures, were made for high and low yield loadings during Operation Hardtack at the Pacific Proving Grounds (Reference 2). Surface measurements of the shock spectrum generated by underground nuclear detonations were made during Operation Hardtack, Phase II, and Operation Nougat (Reference 3) at the Nevada Test Site.

Measurements of the surface ground-shock spectrum were obtained during the 20-ton trial at the Suffield Experimental Station (SES),
Ralston, Alberta, Canada, and both the surface and near-surface spectrum resulting from the 100-ton trial at SES in 1961 (Reference 4).

These data have been utilized in preparing the environmental information considered essential for the design of missile systems hard bases for the Air Force Ballistic Systems Division (AFBSD) and in theoretical studies of scaling effects.

**Theory.** Briefly, if a shock due to ground motions is applied to a linear structure attached to the ground, the displacement of any point of the structure relative to the ground can be expressed as a sum of principal mode responses:

$$u(t,x,y,z) = \sum q(t) \phi \ (x,y,z)$$  \hspace{1cm} (1)

where:

- $u(t,x,y,z)$ = displacement relative to ground
- $q(t)$ = generalized coordinate
- $\phi (x,y,z)$ = mode shape

An upper bound of response is obtained assuming all modes have reached their peak values at the same time.

$$u_{\text{max}} = \sum |q_{\text{max}}| \phi$$  \hspace{1cm} (2)

For an acceleration input it can be shown that for each mode:

$$\ddot{q} + 2\epsilon \omega \dot{q} + \omega^2 q = -\gamma a(t)$$  \hspace{1cm} (3)

where:

- $q$ = generalized displacement relative to ground
- $\omega$ = frequency of mode
\( \epsilon = \text{ratio of damping to critical viscous damping} \)
\( \gamma = \text{kinematic factor} = \int \rho \phi^2 \, dv / \int \rho \phi^2 \, dv \)
\( \rho = \text{mass per unit volume} \)
\( a(t) = \text{acceleration of ground as function of time} \)

The solution to Equation 3 for small damping is
\[
q_{\max}(\omega, \epsilon) = \max \left| \frac{1}{\omega} \int_0^t a(\tau) e^{-\epsilon \omega (t-\tau)} \sin \omega (t-\tau) \, d\tau \right| (4)
\]
Assuming an idealized single-degree-of-freedom system, such as a point mass on a weightless cantilever spring, the equation of motion for the mass is
\[
\ddot{q} + 2 \epsilon \omega \dot{q} + \omega^2 q = -a(t) \quad (5)
\]
The reed shock gages, with an appropriate gage factor to adjust for stylus position and for the fact that the sets of cantilevered mass systems have distributed mass, read directly the peak displacements as solutions of Equation 5. The frequency spectrum of the peak displacements of the masses relative to the base that is being accelerated is called the displacement shock spectrum, which is defined as
\[
D(\omega) = q_{\max} = \max_{t>0} \left| \frac{1}{\omega} \int_0^t a(\tau) e^{-\epsilon \omega (t-\tau)} \sin \omega (t-\tau) \, d\tau \right| (6)
\]
If the displacement spectrum \( D(\omega) \) is known, the modal response of any other structure having the same damping as the gage is given by
\[
q_{\max} = \gamma D \quad (7)
\]
or the upper bound of response by (from Equation 2)
\[
u_{\max} \leq \sum |\tau D \phi| \quad (8)
The velocity shock spectrum is defined as:

\[ V = \omega D \]  

(9)

This quantity has the dimensions of velocity, but is not the peak velocity of the mass relative to the base. The velocity shock spectrum is useful, however, in the determination of an upper bound of strain energy in the structures.

The acceleration shock spectrum is defined as

\[ A = \omega^2 D \]  

(10)

and can be shown to be the peak absolute acceleration of the mass for small damping, namely

\[ A = \max | \ddot{q} + a | \]  

(11)

PROCEDURE.

Operations. Project activities at the site consisted of placement of canisters, installation, and adjustment of gages and record plates, and subsequent postshot recovery.

Instrumentation. Gages used in this test were the Space Technology Laboratories' designed reed gages used to measure shock spectra in previous nuclear tests. The gages consisted of ten masses on cantilever springs or reeds, mounted on a rigid base. The masses and spring constants of the ten reeds were so designed that their natural frequencies covered the range between 3 and 300 cps. Nominal frequencies are 3, 10, 20, 40, 80, 120, 160, 200, 250, and 300 cps.

The masses, which move in one plane, have scribers in contact
with a polished metal record plate. A thin layer of lampblack is
deposited on the record plate prior to final installation by smoking it
with a candle. As the reeds vibrate after being subjected to a
shock, the maximum displacement of each mass is recorded on the
smoked plate by the scribers. These displacements are measured,
and equivalent values for the mass motion are plotted against the
natural frequencies of the reeds to obtain the shock spectrum curves
for the various installations.

Sixteen gages were installed for the event, as shown in
Table 1. Terminology adopted in Table 1 will be used consistently
in this report. Horizontal and vertical refers to gages whose
bases are horizontal and vertical, respectively, and measure
response in the vertical plane containing the burst point. Tangen-
tial refers to a gage whose base is horizontal and measures response
at right angles to this plane. Each gage was housed in a protective
canister. Several sandbags were placed on the lid of each canister,
buried flush with the earth's surface. Each 10-foot deep hole con-
taining gages and canisters was backfilled prior to the event.

(Since accelerations expected at the close-in stations might damage reeds
in the low-frequency range, a few of the 3- and 10-cycle reeds were removed
prior to gage installation.) These reeds are indicated in Table 2. Figure 1
shows a typical horizontal gage installation and Figure 2 a typical vertical
gage.

RESULTS

All of the gages placed in the Small Boy Event yielded
records. The maximum response of each reed corrected for scriber
location is given in Table 2. A few of the readings were questioned due to the fact that a scriber bent or skipped on the plate. With the exception of these readings, it is believed that the recorded values were within 20 percent of the true spectra values. For small displacements, the recorded values were accurate to within 0.002 inch.

The shock spectra for these gages are shown in Figures 3 through 9.

DISCUSSION

Two tangential reed gages were included in the Small Boy Event, since in some instances tangential gages in past events have shown responses as large or larger than horizontal gages at the same location. These gages (see Figures 5 and 7) yielded shock spectra somewhat lower than the horizontal gages at the same location. The shocks, however, were not small and were probably caused by a combination of two effects: (1) asymmetries in the expanding shock wave, and (2) reflections of shock from earth strata, faults or discontinuities.

The results are replotted in Figures 10 through 15 to show the effect of burial depth. As was expected, the attenuation at high frequencies was extremely marked, while 10 feet of cover demonstrated very little attenuation of horizontal shock at frequencies below 50 cycles per second and of vertical shock at frequencies below 25 cycles per second.
Data is replotted in Figures 16 through 19 to show the effect of range on accelerations at various frequencies. Figures 17 and 19 show a peak to be occurring in the horizontal acceleration between 90 and 150 cycles per second at the surface and between 50 and 90 cycles at a 10 foot depth. No similar peaks are noted in the vertical acceleration, Figures 16 and 18.

Examination of Figures 16 through 19 indicates that no simple scaling is possible for the ground shock which occurred. The data will have to be studied in the light of other shock spectra data in order that it may be properly weighed and quantitative scaling rules derived.

CONCLUSIONS

On the basis of results obtained on Project 1.7 of the Small Boy Event, the following conclusions can be drawn:

1. The objective of Project 1.7 was attained. All gages yielded valid readings, which resulted in the shock spectra of Figures 3 through 9.

2. Attenuation of air-induced ground shock with depth in soil was as expected. Large attenuations were experienced at high frequencies and little or none at very low frequencies at a 10-foot depth.

3. Transverse shocks of considerable magnitude (although less than horizontal) can occur in air-induced ground shock. These shocks were probably due to asymmetries
in the blast wave and more importantly, discontinuities in the soil.

4. Scaling laws for ground shock cannot be quantitatively deduced on the basis of the small amount of data obtained in this event. The data should be studied in the light of data from other tests in order to arrive at proper scaling relations.


<table>
<thead>
<tr>
<th>Range from Ground Zero</th>
<th>Gage Position</th>
<th>Depth</th>
</tr>
</thead>
<tbody>
<tr>
<td>135 feet</td>
<td>Vertical</td>
<td>10 feet</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>10 feet</td>
</tr>
<tr>
<td>200 feet</td>
<td>Vertical</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Tangential</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Vertical</td>
<td>10 feet</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>10 feet</td>
</tr>
<tr>
<td>245 feet</td>
<td>Vertical</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Tangential</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Vertical</td>
<td>10 feet</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>10 feet</td>
</tr>
<tr>
<td>290 feet</td>
<td>Vertical</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>Flush with surface</td>
</tr>
<tr>
<td></td>
<td>Vertical</td>
<td>10 feet</td>
</tr>
<tr>
<td></td>
<td>Horizontal</td>
<td>10 feet</td>
</tr>
</tbody>
</table>
### TABLE 2

**FREQUENCY, DISPLACEMENT DATA**

<table>
<thead>
<tr>
<th>Station 507.01, 185 Feet From SZ</th>
<th>Vertical 10 Foot Depth, Gage No. 17</th>
<th>F(cps)</th>
<th>D(inches)</th>
<th>Horizontal 10 Foot Depth, Gage No. 1</th>
<th>F(cps)</th>
<th>D(inches)</th>
</tr>
</thead>
<tbody>
<tr>
<td>3</td>
<td>Removed</td>
<td>3</td>
<td>Removed</td>
<td>3</td>
<td>Removed</td>
<td></td>
</tr>
<tr>
<td>10</td>
<td>Removed</td>
<td>10</td>
<td>Removed</td>
<td>10</td>
<td>Removed</td>
<td></td>
</tr>
<tr>
<td>23</td>
<td>1.23 (1)</td>
<td>23</td>
<td>0.234</td>
<td>23</td>
<td>0.234</td>
<td></td>
</tr>
<tr>
<td>51</td>
<td>0.310</td>
<td>48</td>
<td>0.067</td>
<td>48</td>
<td>0.067</td>
<td></td>
</tr>
<tr>
<td>83</td>
<td>0.074</td>
<td>90</td>
<td>0.047</td>
<td>90</td>
<td>0.047</td>
<td></td>
</tr>
<tr>
<td>138</td>
<td>0.043</td>
<td>138</td>
<td>0.013</td>
<td>138</td>
<td>0.013</td>
<td></td>
</tr>
<tr>
<td>181</td>
<td>0.020</td>
<td>177</td>
<td>0.007</td>
<td>177</td>
<td>0.007</td>
<td></td>
</tr>
<tr>
<td>220</td>
<td>0.005</td>
<td>215</td>
<td>0.005</td>
<td>215</td>
<td>0.005</td>
<td></td>
</tr>
<tr>
<td>260</td>
<td>-----</td>
<td>262</td>
<td>-----</td>
<td>262</td>
<td>-----</td>
<td></td>
</tr>
<tr>
<td>286</td>
<td>0.007</td>
<td>288</td>
<td>-----</td>
<td>288</td>
<td>-----</td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Station 507.02, 200 Feet From SZ</th>
<th>Vertical 10 Ft. Depth Gage No. 7</th>
<th>F(cps)</th>
<th>D(inches)</th>
<th>Horizontal 10 Ft. Depth Gage No. 20</th>
<th>F(cps)</th>
<th>D(inches)</th>
<th>Vertical Surface Gage No. 8</th>
<th>F(cps)</th>
<th>D(inches)</th>
<th>Horizontal Surface Gage No. 21</th>
<th>F(cps)</th>
<th>D(inches)</th>
<th>Tangential Surface Gage No. 5</th>
<th>F(cps)</th>
<th>D(inches)</th>
</tr>
</thead>
<tbody>
<tr>
<td>3</td>
<td>Removed</td>
<td>3</td>
<td>Removed</td>
<td>3</td>
<td>Removed</td>
<td></td>
<td>3</td>
<td>Removed</td>
<td></td>
<td>3</td>
<td>Removed</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>9.5</td>
<td>1.36</td>
<td>10.1</td>
<td>0.762</td>
<td>10</td>
<td>Removed</td>
<td></td>
<td>10</td>
<td>Removed</td>
<td></td>
<td>10</td>
<td>Removed</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>23</td>
<td>1.08 (1)</td>
<td>23</td>
<td>0.173</td>
<td>23</td>
<td>0.927 (1)</td>
<td>23</td>
<td>0.242 (3)</td>
<td>24</td>
<td>0.214 (2)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>43</td>
<td>0.364</td>
<td>49</td>
<td>0.112</td>
<td>49</td>
<td>0.690 (2)</td>
<td>49</td>
<td>0.22 (3)</td>
<td>50</td>
<td>0.134</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>90</td>
<td>0.094</td>
<td>90</td>
<td>0.029</td>
<td>91</td>
<td>0.543 (1)</td>
<td>90</td>
<td>0.450</td>
<td>90</td>
<td>0.133</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>138</td>
<td>0.132</td>
<td>138</td>
<td>0.008</td>
<td>137</td>
<td>0.354</td>
<td>136</td>
<td>0.043</td>
<td>138</td>
<td>0.034</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>182</td>
<td>-----</td>
<td>181</td>
<td>-----</td>
<td>178</td>
<td>0.267</td>
<td>182</td>
<td>0.020</td>
<td>180</td>
<td>0.007</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>216</td>
<td>-----</td>
<td>221</td>
<td>-----</td>
<td>221</td>
<td>0.137</td>
<td>220</td>
<td>0.017</td>
<td>221</td>
<td>0.009</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>262</td>
<td>-----</td>
<td>254</td>
<td>-----</td>
<td>254</td>
<td>0.116</td>
<td>256</td>
<td>0.014</td>
<td>262</td>
<td>0.005</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>281</td>
<td>-----</td>
<td>283</td>
<td>-----</td>
<td>283</td>
<td>0.098</td>
<td>288</td>
<td>0.020</td>
<td>288</td>
<td>0.003</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

(1) At end of recording range
(2) Scriber skipped
(3) Scriber failed
(4) Hit by another reed
(5) No record obtained
TABLE 2 (continued)

FREQUENCY, DISPLACEMENT DATA

<table>
<thead>
<tr>
<th>Station 507.03, 246 Feet From SZ</th>
</tr>
</thead>
<tbody>
<tr>
<td>Vertical 10 Ft. Depth</td>
</tr>
<tr>
<td>Gage No. 4</td>
</tr>
<tr>
<td>2.6</td>
</tr>
<tr>
<td>9.9</td>
</tr>
<tr>
<td>23</td>
</tr>
<tr>
<td>51</td>
</tr>
<tr>
<td>91</td>
</tr>
<tr>
<td>138</td>
</tr>
<tr>
<td>181</td>
</tr>
<tr>
<td>221</td>
</tr>
<tr>
<td>262</td>
</tr>
<tr>
<td>288</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Station 507.04, 290 Feet From SZ</th>
</tr>
</thead>
<tbody>
<tr>
<td>Vertical 10 Ft. Depth</td>
</tr>
<tr>
<td>Gage No. 14</td>
</tr>
<tr>
<td>3.1</td>
</tr>
<tr>
<td>9.4</td>
</tr>
<tr>
<td>23</td>
</tr>
<tr>
<td>49</td>
</tr>
<tr>
<td>88</td>
</tr>
<tr>
<td>137</td>
</tr>
<tr>
<td>181</td>
</tr>
<tr>
<td>214</td>
</tr>
<tr>
<td>250</td>
</tr>
<tr>
<td>288</td>
</tr>
</tbody>
</table>

(1) At end of recording range
(2) Scriber skipped
(3) Scriber failed
(4) Hit by another reed
(5) No record obtained
Figure 1 Typical installation of a horizontal reed gage in a protective canister. (STL 71869-61)

Figure 2 Typical installation of a vertical reed gage in a protective canister. (STL 71870-61)
Figure 4: Vertical $\triangle$ and horizontal $\circ$ spectra at 300 feet, 10-foot depth of burial.
Figure 8 shows the spectral analysis of the test data, specifically focusing on the relationship between frequency and displacement. The diagram illustrates how different frequencies affect the displacement of the system. The horizontal axis represents frequency (cycles per sec), and the vertical axis represents displacement (in. per sec). The test was conducted with a 10-foot depth of burial.
Figure 10 Vertical acceleration versus frequency at the surface and 10-foot depth, 200-foot range.
Figure 12: Vertical acceleration versus frequency at the surface and 10-foot depth, 290-foot range.
Figure 13 Horizontal acceleration versus frequency at the surface and 10-foot depth, 200-foot range.
Figure 15 Horizontal acceleration versus frequency at the surface and 10-foot depth, 290-foot range.
Figure 16: Vertical acceleration versus frequency at 10-foot depth for ranges of 185, 200, 246, and 290 feet.
Figure 17  Horizontal acceleration versus frequency at 10-foot depth for ranges of 185, 200, 246, and 290 feet.
Figure 18  Vertical acceleration versus frequency at the surface for ranges of 200, 246, and 290 feet.
Figure 19 Horizontal acceleration versus frequency at the surface for ranges of 200, 246, and 290 feet.
REFERENCES

1. J.F. Halsey and M.V. Barton; "Spectra of Ground Shock Produced by Nuclear Detonations"; Operation Plumbbob, Project 1.9, WT-1487; Air Force Ballistic Missile Division, Air Research and Development Command, Inglewood, California; Unclassified.

2. J.F. Halsey and others; "Ground Shock Spectra from Surface Bursts"; Project 1.12, Operation Hardtack, WT-1617, Space Technology Laboratories, Inc., Los Angeles, California; Secret Formerly Restricted Data.

